

Section 114 Information Collection Request Emissions Test Report

Ash Grove Cement Company
Durkee Cement Plant
EPA Registry ID: 110070834904
33060 Shirrtail Creek Road
Durkee, Oregon
Report No. M234105





**Section 114 Information Collection Request
Emissions Test Report**

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33060 Shirttail Creek Road
Durkee, Oregon**

**Report Submittal Date:
March 4, 2024**

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Report No. M234105

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1.0 INTRODUCTION

Mostardi Platt conducted an air emissions test program for Ash Grove Cement Company at the Durkee Cement Plant located in Durkee, Oregon. All testing was performed as described in the *Code of Federal Regulations*, Title 40, Part 60, Appendix A (40CFR60), Methods 1, 2, 3A, 4, 26A, and 40CFR63, Appendix A, (40CFR63) Method 320.

The Ash Grove Durkee Cement Plant includes a single Kiln (K1) ~1,000,000 TPY preheater/pre-calciner having an in-line raw mill. There are two calciners; an incline and a separate line calciner. The kiln system employs a SNCR for NO_x control and has a baghouse fabric filtration, and a separate polishing baghouse with activated carbon injection for mercury control.

This test program was completed to satisfy the requirements of the United States Environmental Protection Agency (USEPA) Section 114 Information Collection Request for Portland Cement Manufacturing facilities.

The identification of individuals associated with the test program is summarized below:

Location	Address	Contact
Facility Representative	Ash Grove Cement Company Durkee Cement Plant 33060 Shirttail Creek Road Durkee, OR 97905	Ms. Norma Job Environmental Manager 541-877-2640 norma.job@ashgrove.com
Testing Company Representative	Mostardi Platt 7715 Commercial Way Suite 155 Henderson, NV 89011	Mr. Rich Sollars Regional Manager P: (630) 993-2100 (phone) E: rsollars@mp-mail.com

2.0 TEST REQUIREMENTS

Testing was performed at the kiln stack. The following table presents a list of the parameters tested, the applicable methodologies utilized, and average test results:

Source	Parameter Tested	Test Results	Method/Regulation Citation
Kiln Stack Mill On	Hydrogen Fluoride (HF)	≤ 0.10 ppmvw	USEPA Method 320, 40CFR63, Appendix A
		≤ 0.16 ppmvd @7% O ₂	
		≤ 0.05 lb/hr	
		≤ 0.0005 lb/ton clinker	
	HF ¹	≤ 0.15 ppmvd	Method 26A, 40CFR60, Appendix A
		≤ 0.19 ppmvd @7% O ₂	
		≤ 0.06 lb/hr	
		≤ 0.0005 lb/ton clinker	
	Chlorine (Cl ₂) ¹	≤ 0.04 ppmvd	USEPA Method 26A, 40CFR60, Appendix A
		≤ 0.05 ppmvd @7% O ₂	
		≤ 0.06 lb/hr	
		≤ 0.0005 lb/ton clinker	
	Hydrogen Cyanide (HCN)	1.89 ppmvw	USEPA Method 320, 40CFR63, Appendix A
		3.02 ppmvd @7% O ₂	
1.35 lb/hr			
0.0115 lb/ton clinker			
Oxygen (O ₂)	10.4 % (dry)	USEPA Method 3A, 40CFR60, Appendix A	
Carbon Dioxide (CO ₂)	16.8 % (dry)	USEPA Method 320, 40CFR63, Appendix A	
Moisture (H ₂ O)	17.3 %	USEPA Method 320, 40CFR63, Appendix A	
Cyclonic Flow Determination	PASS	USEPA Method 1, 40CFR60, Appendix A, Section 11.4	
Three-point O ₂ Stratification Determination	< 5 %	USEPA Method 3A, 40CFR60, Appendix A and Method 7E, Section 8.1.2	

¹ HF and Cl₂ Method 26A results are reported as the average from Train A and Train B.

Source	Parameter Tested	Test Results	Method/Regulation Citation
Kiln Stack Mill Off	Hydrogen Fluoride (HF)	≤ 0.10 ppmvw	USEPA Method 320, 40CFR63, Appendix A
		≤ 0.14 ppmvd @7% O ₂	
		≤ 0.05 lb/hr	
		≤ 0.0004 lb/ton clinker	
	HF ²	≤ 0.14 ppmvd	Method 26A, 40CFR60, Appendix A
		≤ 0.16 ppmvd @7% O ₂	
		≤ 0.05 lb/hr	
		≤ 0.0004 lb/ton clinker	
	Chlorine (Cl ₂) ²	≤ 0.04 ppmvd	USEPA Method 26A, 40CFR60, Appendix A
		≤ 0.05 ppmvd @7% O ₂	
		≤ 0.05 lb/hr	
		≤ 0.0005 lb/ton clinker	
	Hydrogen Cyanide (HCN)	2.04 ppmvw	USEPA Method 320, 40CFR63, Appendix A
		2.91 ppmvd @7% O ₂	
		1.28 lb/hr	
0.0109 lb/ton clinker			
Oxygen (O ₂)	8.8 % (dry)	USEPA Method 3A, 40CFR60, Appendix A	
Carbon Dioxide (CO ₂)	19.1 % (dry)	USEPA Method 320, 40CFR63, Appendix A	
Moisture (H ₂ O)	19.4 %	USEPA Method 320, 40CFR63, Appendix A	
Cyclonic Flow Determination	PASS	USEPA Method 1, 40CFR60, Appendix A, Section 11.4	
Three-point O ₂ Stratification Determination	< 5 %	USEPA Method 3A, 40CFR60, Appendix A and Method 7E, Section 8.1.2	

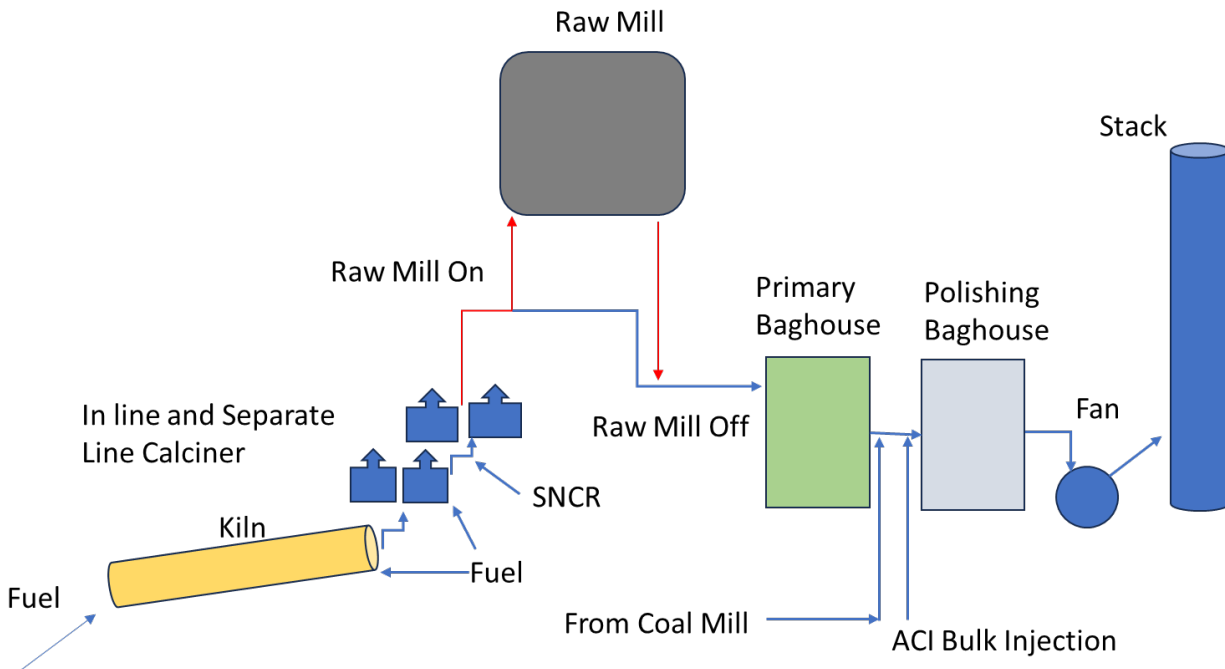
² HF and Cl₂ Method 26A results are reported as the average from Train A and Train B.

3.0 QA SPECIFICATIONS AND PROCESS DIAGRAM

Table 3-1 QA/QC Specifications

Parameter	Method	QA/QC Specification	Acceptance Criteria	Actual Result
HCN	320	Method Detection Limit	0.5 ppm	0.2 ppmvw
		SNR	>2500 at 64 scans	6244 (Run 1 Average)
		S Beam	>0.9	1.161 (Run 1 Average)
		Direct HCN Analysis	±5% of tag value	4.3%
		Dynamic Spike Analysis	≤10% of total sample volume	8.1%
			Spike gas ~twice native concentration or 3-4 ppm addition to native concentration	+4.1 ppm
			≤±20% of expected value or ≤±0.5 ppm, whichever is less restrictive	+1.5 %
Residuals	≤±0.3 ppm, or ≤±5% of measured value, whichever is less restrictive	0.2 ppmvw		
Cl ₂	26A	Paired Train Agreement	≤10% Relative Deviation or ≤0.2 ppm, whichever is less restrictive.	0.01 ppmvd

Table 3-2 Process Flow Diagram



4.0 TEST PROCEDURES

All testing, sampling, analytical, and calibration procedures used for this test program were performed as described in the Title 40, *Code of Federal Regulations*, Part 60, Appendix A (40CFR60), Methods 1, 2, 3A, 4, 26A, and 40CFR63, Appendix A, Method 320; and the latest revisions thereof. Where applicable, the *Quality Assurance Handbook for Air Pollution Measurement Systems*, Volume III, Stationary Source Specific Methods, United States Environmental Protection Agency (USEPA) 600/R-94/038c, September 1994 was used to supplement procedures in addition to the appended "Draft General Test Plan".

4.1 Method 1 Sample and Velocity Traverse Determination

Sample points for testing are determined using USEPA Test Method 1, 40CFR60, Appendix A. The characteristics of the measurement location is summarized below.

Sample Point Selection

Test Location	Stack Diameter	Port Length	Upstream Diameters	Downstream Diameters	Test Parameter	Number of Sampling Points
Main Kiln	10.9 Feet	8.5 Inches	4.1 Diameters	16.5 Diameters	HF/Cl ₂ (26A)	12
					O ₂ (3A)	3 (stratification)
					HCN/HF/CO ₂ (320/3A)	1

A cyclonic flow check was performed in accordance with Section 11.4, which demonstrated it meets the criteria of an average value of less than 20° and therefore is considered to be a suitable testing location for flow rate measurements.

4.2 Method 2 Volumetric Flow Rate Determination

The gas velocity and volumetric flowrate were determined using Method 2, 40CFR60, Appendix A, as an integrated part of the HF/Cl₂ sampling system.

Velocity pressures were determined by traversing the duct with wind tunnel calibrated S-type pitot tube. Temperatures were measured using K-type thermocouples with calibrated digital temperature indicators. The molecular weight and moisture content of the gases were also determined to permit the calculation of the volumetric flowrate.

4.3 Method 3A Oxygen (O₂) and Carbon Dioxide (CO₂) Determination

O₂ and CO₂ concentrations were determined in accordance with Method 3A, 40CFR60, Appendix A and Method 320, 40CFR63, Appendix A, respectively. A Servomex analyzer was used to determine O₂ concentrations while the MKS 2030 analyzer was used to determine CO₂ concentrations. The O₂ instrument has a paramagnetic detector and operates in a nominal range of 0-25%.

A list of calibration gases used and the results of all calibration and other required quality assurance checks are found in the appendix of this report. Copies of calibration gas certifications are also appended.

4.4 Method 26A Hydrogen Fluoride (HF) and Chlorine (Cl₂) Determination

HF and Cl₂ concentrations and emission rates were determined in accordance with Method 26A, 40CFR60, Appendix A. Paired sampling trains were used to collect the samples. A total of twenty (20) test points were sampled per run on the WGS stack. The sample was extracted isokinetically from the gas stream and passed through dilute sulfuric acid (0.1N H₂SO₄). HF was collected in the dilute acid. Cl₂ was collected in the dilute sodium hydroxide (0.1N NaOH) solution. The sample train consisted of a Teflon coated nozzle, a heated borosilicate glass probe liner, a Teflon® filter placed on the outlet of the glass probe liner, and six impingers. The first two impingers contained the 0.1N H₂SO₄, the third remained empty (and was recovered with the first two impingers), the fourth and fifth impingers contained the 0.1N NaOH, while the sixth impinger contained silica gel to absorb any remaining moisture. A de-ionized water rinse was performed on each set of impingers, and samples were stored in Nalgene sample containers for transport. The 0.1N H₂SO₄ impinger catch samples were analyzed for HF while the 0.1N NaOH impinger catch samples were analyzed for Cl₂. A method detection limit (MDL) of 150 µg was determined for both HF and Cl₂ using the "Definition and Procedure for the Determination of the Method Detection Limit, Revision 2". All equipment used was calibrated in accordance with the specifications of the method. Calibration data is appended.

Hand recorded field data sheets were reviewed and scans are retained on the Mostardi Platt network. Copies of this data is available upon request.

4.5 Method 320 Speciated Flue Gas Concentration Determinations

The sampling procedures for HCN and HF were performed in accordance with USEPA Method 320, 40CFR63, Appendix A. Data was continuously recorded with a data logging system throughout sampling, with brief interruption to properly label reference spectra.

The average gas effluent concentrations were determined from the average gas concentration displayed by the MKS 2030 analyzer.

All sampling system components were heated to 375°F +/- 25°F, including: stainless steel sample probe, stainless steel calibration tee, in line glass fiber particulate filter, Teflon® sample line, heated head sample pump, and FTIR detector cell. The sample pump distributes the gas sample to the instrument at a steady sample flow rate (+/- 10%). All components of the sampling system are constructed of stainless steel, glass, or Teflon®.

FTIR technology works on the principle that most gases absorb infrared light. This is true for all compounds except for homonuclear diatomic molecules and noble gases such as: N₂, O₂, H₂, He, Ne, and Ar. Vibrations, stretches, bends, and rotations within the bonds of a molecule determine the infrared absorption distinctiveness. The absorption creates a "fingerprint" which is unique for each given compound. The quantity of infrared light absorbed is proportional to the gas concentration. Most compounds have absorbencies at different infrared frequencies, thus allowing the simultaneous analysis of multiple compounds at one time. The FTIR software compares each sample spectrum to a user-selected list of calibration references and concentration data is generated.

FTIR data was collected using an MKS MultiGas 2030 FTIR spectrometer. Data was generated at 0.5 cm⁻¹. Each Spectra was derived from the coaddition of 62-64 scans with a new data point generated approximately every minute. HCN analyte spiking assured the ability of the FTIR to quantify HCN in the presence of effluent gas. All analyte spikes were introduced using an instrument grade stainless steel rotameter. All QA/QC procedures were within the acceptance criteria allowance of the applicable methodology and the "General Test Plan."

5.0 TEST RESULTS SUMMARIES

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln
Test Method: 26A - Combined Results

Source Condition	Mill On	Mill On	Mill On	
Date	10/11/23	10/11/23	10/11/23	
Start Time	8:30	10:10	11:45	
End Time	9:39	11:21	12:54	
	Run 1	Run 2	Run 3	Average
Stack Conditions				
Average Gas Velocity, ft/sec	44.297	43.771	43.505	43.858
Gas Volumetric Flow Rate, acfm	248,007	245,066	243,572	245,548
Gas Volumetric Flow Rate, dscfm	141,476	139,427	140,381	140,428
Gas Volumetric Flow Rate, scfm	171,083	169,908	169,160	170,050
Average %CO ₂ by volume, dry basis	16.8	16.8	16.7	16.8
Average %O ₂ by volume, dry basis	10.4	10.4	10.4	10.4
Clinker Production, ton/hr	117.0	117.0	118.0	117.3
Chlorine (Cl₂) Emissions				
ppm ≤	0.04	≤ 0.04	≤ 0.04	≤ 0.04
ppmvd@7%O ₂ ≤	0.05	≤ 0.05	≤ 0.05	≤ 0.05
lb/hr ≤	0.0625	≤ 0.0616	≤ 0.0620	≤ 0.0620
lb/ton of clinker ≤	0.0005	≤ 0.0005	≤ 0.0005	≤ 0.0005
Hydrogen Fluoride (HF) Emissions				
ppm ≤	0.15	≤ 0.15	≤ 0.15	≤ 0.15
ppmvd@7%O ₂ ≤	0.19	≤ 0.19	≤ 0.19	≤ 0.19
lb/hr ≤	0.0639	≤ 0.0639	≤ 0.0643	≤ 0.0640
lb/ton of clinker ≤	0.0005	≤ 0.0005	≤ 0.0005	≤ 0.0005

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train A)
 Test Method: 26A

	Source Condition Date	Mill On 10/11/23	Mill On 10/11/23	Mill On 10/11/23		
	Start Time	8:30	10:10	11:45		
	End Time	9:39	11:21	12:54		
		Run 1A	Run 2A	Run 3A	Average	
Stack Conditions						
Average Gas Temperature, °F		227.2	223.5	222.9	224.5	
Flue Gas Moisture, percent by volume		17.0%	17.6%	17.0%	17.2%	
Average Flue Pressure, in. Hg		26.83	26.83	26.83	26.83	
Gas Sample Volume, dscf		51.292	51.056	51.117	51.155	
Average Gas Velocity, ft/sec		44.219	43.966	43.876	44.020	
Gas Volumetric Flow Rate, acfm		247,575	246,159	245,651	246,462	
Gas Volumetric Flow Rate, dscfm		141,517	140,438	141,295	141,083	
Gas Volumetric Flow Rate, scfm		170,587	170,521	170,314	170,474	
Average %CO ₂ by volume, dry basis		16.8	16.8	16.7	16.8	
Average %O ₂ by volume, dry basis		10.4	10.4	10.4	10.4	
Isokinetic Variance		101.6	101.9	101.4	101.6	
Chlorine (Cl₂) Emissions						
ug of sample collected	≤	150	≤	150	≤	150
ppm	≤	0.04	≤	0.04	≤	0.04
Hydrogen Fluoride (HF) Emissions						
ug of sample collected	≤	150	≤	150	≤	150
ppm	≤	0.12	≤	0.13	≤	0.12

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train B)
 Test Method: 26A

	Source Condition Date	Mill On 10/11/23	Mill On 10/11/23	Mill On 10/11/23		
	Start Time	8:30	10:10	11:45		
	End Time	9:39	11:21	12:54		
		Run 1B	Run 2B	Run 3B	Average	
Stack Conditions						
Average Gas Temperature, °F		225.6	222.3	220.6	222.8	
Flue Gas Moisture, percent by volume		17.6%	18.2%	17.0%	17.6%	
Average Flue Pressure, in. Hg		26.83	26.83	26.83	26.83	
Gas Sample Volume, dscf		38.277	37.621	37.451	37.783	
Average Gas Velocity, ft/sec		44.374	43.576	43.133	43.694	
Gas Volumetric Flow Rate, acfm		248,439	243,972	241,492	244,634	
Gas Volumetric Flow Rate, dscfm		141,434	138,415	139,467	139,772	
Gas Volumetric Flow Rate, scfm		171,578	169,295	168,005	169,626	
Average %CO ₂ by volume, dry basis		16.8	16.8	16.7	16.8	
Average %O ₂ by volume, dry basis		10.4	10.4	10.5	10.4	
Isokinetic Variance		101.4	101.8	100.6	101.3	
Chlorine (Cl₂) Emissions						
ug of sample collected	≤	150	≤	150	≤	150
ppm	≤	0.05	≤	0.05	≤	0.05
Hydrogen Fluoride (HF) Emissions						
ug of sample collected	≤	150	≤	150	≤	150
ppm	≤	0.17	≤	0.17	≤	0.17

Ash Grove Cement Company
Durkee Cement Plant
Main Kiln
Mill On
Reference Method Test Data

Test No.	Date	Start Time	End Time	O2 % (dry)	Moisture %	HCN ppmvw	HCN ppmvd @ 7% O2	HF ppmvw	HF ppmvd @ 7% O2
1	10/11/2023	8:30	9:29	10.4	17.2%	2.19	3.50	≤ 0.10	≤ 0.16
2	10/11/2023	10:10	11:09	10.4	17.4%	1.81	2.89	≤ 0.10	≤ 0.16
3	10/11/2023	11:45	12:44	10.4	17.2%	1.66	2.67	≤ 0.10	≤ 0.16
Average				10.4	17.3%	1.89	3.02	≤ 0.10	≤ 0.16

Test No.	Date	Start Time	End Time	Volumetric Flow, DSCFM	Clinker Production, ton/hr	HCN lb/hr	HCN lb/ton	HF lb/hr	HF lb/ton
1	10/11/2023	8:30	9:29	141,476	117.0	1.58	0.0135	≤ 0.05	≤ 0.0005
2	10/11/2023	10:10	11:09	139,427	117.0	1.28	0.0110	≤ 0.05	≤ 0.0004
3	10/11/2023	11:45	12:44	140,381	118.0	1.19	0.0101	≤ 0.05	≤ 0.0004
Average				140,428	117.3	1.35	0.0115	≤ 0.05	≤ 0.0005

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln
Test Method: 26A - Combined Results

Source Condition	Mill Off	Mill Off	Mill Off	
Date	10/12/23	10/12/23	10/12/23	
Start Time	10:45	12:15	13:50	
End Time	11:54	13:24	14:59	
	Run 1	Run 2	Run 3	Average
Stack Conditions				
Average Gas Velocity, ft/sec	41.469	41.378	41.284	41.377
Gas Volumetric Flow Rate, acfm	232,176	231,663	231,139	231,659
Gas Volumetric Flow Rate, dscfm	121,046	121,513	121,155	121,238
Gas Volumetric Flow Rate, scfm	150,633	149,915	149,357	149,968
Average %CO ₂ by volume, dry basis	18.8	19.3	19.1	19.1
Average %O ₂ by volume, dry basis	8.9	8.8	8.8	8.8
Clinker Production, ton/hr	117.0	120.0	118.0	118.3
Chlorine (Cl₂) Emissions				
ppm ≤	0.04	≤ 0.04	≤ 0.04	≤ 0.04
ppmvd@7%O ₂ ≤	0.05	≤ 0.05	≤ 0.05	≤ 0.05
lb/hr ≤	0.0535	≤ 0.0537	≤ 0.0535	≤ 0.0535
lb/ton of clinker ≤	0.0005	≤ 0.0004	≤ 0.0005	≤ 0.0005
Hydrogen Fluoride (HF) Emissions				
ppm ≤	0.14	≤ 0.14	≤ 0.14	≤ 0.14
ppmvd@7%O ₂ ≤	0.16	≤ 0.16	≤ 0.16	≤ 0.16
lb/hr ≤	0.0520	≤ 0.0522	≤ 0.0521	≤ 0.0521
lb/ton of clinker ≤	0.0004	≤ 0.0004	≤ 0.0004	≤ 0.0004

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train A)
 Test Method: 26A

Source Condition	Mill Off	Mill Off	Mill Off	
Date	10/12/23	10/12/23	10/12/23	
Start Time	10:45	12:15	13:50	
End Time	11:54	13:24	14:59	
	Run 1A	Run 2A	Run 3A	Average
Stack Conditions				
Average Gas Temperature, °F	277.8	281.0	282.2	280.3
Flue Gas Moisture, percent by volume	19.3%	18.7%	19.0%	19.0%
Average Flue Pressure, in. Hg	27.10	27.10	27.10	27.10
Gas Sample Volume, dscf	45.595	45.455	45.363	45.471
Average Gas Velocity, ft/sec	42.037	42.033	41.987	42.019
Gas Volumetric Flow Rate, acfm	235,358	235,334	235,074	235,255
Gas Volumetric Flow Rate, dscfm	123,167	123,491	122,762	123,140
Gas Volumetric Flow Rate, scfm	152,570	151,885	151,479	151,978
Average %CO ₂ by volume, dry basis	18.8	19.3	19.1	19.1
Average %O ₂ by volume, dry basis	8.9	8.8	8.8	8.8
Isokinetic Variance	103.8	103.2	103.6	103.5
Chlorine (Cl₂) Emissions				
ug of sample collected	≤ 150	≤ 150	≤ 150	≤ 150
ppm	≤ 0.04	≤ 0.04	≤ 0.04	≤ 0.04
Hydrogen Fluoride (HF) Emissions				
ug of sample collected	≤ 150	≤ 150	≤ 150	≤ 150
ppm	≤ 0.14	≤ 0.14	≤ 0.14	≤ 0.14

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train B)
 Test Method: 26A

	Source Condition	Mill Off	Mill Off	Mill Off		
	Date	10/12/23	10/12/23	10/11/23		
	Start Time	10:45	12:15	13:50		
	End Time	11:54	13:24	14:59		
		Run 1B	Run 2B	Run 3B	Average	
Stack Conditions						
Average Gas Temperature, °F		276.5	277.0	278.0	277.2	
Flue Gas Moisture, percent by volume		20.0%	19.2%	18.8%	19.3%	
Average Flue Pressure, in. Hg		27.10	27.10	27.10	27.10	
Gas Sample Volume, dscf		47.017	46.924	46.836	46.926	
Average Gas Velocity, ft/sec		40.901	40.722	40.581	40.735	
Gas Volumetric Flow Rate, acfm		228,994	227,991	227,204	228,063	
Gas Volumetric Flow Rate, dscfm		118,925	119,534	119,548	119,336	
Gas Volumetric Flow Rate, scfm		148,696	147,945	147,235	147,959	
Average %CO ₂ by volume, dry basis		18.8	19.3	19.1	19.1	
Average %O ₂ by volume, dry basis		8.9	8.8	8.8	8.8	
Isokinetic Variance		104.2	103.5	103.3	103.7	
Chlorine (Cl₂) Emissions						
ug of sample collected	≤	150	≤	150	≤	150
ppm	≤	0.04	≤	0.04	≤	0.04
Hydrogen Fluoride (HF) Emissions						
ug of sample collected	≤	150	≤	150	≤	150
ppm	≤	0.14	≤	0.14	≤	0.14

**Ash Grove Cement Company
Durkee Cement Plant
Main Kiln
Mill Off
Reference Method Test Data**

Test No.	Date	Start Time	End Time	O2 % (dry)	Moisture %	HCN ppmvw	HCN ppmvd @ 7% O2	HF ppmvw	HF ppmvd @ 7% O2
1	10/12/2023	10:45	11:44	8.9	19.9%	2.08	3.01	≤ 0.10	≤ 0.14
2	10/12/2023	12:15	13:14	8.8	19.3%	2.03	2.88	≤ 0.10	≤ 0.14
3	10/12/2023	13:50	14:49	8.8	19.2%	2.00	2.83	≤ 0.10	≤ 0.14
Average				8.8	19.4%	2.04	2.91	≤ 0.10	≤ 0.14

Test No.	Date	Start Time	End Time	Volumetric Flow, DSCFM	Clinker Production, ton/hr	HCN lb/hr	HCN lb/ton	HF lb/hr	HF lb/ton
1	10/12/2023	10:45	11:44	121,046	117.0	1.32	0.0113	≤ 0.05	≤ 0.0004
2	10/12/2023	12:15	13:14	121,513	120.0	1.28	0.0107	≤ 0.05	≤ 0.0004
3	10/12/2023	13:50	14:49	121,155	118.0	1.26	0.0107	≤ 0.05	≤ 0.0004
Average				121,238	118.3	1.29	0.0109	≤ 0.05	≤ 0.0004

6.0 CERTIFICATION

Mostardi Platt is pleased to have been of service to Ash Grove Cement Company. If you have any questions regarding this test report, please do not hesitate to contact us at 630-993-2100.

As project manager, I hereby certify that this test report represents a true and accurate summary of emissions test results and the methodologies employed to obtain those results, and the test program was performed in accordance with the methods specified in this test report.

MOSTARDI PLATT



Richard J. Sollars II

Project Manager



Chet A. Gutwein

Quality Assurance

APPENDICES

Appendix A – Plant Operating Data

HCN Production Data for October 11 & 12, 2023

Fuel Usage - 0% Coal, 97% Natural Gas and 3% Tires

Timestamp	Total Kiln Feed	
	Rate	Total Clinker
	stph	stph

10/11/2023 7:30	197	117
10/11/2023 7:31	199	118
10/11/2023 7:32	199	118
10/11/2023 7:33	200	118
10/11/2023 7:34	198	118
10/11/2023 7:35	198	118
10/11/2023 7:36	198	118
10/11/2023 7:37	198	118
10/11/2023 7:38	197	118
10/11/2023 7:39	199	118
10/11/2023 7:40	198	118
10/11/2023 7:41	199	118
10/11/2023 7:42	198	117
10/11/2023 7:43	198	118
10/11/2023 7:44	198	117
10/11/2023 7:45	198	117
10/11/2023 7:46	199	117
10/11/2023 7:47	197	117
10/11/2023 7:48	196	117
10/11/2023 7:49	200	118
10/11/2023 7:50	198	118
10/11/2023 7:51	198	118
10/11/2023 7:52	199	117
10/11/2023 7:53	197	117
10/11/2023 7:54	196	117
10/11/2023 7:55	195	116
10/11/2023 7:56	195	116
10/11/2023 7:57	196	116
10/11/2023 7:58	196	116
10/11/2023 7:59	196	116
10/11/2023 8:00	196	116
10/11/2023 8:01	196	117
10/11/2023 8:02	198	117
10/11/2023 8:03	196	117
10/11/2023 8:04	196	116
10/11/2023 8:05	195	116
10/11/2023 8:06	197	117
10/11/2023 8:07	196	116
10/11/2023 8:08	196	117
10/11/2023 8:09	196	116
10/11/2023 8:10	195	116
10/11/2023 8:11	196	117
10/11/2023 8:12	195	116
10/11/2023 8:13	196	116
10/11/2023 8:14	195	116
10/11/2023 8:15	197	117
10/11/2023 8:16	198	117
10/11/2023 8:17	196	117
10/11/2023 8:18	195	116
10/11/2023 8:19	196	116
10/11/2023 8:20	196	116
10/11/2023 8:21	195	116
10/11/2023 8:22	195	116
10/11/2023 8:23	197	116
10/11/2023 8:24	196	116
10/11/2023 8:25	197	116
10/11/2023 8:26	197	116
10/11/2023 8:27	197	116
10/11/2023 8:28	198	117
10/11/2023 8:29	197	116

10/11/2023 8:30	195	116
10/11/2023 8:31	196	116
10/11/2023 8:32	197	116
10/11/2023 8:33	197	117
10/11/2023 8:34	196	116
10/11/2023 8:35	196	116
10/11/2023 8:36	194	116
10/11/2023 8:37	195	116
10/11/2023 8:38	197	116
10/11/2023 8:39	198	117

Run 1 Average	197	117
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10/11/2023 9:10	196	116
10/11/2023 9:11	196	117
10/11/2023 9:12	196	116
10/11/2023 9:13	193	116
10/11/2023 9:14	196	116
10/11/2023 9:15	196	116
10/11/2023 9:16	195	116
10/11/2023 9:17	196	116
10/11/2023 9:18	196	117
10/11/2023 9:19	194	116
10/11/2023 9:20	196	117
10/11/2023 9:21	197	117
10/11/2023 9:22	195	116
10/11/2023 9:23	196	116
10/11/2023 9:24	197	117
10/11/2023 9:25	195	116
10/11/2023 9:26	196	116
10/11/2023 9:27	197	117
10/11/2023 9:28	196	117
10/11/2023 9:29	195	117
10/11/2023 9:30	195	116
10/11/2023 9:31	195	116
10/11/2023 9:32	196	116
10/11/2023 9:33	196	116
10/11/2023 9:34	196	117
10/11/2023 9:35	197	117
10/11/2023 9:36	194	116
10/11/2023 9:37	197	116
10/11/2023 9:38	196	116
10/11/2023 9:39	196	116
10/11/2023 9:40	195	116
10/11/2023 9:41	197	117
10/11/2023 9:42	194	116
10/11/2023 9:43	193	116
10/11/2023 9:44	195	116
10/11/2023 9:45	196	117
10/11/2023 9:46	195	116
10/11/2023 9:47	196	116
10/11/2023 9:48	196	117
10/11/2023 9:49	196	116
10/11/2023 9:50	195	116
10/11/2023 9:51	196	117
10/11/2023 9:52	198	117
10/11/2023 9:53	198	117
10/11/2023 9:54	198	117
10/11/2023 9:55	197	117
10/11/2023 9:56	196	117
10/11/2023 9:57	197	117
10/11/2023 9:58	198	118
10/11/2023 9:59	196	117
10/11/2023 10:00	198	117
10/11/2023 10:01	197	117
10/11/2023 10:02	196	117
10/11/2023 10:03	196	117
10/11/2023 10:04	196	117
10/11/2023 10:05	198	117
10/11/2023 10:06	197	117

10/11/2023 10:07	196	117
10/11/2023 10:08	197	117
10/11/2023 10:09	198	117
10/11/2023 10:10	197	117
10/11/2023 10:11	198	117
10/11/2023 10:12	195	117
10/11/2023 10:13	198	117
10/11/2023 10:14	198	117
10/11/2023 10:15	198	117
10/11/2023 10:16	195	117
10/11/2023 10:17	197	117
10/11/2023 10:18	195	116
10/11/2023 10:19	198	117
10/11/2023 10:20	198	117
10/11/2023 10:21	196	117

Run 2 Average	196	117
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10/11/2023 10:45	199	118
10/11/2023 10:46	198	118
10/11/2023 10:47	198	118
10/11/2023 10:48	197	117
10/11/2023 10:49	198	118
10/11/2023 10:50	198	118
10/11/2023 10:51	198	118
10/11/2023 10:52	199	118
10/11/2023 10:53	196	117
10/11/2023 10:54	198	117
10/11/2023 10:55	197	117
10/11/2023 10:56	197	118
10/11/2023 10:57	198	118
10/11/2023 10:58	198	118
10/11/2023 10:59	197	118
10/11/2023 11:00	198	118
10/11/2023 11:01	197	118
10/11/2023 11:02	197	117
10/11/2023 11:03	199	118
10/11/2023 11:04	198	117
10/11/2023 11:05	198	118
10/11/2023 11:06	199	118
10/11/2023 11:07	197	118
10/11/2023 11:08	197	118
10/11/2023 11:09	199	118
10/11/2023 11:10	198	118
10/11/2023 11:11	199	118
10/11/2023 11:12	200	118
10/11/2023 11:13	199	118
10/11/2023 11:14	198	118
10/11/2023 11:15	198	118
10/11/2023 11:16	197	118
10/11/2023 11:17	199	118
10/11/2023 11:18	200	118
10/11/2023 11:19	198	118
10/11/2023 11:20	198	118
10/11/2023 11:21	199	118
10/11/2023 11:22	199	118
10/11/2023 11:23	199	118
10/11/2023 11:24	199	119
10/11/2023 11:25	199	119
10/11/2023 11:26	199	118
10/11/2023 11:27	199	118
10/11/2023 11:28	202	119
10/11/2023 11:29	198	119
10/11/2023 11:30	199	118
10/11/2023 11:31	199	118
10/11/2023 11:32	200	118
10/11/2023 11:33	198	118
10/11/2023 11:34	199	118
10/11/2023 11:35	201	118
10/11/2023 11:36	200	118
10/11/2023 11:37	199	117

10/11/2023 11:38	198	118
10/11/2023 11:39	200	118
10/11/2023 11:40	199	118
10/11/2023 11:41	199	118
10/11/2023 11:42	198	118
10/11/2023 11:43	200	118
10/11/2023 11:44	199	118
10/11/2023 11:45	198	118
10/11/2023 11:46	199	118
10/11/2023 11:47	198	117
10/11/2023 11:48	198	118
10/11/2023 11:49	199	118
10/11/2023 11:50	199	118
10/11/2023 11:51	199	118
10/11/2023 11:52	199	118
10/11/2023 11:53	200	119
10/11/2023 11:54	199	118

Run 3 Average	199	118
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10/12/2023 9:45	193	114
10/12/2023 9:46	195	115
10/12/2023 9:47	193	115
10/12/2023 9:48	193	114
10/12/2023 9:49	192	114
10/12/2023 9:50	193	115
10/12/2023 9:51	194	115
10/12/2023 9:52	193	115
10/12/2023 9:53	193	114
10/12/2023 9:54	192	114
10/12/2023 9:55	194	116
10/12/2023 9:56	195	116
10/12/2023 9:57	196	116
10/12/2023 9:58	196	117
10/12/2023 9:59	196	116
10/12/2023 10:00	197	116
10/12/2023 10:01	195	117
10/12/2023 10:02	196	116
10/12/2023 10:03	193	116
10/12/2023 10:04	194	116
10/12/2023 10:05	194	115
10/12/2023 10:06	195	115
10/12/2023 10:07	195	115
10/12/2023 10:08	195	115
10/12/2023 10:09	195	116
10/12/2023 10:10	194	115
10/12/2023 10:11	194	115
10/12/2023 10:12	194	115
10/12/2023 10:13	195	116
10/12/2023 10:14	193	116
10/12/2023 10:15	195	116
10/12/2023 10:16	197	116
10/12/2023 10:17	195	116
10/12/2023 10:18	194	116
10/12/2023 10:19	197	117
10/12/2023 10:20	197	118
10/12/2023 10:21	197	117
10/12/2023 10:22	196	117
10/12/2023 10:23	197	117
10/12/2023 10:24	198	118
10/12/2023 10:25	198	117
10/12/2023 10:26	200	118
10/12/2023 10:27	199	118
10/12/2023 10:28	196	117
10/12/2023 10:29	200	118
10/12/2023 10:30	198	118
10/12/2023 10:31	198	118
10/12/2023 10:32	200	119
10/12/2023 10:33	199	119
10/12/2023 10:34	199	119
10/12/2023 10:35	199	119

10/12/2023 10:36	199	118
10/12/2023 10:37	197	118
10/12/2023 10:38	197	117
10/12/2023 10:39	198	117
10/12/2023 10:40	197	117
10/12/2023 10:41	198	117
10/12/2023 10:42	199	118
10/12/2023 10:43	197	117
10/12/2023 10:44	198	117
10/12/2023 10:45	198	118
10/12/2023 10:46	199	118
10/12/2023 10:47	197	118
10/12/2023 10:48	197	117
10/12/2023 10:49	197	117
10/12/2023 10:50	199	118
10/12/2023 10:51	200	119
10/12/2023 10:52	202	120
10/12/2023 10:53	201	119
10/12/2023 10:54	199	119

Run 4 Average	196	117
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10/12/2023 11:15	199	119
10/12/2023 11:16	201	119
10/12/2023 11:17	201	119
10/12/2023 11:18	201	119
10/12/2023 11:19	199	118
10/12/2023 11:20	199	118
10/12/2023 11:21	199	119
10/12/2023 11:22	199	119
10/12/2023 11:23	201	119
10/12/2023 11:24	199	119
10/12/2023 11:25	199	118
10/12/2023 11:26	200	119
10/12/2023 11:27	200	119
10/12/2023 11:28	201	119
10/12/2023 11:29	199	118
10/12/2023 11:30	202	120
10/12/2023 11:31	202	120
10/12/2023 11:32	202	120
10/12/2023 11:33	202	120
10/12/2023 11:34	202	120
10/12/2023 11:35	203	121
10/12/2023 11:36	202	120
10/12/2023 11:37	202	120
10/12/2023 11:38	204	121
10/12/2023 11:39	203	121
10/12/2023 11:40	203	121
10/12/2023 11:41	204	121
10/12/2023 11:42	204	121
10/12/2023 11:43	203	121
10/12/2023 11:44	205	121
10/12/2023 11:45	204	121
10/12/2023 11:46	202	120
10/12/2023 11:47	205	122
10/12/2023 11:48	204	121
10/12/2023 11:49	204	121
10/12/2023 11:50	205	121
10/12/2023 11:51	203	121
10/12/2023 11:52	204	121
10/12/2023 11:53	205	121
10/12/2023 11:54	204	122
10/12/2023 11:55	205	122
10/12/2023 11:56	206	122
10/12/2023 11:57	204	122
10/12/2023 11:58	203	121
10/12/2023 11:59	204	121
10/12/2023 12:00	204	121
10/12/2023 12:01	203	121
10/12/2023 12:02	201	120
10/12/2023 12:03	201	120

10/12/2023 12:04	203	119
10/12/2023 12:05	205	120
10/12/2023 12:06	202	121
10/12/2023 12:07	205	121
10/12/2023 12:08	204	121
10/12/2023 12:09	203	121
10/12/2023 12:10	205	121
10/12/2023 12:11	200	120
10/12/2023 12:12	200	119
10/12/2023 12:13	199	120
10/12/2023 12:14	202	120
10/12/2023 12:15	200	120
10/12/2023 12:16	201	120
10/12/2023 12:17	203	120
10/12/2023 12:18	202	121
10/12/2023 12:19	203	120
10/12/2023 12:20	202	121
10/12/2023 12:21	205	120
10/12/2023 12:22	202	120
10/12/2023 12:23	202	120
10/12/2023 12:24	206	122

Run 5 Average	202	120
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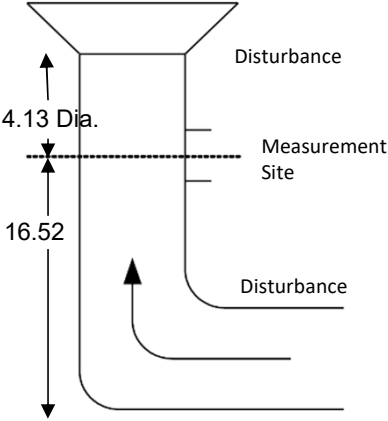
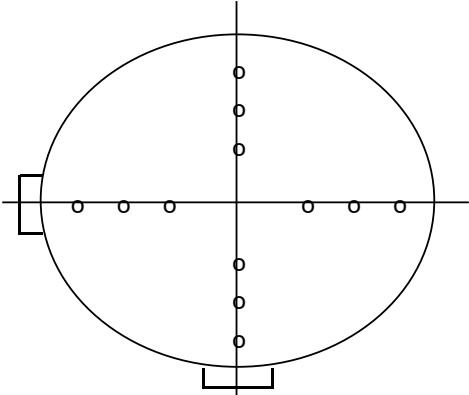
10/12/2023 12:50	201	119
10/12/2023 12:51	201	120
10/12/2023 12:52	200	119
10/12/2023 12:53	201	119
10/12/2023 12:54	200	119
10/12/2023 12:55	201	119
10/12/2023 12:56	201	119
10/12/2023 12:57	199	119
10/12/2023 12:58	200	119
10/12/2023 12:59	200	119
10/12/2023 13:00	201	119
10/12/2023 13:01	200	119
10/12/2023 13:02	200	119
10/12/2023 13:03	200	119
10/12/2023 13:04	199	119
10/12/2023 13:05	200	119
10/12/2023 13:06	200	119
10/12/2023 13:07	200	118
10/12/2023 13:08	200	119
10/12/2023 13:09	199	119
10/12/2023 13:10	201	119
10/12/2023 13:11	198	118
10/12/2023 13:12	201	119
10/12/2023 13:13	203	120
10/12/2023 13:14	200	120
10/12/2023 13:15	199	118
10/12/2023 13:16	200	118
10/12/2023 13:17	199	119
10/12/2023 13:18	200	119
10/12/2023 13:19	200	119
10/12/2023 13:20	201	119
10/12/2023 13:21	199	119
10/12/2023 13:22	202	119
10/12/2023 13:23	200	119
10/12/2023 13:24	201	119
10/12/2023 13:25	203	119
10/12/2023 13:26	200	119
10/12/2023 13:27	199	119
10/12/2023 13:28	201	118
10/12/2023 13:29	198	118
10/12/2023 13:30	200	119
10/12/2023 13:31	199	118
10/12/2023 13:32	201	119
10/12/2023 13:33	202	119
10/12/2023 13:34	198	117
10/12/2023 13:35	194	116
10/12/2023 13:36	196	116

10/12/2023 13:37	197	117
10/12/2023 13:38	197	117
10/12/2023 13:39	197	117
10/12/2023 13:40	196	117
10/12/2023 13:41	195	116
10/12/2023 13:42	196	116
10/12/2023 13:43	197	117
10/12/2023 13:44	194	115
10/12/2023 13:45	196	117
10/12/2023 13:46	194	116
10/12/2023 13:47	196	117
10/12/2023 13:48	196	117
10/12/2023 13:49	196	116
10/12/2023 13:50	194	117
10/12/2023 13:51	197	117
10/12/2023 13:52	198	118
10/12/2023 13:53	197	117
10/12/2023 13:54	197	117
10/12/2023 13:55	196	117
10/12/2023 13:56	195	117
10/12/2023 13:57	195	116
10/12/2023 13:58	196	117
10/12/2023 13:59	197	117

Run 6 Average	199	118
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Appendix B – Test Section Diagrams

EQUAL AREA TRAVERSE FOR ROUND DUCTS



Client: Ash Grove Cement Company

Facility: Durkee Cement Plant

Test Location: Main Kiln

Date: 10/11/2023 & 10/12/2023

Diameter (Feet): 10.900

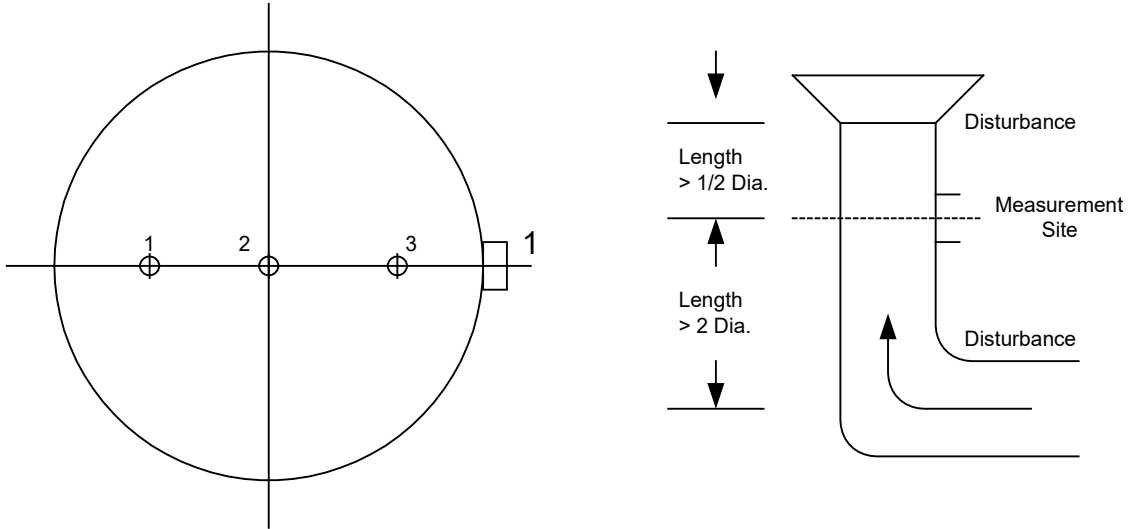
Port Length (In): 8.50

Ports Sampled: 4

Points/Port: 3

	Point Markings	
	From inside wall (in.)	% of Diameter
1	5.76	4.40
2	19.10	14.60
3	38.72	29.60

STRATIFICATION TEST FOR ROUND DUCTS



Job: Ash Grove Cement Company
Durkee Cement Plant
Durkee, Oregon

Test Location: Main Kiln Inlet

Stack Diameter: 10.9 Feet

Stack Area: 93.313 Square Feet

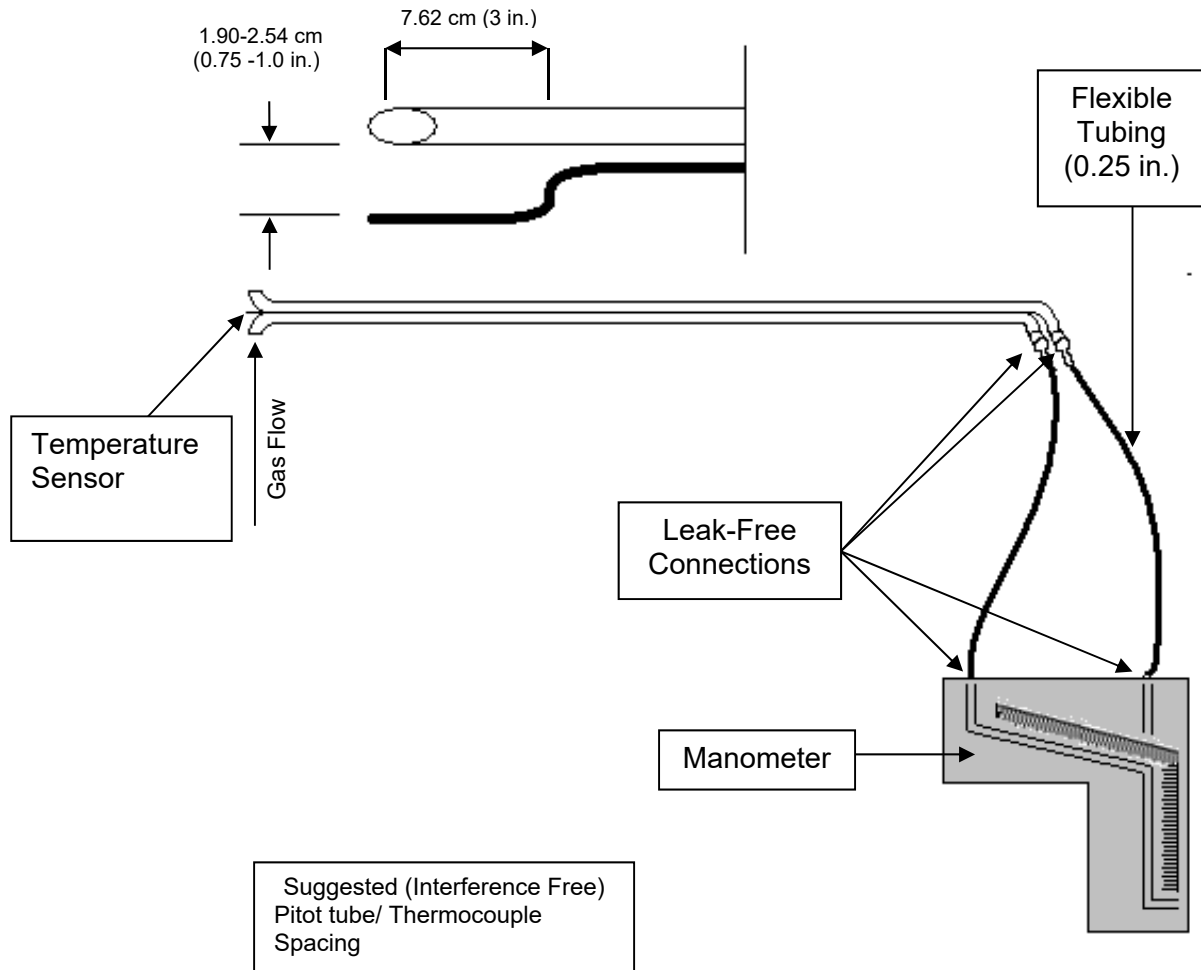
No. Sample Points: 3

Distance from Inside Wall
To Traverse Point:

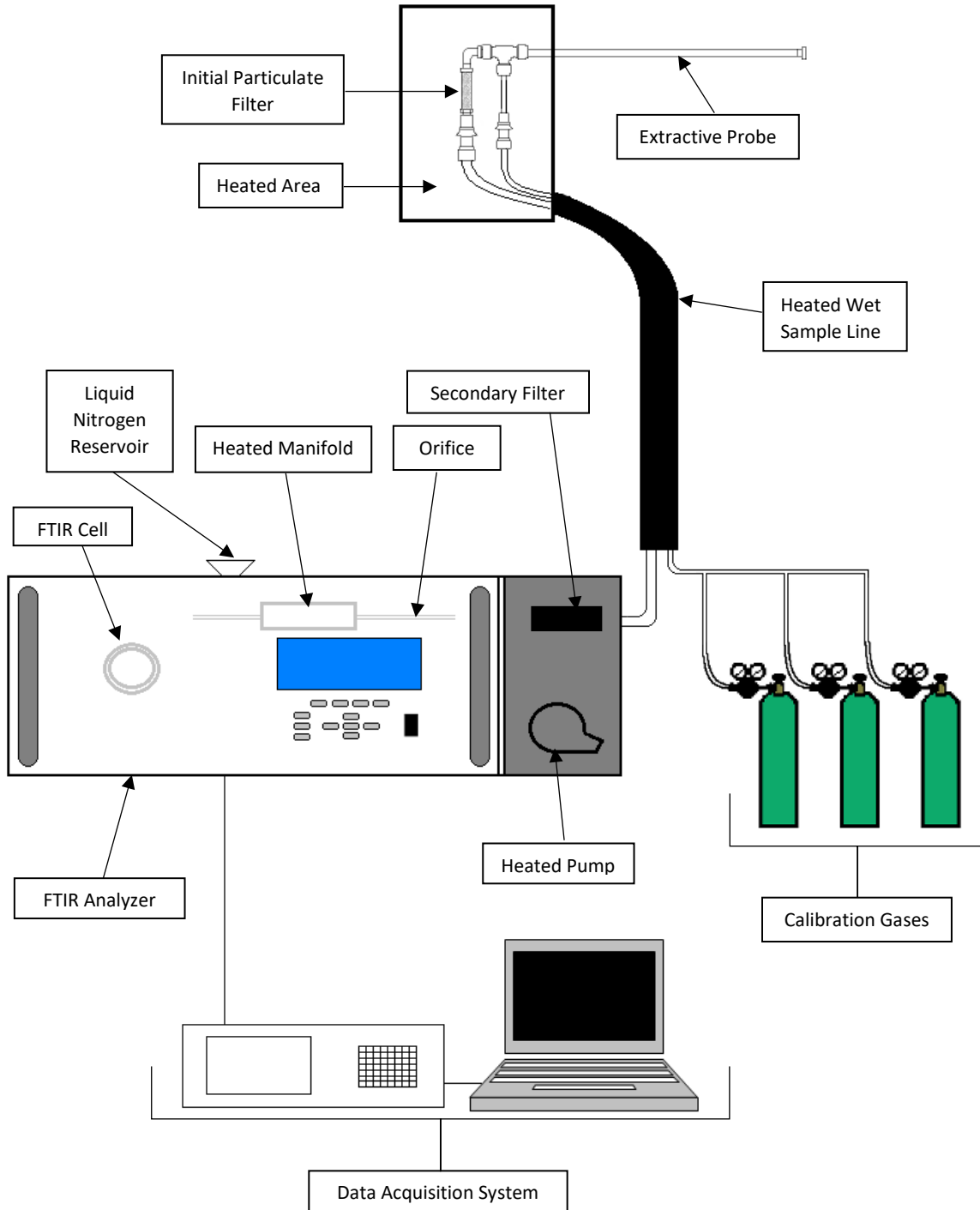
1. 83.3 % of diameter
2. 50.0 % of diameter
3. 16.7 % of diameter

Appendix C – Sample Train Diagrams

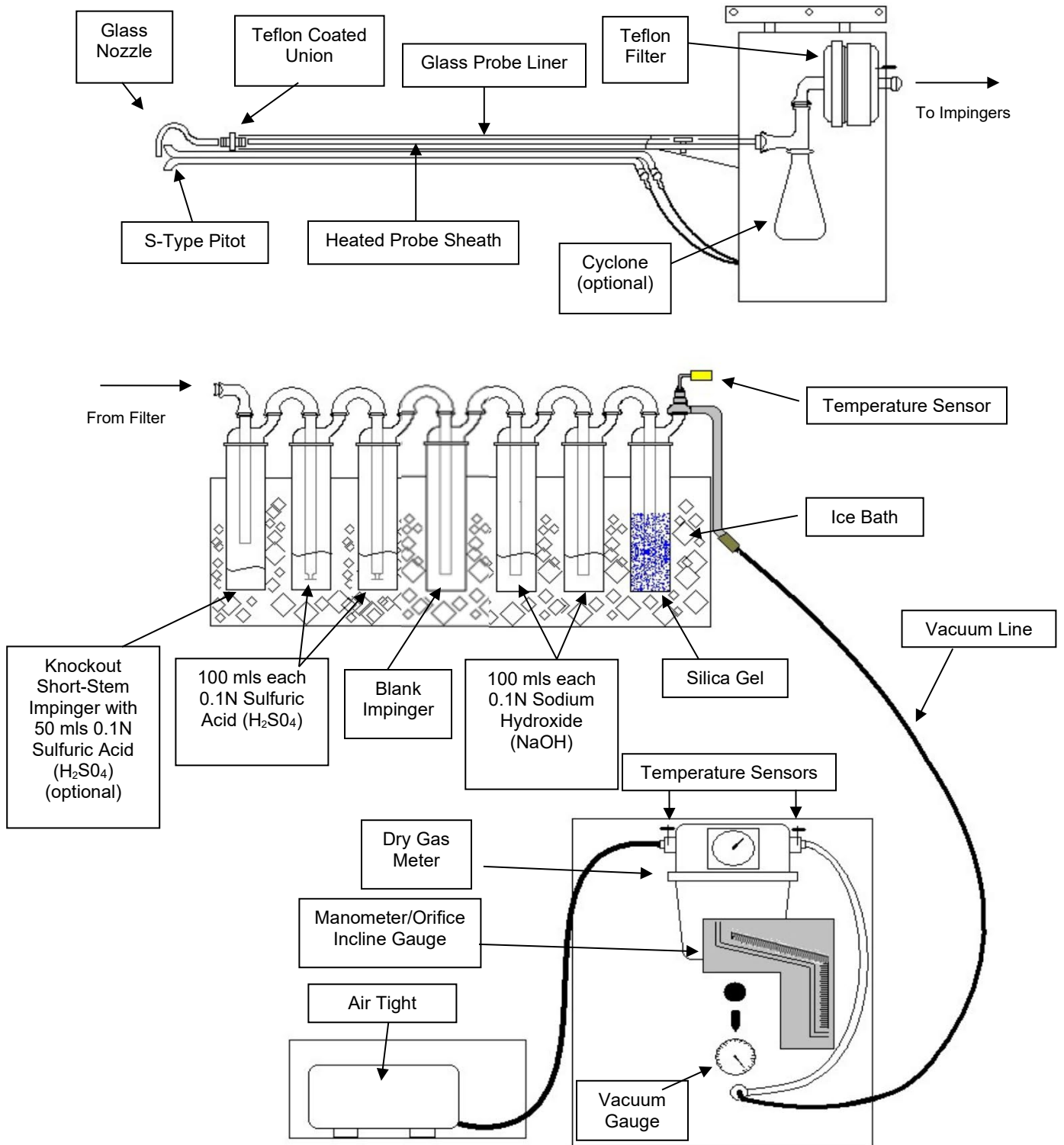
USEPA Method 2 – Type S Pitot Tube Manometer Assembly



USEPA Method 320 – Vapor Phase Organic and Inorganic Emissions by Extractive Fourier Transform Infrared (FTIR) Spectroscopy Sample Train Diagram



USEPA Method 26A – HF and Cl₂ Sample Train Diagram



Appendix D – Calculation Nomenclature and Formulas

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train A)
Run: 1
Date: 10/11/2023
Method: 26A
Source Condition: Mill On

Dry Molecular Weight

$$Md = 0.44 \times (\%CO_2) + 0.32 \times (\%O_2) + 0.28 \times \%N_2$$

$$\%CO_2 = \underline{16.8} \qquad \%O_2 = \underline{10.4} \qquad \%N_2 = \underline{72.8}$$

$$Md = \underline{31.104}$$

Wet Molecular Weight

$$Ms = Md \times (1 - Bws) + (18.0 \times Bws)$$

$$Md = \underline{31.104} \qquad Bws = \underline{0.170}$$

$$Ms = \underline{28.871}$$

Meter Volume at Standard Conditions

$$Vm(std) = 17.647 \times Y \times Vm \times \frac{(Pbar + DH/13.6)}{Tm}$$

$$Y = \underline{1.004} \qquad Vm = \underline{56.432} \qquad Pbar = \underline{26.9}$$

$$DH = \underline{2.6} \qquad Tm = \underline{67.3}$$

$$Vm(std) = \underline{51.292}$$

Volume of Water Vapor Condensed

$$Vw(std) = 0.0471 \times (\text{net H}_2\text{O gain})$$

$$\text{Net H}_2\text{O} = \underline{223.7}$$

$$Vw(std) = \underline{10.536}$$

Moisture Content

$$Bws = \frac{Vw(std)}{Vw(std) + Vm(std)}$$

$$Vw(std) = \underline{10.536} \qquad Vm(std) = \underline{51.292}$$

$$Bws = \underline{0.170}$$

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train A)
Run: 1
Date: 10/11/2023
Method: 26A
Source Condition: Mill On

Average Duct Velocity

$$Vs = 85.49 \times Cp \times \text{Sqrt DP (avg)} \times (Ts \text{ (avg)} + 460 / (Ps \times Ms))^{1/2}$$

$Cp = \frac{0.820}{26.83}$	$Ts \text{ (avg)} = \frac{227.2}{28.871}$	$\text{Sqrt DP (avg)} = \underline{0.670}$
$Ps = \underline{26.83}$	$Ms = \underline{28.871}$	
$Vs = \underline{44.219}$		

Volumetric Flow Rate (Actual Basis)

$$Q = Vs \times A \times 60$$

$Vs = \underline{44.219}$	$A = \underline{93.313}$
$Q = \underline{247,575}$	

Volumetric Flow Rate (Standard Basis)

$$Qstd = 17.647 \times Q \times \frac{Ps}{Ts \text{ (avg)} + 460}$$

$Q = \underline{247,575}$	$Ps = \underline{26.83}$	$Ts \text{ (avg)} = \underline{227.2}$
$Qstd = \underline{170,587}$		

Volumetric Flow Rate (Standard Dry Basis)

$$Qstd(\text{dry}) = Qstd \times (1 - Bws)$$

$Qstd = \underline{170,587}$	$Bws = \underline{0.170}$
$Qstd(\text{dry}) = \underline{141,517}$	

Isokinetic Variation:

$$\%ISO = \frac{0.0945 \times (Ts + 460) \times Vm(\text{std})}{Vs \times \theta \times An \times Ps \times (1 - Bws)}$$

$Ts = \underline{227.2}$	$Vm(\text{std}) = \underline{51.292}$	$Vs = \underline{44.219}$
$An = \underline{0.0005550}$	$\theta = \underline{60}$	$Ps = \underline{26.83}$
$Bws = \underline{0.170}$		
$\%ISO = \underline{101.6}$		

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train A)
Run: 1
Date: 10/11/2023
Method: 26A
Source Condition: Mill On

Chloride (Cl2) Concentration:

$$\text{mg/m}^3 = \frac{\text{mg of Chloride (Cl}_2\text{)}}{\text{Vm(std)} \times 0.02832 \text{ m}^3/\text{ft}^3}$$

$$\text{mg} = \underline{0.15} \quad \text{Vm(std)} = \underline{51.292}$$

$$\text{mg/m}^3 = \underline{0.10}$$

Chloride (Cl2) Emission Rate:

$$\text{lb of Chloride (Cl}_2\text{)} = \frac{\mu\text{g of sample} \times 10^6 \text{ grams}/\mu\text{g}}{453.6 \text{ grams/lb}}$$

$$\text{Emission Rate lb/hr} = \frac{\text{lb of Chloride (Cl}_2\text{)}}{\text{Vm(std)}} \times \text{dscfm} \times 60 \text{ min/hr}$$

$$\text{lb of Chloride (Cl}_2\text{)} = \underline{3.31\text{E-}10} \quad \text{dscfm} = \underline{141,517}$$

$$\text{Emission Rate lb/hr} = \underline{0.0547}$$

$$\text{Emission Rate lb/ton} = \frac{\text{lb/hr of Chloride (Cl}_2\text{)}}{\text{clinker production ton/hr}}$$

$$\text{lb/hr of Chloride (Cl}_2\text{)} = \underline{0.0547} \quad \text{clinker ton/hr} = \underline{117.0}$$

$$\text{Emission Rate lb/ton} = \underline{0.0005}$$

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Project #: M234105
Test Location: Main Kiln
Date: 10/11/23

Sample Calculations

$$(10.37 \% - -0.06 \%) \times \frac{\text{O2 \% (dry)} \quad 11.96 \%}{11.96 \% - -0.06 \%} = 10.38 \%$$

$$C_{\text{gas}} = (C - C_o) \times \frac{C_{\text{ma}}}{C_m - C_o}$$

where:

C_{gas} = Effluent gas concentration, dry basis, ppm or %

C = Average gas concentration indicated by gas analyzer, dry basis, ppm or %

C_o = Average of initial and final system calibration bias check responses for the zero gas, ppm or %

C_m = Average of initial and final system calibration bias check responses for the upscale calibration gas, ppm or %

C_{ma} = Actual concentration of the upscale calibration gas, ppm or %

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234 105
 Test Location: Main Kiln
 Date: 10/11/23

FTIR Sample Calculations

Direct Recovery % of Calibration Transfer Standard

$$DR_{cts} = \frac{D_{cts}}{Cma} \times 100$$

$$Cma = \frac{100.7}{}$$

$$D_{cts} = \frac{99.8}{}$$

$$DR_{cts} = \frac{99.1\%}{}$$

Recovery % with Calibration Transfer Standard System Purge

$$R_{cts} = \frac{Sys_{cts}}{D_{cts}} \times 100$$

$$Sys_{cts} = \frac{99.7}{}$$

$$D_{cts} = \frac{99.8}{}$$

$$R_{cts} = \frac{100\%}{}$$

Direct Recovery % of Analyte Spike Gas

SF6

$$DR_{sf6} = \frac{D_{sf6}}{Cma} \times 100$$

$$Cma = \frac{5.0}{}$$

$$D_{sf6} = \frac{4.9}{}$$

$$DR_{sf6} = \frac{98\%}{}$$

HCN

$$DR_{asg} = \frac{D_{asg}}{Cma} \times 100$$

$$Cma = \frac{49.3}{}$$

$$D_{asg} = \frac{51.4}{}$$

$$DR_{asg} = \frac{104.3\%}{}$$

Dilution Factor for Analyte Spiking

$$DF = \frac{Spk_{sf6}}{D_{sf6}}$$

$$Spk_{sf6} = \frac{0.395}{}$$

$$D_{sf6} = \frac{4.905}{}$$

$$DF = \frac{0.081}{}$$

Recovery % for Analyte Spike With HCN

$$R_x = \frac{Spk_x}{(N_x \times (1-DF) + D_{asg} \times DF)}$$

$$Spk_x = \frac{6.2}{}$$

$$N_x = \frac{2.2}{}$$

$$DF = \frac{0.081}{}$$

$$D_{asg} = \frac{51.4}{}$$

$$R_x = \frac{101.9}{\%}$$

where:

- DR_{cts} = Recovery % of the calibration transfer standard directly to the analyzer
- Cma = certified concentration of calibration gas, ppm
- D_{cts} = Concentration of the calibration transfer standard gas directly to the analyzer, ppm
- R_{cts} = Recovery % of the calibration transfer standard through the sampling system
- Sys_{cts} = Concentration of the calibration transfer standard gas through the system, ppm
- DF = Dilution Factor of analyte spike gas
- Spk_{sf6} = SF6 concentration in effluent during spiking
- Spk_x = Analyte concentration in effluent during spiking
- D_{asg} = Concentration of the analyte spike gas directly to the analyzer, ppm
- D_{sf6} = Concentration of the SF6 directly to the analyzer, ppm
- R_x = Recovery % of the analyte spike gas
- N_x = Native effluent (HCN) concentration prior to analyte spike

MOSTARDI PLATT

Moisture Calculations

$$V_{wc(std)} = \frac{(V_f - V_i)\rho_w RT_{std}}{P_{std}M_w} = 0.04707(V_f - V_i)$$

$$V_{wsg(std)} = \frac{(W_f - W_i)\rho_w RT_{std}}{P_{std}M_w} = 0.04715(W_f - W_i)$$

$$V_{m(std)} = 17.64 V_m Y \frac{P_{bar} + \frac{\Delta H}{13.6}}{T_m}$$

$$B_{ws} = \frac{V_{wc(std)} + V_{wsg(std)}}{V_{wc(std)} + V_{wsg(std)} + V_{m(std)}}$$

Where:

B_{ws} = Water vapor in gas stream, proportion by volume

M_w = Molecular weight of water, 18.015 lb/lb-mole

P_{bar} = Barometric pressure at the testing site, in. Hg

P_{std} = Standard absolute pressure, 29.92 in. Hg

R = Ideal gas constant, $0.048137 \text{ (in. Hg)(ft}^3\text{)/(g-mole)(}^\circ\text{R)} =$
 $[21.8348 \text{ (in. Hg)(ft}^3\text{)/(lb-mole)(}^\circ\text{R)}]/453.592 \text{ g-mole/lb-mole}$

T_m = Absolute average dry gas meter temperature, $^\circ\text{R}$

T_{std} = Standard absolute temperature, 528 $^\circ\text{R}$

V_f = Final volume of condenser water, ml

V_i = Initial volume of condenser water, ml

V_m = Dry gas volume measured by dry gas meter, dcf

$V_{m(std)}$ = Dry gas volume measured by dry gas meter, corrected to standard conditions, scf

$V_{wc(std)}$ = Volume of condensed water vapor, corrected to standard conditions, scf

$V_{wsg(std)}$ = Volume of water vapor collected in silica gel, corrected to standard conditions, scf

W_f = Final weight of silica gel, g

W_i = Initial weight of silica gel, g

Y = Dry gas meter calibration factor

ΔH = Average pressure exerted on dry gas meter outlet by gas sample bag, in. H_2O

ρ_w = Density of water, 0.9982 g/ml

13.6 = Specific gravity of mercury (Hg)

17.64 = T_{std}/P_{std}

0.04707 = ft^3/ml 0.04715 = ft^3/g

MOSTARDI PLATT

Volumetric Flow Nomenclature

- A = Cross-sectional area of stack or duct, ft²
- Bws = Water vapor in gas stream, proportion by volume
- Cp = Pitot tube coefficient, dimensionless
- Md = Dry molecular weight of gas, lb/lb-mole
- Ms = Molecular weight of gas, wet basis, lb/lb-mole
- Mw = Molecular weight of water, 18.0 lb/lb-mole
- Pbar = Barometric pressure at testing site, in. Hg
- Pg = Static pressure of gas, in. Hg (in. H₂O/13.6)
- DH= Static pressure of gas, in.H₂O
- Ps = Absolute pressure of gas, in. Hg = Pbar + Pg
- Pstd = Standard absolute pressure, 29.92 in. Hg
- Acfm = Actual volumetric gas flow rate
- Scfm= Volumetric gas flow rate, corrected to standard conditions
- Dscfm = Standard volumetric flow rate, corrected to dry conditions
- R = Ideal gas constant, 21.85 in. Hg-ft³/°R-lb-mole
- Ts = Average stack gas temperature, °F
- Tm = Average dry gas meter temperature, °F
- Tstd = Standard absolute temperature, 528°R
- vs = Gas velocity, ft/sec
- Vm(std)= Volume of gas sampled, corrected to standard conditions, scf
- Vw(std) = Volume of water vapor in gas sample, corrected to standard conditions, scf
- Vlc= Volume of liquid collected
- Y = Dry gas meter calibration factor
- Δp = Velocity head of gas, in. H₂O
- K1 = 17.647 °R/in. Hg
- %EA = Percent excess air
- %CO₂ = Percent carbon dioxide by volume, dry basis
- %O₂ = Percent oxygen by volume, dry basis
- %N₂ = Percent nitrogen by volume, dry basis
- 0.264 = Ratio of O₂ to N₂ in air, v/v
- 0.28 = Molecular weight of N₂ or CO, divided by 100
- 0.32 = Molecular weight of O₂ divided by 100
- 0.44 = Molecular weight of CO₂ divided by 100
- 13.6 = Specific gravity of mercury (Hg)

MOSTARDI PLATT

Volumetric Air Flow Calculations

$$Vm (std) = 17.647 \times Vm \times \left[\frac{(P_{bar} + \left[\frac{DH}{13.6} \right])}{(460 + Tm)} \right] \times Y$$

$$Vw (std) = 0.0471 \times Vlc$$

$$Bws = \left[\frac{Vw (std)}{Vw (std) + Vm (std)} \right]$$

$$Md = (0.44 \times \%CO_2) + (0.32 \times \%O_2) + [0.28 \times (100 - \%CO_2 - \%O_2)]$$

$$Ms = Md \times (1 - Bws) + (18 \times Bws)$$

$$Vs = \sqrt{\frac{(Ts + 460)}{Ms \times Ps}} \times \sqrt{DP} \times Cp \times 85.49$$

$$Acfm = Vs \times Area (of\ stack\ or\ duct) \times 60$$

$$Scfm = Acfm \times 17.647 \times \left[\frac{Ps}{(460 + Ts)} \right]$$

$$Scfh = Scfm \times 60 \frac{min}{hr}$$

$$Dscfm = Scfm \times (1 - Bws)$$

MOSTARDI PLATT

Isokinetic Calculation Formulas

$$1. V_{w(std)} = V_{lc} \left(\frac{\rho_w}{M_w} \right) \left(\frac{RT_{std}}{P_{std}} \right) = K_2 V_{lc}$$

$$2. V_{m(std)} = V_m Y \left(\frac{T_{std}}{T_m} \right) \left(\frac{(P_{bar} + (\frac{\Delta H}{13.6}))}{P_{std}} \right) = K_1 V_m Y \frac{(P_{bar} + (\frac{\Delta H}{13.6}))}{T_m}$$

$$3. B_{ws} = \frac{V_{w(std)}}{(V_{m(std)} + V_{w(std)})}$$

$$4. M_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2)$$

$$5. M_s = M_d(1 - B_{ws}) + 18.0(B_{ws})$$

$$6. C_a = \frac{m_a}{V_a \rho_a}$$

$$7. W_a = C_a V_{aw} \rho_a$$

$$8. C_{acf} = 15.43 K_i \left(\frac{m_n P_s}{(V_{w(std)} + V_{m(std)}) T_s} \right)$$

$$9. C_s = (15.43 \text{ grains/gram}) (m_n / V_{m(std)})$$

$$10. v_s = K_p C_p \sqrt{\frac{\Delta P T_s}{P_s M_s}}$$

$$11. Q_{acfm} = v_s A (60_{\text{sec/min}})$$

$$12. Q_{sd} = (3600_{\text{sec/hr}}) (1 - B_{ws}) v_s \left(\frac{T_{std} P_s}{T_s P_{std}} \right) A$$

$$13. E \text{ (emission rate, lbs/hr)} = Q_{std} (C_s / 7000 \text{ grains/lb})$$

$$14. IKV = \frac{T_s V_{m(std)} P_{std}}{T_{std} v_s \theta A_n P_s 60(1 - B_{ws})} = K_4 \frac{T_s V_{m(std)}}{P_s v_s A_n \theta (1 - B_{ws})}$$

$$15. \%EA = \left(\frac{\%O_2 - (0.5 \%CO)}{0.264 \%N_2 - (\%O_2 - 0.5 \%CO)} \right) \times 100$$

MOSTARDI PLATT

Isokinetic Nomenclature

- A = Cross-sectional area of stack or duct, square feet
A_n = Cross-sectional area of nozzle, square feet
B_{ws} = Water vapor in gas stream, by volume
C_a = Acetone blank residue concentration, g/g
C_{act} = Concentration of particulate matter in gas stream at actual conditions, gr/acf
C_p = Pitot tube coefficient
C_s = Concentration of particulate matter in gas stream, dry basis, corrected to standard conditions, gr/dscf
IKV = Isokinetic sampling variance, must be 90.0 % ≤ IKV ≤ 110.0%
M_d = Dry molecular weight of gas, lb/lb-mole
M_s = Molecular weight of gas, wet basis, lb/lb-mole
M_w = Molecular weight of water, 18.0 lb/lb-mole
m_a = Mass of residue of acetone after evaporation, grams
P_{bar} = Barometric pressure at testing site, inches mercury
P_g = Static pressure of gas, inches mercury (inches water/13.6)
P_s = Absolute pressure of gas, inches mercury = P_{bar} + P_g
P_{std} = Standard absolute pressure, 29.92 inches mercury
Q_{acfm} = Actual volumetric gas flow rate, acfm
Q_{sd} = Dry volumetric gas flow rate corrected to standard conditions, dscfh
R = Ideal gas constant, 21.85 inches mercury cubic foot/°R-lb-mole
T_m = Dry gas meter temperature, °R
T_s = Gas temperature, °R
T_{std} = Absolute temperature, 528°R
V_a = Volume of acetone blank, ml
V_{aw} = Volume of acetone used in wash, ml
W_a = Weight of residue in acetone wash, grams
m_n = Total amount of particulate matter collected, grams
V_{1c} = Total volume of liquid collected in impingers and silica gel, ml
V_m = Volume of gas sample as measured by dry gas meter, dcf
V_{m(std)} = Volume of gas sample measured by dry gas meter, corrected to standard conditions, dscf
V_s = Gas velocity, ft/sec
V_{w(std)} = Volume of water vapor in gas sample, corrected to standard conditions, scf
Y = Dry gas meter calibration factor
ΔH = Average pressure differential across the orifice meter, inches water
Δp = Velocity head of gas, inches water
ρ_a = Density of acetone, 0.7855 g/ml (average)
ρ_w = Density of water, 0.002201 lb/ml
θ = Total sampling time, minutes
K₁ = 17.647 °R/in. Hg
K₂ = 0.04707 ft³/ml
K₄ = 0.09450/100 = 0.000945
K_p = Pitot tube constant, $85.49 \frac{ft}{sec} \left[\frac{(lb/lb-mole)(in. Hg)}{(°R)(in. H_2O)} \right]^{1/2}$
%EA = Percent excess air
%CO₂ = Percent carbon dioxide by volume, dry basis
%O₂ = Percent oxygen by volume, dry basis
%CO = Percent carbon monoxide by volume, dry basis
%N₂ = Percent nitrogen by volume, dry basis
0.264 = Ratio of O₂ to N₂ in air, v/v
28 = Molecular weight of N₂ or CO
32 = Molecular weight of O₂
44 = Molecular weight of CO₂
13.6 = Specific gravity of mercury (Hg)

MOSTARDI PLATT

Calculations for Hydrogen Fluoride By Method 26 or 26A

Concentration

$$\frac{\text{lbs HF}}{\text{dscf}} = \frac{\mu\text{g HF in sample}}{4.536 \times 10^8 \times \text{dscf}}$$

where:

$$4.536 \times 10^8 = \mu\text{g/lb}$$

dscf = Volume of gas sampled

$$\mu\text{g/lb HF} = \mu\text{g F} \times \frac{20.008}{19.000}$$

Parts Per Million

$$\text{ppm HF} = \frac{\text{lbs HF}}{\text{dscf}} \div \frac{20.008}{385 \times 10^6}$$

where:

385 = Volume of 1 lb mole of gas at 68°F and 29.92 in. Hg

106 = Conversion of ppm v/v

Emission Rate

$$\text{lbs HF /dscf} \times \text{dscfm} \times 60 \text{ min/hr} = \text{lbs/hr HF}$$

MOSTARDI PLATT

Pollutant Concentration Correction 7% for Percent Oxygen

$$C_{adj} = C_d \frac{20.9 - 7\%}{20.9 - \%O_2}$$

where:

C_{adj} = Pollutant concentration corrected to percent O_2

$20.9 - 7\%$ = Percent O_2 , the defined O_2 correction value, percent

20.9 = Percent O_2 in air

$\%O_2$ = Measured O_2 concentration dry basis, percent

C_d = Pollutant concentration measured, dry basis, ppm.

Appendix E- Laboratory Sample Analysis

Chain-of-Custody Form						
Project Number: M234105				Date Results Required:		
Client: Ash Grove Cement – Durkee, OR				TAT Required:		
Plant/Test Location: Kiln				Project Supervisor: Rich S		
Sample Number	Sample Date	Sample Point Identification	# of Conts	Sub Lab	Analysis Required	Volume, mls
001	10/12/23	#1A 26A Mill off 0.1N H2SO4	1		M26A (HF)	
002	10/12/23	#1A 26A Mill off 0.1N NaOH	1		M26A (Cl ₂)	
003	10/12/23	#2A 26A Mill off 0.1N H2SO4	1		M26A (HF)	
004	10/12/23	#2A 26A Mill off 0.1N NaOH	1		M26A (Cl ₂)	
005	10/12/23	#3A 26A Mill off 0.1N H2SO4	1		M26A (HF)	
006	10/12/23	#3A 26A Mill off 0.1N NaOH	1		M26A (Cl ₂)	
007	10/12/23	#1B 26A Mill off 0.1N H2SO4	1		M26A (HF)	
008	10/12/23	#1B 26A Mill off 0.1N NaOH	1		M26A (Cl ₂)	
009	10/12/23	#2B 26A Mill off 0.1N H2SO4	1		M26A (HF)	
010	10/12/23	#2B 26A Mill off 0.1N NaOH	1		M26A (Cl ₂)	
011	10/12/23	#3B 26A Mill off 0.1N H2SO4	1		M26A (HF)	
012	10/12/23	#3B 26A Mill off 0.1N NaOH	1		M26A (Cl ₂)	
013	10/11/23	#1A 26A Mill on 0.1N H2SO4	1		M26A (HF)	
014	10/11/23	#1A 26A Mill on 0.1N NaOH	1		M26A (Cl ₂)	
015	10/11/23	#2A 26A Mill on 0.1N H2SO4	1		M26A (HF)	
016	10/11/23	#2A 26A Mill on 0.1N NaOH	1		M26A (Cl ₂)	
017	10/11/23	#3A 26A Mill on 0.1N H2SO4	1		M26A (HF)	
018	10/11/23	#3A 26A Mill on 0.1N NaOH	1		M26A (Cl ₂)	
019	10/11/23	#1B 26A Mill on 0.1N H2SO4	1		M26A (HF)	
020	10/11/23	#1B 26A Mill on 0.1N NaOH	1		M26A (Cl ₂)	
021	10/11/23	#2B 26A Mill on 0.1N H2SO4	1		M26A (HF)	
022	10/11/23	#2B 26A Mill on 0.1N NaOH	1		M26A (Cl ₂)	
023	10/11/23	#3B 26A Mill on 0.1N H2SO4	1		M26A (HF)	
024	10/11/23	#3B 26A Mill on 0.1N NaOH	1		M26A (Cl ₂)	

025	10/11/23	A Train Field Blank 0.1N H2SO4	1		M26A (HF)	
026	10/11/23	A Train Field Blank 0.1N NaOH	1		M26A (Cl ₂)	
027	10/11/23	B Train Field Blank 0.1N H2SO4	1		M26A (HF)	
028	10/11/23	B Train Field Blank 0.1N NaOH	1		M26A (Cl ₂)	
029	10/11/23	0.1N H2SO4 Reagent Blank	1		M26A (HF)	
030	10/11/23	0.1N NaOH Reagent Blank	1		M26A (Cl ₂)	
031	10/11/23	DI Water Reagent Blank	1		M26A (HF and Cl ₂)	
Delivered to Lab by: Date/Time:		Received by: Date/Time:		Processed by: Date/Time:		

Laboratory Notes:

Kiln

Client: Ash Grove	Analysis Date: 11/2/2023
Facility: Durkee	Analysis Location: Elmhurst
Test Location: Kiln	Analyst: JMG
Project Number: M234105	
Method: 26A	
Date Samples Received: 10/20/2023	

Train A

Sampling Date		10/12/2023	10/12/2023	10/12/2023	10/12/2023		
	UNITS	M26A DI Blank	M26A H2SO4 Blank	M26A H2SO4-R1	M26A H2SO4-R1 Dup	RDL	MDL
Sulfuric Acid Volume	ml	200	200	445	445		
Hydrofluoric Acid	ug	150	150	150	150	150	15

Sampling Date		10/12/2023	10/12/2023	10/12/2023		
	UNITS	M26A- H2SO4 R2	M26A- H2SO4 R3	M26A Train Blank	RDL	MDL
Sulfuric Acid Volume	ml	420	490	265		
Hydrofluoric Acid	ug	150	150	150	150	15

Train B

Sampling Date		10/12/2023	10/12/2023	10/12/2023	10/12/2023		
	UNITS	M26A DI Blank	M26A H2SO4 Blank	M26A H2SO4-R1	M26A H2SO4-R1 Dup	RDL	MDL
Sulfuric Acid Volume	ml	200	200	387	387		
Hydrofluoric Acid	ug	150	150	150	150	150	15

Sampling Date		10/12/2023	10/12/2023				
	UNITS	M26A- H2SO4 R2	M26A- H2SO4 R3	RDL	MDL		
Sulfuric Acid Volume	ml	378	428				
Hydrofluoric Acid	ug	150	150			150	15

Client: Ash Grove	Analysis Date: 11/2/2023												
Facility: Durkee	Analysis Location: Elmhurst												
Test Location: Kln	Analyst: JMG												
Project Number: M234105													
Method: 26A													
Date Samples Received: 10/20/2023													
Standard ppm HF	Area	Response Factor	Calculated Value	Slope of Regression Curve									
1	0.2338	0.2338	0.94	0.2474									
2	0.4867	0.2434	1.97										
5	1.2557	0.2511	5.07	Response Factor Ave									
8	1.9964	0.2496	8.07	0.2473									
10	2.5855	0.2586	10.45										
Lot Number	Ricca 8209004												
	R ²	0.9993											
Sample Number	Sample Date	Sample ID	Sample Area	PPM F	PPM X Dilution Factor	Dilution Factor	Total ml	mg F in soln	mg HF in soln	mg HF in soln avg	ug HF in soln		
031	10/12/2023	DI Reagent Blank	0.0050	0.0202	0.0202	1	200	0.0040	0.0043				
031	10/12/2023	DI Reagent Blank	0.0022	0.0089	0.0089	1	200	0.0018	0.0019	0.0031	3.064702009		
029	10/12/2023	H2SO4 Reagent Blank	0.0055	0.0222	0.0222	1	200	0.0044	0.0047				
029	10/12/2023	H2SO4 Reagent Blank	0.0061	0.0247	0.0247	1	200	0.0049	0.0052	0.0049	4.937575459		
019	10/12/2023	Test 1B H2SO4 Imp	0.0191	0.0772	0.0772	1	387	0.0299	0.0315				
019	10/12/2023	Test 1B H2SO4 Imp	0.0112	0.0453	0.0453	1	387	0.0175	0.0184	0.0250	24.95625155		
019	10/12/2023	Test 1B H2SO4 Imp	0.0148	0.0598	0.0598	1	387	0.0231	0.0244				
019	10/12/2023	Test 1B H2SO4 Imp	0.0186	0.0752	0.0752	1	387	0.0291	0.0306	0.0275	27.50953141		
021	10/12/2023	Test 2B H2SO4 Imp	0.0217	0.0877	0.0877	1	378	0.0331	0.0349				
021	10/12/2023	Test 2B H2SO4 Imp	0.0287	0.1160	0.1160	1	378	0.0438	0.0462	0.0405	40.54600758		
023	10/12/2023	Test 3B H2SO4 Imp	0.0403	0.1629	0.1629	1	428	0.0897	0.0734				
023	10/12/2023	Test 3B H2SO4 Imp	0.0466	0.1883	0.1883	1	428	0.0806	0.0849	0.0792	79.15699636		
CCV ppm F	Area	PPM F											
1 ppm ICV	0.2585	1.0447											
5 ppm CCV	1.1864	4.7945											
5 ppm CCV	1.1759	4.7521											
5 ppm CCV	1.1783	4.7618											
5 ppm CCV	0	0.0000											

Kiln

Client: Ash Grove	Analysis Date: 11/2/2023
Facility: Durkee	Analysis Location: Elmhurst
Test Location: Kiln	Analyst: JMG
Project Number: M234105	
Method: 26A	
Date Samples Received: 10/20/2023	

Train A

Sampling Date		10/12/2023	10/12/2023	10/12/2023	10/12/2023		
	UNITS	M26A DI Blank	M26A NaOH Blank	M26A NaOH-R1	M26A NaOH-R1 Dup	RDL	MDL
Sodium Hydroxide Volume	ml	200	200	220	220		
Chlorine	ug	150	150	150	150	150	15

Sampling Date		10/12/2023	10/12/2023	10/12/2023		
	UNITS	M26A- NaOH R2	M26A- NaOH R3	M26A- Train Blank	RDL	MDL
Sodium Hydroxide Volume	ml	233	241	247		
Chlorine	ug	150	150	150	150	15

Train B

Sampling Date		10/12/2023	10/12/2023	10/12/2023	10/12/2023		
	UNITS	M26A DI Blank	M26A NaOH Blank	M26A NaOH-R1	M26A NaOH-R1 Dup	RDL	MDL
Sodium Hydroxide Volume	ml	200	200	237	237		
Chlorine	ug	150	150	150	150	150	15

Sampling Date		10/12/2023	10/12/2023				
	UNITS	M26A- NaOH R2	M26A- NaOH R3	RDL	MDL		
Sodium Hydroxide Volume	ml	211	250				
Chlorine	ug	150	150	150	15		

Client:	Ash Grove	Analysis Date:	11/2/2023																	
Facility:	Durkee	Analysis Location:	Elmhurst Lab																	
Test Location:	Kiln	Analyst:	JMG																	
Project Number:	M234105																			
Method:	26A																			
Date Samples Received:	10/20/2023																			
Standard ppm Cl	Area	Response Factor	Calculated Value	Slope of Regression Curve																
1	0.1443	0.1443	0.97	0.1493																
2	0.2936	0.1468	1.97																	
5	0.7479	0.1496	5.01	Response Factor Ave																
8	1.2139	0.1517	8.13	0.1493																
10	1.5385	0.1539	10.31																	
Lot Number	Ricca 8209004																			
	R²	0.9998																		
Sample Number	Sample Date	Sample ID	Sample Area	PPM Cl	PPM X Dilution Factor	Dilution Factor	Total ml	mg Cl in soln	ug Cl2 in soln	ug Cl2 in soln										
031	10/12/2023	DI Reagent Blank	0.0007	0.0047	0.0047	1	200	0.0009												
031	10/12/2023	DI Reagent Blank	0.0003	0.0020	0.0020	1	200	0.0004	0.0007	0.669889041										
030	10/12/2023	NaOH Reagent Blank	0.0134	0.0898	0.0898	1	200	0.0180												
030	10/12/2023	NaOH Reagent Blank	0.0187	0.1253	0.1253	1	200	0.0251	0.0215	21.50343821										
014	10/12/2023	Test 1A NaOH Imp	0.0007	0.0047	0.0047	1	220	0.0010												
014	10/12/2023	Test 1A NaOH Imp	0.0008	0.0054	0.0054	1	220	0.0012	0.0011	1.105316917										
014	10/12/2023	Test 1A NaOH Imp	0.0007	0.0047	0.0047	1	220	0.0010												
014	10/12/2023	Test 1A NaOH Imp	0.0005	0.0033	0.0033	1	220	0.0007	0.0009	0.884253534										
016	10/12/2023	Test 2A NaOH Imp	0.0020	0.0134	0.0134	1	233	0.0031												
016	10/12/2023	Test 2A NaOH Imp	0.0035	0.0234	0.0234	1	233	0.0055	0.0043	4.292314029										
018	10/12/2023	Test 3A NaOH Imp	0.0037	0.0248	0.0248	1	241	0.0060												
018	10/12/2023	Test 3A NaOH Imp	0.0040	0.0268	0.0268	1	241	0.0065	0.0062	6.215565466										
028	1/0/1900	Train Blank	0.0120	0.0804	0.0804	1	247	0.0199												
028	1/0/1900	Train Blank	0.0097	0.0650	0.0650	1	247	0.0160	0.0180	17.95269135										
					Expected Value	% Difference														
		Run 1 H2SO4 Spike W/ 2ppm	0.1344	0.9003	0.9859															
		Run 1 H2SO4 Spike W/ 2ppm	0.1326	0.8883	0.9859	9.29%														
CCV ppm Cl	Area	PPM Cl																		
5 ppm ICV	0.7485	5.0141																		
5 ppm CCV	0.7127	4.7743																		
5 ppm CCV	0.7169	4.8024																		

Client:	Ash Grove	Analysis Date:	11/2/2023										
Facility:	Durkee	Analysis Location:	Elmhurst Lab										
Test Location:	Kiln	Analyst:	JMG										
Project Number:	M234105												
Method:	26A												
Date Samples Received:	10/20/2023												
Standard ppm Cl	Area	Response Factor	Calculated Value	Slope of Regression Curve									
1	0.1443	0.1443	0.97	0.1493									
2	0.2936	0.1468	1.97										
5	0.7479	0.1496	5.01	Response Factor Ave									
8	1.2139	0.1517	8.13	0.1493									
10	1.5385	0.1539	10.31										
Lot Number	Ricca 8209004												
	R²	0.9998											
Sample Number	Sample Date	Sample ID	Sample Area	PPM Cl	PPM X Dilution Factor	Dilution Factor	Total ml	mg Cl in soln	mg Cl2 in soln avg	ug Cl2 in soln			
031	10/12/2023	DI Reagent Blank	0.0007	0.0047	0.0047	1	200	0.0009					
031	10/12/2023	DI Reagent Blank	0.0003	0.0020	0.0020	1	200	0.0004	0.0007	0.669889041			
030	10/12/2023	NaOH Reagent Blank	0.0134	0.0898	0.0898	1	200	0.0180					
030	10/12/2023	NaOH Reagent Blank	0.0187	0.1253	0.1253	1	200	0.0251	0.0215	21.50343821			
020	10/12/2023	Test 1B NaOH Imp	0.0050	0.0335	0.0335	1	237	0.0079					
020	10/12/2023	Test 1B NaOH Imp	0.0040	0.0268	0.0268	1	237	0.0064	0.0071	7.144366621			
020	10/12/2023	Test 1B NaOH Imp	0.0029	0.0194	0.0194	1	237	0.0046					
020	10/12/2023	Test 1B NaOH Imp	0.0055	0.0368	0.0368	1	237	0.0087	0.0067	6.668075513			
021	10/12/2023	Test 2B NaOH Imp	0.0015	0.0100	0.0100	1	211	0.0021					
021	10/12/2023	Test 2B NaOH Imp	0.0011	0.0074	0.0074	1	211	0.0016	0.0018	1.837505639			
022	10/12/2023	Test 3B NaOH Imp	0.0060	0.0402	0.0402	1	250	0.0100					
022	10/12/2023	Test 3B NaOH Imp	0.0038	0.0255	0.0255	1	250	0.0064	0.0082	8.20614075			
CCV ppm Cl	Area	PPM Cl											
5 ppm ICV	0.7485	5.0141											
5 ppm CCV	0.7127	4.7743											
5 ppm CCV	0.7169	4.8024											

Kiln

Client: Ash Grove	Analysis Date: 11/2/2023
Facility: Durkee	Analysis Location: Elmhurst
Test Location: Kiln	Analyst: JMG
Project Number: M234105	
Method: 26A	
Date Samples Received: 10/20/2023	

Train A

Sampling Date		10/12/2023	10/12/2023	10/12/2023	10/12/2023		
	UNITS	M26A DI Blank	M26A H2SO4 Blank	M26A H2SO4-R1	M26A H2SO4-R1 Dup	RDL	MDL
Sulfuric Acid Volume	ml	200	200	559	559		
Hydrofluoric Acid	ug	150	150	150	150	150	15

Sampling Date		10/12/2023	10/12/2023				
	UNITS	M26A- H2SO4 R2	M26A- H2SO4 R3	M26A- H2SO4 R4		RDL	MDL
Sulfuric Acid Volume	ml	444	424				
Hydrofluoric Acid	ug	150	150			150	15

Train B

Sampling Date		10/12/2023	10/12/2023	10/12/2023	10/12/2023		
	UNITS	M26A DI Blank	M26A H2SO4 Blank	M26A H2SO4-R1	M26A H2SO4-R1 Dup	RDL	MDL
Sulfuric Acid Volume	ml	200	200	499	499		
Hydrofluoric Acid	ug	150	150	150	150	150	15

Sampling Date		10/12/2023	10/12/2023				
	UNITS	M26A- H2SO4 R2	M26A- H2SO4 R3			RDL	MDL
Sulfuric Acid Volume	ml	466	434				
Hydrofluoric Acid	ug	150	150			150	15

Kiln

Client: Ash Grove Facility: Durkee Test Location: Kiln Project Number: M234105 Method: 26A Date Samples Received: 10/20/2023	Analysis Date: 11/2/2023 Analysis Location: Elmhurst Analyst: JMG
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Train A

Sampling Date		10/12/2023	10/12/2023	10/12/2023	10/12/2023		
	UNITS	M26A DI Blank	M26A NaOH Blank	M26A NaOH-R1	M26A NaOH-R1 Dup	RDL	MDL
Sodium Hydroxide Volume	ml	200	200	159	159		
Chlorine	ug	150	150	150	150	150	15

Sampling Date		10/12/2023	10/12/2023				
	UNITS	M26A- NaOH R2	M26A- NaOH R3			RDL	MDL
Sodium Hydroxide Volume	ml	250	242				
Chlorine	ug	150	150			150	15

Train B

Sampling Date		10/12/2023	10/12/2023	10/12/2023	10/12/2023		
	UNITS	M26A DI Blank	M26A NaOH Blank	M26A NaOH-R1	M26A NaOH-R1 Dup	RDL	MDL
Sodium Hydroxide Volume	ml	200	200	247	247		
Chlorine	ug	150	150	150	150	150	15

Sampling Date		10/12/2023	10/12/2023				
	UNITS	M26A- NaOH R2	M26A- NaOH R3			RDL	MDL
Sodium Hydroxide Volume	ml	247	232				
Chlorine	ug	150	150			150	15

Client:	Ash Grove	Analysis Date:	11/2/2023																	
Facility:	Durkee	Analysis Location:	Elmhurst Lab																	
Test Location:	Kiln	Analyst:	JMG																	
Project Number:	M234105																			
Method:	26A																			
Date Samples Received:	10/20/2023																			
Standard ppm Cl	Area	Response Factor	Calculated Value	Slope of Regression Curve																
1	0.1443	0.1443	0.97	0.1493																
2	0.2936	0.1468	1.97																	
5	0.7479	0.1496	5.01	Response Factor Ave																
8	1.2139	0.1517	8.13	0.1493																
10	1.5385	0.1539	10.31																	
Lot Number	Ricca 8209004																			
	R²	0.9998																		
Sample Number	Sample Date	Sample ID	Sample Area	PPM Cl	PPM X Dilution Factor	Dilution Factor	Total ml	mg Cl in soln	ug Cl2 in soln	ug Cl2 in soln										
031	10/12/2023	DI Reagent Blank	0.0007	0.0047	0.0047	1	200	0.0009												
031	10/12/2023	DI Reagent Blank	0.0003	0.0020	0.0020	1	200	0.0004	0.0007	0.669889041										
030	10/12/2023	NaOH Reagent Blank	0.0134	0.0898	0.0898	1	200	0.0180												
030	10/12/2023	NaOH Reagent Blank	0.0187	0.1253	0.1253	1	200	0.0251	0.0215	21.50343821										
002	10/12/2023	Test 1A NaOH Imp	0.0021	0.0141	0.0141	1	159	0.0022												
002	10/12/2023	Test 1A NaOH Imp	0.0015	0.0100	0.0100	1	159	0.0016	0.0019	1.917222435										
002	10/12/2023	Test 1A NaOH Imp	0.0025	0.0167	0.0167	1	159	0.0027												
002	10/12/2023	Test 1A NaOH Imp	0.0019	0.0127	0.0127	1	159	0.0020	0.0023	2.343271865										
004	10/12/2023	Test 2A NaOH Imp	0.0035	0.0234	0.0234	1	250	0.0059												
004	10/12/2023	Test 2A NaOH Imp	0.0016	0.0107	0.0107	1	250	0.0027	0.0043	4.270542635										
006	10/12/2023	Test 3A NaOH Imp	0.0011	0.0074	0.0074	1	242	0.0018												
006	10/12/2023	Test 3A NaOH Imp	0.0004	0.0027	0.0027	1	242	0.0006	0.0012	1.215848609										
026	10/12/2023	Train Blank	0.0120	0.0804	0.0804	1	247	0.0199												
026	10/12/2023	Train Blank	0.0097	0.0650	0.0650	1	247	0.0160	0.0180	17.95269135										
		Run 1 H2SO4 Spike W/ 2ppm	0.1319	0.8836	0.9894															
		Run 1 H2SO4 Spike W/ 2ppm	0.1348	0.9030	0.9894	9.72%														
CCV ppm Cl	Area	PPM Cl																		
5 ppm ICV	0.7485	5.0141																		
5 ppm CCV	0.7127	4.7743																		
5 ppm CCV	0.7169	4.8024																		
5 ppm CCV		0.0000																		
Standard ppm Cl	Area	Difference																		
1	0.1452	0.31%																		
2	0.2843	1.64%																		
5	0.7229	1.73%																		
8	1.1735	1.72%																		
10	1.4938	1.50%																		

Appendix F - Reference Method Test Data

Client:	Ash Grove Cement Company
Facility:	Durkee Cement Plant
Test Location:	Main Kiln (Train A)
Project #:	M234105
Test Method:	26A
Test Engineer:	CPD
Test Technician:	ER

	<u>Run 1A</u>	<u>Run 2A</u>	<u>Run 3A</u>
Temp ID:	CM46	CM46	CM46
Meter ID:	CM46	CM46	CM46
Pitot ID:	S8-031A	S8-031A	S8-031A
Nozzle Diameter (Inches):	0.319	0.319	0.319
Meter Calibration Date:	9/5/2023	9/5/2023	9/5/2023
Meter Calibration Factor (Y):	1.004	1.004	1.004
Meter Orifice Setting (Delta H):	1.744	1.744	1.744
Nozzle Kit ID Number and Material:	Glass #39	Glass #39	Glass #39
Pitot Tube Coefficient:		0.820	
Probe Length (Feet):		4.0	
Probe Liner Material:		Glass	
Sample Plane:		Horizontal	
Port Length (Inches):		8.50	
Port Size (Diameter, Inches):		6.00	
Port Type:		Nipple	
Duct Shape:		Circular	
Diameter (Feet):		10.9	
Duct Area (Square Feet):		93.313	
Upstream Diameters:		4.13	
Downstream Diameters:		16.52	
Number of Ports Sampled:		4	
Number of Points per Port:		3	
Minutes per Point:		5.0	
Minutes per Reading:		5.0	
Total Number of Traverse Points:		12	
Test Length (Minutes):		60	
Train Type:		Anderson Box	
Source Condition:		Mill On	
Diluent Model/Serial Number:		CAI 700 and MKS 2030	
Moisture Balance ID:		LV3	
# of Runs		3	

Run 1A - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train A)
 Source Condition: Mill On

Date: 10/11/23
 Start Time: 8:30
 End Time: 9:39

DRY GAS METER CONDITIONS

STACK CONDITIONS

H:	2.56	in. H ₂ O	Static Pressure	-0.40	in. H ₂ O
Meter Temperature, Tm:	67.3	F	Flue Pressure (Ps):	26.83	in. Hg. abs.
Sqrt P:	0.670	in. H ₂ O	Carbon Dioxide:	16.8	%
Stack Temperature, Ts:	227.2	F	Oxygen:	10.4	%
Meter Volume, Vm:	56.432	ft ³	Nitrogen:	72.80	%
Meter Volume, Vmstd:	51.292	dscf	Gas Weight dry, Md:	31.104	lb/lb mole
Meter Volume, Vwstd:	10.536	wscf	Gas Weight wet, Ms:	28.871	lb/lb mole
Isokinetic Variance:	101.6	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, Vs:	44.219	fps
Nozzle Diameter:	0.319	in inches	Volumetric Flow:	247,575	acfm
Barometric Pressure:	26.86	in Hg	Volumetric Flow:	141,517	dscfm
			Volumetric Flow:	170,587	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3533.6	ml	Silica Initial Wt.	856.3	grams
Final Impinger Content:	3744.1	ml	Silica Final Wt.	869.5	grams
Impinger Difference:	210.5	ml	Silica Difference:	13.2	grams
Total Water Gain:	223.7		Moisture, Bws:	0.170	

Port-Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp Inlet °F	Meter Temp Outlet °F	Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
1-1	8:30:00	0.53	3.00	360.819	225	65	65	259	263	58
1-2	8:35:00	0.52	2.90	365.820	227	65	65	259	258	47
1-3	8:40:00	0.35	2.00	370.930	227	65	65	261	260	53
	8:45:00			375.090						
2-1	8:48:00	0.54	3.10	375.090	226	66	66	260	260	55
2-2	8:53:00	0.50	2.80	380.260	228	66	66	263	260	55
2-3	8:58:00	0.36	2.00	385.220	228	67	67	260	259	53
	9:03:00			389.370						
3-1	9:06:00	0.51	2.90	389.370	224	68	68	260	260	56
3-2	9:11:00	0.45	2.60	394.420	229	68	68	264	261	59
3-3	9:16:00	0.36	2.00	399.710	229	68	68	262	260	60
	9:21:00			403.320						
4-1	9:24:00	0.51	2.90	403.320	228	69	69	263	261	55
4-2	9:29:00	0.44	2.50	408.260	228	70	70	258	260	54
4-3	9:34:00	0.35	2.00	412.810	227	70	70	261	260	57
	9:39:00			417.251						

Total	1:00:00			56.432		67.3	67.3			
Average			2.56		227.2		67.3			
Min			2.00		224.0		65.0			
Max			3.10		229.0		70.0			

Impinger Weight Sheet - Run 1A

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train A)
Project #: M234105
Date: 10/11/2023
Test Method: 26A
Weighed/Measured By: RICHS
Balance ID: LV3

Scale Calibration Check Date: 10/11/2023
Scale Calibration Check (see QS-6.05C for procedure)

must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	832.7	736.6	96.1
0.1N H2SO4	756.4	683.5	72.9
Empty	663.3	640.4	22.9
0.1N NaOH	789.3	776.1	13.2
0.1N NaOH	702.4	697.0	5.4
Silica Gel	869.5	856.3	13.2

<u>3,744.1</u> Liquid Final	<u>3,533.6</u> Liquid Initial	<u>210.5</u> Liquid Gain
<u>869.5</u> Silica Final	<u>856.3</u> Silica Initial	<u>13.2</u> Silica Gain

Run 2A - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train A)
 Source Condition: Mill On

Date: 10/11/23
 Start Time: 10:10
 End Time: 11:21

DRY GAS METER CONDITIONS

STACK CONDITIONS

H:	2.60	In. H ₂ O	Static Pressure	-0.40	in. H ₂ O
Meter Temperature, Tm:	74.8	F	Flue Pressure (Ps):	26.83	in. Hg. abs.
Sqrt P:	0.667	In. H ₂ O	Carbon Dioxide:	16.8	%
Stack Temperature, Ts:	223.5	F	Oxygen:	10.4	%
Meter Volume, Vm:	56.974	ft ³	Nitrogen:	72.8	%
Meter Volume, Vmstd:	51.056	dscf	Gas Weight dry, Md:	31.104	lb/lb mole
Meter Volume, Vwstd:	10.937	wscf	Gas Weight wet, Ms:	28.792	lb/lb mole
Isokinetic Variance:	101.9	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, Vs:	43.966	fps
Nozzle Diameter:	0.319	in inches	Volumetric Flow:	246,159	acfm
Barometric Pressure:	26.86	in Hg	Volumetric Flow:	140,438	dscfm
			Volumetric Flow:	170,521	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3642.1	ml	Silica Initial Wt.	882.5	grams
Final Impinger Content:	3857.2	ml	Silica Final Wt.	899.6	grams
Impinger Difference:	215.1	ml	Silica Difference:	17.1	grams
Total Water Gain:	232.2		Moisture, Bws:	0.176	

Port- Point No.	Clock Time	Velocity	Orifice	Actual	Stack	Meter Temp		Probe	Filter	Impinger
		Head Δp in. H ₂ O	ΔH in. H ₂ O	Meter Vol. ft ³	Temp °F	Inlet °F	Outlet °F	Temp °F	Exit Temp °F	Exit Temp °F
1-1	10:10:00	0.53	3.10	417.721	224	73	73	260	257	56
1-2	10:15:00	0.49	2.80	422.820	225	73	73	263	262	54
1-3	10:20:00	0.36	2.10	427.850	224	73	73	265	260	55
	10:25:00			432.120						
2-1	10:28:00	0.51	3.00	432.120	223	73	73	258	260	59
2-2	10:33:00	0.50	2.90	437.250	224	74	74	260	260	59
2-3	10:38:00	0.34	1.97	442.240	224	74	74	260	260	58
	10:43:00			446.310						
3-1	10:48:00	0.52	3.00	446.310	224	75	75	260	260	58
3-2	10:53:00	0.46	2.70	451.380	224	75	75	260	259	56
3-3	10:58:00	0.35	2.00	456.310	223	77	77	264	260	57
	11:03:00			460.510						
4-1	11:06:00	0.50	2.90	460.510	222	77	77	259	260	55
4-2	11:11:00	0.45	2.60	465.630	223	77	77	261	261	54
4-3	11:16:00	0.36	2.10	470.420	222	77	77	258	260	53
	11:21:00			474.695						

Total	1:00:00			56.974		74.8	74.8			
Average			2.60		223.5	74.8				
Min			1.97		222.0	73.0				
Max			3.10		225.0	77.0				

Impinger Weight Sheet - Run 2A

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train A)
Project #: M234105
Date: 10/11/2023
Test Method: 26A
Weighed/Measured By: RICHS
Balance ID: LV3

Scale Calibration Check Date: 10/11/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	852.3	752.0	100.3
0.1N H2SO4	859.5	790.5	69.0
Empty	654.9	630.0	24.9
0.1N NaOH	745.8	729.1	16.7
0.1N NaOH	744.7	740.5	4.2
Silica Gel	899.6	882.5	17.1

<u>3,857.2</u> Liquid Final	<u>3,642.1</u> Liquid Initial	<u>215.1</u> Liquid Gain
<u>899.6</u> Silica Final	<u>882.5</u> Silica Initial	<u>17.1</u> Silica Gain

Run 3A - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train A)
 Source Condition: Mill On

Date: 10/11/23
 Start Time: 11:45
 End Time: 12:54

DRY GAS METER CONDITIONS

STACK CONDITIONS

H:	2.60	In. H ₂ O	Static Pressure	-0.40	in. H ₂ O
Meter Temperature, Tm:	78.2	F	Flue Pressure (Ps):	26.83	in. Hg. abs.
Sqrt P:	0.666	In. H ₂ O	Carbon Dioxide:	16.7	%
Stack Temperature, Ts:	222.9	F	Oxygen:	10.4	%
Meter Volume, Vm:	57.397	ft ³	Nitrogen:	72.9	%
Meter Volume, Vmstd:	51.117	dscf	Gas Weight dry, Md:	31.088	lb/lb mole
Meter Volume, Vwstd:	10.499	wscf	Gas Weight wet, Ms:	28.858	lb/lb mole
Isokinetic Variance:	101.4	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, Vs:	43.876	fps
Nozzle Diameter:	0.319	in inches	Volumetric Flow:	245,651	acfm
Barometric Pressure:	26.86	in Hg	Volumetric Flow:	141,295	dscfm
			Volumetric Flow:	170,314	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3546.8	ml	Silica Initial Wt.	765.6	grams
Final Impinger Content:	3759.6	ml	Silica Final Wt.	775.7	grams
Impinger Difference:	212.8	ml	Silica Difference:	10.1	grams
Total Water Gain:	222.9		Moisture, Bws:	0.170	

Port- Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp Inlet °F	Meter Temp Outlet °F	Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
1-1	11:45:00	0.54	3.10	476.019	224	78	78	258	260	57
1-2	11:50:00	0.50	2.90	481.370	224	78	78	260	260	55
1-3	11:55:00	0.36	2.10	486.290	224	78	78	258	261	54
	12:00:00			490.620						
2-1	12:03:00	0.51	3.00	490.620	221	78	78	259	259	53
2-2	12:08:00	0.49	2.90	495.850	220	78	78	263	260	54
2-3	12:13:00	0.36	2.10	500.680	221	78	78	257	258	52
	12:18:00			505.090						
3-1	12:21:00	0.49	2.80	505.090	222	78	78	264	258	53
3-2	12:26:00	0.45	2.60	510.210	222	78	78	260	260	54
3-3	12:31:00	0.37	2.20	514.810	223	78	78	263	260	55
	12:36:00			519.330						
4-1	12:39:00	0.50	2.90	519.330	224	78	78	262	259	57
4-2	12:44:00	0.44	2.60	524.330	225	79	79	264	260	59
4-3	12:49:00	0.35	2.00	529.160	225	79	79	261	260	61
	12:54:00			533.416						

Total	1:00:00			57.397		78.2	78.2			
Average			2.60		222.9	78.2				
Min			2.00		220.0	78.0				
Max			3.10		225.0	79.0				

Impinger Weight Sheet - Run 3A

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train A)
Project #: M234105
Date: 10/11/2023
Test Method: 26A
Weighed/Measured By: RICHS
Balance ID: LV3

Scale Calibration Check Date: 10/11/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	893.1	745.1	148.0
0.1N H2SO4	735.1	685.1	50.0
Empty	653.3	645.3	8.0
0.1N NaOH	788.0	783.1	4.9
0.1N NaOH	690.1	688.2	1.9
Silica Gel	775.7	765.6	10.1

<u>3,759.6</u> Liquid Final	<u>3,546.8</u> Liquid Initial	<u>212.8</u> Liquid Gain
<u>775.7</u> Silica Final	<u>765.6</u> Silica Initial	<u>10.1</u> Silica Gain

Client:	Ash Grove Cement Company		
Facility:	Durkee Cement Plant		
Test Location:	Main Kiln (Train B)		
Project #:	M234105		
Test Method:	26A		
Test Engineer:	KAW		
Test Technician:	EROD		
	<u>Run 1B</u>	<u>Run 2B</u>	<u>Run 3B</u>
Meter ID:	CM54	CM54	CM54
Pitot ID:	S8-032A	S8-032A	S8-032A
Nozzle Diameter (Inches):	0.276	0.276	0.276
Meter Calibration Date:	9/20/2023	9/20/2023	9/20/2023
Meter Calibration Factor (Y):	0.986	0.986	0.986
Meter Orifice Setting (Delta H):	1.914	1.914	1.914
Nozzle Kit ID Number and Material:	uartz	uartz	uartz
Pitot Tube Coefficient:		0.822	
Probe Length (Feet):		4.0	
Probe Liner Material:		Glass	
Sample Plane:		Horizontal	
Port Length (Inches):		8.50	
Port Size (Diameter, Inches):		6.00	
Port Type:		Nipple	
Duct Shape:		Circular	
Diameter (Feet):		10.9	
Duct Area (Square Feet):		93.313	
Upstream Diameters:		4.13	
Downstream Diameters:		16.52	
Number of Ports Sampled:		4	
Number of Points per Port:		3	
Minutes per Point:		5.0	
Minutes per Reading:		5.0	
Total Number of Traverse Points:		12	
Test Length (Minutes):		60	
Train Type:		Anderson Box	
Source Condition:		Mill On	
Diluent Model/Serial Number:		CAI 700 and MKS 2030	
Moisture Balance ID:		LV4	
# of Runs		3	

Run 1B - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train B)
 Source Condition: Mill On

Date: 10/11/23
 Start Time: 8:30
 End Time: 9:39

DRY GAS METER CONDITIONS

STACK CONDITIONS

H:	1.53	in. H ₂ O	Static Pressure	-0.40	in. H ₂ O
Meter Temperature, Tm:	66.4	F	Flue Pressure (Ps):	26.83	in. Hg. abs.
Sqrt P:	0.670	in. H ₂ O	Carbon Dioxide:	16.8	%
Stack Temperature, Ts:	225.6	F	Oxygen:	10.4	%
Meter Volume, Vm:	42.933	ft ³	Nitrogen:	72.80	%
Meter Volume, Vmstd:	38.277	dscf	Gas Weight dry, Md:	31.104	lb/lb mole
Meter Volume, Vwstd:	8.158	wscf	Gas Weight wet, Ms:	28.802	lb/lb mole
Isokinetic Variance:	101.4	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, Vs:	44.374	fps
Nozzle Diameter:	0.276	in inches	Volumetric Flow:	248,439	acfm
Barometric Pressure:	26.86	in Hg	Volumetric Flow:	141,434	dscfm
			Volumetric Flow:	171,578	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3408.9	ml	Silica Initial Wt.	823.5	grams
Final Impinger Content:	3572.9	ml	Silica Final Wt.	832.7	grams
Impinger Difference:	164.0	ml	Silica Difference:	9.2	grams
Total Water Gain:	173.2		Moisture, Bws:	0.176	

Port- Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp Inlet °F	Meter Temp Outlet °F	Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
1-1	8:30:00	0.51	1.73	78.632	223	64	64	255	261	55
1-2	8:35:00	0.46	1.56	82.490	225	64	64	258	260	55
1-3	8:40:00	0.35	1.18	85.970	225	64	64	255	261	59
	8:45:00			89.150						
2-1	8:48:00	0.51	1.73	89.150	225	65	65	268	260	62
2-2	8:53:00	0.45	1.52	92.910	226	65	65	251	260	62
2-3	8:58:00	0.36	1.22	96.440	226	66	66	254	260	62
	9:03:00			99.700						
3-1	9:06:00	0.53	1.80	99.700	226	67	67	264	260	62
3-2	9:11:00	0.52	1.77	103.640	227	67	67	256	258	62
3-3	9:16:00	0.35	1.19	107.250	227	68	68	262	260	62
	9:21:00			110.560						
4-1	9:24:00	0.53	1.80	110.560	226	69	69	260	261	57
4-2	9:29:00	0.50	1.70	114.580	226	69	69	261	258	58
4-3	9:34:00	0.36	1.20	118.340	225	69	69	263	260	59
	9:39:00			121.565						

Total	1:00:00			42.933		66.4	66.4			
Average			1.53		225.6		66.4			
Min			1.18		223.0		64.0			
Max			1.80		227.0		69.0			

Impinger Weight Sheet - Run 1B

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train B)
Project #: M234105
Date: 10/11/2023
Test Method: 26A
Weighed/Measured By: RICHS
Balance ID: LV4

Scale Calibration Check Date: 10/11/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	250.0
500	500.0
750	750.0

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	832.1	743.3	88.8
0.1N H2SO4	738.6	685.2	53.4
Empty	654.1	640.0	14.1
0.1N NaOH	740.4	735.1	5.3
0.1N NaOH	607.7	605.3	2.4
Silica Gel	832.7	823.5	9.2

<u>3,572.9</u> Liquid Final	<u>3,408.9</u> Liquid Initial	<u>164.0</u> Liquid Gain
<u>832.7</u> Silica Final	<u>823.5</u> Silica Initial	<u>9.2</u> Silica Gain

Run 2B - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train B)
 Source Condition: Mill On

Date: 10/11/23
 Start Time: 10:10
 End Time: 11:21

DRY GAS METER CONDITIONS

STACK CONDITIONS

H:	1.50	In. H ₂ O	Static Pressure	-0.40	in. H ₂ O
Meter Temperature, Tm:	71.0	F	Flue Pressure (Ps):	26.83	in. Hg. abs.
Sqrt P:	0.659	In. H ₂ O	Carbon Dioxide:	16.8	%
Stack Temperature, Ts:	222.3	F	Oxygen:	10.4	%
Meter Volume, Vm:	42.572	ft ³	Nitrogen:	72.8	%
Meter Volume, Vmstd:	37.621	dscf	Gas Weight dry, Md:	31.104	lb/lb mole
Meter Volume, Vwstd:	8.393	wscf	Gas Weight wet, Ms:	28.714	lb/lb mole
Isokinetic Variance:	101.8	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, Vs:	43.576	fps
Nozzle Diameter:	0.276	in inches	Volumetric Flow:	243,972	acfm
Barometric Pressure:	26.86	in Hg	Volumetric Flow:	138,415	dscfm
			Volumetric Flow:	169,295	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3474.1	ml	Silica Initial Wt.	828.6	grams
Final Impinger Content:	3641.0	ml	Silica Final Wt.	839.9	grams
Impinger Difference:	166.9	ml	Silica Difference:	11.3	grams
Total Water Gain:	178.2		Moisture, Bws:	0.182	

Port- Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp Inlet °F	Meter Temp Outlet °F	Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
1-1	10:10:00	0.50	1.72	122.056	223	71	71	262	262	55
1-2	10:15:00	0.46	1.59	125.910	222	72	72	250	260	57
1-3	10:20:00	0.37	1.28	129.570	222	72	72	253	260	55
	10:25:00			132.800						
2-1	10:28:00	0.51	1.76	132.800	223	72	72	259	261	59
2-2	10:33:00	0.45	1.55	136.600	223	72	72	251	262	56
2-3	10:38:00	0.34	1.17	140.210	223	72	72	252	261	55
	10:43:00			143.410						
3-1	10:48:00	0.52	1.79	143.410	223	72	72	261	260	61
3-2	10:53:00	0.47	1.62	147.240	223	72	72	256	259	59
3-3	10:58:00	0.37	1.27	150.960	222	71	71	263	259	58
	11:03:00			154.270						
4-1	11:06:00	0.49	1.69	154.270	222	70	70	257	260	60
4-2	11:11:00	0.43	1.48	157.960	221	68	69	255	261	59
4-3	11:16:00	0.33	1.13	161.470	221	68	68	255	260	60
	11:21:00			164.628						

Total	1:00:00			42.572		71.0	71.1			
Average			1.50		222.3	71.0				
Min			1.13		221.0	68.0				
Max			1.79		223.0	72.0				

Impinger Weight Sheet - Run 2B

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train B)
Project #: M234105
Date: 10/11/2023
Test Method: 26A
Weighed/Measured By: RICHS
Balance ID: LV4

Scale Calibration Check Date: 10/11/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	875.3	751.3	124.0
0.1N H2SO4	734.1	700.0	34.1
Empty	584.5	580.0	4.5
0.1N NaOH	756.6	754.7	1.9
0.1N NaOH	690.5	688.1	2.4
Silica Gel	839.9	828.6	11.3

<u>3,641.0</u> Liquid Final	<u>3,474.1</u> Liquid Initial	<u>166.9</u> Liquid Gain
<u>839.9</u> Silica Final	<u>828.6</u> Silica Initial	<u>11.3</u> Silica Gain

Run 3B - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train B)
 Source Condition: Mill On

Date: 10/11/23
 Start Time: 11:45
 End Time: 12:54

DRY GAS METER CONDITIONS

STACK CONDITIONS

H:	1.47	In. H ₂ O	Static Pressure	-0.40	in. H ₂ O
Meter Temperature, Tm:	63.3	F	Flue Pressure (Ps):	26.83	in. Hg. abs.
Sqrt P:	0.655	In. H ₂ O	Carbon Dioxide:	16.7	%
Stack Temperature, Ts:	220.6	F	Oxygen:	10.5	%
Meter Volume, Vm:	41.768	ft ³	Nitrogen:	72.8	%
Meter Volume, Vmstd:	37.451	dscf	Gas Weight dry, Md:	31.092	lb/lb mole
Meter Volume, Vwstd:	7.663	wscf	Gas Weight wet, Ms:	28.868	lb/lb mole
Isokinetic Variance:	100.6	%I	Excess Air:	---	%
Test Length:	60.00	in mins.	Gas Velocity, Vs:	43.133	fps
Nozzle Diameter:	0.276	in inches	Volumetric Flow:	241,492	acfm
Barometric Pressure:	26.86	in Hg	Volumetric Flow:	139,467	dscfm
			Volumetric Flow:	168,005	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3441.2	ml	Silica Initial Wt.	832.5	grams
Final Impinger Content:	3595.9	ml	Silica Final Wt.	840.5	grams
Impinger Difference:	154.7	ml	Silica Difference:	8.0	grams
Total Water Gain:	162.7		Moisture, Bws:	0.170	

Port- Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp Inlet °F	Meter Temp Outlet °F	Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
1-1	11:45:00	0.49	1.68	165.137	220	66	66	258	261	55
1-2	11:50:00	0.45	1.54	168.920	221	65	65	255	260	58
1-3	11:55:00	0.35	1.19	172.380	221	63	63	260	261	60
	12:00:00			175.580						
2-1	12:03:00	0.51	1.73	175.580	220	62	62	266	260	60
2-2	12:08:00	0.45	1.53	179.370	220	63	63	262	261	60
2-3	12:13:00	0.38	1.29	183.010	220	63	63	261	263	60
	12:18:00			186.210						
3-1	12:21:00	0.48	1.63	186.210	221	63	63	260	260	62
3-2	12:26:00	0.43	1.46	189.880	221	63	63	260	261	62
3-3	12:31:00	0.35	1.19	193.340	221	63	63	261	261	62
	12:36:00			196.530						
4-1	12:39:00	0.50	1.70	196.530	221	63	63	260	261	62
4-2	12:44:00	0.44	1.50	200.230	221	63	63	261	261	62
4-3	12:49:00	0.34	1.16	203.820	220	63	63	257	260	62
	12:54:00			206.905						

Total	1:00:00			41.768		63.3	63.3			
Average			1.47		220.6	63.3				
Min			1.16		220.0	62.0				
Max			1.73		221.0	66.0				

Impinger Weight Sheet - Run 3B

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train B)
Project #: M234105
Date: 10/11/2023
Test Method: 26A
Weighed/Measured By: RICHS
Balance ID: LV4

Scale Calibration Check Date: 10/11/2023
Scale Calibration Check (see QS-6.05C for procedure)

must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	864.8	747.5	117.3
0.1N H2SO4	723.1	694.1	29.0
Empty	650.0	644.5	5.5
0.1N NaOH	769.4	766.8	2.6
0.1N NaOH	588.6	588.3	0.3
Silica Gel	840.5	832.5	8.0

<u>3,595.9</u> Liquid Final	<u>3,441.2</u> Liquid Initial	<u>154.7</u> Liquid Gain
<u>840.5</u> Silica Final	<u>832.5</u> Silica Initial	<u>8.0</u> Silica Gain

Client:	Ash Grove Cement Company		
Facility:	Durkee Cement Plant		
Test Location:	Main Kiln (Train A)		
Project #:	M234105		
Test Method:	26A		
Test Engineer:	CPD		
Test Technician:	EROD		
	<u>Run 1A</u>	<u>Run 2A</u>	<u>Run 3A</u>
Temp ID:	CM46	CM46	CM46
Meter ID:	CM46	CM46	CM46
Pitot ID:	S8-031A	S8-031A	S8-031A
Nozzle Diameter (Inches):	0.319	0.319	0.319
Meter Calibration Date:	9/5/2023	9/5/2023	9/5/2023
Meter Calibration Factor (Y):	1.004	1.004	1.004
Meter Orifice Setting (Delta H):	1.744	1.744	1.744
Nozzle Kit ID Number and Material:	Glass #39	Glass #39	Glass #39
Pitot Tube Coefficient:		0.820	
Probe Length (Feet):		4.0	
Probe Liner Material:		Glass	
Sample Plane:		Horizontal	
Port Length (Inches):		8.50	
Port Size (Diameter, Inches):		6.00	
Port Type:		Nipple	
Duct Shape:		Circular	
Diameter (Feet):		10.9	
Duct Area (Square Feet):		93.313	
Upstream Diameters:		4.13	
Downstream Diameters:		16.52	
Number of Ports Sampled:		4	
Number of Points per Port:		3	
Minutes per Point:		5.0	
Minutes per Reading:		5.0	
Total Number of Traverse Points:		12	
Test Length (Minutes):		60	
Train Type:		Anderson Box	
Source Condition:		Mill Off	
Diluent Model/Serial Number:		CAI 700 and MKS 2030	
Moisture Balance ID:		LV3	
# of Runs		3	

Run 1A - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train A)
 Source Condition: Mill Off

Date: 10/12/23
 Start Time: 10:45
 End Time: 11:54

DRY GAS METER CONDITIONS

H: 2.05 in. H₂O
 Meter Temperature, Tm: 74.2 F
 Sqrt P: 0.617 in. H₂O
 Stack Temperature, Ts: 277.8 F
 Meter Volume, Vm: 50.389 ft³
 Meter Volume, Vmstd: 45.595 dscf
 Meter Volume, Vwstd: 10.885 wscf
 Isokinetic Variance: 103.8 %I
 Test Length: 60.00 in mins.
 Nozzle Diameter: 0.319 in inches
 Barometric Pressure: 27.13 in Hg

STACK CONDITIONS

Static Pressure -0.40 in. H₂O
 Flue Pressure (Ps): 27.10 in. Hg. abs.
 Carbon Dioxide: 18.8 %
 Oxygen: 8.9 %
 Nitrogen: 72.30 %
 Gas Weight dry, Md: 31.364 lb/lb mole
 Gas Weight wet, Ms: 28.788 lb/lb mole
 Excess Air: 87.365 %
 Gas Velocity, Vs: 42.037 fps
 Volumetric Flow: 235,358 acfm
 Volumetric Flow: 123,167 dscfm
 Volumetric Flow: 152,570 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3679.6 ml
 Final Impinger Content: 3894.8 ml
 Impinger Difference: 215.2 ml
 Silica Initial Wt. 854.4 grams
 Silica Final Wt. 870.3 grams
 Silica Difference: 15.9 grams
 Total Water Gain: 231.1
 Moisture, Bws: 0.193

Port- Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp Inlet °F	Meter Temp Outlet °F	Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
1-1	10:45:00	0.48	2.60	533.907	278	70	70	262	260	53
1-2	10:50:00	0.40	2.10	538.640	276	72	72	261	260	54
1-3	10:55:00	0.33	1.80	542.770	276	74	74	261	259	54
	11:00:00			546.830						
2-1	11:03:00	0.47	2.50	546.830	275	74	74	260	260	56
2-2	11:08:00	0.41	2.20	551.590	277	74	74	257	260	57
2-3	11:13:00	0.33	1.80	555.870	278	74	74	262	259	57
	11:18:00			559.820						
3-1	11:21:00	0.42	2.20	559.820	279	74	74	260	260	55
3-2	11:26:00	0.35	1.90	564.340	279	74	74	264	259	55
3-3	11:31:00	0.30	1.60	568.370	278	75	75	261	260	56
	11:36:00			571.880						
4-1	11:39:00	0.43	2.30	571.880	279	76	76	263	260	57
4-2	11:44:00	0.36	1.90	576.410	279	76	76	262	260	58
4-3	11:49:00	0.31	1.70	580.340	279	77	77	260	260	60
	11:54:00			584.296						

Total 1:00:00 50.389 74.2 74.2
 Average 2.05 277.8 74.2
 Min 1.60 275.0 70.0
 Max 2.60 279.0 77.0

Impinger Weight Sheet - Run 1A

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train A)
Project #: M234105
Date: 10/12/2023
Test Method: 26A
Weighed/Measured By: RICHS
Balance ID: LV3

Scale Calibration Check Date: 10/12/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	915.2	760.5	154.7
0.1N H2SO4	850.4	798.8	51.6
Empty	727.2	635.1	92.1
0.1N NaOH	692.0	714.7	-22.7
0.1N NaOH	710.0	770.5	-60.5
Silica Gel	870.3	854.4	15.9

<u>3,894.8</u> Liquid Final	<u>3,679.6</u> Liquid Initial	<u>215.2</u> Liquid Gain
<u>870.3</u> Silica Final	<u>854.4</u> Silica Initial	<u>15.9</u> Silica Gain

Run 2A - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train A)
 Source Condition: Mill Off

Date: 10/12/23
 Start Time: 12:15
 End Time: 13:24

DRY GAS METER CONDITIONS

H: 2.06 in. H₂O
 Meter Temperature, Tm: 76.6 F
 Sqrt P: 0.617 in. H₂O
 Stack Temperature, Ts: 281.0 F
 Meter Volume, Vm: 50.460 ft³
 Meter Volume, Vmstd: 45.455 dscf
 Meter Volume, Vwstd: 10.451 wscf
 Isokinetic Variance: 103.2 %I
 Test Length: 60.00 in mins.
 Nozzle Diameter: 0.319 in inches
 Barometric Pressure: 27.13 in Hg

STACK CONDITIONS

Static Pressure -0.40 in. H₂O
 Flue Pressure (Ps): 27.10 in. Hg. abs.
 Carbon Dioxide: 19.3 %
 Oxygen: 8.8 %
 Nitrogen: 71.9 %
 Gas Weight dry, Md: 31.440 lb/lb mole
 Gas Weight wet, Ms: 28.927 lb/lb mole
 Excess Air: 86.430 %
 Gas Velocity, Vs: 42.033 fps
 Volumetric Flow: 235,334 acfm
 Volumetric Flow: 123,491 dscfm
 Volumetric Flow: 151,885 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3560.7 ml
 Final Impinger Content: 3776.3 ml
 Impinger Difference: 215.6 ml
 Silica Initial Wt. 775.2 grams
 Silica Final Wt. 781.5 grams
 Silica Difference: 6.3 grams
 Total Water Gain: 221.9
 Moisture, Bws: 0.187

Port- Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp Inlet °F	Meter Temp Outlet °F	Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
1-1	12:15:00	0.46	2.50	585.051	278	77	77	262	259	56
1-2	12:20:00	0.39	2.10	589.740	279	77	77	260	263	55
1-3	12:25:00	0.32	1.70	593.850	278	77	77	261	262	56
	12:30:00			597.710						
2-1	12:33:00	0.48	2.60	597.710	278	76	76	262	260	56
2-2	12:38:00	0.40	2.20	602.460	278	76	76	261	260	57
2-3	12:43:00	0.34	1.80	606.760	277	76	76	260	260	58
	12:48:00			610.770						
3-1	12:51:00	0.43	2.30	610.770	279	76	76	260	260	59
3-2	12:56:00	0.37	2.00	615.380	280	76	76	264	259	60
3-3	13:01:00	0.31	1.70	619.320	282	77	77	261	260	60
	13:06:00			623.240						
4-1	13:09:00	0.44	2.30	623.240	287	77	77	261	261	55
4-2	13:14:00	0.34	1.80	627.810	288	77	77	261	261	56
4-3	13:19:00	0.31	1.70	631.750	288	77	77	264	259	58
	13:24:00			635.511						

Total 1:00:00 50.460 76.6 76.6
 Average 2.06 281.0 76.6
 Min 1.70 277.0 76.0
 Max 2.60 288.0 77.0

Impinger Weight Sheet - Run 2A

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train A)
Project #: M234105
Date: 10/12/2023
Test Method: 26A
Weighed/Measured By: RICHS
Balance ID: LV3

Scale Calibration Check Date: 10/12/2023
Scale Calibration Check (see QS-6.05C for procedure)

must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	890.6	749.3	141.3
0.1N H2SO4	740.6	683.6	57.0
Empty	650.1	641.7	8.4
0.1N NaOH	791.3	786.1	5.2
0.1N NaOH	703.7	700.0	3.7
Silica Gel	781.5	775.2	6.3

<u>3,776.3</u> Liquid Final	<u>3,560.7</u> Liquid Initial	<u>215.6</u> Liquid Gain
<u>781.5</u> Silica Final	<u>775.2</u> Silica Initial	<u>6.3</u> Silica Gain

Run 3A - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train A)
 Source Condition: Mill Off

Date: 10/12/23
 Start Time: 13:50
 End Time: 14:59

DRY GAS METER CONDITIONS

STACK CONDITIONS

H:	2.05	In. H ₂ O	Static Pressure	-0.40	in. H ₂ O
Meter Temperature, Tm:	76.9	F	Flue Pressure (Ps):	27.10	in. Hg. abs.
Sqrt P:	0.615	In. H ₂ O	Carbon Dioxide:	19.1	%
Stack Temperature, Ts:	282.2	F	Oxygen:	8.8	%
Meter Volume, Vm:	50.390	ft ³	Nitrogen:	72.1	%
Meter Volume, Vmstd:	45.363	dscf	Gas Weight dry, Md:	31.408	lb/lb mole
Meter Volume, Vwstd:	10.612	wscf	Gas Weight wet, Ms:	28.866	lb/lb mole
Isokinetic Variance:	103.6	%I	Excess Air:	85.985	%
Test Length:	60.00	in mins.	Gas Velocity, Vs:	41.987	fps
Nozzle Diameter:	0.319	in inches	Volumetric Flow:	235,074	acfm
Barometric Pressure:	27.13	in Hg	Volumetric Flow:	122,762	dscfm
			Volumetric Flow:	151,479	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3681.3	ml	Silica Initial Wt.	869.5	grams
Final Impinger Content:	3892.6	ml	Silica Final Wt.	883.5	grams
Impinger Difference:	211.3	ml	Silica Difference:	14.0	grams
Total Water Gain:	225.3		Moisture, Bws:	0.190	

Port- Point No.	Clock Time	Velocity	Orifice	Actual	Stack	Meter Temp		Probe	Filter	Impinger
		Head Δp in. H ₂ O	ΔH in. H ₂ O	Meter Vol. ft ³	Temp °F	Inlet °F	Outlet °F	Temp °F	Exit Temp °F	Exit Temp °F
1-1	13:50:00	0.48	2.60	636.038	284	77	77	263	258	57
1-2	13:55:00	0.41	2.20	640.710	283	77	77	261	262	55
1-3	14:00:00	0.34	1.80	645.170	282	77	77	264	261	53
	14:05:00			649.110						
2-1	14:08:00	0.46	2.50	649.110	282	76	76	261	261	55
2-2	14:13:00	0.39	2.10	653.750	282	76	76	263	260	55
2-3	14:18:00	0.33	1.80	657.970	282	77	77	261	260	56
	14:23:00			661.920						
3-1	14:26:00	0.41	2.20	661.920	281	77	77	258	260	58
3-2	14:31:00	0.34	1.80	666.320	281	77	77	262	260	57
3-3	14:36:00	0.31	1.70	670.140	281	77	77	258	261	58
	14:41:00			674.080						
4-1	14:44:00	0.42	2.30	674.080	282	77	77	259	260	59
4-2	14:49:00	0.35	1.90	678.410	283	77	77	261	260	60
4-3	14:54:00	0.32	1.70	682.480	283	78	78	261	260	62
	14:59:00			686.428						

Total	1:00:00			50.390		76.9	76.9			
Average			2.05		282.2	76.9				
Min			1.70		281.0	76.0				
Max			2.60		284.0	78.0				

Impinger Weight Sheet - Run 3A

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train A)
Project #: M234105
Date: 10/12/2023
Test Method: 26A
Weighed/Measured By: RICHS
Balance ID: LV3

Scale Calibration Check Date: 10/12/2023
Scale Calibration Check (see QS-6.05C for procedure)

must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	863.7	760.7	103.0
0.1N H2SO4	867.7	798.1	69.6
Empty	657.3	635.9	21.4
0.1N NaOH	747.5	735.4	12.1
0.1N NaOH	756.4	751.2	5.2
Silica Gel	883.5	869.5	14.0

<u>3,892.6</u> Liquid Final	<u>3,681.3</u> Liquid Initial	<u>211.3</u> Liquid Gain
<u>883.5</u> Silica Final	<u>869.5</u> Silica Initial	<u>14.0</u> Silica Gain

Client:	Ash Grove Cement Company		
Facility:	Durkee Cement Plant		
Test Location:	Main Kiln (Train B)		
Project #:	M234105		
Test Method:	26A		
Test Engineer:	KAW		
Test Technician:	EROD		
	<u>Run 1B</u>	<u>Run 2B</u>	<u>Run 3B</u>
Meter ID:	CM54	CM54	CM54
Pitot ID:	S8-032A	S8-032A	S8-032A
Nozzle Diameter (Inches):	0.329	0.329	0.329
Meter Calibration Date:	9/20/2023	9/20/2023	9/20/2023
Meter Calibration Factor (Y):	0.986	0.986	0.986
Meter Orifice Setting (Delta H):	1.914	1.914	1.914
Nozzle Kit ID Number and Material:	uartz	uartz	uartz
Pitot Tube Coefficient:		0.822	
Probe Length (Feet):		4.0	
Probe Liner Material:		Glass	
Sample Plane:		Horizontal	
Port Length (Inches):		8.50	
Port Size (Diameter, Inches):		6.00	
Port Type:		Nipple	
Duct Shape:		Circular	
Diameter (Feet):		10.9	
Duct Area (Square Feet):		93.313	
Upstream Diameters:		4.13	
Downstream Diameters:		16.52	
Number of Ports Sampled:		4	
Number of Points per Port:		3	
Minutes per Point:		5.0	
Minutes per Reading:		5.0	
Total Number of Traverse Points:		12	
Test Length (Minutes):		60	
Train Type:		Anderson Box	
Source Condition:		Mill Off	
Diluent Model/Serial Number:		CAI 700 and MKS 2030	
Moisture Balance ID:		LV4	
# of Runs		3	

Run 1B - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train B)
 Source Condition: Mill Off

Date: 10/12/23
 Start Time: 10:45
 End Time: 11:54

DRY GAS METER CONDITIONS

H: 2.29 in. H₂O
 Meter Temperature, Tm: 66.8 F
 Sqrt P: 0.598 in. H₂O
 Stack Temperature, Ts: 276.5 F
 Meter Volume, Vm: 52.140 ft³
 Meter Volume, Vmstd: 47.017 dscf
 Meter Volume, Vwstd: 11.770 wscf
 Isokinetic Variance: 104.2 %I

 Test Length: 60.00 in mins.
 Nozzle Diameter: 0.329 in inches
 Barometric Pressure: 27.13 in Hg

STACK CONDITIONS

Static Pressure -0.40 in. H₂O
 Flue Pressure (Ps): 27.10 in. Hg. abs.
 Carbon Dioxide: 18.8 %
 Oxygen: 8.9 %
 Nitrogen: 72.30 %
 Gas Weight dry, Md: 31.364 lb/lb mole
 Gas Weight wet, Ms: 28.688 lb/lb mole
 Excess Air: 87.365 %
 Gas Velocity, Vs: 40.901 fps
 Volumetric Flow: 228,994 acfm
 Volumetric Flow: 118,925 dscfm
 Volumetric Flow: 148,696 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3504.2 ml
 Final Impinger Content: 3742.8 ml
 Impinger Difference: 238.6 ml

 Silica Initial Wt. 839.5 grams
 Silica Final Wt. 850.8 grams
 Silica Difference: 11.3 grams

 Total Water Gain: 249.9
 Moisture, Bws: 0.200

Port- Point No.	Clock Time	Velocity	Orifice	Actual	Stack	Meter Temp		Probe	Filter	Impinger
		Head Δp in. H ₂ O	ΔH in. H ₂ O	Meter Vol. ft ³	Temp °F	Inlet °F	Outlet °F	Temp °F	Exit Temp °F	Exit Temp °F
1-1	10:45:00	0.40	2.57	207.576	276	69	69	263	261	55
1-2	10:50:00	0.35	2.25	212.240	275	69	69	251	260	55
1-3	10:55:00	0.28	1.80	216.510	274	69	69	262	260	58
	11:00:00			220.390						
2-1	11:03:00	0.42	2.68	220.390	277	67	67	265	261	62
2-2	11:08:00	0.38	2.42	225.070	277	65	65	250	260	57
2-3	11:13:00	0.30	1.91	229.530	277	64	64	265	262	53
	11:18:00			233.510						
3-1	11:21:00	0.41	2.60	233.510	277	64	64	264	261	55
3-2	11:26:00	0.39	2.48	238.100	277	64	64	260	260	52
3-3	11:31:00	0.34	2.17	242.690	277	66	66	264	260	53
	11:36:00			246.880						
4-1	11:39:00	0.40	2.56	246.880	277	68	68	258	259	54
4-2	11:44:00	0.35	2.24	251.490	277	68	68	260	260	55
4-3	11:49:00	0.29	1.86	255.800	277	68	68	261	260	56
	11:54:00			259.716						

Total 1:00:00 52.140 66.8 66.8
 Average 2.29 276.5 66.8
 Min 1.80 274.0 64.0
 Max 2.68 277.0 69.0

Impinger Weight Sheet - Run 1B

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train B)
Project #: M234105
Date: 10/12/2023
Test Method: 26A
Weighed/Measured By: RICHS
Balance ID: LV4

Scale Calibration Check Date: 10/12/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	934.4	779.5	154.9
0.1N H2SO4	755.0	689.1	65.9
Empty	594.8	583.6	11.2
0.1N NaOH	749.2	745.7	3.5
0.1N NaOH	709.4	706.3	3.1
Silica Gel	850.8	839.5	11.3

<u>3,742.8</u> Liquid Final	<u>3,504.2</u> Liquid Initial	<u>238.6</u> Liquid Gain
<u>850.8</u> Silica Final	<u>839.5</u> Silica Initial	<u>11.3</u> Silica Gain

Run 2B - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train B)
 Source Condition: Mill Off

Date: 10/12/23
 Start Time: 12:15
 End Time: 13:24

DRY GAS METER CONDITIONS

STACK CONDITIONS

H:	2.25	In. H ₂ O	Static Pressure	-0.40	in. H ₂ O
Meter Temperature, Tm:	59.1	F	Flue Pressure (Ps):	27.10	in. Hg. abs.
Sqrt P:	0.597	In. H ₂ O	Carbon Dioxide:	19.3	%
Stack Temperature, Ts:	277.0	F	Oxygen:	8.8	%
Meter Volume, Vm:	51.286	ft ³	Nitrogen:	71.9	%
Meter Volume, Vmstd:	46.924	dscf	Gas Weight dry, Md:	31.440	lb/lb mole
Meter Volume, Vwstd:	11.153	wscf	Gas Weight wet, Ms:	28.859	lb/lb mole
Isokinetic Variance:	103.5	%I	Excess Air:	86.430	%
Test Length:	60.00	in mins.	Gas Velocity, Vs:	40.722	fps
Nozzle Diameter:	0.329	in inches	Volumetric Flow:	227,991	acfm
Barometric Pressure:	27.13	in Hg	Volumetric Flow:	119,534	dscfm
			Volumetric Flow:	147,945	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3435.5	ml	Silica Initial Wt.	839.5	grams
Final Impinger Content:	3664.2	ml	Silica Final Wt.	847.6	grams
Impinger Difference:	228.7	ml	Silica Difference:	8.1	grams
Total Water Gain:	236.8		Moisture, Bws:	0.192	

Port- Point No.	Clock Time	Velocity Head Δp in. H ₂ O	Orifice ΔH in. H ₂ O	Actual Meter Vol. ft ³	Stack Temp °F	Meter Temp Inlet °F	Meter Temp Outlet °F	Probe Temp °F	Filter Exit Temp °F	Impinger Exit Temp °F
1-1	12:15:00	0.41	2.60	259.890	277	63	63	260	261	55
1-2	12:20:00	0.39	2.48	264.530	277	64	64	260	260	56
1-3	12:25:00	0.35	2.23	269.020	277	65	65	261	261	58
	12:30:00			273.300						
2-1	12:33:00	0.40	2.51	273.300	277	57	57	261	259	59
2-2	12:38:00	0.37	2.31	277.790	277	56	56	259	261	58
2-3	12:43:00	0.32	2.00	282.160	277	56	56	258	262	59
	12:48:00			286.170						
3-1	12:51:00	0.40	2.51	286.170	277	57	57	260	259	62
3-2	12:56:00	0.35	2.19	290.650	277	57	57	260	258	62
3-3	13:01:00	0.30	1.88	294.740	277	57	57	261	262	62
	13:06:00			298.800						
4-1	13:09:00	0.39	2.45	298.800	277	59	59	260	260	58
4-2	13:14:00	0.32	2.01	303.270	277	59	59	260	261	58
4-3	13:19:00	0.29	1.82	307.320	277	59	59	261	261	59
	13:24:00			311.176						

Total	1:00:00			51.286		59.1	59.1			
Average			2.25		277.0	59.1				
Min			1.82		277.0	56.0				
Max			2.60		277.0	65.0				

Impinger Weight Sheet - Run 2B

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln (Train B)
Project #: M234105
Date: 10/12/2023
Test Method: 26A
Weighed/Measured By: RICHS
Balance ID: LV4

Scale Calibration Check Date: 10/12/2023
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	908.8	749.1	159.7
0.1N H2SO4	745.2	691.9	53.3
Empty	652.7	643.2	9.5
0.1N NaOH	747.1	742.6	4.5
0.1N NaOH	610.4	608.7	1.7
Silica Gel	847.6	839.5	8.1

<u>3,664.2</u> Liquid Final	<u>3,435.5</u> Liquid Initial	<u>228.7</u> Liquid Gain
<u>847.6</u> Silica Final	<u>839.5</u> Silica Initial	<u>8.1</u> Silica Gain

Run 3B - Method 26A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train B)
 Source Condition: Mill Off

Date: 10/11/23
 Start Time: 13:50
 End Time: 14:59

DRY GAS METER CONDITIONS

STACK CONDITIONS

H:	2.24	In. H ₂ O	Static Pressure	-0.40	in. H ₂ O
Meter Temperature, Tm:	60.5	F	Flue Pressure (Ps):	27.10	in. Hg. abs.
Sqrt P:	0.595	In. H ₂ O	Carbon Dioxide:	19.1	%
Stack Temperature, Ts:	278.0	F	Oxygen:	8.8	%
Meter Volume, Vm:	51.331	ft ³	Nitrogen:	72.1	%
Meter Volume, Vmstd:	46.836	dscf	Gas Weight dry, Md:	31.408	lb/lb mole
Meter Volume, Vwstd:	10.847	wscf	Gas Weight wet, Ms:	28.887	lb/lb mole
Isokinetic Variance:	103.3	%I	Excess Air:	85.985	%
Test Length:	60.00	in mins.	Gas Velocity, Vs:	40.581	fps
Nozzle Diameter:	0.329	in inches	Volumetric Flow:	227,204	acfm
Barometric Pressure:	27.13	in Hg	Volumetric Flow:	119,548	dscfm
			Volumetric Flow:	147,235	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3506.8	ml	Silica Initial Wt.	850.6	grams
Final Impinger Content:	3722.2	ml	Silica Final Wt.	865.5	grams
Impinger Difference:	215.4	ml	Silica Difference:	14.9	grams
Total Water Gain:	230.3		Moisture, Bws:	0.188	

Port- Point No.	Clock Time	Velocity	Orifice	Actual	Stack	Meter Temp		Probe	Filter	Impinger
		Head Δp in. H ₂ O	ΔH in. H ₂ O	Meter Vol. ft ³	Temp °F	Inlet °F	Outlet °F	Temp °F	Exit Temp °F	Exit Temp °F
1-1	13:50:00	0.41	2.59	311.340	277	60	60	260	260	55
1-2	13:55:00	0.36	2.27	315.920	277	60	60	260	258	55
1-3	14:00:00	0.33	2.08	320.180	277	60	60	260	258	57
	14:05:00			324.360						
2-1	14:08:00	0.40	2.53	324.360	277	62	62	260	260	62
2-2	14:13:00	0.34	2.15	328.930	277	62	62	260	261	62
2-3	14:18:00	0.29	1.84	333.200	277	62	62	261	260	62
	14:23:00			336.990						
3-1	14:26:00	0.41	2.59	336.990	278	61	61	257	262	62
3-2	14:31:00	0.35	2.21	341.550	278	61	61	257	262	62
3-3	14:36:00	0.31	1.96	345.880	278	61	61	257	262	62
	14:41:00			349.950						
4-1	14:44:00	0.41	2.57	349.950	280	59	59	256	258	62
4-2	14:49:00	0.35	2.20	354.500	280	59	59	258	262	62
4-3	14:54:00	0.30	1.88	358.750	280	59	59	261	265	62
	14:59:00			362.671						

Total	1:00:00			51.331		60.5	60.5			
Average			2.24		278.0	60.5				
Min			1.84		277.0	59.0				
Max			2.59		280.0	62.0				

Impinger Weight Sheet - Run 3B

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Test Location: Main Kiln (Train B)
 Project #: M234105
 Date: 10/11/2023
 Test Method: 26A
 Weighed/Measured By: RICHS
 Balance ID: LV4

Scale Calibration Check Date: 10/12/2023
Scale Calibration Check (see QS-6.05C for procedure)

must be within ± 0.5g of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER	FINAL	INITIAL	GAIN
CONTENTS	MLS / GRAMS	MLS / GRAMS	MLS / GRAMS
0.1N H2SO4	925.3	767.5	157.8
0.1N H2SO4	744.2	696.6	47.6
Empty	590.5	583.4	7.1
0.1N NaOH	769.9	767.2	2.7
0.1N NaOH	692.3	692.1	0.2
Silica Gel	865.5	850.6	14.9

<u>3,722.2</u>	<u>3,506.8</u>	<u>215.4</u>
Liquid Final	Liquid Initial	Liquid Gain
<u>865.5</u>	<u>850.6</u>	<u>14.9</u>
Silica Final	Silica Initial	Silica Gain

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Test Location: Main Kiln
 Date: 10/11/23

Run 1

Spectrum	Time	FTIR Data				HF ppmvw	Cell Temp	Pressure	Analyzer Data O2 % (dry)
		H2O %	CO2 % (wet)	HCN ppmvw					
RUN1_000309.LAB	8:30	17.21	13.90	2.23	≤ 0.10	191.20	0.92	10.28	
RUN1_000310.LAB	8:31	17.25	14.13	2.22	≤ 0.10	191.21	0.92	10.23	
RUN1_000311.LAB	8:32	17.22	13.93	2.22	≤ 0.10	191.22	0.92	10.26	
RUN1_000312.LAB	8:33	17.26	14.02	2.24	≤ 0.10	191.21	0.92	10.29	
RUN1_000313.LAB	8:34	17.30	14.42	2.11	≤ 0.10	191.21	0.92	10.15	
RUN1_000314.LAB	8:35	17.15	14.11	2.25	≤ 0.10	191.26	0.92	10.23	
RUN1_000315.LAB	8:36	17.26	13.92	2.20	≤ 0.10	191.23	0.92	10.30	
RUN1_000316.LAB	8:37	17.27	13.95	2.18	≤ 0.10	191.21	0.92	10.26	
RUN1_000317.LAB	8:38	17.28	13.89	2.17	≤ 0.10	191.19	0.92	10.33	
RUN1_000318.LAB	8:39	17.27	14.25	2.21	≤ 0.10	191.21	0.92	10.22	
RUN1_000319.LAB	8:40	17.33	14.22	2.20	≤ 0.10	191.19	0.92	10.24	
RUN1_000320.LAB	8:41	17.40	13.93	2.20	≤ 0.10	191.21	0.92	10.31	
RUN1_000321.LAB	8:42	17.28	13.95	2.18	≤ 0.10	191.23	0.92	10.29	
RUN1_000322.LAB	8:43	17.45	13.97	2.20	≤ 0.10	191.24	0.92	10.27	
RUN1_000323.LAB	8:44	17.31	13.83	2.22	≤ 0.10	191.25	0.92	10.29	
RUN1_000324.LAB	8:45	17.19	13.91	2.28	≤ 0.10	191.25	0.92	10.36	
RUN1_000325.LAB	8:46	17.02	13.93	2.24	≤ 0.10	191.24	0.92	10.31	
RUN1_000326.LAB	8:47	17.03	13.96	2.27	≤ 0.10	191.23	0.92	10.36	
RUN1_000327.LAB	8:48	17.02	14.12	2.21	≤ 0.10	191.21	0.92	10.32	
RUN1_000328.LAB	8:49	16.94	13.83	2.28	≤ 0.10	191.22	0.92	10.32	
RUN1_000329.LAB	8:50	16.94	13.67	2.15	≤ 0.10	191.22	0.92	10.38	
RUN1_000330.LAB	8:51	17.11	13.98	2.23	≤ 0.10	191.24	0.92	10.43	
RUN1_000331.LAB	8:52	16.99	13.91	2.31	≤ 0.10	191.26	0.92	10.31	
RUN1_000332.LAB	8:53	17.07	14.11	2.26	≤ 0.10	191.32	0.92	10.34	
RUN1_000333.LAB	8:54	17.10	13.87	2.25	≤ 0.10	191.32	0.92	10.32	
RUN1_000334.LAB	8:55	17.10	13.89	2.26	≤ 0.10	191.26	0.92	10.35	
RUN1_000335.LAB	8:56	17.08	13.90	2.24	≤ 0.10	191.20	0.92	10.34	
RUN1_000336.LAB	8:57	17.13	13.84	2.23	≤ 0.10	191.18	0.92	10.36	
RUN1_000337.LAB	8:58	17.14	13.80	2.27	≤ 0.10	191.26	0.92	10.38	
RUN1_000338.LAB	8:59	17.08	13.89	2.30	≤ 0.10	191.34	0.92	10.33	
RUN1_000339.LAB	9:00	17.04	13.70	2.25	≤ 0.10	191.28	0.92	10.35	
RUN1_000340.LAB	9:01	17.20	13.67	2.17	≤ 0.10	191.34	0.92	10.34	
RUN1_000341.LAB	9:02	17.15	14.15	2.23	≤ 0.10	191.34	0.92	10.46	
RUN1_000342.LAB	9:03	17.14	14.27	2.23	≤ 0.10	191.35	0.92	10.34	
RUN1_000343.LAB	9:04	17.14	13.59	2.28	≤ 0.10	191.34	0.92	10.26	
RUN1_000344.LAB	9:05	17.02	13.47	2.17	≤ 0.10	191.32	0.92	10.36	
RUN1_000345.LAB	9:06	17.17	13.69	2.23	≤ 0.10	191.30	0.92	10.53	
RUN1_000346.LAB	9:07	17.23	13.87	2.25	≤ 0.10	191.27	0.92	10.53	
RUN1_000347.LAB	9:08	17.24	13.86	2.21	≤ 0.10	191.28	0.92	10.49	
RUN1_000348.LAB	9:09	17.22	13.67	2.21	≤ 0.10	191.31	0.92	10.44	
RUN1_000349.LAB	9:10	17.33	13.73	2.23	≤ 0.10	191.25	0.92	10.48	
RUN1_000350.LAB	9:11	17.41	13.81	2.21	≤ 0.10	191.19	0.92	10.50	
RUN1_000351.LAB	9:12	17.27	13.80	2.22	≤ 0.10	191.15	0.92	10.44	
RUN1_000352.LAB	9:13	17.16	13.51	2.18	≤ 0.10	191.15	0.92	10.44	
RUN1_000353.LAB	9:14	17.28	13.64	2.16	≤ 0.10	191.14	0.92	10.38	
RUN1_000354.LAB	9:15	17.32	13.67	2.13	≤ 0.10	190.96	0.92	10.52	
RUN1_000355.LAB	9:16	17.43	13.81	2.11	≤ 0.10	190.78	0.92	10.48	
RUN1_000356.LAB	9:17	17.30	13.88	2.07	≤ 0.10	190.73	0.92	10.47	
RUN1_000357.LAB	9:18	17.32	13.61	2.13	≤ 0.10	190.85	0.92	10.41	
RUN1_000358.LAB	9:19	17.30	13.60	2.08	≤ 0.10	191.04	0.92	10.37	
RUN1_000359.LAB	9:20	17.43	13.71	2.08	≤ 0.10	191.18	0.92	10.44	
RUN1_000360.LAB	9:21	17.32	13.69	2.09	≤ 0.10	191.16	0.92	10.51	
RUN1_000361.LAB	9:22	17.45	13.79	2.08	≤ 0.10	191.15	0.92	10.41	
RUN1_000362.LAB	9:23	17.33	13.75	2.15	≤ 0.10	191.13	0.92	10.51	
RUN1_000363.LAB	9:24	17.48	13.74	2.18	≤ 0.10	191.16	0.92	10.45	
RUN1_000364.LAB	9:25	17.29	13.81	2.18	≤ 0.10	191.20	0.92	10.44	
RUN1_000365.LAB	9:26	17.51	13.80	2.04	≤ 0.10	191.19	0.92	10.45	
RUN1_000366.LAB	9:27	17.34	13.82	2.04	≤ 0.10	191.18	0.92	10.41	
RUN1_000367.LAB	9:28	17.39	13.77	2.01	≤ 0.10	191.23	0.92	10.41	
RUN1_000368.LAB	9:29	17.22	13.57	2.02	≤ 0.10	191.28	0.92	10.42	
Average		17.23	13.86	2.19	≤ 0.10	191.20	0.92	10.37	

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Test Location: Main Kiln
 Date: 10/11/23

Run 2

Spectrum	Time	FTIR Data					Analyzer Data	
		H2O %	CO2 % (wet)	HCN ppmvw	HF ppmvw	Cell Temp	Pressure	O2 % (dry)
RUN2_000527.LAB	10:10	17.28	14.1	1.87	≤ 0.10	5.4	0.03	10.37
RUN2_000528.LAB	10:11	17.22	13.5	1.83	≤ 0.10	5.3	0.10	10.53
RUN2_000529.LAB	10:12	17.21	13.5	1.84	≤ 0.10	5.4	0.03	10.47
RUN2_000530.LAB	10:13	17.26	13.8	1.78	≤ 0.10	5.3	0.08	10.41
RUN2_000531.LAB	10:14	17.18	13.8	1.84	≤ 0.10	5.6	0.06	10.44
RUN2_000532.LAB	10:15	17.18	13.8	1.85	≤ 0.10	5.4	0.13	10.47
RUN2_000533.LAB	10:16	17.36	13.7	1.79	≤ 0.10	5.4	0.03	10.44
RUN2_000534.LAB	10:17	17.26	13.7	1.88	≤ 0.10	5.5	0.10	10.44
RUN2_000535.LAB	10:18	17.27	13.7	1.73	≤ 0.10	5.5	0.13	10.42
RUN2_000536.LAB	10:19	17.35	13.8	1.90	≤ 0.10	5.3	0.12	10.37
RUN2_000537.LAB	10:20	17.19	13.8	1.72	≤ 0.10	5.3	0.14	10.37
RUN2_000538.LAB	10:21	17.26	13.7	1.82	≤ 0.10	5.3	0.11	10.39
RUN2_000539.LAB	10:22	17.34	13.9	1.81	≤ 0.10	5.5	0.11	10.35
RUN2_000540.LAB	10:23	17.25	14.1	1.79	≤ 0.10	5.4	0.04	10.27
RUN2_000541.LAB	10:24	17.42	14.3	1.77	≤ 0.10	5.6	0.11	10.27
RUN2_000542.LAB	10:25	17.34	14.0	1.80	≤ 0.10	5.3	0.14	10.25
RUN2_000543.LAB	10:26	17.47	13.7	1.88	≤ 0.10	5.3	0.09	10.38
RUN2_000544.LAB	10:27	17.31	13.9	1.80	≤ 0.10	5.4	0.08	10.27
RUN2_000545.LAB	10:28	17.43	13.9	1.80	≤ 0.10	5.5	0.03	10.26
RUN2_000546.LAB	10:29	17.30	13.9	1.84	≤ 0.10	5.3	0.09	10.27
RUN2_000547.LAB	10:30	17.34	13.8	1.75	≤ 0.10	5.1	0.01	10.32
RUN2_000548.LAB	10:31	17.31	13.8	1.80	≤ 0.10	5.3	0.08	10.27
RUN2_000549.LAB	10:32	17.34	13.9	1.77	≤ 0.10	5.2	0.04	10.27
RUN2_000550.LAB	10:33	17.34	14.1	1.80	≤ 0.10	5.2	-0.04	10.27
RUN2_000551.LAB	10:34	17.40	13.8	1.70	≤ 0.10	5.1	0.09	10.30
RUN2_000552.LAB	10:35	17.25	13.5	1.70	≤ 0.10	5.0	0.12	10.37
RUN2_000553.LAB	10:36	17.34	13.7	1.68	≤ 0.10	5.1	0.02	10.43
RUN2_000554.LAB	10:37	17.42	13.8	1.76	≤ 0.10	5.2	0.07	10.37
RUN2_000555.LAB	10:38	17.38	14.0	1.82	≤ 0.10	5.2	-0.06	10.32
RUN2_000556.LAB	10:39	17.29	13.8	1.75	≤ 0.10	5.1	0.03	10.28
RUN2_000557.LAB	10:40	17.44	13.8	1.79	≤ 0.10	5.2	0.08	10.32
RUN2_000558.LAB	10:41	17.42	13.6	1.72	≤ 0.10	5.2	0.12	10.38
RUN2_000559.LAB	10:42	17.53	13.9	1.82	≤ 0.10	5.0	0.07	10.41
RUN2_000560.LAB	10:43	17.36	13.8	1.79	≤ 0.10	4.9	0.04	10.31
RUN2_000561.LAB	10:44	17.46	13.8	1.82	≤ 0.10	5.0	-0.01	10.33
RUN2_000562.LAB	10:45	17.55	13.7	1.78	≤ 0.10	5.0	0.09	10.38
RUN2_000563.LAB	10:46	17.50	13.7	1.80	≤ 0.10	5.0	0.06	10.39
RUN2_000564.LAB	10:47	17.52	13.9	1.83	≤ 0.10	4.9	0.13	10.41
RUN2_000565.LAB	10:48	17.61	14.1	1.80	≤ 0.10	4.9	0.07	10.31
RUN2_000566.LAB	10:49	17.59	14.0	1.81	≤ 0.10	5.0	0.11	10.34
RUN2_000567.LAB	10:50	17.41	13.9	1.74	≤ 0.10	4.9	0.04	10.32
RUN2_000568.LAB	10:51	17.39	13.7	1.72	≤ 0.10	4.8	0.05	10.29
RUN2_000569.LAB	10:52	17.66	13.8	1.85	≤ 0.10	4.9	0.01	10.35
RUN2_000570.LAB	10:53	17.63	14.1	1.80	≤ 0.10	4.9	0.05	10.37
RUN2_000571.LAB	10:54	17.60	14.0	1.80	≤ 0.10	4.9	0.04	10.31
RUN2_000572.LAB	10:55	17.59	13.6	1.82	≤ 0.10	4.9	0.04	10.27
RUN2_000573.LAB	10:56	17.58	13.8	1.88	≤ 0.10	4.8	0.12	10.34
RUN2_000574.LAB	10:57	17.70	13.8	1.82	≤ 0.10	4.6	0.03	10.39
RUN2_000575.LAB	10:58	17.70	13.9	1.81	≤ 0.10	4.9	0.16	10.34
RUN2_000576.LAB	10:59	17.38	13.8	1.81	≤ 0.10	4.9	0.03	10.34
RUN2_000577.LAB	11:00	17.32	13.5	1.78	≤ 0.10	4.8	0.05	10.27
RUN2_000578.LAB	11:01	17.51	13.9	1.78	≤ 0.10	4.8	-0.01	10.38
RUN2_000579.LAB	11:02	17.53	14.7	1.83	≤ 0.10	5.1	0.03	10.51
RUN2_000580.LAB	11:03	17.44	14.3	1.87	≤ 0.10	5.0	-0.05	10.26
RUN2_000581.LAB	11:04	17.18	13.7	1.78	≤ 0.10	5.1	0.09	10.13
RUN2_000582.LAB	11:05	17.36	13.8	1.84	≤ 0.10	4.9	-0.01	10.23
RUN2_000583.LAB	11:06	17.43	13.8	1.87	≤ 0.10	5.0	-0.01	10.38
RUN2_000584.LAB	11:07	17.58	14.1	1.91	≤ 0.10	4.9	0.06	10.31
RUN2_000585.LAB	11:08	17.52	14.1	1.94	≤ 0.10	4.9	0.02	10.33
RUN2_000586.LAB	11:09	17.55	13.8	1.88	≤ 0.10	4.9	0.07	10.25
Average		17.40	13.86	1.81	≤ 0.10	5.13	0.06	10.34

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Test Location: Main Kiln
 Date: 10/11/23

Run 3

Spectrum	Time	FTIR Data					Cell Temp	Pressure	Analyzer Data O2 % (dry)
		H2O %	CO2 % (wet)	HCN ppmvw	HF ppmvw				
RUN3_000657.LAB	11:45	17.56	13.7	1.72	≤ 0.10	4.6	0.13	10.31	
RUN3_000658.LAB	11:46	17.52	14.0	1.70	≤ 0.10	4.7	0.07	10.30	
RUN3_000659.LAB	11:47	17.66	13.8	1.72	≤ 0.10	4.6	0.07	10.33	
RUN3_000660.LAB	11:48	17.70	13.7	1.75	≤ 0.10	4.7	0.03	10.31	
RUN3_000661.LAB	11:49	17.48	13.7	1.73	≤ 0.10	4.6	0.09	10.37	
RUN3_000662.LAB	11:50	17.54	13.8	1.77	≤ 0.10	4.6	0.02	10.35	
RUN3_000663.LAB	11:51	17.73	13.7	1.74	≤ 0.10	4.6	0.11	10.37	
RUN3_000664.LAB	11:52	17.73	13.9	1.74	≤ 0.10	4.4	0.07	10.31	
RUN3_000665.LAB	11:53	17.75	13.6	1.69	≤ 0.10	4.4	0.10	10.38	
RUN3_000666.LAB	11:54	17.61	13.7	1.65	≤ 0.10	4.4	0.02	10.41	
RUN3_000667.LAB	11:55	17.51	13.6	1.62	≤ 0.10	4.4	0.11	10.48	
RUN3_000668.LAB	11:56	17.51	13.7	1.64	≤ 0.10	4.4	0.04	10.46	
RUN3_000669.LAB	11:57	17.55	13.9	1.64	≤ 0.10	4.4	0.15	10.38	
RUN3_000670.LAB	11:58	17.59	13.8	1.66	≤ 0.10	4.4	0.07	10.37	
RUN3_000671.LAB	11:59	17.65	13.7	1.63	≤ 0.10	4.4	0.11	10.44	
RUN3_000672.LAB	12:00	17.56	13.8	1.71	≤ 0.10	4.4	0.07	10.38	
RUN3_000673.LAB	12:01	17.49	13.8	1.73	≤ 0.10	4.7	0.15	10.39	
RUN3_000674.LAB	12:02	17.29	13.9	1.74	≤ 0.10	4.5	0.16	10.38	
RUN3_000675.LAB	12:03	17.27	13.8	1.69	≤ 0.10	4.5	0.15	10.38	
RUN3_000676.LAB	12:04	17.26	14.4	1.76	≤ 0.10	4.5	0.09	10.32	
RUN3_000677.LAB	12:05	17.20	13.8	1.70	≤ 0.10	4.4	0.19	10.39	
RUN3_000678.LAB	12:06	17.18	13.6	1.75	≤ 0.10	4.3	0.20	10.52	
RUN3_000679.LAB	12:07	17.18	13.6	1.73	≤ 0.10	4.5	0.21	10.53	
RUN3_000680.LAB	12:08	17.10	14.1	1.72	≤ 0.10	4.4	0.14	10.49	
RUN3_000681.LAB	12:09	16.93	14.2	1.61	≤ 0.10	4.4	0.21	10.38	
RUN3_000682.LAB	12:10	17.05	14.0	1.63	≤ 0.10	4.4	0.19	10.44	
RUN3_000683.LAB	12:11	17.00	13.7	1.68	≤ 0.10	4.4	0.20	10.47	
RUN3_000684.LAB	12:12	16.96	13.7	1.67	≤ 0.10	4.5	0.24	10.52	
RUN3_000685.LAB	12:13	16.91	13.9	1.69	≤ 0.10	4.5	0.20	10.53	
RUN3_000686.LAB	12:14	16.86	13.8	1.67	≤ 0.10	4.5	0.27	10.48	
RUN3_000687.LAB	12:15	16.85	13.8	1.70	≤ 0.10	4.3	0.27	10.50	
RUN3_000688.LAB	12:16	16.90	13.8	1.70	≤ 0.10	4.5	0.27	10.48	
RUN3_000689.LAB	12:17	16.99	13.8	1.60	≤ 0.10	4.4	0.22	10.48	
RUN3_000690.LAB	12:18	17.14	13.8	1.68	≤ 0.10	4.4	0.24	10.48	
RUN3_000691.LAB	12:19	16.99	14.0	1.75	≤ 0.10	4.4	0.23	10.48	
RUN3_000692.LAB	12:20	16.95	14.1	1.65	≤ 0.10	4.6	0.32	10.37	
RUN3_000693.LAB	12:21	17.01	13.8	1.71	≤ 0.10	4.5	0.32	10.36	
RUN3_000694.LAB	12:22	16.93	14.1	1.64	≤ 0.10	4.6	0.32	10.36	
RUN3_000695.LAB	12:23	16.80	14.3	1.62	≤ 0.10	4.5	0.27	10.34	
RUN3_000696.LAB	12:24	16.82	14.2	1.65	≤ 0.10	4.6	0.33	10.27	
RUN3_000697.LAB	12:25	16.73	13.8	1.63	≤ 0.10	4.6	0.30	10.31	
RUN3_000698.LAB	12:26	16.75	13.9	1.55	≤ 0.10	4.6	0.23	10.38	
RUN3_000699.LAB	12:27	16.81	13.9	1.65	≤ 0.10	4.6	0.19	10.40	
RUN3_000700.LAB	12:28	16.85	14.1	1.57	≤ 0.10	4.7	0.23	10.40	
RUN3_000701.LAB	12:29	16.67	14.1	1.61	≤ 0.10	4.8	0.30	10.37	
RUN3_000702.LAB	12:30	16.58	14.1	1.66	≤ 0.10	4.7	0.24	10.30	
RUN3_000703.LAB	12:31	16.60	14.1	1.59	≤ 0.10	5.1	0.20	10.36	
RUN3_000704.LAB	12:32	16.54	14.1	1.64	≤ 0.10	4.8	0.27	10.36	
RUN3_000705.LAB	12:33	16.48	14.2	1.53	≤ 0.10	4.9	0.19	10.33	
RUN3_000706.LAB	12:34	16.51	13.9	1.70	≤ 0.10	4.8	0.23	10.36	
RUN3_000707.LAB	12:35	16.74	13.7	1.59	≤ 0.10	4.7	0.18	10.36	
RUN3_000708.LAB	12:36	17.12	13.7	1.58	≤ 0.10	4.6	0.19	10.45	
RUN3_000709.LAB	12:37	17.40	13.8	1.67	≤ 0.10	4.6	0.17	10.56	
RUN3_000710.LAB	12:38	17.34	14.0	1.57	≤ 0.10	4.5	0.11	10.47	
RUN3_000711.LAB	12:39	17.36	13.4	1.61	≤ 0.10	4.4	0.09	10.40	
RUN3_000712.LAB	12:40	17.52	13.7	1.61	≤ 0.10	4.4	0.14	10.35	
RUN3_000713.LAB	12:41	17.49	13.9	1.61	≤ 0.10	4.3	0.10	10.52	
RUN3_000714.LAB	12:42	17.49	13.8	1.63	≤ 0.10	4.2	0.09	10.39	
RUN3_000715.LAB	12:43	17.56	13.7	1.64	≤ 0.10	4.3	0.22	10.36	
RUN3_000716.LAB	12:44	17.47	13.9	1.71	≤ 0.10	4.2	0.12	10.33	
Average		17.18	13.87	1.66	≤ 0.10	4.52	0.17	10.40	

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Test Location: Main Kiln
 Date: 10/12/23

Run 1

Spectrum	Time	FTIR Data					Analyzer Data	
		H2O %	CO2 % (wet)	HCN ppmvw	HF ppmvw	Cell Temp	Pressure	O2 % (dry)
RUN1_000440.LAB	10:45	19.84	14.74	2.05	≤ 0.10	190.83	0.94	8.99
RUN1_000441.LAB	10:46	19.83	14.73	1.99	≤ 0.10	190.82	0.94	9.07
RUN1_000442.LAB	10:47	19.80	14.83	2.04	≤ 0.10	190.84	0.94	9.06
RUN1_000443.LAB	10:48	19.80	14.90	2.04	≤ 0.10	190.84	0.94	8.99
RUN1_000444.LAB	10:49	19.79	14.76	1.99	≤ 0.10	190.83	0.94	9.03
RUN1_000445.LAB	10:50	19.80	14.77	1.99	≤ 0.10	190.80	0.94	9.05
RUN1_000446.LAB	10:51	19.82	14.97	1.99	≤ 0.10	190.81	0.94	9.02
RUN1_000447.LAB	10:52	19.82	14.86	2.06	≤ 0.10	190.84	0.94	8.95
RUN1_000448.LAB	10:53	19.86	15.13	2.15	≤ 0.10	190.84	0.94	8.96
RUN1_000449.LAB	10:54	19.83	15.30	2.11	≤ 0.10	190.82	0.94	8.88
RUN1_000450.LAB	10:55	19.87	15.21	2.09	≤ 0.10	190.77	0.93	8.87
RUN1_000451.LAB	10:56	19.79	14.97	2.11	≤ 0.10	190.76	0.94	8.81
RUN1_000452.LAB	10:57	19.78	14.86	2.05	≤ 0.10	190.72	0.94	8.91
RUN1_000453.LAB	10:58	19.88	14.97	2.13	≤ 0.10	190.67	0.94	8.95
RUN1_000454.LAB	10:59	19.83	14.93	2.09	≤ 0.10	190.69	0.94	8.89
RUN1_000455.LAB	11:00	19.90	15.00	2.09	≤ 0.10	190.68	0.94	8.91
RUN1_000456.LAB	11:01	19.91	14.78	2.11	≤ 0.10	190.74	0.93	8.85
RUN1_000457.LAB	11:02	19.95	14.92	2.11	≤ 0.10	190.74	0.94	8.94
RUN1_000458.LAB	11:03	19.95	15.49	2.09	≤ 0.10	190.73	0.94	8.91
RUN1_000459.LAB	11:04	19.90	15.19	2.11	≤ 0.10	190.73	0.94	8.75
RUN1_000460.LAB	11:05	19.84	14.85	2.11	≤ 0.10	190.73	0.94	8.75
RUN1_000461.LAB	11:06	19.92	14.91	2.06	≤ 0.10	190.74	0.94	8.89
RUN1_000462.LAB	11:07	19.97	15.00	2.09	≤ 0.10	190.73	0.94	8.94
RUN1_000463.LAB	11:08	19.93	15.24	2.05	≤ 0.10	190.74	0.94	8.81
RUN1_000464.LAB	11:09	19.93	15.04	2.10	≤ 0.10	190.76	0.94	8.74
RUN1_000465.LAB	11:10	19.94	14.93	2.12	≤ 0.10	190.77	0.94	8.77
RUN1_000466.LAB	11:11	19.91	14.99	2.10	≤ 0.10	190.77	0.93	8.81
RUN1_000467.LAB	11:12	19.84	15.09	2.06	≤ 0.10	190.75	0.93	8.86
RUN1_000468.LAB	11:13	19.80	14.96	2.11	≤ 0.10	190.82	0.94	8.88
RUN1_000469.LAB	11:14	19.82	14.91	2.10	≤ 0.10	190.84	0.94	8.89
RUN1_000470.LAB	11:15	19.95	14.90	2.11	≤ 0.10	190.84	0.94	8.98
RUN1_000471.LAB	11:16	19.83	14.97	2.13	≤ 0.10	190.84	0.93	8.97
RUN1_000472.LAB	11:17	19.79	15.03	2.10	≤ 0.10	190.81	0.93	8.94
RUN1_000473.LAB	11:18	19.81	15.02	2.16	≤ 0.10	190.84	0.93	8.94
RUN1_000474.LAB	11:19	19.80	14.92	2.07	≤ 0.10	190.84	0.94	8.97
RUN1_000475.LAB	11:20	19.81	14.76	2.07	≤ 0.10	190.79	0.94	8.96
RUN1_000476.LAB	11:21	19.79	14.68	2.04	≤ 0.10	190.56	0.93	8.96
RUN1_000477.LAB	11:22	19.82	15.09	2.09	≤ 0.10	190.36	0.94	9.03
RUN1_000478.LAB	11:23	19.84	15.11	2.03	≤ 0.10	190.28	0.94	9.02
RUN1_000479.LAB	11:24	19.79	14.85	2.11	≤ 0.10	190.43	0.94	8.95
RUN1_000480.LAB	11:25	19.83	14.82	2.03	≤ 0.10	190.57	0.94	8.89
RUN1_000481.LAB	11:26	19.83	14.93	2.03	≤ 0.10	190.59	0.93	8.95
RUN1_000482.LAB	11:27	19.81	15.15	2.10	≤ 0.10	190.63	0.94	9.02
RUN1_000483.LAB	11:28	19.86	15.00	2.03	≤ 0.10	190.63	0.93	8.97
RUN1_000484.LAB	11:29	19.93	15.04	2.10	≤ 0.10	190.67	0.94	8.94
RUN1_000485.LAB	11:30	19.99	14.94	2.12	≤ 0.10	190.72	0.93	8.88
RUN1_000486.LAB	11:31	20.00	15.21	2.08	≤ 0.10	190.74	0.94	8.87
RUN1_000487.LAB	11:32	20.04	15.63	2.16	≤ 0.10	190.76	0.93	8.82
RUN1_000488.LAB	11:33	20.07	15.40	2.13	≤ 0.10	190.74	0.94	8.79
RUN1_000489.LAB	11:34	20.07	15.37	2.11	≤ 0.10	190.74	0.93	8.70
RUN1_000490.LAB	11:35	20.04	15.46	2.14	≤ 0.10	190.73	0.94	8.58
RUN1_000491.LAB	11:36	20.02	15.50	2.13	≤ 0.10	190.75	0.94	8.62
RUN1_000492.LAB	11:37	19.96	15.24	2.11	≤ 0.10	190.83	0.93	8.59
RUN1_000493.LAB	11:38	19.96	15.02	2.10	≤ 0.10	190.84	0.93	8.57
RUN1_000494.LAB	11:39	20.03	15.38	2.07	≤ 0.10	190.84	0.93	8.61
RUN1_000495.LAB	11:40	19.94	15.43	2.07	≤ 0.10	190.83	0.93	8.70
RUN1_000496.LAB	11:41	19.84	15.19	2.07	≤ 0.10	190.84	0.93	8.79
RUN1_000497.LAB	11:42	19.80	14.95	2.10	≤ 0.10	190.83	0.94	8.65
RUN1_000498.LAB	11:43	19.81	14.99	2.03	≤ 0.10	190.83	0.94	8.65
RUN1_000499.LAB	11:44	19.81	15.23	2.06	≤ 0.10	190.84	0.94	8.77
Average		19.88	15.04	2.08	≤ 0.10	190.75	0.94	8.87

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Test Location: Main Kiln
 Date: 10/12/23

Run 2

Spectrum	Time	FTIR Data					Cell Temp	Pressure	Analyzer Data O2 % (dry)
		H2O %	CO2 % (wet)	HCN ppmvw	HF ppmvw				
RUN2_000581.LAB	12:15	19.56	15.3	2.10	≤	0.10	1.1	0.16	8.76
RUN2_000582.LAB	12:16	19.57	15.1	2.11	≤	0.10	1.1	0.24	8.93
RUN2_000583.LAB	12:17	19.63	15.1	2.05	≤	0.10	1.1	0.18	8.90
RUN2_000584.LAB	12:18	19.63	15.2	2.03	≤	0.10	1.1	0.21	8.93
RUN2_000585.LAB	12:19	19.65	15.2	2.08	≤	0.10	1.1	0.20	8.94
RUN2_000586.LAB	12:20	19.66	15.2	2.06	≤	0.10	1.1	0.20	8.96
RUN2_000587.LAB	12:21	19.68	15.1	2.05	≤	0.10	1.1	0.29	8.90
RUN2_000588.LAB	12:22	19.67	15.1	2.05	≤	0.10	1.1	0.19	8.95
RUN2_000589.LAB	12:23	19.72	15.2	2.08	≤	0.10	1.1	0.25	8.98
RUN2_000590.LAB	12:24	19.69	15.5	2.00	≤	0.10	1.1	0.16	8.90
RUN2_000591.LAB	12:25	19.67	15.2	2.00	≤	0.10	1.1	0.21	8.81
RUN2_000592.LAB	12:26	19.66	14.9	2.05	≤	0.10	1.1	0.14	8.91
RUN2_000593.LAB	12:27	19.70	15.1	2.01	≤	0.10	1.2	0.20	8.97
RUN2_000594.LAB	12:28	19.69	15.2	1.93	≤	0.10	1.2	0.20	8.87
RUN2_000595.LAB	12:29	19.75	15.1	2.07	≤	0.10	1.1	0.21	8.91
RUN2_000596.LAB	12:30	19.73	15.2	2.02	≤	0.10	1.1	0.18	8.89
RUN2_000597.LAB	12:31	19.72	15.2	2.01	≤	0.10	1.2	0.21	8.88
RUN2_000598.LAB	12:32	19.75	15.3	2.06	≤	0.10	1.2	0.18	8.89
RUN2_000599.LAB	12:33	19.77	15.8	2.04	≤	0.10	1.1	0.18	8.79
RUN2_000600.LAB	12:34	19.72	15.3	2.05	≤	0.10	1.2	0.25	8.68
RUN2_000601.LAB	12:35	19.74	14.9	2.11	≤	0.10	1.2	0.24	8.78
RUN2_000602.LAB	12:36	19.78	15.1	2.07	≤	0.10	1.2	0.18	8.96
RUN2_000603.LAB	12:37	19.80	15.3	2.05	≤	0.10	1.1	0.22	8.93
RUN2_000604.LAB	12:38	19.79	15.6	2.07	≤	0.10	1.1	0.19	8.86
RUN2_000605.LAB	12:39	19.76	15.3	2.04	≤	0.10	1.1	0.18	8.80
RUN2_000606.LAB	12:40	19.78	15.2	2.05	≤	0.10	1.2	0.21	8.78
RUN2_000607.LAB	12:41	19.87	15.4	1.98	≤	0.10	1.1	0.20	8.90
RUN2_000608.LAB	12:42	19.85	15.4	2.04	≤	0.10	1.2	0.21	8.88
RUN2_000609.LAB	12:43	19.29	15.5	2.14	≤	0.10	1.2	0.18	8.85
RUN2_000610.LAB	12:44	16.56	16.0	1.97	≤	0.10	1.7	0.21	8.80
RUN2_000611.LAB	12:45	16.30	15.9	1.99	≤	0.10	1.2	0.24	8.79
RUN2_000612.LAB	12:46	17.93	15.8	1.91	≤	0.10	1.3	0.21	8.89
RUN2_000613.LAB	12:47	18.70	16.0	1.97	≤	0.10	1.3	0.21	8.96
RUN2_000614.LAB	12:48	18.70	16.0	2.02	≤	0.10	1.2	0.25	8.82
RUN2_000615.LAB	12:49	18.71	15.8	2.05	≤	0.10	1.3	0.21	8.61
RUN2_000616.LAB	12:50	18.65	15.7	1.97	≤	0.10	1.3	0.23	8.55
RUN2_000617.LAB	12:51	18.64	15.6	1.97	≤	0.10	1.3	0.21	8.61
RUN2_000618.LAB	12:52	18.70	16.1	2.00	≤	0.10	1.3	0.26	8.70
RUN2_000619.LAB	12:53	18.74	16.2	2.00	≤	0.10	1.3	0.20	8.73
RUN2_000620.LAB	12:54	18.68	15.7	1.91	≤	0.10	1.2	0.20	8.63
RUN2_000621.LAB	12:55	18.66	15.7	1.89	≤	0.10	1.2	0.18	8.52
RUN2_000622.LAB	12:56	18.68	15.9	1.92	≤	0.10	1.2	0.17	8.60
RUN2_000623.LAB	12:57	18.61	15.9	1.91	≤	0.10	1.2	0.24	8.72
RUN2_000624.LAB	12:58	18.62	15.7	1.89	≤	0.10	1.2	0.27	8.68
RUN2_000625.LAB	12:59	18.90	15.6	1.96	≤	0.10	1.2	0.26	8.63
RUN2_000626.LAB	13:00	19.17	15.3	1.99	≤	0.10	1.3	0.27	8.66
RUN2_000627.LAB	13:01	19.25	15.7	2.05	≤	0.10	1.2	0.27	8.72
RUN2_000628.LAB	13:02	19.34	16.3	2.06	≤	0.10	1.2	0.27	8.77
RUN2_000629.LAB	13:03	19.40	15.8	2.07	≤	0.10	1.2	0.23	8.82
RUN2_000630.LAB	13:04	19.45	15.5	2.12	≤	0.10	1.7	0.32	8.62
RUN2_000631.LAB	13:05	19.48	15.7	2.05	≤	0.10	1.3	0.24	8.47
RUN2_000632.LAB	13:06	19.48	16.1	2.05	≤	0.10	1.4	0.27	8.61
RUN2_000633.LAB	13:07	19.46	16.1	2.06	≤	0.10	1.4	0.24	8.65
RUN2_000634.LAB	13:08	19.53	15.8	2.07	≤	0.10	1.5	0.19	8.63
RUN2_000635.LAB	13:09	19.53	15.7	2.10	≤	0.10	1.5	0.23	8.49
RUN2_000636.LAB	13:10	19.54	15.8	2.08	≤	0.10	1.4	0.25	8.48
RUN2_000637.LAB	13:11	19.54	15.9	2.04	≤	0.10	1.5	0.21	8.53
RUN2_000638.LAB	13:12	19.55	15.9	2.07	≤	0.10	1.5	0.26	8.53
RUN2_000639.LAB	13:13	19.57	15.9	2.06	≤	0.10	1.3	0.28	8.58
RUN2_000640.LAB	13:14	19.54	15.8	2.02	≤	0.10	1.8	0.21	8.56
Average		19.28	15.54	2.03	≤	0.10	1.23	0.22	8.77

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Test Location: Main Kiln
 Date: 10/12/23



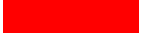
Run 3




Spectrum	Time	FTIR Data					Analyzer Data	
		H2O %	CO2 % (wet)	HCN ppmvw	HF ppmvw	Cell Temp	Pressure	O2 % (dry)
RUN3_000708.LAB	13:50	19.47	15.4	2.07	≤ 0.10	1.1	0.13	8.61
RUN3_000709.LAB	13:51	19.52	15.7	2.14	≤ 0.10	1.1	0.18	8.59
RUN3_000710.LAB	13:52	19.51	15.4	2.10	≤ 0.10	1.1	0.23	8.69
RUN3_000711.LAB	13:53	19.58	15.2	2.09	≤ 0.10	1.2	0.24	8.65
RUN3_000712.LAB	13:54	19.59	15.5	2.01	≤ 0.10	1.2	0.17	8.59
RUN3_000713.LAB	13:55	19.58	15.7	2.08	≤ 0.10	1.2	0.24	8.56
RUN3_000714.LAB	13:56	19.57	15.8	2.13	≤ 0.10	1.2	0.15	8.52
RUN3_000715.LAB	13:57	19.56	15.6	2.06	≤ 0.10	1.2	0.17	8.56
RUN3_000716.LAB	13:58	19.56	15.4	2.04	≤ 0.10	1.2	0.21	8.66
RUN3_000717.LAB	13:59	19.54	15.6	2.01	≤ 0.10	1.2	0.19	8.68
RUN3_000718.LAB	14:00	19.50	15.3	2.07	≤ 0.10	1.2	0.18	8.81
RUN3_000719.LAB	14:01	19.56	15.6	2.02	≤ 0.10	1.2	0.24	8.75
RUN3_000720.LAB	14:02	19.54	15.9	2.01	≤ 0.10	1.3	0.18	8.58
RUN3_000721.LAB	14:03	19.51	15.7	2.04	≤ 0.10	1.2	0.16	8.66
RUN3_000722.LAB	14:04	19.46	16.0	2.05	≤ 0.10	1.2	0.22	8.65
RUN3_000723.LAB	14:05	19.42	15.8	2.02	≤ 0.10	1.1	0.18	8.64
RUN3_000724.LAB	14:06	19.38	15.2	2.02	≤ 0.10	1.1	0.15	8.82
RUN3_000725.LAB	14:07	19.31	15.0	1.98	≤ 0.10	1.2	0.25	9.00
RUN3_000726.LAB	14:08	19.36	15.5	2.00	≤ 0.10	1.2	0.10	9.02
RUN3_000727.LAB	14:09	19.35	15.6	1.98	≤ 0.10	1.1	0.18	8.85
RUN3_000728.LAB	14:10	19.32	15.2	1.97	≤ 0.10	1.1	0.18	8.89
RUN3_000729.LAB	14:11	19.30	15.1	1.98	≤ 0.10	1.1	0.13	8.97
RUN3_000730.LAB	14:12	19.36	15.3	2.03	≤ 0.10	1.1	0.13	9.01
RUN3_000731.LAB	14:13	19.41	15.3	2.01	≤ 0.10	1.1	0.14	8.94
RUN3_000732.LAB	14:14	19.47	15.3	1.99	≤ 0.10	1.1	0.14	8.89
RUN3_000733.LAB	14:15	19.47	15.3	2.01	≤ 0.10	1.2	0.16	8.83
RUN3_000734.LAB	14:16	19.51	15.2	2.07	≤ 0.10	1.1	0.09	8.80
RUN3_000735.LAB	14:17	19.58	15.4	2.00	≤ 0.10	1.1	0.16	8.82
RUN3_000736.LAB	14:18	19.59	15.5	2.05	≤ 0.10	1.2	0.16	8.73
RUN3_000737.LAB	14:19	19.58	15.4	1.97	≤ 0.10	1.2	0.14	8.66
RUN3_000738.LAB	14:20	19.53	15.2	2.05	≤ 0.10	1.2	0.17	8.70
RUN3_000739.LAB	14:21	19.57	15.4	2.02	≤ 0.10	1.1	0.20	8.77
RUN3_000740.LAB	14:22	19.53	15.2	1.96	≤ 0.10	1.2	0.11	8.69
RUN3_000741.LAB	14:23	19.55	15.4	1.96	≤ 0.10	1.1	0.16	8.76
RUN3_000742.LAB	14:24	19.54	15.3	1.95	≤ 0.10	1.1	0.14	8.75
RUN3_000743.LAB	14:25	19.58	15.5	2.01	≤ 0.10	1.2	0.15	8.75
RUN3_000744.LAB	14:26	19.56	15.9	2.02	≤ 0.10	1.2	0.17	8.69
RUN3_000745.LAB	14:27	19.59	15.5	2.01	≤ 0.10	1.2	0.14	8.59
RUN3_000746.LAB	14:28	19.60	15.6	1.94	≤ 0.10	1.2	0.18	8.63
RUN3_000747.LAB	14:29	19.62	15.5	2.01	≤ 0.10	1.2	0.12	8.59
RUN3_000748.LAB	14:30	19.56	15.2	2.00	≤ 0.10	1.1	0.21	8.53
RUN3_000749.LAB	14:31	19.53	15.4	1.93	≤ 0.10	1.3	0.14	8.62
RUN3_000750.LAB	14:32	19.49	15.8	1.93	≤ 0.10	1.2	0.17	8.74
RUN3_000751.LAB	14:33	19.51	15.6	1.94	≤ 0.10	1.1	0.13	8.63
RUN3_000752.LAB	14:34	19.50	15.0	2.00	≤ 0.10	1.1	0.13	8.55
RUN3_000753.LAB	14:35	18.86	15.0	1.97	≤ 0.10	1.1	0.12	8.71
RUN3_000754.LAB	14:36	16.45	15.6	1.90	≤ 0.10	1.1	0.19	8.91
RUN3_000755.LAB	14:37	16.22	16.0	1.83	≤ 0.10	1.2	0.16	8.88
RUN3_000756.LAB	14:38	16.19	16.0	1.80	≤ 0.10	1.2	0.19	8.88
RUN3_000757.LAB	14:39	16.23	15.6	1.85	≤ 0.10	1.2	0.17	8.82
RUN3_000758.LAB	14:40	16.88	15.6	1.89	≤ 0.10	1.2	0.32	8.80
RUN3_000759.LAB	14:41	17.57	15.6	1.87	≤ 0.10	1.2	0.14	8.89
RUN3_000760.LAB	14:42	18.26	15.4	1.87	≤ 0.10	1.2	0.17	8.86
RUN3_000761.LAB	14:43	18.74	15.3	1.97	≤ 0.10	1.1	0.23	8.79
RUN3_000762.LAB	14:44	18.92	15.1	2.04	≤ 0.10	1.2	0.21	8.77
RUN3_000763.LAB	14:45	19.18	15.3	2.03	≤ 0.10	1.2	0.18	8.73
RUN3_000764.LAB	14:46	19.34	15.6	2.00	≤ 0.10	1.1	0.24	8.80
RUN3_000765.LAB	14:47	19.42	15.5	2.04	≤ 0.10	1.1	0.24	8.74
RUN3_000766.LAB	14:48	19.52	15.1	2.03	≤ 0.10	1.1	0.15	8.59
RUN3_000767.LAB	14:49	19.56	15.0	2.02	≤ 0.10	1.1	0.19	8.54
Average		19.15	15.45	2.00	≤ 0.10	1.16	0.17	8.74

Stratification Test Results Summary
Ash Grove Cement Company
Durkee Cement Plant
Main Kiln
October 11, 2023

Number of Ports Sampled: 1
Number of Points per Port: 3
Total Number of Traverse Points: 3

Port No.	Point No.	Time	O ₂ %	Actual % Difference O ₂ %	Mean Difference O ₂ %
1	1	8:09	10.55	0.25	0.03
	2	8:11	10.55	0.25	0.03
	3	8:13	10.47	0.51	0.05
Average			10.52		

One point traverse (5% difference) 
Three point traverse (0.4, 1.2, and 2.0 meters), 10% difference 
Twelve point traverse (Method 1 points) 10% difference 

One point traverse (0.3% mean difference) 
Three point traverse (0.4, 1.2, and 2.0 meters), 0.5% mean difference for O₂ 
Twelve point traverse (Method 1 points) 0.5% mean difference for O₂ 

Method 1 and 2 Cyclonic Flow Check Data

Project Number M233901
Client: Ash Grove Cement Company
Facility: Montana City Cement Plant
Location: Main Kiln (Train A)
Pitot ID: S8-031A
Pitot Coefficient: 0.820
Probe Length: 10

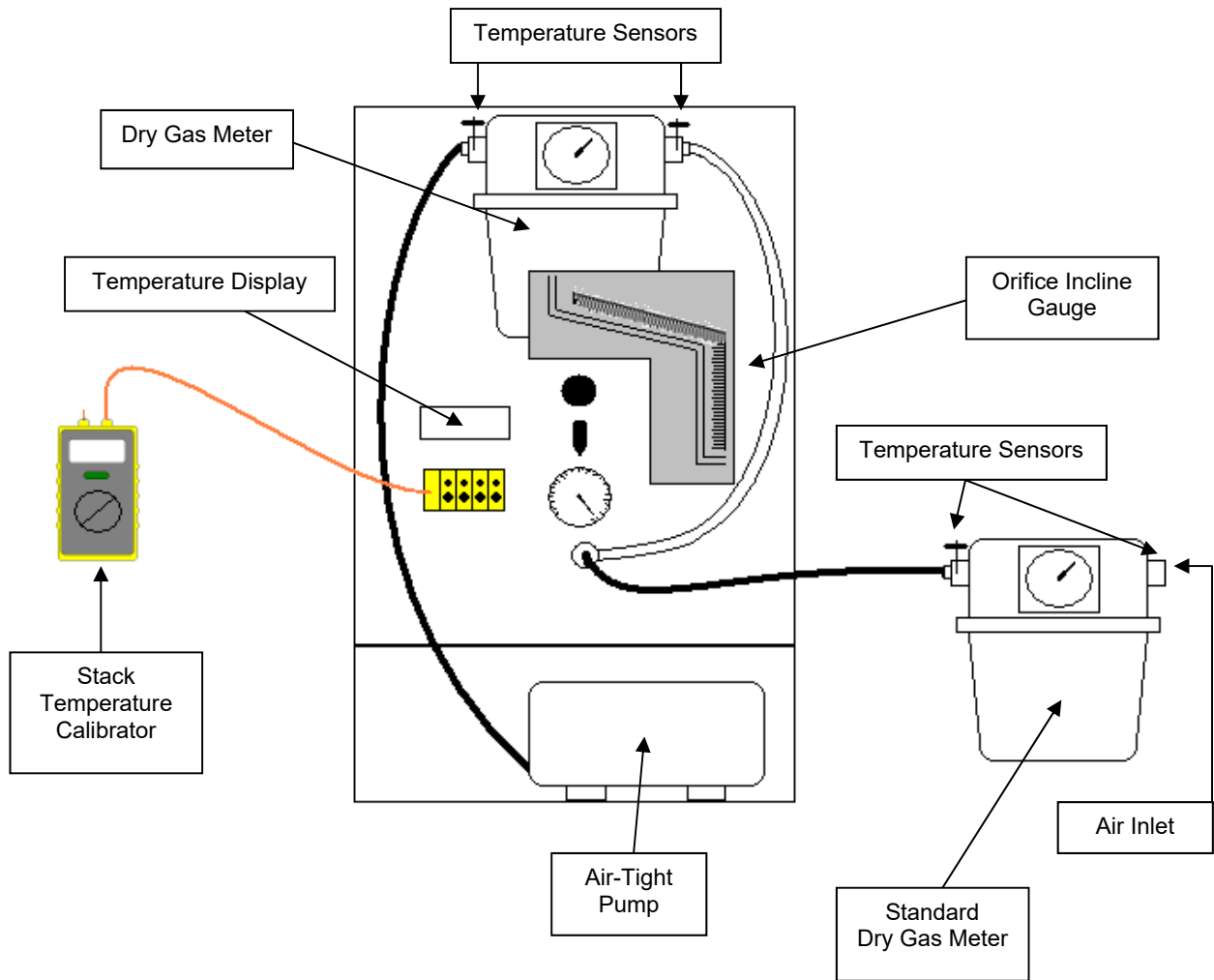
Source Condition: Normal
Run No.: 1
Date: 9/26/2023
Start Time: 14:07
End Time: 14:22
RM Testers: NJC
Port Length: 5.50

Port	Point	DP (in. H ₂ O)	Sqrt. DP	Temp (°F)	Yaw (o)	Velocity (V)	Port	Point	DP (in. H ₂ O)	Sqrt. DP	Temp (°F)	Yaw (o)	Velocity (V)
A	1	0.23	0.4796	345.0	6.0	33.24	B	1	0.28	0.5292	350.0	7.0	36.79
A	2	0.25	0.5000	348.0	6.0	34.72	B	2	0.29	0.5385	351.0	7.0	37.46
A	3	0.26	0.5099	351.0	5.0	35.47	B	3	0.29	0.5385	353.0	6.0	37.51
A	4	0.28	0.5292	354.0	5.0	36.88	B	4	0.30	0.5477	354.0	7.0	38.17
A	5	0.29	0.5385	355.0	5.0	37.55	B	5	0.29	0.5385	356.0	5.0	37.58
A	6	0.28	0.5292	356.0	4.0	36.92	B	6	0.28	0.5292	356.0	5.0	36.92
A	7	0.25	0.5000	357.0	4.0	34.91	B	7	0.26	0.5099	357.0	5.0	35.60
A	8	0.24	0.4899	357.0	3.0	34.21	B	8	0.23	0.4796	357.0	3.0	33.49
A	9	0.23	0.4796	357.0	2.0	33.49	B	9	0.22	0.4690	356.0	2.0	32.73
A	10	0.20	0.4472	356.0	1.0	31.21	B	10	0.20	0.4472	354.0	2.0	31.17
A	11	0.20	0.4472	356.0	1.0	31.21	B	11	0.16	0.4000	354.0	1.0	27.88
A	12	0.16	0.4000	354.0	2.0	27.88	B	12	0.14	0.3742	354.0	1.0	26.08

Average Yaw Angle 4.0 °

Appendix G - Calibration Data

Dry Gas Meter/Control Module Calibration Diagram



Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM46
 Standard Meter No. 25125408
 Standard Meter (Y) 0.99800

Date: September 5, 2023
 Calibrated By: DV
 Barometric Pressure: 28.09

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		109.822	84.911	80	79	79					
Initial		104.567	79.639	79	77	77					
Difference	1 0.20	5.255	5.272	80	78	78	78	19	36	0.991	1.714
Final		115.015	90.033	81	80	80					
Initial		109.822	84.911	80	79	79					
Difference	2 0.50	5.193	5.122	81	80	80	80	12	26	1.009	1.767
Final		120.336	95.378	81	81	81					
Initial		115.015	90.033	81	80	80					
Difference	3 0.70	5.321	5.345	81	81	81	81	10	39	0.991	1.729
Final		125.421	100.386	82	82	82					
Initial		120.336	95.378	81	81	81					
Difference	4 0.90	5.085	5.008	82	82	82	82	8	59	1.011	1.732
Final		133.350	108.110	82	83	83					
Initial		128.200	103.044	82	83	83					
Difference	5 1.20	5.150	5.066	82	83	83	83	7	51	1.013	1.717
Final		140.985	115.640	82	84	84					
Initial		133.350	108.110	82	83	83					
Difference	6 2.00	7.635	7.530	82	84	84	84	9	15	1.009	1.807

Average 1.004 1.744

Stack Temperature Sensor Calibration

Meter Box # : CM46 Name : DV

Ambient Temperature : 80.7 °F Date : September 5, 2023

Calibrator Model # : CL940A

Serial # : 526

Date Of Certification : December 28, 2022

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

Reference Source Temperature (°F)	Test Thermometer Temperature (°F)	Temperature Difference %
0	0	0.0
250	251	0.1
600	601	0.1
1200	1205	0.3

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM46
 Standard Meter No. 18654530
 Standard Meter (Y) 0.99730

Date: November 17, 2023
 Calibrated By: ER
 Barometric Pressure: 28.27

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		80.549	65.360	65	66	66					
Initial		75.465	60.345	65	65	65					
Difference	1 0.20	5.084	5.015	65	66	66	66	18	5	1.011	1.504
Final		85.559	70.350	66	67	67					
Initial		80.549	65.360	65	66	66					
Difference	2 0.50	5.010	5.000	66	67	67	67	12	10	1.002	1.752
Final		90.641	75.396	66	68	68					
Initial		85.559	70.350	66	67	67					
Difference	3 0.70	5.082	5.046	66	68	68	68	10	10	1.005	1.665
Final		95.668	80.395	66	68	68					
Initial		90.641	75.396	66	68	68					
Difference	4 0.90	5.027	5.002	66	68	68	68	9	10	1.004	1.777
Final		100.775	85.482	67	70	70					
Initial		95.668	80.395	66	68	68					
Difference	5 1.20	5.107	5.087	67	69	69	69	8	10	1.003	1.822
Final		75.465	60.345	65	65	65					
Initial		70.355	55.335	65	65	65					
Difference	6 2.00	5.110	5.010	65	65	65	65	6	5	1.012	1.686

Average **1.006** **1.701**

Stack Temperature Sensor Calibration			
Temperature ID :	100769	Name :	ER
Ambient Temperature, °F :	66.5	Date :	11/17/2023

Temperature Calibrator			
Model # :	CL23A	Certification Date:	May 1,2023
Serial # :	T-285668	Expiration Date:	May 2,2024

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

Reference Source Temperature (° F)	Test Thermometer Temperature (° F)	Temperature Difference %
0	0	0.0
250	251	0.1
600	601	0.1
1200	1205	0.3

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM54
 Standard Meter No. 18654530
 Standard Meter (Y) 0.99730

Date: September 20, 2023
 Calibrated By: IB
 Barometric Pressure: 27.90

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		46.811	120.965	85	88	88					
Initial		41.799	115.861	85	88	88					
Difference	1 0.20	5.012	5.104	85	88	88	88	20	5	0.984	1.998
Final		41.799	115.861	85	88	88					
Initial		36.741	110.737	86	87	87					
Difference	2 0.50	5.058	5.124	86	88	88	88	12	7	0.987	1.790
Final		36.741	110.737	86	87	87					
Initial		31.639	105.575	86	85	85					
Difference	3 0.70	5.102	5.162	86	86	86	86	10	27	0.984	1.841
Final		31.639	105.575	86	85	85					
Initial		26.613	100.508	86	85	85					
Difference	4 0.90	5.026	5.067	86	85	85	85	9	8	0.985	1.866
Final		26.613	100.508	86	85	85					
Initial		21.558	95.419	86	84	84					
Difference	5 1.20	5.055	5.089	86	85	85	85	8	15	0.985	2.009
Final		21.558	95.419	86	84	84					
Initial		16.526	90.382	85	84	84					
Difference	6 2.00	5.032	5.037	86	84	84	84	6	19	0.988	1.979

Average 0.986 1.914

Stack Temperature Sensor Calibration

Meter Box # : CM 54 Name : IB

Ambient Temperature : 88.7 °F Date : September 20, 2023

Calibrator Model # : CL940A

Serial # : 526

Date Of Certification : December 28, 2022

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

Reference Source Temperature (°F)	Test Thermometer Temperature (°F)	Temperature Difference %
0	0	0.0
250	250	0.0
600	599	0.1
1200	1200	0.0

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM54
 Standard Meter No. 18654530
 Standard Meter (Y) 0.99730

Date: December 1, 2023
 Calibrated By: ER
 Barometric Pressure: 28.09

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		85.075	50.792	63	62	62					
Initial		80.075	45.760	62	61	61					
Difference	1 0.20	5.000	5.032	63	62	62	62	18	10	0.989	1.576
Final		90.083	55.842	63	64	64					
Initial		85.075	50.792	63	62	62					
Difference	2 0.50	5.008	5.050	63	63	63	63	12	5	0.988	1.736
Final		95.085	60.901	64	65	65					
Initial		90.083	55.842	63	64	64					
Difference	3 0.70	5.002	5.059	64	65	65	65	10	0	0.986	1.667
Final		100.343	66.210	64	66	66					
Initial		95.085	60.901	64	65	65					
Difference	4 0.90	5.258	5.309	64	66	66	66	9	15	0.988	1.659
Final		105.348	71.269	64	67	67					
Initial		100.343	66.210	64	66	66					
Difference	5 1.20	5.005	5.059	64	67	67	67	8	0	0.988	1.823
Final		80.075	45.760	62	61	61					
Initial		75.060	40.748	61	61	61					
Difference	6 2.00	5.015	5.012	62	61	61	61	6	0	0.992	1.704

Average 0.988 1.694

Stack Temperature Sensor Calibration

Meter Box # : CM54 Name : ER

Ambient Temperature : 63.5 °F Date : December 1, 2023

Calibrator Model # : CL940

Serial # : 526

Date Of Certification : December 28, 2022

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

Reference Source Temperature (°F)	Test Thermometer Temperature (°F)	Temperature Difference %
0	1	0.2
250	252	0.3
600	602	0.2
1200	1205	0.3

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-A
 Probe Calibration Date: 07/10/17
 Test Point Location: center
 Ambient Temperature (°F): 77.8
 Barometric Pressure ("Hg): 29.23

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	77.8	1.18	0	0.82
2	60	0.80	77.8	1.18	0	0.82
3	60	0.81	77.8	1.18	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.81	77.8	2.63	0	0.82
2	90	1.81	77.8	2.62	0	0.82
3	90	1.81	77.8	2.63	0	0.82
Average (C _{p(avg-high)})						0.82

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.49\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.820



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-B
 Probe Calibration Date: 07/10/17
 Test Point Location: center
 Ambient Temperature (°F): 77.5
 Barometric Pressure ("Hg): 29.23

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	77.5	1.19	0	0.82
2	60	0.81	77.5	1.19	0	0.82
3	60	0.81	77.5	1.19	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.81	77.5	2.65	0	0.82
2	90	1.81	77.5	2.64	0	0.82
3	90	1.81	77.5	2.64	0	0.82
Average (C _{p(avg-high)})						0.82

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.55\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.818



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 6/8/2017
 Temperature (°F): 72.2
 Pressure ("Hg): 29.33
 Personnel: wgj
 Probe: S8-031-A

Wind Tunnel Target DP [I.W.C.]	Wind Tunnel Actual DP [I.W.C.]	S-Probe DP [I.W.C.]	C _p	C _{p(avg)}	C _p -C _{p(avg)}	σ _{max}	
0.81	0.81	1.19	0.818	0.818	0.000	0.001	Pass
0.81	0.81	1.19	0.818		0.000		
0.81	0.81	1.19	0.817		-0.001		
1.81	1.82	2.63	0.823	0.822	0.001	0.001	Pass
1.81	1.82	2.64	0.822		0.000		
1.81	1.81	2.64	0.820		-0.001		



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 6/8/2017
 Temperature (°F): 72.0
 Pressure ("Hg): 29.33
 Personnel: wgj
 Probe: S8-031-B

Wind Tunnel Target DP [I.W.C.]	Wind Tunnel Actual DP [I.W.C.]	S-Probe DP [I.W.C.]	C _p	C _{p(avg)}	C _p -C _{p(avg)}	σ _{max}	
0.81	0.81	1.19	0.817	0.816	0.000	0.001	Pass
0.81	0.81	1.19	0.817		0.000		
0.81	0.81	1.19	0.816		-0.001		
1.81	1.82	2.65	0.820	0.820	0.000	0.000	Pass
1.81	1.82	2.65	0.820		0.000		
1.81	1.82	2.64	0.820		0.000		



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-A
 Probe Calibration Date: 06/08/17
 Test Point Location: center
 Ambient Temperature (°F): 72.2
 Barometric Pressure ("Hg): 29.33

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	72.2	1.19	0	0.82
2	60	0.81	72.2	1.19	0	0.82
3	60	0.81	72.2	1.19	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.82	72.2	2.63	0	0.82
2	90	1.82	72.2	2.64	0	0.82
3	90	1.81	72.2	2.64	0	0.82
Average (C _{p(avg-high)})						0.82

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.51\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.820



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
 Wind Tunnel Location: Livonia, MI
 Probe Type: S-Type Pitot
 Probe ID: S8-031-B
 Probe Calibration Date: 06/08/17
 Test Point Location: center
 Ambient Temperature (°F): 72.0
 Barometric Pressure ("Hg): 29.33

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	72.0	1.19	0	0.82
2	60	0.81	72.0	1.19	0	0.82
3	60	0.81	72.0	1.19	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.82	72.0	2.65	0	0.82
2	90	1.82	72.0	2.65	0	0.82
3	90	1.82	72.0	2.64	0	0.82
Average (C _{p(avg-high)})						0.82

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.45\%}} \quad \text{Pass}$$

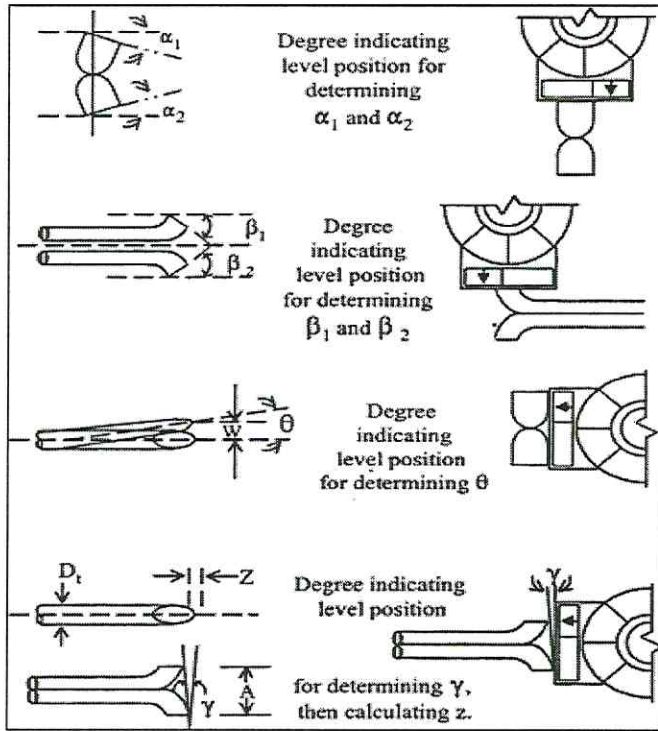
Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.818

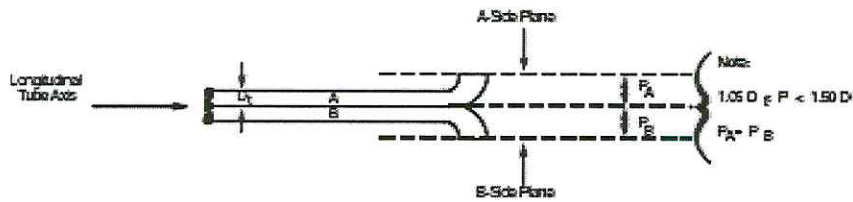


Airflow Sciences Corporation

Probe Inspection for Method 2



α_1	0.8 (°)	Pass
α_2	0.3 (°)	Pass
β_1	0.3 (°)	Pass
β_2	1.1 (°)	Pass
D_t	0.375 (")	Pass
P_a	0.459 (")	Pass
P_b	0.459 (")	Pass
z	<0.02 (")	Pass
w	0.005 (")	Pass



Certification

I certify that Type S probe ID **S8-031** meets or exceeds all specifications, criteria, and applicable design features.

Certified by: Craig Rood

Date: 6/8/2017



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 8/31/2017
Temperature (°F): 73.7
Pressure ("Hg): 29.43
Personnel: wgj
Probe: S8-032-A

Wind Tunnel Target DP [I.W.C.]	Wind Tunnel Actual DP [I.W.C.]	S-Probe DP [I.W.C.]	C _p	C _{p(avg)}	C _p -C _{p(avg)}	σ _{max}	
0.81	0.81	1.18	0.820	0.821	0.000	0.000	Pass
0.81	0.81	1.18	0.821		0.000		
0.81	0.81	1.18	0.821		0.000		
1.81	1.82	2.62	0.825	0.824	0.000	0.000	Pass
1.81	1.82	2.63	0.824		0.000		
1.81	1.82	2.63	0.824		0.000		



Airflow Sciences Corporation

Probe Calibration for Method 2

Data Collection and Analysis

Date: 8/31/2017
 Temperature (°F): 74.5
 Pressure ("Hg): 29.43
 Personnel: wgj
 Probe: S8-032-B

Wind Tunnel Target DP [I.W.C.]	Wind Tunnel Actual DP [I.W.C.]	S-Probe DP [I.W.C.]	C _p	C _{p(avg)}	C _p -C _{p(avg)}	σ _{max}	
0.81	0.81	1.19	0.819	0.819	0.000	0.000	Pass
0.81	0.81	1.19	0.819		0.000		
0.81	0.81	1.19	0.820		0.000		
1.81	1.81	2.63	0.823	0.823	0.000	0.000	Pass
1.81	1.82	2.63	0.823		0.000		
1.81	1.82	2.63	0.823		0.000		



Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
Wind Tunnel Location: Livonia, MI
Probe Type: S-Type Pitot
Probe ID: S8-032-A
Probe Calibration Date: 08/31/17
Test Point Location: center
Ambient Temperature (°F): 73.7
Barometric Pressure ("Hg): 29.43

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	73.7	1.18	0	0.82
2	60	0.81	73.7	1.18	0	0.82
3	60	0.81	73.7	1.18	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.82	73.7	2.62	0	0.82
2	90	1.82	73.7	2.63	0	0.82
3	90	1.82	73.7	2.63	0	0.82
Average (C _{p(avg-high)})						0.82

$$\text{\% Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.46\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
(2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.822

Airflow Sciences Corporation

Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation
Wind Tunnel Location: Livonia, MI
Probe Type: S-Type Pitot
Probe ID: S8-032-B
Probe Calibration Date: 08/31/17
Test Point Location: center
Ambient Temperature (°F): 74.5
Barometric Pressure ("Hg): 29.43

Repetition	Nominal Low Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (°)	
1	60	0.81	74.5	1.19	0	0.82
2	60	0.81	74.5	1.19	0	0.82
3	60	0.81	74.5	1.19	0	0.82
Average (C _{p(avg-low)})						0.82

Repetition	Nominal High Velocity Setting (ft/s)	Calibration Pitot		Tested Probe		Calculated C _p
		DP _{std} ("H ₂ O)	Temperature (°F)	DP ("H ₂ O)	Yaw Angle (deg)	
1	90	1.81	74.5	2.63	0	0.82
2	90	1.82	74.5	2.63	0	0.82
3	90	1.82	74.5	2.63	0	0.82
Average (C _{p(avg-high)})						0.82

$$\text{\% Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.43\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C_p values shall be within +/- 3 %.
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

C_p = 0.821

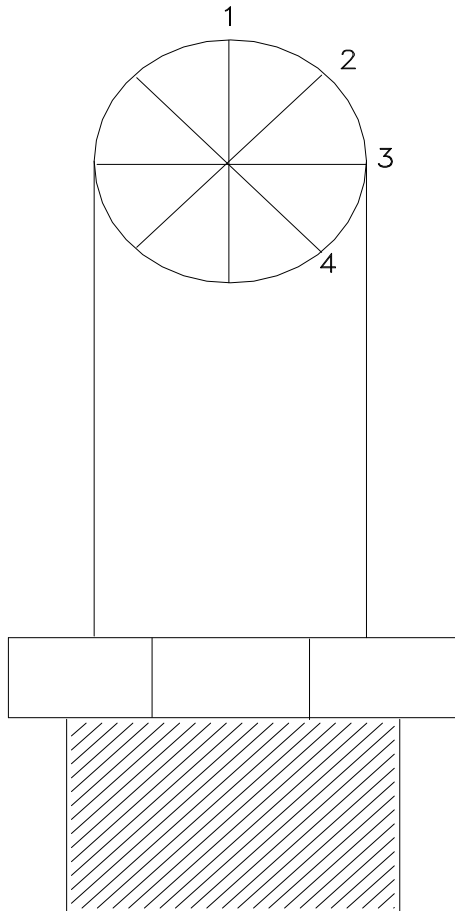
Nozzle Calibration

Date: 7/14/2023

Nozzle ID No.: 953

Analyst: RB

Material/Type: Glass



0.321 1

0.317 2

0.319 3

0.318 4

Out of Tolerance

Average
<u>0.319</u>

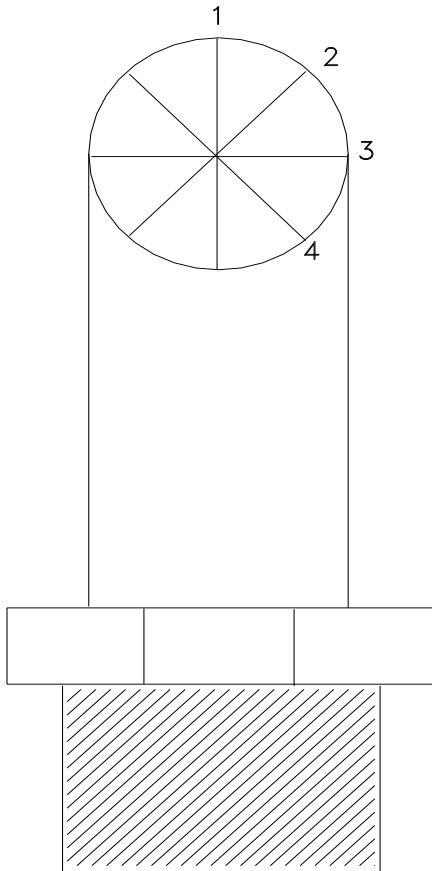
Nozzle Calibration

Date: 7/14/2023

Nozzle ID No.: 314

Analyst: RB

Material/Type: Quartz



0.276	1
0.275	2
0.276	3
0.276	4

Valid Data

Average
<div style="display: flex; justify-content: center; align-items: center;"> <div style="border-bottom: 1px solid black; width: 80%;"></div> 0.276 </div>

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Project #: M234105
Test Location: Main Kiln
Date: 10/11/2023
Operator: R. Sollars
Operating Condition: Mill On

Sample System: FTIR
Probe Length: 4.0 ft
Probe Type: FTIR
Sample Plane: Vertical
Port Length: 8.5 in.
Port Size (diameter): 6 in.
Port Type: Nipple
Duct Shape: Circular
Diameter: 10.9 ft
Duct Area: 93.31 Sq. Ft.
Upstream Diameters: 4.13
Downstream Diameters: 16.52
Number of Ports Sampled: 1
Number of Points per Port: 1
Total Number of Traverse Points: 1

Minimum Upstream Distance: 5.5 Feet
 Minimum Downstream Distance: 21.8 Feet
 Ideal Upstream Distance: 21.8 Feet
 Ideal Downstream Distance: 87.2 Feet

Calibration Gases

Type	Setting	Cylinder ID	Cylinder Value	Analyzer Response	Difference, % of Span	Expiration Date	Mid cylinder % of high cylinder	Final Bottle Pressure, PSI
O2 % (dry)	Zero	Zero Nitrogen	0.0	-0.12	0.54%	N/A		1500
	Mid	CC153857	11.96	11.98	-0.09%	7/19/2031	53.37%	950
	High	CC420519	22.41	22.38	0.13%	7/15/2029		1000

Type	Compound	Cylinder ID	Cylinder Value	Expiration Date	Final Bottle Pressure, PSI
Zero Gas	Nitrogen	Zero Nitrogen	0.0	N/A	1700
Calibration Transfer Standard	Ethylene	CC401933	100.7	7/10/2026	1800
Analyte Spike Gas	HCN	CC768228	49.30	3/11/2024	1900
	SF6		5.009		

Response Time Data

Type	RM Analyzer Make/Model	RM Analyzer s/n	Analyzer Span	RM Gas Span
O2 % (dry)	Servomex 1440	4447	25	22.41
HF ppmvw	MKS 2030	110161896	10	N/A
HCN ppmvw	MKS 2030	110161896	100	N/A

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Project #: M234105
Diluent: O2 %

Test Location: Main Kiln
Date: 10/11/23
Operator: R. Sollars
O2 % Correction: 7

O2 % (dry) Correction Data

Run #	Cma	Precal	Postcal	Pre zero	Post zero	Co	Cm	C	Cgas	Span Bias	Span Drift	Zero Bias	Zero Drift
1	11.96	12.00	11.91	-0.06	-0.06	-0.06	11.96	10.37	10.4	0.31	-0.40	-0.27	0.00
2	11.96	11.91	11.93	-0.06	-0.09	-0.08	11.92	10.34	10.4	0.22	0.09	-0.13	-0.13
3	11.96	11.93	11.91	-0.09	-0.10	-0.10	11.92	10.40	10.4	0.31	-0.09	-0.09	-0.04

Concentration of Cal Gas erage Pre and Post Span C = Average value of test Co=Average Pre and Post Zero
 Cgas = Corrected gas value of test

Calibration Corrected and Calculated Data

Run #	Run Date	Start Time	End Time	Moisture %	O2 % (dry)	CO2 % (wet)	CO2 % (dry)	HCN ppmvw	HCN ppmvd @ 7% O2	HF ppmvw	HF ppmvd @ 7% O2
1	10/11/23	8:30	9:29	17.23%	10.38	13.86	16.75	2.19	3.50	0.10	0.16
2	10/11/23	10:10	11:09	17.40%	10.39	13.86	16.78	1.81	2.89	0.10	0.16
3	10/11/23	11:45	12:44	17.18%	10.45	13.87	16.74	1.66	2.67	0.10	0.16

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln
Date: 10/11/23
Project #: M234105

Linearity Cal/Pre 1 Cal

<u>Time</u>	<u>O2 % (dry)</u>	
7:26	-0.05	
7:27	-0.11	
7:28	-0.12	iz
7:29	9.78	
7:30	21.36	
7:31	22.36	
7:32	22.38	ih
7:33	21.74	
7:34	12.94	
7:35	11.92	
7:36	11.98	im
7:37	14.65	
7:38	20.96	
7:39	20.24	
7:40	21.03	
7:41	21.08	
7:42	20.99	
7:43	19.18	
7:44	1.15	
7:45	0.05	
7:46	0.00	
7:47	6.50	
7:48	14.86	
7:49	0.56	
7:50	-0.01	
7:51	-0.04	
7:52	-0.05	
7:53	-0.06	z
7:54	-0.06	
7:55	7.32	
7:56	20.71	
7:57	20.99	
7:58	21.04	
7:59	21.06	
8:00	21.07	
8:01	21.09	
8:02	21.09	
8:03	16.20	
8:04	12.02	
8:05	12.00	m
8:06	11.99	

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Project #: M234105
Test Location: Main Kiln
Date: 10/11/23

Post 1/Pre 2			Post 2/Pre 3		
<u>Time</u>	<u>O2 % (dry)</u>		<u>Time</u>	<u>O2 % (dry)</u>	
9:53	2.48		11:31	10.59	
9:54	0.00		11:32	11.87	
9:55	-0.05		11:33	11.91	
9:56	-0.07		11:34	11.92	
9:57	-0.06	z	11:35	11.93	m
9:58	9.55		11:36	11.93	
9:59	11.86		11:37	2.84	
10:00	11.91	m	11:38	0.00	
			11:39	-0.07	
			11:40	-0.09	z

Post 3		
<u>Time</u>	<u>O2 % (dry)</u>	
13:05	10.54	
13:06	11.85	
13:07	11.89	
13:08	11.91	m
13:09	4.70	
13:10	0.05	
13:11	-0.08	
13:12	-0.10	z

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Project #: M234105
Test Location: Main Kiln
Date: 10/12/2023
Operator: R. Sollars
Operating Condition: Mill Off

Sample System: FTIR
Probe Length: 4.0 ft
Probe Type: FTIR
Sample Plane: Vertical
Port Length: 8.5 in.
Port Size (diameter): 6 in.
Port Type: Nipple
Duct Shape: Circular
Diameter: 10.9 ft
Duct Area: 93.31 Sq. Ft.
Upstream Diameters: 4.13
Downstream Diameters: 16.52
Number of Ports Sampled: 1
Number of Points per Port: 1
Total Number of Traverse Points: 1

Minimum Upstream Distance: 5.5 Feet
 Minimum Downstream Distance: 21.8 Feet
 Ideal Upstream Distance: 21.8 Feet
 Ideal Downstream Distance: 87.2 Feet

Calibration Gases

Type	Setting	Cylinder ID	Cylinder Value	Analyzer Response	Difference, % of Span	Expiration Date	Mid cylinder % of high cylinder	Final Bottle Pressure, PSI
O2 % (dry)	Zero	Zero Nitrogen	0.0	-0.15	0.87%	N/A		1500
	Mid	CC153857	11.96	11.91	0.22%	7/19/2031	53.37%	950
	High	CC420519	22.41	22.41	0.00%	7/15/2029		1000

Type	Compound	Cylinder ID	Cylinder Value	Expiration Date	Final Bottle Pressure, PSI
Zero Gas	Nitrogen	Zero Nitrogen	0.0	N/A	1700
Calibration Transfer Standard	Ethylene	CC401933	100.7	7/10/2026	1800
Analyte Spike Gas	HCN	CC768228	49.30	3/11/2024	1900
	SF6		5.009		

Response Time Data

Type	RM Analyzer Make/Model	RM Analyzer s/n	Analyzer Span	RM Gas Span
O2 % (dry)	Servomex 1440	4447	25	22.41
HF ppmvw	MKS 2030	110161896	10	N/A
HCN ppmvw	MKS 2030	110161896	100	N/A

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Diluent: O2 %

Test Location: Main Kiln
 Date: 10/12/23
 Operator: R. Sollars
 O2 % Correction: 7

O2 % (dry) Correction Data

Run #	Cma	Precal	Postcal	Pre zero	Post zero	Co	Cm	C	Cgas	Span Bias	Span Drift	Zero Bias	Zero Drift
1	11.96	11.98	11.94	-0.11	-0.09	-0.10	11.96	8.87	8.9	-0.13	-0.18	-0.27	0.09
2	11.96	11.94	11.97	-0.09	-0.11	-0.10	11.96	8.76	8.8	-0.27	0.13	-0.18	-0.09
3	11.96	11.97	11.99	-0.11	-0.11	-0.11	11.98	8.74	8.8	-0.36	0.09	-0.18	0.00

Concentration of Cal Gas C = Average value of test Co=Average Pre and Post Zero
 erage Pre and Post Span Cgas = Corrected gas value of test

Calibration Corrected and Calculated Data

Run #	Run Date	Start Time	End Time	Moisture %	O2 % (dry)	CO2 % (wet)	CO2 % (dry)	HCN ppmvw	HCN ppmvd @ 7% O2	HF ppmvw	HF ppmvd @ 7% O2
1	10/12/23	10:45	11:44	19.88%	8.90	15.04	18.77	2.08	3.01	0.10	0.14
2	10/12/23	12:15	13:14	19.28%	8.79	15.55	19.26	2.03	2.88	0.10	0.14
3	10/12/23	13:50	14:49	19.15%	8.75	15.45	19.11	2.00	2.83	0.10	0.14

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Test Location: Main Kiln
Date: 10/12/23
Project #: M234105

Linearity Cal/Pre 1 Cal

<u>Time</u>	<u>O2 % (dry)</u>	
7:06	-0.03	
7:07	-0.15	iz
7:08	0.28	
7:09	17.02	
7:10	21.83	
7:11	22.49	
7:12	22.41	ih
7:13	22.22	
7:14	18.86	
7:15	12.45	
7:16	11.96	
7:17	11.91	im
7:18	14.02	
7:19	19.13	
7:20	20.85	
7:21	15.57	
7:22	1.26	
7:23	0.16	
7:24	14.40	
7:25	20.45	
7:26	20.89	
7:27	20.96	
7:28	20.98	
7:29	19.70	
7:30	10.03	
7:31	8.95	
7:32	9.01	
7:33	9.16	
7:34	6.55	
7:35	0.44	
7:36	-0.02	
7:37	-0.09	
7:38	-0.11	z
7:39	1.23	
7:40	10.58	
7:41	11.72	
7:42	11.87	
7:43	11.98	
7:44	11.97	
7:45	11.98	m

Client: Ash Grove Cement Company
Facility: Durkee Cement Plant
Project #: M234105
Test Location: Main Kiln
Date: 10/12/23

Post 1/Pre 2			Post 2/Pre 3		
<u>Time</u>	<u>O2 % (dry)</u>		<u>Time</u>	<u>O2 % (dry)</u>	
12:00	6.15		13:31	2.20	
12:01	0.50		13:32	0.09	
12:02	-0.01		13:33	-0.08	
12:03	-0.09	z	13:34	-0.11	z
12:04	0.88		13:35	6.64	
12:05	10.52		13:36	11.63	
12:06	11.77		13:37	11.98	
12:07	11.94	m	13:38	11.97	m

Post 3		
<u>Time</u>	<u>O2 % (dry)</u>	
15:08	0.22	
15:09	-0.05	
15:10	-0.11	z
15:11	2.69	
15:12	11.09	
15:13	13.68	
15:14	12.31	
15:15	12.02	
15:16	11.99	m
15:17	11.99	

Appendix H - FTIR QA/QC

Method 320 FTIR Detector Multi-Gas Determination QA/QC

FTIR data was collected using an MKS MultiGas 2030 FTIR spectrometer.

The FTIR was equipped with a temperature-controlled, 5.11 meter multi-pass gas cell maintained at 191°C. Gas flows and sampling system pressures were monitored using a rotameter and pressure transducer. All data was collected at 0.5 cm⁻¹ resolution. Each spectrum was derived from the coaddition of 64 scans, with a new data point generated approximately every one minute. Analyzer data for each run is presented in the Reference Method Test Data appendix.

SAMPLING SYSTEM PARAMETERS				
MKS Serial #	Sampling Line	Probe Assembly	Particulate Filter Media	Operating Temperatures
110161896	100 3/8 dia., heated Teflon	Heated 12, 3/8 dia. SS	0.01 heated borosilicate glass fiber	191°C

A/ C procedures followed US EPA Method 320 guidelines. See below for A/ C procedure details and list of calibration gas standards. All calibration gases were introduced to the analyzer and the sampling system using an instrument grade stainless steel rotameter. All A/ C procedures were within the acceptance criteria allowance of the applicable EPA methodology. Detailed FTIR A/ C data follow the narrative portion of this appendix.

FTIR QA/QC Procedures						
QA/QC Specification	Purpose	Calibration Gas Analyte	Delivery	Frequency	Acceptance Criteria	Result
M320: Zero	Verify that the FTIR is free of contaminants & zero the FTIR	Nitrogen (zero)	Direct to FTIR	pre/post test	MDL or Noise	Pass
M320: Calibration Transfer Standard (CTS) Direct	Verify FTIR stability, confirm optical path length	Ethylene	Direct to FTIR	pretest	/- 5% cert. value	Pass
M320: Analyte Direct	Verify FTIR calibration	HCN, SF ₆	Direct to FTIR	Pretest	/- 5% cert. value	Pass
M320: CTS Response	Verify system stability, recovery, response time	Ethylene	Sampling System	Daily, pre/post test	/- 5% of Direct Measurement	Pass
M320: Zero Response	Verify system is free of contaminants, system bias	Nitrogen (zero)	Sampling System	pretest	Bias correct data	Pass
M320: Analyte Spike	Verify system ability to deliver and quantify analyte of interest in the presence of other effluent gases	HCN, SF ₆	Dynamic Addition to Sampling System, 1:10 effluent	Throughout testing – daily	/- 20% theoretical recovery	Pass

Note: The determined concentrations from direct analyses were used in all system/spike recovery calculations.

CALIBRATION GAS STANDARDS				
Components	Concentration (ppm)	Vendor	Cylinder #	Standard Type
Ethylene	100.7	Airgas	CC401933	Primary /- 1%
HCN/SF ₆	49.30/5.009	Airgas	CC768228	Certified Standard-Spec /- 5%
Nitrogen	ZZero Gas	Airgas	ZZero Nitrogen	UHP Grade

Analyte Spiking

HCN spiking was performed prior to testing to verify the ability of the sampling system to quantitatively deliver a sample containing HCN from the base of the probe to the FTIR. Analyte spiking assures the ability of the FTIR sampling system to recover acid gases in the presence of effluent gas.

As part of the spiking procedure, samples were measured to determine native HCN concentrations to be used in the spike recovery calculations. The analyte spiking gases contained a low concentration of sulfur hexafluoride (SF₆). The determined SF₆ concentration in the spiked sample was used to calculate the dilution factor of the spike and thus used to calculate the concentration of the spiked HCN. The spike target dilution ratio was 1:10 or less.

The following equation illustrates the percent recovery calculation.

$$DF = \frac{SF_6(spik)}{SF_6(direct)} \quad (\text{Sec. 9.2.3 (3) USEPA Method 320})$$

$$CS = DF * Spike(dir) + Unspike(1 - DF) \quad (\text{Sec. 9.2.3 (4) USEPA Method 320})$$

- DF Dilution factor of the spike gas
- SF_{6(dir)} SF₆ concentration measured directly in undiluted spike gas
- SF_{6(spik)} Diluted SF₆ concentration measured in a spiked sample
- Spike_{dir} Concentration of the analyte in the spike standard measure by the FTIR directly
- CS Expected concentration of the spiked samples
- Unspike Native concentration of analytes in unspiked samples

Post Collection Data Validation

As part of the data validation procedure, reference spectra are manually fit to that of the sample spectra and a concentration is determined. The reference spectra are scaled to match the peak amplitude of the sample, thus providing a scale factor. The scale factor multiplied by the reference spectra concentration is used to determine the concentration value for the sample spectra. Sample pressure and temperature corrections are then applied to compute the final sample concentration. The manually calculated results are then compared with the software-generated results. The data is then validated if the two concentrations are within 20% agreement. If there is a difference greater than 20% the spectra are reviewed for possible spectra interferences or any other possible causes leading to incorrectly quantified data.

Detection Limit

The detection limit of each analyte was calculated following Annex A2 of ASTM D6348-12 procedure using spectra that contained similar amounts of moisture.

FTIR DETECTION LIMITS			
Analyte	Detection Limit (ppmv wet)	Detection Limit (%v)	Detection Limit (%v wet)
Hydrogen Cyanide	0.2		
Hydrogen Fluoride	0.1		
Water		0.1	N/A
Carbon Dioxide		N/A	0.1

Copies of gas cylinder certifications are appended. All concentration data were recorded on a wet, volume basis. HCN spiking was performed prior to testing to confirm the measurement system's ability to deliver and quantify HCN. The sample and data collection followed the procedures outlined in Methods 320.

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Operating Condition: Mill On

Test Location: Main Kiln
 Date: 10/11/2023
 Operator: R. Sollars
 FTIR s/in: 110161896

System Leak Check: 0.0 mL/min

Nitrogen (Zero) Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
N2_DIR_000002.LAB	10/11/23	7:14:51	0.0	0.0	0.0	190.3	0.97	0.6	0.1	-0.003
N2_DIR_000003BKGLAB	10/11/23	7:17:04	0.0	0.0	0.0	190.5	0.97	0.0	0.0	0.000
N2_DIR_000004.LAB	10/11/23	7:17:18	0.0	0.0	0.0	190.6	0.97	0.0	0.1	0.004
N2_DIR_000005.LAB	10/11/23	7:17:26	0.0	0.0	0.0	190.6	0.97	-0.1	0.0	-0.010
N2_DIR_000006.LAB	10/11/23	7:17:34	0.0	0.0	0.0	190.6	0.97	-0.1	-0.1	0.012
N2_DIR_000007.LAB	10/11/23	7:17:41	0.0	0.0	0.0	190.6	0.97	0.1	0.1	-0.004
N2_DIR_000008.LAB	10/11/23	7:17:49	0.0	0.0	0.0	190.6	0.97	-0.1	-0.3	0.000
N2_DIR_000009.LAB	10/11/23	7:17:57	0.0	0.0	0.0	190.6	0.97	-0.1	0.1	-0.009
N2_DIR_000010.LAB	10/11/23	7:18:05	0.0	0.0	0.0	190.6	0.97	-0.1	0.0	0.002

Calibration Transfer Standard (CTS), Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
CTS_DIR_000038.LAB	10/11/23	7:23:09	0.0	0.0	0.0	191.1	0.91	99.9	-0.1	-0.024	99.2%
CTS_DIR_000039.LAB	10/11/23	7:23:17	0.0	0.0	0.0	191.1	0.91	99.6	-0.1	-0.023	98.9%
CTS_DIR_000040.LAB	10/11/23	7:23:25	0.0	0.0	0.0	191.1	0.91	99.7	-0.1	-0.024	99.0%
CTS_DIR_000041.LAB	10/11/23	7:23:32	0.0	0.0	0.0	191.1	0.91	99.7	0.1	-0.027	99.0%
CTS_DIR_000042.LAB	10/11/23	7:23:41	0.0	0.0	0.0	191.2	0.91	99.7	0.1	-0.022	99.1%
CTS_DIR_000043.LAB	10/11/23	7:23:48	0.0	0.0	0.0	191.1	0.91	100.1	-0.2	-0.020	99.4%
CTS_DIR_000044.LAB	10/11/23	7:23:56	0.0	0.0	0.0	191.1	0.91	99.6	0.0	-0.027	98.9%
Average								99.8			99.1%

Analyte Spike Gas (HCN) Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % HCN
HCN_DIR_000060.LAB	10/11/23	7:27:39	0.0	0.0	0.0	191.2	0.93	-0.2	51.1	4.910	103.8%
HCN_DIR_000061.LAB	10/11/23	7:27:47	0.0	0.0	0.0	191.2	0.93	-0.1	51.5	4.915	104.6%
HCN_DIR_000062.LAB	10/11/23	7:27:55	0.0	0.0	0.1	191.2	0.92	0.1	51.6	4.899	104.6%
HCN_DIR_000063.LAB	10/11/23	7:28:03	0.0	0.0	0.0	191.2	0.93	-0.2	51.4	4.899	104.3%
HCN_DIR_000064.LAB	10/11/23	7:28:11	0.0	0.0	0.0	191.2	0.93	-0.1	51.4	4.904	104.3%
HCN_DIR_000065.LAB	10/11/23	7:28:19	0.0	0.0	0.0	191.2	0.93	-0.2	51.6	4.903	104.7%
HCN_DIR_000066.LAB	10/11/23	7:28:27	0.0	0.0	0.0	191.2	0.92	-0.2	51.3	4.908	104.0%
HCN_DIR_000067.LAB	10/11/23	7:28:34	0.0	0.0	0.1	191.2	0.92	-0.1	51.3	4.903	104.0%
Average								51.4	4.905		104.3%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
CTS_RT2_000094.LAB	10/11/23	7:43:53	0.0	0.0	0.0	191.1	0.92	99.3	-0.2	-0.033	98.6%
CTS_RT2_000095.LAB	10/11/23	7:44:01	0.0	0.0	0.0	191.2	0.92	99.5	0.0	-0.029	98.8%
CTS_RT2_000096.LAB	10/11/23	7:44:09	0.0	0.0	0.0	191.1	0.92	99.7	0.0	-0.028	100.0%
CTS_RT2_000097.LAB	10/11/23	7:44:17	0.0	0.0	0.0	191.2	0.92	99.7	-0.2	-0.035	99.9%
CTS_RT2_000098.LAB	10/11/23	7:44:25	0.0	0.0	0.0	191.2	0.92	99.6	-0.1	-0.032	99.9%
CTS_RT2_000099.LAB	10/11/23	7:44:33	0.0	0.0	0.0	191.2	0.92	100.0	-0.1	-0.027	100.2%
CTS_RT2_000100.LAB	10/11/23	7:44:41	0.0	0.0	0.0	191.2	0.92	100.1	-0.2	-0.024	100.3%
CTS_RT2_000101.LAB	10/11/23	7:44:48	0.0	0.0	0.1	191.2	0.92	99.9	0.0	-0.033	100.1%

Response Time Test

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Response Time (sec)
CTS_RT2_000090.LAB	10/11/23	7:43:22	0.9	0.1	0.0	191.2	0.92	0.3	-0.3	-0.021	-
CTS_RT2_000091.LAB	10/11/23	7:43:30	0.8	0.0	0.0	191.2	0.92	7.7	0.5	-0.026	15.527
CTS_RT2_000092.LAB	10/11/23	7:43:38	0.2	0.0	0.0	191.2	0.92	91.4	0.8	-0.022	23.527
CTS_RT2_000093.LAB	10/11/23	7:43:45	0.1	0.0	0.0	191.2	0.92	98.9	-0.1	-0.034	
CTS_RT2_000094.LAB	10/11/23	7:43:53	0.0	0.0	0.0	191.1	0.92	99.3	-0.2	-0.033	
CTS_RT2_000095.LAB	10/11/23	7:44:01	0.0	0.0	0.0	191.2	0.92	99.5	0.0	-0.029	
CTS_RT2_000096.LAB	10/11/23	7:44:09	0.0	0.0	0.0	191.1	0.92	99.7	0.0	-0.028	
CTS_RT2_000097.LAB	10/11/23	7:44:17	0.0	0.0	0.0	191.2	0.92	99.7	-0.2	-0.035	
CTS_RT2_000098.LAB	10/11/23	7:44:25	0.0	0.0	0.0	191.2	0.92	99.6	-0.1	-0.032	

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Operating Condition: Mill On

Test Location: Main Kiln
 Date: 10/11/2023
 Operator: R. Sollars
 FTIR s/n: 110161896

Pre 1 Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
PRE1_SAMPLE_000240.LAB	10/11/23	8:11:49	17.1	13.5	-0.1	191.1	0.92	1.1	2.1	-0.024
PRE1_SAMPLE_000241.LAB	10/11/23	8:11:57	17.0	13.6	-0.1	191.2	0.92	1.2	2.2	-0.021
PRE1_SAMPLE_000242.LAB	10/11/23	8:12:05	17.1	13.7	-0.2	191.2	0.92	1.1	2.1	-0.020
									2.2	-0.022

Pre 1 Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
PRE1_SPIKE_000255.LAB	10/11/23	8:16:07	15.7	12.5	-0.2	190.8	0.92	1.0	6.2	0.395	0.081	101.9%
PRE1_SPIKE_000256.LAB	10/11/23	8:16:15	15.8	12.4	-0.2	190.7	0.92	1.2	6.4	0.393	0.080	105.1%
PRE1_SPIKE_000257.LAB	10/11/23	8:16:23	15.8	12.3	-0.2	190.7	0.92	0.9	6.4	0.391	0.080	104.6%
PRE1_SPIKE_000258.LAB	10/11/23	8:16:31	15.8	12.3	-0.1	190.7	0.92	0.9	6.2	0.394	0.080	101.0%
PRE1_SPIKE_000259.LAB	10/11/23	8:16:38	15.8	12.3	-0.1	190.7	0.92	1.0	6.3	0.394	0.080	102.7%
PRE1_SPIKE_000260.LAB	10/11/23	8:16:46	15.7	12.4	-0.2	190.7	0.92	1.2	6.3	0.393	0.080	103.0%
PRE1_SPIKE_000261.LAB	10/11/23	8:16:54	15.7	12.5	-0.1	190.7	0.92	1.1	6.3	0.391	0.080	104.4%
PRE1_SPIKE_000262.LAB	10/11/23	8:17:02	15.7	12.6	-0.2	190.7	0.92	1.1	6.1	0.388	0.079	100.7%

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN1_000374.LAB	10/11/23	9:38:41	17.3	13.7	-0.2	191.2	0.93	1.2	2.0	-0.023
RUN1_000375.LAB	10/11/23	9:39:44	17.2	13.9	-0.2	191.2	0.92	1.2	2.0	-0.022
RUN1_000376.LAB	10/11/23	9:40:47	17.4	13.7	-0.2	191.2	0.92	1.2	2.0	-0.023
									2.0	-0.023

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST1_SPK_000424.LAB	10/11/23	9:50:16	15.6	12.5	-0.2	191.2	0.93	1.1	6.1	0.404	0.082	100.8%
POST1_SPK_000425.LAB	10/11/23	9:50:24	15.7	12.4	-0.2	191.2	0.92	1.0	6.1	0.404	0.082	101.0%
POST1_SPK_000426.LAB	10/11/23	9:50:32	15.8	12.4	-0.2	191.2	0.93	1.0	6.2	0.407	0.083	101.1%
POST1_SPK_000427.LAB	10/11/23	9:50:40	15.8	12.5	-0.2	191.2	0.93	1.1	6.1	0.405	0.083	99.5%
POST1_SPK_000428.LAB	10/11/23	9:50:48	15.7	12.6	-0.2	191.2	0.93	1.0	6.1	0.410	0.084	99.6%
POST1_SPK_000429.LAB	10/11/23	9:50:55	15.7	12.7	-0.2	191.2	0.92	1.1	6.1	0.407	0.083	100.1%
POST1_SPK_000430.LAB	10/11/23	9:51:03	15.7	12.7	-0.2	191.2	0.92	1.0	6.2	0.400	0.082	102.4%
POST1_SPK_000431.LAB	10/11/23	9:51:11	15.8	12.7	-0.2	191.2	0.92	1.0	6.2	0.404	0.082	101.6%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST1_CTS_000465.LAB	10/11/23	9:56:34	0.1	0.0	0.0	191.2	0.92	99.5	0.3	-0.035	99.8%
POST1_CTS_000466.LAB	10/11/23	9:56:42	0.1	0.0	0.0	191.2	0.92	99.7	0.1	-0.027	99.9%
POST1_CTS_000467.LAB	10/11/23	9:56:50	0.1	0.0	0.0	191.2	0.92	99.9	0.3	-0.036	100.1%
POST1_CTS_000468.LAB	10/11/23	9:56:58	0.1	0.0	0.0	191.2	0.92	99.7	0.2	-0.030	99.9%
POST1_CTS_000469.LAB	10/11/23	9:57:06	0.1	0.0	0.0	191.2	0.92	100.0	0.2	-0.035	100.2%
POST1_CTS_000470.LAB	10/11/23	9:57:13	0.1	0.0	0.0	191.2	0.92	99.5	0.0	-0.032	99.7%
POST1_CTS_000471.LAB	10/11/23	9:57:21	0.1	0.0	0.0	191.2	0.92	99.6	0.2	-0.029	99.8%
POST1_CTS_000472.LAB	10/11/23	9:57:29	0.1	0.0	0.0	191.2	0.92	99.7	0.2	-0.029	99.9%

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Operating Condition: Mill On

Test Location: Main Kiln
 Date: 10/11/2023
 Operator: R. Sollars
 FTIR s/in: 110161896

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN2_000594.LAB	10/11/23	11:20:18	17.2	13.9	-0.2	191.2	0.93	1.1	1.9	-0.018
RUN2_000595.LAB	10/11/23	11:21:20	17.4	13.9	-0.2	191.2	0.93	1.1	1.9	-0.020
RUN2_000596.LAB	10/11/23	11:22:23	17.8	13.8	-0.2	191.1	0.93	1.1	1.8	-0.020
									1.9	-0.019

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST2_SPK_000609.LAB	10/11/23	11:26:41	16.1	12.8	-0.2	191.0	0.93	0.9	5.8	0.398	0.081	99.4%
POST2_SPK_000610.LAB	10/11/23	11:26:49	16.1	12.8	-0.2	191.0	0.93	0.8	6.0	0.396	0.081	102.7%
POST2_SPK_000611.LAB	10/11/23	11:26:56	16.2	12.8	-0.2	191.0	0.93	1.1	5.7	0.399	0.081	96.7%
POST2_SPK_000612.LAB	10/11/23	11:27:04	16.2	12.8	-0.2	191.0	0.93	1.0	5.9	0.397	0.081	100.5%
POST2_SPK_000613.LAB	10/11/23	11:27:12	16.2	12.8	-0.2	191.0	0.93	1.2	6.0	0.400	0.082	101.0%
POST2_SPK_000614.LAB	10/11/23	11:27:20	16.2	12.8	-0.2	191.0	0.92	0.9	5.9	0.396	0.081	100.7%
POST2_SPK_000615.LAB	10/11/23	11:27:28	16.2	12.8	-0.2	191.0	0.93	0.8	6.0	0.391	0.080	103.7%
POST2_SPK_000616.LAB	10/11/23	11:27:35	16.2	12.8	-0.2	191.0	0.93	1.1	5.9	0.393	0.080	101.9%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST2_CTS_000620.LAB	10/11/23	11:29:06	0.2	0.1	0.0	191.2	0.93	99.0	0.3	-0.025	99.2%
POST2_CTS_000621.LAB	10/11/23	11:29:14	0.2	0.1	0.0	191.2	0.93	99.1	0.3	-0.024	99.3%
POST2_CTS_000622.LAB	10/11/23	11:29:21	0.2	0.1	0.0	191.2	0.93	99.6	0.2	-0.025	99.9%
POST2_CTS_000623.LAB	10/11/23	11:29:29	0.2	0.1	0.0	191.1	0.93	99.3	0.3	-0.027	99.5%
POST2_CTS_000624.LAB	10/11/23	11:29:37	0.1	0.1	0.0	191.2	0.93	99.5	0.3	-0.027	99.8%
POST2_CTS_000625.LAB	10/11/23	11:29:45	0.1	0.1	0.0	191.2	0.93	99.1	0.3	-0.040	99.3%
POST2_CTS_000626.LAB	10/11/23	11:29:53	0.1	0.0	0.0	191.2	0.93	99.7	0.5	-0.032	99.9%
POST2_CTS_000627.LAB	10/11/23	11:30:01	0.1	0.0	0.0	191.2	0.93	99.3	0.1	-0.026	99.5%

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN3_000721.LAB	10/11/23	12:52:05	17.7	13.7	-0.2	191.3	0.93	1.1	1.7	-0.017
RUN3_000722.LAB	10/11/23	12:53:08	17.5	13.6	-0.2	191.4	0.93	1.0	1.7	-0.017
RUN3_000723.LAB	10/11/23	12:54:10	17.6	13.9	-0.2	191.4	0.93	1.1	1.7	-0.016
									1.7	-0.017

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST3_SPK_000747.LAB	10/11/23	13:00:13	16.0	12.5	-0.2	191.2	0.93	0.8	5.8	0.421	0.086	97.1%
POST3_SPK_000748.LAB	10/11/23	13:00:21	16.0	12.5	-0.2	191.2	0.93	1.0	6.0	0.425	0.087	99.8%
POST3_SPK_000749.LAB	10/11/23	13:00:29	16.1	12.6	-0.2	191.2	0.93	1.0	6.0	0.414	0.084	101.1%
POST3_SPK_000750.LAB	10/11/23	13:00:36	16.0	12.6	-0.2	191.2	0.93	0.9	6.0	0.421	0.086	101.4%
POST3_SPK_000751.LAB	10/11/23	13:00:44	15.9	12.6	-0.2	191.2	0.93	0.9	6.0	0.432	0.088	98.6%
POST3_SPK_000752.LAB	10/11/23	13:00:52	15.9	12.6	-0.3	191.2	0.93	0.9	5.8	0.427	0.087	95.8%
POST3_SPK_000753.LAB	10/11/23	13:01:00	15.9	12.7	-0.2	191.2	0.93	0.8	6.0	0.423	0.086	100.3%
POST3_SPK_000754.LAB	10/11/23	13:01:08	16.0	12.7	-0.2	191.2	0.93	0.9	6.1	0.419	0.085	102.6%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST3_CTS_000762.LAB	10/11/23	13:03:04	0.2	0.1	0.0	191.3	0.93	99.2	0.1	-0.026	99.4%
POST3_CTS_000763.LAB	10/11/23	13:03:12	0.1	0.1	0.0	191.3	0.93	99.2	0.3	-0.031	99.4%
POST3_CTS_000764.LAB	10/11/23	13:03:20	0.1	0.1	0.0	191.2	0.93	99.3	0.1	-0.020	99.6%
POST3_CTS_000765.LAB	10/11/23	13:03:28	0.1	0.1	0.0	191.2	0.93	99.5	0.2	-0.028	99.7%
POST3_CTS_000766.LAB	10/11/23	13:03:36	0.1	0.1	0.0	191.2	0.93	99.4	0.1	-0.025	99.6%
POST3_CTS_000767.LAB	10/11/23	13:03:43	0.1	0.1	0.1	191.2	0.93	99.4	0.2	-0.025	99.6%
POST3_CTS_000768.LAB	10/11/23	13:03:51	0.1	0.1	0.0	191.2	0.93	99.6	0.1	-0.019	99.8%
POST3_CTS_000769.LAB	10/11/23	13:03:59	0.1	0.1	0.1	191.2	0.93	99.6	0.1	-0.029	99.8%

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Operating Condition: Mill On

Test Location: Main Kiln
 Date: 10/11/2023
 Operator: R. Sollars
 FTIR s/n: 110161896

Post Test CTS, Direct Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST3_CTS_DIR_000821.LAB	10/11/23	13:19:34	0.0	0.0	0.0	191.2	0.93	100.1	-0.1	-0.022	100.3%
POST3_CTS_DIR_000822.LAB	10/11/23	13:19:42	0.0	0.0	0.0	191.2	0.93	100.0	-0.2	-0.026	100.6%
POST3_CTS_DIR_000823.LAB	10/11/23	13:19:50	0.0	0.0	0.0	191.2	0.93	100.3	-0.2	-0.017	100.6%
POST3_CTS_DIR_000824.LAB	10/11/23	13:19:58	0.0	0.0	0.0	191.1	0.93	100.5	-0.1	-0.015	100.7%
POST3_CTS_DIR_000825.LAB	10/11/23	13:20:06	0.0	0.0	0.0	191.1	0.93	100.5	-0.1	-0.008	100.7%
POST3_CTS_DIR_000826.LAB	10/11/23	13:20:13	0.0	0.0	0.0	191.1	0.93	100.2	-0.3	-0.017	100.4%
POST3_CTS_DIR_000827.LAB	10/11/23	13:20:21	0.0	0.0	0.0	191.1	0.93	100.3	-0.1	-0.010	100.6%
POST3_CTS_DIR_000828.LAB	10/11/23	13:20:29	0.0	0.0	0.0	191.1	0.93	100.2	0.1	-0.014	100.5%
Average								100.3			

Post Test N2, Direct Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
POST3_N2_DIR_000831.LAB	10/11/23	13:26:43	0.0	0.0	0.0	191.1	0.93	0.0	-0.1	-0.002
POST3_N2_DIR_000832.LAB	10/11/23	13:28:49	0.0	0.0	0.0	190.8	0.93	0.0	-0.1	-0.001
POST3_N2_DIR_000833.LAB	10/11/23	13:30:54	0.0	0.0	0.0	190.6	0.93	0.0	-0.1	-0.002

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Operating Condition: Mill Off

Test Location: Main Kiln
 Date: 10/12/2023
 Operator: R. Sollars
 FTIR s/n: 110161896

System Leak Check: 0.0 mL/min

Nitrogen (Zero) Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
N2_DIR_000002.LAB	10/12/23	6:56:40	0.0	0.0	0.0	190.8	0.93	-0.1	-0.2	-0.006
N2_DIR_000003BKGLAB	10/12/23	6:58:53	0.0	0.0	0.0	190.8	0.93	0.0	0.0	0.000
N2_DIR_000004.LAB	10/12/23	6:59:07	0.0	0.0	0.1	190.7	0.93	0.0	0.1	-0.009
N2_DIR_000005.LAB	10/12/23	6:59:15	0.0	0.0	0.0	190.7	0.93	0.1	0.1	-0.002
N2_DIR_000006.LAB	10/12/23	6:59:23	0.0	0.0	0.0	190.7	0.93	0.2	0.1	-0.001
N2_DIR_000007.LAB	10/12/23	6:59:31	0.0	0.0	0.0	190.7	0.93	0.2	0.0	-0.001
N2_DIR_000008.LAB	10/12/23	6:59:39	0.0	0.0	0.0	190.7	0.93	0.0	0.0	0.009
N2_DIR_000009.LAB	10/12/23	6:59:46	0.0	0.0	0.0	190.7	0.93	0.1	-0.1	0.001
N2_DIR_000010.LAB	10/12/23	6:59:54	0.0	0.0	0.0	190.7	0.93	0.1	-0.1	-0.001

Calibration Transfer Standard (CTS), Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
CTS_DIR_000021.LAB	10/12/23	7:02:19	0.0	0.0	0.0	190.7	0.93	99.8	-0.2	-0.021	99.1%
CTS_DIR_000022.LAB	10/12/23	7:02:27	0.0	0.0	0.0	190.7	0.93	100.0	0.0	-0.017	99.3%
CTS_DIR_000023.LAB	10/12/23	7:02:35	0.0	0.0	0.0	190.8	0.93	100.0	-0.1	-0.024	99.4%
CTS_DIR_000024.LAB	10/12/23	7:02:43	0.0	0.0	-0.1	190.8	0.93	99.4	-0.2	-0.023	98.7%
CTS_DIR_000025.LAB	10/12/23	7:02:50	0.0	0.0	0.0	190.7	0.93	99.7	0.2	-0.011	99.0%
CTS_DIR_000026.LAB	10/12/23	7:02:59	0.0	0.0	0.0	190.7	0.93	99.9	-0.1	-0.022	99.2%
CTS_DIR_000027.LAB	10/12/23	7:03:06	0.0	0.0	0.0	190.7	0.93	99.6	0.0	-0.022	98.9%
Average								99.8		-0.022	98.9%

Analyte Spike Gas (HCN) Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % HCN
HCN_DIR_000043.LAB	10/12/23	7:06:58	0.0	0.0	0.0	190.6	0.94	4.875	50.9	4.875	103.3%
HCN_DIR_000044.LAB	10/12/23	7:07:06	0.0	0.0	0.0	190.6	0.94	-0.4	50.9	4.870	103.3%
HCN_DIR_000045.LAB	10/12/23	7:07:14	0.0	0.0	0.0	190.6	0.94	-0.4	51.0	4.873	103.4%
HCN_DIR_000046.LAB	10/12/23	7:07:21	0.0	0.0	0.0	190.6	0.94	-0.3	51.2	4.878	103.8%
HCN_DIR_000047.LAB	10/12/23	7:07:29	0.0	0.0	0.0	190.6	0.94	-0.2	51.2	4.875	103.9%
HCN_DIR_000048.LAB	10/12/23	7:07:37	0.0	0.0	0.0	190.6	0.94	-0.2	51.0	4.866	103.4%
HCN_DIR_000049.LAB	10/12/23	7:07:45	0.0	0.0	0.0	190.6	0.94	-0.4	50.9	4.883	103.3%
HCN_DIR_000050.LAB	10/12/23	7:07:53	0.0	0.0	0.0	190.6	0.94	-0.4	51.3	4.868	104.1%
Average								51.1	4.874		103.6%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
CTS_RT_000088.LAB	10/12/23	7:21:39	0.1	0.0	0.0	190.7	0.94	99.2	-0.1	-0.015	98.5%
CTS_RT_000089.LAB	10/12/23	7:21:46	0.1	0.0	0.0	190.7	0.94	99.4	0.0	-0.008	98.7%
CTS_RT_000090.LAB	10/12/23	7:21:54	0.0	0.0	0.0	190.7	0.94	99.1	0.0	-0.026	99.3%
CTS_RT_000091.LAB	10/12/23	7:22:02	0.1	0.0	0.0	190.7	0.94	99.2	0.0	-0.027	99.4%
CTS_RT_000092.LAB	10/12/23	7:22:10	0.1	0.0	0.0	190.7	0.94	99.1	0.2	-0.022	99.3%
CTS_RT_000093.LAB	10/12/23	7:22:18	0.0	0.0	0.0	190.7	0.94	99.2	0.0	-0.030	99.4%
CTS_RT_000094.LAB	10/12/23	7:22:26	0.1	0.0	0.0	190.7	0.94	99.0	0.1	-0.016	99.2%
CTS_RT_000095.LAB	10/12/23	7:22:34	0.0	0.0	0.0	190.7	0.94	99.2	0.2	-0.017	99.4%

Response Time Test

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Response Time (sec)
CTS_RT_000082.LAB	10/12/23	7:20:52	0.9	0.0	0.0	190.7	0.94	-0.2	0.2	-0.005	-
CTS_RT_000083.LAB	10/12/23	7:20:59	0.8	0.2	0.0	190.7	0.94	29.0	1.6	-0.029	15.626
CTS_RT_000084.LAB	10/12/23	7:21:07	0.1	0.0	0.0	190.7	0.94	96.3	0.2	-0.018	23.626
CTS_RT_000085.LAB	10/12/23	7:21:15	0.1	0.0	0.0	190.7	0.94	98.3	0.1	-0.029	
CTS_RT_000086.LAB	10/12/23	7:21:23	0.1	0.0	0.0	190.7	0.94	98.6	0.1	-0.017	
CTS_RT_000087.LAB	10/12/23	7:21:31	0.1	0.0	0.0	190.7	0.94	99.2	0.1	-0.024	
CTS_RT_000088.LAB	10/12/23	7:21:39	0.1	0.0	0.0	190.7	0.94	99.2	-0.1	-0.015	
CTS_RT_000089.LAB	10/12/23	7:21:46	0.1	0.0	0.0	190.7	0.94	99.4	0.0	-0.008	
CTS_RT_000090.LAB	10/12/23	7:21:54	0.0	0.0	0.0	190.7	0.94	99.1	0.0	-0.026	

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Operating Condition: Mill Off

Test Location: Main Kiln
 Date: 10/12/2023
 Operator: R. Sollars
 FTIR s/n: 110161896

Pre 1 Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
PRE1_SAMPLE_000218.LAB	10/12/23	7:48:00	20.4	14.0	-0.1	190.9	0.94	1.1	1.9	-0.010
PRE1_SAMPLE_000219.LAB	10/12/23	7:48:07	20.4	14.0	-0.2	190.9	0.94	1.2	1.8	-0.006
PRE1_SAMPLE_000220.LAB	10/12/23	7:48:15	20.4	14.1	-0.2	190.9	0.94	1.1	1.8	-0.005
									1.9	-0.007

Pre 1 Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
PRE1_SPK_000243.LAB	10/12/23	7:53:49	19.2	12.6	-0.2	190.7	0.94	1.0	5.4	0.372	0.076	95.1%
PRE1_SPK_000244.LAB	10/12/23	7:53:57	19.3	12.6	-0.1	190.7	0.94	1.0	5.4	0.371	0.076	96.6%
PRE1_SPK_000245.LAB	10/12/23	7:54:05	19.3	12.7	-0.2	190.7	0.94	1.0	5.3	0.373	0.076	95.0%
PRE1_SPK_000246.LAB	10/12/23	7:54:13	19.3	12.8	-0.2	190.7	0.94	1.1	5.5	0.373	0.076	96.9%
PRE1_SPK_000247.LAB	10/12/23	7:54:21	19.3	12.8	-0.2	190.7	0.94	1.0	5.5	0.372	0.076	96.9%
PRE1_SPK_000248.LAB	10/12/23	7:54:28	19.3	12.9	-0.2	190.7	0.94	1.0	5.3	0.363	0.075	96.4%
PRE1_SPK_000249.LAB	10/12/23	7:54:36	19.3	12.9	-0.2	190.7	0.94	1.1	5.5	0.365	0.075	98.7%
PRE1_SPK_000250.LAB	10/12/23	7:54:44	19.3	12.9	-0.2	190.7	0.94	1.2	5.3	0.366	0.075	96.0%

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN1_000503.LAB	10/12/23	11:51:50	19.8	15.0	-0.2	190.8	0.93	1.1	2.1	-0.006
RUN1_000504.LAB	10/12/23	11:52:53	19.8	14.9	-0.2	190.8	0.93	1.1	2.1	-0.011
RUN1_000505.LAB	10/12/23	11:53:56	19.8	14.9	-0.2	190.8	0.93	1.1	2.1	-0.007
									2.1	-0.008

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST1_SPK_000523.LAB	10/12/23	11:58:10	18.3	14.2	-0.2	190.8	0.93	0.9	5.6	0.380	0.078	94.6%
POST1_SPK_000524.LAB	10/12/23	11:58:18	18.3	14.2	-0.2	190.8	0.93	1.0	5.6	0.383	0.079	94.6%
POST1_SPK_000525.LAB	10/12/23	11:58:26	18.2	14.1	-0.2	190.8	0.93	0.9	5.7	0.375	0.077	97.0%
POST1_SPK_000526.LAB	10/12/23	11:58:34	18.2	14.1	-0.2	190.8	0.93	0.9	5.5	0.373	0.076	94.5%
POST1_SPK_000527.LAB	10/12/23	11:58:41	18.2	14.0	-0.2	190.8	0.93	1.0	5.4	0.379	0.078	91.7%
POST1_SPK_000528.LAB	10/12/23	11:58:49	18.2	14.0	-0.2	190.8	0.93	1.0	5.6	0.376	0.077	95.5%
POST1_SPK_000529.LAB	10/12/23	11:58:57	18.3	14.0	-0.2	190.8	0.93	1.0	5.6	0.382	0.078	94.3%
POST1_SPK_000530.LAB	10/12/23	11:59:05	18.3	14.0	-0.2	190.8	0.93	0.8	5.6	0.378	0.078	95.6%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST1_CTS_000551.LAB	10/12/23	12:02:36	1.2	0.0	0.0	190.8	0.94	98.2	0.3	-0.009	98.4%
POST1_CTS_000552.LAB	10/12/23	12:02:44	1.2	0.0	0.0	190.8	0.94	98.2	0.3	-0.008	98.4%
POST1_CTS_000553.LAB	10/12/23	12:02:52	1.2	0.0	0.0	190.8	0.94	98.1	0.5	-0.021	98.3%
POST1_CTS_000554.LAB	10/12/23	12:02:59	1.2	0.0	0.0	190.8	0.94	98.2	0.2	-0.016	98.4%
POST1_CTS_000555.LAB	10/12/23	12:03:08	1.1	0.0	0.0	190.9	0.94	98.1	0.4	-0.022	98.3%
POST1_CTS_000556.LAB	10/12/23	12:03:15	1.1	0.0	0.0	190.9	0.94	98.0	0.4	-0.007	98.2%
POST1_CTS_000557.LAB	10/12/23	12:03:23	1.1	0.0	0.0	190.9	0.94	98.0	0.2	-0.021	98.2%
POST1_CTS_000558.LAB	10/12/23	12:03:31	1.1	0.0	0.0	190.9	0.94	98.2	0.2	-0.013	98.4%

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Operating Condition: Mill Off

Test Location: Main Kiln
 Date: 10/12/2023
 Operator: R. Sollars
 FTIR s/in: 110161896

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN2_000645.LAB	10/12/23	13:22:43	19.6	16.0	-0.2	190.9	0.93	1.2	2.1	-0.009
RUN2_000646.LAB	10/12/23	13:23:46	19.7	16.0	-0.2	190.9	0.93	1.1	2.2	-0.007
RUN2_000647.LAB	10/12/23	13:24:49	19.6	16.4	-0.2	190.8	0.93	1.2	2.2	-0.012
									2.2	-0.010

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST2_SPK_000653.LAB	10/12/23	13:28:44	17.7	15.3	-0.2	190.4	0.93	1.2	6.3	0.418	0.086	98.6%
POST2_SPK_000654.LAB	10/12/23	13:28:52	17.7	15.4	-0.2	190.4	0.93	1.0	6.3	0.417	0.085	98.7%
POST2_SPK_000655.LAB	10/12/23	13:29:00	17.7	15.3	-0.2	190.3	0.93	1.2	6.3	0.416	0.085	100.1%
POST2_SPK_000656.LAB	10/12/23	13:29:08	17.7	15.3	-0.2	190.3	0.93	1.1	6.1	0.412	0.085	96.4%
POST2_SPK_000657.LAB	10/12/23	13:29:16	17.7	15.3	-0.1	190.3	0.93	1.1	6.1	0.402	0.082	99.3%
POST2_SPK_000658.LAB	10/12/23	13:29:24	17.8	15.2	-0.2	190.3	0.94	1.1	6.2	0.407	0.083	99.2%
POST2_SPK_000659.LAB	10/12/23	13:29:31	17.8	15.2	-0.2	190.3	0.93	1.1	6.0	0.404	0.083	95.8%
POST2_SPK_000660.LAB	10/12/23	13:29:39	17.8	15.1	-0.1	190.3	0.93	1.1	6.1	0.410	0.084	96.5%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST2_CTS_000670.LAB	10/12/23	13:32:55	0.8	0.0	0.0	190.6	0.93	98.4	0.5	-0.019	98.6%
POST2_CTS_000671.LAB	10/12/23	13:33:03	0.8	0.0	0.0	190.6	0.93	98.4	0.3	-0.013	98.6%
POST2_CTS_000672.LAB	10/12/23	13:33:11	0.8	0.0	-0.1	190.7	0.93	98.1	0.4	-0.012	98.3%
POST2_CTS_000673.LAB	10/12/23	13:33:19	0.8	0.0	0.0	190.7	0.93	97.9	0.5	-0.019	98.1%
POST2_CTS_000674.LAB	10/12/23	13:33:26	0.8	0.0	0.0	190.6	0.93	98.5	0.3	-0.018	98.7%
POST2_CTS_000675.LAB	10/12/23	13:33:35	0.7	0.0	0.0	190.7	0.93	98.3	0.3	-0.012	98.6%
POST2_CTS_000676.LAB	10/12/23	13:33:42	0.7	0.0	0.0	190.7	0.93	98.5	0.3	-0.020	98.7%
POST2_CTS_000677.LAB	10/12/23	13:33:50	0.7	0.0	0.0	190.7	0.93	98.8	0.4	-0.014	99.0%

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN3_000774.LAB	10/12/23	14:59:08	19.9	15.3	-0.2	190.8	0.93	1.1	2.1	-0.008
RUN3_000775.LAB	10/12/23	15:00:11	19.9	15.5	-0.2	190.8	0.93	1.1	2.0	-0.007
RUN3_000776.LAB	10/12/23	15:01:14	19.9	15.3	-0.2	190.8	0.93	1.0	2.0	-0.006
									2.0	-0.007

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST3_SPK_000787.LAB	10/12/23	15:04:16	18.2	14.5	-0.2	190.7	0.93	0.9	5.6	0.373	0.077	96.3%
POST3_SPK_000788.LAB	10/12/23	15:04:24	18.2	14.4	-0.2	190.7	0.93	1.0	5.6	0.375	0.077	95.6%
POST3_SPK_000789.LAB	10/12/23	15:04:32	18.2	14.5	-0.2	190.7	0.93	1.1	5.6	0.379	0.078	96.1%
POST3_SPK_000790.LAB	10/12/23	15:04:40	18.2	14.4	-0.2	190.7	0.93	1.0	5.6	0.375	0.077	95.4%
POST3_SPK_000791.LAB	10/12/23	15:04:47	18.2	14.3	-0.2	190.7	0.93	0.9	5.6	0.377	0.077	95.5%
POST3_SPK_000792.LAB	10/12/23	15:04:55	18.2	14.2	-0.2	190.8	0.93	1.0	5.7	0.369	0.076	99.1%
POST3_SPK_000793.LAB	10/12/23	15:05:03	18.1	14.1	-0.2	190.7	0.93	1.1	5.6	0.370	0.076	97.1%
POST3_SPK_000794.LAB	10/12/23	15:05:11	18.1	14.0	-0.2	190.8	0.93	0.9	5.6	0.376	0.077	95.7%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST3_CTS_000814.LAB	10/12/23	15:09:04	0.9	0.0	0.0	190.8	0.93	98.3	0.2	-0.020	98.5%
POST3_CTS_000815.LAB	10/12/23	15:09:12	0.9	0.0	0.0	190.8	0.93	98.2	0.3	-0.012	98.4%
POST3_CTS_000816.LAB	10/12/23	15:09:20	0.9	0.0	0.0	190.8	0.93	98.2	0.2	-0.019	98.4%
POST3_CTS_000817.LAB	10/12/23	15:09:28	0.9	0.0	0.1	190.8	0.93	98.1	0.3	-0.019	98.3%
POST3_CTS_000818.LAB	10/12/23	15:09:36	0.9	0.0	0.0	190.8	0.93	98.4	0.3	-0.018	98.6%
POST3_CTS_000819.LAB	10/12/23	15:09:43	0.9	0.0	0.0	190.8	0.93	98.4	0.2	-0.020	98.6%
POST3_CTS_000820.LAB	10/12/23	15:09:51	0.8	0.0	-0.1	190.8	0.93	98.1	0.4	-0.020	98.3%
POST3_CTS_000821.LAB	10/12/23	15:09:59	0.8	0.0	0.0	190.8	0.93	98.2	0.1	-0.019	98.4%

Client: Ash Grove Cement Company
 Facility: Durkee Cement Plant
 Project #: M234105
 Operating Condition: Mill Off

Test Location: Main Kiln
 Date: 10/12/2023
 Operator: R. Sollars
 FTIR s/n: 110161896

Post Test CTS, Direct Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST3_CTS_DIR_000854.LAB	10/12/23	15:24:18	0.0	0.0	0.0	190.7	0.93	99.4	0.0	-0.022	99.7%
POST3_CTS_DIR_000855.LAB	10/12/23	15:24:26	0.0	0.0	0.0	190.7	0.93	99.3	0.0	-0.015	99.5%
POST3_CTS_DIR_000856.LAB	10/12/23	15:24:34	0.0	0.0	0.0	190.7	0.93	99.6	0.0	-0.016	99.8%
POST3_CTS_DIR_000857.LAB	10/12/23	15:24:42	0.0	0.0	0.0	190.7	0.93	99.4	-0.1	-0.008	99.6%
POST3_CTS_DIR_000858.LAB	10/12/23	15:24:50	0.0	0.0	0.0	190.7	0.93	99.5	-0.1	-0.017	99.8%
POST3_CTS_DIR_000859.LAB	10/12/23	15:24:57	0.0	0.0	0.0	190.7	0.93	99.3	-0.2	-0.020	99.5%
POST3_CTS_DIR_000860.LAB	10/12/23	15:25:05	0.0	0.0	0.0	190.7	0.93	99.6	-0.2	-0.010	99.8%
POST3_CTS_DIR_000861.LAB	10/12/23	15:25:13	0.0	0.0	0.0	190.7	0.93	99.3	-0.1	-0.012	99.5%
Average								99.4			

Post Test N2, Direct Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
N2_DIR_000862.LAB	10/12/23	15:28:36	0.0	0.0	0.0	190.8	0.93	0.0	-0.1	0.006
N2_DIR_000863.LAB	10/12/23	15:30:42	0.0	0.0	0.0	190.8	0.93	0.1	-0.2	0.004
N2_DIR_000864.LAB	10/12/23	15:32:48	0.0	0.0	0.0	190.7	0.93	0.0	-0.1	0.004

Appendix I - Gas Cylinder Certifications

CERTIFICATE OF ANALYSIS

Grade of Product: EPA PROTOCOL STANDARD

Part Number: E03NI78E15A1066	Reference Number: 153-402794083-1
Cylinder Number: CC153857	Cylinder Volume: 151.1 CF
Laboratory: 124 - Tooele (SAP) - UT	Cylinder Pressure: 2015 PSIG
PGVP Number: B72023	Valve Outlet: 590
Gas Code: CO2,O2,BALN	Certification Date: Jul 19, 2023

Expiration Date: Jul 19, 2031

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	10.00 %	9.914 %	G1	+/- 0.9% NIST Traceable	07/19/2023
OXYGEN	12.00 %	11.96 %	G1	+/- 1.0% NIST Traceable	07/19/2023
NITROGEN	Balance				

CALIBRATION STANDARDS

Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	13060405	CC411744	7.489 % CARBON DIOXIDE/NITROGEN	0.6%	May 14, 2025
NTRM	98051010	SG9161286BAL	12.05 % OXYGEN/NITROGEN	0.7%	Dec 14, 2023

ANALYTICAL EQUIPMENT

Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA-510 SV4MEUTJ CO2	CO2 NDIR (Dixon)	Jun 28, 2023
Horiba MPA-510 W603MM58 O2	O2 Paramagnetic (DIXON)	Jun 29, 2023

Triad Data Available Upon Request



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: EPA PROTOCOL STANDARD

Part Number: E03NI59E15A3452	Reference Number: 153-402157382-1
Cylinder Number: CC420519	Cylinder Volume: 159.0 CF
Laboratory: 124 - Tooele (SAP) - UT	Cylinder Pressure: 2015 PSIG
PGVP Number: B72021	Valve Outlet: 590
Gas Code: CO2,O2,BALN	Certification Date: Jul 15, 2021

Expiration Date: Jul 15, 2029

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	19.00 %	18.99 %	G1	+/- 0.6% NIST Traceable	07/15/2021
OXYGEN	22.00 %	22.41 %	G1	+/- 0.3% NIST Traceable	07/15/2021
NITROGEN	Balance				

CALIBRATION STANDARDS

Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	13060802	CC415397	24.04 % CARBON DIOXIDE/NITROGEN	0.6%	Dec 11, 2025
NTRM	12062008	CC367433	22.883 % OXYGEN/NITROGEN	0.2%	May 14, 2024

ANALYTICAL EQUIPMENT

Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA-510 SV4MEUTJ CO2	CO2 NDIR (Dixon)	Jun 17, 2021
Horiba MPA-510 W603MM58 O2	O2 Paramagnetic (Mason)	Jul 12, 2021

Triad Data Available Upon Request



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: CERTIFIED STANDARD-SPEC

Part Number:	X02NI99C15A1268	Reference Number:	153-402780689-1
Cylinder Number:	CC401933	Cylinder Volume:	144.0 CF
Laboratory:	124 - Tooele (SAP) - UT	Cylinder Pressure:	2015 PSIG
Analysis Date:	Jul 10, 2023	Valve Outlet:	350
Lot Number:	153-402780689-1		

Expiration Date: Jul 10, 2026

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

Component	Req Conc	Actual Concentration (Mole %)	Analytical Uncertainty
ETHYLENE	100.0 PPM	100.7 PPM	+/- 2%
NITROGEN	Balance		



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: CERTIFIED STANDARD-SPEC

Customer:	MOSTARDI PLATT	Reference Number:	160-402841639-1
Part Number:	X03NI99C15AC0W8	Cylinder Volume:	144.4 CF
Cylinder Number:	CC768228	Cylinder Pressure:	2015 PSIG
Laboratory:	124 - Plumsteadville - PA	Valve Outlet:	350SS
Analysis Date:	Sep 11, 2023		
Lot Number:	160-402841639-1		

Expiration Date: Mar 11, 2024

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

Component	Req Conc	Actual Concentration (Mole %)	Analytical Uncertainty
SULFUR HEXAFLUORIDE	5.000 PPM	5.009 PPM	+/- 5%
HYDROGEN CYANIDE	50.00 PPM	49.30 PPM	+/- 5%
NITROGEN	Balance		



Signature on file

END OF THE REPORT