

Section 114 Information Collection Request Emissions Test Report

GCC Rio Grande Inc.
Pueblo Plant
EPA Registry ID: 110037262636
3372 Lime Road
Pueblo, CO 81004
Report No. M234207A





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Emissions Test Report**

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**Report Submittal Date:
December 19, 2023**

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Report No. M234207A

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1.0 INTRODUCTION

Mostardi Platt conducted an air emissions test program for GCC Rio Grande Inc. at the Pueblo Plant located in Pueblo, Colorado. All testing was performed as described in the *Code of Federal Regulations*, Title 40, Part 60, Appendix A (40CFR60), Methods 1, 2, 3A, 4, 26A, and 40CFR63, Appendix A, (40CFR63) Method 320.

This test program was completed to satisfy the requirements of the United States Environmental Protection Agency (USEPA) Section 114 Information Collection Request for Portland Cement Manufacturing facilities.

The identification of individuals associated with the test program is summarized below:

| Location | Address | Contact |
|--------------------------------|---|--|
| Facility Representative | GCC Rio Grande, Inc. 3372 Lime Road Pueblo, CO 81004 | Amy Veek (719) 647-6861 aveek@gcc.com |
| Testing Company Representative | Mostardi Platt 7715 Commercial Way Suite 155 Henderson, NV 89011 | Rich Sollars P: (630) 993-2100 (phone) E: rsollars@mp-mail.com |

2.0 TEST REQUIREMENTS

Testing was performed at the kiln stack. The following table presents a list of the parameters tested, the applicable methodologies utilized, and average test results:

| Source | Parameter Tested | Test Results | Method/Regulation Citation |
|---|--|---|--|
| Kiln Stack Mill On | Hydrogen Fluoride (HF) | ≤ 0.10 ppmvw | USEPA Method 320, 40CFR63, Appendix A |
| | | ≤ 0.14 ppmvd @7% O ₂ | |
| | | ≤ 0.05 lb/hr | |
| | | ≤ 0.0005 lb/ton clinker | |
| | HF ¹ | ≤ 0.14 ppmvd | Method 26A, 40CFR60, Appendix A |
| | | ≤ 0.17 ppmvd @7% O ₂ | |
| | | ≤ 0.06 lb/hr | |
| | | ≤ 0.0006 lb/ton clinker | |
| | Chlorine (Cl ₂) ¹ | ≤ 0.04 ppmvd | USEPA Method 26A, 40CFR60, Appendix A |
| | | ≤ 0.05 ppmvd @7% O ₂ | |
| | | ≤ 0.07 lb/hr | |
| | | ≤ 0.0006 lb/ton clinker | |
| | Hydrogen Cyanide (HCN) | 8.40 ppmvw | USEPA Method 320, 40CFR63, Appendix A |
| | | 11.77 ppmvd @7% O ₂ | |
| 6.02 lb/hr | | | |
| 0.0521 lb/ton clinker | | | |
| Oxygen (O ₂) | 9.4 % (dry) | USEPA Method 3A, 40CFR60, Appendix A | |
| Carbon Dioxide (CO ₂) | 20.0 % (dry) | USEPA Method 320, 40CFR63, Appendix A | |
| Moisture (H ₂ O) | 13.4 % | USEPA Method 320, 40CFR63, Appendix A | |
| Cyclonic Flow Determination | PASS | USEPA Method 1, 40CFR60, Appendix A, Section 11.4 | |
| Three-point O ₂ Stratification Determination | < 5 % | USEPA Method 3A, 40CFR60, Appendix A and Method 7E, Section 8.1.2 | |

¹ HF and Cl₂ Method 26A results are reported as the average from Train A and Train B.

| Source | Parameter Tested | Test Results | Method/Regulation Citation |
|---|--|---|--|
| Kiln Stack Mill Off | Hydrogen Fluoride (HF) | ≤ 0.10 ppmvw | USEPA Method 320, 40CFR63, Appendix A |
| | | ≤ 0.10 ppmvd @7% O ₂ | |
| | | ≤ 0.04 lb/hr | |
| | | ≤ 0.0003 lb/ton clinker | |
| | HF ² | ≤ 0.19 ppmvd | Method 26A, 40CFR60, Appendix A |
| | | ≤ 0.16 ppmvd @7% O ₂ | |
| | | ≤ 0.06 lb/hr | |
| | | ≤ 0.0005 lb/ton clinker | |
| | Chlorine (Cl ₂) ² | ≤ 0.05 ppmvd | USEPA Method 26A, 40CFR60, Appendix A |
| | | ≤ 0.04 ppmvd @7% O ₂ | |
| | | ≤ 0.06 lb/hr | |
| | | ≤ 0.0005 lb/ton clinker | |
| | Hydrogen Cyanide (HCN) | 13.02 ppmvw | USEPA Method 320, 40CFR63, Appendix A |
| | | 12.64 ppmvd @7% O ₂ | |
| 6.39 lb/hr | | | |
| 0.0534 lb/ton clinker | | | |
| Oxygen (O ₂) | 4.6 % (dry) | USEPA Method 3A, 40CFR60, Appendix A | |
| Carbon Dioxide (CO ₂) | 28.9 % (dry) | USEPA Method 320, 40CFR63, Appendix A | |
| Moisture (H ₂ O) | 12.4 % | USEPA Method 320, 40CFR63, Appendix A | |
| Cyclonic Flow Determination | PASS | USEPA Method 1, 40CFR60, Appendix A, Section 11.4 | |
| Three-point O ₂ Stratification Determination | < 5 % | USEPA Method 3A, 40CFR60, Appendix A and Method 7E, Section 8.1.2 | |

² HF and Cl₂ Method 26A results are reported as the average from Train A and Train B.

3.0 QA SPECIFICATIONS AND PROCESS DIAGRAM

Table 3-1 QA/QC Specifications

| Parameter | Method | QA/QC Specification | Acceptance Criteria | Actual Result |
|-----------------|---|------------------------|---|-----------------------------|
| HCN | 320 | Method Detection Limit | 0.5 ppm | 0.4 ppmvw |
| | | SNR | >2500 at 64 scans | 4826 (Run 1 Average) |
| | | S Beam | >0.9 | 1.320 (Run 1 Average) |
| | | Direct HCN Analysis | ±5% of tag value | -2.5% |
| | | Dynamic Spike Analysis | ≤10% of total sample volume | 4.5% |
| | | | Spike gas ~twice native concentration or 3-4 ppm addition to native concentration | ~twice native concentration |
| | | | ≤±20% of expected value or ≤±0.5 ppm, whichever is less restrictive | +1.0 % |
| Residuals | ≤±0.3 ppm, or ≤±5% of measured value, whichever is less restrictive | 0.2 ppmvw | | |
| Cl ₂ | 26A | Detection Limit | 300 µg | 150 µg |
| | | Paired Train Agreement | ≤10% Relative Deviation or ≤0.2 ppm, whichever is less restrictive. | 0.01 ppmvd |

4.0 TEST PROCEDURES

All testing, sampling, analytical, and calibration procedures used for this test program were performed as described in the Title 40, *Code of Federal Regulations*, Part 60, Appendix A (40CFR60), Methods 1, 2, 3A, 4, 26A, and 40CFR63, Appendix A, Method 320; and the latest revisions thereof. Where applicable, the *Quality Assurance Handbook for Air Pollution Measurement Systems*, Volume III, Stationary Source Specific Methods, United States Environmental Protection Agency (USEPA) 600/R-94/038c, September 1994 was used to supplement procedures in addition to the appended "Draft General Test Plan".

4.1 Method 1 Sample and Velocity Traverse Determination

Sample points for testing are determined using USEPA Test Method 1, 40CFR60, Appendix A. The characteristics of the measurement location is summarized below.

Sample Point Selection

| Test Location | Stack Diameter | Port Length | Upstream Diameters | Downstream Diameters | Test Parameter | Number of Sampling Points |
|---------------|----------------|-------------|--------------------|----------------------|---------------------------------|---------------------------|
| Main Kiln | 10.25 Feet | 9.5 Inches | 4.9 Diameters | 24.4 Diameters | HF/Cl ₂ (26A) | 12 |
| | | | | | O ₂ (3A) | 3 (stratification) |
| | | | | | HCN/HF/CO ₂ (320/3A) | 1 |

A cyclonic flow check was performed in accordance with Section 11.4, which demonstrated it meets the criteria of an average value of less than 20° and therefore is considered to be a suitable testing location for flow rate measurements.

4.2 Method 2 Volumetric Flow Rate Determination

The gas velocity and volumetric flowrate were determined using Method 2, 40CFR60, Appendix A, as an integrated part of the HF/Cl₂ sampling system.

Velocity pressures were determined by traversing the duct with wind tunnel calibrated S-type pitot tube. Temperatures were measured using K-type thermocouples with calibrated digital temperature indicators. The molecular weight and moisture content of the gases were also determined to permit the calculation of the volumetric flowrate.

4.3 Method 3A Oxygen (O₂) and Carbon Dioxide (CO₂) Determination

O₂ and CO₂ concentrations were determined in accordance with Method 3A, 40CFR60, Appendix A and Method 320, 40CFR63, Appendix A, respectively. A Servomex analyzer was used to determine O₂ concentrations while the MKS 2030 analyzer was used to determine CO₂ concentrations. The O₂ instrument has a paramagnetic detector and operates in a nominal range of 0-25%.

A list of calibration gases used and the results of all calibration and other required quality assurance checks are found in the appendix of this report. Copies of calibration gas certifications are also appended.

4.4 Method 26A Hydrogen Fluoride (HF) and Chlorine (Cl₂) Determination

HF and Cl₂ concentrations and emission rates were determined in accordance with Method 26A, 40CFR60, Appendix A. Paired sampling trains were used to collect the samples. A total of twelve (12) test points were sampled per run on the kiln stack. The sample was extracted isokinetically from the gas stream and passed through dilute sulfuric acid (0.1N H₂SO₄). HF was collected in the dilute acid. Cl₂ was collected in the dilute sodium hydroxide (0.1N NaOH) solution. The sample train consisted of a Teflon coated nozzle, a heated borosilicate glass probe liner, a Teflon® filter placed on the outlet of the glass probe liner, and six impingers. The first two impingers contained the 0.1N H₂SO₄, the third remained empty (and was recovered with the first two impingers), the fourth and fifth impingers contained the 0.1N NaOH, while the sixth impinger contained silica gel to absorb any remaining moisture. A de-ionized water rinse was performed on each set of impingers, and samples were stored in Nalgene sample containers for transport. The 0.1N H₂SO₄ impinger catch samples were analyzed for HF while the 0.1N NaOH impinger catch samples were analyzed for Cl₂. A method detection limit (MDL) of 150 µg was determined for both HF and Cl₂ using the "Definition and Procedure for the Determination of the Method Detection Limit, Revision 2". All equipment used was calibrated in accordance with the specifications of the method. Calibration data is appended.

Hand recorded field data sheets were reviewed and scans are retained on the Mostardi Platt network. Copies of this data is available upon request.

4.5 Method 320 Speciated Flue Gas Concentration Determinations

The sampling procedures for HCN and HF were performed in accordance with USEPA Method 320, 40CFR63, Appendix A. Data was continuously recorded with a data logging system throughout sampling, with brief interruption to properly label reference spectra.

The average gas effluent concentrations were determined from the average gas concentration displayed by the MKS 2030 analyzer.

All sampling system components were heated to 375°F +/- 25°F, including: stainless steel sample probe, stainless steel calibration tee, in line glass fiber particulate filter, Teflon® sample line, heated head sample pump, and FTIR detector cell. The sample pump distributes the gas sample to the instrument at a steady sample flow rate (+/- 10%). All components of the sampling system are constructed of stainless steel, glass, or Teflon®.

FTIR technology works on the principle that most gases absorb infrared light. This is true for all compounds except for homonuclear diatomic molecules and noble gases such as: N₂, O₂, H₂, He, Ne, and Ar. Vibrations, stretches, bends, and rotations within the bonds of a molecule determine the infrared absorption distinctiveness. The absorption creates a "fingerprint" which is unique for each given compound. The quantity of infrared light absorbed is proportional to the gas concentration. Most compounds have absorbencies at different infrared frequencies, thus allowing the simultaneous analysis of multiple compounds at one time. The FTIR software compares each sample spectrum to a user-selected list of calibration references and concentration data is generated.

FTIR data was collected using an MKS MultiGas 2030 FTIR spectrometer. Data was generated at 0.5 cm⁻¹. Each Spectra was derived from the coaddition of 62-64 scans with a new data point generated approximately every minute. HCN analyte spiking assured the ability of the FTIR to quantify HCN in the presence of effluent gas. All analyte spikes were introduced using an instrument grade stainless steel rotameter. All QA/QC procedures were within the acceptance criteria allowance of the applicable methodology and the "General Test Plan."

5.0 TEST RESULTS SUMMARIES

Client: GCC Rio Grande, Inc.
Facility: Pueblo Plant
Test Location: Main Kiln Stack
Test Method: 26A

| Source Condition Date | Mill On 10/18/23 | Mill On 10/18/23 | Mill On 10/18/23 | |
|---|---------------------|---------------------|---------------------|----------|
| Start Time | 8:40 | 9:40 | 12:25 | |
| End Time | 9:46 | 12:02 | 13:31 | |
| | Run 1 | Run 2 | Run 3 | Average |
| Stack Conditions | | | | |
| Average Gas Velocity, ft/sec | 52.564 | 51.821 | 51.923 | 52.103 |
| Gas Volumetric Flow Rate, acfm | 260,243 | 256,563 | 257,069 | 257,958 |
| Gas Volumetric Flow Rate, dscfm | 146,674 | 151,130 | 144,575 | 147,460 |
| Gas Volumetric Flow Rate, scfm | 170,216 | 169,789 | 168,268 | 169,424 |
| Average %CO ₂ by volume, dry basis | 19.4 | 19.9 | 20.6 | 20.0 |
| Average %O ₂ by volume, dry basis | 9.7 | 9.5 | 9.1 | 9.4 |
| Clinker Production, ton/hr | 112.6 | 114.3 | 119.7 | 115.5 |
| Chloride (Cl₂) Emissions | | | | |
| ppm ≤ | 0.04 | ≤ 0.04 | ≤ 0.04 | ≤ 0.04 |
| ppm@7%O ₂ ≤ | 0.05 | ≤ 0.05 | ≤ 0.05 | ≤ 0.05 |
| lb/hr ≤ | 0.06 | ≤ 0.07 | ≤ 0.06 | ≤ 0.07 |
| lb/ton ≤ | 0.0006 | ≤ 0.0006 | ≤ 0.0005 | ≤ 0.0006 |
| Hydrogen Fluoride (HF) Emissions | | | | |
| ppm ≤ | 0.14 | ≤ 0.14 | ≤ 0.14 | ≤ 0.14 |
| ppm@7%O ₂ ≤ | 0.17 | ≤ 0.17 | ≤ 0.16 | ≤ 0.17 |
| lb/hr ≤ | 0.06 | ≤ 0.07 | ≤ 0.06 | ≤ 0.06 |
| lb/ton ≤ | 0.0006 | ≤ 0.0006 | ≤ 0.0005 | ≤ 0.0006 |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Test Method: 26A

| Source Condition | Mill On | Mill On | Mill On | |
|---|----------|----------|----------|----------|
| Date | 10/18/23 | 10/18/23 | 10/18/23 | |
| Start Time | 8:40 | 9:40 | 12:25 | |
| End Time | 9:46 | 12:02 | 13:31 | |
| | Run 1A | Run 2A | Run 3A | Average |
| Stack Conditions | | | | |
| Average Gas Temperature, °F | 215.3 | 206.8 | 214.3 | 212.1 |
| Flue Gas Moisture, percent by volume | 14.1% | 12.9% | 14.1% | 13.7% |
| Average Flue Pressure, in. Hg | 24.94 | 24.94 | 24.94 | 24.94 |
| Gas Sample Volume, dscf | 46.481 | 47.302 | 45.248 | 46.344 |
| Average Gas Velocity, ft/sec | 53.009 | 53.197 | 53.178 | 53.128 |
| Gas Volumetric Flow Rate, acfm | 262,445 | 263,375 | 263,281 | 263,034 |
| Gas Volumetric Flow Rate, dscfm | 146,915 | 151,414 | 147,497 | 148,609 |
| Gas Volumetric Flow Rate, scfm | 171,002 | 173,818 | 171,802 | 172,207 |
| Average %CO ₂ by volume, dry basis | 19.4 | 19.9 | 20.6 | 20.0 |
| Average %O ₂ by volume, dry basis | 9.7 | 9.5 | 9.1 | 9.4 |
| Isokinetic Variance | 101.1 | 99.8 | 98.0 | 99.6 |
| Chloride (Cl₂) Emissions | | | | |
| ug of sample collected | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 |
| ppm | ≤ 0.04 | ≤ 0.04 | ≤ 0.04 | ≤ 0.04 |
| Hydrogen Fluoride (HF) Emissions | | | | |
| ug of sample collected | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 |
| ppm | ≤ 0.14 | ≤ 0.14 | ≤ 0.14 | ≤ 0.14 |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Test Method: 26A

| Source Condition | Mill On | Mill On | Mill On | |
|---|----------|----------|----------|----------|
| Date | 10/18/23 | 10/18/23 | 10/18/23 | |
| Start Time | 8:40 | 10:10 | 12:25 | |
| End Time | 9:46 | 12:02 | 13:31 | |
| | Run 1B | Run 2B | Run 3B | Average |
| Stack Conditions | | | | |
| Average Gas Temperature, °F | 210.2 | 203.0 | 210.1 | 207.8 |
| Flue Gas Moisture, percent by volume | 13.6% | 9.0% | 14.0% | 12.2% |
| Average Flue Pressure, in. Hg | 24.94 | 24.94 | 24.94 | 24.94 |
| Gas Sample Volume, dscf | 47.238 | 46.403 | 46.482 | 46.708 |
| Average Gas Velocity, ft/sec | 52.119 | 50.445 | 50.668 | 51.077 |
| Gas Volumetric Flow Rate, acfm | 258,040 | 249,751 | 250,857 | 252,883 |
| Gas Volumetric Flow Rate, dscfm | 146,433 | 150,846 | 141,652 | 146,310 |
| Gas Volumetric Flow Rate, scfm | 169,429 | 165,759 | 164,733 | 166,640 |
| Average %CO ₂ by volume, dry basis | 19.4 | 19.9 | 20.6 | 20.0 |
| Average %O ₂ by volume, dry basis | 9.7 | 9.5 | 9.1 | 9.4 |
| Isokinetic Variance | 102.3 | 97.6 | 104.1 | 101.3 |
| Chloride (Cl₂) Emissions | | | | |
| ug of sample collected | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 |
| ppm | ≤ 0.04 | ≤ 0.04 | ≤ 0.04 | ≤ 0.04 |
| Hydrogen Fluoride (HF) Emissions | | | | |
| ug of sample collected | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 |
| ppm | ≤ 0.14 | ≤ 0.14 | ≤ 0.14 | ≤ 0.14 |

GCC Rio Grande, Inc.
Pueblo Plant
Main Kiln
Reference Method Test Data
Mill On

| Test No. | Date | Start Time | End Time | O2 % (dry) | Moisture % | HCN ppmvw | HCN ppmvd @ 7% O2 | HF ppmvw | HF ppmvd @ 7% O2 |
|----------------|------------|------------|----------|------------|--------------|-------------|-------------------|-------------|------------------|
| 1 | 10/18/2023 | 8:40 | 9:39 | 9.7 | 13.6% | 8.14 | 11.69 | 0.10 | 0.14 |
| 2 | 10/18/2023 | 10:10 | 11:09 | 9.5 | 13.0% | 8.59 | 12.06 | 0.10 | 0.14 |
| 3 | 10/18/2023 | 12:25 | 13:24 | 9.1 | 13.7% | 8.46 | 11.57 | 0.10 | 0.14 |
| Average | | | | 9.4 | 13.4% | 8.40 | 11.77 | 0.10 | 0.14 |

| Test No. | Date | Start Time | End Time | Volumetric Flow, DSCFM | Clinker Production, ton/hr | HCN lb/hr | HCN lb/ton | HF lb/hr | HF lb/ton |
|----------------|------------|------------|----------|------------------------|----------------------------|-------------|---------------|-------------|---------------|
| 1 | 10/18/2023 | 8:40 | 9:39 | 146,674 | 112.6 | 5.81 | 0.0516 | 0.05 | 0.0005 |
| 2 | 10/18/2023 | 10:10 | 11:09 | 151,130 | 114.3 | 6.28 | 0.0549 | 0.05 | 0.0005 |
| 3 | 10/18/2023 | 12:25 | 13:24 | 144,575 | 119.7 | 5.97 | 0.0498 | 0.05 | 0.0004 |
| Average | | | | 147,460 | 115.5 | 6.02 | 0.0521 | 0.05 | 0.0005 |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Test Method: 26A

| Source Condition | Mill Off | Mill Off | Mill Off | |
|---|----------|----------|----------|----------|
| Date | 10/17/23 | 10/17/23 | 10/17/23 | |
| Start Time | 8:00 | 13:40 | 15:05 | |
| End Time | 9:09 | 14:46 | 16:14 | |
| | Run 1 | Run 2 | Run 3 | Average |
| Stack Conditions | | | | |
| Average Gas Velocity, ft/sec | 43.299 | 45.276 | 44.940 | 44.505 |
| Gas Volumetric Flow Rate, acfm | 214,367 | 224,159 | 222,495 | 220,340 |
| Gas Volumetric Flow Rate, dscfm | 101,191 | 103,004 | 102,211 | 102,135 |
| Gas Volumetric Flow Rate, scfm | 114,976 | 119,177 | 116,973 | 117,042 |
| Average %CO ₂ by volume, dry basis | 29.1 | 27.9 | 29.8 | 28.9 |
| Average %O ₂ by volume, dry basis | 4.2 | 5.2 | 4.2 | 4.5 |
| Clinker Production, ton/hr | 119.5 | 119.6 | 119.7 | 119.6 |
| Chloride (Cl₂) Emissions | | | | |
| ppm ≤ | 0.05 | ≤ 0.05 | ≤ 0.05 | ≤ 0.05 |
| ppm@7%O ₂ ≤ | 0.04 | ≤ 0.04 | ≤ 0.04 | ≤ 0.04 |
| lb/hr ≤ | 0.06 | ≤ 0.06 | ≤ 0.06 | ≤ 0.06 |
| lb/ton ≤ | 0.0005 | ≤ 0.0005 | ≤ 0.0005 | ≤ 0.0005 |
| Hydrogen Fluoride (HF) Emissions | | | | |
| ppm ≤ | 0.19 | ≤ 0.19 | ≤ 0.19 | ≤ 0.19 |
| ppm@7%O ₂ ≤ | 0.16 | ≤ 0.17 | ≤ 0.16 | ≤ 0.16 |
| lb/hr ≤ | 0.06 | ≤ 0.06 | ≤ 0.06 | ≤ 0.06 |
| lb/ton ≤ | 0.0005 | ≤ 0.0005 | ≤ 0.0005 | ≤ 0.0005 |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Test Method: 26A

| | Source Condition Date | Mill Off 10/17/23 | Mill Off 10/17/23 | Mill Off 10/17/23 | | | | |
|---|--------------------------|----------------------|----------------------|----------------------|---------|--------|---|--------|
| | Start Time | 8:00 | 13:40 | 15:05 | | | | |
| | End Time | 9:09 | 14:46 | 16:14 | | | | |
| | | Run 1A | Run 2A | Run 3A | Average | | | |
| Stack Conditions | | | | | | | | |
| Average Gas Temperature, °F | | 356.4 | 364.0 | 369.8 | 363.4 | | | |
| Flue Gas Moisture, percent by volume | | 12.4% | 12.8% | 12.7% | 12.6% | | | |
| Average Flue Pressure, in. Hg | | 24.76 | 24.76 | 24.76 | 24.76 | | | |
| Gas Sample Volume, dscf | | 34.855 | 32.877 | 33.567 | 33.766 | | | |
| Average Gas Velocity, ft/sec | | 44.684 | 45.051 | 44.674 | 44.803 | | | |
| Gas Volumetric Flow Rate, acfm | | 221,226 | 223,044 | 221,180 | 221,817 | | | |
| Gas Volumetric Flow Rate, dscfm | | 103,676 | 103,155 | 101,677 | 102,836 | | | |
| Gas Volumetric Flow Rate, scfm | | 118,414 | 118,288 | 116,487 | 117,730 | | | |
| Average %CO ₂ by volume, dry basis | | 29.1 | 27.9 | 29.8 | 28.9 | | | |
| Average %O ₂ by volume, dry basis | | 4.2 | 5.2 | 4.2 | 4.5 | | | |
| Isokinetic Variance | | 107.4 | 101.8 | 105.5 | 104.9 | | | |
| Chloride (Cl₂) Emissions | | | | | | | | |
| ug of sample collected | ≤ | 150.00 | ≤ | 150.00 | ≤ | 150.00 | ≤ | 150.00 |
| ppm | ≤ | 0.05 | ≤ | 0.06 | ≤ | 0.05 | ≤ | 0.05 |
| Hydrogen Fluoride (HF) Emissions | | | | | | | | |
| ug of sample collected | ≤ | 150.00 | ≤ | 150.00 | ≤ | 150.00 | ≤ | 150.00 |
| ppm | ≤ | 0.18 | ≤ | 0.19 | ≤ | 0.19 | ≤ | 0.19 |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Test Method: 26A

| | Source Condition | Mill Off | Mill Off | Mill Off | | | | |
|---|------------------|----------|----------|----------|---------|--------|---|--------|
| | Date | 10/17/23 | 10/17/23 | 10/17/23 | | | | |
| | Start Time | 8:00 | 13:40 | 15:05 | | | | |
| | End Time | 9:09 | 14:46 | 16:14 | | | | |
| | | Run 1B | Run 2B | Run 3B | Average | | | |
| Stack Conditions | | | | | | | | |
| Average Gas Temperature, °F | | 353.0 | 359.9 | 372.7 | 361.9 | | | |
| Flue Gas Moisture, percent by volume | | 11.5% | 14.3% | 12.5% | 12.8% | | | |
| Average Flue Pressure, in. Hg | | 24.76 | 24.76 | 24.76 | 24.76 | | | |
| Gas Sample Volume, dscf | | 33.079 | 34.929 | 34.830 | 34.279 | | | |
| Average Gas Velocity, ft/sec | | 41.913 | 45.501 | 45.205 | 44.206 | | | |
| Gas Volumetric Flow Rate, acfm | | 207,507 | 225,273 | 223,809 | 218,863 | | | |
| Gas Volumetric Flow Rate, dscfm | | 98,706 | 102,853 | 102,745 | 101,435 | | | |
| Gas Volumetric Flow Rate, scfm | | 111,538 | 120,065 | 117,459 | 116,354 | | | |
| Average %CO ₂ by volume, dry basis | | 29.1 | 27.9 | 29.8 | 28.9 | | | |
| Average %O ₂ by volume, dry basis | | 4.2 | 5.2 | 4.2 | 4.5 | | | |
| Isokinetic Variance | | 106.3 | 107.7 | 107.6 | 107.2 | | | |
| Chloride (Cl₂) Emissions | | | | | | | | |
| ug of sample collected | ≤ | 150.00 | ≤ | 150.00 | ≤ | 150.00 | ≤ | 150.00 |
| ppm | ≤ | 0.05 | ≤ | 0.05 | ≤ | 0.05 | ≤ | 0.05 |
| Hydrogen Fluoride (HF) Emissions | | | | | | | | |
| ug of sample collected | ≤ | 150.00 | ≤ | 150.00 | ≤ | 150.00 | ≤ | 150.00 |
| ppm | ≤ | 0.19 | ≤ | 0.18 | ≤ | 0.18 | ≤ | 0.19 |

GCC Rio Grande, Inc.
Pueblo Plant
Main Kiln
Reference Method Test Data
Mill Off

| Test No. | Date | Start Time | End Time | O2 % (dry) | Moisture % | HCN ppmvw | HCN ppmvd @ 7% O2 | HF ppmvw | HF ppmvd @ 7% O2 |
|----------------|------------|------------|----------|------------|--------------|--------------|-------------------|-------------|------------------|
| 1 | 10/17/2023 | 8:00 | 8:59 | 4.2 | 12.4% | 13.04 | 12.41 | 0.10 | 0.10 |
| 2 | 10/17/2023 | 13:40 | 14:39 | 5.2 | 12.5% | 11.78 | 11.95 | 0.10 | 0.10 |
| 3 | 10/17/2023 | 15:05 | 16:04 | 4.2 | 12.4% | 14.24 | 13.56 | 0.10 | 0.10 |
| Average | | | | 4.6 | 12.4% | 13.02 | 12.64 | 0.10 | 0.10 |

| Test No. | Date | Start Time | End Time | Volumetric Flow, DSCFM | Clinker Production, ton/hr | HCN lb/hr | HCN lb/ton | HF lb/hr | HF lb/ton |
|----------------|------------|------------|----------|------------------------|----------------------------|-------------|---------------|-------------|---------------|
| 1 | 10/17/2023 | 8:00 | 8:59 | 101,191 | 119.5 | 6.34 | 0.0530 | 0.04 | 0.0003 |
| 2 | 10/17/2023 | 13:40 | 14:39 | 103,004 | 119.6 | 5.83 | 0.0488 | 0.04 | 0.0003 |
| 3 | 10/17/2023 | 15:05 | 16:04 | 102,211 | 119.7 | 6.99 | 0.0584 | 0.04 | 0.0003 |
| Average | | | | 102,135 | 119.6 | 6.39 | 0.0534 | 0.04 | 0.0003 |

6.0 CERTIFICATION

Mostardi Platt is pleased to have been of service to GCC Rio Grande Inc. If you have any questions regarding this test report, please do not hesitate to contact us at 630-993-2100.


As project manager, I hereby certify that this test report represents a true and accurate summary of emissions test results and the methodologies employed to obtain those results, and the test program was performed in accordance with the methods specified in this test report.

MOSTARDI PLATT



Richard J. Sollars II

Project Manager



Chet A. Gutwein

Quality Assurance

APPENDICES

Appendix A – Plant Operating Data

| Date/Time | Expression Value (sT/hr) (TNHR) |
|------------------|------------------------------------|
| 10/17/2023 08:00 | 119.4 |
| 10/17/2023 08:01 | 119.4 |
| 10/17/2023 08:02 | 119.4 |
| 10/17/2023 08:03 | 119.4 |
| 10/17/2023 08:04 | 119.4 |
| 10/17/2023 08:05 | 119.4 |
| 10/17/2023 08:06 | 119.4 |
| 10/17/2023 08:07 | 119.4 |
| 10/17/2023 08:08 | 119.3 |
| 10/17/2023 08:09 | 119.5 |
| 10/17/2023 08:10 | 119.4 |
| 10/17/2023 08:11 | 119.4 |
| 10/17/2023 08:12 | 119.4 |
| 10/17/2023 08:13 | 119.5 |
| 10/17/2023 08:14 | 119.4 |
| 10/17/2023 08:15 | 119.4 |
| 10/17/2023 08:16 | 119.4 |
| 10/17/2023 08:17 | 119.5 |
| 10/17/2023 08:18 | 119.4 |
| 10/17/2023 08:19 | 119.3 |
| 10/17/2023 08:20 | 119.4 |
| 10/17/2023 08:21 | 119.4 |
| 10/17/2023 08:22 | 119.4 |
| 10/17/2023 08:23 | 119.4 |
| 10/17/2023 08:24 | 119.4 |
| 10/17/2023 08:25 | 119.4 |
| 10/17/2023 08:26 | 119.4 |
| 10/17/2023 08:27 | 119.5 |
| 10/17/2023 08:28 | 119.4 |
| 10/17/2023 08:29 | 119.4 |
| 10/17/2023 08:30 | 119.4 |
| 10/17/2023 08:31 | 119.3 |
| 10/17/2023 08:32 | 119.4 |
| 10/17/2023 08:33 | 119.4 |
| 10/17/2023 08:34 | 119.4 |
| 10/17/2023 08:35 | 119.4 |
| 10/17/2023 08:36 | 119.5 |
| 10/17/2023 08:37 | 119.4 |
| 10/17/2023 08:38 | 119.4 |
| 10/17/2023 08:39 | 119.4 |
| 10/17/2023 08:40 | 119.4 |
| 10/17/2023 08:41 | 119.4 |
| 10/17/2023 08:42 | 119.4 |
| 10/17/2023 08:43 | 119.4 |
| 10/17/2023 08:44 | 119.4 |
| 10/17/2023 08:45 | 119.3 |
| 10/17/2023 08:46 | 119.4 |
| 10/17/2023 08:47 | 119.4 |
| 10/17/2023 08:48 | 119.4 |
| 10/17/2023 08:49 | 119.4 |
| 10/17/2023 08:50 | 119.4 |
| 10/17/2023 08:51 | 119.4 |
| 10/17/2023 08:52 | 119.4 |
| 10/17/2023 08:53 | 121.3 |
| 10/17/2023 08:54 | 120.3 |
| 10/17/2023 08:55 | 119.7 |
| 10/17/2023 08:56 | 119.6 |
| 10/17/2023 08:57 | 119.6 |
| 10/17/2023 08:58 | 119.6 |
| 10/17/2023 08:59 | 119.6 |

119.5 Run 1 Mill Off HCN

| Date/Time | Expression Value |
|------------------|------------------|
| 10/17/2023 13:40 | 119.7 |
| 10/17/2023 13:41 | 119.7 |
| 10/17/2023 13:42 | 119.6 |
| 10/17/2023 13:43 | 119.7 |
| 10/17/2023 13:44 | 119.6 |
| 10/17/2023 13:45 | 119.6 |
| 10/17/2023 13:46 | 119.6 |
| 10/17/2023 13:47 | 119.7 |
| 10/17/2023 13:48 | 119.6 |
| 10/17/2023 13:49 | 119.7 |
| 10/17/2023 13:50 | 119.6 |
| 10/17/2023 13:51 | 119.6 |
| 10/17/2023 13:52 | 119.6 |
| 10/17/2023 13:53 | 119.6 |
| 10/17/2023 13:54 | 119.6 |
| 10/17/2023 13:55 | 119.7 |
| 10/17/2023 13:56 | 119.7 |
| 10/17/2023 13:57 | 119.6 |
| 10/17/2023 13:58 | 119.7 |
| 10/17/2023 13:59 | 119.7 |
| 10/17/2023 14:00 | 119.7 |
| 10/17/2023 14:01 | 119.7 |
| 10/17/2023 14:02 | 119.6 |
| 10/17/2023 14:03 | 119.6 |
| 10/17/2023 14:04 | 119.6 |
| 10/17/2023 14:05 | 119.6 |
| 10/17/2023 14:06 | 119.7 |
| 10/17/2023 14:07 | 119.7 |
| 10/17/2023 14:08 | 119.7 |
| 10/17/2023 14:09 | 119.6 |
| 10/17/2023 14:10 | 119.7 |
| 10/17/2023 14:11 | 119.6 |
| 10/17/2023 14:12 | 119.6 |
| 10/17/2023 14:13 | 119.7 |
| 10/17/2023 14:14 | 119.7 |
| 10/17/2023 14:15 | 119.6 |
| 10/17/2023 14:16 | 119.6 |
| 10/17/2023 14:17 | 119.7 |
| 10/17/2023 14:18 | 119.7 |
| 10/17/2023 14:19 | 119.6 |
| 10/17/2023 14:20 | 119.7 |
| 10/17/2023 14:21 | 119.7 |
| 10/17/2023 14:22 | 119.6 |
| 10/17/2023 14:23 | 119.6 |
| 10/17/2023 14:24 | 119.7 |
| 10/17/2023 14:25 | 119.7 |
| 10/17/2023 14:26 | 119.7 |
| 10/17/2023 14:27 | 119.7 |
| 10/17/2023 14:28 | 119.6 |
| 10/17/2023 14:29 | 119.6 |
| 10/17/2023 14:30 | 119.6 |
| 10/17/2023 14:31 | 119.7 |
| 10/17/2023 14:32 | 119.6 |
| 10/17/2023 14:33 | 119.7 |
| 10/17/2023 14:34 | 119.6 |
| 10/17/2023 14:35 | 119.7 |
| 10/17/2023 14:36 | 119.7 |
| 10/17/2023 14:37 | 119.6 |
| 10/17/2023 14:38 | 119.6 |
| 10/17/2023 14:39 | 119.6 |

119.6 Run 2 Mill Off HCN

| Date/Time | Expression Value |
|------------------|------------------|
| 10/17/2023 15:05 | 119.6 |
| 10/17/2023 15:06 | 119.7 |
| 10/17/2023 15:07 | 119.6 |
| 10/17/2023 15:08 | 119.6 |
| 10/17/2023 15:09 | 119.7 |
| 10/17/2023 15:10 | 119.7 |
| 10/17/2023 15:11 | 119.7 |
| 10/17/2023 15:12 | 119.7 |
| 10/17/2023 15:13 | 119.7 |
| 10/17/2023 15:14 | 119.7 |
| 10/17/2023 15:15 | 119.7 |
| 10/17/2023 15:16 | 119.7 |
| 10/17/2023 15:17 | 119.6 |
| 10/17/2023 15:18 | 119.6 |
| 10/17/2023 15:19 | 119.6 |
| 10/17/2023 15:20 | 119.7 |
| 10/17/2023 15:21 | 119.7 |
| 10/17/2023 15:22 | 119.6 |
| 10/17/2023 15:23 | 119.7 |
| 10/17/2023 15:24 | 119.7 |
| 10/17/2023 15:25 | 119.7 |
| 10/17/2023 15:26 | 119.7 |
| 10/17/2023 15:27 | 119.7 |
| 10/17/2023 15:28 | 119.6 |
| 10/17/2023 15:29 | 119.7 |
| 10/17/2023 15:30 | 119.7 |
| 10/17/2023 15:31 | 119.6 |
| 10/17/2023 15:32 | 119.6 |
| 10/17/2023 15:33 | 119.6 |
| 10/17/2023 15:34 | 119.6 |
| 10/17/2023 15:35 | 119.7 |
| 10/17/2023 15:36 | 119.6 |
| 10/17/2023 15:37 | 119.7 |
| 10/17/2023 15:38 | 119.6 |
| 10/17/2023 15:39 | 119.7 |
| 10/17/2023 15:40 | 119.7 |
| 10/17/2023 15:41 | 119.7 |
| 10/17/2023 15:42 | 119.7 |
| 10/17/2023 15:43 | 119.7 |
| 10/17/2023 15:44 | 119.6 |
| 10/17/2023 15:45 | 119.7 |
| 10/17/2023 15:46 | 119.7 |
| 10/17/2023 15:47 | 119.7 |
| 10/17/2023 15:48 | 119.6 |
| 10/17/2023 15:49 | 119.6 |
| 10/17/2023 15:50 | 119.7 |
| 10/17/2023 15:51 | 119.7 |
| 10/17/2023 15:52 | 119.6 |
| 10/17/2023 15:53 | 119.7 |
| 10/17/2023 15:54 | 119.6 |
| 10/17/2023 15:55 | 119.6 |
| 10/17/2023 15:56 | 119.6 |
| 10/17/2023 15:57 | 119.6 |
| 10/17/2023 15:58 | 119.6 |
| 10/17/2023 15:59 | 119.6 |
| 10/17/2023 16:00 | 119.6 |
| 10/17/2023 16:01 | 119.7 |
| 10/17/2023 16:02 | 119.6 |
| 10/17/2023 16:03 | 119.7 |
| 10/17/2023 16:04 | 119.7 |

119.7 Run 3 Mill Off HCN

| Date/Time | Expression Value (sT/hr) (TNHR) |
|------------------|------------------------------------|
| 10/18/2023 08:40 | 112.5 |
| 10/18/2023 08:41 | 112.5 |
| 10/18/2023 08:42 | 112.7 |
| 10/18/2023 08:43 | 112.5 |
| 10/18/2023 08:44 | 112.5 |
| 10/18/2023 08:45 | 112.5 |
| 10/18/2023 08:46 | 112.5 |
| 10/18/2023 08:47 | 112.5 |
| 10/18/2023 08:48 | 112.5 |
| 10/18/2023 08:49 | 112.7 |
| 10/18/2023 08:50 | 112.5 |
| 10/18/2023 08:51 | 112.5 |
| 10/18/2023 08:52 | 112.7 |
| 10/18/2023 08:53 | 112.7 |
| 10/18/2023 08:54 | 112.5 |
| 10/18/2023 08:55 | 112.7 |
| 10/18/2023 08:56 | 112.5 |
| 10/18/2023 08:57 | 112.7 |
| 10/18/2023 08:58 | 112.7 |
| 10/18/2023 08:59 | 112.7 |
| 10/18/2023 09:00 | 112.5 |
| 10/18/2023 09:01 | 112.7 |
| 10/18/2023 09:02 | 112.7 |
| 10/18/2023 09:03 | 112.5 |
| 10/18/2023 09:04 | 112.7 |
| 10/18/2023 09:05 | 112.7 |
| 10/18/2023 09:06 | 112.5 |
| 10/18/2023 09:07 | 112.7 |
| 10/18/2023 09:08 | 112.7 |
| 10/18/2023 09:09 | 112.7 |
| 10/18/2023 09:10 | 112.5 |
| 10/18/2023 09:11 | 112.5 |
| 10/18/2023 09:12 | 112.5 |
| 10/18/2023 09:13 | 112.7 |
| 10/18/2023 09:14 | 112.7 |
| 10/18/2023 09:15 | 112.5 |
| 10/18/2023 09:16 | 112.7 |
| 10/18/2023 09:17 | 112.5 |
| 10/18/2023 09:18 | 112.7 |
| 10/18/2023 09:19 | 112.5 |
| 10/18/2023 09:20 | 112.7 |
| 10/18/2023 09:21 | 112.5 |
| 10/18/2023 09:22 | 112.7 |
| 10/18/2023 09:23 | 112.5 |
| 10/18/2023 09:24 | 112.5 |
| 10/18/2023 09:25 | 112.7 |
| 10/18/2023 09:26 | 112.7 |
| 10/18/2023 09:27 | 112.7 |
| 10/18/2023 09:28 | 112.5 |
| 10/18/2023 09:29 | 112.7 |
| 10/18/2023 09:30 | 112.5 |
| 10/18/2023 09:31 | 112.7 |
| 10/18/2023 09:32 | 112.5 |
| 10/18/2023 09:33 | 112.5 |
| 10/18/2023 09:34 | 112.7 |
| 10/18/2023 09:35 | 112.5 |
| 10/18/2023 09:36 | 112.5 |
| 10/18/2023 09:37 | 112.7 |
| 10/18/2023 09:38 | 112.7 |
| 10/18/2023 09:39 | 112.7 |

112.6 Run 1 Mill On HCN

| Date/Time | MAN_KILN_STACK (sT/hr) (TNHR) Expression Value |
|------------------|---|
| 10/18/2023 10:10 | 112.7 |
| 10/18/2023 10:11 | 112.5 |
| 10/18/2023 10:12 | 112.7 |
| 10/18/2023 10:13 | 112.7 |
| 10/18/2023 10:14 | 112.5 |
| 10/18/2023 10:15 | 112.5 |
| 10/18/2023 10:16 | 112.7 |
| 10/18/2023 10:17 | 112.7 |
| 10/18/2023 10:18 | 112.7 |
| 10/18/2023 10:19 | 112.7 |
| 10/18/2023 10:20 | 112.7 |
| 10/18/2023 10:21 | 112.5 |
| 10/18/2023 10:22 | 112.7 |
| 10/18/2023 10:23 | 112.5 |
| 10/18/2023 10:24 | 112.7 |
| 10/18/2023 10:25 | 112.7 |
| 10/18/2023 10:26 | 112.5 |
| 10/18/2023 10:27 | 112.7 |
| 10/18/2023 10:28 | 112.5 |
| 10/18/2023 10:29 | 112.7 |
| 10/18/2023 10:30 | 112.7 |
| 10/18/2023 10:31 | 112.7 |
| 10/18/2023 10:32 | 112.7 |
| 10/18/2023 10:33 | 112.7 |
| 10/18/2023 10:34 | 112.5 |
| 10/18/2023 10:35 | 112.7 |
| 10/18/2023 10:36 | 112.9 |
| 10/18/2023 10:37 | 114.3 |
| 10/18/2023 10:38 | 114.4 |
| 10/18/2023 10:39 | 114.4 |
| 10/18/2023 10:40 | 114.4 |
| 10/18/2023 10:41 | 114.3 |
| 10/18/2023 10:42 | 114.4 |
| 10/18/2023 10:43 | 114.3 |
| 10/18/2023 10:44 | 114.4 |
| 10/18/2023 10:45 | 114.3 |
| 10/18/2023 10:46 | 114.3 |
| 10/18/2023 10:47 | 114.4 |
| 10/18/2023 10:48 | 116.1 |
| 10/18/2023 10:49 | 116.2 |
| 10/18/2023 10:50 | 116.1 |
| 10/18/2023 10:51 | 116.1 |
| 10/18/2023 10:52 | 116.2 |
| 10/18/2023 10:53 | 116.1 |
| 10/18/2023 10:54 | 116.2 |
| 10/18/2023 10:55 | 116.2 |
| 10/18/2023 10:56 | 116.2 |
| 10/18/2023 10:57 | 116.2 |
| 10/18/2023 10:58 | 116.2 |
| 10/18/2023 10:59 | 116.1 |
| 10/18/2023 11:00 | 116.2 |
| 10/18/2023 11:01 | 116.2 |
| 10/18/2023 11:02 | 116.2 |
| 10/18/2023 11:03 | 116.2 |
| 10/18/2023 11:04 | 116.2 |
| 10/18/2023 11:05 | 116.1 |
| 10/18/2023 11:06 | 116.2 |
| 10/18/2023 11:07 | 116.7 |
| 10/18/2023 11:08 | 117.8 |
| 10/18/2023 11:09 | 117.9 |

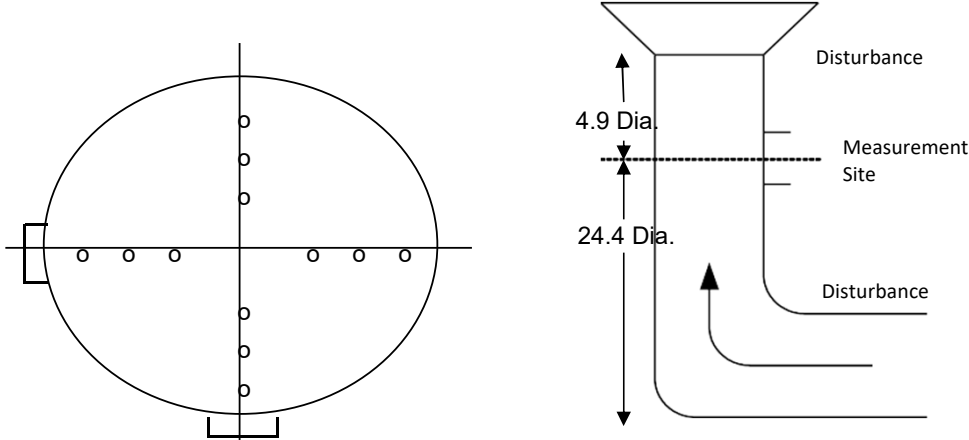
114.3 Run 2 Mill On HCN

| Date/Time | Expression Value |
|------------------|------------------|
| 10/18/2023 12:25 | 119.7 |
| 10/18/2023 12:26 | 119.6 |
| 10/18/2023 12:27 | 119.6 |
| 10/18/2023 12:28 | 119.6 |
| 10/18/2023 12:29 | 119.7 |
| 10/18/2023 12:30 | 119.6 |
| 10/18/2023 12:31 | 119.7 |
| 10/18/2023 12:32 | 119.7 |
| 10/18/2023 12:33 | 119.7 |
| 10/18/2023 12:34 | 119.6 |
| 10/18/2023 12:35 | 119.7 |
| 10/18/2023 12:36 | 119.7 |
| 10/18/2023 12:37 | 119.6 |
| 10/18/2023 12:38 | 119.6 |
| 10/18/2023 12:39 | 119.7 |
| 10/18/2023 12:40 | 119.7 |
| 10/18/2023 12:41 | 119.8 |
| 10/18/2023 12:42 | 119.7 |
| 10/18/2023 12:43 | 119.6 |
| 10/18/2023 12:44 | 119.6 |
| 10/18/2023 12:45 | 119.7 |
| 10/18/2023 12:46 | 119.6 |
| 10/18/2023 12:47 | 119.7 |
| 10/18/2023 12:48 | 119.6 |
| 10/18/2023 12:49 | 119.6 |
| 10/18/2023 12:50 | 119.7 |
| 10/18/2023 12:51 | 119.7 |
| 10/18/2023 12:52 | 119.7 |
| 10/18/2023 12:53 | 119.7 |
| 10/18/2023 12:54 | 119.6 |
| 10/18/2023 12:55 | 119.7 |
| 10/18/2023 12:56 | 119.6 |
| 10/18/2023 12:57 | 119.6 |
| 10/18/2023 12:58 | 119.6 |
| 10/18/2023 12:59 | 119.6 |
| 10/18/2023 13:00 | 119.7 |
| 10/18/2023 13:01 | 119.7 |
| 10/18/2023 13:02 | 119.7 |
| 10/18/2023 13:03 | 119.7 |
| 10/18/2023 13:04 | 119.7 |
| 10/18/2023 13:05 | 119.7 |
| 10/18/2023 13:06 | 119.7 |
| 10/18/2023 13:07 | 119.6 |
| 10/18/2023 13:08 | 119.6 |
| 10/18/2023 13:09 | 119.6 |
| 10/18/2023 13:10 | 119.6 |
| 10/18/2023 13:11 | 119.6 |
| 10/18/2023 13:12 | 119.6 |
| 10/18/2023 13:13 | 119.6 |
| 10/18/2023 13:14 | 119.7 |
| 10/18/2023 13:15 | 119.7 |
| 10/18/2023 13:16 | 119.6 |
| 10/18/2023 13:17 | 119.7 |
| 10/18/2023 13:18 | 119.6 |
| 10/18/2023 13:19 | 119.7 |
| 10/18/2023 13:20 | 119.6 |
| 10/18/2023 13:21 | 119.7 |
| 10/18/2023 13:22 | 119.6 |
| 10/18/2023 13:23 | 119.6 |
| 10/18/2023 13:24 | 119.6 |

119.7 Run 3 Mill On HCN

Appendix B – Test Section Diagrams

EQUAL AREA TRAVERSE FOR ROUND DUCTS



Client: GCC Rio Grande, Inc.

Facility: Pueblo Plant

Test Location: Main Kiln Stack

Date: 10/17/23 & 10/18/23

Diameter (Feet): 10.250

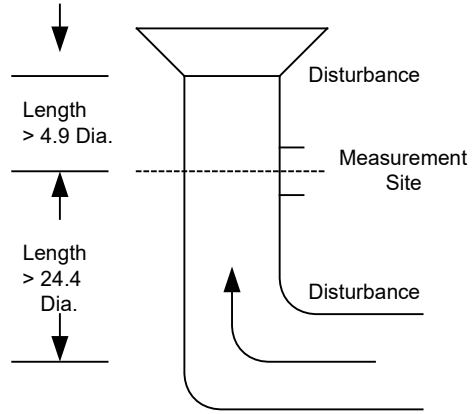
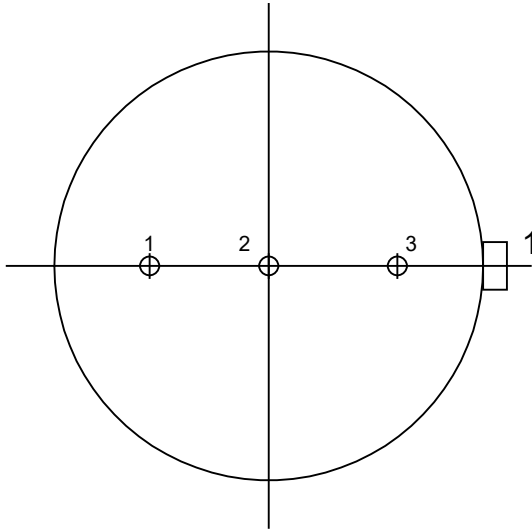
Port Length (In): 9.50

Ports Sampled: 4

Points/Port: 3

| Point Markings | | |
|----------------|------------------------|---------------|
| | From inside wall (in.) | % of Diameter |
| 1 | 5.41 | 4.40 |
| 2 | 17.96 | 14.60 |
| 3 | 36.41 | 29.60 |

STRATIFICATION TEST FOR ROUND DUCTS



Job: GCC Rio Grande Inc.
Pueblo Plant
Pueblo, Colorado

Test Location: Main Kiln

Stack Diameter: 10.25 Feet

Stack Area: 82.516 Square Feet

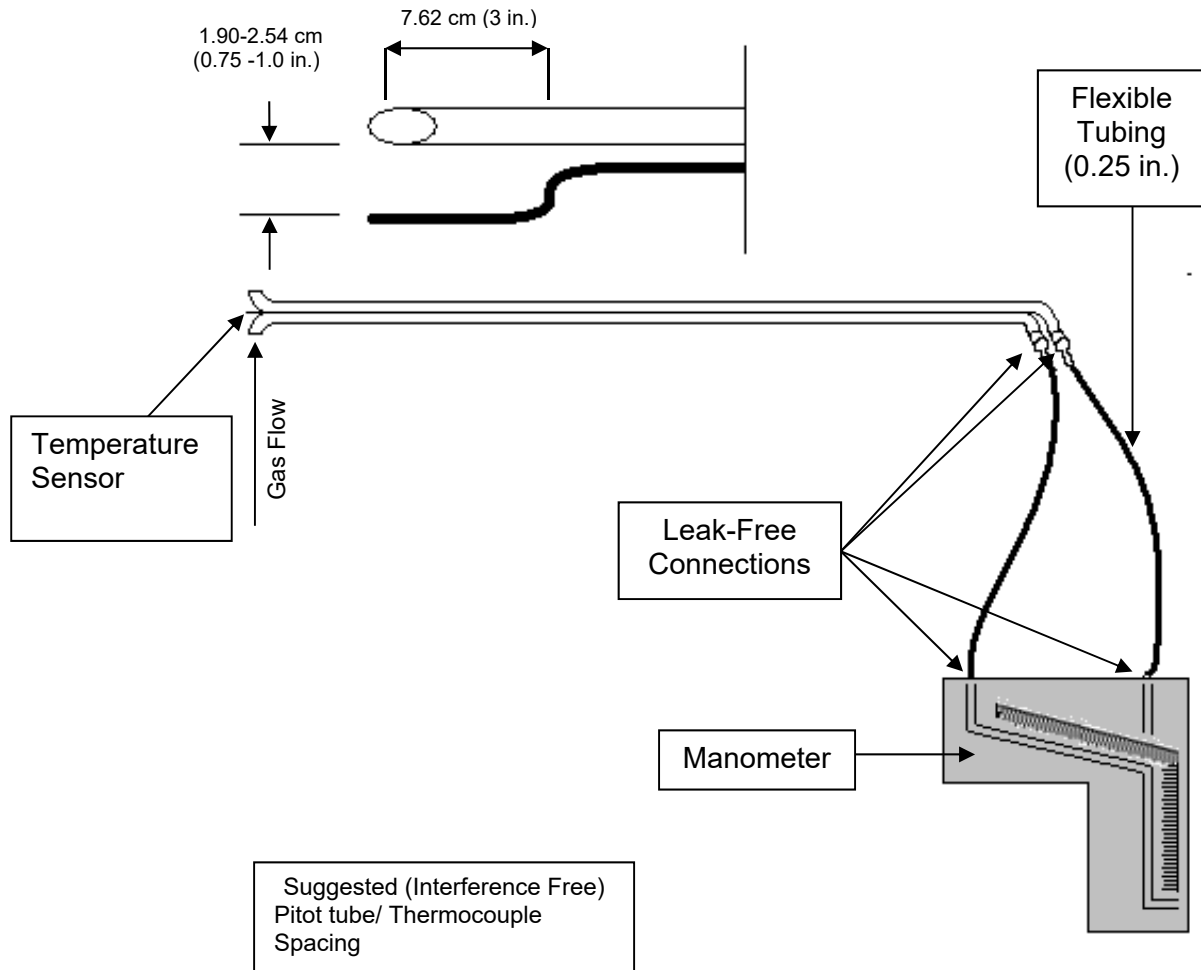
No. Sample Points: 3

Distance from Inside Wall
To Traverse Point:

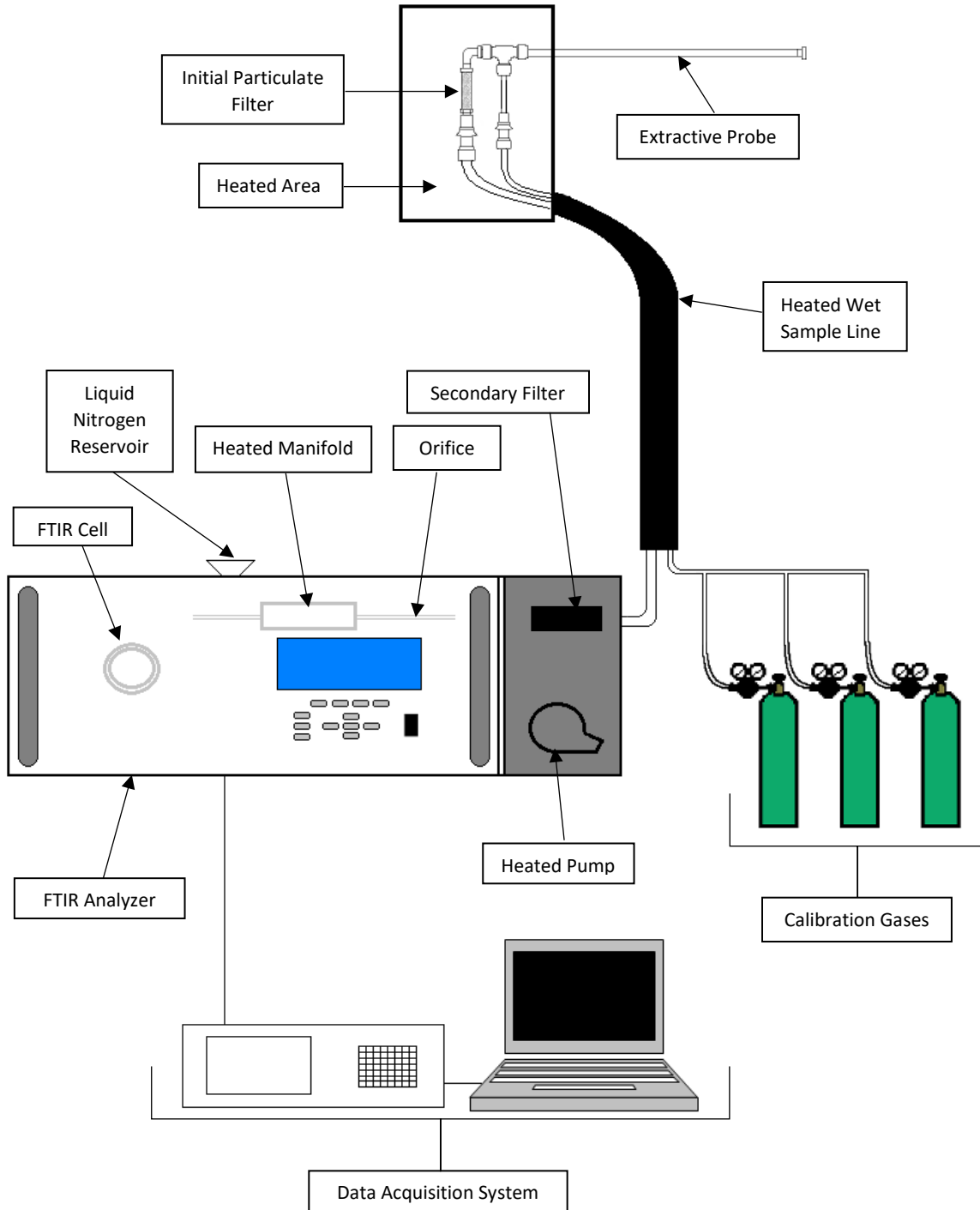
1. 83.3 % of diameter
2. 50.0 % of diameter
3. 16.7 % of diameter

Appendix C – Sample Train Diagrams

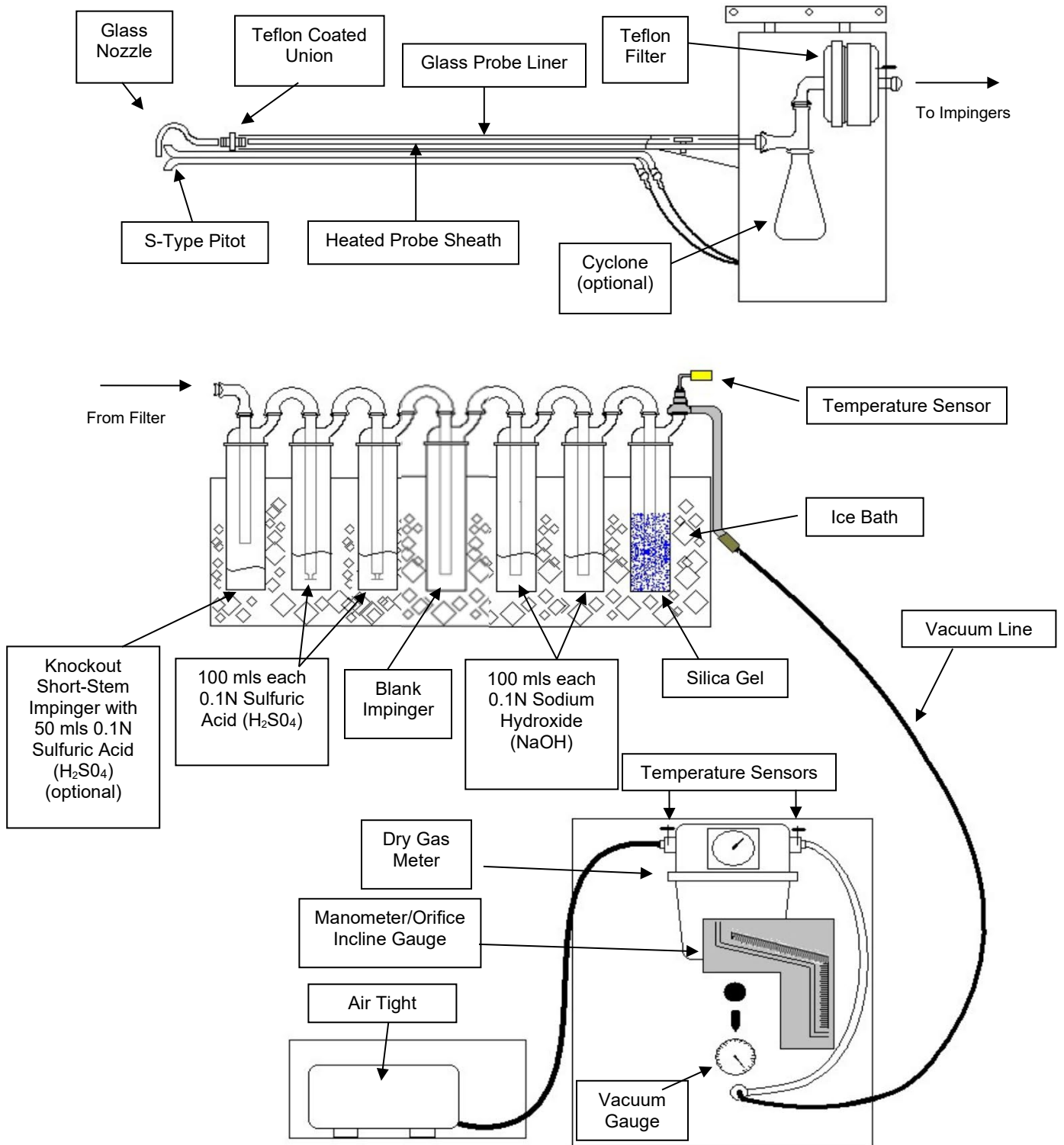
USEPA Method 2 – Type S Pitot Tube Manometer Assembly



USEPA Method 320 – Vapor Phase Organic and Inorganic Emissions by Extractive Fourier Transform Infrared (FTIR) Spectroscopy Sample Train Diagram



USEPA Method 26A – HF and Cl₂ Sample Train Diagram



Appendix D – Calculation Nomenclature and Formulas

Client: GCC Rio Grande, Inc.
Facility: Pueblo Plant
Test Location: Main Kiln Stack
Run: 1
Date: 10/18/2023
Method: 26A
Source Condition: Mill On

Dry Molecular Weight

$$Md = 0.44 \times (\%CO_2) + 0.32 \times (\%O_2) + 0.28 \times \%N_2$$

$$\%CO_2 = \underline{19.4} \qquad \%O_2 = \underline{9.7} \qquad \%N_2 = \underline{70.9}$$

$$Md = \underline{31.492}$$

Wet Molecular Weight

$$Ms = Md \times (1 - Bws) + (18.0 \times Bws)$$

$$Md = \underline{31.492} \qquad Bws = \underline{0.141}$$

$$Ms = \underline{29.592}$$

Meter Volume at Standard Conditions

$$Vm(std) = 17.647 \times Y \times Vm \times \frac{(Pbar + DH/13.6)}{Tm}$$

$$Y = \underline{0.994} \qquad Vm = \underline{55.293} \qquad Pbar = \underline{24.9}$$

$$DH = \underline{2.3} \qquad Tm = \underline{62.8}$$

$$Vm(std) = \underline{46.481}$$

Volume of Water Vapor Condensed

$$Vw(std) = 0.0471 \times (\text{net H}_2\text{O gain})$$

$$\text{Net H}_2\text{O} = \underline{161.8}$$

$$Vw(std) = \underline{7.621}$$

Moisture Content

$$Bws = \frac{Vw(std)}{Vw(std) + Vm(std)}$$

$$Vw(std) = \underline{7.621} \qquad Vm(std) = \underline{46.481}$$

$$Bws = \underline{0.141}$$

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Run: 1
 Date: 10/18/2023
 Method: 26A
 Source Condition: Mill On

Average Duct Velocity

$$V_s = 85.49 \times C_p \times \text{Sqrt DP (avg)} \times (T_s \text{ (avg)} + 460 / (P_s \times M_s))^{1/2}$$

| | | |
|-----------------------------|--|---|
| $C_p = \frac{0.820}{24.94}$ | $T_s \text{ (avg)} = \frac{215.3}{29.592}$ | $\text{Sqrt DP (avg)} = \frac{0.790}{}$ |
| $P_s = \frac{24.94}{}$ | $M_s = \frac{29.592}{}$ | |
| $V_s = \frac{53.009}{}$ | | |

Volumetric Flow Rate (Actual Basis)

$$Q = V_s \times A \times 60$$

| | |
|-------------------------|-----------------------|
| $V_s = \frac{53.009}{}$ | $A = \frac{82.516}{}$ |
| $Q = \frac{262,445}{}$ | |

Volumetric Flow Rate (Standard Basis)

$$Q_{std} = 17.647 \times Q \times \frac{P_s}{T_s \text{ (avg)} + 460}$$

| | | |
|------------------------------|------------------------|--------------------------------------|
| $Q = \frac{262,445}{}$ | $P_s = \frac{24.94}{}$ | $T_s \text{ (avg)} = \frac{215.3}{}$ |
| $Q_{std} = \frac{171,002}{}$ | | |

Volumetric Flow Rate (Standard Dry Basis)

$$Q_{std(dry)} = Q_{std} \times (1 - B_{ws})$$

| | |
|-----------------------------------|---------------------------|
| $Q_{std} = \frac{171,002}{}$ | $B_{ws} = \frac{0.141}{}$ |
| $Q_{std(dry)} = \frac{146,915}{}$ | |

Isokinetic Variation:

$$\%ISO = \frac{0.0945 \times (T_s + 460) \times V_m(std)}{V_s \times \theta \times A_n \times P_s \times (1 - B_{ws})}$$

| | | |
|----------------------------|------------------------------|-------------------------|
| $T_s = \frac{215.3}{}$ | $V_m(std) = \frac{46.481}{}$ | $V_s = \frac{53.009}{}$ |
| $A_n = \frac{0.0004307}{}$ | $\theta = \frac{60}{}$ | $P_s = \frac{24.94}{}$ |
| $B_{ws} = \frac{0.141}{}$ | | |
| $\%ISO = \frac{101.1}{}$ | | |

Client: GCC Rio Grande, Inc.
Facility: Pueblo Plant
Test Location: Main Kiln Stack
Run: 1
Date: 10/18/2023
Method: 26A
Source Condition: Mill On

Chloride (Cl2) Concentration:

$$\text{mg/m}^3 = \frac{\text{mg of Chloride (Cl}_2\text{)}}{\text{Vm(std)} \times 0.02832 \text{ m}^3/\text{ft}^3}$$

mg = 0.15 Vm(std) = 46.481
 mg/m³ = 0.11

Chloride (Cl2) Emission Rate:

$$\text{lb of Chloride (Cl}_2\text{)} = \frac{\mu\text{g of sample} \times 10^6 \text{ grams}/\mu\text{g}}{453.6 \text{ grams/lb}}$$

$$\text{Emission Rate lb/hr} = \frac{\text{lb of Chloride (Cl}_2\text{)}}{\text{Vm(std)}} \times \text{dscfm} \times 60 \text{ min/hr}$$

lb of Chloride (Cl₂) = 3.31E-10 dscfm = 146,915
 Emission Rate lb/hr = 0.0627
 Emission Rate lb/ton = $\frac{\text{lb/hr of Chloride (Cl}_2\text{)}}{\text{clinker production ton/hr}}$
 lb/hr of Chloride (Cl₂) = 0.0627 clinker ton/hr = 112.6
 Emission Rate lb/ton = 0.0006

Client: GCC Rio Grande, Inc.
Facility: Pueblo Plant
Project #: M234207
Test Location: Main Kiln
Date: 10/18/23

Sample Calculations

$$(9.66\% - 0.04\%) \times \frac{\text{O2 \% (dry)} \quad 11.07\%}{11.02\% - 0.04\%} = 9.70\%$$

$$C_{\text{gas}} = (C - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0}$$

where:

C_{gas} = Effluent gas concentration, dry basis, ppm or %

C = Average gas concentration indicated by gas analyzer, dry basis, ppm or %

C_0 = Average of initial and final system calibration bias check responses for the zero gas, ppm or %

C_{m} = Average of initial and final system calibration bias check responses for the upscale calibration gas, ppm or %

C_{ma} = Actual concentration of the upscale calibration gas, ppm or %

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Test Location: Main Kiln
 Date: 10/18/23

FTIR Sample Calculations

Direct Recovery % of Calibration Transfer Standard

$$DR_{cts} = \frac{D_{cts}}{Cma} \times 100$$

$$Cma = \frac{100.7}{}$$

$$D_{cts} = \frac{100.8}{}$$

$$DR_{cts} = \frac{100.1\%}{}$$

Recovery % with Calibration Transfer Standard System Purge

$$R_{cts} = \frac{Sys_{cts}}{D_{cts}} \times 100$$

$$Sys_{cts} = \frac{100.5}{}$$

$$D_{cts} = \frac{100.8}{}$$

$$R_{cts} = \frac{100\%}{}$$

Direct Recovery % of Analyte Spike Gas

SF6

$$DR_{sf6} = \frac{D_{sf6}}{Cma} \times 100$$

$$Cma = \frac{10.0}{}$$

$$D_{sf6} = \frac{10.0}{}$$

$$DR_{sf6} = \frac{100\%}{}$$

HCN

$$DR_{asg} = \frac{D_{asg}}{Cma} \times 100$$

$$Cma = \frac{199.2}{}$$

$$D_{asg} = \frac{194.2}{}$$

$$DR_{asg} = \frac{97.5\%}{}$$

Dilution Factor for Analyte Spiking

$$DF = \frac{Spk_{sf6}}{D_{sf6}}$$

$$Spk_{sf6} = \frac{0.594}{}$$

$$D_{sf6} = \frac{10.000}{}$$

$$DF = \frac{0.059}{}$$

Recovery % for Analyte Spike With HCN

$$R_x = \frac{Spk_x}{(N_x \times (1-DF) + D_{asg} \times DF)}$$

$$Spk_x = \frac{21.2}{}$$

$$N_x = \frac{10.5}{}$$

$$DF = \frac{0.059}{}$$

$$D_{asg} = \frac{194.2}{}$$

$$R_x = \frac{98.8}{} \%$$

where:

- DR_{cts} = Recovery % of the calibration transfer standard directly to the analyzer
- Cma = certified concentration of calibration gas, ppm
- D_{cts} = Concentration of the calibration transfer standard gas directly to the analyzer, ppm
- R_{cts} = Recovery % of the calibration transfer standard through the sampling system
- Sys_{cts} = Concentration of the calibration transfer standard gas through the system, ppm
- DF = Dilution Factor of analyte spike gas
- Spk_{sf6} = SF6 concentration in effluent during spiking
- Spk_x = Analyte concentration in effluent during spiking
- D_{asg} = Concentration of the analyte spike gas directly to the analyzer, ppm
- D_{sf6} = Concentration of the SF6 directly to the analyzer, ppm
- R_x = Recovery % of the analyte spike gas
- N_x = Native effluent (HCN) concentration prior to analyte spike

MOSTARDI PLATT

Moisture Calculations

$$V_{wc(std)} = \frac{(V_f - V_i)\rho_w RT_{std}}{P_{std}M_w} = 0.04707(V_f - V_i)$$

$$V_{wsg(std)} = \frac{(W_f - W_i)\rho_w RT_{std}}{P_{std}M_w} = 0.04715(W_f - W_i)$$

$$V_{m(std)} = 17.64 V_m Y \frac{P_{bar} + \frac{\Delta H}{13.6}}{T_m}$$

$$B_{ws} = \frac{V_{wc(std)} + V_{wsg(std)}}{V_{wc(std)} + V_{wsg(std)} + V_{m(std)}}$$

Where:

B_{ws} = Water vapor in gas stream, proportion by volume

M_w = Molecular weight of water, 18.015 lb/lb-mole

P_{bar} = Barometric pressure at the testing site, in. Hg

P_{std} = Standard absolute pressure, 29.92 in. Hg

R = Ideal gas constant, $0.048137 \text{ (in. Hg)(ft}^3\text{)/(g-mole)(}^\circ\text{R)} =$
 $[21.8348 \text{ (in. Hg)(ft}^3\text{)/(lb-mole)(}^\circ\text{R)}]/453.592 \text{ g-mole/lb-mole}$

T_m = Absolute average dry gas meter temperature, $^\circ\text{R}$

T_{std} = Standard absolute temperature, 528 $^\circ\text{R}$

V_f = Final volume of condenser water, ml

V_i = Initial volume of condenser water, ml

V_m = Dry gas volume measured by dry gas meter, dcf

$V_{m(std)}$ = Dry gas volume measured by dry gas meter, corrected to standard conditions, scf

$V_{wc(std)}$ = Volume of condensed water vapor, corrected to standard conditions, scf

$V_{wsg(std)}$ = Volume of water vapor collected in silica gel, corrected to standard conditions, scf

W_f = Final weight of silica gel, g

W_i = Initial weight of silica gel, g

Y = Dry gas meter calibration factor

ΔH = Average pressure exerted on dry gas meter outlet by gas sample bag, in. H_2O

ρ_w = Density of water, 0.9982 g/ml

13.6 = Specific gravity of mercury (Hg)

17.64 = T_{std}/P_{std}

0.04707 = ft^3/ml 0.04715 = ft^3/g

MOSTARDI PLATT

Volumetric Flow Nomenclature

- A = Cross-sectional area of stack or duct, ft²
- B_{ws} = Water vapor in gas stream, proportion by volume
- C_p = Pitot tube coefficient, dimensionless
- M_d = Dry molecular weight of gas, lb/lb-mole
- M_s = Molecular weight of gas, wet basis, lb/lb-mole
- M_w = Molecular weight of water, 18.0 lb/lb-mole
- P_{bar} = Barometric pressure at testing site, in. Hg
- P_g = Static pressure of gas, in. Hg (in. H₂O/13.6)
- DH = Static pressure of gas, in. H₂O
- P_s = Absolute pressure of gas, in. Hg = P_{bar} + P_g
- P_{std} = Standard absolute pressure, 29.92 in. Hg
- A_{cfm} = Actual volumetric gas flow rate
- Sc_{fm} = Volumetric gas flow rate, corrected to standard conditions
- D_{scfm} = Standard volumetric flow rate, corrected to dry conditions
- R = Ideal gas constant, 21.85 in. Hg-ft³/°R-lb-mole
- T_s = Average stack gas temperature, °F
- T_m = Average dry gas meter temperature, °F
- T_{std} = Standard absolute temperature, 528°R
- v_s = Gas velocity, ft/sec
- V_{m(std)} = Volume of gas sampled, corrected to standard conditions, scf
- V_{w(std)} = Volume of water vapor in gas sample, corrected to standard conditions, scf
- V_{lc} = Volume of liquid collected
- Y = Dry gas meter calibration factor
- Δp = Velocity head of gas, in. H₂O
- K₁ = 17.647 °R/in. Hg
- %EA = Percent excess air
- %CO₂ = Percent carbon dioxide by volume, dry basis
- %O₂ = Percent oxygen by volume, dry basis
- %N₂ = Percent nitrogen by volume, dry basis
- 0.264 = Ratio of O₂ to N₂ in air, v/v
- 0.28 = Molecular weight of N₂ or CO, divided by 100
- 0.32 = Molecular weight of O₂ divided by 100
- 0.44 = Molecular weight of CO₂ divided by 100
- 13.6 = Specific gravity of mercury (Hg)

MOSTARDI PLATT

Volumetric Air Flow Calculations

$$Vm (std) = 17.647 \times Vm \times \left[\frac{(P_{bar} + \left[\frac{DH}{13.6} \right])}{(460 + Tm)} \right] \times Y$$

$$Vw (std) = 0.0471 \times Vlc$$

$$Bws = \left[\frac{Vw (std)}{Vw (std) + Vm (std)} \right]$$

$$Md = (0.44 \times \%CO_2) + (0.32 \times \%O_2) + [0.28 \times (100 - \%CO_2 - \%O_2)]$$

$$Ms = Md \times (1 - Bws) + (18 \times Bws)$$

$$Vs = \sqrt{\frac{(Ts + 460)}{Ms \times Ps}} \times \sqrt{DP} \times Cp \times 85.49$$

$$Acfm = Vs \times Area (of\ stack\ or\ duct) \times 60$$

$$Scfm = Acfm \times 17.647 \times \left[\frac{Ps}{(460 + Ts)} \right]$$

$$Scfh = Scfm \times 60 \frac{min}{hr}$$

$$Dscfm = Scfm \times (1 - Bws)$$

MOSTARDI PLATT

Isokinetic Calculation Formulas

$$1. V_{w(std)} = V_{lc} \left(\frac{\rho_w}{M_w} \right) \left(\frac{RT_{std}}{P_{std}} \right) = K_2 V_{lc}$$

$$2. V_{m(std)} = V_m Y \left(\frac{T_{std}}{T_m} \right) \left(\frac{(P_{bar} + (\frac{\Delta H}{13.6}))}{P_{std}} \right) = K_1 V_m Y \frac{(P_{bar} + (\frac{\Delta H}{13.6}))}{T_m}$$

$$3. B_{ws} = \frac{V_{w(std)}}{(V_{m(std)} + V_{w(std)})}$$

$$4. M_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2)$$

$$5. M_s = M_d(1 - B_{ws}) + 18.0(B_{ws})$$

$$6. C_a = \frac{m_a}{V_a \rho_a}$$

$$7. W_a = C_a V_{aw} \rho_a$$

$$8. C_{acf} = 15.43 K_i \left(\frac{m_n P_s}{(V_{w(std)} + V_{m(std)}) T_s} \right)$$

$$9. C_s = (15.43 \text{ grains/gram}) (m_n / V_{m(std)})$$

$$10. v_s = K_p C_p \sqrt{\frac{\Delta P T_s}{P_s M_s}}$$

$$11. Q_{acfm} = v_s A (60_{\text{sec/min}})$$

$$12. Q_{sd} = (3600_{\text{sec/hr}}) (1 - B_{ws}) v_s \left(\frac{T_{std} P_s}{T_s P_{std}} \right) A$$

$$13. E \text{ (emission rate, lbs/hr)} = Q_{std} (C_s / 7000 \text{ grains/lb})$$

$$14. IKV = \frac{T_s V_{m(std)} P_{std}}{T_{std} v_s \theta A_n P_s 60(1 - B_{ws})} = K_4 \frac{T_s V_{m(std)}}{P_s v_s A_n \theta (1 - B_{ws})}$$

$$15. \%EA = \left(\frac{\%O_2 - (0.5 \%CO)}{0.264 \%N_2 - (\%O_2 - 0.5 \%CO)} \right) \times 100$$

MOSTARDI PLATT

Isokinetic Nomenclature

- A = Cross-sectional area of stack or duct, square feet
A_n = Cross-sectional area of nozzle, square feet
B_{ws} = Water vapor in gas stream, by volume
C_a = Acetone blank residue concentration, g/g
C_{act} = Concentration of particulate matter in gas stream at actual conditions, gr/acf
C_p = Pitot tube coefficient
C_s = Concentration of particulate matter in gas stream, dry basis, corrected to standard conditions, gr/dscf
IKV = Isokinetic sampling variance, must be 90.0 % ≤ IKV ≤ 110.0%
M_d = Dry molecular weight of gas, lb/lb-mole
M_s = Molecular weight of gas, wet basis, lb/lb-mole
M_w = Molecular weight of water, 18.0 lb/lb-mole
m_a = Mass of residue of acetone after evaporation, grams
P_{bar} = Barometric pressure at testing site, inches mercury
P_g = Static pressure of gas, inches mercury (inches water/13.6)
P_s = Absolute pressure of gas, inches mercury = P_{bar} + P_g
P_{std} = Standard absolute pressure, 29.92 inches mercury
Q_{acfm} = Actual volumetric gas flow rate, acfm
Q_{sd} = Dry volumetric gas flow rate corrected to standard conditions, dscfh
R = Ideal gas constant, 21.85 inches mercury cubic foot/°R-lb-mole
T_m = Dry gas meter temperature, °R
T_s = Gas temperature, °R
T_{std} = Absolute temperature, 528°R
V_a = Volume of acetone blank, ml
V_{aw} = Volume of acetone used in wash, ml
W_a = Weight of residue in acetone wash, grams
m_n = Total amount of particulate matter collected, grams
V_{1c} = Total volume of liquid collected in impingers and silica gel, ml
V_m = Volume of gas sample as measured by dry gas meter, dcf
V_{m(std)} = Volume of gas sample measured by dry gas meter, corrected to standard conditions, dscf
V_s = Gas velocity, ft/sec
V_{w(std)} = Volume of water vapor in gas sample, corrected to standard conditions, scf
Y = Dry gas meter calibration factor
ΔH = Average pressure differential across the orifice meter, inches water
Δp = Velocity head of gas, inches water
ρ_a = Density of acetone, 0.7855 g/ml (average)
ρ_w = Density of water, 0.002201 lb/ml
θ = Total sampling time, minutes
K₁ = 17.647 °R/in. Hg
K₂ = 0.04707 ft³/ml
K₄ = 0.09450/100 = 0.000945
K_p = Pitot tube constant, $85.49 \frac{ft}{sec} \left[\frac{(lb/lb-mole)(in. Hg)}{(^{\circ}R)(in. H_2O)} \right]^{1/2}$
%EA = Percent excess air
%CO₂ = Percent carbon dioxide by volume, dry basis
%O₂ = Percent oxygen by volume, dry basis
%CO = Percent carbon monoxide by volume, dry basis
%N₂ = Percent nitrogen by volume, dry basis
0.264 = Ratio of O₂ to N₂ in air, v/v
28 = Molecular weight of N₂ or CO
32 = Molecular weight of O₂
44 = Molecular weight of CO₂
13.6 = Specific gravity of mercury (Hg)

MOSTARDI PLATT

Calculations for Hydrogen Fluoride By Method 26 or 26A

Concentration

$$\frac{\text{lbs HF}}{\text{dscf}} = \frac{\mu\text{g HF in sample}}{4.536 \times 10^8 \times \text{dscf}}$$

where:

$$4.536 \times 10^8 = \mu\text{g/lb}$$

dscf = Volume of gas sampled

$$\mu\text{g/lb HF} = \mu\text{g F} \times \frac{20.008}{19.000}$$

Parts Per Million

$$\text{ppm HF} = \frac{\text{lbs HF}}{\text{dscf}} \div \frac{20.008}{385 \times 10^6}$$

where:

385 = Volume of 1 lb mole of gas at 68°F and 29.92 in. Hg

106 = Conversion of ppm v/v

Emission Rate

$$\text{lbs HF /dscf} \times \text{dscfm} \times 60 \text{ min/hr} = \text{lbs/hr HF}$$

MOSTARDI PLATT

Pollutant Concentration Correction 7% for Percent Oxygen

$$C_{adj} = C_d \frac{20.9 - 7\%}{20.9 - \%O_2}$$

where:

C_{adj} = Pollutant concentration corrected to percent O_2

$20.9 - 7\%$ = Percent O_2 , the defined O_2 correction value, percent

20.9 = Percent O_2 in air

$\%O_2$ = Measured O_2 concentration dry basis, percent

C_d = Pollutant concentration measured, dry basis, ppm.

Appendix E- Laboratory Sample Analysis

| Chain-of-Custody Form | | | | | | |
|---|-------------|-----------------------------|------------|--------------------------------|--------------------|-------------|
| Project Number: M234207 | | | | Date Results Required: | | |
| Client: GCC Rio Grande Inc. | | | | TAT Required: | | |
| Plant/Test Location: Pueblo Kiln Stack (Mill Off) | | | | Project Supervisor: R. Sollars | | |
| Sample Number | Sample Date | Sample Point Identification | # of Conts | Sub Lab | Analysis Required | Volume, mls |
| 001 | 10/17/23 | #1A KILN M26A H2SO4 | 1 | | HF | 432.9 |
| 002 | 10/17/23 | #1A KILN M26A NaOH | 1 | | Cl ₂ | 314.4 |
| 003 | 10/17/23 | #1B KILN M26A H2SO4 | 1 | | HF | 436.4 |
| 004 | 10/17/23 | #1B KILN M26A NaOH | 1 | | Cl ₂ | 340.0 |
| 005 | 10/17/23 | #2A KILN M26A H2SO4 | 1 | | HF | 411.3 |
| 006 | 10/17/23 | #2A KILN M26A NaOH | 1 | | Cl ₂ | 320.0 |
| 007 | 10/17/23 | #2B KILN M26A H2SO4 | 1 | | HF | 421.7 |
| 008 | 10/17/23 | #2B KILN M26A NaOH | 1 | | Cl ₂ | 284.0 |
| 009 | 10/17/23 | #3A KILN M26A H2SO4 | 1 | | HF | 378.0 |
| 010 | 10/17/23 | #3A KILN M26A NaOH | 1 | | Cl ₂ | 319.0 |
| 011 | 10/17/23 | #3B KILN M26A H2SO4 | 1 | | HF | 441.3 |
| 012 | 10/17/23 | #3B KILN M26A NaOH | 1 | | Cl ₂ | 302.2 |
| 013 | 10/17/23 | A Train Blank H2SO4 | 1 | | HF | 284.4 |
| 014 | 10/17/23 | A Train Blank NaOH | 1 | | Cl ₂ | 216.5 |
| 015 | 10/17/23 | DI Reagent Blank | 1 | | HF/Cl ₂ | 207.8 |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| Delivered to Lab by: | | Received by: | | Processed by: | | Date/Time: |
| Date/Time: | | Date/Time: | | Date/Time: | | |

Laboratory Notes:

Chain-of-Custody Form

| Project Number: M234207 | | | | Date Results Required: | | |
|--|-------------|-----------------------------|------------------------------|--------------------------------|-------------------------------|-------------|
| Client: GCC Rio Grande Inc. | | | | TAT Required: | | |
| Plant/Test Location: Pueblo Kiln Stack (Mill On) | | | | Project Supervisor: R. Sollars | | |
| Sample Number | Sample Date | Sample Point Identification | # of Conts | Sub Lab | Analysis Required | Volume, mls |
| 001 | 10/18/23 | #1A KILN M26A H2SO4 | 1 | | HF | 535.5 |
| 002 | 10/18/23 | #1A KILN M26A NaOH | 1 | | Cl ₂ | 315.5 |
| 003 | 10/18/23 | #1B KILN M26A H2SO4 | 1 | | HF | 467.5 |
| 004 | 10/18/23 | #1B KILN M26A NaOH | 1 | | Cl ₂ | 289.6 |
| 005 | 10/18/23 | #2A KILN M26A H2SO4 | 1 | | HF | 462.9 |
| 006 | 10/18/23 | #2A KILN M26A NaOH | 1 | | Cl ₂ | 327.3 |
| 007 | 10/18/23 | #2B KILN M26A H2SO4 | 1 | | HF | 404.5 |
| 008 | 10/18/23 | #2B KILN M26A NaOH | 1 | | Cl ₂ | 327.2 |
| 009 | 10/18/23 | #3A KILN M26A H2SO4 | 1 | | HF | 499.1 |
| 010 | 10/18/23 | #3A KILN M26A NaOH | 1 | | Cl ₂ | 303.3 |
| 011 | 10/18/23 | #3B KILN M26A H2SO4 | 1 | | HF | 434.9 |
| 012 | 10/18/23 | #3B KILN M26A NaOH | 1 | | Cl ₂ | 278.7 |
| | | | | | | |
| | | | | | | |
| | | | | | | |
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| | | | | | | |
| | | | | | | |
| Delivered to Lab by: Date/Time: | | | Received by: Date/Time: | | Processed by: Date/Time: | |

Laboratory Notes:

Main Kiln Mill On

| | |
|---|--|
| Client: GCC Facility: Pueblo Test Location: Main Kiln Mill On Project Number: M234207 Method: 26A Date Samples Received: 11/3/2023 | Analysis Date: 11/15/2023 Analysis Location: Elmhurst Analyst: JMG |
|---|--|

Train A

| Sampling Date | | 10/18/2023 | 10/18/2023 | 10/18/2023 | 10/18/2023 | | |
|----------------------|-------|---------------|------------------|---------------|-------------------|-----|-----|
| | UNITS | M26A DI Blank | M26A H2SO4 Blank | M26A H2SO4-R1 | M26A H2SO4-R1 Dup | RDL | MDL |
| Sulfuric Acid Volume | ml | 215 | 254 | 499 | 499 | | |
| Hydrofluoric Acid | ug | <150 | <150 | <150 | <150 | 150 | 15 |

| Sampling Date | | 10/18/2023 | 10/18/2023 | 10/18/2023 | | |
|----------------------|-------|----------------|----------------|-------------------------|-----|-----|
| | UNITS | M26A- H2SO4 R2 | M26A- H2SO4 R3 | M26A- H2SO4 Field Blank | RDL | MDL |
| Sulfuric Acid Volume | ml | 472 | 505 | 231 | | |
| Hydrofluoric Acid | ug | <150 | <150 | <150 | 150 | 15 |

Train B

| Sampling Date | | 10/18/2023 | 10/18/2023 | 10/18/2023 | 10/18/2023 | | |
|----------------------|-------|---------------|------------------|---------------|-------------------|-----|-----|
| | UNITS | M26A DI Blank | M26A H2SO4 Blank | M26A H2SO4-R1 | M26A H2SO4-R1 Dup | RDL | MDL |
| Sulfuric Acid Volume | ml | 215 | 254 | 475 | 475 | | |
| Hydrofluoric Acid | ug | <150 | <150 | <150 | <150 | 150 | 15 |

| Sampling Date | | 10/18/2023 | 10/18/2023 | | | | |
|----------------------|-------|----------------|----------------|-----|-----|--|--|
| | UNITS | M26A- H2SO4 R2 | M26A- H2SO4 R3 | RDL | MDL | | |
| Sulfuric Acid Volume | ml | 407 | 452 | | | | |
| Hydrofluoric Acid | ug | <150 | <150 | 150 | 15 | | |

| | | | | | | | | | | | | | | | |
|-------------------------------|--------------------|------------------------|---------------------------|----------------------------------|------------------------------|------------------------|-----------------|---------------------|----------------------|--------------------------|----------------------|--|--|--|--|
| Client: | GCC | | Analysis Date: | 11/15/2023 | | | | | | | | | | | |
| Facility: | Pueblo | | Analysis Location: | Elmhurst | | | | | | | | | | | |
| Test Location: | Main Kiln Mill On | | Analyst: | JMG | | | | | | | | | | | |
| Project Number: | M234207 | | | | | | | | | | | | | | |
| Method: | 26A | | | | | | | | | | | | | | |
| Date Samples Received: | 11/3/2023 | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| Standard ppm HF | Area | Response Factor | Calculated Value | Slope of Regression Curve | | | | | | | | | | | |
| 1 | 0.2190 | 0.2190 | 0.95 | 0.2296 | | | | | | | | | | | |
| 2 | 0.4460 | 0.2230 | 1.94 | | | | | | | | | | | | |
| 5 | 1.1517 | 0.2303 | 5.02 | Response Factor Ave | | | | | | | | | | | |
| 8 | 1.8720 | 0.2340 | 8.15 | 0.2295 | | | | | | | | | | | |
| 10 | 2.4109 | 0.2411 | 10.50 | | | | | | | | | | | | |
| Lot Number | Ricca 8209004 | | | | | | | | | | | | | | |
| | R ² | | 0.9994 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| Sample Number | Sample Date | Sample ID | Sample Area | PPM F | PPM X Dilution Factor | Dilution Factor | Total ml | mg F in soln | mg HF in soln | mg HF in soln avg | ug HF in soln | | | | |
| 003 | 10/18/2023 | Test 1B H2SO4 Imp | 0.0112 | 0.0488 | 0.0488 | 1 | 475 | 0.0232 | 0.0244 | | | | | | |
| 003 | 10/18/2023 | Test 1B H2SO4 Imp | 0.0179 | 0.0780 | 0.0780 | 1 | 475 | 0.0370 | 0.0390 | 0.0317 | 31.70073069 | | | | |
| 003 | 10/18/2023 | Test 1B H2SO4 Imp | 0.0185 | 0.0806 | 0.0806 | 1 | 475 | 0.0383 | 0.0403 | | | | | | |
| 003 | 10/18/2023 | Test 1B H2SO4 Imp | 0.0186 | 0.0810 | 0.0810 | 1 | 475 | 0.0385 | 0.0405 | 0.0404 | 40.41570819 | | | | |
| 007 | 10/18/2023 | Test 2B H2SO4 Imp | 0.0342 | 0.1489 | 0.1489 | 1 | 407 | 0.0606 | 0.0638 | | | | | | |
| 007 | 10/18/2023 | Test 2B H2SO4 Imp | 0.0375 | 0.1633 | 0.1633 | 1 | 407 | 0.0665 | 0.0700 | 0.0669 | 66.92621109 | | | | |
| 011 | 10/18/2023 | Test 3B H2SO4 Imp | 0.0079 | 0.0344 | 0.0344 | 1 | 452 | 0.0156 | 0.0164 | | | | | | |
| 011 | 10/18/2023 | Test 3B H2SO4 Imp | 0.0075 | 0.0327 | 0.0327 | 1 | 452 | 0.0148 | 0.0155 | 0.0160 | 15.96400406 | | | | |
| Standard ppm F | Area | Difference | | | | | | | | | | | | | |
| 1 | 0.2059 | 3.18% | | | | | | | | | | | | | |
| 2 | 0.4244 | 2.54% | | | | | | | | | | | | | |
| 5 | 1.1246 | 1.20% | | | | | | | | | | | | | |
| 8 | 1.8850 | 0.34% | | | | | | | | | | | | | |
| 10 | 2.3985 | 0.26% | | | | | | | | | | | | | |

Main Kiln Mill On

| | |
|---|--|
| Client: GCC Facility: Pueblo Test Location: Main Kiln Mill On Project Number: M234207 Method: 26A Date Samples Received: 11/3/2023 | Analysis Date: 11/15/2023 Analysis Location: Elmhurst Analyst: JMG |
|---|--|

Train A

| Sampling Date | | 10/18/2023 | 10/18/2023 | 10/18/2023 | 10/18/2023 | | |
|-------------------------|-------|---------------|-----------------|--------------|------------------|-----|-----|
| | UNITS | M26A DI Blank | M26A NaOH Blank | M26A NaOH-R1 | M26A NaOH-R1 Dup | RDL | MDL |
| Sodium Hydroxide Volume | ml | 215 | 254 | 312 | 312 | | |
| Chlorine | ug | <150 | <150 | <150 | <150 | 150 | 15 |

| Sampling Date | | 10/18/2023 | 10/18/2023 | 10/18/2023 | | | |
|-------------------------|-------|---------------|---------------|---------------|--|-----|-----|
| | UNITS | M26A- NaOH R2 | M26A- NaOH R3 | Train A Blank | | RDL | MDL |
| Sodium Hydroxide Volume | ml | 323 | 299 | 215 | | | |
| Chlorine | ug | <150 | <150 | <150 | | 150 | 15 |

Train B

| Sampling Date | | 10/18/2023 | 10/18/2023 | 10/18/2023 | 10/18/2023 | | |
|-------------------------|-------|---------------|-----------------|--------------|------------------|-----|-----|
| | UNITS | M26A DI Blank | M26A NaOH Blank | M26A NaOH-R1 | M26A NaOH-R1 Dup | RDL | MDL |
| Sodium Hydroxide Volume | ml | 215 | 254 | 300 | 300 | | |
| Chlorine | ug | <150 | <150 | <150 | <150 | 150 | 15 |

| Sampling Date | | 10/18/2023 | 10/18/2023 | | | | |
|-------------------------|-------|---------------|---------------|--|--|-----|-----|
| | UNITS | M26A- NaOH R2 | M26A- NaOH R3 | | | RDL | MDL |
| Sodium Hydroxide Volume | ml | 329 | 288 | | | | |
| Chlorine | ug | <150 | <150 | | | 150 | 15 |

| | | | | | | | | | | | | | |
|-------------------------------|----------------------|---------------------------|-------------------------|----------------------------------|------------------------------|------------------------|-----------------|----------------------|-----------------------|-----------------------|--|--|--|
| Client: | GCC | Analysis Date: | 11/15/2023 | | | | | | | | | | |
| Facility: | Pueblo | Analysis Location: | Elmhurst Lab | | | | | | | | | | |
| Test Location: | Main Kiln Mill On | Analyst: | JMG | | | | | | | | | | |
| Project Number: | M234207 | | | | | | | | | | | | |
| Method: | 26A | | | | | | | | | | | | |
| Date Samples Received: | 11/3/2023 | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| Standard ppm Cl | Area | Response Factor | Calculated Value | Slope of Regression Curve | | | | | | | | | |
| 1 | 0.1523 | 0.1523 | 1.01 | 0.1513 | | | | | | | | | |
| 2 | 0.2939 | 0.1470 | 1.94 | | | | | | | | | | |
| 5 | 0.7660 | 0.1532 | 5.06 | Response Factor Ave | | | | | | | | | |
| 8 | 1.2141 | 0.1518 | 8.03 | 0.1512 | | | | | | | | | |
| 10 | 1.5201 | 0.1520 | 10.05 | | | | | | | | | | |
| Lot Number | Ricca 8209004 | | | | | | | | | | | | |
| | R² | 0.9999 | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| Sample Number | Sample Date | Sample ID | Sample Area | PPM Cl | PPM X Dilution Factor | Dilution Factor | Total ml | mg Cl in soln | ug Cl2 in soln | ug Cl2 in soln | | | |
| | 10/18/2023 | DI Reagent Blank | 0.0027 | 0.0179 | 0.0179 | 1 | 215 | 0.0038 | | | | | |
| | 10/18/2023 | DI Reagent Blank | 0.0017 | 0.0112 | 0.0112 | 1 | 215 | 0.0024 | 0.0031 | 3.127100777 | | | |
| | 10/18/2023 | NaOH Reagent Blank | 0.0470 | 0.3107 | 0.3107 | 1 | 254 | 0.0789 | | | | | |
| | 10/18/2023 | NaOH Reagent Blank | 0.0335 | 0.2215 | 0.2215 | 1 | 254 | 0.0563 | 0.0676 | 67.58967187 | | | |
| 002 | 10/18/2023 | Test 1A NaOH Imp | 0.0166 | 0.1097 | 0.1097 | 1 | 312 | 0.0342 | | | | | |
| 002 | 10/18/2023 | Test 1A NaOH Imp | 0.0175 | 0.1157 | 0.1157 | 1 | 312 | 0.0361 | 0.0352 | 35.16897525 | | | |
| 002 | 10/18/2023 | Test 1A NaOH Imp | 0.0111 | 0.0734 | 0.0734 | 1 | 312 | 0.0229 | | | | | |
| 002 | 10/18/2023 | Test 1A NaOH Imp | 0.0116 | 0.0767 | 0.0767 | 1 | 312 | 0.0239 | 0.0234 | 23.41160523 | | | |
| 006 | 10/18/2023 | Test 2A NaOH Imp | 0.0014 | 0.0093 | 0.0093 | 1 | 323 | 0.0030 | | | | | |
| 006 | 10/18/2023 | Test 2A NaOH Imp | 0.0031 | 0.0205 | 0.0205 | 1 | 323 | 0.0066 | 0.0048 | 4.804694481 | | | |
| 010 | 10/18/2023 | Test 3A NaOH Imp | 0.0122 | 0.0807 | 0.0807 | 1 | 299 | 0.0241 | | | | | |
| 010 | 10/18/2023 | Test 3A NaOH Imp | 0.0096 | 0.0635 | 0.0635 | 1 | 299 | 0.0190 | 0.0215 | 21.54658381 | | | |
| | 10/18/2023 | Train Blank | 0.0140 | 0.0926 | 0.0926 | 1 | 215 | 0.0199 | | | | | |
| | 10/18/2023 | Train Blank | 0.0152 | 0.1005 | 0.1005 | 1 | 215 | 0.0216 | 0.0208 | 20.75257788 | | | |
| | | | | | Expected Value | % Difference | | | | | | | |
| | | Run 1 H2SO4 Spike W/ 2ppm | 0.1858 | 1.2284 | 1.0279 | | | | | | | | |
| | | Run 1 H2SO4 Spike W/ 2ppm | 0.1683 | 1.1127 | 1.0279 | 13.88% | | | | | | | |
| CCV ppm Cl | Area | PPM Cl | | | | | | | | | | | |
| 5 ppm ICV | 0.7339 | 4.8520 | | | | | | | | | | | |
| 5 ppm CCV | 0.761 | 5.0311 | | | | | | | | | | | |
| 5 ppm CCV | | 0.0000 | | | | | | | | | | | |
| 5 ppm CCV | | 0.0000 | | | | | | | | | | | |
| Standard ppm Cl | Area | Difference | | | | | | | | | | | |
| 1 | 0.1575 | 1.65% | | | | | | | | | | | |
| 2 | 0.2902 | 0.64% | | | | | | | | | | | |
| 5 | 0.7781 | 0.78% | | | | | | | | | | | |
| 8 | 1.2309 | 0.68% | | | | | | | | | | | |
| 10 | 1.5781 | 1.84% | | | | | | | | | | | |

Main Kiln Mill Off

| | |
|--|--|
| Client: GCC Facility: Pueblo Test Location: Main Kiln Mill Off Project Number: M234207 Method: 26A Date Samples Received: 11/3/2023 | Analysis Date: 11/15/2023 Analysis Location: Elmhurst Analyst: JMG |
|--|--|

Train A

| Sampling Date | | 10/18/2023 | 10/18/2023 | 10/17/2023 | 10/17/2023 | | |
|----------------------|-------|---------------|------------------|---------------|-------------------|-----|-----|
| | UNITS | M26A DI Blank | M26A H2SO4 Blank | M26A H2SO4-R1 | M26A H2SO4-R1 Dup | RDL | MDL |
| Sulfuric Acid Volume | ml | 215 | 254 | 440 | 440 | | |
| Hydrofluoric Acid | ug | <150 | <150 | <150 | <150 | 150 | 15 |

| Sampling Date | | 10/17/2023 | 10/17/2023 | 10/18/2023 | | |
|----------------------|-------|----------------|----------------|-------------------------|-----|-----|
| | UNITS | M26A- H2SO4 R2 | M26A- H2SO4 R3 | M26A- H2SO4 Train Blank | RDL | MDL |
| Sulfuric Acid Volume | ml | 425 | 382 | 231 | | |
| Hydrofluoric Acid | ug | <150 | <150 | <150 | 150 | 15 |

Train B

| Sampling Date | | 10/18/2023 | 10/18/2023 | 10/18/2023 | 10/17/2023 | | |
|----------------------|-------|---------------|------------------|---------------|-------------------|-----|-----|
| | UNITS | M26A DI Blank | M26A H2SO4 Blank | M26A H2SO4-R1 | M26A H2SO4-R1 Dup | RDL | MDL |
| Sulfuric Acid Volume | ml | 215 | 254 | 449 | 449 | | |
| Hydrofluoric Acid | ug | <150 | <150 | <150 | <150 | 150 | 15 |

| Sampling Date | | 10/17/2023 | 10/17/2023 | | | |
|----------------------|-------|----------------|----------------|-----|-----|--|
| | UNITS | M26A- H2SO4 R2 | M26A- H2SO4 R3 | RDL | MDL | |
| Sulfuric Acid Volume | ml | 430 | 453 | | | |
| Hydrofluoric Acid | ug | <150 | <150 | 150 | 15 | |

| | | | | | | | | | | | | | | |
|------------------------|--------------------|------------------------|-------------------------|----------------------------------|------------------------------|------------------------|-----------------|---------------------|----------------------|--------------------------|----------------------|--|--|--|
| Client: | GCC | Analysis Date: | 11/15/2023 | | | | | | | | | | | |
| Facility: | Pueblo | Analysis Location: | Elmhurst | | | | | | | | | | | |
| Test Location: | Main Kiln Mill Off | Analyst: | JMG | | | | | | | | | | | |
| Project Number: | M234207 | | | | | | | | | | | | | |
| Method: | 26A | | | | | | | | | | | | | |
| Date Samples Received: | 11/3/2023 | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| Standard ppm HF | Area | Response Factor | Calculated Value | Slope of Regression Curve | | | | | | | | | | |
| 1 | 0.2190 | 0.2190 | 0.95 | 0.2296 | | | | | | | | | | |
| 2 | 0.4460 | 0.2230 | 1.94 | | | | | | | | | | | |
| 5 | 1.1517 | 0.2303 | 5.02 | Response Factor Ave | | | | | | | | | | |
| 8 | 1.8720 | 0.2340 | 8.15 | 0.2295 | | | | | | | | | | |
| 10 | 2.4109 | 0.2411 | 10.50 | | | | | | | | | | | |
| Lot Number | Ricca 8209004 | | | | | | | | | | | | | |
| | R ² | 0.9994 | | | | | | | | | | | | |
| Sample Number | Sample Date | Sample ID | Sample Area | PPM F | PPM X Dilution Factor | Dilution Factor | Total ml | mg F in soln | mg HF in soln | mg HF in soln avg | ug HF in soln | | | |
| 015 | 10/18/2023 | DI Reagent Blank | 0.0065 | 0.0283 | 0.0283 | 1 | 215 | 0.0061 | 0.0064 | | | | | |
| 015 | 10/18/2023 | DI Reagent Blank | 0.0057 | 0.0248 | 0.0248 | 1 | 215 | 0.0053 | 0.0056 | 0.0060 | 6.015627896 | | | |
| | 10/18/2023 | H2SO4 Reagent Blank | 0.0392 | 0.1707 | 0.1707 | 1 | 254 | 0.0434 | 0.0457 | | | | | |
| | 10/18/2023 | H2SO4 Reagent Blank | 0.0388 | 0.1690 | 0.1690 | 1 | 254 | 0.0429 | 0.0452 | 0.0454 | 45.43714063 | | | |
| | 10/17/2023 | Test 1B H2SO4 Imp | 0.0120 | 0.0523 | 0.0523 | 1 | 449 | 0.0235 | 0.0247 | | | | | |
| 003 | 10/17/2023 | Test 1B H2SO4 Imp | 0.0118 | 0.0514 | 0.0514 | 1 | 449 | 0.0231 | 0.0243 | 0.0245 | 24.5078928 | | | |
| 003 | 10/17/2023 | Test 1B H2SO4 Imp | 0.0138 | 0.0601 | 0.0601 | 1 | 449 | 0.0270 | 0.0284 | | | | | |
| 003 | 10/17/2023 | Test 1B H2SO4 Imp | 0.0122 | 0.0531 | 0.0531 | 1 | 449 | 0.0239 | 0.0251 | 0.0268 | 26.77332827 | | | |
| 007 | 10/17/2023 | Test 2B H2SO4 Imp | 0.0221 | 0.0962 | 0.0962 | 1 | 430 | 0.0414 | 0.0436 | | | | | |
| 007 | 10/17/2023 | Test 2B H2SO4 Imp | 0.0227 | 0.0989 | 0.0989 | 1 | 430 | 0.0425 | 0.0448 | 0.0442 | 44.18034914 | | | |
| 011 | 10/17/2023 | Test 3B H2SO4 Imp | 0.0179 | 0.0780 | 0.0780 | 1 | 453 | 0.0353 | 0.0372 | | | | | |
| 011 | 10/17/2023 | Test 3B H2SO4 Imp | 0.0145 | 0.0631 | 0.0631 | 1 | 453 | 0.0286 | 0.0301 | 0.0337 | 33.6609126 | | | |
| | 10/17/2023 | Train Blank B | 0.0169 | 0.0736 | 0.0736 | 1 | 222 | 0.0163 | 0.0172 | | | | | |
| | 10/17/2023 | Train Blank B | 0.0181 | 0.0788 | 0.0788 | 1 | 222 | 0.0175 | 0.0184 | 0.0178 | 17.81983559 | | | |
| Standard ppm F | Area | Difference | | | | | | | | | | | | |
| 1 | 0.2059 | 3.18% | | | | | | | | | | | | |
| 2 | 0.4244 | 2.54% | | | | | | | | | | | | |
| 5 | 1.1246 | 1.20% | | | | | | | | | | | | |
| 8 | 1.8850 | 0.34% | | | | | | | | | | | | |
| 10 | 2.3985 | 0.26% | | | | | | | | | | | | |

Main Kiln Mill Off

| | |
|--|--|
| Client: GCC Facility: Pueblo Test Location: Main Kiln Mill Off Project Number: M234207 Method: 26A Date Samples Received: 11/3/2023 | Analysis Date: 11/15/2023 Analysis Location: Elmhurst Analyst: JMG |
|--|--|

Train A

| Sampling Date | | 10/18/2023 | 10/18/2023 | 10/17/2023 | 10/17/2023 | | |
|-------------------------|-------|---------------|-----------------|--------------|------------------|-----|-----|
| | UNITS | M26A DI Blank | M26A NaOH Blank | M26A NaOH-R1 | M26A NaOH-R1 Dup | RDL | MDL |
| Sodium Hydroxide Volume | ml | 215 | 254 | 315 | 315 | | |
| Chlorine | ug | <150 | <150 | <150 | <150 | 150 | 15 |

| Sampling Date | | 10/17/2023 | 10/17/2023 | 10/18/2023 | | |
|-------------------------|-------|---------------|---------------|---------------|-----|-----|
| | UNITS | M26A- NaOH R2 | M26A- NaOH R3 | Train A Blank | RDL | MDL |
| Sodium Hydroxide Volume | ml | 318 | 299 | 215 | | |
| Chlorine | ug | <150 | <150 | <150 | 150 | 15 |

Train B

| Sampling Date | | 10/17/2023 | 10/18/2023 | 10/17/2023 | 10/17/2023 | | |
|-------------------------|-------|---------------|-----------------|--------------|------------------|-----|-----|
| | UNITS | M26A DI Blank | M26A NaOH Blank | M26A NaOH-R1 | M26A NaOH-R1 Dup | RDL | MDL |
| Sodium Hydroxide Volume | ml | 215 | 254 | 330 | 330 | | |
| Chlorine | ug | <150 | <150 | <150 | <150 | 150 | 15 |

| Sampling Date | | 10/17/2023 | 10/17/2023 | | | | |
|-------------------------|-------|---------------|---------------|-----|-----|--|--|
| | UNITS | M26A- NaOH R2 | M26A- NaOH R3 | RDL | MDL | | |
| Sodium Hydroxide Volume | ml | 292 | 328 | | | | |
| Chlorine | ug | <150 | <150 | 150 | 15 | | |

Appendix F - Reference Method Test Data

Client: GCC Rio Grande, Inc.
Facility: Pueblo Plant
Test Location: Main Kiln Stack
Project #: M234207
Test Method: 26A
Test Engineer: DCS
Test Technician: SWK

| | <u>Run 1A</u> | <u>Run 2A</u> | <u>Run 3A</u> |
|---|---------------|---------------|---------------|
| Temp ID: | CM53 | CM53 | CM53 |
| Meter ID: | CM53 | CM53 | CM53 |
| Pitot ID: | S8-031A | S8-031A | S8-031A |
| Nozzle Diameter (Inches): | 0.281 | 0.281 | 0.281 |
| Meter Calibration Date: | 9/6/2023 | 9/6/2023 | 9/6/2023 |
| Meter Calibration Factor (Y): | 0.994 | 0.994 | 0.994 |
| Meter Orifice Setting (Delta H): | 1.775 | 1.775 | 1.775 |
| Nozzle Kit ID Number and Material: | #32 Glass | #32 Glass | #32 Glass |
| Pitot Tube Coefficient: | | 0.820 | |
| Probe Length (Feet): | | 6.0 | |
| Probe Liner Material: | | Glass | |
| Sample Plane: | | Horizontal | |
| Port Length (Inches): | | 9.50 | |
| Port Size (Diameter, Inches): | | 6.00 | |
| Port Type: | | Flange | |
| Duct Shape: | | Circular | |
| Diameter (Feet): | | 10.25 | |
| Duct Area (Square Feet): | | 82.516 | |
| Upstream Diameters: | | 4.9 | |
| Downstream Diameters: | | 24.4 | |
| Number of Ports Sampled: | | 4 | |
| Number of Points per Port: | | 3 | |
| Minutes per Point: | | 5.0 | |
| Minutes per Reading: | | 5.0 | |
| Total Number of Traverse Points: | | 12 | |
| Test Length (Minutes): | | 60 | |
| Train Type: | | Anderson Box | |
| Source Condition: | | Mill On | |
| Diluent Model/Serial Number: | | CAI700 | |
| Moisture Balance ID: | | LV3 | |
| # of Runs | | 3 | |

Run 1A - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill On

Date: 10/18/23
 Start Time: 8:40
 End Time: 9:46

DRY GAS METER CONDITIONS

ΔH: 2.34 in. H₂O
 Meter Temperature, Tm: 62.8 °F
 Sqrt ΔP: 0.790 in. H₂O
 Stack Temperature, Ts: 215.3 °F
 Meter Volume, Vm: 55.293 ft³
 Meter Volume, Vmstd: 46.481 dscf
 Meter Volume, Vwstd: 7.621 wscf
 Isokinetic Variance: 101.1 %
 Test Length: 60.00 in mins.
 Nozzle Diameter: 0.281 in inches
 Barometric Pressure: 24.88 in Hg

STACK CONDITIONS

Static Pressure 0.75 in. H₂O
 Flue Pressure (Ps): 24.94 in. Hg. abs.
 Carbon Dioxide: 19.40 %
 Oxygen: 9.70 %
 Nitrogen: 70.90 %
 Gas Weight dry, Md: 31.492 lb/lb mole
 Gas Weight wet, Ms: 29.592 lb/lb mole
 Excess Air: --- %
 Gas Velocity, Vs: 53.009 fps
 Volumetric Flow: 262.445 acfm
 Volumetric Flow: 146,915 dscfm
 Volumetric Flow: 171,002 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3547.1 ml Silica Initial Wt. 832.7 grams
 Final Impinger Content: 3662.5 ml Silica Final Wt. 879.1 grams
 Impinger Difference: 115.4 ml Silica Difference: 46.4 grams
 Total Water Gain: 161.8 Moisture, Bws: 0.141

| Port- Point No. | Clock Time | Velocity | Orifice | Actual | Stack | Meter Temp | | Probe | Filter | Impinger |
|--------------------|---------------|---------------------------------|----------------------------|-------------------------------|------------|-------------|--------------|------------|-----------------|-----------------|
| | | Head Δp in. H ₂ O | ΔH in. H ₂ O | Meter Vol. ft ³ | Temp °F | Inlet °F | Outlet °F | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1 | 8:40:00 | 0.71 | 2.80 | 290.780 | 239 | 71 | 57 | 263 | 273 | 53 |
| 1-2 | 8:45:00 | 0.67 | 2.40 | 295.620 | 233 | 70 | 57 | 269 | 270 | 53 |
| 1-3 | 8:50:00 | 0.49 | 1.80 | 300.260 | 230 | 69 | 58 | 270 | 268 | 53 |
| | 8:55:00 | | | 304.515 | | | | | | |
| 2-1 | 8:57:00 | 0.69 | 2.50 | 304.515 | 221 | 67 | 58 | 270 | 270 | 53 |
| 2-2 | 9:02:00 | 0.64 | 2.40 | 309.350 | 217 | 67 | 58 | 267 | 268 | 53 |
| 2-3 | 9:07:00 | 0.55 | 2.00 | 314.050 | 215 | 67 | 58 | 265 | 265 | 53 |
| | 9:12:00 | | | 318.524 | | | | | | |
| 3-1 | 9:14:00 | 0.70 | 2.60 | 318.524 | 210 | 66 | 58 | 265 | 265 | 53 |
| 3-2 | 9:19:00 | 0.63 | 2.40 | 323.060 | 208 | 65 | 59 | 264 | 266 | 53 |
| 3-3 | 9:24:00 | 0.56 | 2.10 | 328.030 | 206 | 65 | 61 | 264 | 268 | 53 |
| | 9:29:00 | | | 332.682 | | | | | | |
| 4-1 | 9:31:00 | 0.69 | 2.60 | 332.682 | 203 | 65 | 60 | 266 | 261 | 53 |
| 4-2 | 9:36:00 | 0.63 | 2.40 | 337.110 | 201 | 64 | 60 | 265 | 260 | 53 |
| 4-3 | 9:41:00 | 0.56 | 2.10 | 341.620 | 201 | 65 | 61 | 267 | 264 | 53 |
| | 9:46:00 | | | 346.073 | | | | | | |

Total 1:00:00 55.293 66.8 58.8
 Average 2.34 215.3 62.8
 Min 1.80 201.0 57.0
 Max 2.80 239.0 71.0

Impinger Weight Sheet - Run 1A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/18/2023
 Test Method: 26A
 Weighed/Measured By: WAP
 Balance ID: LV3

Scale Calibration Check Date: 10/18/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250 | <u>250.0</u> |
| 500 | <u>500.0</u> |
| 750 | <u>750.0</u> |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|----------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 823.5 | 740.8 | 82.7 |
| 0.1N H2SO4 | 691.2 | 682.8 | 8.4 |
| Empty | 652.0 | 642.4 | 9.6 |
| 0.1N NaOH | 746.7 | 782.3 | -35.6 |
| 0.1N NaOH | 749.1 | 698.8 | 50.3 |
| Silica Gel | 879.1 | 832.7 | 46.4 |

| | | |
|---------------------------------------|---|------------------------------------|
| <u>3,662.5</u> Liquid Final | <u>3,547.1</u> Liquid Initial | <u>115.4</u> Liquid Gain |
| <u>879.1</u> Silica Final | <u>832.7</u> Silica Initial | <u>46.4</u> Silica Gain |

Run 2A - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill On

Date: 10/18/23
 Start Time: 9:40
 End Time: 12:02

DRY GAS METER CONDITIONS

STACK CONDITIONS

| | | | | | |
|------------------------|--------|----------------------|---------------------|---------|----------------------|
| ΔH: | 2.47 | In. H ₂ O | Static Pressure | 0.75 | in. H ₂ O |
| Meter Temperature, Tm: | 64.9 | °F | Flue Pressure (Ps): | 24.94 | in. Hg. abs. |
| Sqrt ΔP: | 0.801 | In. H ₂ O | Carbon Dioxide: | 19.90 | % |
| Stack Temperature, Ts: | 206.8 | °F | Oxygen: | 9.50 | % |
| Meter Volume, Vm: | 56.477 | ft ³ | Nitrogen: | 70.6 | % |
| Meter Volume, Vmstd: | 47.302 | dscf | Gas Weight dry, Md: | 31.564 | lb/lb mole |
| Meter Volume, Vwstd: | 6.999 | wscf | Gas Weight wet, Ms: | 29.816 | lb/lb mole |
| Isokinetic Variance: | 99.8 | %I | Excess Air: | --- | % |
| Test Length: | 60.00 | in mins. | Gas Velocity, Vs: | 53.197 | fps |
| Nozzle Diameter: | 0.281 | in inches | Volumetric Flow: | 263,375 | acfm |
| Barometric Pressure: | 24.88 | in Hg | Volumetric Flow: | 151,414 | dscfm |
| | | | Volumetric Flow: | 173,818 | scfm |

MOISTURE DETERMINATION

| | | | | | |
|---------------------------|--------|----|--------------------|-------|-------|
| Initial Impinger Content: | 3551.1 | ml | Silica Initial Wt. | 833.0 | grams |
| Final Impinger Content: | 3688.2 | ml | Silica Final Wt. | 844.5 | grams |
| Impinger Difference: | 137.1 | ml | Silica Difference: | 11.5 | grams |
| Total Water Gain: | 148.6 | | Moisture, Bws: | 0.129 | |

| Port- Point No. | Clock Time | Velocity | Orifice | Actual | Stack | Meter Temp | | Probe | Filter | Impinger |
|--------------------|---------------|---------------------------------|----------------------------|-------------------------------|------------|-------------|--------------|------------|-----------------|-----------------|
| | | Head Δp in. H ₂ O | ΔH in. H ₂ O | Meter Vol. ft ³ | Temp °F | Inlet °F | Outlet °F | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1 | 10:10:00 | 0.70 | 2.70 | 346.419 | 197 | 64 | 61 | 263 | 265 | 54 |
| 1-2 | 10:15:00 | 0.67 | 2.60 | 351.450 | 196 | 65 | 62 | 263 | 263 | 54 |
| 1-3 | 10:20:00 | 0.50 | 2.40 | 356.210 | 196 | 66 | 61 | 266 | 264 | 54 |
| | 10:25:00 | | | 361.051 | | | | | | |
| 2-1 | 10:27:00 | 0.71 | 2.70 | 361.051 | 195 | 67 | 62 | 265 | 267 | 54 |
| 2-2 | 10:32:00 | 0.66 | 2.50 | 366.090 | 195 | 67 | 63 | 265 | 270 | 54 |
| 2-3 | 10:37:00 | 0.59 | 2.20 | 370.780 | 195 | 67 | 62 | 264 | 269 | 54 |
| | 10:42:00 | | | 375.679 | | | | | | |
| 3-1 | 10:44:00 | 0.70 | 2.70 | 375.679 | 194 | 67 | 62 | 270 | 267 | 54 |
| 3-2 | 10:49:00 | 0.68 | 2.60 | 380.310 | 194 | 67 | 63 | 268 | 269 | 54 |
| 3-3 | 11:40:00 | 0.60 | 2.30 | 384.645 | 232 | 67 | 66 | 269 | 269 | 54 |
| | 11:45:00 | | | 389.134 | | | | | | |
| 4-1 | 11:47:00 | 0.74 | 2.70 | 389.134 | 232 | 66 | 66 | 265 | 265 | 54 |
| 4-2 | 11:52:00 | 0.65 | 2.30 | 393.560 | 229 | 66 | 66 | 265 | 267 | 54 |
| 4-3 | 11:57:00 | 0.53 | 1.90 | 398.620 | 226 | 67 | 67 | 265 | 264 | 54 |
| | 12:02:00 | | | 402.896 | | | | | | |

| | | | | | | | | | | |
|---------|---------|--|------|--------|-------|------|------|--|--|--|
| Total | 1:46:00 | | | 56.477 | | 66.3 | 63.4 | | | |
| Average | | | 2.47 | | 206.8 | 64.9 | | | | |
| Min | | | 1.90 | | 194.0 | 61.0 | | | | |
| Max | | | 2.70 | | 232.0 | 67.0 | | | | |

Impinger Weight Sheet - Run 2A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/18/2023
 Test Method: 26A
 Weighed/Measured By: WAP
 Balance ID: LV3

Scale Calibration Check Date: 10/18/2023
 Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250 | 250.0 |
| 500 | 500.0 |
| 750 | 750.0 |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 834.3 | 741.5 | 92.8 |
| 0.1N H2SO4 | 718.3 | 684.4 | 33.9 |
| Empty | 649.3 | 642.7 | 6.6 |
| 0.1N NaOH | 782.6 | 781.0 | 1.6 |
| 0.1N NaOH | 703.7 | 701.5 | 2.2 |
| Silica Gel | 844.5 | 833.0 | 11.5 |

| | | |
|---------------------------------------|---|------------------------------------|
| <u>3,688.2</u> Liquid Final | <u>3,551.1</u> Liquid Initial | <u>137.1</u> Liquid Gain |
| <u>844.5</u> Silica Final | <u>833.0</u> Silica Initial | <u>11.5</u> Silica Gain |

Run 3A - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill On

Date: 10/18/23
 Start Time: 12:25
 End Time: 13:31

DRY GAS METER CONDITIONS

| | | |
|------------------------|--------|----------------------|
| ΔH: | 2.33 | In. H ₂ O |
| Meter Temperature, Tm: | 70.3 | °F |
| Sqrt ΔP: | 0.795 | In. H ₂ O |
| Stack Temperature, Ts: | 214.3 | °F |
| Meter Volume, Vm: | 54.609 | ft ³ |
| Meter Volume, Vmstd: | 45.248 | dscf |
| Meter Volume, Vwstd: | 7.456 | wscf |
| Isokinetic Variance: | 98.0 | %I |
| Test Length: | 60.00 | in mins. |
| Nozzle Diameter: | 0.281 | in inches |
| Barometric Pressure: | 24.88 | in Hg |

STACK CONDITIONS

| | | |
|---------------------|---------|----------------------|
| Static Pressure | 0.75 | in. H ₂ O |
| Flue Pressure (Ps): | 24.94 | in. Hg. abs. |
| Carbon Dioxide: | 20.60 | % |
| Oxygen: | 9.10 | % |
| Nitrogen: | 70.3 | % |
| Gas Weight dry, Md: | 31.660 | lb/lb mole |
| Gas Weight wet, Ms: | 29.728 | lb/lb mole |
| Excess Air: | 96.203 | % |
| Gas Velocity, Vs: | 53.178 | fps |
| Volumetric Flow: | 263,281 | acfm |
| Volumetric Flow: | 147,497 | dscfm |
| Volumetric Flow: | 171,802 | scfm |

MOISTURE DETERMINATION

| | | | | | |
|---------------------------|--------|----|--------------------|-------|-------|
| Initial Impinger Content: | 3662.8 | ml | Silica Initial Wt. | 863.6 | grams |
| Final Impinger Content: | 3804.3 | ml | Silica Final Wt. | 880.4 | grams |
| Impinger Difference: | 141.5 | ml | Silica Difference: | 16.8 | grams |
| Total Water Gain: | 158.3 | | Moisture, Bws: | 0.141 | |

| Port- Point No. | Clock Time | Velocity Head Δp in. H ₂ O | Orifice ΔH in. H ₂ O | Actual Meter Vol. ft ³ | Stack Temp °F | Meter Temp Inlet °F | Meter Temp Outlet °F | Probe Temp °F | Filter Exit Temp °F | Impinger Exit Temp °F |
|--------------------|---------------|---|---------------------------------------|---|---------------------|---------------------------|----------------------------|---------------------|---------------------------|-----------------------------|
| 1-1 | 12:25:00 | 0.72 | 2.60 | 402.932 | 217 | 69 | 67 | 260 | 267 | 55 |
| 1-2 | 12:30:00 | 0.67 | 2.40 | 407.550 | 217 | 69 | 69 | 266 | 269 | 55 |
| 1-3 | 12:35:00 | 0.51 | 1.90 | 411.640 | 216 | 69 | 69 | 268 | 269 | 55 |
| | 12:40:00 | | | 416.145 | | | | | | |
| 2-1 | 12:42:00 | 0.71 | 2.60 | 416.145 | 215 | 70 | 68 | 265 | 266 | 55 |
| 2-2 | 12:47:00 | 0.67 | 2.50 | 420.740 | 215 | 70 | 68 | 265 | 265 | 56 |
| 2-3 | 12:52:00 | 0.54 | 2.00 | 425.830 | 214 | 71 | 70 | 265 | 268 | 56 |
| | 12:57:00 | | | 430.049 | | | | | | |
| 3-1 | 12:59:00 | 0.70 | 2.60 | 430.049 | 214 | 72 | 68 | 264 | 267 | 56 |
| 3-2 | 13:04:00 | 0.66 | 2.40 | 434.810 | 213 | 72 | 71 | 265 | 267 | 56 |
| 3-3 | 13:09:00 | 0.55 | 2.00 | 439.420 | 213 | 73 | 72 | 266 | 267 | 57 |
| | 13:14:00 | | | 443.821 | | | | | | |
| 4-1 | 13:16:00 | 0.71 | 2.60 | 443.821 | 213 | 73 | 70 | 265 | 267 | 57 |
| 4-2 | 13:21:00 | 0.66 | 2.40 | 448.680 | 213 | 73 | 71 | 265 | 267 | 58 |
| 4-3 | 13:26:00 | 0.52 | 1.90 | 453.210 | 212 | 74 | 70 | 265 | 269 | 58 |
| | 13:31:00 | | | 457.541 | | | | | | |

| | | | | | | | | | | |
|---------|---------|--|------|--------|-------|------|------|--|--|--|
| Total | 1:00:00 | | | 54.609 | | 71.3 | 69.4 | | | |
| Average | | | 2.33 | | 214.3 | 70.3 | | | | |
| Min | | | 1.90 | | 212.0 | 67.0 | | | | |
| Max | | | 2.60 | | 217.0 | 74.0 | | | | |

Impinger Weight Sheet - Run 3A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/18/2023
 Test Method: 26A
 Weighed/Measured By: WAP
 Balance ID: LV3

Scale Calibration Check Date: 10/18/2023
 Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250 | 250.0 |
| 500 | 500.0 |
| 750 | 750.0 |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 864.6 | 758.1 | 106.5 |
| 0.1N H2SO4 | 820.0 | 794.5 | 25.5 |
| Empty | 640.6 | 633.6 | 7.0 |
| 0.1N NaOH | 734.9 | 733.1 | 1.8 |
| 0.1N NaOH | 744.2 | 743.5 | 0.7 |
| Silica Gel | 880.4 | 863.6 | 16.8 |

| | | |
|---------------------|-----------------------|--------------------|
| 3,804.3 | 3,662.8 | 141.5 |
| Liquid Final | Liquid Initial | Liquid Gain |
| 880.4 | 863.6 | 16.8 |
| Silica Final | Silica Initial | Silica Gain |

Client: GCC Rio Grande, Inc.
Facility: Pueblo Plant
Test Location: Main Kiln Stack
Project #: M234207
Test Method: 26A
Test Engineer: SWK
Test Technician: DCS

| | <u>Run 1</u> | <u>Run 2</u> | <u>Run 3</u> |
|---|--------------|--------------|--------------|
| Meter ID: | CM4 | CM4 | CM4 |
| Pitot ID: | S8-032A | S8-032A | S8-032A |
| Nozzle Diameter (Inches): | 0.282 | 0.282 | 0.282 |
| Meter Calibration Date: | 10/5/2023 | 10/5/2023 | 10/5/2023 |
| Meter Calibration Factor (Y): | 0.990 | 0.990 | 0.990 |
| Meter Orifice Setting (Delta H): | 1.889 | 1.889 | 1.889 |
| Nozzle Kit ID Number and Material: | 21 Glass | 21 Glass | 21 Glass |
| Pitot Tube Coefficient: | | 0.822 | |
| Probe Length (Feet): | | 4.0 | |
| Probe Liner Material: | | Glass | |
| Sample Plane: | | Horizontal | |
| Port Length (Inches): | | 9.50 | |
| Port Size (Diameter, Inches): | | 6.00 | |
| Port Type: | | Flange | |
| Duct Shape: | | Circular | |
| Diameter (Feet): | | 10.25 | |
| Duct Area (Square Feet): | | 82.516 | |
| Upstream Diameters: | | 4.9 | |
| Downstream Diameters: | | 24.4 | |
| Number of Ports Sampled: | | 4 | |
| Number of Points per Port: | | 3 | |
| Minutes per Point: | | 5.0 | |
| Minutes per Reading: | | 5.0 | |
| Total Number of Traverse Points: | | 12 | |
| Test Length (Minutes): | | 60 | |
| Train Type: | | Anderson Box | |
| Source Condition: | | Mill On | |
| Diluent Model/Serial Number: | | CAI700 | |
| Moisture Balance ID: | | LV3 | |
| # of Runs | | 3 | |

Run 1 - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill On

Date: 10/18/23
 Start Time: 8:40
 End Time: 9:46

DRY GAS METER CONDITIONS

ΔH: 2.48 in. H₂O
 Meter Temperature, Tm: 66.4 °F
 Sqrt ΔP: 0.779 in. H₂O
 Stack Temperature, Ts: 210.2 °F
 Meter Volume, Vm: 56.794 ft³
 Meter Volume, Vmstd: 47.238 dscf
 Meter Volume, Vwstd: 7.418 wscf
 Isokinetic Variance: 102.3 %
 Test Length: 60.00 in mins.
 Nozzle Diameter: 0.282 in inches
 Barometric Pressure: 24.88 in Hg

STACK CONDITIONS

Static Pressure 0.75 in. H₂O
 Flue Pressure (Ps): 24.94 in. Hg. abs.
 Carbon Dioxide: 19.40 %
 Oxygen: 9.70 %
 Nitrogen: 70.90 %
 Gas Weight dry, Md: 31.492 lb/lb mole
 Gas Weight wet, Ms: 29.661 lb/lb mole
 Excess Air: --- %
 Gas Velocity, Vs: 52.119 fps
 Volumetric Flow: 258,040 acfm
 Volumetric Flow: 146,433 dscfm
 Volumetric Flow: 169,429 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3418.5 ml Silica Initial Wt. 813.3 grams
 Final Impinger Content: 3563.2 ml Silica Final Wt. 826.1 grams
 Impinger Difference: 144.7 ml Silica Difference: 12.8 grams
 Total Water Gain: 157.5 Moisture, Bws: 0.136

| Port-Point No. | Clock Time | Velocity | Orifice | Actual | Stack | Meter Temp | | Probe | Filter | Impinger |
|----------------|------------|------------------------------|-------------------------|----------------------------|---------|------------|-----------|---------|--------------|--------------|
| | | Head Δp in. H ₂ O | ΔH in. H ₂ O | Meter Vol. ft ³ | Temp °F | Inlet °F | Outlet °F | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1 | 8:40:00 | 0.72 | 2.80 | 0.571 | 234 | 72 | 71 | 255 | 266 | 52 |
| 1-2 | 8:45:00 | 0.65 | 2.60 | 5.670 | 227 | 71 | 70 | 257 | 267 | 53 |
| 1-3 | 8:50:00 | 0.55 | 2.20 | 10.530 | 224 | 71 | 68 | 257 | 268 | 53 |
| | 8:55:00 | | | 15.053 | | | | | | |
| 2-1 | 8:57:00 | 0.65 | 2.60 | 15.053 | 216 | 68 | 66 | 260 | 267 | 54 |
| 2-2 | 9:02:00 | 0.63 | 2.60 | 19.970 | 212 | 68 | 65 | 261 | 264 | 54 |
| 2-3 | 9:07:00 | 0.56 | 2.30 | 24.720 | 209 | 68 | 64 | 261 | 267 | 55 |
| | 9:12:00 | | | 29.290 | | | | | | |
| 3-1 | 9:14:00 | 0.62 | 2.50 | 29.290 | 206 | 65 | 63 | 262 | 268 | 55 |
| 3-2 | 9:19:00 | 0.62 | 2.50 | 33.990 | 203 | 67 | 63 | 261 | 266 | 55 |
| 3-3 | 9:24:00 | 0.53 | 2.20 | 38.830 | 201 | 67 | 62 | 261 | 266 | 56 |
| | 9:29:00 | | | 43.304 | | | | | | |
| 4-1 | 9:31:00 | 0.63 | 2.60 | 43.304 | 198 | 65 | 62 | 266 | 265 | 57 |
| 4-2 | 9:36:00 | 0.62 | 2.60 | 48.120 | 196 | 67 | 62 | 262 | 266 | 57 |
| 4-3 | 9:41:00 | 0.52 | 2.20 | 52.940 | 196 | 67 | 62 | 263 | 265 | 57 |
| | 9:46:00 | | | 57.365 | | | | | | |

Total 1:00:00 56.794 68.0 64.8
 Average 2.48 210.2 66.4
 Min 2.20 196.0 62.0
 Max 2.80 234.0 72.0

Impinger Weight Sheet - Run 1

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/18/2023
 Test Method: 26A
 Weighed/Measured By:
 Balance ID: LV3

Scale Calibration Check Date: 10/18/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250 | 250.0 |
| 500 | 500.0 |
| 750 | 750.0 |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 818.0 | 744.3 | 73.7 |
| 0.1N H2SO4 | 734.8 | 685.6 | 49.2 |
| Empty | 654.3 | 643.1 | 11.2 |
| 0.1N NaOH | 745.2 | 738.2 | 7.0 |
| 0.1N NaOH | 610.9 | 607.3 | 3.6 |
| Silica Gel | 826.1 | 813.3 | 12.8 |

| | | |
|---------------------|-----------------------|--------------------|
| 3,563.2 | 3,418.5 | 144.7 |
| Liquid Final | Liquid Initial | Liquid Gain |
| 826.1 | 813.3 | 12.8 |
| Silica Final | Silica Initial | Silica Gain |

Run 2 - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill On

Date: 10/18/23
 Start Time: 10:10
 End Time: 12:02

DRY GAS METER CONDITIONS

STACK CONDITIONS

| | | | | | |
|------------------------|--------|----------------------|---------------------|---------|----------------------|
| ΔH: | 2.40 | In. H ₂ O | Static Pressure | 0.75 | in. H ₂ O |
| Meter Temperature, Tm: | 65.8 | °F | Flue Pressure (Ps): | 24.94 | in. Hg. abs. |
| Sqrt ΔP: | 0.767 | In. H ₂ O | Carbon Dioxide: | 19.90 | % |
| Stack Temperature, Ts: | 203.0 | °F | Oxygen: | 9.50 | % |
| Meter Volume, Vm: | 55.736 | ft ³ | Nitrogen: | 70.6 | % |
| Meter Volume, Vmstd: | 46.403 | dscf | Gas Weight dry, Md: | 31.564 | lb/lb mole |
| Meter Volume, Vwstd: | 4.588 | wscf | Gas Weight wet, Ms: | 30.344 | lb/lb mole |
| Isokinetic Variance: | 97.6 | %I | Excess Air: | --- | % |
| Test Length: | 60.00 | in mins. | Gas Velocity, Vs: | 50.445 | fps |
| Nozzle Diameter: | 0.282 | in inches | Volumetric Flow: | 249,751 | acfm |
| Barometric Pressure: | 24.88 | in Hg | Volumetric Flow: | 150,846 | dscfm |
| | | | Volumetric Flow: | 165,759 | scfm |

MOISTURE DETERMINATION

| | | | | | |
|---------------------------|--------|----|--------------------|-------|-------|
| Initial Impinger Content: | 3495.9 | ml | Silica Initial Wt. | 891.6 | grams |
| Final Impinger Content: | 3584.4 | ml | Silica Final Wt. | 900.5 | grams |
| Impinger Difference: | 88.5 | ml | Silica Difference: | 8.9 | grams |
| Total Water Gain: | 97.4 | | Moisture, Bws: | 0.090 | |

| Port- Point No. | Clock Time | Velocity | Orifice | Actual | Stack | Meter Temp | | Probe | Filter | Impinger |
|--------------------|---------------|---------------------------------|----------------------------|-------------------------------|------------|-------------|--------------|------------|-----------------|-----------------|
| | | Head Δp in. H ₂ O | ΔH in. H ₂ O | Meter Vol. ft ³ | Temp °F | Inlet °F | Outlet °F | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1 | 10:10:00 | 0.63 | 2.60 | 57.785 | 192 | 61 | 60 | 250 | 265 | 53 |
| 1-2 | 10:15:00 | 0.61 | 2.50 | 62.610 | 192 | 66 | 61 | 254 | 267 | 54 |
| 1-3 | 10:20:00 | 0.51 | 2.10 | 67.340 | 191 | 68 | 61 | 255 | 266 | 55 |
| | 10:25:00 | | | 71.709 | | | | | | |
| 2-1 | 10:27:00 | 0.61 | 2.50 | 71.709 | 191 | 66 | 62 | 255 | 265 | 55 |
| 2-2 | 10:32:00 | 0.60 | 2.50 | 76.460 | 190 | 71 | 63 | 254 | 265 | 56 |
| 2-3 | 10:37:00 | 0.54 | 2.30 | 81.240 | 190 | 72 | 63 | 258 | 265 | 56 |
| | 10:42:00 | | | 85.759 | | | | | | |
| 3-1 | 10:44:00 | 0.64 | 2.70 | 85.759 | 189 | 68 | 64 | 260 | 266 | 56 |
| 3-2 | 10:49:00 | 0.64 | 2.70 | 90.670 | 189 | 71 | 64 | 260 | 268 | 57 |
| | 10:54:00 | | | 95.582 | | | | | | |
| 3-3 | 11:40:00 | 0.60 | 2.30 | 95.582 | 237 | 67 | 65 | 262 | 267 | 61 |
| | 11:45:00 | | | 100.148 | | | | | | |
| 4-1 | 11:47:00 | 0.62 | 2.40 | 100.148 | 229 | 67 | 65 | 260 | 265 | 62 |
| 4-2 | 11:52:00 | 0.59 | 2.30 | 104.800 | 224 | 70 | 66 | 260 | 264 | 63 |
| 4-3 | 11:57:00 | 0.48 | 1.90 | 109.350 | 222 | 72 | 66 | 263 | 266 | 63 |
| | 12:02:00 | | | 113.521 | | | | | | |
| Total | 1:00:00 | | | 55.736 | | 68.3 | 63.3 | | | |
| Average | | | 2.40 | | 203.0 | 65.8 | | | | |
| Min | | | 1.90 | | 189.0 | 60.0 | | | | |
| Max | | | 2.70 | | 237.0 | 72.0 | | | | |

Impinger Weight Sheet - Run 2

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/18/2023
 Test Method: 26A
 Weighed/Measured By: 0
 Balance ID: LV3

Scale Calibration Check Date: 10/18/2023
 Scale Calibration Check (see QS-6.05C for procedure)

must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250 | 250.0 |
| 500 | 500.0 |
| 750 | 750.0 |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 814.5 | 747.8 | 66.7 |
| 0.1N H2SO4 | 687.3 | 674.6 | 12.7 |
| Empty | 599.3 | 597.9 | 1.4 |
| 0.1N NaOH | 697.8 | 692.0 | 5.8 |
| 0.1N NaOH | 785.5 | 783.6 | 1.9 |
| Silica Gel | 900.5 | 891.6 | 8.9 |

| | | |
|---------------------|-----------------------|--------------------|
| 3,584.4 | 3,495.9 | 88.5 |
| Liquid Final | Liquid Initial | Liquid Gain |
| 900.5 | 891.6 | 8.9 |
| Silica Final | Silica Initial | Silica Gain |

Run 3 - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill On

Date: 10/18/23
 Start Time: 12:25
 End Time: 13:31

DRY GAS METER CONDITIONS

ΔH : 2.45 in. H₂O
 Meter Temperature, Tm: 71.2 °F
 $\sqrt{\Delta P}$: 0.759 in. H₂O
 Stack Temperature, Ts: 210.1 °F
 Meter Volume, Vm: 56.397 ft³
 Meter Volume, Vmstd: 46.482 dscf
 Meter Volume, Vwstd: 7.574 wscf
 Isokinetic Variance: 104.1 %I

 Test Length: 60.00 in mins.
 Nozzle Diameter: 0.282 in inches
 Barometric Pressure: 24.88 in Hg

STACK CONDITIONS

Static Pressure 0.75 in. H₂O
 Flue Pressure (Ps): 24.94 in. Hg. abs.
 Carbon Dioxide: 20.60 %
 Oxygen: 9.10 %
 Nitrogen: 70.3 %
 Gas Weight dry, Md: 31.660 lb/lb mole
 Gas Weight wet, Ms: 29.746 lb/lb mole
 Excess Air: 96.203 %
 Gas Velocity, Vs: 50.668 fps
 Volumetric Flow: 250,857 acfm
 Volumetric Flow: 141,652 dscfm
 Volumetric Flow: 164,733 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3427.3 ml
 Final Impinger Content: 3574.7 ml
 Impinger Difference: 147.4 ml

 Silica Initial Wt. 825.6 grams
 Silica Final Wt. 839.0 grams
 Silica Difference: 13.4 grams

 Total Water Gain: 160.8
 Moisture, Bws: 0.140

| Port- Point No. | Clock Time | Velocity Head Δp in. H ₂ O | Orifice ΔH in. H ₂ O | Actual Meter Vol. ft ³ | Stack Temp °F | Meter Temp Inlet °F | Meter Temp Outlet °F | Probe Temp °F | Filter Exit Temp °F | Impinger Exit Temp °F |
|--------------------|---------------|---|---|---|---------------------|---------------------------|----------------------------|---------------------|---------------------------|-----------------------------|
| 1-1 | 12:25:00 | 0.63 | 2.70 | 114.590 | 213 | 67 | 66 | 250 | 253 | 51 |
| 1-2 | 12:30:00 | 0.60 | 2.50 | 119.490 | 212 | 71 | 67 | 263 | 264 | 51 |
| 1-3 | 12:35:00 | 0.55 | 2.30 | 124.310 | 212 | 73 | 67 | 257 | 263 | 51 |
| | 12:40:00 | | | 128.930 | | | | | | |
| 2-1 | 12:42:00 | 0.63 | 2.70 | 128.930 | 211 | 71 | 68 | 253 | 265 | 51 |
| 2-2 | 12:47:00 | 0.59 | 2.50 | 133.860 | 210 | 75 | 68 | 250 | 264 | 52 |
| 2-3 | 12:52:00 | 0.52 | 2.20 | 138.690 | 210 | 76 | 69 | 253 | 265 | 52 |
| | 12:57:00 | | | 143.196 | | | | | | |
| 3-1 | 12:59:00 | 0.62 | 2.70 | 143.196 | 209 | 73 | 69 | 258 | 264 | 53 |
| 3-2 | 13:04:00 | 0.59 | 2.50 | 148.100 | 209 | 76 | 70 | 259 | 265 | 53 |
| 3-3 | 13:09:00 | 0.48 | 2.10 | 152.920 | 209 | 76 | 70 | 257 | 265 | 54 |
| | 13:14:00 | | | 157.293 | | | | | | |
| 4-1 | 13:16:00 | 0.63 | 2.70 | 157.293 | 209 | 73 | 70 | 262 | 263 | 56 |
| 4-2 | 13:21:00 | 0.59 | 2.50 | 162.270 | 209 | 76 | 71 | 257 | 265 | 56 |
| 4-3 | 13:26:00 | 0.49 | 2.00 | 166.990 | 208 | 76 | 71 | 253 | 264 | 56 |
| | 13:31:00 | | | 170.987 | | | | | | |

Total 1:00:00 56.397 73.6 68.8
 Average 2.45 210.1 71.2
 Min 2.00 208.0 66.0
 Max 2.70 213.0 76.0

Impinger Weight Sheet - Run 3

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/18/2023
 Test Method: 26A
 Weighed/Measured By: 0
 Balance ID: LV3

Scale Calibration Check Date: 10/18/2023
 Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250 | 250.0 |
| 500 | 500.0 |
| 750 | 750.0 |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 851.0 | 745.1 | 105.9 |
| 0.1N H2SO4 | 722.0 | 689.5 | 32.5 |
| Empty | 650.3 | 643.2 | 7.1 |
| 0.1N NaOH | 742.5 | 740.8 | 1.7 |
| 0.1N NaOH | 608.9 | 608.7 | 0.2 |
| Silica Gel | 839.0 | 825.6 | 13.4 |

| | | |
|---------------------|-----------------------|--------------------|
| 3,574.7 | 3,427.3 | 147.4 |
| Liquid Final | Liquid Initial | Liquid Gain |
| 839.0 | 825.6 | 13.4 |
| Silica Final | Silica Initial | Silica Gain |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Test Location: Main Kiln
 Date: 10/18/23

Run 1

| Spectrum | Time | FTIR Data | | | | | Cell Temp | Pressure | Analyzer Data O2 % (dry) |
|----------------|------|--------------|--------------|-------------|-------------|---------------|-------------|-------------|-----------------------------|
| | | H2O % | CO2 % (wet) | HCN ppmvw | HF ppmvw | | | | |
| RUN1_0360.LAB | 8:40 | 14.42 | 15.49 | 7.74 | 0.10 | 190.74 | 0.85 | 10.72 | |
| RUN1_0361.LAB | 8:41 | 14.40 | 15.38 | 7.75 | 0.10 | 190.70 | 0.85 | 10.80 | |
| RUN1_0362.LAB | 8:42 | 13.78 | 15.99 | 7.78 | 0.10 | 190.71 | 0.85 | 10.31 | |
| RUN1_0363.LAB | 8:43 | 12.89 | 16.50 | 7.62 | 0.10 | 190.74 | 0.85 | 9.92 | |
| RUN1_0364.LAB | 8:44 | 12.71 | 16.60 | 7.94 | 0.10 | 190.69 | 0.85 | 9.98 | |
| RUN1_0365.LAB | 8:45 | 12.50 | 16.33 | 8.53 | 0.10 | 190.55 | 0.85 | 10.31 | |
| RUN1_0366.LAB | 8:46 | 13.19 | 16.47 | 8.62 | 0.10 | 190.67 | 0.85 | 10.14 | |
| RUN1_0367.LAB | 8:47 | 13.40 | 16.72 | 8.07 | 0.10 | 190.64 | 0.85 | 9.64 | |
| RUN1_0368.LAB | 8:48 | 13.54 | 17.13 | 7.97 | 0.10 | 190.58 | 0.85 | 9.42 | |
| RUN1_0369.LAB | 8:49 | 13.87 | 17.43 | 8.07 | 0.10 | 190.48 | 0.85 | 9.02 | |
| RUN1_0370.LAB | 8:50 | 13.76 | 17.21 | 7.72 | 0.10 | 190.54 | 0.85 | 9.21 | |
| RUN1_0371.LAB | 8:51 | 13.55 | 17.01 | 7.92 | 0.10 | 190.63 | 0.85 | 9.24 | |
| RUN1_0372.LAB | 8:52 | 13.65 | 16.69 | 7.77 | 0.10 | 190.65 | 0.85 | 9.53 | |
| RUN1_0373.LAB | 8:53 | 13.33 | 16.33 | 7.87 | 0.10 | 190.74 | 0.85 | 10.02 | |
| RUN1_0374.LAB | 8:54 | 13.36 | 16.54 | 8.07 | 0.10 | 190.68 | 0.85 | 10.02 | |
| RUN1_0375.LAB | 8:55 | 13.32 | 16.68 | 8.02 | 0.10 | 190.59 | 0.85 | 9.89 | |
| RUN1_0376.LAB | 8:56 | 13.56 | 17.09 | 7.98 | 0.10 | 190.72 | 0.85 | 9.65 | |
| RUN1_0377.LAB | 8:57 | 13.78 | 17.24 | 8.12 | 0.10 | 190.79 | 0.85 | 9.19 | |
| RUN1_0378.LAB | 8:58 | 13.66 | 16.70 | 7.96 | 0.10 | 190.76 | 0.85 | 9.38 | |
| RUN1_0379.LAB | 8:59 | 13.54 | 16.81 | 7.95 | 0.10 | 190.74 | 0.85 | 9.59 | |
| RUN1_0380.LAB | 9:00 | 13.71 | 16.92 | 7.83 | 0.10 | 190.73 | 0.85 | 9.59 | |
| RUN1_0381.LAB | 9:01 | 13.68 | 17.03 | 7.87 | 0.10 | 190.50 | 0.85 | 9.53 | |
| RUN1_0382.LAB | 9:02 | 13.94 | 17.22 | 8.04 | 0.10 | 190.48 | 0.85 | 9.32 | |
| RUN1_0383.LAB | 9:03 | 13.84 | 16.79 | 8.08 | 0.10 | 190.57 | 0.85 | 9.07 | |
| RUN1_0384.LAB | 9:04 | 13.81 | 16.77 | 8.22 | 0.10 | 190.60 | 0.85 | 9.81 | |
| RUN1_0385.LAB | 9:05 | 14.07 | 17.21 | 8.53 | 0.10 | 190.58 | 0.85 | 9.24 | |
| RUN1_0386.LAB | 9:06 | 13.57 | 16.65 | 8.40 | 0.10 | 190.68 | 0.85 | 9.31 | |
| RUN1_0387.LAB | 9:07 | 13.68 | 17.07 | 8.66 | 0.10 | 190.72 | 0.85 | 9.93 | |
| RUN1_0388.LAB | 9:08 | 13.73 | 16.60 | 8.28 | 0.10 | 190.63 | 0.85 | 9.44 | |
| RUN1_0389.LAB | 9:09 | 13.80 | 17.01 | 8.31 | 0.10 | 190.80 | 0.85 | 9.74 | |
| RUN1_0390.LAB | 9:10 | 13.98 | 17.03 | 8.24 | 0.10 | 190.76 | 0.85 | 9.44 | |
| RUN1_0391.LAB | 9:11 | 13.92 | 17.07 | 8.17 | 0.10 | 190.82 | 0.85 | 9.29 | |
| RUN1_0392.LAB | 9:12 | 14.05 | 17.54 | 8.33 | 0.10 | 190.68 | 0.85 | 9.34 | |
| RUN1_0393.LAB | 9:13 | 14.08 | 17.23 | 8.23 | 0.10 | 190.49 | 0.85 | 8.90 | |
| RUN1_0394.LAB | 9:14 | 13.84 | 16.72 | 8.01 | 0.10 | 190.82 | 0.85 | 8.98 | |
| RUN1_0395.LAB | 9:15 | 13.89 | 16.70 | 8.00 | 0.10 | 191.04 | 0.85 | 9.39 | |
| RUN1_0396.LAB | 9:16 | 13.62 | 16.81 | 7.97 | 0.10 | 190.89 | 0.85 | 9.58 | |
| RUN1_0397.LAB | 9:17 | 13.67 | 16.56 | 7.70 | 0.10 | 190.62 | 0.85 | 9.72 | |
| RUN1_0398.LAB | 9:18 | 13.58 | 16.50 | 8.02 | 0.10 | 190.64 | 0.85 | 9.65 | |
| RUN1_0399.LAB | 9:19 | 13.85 | 16.73 | 7.88 | 0.10 | 190.65 | 0.85 | 9.99 | |
| RUN1_0400.LAB | 9:20 | 13.35 | 16.14 | 8.20 | 0.10 | 190.41 | 0.85 | 9.56 | |
| RUN1_0401.LAB | 9:21 | 13.57 | 16.92 | 8.53 | 0.10 | 190.33 | 0.85 | 9.97 | |
| RUN1_0402.LAB | 9:22 | 13.57 | 16.94 | 8.21 | 0.10 | 190.40 | 0.85 | 9.98 | |
| RUN1_0403.LAB | 9:23 | 13.75 | 17.08 | 8.08 | 0.10 | 190.54 | 0.85 | 9.56 | |
| RUN1_0404.LAB | 9:24 | 13.95 | 17.10 | 8.07 | 0.10 | 190.63 | 0.85 | 9.63 | |
| RUN1_0405.LAB | 9:25 | 13.55 | 16.03 | 7.76 | 0.10 | 190.71 | 0.85 | 9.23 | |
| RUN1_0406.LAB | 9:26 | 13.55 | 16.14 | 8.26 | 0.10 | 190.64 | 0.85 | 9.41 | |
| RUN1_0407.LAB | 9:27 | 13.61 | 16.66 | 8.44 | 0.10 | 190.63 | 0.85 | 10.30 | |
| RUN1_0408.LAB | 9:28 | 13.52 | 16.72 | 8.42 | 0.10 | 190.67 | 0.85 | 10.08 | |
| RUN1_0409.LAB | 9:29 | 13.41 | 16.66 | 8.40 | 0.10 | 190.55 | 0.85 | 9.78 | |
| RUN1_0410.LAB | 9:30 | 13.68 | 16.74 | 8.32 | 0.10 | 190.59 | 0.84 | 9.78 | |
| RUN1_0411.LAB | 9:31 | 13.60 | 16.66 | 8.34 | 0.10 | 190.59 | 0.84 | 9.87 | |
| RUN1_0412.LAB | 9:32 | 13.66 | 16.74 | 8.69 | 0.10 | 190.61 | 0.85 | 9.72 | |
| RUN1_0413.LAB | 9:33 | 13.41 | 16.93 | 8.65 | 0.10 | 190.64 | 0.84 | 9.59 | |
| RUN1_0414.LAB | 9:34 | 13.45 | 16.85 | 8.46 | 0.10 | 190.56 | 0.85 | 9.71 | |
| RUN1_0415.LAB | 9:35 | 13.43 | 16.83 | 8.28 | 0.10 | 190.66 | 0.85 | 9.62 | |
| RUN1_0416.LAB | 9:36 | 13.47 | 16.91 | 8.21 | 0.10 | 190.51 | 0.84 | 9.67 | |
| RUN1_0417.LAB | 9:37 | 13.40 | 16.89 | 8.20 | 0.10 | 190.48 | 0.84 | 9.73 | |
| RUN1_0418.LAB | 9:38 | 13.78 | 17.08 | 8.26 | 0.10 | 190.59 | 0.85 | 9.58 | |
| RUN1_0419.LAB | 9:39 | 13.60 | 17.02 | 8.09 | 0.10 | 190.60 | 0.84 | 9.64 | |
| Average | | 13.63 | 16.76 | 8.14 | 0.10 | 190.64 | 0.85 | 9.66 | |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Test Location: Main Kiln
 Date: 10/18/23

Run 2

| Spectrum | Time | FTIR Data | | | | | Cell Temp | Pressure | Analyzer Data O2 % (dry) |
|----------------|-------|--------------|--------------|-------------|-------------|---------------|-------------|-------------|-----------------------------|
| | | H2O % | CO2 % (wet) | HCN ppmvw | HF ppmvw | | | | |
| RUN2_0490.LAB | 10:10 | 12.97 | 16.9 | 8.08 | 0.10 | 190.5 | 0.84 | 9.45 | |
| RUN2_0491.LAB | 10:11 | 13.43 | 17.0 | 8.10 | 0.10 | 190.5 | 0.84 | 9.56 | |
| RUN2_0492.LAB | 10:12 | 13.14 | 16.8 | 8.12 | 0.10 | 190.5 | 0.84 | 9.60 | |
| RUN2_0493.LAB | 10:13 | 13.30 | 17.1 | 8.17 | 0.10 | 190.6 | 0.84 | 9.42 | |
| RUN2_0494.LAB | 10:14 | 13.47 | 16.9 | 7.89 | 0.10 | 190.5 | 0.84 | 9.40 | |
| RUN2_0495.LAB | 10:15 | 13.43 | 17.0 | 8.09 | 0.10 | 190.5 | 0.84 | 9.39 | |
| RUN2_0496.LAB | 10:16 | 13.20 | 17.1 | 8.05 | 0.10 | 190.3 | 0.84 | 9.24 | |
| RUN2_0497.LAB | 10:17 | 13.46 | 16.8 | 7.98 | 0.10 | 190.4 | 0.84 | 9.55 | |
| RUN2_0498.LAB | 10:18 | 13.18 | 16.8 | 8.08 | 0.10 | 190.4 | 0.84 | 9.77 | |
| RUN2_0499.LAB | 10:19 | 13.40 | 16.9 | 8.03 | 0.10 | 190.4 | 0.85 | 9.49 | |
| RUN2_0500.LAB | 10:20 | 13.60 | 17.0 | 7.88 | 0.10 | 190.5 | 0.85 | 9.36 | |
| RUN2_0501.LAB | 10:21 | 13.23 | 17.1 | 8.18 | 0.10 | 190.4 | 0.84 | 9.36 | |
| RUN2_0502.LAB | 10:22 | 13.71 | 16.9 | 8.15 | 0.10 | 190.5 | 0.84 | 9.48 | |
| RUN2_0503.LAB | 10:23 | 13.50 | 17.1 | 8.20 | 0.10 | 190.5 | 0.85 | 9.35 | |
| RUN2_0504.LAB | 10:24 | 13.40 | 16.6 | 8.07 | 0.10 | 190.5 | 0.85 | 9.83 | |
| RUN2_0505.LAB | 10:25 | 13.41 | 16.8 | 8.41 | 0.10 | 190.5 | 0.84 | 9.73 | |
| RUN2_0506.LAB | 10:26 | 13.03 | 16.9 | 8.27 | 0.10 | 190.5 | 0.85 | 9.63 | |
| RUN2_0507.LAB | 10:27 | 13.56 | 17.3 | 8.25 | 0.10 | 190.5 | 0.85 | 9.23 | |
| RUN2_0508.LAB | 10:28 | 13.72 | 17.2 | 8.13 | 0.10 | 190.5 | 0.84 | 9.18 | |
| RUN2_0509.LAB | 10:29 | 13.80 | 17.4 | 8.47 | 0.10 | 190.6 | 0.85 | 9.00 | |
| RUN2_0510.LAB | 10:30 | 13.53 | 17.1 | 8.19 | 0.10 | 190.4 | 0.85 | 9.14 | |
| RUN2_0511.LAB | 10:31 | 13.86 | 17.0 | 8.14 | 0.10 | 190.5 | 0.84 | 9.29 | |
| RUN2_0512.LAB | 10:32 | 13.34 | 16.8 | 8.05 | 0.10 | 190.6 | 0.85 | 9.56 | |
| RUN2_0513.LAB | 10:33 | 13.61 | 16.8 | 7.72 | 0.10 | 190.6 | 0.85 | 9.55 | |
| RUN2_0514.LAB | 10:34 | 13.58 | 16.8 | 7.85 | 0.10 | 190.6 | 0.85 | 9.68 | |
| RUN2_0515.LAB | 10:35 | 13.03 | 16.8 | 7.94 | 0.10 | 190.7 | 0.85 | 9.72 | |
| RUN2_0516.LAB | 10:36 | 13.33 | 16.8 | 7.92 | 0.10 | 190.5 | 0.85 | 9.58 | |
| RUN2_0517.LAB | 10:37 | 13.06 | 16.9 | 7.98 | 0.10 | 190.4 | 0.84 | 9.77 | |
| RUN2_0518.LAB | 10:38 | 13.24 | 16.6 | 7.68 | 0.10 | 190.3 | 0.85 | 9.70 | |
| RUN2_0519.LAB | 10:39 | 13.17 | 16.6 | 7.69 | 0.10 | 190.3 | 0.85 | 9.75 | |
| RUN2_0520.LAB | 10:40 | 12.70 | 16.8 | 8.27 | 0.10 | 190.4 | 0.84 | 9.92 | |
| RUN2_0521.LAB | 10:41 | 13.08 | 16.6 | 8.16 | 0.10 | 190.6 | 0.84 | 9.84 | |
| RUN2_0522.LAB | 10:42 | 13.03 | 16.5 | 8.19 | 0.10 | 190.6 | 0.84 | 9.95 | |
| RUN2_0523.LAB | 10:43 | 12.71 | 16.9 | 8.64 | 0.10 | 190.5 | 0.84 | 10.02 | |
| RUN2_0524.LAB | 10:44 | 12.99 | 17.0 | 8.49 | 0.10 | 190.5 | 0.85 | 9.80 | |
| RUN2_0525.LAB | 10:45 | 13.15 | 16.7 | 8.31 | 0.10 | 190.5 | 0.84 | 9.63 | |
| RUN2_0526.LAB | 10:46 | 12.70 | 16.6 | 8.43 | 0.10 | 190.3 | 0.84 | 9.83 | |
| RUN2_0527.LAB | 10:47 | 12.75 | 16.9 | 8.51 | 0.10 | 190.4 | 0.84 | 10.02 | |
| RUN2_0528.LAB | 10:48 | 13.13 | 16.9 | 7.97 | 0.10 | 190.5 | 0.84 | 9.85 | |
| RUN2_0529.LAB | 10:49 | 12.91 | 16.7 | 7.94 | 0.10 | 190.5 | 0.84 | 9.61 | |
| RUN2_0530.LAB | 10:50 | 12.72 | 16.9 | 7.99 | 0.10 | 190.4 | 0.84 | 9.90 | |
| RUN2_0531.LAB | 10:51 | 11.84 | 16.9 | 7.87 | 0.10 | 190.5 | 0.85 | 9.77 | |
| RUN2_0532.LAB | 10:52 | 10.36 | 19.3 | 9.39 | 0.10 | 190.6 | 0.84 | 9.70 | |
| RUN2_0576.LAB | 11:40 | 12.40 | 17.8 | 9.43 | 0.10 | 190.5 | 0.84 | 9.40 | |
| RUN2_0577.LAB | 11:41 | 12.21 | 17.7 | 9.84 | 0.10 | 190.4 | 0.84 | 9.53 | |
| RUN2_0578.LAB | 11:42 | 12.26 | 18.0 | 10.11 | 0.10 | 190.3 | 0.84 | 9.26 | |
| RUN2_0579.LAB | 11:43 | 12.39 | 18.0 | 9.79 | 0.10 | 190.3 | 0.84 | 9.17 | |
| RUN2_0580.LAB | 11:44 | 12.30 | 18.2 | 9.76 | 0.10 | 190.4 | 0.84 | 8.88 | |
| RUN2_0581.LAB | 11:45 | 12.52 | 18.5 | 9.74 | 0.10 | 190.5 | 0.84 | 8.64 | |
| RUN2_0582.LAB | 11:46 | 12.68 | 18.3 | 9.66 | 0.10 | 190.4 | 0.84 | 8.53 | |
| RUN2_0583.LAB | 11:47 | 12.70 | 18.6 | 9.94 | 0.10 | 190.3 | 0.84 | 8.55 | |
| RUN2_0584.LAB | 11:48 | 12.48 | 18.3 | 9.91 | 0.10 | 190.2 | 0.84 | 8.88 | |
| RUN2_0585.LAB | 11:49 | 12.33 | 17.9 | 9.81 | 0.10 | 190.2 | 0.84 | 9.36 | |
| RUN2_0586.LAB | 11:50 | 12.69 | 17.9 | 10.07 | 0.10 | 190.3 | 0.84 | 9.08 | |
| RUN2_0587.LAB | 11:51 | 13.39 | 18.1 | 9.75 | 0.10 | 190.3 | 0.84 | 8.71 | |
| RUN2_0588.LAB | 11:52 | 13.11 | 18.3 | 9.62 | 0.10 | 190.3 | 0.84 | 8.73 | |
| RUN2_0589.LAB | 11:53 | 13.10 | 18.5 | 9.63 | 0.10 | 190.4 | 0.84 | 8.53 | |
| RUN2_0590.LAB | 11:54 | 12.96 | 18.2 | 9.46 | 0.10 | 190.6 | 0.84 | 8.67 | |
| RUN2_0591.LAB | 11:55 | 12.86 | 18.1 | 9.38 | 0.10 | 190.5 | 0.84 | 8.97 | |
| RUN2_0592.LAB | 11:56 | 13.26 | 18.2 | 9.43 | 0.10 | 190.4 | 0.84 | 8.69 | |
| Average | | 13.02 | 17.29 | 8.59 | 0.10 | 190.46 | 0.84 | 9.40 | |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Test Location: Main Kiln
 Date: 10/18/23

Run 3

| Spectrum | Time | FTIR Data | | | | | Cell Temp | Pressure | Analyzer Data |
|----------------|-------|--------------|--------------|-------------|-------------|---------------|-------------|-------------|---------------|
| | | H2O % | CO2 % (wet) | HCN ppmvw | HF ppmvw | O2 % (dry) | | | |
| RUN3_0659.LAB | 12:25 | 13.50 | 17.6 | 8.79 | 0.10 | 190.5 | 0.84 | 9.00 | |
| RUN3_0660.LAB | 12:26 | 13.43 | 17.9 | 8.91 | 0.10 | 190.5 | 0.84 | 8.93 | |
| RUN3_0661.LAB | 12:27 | 13.58 | 17.9 | 8.75 | 0.10 | 190.4 | 0.84 | 9.00 | |
| RUN3_0662.LAB | 12:28 | 13.50 | 17.8 | 8.77 | 0.10 | 190.4 | 0.84 | 8.87 | |
| RUN3_0663.LAB | 12:29 | 13.62 | 17.9 | 8.81 | 0.10 | 190.5 | 0.84 | 8.93 | |
| RUN3_0664.LAB | 12:30 | 13.34 | 17.9 | 8.71 | 0.10 | 190.3 | 0.84 | 9.32 | |
| RUN3_0665.LAB | 12:31 | 13.51 | 17.6 | 8.78 | 0.10 | 190.1 | 0.84 | 8.86 | |
| RUN3_0666.LAB | 12:32 | 13.58 | 18.1 | 8.80 | 0.10 | 190.2 | 0.84 | 8.42 | |
| RUN3_0667.LAB | 12:33 | 13.87 | 18.2 | 8.99 | 0.10 | 190.3 | 0.84 | 8.95 | |
| RUN3_0668.LAB | 12:34 | 13.34 | 17.9 | 8.66 | 0.10 | 190.2 | 0.84 | 9.01 | |
| RUN3_0669.LAB | 12:35 | 13.50 | 17.7 | 8.75 | 0.10 | 190.2 | 0.84 | 9.27 | |
| RUN3_0670.LAB | 12:36 | 13.41 | 17.5 | 8.87 | 0.10 | 190.1 | 0.84 | 9.47 | |
| RUN3_0671.LAB | 12:37 | 13.32 | 17.7 | 8.88 | 0.10 | 190.2 | 0.84 | 9.13 | |
| RUN3_0672.LAB | 12:38 | 13.63 | 17.7 | 8.70 | 0.10 | 190.2 | 0.84 | 9.09 | |
| RUN3_0673.LAB | 12:39 | 13.61 | 17.9 | 8.60 | 0.10 | 190.3 | 0.84 | 8.78 | |
| RUN3_0674.LAB | 12:40 | 13.94 | 18.2 | 8.79 | 0.10 | 190.4 | 0.84 | 8.56 | |
| RUN3_0675.LAB | 12:41 | 13.91 | 18.1 | 8.59 | 0.10 | 190.2 | 0.84 | 8.61 | |
| RUN3_0676.LAB | 12:42 | 13.89 | 18.0 | 8.64 | 0.10 | 190.4 | 0.84 | 8.67 | |
| RUN3_0677.LAB | 12:43 | 13.69 | 17.7 | 8.56 | 0.10 | 190.4 | 0.84 | 8.98 | |
| RUN3_0678.LAB | 12:44 | 13.59 | 17.8 | 8.81 | 0.10 | 190.2 | 0.84 | 9.02 | |
| RUN3_0679.LAB | 12:45 | 13.78 | 18.0 | 8.61 | 0.10 | 190.2 | 0.84 | 8.67 | |
| RUN3_0680.LAB | 12:46 | 13.84 | 17.8 | 8.40 | 0.10 | 190.0 | 0.84 | 8.82 | |
| RUN3_0681.LAB | 12:47 | 13.72 | 17.5 | 8.47 | 0.10 | 190.2 | 0.84 | 9.08 | |
| RUN3_0682.LAB | 12:48 | 13.61 | 17.8 | 8.77 | 0.10 | 190.3 | 0.84 | 9.04 | |
| RUN3_0683.LAB | 12:49 | 13.67 | 17.5 | 8.66 | 0.10 | 190.2 | 0.84 | 9.30 | |
| RUN3_0684.LAB | 12:50 | 13.38 | 17.7 | 8.78 | 0.10 | 190.4 | 0.84 | 9.15 | |
| RUN3_0685.LAB | 12:51 | 13.65 | 17.7 | 8.80 | 0.10 | 190.3 | 0.84 | 9.14 | |
| RUN3_0686.LAB | 12:52 | 13.55 | 17.8 | 8.72 | 0.10 | 190.1 | 0.84 | 9.06 | |
| RUN3_0687.LAB | 12:53 | 13.56 | 18.0 | 8.79 | 0.10 | 190.3 | 0.84 | 8.81 | |
| RUN3_0688.LAB | 12:54 | 13.79 | 18.0 | 8.60 | 0.10 | 190.2 | 0.84 | 8.94 | |
| RUN3_0689.LAB | 12:55 | 13.59 | 17.8 | 8.57 | 0.10 | 190.3 | 0.84 | 8.74 | |
| RUN3_0690.LAB | 12:56 | 13.74 | 17.4 | 8.54 | 0.10 | 190.6 | 0.84 | 9.04 | |
| RUN3_0691.LAB | 12:57 | 13.42 | 17.5 | 8.88 | 0.10 | 190.3 | 0.84 | 9.29 | |
| RUN3_0692.LAB | 12:58 | 13.64 | 17.6 | 8.89 | 0.10 | 190.4 | 0.84 | 9.35 | |
| RUN3_0693.LAB | 12:59 | 13.69 | 17.7 | 8.89 | 0.10 | 190.3 | 0.84 | 9.18 | |
| RUN3_0694.LAB | 13:00 | 13.60 | 17.7 | 8.96 | 0.10 | 190.3 | 0.84 | 9.12 | |
| RUN3_0695.LAB | 13:01 | 13.57 | 17.8 | 8.84 | 0.10 | 190.3 | 0.84 | 9.02 | |
| RUN3_0696.LAB | 13:02 | 13.63 | 17.7 | 8.61 | 0.10 | 190.2 | 0.84 | 9.06 | |
| RUN3_0697.LAB | 13:03 | 13.52 | 17.9 | 8.62 | 0.10 | 190.2 | 0.84 | 9.20 | |
| RUN3_0698.LAB | 13:04 | 13.71 | 18.0 | 8.73 | 0.10 | 190.3 | 0.84 | 8.97 | |
| RUN3_0699.LAB | 13:05 | 13.62 | 17.9 | 8.46 | 0.10 | 190.3 | 0.84 | 8.88 | |
| RUN3_0700.LAB | 13:06 | 13.73 | 17.6 | 8.15 | 0.10 | 190.2 | 0.84 | 8.90 | |
| RUN3_0701.LAB | 13:07 | 13.50 | 17.6 | 8.20 | 0.10 | 190.2 | 0.84 | 9.12 | |
| RUN3_0702.LAB | 13:08 | 13.73 | 17.7 | 7.96 | 0.10 | 190.3 | 0.84 | 9.13 | |
| RUN3_0703.LAB | 13:09 | 13.79 | 17.8 | 7.94 | 0.10 | 190.2 | 0.84 | 8.97 | |
| RUN3_0704.LAB | 13:10 | 13.61 | 17.6 | 7.86 | 0.10 | 190.2 | 0.84 | 8.87 | |
| RUN3_0705.LAB | 13:11 | 13.87 | 17.7 | 8.08 | 0.10 | 190.2 | 0.84 | 9.08 | |
| RUN3_0706.LAB | 13:12 | 13.56 | 17.8 | 8.43 | 0.10 | 190.2 | 0.84 | 8.96 | |
| RUN3_0707.LAB | 13:13 | 13.68 | 17.7 | 8.39 | 0.10 | 190.2 | 0.84 | 8.81 | |
| RUN3_0708.LAB | 13:14 | 13.67 | 17.9 | 8.16 | 0.10 | 190.3 | 0.84 | 9.11 | |
| RUN3_0709.LAB | 13:15 | 14.01 | 18.1 | 7.90 | 0.10 | 190.2 | 0.84 | 8.98 | |
| RUN3_0710.LAB | 13:16 | 13.75 | 17.6 | 7.56 | 0.10 | 190.4 | 0.84 | 8.59 | |
| RUN3_0711.LAB | 13:17 | 13.61 | 17.4 | 7.40 | 0.10 | 190.5 | 0.84 | 8.78 | |
| RUN3_0712.LAB | 13:18 | 13.94 | 17.4 | 7.60 | 0.10 | 190.4 | 0.84 | 9.19 | |
| RUN3_0713.LAB | 13:19 | 13.91 | 17.4 | 8.23 | 0.10 | 190.4 | 0.84 | 9.02 | |
| RUN3_0714.LAB | 13:20 | 14.00 | 17.4 | 8.16 | 0.10 | 190.3 | 0.84 | 9.42 | |
| RUN3_0715.LAB | 13:21 | 14.08 | 17.8 | 7.93 | 0.10 | 190.3 | 0.84 | 9.36 | |
| RUN3_0716.LAB | 13:22 | 14.03 | 17.5 | 7.59 | 0.10 | 190.0 | 0.84 | 9.12 | |
| RUN3_0717.LAB | 13:23 | 14.07 | 17.4 | 7.32 | 0.10 | 190.0 | 0.84 | 8.82 | |
| RUN3_0718.LAB | 13:24 | 14.00 | 17.2 | 7.31 | 0.10 | 190.2 | 0.84 | 9.07 | |
| Average | | 13.68 | 17.75 | 8.46 | 0.10 | 190.27 | 0.84 | 9.00 | |

Client: GCC Rio Grande, Inc.
Facility: Pueblo Plant
Test Location: Main Kiln Stack
Project #: M234207
Test Method: 26A
Test Engineer: DCS
Test Technician: SWK

| | <u>Run 1A</u> | <u>Run 2A</u> | <u>Run 3A</u> |
|---|---------------|---------------|---------------|
| Temp ID: | CM53 | CM53 | CM53 |
| Meter ID: | CM53 | CM53 | CM53 |
| Pitot ID: | S8-031A | S8-031A | S8-031A |
| Nozzle Diameter (Inches): | 0.281 | 0.281 | 0.281 |
| Meter Calibration Date: | 9/6/2023 | 9/6/2023 | 9/6/2023 |
| Meter Calibration Factor (Y): | 0.994 | 0.994 | 0.994 |
| Meter Orifice Setting (Delta H): | 1.775 | 1.775 | 1.775 |
| Nozzle Kit ID Number and Material: | #32 Glass | #32 Glass | #32 Glass |
| Pitot Tube Coefficient: | | 0.820 | |
| Probe Length (Feet): | | 6.0 | |
| Probe Liner Material: | | Glass | |
| Sample Plane: | | Horizontal | |
| Port Length (Inches): | | 9.50 | |
| Port Size (Diameter, Inches): | | 6.00 | |
| Port Type: | | Flange | |
| Duct Shape: | | Circular | |
| Diameter (Feet): | | 10.25 | |
| Duct Area (Square Feet): | | 82.516 | |
| Upstream Diameters: | | 4.9 | |
| Downstream Diameters: | | 24.4 | |
| Number of Ports Sampled: | | 4 | |
| Number of Points per Port: | | 3 | |
| Minutes per Point: | | 5.0 | |
| Minutes per Reading: | | 5.0 | |
| Total Number of Traverse Points: | | 12 | |
| Test Length (Minutes): | | 60 | |
| Train Type: | | Anderson Box | |
| Source Condition: | | Mill Off | |
| Diluent Model/Serial Number: | | CAI700 | |
| Moisture Balance ID: | | LV3 | |
| # of Runs | | 3 | |

Run 1A - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill Off

Date: 10/17/23
 Start Time: 8:00
 End Time: 9:09

DRY GAS METER CONDITIONS

ΔH: 1.22 in. H₂O
 Meter Temperature, Tm: 65.6 °F
 Sqrt ΔP: 0.618 in. H₂O
 Stack Temperature, Ts: 356.4 °F
 Meter Volume, Vm: 41.960 ft³
 Meter Volume, Vmstd: 34.855 dscf
 Meter Volume, Vwstd: 4.955 wscf
 Isokinetic Variance: 107.4 %I
 Test Length: 60.00 in mins.
 Nozzle Diameter: 0.281 in inches
 Barometric Pressure: 24.80 in Hg

STACK CONDITIONS

Static Pressure -0.50 in. H₂O
 Flue Pressure (Ps): 24.76 in. Hg. abs.
 Carbon Dioxide: 29.10 %
 Oxygen: 4.20 %
 Nitrogen: 66.70 %
 Gas Weight dry, Md: 32.824 lb/lb mole
 Gas Weight wet, Ms: 30.979 lb/lb mole
 Excess Air: 31.323 %
 Gas Velocity, Vs: 44.684 fps
 Volumetric Flow: 221.226 acfm
 Volumetric Flow: 103,676 dscfm
 Volumetric Flow: 118,414 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3557.8 ml Silica Initial Wt. 780.4 grams
 Final Impinger Content: 3657.6 ml Silica Final Wt. 785.8 grams
 Impinger Difference: 99.8 ml Silica Difference: 5.4 grams
 Total Water Gain: 105.2 Moisture, Bws: 0.124

| Port- Point No. | Clock Time | Velocity | Orifice | Actual | Stack | Meter Temp | | Probe | Filter | Impinger |
|--------------------|---------------|---------------------------------|----------------------------|-------------------------------|------------|-------------|--------------|------------|-----------------|-----------------|
| | | Head Δp in. H ₂ O | ΔH in. H ₂ O | Meter Vol. ft ³ | Temp °F | Inlet °F | Outlet °F | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1 | 8:00:00 | 0.45 | 1.50 | 132.931 | 344 | 64 | 63 | 252 | 259 | 50 |
| 1-2 | 8:05:00 | 0.38 | 1.20 | 136.655 | 347 | 61 | 64 | 261 | 267 | 50 |
| 1-3 | 8:10:00 | 0.35 | 1.10 | 140.067 | 347 | 59 | 64 | 272 | 269 | 50 |
| | 8:15:00 | | | 144.322 | | | | | | |
| 2-1 | 8:18:00 | 0.42 | 1.30 | 144.322 | 354 | 59 | 65 | 273 | 269 | 51 |
| 2-2 | 8:23:00 | 0.42 | 1.30 | 147.867 | 356 | 59 | 67 | 271 | 268 | 51 |
| 2-3 | 8:28:00 | 0.29 | 0.90 | 151.400 | 356 | 59 | 65 | 273 | 267 | 51 |
| | 8:33:00 | | | 154.361 | | | | | | |
| 3-1 | 8:36:00 | 0.45 | 1.40 | 154.361 | 356 | 66 | 69 | 272 | 267 | 51 |
| 3-2 | 8:41:00 | 0.40 | 1.30 | 158.086 | 364 | 64 | 69 | 270 | 269 | 51 |
| 3-3 | 8:46:00 | 0.32 | 1.00 | 161.577 | 363 | 72 | 70 | 266 | 270 | 51 |
| | 8:51:00 | | | 164.727 | | | | | | |
| 4-1 | 8:54:00 | 0.40 | 1.30 | 164.727 | 354 | 67 | 70 | 273 | 269 | 53 |
| 4-2 | 8:59:00 | 0.38 | 1.20 | 168.250 | 368 | 68 | 70 | 270 | 270 | 53 |
| 4-3 | 9:04:00 | 0.34 | 1.10 | 171.660 | 368 | 69 | 71 | 267 | 270 | 55 |
| | 9:09:00 | | | 174.891 | | | | | | |

Total 1:00:00 41.960 63.9 67.3
 Average 1.22 356.4 65.6
 Min 0.90 344.0 59.0
 Max 1.50 368.0 72.0

Impinger Weight Sheet - Run 1A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/17/2023
 Test Method: 26A
 Weighed/Measured By: WAP
 Balance ID: LV3

Scale Calibration Check Date: 10/17/2023
 Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight. grams</u> | <u>Result. grams</u> |
|--------------------------------|----------------------|
| 250 | <u>250.0</u> |
| 500 | <u>500.0</u> |
| 750 | <u>750.0</u> |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 776.5 | 743.8 | 32.7 |
| 0.1N H2SO4 | 725.1 | 688.0 | 37.1 |
| Empty | 659.5 | 643.5 | 16.0 |
| 0.1N NaOH | 789.4 | 780.8 | 8.6 |
| 0.1N NaOH | 707.1 | 701.7 | 5.4 |
| Silica Gel | 785.8 | 780.4 | 5.4 |

| | | |
|---------------------------------------|---|-----------------------------------|
| <u>3,657.6</u> Liquid Final | <u>3,557.8</u> Liquid Initial | <u>99.8</u> Liquid Gain |
| <u>785.8</u> Silica Final | <u>780.4</u> Silica Initial | <u>5.4</u> Silica Gain |

Run 2A - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill Off

Date: 10/17/23
 Start Time: 13:40
 End Time: 14:46

DRY GAS METER CONDITIONS

STACK CONDITIONS

| | | | | | |
|------------------------|--------|----------------------|---------------------|---------|----------------------|
| ΔH: | 1.29 | In. H ₂ O | Static Pressure | -0.50 | in. H ₂ O |
| Meter Temperature, Tm: | 86.1 | °F | Flue Pressure (Ps): | 24.76 | in. Hg. abs. |
| Sqrt ΔP: | 0.618 | In. H ₂ O | Carbon Dioxide: | 27.90 | % |
| Stack Temperature, Ts: | 364.0 | °F | Oxygen: | 5.20 | % |
| Meter Volume, Vm: | 41.116 | ft ³ | Nitrogen: | 66.9 | % |
| Meter Volume, Vmstd: | 32.877 | dscf | Gas Weight dry, Md: | 32.672 | lb/lb mole |
| Meter Volume, Vwstd: | 4.823 | wscf | Gas Weight wet, Ms: | 30.795 | lb/lb mole |
| Isokinetic Variance: | 101.8 | %I | Excess Air: | 41.728 | % |
| Test Length: | 60.00 | in mins. | Gas Velocity, Vs: | 45.051 | fps |
| Nozzle Diameter: | 0.281 | in inches | Volumetric Flow: | 223,044 | acfm |
| Barometric Pressure: | 24.80 | in Hg | Volumetric Flow: | 103,155 | dscfm |
| | | | Volumetric Flow: | 118,288 | scfm |

MOISTURE DETERMINATION

| | | | | | |
|---------------------------|--------|----|--------------------|-------|-------|
| Initial Impinger Content: | 3480.1 | ml | Silica Initial Wt. | 857.5 | grams |
| Final Impinger Content: | 3572.7 | ml | Silica Final Wt. | 867.3 | grams |
| Impinger Difference: | 92.6 | ml | Silica Difference: | 9.8 | grams |
| Total Water Gain: | 102.4 | | Moisture, Bws: | 0.128 | |

| Port- Point No. | Clock Time | Velocity | Orifice | Actual | Stack | Meter Temp | | Probe | Filter | Impinger |
|--------------------|---------------|---------------------------------|----------------------------|-------------------------------|------------|-------------|--------------|------------|-----------------|-----------------|
| | | Head Δp in. H ₂ O | ΔH in. H ₂ O | Meter Vol. ft ³ | Temp °F | Inlet °F | Outlet °F | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1 | 13:40:00 | 0.43 | 1.40 | 181.959 | 375 | 87 | 83 | 259 | 268 | 61 |
| 1-2 | 13:45:00 | 0.40 | 1.30 | 185.860 | 375 | 87 | 83 | 264 | 268 | 60 |
| 1-3 | 13:50:00 | 0.30 | 1.00 | 189.430 | 374 | 87 | 83 | 266 | 267 | 63 |
| | 13:55:00 | | | 192.815 | | | | | | |
| 2-1 | 13:57:00 | 0.46 | 1.50 | 192.815 | 353 | 90 | 85 | 260 | 267 | 65 |
| 2-2 | 14:02:00 | 0.42 | 1.40 | 196.060 | 352 | 85 | 84 | 263 | 266 | 64 |
| 2-3 | 14:07:00 | 0.29 | 1.00 | 199.230 | 351 | 85 | 86 | 266 | 266 | 62 |
| | 14:12:00 | | | 202.435 | | | | | | |
| 3-1 | 14:14:00 | 0.46 | 1.50 | 202.435 | 352 | 83 | 88 | 271 | 264 | 67 |
| 3-2 | 14:19:00 | 0.41 | 1.40 | 205.940 | 353 | 83 | 88 | 270 | 265 | 63 |
| 3-3 | 14:24:00 | 0.29 | 1.00 | 209.530 | 353 | 87 | 89 | 270 | 267 | 64 |
| | 14:29:00 | | | 212.709 | | | | | | |
| 4-1 | 14:31:00 | 0.45 | 1.50 | 212.709 | 375 | 82 | 91 | 265 | 261 | 66 |
| 4-2 | 14:36:00 | 0.39 | 1.30 | 216.110 | 378 | 83 | 92 | 261 | 267 | 65 |
| 4-3 | 14:41:00 | 0.32 | 1.20 | 219.570 | 377 | 84 | 92 | 263 | 267 | 66 |
| | 14:46:00 | | | 223.075 | | | | | | |

| | | | | | | | | | | |
|---------|---------|--|------|--------|-------|------|------|--|--|--|
| Total | 1:00:00 | | | 41.116 | | 85.3 | 87.0 | | | |
| Average | | | 1.29 | | 364.0 | 86.1 | | | | |
| Min | | | 1.00 | | 351.0 | 82.0 | | | | |
| Max | | | 1.50 | | 378.0 | 92.0 | | | | |

Impinger Weight Sheet - Run 2A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/17/2023
 Test Method: 26A
 Weighed/Measured By: WAP
 Balance ID: LV3

Scale Calibration Check Date: 10/17/2023
 Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight. grams</u> | <u>Result. grams</u> |
|--------------------------------|----------------------|
| 250 | <u>250.0</u> |
| 500 | <u>500.0</u> |
| 750 | <u>750.0</u> |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 810.6 | 746.6 | 64.0 |
| 0.1N H2SO4 | 690.0 | 673.6 | 16.4 |
| Empty | 597.8 | 593.4 | 4.4 |
| 0.1N NaOH | 691.3 | 685.2 | 6.1 |
| 0.1N NaOH | 783.0 | 781.3 | 1.7 |
| Silica Gel | 867.3 | 857.5 | 9.8 |

| | | |
|---------------------------------------|---|-----------------------------------|
| <u>3,572.7</u> Liquid Final | <u>3,480.1</u> Liquid Initial | <u>92.6</u> Liquid Gain |
| <u>867.3</u> Silica Final | <u>857.5</u> Silica Initial | <u>9.8</u> Silica Gain |

Run 3A - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill Off

Date: 10/17/23
 Start Time: 15:05
 End Time: 16:14

DRY GAS METER CONDITIONS

| | | |
|------------------------|--------|----------------------|
| ΔH: | 1.24 | In. H ₂ O |
| Meter Temperature, Tm: | 92.2 | °F |
| Sqrt ΔP: | 0.613 | In. H ₂ O |
| Stack Temperature, Ts: | 369.8 | °F |
| Meter Volume, Vm: | 42.450 | ft ³ |
| Meter Volume, Vmstd: | 33.567 | dscf |
| Meter Volume, Vwstd: | 4.889 | wscf |
| Isokinetic Variance: | 105.5 | %I |
| Test Length: | 60.00 | in mins. |
| Nozzle Diameter: | 0.281 | in inches |
| Barometric Pressure: | 24.80 | in Hg |

STACK CONDITIONS

| | | |
|---------------------|---------|----------------------|
| Static Pressure | -0.50 | in. H ₂ O |
| Flue Pressure (Ps): | 24.76 | in. Hg. abs. |
| Carbon Dioxide: | 29.80 | % |
| Oxygen: | 4.20 | % |
| Nitrogen: | 66 | % |
| Gas Weight dry, Md: | 32.936 | lb/lb mole |
| Gas Weight wet, Ms: | 31.037 | lb/lb mole |
| Excess Air: | 31.760 | % |
| Gas Velocity, Vs: | 44.674 | fps |
| Volumetric Flow: | 221,180 | acfm |
| Volumetric Flow: | 101,677 | dscfm |
| Volumetric Flow: | 116,487 | scfm |

MOISTURE DETERMINATION

| | | | | | |
|---------------------------|--------|----|--------------------|-------|-------|
| Initial Impinger Content: | 3553.5 | ml | Silica Initial Wt. | 830.0 | grams |
| Final Impinger Content: | 3647.3 | ml | Silica Final Wt. | 840.0 | grams |
| Impinger Difference: | 93.8 | ml | Silica Difference: | 10.0 | grams |
| Total Water Gain: | 103.8 | | Moisture, Bws: | 0.127 | |

| Port- Point No. | Clock Time | Velocity Head Δp in. H ₂ O | Orifice ΔH in. H ₂ O | Actual Meter Vol. ft ³ | Stack Temp °F | Meter Temp Inlet °F | Meter Temp Outlet °F | Probe Temp °F | Filter Exit Temp °F | Impinger Exit Temp °F |
|--------------------|---------------|---|---------------------------------------|---|---------------------|---------------------------|----------------------------|---------------------|---------------------------|-----------------------------|
| 1-1 | 15:05:00 | 0.43 | 1.40 | 223.435 | 381 | 84 | 96 | 268 | 269 | 64 |
| 1-2 | 15:10:00 | 0.38 | 1.20 | 227.530 | 382 | 83 | 97 | 264 | 270 | 64 |
| 1-3 | 15:15:00 | 0.29 | 1.10 | 231.040 | 281 | 85 | 98 | 270 | 267 | 64 |
| | 15:20:00 | | | 234.291 | | | | | | |
| 2-1 | 15:22:00 | 0.44 | 1.40 | 234.291 | 381 | 88 | 100 | 270 | 265 | 65 |
| 2-2 | 15:27:00 | 0.38 | 1.20 | 236.230 | 383 | 90 | 101 | 268 | 265 | 65 |
| 2-3 | 15:32:00 | 0.27 | 0.90 | 241.570 | 381 | 84 | 102 | 265 | 264 | 65 |
| | 15:37:00 | | | 244.615 | | | | | | |
| 3-1 | 15:39:00 | 0.43 | 1.40 | 244.615 | 383 | 81 | 103 | 265 | 266 | 65 |
| 3-2 | 15:44:00 | 0.38 | 1.20 | 248.320 | 384 | 81 | 104 | 268 | 265 | 65 |
| 3-3 | 15:49:00 | 0.29 | 0.90 | 251.880 | 384 | 79 | 103 | 265 | 263 | 65 |
| | 15:54:00 | | | 254.819 | | | | | | |
| 4-1 | 15:59:00 | 0.48 | 1.60 | 254.819 | 380 | 82 | 102 | 270 | 268 | 66 |
| 4-2 | 16:04:00 | 0.44 | 1.50 | 258.510 | 360 | 82 | 102 | 271 | 266 | 66 |
| 4-3 | 16:09:00 | 0.34 | 1.10 | 262.430 | 357 | 83 | 102 | 272 | 269 | 66 |
| | 16:14:00 | | | 265.885 | | | | | | |

| | | | | | | | | | | |
|---------|---------|--|------|--------|-------|-------|-------|--|--|--|
| Total | 1:00:00 | | | 42.450 | | 83.5 | 100.8 | | | |
| Average | | | 1.24 | | 369.8 | 92.2 | | | | |
| Min | | | 0.90 | | 281.0 | 79.0 | | | | |
| Max | | | 1.60 | | 384.0 | 104.0 | | | | |

Impinger Weight Sheet - Run 3A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/17/2023
 Test Method: 26A
 Weighed/Measured By: WAP
 Balance ID: LV3

Scale Calibration Check Date: 10/17/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250 | <u>250.0</u> |
| 500 | <u>500.0</u> |
| 750 | <u>750.0</u> |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 811.1 | 743.2 | 67.9 |
| 0.1N H2SO4 | 709.0 | 687.8 | 21.2 |
| Empty | 646.4 | 643.8 | 2.6 |
| 0.1N NaOH | 781.8 | 781.8 | 0.0 |
| 0.1N NaOH | 699.0 | 696.9 | 2.1 |
| Silica Gel | 840.0 | 830.0 | 10.0 |

| | | |
|--------------------------------|----------------------------------|----------------------------|
| <u>3,647.3</u> Liquid Final | <u>3,553.5</u> Liquid Initial | <u>93.8</u> Liquid Gain |
| <u>840.0</u> Silica Final | <u>830.0</u> Silica Initial | <u>10.0</u> Silica Gain |

Client: GCC Rio Grande, Inc.
Facility: Pueblo Plant
Test Location: Main Kiln Stack
Project #: M234207
Test Method: 26A
Test Engineer: SWK
Test Technician: DCS

| | <u>Run 1B</u> | <u>Run 2B</u> | <u>Run 3B</u> |
|---|---------------|---------------|---------------|
| Temp ID: | CM4 | CM4 | CM4 |
| Meter ID: | CM4 | CM4 | CM4 |
| Pitot ID: | S8-032A | S8-032A | S8-032A |
| Nozzle Diameter (Inches): | 0.282 | 0.282 | 0.282 |
| Meter Calibration Date: | 10/5/2023 | 10/5/2023 | 10/5/2023 |
| Meter Calibration Factor (Y): | 0.990 | 0.990 | 0.990 |
| Meter Orifice Setting (Delta H): | 1.889 | 1.889 | 1.889 |
| Nozzle Kit ID Number and Material: | 21 Glass | 21 Glass | 21 Glass |
| Pitot Tube Coefficient: | | 0.822 | |
| Probe Length (Feet): | | 4.0 | |
| Probe Liner Material: | | Glass | |
| Sample Plane: | | Horizontal | |
| Port Length (Inches): | | 9.50 | |
| Port Size (Diameter, Inches): | | 6.00 | |
| Port Type: | | Flange | |
| Duct Shape: | | Circular | |
| Diameter (Feet): | | 10.25 | |
| Duct Area (Square Feet): | | 82.516 | |
| Upstream Diameters: | | 4.9 | |
| Downstream Diameters: | | 24.4 | |
| Number of Ports Sampled: | | 4 | |
| Number of Points per Port: | | 3 | |
| Minutes per Point: | | 5.0 | |
| Minutes per Reading: | | 5.0 | |
| Total Number of Traverse Points: | | 12 | |
| Test Length (Minutes): | | 60 | |
| Train Type: | | Anderson Box | |
| Source Condition: | | Mill Off | |
| Diluent Model/Serial Number: | | CAI 700 | |
| Moisture Balance ID: | | LV3 | |
| # of Runs | | 3 | |

Run 1B - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill Off

Date: 10/17/23
 Start Time: 8:00
 End Time: 9:09

DRY GAS METER CONDITIONS

ΔH: 1.17 in. H₂O
 Meter Temperature, Tm: 73.8 °F
 Sqrt ΔP: 0.581 in. H₂O
 Stack Temperature, Ts: 353.0 °F
 Meter Volume, Vm: 40.617 ft³
 Meter Volume, Vmstd: 33.079 dscf
 Meter Volume, Vwstd: 4.300 wscf
 Isokinetic Variance: 106.3 %I

 Test Length: 60.00 in mins.
 Nozzle Diameter: 0.282 in inches
 Barometric Pressure: 24.80 in Hg

STACK CONDITIONS

Static Pressure -0.50 in. H₂O
 Flue Pressure (Ps): 24.76 in. Hg. abs.
 Carbon Dioxide: 29.10 %
 Oxygen: 4.20 %
 Nitrogen: 66.70 %
 Gas Weight dry, Md: 32.824 lb/lb mole
 Gas Weight wet, Ms: 31.119 lb/lb mole
 Excess Air: 31.323 %
 Gas Velocity, Vs: 41.913 fps
 Volumetric Flow: 207,507 acfm
 Volumetric Flow: 98,706 dscfm
 Volumetric Flow: 111,538 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3450.4 ml
 Final Impinger Content: 3530.3 ml
 Impinger Difference: 79.9 ml

 Silica Initial Wt. 799.0 grams
 Silica Final Wt. 810.4 grams
 Silica Difference: 11.4 grams

 Total Water Gain: 91.3
 Moisture, Bws: 0.115

| Port- Point No. | Clock Time | Velocity | Orifice | Actual | Stack | Meter Temp | | Probe | Filter | Impinger |
|--------------------|---------------|---------------------------------|----------------------------|-------------------------------|------------|-------------|--------------|------------|-----------------|-----------------|
| | | Head Δp in. H ₂ O | ΔH in. H ₂ O | Meter Vol. ft ³ | Temp °F | Inlet °F | Outlet °F | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1 | 8:00:00 | 0.30 | 1.00 | 37.342 | 337 | 71 | 65 | 250 | 250 | 55 |
| 1-2 | 8:05:00 | 0.35 | 1.20 | 40.520 | 343 | 73 | 66 | 255 | 250 | 55 |
| 1-3 | 8:10:00 | 0.30 | 1.10 | 43.980 | 342 | 74 | 66 | 252 | 259 | 55 |
| | 8:15:00 | | | 47.167 | | | | | | |
| 2-1 | 8:18:00 | 0.38 | 1.30 | 47.167 | 350 | 77 | 68 | 258 | 255 | 56 |
| 2-2 | 8:23:00 | 0.37 | 1.30 | 50.760 | 352 | 79 | 69 | 262 | 269 | 57 |
| 2-3 | 8:28:00 | 0.32 | 1.10 | 54.300 | 351 | 81 | 71 | 259 | 264 | 57 |
| | 8:33:00 | | | 57.619 | | | | | | |
| 3-1 | 8:36:00 | 0.37 | 1.30 | 57.619 | 356 | 80 | 72 | 252 | 264 | 57 |
| 3-2 | 8:41:00 | 0.32 | 1.10 | 61.180 | 359 | 81 | 73 | 255 | 263 | 58 |
| 3-3 | 8:46:00 | 0.28 | 0.98 | 64.470 | 358 | 81 | 74 | 256 | 264 | 59 |
| | 8:51:00 | | | 67.571 | | | | | | |
| 4-1 | 8:54:00 | 0.40 | 1.40 | 67.571 | 362 | 79 | 73 | 260 | 264 | 62 |
| 4-2 | 8:59:00 | 0.38 | 1.10 | 71.240 | 364 | 70 | 74 | 259 | 264 | 61 |
| 4-3 | 9:04:00 | 0.29 | 1.10 | 74.810 | 362 | 81 | 74 | 262 | 264 | 62 |
| | 9:09:00 | | | 77.959 | | | | | | |

Total 1:00:00 40.617 77.3 70.4
 Average 1.17 353.0 73.8
 Min 0.98 337.0 65.0
 Max 1.40 364.0 81.0

Impinger Weight Sheet - Run 1B

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/17/2023
 Test Method: 26A
 Weighed/Measured By: WAP
 Balance ID: LV3

Scale Calibration Check Date: 10/17/2023
 Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250 | <u>250.0</u> |
| 500 | <u>500.0</u> |
| 750 | <u>750.0</u> |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|----------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 773.3 | 746.0 | 27.3 |
| 0.1N H2SO4 | 727.3 | 689.1 | 38.2 |
| Empty | 664.2 | 664.1 | 0.1 |
| 0.1N NaOH | 750.5 | 741.2 | 9.3 |
| 0.1N NaOH | 615.0 | 610.0 | 5.0 |
| Silica Gel | 810.4 | 799.0 | 11.4 |

| | | |
|---------------------------------------|---|-----------------------------------|
| <u>3,530.3</u> Liquid Final | <u>3,450.4</u> Liquid Initial | <u>79.9</u> Liquid Gain |
| <u>810.4</u> Silica Final | <u>799.0</u> Silica Initial | <u>11.4</u> Silica Gain |

Run 2B - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill Off

Date: 10/17/23
 Start Time: 13:40
 End Time: 14:46

DRY GAS METER CONDITIONS

STACK CONDITIONS

| | | | | | |
|------------------------|--------|----------------------|---------------------|---------|----------------------|
| ΔH: | 1.44 | In. H ₂ O | Static Pressure | -0.50 | in. H ₂ O |
| Meter Temperature, Tm: | 86.6 | °F | Flue Pressure (Ps): | 24.76 | in. Hg. abs. |
| Sqrt ΔP: | 0.622 | In. H ₂ O | Carbon Dioxide: | 27.90 | % |
| Stack Temperature, Ts: | 359.9 | °F | Oxygen: | 5.20 | % |
| Meter Volume, Vm: | 43.876 | ft ³ | Nitrogen: | 66.9 | % |
| Meter Volume, Vmstd: | 34.929 | dscf | Gas Weight dry, Md: | 32.672 | lb/lb mole |
| Meter Volume, Vwstd: | 5.845 | wscf | Gas Weight wet, Ms: | 30.569 | lb/lb mole |
| Isokinetic Variance: | 107.7 | %I | Excess Air: | 41.728 | % |
| Test Length: | 60.00 | in mins. | Gas Velocity, Vs: | 45.501 | fps |
| Nozzle Diameter: | 0.282 | in inches | Volumetric Flow: | 225,273 | acfm |
| Barometric Pressure: | 24.80 | in Hg | Volumetric Flow: | 102,853 | dscfm |
| | | | Volumetric Flow: | 120,065 | scfm |

MOISTURE DETERMINATION

| | | | | | |
|---------------------------|--------|----|--------------------|-------|-------|
| Initial Impinger Content: | 3663.9 | ml | Silica Initial Wt. | 844.1 | grams |
| Final Impinger Content: | 3774.6 | ml | Silica Final Wt. | 857.5 | grams |
| Impinger Difference: | 110.7 | ml | Silica Difference: | 13.4 | grams |
| Total Water Gain: | 124.1 | | Moisture, Bws: | 0.143 | |

| Port- Point No. | Clock Time | Velocity Head Δp in. H ₂ O | Orifice ΔH in. H ₂ O | Actual Meter Vol. ft ³ | Stack Temp °F | Meter Temp Inlet °F | Meter Temp Outlet °F | Probe Temp °F | Filter Exit Temp °F | Impinger Exit Temp °F |
|--------------------|---------------|---|---------------------------------------|---|---------------------|---------------------------|----------------------------|---------------------|---------------------------|-----------------------------|
| 1-1 | 13:40:00 | 0.42 | 1.50 | 84.286 | 370 | 77 | 74 | 255 | 250 | 52 |
| 1-2 | 13:45:00 | 0.40 | 1.30 | 88.050 | 371 | 79 | 75 | 253 | 259 | 54 |
| 1-3 | 13:50:00 | 0.34 | 1.20 | 91.100 | 368 | 80 | 75 | 256 | 267 | 56 |
| | 13:55:00 | | | 94.560 | | | | | | |
| 2-1 | 13:57:00 | 0.44 | 1.70 | 94.560 | 349 | 86 | 85 | 257 | 263 | 53 |
| 2-2 | 14:02:00 | 0.41 | 1.60 | 98.550 | 349 | 90 | 85 | 256 | 261 | 53 |
| 2-3 | 14:07:00 | 0.34 | 1.30 | 102.350 | 346 | 91 | 86 | 256 | 263 | 54 |
| | 14:12:00 | | | 105.872 | | | | | | |
| 3-1 | 14:14:00 | 0.44 | 1.70 | 105.872 | 349 | 90 | 87 | 258 | 255 | 54 |
| 3-2 | 14:19:00 | 0.40 | 1.50 | 109.880 | 349 | 94 | 88 | 257 | 264 | 55 |
| 3-3 | 14:24:00 | 0.35 | 1.30 | 113.650 | 347 | 95 | 88 | 265 | 264 | 56 |
| | 14:29:00 | | | 117.250 | | | | | | |
| 4-1 | 14:31:00 | 0.43 | 1.60 | 117.250 | 370 | 93 | 89 | 252 | 263 | 56 |
| 4-2 | 14:36:00 | 0.39 | 1.50 | 121.180 | 375 | 96 | 89 | 256 | 262 | 57 |
| 4-3 | 14:41:00 | 0.30 | 1.10 | 124.890 | 376 | 96 | 90 | 270 | 264 | 58 |
| | 14:46:00 | | | 128.162 | | | | | | |

| | | | | | | | | | | |
|---------|---------|--|------|--------|-------|------|------|--|--|--|
| Total | 1:00:00 | | | 43.876 | | 88.9 | 84.3 | | | |
| Average | | | 1.44 | | 359.9 | 86.6 | | | | |
| Min | | | 1.10 | | 346.0 | 74.0 | | | | |
| Max | | | 1.70 | | 376.0 | 96.0 | | | | |

Impinger Weight Sheet - Run 2B

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/17/2023
 Test Method: 26A
 Weighed/Measured By: WAP
 Balance ID: LV3

Scale Calibration Check Date: 10/17/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250 | <u>250.0</u> |
| 500 | <u>500.0</u> |
| 750 | <u>750.0</u> |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 830.9 | 754.6 | 76.3 |
| 0.1N H2SO4 | 814.6 | 796.1 | 18.5 |
| Empty | 636.9 | 634.2 | 2.7 |
| 0.1N NaOH | 743.2 | 735.0 | 8.2 |
| 0.1N NaOH | 749.0 | 744.0 | 5.0 |
| Silica Gel | 857.5 | 844.1 | 13.4 |

| | | |
|--------------------------------|----------------------------------|-----------------------------|
| <u>3,774.6</u> Liquid Final | <u>3,663.9</u> Liquid Initial | <u>110.7</u> Liquid Gain |
| <u>857.5</u> Silica Final | <u>844.1</u> Silica Initial | <u>13.4</u> Silica Gain |

Run 3B - Method 26A

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Source Condition: Mill Off

Date: 10/17/23
 Start Time: 15:05
 End Time: 16:14

DRY GAS METER CONDITIONS

STACK CONDITIONS

| | | | | | |
|------------------------|--------|----------------------|---------------------|---------|----------------------|
| ΔH: | 1.43 | In. H ₂ O | Static Pressure | -0.50 | in. H ₂ O |
| Meter Temperature, Tm: | 97.9 | °F | Flue Pressure (Ps): | 24.76 | in. Hg. abs. |
| Sqrt ΔP: | 0.618 | In. H ₂ O | Carbon Dioxide: | 29.80 | % |
| Stack Temperature, Ts: | 372.7 | °F | Oxygen: | 4.20 | % |
| Meter Volume, Vm: | 44.657 | ft ³ | Nitrogen: | 66 | % |
| Meter Volume, Vmstd: | 34.830 | dscf | Gas Weight dry, Md: | 32.936 | lb/lb mole |
| Meter Volume, Vwstd: | 4.988 | wscf | Gas Weight wet, Ms: | 31.065 | lb/lb mole |
| Isokinetic Variance: | 107.6 | %I | Excess Air: | 31.760 | % |
| | | | Gas Velocity, Vs: | 45.205 | fps |
| Test Length: | 60.00 | in mins. | Volumetric Flow: | 223,809 | acfm |
| Nozzle Diameter: | 0.282 | in inches | Volumetric Flow: | 102,745 | dscfm |
| Barometric Pressure: | 24.80 | in Hg | Volumetric Flow: | 117,459 | scfm |

MOISTURE DETERMINATION

| | | | | | |
|---------------------------|--------|----|--------------------|-------|-------|
| Initial Impinger Content: | 3426.8 | ml | Silica Initial Wt. | 797.3 | grams |
| Final Impinger Content: | 3523.5 | ml | Silica Final Wt. | 806.5 | grams |
| Impinger Difference: | 96.7 | ml | Silica Difference: | 9.2 | grams |
| Total Water Gain: | 105.9 | | Moisture, Bws: | 0.125 | |

| Port- Point No. | Clock Time | Velocity | Orifice | Actual | Stack | Meter Temp | | Probe | Filter | Impinger |
|--------------------|---------------|---------------------------------|----------------------------|-------------------------------|------------|-------------|--------------|------------|-----------------|-----------------|
| | | Head Δp in. H ₂ O | ΔH in. H ₂ O | Meter Vol. ft ³ | Temp °F | Inlet °F | Outlet °F | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1 | 15:05:00 | 0.42 | 1.60 | 129.827 | 379 | 93 | 92 | 252 | 250 | 52 |
| 1-2 | 15:10:00 | 0.40 | 1.50 | 133.670 | 380 | 97 | 93 | 255 | 254 | 52 |
| 1-3 | 15:15:00 | 0.33 | 1.20 | 137.480 | 377 | 99 | 95 | 257 | 264 | 52 |
| | 15:20:00 | | | 140.902 | | | | | | |
| 2-1 | 15:22:00 | 0.40 | 1.50 | 140.902 | 378 | 99 | 96 | 257 | 264 | 53 |
| 2-2 | 15:27:00 | 0.41 | 1.50 | 144.690 | 380 | 104 | 99 | 255 | 264 | 53 |
| 2-3 | 15:32:00 | 0.33 | 1.20 | 148.540 | 377 | 106 | 99 | 257 | 263 | 54 |
| | 15:37:00 | | | 152.039 | | | | | | |
| 3-1 | 15:39:00 | 0.42 | 1.60 | 152.039 | 379 | 101 | 98 | 259 | 265 | 55 |
| 3-2 | 15:44:00 | 0.40 | 1.50 | 155.940 | 381 | 101 | 98 | 262 | 265 | 55 |
| 3-3 | 15:49:00 | 0.32 | 1.20 | 159.710 | 377 | 100 | 98 | 261 | 266 | 56 |
| | 15:54:00 | | | 163.120 | | | | | | |
| 4-1 | 15:59:00 | 0.43 | 1.60 | 163.120 | 360 | 97 | 96 | 250 | 266 | 57 |
| 4-2 | 16:04:00 | 0.40 | 1.50 | 167.090 | 353 | 98 | 96 | 253 | 265 | 57 |
| 4-3 | 16:09:00 | 0.34 | 1.30 | 170.900 | 351 | 98 | 96 | 259 | 264 | 58 |
| | 16:14:00 | | | 174.484 | | | | | | |

| | | | | | | | | | | |
|---------|---------|--|------|--------|-------|------|-------|--|--|--|
| Total | 1:00:00 | | | 44.657 | | 99.4 | 96.3 | | | |
| Average | | | 1.43 | | 372.7 | | 97.9 | | | |
| Min | | | 1.20 | | 351.0 | | 92.0 | | | |
| Max | | | 1.60 | | 381.0 | | 106.0 | | | |

Impinger Weight Sheet - Run 3B

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Test Location: Main Kiln Stack
 Project #: M234207
 Date: 10/17/2023
 Test Method: 26A
 Weighed/Measured By: WAP
 Balance ID: LV3

Scale Calibration Check Date: 10/17/2023
 Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250 | 250.0 |
| 500 | 500.0 |
| 750 | 750.0 |

| IMPINGER CONTENTS | FINAL MLS / GRAMS | INITIAL MLS / GRAMS | GAIN MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4 | 816.9 | 743.8 | 73.1 |
| 0.1N H2SO4 | 705.1 | 685.9 | 19.2 |
| Empty | 646.1 | 642.7 | 3.4 |
| 0.1N NaOH | 743.3 | 742.7 | 0.6 |
| 0.1N NaOH | 612.1 | 611.7 | 0.4 |
| Silica Gel | 806.5 | 797.3 | 9.2 |

| | | |
|---------------------|-----------------------|--------------------|
| 3,523.5 | 3,426.8 | 96.7 |
| Liquid Final | Liquid Initial | Liquid Gain |
| 806.5 | 797.3 | 9.2 |
| Silica Final | Silica Initial | Silica Gain |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Test Location: Main Kiln
 Date: 10/17/23

Run 1

| Spectrum | Time | FTIR Data | | | | | Cell Temp | Pressure | Analyzer Data |
|----------------|------|--------------|--------------|--------------|-------------|---------------|-------------|-------------|---------------|
| | | H2O % | CO2 % (wet) | HCN ppmvw | HF ppmvw | O2 % (dry) | | | |
| Run1_0377.LAB | 8:00 | 12.25 | 25.52 | 12.40 | 0.10 | 190.43 | 0.85 | 4.24 | |
| Run1_0378.LAB | 8:01 | 12.24 | 25.62 | 12.59 | 0.10 | 190.47 | 0.85 | 4.35 | |
| Run1_0379.LAB | 8:02 | 12.51 | 25.46 | 12.34 | 0.10 | 190.55 | 0.85 | 4.40 | |
| Run1_0380.LAB | 8:03 | 12.20 | 25.11 | 12.40 | 0.10 | 190.67 | 0.85 | 4.81 | |
| Run1_0381.LAB | 8:04 | 12.26 | 25.38 | 12.33 | 0.10 | 190.47 | 0.85 | 4.34 | |
| Run1_0382.LAB | 8:05 | 12.68 | 25.31 | 12.18 | 0.10 | 190.57 | 0.85 | 4.30 | |
| Run1_0383.LAB | 8:06 | 12.16 | 25.59 | 12.36 | 0.10 | 190.67 | 0.85 | 4.19 | |
| Run1_0384.LAB | 8:07 | 12.35 | 25.52 | 12.43 | 0.10 | 190.49 | 0.85 | 4.31 | |
| Run1_0385.LAB | 8:08 | 12.50 | 25.72 | 12.59 | 0.10 | 190.55 | 0.85 | 4.09 | |
| Run1_0386.LAB | 8:09 | 12.13 | 25.22 | 12.66 | 0.10 | 190.54 | 0.85 | 4.54 | |
| Run1_0387.LAB | 8:10 | 12.28 | 25.65 | 12.63 | 0.10 | 190.59 | 0.85 | 4.30 | |
| Run1_0388.LAB | 8:11 | 12.87 | 25.60 | 12.69 | 0.10 | 190.70 | 0.85 | 3.60 | |
| Run1_0389.LAB | 8:12 | 12.17 | 25.29 | 12.78 | 0.10 | 190.70 | 0.85 | 4.76 | |
| Run1_0390.LAB | 8:13 | 12.44 | 25.02 | 12.66 | 0.10 | 190.61 | 0.85 | 4.47 | |
| Run1_0391.LAB | 8:14 | 12.18 | 25.46 | 12.70 | 0.10 | 190.51 | 0.85 | 4.55 | |
| Run1_0392.LAB | 8:15 | 12.40 | 25.56 | 13.00 | 0.10 | 190.54 | 0.85 | 4.08 | |
| Run1_0393.LAB | 8:16 | 12.23 | 25.67 | 13.21 | 0.10 | 190.52 | 0.85 | 4.18 | |
| Run1_0394.LAB | 8:17 | 12.08 | 25.22 | 13.22 | 0.10 | 190.53 | 0.85 | 4.31 | |
| Run1_0395.LAB | 8:18 | 12.13 | 25.72 | 13.12 | 0.10 | 190.45 | 0.85 | 4.51 | |
| Run1_0396.LAB | 8:19 | 12.14 | 25.56 | 13.19 | 0.10 | 190.40 | 0.85 | 4.17 | |
| Run1_0397.LAB | 8:20 | 12.37 | 26.05 | 12.80 | 0.10 | 190.36 | 0.85 | 4.34 | |
| Run1_0398.LAB | 8:21 | 12.38 | 26.00 | 13.17 | 0.10 | 190.30 | 0.85 | 3.62 | |
| Run1_0399.LAB | 8:22 | 12.64 | 25.40 | 13.17 | 0.10 | 190.19 | 0.85 | 3.75 | |
| Run1_0400.LAB | 8:23 | 12.15 | 25.57 | 13.21 | 0.10 | 190.22 | 0.85 | 4.24 | |
| Run1_0401.LAB | 8:24 | 12.60 | 25.64 | 13.14 | 0.10 | 190.36 | 0.85 | 3.98 | |
| Run1_0402.LAB | 8:25 | 12.40 | 25.74 | 12.98 | 0.10 | 190.53 | 0.85 | 3.75 | |
| Run1_0403.LAB | 8:26 | 12.68 | 26.13 | 12.86 | 0.10 | 190.57 | 0.85 | 3.86 | |
| Run1_0404.LAB | 8:27 | 12.26 | 25.83 | 13.39 | 0.10 | 190.64 | 0.85 | 3.57 | |
| Run1_0405.LAB | 8:28 | 12.11 | 25.28 | 13.22 | 0.10 | 190.68 | 0.85 | 4.03 | |
| Run1_0406.LAB | 8:29 | 12.17 | 25.59 | 13.48 | 0.10 | 190.59 | 0.85 | 4.53 | |
| Run1_0407.LAB | 8:30 | 12.34 | 26.17 | 13.18 | 0.10 | 190.59 | 0.85 | 4.20 | |
| Run1_0408.LAB | 8:31 | 12.73 | 25.82 | 12.96 | 0.10 | 190.61 | 0.85 | 3.83 | |
| Run1_0409.LAB | 8:32 | 12.27 | 25.32 | 13.21 | 0.10 | 190.54 | 0.85 | 3.66 | |
| Run1_0410.LAB | 8:33 | 12.33 | 25.47 | 13.48 | 0.10 | 190.40 | 0.85 | 4.14 | |
| Run1_0411.LAB | 8:34 | 12.24 | 25.55 | 13.57 | 0.10 | 190.51 | 0.85 | 4.28 | |
| Run1_0412.LAB | 8:35 | 12.08 | 25.03 | 13.31 | 0.10 | 190.49 | 0.85 | 4.30 | |
| Run1_0413.LAB | 8:36 | 12.10 | 25.04 | 13.04 | 0.10 | 190.42 | 0.85 | 4.46 | |
| Run1_0414.LAB | 8:37 | 12.26 | 25.49 | 12.87 | 0.10 | 190.28 | 0.85 | 5.05 | |
| Run1_0415.LAB | 8:38 | 12.37 | 25.45 | 12.84 | 0.10 | 190.36 | 0.85 | 4.34 | |
| Run1_0416.LAB | 8:39 | 12.75 | 25.77 | 13.16 | 0.10 | 190.38 | 0.85 | 4.21 | |
| Run1_0417.LAB | 8:40 | 12.50 | 25.74 | 13.37 | 0.10 | 190.38 | 0.85 | 3.97 | |
| Run1_0418.LAB | 8:41 | 12.22 | 25.28 | 13.27 | 0.10 | 190.43 | 0.85 | 3.79 | |
| Run1_0419.LAB | 8:42 | 12.32 | 25.79 | 13.13 | 0.10 | 190.34 | 0.85 | 4.02 | |
| Run1_0420.LAB | 8:43 | 12.60 | 25.41 | 13.08 | 0.10 | 190.38 | 0.85 | 4.38 | |
| Run1_0421.LAB | 8:44 | 12.64 | 25.37 | 13.02 | 0.10 | 190.42 | 0.85 | 3.81 | |
| Run1_0422.LAB | 8:45 | 12.72 | 25.52 | 13.03 | 0.10 | 190.45 | 0.85 | 4.09 | |
| Run1_0423.LAB | 8:46 | 12.15 | 25.26 | 13.24 | 0.10 | 190.39 | 0.85 | 4.07 | |
| Run1_0424.LAB | 8:47 | 12.52 | 25.33 | 13.21 | 0.10 | 190.34 | 0.85 | 3.90 | |
| Run1_0425.LAB | 8:48 | 12.66 | 25.28 | 13.00 | 0.10 | 190.33 | 0.85 | 4.54 | |
| Run1_0426.LAB | 8:49 | 12.19 | 25.37 | 13.47 | 0.10 | 190.33 | 0.85 | 4.30 | |
| Run1_0427.LAB | 8:50 | 12.76 | 25.52 | 13.05 | 0.10 | 190.41 | 0.85 | 4.25 | |
| Run1_0428.LAB | 8:51 | 12.23 | 25.32 | 13.27 | 0.10 | 190.45 | 0.85 | 4.34 | |
| Run1_0429.LAB | 8:52 | 12.77 | 25.44 | 13.21 | 0.10 | 190.52 | 0.85 | 4.03 | |
| Run1_0430.LAB | 8:53 | 12.05 | 24.77 | 13.62 | 0.10 | 190.49 | 0.85 | 4.42 | |
| Run1_0431.LAB | 8:54 | 12.30 | 25.44 | 13.83 | 0.10 | 190.55 | 0.85 | 4.19 | |
| Run1_0432.LAB | 8:55 | 12.56 | 25.49 | 13.43 | 0.10 | 190.45 | 0.85 | 4.94 | |
| Run1_0433.LAB | 8:56 | 12.04 | 25.15 | 13.25 | 0.10 | 190.47 | 0.85 | 4.57 | |
| Run1_0434.LAB | 8:57 | 12.15 | 24.64 | 13.22 | 0.10 | 190.41 | 0.85 | 4.32 | |
| Run1_0435.LAB | 8:58 | 12.58 | 25.37 | 13.42 | 0.10 | 190.48 | 0.85 | 4.35 | |
| Run1_0436.LAB | 8:59 | 12.21 | 25.21 | 13.75 | 0.10 | 190.45 | 0.85 | 5.16 | |
| Average | | 12.36 | 25.47 | 13.04 | 0.10 | 190.47 | 0.85 | 4.23 | |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Test Location: Main Kiln
 Date: 10/17/23

Run 2

| Spectrum | Time | FTIR Data | | | | | Cell Temp | Pressure | Analyzer Data O2 % (dry) |
|----------------|-------|--------------|--------------|--------------|-------------|---------------|-------------|-------------|-----------------------------|
| | | H2O % | CO2 % (wet) | HCN ppmvw | HF ppmvw | | | | |
| RUN2_0743.LAB | 13:40 | 12.72 | 23.9 | 11.37 | 0.10 | 189.8 | 0.84 | 5.35 | |
| RUN2_0744.LAB | 13:41 | 12.95 | 24.2 | 11.14 | 0.10 | 189.9 | 0.84 | 5.16 | |
| RUN2_0745.LAB | 13:42 | 12.71 | 23.7 | 10.93 | 0.10 | 190.1 | 0.84 | 5.61 | |
| RUN2_0746.LAB | 13:43 | 12.67 | 23.7 | 10.67 | 0.10 | 190.0 | 0.84 | 5.58 | |
| RUN2_0747.LAB | 13:44 | 12.53 | 23.4 | 10.68 | 0.10 | 189.9 | 0.84 | 6.06 | |
| RUN2_0748.LAB | 13:45 | 12.58 | 23.6 | 10.94 | 0.10 | 189.7 | 0.84 | 5.68 | |
| RUN2_0749.LAB | 13:46 | 12.36 | 24.0 | 11.21 | 0.10 | 190.0 | 0.84 | 5.40 | |
| RUN2_0750.LAB | 13:47 | 12.49 | 23.8 | 11.47 | 0.10 | 190.0 | 0.84 | 5.71 | |
| RUN2_0751.LAB | 13:48 | 12.44 | 23.8 | 11.30 | 0.10 | 189.7 | 0.84 | 5.69 | |
| RUN2_0752.LAB | 13:49 | 12.57 | 24.2 | 11.01 | 0.10 | 189.3 | 0.84 | 5.34 | |
| RUN2_0753.LAB | 13:50 | 12.41 | 23.6 | 10.90 | 0.10 | 189.6 | 0.84 | 5.64 | |
| RUN2_0754.LAB | 13:51 | 12.36 | 23.6 | 10.99 | 0.10 | 189.7 | 0.84 | 5.86 | |
| RUN2_0755.LAB | 13:52 | 12.42 | 23.7 | 11.39 | 0.10 | 189.7 | 0.84 | 5.87 | |
| RUN2_0756.LAB | 13:53 | 12.65 | 24.4 | 11.58 | 0.10 | 189.7 | 0.84 | 5.33 | |
| RUN2_0757.LAB | 13:54 | 12.52 | 23.8 | 10.90 | 0.10 | 189.8 | 0.84 | 5.33 | |
| RUN2_0758.LAB | 13:55 | 12.32 | 23.5 | 10.95 | 0.10 | 189.8 | 0.84 | 5.88 | |
| RUN2_0759.LAB | 13:56 | 12.42 | 23.9 | 11.33 | 0.10 | 189.6 | 0.84 | 5.73 | |
| RUN2_0760.LAB | 13:57 | 12.35 | 23.8 | 11.29 | 0.10 | 189.7 | 0.84 | 5.67 | |
| RUN2_0761.LAB | 13:58 | 12.60 | 24.2 | 11.37 | 0.10 | 190.0 | 0.84 | 5.61 | |
| RUN2_0762.LAB | 13:59 | 12.33 | 23.5 | 10.94 | 0.10 | 189.9 | 0.84 | 5.58 | |
| RUN2_0763.LAB | 14:00 | 12.46 | 23.8 | 11.03 | 0.10 | 189.8 | 0.84 | 5.93 | |
| RUN2_0764.LAB | 14:01 | 12.56 | 24.0 | 11.22 | 0.10 | 189.8 | 0.84 | 5.62 | |
| RUN2_0765.LAB | 14:02 | 12.49 | 23.9 | 11.25 | 0.10 | 189.7 | 0.84 | 5.47 | |
| RUN2_0766.LAB | 14:03 | 12.52 | 24.0 | 11.14 | 0.10 | 189.9 | 0.84 | 5.62 | |
| RUN2_0767.LAB | 14:04 | 12.60 | 24.1 | 11.15 | 0.10 | 189.9 | 0.84 | 5.35 | |
| RUN2_0768.LAB | 14:05 | 12.52 | 23.9 | 10.98 | 0.10 | 189.7 | 0.84 | 5.24 | |
| RUN2_0769.LAB | 14:06 | 12.64 | 24.3 | 11.21 | 0.10 | 189.7 | 0.84 | 5.52 | |
| RUN2_0770.LAB | 14:07 | 12.54 | 24.0 | 11.48 | 0.10 | 189.8 | 0.84 | 5.13 | |
| RUN2_0771.LAB | 14:08 | 12.34 | 23.8 | 11.65 | 0.10 | 189.8 | 0.84 | 5.36 | |
| RUN2_0772.LAB | 14:09 | 12.11 | 24.3 | 12.03 | 0.10 | 189.8 | 0.84 | 5.81 | |
| RUN2_0773.LAB | 14:10 | 12.67 | 24.4 | 11.68 | 0.10 | 189.7 | 0.84 | 5.60 | |
| RUN2_0774.LAB | 14:11 | 12.60 | 23.9 | 11.40 | 0.10 | 189.8 | 0.84 | 5.00 | |
| RUN2_0775.LAB | 14:12 | 12.37 | 24.7 | 11.93 | 0.10 | 189.6 | 0.84 | 5.38 | |
| RUN2_0776.LAB | 14:13 | 12.60 | 24.6 | 11.59 | 0.10 | 189.6 | 0.84 | 4.92 | |
| RUN2_0777.LAB | 14:14 | 12.80 | 24.8 | 11.64 | 0.10 | 189.6 | 0.84 | 4.83 | |
| RUN2_0778.LAB | 14:15 | 12.05 | 23.6 | 11.76 | 0.10 | 189.6 | 0.84 | 4.53 | |
| RUN2_0779.LAB | 14:16 | 12.27 | 24.1 | 12.31 | 0.10 | 189.7 | 0.84 | 5.60 | |
| RUN2_0780.LAB | 14:17 | 12.41 | 25.0 | 12.41 | 0.10 | 189.7 | 0.84 | 6.07 | |
| RUN2_0781.LAB | 14:18 | 12.37 | 24.1 | 12.04 | 0.10 | 189.7 | 0.84 | 5.00 | |
| RUN2_0782.LAB | 14:19 | 12.26 | 24.6 | 12.35 | 0.10 | 189.6 | 0.84 | 5.02 | |
| RUN2_0783.LAB | 14:20 | 12.50 | 24.8 | 12.25 | 0.10 | 189.7 | 0.84 | 5.58 | |
| RUN2_0784.LAB | 14:21 | 12.44 | 24.3 | 11.91 | 0.10 | 190.0 | 0.84 | 5.03 | |
| RUN2_0785.LAB | 14:22 | 12.55 | 24.5 | 12.03 | 0.10 | 189.8 | 0.84 | 5.00 | |
| RUN2_0786.LAB | 14:23 | 12.58 | 24.5 | 11.92 | 0.10 | 189.8 | 0.84 | 5.20 | |
| RUN2_0787.LAB | 14:24 | 12.66 | 24.8 | 11.63 | 0.10 | 189.7 | 0.84 | 4.96 | |
| RUN2_0788.LAB | 14:25 | 12.77 | 24.7 | 10.72 | 0.10 | 189.6 | 0.84 | 4.95 | |
| RUN2_0789.LAB | 14:26 | 12.36 | 25.0 | 12.99 | 0.10 | 189.9 | 0.84 | 4.49 | |
| RUN2_0790.LAB | 14:27 | 12.11 | 25.8 | 13.26 | 0.10 | 189.7 | 0.84 | 4.51 | |
| RUN2_0791.LAB | 14:28 | 12.60 | 26.4 | 13.20 | 0.10 | 189.7 | 0.84 | 4.88 | |
| RUN2_0792.LAB | 14:29 | 12.61 | 26.1 | 13.06 | 0.10 | 189.6 | 0.84 | 4.34 | |
| RUN2_0793.LAB | 14:30 | 12.42 | 25.0 | 12.76 | 0.10 | 189.9 | 0.84 | 3.62 | |
| RUN2_0794.LAB | 14:31 | 12.46 | 25.3 | 12.77 | 0.10 | 190.1 | 0.84 | 3.70 | |
| RUN2_0795.LAB | 14:32 | 12.40 | 25.3 | 12.64 | 0.10 | 190.0 | 0.84 | 4.64 | |
| RUN2_0796.LAB | 14:33 | 12.44 | 25.0 | 12.60 | 0.10 | 189.9 | 0.84 | 4.56 | |
| RUN2_0797.LAB | 14:34 | 12.63 | 26.0 | 12.44 | 0.10 | 189.7 | 0.84 | 4.48 | |
| RUN2_0798.LAB | 14:35 | 12.75 | 26.3 | 12.53 | 0.10 | 189.6 | 0.84 | 4.84 | |
| RUN2_0799.LAB | 14:36 | 12.49 | 25.6 | 13.21 | 0.10 | 189.6 | 0.84 | 4.31 | |
| RUN2_0800.LAB | 14:37 | 12.54 | 25.7 | 13.23 | 0.10 | 189.7 | 0.84 | 3.28 | |
| RUN2_0801.LAB | 14:38 | 12.45 | 25.8 | 13.51 | 0.10 | 189.7 | 0.84 | 4.58 | |
| RUN2_0802.LAB | 14:39 | 12.47 | 25.8 | 13.43 | 0.10 | 189.7 | 0.84 | 4.21 | |
| Average | | 12.50 | 24.45 | 11.78 | 0.10 | 189.76 | 0.84 | 5.17 | |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Test Location: Main Kiln
 Date: 10/17/23

Run 3

| Spectrum | Time | FTIR Data | | | | | Cell Temp | Pressure | Analyzer Data O2 % (dry) |
|----------------|-------|--------------|--------------|--------------|-------------|---------------|-------------|-------------|-----------------------------|
| | | H2O % | CO2 % (wet) | HCN ppmvw | HF ppmvw | | | | |
| RUN3_0869.LAB | 15:05 | 12.60 | 26.7 | 13.73 | 0.10 | 189.9 | 0.83 | 3.59 | |
| RUN3_0870.LAB | 15:06 | 12.74 | 26.5 | 14.09 | 0.10 | 189.8 | 0.83 | 4.18 | |
| RUN3_0871.LAB | 15:07 | 12.52 | 26.0 | 14.14 | 0.10 | 189.9 | 0.83 | 3.81 | |
| RUN3_0872.LAB | 15:08 | 12.66 | 26.3 | 13.60 | 0.10 | 189.7 | 0.83 | 4.39 | |
| RUN3_0873.LAB | 15:09 | 12.40 | 25.7 | 13.51 | 0.10 | 189.5 | 0.83 | 4.30 | |
| RUN3_0874.LAB | 15:10 | 12.45 | 25.6 | 13.47 | 0.10 | 189.4 | 0.83 | 4.46 | |
| RUN3_0875.LAB | 15:11 | 12.49 | 26.0 | 13.37 | 0.10 | 189.4 | 0.83 | 3.86 | |
| RUN3_0876.LAB | 15:12 | 12.64 | 26.3 | 13.55 | 0.10 | 189.6 | 0.83 | 3.58 | |
| RUN3_0877.LAB | 15:13 | 12.57 | 26.2 | 13.45 | 0.10 | 189.6 | 0.83 | 4.46 | |
| RUN3_0878.LAB | 15:14 | 12.33 | 25.1 | 13.18 | 0.10 | 189.5 | 0.83 | 4.82 | |
| RUN3_0879.LAB | 15:15 | 12.40 | 25.4 | 13.55 | 0.10 | 189.3 | 0.83 | 4.42 | |
| RUN3_0880.LAB | 15:16 | 12.45 | 25.9 | 14.07 | 0.10 | 189.4 | 0.83 | 4.72 | |
| RUN3_0881.LAB | 15:17 | 12.23 | 25.9 | 14.16 | 0.10 | 189.6 | 0.83 | 4.45 | |
| RUN3_0882.LAB | 15:18 | 11.89 | 26.2 | 14.29 | 0.10 | 189.4 | 0.83 | 4.40 | |
| RUN3_0883.LAB | 15:19 | 12.52 | 26.5 | 14.19 | 0.10 | 189.4 | 0.83 | 4.12 | |
| RUN3_0884.LAB | 15:20 | 12.33 | 26.8 | 13.61 | 0.10 | 189.2 | 0.83 | 3.44 | |
| RUN3_0885.LAB | 15:21 | 12.69 | 26.7 | 13.70 | 0.10 | 189.4 | 0.83 | 3.50 | |
| RUN3_0886.LAB | 15:22 | 12.72 | 26.4 | 14.29 | 0.10 | 189.6 | 0.84 | 3.67 | |
| RUN3_0887.LAB | 15:23 | 12.50 | 25.9 | 14.49 | 0.10 | 189.6 | 0.83 | 4.39 | |
| RUN3_0888.LAB | 15:24 | 11.96 | 25.7 | 14.27 | 0.10 | 189.4 | 0.84 | 4.81 | |
| RUN3_0889.LAB | 15:25 | 12.33 | 26.0 | 14.30 | 0.10 | 189.4 | 0.84 | 4.45 | |
| RUN3_0890.LAB | 15:26 | 11.84 | 26.0 | 14.61 | 0.10 | 189.3 | 0.84 | 4.73 | |
| RUN3_0891.LAB | 15:27 | 11.96 | 25.9 | 14.60 | 0.10 | 189.6 | 0.84 | 4.60 | |
| RUN3_0892.LAB | 15:28 | 12.72 | 26.4 | 14.01 | 0.10 | 189.8 | 0.84 | 3.87 | |
| RUN3_0893.LAB | 15:29 | 12.73 | 26.6 | 14.08 | 0.10 | 190.0 | 0.84 | 3.56 | |
| RUN3_0894.LAB | 15:30 | 12.58 | 26.7 | 14.28 | 0.10 | 190.1 | 0.84 | 3.69 | |
| RUN3_0895.LAB | 15:31 | 12.49 | 26.6 | 14.29 | 0.10 | 189.8 | 0.84 | 3.60 | |
| RUN3_0896.LAB | 15:32 | 12.49 | 26.3 | 14.59 | 0.10 | 189.9 | 0.84 | 4.14 | |
| RUN3_0897.LAB | 15:33 | 12.60 | 26.3 | 14.59 | 0.10 | 189.8 | 0.84 | 3.97 | |
| RUN3_0898.LAB | 15:34 | 12.65 | 26.1 | 14.69 | 0.10 | 189.6 | 0.84 | 3.83 | |
| RUN3_0899.LAB | 15:35 | 12.33 | 26.9 | 14.25 | 0.10 | 189.6 | 0.84 | 4.08 | |
| RUN3_0900.LAB | 15:36 | 12.80 | 26.8 | 14.60 | 0.10 | 189.6 | 0.84 | 3.55 | |
| RUN3_0901.LAB | 15:37 | 12.69 | 26.5 | 14.74 | 0.10 | 189.6 | 0.84 | 3.72 | |
| RUN3_0902.LAB | 15:38 | 12.31 | 26.4 | 15.07 | 0.10 | 189.5 | 0.84 | 4.10 | |
| RUN3_0903.LAB | 15:39 | 12.42 | 26.6 | 14.88 | 0.10 | 189.6 | 0.84 | 3.98 | |
| RUN3_0904.LAB | 15:40 | 12.40 | 26.8 | 14.81 | 0.10 | 189.6 | 0.84 | 3.96 | |
| RUN3_0905.LAB | 15:41 | 12.32 | 27.2 | 14.39 | 0.10 | 189.6 | 0.84 | 3.83 | |
| RUN3_0906.LAB | 15:42 | 12.71 | 26.6 | 14.69 | 0.10 | 189.7 | 0.84 | 3.59 | |
| RUN3_0907.LAB | 15:43 | 12.78 | 26.6 | 14.84 | 0.10 | 189.9 | 0.84 | 3.77 | |
| RUN3_0908.LAB | 15:44 | 12.37 | 26.8 | 14.84 | 0.10 | 189.7 | 0.84 | 3.76 | |
| RUN3_0909.LAB | 15:45 | 12.63 | 26.8 | 14.70 | 0.10 | 189.6 | 0.84 | 3.86 | |
| RUN3_0910.LAB | 15:46 | 12.26 | 26.8 | 14.99 | 0.10 | 189.7 | 0.84 | 3.74 | |
| RUN3_0911.LAB | 15:47 | 11.25 | 26.8 | 15.66 | 0.10 | 189.9 | 0.84 | 3.72 | |
| RUN3_0912.LAB | 15:48 | 12.29 | 27.0 | 15.30 | 0.10 | 189.6 | 0.84 | 3.99 | |
| RUN3_0913.LAB | 15:49 | 12.66 | 26.6 | 14.87 | 0.10 | 189.5 | 0.84 | 3.91 | |
| RUN3_0914.LAB | 15:50 | 12.28 | 26.4 | 14.78 | 0.10 | 189.6 | 0.84 | 3.93 | |
| RUN3_0915.LAB | 15:51 | 12.57 | 26.3 | 14.82 | 0.10 | 189.7 | 0.84 | 4.15 | |
| RUN3_0916.LAB | 15:52 | 12.64 | 26.1 | 14.63 | 0.10 | 189.7 | 0.84 | 4.00 | |
| RUN3_0917.LAB | 15:53 | 12.15 | 25.0 | 14.05 | 0.10 | 189.7 | 0.84 | 4.13 | |
| RUN3_0918.LAB | 15:54 | 12.09 | 24.9 | 13.89 | 0.10 | 189.8 | 0.84 | 4.54 | |
| RUN3_0919.LAB | 15:55 | 12.16 | 25.3 | 13.74 | 0.10 | 189.9 | 0.84 | 4.84 | |
| RUN3_0920.LAB | 15:56 | 12.31 | 25.5 | 13.79 | 0.10 | 189.8 | 0.84 | 4.91 | |
| RUN3_0921.LAB | 15:57 | 12.21 | 25.6 | 14.22 | 0.10 | 189.7 | 0.84 | 4.67 | |
| RUN3_0922.LAB | 15:58 | 12.09 | 25.0 | 14.13 | 0.10 | 189.6 | 0.84 | 4.45 | |
| RUN3_0923.LAB | 15:59 | 11.92 | 24.7 | 13.69 | 0.10 | 189.6 | 0.84 | 4.74 | |
| RUN3_0924.LAB | 16:00 | 11.98 | 24.9 | 13.92 | 0.10 | 189.7 | 0.84 | 4.92 | |
| RUN3_0925.LAB | 16:01 | 12.47 | 26.1 | 13.27 | 0.10 | 189.7 | 0.84 | 5.11 | |
| RUN3_0926.LAB | 16:02 | 12.64 | 25.8 | 13.93 | 0.10 | 189.6 | 0.84 | 5.03 | |
| RUN3_0927.LAB | 16:03 | 12.63 | 25.5 | 14.24 | 0.10 | 189.6 | 0.84 | 4.23 | |
| RUN3_0928.LAB | 16:04 | 12.60 | 25.0 | 14.02 | 0.10 | 189.6 | 0.84 | 4.36 | |
| Average | | 12.41 | 26.13 | 14.24 | 0.10 | 189.63 | 0.84 | 4.16 | |

Method 1 and 2 Cyclonic Flow Check Data

Project Number: M234207
Client: GCC Rio Grande, Inc.
Facility: Pueblo Plant
Location: Main Kiln Stack
Pitot ID: S8-031A
Pitot Coefficient: 0.820
Probe Length: 6

Source Condition: Mill On
Run No.: 1
Date: 10/18/2023
Start Time: 7:30
End Time: 8:00
RM Testers:
Port Length: 9.50




| Port | Point | DP (in. H ₂ O) | Sqrt. DP | Temp (°F) | Yaw (o) | Velocity (V) | Port | Point | DP (in. H ₂ O) | Sqrt. DP | Temp (°F) | Yaw (o) | Velocity (V) | |
|------|-------|------------------------------|-------------|--------------|------------|-----------------|------|-------|------------------------------|-------------|--------------|------------|-----------------|-------|
| A | 1 | 0.51 | 0.7141 | 287.0 | 2.0 | 2.0 | C | 1 | 0.63 | 0.7937 | 289.0 | 2.0 | 2.0 | 53.23 |
| A | 2 | 0.55 | 0.7416 | 291.0 | 6.0 | 6.0 | C | 2 | 0.55 | 0.7416 | 291.0 | 7.0 | 7.0 | 49.80 |
| A | 3 | 0.43 | 0.6557 | 294.0 | 4.0 | 4.0 | C | 3 | 0.50 | 0.7071 | 291.0 | 4.0 | 4.0 | 47.48 |
| | | | | | | | | | | | | | | |
| B | 1 | 0.63 | 0.7937 | 292.0 | 3.0 | 3.0 | D | 1 | 0.57 | 0.7550 | 293.0 | 3.0 | 3.0 | 50.76 |
| B | 2 | 0.58 | 0.7616 | 292.0 | 7.0 | 7.0 | D | 2 | 0.55 | 0.7416 | 295.0 | 5.0 | 5.0 | 49.93 |
| B | 3 | 0.47 | 0.6856 | 291.0 | 5.0 | 5.0 | D | 3 | 0.49 | 0.7000 | 295.0 | 4.0 | 4.0 | 47.13 |




Average Yaw Angle 4.3 °

Stratification Test Results Summary
GCC Rio Grande, Inc.
Pueblo Plant
Main Kiln
October 18, 2023

Number of Ports Sampled: 1
Number of Points per Port: 3
Total Number of Traverse Points: 3

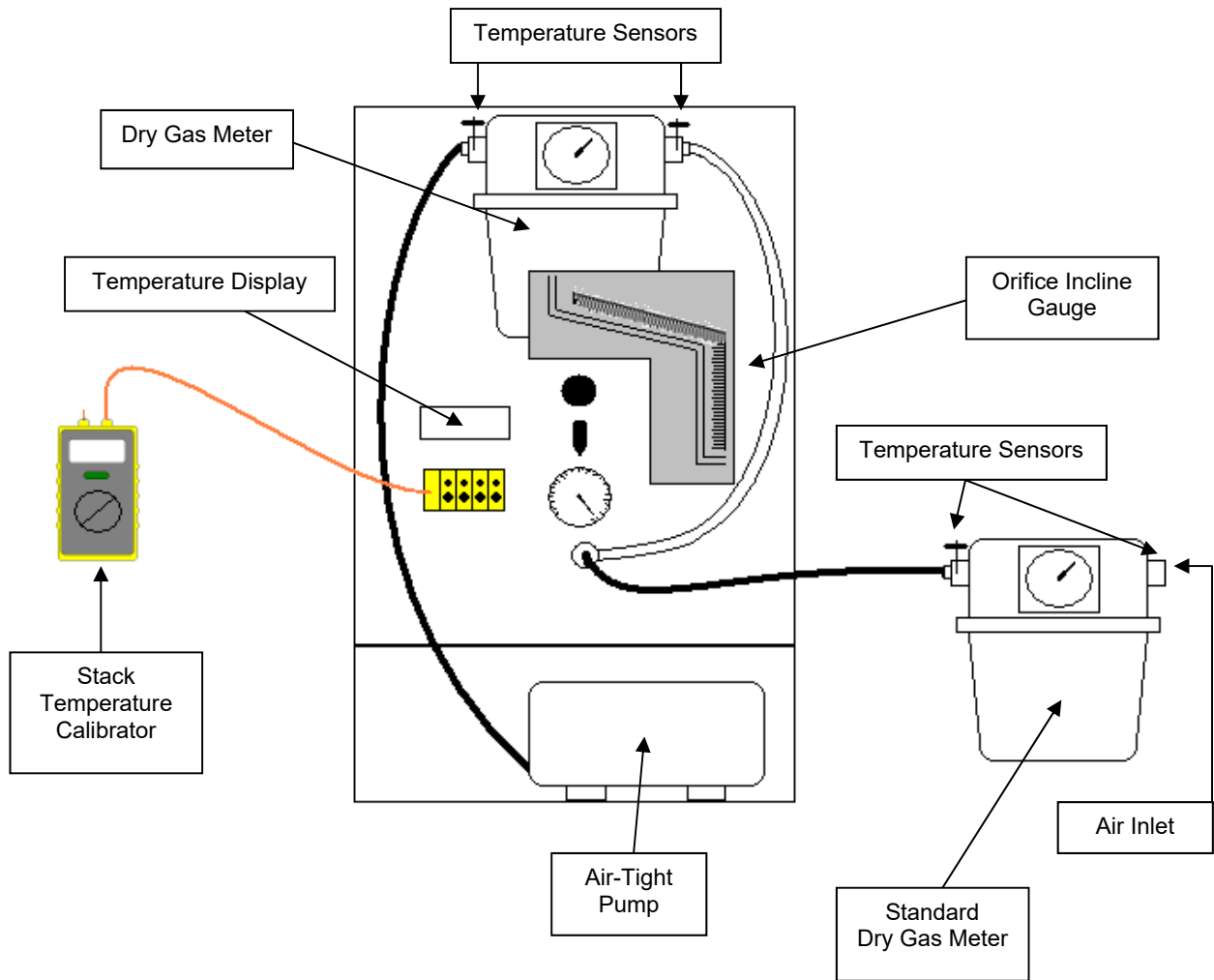
| Port No. | Point No. | Time | O ₂ % | Actual % Difference O ₂ % | Mean Difference O ₂ % |
|----------------|-----------|------|------------------|--------------------------------------|----------------------------------|
| 1 | 1 | 8:30 | 10.07 | 0.47 | 0.05 |
| | 2 | 8:34 | 9.94 | 0.83 | 0.08 |
| | 3 | 8:38 | 10.06 | 0.37 | 0.04 |
| Average | | | 10.02 | | |

One point traverse (<5% difference) 
Three point traverse (0.4, 1.2, and 2.0 meters), <10% difference 
Twelve point traverse (Method 1 points) >10% difference 

One point traverse (<0.3% mean difference) 
Three point traverse (0.4, 1.2, and 2.0 meters), < 0.5% mean difference for O₂ 
Twelve point traverse (Method 1 points) >0.5% mean difference for O₂ 

Appendix G - Calibration Data

Dry Gas Meter/Control Module Calibration Diagram



Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM4
 Standard Meter No. 18654513
 Standard Meter (Y) 1.00630

Date: October 5, 2023
 Calibrated By: PJC1
 Barometric Pressure: 25.08

| Run Number | Orifice Setting in H ₂ O Chg (H) | Standard Meter Gas Volume vr | Dry Gas Meter Gas Volume vd | Standard Meter Temp. F° tr | Dry Gas Meter Inlet Temp. F° tdi | Dry Gas Meter Outlet Temp. F° tdo | Dry Gas Meter Avg. Temp. F° td | Time Min | Time Sec | Y | Chg (H) |
|------------|---|------------------------------|-----------------------------|----------------------------|----------------------------------|-----------------------------------|--------------------------------|----------|----------|-------|---------|
| Final | | 754.625 | 515.870 | 67 | 72 | 72 | | | | | |
| Initial | | 750.054 | 511.167 | 66 | 71 | 71 | | | | | |
| Difference | 1 0.20 | 4.571 | 4.703 | 67 | 72 | 72 | 72 | 18 | 0 | 0.987 | 2.029 |
| Final | | 759.516 | 520.890 | 67 | 73 | 72 | | | | | |
| Initial | | 754.625 | 515.870 | 67 | 72 | 72 | | | | | |
| Difference | 2 0.50 | 4.891 | 5.020 | 67 | 73 | 72 | 72 | 12 | 0 | 0.989 | 1.970 |
| Final | | 764.457 | 525.963 | 68 | 74 | 73 | | | | | |
| Initial | | 759.516 | 520.890 | 67 | 73 | 72 | | | | | |
| Difference | 3 0.70 | 4.941 | 5.073 | 68 | 74 | 73 | 73 | 10 | 0 | 0.988 | 1.877 |
| Final | | 769.565 | 531.209 | 68 | 75 | 73 | | | | | |
| Initial | | 764.457 | 525.963 | 68 | 74 | 73 | | | | | |
| Difference | 4 0.90 | 5.108 | 5.246 | 68 | 75 | 73 | 74 | 9 | 0 | 0.988 | 1.830 |
| Final | | 774.817 | 536.590 | 68 | 76 | 74 | | | | | |
| Initial | | 769.565 | 531.209 | 68 | 75 | 73 | | | | | |
| Difference | 5 1.20 | 5.252 | 5.381 | 68 | 76 | 74 | 75 | 8 | 0 | 0.991 | 1.821 |
| Final | | 745.815 | 506.810 | 66 | 73 | 71 | | | | | |
| Initial | | 740.711 | 501.625 | 66 | 71 | 70 | | | | | |
| Difference | 6 2.00 | 5.104 | 5.185 | 66 | 72 | 71 | 71 | 6 | 0 | 0.995 | 1.805 |

Average **0.990** **1.889**

| Stack Temperature Sensor Calibration | | | |
|---|------|--------|-----------------|
| Temperature ID : | CM4 | Name : | PJC1 |
| Ambient Temperature, °F : | 68.8 | Date : | October 5, 2023 |

| Temperature Calibrator | | | |
|-------------------------------|----------|---------------------|------------------|
| Model # : | CL23A | Certification Date: | November 8, 2022 |
| Serial # : | T-314718 | Expiration Date: | November 8, 2023 |

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

| Reference Source Temperature (°F) | Test Thermometer Temperature (°F) | Temperature Difference % |
|--|--|---------------------------------|
| 0 | -2 | 0.4 |
| 250 | 247 | 0.4 |
| 600 | 596 | 0.4 |
| 1200 | 1197 | 0.2 |

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM4
 Standard Meter No. 15788714
 Standard Meter (Y) 0.98570

Date: December 18, 2023
 Calibrated By: PJC1
 Barometric Pressure: 24.93

| Run Number | Orifice Setting in H ₂ O Chg (H) | Standard Meter Gas Volume vr | Dry Gas Meter Gas Volume vd | Standard Meter Temp. F° tr | Dry Gas Meter Inlet Temp. F° tdi | Dry Gas Meter Outlet Temp. F° tdo | Dry Gas Meter Avg. Temp. F° td | Time Min | Time Sec | Y | Chg (H) |
|------------|---|------------------------------|-----------------------------|----------------------------|----------------------------------|-----------------------------------|--------------------------------|----------|----------|-------|---------|
| Final | | 332.019 | 903.402 | 60 | 64 | 64 | | | | | |
| Initial | | 327.011 | 898.401 | 60 | 63 | 62 | | | | | |
| Difference | 1 0.20 | 5.008 | 5.001 | 60 | 64 | 63 | 63 | 18 | 0 | 0.993 | 1.756 |
| Final | | 337.024 | 908.451 | 60 | 65 | 64 | | | | | |
| Initial | | 332.019 | 903.402 | 60 | 64 | 64 | | | | | |
| Difference | 2 0.50 | 5.005 | 5.049 | 60 | 65 | 64 | 64 | 12 | 0 | 0.984 | 1.950 |
| Final | | 342.280 | 913.608 | 60 | 66 | 65 | | | | | |
| Initial | | 337.024 | 908.451 | 60 | 65 | 64 | | | | | |
| Difference | 3 0.70 | 5.256 | 5.157 | 60 | 66 | 65 | 65 | 10 | 0 | 1.012 | 1.716 |
| Final | | 347.665 | 918.963 | 60 | 67 | 65 | | | | | |
| Initial | | 342.280 | 913.601 | 60 | 66 | 65 | | | | | |
| Difference | 4 0.90 | 5.385 | 5.362 | 60 | 67 | 65 | 66 | 9 | 0 | 0.998 | 1.700 |
| Final | | 353.012 | 924.278 | 61 | 68 | 66 | | | | | |
| Initial | | 347.665 | 918.963 | 60 | 67 | 65 | | | | | |
| Difference | 5 1.20 | 5.347 | 5.315 | 61 | 68 | 66 | 67 | 8 | 0 | 1.000 | 1.818 |
| Final | | 311.894 | 883.397 | 59 | 57 | 57 | | | | | |
| Initial | | 306.651 | 878.334 | 59 | 60 | 60 | | | | | |
| Difference | 6 2.00 | 5.243 | 5.063 | 59 | 59 | 59 | 59 | 6 | 0 | 1.014 | 1.789 |

Average 1.000 1.788

| Stack Temperature Sensor Calibration | | | |
|---|------|--------|-------|
| Temperature ID : | CM4 | Name : | PJC1 |
| Ambient Temperature, °F : | 66.4 | Date : | ##### |

| Temperature Calibrator | | | |
|-------------------------------|----------|---------------------|------------------|
| Model # : | CL23A | Certification Date: | October 19, 2023 |
| Serial # : | T-314718 | Expiration Date: | October 18, 2024 |

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

| Reference Source Temperature (°F) | Test Thermometer Temperature (°F) | Temperature Difference % |
|--|--|---------------------------------|
| 0 | -2 | 0.4 |
| 250 | 247 | 0.4 |
| 600 | 595 | 0.5 |
| 1200 | 1197 | 0.2 |

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM53
 Standard Meter No. 18654530
 Standard Meter (Y) 0.99730

Date: September 6, 2023
 Calibrated By: DV
 Barometric Pressure: 28.12

| Run Number | Orifice Setting in H ₂ O Chg (H) | Standard Meter Gas Volume vr | Dry Gas Meter Gas Volume vd | Standard Meter Temp. F° tr | Dry Gas Meter Inlet Temp. F° tdi | Dry Gas Meter Outlet Temp. F° tdo | Dry Gas Meter Avg. Temp. F° td | Time Min | Time Sec | Y | Chg (H) |
|------------|---|------------------------------|-----------------------------|----------------------------|----------------------------------|-----------------------------------|--------------------------------|----------|----------|-------|---------|
| Final | | 108.455 | 58.760 | 81 | 82 | 82 | | | | | |
| Initial | | 103.434 | 53.667 | 80 | 81 | 81 | | | | | |
| Difference | 1 0.20 | 5.021 | 5.093 | 81 | 82 | 82 | 82 | 18 | 35 | 0.985 | 1.683 |
| Final | | 103.434 | 53.667 | 80 | 81 | 81 | | | | | |
| Initial | | 98.353 | 48.581 | 80 | 80 | 80 | | | | | |
| Difference | 2 0.50 | 5.081 | 5.086 | 80 | 81 | 81 | 81 | 12 | 12 | 0.996 | 1.771 |
| Final | | 98.353 | 48.581 | 80 | 80 | 80 | | | | | |
| Initial | | 93.335 | 43.543 | 79 | 79 | 79 | | | | | |
| Difference | 3 0.70 | 5.018 | 5.038 | 80 | 80 | 80 | 80 | 10 | 15 | 0.992 | 1.795 |
| Final | | 93.335 | 43.543 | 79 | 79 | 79 | | | | | |
| Initial | | 88.268 | 38.486 | 79 | 78 | 78 | | | | | |
| Difference | 4 0.90 | 5.067 | 5.057 | 79 | 79 | 79 | 79 | 9 | 10 | 0.996 | 1.810 |
| Final | | 88.268 | 38.486 | 79 | 78 | 78 | | | | | |
| Initial | | 83.006 | 33.210 | 79 | 77 | 77 | | | | | |
| Difference | 5 1.20 | 5.262 | 5.276 | 79 | 78 | 78 | 78 | 8 | 12 | 0.989 | 1.794 |
| Final | | 83.006 | 33.210 | 79 | 77 | 77 | | | | | |
| Initial | | 76.885 | 27.189 | 78 | 77 | 77 | | | | | |
| Difference | 6 2.00 | 6.121 | 6.021 | 79 | 77 | 77 | 77 | 7 | 24 | 1.006 | 1.798 |

Average **0.994** **1.775**

Stack Temperature Sensor Calibration

Meter Box # : CM53 Name : DV

Ambient Temperature : 80.1 °F Date : September 6, 2023

Calibrator Model # : CL940A

Serial # : 526

Date Of Certification : December 28, 2022

Primary Standards Directly Traceable National Institute of Standards and Technology
 108.5 58.76
 103.4 53.667

| Reference Source Temperature (°F) | Test Thermometer Temperature (°F) | Temperature Difference % |
|--|--|---------------------------------|
| 0 | 1 | 0.2 |
| 250 | 252 | 0.3 |
| 600 | 601 | 0.1 |
| 1200 | 1205 | 0.3 |

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM53
 Standard Meter No. 18654530
 Standard Meter (Y) 0.99730

Date: October 26, 2023
 Calibrated By: ER
 Barometric Pressure: 28.05

| Run Number | Orifice Setting in H ₂ O Chg (H) | Standard Meter Gas Volume vr | Dry Gas Meter Gas Volume vd | Standard Meter Temp. F° tr | Dry Gas Meter Inlet Temp. F° tdi | Dry Gas Meter Outlet Temp. F° tdo | Dry Gas Meter Avg. Temp. F° td | Time Min | Time Sec | Y | Chg (H) |
|------------|---|------------------------------|-----------------------------|----------------------------|----------------------------------|-----------------------------------|--------------------------------|----------|----------|-------|---------|
| Final | | 10.800 | 37.210 | 71 | 71 | 71 | | | | | |
| Initial | | 5.798 | 32.147 | 71 | 71 | 71 | | | | | |
| Difference | 1 0.20 | 5.002 | 5.063 | 71 | 71 | 71 | 71 | 18 | 35 | 0.985 | 1.674 |
| Final | | 15.810 | 42.298 | 73 | 73 | 73 | | | | | |
| Initial | | 10.800 | 37.210 | 71 | 71 | 71 | | | | | |
| Difference | 2 0.50 | 5.010 | 5.088 | 72 | 72 | 72 | 72 | 12 | 10 | 0.981 | 1.791 |
| Final | | 20.871 | 47.430 | 72 | 73 | 73 | | | | | |
| Initial | | 15.810 | 42.298 | 73 | 73 | 72 | | | | | |
| Difference | 3 0.70 | 5.061 | 5.132 | 73 | 73 | 73 | 73 | 10 | 19 | 0.982 | 1.768 |
| Final | | 25.915 | 52.558 | 72 | 73 | 73 | | | | | |
| Initial | | 20.871 | 47.430 | 72 | 73 | 73 | | | | | |
| Difference | 4 0.90 | 5.044 | 5.128 | 72 | 73 | 73 | 73 | 9 | 0 | 0.980 | 1.737 |
| Final | | 30.935 | 57.662 | 72 | 74 | 74 | | | | | |
| Initial | | 25.915 | 52.558 | 72 | 73 | 73 | | | | | |
| Difference | 5 1.20 | 5.020 | 5.104 | 72 | 74 | 74 | 74 | 8 | 15 | 0.981 | 1.963 |
| Final | | 5.798 | 32.147 | 71 | 71 | 71 | | | | | |
| Initial | | 0.792 | 27.133 | 71 | 71 | 71 | | | | | |
| Difference | 6 2.00 | 5.006 | 5.014 | 71 | 71 | 71 | 71 | 6 | 20 | 0.991 | 1.941 |

Average **0.983** **1.812**

| Stack Temperature Sensor Calibration | | | |
|---|--------|--------|------------|
| Temperature ID : | 100769 | Name : | ER |
| Ambient Temperature, °F : | 72.2 | Date : | 10/25/2023 |

| Temperature Calibrator | | | |
|-------------------------------|----------|---------------------|------------|
| Model # : | CL23A | Certification Date: | May 1,2023 |
| Serial # : | T-285668 | Expiration Date: | May 2,2024 |

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

| Reference Source Temperature (° F) | Test Thermometer Temperature (° F) | Temperature Difference % |
|---|---|---------------------------------|
| 0 | 0 | 0.0 |
| 250 | 251 | 0.1 |
| 600 | 601 | 0.1 |
| 1200 | 1205 | 0.3 |

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-A
 Probe Calibration Date: 07/10/17
 Test Point Location: center
 Ambient Temperature (°F): 77.8
 Barometric Pressure ("Hg): 29.23

| Repetition | Nominal Low Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (°) | |
| 1 | 60 | 0.81 | 77.8 | 1.18 | 0 | 0.82 |
| 2 | 60 | 0.80 | 77.8 | 1.18 | 0 | 0.82 |
| 3 | 60 | 0.81 | 77.8 | 1.18 | 0 | 0.82 |
| Average (C _{p(avg-low)}) | | | | | | 0.82 |

| Repetition | Nominal High Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (deg) | |
| 1 | 90 | 1.81 | 77.8 | 2.63 | 0 | 0.82 |
| 2 | 90 | 1.81 | 77.8 | 2.62 | 0 | 0.82 |
| 3 | 90 | 1.81 | 77.8 | 2.63 | 0 | 0.82 |
| Average (C _{p(avg-high)}) | | | | | | 0.82 |

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.49\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

| |
|------------------------------|
| C_p = 0.820 |
|------------------------------|



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-B
 Probe Calibration Date: 07/10/17
 Test Point Location: center
 Ambient Temperature (°F): 77.5
 Barometric Pressure ("Hg): 29.23

| Repetition | Nominal Low Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (°) | |
| 1 | 60 | 0.81 | 77.5 | 1.19 | 0 | 0.82 |
| 2 | 60 | 0.81 | 77.5 | 1.19 | 0 | 0.82 |
| 3 | 60 | 0.81 | 77.5 | 1.19 | 0 | 0.82 |
| Average (C _{p(avg-low)}) | | | | | | 0.82 |

| Repetition | Nominal High Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (deg) | |
| 1 | 90 | 1.81 | 77.5 | 2.65 | 0 | 0.82 |
| 2 | 90 | 1.81 | 77.5 | 2.64 | 0 | 0.82 |
| 3 | 90 | 1.81 | 77.5 | 2.64 | 0 | 0.82 |
| Average (C _{p(avg-high)}) | | | | | | 0.82 |

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.55\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.818



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 6/8/2017
 Temperature (°F): 72.2
 Pressure ("Hg): 29.33
 Personnel: wgj
 Probe: S8-031-A

| Wind Tunnel Target DP [I.W.C] | Wind Tunnel Actual DP [I.W.C] | S-Probe DP [I.W.C.] | C _p | C _{p(avg)} | C _p -C _{p(avg)} | σ _{max} | |
|-------------------------------|-------------------------------|---------------------|----------------|---------------------|-------------------------------------|------------------|------|
| 0.81 | 0.81 | 1.19 | 0.818 | 0.818 | 0.000 | 0.001 | Pass |
| 0.81 | 0.81 | 1.19 | 0.818 | | 0.000 | | |
| 0.81 | 0.81 | 1.19 | 0.817 | | -0.001 | | |
| 1.81 | 1.82 | 2.63 | 0.823 | 0.822 | 0.001 | 0.001 | Pass |
| 1.81 | 1.82 | 2.64 | 0.822 | | 0.000 | | |
| 1.81 | 1.81 | 2.64 | 0.820 | | -0.001 | | |



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 6/8/2017
 Temperature (°F): 72.0
 Pressure ("Hg): 29.33
 Personnel: wgj
 Probe: S8-031-B

| Wind Tunnel Target DP [I.W.C] | Wind Tunnel Actual DP [I.W.C] | S-Probe DP [I.W.C.] | C_p | $C_{p(avg)}$ | $C_p - C_{p(avg)}$ | σ_{max} | |
|-------------------------------|-------------------------------|---------------------|-------|--------------|--------------------|----------------|------|
| 0.81 | 0.81 | 1.19 | 0.817 | 0.816 | 0.000 | 0.001 | Pass |
| 0.81 | 0.81 | 1.19 | 0.817 | | 0.000 | | |
| 0.81 | 0.81 | 1.19 | 0.816 | | -0.001 | | |
| 1.81 | 1.82 | 2.65 | 0.820 | 0.820 | 0.000 | 0.000 | Pass |
| 1.81 | 1.82 | 2.65 | 0.820 | | 0.000 | | |
| 1.81 | 1.82 | 2.64 | 0.820 | | 0.000 | | |



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-A
 Probe Calibration Date: 06/08/17
 Test Point Location: center
 Ambient Temperature (°F): 72.2
 Barometric Pressure ("Hg): 29.33

| Repetition | Nominal Low Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (°) | |
| 1 | 60 | 0.81 | 72.2 | 1.19 | 0 | 0.82 |
| 2 | 60 | 0.81 | 72.2 | 1.19 | 0 | 0.82 |
| 3 | 60 | 0.81 | 72.2 | 1.19 | 0 | 0.82 |
| Average (C _{p(avg-low)}) | | | | | | 0.82 |

| Repetition | Nominal High Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (deg) | |
| 1 | 90 | 1.82 | 72.2 | 2.63 | 0 | 0.82 |
| 2 | 90 | 1.82 | 72.2 | 2.64 | 0 | 0.82 |
| 3 | 90 | 1.81 | 72.2 | 2.64 | 0 | 0.82 |
| Average (C _{p(avg-high)}) | | | | | | 0.82 |

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.51\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3%.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

| |
|------------------------------|
| C_p = 0.820 |
|------------------------------|



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-B
 Probe Calibration Date: 06/08/17
 Test Point Location: center
 Ambient Temperature (°F): 72.0
 Barometric Pressure ("Hg): 29.33

| Repetition | Nominal Low Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (°) | |
| 1 | 60 | 0.81 | 72.0 | 1.19 | 0 | 0.82 |
| 2 | 60 | 0.81 | 72.0 | 1.19 | 0 | 0.82 |
| 3 | 60 | 0.81 | 72.0 | 1.19 | 0 | 0.82 |
| Average (C _{p(avg-low)}) | | | | | | 0.82 |

| Repetition | Nominal High Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (deg) | |
| 1 | 90 | 1.82 | 72.0 | 2.65 | 0 | 0.82 |
| 2 | 90 | 1.82 | 72.0 | 2.65 | 0 | 0.82 |
| 3 | 90 | 1.82 | 72.0 | 2.64 | 0 | 0.82 |
| Average (C _{p(avg-high)}) | | | | | | 0.82 |

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.45\%}} \quad \text{Pass}$$

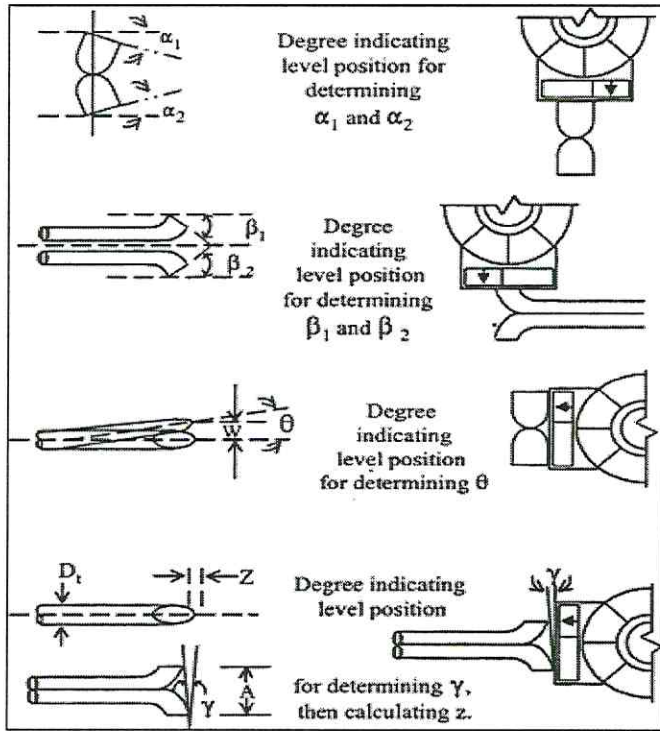
Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

| |
|------------------------------|
| C_p = 0.818 |
|------------------------------|

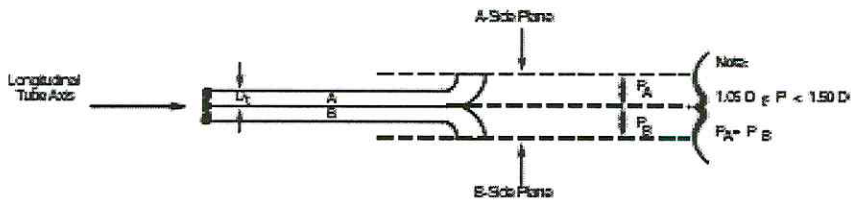


Airflow Sciences Corporation

Probe Inspection for Method 2



| | | |
|------------|-----------|------|
| α_1 | 0.8 (°) | Pass |
| α_2 | 0.3 (°) | Pass |
| β_1 | 0.3 (°) | Pass |
| β_2 | 1.1 (°) | Pass |
| D_t | 0.375 (") | Pass |
| P_a | 0.459 (") | Pass |
| P_b | 0.459 (") | Pass |
| z | <0.02 (") | Pass |
| w | 0.005 (") | Pass |



Certification

I certify that Type S probe ID **S8-031** meets or exceeds all specifications, criteria, and applicable design features.

Certified by: Craig Rood

Date: 6/8/2017



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 8/31/2017
 Temperature (°F): 73.7
 Pressure ("Hg): 29.43
 Personnel: wgj
 Probe: S8-032-A

| Wind Tunnel Target DP [I.W.C.] | Wind Tunnel Actual DP [I.W.C.] | S-Probe DP [I.W.C.] | C _p | C _{p(avg)} | C _p -C _{p(avg)} | σ _{max} | |
|--------------------------------|--------------------------------|---------------------|----------------|---------------------|-------------------------------------|------------------|------|
| 0.81 | 0.81 | 1.18 | 0.820 | 0.821 | 0.000 | 0.000 | Pass |
| 0.81 | 0.81 | 1.18 | 0.821 | | 0.000 | | |
| 0.81 | 0.81 | 1.18 | 0.821 | | 0.000 | | |
| 1.81 | 1.82 | 2.62 | 0.825 | 0.824 | 0.000 | 0.000 | Pass |
| 1.81 | 1.82 | 2.63 | 0.824 | | 0.000 | | |
| 1.81 | 1.82 | 2.63 | 0.824 | | 0.000 | | |



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 8/31/2017
 Temperature (°F): 74.5
 Pressure ("Hg): 29.43
 Personnel: wgj
 Probe: S8-032-B

| Wind Tunnel Target DP [I.W.C.] | Wind Tunnel Actual DP [I.W.C.] | S-Probe DP [I.W.C.] | C _p | C _{p(avg)} | C _p -C _{p(avg)} | σ _{max} | |
|--------------------------------|--------------------------------|---------------------|----------------|---------------------|-------------------------------------|------------------|------|
| 0.81 | 0.81 | 1.19 | 0.819 | 0.819 | 0.000 | 0.000 | Pass |
| 0.81 | 0.81 | 1.19 | 0.819 | | 0.000 | | |
| 0.81 | 0.81 | 1.19 | 0.820 | | 0.000 | | |
| 1.81 | 1.81 | 2.63 | 0.823 | 0.823 | 0.000 | 0.000 | Pass |
| 1.81 | 1.82 | 2.63 | 0.823 | | 0.000 | | |
| 1.81 | 1.82 | 2.63 | 0.823 | | 0.000 | | |



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
Wind Tunnel Location: Livonia, MI
Probe Type: S-Type Pitot
Probe ID: S8-032-A
Probe Calibration Date: 08/31/17
Test Point Location: center
Ambient Temperature (°F): 73.7
Barometric Pressure ("Hg): 29.43

| Repetition | Nominal Low Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (°) | |
| 1 | 60 | 0.81 | 73.7 | 1.18 | 0 | 0.82 |
| 2 | 60 | 0.81 | 73.7 | 1.18 | 0 | 0.82 |
| 3 | 60 | 0.81 | 73.7 | 1.18 | 0 | 0.82 |
| Average (C _{p(avg-low)}) | | | | | | 0.82 |

| Repetition | Nominal High Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (deg) | |
| 1 | 90 | 1.82 | 73.7 | 2.62 | 0 | 0.82 |
| 2 | 90 | 1.82 | 73.7 | 2.63 | 0 | 0.82 |
| 3 | 90 | 1.82 | 73.7 | 2.63 | 0 | 0.82 |
| Average (C _{p(avg-high)}) | | | | | | 0.82 |

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.46\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

| |
|------------------------------|
| C_p = 0.822 |
|------------------------------|



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-032-B
 Probe Calibration Date: 08/31/17
 Test Point Location: center
 Ambient Temperature (°F): 74.5
 Barometric Pressure ("Hg): 29.43

| Repetition | Nominal Low Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (°) | |
| 1 | 60 | 0.81 | 74.5 | 1.19 | 0 | 0.82 |
| 2 | 60 | 0.81 | 74.5 | 1.19 | 0 | 0.82 |
| 3 | 60 | 0.81 | 74.5 | 1.19 | 0 | 0.82 |
| Average (C _{p(avg-low)}) | | | | | | 0.82 |

| Repetition | Nominal High Velocity Setting (ft/s) | Calibration Pitot | | Tested Probe | | Calculated C _p |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
| | | DP _{std} ("H ₂ O) | Temperature (°F) | DP ("H ₂ O) | Yaw Angle (deg) | |
| 1 | 90 | 1.81 | 74.5 | 2.63 | 0 | 0.82 |
| 2 | 90 | 1.82 | 74.5 | 2.63 | 0 | 0.82 |
| 3 | 90 | 1.82 | 74.5 | 2.63 | 0 | 0.82 |
| Average (C _{p(avg-high)}) | | | | | | 0.82 |

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.43\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.821

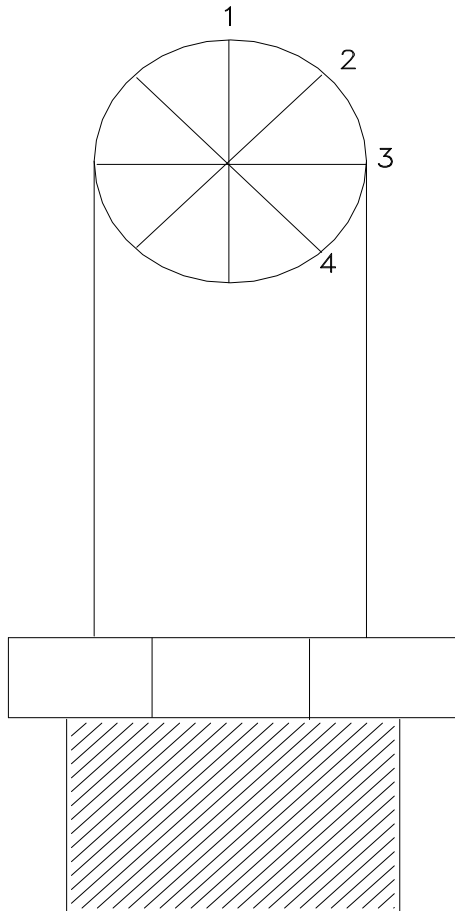
Nozzle Calibration

Date: 4/25/2023

Nozzle ID No.: 909

Analyst: WAP

Material/Type: Glass



| | |
|-------|---|
| 0.282 | 1 |
| 0.282 | 2 |
| 0.281 | 3 |
| 0.281 | 4 |

Valid Data

| |
|----------------|
| Average |
| <u>0.282</u> |

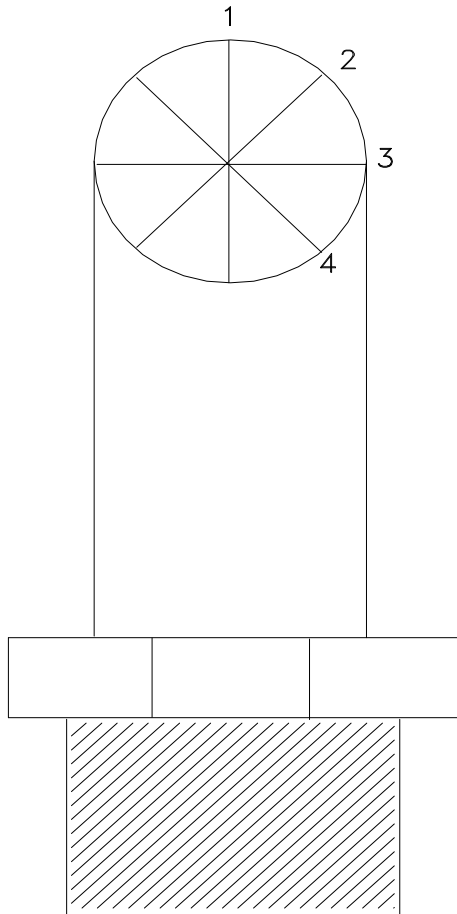
Nozzle Calibration

Date: 10/13/2023

Nozzle ID No.: 981

Analyst: WAP

Material/Type: Glass



| | |
|-------|---|
| 0.281 | 1 |
| 0.281 | 2 |
| 0.281 | 3 |
| 0.281 | 4 |



| |
|----------------|
| Average |
| <u>0.281</u> |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Test Location: Main Kiln
 Date: 10/18/2023
 Operator: R. Sollars
 Operating Condition Mill On

Sample System: FTIR
 Probe Length: 8.0 ft
 Probe Type: FTIR
 Sample Plane: Vertical
 Port Length: 9.5 in.
 Port Size (diameter): 6 in.
 Port Type: Flange
 Duct Shape: Circular
 Diameter: 10.25 ft
 Duct Area: 82.52 Sq. Ft.
 Upstream Diameters: 4.90
 Downstream Diameters: 24.40
 Number of Ports Sampled: 1
 Number of Points per Port: 1
 Total Number of Traverse Points: 1

Minimum Upstream Distance 5.1 Feet
 Minimum Downstream Distance 20.5 Feet
 Ideal Upstream Distance 20.5 Feet
 Ideal Downstream Distance 82.0 Feet

Calibration Gases

| Type | Setting | Cylinder ID | Cylinder Value | Analyzer Response | Difference, % of Span | Expiration Date | Mid cylinder % of high cylinder | Final Bottle Pressure, PSI |
|------------|---------|---------------|----------------|-------------------|-----------------------|-----------------|---------------------------------|----------------------------|
| O2 % (dry) | Zero | Zero Nitrogen | 0.0 | 0.02 | -0.09% | N/A | | 1500 |
| | Mid | CC175274 | 11.07 | 11.08 | -0.04% | 5/11/2031 | 49.40% | 1500 |
| | High | CC420519 | 22.41 | 22.43 | -0.09% | 7/15/2029 | | 1000 |

| Type | Compound | Cylinder ID | Cylinder Value | Expiration Date | Final Bottle Pressure, PSI |
|-------------------------------|----------|---------------|----------------|-----------------|----------------------------|
| Zero Gas | Nitrogen | Zero Nitrogen | 0.0 | N/A | 1700 |
| Calibration Transfer Standard | Ethylene | CC401933 | 100.7 | 7/10/2026 | 1800 |
| Analyte Spike Gas | HCN | CC768255 | 199.20 | 3/12/2024 | 1900 |
| | SF6 | | 10.000 | | |

Response Time Data

| Type | RM Analyzer Make/Model | RM Analyzer s/n | Analyzer Span | RM Gas Span |
|------------|------------------------|-----------------|---------------|-------------|
| O2 % (dry) | CAL 700 | 221018 | 25 | 22.41 |
| HF ppmvw | MKS 2030 | E10004 | 10 | N/A |
| HCN ppmvw | MKS 2030 | E10004 | 100 | N/A |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Diluent: O2 %

Test Location: Main Kiln
 Date: 10/18/23
 Operator: R. Sollars
 O2 % Correction: 7

O2 % (dry) Correction Data

| Run # | Cma | Precal | Postcal | Pre zero | Post zero | Co | Cm | C | Cgas | Span Bias | Span Drift | Zero Bias | Zero Drift |
|-------|-------|--------|---------|----------|-----------|------|-------|------|------|-----------|------------|-----------|------------|
| 1 | 11.07 | 11.10 | 10.94 | 0.05 | 0.03 | 0.04 | 11.02 | 9.66 | 9.7 | 0.62 | -0.71 | -0.04 | -0.09 |
| 2 | 11.07 | 10.94 | 10.92 | 0.03 | 0.02 | 0.03 | 10.93 | 9.40 | 9.5 | 0.71 | -0.09 | 0.00 | -0.04 |
| 3 | 11.07 | 10.92 | 10.92 | 0.02 | 0.02 | 0.02 | 10.92 | 9.00 | 9.1 | 0.71 | 0.00 | 0.00 | 0.00 |

Concentration of Cal Gas erage Pre and Post Span C = Average value of test Co=Average Pre and Post Zero
 Cgas = Corrected gas value of test

Calibration Corrected and Calculated Data

| Run # | Run Date | Start Time | End Time | Moisture % | O2 % (dry) | CO2 % (wet) | CO2 % (dry) | HCN ppmw | HCN ppmvd @ 7% O2 | HF ppmvw | HF ppmvd @ 7% O2 |
|-------|----------|------------|----------|------------|------------|-------------|-------------|----------|-------------------|----------|------------------|
| 1 | 10/18/23 | 8:40 | 9:39 | 13.63% | 9.70 | 16.76 | 19.40 | 8.14 | 11.69 | 0.10 | 0.14 |
| 2 | 10/18/23 | 10:10 | 11:09 | 13.02% | 9.52 | 17.29 | 19.87 | 8.59 | 12.06 | 0.10 | 0.14 |
| 3 | 10/18/23 | 12:25 | 13:24 | 13.68% | 9.12 | 17.75 | 20.56 | 8.46 | 11.57 | 0.10 | 0.14 |

Client: GCC Rio Grande, Inc.
Facility: Pueblo Plant
Test Location: Main Kiln
Date: 10/18/23
Project #: M234207

| <u>Time</u> | <u>O2 % (dry)</u> | |
|-------------|-------------------|----|
| 6:08 | 0.03 | |
| 6:09 | 0.02 | iz |
| 6:10 | 9.92 | |
| 6:11 | 22.36 | |
| 6:12 | 22.43 | ih |
| 6:13 | 16.48 | |
| 6:14 | 0.05 | |
| 6:15 | 0.02 | |
| 6:16 | 0.09 | |
| 6:17 | 14.61 | |
| 6:18 | 11.07 | |
| 6:19 | 11.08 | im |
| 6:20 | 18.88 | |
| 6:21 | 20.89 | |
| 6:22 | 20.88 | |
| 6:23 | 11.43 | |
| 6:24 | 0.07 | |
| 6:25 | 0.05 | z |
| 6:26 | 11.18 | |
| 6:27 | 11.08 | |
| 6:28 | 11.10 | m |

Client: GCC Rio Grande, Inc.

Facility: Pueblo Plant

Project #: M234207

Test Location: Main Kiln

Date: 10/18/23

| Post 1/Pre 2 | | | Post 2/Pre 3 | | |
|---------------------|-------------------|---|---------------------|-------------------|---|
| <u>Time</u> | <u>O2 % (dry)</u> | | <u>Time</u> | <u>O2 % (dry)</u> | |
| 9:55 | 2.52 | | 12:09 | 1.45 | |
| 9:56 | 0.03 | | 12:10 | 0.02 | |
| 9:57 | 0.03 | z | 12:11 | 0.02 | z |
| 9:58 | 0.02 | | 12:12 | 0.02 | |
| 9:59 | 9.14 | | 12:13 | 5.70 | |
| 10:00 | 10.93 | | 12:14 | 10.91 | |
| 10:01 | 10.94 | m | 12:15 | 10.92 | m |

| Post 3 | | |
|---------------|-------------------|---|
| <u>Time</u> | <u>O2 % (dry)</u> | |
| 13:40 | 2.78 | |
| 13:41 | 0.03 | |
| 13:42 | 0.02 | z |
| 13:43 | 0.02 | |
| 13:44 | 3.79 | |
| 13:45 | 10.90 | |
| 13:46 | 10.92 | m |
| | 10.93 | |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Test Location: Main Kiln
 Date: 10/17/2023
 Operator: R. Sollars
 Operating Condition Mill Off

Sample System: FTIR
 Probe Length: 8.0 ft
 Probe Type: FTIR
 Sample Plane: Vertical
 Port Length: 9.5 in.
 Port Size (diameter): 6 in.
 Port Type: Flange
 Duct Shape: Circular
 Diameter: 10.25 ft
 Duct Area: 82.52 Sq. Ft.
 Upstream Diameters: 4.90
 Downstream Diameters: 24.40
 Number of Ports Sampled: 1
 Number of Points per Port: 1
 Total Number of Traverse Points: 1

Minimum Upstream Distance 5.1 Feet
 Minimum Downstream Distance 20.5 Feet
 Ideal Upstream Distance 20.5 Feet
 Ideal Downstream Distance 82.0 Feet

Calibration Gases

| Type | Setting | Cylinder ID | Cylinder Value | Analyzer Response | Difference, % of Span | Expiration Date | Mid cylinder % of high cylinder | Final Bottle Pressure, PSI |
|------------|---------|---------------|----------------|-------------------|-----------------------|-----------------|---------------------------------|----------------------------|
| O2 % (dry) | Zero | Zero Nitrogen | 0.0 | 0.03 | -0.13% | N/A | | 1500 |
| | Mid | CC175274 | 11.07 | 11.09 | -0.09% | 5/11/2031 | 49.40% | 1500 |
| | High | CC420519 | 22.41 | 22.46 | -0.22% | 7/15/2029 | | 1000 |

| Type | Compound | Cylinder ID | Cylinder Value | Expiration Date | Final Bottle Pressure, PSI |
|-------------------------------|----------|---------------|----------------|-----------------|----------------------------|
| Zero Gas | Nitrogen | Zero Nitrogen | 0.0 | N/A | 1700 |
| Calibration Transfer Standard | Ethylene | CC401933 | 100.7 | 7/10/2026 | 1800 |
| Analyte Spike Gas | HCN | CC768255 | 199.20 | 3/12/2024 | 1900 |
| | SF6 | | 10.000 | | |

Response Time Data

| Type | RM Analyzer Make/Model | RM Analyzer s/n | Analyzer Span | RM Gas Span |
|------------|------------------------|-----------------|---------------|-------------|
| O2 % (dry) | CAL 700 | 221018 | 25 | 22.41 |
| HF ppmvw | MKS 2030 | E10004 | 10 | N/A |
| HCN ppmvw | MKS 2030 | E10004 | 100 | N/A |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Diluent: O2 %

Test Location: Main Kiln
 Date: 10/17/23
 Operator: R. Sollars
 O2 % Correction: 7

O2 % (dry) Correction Data

| Run # | Cma | Precal | Postcal | Pre zero | Post zero | Co | Cm | C | Cgas | Span Bias | Span Drift | Zero Bias | Zero Drift |
|-------|-------|--------|---------|----------|-----------|------|-------|------|------|-----------|------------|-----------|------------|
| 1 | 11.07 | 11.09 | 10.93 | 0.06 | 0.02 | 0.04 | 11.01 | 4.23 | 4.2 | 0.71 | -0.71 | 0.04 | -0.18 |
| 2 | 11.07 | 10.93 | 10.87 | 0.02 | 0.01 | 0.02 | 10.90 | 5.17 | 5.2 | 0.98 | -0.27 | 0.09 | -0.04 |
| 3 | 11.07 | 10.87 | 10.87 | 0.01 | 0.00 | 0.01 | 10.87 | 4.16 | 4.2 | 0.98 | 0.00 | 0.13 | -0.04 |

Concentration of Cal Gas erage Pre and Post Span C = Average value of test Co=Average Pre and Post Zero
 Cgas = Corrected gas value of test

Calibration Corrected and Calculated Data

| Run # | Run Date | Start Time | End Time | Moisture % | O2 % (dry) | CO2 % (wet) | CO2 % (dry) | HCN ppmvw | HCN ppmvd @ 7% O2 | HF ppmvw | HF ppmvd @ 7% O2 |
|-------|----------|------------|----------|------------|------------|-------------|-------------|-----------|-------------------|----------|------------------|
| 1 | 10/17/23 | 8:00 | 8:59 | 12.36% | 4.23 | 25.47 | 29.06 | 13.04 | 12.41 | 0.10 | 0.10 |
| 2 | 10/17/23 | 13:40 | 14:39 | 12.50% | 5.24 | 24.45 | 27.94 | 11.78 | 11.95 | 0.10 | 0.10 |
| 3 | 10/17/23 | 15:05 | 16:04 | 12.41% | 4.23 | 26.13 | 29.83 | 14.24 | 13.56 | 0.10 | 0.10 |

Client: GCC Rio Grande, Inc.
Facility: Pueblo Plant
Test Location: Main Kiln
Date: 10/17/23
Project #: M234207

| <u>Time</u> | <u>O2 % (dry)</u> | |
|-------------|-------------------|----|
| 6:14 | 0.03 | |
| 6:15 | 0.03 | iz |
| 6:16 | 8.84 | |
| 6:17 | 20.85 | |
| 6:18 | 22.71 | |
| 6:19 | 22.69 | |
| 6:20 | 22.46 | ih |
| 6:21 | 19.76 | |
| 6:22 | 11.10 | |
| 6:23 | 11.09 | im |
| 6:24 | 11.35 | |
| 6:25 | 20.52 | |
| 6:26 | 20.92 | |
| 6:27 | 20.91 | |
| 6:28 | 11.89 | |
| 6:29 | 0.08 | |
| 6:30 | 0.06 | z |
| 6:31 | 10.45 | |
| 6:32 | 11.08 | |
| 6:33 | 11.09 | m |

Client: GCC Rio Grande, Inc.

Facility: Pueblo Plant

Project #: M234207

Test Location: Main Kiln

Date: 10/17/23

Post 1/Pre 2

| <u>Time</u> | <u>O2 % (dry)</u> | |
|-------------|-------------------|----------|
| 9:15 | 1.25 | |
| 9:16 | 0.02 | |
| 9:17 | 0.91 | |
| 9:18 | 0.37 | |
| 9:19 | 0.02 | |
| 9:20 | 0.02 | z |
| 9:21 | 0.53 | |
| 9:22 | 8.86 | |
| 9:23 | 10.91 | |
| 9:24 | 10.92 | |
| 9:25 | 10.93 | m |

Post 2/Pre 3

| <u>Time</u> | <u>O2 % (dry)</u> | |
|-------------|-------------------|----------|
| 14:53 | 1.05 | |
| 14:54 | 0.02 | |
| 14:55 | 0.01 | |
| 14:56 | 0.01 | z |
| 14:57 | 0.33 | |
| 14:58 | 9.42 | |
| 14:59 | 10.86 | |
| 15:00 | 10.87 | m |

Post 3

| <u>Time</u> | <u>O2 % (dry)</u> | |
|-------------|-------------------|----------|
| 16:20 | 1.96 | |
| 16:21 | 0.01 | |
| 16:22 | 2.31 | |
| 16:23 | 0.01 | |
| 16:24 | 0.00 | z |
| 16:25 | 0.96 | |
| 16:26 | 9.82 | |
| 16:27 | 10.85 | |
| 16:28 | 10.87 | m |

Appendix H - FTIR QA/QC

Method 320 FTIR Detector Multi-Gas Determination QA/QC

FTIR data was collected using an MKS MultiGas 2030 FTIR spectrometer.

The FTIR was equipped with a temperature-controlled, 5.11 meter multi-pass gas cell maintained at 191°C. Gas flows and sampling system pressures were monitored using a rotameter and pressure transducer. All data was collected at 0.5 cm⁻¹ resolution. Each spectrum was derived from the coaddition of 64 scans, with a new data point generated approximately every one minute. Analyzer data for each run is presented in the Reference Method Test Data appendix.

| SAMPLING SYSTEM PARAMETERS | | | | |
|----------------------------|-------------------------------|--------------------------|---------------------------------------|------------------------|
| MKS Serial # | Sampling Line | Probe Assembly | Particulate Filter Media | Operating Temperatures |
| E10004 | 100' 3/8" dia., heated Teflon | Heated 12', 3/8" dia. SS | 0.01µ heated borosilicate glass fiber | 191°C |

QA/QC procedures followed US EPA Method 320 guidelines. See below for QA/QC procedure details and list of calibration gas standards. All calibration gases were introduced to the analyzer and the sampling system using an instrument grade stainless steel rotameter. All QA/QC procedures were within the acceptance criteria allowance of the applicable EPA methodology. Detailed FTIR QA/QC data follow the narrative portion of this appendix.

| FTIR QA/QC Procedures | | | | | | |
|--|---|-------------------------|--|----------------------------|------------------------------|--------|
| QA/QC Specification | Purpose | Calibration Gas Analyte | Delivery | Frequency | Acceptance Criteria | Result |
| M320: Zero | Verify that the FTIR is free of contaminants & zero the FTIR | Nitrogen (zero) | Direct to FTIR | pre/post test | < MDL or Noise | Pass |
| M320: Calibration Transfer Standard (CTS) Direct | Verify FTIR stability, confirm optical path length | Ethylene | Direct to FTIR | pretest | +/- 5% cert. value | Pass |
| M320: Analyte Direct | Verify FTIR calibration | HCN, SF ₆ | Direct to FTIR | Pretest | +/- 5% cert. value | Pass |
| M320: CTS Response | Verify system stability, recovery, response time | Ethylene | Sampling System | Daily, pre/post test | +/- 5% of Direct Measurement | Pass |
| M320: Zero Response | Verify system is free of contaminants, system bias | Nitrogen (zero) | Sampling System | pretest | Bias correct data | Pass |
| M320: Analyte Spike | Verify system ability to deliver and quantify analyte of interest in the presence of other effluent gases | HCN, SF ₆ | Dynamic Addition to Sampling System, 1:10 effluent | Throughout testing – daily | +/- 20% theoretical recovery | Pass |

Note: The determined concentrations from direct analyses were used in all system/spike recovery calculations.

| CALIBRATION GAS STANDARDS | | | | |
|---------------------------|---------------------|--------|---------------|--------------------------------|
| Components | Concentration (ppm) | Vendor | Cylinder # | Standard Type |
| Ethylene | 100.7 | Airgas | CC401933 | Primary +/- 1% |
| HCN/SF ₆ | 199.2/10.00 | Airgas | CC768255 | Certified Standard-Spec +/- 5% |
| Nitrogen | Zero Gas | Airgas | Zero Nitrogen | UHP Grade |

Analyte Spiking

HCN spiking was performed prior to testing to verify the ability of the sampling system to quantitatively deliver a sample containing HCN from the base of the probe to the FTIR. Analyte spiking assures the ability of the FTIR sampling system to recover acid gases in the presence of effluent gas.

As part of the spiking procedure, samples were measured to determine native HCN concentrations to be used in the spike recovery calculations. The analyte spiking gases contained a low concentration of sulfur hexafluoride (SF₆). The determined SF₆ concentration in the spiked sample was used to calculate the dilution factor of the spike and thus used to calculate the concentration of the spiked HCN. The spike target dilution ratio was 1:10 or less.

The following equation illustrates the percent recovery calculation.

$$DF = \frac{SF_6(spik)}{SF_6(direct)} \quad (\text{Sec. 9.2.3 (3) USEPA Method 320})$$

$$CS = DF * Spike(dir) + Unspike(1 - DF) \quad (\text{Sec. 9.2.3 (4) USEPA Method 320})$$

DF = Dilution factor of the spike gas

SF_{6(dir)} = SF₆ concentration measured directly in undiluted spike gas

SF_{6(spik)} = Diluted SF₆ concentration measured in a spiked sample

Spike_{dir} = Concentration of the analyte in the spike standard measure by the FTIR directly

CS = Expected concentration of the spiked samples

Unspike = Native concentration of analytes in unspiked samples

Post Collection Data Validation

As part of the data validation procedure, reference spectra are manually fit to that of the sample spectra and a concentration is determined. The reference spectra are scaled to match the peak amplitude of the sample, thus providing a scale factor. The scale factor multiplied by the reference spectra concentration is used to determine the concentration value for the sample spectra. Sample pressure and temperature corrections are then applied to compute the final sample concentration. The manually calculated results are then compared with the software-generated results. The data is then validated if the two concentrations are within ± 20% agreement. If there is a difference greater than ± 20% the spectra are reviewed for possible spectra interferences or any other possible causes leading to incorrectly quantified data.

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Operating Condition: Mill On

Test Location: Main Kiln
 Date: 10/18/2023
 Operator: R. Sollars
 FTIR s/n: E10004

System Leak Check: 0.0 mL/min

Nitrogen (Zero) Direct to FTIR

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet |
|--------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| N2_DIR_0001BKG.LAB | 10/18/23 | 6:02:49 | 0.0 | 0.0 | 0.0 | 191.2 | 0.83 | 0.0 | 0.0 | 0.000 |
| N2_DIR_0002.LAB | 10/18/23 | 6:03:04 | 0.0 | 0.0 | 0.0 | 190.8 | 0.83 | 0.0 | 0.0 | 0.001 |
| N2_DIR_0003.LAB | 10/18/23 | 6:03:12 | 0.0 | 0.0 | 0.1 | 190.8 | 0.83 | 0.0 | 0.0 | 0.003 |
| N2_DIR_0004.LAB | 10/18/23 | 6:03:20 | 0.0 | 0.0 | 0.0 | 190.8 | 0.83 | -0.1 | -0.2 | -0.007 |
| N2_DIR_0005.LAB | 10/18/23 | 6:03:28 | 0.0 | 0.0 | 0.0 | 190.8 | 0.83 | 0.0 | 0.1 | 0.004 |
| N2_DIR_0006.LAB | 10/18/23 | 6:03:36 | 0.0 | 0.0 | 0.0 | 190.8 | 0.83 | 0.0 | -0.1 | 0.003 |
| N2_DIR_0007.LAB | 10/18/23 | 6:03:44 | 0.0 | 0.0 | 0.0 | 190.7 | 0.83 | 0.0 | -0.1 | 0.003 |
| N2_DIR_0008.LAB | 10/18/23 | 6:03:51 | 0.0 | 0.0 | 0.0 | 190.7 | 0.83 | -0.2 | 0.1 | -0.004 |
| N2_DIR_0009.LAB | 10/18/23 | 6:03:59 | 0.0 | 0.0 | 0.0 | 190.7 | 0.83 | -0.1 | 0.3 | -0.001 |

Calibration Transfer Standard (CTS), Direct to FTIR

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene | |
|------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|--------|
| CTS_DIR_0017.LAB | 10/18/23 | 6:05:55 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 100.7 | 0.1 | -0.023 | 100.0% | |
| CTS_DIR_0018.LAB | 10/18/23 | 6:06:02 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 100.9 | 0.0 | -0.035 | 100.2% | |
| CTS_DIR_0019.LAB | 10/18/23 | 6:06:10 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 100.9 | 0.1 | -0.025 | 100.2% | |
| CTS_DIR_0020.LAB | 10/18/23 | 6:06:19 | 0.0 | 0.0 | 0.0 | 190.7 | 0.83 | 100.7 | 0.1 | -0.025 | 100.0% | |
| CTS_DIR_0021.LAB | 10/18/23 | 6:06:26 | 0.0 | 0.0 | 0.0 | 190.7 | 0.83 | 100.8 | 0.0 | -0.031 | 100.1% | |
| CTS_DIR_0022.LAB | 10/18/23 | 6:06:34 | 0.0 | 0.0 | -0.1 | 190.7 | 0.83 | 100.8 | -0.1 | -0.032 | 100.1% | |
| CTS_DIR_0023.LAB | 10/18/23 | 6:06:42 | 0.0 | 0.0 | 0.0 | 190.7 | 0.83 | 101.0 | 0.1 | -0.030 | 100.3% | |
| Average | | | | | | | | 100.8 | | | | 100.1% |

Analyte Spike Gas (HCN) Direct to FTIR

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % HCN |
|-----------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|-------------------|
| 199.2HCN_DIR_0035.LAB | 10/18/23 | 6:09:24 | 0.0 | 0.0 | -0.1 | 190.7 | 0.83 | 0.6 | 193.7 | 10.007 | 97.2% |
| 199.2HCN_DIR_0036.LAB | 10/18/23 | 6:09:31 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 0.5 | 194.2 | 10.001 | 97.5% |
| 199.2HCN_DIR_0037.LAB | 10/18/23 | 6:09:39 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 0.5 | 194.1 | 9.993 | 97.4% |
| 199.2HCN_DIR_0038.LAB | 10/18/23 | 6:09:47 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 0.7 | 194.3 | 10.011 | 97.6% |
| 199.2HCN_DIR_0039.LAB | 10/18/23 | 6:09:55 | 0.0 | 0.0 | 0.0 | 190.7 | 0.83 | 0.6 | 194.5 | 10.012 | 97.7% |
| 199.2HCN_DIR_0040.LAB | 10/18/23 | 6:10:03 | 0.0 | 0.0 | 0.0 | 190.7 | 0.83 | 0.7 | 194.3 | 9.990 | 97.5% |
| 199.2HCN_DIR_0041.LAB | 10/18/23 | 6:10:11 | 0.0 | 0.0 | -0.1 | 190.7 | 0.83 | 0.7 | 194.2 | 9.993 | 97.5% |
| 199.2HCN_DIR_0042.LAB | 10/18/23 | 6:10:18 | 0.0 | 0.0 | 0.0 | 190.8 | 0.83 | 0.5 | 194.1 | 9.996 | 97.4% |
| Average | | | | | | | | 194.2 | 10.000 | | 97.5% |

CTS, System Purge

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene |
|-----------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| CTS_RT_0079.LAB | 10/18/23 | 6:24:38 | 0.0 | 0.0 | 0.0 | 190.9 | 0.84 | 101.2 | 0.2 | -0.022 | 100.5% |
| CTS_RT_0080.LAB | 10/18/23 | 6:24:45 | 0.0 | 0.0 | 0.0 | 190.8 | 0.84 | 101.2 | 0.3 | -0.012 | 100.5% |
| CTS_RT_0081.LAB | 10/18/23 | 6:24:54 | 0.0 | 0.0 | 0.0 | 190.9 | 0.84 | 100.5 | 0.1 | -0.012 | 99.7% |
| CTS_RT_0082.LAB | 10/18/23 | 6:25:01 | 0.0 | 0.0 | 0.0 | 190.9 | 0.84 | 100.8 | 0.2 | -0.025 | 100.0% |
| CTS_RT_0083.LAB | 10/18/23 | 6:25:09 | 0.0 | 0.0 | 0.0 | 190.9 | 0.84 | 100.6 | 0.1 | -0.024 | 99.8% |
| CTS_RT_0084.LAB | 10/18/23 | 6:25:17 | 0.0 | 0.0 | 0.0 | 190.9 | 0.84 | 100.7 | 0.3 | -0.019 | 99.8% |
| CTS_RT_0085.LAB | 10/18/23 | 6:25:25 | 0.0 | 0.0 | 0.0 | 190.9 | 0.84 | 100.4 | 0.1 | -0.044 | 99.6% |
| CTS_RT_0086.LAB | 10/18/23 | 6:25:33 | 0.0 | 0.0 | 0.0 | 191.0 | 0.84 | 100.9 | 0.2 | -0.012 | 100.1% |

Response Time Test

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Response Time (sec) |
|-----------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|---------------------|
| CTS_RT_0071.LAB | 10/18/23 | 6:23:35 | 0.7 | 0.0 | 0.0 | 190.9 | 0.84 | 0.1 | -0.2 | 0.008 | - |
| CTS_RT_0072.LAB | 10/18/23 | 6:23:43 | 0.4 | 1.6 | 0.0 | 190.9 | 0.84 | 44.2 | 0.6 | -0.011 | 15.653 |
| CTS_RT_0073.LAB | 10/18/23 | 6:23:50 | 0.1 | 0.0 | 0.1 | 190.9 | 0.84 | 100.5 | 0.2 | -0.023 | 23.653 |
| CTS_RT_0074.LAB | 10/18/23 | 6:23:58 | 0.0 | 0.0 | 0.0 | 190.9 | 0.84 | 100.5 | 0.2 | -0.011 | |
| CTS_RT_0075.LAB | 10/18/23 | 6:24:06 | 0.0 | 0.0 | 0.0 | 190.9 | 0.84 | 100.2 | 0.3 | -0.023 | |
| CTS_RT_0076.LAB | 10/18/23 | 6:24:14 | 0.0 | 0.0 | -0.1 | 190.9 | 0.84 | 100.9 | 0.3 | -0.027 | |
| CTS_RT_0077.LAB | 10/18/23 | 6:24:22 | 0.0 | 0.0 | 0.0 | 190.9 | 0.84 | 101.3 | 0.1 | -0.034 | |
| CTS_RT_0078.LAB | 10/18/23 | 6:24:30 | 0.0 | 0.0 | 0.0 | 190.8 | 0.84 | 100.9 | 0.1 | -0.021 | |
| CTS_RT_0079.LAB | 10/18/23 | 6:24:38 | 0.0 | 0.0 | 0.0 | 190.9 | 0.84 | 101.2 | 0.2 | -0.022 | |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Operating Condition: Mill On

Test Location: Main Kiln
 Date: 10/18/2023
 Operator: R. Sollars
 FTIR s/n: E10004

Pre 1 Native Effluent Prior to Analyte Spike

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet |
|------------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| AMBIENT_STACK_0204.LAB | 10/18/23 | 6:44:51 | 12.5 | 22.1 | -0.1 | 190.9 | 0.84 | 3.1 | 10.7 | -0.019 |
| AMBIENT_STACK_0205.LAB | 10/18/23 | 6:44:59 | 12.6 | 22.1 | -0.1 | 190.9 | 0.83 | 2.8 | 10.3 | -0.032 |
| AMBIENT_STACK_0206.LAB | 10/18/23 | 6:45:06 | 12.6 | 22.1 | -0.1 | 190.9 | 0.84 | 2.9 | 10.6 | -0.032 |
| | | | | | | | | | 10.5 | -0.028 |

Pre 1 Effluent Spike Using Analyte

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Dilution Factor | Recovery % HCN |
|-------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| PRE1_SPK_0219.LAB | 10/18/23 | 6:48:42 | 11.9 | 19.9 | -0.1 | 190.8 | 0.84 | 2.3 | 21.2 | 0.594 | 0.059 | 98.8% |
| PRE1_SPK_0220.LAB | 10/18/23 | 6:48:50 | 11.9 | 20.0 | -0.1 | 190.8 | 0.84 | 2.7 | 21.4 | 0.582 | 0.058 | 101.0% |
| PRE1_SPK_0221.LAB | 10/18/23 | 6:48:58 | 11.9 | 19.9 | 0.0 | 190.8 | 0.84 | 2.9 | 21.2 | 0.597 | 0.060 | 98.7% |
| PRE1_SPK_0222.LAB | 10/18/23 | 6:49:06 | 11.9 | 19.9 | -0.1 | 190.8 | 0.84 | 2.6 | 21.4 | 0.583 | 0.058 | 101.0% |
| PRE1_SPK_0223.LAB | 10/18/23 | 6:49:14 | 11.8 | 19.9 | -0.1 | 190.8 | 0.84 | 2.4 | 21.3 | 0.587 | 0.059 | 100.4% |
| PRE1_SPK_0224.LAB | 10/18/23 | 6:49:22 | 11.9 | 20.0 | -0.1 | 190.7 | 0.84 | 2.6 | 21.3 | 0.584 | 0.058 | 100.5% |
| PRE1_SPK_0225.LAB | 10/18/23 | 6:49:29 | 11.9 | 20.0 | -0.1 | 190.7 | 0.84 | 2.6 | 21.2 | 0.585 | 0.059 | 99.8% |
| PRE1_SPK_0226.LAB | 10/18/23 | 6:49:37 | 11.9 | 20.0 | -0.1 | 190.8 | 0.84 | 2.6 | 21.4 | 0.589 | 0.059 | 100.5% |

Native Effluent Prior to Analyte Spike

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet |
|---------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| RUN1_0421.LAB | 10/18/23 | 9:44:38 | 13.1 | 16.9 | -0.1 | 190.5 | 0.85 | 2.9 | 7.9 | -0.016 |
| RUN1_0422.LAB | 10/18/23 | 9:45:41 | 12.8 | 16.9 | -0.1 | 190.6 | 0.84 | 2.9 | 8.2 | -0.013 |
| RUN1_0423.LAB | 10/18/23 | 9:46:44 | 13.0 | 17.2 | -0.1 | 190.7 | 0.84 | 2.9 | 8.5 | -0.016 |
| | | | | | | | | | 8.2 | -0.015 |

Effluent Spike Using Analyte

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Dilution Factor | Recovery % HCN |
|--------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST1_SPK_0436.LAB | 10/18/23 | 9:51:15 | 12.8 | 16.4 | -0.1 | 191.1 | 0.84 | 2.5 | 16.3 | 0.417 | 0.042 | 101.9% |
| POST1_SPK_0437.LAB | 10/18/23 | 9:51:23 | 12.7 | 16.3 | -0.1 | 191.0 | 0.84 | 2.5 | 15.9 | 0.434 | 0.043 | 97.6% |
| POST1_SPK_0438.LAB | 10/18/23 | 9:51:31 | 12.9 | 16.2 | 0.0 | 191.0 | 0.84 | 2.8 | 16.0 | 0.441 | 0.044 | 97.7% |
| POST1_SPK_0439.LAB | 10/18/23 | 9:51:39 | 13.3 | 16.1 | -0.1 | 191.0 | 0.84 | 2.7 | 15.9 | 0.424 | 0.042 | 98.6% |
| POST1_SPK_0440.LAB | 10/18/23 | 9:51:47 | 13.3 | 16.0 | -0.1 | 191.0 | 0.84 | 2.6 | 15.7 | 0.422 | 0.042 | 97.7% |
| POST1_SPK_0441.LAB | 10/18/23 | 9:51:55 | 13.0 | 15.9 | -0.1 | 191.0 | 0.84 | 2.5 | 15.7 | 0.431 | 0.043 | 96.8% |
| POST1_SPK_0442.LAB | 10/18/23 | 9:52:03 | 12.7 | 15.9 | -0.1 | 191.0 | 0.84 | 2.8 | 15.8 | 0.426 | 0.043 | 98.1% |
| POST1_SPK_0443.LAB | 10/18/23 | 9:52:11 | 12.6 | 15.8 | -0.1 | 190.9 | 0.84 | 2.4 | 15.8 | 0.437 | 0.044 | 96.6% |

CTS, System Purge

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene |
|--------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST1_CTS_0450.LAB | 10/18/23 | 9:54:06 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 100.4 | 0.7 | -0.022 | 99.5% |
| POST1_CTS_0451.LAB | 10/18/23 | 9:54:14 | 0.0 | 0.0 | 0.1 | 190.7 | 0.84 | 99.6 | 0.5 | -0.031 | 98.8% |
| POST1_CTS_0452.LAB | 10/18/23 | 9:54:22 | 0.1 | 0.0 | 0.0 | 190.7 | 0.84 | 100.9 | 0.6 | -0.015 | 100.0% |
| POST1_CTS_0453.LAB | 10/18/23 | 9:54:30 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 100.6 | 0.6 | -0.022 | 99.8% |
| POST1_CTS_0454.LAB | 10/18/23 | 9:54:38 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 100.5 | 0.5 | -0.029 | 99.7% |
| POST1_CTS_0455.LAB | 10/18/23 | 9:54:46 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 100.6 | 0.5 | -0.026 | 99.8% |
| POST1_CTS_0456.LAB | 10/18/23 | 9:54:53 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 100.5 | 0.5 | -0.016 | 99.7% |
| POST1_CTS_0457.LAB | 10/18/23 | 9:55:01 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 100.3 | 0.4 | -0.024 | 99.5% |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Operating Condition: Mill On

Test Location: Main Kiln
 Date: 10/18/2023
 Operator: R. Sollars
 FTIR s/n: E10004

Native Effluent Prior to Analyte Spike

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet |
|---------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| RUN2_0571.LAB | 10/18/23 | 11:35:11 | 12.2 | 16.6 | -0.1 | 190.5 | 0.84 | 2.6 | 7.8 | -0.017 |
| RUN2_0572.LAB | 10/18/23 | 11:36:14 | 12.1 | 17.1 | -0.1 | 190.4 | 0.84 | 2.5 | 8.3 | -0.014 |
| RUN2_0573.LAB | 10/18/23 | 11:37:17 | 12.4 | 17.2 | -0.1 | 190.4 | 0.84 | 2.6 | 8.5 | -0.017 |
| | | | | | | | | | 8.2 | -0.016 |

Effluent Spike Using Analyte

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Dilution Factor | Recovery % HCN |
|--------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST2_SPK_0607.LAB | 10/18/23 | 12:04:56 | 12.2 | 17.7 | -0.1 | 190.3 | 0.84 | 2.4 | 15.7 | 0.331 | 0.033 | 109.2% |
| POST2_SPK_0608.LAB | 10/18/23 | 12:05:04 | 12.3 | 17.7 | -0.1 | 190.3 | 0.84 | 2.5 | 15.6 | 0.338 | 0.034 | 107.8% |
| POST2_SPK_0609.LAB | 10/18/23 | 12:05:12 | 12.3 | 17.8 | 0.0 | 190.2 | 0.84 | 2.7 | 15.9 | 0.327 | 0.033 | 111.0% |
| POST2_SPK_0610.LAB | 10/18/23 | 12:05:20 | 12.2 | 17.7 | -0.1 | 190.3 | 0.84 | 2.6 | 15.7 | 0.331 | 0.033 | 109.4% |
| POST2_SPK_0611.LAB | 10/18/23 | 12:05:27 | 12.2 | 17.6 | -0.1 | 190.2 | 0.84 | 2.5 | 15.7 | 0.339 | 0.034 | 108.4% |
| POST2_SPK_0612.LAB | 10/18/23 | 12:05:35 | 12.2 | 17.6 | -0.1 | 190.1 | 0.84 | 2.3 | 15.6 | 0.333 | 0.033 | 108.4% |
| POST2_SPK_0613.LAB | 10/18/23 | 12:05:43 | 12.2 | 17.5 | -0.1 | 190.2 | 0.84 | 2.5 | 15.6 | 0.345 | 0.034 | 106.6% |
| POST2_SPK_0614.LAB | 10/18/23 | 12:05:51 | 12.1 | 17.4 | -0.1 | 190.2 | 0.84 | 2.6 | 15.5 | 0.327 | 0.033 | 108.2% |

CTS, System Purge

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene |
|--------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST2_CTS_0622.LAB | 10/18/23 | 12:08:08 | 0.1 | 0.0 | -0.1 | 190.5 | 0.84 | 101.1 | 0.5 | -0.019 | 100.2% |
| POST2_CTS_0623.LAB | 10/18/23 | 12:08:16 | 0.1 | 0.0 | -0.1 | 190.6 | 0.84 | 100.8 | 0.5 | -0.029 | 100.0% |
| POST2_CTS_0624.LAB | 10/18/23 | 12:08:24 | 0.1 | 0.0 | 0.1 | 190.6 | 0.84 | 100.9 | 0.4 | -0.026 | 100.1% |
| POST2_CTS_0625.LAB | 10/18/23 | 12:08:32 | 0.1 | 0.0 | 0.0 | 190.6 | 0.84 | 100.3 | 0.5 | -0.010 | 99.5% |
| POST2_CTS_0626.LAB | 10/18/23 | 12:08:40 | 0.1 | 0.0 | 0.0 | 190.5 | 0.84 | 100.6 | 0.3 | -0.016 | 99.7% |
| POST2_CTS_0627.LAB | 10/18/23 | 12:08:47 | 0.1 | 0.0 | 0.0 | 190.6 | 0.84 | 101.1 | 0.5 | -0.023 | 100.2% |
| POST2_CTS_0628.LAB | 10/18/23 | 12:08:55 | 0.1 | 0.0 | 0.0 | 190.5 | 0.84 | 100.4 | 0.1 | -0.035 | 99.6% |
| POST2_CTS_0629.LAB | 10/18/23 | 12:09:03 | 0.1 | 0.0 | 0.0 | 190.5 | 0.84 | 100.6 | 0.2 | -0.020 | 99.8% |

Native Effluent Prior to Analyte Spike

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet |
|---------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| RUN3_0720.LAB | 10/18/23 | 13:29:00 | 14.2 | 17.6 | 0.0 | 190.2 | 0.84 | 2.6 | 7.9 | -0.023 |
| RUN3_0721.LAB | 10/18/23 | 13:30:03 | 14.3 | 17.9 | 0.0 | 190.1 | 0.84 | 2.8 | 8.0 | -0.018 |
| RUN3_0722.LAB | 10/18/23 | 13:31:05 | 14.1 | 17.6 | 0.0 | 190.1 | 0.84 | 2.8 | 8.0 | -0.015 |
| | | | | | | | | | 8.0 | -0.019 |

Effluent Spike Using Analyte

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Dilution Factor | Recovery % HCN |
|--------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST3_SPK_0737.LAB | 10/18/23 | 13:35:44 | 13.2 | 16.8 | 0.0 | 190.1 | 0.84 | 2.6 | 15.8 | 0.411 | 0.041 | 101.2% |
| POST3_SPK_0738.LAB | 10/18/23 | 13:35:52 | 13.0 | 16.7 | 0.0 | 190.1 | 0.84 | 2.6 | 15.5 | 0.416 | 0.042 | 98.8% |
| POST3_SPK_0739.LAB | 10/18/23 | 13:36:01 | 13.5 | 16.6 | 0.0 | 190.1 | 0.84 | 2.7 | 15.4 | 0.411 | 0.041 | 98.9% |
| POST3_SPK_0740.LAB | 10/18/23 | 13:36:08 | 13.6 | 16.6 | -0.1 | 190.1 | 0.84 | 2.3 | 15.6 | 0.426 | 0.043 | 98.2% |
| POST3_SPK_0741.LAB | 10/18/23 | 13:36:16 | 13.1 | 16.6 | 0.0 | 190.1 | 0.84 | 2.7 | 15.7 | 0.421 | 0.042 | 99.5% |
| POST3_SPK_0742.LAB | 10/18/23 | 13:36:24 | 12.9 | 16.5 | -0.1 | 190.2 | 0.84 | 2.6 | 15.4 | 0.407 | 0.041 | 99.4% |
| POST3_SPK_0743.LAB | 10/18/23 | 13:36:32 | 13.5 | 16.6 | 0.0 | 190.1 | 0.84 | 2.7 | 15.8 | 0.424 | 0.042 | 99.5% |
| POST3_SPK_0744.LAB | 10/18/23 | 13:36:39 | 13.4 | 16.7 | 0.0 | 190.1 | 0.84 | 2.6 | 15.5 | 0.418 | 0.042 | 98.6% |

CTS, System Purge

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene |
|--------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST3_CTS_0756.LAB | 10/18/23 | 13:39:15 | 0.0 | 0.0 | -0.1 | 190.1 | 0.84 | 101.1 | 0.5 | -0.024 | 100.2% |
| POST3_CTS_0757.LAB | 10/18/23 | 13:39:22 | 0.0 | 0.0 | 0.0 | 190.1 | 0.84 | 100.8 | 0.6 | -0.030 | 100.0% |
| POST3_CTS_0758.LAB | 10/18/23 | 13:39:30 | 0.0 | 0.0 | 0.0 | 190.0 | 0.84 | 100.3 | 0.3 | -0.025 | 99.5% |
| POST3_CTS_0759.LAB | 10/18/23 | 13:39:38 | 0.0 | 0.0 | 0.0 | 190.0 | 0.84 | 100.6 | 0.6 | -0.026 | 99.8% |
| POST3_CTS_0760.LAB | 10/18/23 | 13:39:46 | 0.0 | 0.0 | 0.0 | 190.0 | 0.84 | 100.4 | 0.5 | -0.016 | 99.6% |
| POST3_CTS_0761.LAB | 10/18/23 | 13:39:54 | 0.0 | 0.0 | 0.0 | 190.0 | 0.84 | 101.3 | 0.3 | -0.022 | 100.4% |
| POST3_CTS_0762.LAB | 10/18/23 | 13:40:01 | 0.0 | 0.0 | 0.1 | 190.1 | 0.84 | 100.9 | 0.2 | -0.016 | 100.1% |
| POST3_CTS_0763.LAB | 10/18/23 | 13:40:10 | 0.0 | 0.0 | 0.0 | 190.1 | 0.84 | 100.7 | 0.5 | -0.031 | 99.8% |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Operating Condition: Mill On

Test Location: Main Kiln
 Date: 10/18/2023
 Operator: R. Sollars
 FTIR s/n: E10004

Post Test CTS, Direct Purge

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene |
|------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| CTS_DIR_0854.LAB | 10/18/23 | 14:57:57 | 0.0 | 0.0 | -0.1 | 190.5 | 0.83 | 100.7 | 0.4 | -0.021 | 99.8% |
| CTS_DIR_0855.LAB | 10/18/23 | 14:58:05 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 100.6 | 0.2 | -0.031 | 99.8% |
| CTS_DIR_0856.LAB | 10/18/23 | 14:58:13 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 100.8 | 0.2 | -0.035 | 100.0% |
| CTS_DIR_0857.LAB | 10/18/23 | 14:58:21 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 100.9 | 0.4 | -0.017 | 100.1% |
| CTS_DIR_0858.LAB | 10/18/23 | 14:58:29 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 100.6 | 0.5 | -0.022 | 99.8% |
| CTS_DIR_0859.LAB | 10/18/23 | 14:58:37 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 100.9 | 0.4 | -0.029 | 100.1% |
| CTS_DIR_0860.LAB | 10/18/23 | 14:58:44 | 0.0 | 0.0 | 0.0 | 190.4 | 0.83 | 100.8 | 0.3 | -0.025 | 100.0% |
| CTS_DIR_0861.LAB | 10/18/23 | 14:58:52 | 0.0 | 0.0 | 0.0 | 190.4 | 0.83 | 100.8 | 0.4 | -0.024 | 100.0% |
| Average | | | | | | | | | 100.8 | | |

Post Test N2, Direct Purge

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet |
|-----------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| N2_DIR_0863.LAB | 10/18/23 | 15:02:01 | 0.0 | 0.0 | 0.0 | 190.3 | 0.83 | 0.0 | -0.1 | 0.001 |
| N2_DIR_0864.LAB | 10/18/23 | 15:04:07 | 0.0 | 0.0 | 0.0 | 190.3 | 0.83 | 0.0 | -0.1 | 0.001 |
| N2_DIR_0865.LAB | 10/18/23 | 15:06:13 | 0.0 | 0.0 | 0.0 | 190.3 | 0.83 | 0.0 | 0.0 | 0.001 |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Operating Condition: Mill Off

Test Location: Main Kiln
 Date: 10/17/2023
 Operator: R. Sollars
 FTIR s/n: E10004

System Leak Check: 0.0 mL/min

Nitrogen (Zero) Direct to FTIR

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet |
|--------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| N2_DIR_0012.LAB | 10/17/23 | 6:07:44 | 0.0 | 0.0 | 0.0 | 191.2 | 0.83 | 0.1 | 0.0 | 0.006 |
| N2_DIR_0013BKG.LAB | 10/17/23 | 6:10:01 | 0.0 | 0.0 | 0.0 | 191.1 | 0.83 | 0.0 | 0.0 | 0.000 |
| N2_DIR_0014.LAB | 10/17/23 | 6:10:15 | 0.0 | 0.0 | 0.0 | 191.0 | 0.83 | -0.1 | 0.3 | 0.003 |
| N2_DIR_0015.LAB | 10/17/23 | 6:10:23 | 0.0 | 0.0 | 0.0 | 190.9 | 0.83 | 0.0 | -0.2 | -0.005 |
| N2_DIR_0016.LAB | 10/17/23 | 6:10:30 | 0.0 | 0.0 | 0.0 | 190.9 | 0.83 | -0.2 | -0.1 | 0.001 |
| N2_DIR_0017.LAB | 10/17/23 | 6:10:38 | 0.0 | 0.0 | 0.0 | 190.8 | 0.83 | -0.1 | 0.1 | -0.002 |
| N2_DIR_0018.LAB | 10/17/23 | 6:10:46 | 0.0 | 0.0 | 0.0 | 190.8 | 0.83 | 0.0 | -0.1 | 0.002 |
| N2_DIR_0019.LAB | 10/17/23 | 6:10:54 | 0.0 | 0.0 | 0.0 | 190.8 | 0.83 | 0.1 | -0.1 | -0.001 |
| N2_DIR_0020.LAB | 10/17/23 | 6:11:02 | 0.0 | 0.0 | 0.0 | 190.8 | 0.83 | 0.0 | 0.0 | -0.003 |

Calibration Transfer Standard (CTS), Direct to FTIR

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene |
|------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| CTS_DIR_0035.LAB | 10/17/23 | 6:14:34 | 0.0 | 0.0 | 0.1 | 190.6 | 0.83 | 100.6 | 0.0 | -0.023 | 99.9% |
| CTS_DIR_0036.LAB | 10/17/23 | 6:14:42 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 100.4 | -0.2 | -0.022 | 99.7% |
| CTS_DIR_0037.LAB | 10/17/23 | 6:14:50 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 100.5 | 0.0 | -0.036 | 99.8% |
| CTS_DIR_0038.LAB | 10/17/23 | 6:14:58 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 100.5 | 0.1 | -0.031 | 99.8% |
| CTS_DIR_0039.LAB | 10/17/23 | 6:15:06 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 100.4 | 0.1 | -0.036 | 99.7% |
| CTS_DIR_0040.LAB | 10/17/23 | 6:15:13 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 100.3 | 0.2 | -0.038 | 99.6% |
| CTS_DIR_0041.LAB | 10/17/23 | 6:15:22 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 100.3 | 0.0 | -0.039 | 99.6% |
| Average | | | | | | | | 100.4 | | | 99.7% |

Analyte Spike Gas (HCN) Direct to FTIR

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % HCN |
|-----------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|-------------------|
| 199.2HCN_DIR_0250.LAB | 10/17/23 | 7:06:38 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 1.0 | 198.2 | 10.143 | 99.5% |
| 199.2HCN_DIR_0251.LAB | 10/17/23 | 7:06:46 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 1.2 | 198.4 | 10.145 | 99.6% |
| 199.2HCN_DIR_0252.LAB | 10/17/23 | 7:06:53 | 0.0 | 0.0 | 0.0 | 190.6 | 0.83 | 0.9 | 198.4 | 10.137 | 99.6% |
| 199.2HCN_DIR_0253.LAB | 10/17/23 | 7:07:01 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 0.8 | 198.3 | 10.140 | 99.5% |
| 199.2HCN_DIR_0254.LAB | 10/17/23 | 7:07:10 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 1.1 | 198.2 | 10.137 | 99.5% |
| 199.2HCN_DIR_0255.LAB | 10/17/23 | 7:07:17 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 1.1 | 198.2 | 10.137 | 99.5% |
| 199.2HCN_DIR_0256.LAB | 10/17/23 | 7:07:25 | 0.0 | 0.0 | 0.0 | 190.5 | 0.83 | 0.9 | 198.6 | 10.143 | 99.7% |
| 199.2HCN_DIR_0257.LAB | 10/17/23 | 7:07:33 | 0.0 | 0.0 | 0.0 | 190.4 | 0.83 | 0.9 | 198.6 | 10.145 | 99.7% |
| Average | | | | | | | | | 198.4 | 10.141 | 99.6% |

CTS, System Purge

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene |
|-----------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| CTS_RT_0095.LAB | 10/17/23 | 6:35:59 | 0.1 | 0.0 | 0.0 | 190.8 | 0.83 | 101.0 | 0.0 | -0.021 | 100.3% |
| CTS_RT_0096.LAB | 10/17/23 | 6:36:07 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 100.5 | 0.1 | -0.027 | 99.8% |
| CTS_RT_0097.LAB | 10/17/23 | 6:36:15 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 100.9 | 0.1 | -0.029 | 100.5% |
| CTS_RT_0098.LAB | 10/17/23 | 6:36:23 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 101.5 | -0.1 | -0.022 | 101.1% |
| CTS_RT_0099.LAB | 10/17/23 | 6:36:31 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 101.0 | 0.2 | -0.030 | 100.6% |
| CTS_RT_0100.LAB | 10/17/23 | 6:36:39 | 0.0 | 0.0 | 0.1 | 190.8 | 0.84 | 101.1 | 0.0 | -0.026 | 100.7% |
| CTS_RT_0101.LAB | 10/17/23 | 6:36:47 | 0.0 | 0.0 | 0.1 | 190.8 | 0.83 | 101.5 | -0.1 | -0.022 | 101.0% |
| CTS_RT_0102.LAB | 10/17/23 | 6:36:55 | 0.0 | 0.0 | 0.0 | 190.8 | 0.84 | 100.8 | 0.0 | -0.027 | 100.3% |

Response Time Test

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Response Time (sec) |
|-----------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| CTS_RT_0090.LAB | 10/17/23 | 6:35:20 | 0.6 | 0.0 | 0.1 | 190.8 | 0.84 | 0.0 | -0.2 | 0.000 | - |
| CTS_RT_0091.LAB | 10/17/23 | 6:35:28 | 0.5 | 0.8 | 0.1 | 190.8 | 0.84 | 43.6 | -0.3 | -0.025 | 15.657 |
| CTS_RT_0092.LAB | 10/17/23 | 6:35:36 | 0.1 | 0.0 | 0.0 | 190.8 | 0.84 | 100.8 | 0.0 | -0.032 | 23.657 |
| CTS_RT_0093.LAB | 10/17/23 | 6:35:44 | 0.1 | 0.0 | 0.1 | 190.8 | 0.84 | 100.3 | 0.0 | -0.032 | |
| CTS_RT_0094.LAB | 10/17/23 | 6:35:52 | 0.1 | 0.0 | 0.0 | 190.7 | 0.84 | 100.5 | 0.1 | -0.029 | |
| CTS_RT_0095.LAB | 10/17/23 | 6:35:59 | 0.1 | 0.0 | 0.0 | 190.8 | 0.83 | 101.0 | 0.0 | -0.021 | |
| CTS_RT_0096.LAB | 10/17/23 | 6:36:07 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 100.5 | 0.1 | -0.027 | |
| CTS_RT_0097.LAB | 10/17/23 | 6:36:15 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 100.9 | 0.1 | -0.029 | |
| CTS_RT_0098.LAB | 10/17/23 | 6:36:23 | 0.0 | 0.0 | 0.0 | 190.7 | 0.84 | 101.5 | -0.1 | -0.022 | |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Operating Condition: Mill Off

Test Location: Main Kiln
 Date: 10/17/2023
 Operator: R. Sollars
 FTIR s/n: E10004

Pre 1 Native Effluent Prior to Analyte Spike

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet |
|----------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| PRE1_NATIVE_0293.LAB | 10/17/23 | 7:13:40 | 13.1 | 23.8 | -0.1 | 190.7 | 0.83 | 3.3 | 11.3 | -0.034 |
| PRE1_NATIVE_0294.LAB | 10/17/23 | 7:13:48 | 12.6 | 23.8 | -0.1 | 190.7 | 0.84 | 3.7 | 11.1 | -0.039 |
| PRE1_NATIVE_0295.LAB | 10/17/23 | 7:13:56 | 11.6 | 23.8 | -0.1 | 190.7 | 0.84 | 3.6 | 11.3 | -0.036 |
| | | | | | | | | | 11.3 | -0.036 |

Pre 1 Effluent Spike Using Analyte

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Dilution Factor | Recovery % HCN |
|-------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| PRE1_SPK_0305.LAB | 10/17/23 | 7:16:56 | 11.6 | 21.5 | -0.1 | 190.5 | 0.83 | 2.8 | 21.9 | 0.609 | 0.060 | 97.6% |
| PRE1_SPK_0306.LAB | 10/17/23 | 7:17:04 | 11.4 | 21.3 | -0.1 | 190.5 | 0.83 | 2.7 | 22.0 | 0.617 | 0.061 | 97.1% |
| PRE1_SPK_0307.LAB | 10/17/23 | 7:17:11 | 10.7 | 21.2 | -0.1 | 190.5 | 0.84 | 3.0 | 22.0 | 0.610 | 0.060 | 97.6% |
| PRE1_SPK_0308.LAB | 10/17/23 | 7:17:19 | 10.4 | 21.3 | 0.1 | 190.4 | 0.84 | 3.0 | 22.1 | 0.622 | 0.061 | 97.2% |
| PRE1_SPK_0309.LAB | 10/17/23 | 7:17:27 | 10.7 | 21.5 | 0.0 | 190.4 | 0.83 | 2.6 | 22.3 | 0.620 | 0.061 | 98.1% |
| PRE1_SPK_0310.LAB | 10/17/23 | 7:17:35 | 11.0 | 21.6 | 0.0 | 190.4 | 0.84 | 2.8 | 22.1 | 0.608 | 0.060 | 98.3% |
| PRE1_SPK_0311.LAB | 10/17/23 | 7:17:43 | 11.3 | 21.7 | 0.0 | 190.4 | 0.83 | 2.9 | 22.2 | 0.620 | 0.061 | 98.0% |
| PRE1_SPK_0312.LAB | 10/17/23 | 7:17:51 | 11.4 | 21.8 | -0.1 | 190.4 | 0.84 | 3.4 | 22.0 | 0.616 | 0.061 | 97.4% |

Native Effluent Prior to Analyte Spike

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet |
|---------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| Run1_0440.LAB | 10/17/23 | 9:06:51 | 12.7 | 25.3 | -0.1 | 190.5 | 0.85 | 3.4 | 13.3 | -0.040 |
| Run1_0441.LAB | 10/17/23 | 9:07:54 | 12.0 | 24.5 | -0.1 | 190.4 | 0.85 | 2.9 | 13.5 | -0.040 |
| Run1_0442.LAB | 10/17/23 | 9:08:57 | 12.3 | 24.7 | -0.1 | 190.5 | 0.85 | 2.8 | 13.4 | -0.042 |
| | | | | | | | | | 13.4 | -0.041 |

Effluent Spike Using Analyte

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Dilution Factor | Recovery % HCN |
|--------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST1_SPK_0452.LAB | 10/17/23 | 9:13:26 | 11.6 | 23.0 | -0.1 | 190.1 | 0.84 | 2.8 | 23.5 | 0.556 | 0.055 | 99.8% |
| POST1_SPK_0453.LAB | 10/17/23 | 9:13:34 | 11.0 | 23.5 | 0.0 | 190.1 | 0.84 | 2.5 | 23.9 | 0.549 | 0.054 | 102.1% |
| POST1_SPK_0454.LAB | 10/17/23 | 9:13:42 | 10.7 | 24.0 | 0.0 | 190.1 | 0.84 | 3.1 | 23.8 | 0.547 | 0.054 | 101.9% |
| POST1_SPK_0455.LAB | 10/17/23 | 9:13:50 | 11.0 | 24.2 | -0.1 | 190.1 | 0.84 | 2.9 | 23.5 | 0.547 | 0.054 | 100.4% |
| POST1_SPK_0456.LAB | 10/17/23 | 9:13:58 | 11.5 | 24.4 | 0.0 | 190.2 | 0.84 | 2.7 | 23.7 | 0.545 | 0.054 | 101.7% |
| POST1_SPK_0457.LAB | 10/17/23 | 9:14:05 | 11.7 | 24.4 | -0.1 | 190.2 | 0.84 | 3.1 | 23.5 | 0.561 | 0.055 | 99.5% |
| POST1_SPK_0458.LAB | 10/17/23 | 9:14:13 | 11.7 | 24.3 | 0.0 | 190.2 | 0.84 | 2.9 | 23.5 | 0.557 | 0.055 | 99.8% |
| POST1_SPK_0459.LAB | 10/17/23 | 9:14:21 | 11.7 | 23.9 | -0.1 | 190.2 | 0.84 | 3.0 | 23.7 | 0.546 | 0.054 | 101.7% |

CTS, System Purge

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene |
|--------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST1_CTS_0470.LAB | 10/17/23 | 9:16:42 | 0.1 | 0.0 | 0.1 | 190.5 | 0.84 | 100.7 | 0.4 | -0.024 | 100.3% |
| POST1_CTS_0471.LAB | 10/17/23 | 9:16:50 | 0.1 | 0.1 | 0.0 | 190.5 | 0.84 | 100.2 | 0.5 | -0.024 | 99.8% |
| POST1_CTS_0472.LAB | 10/17/23 | 9:16:58 | 0.0 | 0.0 | 0.0 | 190.5 | 0.84 | 100.9 | 0.3 | -0.032 | 100.5% |
| POST1_CTS_0473.LAB | 10/17/23 | 9:17:06 | 0.0 | 0.0 | 0.0 | 190.6 | 0.84 | 100.8 | 0.4 | -0.012 | 100.4% |
| POST1_CTS_0474.LAB | 10/17/23 | 9:17:14 | 0.1 | 0.0 | 0.0 | 190.6 | 0.84 | 100.4 | 0.5 | -0.027 | 100.0% |
| POST1_CTS_0475.LAB | 10/17/23 | 9:17:21 | 0.0 | 0.0 | 0.1 | 190.6 | 0.84 | 100.2 | 0.4 | -0.030 | 99.7% |
| POST1_CTS_0476.LAB | 10/17/23 | 9:17:29 | 0.0 | 0.0 | 0.1 | 190.5 | 0.84 | 100.8 | 0.6 | -0.026 | 100.4% |
| POST1_CTS_0477.LAB | 10/17/23 | 9:17:37 | 0.0 | 0.1 | 0.1 | 190.5 | 0.84 | 100.4 | 0.2 | -0.028 | 100.0% |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Operating Condition: Mill Off

Test Location: Main Kiln
 Date: 10/17/2023
 Operator: R. Sollars
 FTIR s/n: E10004

Native Effluent Prior to Analyte Spike

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet |
|---------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| RUN2_0803.LAB | 10/17/23 | 14:43:41 | 12.6 | 25.8 | -0.1 | 189.7 | 0.84 | 3.0 | 13.7 | -0.035 |
| RUN2_0804.LAB | 10/17/23 | 14:44:44 | 12.4 | 25.6 | -0.1 | 189.6 | 0.84 | 2.8 | 13.6 | -0.033 |
| RUN2_0805.LAB | 10/17/23 | 14:45:47 | 12.6 | 25.8 | -0.1 | 189.7 | 0.84 | 3.0 | 13.5 | -0.035 |
| | | | | | | | | | 13.6 | -0.034 |

Effluent Spike Using Analyte

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Dilution Factor | Recovery % HCN |
|--------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST2_SPK_0822.LAB | 10/17/23 | 14:49:49 | 11.8 | 24.1 | -0.2 | 189.6 | 0.84 | 3.3 | 25.7 | 0.658 | 0.065 | 100.4% |
| POST2_SPK_0823.LAB | 10/17/23 | 14:49:57 | 11.8 | 24.3 | -0.1 | 189.6 | 0.83 | 3.1 | 25.8 | 0.668 | 0.066 | 100.1% |
| POST2_SPK_0824.LAB | 10/17/23 | 14:50:05 | 11.8 | 24.3 | -0.1 | 189.5 | 0.83 | 2.9 | 25.7 | 0.668 | 0.066 | 99.8% |
| POST2_SPK_0825.LAB | 10/17/23 | 14:50:13 | 11.8 | 24.4 | -0.1 | 189.6 | 0.84 | 3.0 | 25.3 | 0.668 | 0.066 | 98.3% |
| POST2_SPK_0826.LAB | 10/17/23 | 14:50:21 | 11.8 | 24.2 | -0.1 | 189.5 | 0.84 | 3.0 | 25.8 | 0.673 | 0.066 | 99.9% |
| POST2_SPK_0827.LAB | 10/17/23 | 14:50:28 | 11.7 | 24.0 | -0.1 | 189.6 | 0.83 | 3.1 | 26.1 | 0.679 | 0.067 | 100.5% |
| POST2_SPK_0828.LAB | 10/17/23 | 14:50:36 | 11.6 | 23.6 | -0.1 | 189.6 | 0.84 | 3.1 | 26.1 | 0.672 | 0.066 | 101.0% |
| POST2_SPK_0829.LAB | 10/17/23 | 14:50:44 | 11.5 | 23.3 | -0.1 | 189.6 | 0.83 | 2.9 | 25.7 | 0.659 | 0.065 | 100.6% |

CTS, System Purge

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene |
|--------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST2_CTS_0832.LAB | 10/17/23 | 14:52:19 | 0.1 | 0.1 | 0.0 | 189.6 | 0.83 | 100.7 | 0.9 | -0.026 | 100.2% |
| POST2_CTS_0833.LAB | 10/17/23 | 14:52:27 | 0.1 | 0.1 | 0.1 | 189.7 | 0.83 | 100.5 | 0.4 | -0.014 | 100.1% |
| POST2_CTS_0834.LAB | 10/17/23 | 14:52:35 | 0.1 | 0.1 | 0.1 | 189.7 | 0.83 | 101.6 | 0.8 | -0.042 | 101.2% |
| POST2_CTS_0835.LAB | 10/17/23 | 14:52:43 | 0.1 | 0.0 | 0.0 | 189.7 | 0.83 | 100.9 | 0.6 | -0.018 | 100.5% |
| POST2_CTS_0836.LAB | 10/17/23 | 14:52:51 | 0.1 | 0.1 | 0.0 | 189.8 | 0.83 | 100.2 | 0.6 | -0.028 | 99.8% |
| POST2_CTS_0837.LAB | 10/17/23 | 14:52:59 | 0.1 | 0.1 | 0.0 | 189.8 | 0.83 | 100.7 | 0.5 | -0.009 | 100.3% |
| POST2_CTS_0838.LAB | 10/17/23 | 14:53:07 | 0.1 | 0.0 | 0.0 | 189.7 | 0.84 | 101.1 | 0.5 | -0.019 | 100.7% |
| POST2_CTS_0839.LAB | 10/17/23 | 14:53:14 | 0.1 | 0.0 | 0.0 | 189.7 | 0.83 | 101.2 | 0.5 | -0.017 | 100.8% |

Native Effluent Prior to Analyte Spike

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene |
|--------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST3_CTS_0965.LAB | 10/17/23 | 16:21:08 | 0.1 | 0.1 | 0.0 | 189.7 | 0.83 | 100.2 | 0.8 | -0.001 | 99.7% |
| POST3_CTS_0966.LAB | 10/17/23 | 16:21:16 | 0.1 | 0.1 | 0.0 | 189.7 | 0.83 | 100.8 | 0.9 | -0.007 | 100.4% |
| POST3_CTS_0967.LAB | 10/17/23 | 16:21:24 | 0.1 | 0.1 | 0.0 | 189.7 | 0.83 | 100.7 | 1.1 | -0.015 | 100.3% |
| POST3_CTS_0968.LAB | 10/17/23 | 16:21:31 | 0.1 | 0.1 | 0.0 | 189.7 | 0.83 | 100.7 | 0.8 | -0.013 | 100.3% |
| POST3_CTS_0969.LAB | 10/17/23 | 16:21:40 | 0.1 | 0.1 | 0.0 | 189.7 | 0.83 | 100.6 | 0.7 | -0.024 | 100.2% |
| POST3_CTS_0970.LAB | 10/17/23 | 16:21:47 | 0.1 | 0.0 | 0.0 | 189.6 | 0.83 | 101.0 | 0.6 | -0.024 | 100.6% |
| POST3_CTS_0971.LAB | 10/17/23 | 16:21:55 | 0.1 | 0.0 | 0.0 | 189.6 | 0.83 | 101.0 | 0.7 | -0.016 | 100.6% |
| POST3_CTS_0972.LAB | 10/17/23 | 16:22:03 | 0.1 | 0.0 | 0.0 | 189.6 | 0.83 | 101.0 | 0.8 | -0.008 | 100.6% |

Client: GCC Rio Grande, Inc.
 Facility: Pueblo Plant
 Project #: M234207
 Operating Condition: Mill Off

Test Location: Main Kiln
 Date: 10/17/2023
 Operator: R. Sollars
 FTIR s/n: E10004

Post Test CTS, Direct Purge

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet | Recovery % Ethylene |
|------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| CTS_DIR_1045.LAB | 10/17/23 | 17:20:16 | 0.0 | 0.0 | 0.0 | 189.5 | 0.82 | 100.6 | 0.2 | -0.020 | 100.2% |
| CTS_DIR_1046.LAB | 10/17/23 | 17:20:32 | 0.0 | 0.0 | 0.1 | 189.5 | 0.82 | 100.5 | 0.2 | -0.030 | 100.1% |
| CTS_DIR_1047.LAB | 10/17/23 | 17:20:47 | 0.0 | 0.0 | 0.0 | 189.5 | 0.82 | 100.6 | 0.2 | -0.022 | 100.2% |
| CTS_DIR_1048.LAB | 10/17/23 | 17:21:03 | 0.0 | 0.0 | 0.0 | 189.4 | 0.82 | 100.6 | 0.3 | -0.025 | 100.1% |
| CTS_DIR_1049.LAB | 10/17/23 | 17:21:19 | 0.0 | 0.0 | 0.0 | 189.5 | 0.82 | 100.9 | 0.2 | -0.017 | 100.5% |
| CTS_DIR_1050.LAB | 10/17/23 | 17:21:34 | 0.0 | 0.0 | 0.0 | 189.5 | 0.82 | 100.5 | 0.1 | -0.023 | 100.1% |
| CTS_DIR_1051.LAB | 10/17/23 | 17:21:50 | 0.0 | 0.0 | 0.0 | 189.5 | 0.82 | 100.5 | 0.3 | -0.023 | 100.1% |
| CTS_DIR_1052.LAB | 10/17/23 | 17:22:06 | 0.0 | 0.0 | 0.0 | 189.5 | 0.82 | 100.2 | 0.0 | -0.023 | 99.8% |
| Average | | | | | | | | 100.6 | | | |

Post Test N2, Direct Purge

| Spectrum | Date | Time | H2O% %v | CO2 %v wet | HF ppmv wet | FTIR Gas Cell Temperature deg C | FTIR Gas Cell Pressure atm | Ethylene ppmv wet | HCN ppmv wet | SF6 ppmv wet |
|-----------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| N2_DIR_1054.LAB | 10/17/23 | 17:25:26 | 0.0 | 0.0 | 0.0 | 189.5 | 0.82 | -0.1 | 0.1 | 0.002 |
| N2_DIR_1055.LAB | 10/17/23 | 17:27:32 | 0.0 | 0.0 | 0.0 | 189.5 | 0.82 | -0.1 | 0.1 | 0.001 |
| N2_DIR_1056.LAB | 10/17/23 | 17:29:38 | 0.0 | 0.0 | 0.0 | 189.5 | 0.82 | -0.1 | 0.2 | 0.001 |

| Time | DL summary - zero gas | | Time | DL summary - in stack | |
|---------------------------|-----------------------|----------------|---------------------------|-----------------------|----------------|
| | HF ppm (10) 191C | HCN (100) 191C | | HF ppm (10) 191C | HCN (100) 191C |
| 6:03:36 AM | 0.02 | 0.14 | 6:53:47 AM | -0.04 | -0.23 |
| 6:03:44 AM | -0.02 | 0.02 | 6:53:55 AM | 0.02 | -0.12 |
| 6:03:51 AM | -0.03 | 0.14 | 6:54:03 AM | 0.00 | -0.50 |
| 6:03:59 AM | 0.03 | -0.01 | 6:54:10 AM | -0.04 | -0.33 |
| 6:04:07 AM | -0.06 | -0.33 | 6:54:18 AM | -0.02 | -0.09 |
| 6:04:15 AM | -0.03 | -0.18 | 6:54:26 AM | -0.05 | -0.14 |
| 6:04:23 AM | -0.05 | -0.23 | 6:54:34 AM | -0.04 | -0.21 |
| Standard Deviation | 0.03 | 0.17 | Standard Deviation | 0.02 | 0.13 |
| 3x = DL | 0.10 | 0.51 | 3x = DL | 0.07 | 0.40 |

Appendix I - Gas Cylinder Certifications

Detection Limit

The detection limit of each analyte was calculated following Annex A2 of ASTM D6348-12 procedure using spectra that contained similar amounts of moisture.

| FTIR DETECTION LIMITS | | | |
|------------------------------|-----------------------------------|-----------------------------|---------------------------------|
| Analyte | Detection Limit (ppmv wet) | Detection Limit (%v) | Detection Limit (%v wet) |
| Hydrogen Cyanide | 0.4 | — | — |
| Hydrogen Fluoride | 0.1 | | |
| Water | — | 0.1 | N/A |
| Carbon Dioxide | — | N/A | 0.1 |

Copies of gas cylinder certifications are appended. All concentration data were recorded on a wet, volume basis. HCN spiking was performed prior to testing to confirm the measurement system's ability to deliver and quantify HCN. The sample and data collection followed the procedures outlined in Methods 320.

CERTIFICATE OF ANALYSIS

Grade of Product: EPA PROTOCOL STANDARD

| | |
|--|----------------------------------|
| Part Number: E03NI78E15A0225 | Reference Number: 48-402737254-1 |
| Cylinder Number: CC175274 | Cylinder Volume: 152.0 CF |
| Laboratory: 124 - Los Angeles (SAP) - CA | Cylinder Pressure: 2015 PSIG |
| PGVP Number: B32023 | Valve Outlet: 590 |
| Gas Code: CO2,O2,BALN | Certification Date: May 11, 2023 |

Expiration Date: May 11, 2031

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS

| Component | Requested Concentration | Actual Concentration | Protocol Method | Total Relative Uncertainty | Assay Dates |
|----------------|-------------------------|----------------------|-----------------|----------------------------|-------------|
| CARBON DIOXIDE | 11.00 % | 11.18 % | G1 | +/- 0.6% NIST Traceable | 05/11/2023 |
| OXYGEN | 11.00 % | 11.07 % | G1 | +/- 0.9% NIST Traceable | 05/11/2023 |
| NITROGEN | Balance | | | | |

CALIBRATION STANDARDS

| Type | Lot ID | Cylinder No | Concentration | Uncertainty | Expiration Date |
|------|----------|--------------|---------------------------------|-------------|-----------------|
| NTRM | 08010611 | K005428 | 13.94 % CARBON DIOXIDE/NITROGEN | +/- 0.6% | Jan 30, 2024 |
| NTRM | 98051002 | SG9150866BAL | 12.05 % OXYGEN/NITROGEN | +/- 0.7% | Dec 14, 2023 |

ANALYTICAL EQUIPMENT

| Instrument/Make/Model | Analytical Principle | Last Multipoint Calibration |
|-----------------------|----------------------|-----------------------------|
| SIEMENS 6E CO2 | NDIR | Apr 26, 2023 |
| SIEMENS OXYMAT 6 | PARAMAGNETIC | Apr 21, 2023 |

Triad Data Available Upon Request



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: CERTIFIED STANDARD-SPEC

| | | | |
|------------------|-------------------------|--------------------|-----------------|
| Part Number: | X02NI99C15A1268 | Reference Number: | 153-402780689-1 |
| Cylinder Number: | CC401933 | Cylinder Volume: | 144.0 CF |
| Laboratory: | 124 - Tooele (SAP) - UT | Cylinder Pressure: | 2015 PSIG |
| Analysis Date: | Jul 10, 2023 | Valve Outlet: | 350 |
| Lot Number: | 153-402780689-1 | | |

Expiration Date: Jul 10, 2026

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

| Component | Req Conc | Actual Concentration (Mole %) | Analytical Uncertainty |
|-----------|-----------|----------------------------------|---------------------------|
| ETHYLENE | 100.0 PPM | 100.7 PPM | +/- 2% |
| NITROGEN | Balance | | |



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: EPA PROTOCOL STANDARD

| | |
|-------------------------------------|-----------------------------------|
| Part Number: E03NI59E15A3452 | Reference Number: 153-402157382-1 |
| Cylinder Number: CC420519 | Cylinder Volume: 159.0 CF |
| Laboratory: 124 - Tooele (SAP) - UT | Cylinder Pressure: 2015 PSIG |
| PGVP Number: B72021 | Valve Outlet: 590 |
| Gas Code: CO2,O2,BALN | Certification Date: Jul 15, 2021 |

Expiration Date: Jul 15, 2029

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS

| Component | Requested Concentration | Actual Concentration | Protocol Method | Total Relative Uncertainty | Assay Dates |
|----------------|-------------------------|----------------------|-----------------|----------------------------|-------------|
| CARBON DIOXIDE | 19.00 % | 18.99 % | G1 | +/- 0.6% NIST Traceable | 07/15/2021 |
| OXYGEN | 22.00 % | 22.41 % | G1 | +/- 0.3% NIST Traceable | 07/15/2021 |
| NITROGEN | Balance | | | | |

CALIBRATION STANDARDS

| Type | Lot ID | Cylinder No | Concentration | Uncertainty | Expiration Date |
|------|----------|-------------|---------------------------------|-------------|-----------------|
| NTRM | 13060802 | CC415397 | 24.04 % CARBON DIOXIDE/NITROGEN | 0.6% | Dec 11, 2025 |
| NTRM | 12062008 | CC367433 | 22.883 % OXYGEN/NITROGEN | 0.2% | May 14, 2024 |

ANALYTICAL EQUIPMENT

| Instrument/Make/Model | Analytical Principle | Last Multipoint Calibration |
|-----------------------------|-------------------------|-----------------------------|
| Horiba VIA-510 SV4MEUTJ CO2 | CO2 NDIR (Dixon) | Jun 17, 2021 |
| Horiba MPA-510 W603MM58 O2 | O2 Paramagnetic (Mason) | Jul 12, 2021 |

Triad Data Available Upon Request



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: CERTIFIED STANDARD-SPEC

| | | | |
|------------------|---------------------------|--------------------|-----------------|
| Part Number: | X03NI99C15AC0Y6 | Reference Number: | 160-402841636-1 |
| Cylinder Number: | CC768255 | Cylinder Volume: | 144.4 CF |
| Laboratory: | 124 - Plumsteadville - PA | Cylinder Pressure: | 2015 PSIG |
| Analysis Date: | Sep 12, 2023 | Valve Outlet: | 350SS |
| Lot Number: | 160-402841636-1 | | |

Expiration Date: Mar 12, 2024

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

| Component | Req Conc | Actual Concentration (Mole %) | Analytical Uncertainty |
|---------------------|-----------|----------------------------------|---------------------------|
| SULFUR HEXAFLUORIDE | 10.00 PPM | 10.00 PPM | +/- 5% |
| HYDROGEN CYANIDE | 200.0 PPM | 199.2 PPM | +/- 5% |
| NITROGEN | Balance | | |



Signature on file

END OF THE REPORT