

Section 114 Information Collection Request Emissions Test Report

GCC Rio Grande Inc.
Tijeras Plant
EPA Registry ID: 110000600831
Kiln Stack
11783 Highway 337
Tijeras, NM 87059
Report No. M234302





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Emissions Test Report**

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**Report Submittal Date:
December 20, 2023**

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1.0 INTRODUCTION

Mostardi Platt conducted an air emissions test program for GCC Rio Grande Inc. at the Tijeras Plant located in Tijeras, New Mexico. All testing was performed as described in the *Code of Federal Regulations*, Title 40, Part 60, Appendix A (40CFR60), Methods 1, 2, 3A, 4, 26A, and 40CFR63, Appendix A, (40CFR63) Method 320.

This test program was completed to satisfy the requirements of the United States Environmental Protection Agency (USEPA) Section 114 Information Collection Request for Portland Cement Manufacturing facilities.

The identification of individuals associated with the test program is summarized below:

Location	Address	Contact
Facility Representative	GCC Rio Grande, Inc. 11783 Highway 337 Tijeras, NM 87059	Samantha Kretz P: 505-286-6081 E: skretz@gcc.com
Testing Company Representative	Mostardi Platt 7715 Commercial Way Suite 155 Henderson, NV 89011	Rich Sollars P: (630) 993-2100 (phone) E: rsollars@mp-mail.com

2.0 TEST REQUIREMENTS

Testing was performed at the kiln stack. The following table presents a list of the parameters tested, the applicable methodologies utilized, and average test results:

Source	Parameter Tested	Test Results	Method/Regulation Citation
Kiln Stack	Hydrogen Fluoride (HF)	≤ 0.10 ppmvw	USEPA Method 320, 40CFR63, Appendix A
		≤ 0.30 ppmvd @7% O ₂	
		≤ 0.06 lb/hr	
		≤ 0.0010 lb/ton clinker	
	HF ¹	≤ 0.13 ppmvd	Method 26A, 40CFR60, Appendix A
		≤ 0.38 ppmvd @7% O ₂	
		≤ 0.07 lb/hr	
		≤ 0.0013 lb/ton clinker	
	Chlorine (Cl ₂) ¹	≤ 0.04 ppmvd	USEPA Method 26A, 40CFR60, Appendix A
		≤ 0.12 ppmvd @7% O ₂	
		≤ 0.08 lb/hr	
		≤ 0.0014 lb/ton clinker	
	Hydrogen Cyanide (HCN)	1.91 ppmvw	USEPA Method 320, 40CFR63, Appendix A
		5.78 ppmvd @7% O ₂	
1.48 lb/hr			
0.0271 lb/ton clinker			
Oxygen (O ₂)	16.2 % (dry)	USEPA Method 3A, 40CFR60, Appendix A	
Carbon Dioxide (CO ₂)	6.3 % (dry)	USEPA Method 320, 40CFR63, Appendix A	
Moisture (H ₂ O)	2.8 %	USEPA Method 320, 40CFR63, Appendix A	
Cyclonic Flow Determination	PASS	USEPA Method 1, 40CFR60, Appendix A, Section 11.4	
Three-point O ₂ Stratification Determination	< 5 %	USEPA Method 3A, 40CFR60, Appendix A and Method 7E, Section 8.1.2	

¹ HF and Cl₂ Method 26A results are reported as the average from Train A and Train B.

3.0 QA SPECIFICATIONS AND PROCESS DIAGRAM

Table 3-1 QA/QC Specifications

Parameter	Method	QA/QC Specification	Acceptance Criteria	Actual Result
HCN	320	Method Detection Limit	0.5 ppm	0.2 ppmvw
		SNR	>2500 at 64 scans	6266 (Run 1 Average)
		S Beam	>0.9	1.549 (Run 1 Average)
		Direct HCN Analysis	±5% of tag value	-3.1%
		Dynamic Spike Analysis	≤10% of total sample volume	8.4%
			Spike gas ~twice native concentration or 3-4 ppm addition to native concentration	+4.0 ppmvw
			≤±20% of expected value or ≤±0.5 ppm, whichever is less restrictive	+1.2 %
Residuals	≤±0.3 ppm, or ≤±5% of measured value, whichever is less restrictive	0.4 ppmvw		
Cl ₂	26A	Detection Limit	300 µg	150 µg
		Paired Train Agreement	≤10% Relative Deviation or ≤0.2 ppm, whichever is less restrictive.	0.01 ppmvd

4.0 TEST PROCEDURES

All testing, sampling, analytical, and calibration procedures used for this test program were performed as described in the Title 40, *Code of Federal Regulations*, Part 60, Appendix A (40CFR60), Methods 1, 2, 3A, 4, 26A, and 40CFR63, Appendix A, Method 320; and the latest revisions thereof. Where applicable, the *Quality Assurance Handbook for Air Pollution Measurement Systems*, Volume III, Stationary Source Specific Methods, United States Environmental Protection Agency (USEPA) 600/R-94/038c, September 1994 was used to supplement procedures in addition to the appended "Draft General Test Plan".

4.1 Method 1 Sample and Velocity Traverse Determination

Sample points for testing are determined using USEPA Test Method 1, 40CFR60, Appendix A. The characteristics of the measurement location is summarized below.

Sample Point Selection

Test Location	Stack Diameter	Port Length	Upstream Diameters	Downstream Diameters	Test Parameter	Number of Sampling Points
Main Kiln	132 Inches	6.0 Inches	3.3 Diameters	9.2 Diameters	HF/Cl ₂ (26A)	24
					O ₂ (3A)	3 (stratification)
					HCN/HF/CO ₂ (320/3A)	1

A cyclonic flow check was performed in accordance with Section 11.4, which demonstrated it meets the criteria of an average value of less than 20° and therefore is considered to be a suitable testing location for flow rate measurements.

4.2 Method 2 Volumetric Flow Rate Determination

The gas velocity and volumetric flowrate were determined using Method 2, 40CFR60, Appendix A, as an integrated part of the HF/Cl₂ sampling system.

Velocity pressures were determined by traversing the duct with wind tunnel calibrated S-type pitot tube. Temperatures were measured using K-type thermocouples with calibrated digital temperature indicators. The molecular weight and moisture content of the gases were also determined to permit the calculation of the volumetric flowrate.

4.3 Method 3A Oxygen (O₂) and Carbon Dioxide (CO₂) Determination

O₂ and CO₂ concentrations were determined in accordance with Method 3A, 40CFR60, Appendix A and Method 320, 40CFR63, Appendix A, respectively. A Servomex analyzer was used to determine O₂ concentrations while the MKS 2030 analyzer was used to determine CO₂ concentrations. The O₂ instrument has a paramagnetic detector and operates in a nominal range of 0-25%.

A list of calibration gases used and the results of all calibration and other required quality assurance checks are found in the appendix of this report. Copies of calibration gas certifications are also appended.

4.4 Method 26A Hydrogen Fluoride (HF) and Chlorine (Cl₂) Determination

HF and Cl₂ concentrations and emission rates were determined in accordance with Method 26A, 40CFR60, Appendix A. Paired sampling trains were used to collect the samples. A total of twelve (12) test points were sampled per run on the kiln stack. The sample was extracted isokinetically from the gas stream and passed through dilute sulfuric acid (0.1N H₂SO₄). HF was collected in the dilute acid. Cl₂ was collected in the dilute sodium hydroxide (0.1N NaOH) solution. The sample train consisted of a Teflon coated nozzle, a heated borosilicate glass probe liner, a Teflon® filter placed on the outlet of the glass probe liner, and six impingers. The first two impingers contained the 0.1N H₂SO₄, the third remained empty (and was recovered with the first two impingers), the fourth and fifth impingers contained the 0.1N NaOH, while the sixth impinger contained silica gel to absorb any remaining moisture. A de-ionized water rinse was performed on each set of impingers, and samples were stored in Nalgene sample containers for transport. The 0.1N H₂SO₄ impinger catch samples were analyzed for HF while the 0.1N NaOH impinger catch samples were analyzed for Cl₂. A method detection limit (MDL) of 150 µg was determined for both HF and Cl₂ using the "Definition and Procedure for the Determination of the Method Detection Limit, Revision 2". All equipment used was calibrated in accordance with the specifications of the method. Calibration data is appended.

Hand recorded field data sheets were reviewed and scans are retained on the Mostardi Platt network. Copies of this data is available upon request.

4.5 Method 320 Speciated Flue Gas Concentration Determinations

The sampling procedures for HCN and HF were performed in accordance with USEPA Method 320, 40CFR63, Appendix A. Data was continuously recorded with a data logging system throughout sampling, with brief interruption to properly label reference spectra.

The average gas effluent concentrations were determined from the average gas concentration displayed by the MKS 2030 analyzer.

All sampling system components were heated to 375°F +/- 25°F, including: stainless steel sample probe, stainless steel calibration tee, in line glass fiber particulate filter, Teflon® sample line, heated head sample pump, and FTIR detector cell. The sample pump distributes the gas sample to the instrument at a steady sample flow rate (+/- 10%). All components of the sampling system are constructed of stainless steel, glass, or Teflon®.

FTIR technology works on the principle that most gases absorb infrared light. This is true for all compounds except for homonuclear diatomic molecules and noble gases such as: N₂, O₂, H₂, He, Ne, and Ar. Vibrations, stretches, bends, and rotations within the bonds of a molecule determine the infrared absorption distinctiveness. The absorption creates a "fingerprint" which is unique for each given compound. The quantity of infrared light absorbed is proportional to the gas concentration. Most compounds have absorbencies at different infrared frequencies, thus allowing the simultaneous analysis of multiple compounds at one time. The FTIR software compares each sample spectrum to a user-selected list of calibration references and concentration data is generated.

FTIR data was collected using an MKS MultiGas 2030 FTIR spectrometer. Data was generated at 0.5 cm⁻¹. Each Spectra was derived from the coaddition of 62-64 scans with a new data point generated approximately every minute. HCN analyte spiking assured the ability of the FTIR to quantify HCN in the presence of effluent gas. All analyte spikes were introduced using an instrument grade stainless steel rotameter. All QA/QC procedures were within the acceptance criteria allowance of the applicable methodology and the "General Test Plan."

5.0 TEST RESULTS SUMMARIES

Client: GCC Rio Grande Inc.
Facility: Tijeras Plant
Test Location: Main Stack
Test Method: 26A Combined

	Source Condition	Normal	Normal	Normal	
	Date	10/24/23	10/24/23	10/24/23	
	Start Time	8:00	10:00	12:00	
	End Time	9:20	11:11	13:10	
	Run 1	Run 2	Run 3	Average	
Stack Conditions					
Average Gas Velocity, ft/sec	62.325	62.631	61.152	62.036	
Gas Volumetric Flow Rate, acfm	355,373	357,119	348,689	353,727	
Gas Volumetric Flow Rate, dscfm	179,986	179,302	176,009	178,432	
Gas Volumetric Flow Rate, scfm	185,601	185,368	181,849	184,272	
Average %CO ₂ by volume, dry basis	6.2	6.3	6.5	6.3	
Average %O ₂ by volume, dry basis	16.1	16.2	16.2	16.2	
Clinker Production, ton/hr	53.5	53.5	57.6	54.9	
Chloride (Cl₂) Emissions					
ppm	≤ 0.04	≤ 0.04	≤ 0.04	≤ 0.04	
ppm@7%O ₂	≤ 0.12	≤ 0.12	≤ 0.12	≤ 0.12	
lb/hr	≤ 0.08	≤ 0.08	≤ 0.08	≤ 0.08	
lb/ton of clinker	≤ 0.0015	≤ 0.0015	≤ 0.0013	≤ 0.0014	
Hydrogen Fluoride (HF) Emissions					
ppm	≤ 0.13	≤ 0.13	≤ 0.13	≤ 0.13	
ppm@7%O ₂	≤ 0.38	≤ 0.38	≤ 0.38	≤ 0.38	
lb/hr	≤ 0.07	≤ 0.07	≤ 0.07	≤ 0.07	
lb/ton of clinker	≤ 0.0014	≤ 0.0014	≤ 0.0012	≤ 0.0013	

Client: GCC Rio Grande Inc.
Facility: Tijeras Plant
Test Location: Main Stack
Test Method: 5/26A

Source Condition	Normal	Normal	Normal
Date	10/24/23	10/24/23	10/24/23
Start Time	8:00	10:00	12:00
End Time	9:20	11:11	13:10

	Run 1A	Run 2A	Run 3A	Average
Stack Conditions				
Average Gas Temperature, °F	337.8	343.8	341.4	341.0
Flue Gas Moisture, percent by volume	3.1%	3.3%	3.0%	3.1%
Average Flue Pressure, in. Hg	23.64	23.64	23.64	23.64
Gas Sample Volume, dscf	49.875	50.403	49.143	49.807
Average Gas Velocity, ft/sec	60.514	61.667	59.909	60.697
Gas Volumetric Flow Rate, acfm	345,051	351,625	341,603	346,093
Gas Volumetric Flow Rate, dscfm	174,778	176,437	172,400	174,538
Gas Volumetric Flow Rate, scfm	180,423	182,488	177,803	180,238
Average %CO ₂ by volume, dry basis	6.2	6.3	6.5	6.3
Average %O ₂ by volume, dry basis	16.1	16.2	16.2	16.2
Isokinetic Variance	100.7	100.8	100.6	100.7
Clinker Production, ton/hr	53.5	53.5	57.6	54.9

Chloride (Cl₂) Emissions				
ug of sample collected	≤ 150.00	≤ 150.00	≤ 150.00	≤ 150.00
ppm	≤ 0.04	≤ 0.04	≤ 0.04	≤ 0.04

Hydrogen Fluoride (HF) Emissions				
ug of sample collected	≤ 150.00	≤ 150.00	≤ 150.00	≤ 150.00
ppm	≤ 0.13	≤ 0.13	≤ 0.13	≤ 0.13

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Test Method: 26A

	Source Condition	Normal	Normal	Normal	
	Date	10/24/23	10/24/23	10/24/23	
	Start Time	8:00	10:00	12:00	
	End Time	9:20	11:11	13:10	
	Run 1B	Run 2B	Run 3B	Average	
Stack Conditions					
Average Gas Temperature, °F	339.4	343.3	338.2	340.3	
Flue Gas Moisture, percent by volume	2.9%	3.2%	3.4%	3.2%	
Average Flue Pressure, in. Hg	23.63	23.63	23.63	23.63	
Gas Sample Volume, dscf	50.924	50.220	49.605	50.250	
Average Gas Velocity, ft/sec	64.135	63.594	62.395	63.375	
Gas Volumetric Flow Rate, acfm	365,695	362,612	355,774	361,360	
Gas Volumetric Flow Rate, dscfm	185,194	182,166	179,617	182,326	
Gas Volumetric Flow Rate, scfm	190,778	188,248	185,894	188,307	
Average %CO ₂ by volume, dry basis	6.2	6.3	6.5	6.3	
Average %O ₂ by volume, dry basis	16.1	16.2	16.2	16.2	
Isokinetic Variance	100.5	100.7	100.9	100.7	
Clinker Production, ton/hr	53.5	53.5	57.6	54.9	
Chloride (Cl₂) Emissions					
ug of sample collected	≤ 150.00	≤ 150.00	≤ 150.00	≤ 150.00	
ppm	≤ 0.04	≤ 0.04	≤ 0.04	≤ 0.04	
Hydrogen Fluoride (HF) Emissions					
ug of sample collected	≤ 150.00	≤ 150.00	≤ 150.00	≤ 150.00	
ppm	≤ 0.13	≤ 0.13	≤ 0.13	≤ 0.13	

GCC Rio Grande, Inc.

Tijeras Plant

Main Stack

Reference Method Test Data

Test No.	Date	Start Time	End Time	O2 % (dry)	Moisture %	HCN ppmvw	HCN ppmvd @ 7% O2	HF ppmvw	HF ppmvd @ 7% O2
1	10/24/2023	8:00	8:59	16.1	2.9%	2.03	6.07	0.10	0.30
2	10/24/2023	10:00	10:59	16.2	2.7%	1.82	5.55	0.10	0.30
3	10/24/2023	12:00	12:59	16.2	2.7%	1.89	5.74	0.10	0.30
Average				16.2	2.8%	1.91	5.78	0.10	0.30

Test No.	Date	Start Time	End Time	Volumetric Flow, SCFH	Clinker Production, ton/hr	HCN lb/hr	HCN lb/ton	HF lb/hr	HF lb/ton
1	10/24/2023	8:00	8:59	11,136,060	53.5	1.58	0.0296	0.06	0.0011
2	10/24/2023	10:00	10:59	11,122,080	53.5	1.42	0.0266	0.06	0.0011
3	10/24/2023	12:00	12:59	10,910,940	57.6	1.45	0.0251	0.06	0.0010
Average				11,056,360	54.9	1.48	0.0271	0.06	0.0010

6.0 CERTIFICATION

Mostardi Platt is pleased to have been of service to GCC Rio Grande Inc. If you have any questions regarding this test report, please do not hesitate to contact us at 630-993-2100.


As project manager, I hereby certify that this test report represents a true and accurate summary of emissions test results and the methodologies employed to obtain those results, and the test program was performed in accordance with the methods specified in this test report.

MOSTARDI PLATT



Richard J. Sollars II

Project Manager



Chet A. Gutwein

Quality Assurance

APPENDICES

Appendix A – Plant Operating Data

Tijeras PM RUN 1

Run	Clk Prod st/hr
10/24/2023 8:00	49.1
10/24/2023 8:01	48.3
10/24/2023 8:02	48.6
10/24/2023 8:03	50.4
10/24/2023 8:04	48.9
10/24/2023 8:05	49.6
10/24/2023 8:06	50.6
10/24/2023 8:07	51.5
10/24/2023 8:08	49.2
10/24/2023 8:09	50.3
10/24/2023 8:10	50.4
10/24/2023 8:11	50.2
10/24/2023 8:12	51
10/24/2023 8:13	51.8
10/24/2023 8:14	51.1
10/24/2023 8:15	51.4
10/24/2023 8:16	51.4
10/24/2023 8:17	50.7
10/24/2023 8:18	52.9
10/24/2023 8:19	50.9
10/24/2023 8:20	51
10/24/2023 8:21	51.4
10/24/2023 8:22	49.2
10/24/2023 8:23	49.1
10/24/2023 8:24	49.7
10/24/2023 8:25	50.5
10/24/2023 8:26	48.2
10/24/2023 8:27	49.7
10/24/2023 8:28	50.4
10/24/2023 8:29	49.5
10/24/2023 8:30	49.1
10/24/2023 8:31	49.9
10/24/2023 8:32	47.7
10/24/2023 8:33	51.1
10/24/2023 8:34	49.9
10/24/2023 8:35	48.9
10/24/2023 8:36	51.3
10/24/2023 8:37	50.3
10/24/2023 8:38	49.6
10/24/2023 8:39	52.7
10/24/2023 8:40	50.9
10/24/2023 8:41	51.7
10/24/2023 8:42	54.8
10/24/2023 8:43	56.2
10/24/2023 8:44	55
10/24/2023 8:45	58.2
10/24/2023 8:46	57.7
10/24/2023 8:47	56.3
10/24/2023 8:48	56.7
10/24/2023 8:49	58.8
10/24/2023 8:50	58
10/24/2023 8:51	59.4
10/24/2023 8:52	58.2
10/24/2023 8:53	57.9
10/24/2023 8:54	58.8
10/24/2023 8:55	59.3
10/24/2023 8:56	57.8
10/24/2023 8:57	58.1
10/24/2023 8:58	56.4
10/24/2023 8:59	57.3
10/24/2023 9:00	58
10/24/2023 9:01	56.8
10/24/2023 9:02	58
10/24/2023 9:03	57.9
10/24/2023 9:04	59.5
10/24/2023 9:05	57.3
10/24/2023 9:06	56.9
10/24/2023 9:07	58.5
10/24/2023 9:08	55.2
10/24/2023 9:09	57
10/24/2023 9:10	55.2
10/24/2023 9:11	56.4
10/24/2023 9:12	55.6
10/24/2023 9:13	54.3
10/24/2023 9:14	55.2
10/24/2023 9:15	55.9
10/24/2023 9:16	55.6
10/24/2023 9:17	55.4
10/24/2023 9:18	55.4
10/24/2023 9:19	56.2
10/24/2023 9:20	54.6
Average	53.5

Tijeras PM Run 2

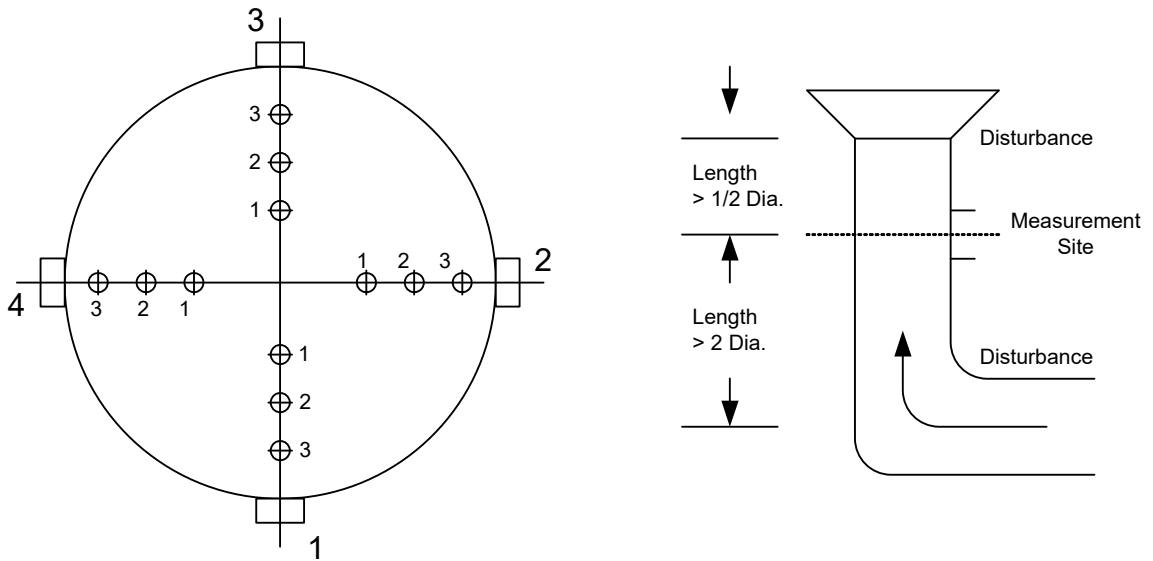
Run	Clk Prod st/hr
10/24/2023 8:00	49.1
10/24/2023 8:01	48.3
10/24/2023 8:02	48.6
10/24/2023 8:03	50.4
10/24/2023 8:04	48.9
10/24/2023 8:05	49.6
10/24/2023 8:06	50.6
10/24/2023 8:07	51.5
10/24/2023 8:08	49.2
10/24/2023 8:09	50.3
10/24/2023 8:10	50.4
10/24/2023 8:11	50.2
10/24/2023 8:12	51
10/24/2023 8:13	51.8
10/24/2023 8:14	51.1
10/24/2023 8:15	51.4
10/24/2023 8:16	51.4
10/24/2023 8:17	50.7
10/24/2023 8:18	52.9
10/24/2023 8:19	50.9
10/24/2023 8:20	51
10/24/2023 8:21	51.4
10/24/2023 8:22	49.2
10/24/2023 8:23	49.1
10/24/2023 8:24	49.7
10/24/2023 8:25	50.5
10/24/2023 8:26	48.2
10/24/2023 8:27	49.7
10/24/2023 8:28	50.4
10/24/2023 8:29	49.5
10/24/2023 8:30	49.1
10/24/2023 8:31	49.9
10/24/2023 8:32	47.7
10/24/2023 8:33	51.1
10/24/2023 8:34	49.9
10/24/2023 8:35	48.9
10/24/2023 8:36	51.3
10/24/2023 8:37	50.3
10/24/2023 8:38	49.6
10/24/2023 8:39	52.7
10/24/2023 8:40	50.9
10/24/2023 8:41	51.7
10/24/2023 8:42	54.8
10/24/2023 8:43	56.2
10/24/2023 8:44	55
10/24/2023 8:45	58.2
10/24/2023 8:46	57.7
10/24/2023 8:47	56.3
10/24/2023 8:48	56.7
10/24/2023 8:49	58.8
10/24/2023 8:50	58
10/24/2023 8:51	59.4
10/24/2023 8:52	58.2
10/24/2023 8:53	57.9
10/24/2023 8:54	58.8
10/24/2023 8:55	59.3
10/24/2023 8:56	57.8
10/24/2023 8:57	58.1
10/24/2023 8:58	56.4
10/24/2023 8:59	57.3
10/24/2023 9:00	58
10/24/2023 9:01	56.8
10/24/2023 9:02	58
10/24/2023 9:03	57.9
10/24/2023 9:04	59.5
10/24/2023 9:05	57.3
10/24/2023 9:06	56.9
10/24/2023 9:07	58.5
10/24/2023 9:08	55.2
10/24/2023 9:09	57
10/24/2023 9:10	55.2
10/24/2023 9:11	56.4
10/24/2023 9:12	55.6
10/24/2023 9:13	54.3
10/24/2023 9:14	55.2
10/24/2023 9:15	55.9
10/24/2023 9:16	55.6
10/24/2023 9:17	55.4
10/24/2023 9:18	55.4
10/24/2023 9:19	56.2
10/24/2023 9:20	54.6
Average	53.5

Tijeras PM Run 3

Run	Clk Prod st/hr
10/24/2023 12:00	50.2
10/24/2023 12:01	49.4
10/24/2023 12:02	52
10/24/2023 12:03	51.4
10/24/2023 12:04	50.6
10/24/2023 12:05	52.2
10/24/2023 12:06	52.2
10/24/2023 12:07	52.8
10/24/2023 12:08	54.6
10/24/2023 12:09	54.8
10/24/2023 12:10	52.4
10/24/2023 12:11	57.1
10/24/2023 12:12	56.3
10/24/2023 12:13	57.3
10/24/2023 12:14	59.5
10/24/2023 12:15	57.9
10/24/2023 12:16	57.5
10/24/2023 12:17	58.3
10/24/2023 12:18	58.8
10/24/2023 12:19	59
10/24/2023 12:20	59.2
10/24/2023 12:21	60
10/24/2023 12:22	59.5
10/24/2023 12:23	57.9
10/24/2023 12:24	56.9
10/24/2023 12:25	55.1
10/24/2023 12:26	58.2
10/24/2023 12:27	55.8
10/24/2023 12:28	54.1
10/24/2023 12:29	56.3
10/24/2023 12:30	54.2
10/24/2023 12:31	52.5
10/24/2023 12:32	53.9
10/24/2023 12:33	50.4
10/24/2023 12:34	51.8
10/24/2023 12:35	54
10/24/2023 12:36	52.9
10/24/2023 12:37	51.7
10/24/2023 12:38	54
10/24/2023 12:39	53.8
10/24/2023 12:40	55.4
10/24/2023 12:41	57.8
10/24/2023 12:42	60.3
10/24/2023 12:43	61.8
10/24/2023 12:44	63.2
10/24/2023 12:45	64
10/24/2023 12:46	70.9
10/24/2023 12:47	71.9
10/24/2023 12:48	73
10/24/2023 12:49	69.2
10/24/2023 12:50	69
10/24/2023 12:51	68.9
10/24/2023 12:52	64.6
10/24/2023 12:53	66.2
10/24/2023 12:54	69.9
10/24/2023 12:55	62.4
10/24/2023 12:56	59.2
10/24/2023 12:57	56.3
10/24/2023 12:58	53.2
10/24/2023 12:59	52.5
10/24/2023 13:00	53.5
10/24/2023 13:01	55
10/24/2023 13:02	54.9
10/24/2023 13:03	53.6
10/24/2023 13:04	57.2
10/24/2023 13:05	68.3
10/24/2023 13:06	64.3
10/24/2023 13:07	58.3
10/24/2023 13:08	53
10/24/2023 13:09	50.3
10/24/2023 13:10	53.7
Average	57.6

Appendix B – Test Section Diagrams

STRATIFICATION TEST FOR ROUND DUCTS



Project: GCC Rio Grande Inc. Tijeras Plant

Test Location: Main Kiln

Duct Diameter: 132 Inches

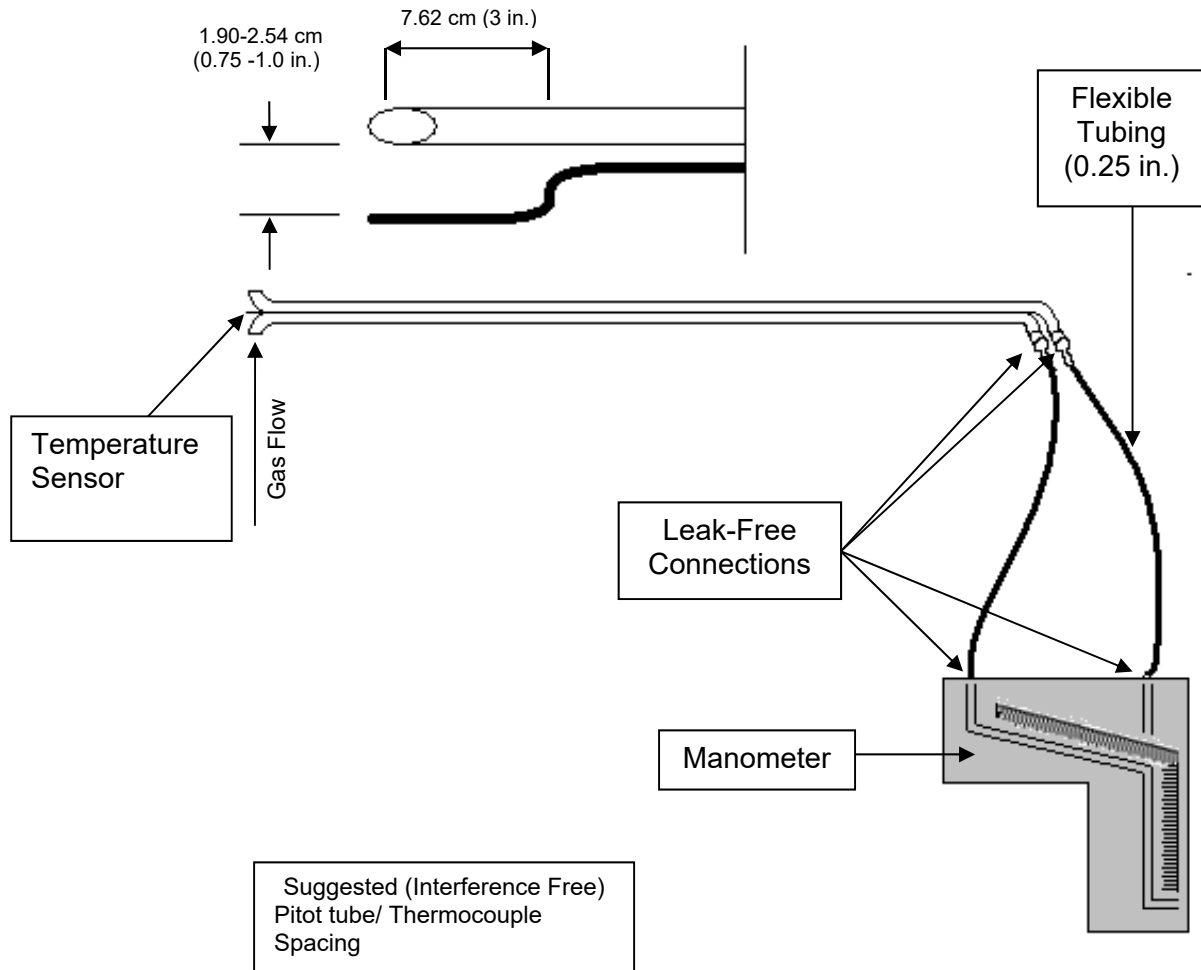
Duct Area: 95.03 Square Feet

No. Points Across Diameter: 6

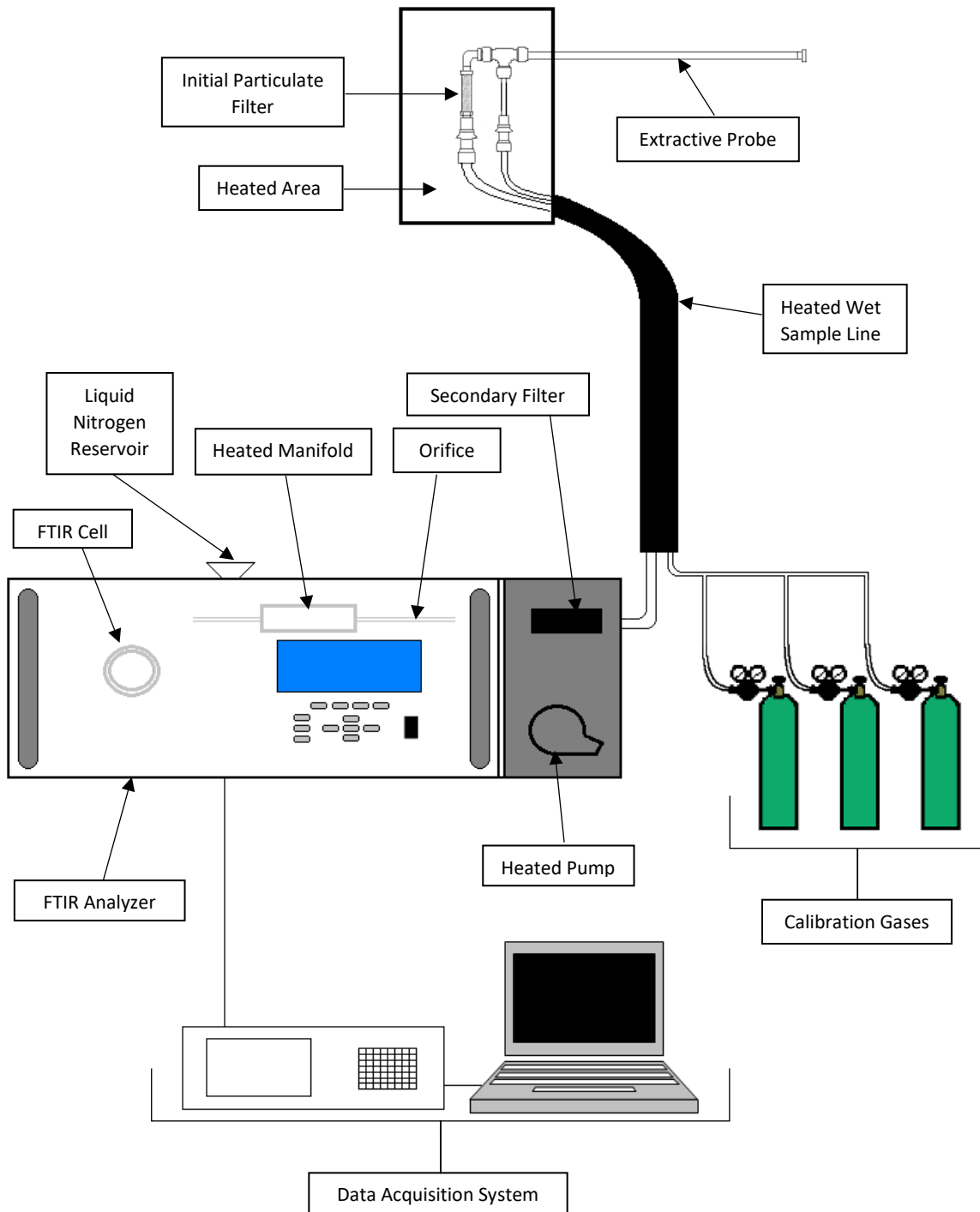
No. of Ports: 2

Appendix C – Sample Train Diagrams

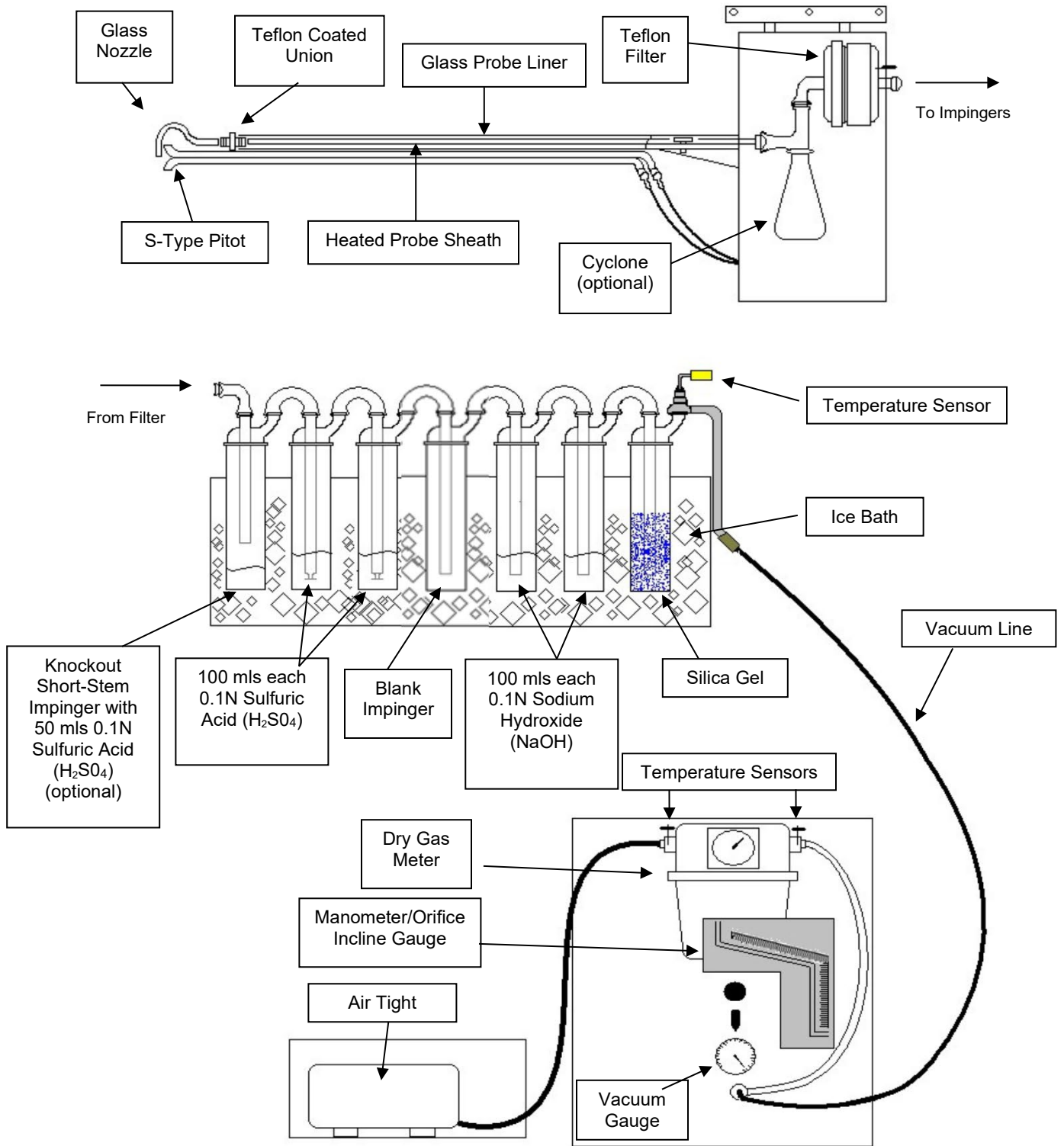
USEPA Method 2 – Type S Pitot Tube Manometer Assembly



USEPA Method 320 – Vapor Phase Organic and Inorganic Emissions by Extractive Fourier Transform Infrared (FTIR) Spectroscopy Sample Train Diagram



USEPA Method 26A – HF and Cl₂ Sample Train Diagram



Appendix D – Calculation Nomenclature and Formulas

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Run: 1
 Date: 10/24/2023
 Method: 5/26A
 Source Condition: Normal

Dry Molecular Weight

$$Md = 0.44 \times (\%CO_2) + 0.32 \times (\%O_2) + 0.28 \times \%N_2$$

$$\%CO_2 = \frac{6.2}{\quad} \quad \%O_2 = \frac{16.1}{\quad} \quad \%N_2 = \frac{77.7}{\quad}$$

$$Md = \frac{29.636}{\quad}$$

Wet Molecular Weight

$$Ms = Md \times (1 - Bws) + (18.0 \times Bws)$$

$$Md = \frac{29.636}{\quad} \quad Bws = \frac{0.031}{\quad}$$

$$Ms = \frac{29.272}{\quad}$$

Meter Volume at Standard Conditions

$$Vm(std) = 17.647 \times Y \times Vm \times \frac{(Pbar + DH/13.6)}{Tm}$$

$$Y = \frac{0.994}{\quad} \quad DH = \frac{2.7}{\quad} \quad Vm = \frac{61.904}{\quad} \quad Tm = \frac{59.1}{\quad} \quad Pbar = \frac{23.6}{\quad}$$

$$Vm(std) = \frac{49.875}{\quad}$$

Volume of Water Vapor Condensed

$$Vw(std) = 0.0471 \times (\text{net H}_2\text{O gain})$$

$$\text{Net H}_2\text{O} = \frac{34.2}{\quad}$$

$$Vw(std) = \frac{1.611}{\quad}$$

Moisture Content

$$Bws = \frac{Vw(std)}{Vw(std) + Vm(std)}$$

$$Vw(std) = \frac{1.611}{\quad} \quad Vm(std) = \frac{49.875}{\quad}$$

$$Bws = \frac{0.031}{\quad}$$

Average Duct Velocity

$$Vs = 85.49 \times Cp \times \text{Sqrt DP (avg)} \times (Ts (\text{avg}) + 460 / (Ps \times Ms))^{1/2}$$

$$Cp = \frac{0.820}{\quad} \quad Ps = \frac{23.64}{\quad} \quad Ts (\text{avg}) = \frac{337.8}{\quad} \quad Ms = \frac{29.272}{\quad} \quad \text{Sqrt DP (avg)} = \frac{0.804}{\quad}$$

$$Vs = \frac{60.514}{\quad}$$

Volumetric Flow Rate (Actual Basis)

$$Q = Vs \times A \times 60$$

$$Vs = \frac{60.514}{\quad} \quad A = \frac{95.033}{\quad}$$

$$Q = \frac{345,051}{\quad}$$

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Run: 1
 Date: 10/24/2023
 Method: 5/26A
 Source Condition: Normal

Volumetric Flow Rate (Standard Basis)

$$Q_{std} = 17.647 \times Q \times \frac{Ps}{Ts \text{ (avg)} + 460}$$

$Q = \underline{345,051}$ $Ps = \underline{23.64}$ $Ts \text{ (avg)} = \underline{337.8}$
 $Q_{std} = \underline{180,423}$

Volumetric Flow Rate (Standard Dry Basis)

$$Q_{std}(\text{dry}) = Q_{std} \times (1 - Bws)$$

$Q_{std} = \underline{180,423}$ $Bws = \underline{0.031}$
 $Q_{std}(\text{dry}) = \underline{174,778}$

Isokinetic Variation:

$$\%ISO = \frac{0.0945 \times (Ts + 460) \times Vm(\text{std})}{Vs \times \theta \times An \times Ps \times (1 - Bws)}$$

$Ts = \underline{337.8}$ $Vm(\text{std}) = \underline{49.875}$ $Vs = \underline{60.514}$
 $An = \underline{0.0004492}$ $\theta = \underline{60}$ $Ps = \underline{23.64}$
 $Bws = \underline{0.031}$
 $\%ISO = \underline{100.7}$

Chloride (Cl2) Concentration:

$$\text{mg/m}^3 = \frac{\text{mg of Chloride (Cl2)}}{Vm(\text{std}) \times 0.02832 \text{ m}^3/\text{ft}^3}$$

$\text{mg} = \underline{0.15}$ $Vm(\text{std}) = \underline{49.875}$
 $\text{mg/m}^3 = \underline{0.11}$

Chloride (Cl2) Emission Rate:

$$\text{lb of Chloride (Cl2)} = \frac{\mu\text{g of sample} \times 10^{-6} \text{ grams}/\mu\text{g}}{453.6 \text{ grams/lb}}$$

$$\text{Emission Rate lb/hr} = \frac{\text{lb of Chloride (Cl2)}}{Vm(\text{std})} \times \text{dscfm} \times 60 \text{ min/hr}$$

$\text{lb of Chloride (Cl2)} = \underline{3.31E-10}$ $\text{dscfm} = \underline{174,778}$
 $\text{Emission Rate lb/hr} = \underline{0.0695}$
 $\text{Emission Rate lb/ton} = \frac{\text{lb/hr of Chloride (Cl2)}}{\text{clinker production ton/hr}}$
 $\text{lb/hr of Chloride (Cl2)} = \underline{0.0695}$ $\text{clinker ton/hr} = \underline{53.5}$
 $\text{Emission Rate lb/ton} = \underline{0.0013}$

Client: GCC Rio Grande, Inc.
Facility: Tijeras Plant
Project #: M234302
Test Location: Main Stack
Date: 10/24/23

Sample Calculations

$$(16.25\% - 0.08\%) \times \frac{\text{O2 \% (dry)} \\ 12.03\%}{12.14\% - 0.08\%} = 16.13\%$$

$$C_{\text{gas}} = (C - C_0) \times \frac{C_{\text{ma}}}{C_m - C_0}$$

where:

C_{gas} = Effluent gas concentration, dry basis, ppm or %

C = Average gas concentration indicated by gas analyzer, dry basis, ppm or %

C_0 = Average of initial and final system calibration bias check responses for the zero gas, ppm or %

C_m = Average of initial and final system calibration bias check responses for the upscale calibration gas, ppm or %

C_{ma} = Actual concentration of the upscale calibration gas, ppm or %

Client: GCC Rio Grande, Inc.
 Facility: Tijeras Plant
 Project #: M234302
 Test Location: Main Stack
 Date: 10/24/23

FTIR Sample Calculations

Direct Recovery % of Calibration Transfer Standard

$$DR_{cts} = \frac{D_{cts}}{Cma} \times 100$$

$$Cma = \frac{100.6}{}$$

$$D_{cts} = \frac{100.6}{}$$

$$DR_{cts} = \frac{100.0\%}{}$$

Recovery % with Calibration Transfer Standard System Purge

$$R_{cts} = \frac{Sys_{cts}}{D_{cts}} \times 100$$

$$Sys_{cts} = \frac{101.0}{}$$

$$D_{cts} = \frac{100.6}{}$$

$$R_{cts} = \frac{100\%}{}$$

Direct Recovery % of Analyte Spike Gas

SF6

$$DR_{sf6} = \frac{D_{sf6}}{Cma} \times 100$$

$$Cma = \frac{5.0}{}$$

$$D_{sf6} = \frac{5.1}{}$$

$$DR_{sf6} = \frac{102\%}{}$$

HCN

$$DR_{asg} = \frac{D_{asg}}{Cma} \times 100$$

$$Cma = \frac{49.6}{}$$

$$D_{asg} = \frac{48.0}{}$$

$$DR_{asg} = \frac{96.9\%}{}$$

Dilution Factor for Analyte Spiking

$$DF = \frac{Spk_{sf6}}{D_{sf6}}$$

$$Spk_{sf6} = \frac{0.424}{}$$

$$D_{sf6} = \frac{5.101}{}$$

$$DF = \frac{0.083}{}$$

Recovery % for Analyte Spike With HCN

$$R_x = \frac{Spk_x}{(N_x \times (1-DF) + D_{asg} \times DF)}$$

$$Spk_x = \frac{6.1}{}$$

$$N_x = \frac{2.0}{}$$

$$DF = \frac{0.083}{}$$

$$D_{asg} = \frac{48.0}{}$$

$$R_x = \frac{103.4}{\%}$$

where:

- DR_{cts} = Recovery % of the calibration transfer standard directly to the analyzer
- Cma = certified concentration of calibration gas, ppm
- D_{cts} = Concentration of the calibration transfer standard gas directly to the analyzer, ppm
- R_{cts} = Recovery % of the calibration transfer standard through the sampling system
- Sys_{cts} = Concentration of the calibration transfer standard gas through the system, ppm
- DF = Dilution Factor of analyte spike gas
- Spk_{sf6} = SF6 concentration in effluent during spiking
- Spk_x = Analyte concentration in effluent during spiking
- D_{asg} = Concentration of the analyte spike gas directly to the analyzer, ppm
- D_{sf6} = Concentration of the SF6 directly to the analyzer, ppm
- R_x = Recovery % of the analyte spike gas
- N_x = Native effluent (HCN) concentration prior to analyte spike

MOSTARDI PLATT

Moisture Calculations

$$V_{wc(std)} = \frac{(V_f - V_i)\rho_w RT_{std}}{P_{std}M_w} = 0.04707(V_f - V_i)$$

$$V_{wsg(std)} = \frac{(W_f - W_i)\rho_w RT_{std}}{P_{std}M_w} = 0.04715(W_f - W_i)$$

$$V_{m(std)} = 17.64 V_m Y \frac{P_{bar} + \frac{\Delta H}{13.6}}{T_m}$$

$$B_{ws} = \frac{V_{wc(std)} + V_{wsg(std)}}{V_{wc(std)} + V_{wsg(std)} + V_{m(std)}}$$

Where:

B_{ws} = Water vapor in gas stream, proportion by volume

M_w = Molecular weight of water, 18.015 lb/lb-mole

P_{bar} = Barometric pressure at the testing site, in. Hg

P_{std} = Standard absolute pressure, 29.92 in. Hg

R = Ideal gas constant, $0.048137 \text{ (in. Hg)(ft}^3\text{)/(g-mole)(}^\circ\text{R)} =$
 $[21.8348 \text{ (in. Hg)(ft}^3\text{)/(lb-mole)(}^\circ\text{R)}]/453.592 \text{ g-mole/lb-mole}$

T_m = Absolute average dry gas meter temperature, $^\circ\text{R}$

T_{std} = Standard absolute temperature, 528 $^\circ\text{R}$

V_f = Final volume of condenser water, ml

V_i = Initial volume of condenser water, ml

V_m = Dry gas volume measured by dry gas meter, dcf

$V_{m(std)}$ = Dry gas volume measured by dry gas meter, corrected to standard conditions, scf

$V_{wc(std)}$ = Volume of condensed water vapor, corrected to standard conditions, scf

$V_{wsg(std)}$ = Volume of water vapor collected in silica gel, corrected to standard conditions, scf

W_f = Final weight of silica gel, g

W_i = Initial weight of silica gel, g

Y = Dry gas meter calibration factor

ΔH = Average pressure exerted on dry gas meter outlet by gas sample bag, in. H_2O

ρ_w = Density of water, 0.9982 g/ml

13.6 = Specific gravity of mercury (Hg)

17.64 = T_{std}/P_{std}

0.04707 = ft^3/ml 0.04715 = ft^3/g

MOSTARDI PLATT

Volumetric Flow Nomenclature

- A = Cross-sectional area of stack or duct, ft²
- B_{ws} = Water vapor in gas stream, proportion by volume
- C_p = Pitot tube coefficient, dimensionless
- M_d = Dry molecular weight of gas, lb/lb-mole
- M_s = Molecular weight of gas, wet basis, lb/lb-mole
- M_w = Molecular weight of water, 18.0 lb/lb-mole
- P_{bar} = Barometric pressure at testing site, in. Hg
- P_g = Static pressure of gas, in. Hg (in. H₂O/13.6)
- DH = Static pressure of gas, in. H₂O
- P_s = Absolute pressure of gas, in. Hg = P_{bar} + P_g
- P_{std} = Standard absolute pressure, 29.92 in. Hg
- A_{cfm} = Actual volumetric gas flow rate
- Sc_{fm} = Volumetric gas flow rate, corrected to standard conditions
- D_{scfm} = Standard volumetric flow rate, corrected to dry conditions
- R = Ideal gas constant, 21.85 in. Hg-ft³/°R-lb-mole
- T_s = Average stack gas temperature, °F
- T_m = Average dry gas meter temperature, °F
- T_{std} = Standard absolute temperature, 528°R
- v_s = Gas velocity, ft/sec
- V_{m(std)} = Volume of gas sampled, corrected to standard conditions, scf
- V_{w(std)} = Volume of water vapor in gas sample, corrected to standard conditions, scf
- V_{lc} = Volume of liquid collected
- Y = Dry gas meter calibration factor
- Δp = Velocity head of gas, in. H₂O
- K₁ = 17.647 °R/in. Hg
- %EA = Percent excess air
- %CO₂ = Percent carbon dioxide by volume, dry basis
- %O₂ = Percent oxygen by volume, dry basis
- %N₂ = Percent nitrogen by volume, dry basis
- 0.264 = Ratio of O₂ to N₂ in air, v/v
- 0.28 = Molecular weight of N₂ or CO, divided by 100
- 0.32 = Molecular weight of O₂ divided by 100
- 0.44 = Molecular weight of CO₂ divided by 100
- 13.6 = Specific gravity of mercury (Hg)

MOSTARDI PLATT

Volumetric Air Flow Calculations

$$Vm (std) = 17.647 \times Vm \times \left[\frac{(P_{bar} + \left[\frac{DH}{13.6} \right])}{(460 + Tm)} \right] \times Y$$

$$Vw (std) = 0.0471 \times Vlc$$

$$Bws = \left[\frac{Vw (std)}{Vw (std) + Vm (std)} \right]$$

$$Md = (0.44 \times \%CO_2) + (0.32 \times \%O_2) + [0.28 \times (100 - \%CO_2 - \%O_2)]$$

$$Ms = Md \times (1 - Bws) + (18 \times Bws)$$

$$Vs = \sqrt{\frac{(Ts + 460)}{Ms \times Ps}} \times \sqrt{DP} \times Cp \times 85.49$$

$$Acfm = Vs \times Area (of stack or duct) \times 60$$

$$Scfm = Acfm \times 17.647 \times \left[\frac{Ps}{(460 + Ts)} \right]$$

$$Scfh = Scfm \times 60 \frac{min}{hr}$$

$$Dscfm = Scfm \times (1 - Bws)$$

MOSTARDI PLATT

Isokinetic Calculation Formulas

$$1. V_{w(std)} = V_{lc} \left(\frac{\rho_w}{M_w} \right) \left(\frac{RT_{std}}{P_{std}} \right) = K_2 V_{lc}$$

$$2. V_{m(std)} = V_m Y \left(\frac{T_{std}}{T_m} \right) \left(\frac{(P_{bar} + (\frac{\Delta H}{13.6}))}{P_{std}} \right) = K_1 V_m Y \frac{(P_{bar} + (\frac{\Delta H}{13.6}))}{T_m}$$

$$3. B_{ws} = \frac{V_{w(std)}}{(V_{m(std)} + V_{w(std)})}$$

$$4. M_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2)$$

$$5. M_s = M_d(1 - B_{ws}) + 18.0(B_{ws})$$

$$6. C_a = \frac{m_a}{V_a \rho_a}$$

$$7. W_a = C_a V_{aw} \rho_a$$

$$8. C_{acf} = 15.43 K_i \left(\frac{m_n P_s}{(V_{w(std)} + V_{m(std)}) T_s} \right)$$

$$9. C_s = (15.43 \text{ grains/gram}) (m_n / V_{m(std)})$$

$$10. v_s = K_p C_p \sqrt{\frac{\Delta P T_s}{P_s M_s}}$$

$$11. Q_{acfm} = v_s A (60_{\text{sec/min}})$$

$$12. Q_{sd} = (3600_{\text{sec/hr}}) (1 - B_{ws}) v_s \left(\frac{T_{std} P_s}{T_s P_{std}} \right) A$$

$$13. E \text{ (emission rate, lbs/hr)} = Q_{std} (C_s / 7000 \text{ grains/lb})$$

$$14. IKV = \frac{T_s V_{m(std)} P_{std}}{T_{std} v_s \theta A_n P_s 60(1 - B_{ws})} = K_4 \frac{T_s V_{m(std)}}{P_s v_s A_n \theta (1 - B_{ws})}$$

$$15. \%EA = \left(\frac{\%O_2 - (0.5 \%CO)}{0.264 \%N_2 - (\%O_2 - 0.5 \%CO)} \right) \times 100$$

MOSTARDI PLATT

Isokinetic Nomenclature

- A = Cross-sectional area of stack or duct, square feet
A_n = Cross-sectional area of nozzle, square feet
B_{ws} = Water vapor in gas stream, by volume
C_a = Acetone blank residue concentration, g/g
C_{act} = Concentration of particulate matter in gas stream at actual conditions, gr/acf
C_p = Pitot tube coefficient
C_s = Concentration of particulate matter in gas stream, dry basis, corrected to standard conditions, gr/dscf
IKV = Isokinetic sampling variance, must be 90.0 % ≤ IKV ≤ 110.0%
M_d = Dry molecular weight of gas, lb/lb-mole
M_s = Molecular weight of gas, wet basis, lb/lb-mole
M_w = Molecular weight of water, 18.0 lb/lb-mole
m_a = Mass of residue of acetone after evaporation, grams
P_{bar} = Barometric pressure at testing site, inches mercury
P_g = Static pressure of gas, inches mercury (inches water/13.6)
P_s = Absolute pressure of gas, inches mercury = P_{bar} + P_g
P_{std} = Standard absolute pressure, 29.92 inches mercury
Q_{acfm} = Actual volumetric gas flow rate, acfm
Q_{sd} = Dry volumetric gas flow rate corrected to standard conditions, dscfh
R = Ideal gas constant, 21.85 inches mercury cubic foot/°R-lb-mole
T_m = Dry gas meter temperature, °R
T_s = Gas temperature, °R
T_{std} = Absolute temperature, 528°R
V_a = Volume of acetone blank, ml
V_{aw} = Volume of acetone used in wash, ml
W_a = Weight of residue in acetone wash, grams
m_n = Total amount of particulate matter collected, grams
V_{1c} = Total volume of liquid collected in impingers and silica gel, ml
V_m = Volume of gas sample as measured by dry gas meter, dcf
V_{m(std)} = Volume of gas sample measured by dry gas meter, corrected to standard conditions, dscf
V_s = Gas velocity, ft/sec
V_{w(std)} = Volume of water vapor in gas sample, corrected to standard conditions, scf
Y = Dry gas meter calibration factor
ΔH = Average pressure differential across the orifice meter, inches water
Δp = Velocity head of gas, inches water
ρ_a = Density of acetone, 0.7855 g/ml (average)
ρ_w = Density of water, 0.002201 lb/ml
θ = Total sampling time, minutes
K₁ = 17.647 °R/in. Hg
K₂ = 0.04707 ft³/ml
K₄ = 0.09450/100 = 0.000945
K_p = Pitot tube constant, $85.49 \frac{ft}{sec} \left[\frac{(lb/lb-mole)(in. Hg)}{(^{\circ}R)(in. H_2O)} \right]^{1/2}$
%EA = Percent excess air
%CO₂ = Percent carbon dioxide by volume, dry basis
%O₂ = Percent oxygen by volume, dry basis
%CO = Percent carbon monoxide by volume, dry basis
%N₂ = Percent nitrogen by volume, dry basis
0.264 = Ratio of O₂ to N₂ in air, v/v
28 = Molecular weight of N₂ or CO
32 = Molecular weight of O₂
44 = Molecular weight of CO₂
13.6 = Specific gravity of mercury (Hg)

MOSTARDI PLATT

Calculations for Hydrogen Fluoride By Method 26 or 26A

Concentration

$$\frac{\text{lbs HF}}{\text{dscf}} = \frac{\mu\text{g HF in sample}}{4.536 \times 10^8 \times \text{dscf}}$$

where:

$$4.536 \times 10^8 = \mu\text{g/lb}$$

dscf = Volume of gas sampled

$$\mu\text{g/lb HF} = \mu\text{g F} \times \frac{20.008}{19.000}$$

Parts Per Million

$$\text{ppm HF} = \frac{\text{lbs HF}}{\text{dscf}} \div \frac{20.008}{385 \times 10^6}$$

where:

385 = Volume of 1 lb mole of gas at 68°F and 29.92 in. Hg

106 = Conversion of ppm v/v

Emission Rate

$$\text{lbs HF /dscf} \times \text{dscfm} \times 60 \text{ min/hr} = \text{lbs/hr HF}$$

MOSTARDI PLATT

Pollutant Concentration Correction 7% for Percent Oxygen

$$C_{adj} = C_d \frac{20.9 - 7\%}{20.9 - \%O_2}$$

where:

C_{adj} = Pollutant concentration corrected to percent O_2

$20.9 - 7\%$ = Percent O_2 , the defined O_2 correction value, percent

20.9 = Percent O_2 in air

$\%O_2$ = Measured O_2 concentration dry basis, percent

C_d = Pollutant concentration measured, dry basis, ppm.

Appendix E- Laboratory Sample Analysis

Kiln Stack

Client: GCC Facility: Tijeras Test Location: Kiln Stack Project Number: M234302 Method: 26A Date Samples Received: 11/3/2023	Analysis Date: 11/13/2023 Analysis Location: Elmhurst Analyst: JMG
---	--

Train A

Sampling Date		10/24/2023	10/24/2023	10/24/2023	10/24/2023		
	UNITS	M26A DI Blank	M26A H2SO4 Blank	M26A H2SO4-R1	M26A H2SO4-R1 Dup	RDL	MDL
Sulfuric Acid Volume	ml	237	264	400	400		
Hydrofluoric Acid	ug	<150	<150	<150	<150	150	15

Sampling Date		10/24/2023	10/24/2023	10/23/2023		
	UNITS	M26A- H2SO4 R2	M26A- H2SO4 R3	Train A Blank	RDL	MDL
Sulfuric Acid Volume	ml	288	308	278		
Hydrofluoric Acid	ug	<150	<150	<150	150	15

Train B

Sampling Date		10/24/2023	10/24/2023	10/24/2023	10/24/2023		
	UNITS	M26A DI Blank	M26A H2SO4 Blank	M26A H2SO4-R1	M26A H2SO4-R1 Dup	RDL	MDL
Sulfuric Acid Volume	ml	237	264	329	329		
Hydrofluoric Acid	ug	<150	<150	<150	<150	150	15

Sampling Date		10/24/2023	10/24/2023	10/23/2023		
	UNITS	M26A- H2SO4 R2	M26A- H2SO4 R3	Train B Blank	RDL	MDL
Sulfuric Acid Volume	ml	288	308	278		
Hydrofluoric Acid	ug	<150	<150	<150	150	15

Kiln Stack

Client: GCC Facility: Tijeras Test Location: Kiln Stack Project Number: M234302 Method: 26A Date Samples Received: 11/3/2023	Analysis Date: 11/13/2023 Analysis Location: Elmhurst Analyst: JMG
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Train A

Sampling Date		10/24/2023	10/24/2023	10/24/2023	10/24/2023		
	UNITS	M26A DI Blank	M26A NaOH Blank	M26A NaOH-R1	M26A NaOH-R1 Dup	RDL	MDL
Sodium Hydroxide Volume	ml	253	267	264	264		
Chlorine	ug	<150	<150	<150	<150	150	15

Sampling Date		10/24/2023	10/24/2023	10/23/2023		
	UNITS	M26A- NaOH R2	M26A- NaOH R3	Train A Blank	RDL	MDL
Sodium Hydroxide Volume	ml	276	253	267		
Chlorine	ug	<150	<150	<150	150	15

Train B

Sampling Date		10/24/2023	10/24/2023	10/24/2023	10/24/2023		
	UNITS	M26A DI Blank	M26A NaOH Blank	M26A NaOH-R1	M26A NaOH-R1 Dup	RDL	MDL
Sodium Hydroxide Volume	ml	253	267	304	304		
Chlorine	ug	<150	<150	<150	<150	150	15

Sampling Date		10/24/2023	10/24/2023	1/0/1900		
	UNITS	M26A- NaOH R2	M26A- NaOH R3	Train B Blank	RDL	MDL
Sodium Hydroxide Volume	ml	226	267	267		
Chlorine	ug	<150	<150	<150	150	15

Client:	GCC	Analysis Date:	1/0/1900																	
Facility:	Tijeras	Analysis Location:	Elmhurst Lab																	
Test Location:	Kiln Stack	Analyst:	JMG																	
Project Number:	M234302																			
Method:	26A																			
Date Samples Received:	11/3/2023																			
Standard ppm Cl	Area	Response Factor	Calculated Value	Slope of Regression Curve																
1	0.1523	0.1523	1.01	0.1513																
2	0.2939	0.1470	1.94																	
5	0.7660	0.1532	5.06	Response Factor Ave																
8	1.2141	0.1518	8.03	0.1512																
10	1.5201	0.1520	10.05																	
Lot Number	Ricca 8209004																			
	R²	0.9999																		
	Sample Date	Sample ID	Sample Area	PPM Cl	PPM X Dilution Factor	Dilution Factor	Total ml	mg Cl in soln	mg Cl2 in soln avg	ug Cl2 in soln										
	10/24/2023	DI Reagent Blank	0.0010	0.0066	0.0066	1	253	0.0017												
	10/24/2023	DI Reagent Blank	0.0001	0.0007	0.0007	1	253	0.0002	0.0009	0.919949415										
	10/24/2023	NaOH Reagent Blank	0.0200	0.1322	0.1322	1	267	0.0353												
	10/24/2023	NaOH Reagent Blank	0.0182	0.1203	0.1203	1	267	0.0321	0.0337	33.71517089										
	10/24/2023	Test 1B NaOH Imp	0.0086	0.0569	0.0569	1	304	0.0173												
	10/24/2023	Test 1B NaOH Imp	0.0081	0.0536	0.0536	1	304	0.0163	0.0168	16.78188713										
	10/24/2023	Test 1B NaOH Imp	0.0084	0.0555	0.0555	1	304	0.0169												
	10/24/2023	Test 1B NaOH Imp	0.0088	0.0582	0.0582	1	304	0.0177	0.0173	17.28433884										
	10/24/2023	Test 2B NaOH Imp	0.0368	0.2433	0.2433	1	226	0.0550												
	10/24/2023	Test 2B NaOH Imp	0.0353	0.2334	0.2334	1	226	0.0527	0.0539	53.86348448										
	10/24/2023	Test 3B NaOH Imp	0.0135	0.0893	0.0893	1	267	0.0238												
	10/24/2023	Test 3B NaOH Imp	0.0160	0.1058	0.1058	1	267	0.0282	0.0260	26.03658485										
	1/0/1900	Train B Train Blank	0.0200	0.1322	0.1322	1	267	0.0353												
	1/0/1900	Train B Train Blank	0.0182	0.1203	0.1203	1	267	0.0321	0.0337	33.71517089										
CCV ppm Cl	Area	PPM Cl																		
5 ppm ICV	0.7339	4.8520																		
5 ppm CCV	0.7823	5.1719																		
5 ppm CCV	0.7841	5.1838																		
5 ppm CCV	0	0.0000																		
Standard ppm Cl	Area	Difference																		
1	0.1575	1.65%																		
2	0.2902	0.64%																		
5	0.7781	0.78%																		
8	1.2309	0.68%																		
10	1.5781	1.84%																		

Appendix F - Reference Method Test Data

Client: GCC Rio Grande Inc.
Facility: Tijeras Plant
Test Location: Main Stack
Project #: M234302
Test Method: 5/26A
Test Engineer: KAW
Test Technician: RODS

	<u>Run 1A</u>	<u>Run 2A</u>	<u>Run 3A</u>
Meter ID:	CM53	CM53	CM53
Pitot ID:	S8-031A	S8-031A	S8-031A
Filter ID:	11763	11747	11749
Filter Pre-Weight (grams):	0.26642	0.26870	0.26950
Nozzle Diameter (Inches):	0.287	0.287	0.287
Meter Calibration Date:	9/6/2023	9/6/2023	9/6/2023
Meter Calibration Factor (Y):	0.994	0.994	0.994
Meter Orifice Setting (Delta H):	1.775	1.775	1.775
Nozzle Kit ID Number and Material:	Glass	Glass	Glass
Pitot Tube Coefficient:		0.820	
Probe Length (Feet):		6.0	
Probe Liner Material:		Glass	
Sample Plane:		Horizontal	
Port Length (Inches):		6.50	
Port Size (Diameter, Inches):		4.00	
Port Type:		Flange	
Duct Shape:		Circular	
Diameter (Feet):		11	
Duct Area (Square Feet):		95.033	
Upstream Diameters:		3.3	
Downstream Diameters:		9.2	
Number of Ports Sampled:		4	
Number of Points per Port:		3	
Minutes per Point:		5.0	
Minutes per Reading:		5.0	
Total Number of Traverse Points:		12	
Test Length (Minutes):		60	
Train Type:		Anderson Box	
Source Condition:		Normal	
Diluent Model/Serial Number:		CAI 700 and MKS 2030	
Moisture Balance ID:		LV4	
# of Runs		3	

Run 1A - Method 5/26A

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Source Condition: Normal

Date: 10/24/23
 Start Time: 8:00
 End Time: 9:20

DRY GAS METER CONDITIONS

STACK CONDITIONS

ΔH:	2.68	in. H ₂ O	Static Pressure	-0.10	in. H ₂ O
Meter Temperature, T _m :	59.1	°F	Flue Pressure (Ps):	23.64	in. Hg. abs.
Sqrt ΔP:	0.804	in. H ₂ O	Carbon Dioxide:	6.20	%
Stack Temperature, T _s :	337.8	°F	Oxygen:	16.10	%
Meter Volume, V _m :	61.904	ft ³	Nitrogen:	77.70	%
Meter Volume, V _{mstd} :	49.875	dscf	Gas Weight dry, M _d :	29.636	lb/lb mole
Meter Volume, V _{wstd} :	1.611	wscf	Gas Weight wet, M _s :	29.272	lb/lb mole
Isokinetic Variance:	100.7	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, V _s :	60.514	fps
Nozzle Diameter:	0.287	in inches	Volumetric Flow:	345,051	acfm
Barometric Pressure:	23.65	in Hg	Volumetric Flow:	174,778	dscfm
			Volumetric Flow:	180,423	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3430.9	ml	Silica Initial Wt.	834.6	grams
Final Impinger Content:	3453.7	ml	Silica Final Wt.	846.0	grams
Impinger Difference:	22.8	ml	Silica Difference:	11.4	grams
Total Water Gain:	34.2		Moisture, Bws:	0.031	

Port-Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp		Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
						Inlet °F	Outlet °F			
1-1	8:00:00	0.64	2.65	838.571	336	58	58	251	258	55
1-2	8:05:00	0.64	2.67	843.650	330	58	58	253	252	57
1-3	8:10:00	0.62	2.57	848.670	335	58	58	257	260	60
	8:15:00			853.940						
2-1	8:20:00	0.64	2.65	853.940	336	58	58	270	260	55
2-2	8:25:00	0.64	2.65	859.090	336	58	58	265	256	58
2-3	8:30:00	0.65	2.70	864.150	335	58	58	267	264	58
	8:35:00			869.360						
3-1	8:45:00	0.69	2.87	869.360	335	59	59	266	263	55
3-2	8:50:00	0.68	2.80	874.730	341	59	59	271	260	57
3-3	8:55:00	0.59	2.44	879.940	340	60	60	258	260	60
	9:00:00			884.890						
4-1	9:05:00	0.69	2.86	884.890	340	61	61	257	260	58
4-2	9:10:00	0.67	2.76	890.210	344	61	61	260	261	61
4-3	9:15:00	0.61	2.51	895.290	345	61	61	270	260	61
	9:20:00			900.475						
Total	1:00:00			61.904		59.1	59.1			
Average			2.68		337.8	59.1				
Min			2.44		330.0	58.0				
Max			2.87		345.0	61.0				

Impinger Weight Sheet - Run 1A

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Project #: M234302
 Date: 10/24/2023
 Test Method: 5/26A
 Weighed/Measured By: RODS
 Balance ID: LV4

Scale Calibration Check Date: 10/24/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass
Certified Weight, grams Result, grams
 250 250.0
 500 500.0
 750 750.0

IMPINGER	FINAL	INITIAL	GAIN
CONTENTS	MLS / GRAMS	MLS / GRAMS	MLS / GRAMS
0.1N H2SO4	738.0	738.8	-0.8
0.1N H2SO4	713.4	697.4	16.0
Empty	707.8	703.1	4.7
0.1N NaOH	610.4	607.9	2.5
0.1N NaOH	684.1	683.7	0.4
Silica Gel	846.0	834.6	11.4

<u>3,453.7</u> Liquid Final	<u>3,430.9</u> Liquid Initial	<u>22.8</u> Liquid Gain
<u>846.0</u> Silica Final	<u>834.6</u> Silica Initial	<u>11.4</u> Silica Gain

Run 2A - Method 5/26A

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Source Condition: Normal

Date: 10/24/23
 Start Time: 10:00
 End Time: 11:11

DRY GAS METER CONDITIONS

STACK CONDITIONS

ΔH:	2.79	In. H ₂ O	Static Pressure	-0.10	in. H ₂ O
Meter Temperature, T _m :	67.8	°F	Flue Pressure (Ps):	23.64	in. Hg. abs.
Sqrt ΔP:	0.816	In. H ₂ O	Carbon Dioxide:	6.30	%
Stack Temperature, T _s :	343.8	°F	Oxygen:	16.20	%
Meter Volume, V _m :	63.593	ft ³	Nitrogen:	77.5	%
Meter Volume, V _{mstd} :	50.403	dscf	Gas Weight dry, M _d :	29.656	lb/lb mole
Meter Volume, V _{wstd} :	1.729	wscf	Gas Weight wet, M _s :	29.270	lb/lb mole
Isokinetic Variance:	100.8	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, V _s :	61.667	fps
Nozzle Diameter:	0.287	in inches	Volumetric Flow:	351,625	acfm
Barometric Pressure:	23.65	in Hg	Volumetric Flow:	176,437	dscfm
			Volumetric Flow:	182,488	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3517.9	ml	Silica Initial Wt.	796.8	grams
Final Impinger Content:	3540.7	ml	Silica Final Wt.	810.7	grams
Impinger Difference:	22.8	ml	Silica Difference:	13.9	grams
Total Water Gain:	36.7		Moisture, Bws:	0.033	

Port-Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp		Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
						Inlet °F	Outlet °F			
1-1	10:00:00	0.72	3.01	900.680	340	66	66	260	257	55
1-2	10:05:00	0.67	2.80	906.240	345	68	68	261	260	55
1-3	10:10:00	0.61	2.55	911.580	345	68	68	261	262	57
	10:15:00			916.570						
2-1	10:18:00	0.69	2.88	916.570	345	68	68	258	260	56
2-2	10:23:00	0.68	2.84	921.780	346	68	68	262	261	58
2-3	10:28:00	0.59	2.46	927.180	346	68	68	264	258	59
	10:33:00			932.290						
3-1	10:36:00	0.70	2.92	932.290	345	68	68	254	260	56
3-2	10:41:00	0.65	2.72	937.690	344	69	69	257	256	58
3-3	10:46:00	0.67	2.80	943.150	346	69	69	258	257	60
	10:51:00			948.280						
4-1	10:56:00	0.71	2.97	948.280	342	67	67	258	256	60
4-2	11:01:00	0.68	2.85	953.690	341	67	67	259	257	61
4-3	11:06:00	0.63	2.65	959.100	340	68	68	259	257	62
	11:11:00			964.273						
Total	1:00:00			63.593		67.8	67.8			
Average			2.79		343.8	67.8				
Min			2.46		340.0	66.0				
Max			3.01		346.0	69.0				

Impinger Weight Sheet - Run 2A

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Project #: M234302
 Date: 10/24/2023
 Test Method: 5/26A
 Weighed/Measured By: RODS
 Balance ID: LV4

Scale Calibration Check Date: 10/24/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER	FINAL	INITIAL	GAIN
CONTENTS	MLS / GRAMS	MLS / GRAMS	MLS / GRAMS
0.1N H2SO4	789.7	783.4	6.3
0.1N H2SO4	718.5	704.2	14.3
Empty	663.9	661.2	2.7
0.1N NaOH	679.0	680.0	-1.0
0.1N NaOH	689.6	689.1	0.5
Silica Gel	810.7	796.8	13.9

<u>3,540.7</u> Liquid Final	<u>3,517.9</u> Liquid Initial	<u>22.8</u> Liquid Gain
<u>810.7</u> Silica Final	<u>796.8</u> Silica Initial	<u>13.9</u> Silica Gain

Run 3A - Method 5/26A

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Source Condition: Normal

Date: 10/24/23
 Start Time: 12:00
 End Time: 13:10

DRY GAS METER CONDITIONS

STACK CONDITIONS

ΔH:	2.66	In. H ₂ O	Static Pressure	-0.10	in. H ₂ O
Meter Temperature, T _m :	69.3	°F	Flue Pressure (Ps):	23.64	in. Hg. abs.
Sqrt ΔP:	0.795	In. H ₂ O	Carbon Dioxide:	6.50	%
Stack Temperature, T _s :	341.4	°F	Oxygen:	16.20	%
Meter Volume, V _m :	62.203	ft ³	Nitrogen:	77.3	%
Meter Volume, V _{mstd} :	49.143	dscf	Gas Weight dry, M _d :	29.688	lb/lb mole
Meter Volume, V _{wstd} :	1.540	wscf	Gas Weight wet, M _s :	29.333	lb/lb mole
Isokinetic Variance:	100.6	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, V _s :	59.909	fps
Nozzle Diameter:	0.287	in inches	Volumetric Flow:	341,603	acfm
Barometric Pressure:	23.65	in Hg	Volumetric Flow:	172,400	dscfm
			Volumetric Flow:	177,803	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3380.2	ml	Silica Initial Wt.	846.0	grams
Final Impinger Content:	3402.9	ml	Silica Final Wt.	856.0	grams
Impinger Difference:	22.7	ml	Silica Difference:	10.0	grams
Total Water Gain:	32.7		Moisture, Bws:	0.030	

Port-Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp		Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
						Inlet °F	Outlet °F			
1-1	12:00:00	0.68	2.84	964.942	341	66	66	255	260	55
1-2	12:05:00	0.64	2.69	970.300	341	68	68	267	260	56
1-3	12:10:00	0.59	2.47	975.480	342	68	68	263	256	58
	12:15:00			980.490						
2-1	12:18:00	0.70	2.93	980.490	344	69	69	256	260	58
2-2	12:23:00	0.68	2.85	985.960	344	69	69	256	260	59
2-3	12:28:00	0.55	2.30	991.300	345	69	69	256	261	61
	12:33:00			996.120						
3-1	12:36:00	0.71	2.99	996.120	342	70	70	259	259	62
3-2	12:41:00	0.65	2.73	1001.600	342	70	70	259	259	62
3-3	12:46:00	0.53	2.23	1006.790	343	70	70	260	259	62
	12:51:00			1011.630						
4-1	12:55:00	0.69	2.93	1011.630	337	71	71	257	259	62
4-2	13:00:00	0.62	2.63	1017.050	338	71	71	257	261	62
4-3	13:05:00	0.56	2.37	1022.310	338	71	71	257	260	62
	13:10:00			1027.145						
Total	1:00:00			62.203		69.3	69.3			
Average			2.66		341.4	69.3				
Min			2.23		337.0	66.0				
Max			2.99		345.0	71.0				

Impinger Weight Sheet - Run 3A

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Project #: M234302
 Date: 10/24/2023
 Test Method: 5/26A
 Weighed/Measured By: RODS
 Balance ID: LV4

Scale Calibration Check Date: 10/24/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER	FINAL	INITIAL	GAIN
CONTENTS	MLS / GRAMS	MLS / GRAMS	MLS / GRAMS
0.1N H2SO4	742.2	736.7	5.5
0.1N H2SO4	712.4	701.6	10.8
Empty	649.7	644.9	4.8
0.1N NaOH	609.4	609.9	-0.5
0.1N NaOH	689.2	687.1	2.1
Silica Gel	856.0	846.0	10.0

<u>3,402.9</u> Liquid Final	<u>3,380.2</u> Liquid Initial	<u>22.7</u> Liquid Gain
<u>856.0</u> Silica Final	<u>846.0</u> Silica Initial	<u>10.0</u> Silica Gain

Client:
Facility:
Test Location:
Project #:
Test Method:
Test Engineer:
Test Technician:

GCC Rio Grande Inc.
 Tijeras Plant
 Main Stack
 M234302
 26A
 JLW
 RODS

	<u>Run 1B</u>	<u>Run 2B</u>	<u>Run 3B</u>
Temp ID:	CM46	CM46	CM46
Meter ID:	CM46	CM46	CM46
Pitot ID:	S8-032A	S8-032A	S8-032A
Nozzle Diameter (Inches):	0.282	0.282	0.282
Meter Calibration Date:	9/5/2023	9/5/2023	9/5/2023
Meter Calibration Factor (Y):	1.004	1.004	1.004
Meter Orifice Setting (Delta H):	1.744	1.744	1.744
Nozzle Kit ID Number and Material:	Glass	Glass	Glass
Pitot Tube Coefficient:		0.822	
Probe Length (Feet):		6.0	
Probe Liner Material:		Glass	
Sample Plane:		Horizontal	
Port Length (Inches):		6.50	
Port Size (Diameter, Inches):		4.00	
Port Type:		Flange	
Duct Shape:		Circular	
Diameter (Feet):		11	
Duct Area (Square Feet):		95.033	
Upstream Diameters:		3.3	
Downstream Diameters:		9.2	
Number of Ports Sampled:		4	
Number of Points per Port:		3	
Minutes per Point:		5.0	
Minutes per Reading:		5.0	
Total Number of Traverse Points:		12	
Test Length (Minutes):		60	
Train Type:		Anderson Box	
Source Condition:		Normal	
Diluent Model/Serial Number:		CAI 700 and MKS 2030	
Moisture Balance ID:		LV4	
# of Runs		3	

Run 1B - Method 26A

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Source Condition: Normal

Date: 10/24/23
 Start Time: 8:00
 End Time: 9:20

DRY GAS METER CONDITIONS

STACK CONDITIONS

ΔH:	2.93	in. H ₂ O	Static Pressure	-0.10	in. H ₂ O
Meter Temperature, T _m :	59.4	°F	Flue Pressure (Ps):	23.63	in. Hg. abs.
Sqrt ΔP:	0.849	in. H ₂ O	Carbon Dioxide:	6.20	%
Stack Temperature, T _s :	339.4	°F	Oxygen:	16.10	%
Meter Volume, V _m :	62.581	ft ³	Nitrogen:	77.70	%
Meter Volume, V _{mstd} :	50.924	dscf	Gas Weight dry, M _d :	29.636	lb/lb mole
Meter Volume, V _{wstd} :	1.535	wscf	Gas Weight wet, M _s :	29.295	lb/lb mole
Isokinetic Variance:	100.5	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, V _s :	64.135	fps
Nozzle Diameter:	0.282	in inches	Volumetric Flow:	365,695	acfm
Barometric Pressure:	23.64	in Hg	Volumetric Flow:	185,194	dscfm
			Volumetric Flow:	190,778	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3666.6	ml	Silica Initial Wt.	878.3	grams
Final Impinger Content:	3686.5	ml	Silica Final Wt.	891.0	grams
Impinger Difference:	19.9	ml	Silica Difference:	12.7	grams
Total Water Gain:	32.6		Moisture, Bws:	0.029	

Port-Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp		Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
						Inlet °F	Outlet °F			
1-1	8:00:00	0.70	2.76	87.321	336	58	58	260	260	56
1-2	8:05:00	0.75	3.50	92.460	336	58	58	260	260	56
1-3	8:10:00	0.73	3.00	97.770	336	58	58	260	260	56
	8:15:00			103.013						
2-1	8:20:00	0.74	2.80	103.013	334	59	59	259	259	56
2-2	8:25:00	0.75	3.50	108.308	338	59	59	251	261	56
2-3	8:30:00	0.71	3.00	113.627	339	59	59	260	260	56
	8:35:00			118.798						
3-1	8:45:00	0.75	2.80	118.798	341	60	60	260	259	53
3-2	8:50:00	0.71	2.90	124.118	341	60	60	260	262	52
3-3	8:55:00	0.65	2.80	129.367	341	60	60	264	258	52
	9:00:00			134.242						
4-1	9:05:00	0.75	2.50	134.242	344	60	60	264	260	55
4-2	9:10:00	0.73	2.80	139.555	344	61	61	263	262	56
4-3	9:15:00	0.69	2.80	144.780	343	61	61	260	260	57
	9:20:00			149.902						
Total	1:00:00			62.581		59.4	59.4			
Average			2.93		339.4	59.4				
Min			2.50		334.0	58.0				
Max			3.50		344.0	61.0				

Impinger Weight Sheet - Run 1B

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Project #: M234302
 Date: 10/24/2023
 Test Method: 26A
 Weighed/Measured By: RODS
 Balance ID: LV4

Scale Calibration Check Date: 10/24/2023
 Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	249.9
500	500.1
750	750.0

IMPINGER	FINAL	INITIAL	GAIN
CONTENTS	MLS / GRAMS	MLS / GRAMS	MLS / GRAMS
0.1N H2SO4	743.9	756.2	-12.3
0.1N H2SO4	809.1	793.9	15.2
Empty	639.3	631.7	7.6
0.1N NaOH	756.8	750.7	6.1
0.1N NaOH	737.4	734.1	3.3
Silica Gel	891.0	878.3	12.7

3,686.5	3,666.6	19.9
Liquid Final	Liquid Initial	Liquid Gain
891.0	878.3	12.7
Silica Final	Silica Initial	Silica Gain

Run 2B - Method 26A

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Source Condition: Normal

Date: 10/24/23
 Start Time: 10:00
 End Time: 11:11

DRY GAS METER CONDITIONS

STACK CONDITIONS

ΔH:	2.83	In. H ₂ O	Static Pressure	-0.10	in. H ₂ O
Meter Temperature, T _m :	70.4	°F	Flue Pressure (Ps):	23.63	in. Hg. abs.
Sqrt ΔP:	0.840	In. H ₂ O	Carbon Dioxide:	6.30	%
Stack Temperature, T _s :	343.3	°F	Oxygen:	16.20	%
Meter Volume, V _m :	63.042	ft ³	Nitrogen:	77.5	%
Meter Volume, V _{mstd} :	50.220	dscf	Gas Weight dry, M _d :	29.656	lb/lb mole
Meter Volume, V _{wstd} :	1.677	wscf	Gas Weight wet, M _s :	29.279	lb/lb mole
Isokinetic Variance:	100.7	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, V _s :	63.594	fps
Nozzle Diameter:	0.282	in inches	Volumetric Flow:	362,612	acfm
Barometric Pressure:	23.64	in Hg	Volumetric Flow:	182,166	dscfm
			Volumetric Flow:	188,248	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3478.2	ml	Silica Initial Wt.	862.8	grams
Final Impinger Content:	3496.6	ml	Silica Final Wt.	880.0	grams
Impinger Difference:	18.4	ml	Silica Difference:	17.2	grams
Total Water Gain:	35.6		Moisture, Bws:	0.032	

Port-Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp		Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
						Inlet °F	Outlet °F			
1-1	10:00:00	0.75	2.98	50.080	347	68	68	256	259	58
1-2	10:05:00	0.71	2.82	55.466	347	69	69	255	263	61
1-3	10:10:00	0.69	2.75	60.708	346	69	69	260	260	60
	10:15:00			65.878						
2-1	10:18:00	0.75	3.00	65.878	345	71	71	263	264	58
2-2	10:23:00	0.73	2.80	71.299	344	71	71	260	255	58
2-3	10:28:00	0.71	2.80	76.645	344	71	71	260	259	60
	10:33:00			81.918						
3-1	10:36:00	0.75	3.00	81.918	342	72	72	259	258	60
3-2	10:41:00	0.70	2.90	87.358	341	72	72	260	260	60
3-3	10:46:00	0.69	2.80	92.612	341	72	72	261	260	59
	10:51:00			97.831						
4-1	10:56:00	0.70	2.82	97.831	341	70	70	260	258	61
4-2	11:01:00	0.65	2.75	103.069	341	70	70	265	260	61
4-3	11:06:00	0.64	2.60	108.117	341	70	70	260	260	60
	11:11:00			113.122						
Total	1:00:00			63.042		70.4	70.4			
Average			2.83		343.3	70.4				
Min			2.60		341.0	68.0				
Max			3.00		347.0	72.0				

Impinger Weight Sheet - Run 2B

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Project #: M234302
 Date: 10/24/2023
 Test Method: 26A
 Weighed/Measured By: RODS
 Balance ID: LV4

Scale Calibration Check Date: 10/24/2023
 Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	249.9
500	500.1
750	750.0

IMPINGER	FINAL	INITIAL	GAIN
CONTENTS	MLS / GRAMS	MLS / GRAMS	MLS / GRAMS
0.1N H2SO4	754.7	754.0	0.7
0.1N H2SO4	675.6	668.9	6.7
Empty	674.0	595.7	78.3
0.1N NaOH	676.8	687.5	-10.7
0.1N NaOH	715.5	772.1	-56.6
Silica Gel	880.0	862.8	17.2

3,496.6	3,478.2	18.4
Liquid Final	Liquid Initial	Liquid Gain
880.0	862.8	17.2
Silica Final	Silica Initial	Silica Gain

Run 3B - Method 26A

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Source Condition: Normal

Date: 10/24/23
 Start Time: 12:00
 End Time: 13:10

DRY GAS METER CONDITIONS

STACK CONDITIONS

ΔH:	2.85	In. H ₂ O	Static Pressure	-0.10	in. H ₂ O
Meter Temperature, T _m :	72.4	°F	Flue Pressure (Ps):	23.63	in. Hg. abs.
Sqrt ΔP:	0.827	In. H ₂ O	Carbon Dioxide:	6.50	%
Stack Temperature, T _s :	338.2	°F	Oxygen:	16.20	%
Meter Volume, V _m :	62.501	ft ³	Nitrogen:	77.3	%
Meter Volume, V _{mstd} :	49.605	dscf	Gas Weight dry, M _d :	29.688	lb/lb mole
Meter Volume, V _{wstd} :	1.733	wscf	Gas Weight wet, M _s :	29.293	lb/lb mole
Isokinetic Variance:	100.9	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, V _s :	62.395	fps
Nozzle Diameter:	0.282	in inches	Volumetric Flow:	355,774	acfm
Barometric Pressure:	23.64	in Hg	Volumetric Flow:	179,617	dscfm
			Volumetric Flow:	185,894	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3660.5	ml	Silica Initial Wt.	891.0	grams
Final Impinger Content:	3685.3	ml	Silica Final Wt.	903.0	grams
Impinger Difference:	24.8	ml	Silica Difference:	12.0	grams
Total Water Gain:	36.8		Moisture, Bws:	0.034	

Port-Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp		Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
						Inlet °F	Outlet °F			
1-1	12:00:00	0.75	2.80	13.485	340	70	70	257	260	53
1-2	12:05:00	0.69	3.00	18.910	340	70	70	263	260	54
1-3	12:10:00	0.70	2.72	24.116	339	70	70	258	260	53
	12:15:00			29.355						
2-1	12:18:00	0.73	2.91	29.355	337	72	72	265	262	54
2-2	12:23:00	0.70	2.80	34.738	337	73	73	258	258	56
2-3	12:28:00	0.69	2.76	40.020	337	73	73	258	260	55
	12:33:00			45.258						
3-1	12:36:00	0.69	2.80	45.258	337	73	73	261	261	56
3-2	12:41:00	0.65	2.90	50.510	337	73	73	260	260	56
3-3	12:46:00	0.67	3.00	55.589	337	73	73	261	261	56
	12:51:00			60.753						
4-1	12:55:00	0.65	2.85	60.753	339	74	74	265	260	57
4-2	13:00:00	0.63	2.72	65.846	339	74	74	261	260	57
4-3	13:05:00	0.66	2.98	70.858	339	74	74	261	258	57
	13:10:00			75.986						
Total	1:00:00			62.501		72.4	72.4			
Average			2.85		338.2	72.4				
Min			2.72		337.0	70.0				
Max			3.00		340.0	74.0				

Impinger Weight Sheet - Run 3B

Client: GCC Rio Grande Inc.
 Facility: Tijeras Plant
 Test Location: Main Stack
 Project #: M234302
 Date: 10/24/2023
 Test Method: 26A
 Weighed/Measured By: RODS
 Balance ID: LV4

Scale Calibration Check Date: 10/24/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>249.9</u>
500	<u>500.1</u>
750	<u>750.0</u>

IMPINGER	FINAL	INITIAL	GAIN
CONTENTS	MLS / GRAMS	MLS / GRAMS	MLS / GRAMS
0.1N H2SO4	767.2	760.9	6.3
0.1N H2SO4	798.6	787.0	11.6
Empty	637.8	633.5	4.3
0.1N NaOH	746.8	733.8	13.0
0.1N NaOH	734.9	745.3	-10.4
Silica Gel	903.0	891.0	12.0

<u>3,685.3</u> Liquid Final	<u>3,660.5</u> Liquid Initial	<u>24.8</u> Liquid Gain
<u>903.0</u> Silica Final	<u>891.0</u> Silica Initial	<u>12.0</u> Silica Gain

Client: GCC Rio Grande, Inc.
 Facility: Tijeras Plant
 Project #: M234302
 Test Location: Main Stack
 Date: 10/24/23

Run 1

Spectrum	Time	FTIR Data					Analyzer Data	
		H2O %	CO2 % (wet)	HCN ppmvw	HF ppmvw	Cell Temp	Pressure	O2 % (dry)
RUN1_000250.LAB	8:00	2.89	5.87	1.99	0.10	190.74	0.80	16.33
RUN1_000251.LAB	8:01	2.89	5.92	1.94	0.10	190.76	0.80	16.31
RUN1_000252.LAB	8:02	2.86	5.80	1.90	0.10	190.91	0.80	16.35
RUN1_000253.LAB	8:03	2.87	5.78	1.91	0.10	190.88	0.80	16.36
RUN1_000254.LAB	8:04	2.85	5.75	1.94	0.10	190.71	0.80	16.33
RUN1_000255.LAB	8:05	2.84	5.73	1.92	0.10	190.68	0.80	16.42
RUN1_000256.LAB	8:06	2.83	5.76	1.97	0.10	190.76	0.80	16.36
RUN1_000257.LAB	8:07	2.86	5.84	1.96	0.10	190.78	0.80	16.36
RUN1_000258.LAB	8:08	2.83	5.83	1.92	0.10	190.69	0.80	16.35
RUN1_000259.LAB	8:09	2.89	5.97	2.01	0.10	190.62	0.80	16.35
RUN1_000260.LAB	8:10	2.85	5.95	1.97	0.10	190.74	0.80	16.22
RUN1_000261.LAB	8:11	2.84	5.85	1.95	0.10	190.80	0.80	16.36
RUN1_000262.LAB	8:12	2.89	5.93	2.02	0.10	190.74	0.80	16.37
RUN1_000263.LAB	8:13	2.91	6.01	2.14	0.10	190.66	0.80	16.28
RUN1_000264.LAB	8:14	2.92	5.99	2.08	0.10	190.74	0.80	16.22
RUN1_000265.LAB	8:15	2.93	5.97	2.09	0.10	190.89	0.80	16.30
RUN1_000266.LAB	8:16	2.92	5.97	2.09	0.10	190.81	0.80	16.27
RUN1_000267.LAB	8:17	2.90	5.89	2.03	0.10	190.68	0.80	16.32
RUN1_000268.LAB	8:18	2.90	5.96	2.06	0.10	190.69	0.80	16.34
RUN1_000269.LAB	8:19	2.88	5.92	2.00	0.10	190.74	0.80	16.31
RUN1_000270.LAB	8:20	2.89	6.04	2.10	0.10	190.75	0.80	16.35
RUN1_000271.LAB	8:21	2.87	6.06	2.03	0.10	190.69	0.80	16.27
RUN1_000272.LAB	8:22	2.86	6.09	2.11	0.10	190.72	0.80	16.26
RUN1_000273.LAB	8:23	2.83	5.96	2.03	0.10	190.84	0.80	16.28
RUN1_000274.LAB	8:24	2.84	6.01	1.96	0.10	190.81	0.80	16.29
RUN1_000275.LAB	8:25	2.85	5.97	2.02	0.10	190.69	0.80	16.31
RUN1_000276.LAB	8:26	2.88	6.05	1.96	0.10	190.65	0.80	16.29
RUN1_000277.LAB	8:27	2.85	6.00	2.00	0.10	190.79	0.80	16.27
RUN1_000278.LAB	8:28	2.86	5.92	1.88	0.10	190.84	0.80	16.27
RUN1_000279.LAB	8:29	2.90	6.05	2.05	0.10	190.75	0.80	16.30
RUN1_000280.LAB	8:30	2.89	5.96	1.99	0.10	190.66	0.80	16.28
RUN1_000281.LAB	8:31	2.87	5.92	1.93	0.10	190.74	0.80	16.20
RUN1_000282.LAB	8:32	2.86	5.92	1.94	0.10	190.84	0.80	16.29
RUN1_000283.LAB	8:33	2.85	5.92	1.90	0.10	190.83	0.80	16.28
RUN1_000284.LAB	8:34	2.84	5.86	1.88	0.10	191.01	0.80	16.32
RUN1_000285.LAB	8:35	2.86	5.94	1.93	0.10	191.19	0.80	16.31
RUN1_000286.LAB	8:36	2.87	6.11	1.97	0.10	191.26	0.80	16.37
RUN1_000287.LAB	8:37	2.85	6.08	1.99	0.10	191.24	0.80	16.27
RUN1_000288.LAB	8:38	2.86	6.13	1.87	0.10	191.04	0.80	16.23
RUN1_000289.LAB	8:39	2.87	6.22	2.01	0.10	190.82	0.80	16.25
RUN1_000290.LAB	8:40	2.82	6.05	1.92	0.10	190.73	0.80	16.19
RUN1_000291.LAB	8:41	2.85	6.13	1.88	0.10	190.74	0.80	16.17
RUN1_000292.LAB	8:42	2.85	6.29	2.07	0.10	190.83	0.80	16.27
RUN1_000293.LAB	8:43	2.82	6.20	1.97	0.10	190.74	0.80	16.23
RUN1_000294.LAB	8:44	2.82	6.22	1.95	0.10	190.59	0.80	16.11
RUN1_000295.LAB	8:45	2.80	6.24	1.97	0.10	190.62	0.80	16.12
RUN1_000296.LAB	8:46	2.80	6.25	2.05	0.10	190.73	0.80	16.14
RUN1_000297.LAB	8:47	2.77	6.16	1.86	0.10	190.72	0.80	16.14
RUN1_000298.LAB	8:48	2.80	6.20	1.93	0.10	190.66	0.80	16.10
RUN1_000299.LAB	8:49	2.81	6.25	1.99	0.10	190.65	0.80	16.16
RUN1_000300.LAB	8:50	2.82	6.25	2.01	0.10	190.78	0.80	16.17
RUN1_000301.LAB	8:51	2.85	6.37	2.11	0.10	190.79	0.80	16.11
RUN1_000302.LAB	8:52	2.84	6.31	2.05	0.10	190.73	0.80	16.08
RUN1_000303.LAB	8:53	2.87	6.42	2.23	0.10	190.64	0.80	16.08
RUN1_000304.LAB	8:54	2.85	6.28	2.20	0.10	190.74	0.80	16.08
RUN1_000305.LAB	8:55	2.89	6.33	2.36	0.10	190.82	0.80	16.09
RUN1_000306.LAB	8:56	2.88	6.29	2.39	0.10	190.76	0.80	16.08
RUN1_000307.LAB	8:57	2.90	6.37	2.34	0.10	190.69	0.80	16.12
RUN1_000308.LAB	8:58	2.93	6.47	2.42	0.10	190.73	0.80	16.06
RUN1_000309.LAB	8:59	2.94	6.49	2.38	0.10	190.83	0.80	16.11
Average		2.86	6.06	2.03	0.10	190.78	0.80	16.25

Client: GCC Rio Grande, Inc.
 Facility: Tijeras Plant
 Project #: M234302
 Test Location: Main Stack
 Date: 10/24/23

Run 2

Spectrum	Time	FTIR Data					Cell Temp	Pressure	Analyzer Data
		H2O %	CO2 % (wet)	HCN ppmvw	HF ppmvw	O2 % (dry)			
RUN2_000439.LAB	10:00	2.67	6.3	2.03	0.10	190.6	0.80	16.11	
RUN2_000440.LAB	10:01	2.62	6.2	1.97	0.10	190.7	0.80	16.22	
RUN2_000441.LAB	10:02	2.62	6.2	1.96	0.10	190.7	0.80	16.19	
RUN2_000442.LAB	10:03	2.67	6.4	2.20	0.10	190.6	0.80	16.05	
RUN2_000443.LAB	10:04	2.59	6.2	1.99	0.10	190.6	0.80	16.23	
RUN2_000444.LAB	10:05	2.55	6.0	1.72	0.10	190.6	0.80	16.37	
RUN2_000445.LAB	10:06	2.59	6.1	1.85	0.10	190.5	0.80	16.25	
RUN2_000446.LAB	10:07	2.58	6.1	1.82	0.10	190.4	0.80	16.30	
RUN2_000447.LAB	10:08	2.61	6.1	1.93	0.10	190.6	0.80	16.23	
RUN2_000448.LAB	10:09	2.59	6.0	1.88	0.10	190.6	0.80	16.26	
RUN2_000449.LAB	10:10	2.58	5.9	1.81	0.10	190.5	0.80	16.35	
RUN2_000450.LAB	10:11	2.58	6.0	1.78	0.10	190.6	0.80	16.29	
RUN2_000451.LAB	10:12	2.59	6.0	1.79	0.10	190.7	0.80	16.34	
RUN2_000452.LAB	10:13	2.60	6.0	1.90	0.10	190.7	0.80	16.27	
RUN2_000453.LAB	10:14	2.62	6.1	1.84	0.10	190.5	0.80	16.32	
RUN2_000454.LAB	10:15	2.61	6.2	1.86	0.10	190.6	0.80	16.19	
RUN2_000455.LAB	10:16	2.62	6.2	1.88	0.10	190.7	0.80	16.24	
RUN2_000456.LAB	10:17	2.64	6.3	1.90	0.10	190.7	0.80	16.24	
RUN2_000457.LAB	10:18	2.64	6.3	1.84	0.10	190.6	0.80	16.18	
RUN2_000458.LAB	10:19	2.62	6.2	1.78	0.10	190.7	0.80	16.23	
RUN2_000459.LAB	10:20	2.63	6.1	1.73	0.10	190.7	0.80	16.27	
RUN2_000460.LAB	10:21	2.63	6.1	1.81	0.10	190.6	0.80	16.23	
RUN2_000461.LAB	10:22	2.61	6.0	1.77	0.10	190.6	0.80	16.25	
RUN2_000462.LAB	10:23	2.64	6.1	1.79	0.10	190.7	0.80	16.28	
RUN2_000463.LAB	10:24	2.64	6.1	1.76	0.10	190.7	0.80	16.24	
RUN2_000464.LAB	10:25	2.67	6.2	1.78	0.10	190.6	0.80	16.24	
RUN2_000465.LAB	10:26	2.66	6.1	1.76	0.10	190.7	0.80	16.17	
RUN2_000466.LAB	10:27	2.70	6.2	1.79	0.10	190.7	0.80	16.26	
RUN2_000467.LAB	10:28	2.67	6.1	1.68	0.10	190.7	0.80	16.18	
RUN2_000468.LAB	10:29	2.72	6.2	1.89	0.10	190.6	0.80	16.23	
RUN2_000469.LAB	10:30	2.71	6.2	1.86	0.10	190.7	0.80	16.18	
RUN2_000470.LAB	10:31	2.67	6.1	1.74	0.10	190.8	0.80	16.19	
RUN2_000471.LAB	10:32	2.68	6.1	1.78	0.10	190.7	0.80	16.29	
RUN2_000472.LAB	10:33	2.68	6.1	1.78	0.10	190.6	0.80	16.28	
RUN2_000473.LAB	10:34	2.67	6.0	1.80	0.10	190.8	0.80	16.24	
RUN2_000474.LAB	10:35	2.69	6.2	1.83	0.10	190.7	0.80	16.42	
RUN2_000475.LAB	10:36	2.67	6.2	1.86	0.10	190.6	0.80	16.28	
RUN2_000476.LAB	10:37	2.67	6.2	1.80	0.10	190.7	0.80	16.26	
RUN2_000477.LAB	10:38	2.67	6.2	1.78	0.10	190.8	0.80	16.28	
RUN2_000478.LAB	10:39	2.68	6.2	1.85	0.10	190.8	0.80	16.26	
RUN2_000479.LAB	10:40	2.69	6.2	1.82	0.10	190.7	0.80	16.27	
RUN2_000480.LAB	10:41	2.68	6.1	1.77	0.10	190.7	0.80	16.25	
RUN2_000481.LAB	10:42	2.67	6.0	1.74	0.10	190.8	0.80	16.30	
RUN2_000482.LAB	10:43	2.72	6.1	1.77	0.10	190.7	0.80	16.27	
RUN2_000483.LAB	10:44	2.72	6.1	1.81	0.10	190.6	0.80	16.33	
RUN2_000484.LAB	10:45	2.76	6.2	1.88	0.10	190.7	0.80	16.25	
RUN2_000485.LAB	10:46	2.73	6.1	1.79	0.10	190.8	0.80	16.28	
RUN2_000486.LAB	10:47	2.75	6.1	1.77	0.10	190.7	0.80	16.23	
RUN2_000487.LAB	10:48	2.74	6.1	1.73	0.10	190.6	0.80	16.31	
RUN2_000488.LAB	10:49	2.77	6.2	1.79	0.10	190.8	0.80	16.29	
RUN2_000489.LAB	10:50	2.79	6.3	1.76	0.10	190.8	0.80	16.31	
RUN2_000490.LAB	10:51	2.82	6.4	1.90	0.10	190.7	0.80	16.25	
RUN2_000491.LAB	10:52	2.80	6.3	1.81	0.10	190.7	0.80	16.20	
RUN2_000492.LAB	10:53	2.82	6.4	1.75	0.10	190.8	0.80	16.12	
RUN2_000493.LAB	10:54	2.82	6.4	1.79	0.10	190.7	0.80	16.17	
RUN2_000494.LAB	10:55	2.80	6.3	1.76	0.10	190.6	0.80	16.16	
RUN2_000495.LAB	10:56	2.80	6.1	1.80	0.10	190.7	0.80	16.14	
RUN2_000496.LAB	10:57	2.80	6.2	1.77	0.10	190.8	0.80	16.14	
RUN2_000497.LAB	10:58	2.79	6.1	1.73	0.10	190.7	0.80	16.20	
RUN2_000498.LAB	10:59	2.76	6.1	1.76	0.10	190.6	0.80	16.26	
Average		2.68	6.15	1.82	0.10	190.67	0.80	16.24	

Client: GCC Rio Grande, Inc.
 Facility: Tijeras Plant
 Project #: M234302
 Test Location: Main Stack
 Date: 10/24/23

Run 3

Spectrum	Time	FTIR Data					Analyzer Data	
		H2O %	CO2 % (wet)	HCN ppmvw	HF ppmvw	Cell Temp	Pressure	O2 % (dry)
RUN3_000624.LAB	12:00	2.72	6.3	1.80	0.10	190.8	0.80	16.22
RUN3_000625.LAB	12:01	2.72	6.3	1.65	0.10	190.8	0.80	16.21
RUN3_000626.LAB	12:02	2.71	6.2	1.85	0.10	190.7	0.80	16.23
RUN3_000627.LAB	12:03	2.71	6.2	1.74	0.10	190.7	0.80	16.31
RUN3_000628.LAB	12:04	2.67	6.0	1.78	0.10	190.8	0.80	16.34
RUN3_000629.LAB	12:05	2.69	6.2	1.78	0.10	190.7	0.80	16.31
RUN3_000630.LAB	12:06	2.70	6.2	1.83	0.10	190.6	0.80	16.25
RUN3_000631.LAB	12:07	2.70	6.1	1.79	0.10	190.7	0.80	16.32
RUN3_000632.LAB	12:08	2.70	6.2	1.86	0.10	190.8	0.80	16.22
RUN3_000633.LAB	12:09	2.71	6.2	1.88	0.10	190.7	0.80	16.30
RUN3_000634.LAB	12:10	2.74	6.2	1.87	0.10	190.6	0.80	16.22
RUN3_000635.LAB	12:11	2.70	6.0	1.87	0.10	190.7	0.80	16.23
RUN3_000636.LAB	12:12	2.73	6.1	1.85	0.10	190.7	0.80	16.36
RUN3_000637.LAB	12:13	2.69	6.0	1.78	0.10	190.7	0.80	16.23
RUN3_000638.LAB	12:14	2.68	6.1	1.80	0.10	190.6	0.80	16.33
RUN3_000639.LAB	12:15	2.69	6.1	1.86	0.10	190.7	0.80	16.32
RUN3_000640.LAB	12:16	2.71	6.1	1.86	0.10	190.7	0.80	16.29
RUN3_000641.LAB	12:17	2.72	6.1	1.80	0.10	190.6	0.80	16.25
RUN3_000642.LAB	12:18	2.72	6.2	1.80	0.10	190.6	0.80	16.29
RUN3_000643.LAB	12:19	2.73	6.2	1.82	0.10	190.7	0.80	16.26
RUN3_000644.LAB	12:20	2.72	6.2	1.82	0.10	190.7	0.80	16.23
RUN3_000645.LAB	12:21	2.72	6.2	1.89	0.10	190.6	0.80	16.27
RUN3_000646.LAB	12:22	2.73	6.2	1.84	0.10	190.6	0.80	16.28
RUN3_000647.LAB	12:23	2.72	6.2	1.84	0.10	190.7	0.80	16.25
RUN3_000648.LAB	12:24	2.73	6.3	1.87	0.10	190.7	0.80	16.29
RUN3_000649.LAB	12:25	2.71	6.2	1.88	0.10	190.6	0.80	16.29
RUN3_000650.LAB	12:26	2.73	6.3	1.85	0.10	190.6	0.80	16.23
RUN3_000651.LAB	12:27	2.74	6.3	1.91	0.10	190.7	0.80	16.30
RUN3_000652.LAB	12:28	2.79	6.4	1.94	0.10	190.7	0.80	16.24
RUN3_000653.LAB	12:29	2.75	6.3	1.91	0.10	190.5	0.80	16.17
RUN3_000654.LAB	12:30	2.74	6.3	1.88	0.10	190.6	0.80	16.15
RUN3_000655.LAB	12:31	2.73	6.4	1.96	0.10	190.7	0.80	16.24
RUN3_000656.LAB	12:32	2.75	6.5	1.97	0.10	190.7	0.80	16.21
RUN3_000657.LAB	12:33	2.70	6.3	1.88	0.10	190.5	0.80	16.20
RUN3_000658.LAB	12:34	2.75	6.4	2.00	0.10	190.7	0.80	16.19
RUN3_000659.LAB	12:35	2.73	6.3	1.89	0.10	190.7	0.80	16.19
RUN3_000660.LAB	12:36	2.77	6.4	2.00	0.10	190.7	0.80	16.19
RUN3_000661.LAB	12:37	2.77	6.4	1.98	0.10	190.6	0.80	16.22
RUN3_000662.LAB	12:38	2.77	6.3	1.92	0.10	190.7	0.80	16.13
RUN3_000663.LAB	12:39	2.74	6.3	1.83	0.10	190.7	0.80	16.16
RUN3_000664.LAB	12:40	2.74	6.3	1.85	0.10	190.7	0.80	16.17
RUN3_000665.LAB	12:41	2.80	6.4	1.93	0.10	190.7	0.80	16.23
RUN3_000666.LAB	12:42	2.80	6.4	2.01	0.10	190.8	0.80	16.23
RUN3_000667.LAB	12:43	2.80	6.4	1.89	0.10	190.8	0.80	16.12
RUN3_000668.LAB	12:44	2.78	6.3	1.86	0.10	190.6	0.80	16.11
RUN3_000669.LAB	12:45	2.76	6.3	1.91	0.10	190.6	0.80	16.10
RUN3_000670.LAB	12:46	2.79	6.4	1.98	0.10	190.7	0.80	16.15
RUN3_000671.LAB	12:47	2.77	6.3	1.91	0.10	190.7	0.80	16.18
RUN3_000672.LAB	12:48	2.75	6.3	1.94	0.10	190.6	0.80	16.15
RUN3_000673.LAB	12:49	2.77	6.6	2.06	0.10	190.6	0.80	16.13
RUN3_000674.LAB	12:50	2.77	6.6	2.07	0.10	190.7	0.80	16.21
RUN3_000675.LAB	12:51	2.76	6.6	1.97	0.10	190.7	0.80	16.13
RUN3_000676.LAB	12:52	2.75	6.6	2.00	0.10	190.6	0.80	16.09
RUN3_000677.LAB	12:53	2.75	6.6	1.97	0.10	190.7	0.80	16.16
RUN3_000678.LAB	12:54	2.68	6.3	1.90	0.10	190.7	0.80	16.12
RUN3_000679.LAB	12:55	2.67	6.3	1.96	0.10	190.7	0.80	16.12
RUN3_000680.LAB	12:56	2.68	6.4	1.92	0.10	190.6	0.80	16.19
RUN3_000681.LAB	12:57	2.72	6.5	1.94	0.10	190.7	0.80	16.26
RUN3_000682.LAB	12:58	2.74	6.6	1.99	0.10	190.8	0.80	16.23
RUN3_000683.LAB	12:59	2.78	6.7	2.06	0.10	190.7	0.80	16.18
Average		2.73	6.30	1.89	0.10	190.68	0.80	16.22

Method 1 and 2 Cyclonic Flow Check Data

Project Number M234302
Client: GCC Rio Grande Inc.
Facility: Tijeras Plant
Location: Main Stack
Pitot ID: S8-031A
Pitot Coefficient: 0.820
Probe Length: 6

Source Condition: Normal
Run No.: 1
Date: 9/26/2023
Start Time: 14:07
End Time: 14:22
RM Testers: NJC
Port Length: 6.50



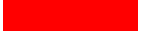
Port	Point	DP (in. H ₂ O)	Sqrt. DP	Temp (°F)	Yaw (°)		Velocity (V)	Port	Point	DP (in. H ₂ O)	Sqrt. DP	Temp (°F)	Yaw (°)		Velocity (V)
A	1	0.70	0.8367	341.0	2.0	2.0	63.11	C	1	0.75	0.8660	343.0	5.0	5.0	65.40
A	2	0.75	0.8660	341.0	2.0	2.0	65.32	C	2	0.71	0.8426	344.0	3.0	3.0	63.67
A	3	0.73	0.8544	341.0	2.0	2.0	64.44	C	3	0.66	0.8124	344.0	3.0	3.0	61.39
B	1	0.74	0.8602	341.0	3.0	3.0	64.88	D	1	0.74	0.8602	344.0	2.0	2.0	65.00
B	2	0.74	0.8602	342.0	1.0	1.0	64.92	D	2	0.73	0.8544	344.0	1.0	1.0	64.56
B	3	0.70	0.8367	342.0	1.0	1.0	63.14	D	3	0.63	0.7937	344.0	1.0	1.0	59.98




Average Yaw Angle 2.2 °

Stratification Test Results Summary
GCC Rio Grande, Inc.
Tijeras Plant
Main Stack
October 24, 2023

Number of Ports Sampled: 1
Number of Points per Port: 3
Total Number of Traverse Points: 3

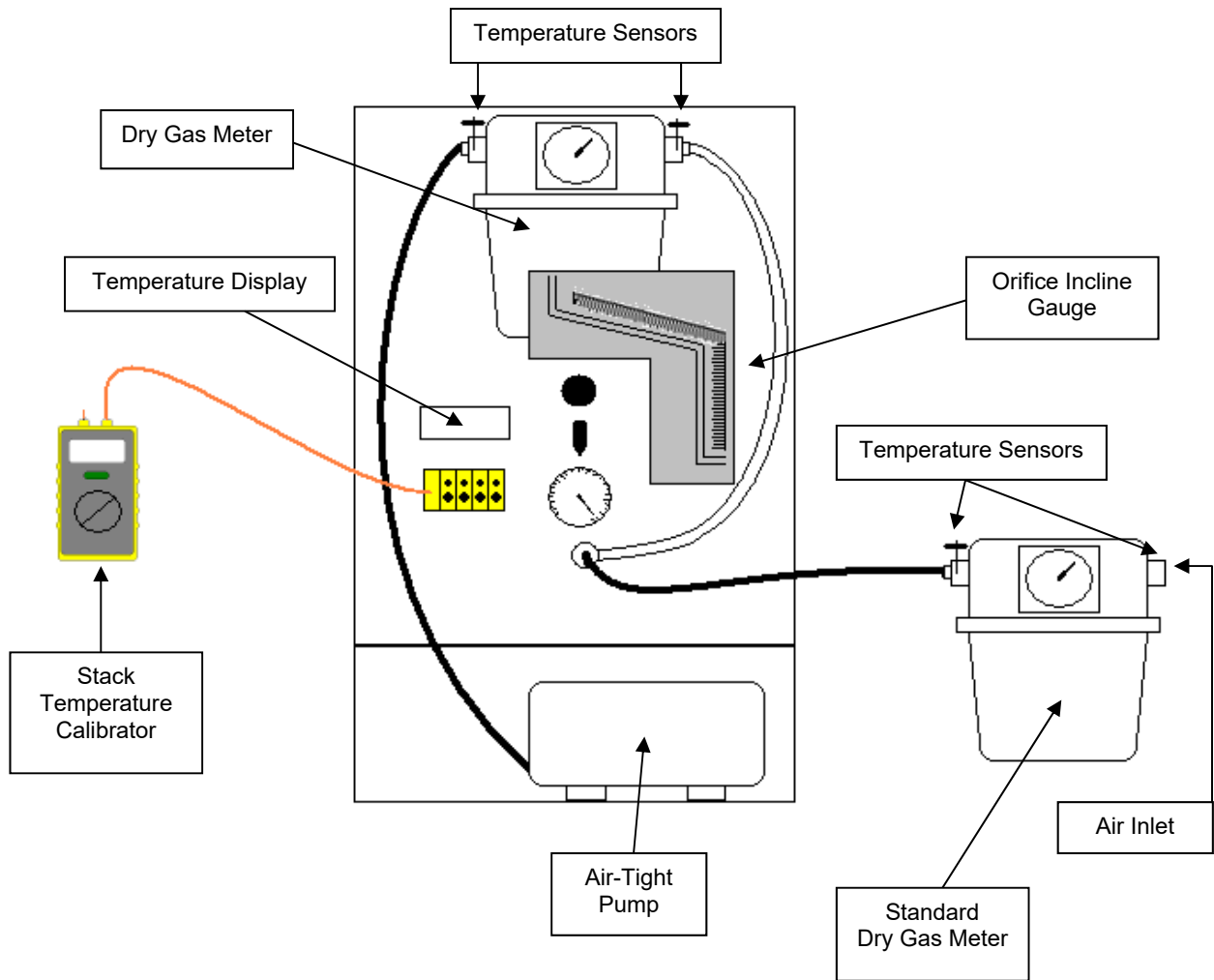
Port No.	Point No.	Time	O ₂ %	Actual % Difference O ₂ %	Mean Difference O ₂ %
1	1	7:51	16.21	0.37	0.06
	2	7:55	16.26	0.06	0.01
	3	7:59	16.34	0.43	0.07
Average			16.27		

One point traverse (<5% difference) 
Three point traverse (0.4, 1.2, and 2.0 meters), <10% difference 
Twelve point traverse (Method 1 points) >10% difference 

One point traverse (<0.3% mean difference) 
Three point traverse (0.4, 1.2, and 2.0 meters), < 0.5% mean difference for O₂ 
Twelve point traverse (Method 1 points) >0.5% mean difference for O₂ 

Appendix G - Calibration Data

Dry Gas Meter/Control Module Calibration Diagram



Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM46
 Standard Meter No. 25125408
 Standard Meter (Y) 0.99800

Date: September 5, 2023
 Calibrated By: DV
 Barometric Pressure: 28.09

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		109.822	84.911	80	79	79					
Initial		104.567	79.639	79	77	77					
Difference	1 0.20	5.255	5.272	80	78	78	78	19	36	0.991	1.714
Final		115.015	90.033	81	80	80					
Initial		109.822	84.911	80	79	79					
Difference	2 0.50	5.193	5.122	81	80	80	80	12	26	1.009	1.767
Final		120.336	95.378	81	81	81					
Initial		115.015	90.033	81	80	80					
Difference	3 0.70	5.321	5.345	81	81	81	81	10	39	0.991	1.729
Final		125.421	100.386	82	82	82					
Initial		120.336	95.378	81	81	81					
Difference	4 0.90	5.085	5.008	82	82	82	82	8	59	1.011	1.732
Final		133.350	108.110	82	83	83					
Initial		128.200	103.044	82	83	83					
Difference	5 1.20	5.150	5.066	82	83	83	83	7	51	1.013	1.717
Final		140.985	115.640	82	84	84					
Initial		133.350	108.110	82	83	83					
Difference	6 2.00	7.635	7.530	82	84	84	84	9	15	1.009	1.807

Average **1.004** **1.744**

Stack Temperature Sensor Calibration

Meter Box # : CM46 Name : DV

Ambient Temperature : 80.7 °F Date : September 5, 2023

Calibrator Model # : CL940A

Serial # : 526

Date Of Certification : December 28, 2022

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

Reference Source Temperature (°F)	Test Thermometer Temperature (°F)	Temperature Difference %
0	0	0.0
250	251	0.1
600	601	0.1
1200	1205	0.3

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM46
 Standard Meter No. 18654530
 Standard Meter (Y) 0.99730

Date: November 28, 2023
 Calibrated By: DV
 Barometric Pressure: 28.43

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		75.159	116.171	60	60	60					
Initial		70.135	111.072	60	61	61					
Difference	1 0.20	5.024	5.099	60	61	61	61	19	50	0.983	1.824
Final		70.135	111.072	60	61	61					
Initial		65.060	105.910	59	61	61					
Difference	2 0.50	5.075	5.162	60	61	61	61	12	45	0.982	1.842
Final		65.060	105.910	59	61	61					
Initial		59.951	100.905	59	59	59					
Difference	3 0.70	5.109	5.005	59	60	60	60	10	30	1.018	1.725
Final		59.951	100.905	59	59	59					
Initial		54.850	95.840	59	58	58					
Difference	4 0.90	5.101	5.065	59	59	59	59	9	32	1.001	1.840
Final		54.850	95.840	59	58	58					
Initial		49.775	90.794	58	58	58					
Difference	5 1.20	5.075	5.046	59	58	58	58	8	15	0.999	1.854
Final		49.775	90.794	58	58	58					
Initial		44.425	85.585	58	57	57					
Difference	6 2.00	5.350	5.209	58	58	58	58	6	48	1.018	1.887

Average **1.000** **1.829**

Stack Temperature Sensor Calibration

Meter Box # : CM46 Name : DV

Ambient Temperature : 58.7 °F Date : November 28, 2023

Calibrator Model # : CL940A

Serial # : 526

Date Of Certification : December 28, 2022

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

Reference Source Temperature (° F)	Test Thermometer Temperature (° F)	Temperature Difference %
0	1	0.2
250	252	0.3
600	602	0.2
1200	1205	0.3

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM53
 Standard Meter No. 18654530
 Standard Meter (Y) 0.99730

Date: September 6, 2023
 Calibrated By: DV
 Barometric Pressure: 28.12

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		108.455	58.760	81	82	82					
Initial		103.434	53.667	80	81	81					
Difference	1 0.20	5.021	5.093	81	82	82	82	18	35	0.985	1.683
Final		103.434	53.667	80	81	81					
Initial		98.353	48.581	80	80	80					
Difference	2 0.50	5.081	5.086	80	81	81	81	12	12	0.996	1.771
Final		98.353	48.581	80	80	80					
Initial		93.335	43.543	79	79	79					
Difference	3 0.70	5.018	5.038	80	80	80	80	10	15	0.992	1.795
Final		93.335	43.543	79	79	79					
Initial		88.268	38.486	79	78	78					
Difference	4 0.90	5.067	5.057	79	79	79	79	9	10	0.996	1.810
Final		88.268	38.486	79	78	78					
Initial		83.006	33.210	79	77	77					
Difference	5 1.20	5.262	5.276	79	78	78	78	8	12	0.989	1.794
Final		83.006	33.210	79	77	77					
Initial		76.885	27.189	78	77	77					
Difference	6 2.00	6.121	6.021	79	77	77	77	7	24	1.006	1.798

Average **0.994** **1.775**

Stack Temperature Sensor Calibration

Meter Box # : CM53 Name : DV

Ambient Temperature : 80.1 °F Date : September 6, 2023

Calibrator Model # : CL940A

Serial # : 526

Date Of Certification : December 28, 2022

Primary Standards Directly Traceable National Institute of Standards and Technology
 108.5 58.76
 103.4 53.667

Reference Source Temperature (°F)	Test Thermometer Temperature (°F)	Temperature Difference %
0	1	0.2
250	252	0.3
600	601	0.1
1200	1205	0.3

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM53
 Standard Meter No. 18654530
 Standard Meter (Y) 0.99730

Date: October 26, 2023
 Calibrated By: ER
 Barometric Pressure: 28.05

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		10.800	37.210	71	71	71					
Initial		5.798	32.147	71	71	71					
Difference	1 0.20	5.002	5.063	71	71	71	71	18	35	0.985	1.674
Final		15.810	42.298	73	73	73					
Initial		10.800	37.210	71	71	71					
Difference	2 0.50	5.010	5.088	72	72	72	72	12	10	0.981	1.791
Final		20.871	47.430	72	73	73					
Initial		15.810	42.298	73	73	72					
Difference	3 0.70	5.061	5.132	73	73	73	73	10	19	0.982	1.768
Final		25.915	52.558	72	73	73					
Initial		20.871	47.430	72	73	73					
Difference	4 0.90	5.044	5.128	72	73	73	73	9	0	0.980	1.737
Final		30.935	57.662	72	74	74					
Initial		25.915	52.558	72	73	73					
Difference	5 1.20	5.020	5.104	72	74	74	74	8	15	0.981	1.963
Final		5.798	32.147	71	71	71					
Initial		0.792	27.133	71	71	71					
Difference	6 2.00	5.006	5.014	71	71	71	71	6	20	0.991	1.941

Average **0.983** **1.812**

Stack Temperature Sensor Calibration			
Temperature ID :	100769	Name :	ER
Ambient Temperature, °F :	72.2	Date :	10/25/2023

Temperature Calibrator			
Model # :	CL23A	Certification Date:	May 1,2023
Serial # :	T-285668	Expiration Date:	May 2,2024

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

Reference Source Temperature (° F)	Test Thermometer Temperature (° F)	Temperature Difference %
0	0	0.0
250	251	0.1
600	601	0.1
1200	1205	0.3

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-A
 Probe Calibration Date: 07/10/17
 Test Point Location: center
 Ambient Temperature (°F): 77.8
 Barometric Pressure ("Hg): 29.23

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	77.8	1.18	0	0.82
2	60	0.80	77.8	1.18	0	0.82
3	60	0.81	77.8	1.18	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.81	77.8	2.63	0	0.82
2	90	1.81	77.8	2.62	0	0.82
3	90	1.81	77.8	2.63	0	0.82
Average (C _{p(avg-high)})						0.82

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.49\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.820



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-B
 Probe Calibration Date: 07/10/17
 Test Point Location: center
 Ambient Temperature (°F): 77.5
 Barometric Pressure ("Hg): 29.23

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	77.5	1.19	0	0.82
2	60	0.81	77.5	1.19	0	0.82
3	60	0.81	77.5	1.19	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.81	77.5	2.65	0	0.82
2	90	1.81	77.5	2.64	0	0.82
3	90	1.81	77.5	2.64	0	0.82
Average (C _{p(avg-high)})						0.82

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.55\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.818



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 6/8/2017
 Temperature (°F): 72.2
 Pressure ("Hg): 29.33
 Personnel: wgj
 Probe: S8-031-A

Wind Tunnel Target DP [I.W.C]	Wind Tunnel Actual DP [I.W.C]	S-Probe DP [I.W.C.]	C_p	$C_{p(avg)}$	$C_p - C_{p(avg)}$	σ_{max}	
0.81	0.81	1.19	0.818	0.818	0.000	0.001	Pass
0.81	0.81	1.19	0.818		0.000		
0.81	0.81	1.19	0.817		-0.001		
1.81	1.82	2.63	0.823	0.822	0.001	0.001	Pass
1.81	1.82	2.64	0.822		0.000		
1.81	1.81	2.64	0.820		-0.001		



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 6/8/2017
 Temperature (°F): 72.0
 Pressure ("Hg): 29.33
 Personnel: wgj
 Probe: S8-031-B

Wind Tunnel Target DP [I.W.C]	Wind Tunnel Actual DP [I.W.C]	S-Probe DP [I.W.C.]	C_p	$C_{p(avg)}$	$C_p - C_{p(avg)}$	σ_{max}	
0.81	0.81	1.19	0.817	0.816	0.000	0.001	Pass
0.81	0.81	1.19	0.817		0.000		
0.81	0.81	1.19	0.816		-0.001		
1.81	1.82	2.65	0.820	0.820	0.000	0.000	Pass
1.81	1.82	2.65	0.820		0.000		
1.81	1.82	2.64	0.820		0.000		



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-A
 Probe Calibration Date: 06/08/17
 Test Point Location: center
 Ambient Temperature (°F): 72.2
 Barometric Pressure ("Hg): 29.33

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	72.2	1.19	0	0.82
2	60	0.81	72.2	1.19	0	0.82
3	60	0.81	72.2	1.19	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.82	72.2	2.63	0	0.82
2	90	1.82	72.2	2.64	0	0.82
3	90	1.81	72.2	2.64	0	0.82
Average (C _{p(avg-high)})						0.82

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.51\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3%.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.820



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-B
 Probe Calibration Date: 06/08/17
 Test Point Location: center
 Ambient Temperature (°F): 72.0
 Barometric Pressure ("Hg): 29.33

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	72.0	1.19	0	0.82
2	60	0.81	72.0	1.19	0	0.82
3	60	0.81	72.0	1.19	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.82	72.0	2.65	0	0.82
2	90	1.82	72.0	2.65	0	0.82
3	90	1.82	72.0	2.64	0	0.82
Average (C _{p(avg-high)})						0.82

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.45\%}} \quad \text{Pass}$$

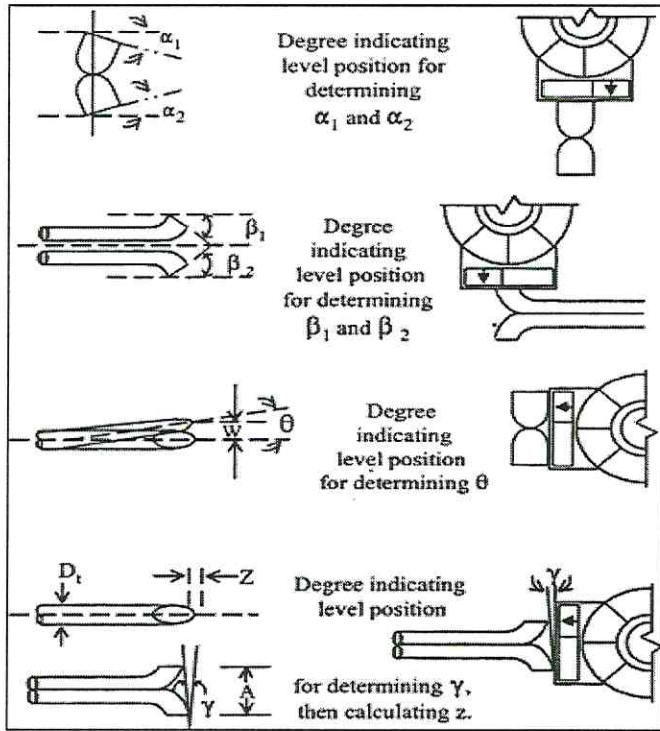
Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.818

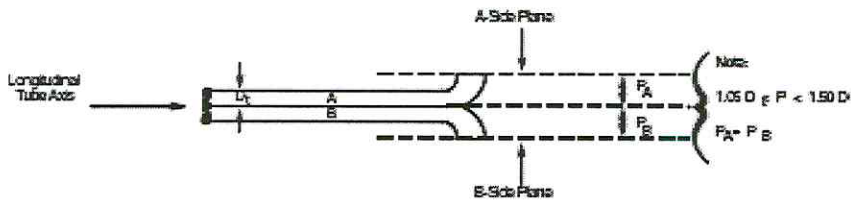


Airflow Sciences Corporation

Probe Inspection for Method 2



α_1	0.8 (°)	Pass
α_2	0.3 (°)	Pass
β_1	0.3 (°)	Pass
β_2	1.1 (°)	Pass
D_t	0.375 (")	Pass
P_a	0.459 (")	Pass
P_b	0.459 (")	Pass
z	<0.02 (")	Pass
w	0.005 (")	Pass



Certification

I certify that Type S probe ID **S8-031** meets or exceeds all specifications, criteria, and applicable design features.

Certified by: Craig Rood

Date: 6/8/2017



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 8/31/2017
Temperature (°F): 73.7
Pressure ("Hg): 29.43
Personnel: wgj
Probe: S8-032-A

Wind Tunnel Target DP [I.W.C.]	Wind Tunnel Actual DP [I.W.C.]	S-Probe DP [I.W.C.]	C _p	C _{p(avg)}	C _p -C _{p(avg)}	σ _{max}	
0.81	0.81	1.18	0.820	0.821	0.000	0.000	Pass
0.81	0.81	1.18	0.821		0.000		
0.81	0.81	1.18	0.821		0.000		
1.81	1.82	2.62	0.825	0.824	0.000	0.000	Pass
1.81	1.82	2.63	0.824		0.000		
1.81	1.82	2.63	0.824		0.000		



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 8/31/2017
Temperature (°F): 74.5
Pressure ("Hg): 29.43
Personnel: wgj
Probe: S8-032-B

Wind Tunnel Target DP [I.W.C.]	Wind Tunnel Actual DP [I.W.C.]	S-Probe DP [I.W.C.]	C_p	$C_{p(avg)}$	$C_p - C_{p(avg)}$	σ_{max}	
0.81	0.81	1.19	0.819	0.819	0.000	0.000	Pass
0.81	0.81	1.19	0.819		0.000		
0.81	0.81	1.19	0.820		0.000		
1.81	1.81	2.63	0.823	0.823	0.000	0.000	Pass
1.81	1.82	2.63	0.823		0.000		
1.81	1.82	2.63	0.823		0.000		

Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
Wind Tunnel Location: Livonia, MI
Probe Type: S-Type Pitot
Probe ID: S8-032-A
Probe Calibration Date: 08/31/17
Test Point Location: center
Ambient Temperature (°F): 73.7
Barometric Pressure ("Hg): 29.43

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	73.7	1.18	0	0.82
2	60	0.81	73.7	1.18	0	0.82
3	60	0.81	73.7	1.18	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.82	73.7	2.62	0	0.82
2	90	1.82	73.7	2.63	0	0.82
3	90	1.82	73.7	2.63	0	0.82
Average (C _{p(avg-high)})						0.82

$$\text{\% Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.46\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.822



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
Wind Tunnel Location: Livonia, MI
Probe Type: S-Type Pitot
Probe ID: S8-032-B
Probe Calibration Date: 08/31/17
Test Point Location: center
Ambient Temperature (°F): 74.5
Barometric Pressure ("Hg): 29.43

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	74.5	1.19	0	0.82
2	60	0.81	74.5	1.19	0	0.82
3	60	0.81	74.5	1.19	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.81	74.5	2.63	0	0.82
2	90	1.82	74.5	2.63	0	0.82
3	90	1.82	74.5	2.63	0	0.82
Average (C _{p(avg-high)})						0.82

$$\text{\% Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.43\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.821

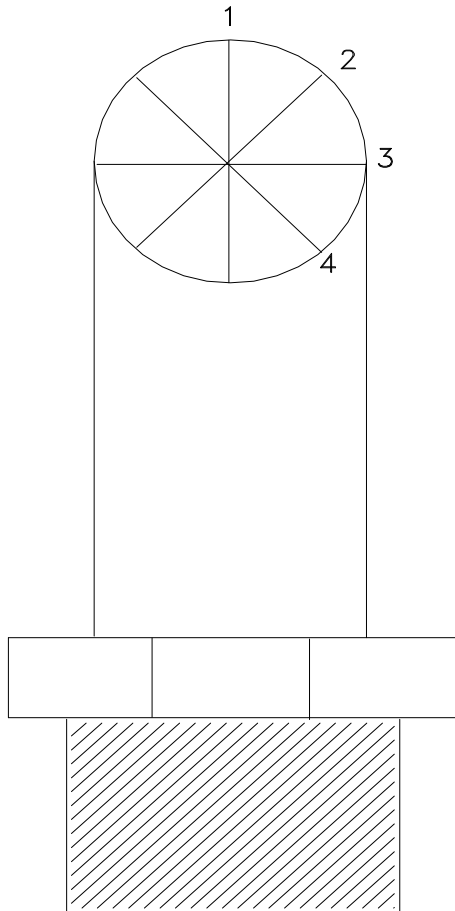
Nozzle Calibration

Date: 4/25/2023

Nozzle ID No.: 909

Analyst: WAP

Material/Type: Glass



0.282	1
0.282	2
0.281	3
0.281	4

Valid Data

Average
<u>0.282</u>

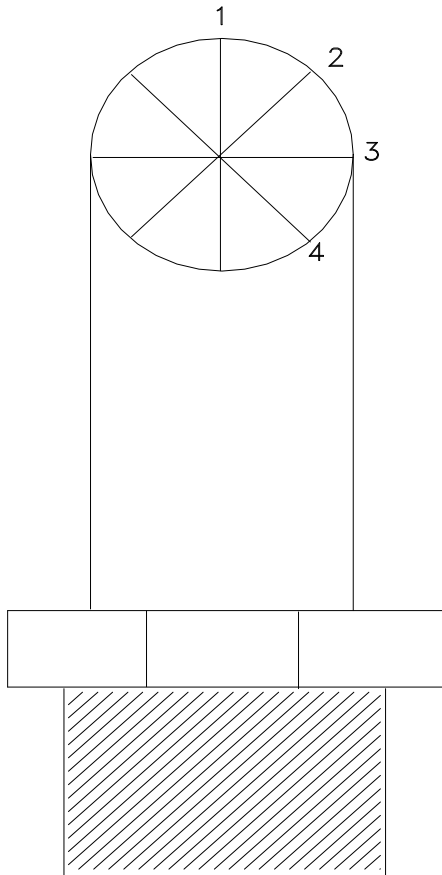
Nozzle Calibration

Date: 4/25/2023

Nozzle ID No.: 267

Analyst: WAP

Material/Type: Glass



<u>0.287</u>	1
<u>0.287</u>	2
<u>0.287</u>	3
<u>0.287</u>	4



Average
<u>0.287</u>

Client: GCC Rio Grande, Inc.
 Facility: Tijeras Plant
 Project #: M234302
 Test Location: Main Stack
 Date: 10/24/2023
 Operator: R. Sollars
 Operating Condition Normal

Sample System: FTIR
 Probe Length: 8.0 ft
 Probe Type: FTIR
 Sample Plane: Vertical
 Port Length: 6.5 in.
 Port Size (diameter): 4 in.
 Port Type: Flange
 Duct Shape: Circular
 Diameter: 11 ft
 Duct Area: 95.03 Sq. Ft.
 Upstream Diameters: 3.30
 Downstream Diameters: 9.20
 Number of Ports Sampled: 1
 Number of Points per Port: 3
 Total Number of Traverse Points: 3

Minimum Upstream Distance: 5.5 Feet
 Minimum Downstream Distance: 22.0 Feet
 Ideal Upstream Distance: 22.0 Feet
 Ideal Downstream Distance: 88.0 Feet

Calibration Gases

Type	Setting	Cylinder ID	Cylinder Value	Analyzer Response	Difference, % of Span	Expiration Date	Mid cylinder % of high cylinder	Final Bottle Pressure, PSI
O2 % (dry)	Zero	Zero Nitrogen	0.0	0.02	-0.09%	N/A		1500
	Mid	CC326608	12.03	12.19	-0.71%	7/19/2031	53.68%	1500
	High	CC420519	22.41	22.35	0.27%	7/15/2029		1000

Type	Compound	Cylinder ID	Cylinder Value	Expiration Date	Final Bottle Pressure, PSI
Zero Gas	Nitrogen	Zero Nitrogen	0.0	N/A	1500
Calibration Transfer Standard	Ethylene	ALM007995	100.6	6/1/2026	1100
Analyte Spike Gas	HCN	CC768241	49.55	3/11/2024	1900
	SF6		5.001		

Response Time Data

Type	RM Analyzer Make/Model	RM Analyzer s/n	Analyzer Span	RM Gas Span
O2 % (dry)	CAI 700	221018	25	22.41
HF ppmvw	MKS 2030	110161896	10	N/A
HCN ppmvw	MKS 2030	110161896	100	N/A

Client: GCC Rio Grande, Inc.
Facility: Tijeras Plant
Test Location: Main Stack
Date: 10/24/23
Project #: M234302

<u>Time</u>	<u>O2 % (dry)</u>	
6:59	0.03	
7:00	0.02	iz
7:01	3.25	
7:02	0.06	
7:03	0.01	
7:04	0.37	
7:05	6.11	
7:06	17.44	
7:07	22.33	
7:08	22.35	ih
7:09	20.56	
7:10	13.85	
7:11	12.18	
7:12	12.19	im
7:13	18.28	
7:14	21.11	
7:15	20.86	
7:16	20.99	
7:17	2.52	
7:18	0.10	
7:19	0.09	z
7:20	10.55	
7:21	12.19	
7:22	12.20	m

Client: GCC Rio Grande, Inc.
Facility: Tijeras Plant
Project #: M234302
Test Location: Main Stack
Date: 10/24/23

Post 1/Pre 2			Post 2/Pre 3		
<u>Time</u>	<u>O2 % (dry)</u>		<u>Time</u>	<u>O2 % (dry)</u>	
9:43	0.11		11:41	14.87	
9:44	6.80		11:42	0.17	
9:45	12.06		11:43	0.10	
9:46	12.08	m	11:44	11.52	
9:47	11.01		11:45	12.06	
9:48	0.11		11:46	12.07	m
9:49	0.08		11:47	7.45	
9:50	0.08		11:48	0.11	
9:51	0.07	z	11:49	0.09	
			11:50	0.08	z

Post 3		
<u>Time</u>	<u>O2 % (dry)</u>	
13:44	16.41	
13:45	3.88	
13:46	0.12	
13:47	5.80	
13:48	12.06	
13:49	12.07	
13:50	12.08	m
13:51	12.08	
13:52	4.85	
13:53	0.10	
13:54	0.09	z

Client: GCC Rio Grande, Inc.
 Facility: Tijeras Plant
 Project #: M234302
 Diluent: O2 %

Test Location: Main Stack
 Date: 10/24/23
 Operator: R. Sollars
 O2 % Correction: 7

O2 % (dry) Correction Data

Run #	Cma	Precal	Postcal	Pre zero	Post zero	Co	Cm	C	Cgas	Span Bias	Span Drift	Zero Bias	Zero Drift
1	12.03	12.20	12.08	0.09	0.07	0.08	12.14	16.25	16.1	0.49	-0.54	-0.22	-0.09
2	12.03	12.08	12.07	0.07	0.08	0.08	12.08	16.24	16.2	0.54	-0.04	-0.27	0.04
3	12.03	12.07	12.08	0.08	0.09	0.09	12.08	16.22	16.2	0.49	0.04	-0.31	0.04

Concentration of Cal Gas C = Average value of test Co=Average Pre and Post Zero
 Average Pre and Post Span Cgas = Corrected gas value of test

Calibration Corrected and Calculated Data

Run #	Run Date	Start Time	End Time	Moisture %	O2 % (dry)	CO2 % (wet)	CO2 % (dry)	HCN ppmvw	HCN ppmvd @ 7% O2	HF ppmvw	HF ppmvd @ 7% O2
1	10/24/23	8:00	8:59	2.86%	16.13	6.06	6.24	2.03	6.07	0.10	0.30
2	10/24/23	10:00	10:59	2.68%	16.21	6.15	6.32	1.82	5.55	0.10	0.30
3	10/24/23	12:00	12:59	2.73%	16.19	6.30	6.48	1.89	5.74	0.10	0.30

Appendix H - FTIR QA/QC

Method 320 FTIR Detector Multi-Gas Determination QA/QC

FTIR data was collected using an MKS MultiGas 2030 FTIR spectrometer.

The FTIR was equipped with a temperature-controlled, 5.11 meter multi-pass gas cell maintained at 191°C. Gas flows and sampling system pressures were monitored using a rotameter and pressure transducer. All data was collected at 0.5 cm⁻¹ resolution. Each spectrum was derived from the coaddition of 64 scans, with a new data point generated approximately every one minute. Analyzer data for each run is presented in the Reference Method Test Data appendix.

SAMPLING SYSTEM PARAMETERS				
MKS Serial #	Sampling Line	Probe Assembly	Particulate Filter Media	Operating Temperatures
110161896	100' 3/8" dia., heated Teflon	Heated 12', 3/8" dia. SS	0.01µ heated borosilicate glass fiber	191°C

QA/QC procedures followed US EPA Method 320 guidelines. See below for QA/QC procedure details and list of calibration gas standards. All calibration gases were introduced to the analyzer and the sampling system using an instrument grade stainless steel rotameter. All QA/QC procedures were within the acceptance criteria allowance of the applicable EPA methodology. Detailed FTIR QA/QC data follow the narrative portion of this appendix.

FTIR QA/QC Procedures						
QA/QC Specification	Purpose	Calibration Gas Analyte	Delivery	Frequency	Acceptance Criteria	Result
M320: Zero	Verify that the FTIR is free of contaminants & zero the FTIR	Nitrogen (zero)	Direct to FTIR	pre/post test	< MDL or Noise	Pass
M320: Calibration Transfer Standard (CTS) Direct	Verify FTIR stability, confirm optical path length	Ethylene	Direct to FTIR	pretest	+/- 5% cert. value	Pass
M320: Analyte Direct	Verify FTIR calibration	HCN, SF ₆	Direct to FTIR	Pretest	+/- 5% cert. value	Pass
M320: CTS Response	Verify system stability, recovery, response time	Ethylene	Sampling System	Daily, pre/post test	+/- 5% of Direct Measurement	Pass
M320: Zero Response	Verify system is free of contaminants, system bias	Nitrogen (zero)	Sampling System	pretest	Bias correct data	Pass
M320: Analyte Spike	Verify system ability to deliver and quantify analyte of interest in the presence of other effluent gases	HCN, SF ₆	Dynamic Addition to Sampling System, 1:10 effluent	Throughout testing – daily	+/- 20% theoretical recovery	Pass

Note: The determined concentrations from direct analyses were used in all system/spike recovery calculations.

CALIBRATION GAS STANDARDS				
Components	Concentration (ppm)	Vendor	Cylinder #	Standard Type
Ethylene	100.6	Airgas	ALM007995	Primary +/- 1%
HCN/SF ₆	49.55/5.001	Airgas	CC768241	Certified Standard-Spec +/- 5%
Nitrogen	Zero Gas	Airgas	Zero Nitrogen	UHP Grade

Analyte Spiking

HCN spiking was performed prior to testing to verify the ability of the sampling system to quantitatively deliver a sample containing HCN from the base of the probe to the FTIR. Analyte spiking assures the ability of the FTIR sampling system to recover acid gases in the presence of effluent gas.

As part of the spiking procedure, samples were measured to determine native HCN concentrations to be used in the spike recovery calculations. The analyte spiking gases contained a low concentration of sulfur hexafluoride (SF₆). The determined SF₆ concentration in the spiked sample was used to calculate the dilution factor of the spike and thus used to calculate the concentration of the spiked HCN. The spike target dilution ratio was 1:10 or less.

The following equation illustrates the percent recovery calculation.

$$DF = \frac{SF_6(spik)}{SF_6(direct)} \quad (\text{Sec. 9.2.3 (3) USEPA Method 320})$$

$$CS = DF * Spike(dir) + Unspike(1 - DF) \quad (\text{Sec. 9.2.3 (4) USEPA Method 320})$$

DF = Dilution factor of the spike gas

SF_{6(dir)} = SF₆ concentration measured directly in undiluted spike gas

SF_{6(spik)} = Diluted SF₆ concentration measured in a spiked sample

Spike_{dir} = Concentration of the analyte in the spike standard measure by the FTIR directly

CS = Expected concentration of the spiked samples

Unspike = Native concentration of analytes in unspiked samples

Post Collection Data Validation

As part of the data validation procedure, reference spectra are manually fit to that of the sample spectra and a concentration is determined. The reference spectra are scaled to match the peak amplitude of the sample, thus providing a scale factor. The scale factor multiplied by the reference spectra concentration is used to determine the concentration value for the sample spectra. Sample pressure and temperature corrections are then applied to compute the final sample concentration. The manually calculated results are then compared with the software-generated results. The data is then validated if the two concentrations are within ± 20% agreement. If there is a difference greater than ± 20% the spectra are reviewed for possible spectra interferences or any other possible causes leading to incorrectly quantified data.

Detection Limit

The detection limit of each analyte was calculated following Annex A2 of ASTM D6348-12 procedure using spectra that contained similar amounts of moisture.

FTIR DETECTION LIMITS			
Analyte	Detection Limit (ppmv wet)	Detection Limit (%v)	Detection Limit (%v wet)
Hydrogen Cyanide	0.2	—	—
Hydrogen Fluoride	0.1		
Water	—	0.1	N/A
Carbon Dioxide	—	N/A	0.1

Copies of gas cylinder certifications are appended. All concentration data were recorded on a wet, volume basis. HCN spiking was performed prior to testing to confirm the measurement system's ability to deliver and quantify HCN. The sample and data collection followed the procedures outlined in Methods 320.

Client: GCC Rio Grande, Inc.
 Facility: Tijeras Plant
 Project #: M234302
 Operating Condition: Normal

Test Location: Main Stack
 Date: 10/24/2023
 Operator: R. Sollars
 FTIR s/n: 110161896

System Leak Check: 0.0 mL/min

Nitrogen (Zero) Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
N2_DIR_000002.LAB	10/24/23	6:49:57	0.0	0.0	0.0	190.5	0.80	0.4	0.1	0.002
N2_DIR_000003BKGLAB	10/24/23	6:52:09	0.0	0.0	0.0	190.4	0.80	0.0	0.0	0.000
N2_DIR_000004.LAB	10/24/23	6:52:23	0.0	0.0	0.0	190.3	0.80	0.1	-0.1	-0.006
N2_DIR_000005.LAB	10/24/23	6:52:31	0.0	0.0	0.0	190.3	0.80	0.3	-0.1	-0.001
N2_DIR_000006.LAB	10/24/23	6:52:39	0.0	0.0	0.0	190.3	0.80	0.1	0.1	-0.015
N2_DIR_000007.LAB	10/24/23	6:52:47	0.0	0.0	0.0	190.3	0.80	0.2	0.0	-0.012
N2_DIR_000008.LAB	10/24/23	6:52:55	0.0	0.0	0.0	190.3	0.80	0.2	-0.1	-0.014
N2_DIR_000009.LAB	10/24/23	6:53:02	0.0	0.0	0.0	190.3	0.80	0.3	-0.1	0.008
N2_DIR_000010.LAB	10/24/23	6:53:10	0.0	0.0	0.0	190.3	0.80	0.2	0.0	0.010

Calibration Transfer Standard (CTS), Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
CTS_DIR_000026.LAB	10/24/23	6:56:20	0.0	0.0	0.0	190.5	0.80	100.6	-0.1	-0.025	100.0%
CTS_DIR_000027.LAB	10/24/23	6:56:28	0.0	0.0	0.0	190.5	0.80	100.5	0.0	-0.030	99.9%
CTS_DIR_000028.LAB	10/24/23	6:56:36	0.0	0.0	0.0	190.5	0.80	100.7	-0.1	-0.031	100.1%
CTS_DIR_000029.LAB	10/24/23	6:56:44	0.0	0.0	0.0	190.5	0.80	100.6	-0.1	-0.031	100.0%
CTS_DIR_000030.LAB	10/24/23	6:56:52	0.0	0.0	0.0	190.6	0.80	100.5	-0.1	-0.025	99.9%
CTS_DIR_000031.LAB	10/24/23	6:57:00	0.0	0.0	-0.1	190.6	0.80	100.7	-0.1	-0.030	100.1%
CTS_DIR_000032.LAB	10/24/23	6:57:08	0.0	0.0	0.0	190.6	0.80	100.6	-0.2	-0.027	100.0%
CTS_DIR_000033.LAB	10/24/23	6:57:15	0.0	0.0	0.0	190.6	0.80	100.5	-0.1	-0.028	99.9%
Average								100.6			100.0%

Analyte Spike Gas (HCN) Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % HCN
HCN_DIR_000043.LAB	10/24/23	7:00:16	0.0	0.0	0.0	190.5	0.80	-0.2	47.9	5.062	96.7%
HCN_DIR_000044.LAB	10/24/23	7:00:24	0.0	0.0	0.0	190.4	0.80	0.1	48.0	5.089	96.9%
HCN_DIR_000045.LAB	10/24/23	7:00:32	0.0	0.0	0.0	190.4	0.80	0.0	48.0	5.109	97.0%
HCN_DIR_000046.LAB	10/24/23	7:00:40	0.0	0.0	0.0	190.4	0.80	-0.2	48.0	5.111	96.9%
HCN_DIR_000047.LAB	10/24/23	7:00:48	0.0	0.0	0.0	190.3	0.80	0.0	47.9	5.107	96.7%
HCN_DIR_000048.LAB	10/24/23	7:00:56	0.0	0.0	0.0	190.3	0.80	-0.1	48.0	5.105	96.9%
HCN_DIR_000049.LAB	10/24/23	7:01:04	0.0	0.0	0.0	190.4	0.80	0.2	48.1	5.110	97.1%
HCN_DIR_000050.LAB	10/24/23	7:01:11	0.0	0.0	0.0	190.3	0.80	0.1	48.2	5.112	97.3%
Average								48.0	5.101	96.9%	

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
CTS_RT_000093.LAB	10/24/23	7:18:32	0.0	0.0	0.0	190.8	0.80	100.9	0.0	-0.034	100.3%
CTS_RT_000094.LAB	10/24/23	7:18:39	0.0	0.0	0.0	190.8	0.80	101.0	0.0	-0.035	100.4%
CTS_RT_000095.LAB	10/24/23	7:18:48	0.0	0.0	0.0	190.8	0.80	101.0	0.0	-0.032	100.4%
CTS_RT_000096.LAB	10/24/23	7:18:55	0.0	0.0	0.0	190.8	0.80	100.9	0.0	-0.035	100.3%
CTS_RT_000097.LAB	10/24/23	7:19:03	0.0	0.0	0.0	190.7	0.80	101.3	0.0	-0.033	100.7%
CTS_RT_000098.LAB	10/24/23	7:19:11	0.0	0.0	0.0	190.7	0.80	101.2	-0.1	-0.021	100.6%
CTS_RT_000099.LAB	10/24/23	7:19:19	0.0	0.0	0.0	190.7	0.80	100.8	-0.1	-0.031	100.2%
CTS_RT_000100.LAB	10/24/23	7:19:27	0.0	0.0	0.0	190.7	0.80	101.2	0.0	-0.035	100.5%

Response Time Test

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Response Time (sec)
CTS_RT_000080.LAB	10/24/23	7:16:49	1.1	0.0	0.0	190.7	0.80	0.0	-0.1	-0.006	-
CTS_RT_000081.LAB	10/24/23	7:16:57	0.6	0.4	0.0	190.7	0.80	52.8	-0.1	-0.032	15.892
CTS_RT_000082.LAB	10/24/23	7:17:05	0.1	0.0	0.0	190.7	0.80	100.1	-0.2	-0.024	23.892
CTS_RT_000083.LAB	10/24/23	7:17:13	0.1	0.0	0.0	190.7	0.80	100.6	-0.2	-0.037	
CTS_RT_000084.LAB	10/24/23	7:17:21	0.0	0.0	0.0	190.7	0.80	100.7	-0.1	-0.035	
CTS_RT_000085.LAB	10/24/23	7:17:29	0.0	0.0	0.0	190.8	0.80	100.8	0.1	-0.014	
CTS_RT_000086.LAB	10/24/23	7:17:37	0.0	0.0	0.0	190.8	0.80	100.9	-0.1	-0.025	
CTS_RT_000087.LAB	10/24/23	7:17:44	0.0	0.0	0.0	190.8	0.80	101.1	-0.1	-0.025	
CTS_RT_000088.LAB	10/24/23	7:17:52	0.0	0.0	0.0	190.8	0.80	101.1	-0.1	-0.030	

Client: GCC Rio Grande, Inc.
 Facility: Tijeras Plant
 Project #: M234302
 Operating Condition: Normal

Test Location: Main Stack
 Date: 10/24/2023
 Operator: R. Sollars
 FTIR s/n: 110161896

Pre 1 Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
AMBIENT_STACK_000169.LAB	10/24/23	7:31:50	6.8	5.7	-0.1	190.8	0.80	0.6	2.1	-0.017
AMBIENT_STACK_000170.LAB	10/24/23	7:31:58	6.6	5.8	-0.1	190.8	0.80	0.8	2.1	-0.001
AMBIENT_STACK_000171.LAB	10/24/23	7:32:06	6.6	5.7	-0.1	190.8	0.80	0.7	1.9	-0.004
									2.0	-0.007

Pre 1 Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
PRE1_SPK_000179.LAB	10/24/23	7:34:56	4.8	5.0	-0.1	190.6	0.80	0.3	6.1	0.424	0.083	103.4%
PRE1_SPK_000180.LAB	10/24/23	7:35:04	4.7	5.1	-0.1	190.6	0.80	0.5	5.9	0.429	0.084	100.1%
PRE1_SPK_000181.LAB	10/24/23	7:35:12	4.6	5.1	-0.1	190.7	0.80	0.6	6.1	0.424	0.083	104.0%
PRE1_SPK_000182.LAB	10/24/23	7:35:19	4.6	5.1	-0.1	190.6	0.80	0.6	6.1	0.423	0.083	104.7%
PRE1_SPK_000183.LAB	10/24/23	7:35:27	4.6	5.1	-0.1	190.7	0.80	0.5	6.0	0.430	0.084	101.8%
PRE1_SPK_000184.LAB	10/24/23	7:35:35	4.6	5.1	-0.1	190.7	0.80	0.7	5.8	0.439	0.086	97.3%
PRE1_SPK_000185.LAB	10/24/23	7:35:43	4.5	5.1	-0.1	190.7	0.80	0.5	5.9	0.433	0.085	99.8%
PRE1_SPK_000186.LAB	10/24/23	7:35:51	4.5	5.1	-0.1	190.7	0.80	0.6	5.8	0.429	0.084	98.7%

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN1_000333.LAB	10/24/23	9:27:43	2.8	6.3	-0.1	190.7	0.80	0.7	1.9	-0.004
RUN1_000334.LAB	10/24/23	9:28:45	2.8	6.4	-0.1	190.9	0.80	0.7	2.0	-0.005
RUN1_000335.LAB	10/24/23	9:29:48	2.9	6.4	-0.1	190.9	0.80	0.7	2.3	-0.005
									2.1	-0.005

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST1_SPK_000340.LAB	10/24/23	9:32:36	2.5	5.6	0.0	190.8	0.80	0.5	5.5	0.374	0.073	101.2%
POST1_SPK_000341.LAB	10/24/23	9:32:44	2.6	5.7	-0.1	190.8	0.80	0.6	5.6	0.371	0.073	103.2%
POST1_SPK_000342.LAB	10/24/23	9:32:52	2.6	5.8	-0.1	190.8	0.80	0.5	5.6	0.367	0.072	104.0%
POST1_SPK_000343.LAB	10/24/23	9:33:00	2.6	5.8	-0.1	190.8	0.80	0.6	5.7	0.373	0.073	104.8%
POST1_SPK_000344.LAB	10/24/23	9:33:08	2.6	5.8	-0.1	190.8	0.80	0.6	5.7	0.367	0.072	105.5%
POST1_SPK_000345.LAB	10/24/23	9:33:15	2.6	5.8	-0.1	190.8	0.80	0.6	5.5	0.366	0.072	102.8%
POST1_SPK_000346.LAB	10/24/23	9:33:23	2.6	5.8	0.0	190.8	0.80	0.6	5.7	0.365	0.072	107.5%
POST1_SPK_000347.LAB	10/24/23	9:33:32	2.6	5.8	-0.1	190.8	0.80	0.6	5.6	0.381	0.075	102.7%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST1_CTS_000393.LAB	10/24/23	9:42:54	0.0	0.0	0.0	190.7	0.80	100.8	0.0	-0.023	100.2%
POST1_CTS_000394.LAB	10/24/23	9:43:01	0.0	0.0	0.0	190.7	0.80	100.8	0.0	-0.031	100.2%
POST1_CTS_000395.LAB	10/24/23	9:43:09	0.0	0.0	0.0	190.7	0.80	100.4	0.0	-0.018	99.8%
POST1_CTS_000396.LAB	10/24/23	9:43:17	0.0	0.0	0.0	190.7	0.80	100.5	-0.1	-0.028	99.9%
POST1_CTS_000397.LAB	10/24/23	9:43:25	0.0	0.0	0.1	190.7	0.80	100.6	0.1	-0.027	100.0%
POST1_CTS_000398.LAB	10/24/23	9:43:33	0.0	0.0	0.0	190.7	0.80	100.7	0.0	-0.019	100.1%
POST1_CTS_000399.LAB	10/24/23	9:43:40	0.0	0.0	0.0	190.6	0.80	100.9	0.1	-0.030	100.3%
POST1_CTS_000400.LAB	10/24/23	9:43:48	0.0	0.0	0.0	190.6	0.80	101.3	-0.1	-0.025	100.7%

Client: GCC Rio Grande, Inc.
 Facility: Tijeras Plant
 Project #: M234302
 Operating Condition: Normal

Test Location: Main Stack
 Date: 10/24/2023
 Operator: R. Sollars
 FTIR s/n: 110161896

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN2_000523.LAB	10/24/23	11:28:27	2.8	6.2	-0.1	190.7	0.80	0.6	1.8	0.000
RUN2_000524.LAB	10/24/23	11:29:30	2.8	6.2	-0.1	190.8	0.80	0.6	1.7	0.001
RUN2_000525.LAB	10/24/23	11:30:33	2.8	6.2	-0.1	190.7	0.80	0.7	1.8	0.000
									1.8	0.000

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST2_SPK_000537.LAB	10/24/23	11:33:45	2.5	5.5	0.0	190.6	0.80	0.7	4.7	0.321	0.063	99.4%
POST2_SPK_000538.LAB	10/24/23	11:33:53	2.5	5.4	-0.1	190.7	0.80	0.5	4.9	0.330	0.065	101.5%
POST2_SPK_000539.LAB	10/24/23	11:34:00	2.5	5.4	-0.1	190.6	0.80	0.6	4.4	0.323	0.063	94.1%
POST2_SPK_000540.LAB	10/24/23	11:34:08	2.5	5.6	-0.1	190.5	0.80	0.3	4.9	0.323	0.063	103.6%
POST2_SPK_000541.LAB	10/24/23	11:34:16	2.5	5.6	-0.1	190.6	0.80	0.5	5.1	0.325	0.064	107.1%
POST2_SPK_000542.LAB	10/24/23	11:34:24	2.5	5.5	-0.1	190.5	0.80	0.6	5.0	0.334	0.065	102.6%
POST2_SPK_000543.LAB	10/24/23	11:34:32	2.5	5.4	-0.1	190.6	0.80	0.7	5.0	0.328	0.064	105.5%
POST2_SPK_000544.LAB	10/24/23	11:34:40	2.5	5.4	-0.1	190.5	0.80	0.5	4.7	0.324	0.064	99.9%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST2_CTS_000582.LAB	10/24/23	11:42:27	0.0	0.0	0.0	190.6	0.80	100.5	-0.1	-0.032	99.9%
POST2_CTS_000583.LAB	10/24/23	11:42:35	0.0	0.0	0.1	190.7	0.80	100.6	0.0	-0.015	100.0%
POST2_CTS_000584.LAB	10/24/23	11:42:43	0.0	0.0	0.0	190.5	0.80	100.8	0.0	-0.028	100.2%
POST2_CTS_000585.LAB	10/24/23	11:42:50	0.0	0.0	0.0	190.6	0.80	100.6	0.1	-0.041	100.0%
POST2_CTS_000586.LAB	10/24/23	11:42:59	0.0	0.0	0.0	190.6	0.80	100.8	0.1	-0.031	100.2%
POST2_CTS_000587.LAB	10/24/23	11:43:06	0.0	0.0	0.0	190.5	0.80	100.5	0.1	-0.025	99.9%
POST2_CTS_000588.LAB	10/24/23	11:43:14	0.0	0.0	0.1	190.5	0.80	100.5	0.2	-0.027	99.9%
POST2_CTS_000589.LAB	10/24/23	11:43:22	0.0	0.0	0.1	190.5	0.80	100.5	-0.1	-0.028	99.9%

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN3_000707.LAB	10/24/23	13:27:37	2.6	5.5	-0.1	190.7	0.80	0.6	1.7	0.001
RUN3_000708.LAB	10/24/23	13:28:40	2.7	5.6	-0.1	190.6	0.80	0.5	1.9	0.004
RUN3_000709.LAB	10/24/23	13:29:43	2.6	5.6	-0.1	190.7	0.80	0.5	1.8	0.000
									1.8	0.002

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST3_SOK_000741.LAB	10/24/23	13:35:31	2.4	4.9	-0.1	190.6	0.80	0.2	5.3	0.408	0.080	95.7%
POST3_SOK_000742.LAB	10/24/23	13:35:39	2.3	4.9	-0.1	190.7	0.80	0.4	5.3	0.412	0.081	96.5%
POST3_SOK_000743.LAB	10/24/23	13:35:47	2.4	4.8	0.0	190.7	0.80	0.2	5.4	0.408	0.080	98.3%
POST3_SOK_000744.LAB	10/24/23	13:35:55	2.4	4.9	0.0	190.7	0.80	0.7	5.1	0.409	0.080	92.3%
POST3_SOK_000745.LAB	10/24/23	13:36:03	2.4	4.9	0.0	190.7	0.80	0.4	5.4	0.404	0.079	98.8%
POST3_SOK_000746.LAB	10/24/23	13:36:11	2.4	5.0	-0.1	190.7	0.80	0.2	5.4	0.405	0.079	98.1%
POST3_SOK_000747.LAB	10/24/23	13:36:18	2.4	5.0	0.0	190.7	0.80	0.3	5.4	0.399	0.078	99.2%
POST3_SOK_000748.LAB	10/24/23	13:36:26	2.4	5.0	0.0	190.8	0.80	0.4	5.1	0.399	0.078	94.9%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST3_CTS_000778.LAB	10/24/23	13:45:49	0.0	0.0	0.0	190.7	0.80	100.3	0.0	-0.037	99.7%
POST3_CTS_000779.LAB	10/24/23	13:45:57	0.0	0.0	0.1	190.7	0.80	100.3	0.1	-0.016	99.7%
POST3_CTS_000780.LAB	10/24/23	13:46:05	0.0	0.0	0.0	190.7	0.80	100.2	0.0	-0.029	99.6%
POST3_CTS_000781.LAB	10/24/23	13:46:12	0.0	0.0	0.1	190.7	0.80	100.4	0.0	-0.034	99.8%
POST3_CTS_000782.LAB	10/24/23	13:46:20	0.0	0.0	0.0	190.7	0.80	100.6	0.2	-0.022	100.0%
POST3_CTS_000783.LAB	10/24/23	13:46:28	0.0	0.0	0.0	190.7	0.80	100.5	0.1	-0.024	99.9%
POST3_CTS_000784.LAB	10/24/23	13:46:36	0.0	0.0	0.1	190.7	0.80	100.6	0.2	-0.022	100.0%
POST3_CTS_000785.LAB	10/24/23	13:46:44	0.0	0.0	0.0	190.7	0.80	100.3	0.1	-0.025	99.7%

Client: GCC Rio Grande, Inc.
 Facility: Tijeras Plant
 Project #: M234302
 Operating Condition: Normal

Test Location: Main Stack
 Date: 10/24/2023
 Operator: R. Sollars
 FTIR s/n: 110161896

Post Test CTS, Direct Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
CTS_DIR_001020.LAB	10/24/23	17:07:22	0.0	0.0	0.0	190.7	0.80	100.5	-0.1	-0.033	99.9%
CTS_DIR_001021.LAB	10/24/23	17:07:30	0.0	0.0	0.0	190.7	0.80	100.6	0.0	-0.031	100.0%
CTS_DIR_001022.LAB	10/24/23	17:07:38	0.0	0.0	0.1	190.7	0.80	100.6	0.1	-0.027	100.0%
CTS_DIR_001023.LAB	10/24/23	17:07:46	0.0	0.0	0.0	190.7	0.80	100.5	0.1	-0.024	99.9%
CTS_DIR_001024.LAB	10/24/23	17:07:53	0.0	0.0	0.0	190.7	0.80	100.5	0.0	-0.023	99.9%
CTS_DIR_001025.LAB	10/24/23	17:08:01	0.0	0.0	0.0	190.7	0.80	100.4	0.0	-0.024	99.8%
CTS_DIR_001026.LAB	10/24/23	17:08:09	0.0	0.0	0.0	190.7	0.80	100.4	0.0	-0.021	99.8%
CTS_DIR_001027.LAB	10/24/23	17:08:17	0.0	0.0	0.0	190.8	0.80	100.4	0.1	-0.028	99.7%
Average								100.5			

Post Test N2, Direct Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
N2_DIR_001029.LAB	10/24/23	17:11:28	0.0	0.0	0.0	190.5	0.80	0.1	-0.2	0.005
N2_DIR_001030.LAB	10/24/23	17:13:33	0.0	0.0	0.0	190.5	0.80	0.1	-0.2	0.005
N2_DIR_001031.LAB	10/24/23	17:15:39	0.0	0.0	0.0	190.5	0.80	0.1	-0.1	0.004

Time	DL summary - zero gas		Time	DL summary - in stack	
	HF ppm (10) 191C	HCN (100) 191C		HF ppm (10) 191C	HCN (100) 191C
6:52:39 AM	-0.02	0.09	7:52:25 AM	-0.09	1.99
6:52:47 AM	-0.01	-0.02	7:53:28 AM	-0.08	1.95
6:52:55 AM	-0.01	-0.08	7:54:30 AM	-0.09	1.94
6:53:02 AM	0.00	-0.05	7:55:34 AM	-0.09	2.00
6:53:10 AM	-0.03	0.02	7:56:36 AM	-0.08	1.97
6:53:18 AM	-0.02	-0.16	7:57:39 AM	-0.09	1.98
6:53:26 AM	0.02	0.03	7:58:42 AM	-0.08	2.09
Standard Deviation	0.01	0.08	Standard Deviation	0.01	0.05
3x = DL	0.04	0.23	3x = DL	0.02	0.14

Appendix I - Gas Cylinder Certifications

CERTIFICATE OF ANALYSIS

Grade of Product: EPA PROTOCOL STANDARD

Part Number: E03NI78E15A1066	Reference Number: 153-402794083-1
Cylinder Number: CC326608	Cylinder Volume: 151.1 CF
Laboratory: 124 - Tooele (SAP) - UT	Cylinder Pressure: 2015 PSIG
PGVP Number: B72023	Valve Outlet: 590
Gas Code: CO2,O2,BALN	Certification Date: Jul 19, 2023

Expiration Date: Jul 19, 2031

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	10.00 %	9.893 %	G1	+/- 0.9% NIST Traceable	07/19/2023
OXYGEN	12.00 %	12.03 %	G1	+/- 0.8% NIST Traceable	07/19/2023
NITROGEN	Balance				

CALIBRATION STANDARDS

Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	13060405	CC411744	7.489 % CARBON DIOXIDE/NITROGEN	0.6%	May 14, 2025
NTRM	98051010	SG9161286BAL	12.05 % OXYGEN/NITROGEN	0.7%	Dec 14, 2023

ANALYTICAL EQUIPMENT

Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA-510 SV4MEUTJ CO2	CO2 NDIR (Dixon)	Jun 28, 2023
Horiba MPA-510 W603MM58 O2	O2 Paramagnetic (DIXON)	Jun 29, 2023

Triad Data Available Upon Request



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: EPA PROTOCOL STANDARD

Part Number: E03NI59E15A3452	Reference Number: 153-402157382-1
Cylinder Number: CC420519	Cylinder Volume: 159.0 CF
Laboratory: 124 - Tooele (SAP) - UT	Cylinder Pressure: 2015 PSIG
PGVP Number: B72021	Valve Outlet: 590
Gas Code: CO2,O2,BALN	Certification Date: Jul 15, 2021

Expiration Date: Jul 15, 2029

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	19.00 %	18.99 %	G1	+/- 0.6% NIST Traceable	07/15/2021
OXYGEN	22.00 %	22.41 %	G1	+/- 0.3% NIST Traceable	07/15/2021
NITROGEN	Balance				

CALIBRATION STANDARDS

Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	13060802	CC415397	24.04 % CARBON DIOXIDE/NITROGEN	0.6%	Dec 11, 2025
NTRM	12062008	CC367433	22.883 % OXYGEN/NITROGEN	0.2%	May 14, 2024

ANALYTICAL EQUIPMENT

Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA-510 SV4MEUTJ CO2	CO2 NDIR (Dixon)	Jun 17, 2021
Horiba MPA-510 W603MM58 O2	O2 Paramagnetic (Mason)	Jul 12, 2021

Triad Data Available Upon Request



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: CERTIFIED STANDARD-SPEC

Part Number:	X02NI99C15A1268	Reference Number:	153-402757278-1
Cylinder Number:	ALM007995	Cylinder Volume:	144.0 CF
Laboratory:	124 - Tooele (SAP) - UT	Cylinder Pressure:	2015 PSIG
Analysis Date:	Jun 01, 2023	Valve Outlet:	350
Lot Number:	153-402757278-1		

Expiration Date: Jun 01, 2026

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

Component	Req Conc	Actual Concentration (Mole %)	Analytical Uncertainty
ETHYLENE	100.0 PPM	100.6 PPM	+/- 2%
NITROGEN	Balance		



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: CERTIFIED STANDARD-SPEC

Customer:	MOSTARDI PLATT	Reference Number:	160-402841635-1
Part Number:	X03NI99C15AC0W8	Cylinder Volume:	144.4 CF
Cylinder Number:	CC768241	Cylinder Pressure:	2015 PSIG
Laboratory:	124 - Plumsteadville - PA	Valve Outlet:	350SS
Analysis Date:	Sep 11, 2023		
Lot Number:	160-402841635-1		

Expiration Date: Mar 11, 2024

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

Component	Req Conc	Actual Concentration (Mole %)	Analytical Uncertainty
SULFUR HEXAFLUORIDE	5.000 PPM	5.001 PPM	+/- 1.3%
HYDROGEN CYANIDE	50.00 PPM	49.55 PPM	+/- 5%
NITROGEN	Balance		



Signature on file

END OF THE REPORT