

Section 114 Information Collection Request Emissions Test Report

Ash Grove Cement Company
Midlothian Cement Plant
EPA Registry ID: 110049749910
900 Gifco Road
Midlothian, Texas 76065
Report No. M235102A





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**Report Submittal Date:
March 4, 2024**

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TABLE OF CONTENTS

1.0 INTRODUCTION	1
2.0 TEST REQUIREMENTS	2
3.0 QA SPECIFICATIONS AND PROCESS DIAGRAM	3
Table 3-1 QA/QC Specifications.....	3
Table 3-2 Process Flow Diagram	3
4.0 TEST PROCEDURES	4
4.1 Method 1 Sample and Velocity Traverse Determination.....	4
4.2 Method 2 Volumetric Flow Rate Determination.....	4
4.3 Method 3A Oxygen (O ₂) and Carbon Dioxide (CO ₂) Determination.....	4
4.4 Method 26A Hydrogen Fluoride (HF) and Chlorine (Cl ₂) Determination	5
4.5 Method 320 Speciated Flue Gas Concentration Determinations	5
5.0 TEST RESULTS SUMMARIES.....	7
6.0 CERTIFICATION.....	10
APPENDICES	
Appendix A – Plant Operating Data.....	12
Appendix B – Test Section Diagrams.....	16
Appendix C – Sample Train Diagrams	19
Appendix D – Calculation Nomenclature and Formulas.....	23
Appendix E – Laboratory Sample Analysis	33
Appendix F – Reference Method Test Data	35
Appendix G – Calibration Data	55
Appendix H – Gas Cylinder Certifications	76

1.0 INTRODUCTION

Mostardi Platt conducted an air emissions test program for Ash Grove Cement Company at the Midlothian Cement Plant located in Midlothian, Texas. All testing was performed as described in the *Code of Federal Regulations*, Title 40, Part 60, Appendix A (40CFR60), Methods 1, 2, 3A, 4, 26A, and 40CFR63, Appendix A, (40CFR63) Method 320.

The Ash Grove Midlothian Cement Plant includes a single Kiln (Kiln 3) ~900,000 TPY semi-dry kiln system with slurry feed unto a jot disk. There is a single in-line calciner. The kiln system employs a SNCR, ACI, and DSI as needed to control NO_x and other compounds. Emission testing was performed at the testing location used for all compliance testing at the kiln stack or the main stack.

This test program was completed to satisfy the requirements of the United States Environmental Protection Agency (USEPA) Section 114 Information Collection Request for Portland Cement Manufacturing facilities as described in "Attachment 3 Source Testing Request for Portland Cement: Reporting Requirements".

The identification of individuals associated with the test program is summarized below:

Location	Address	Contact
Test Coordinator	Ash Grove Cement Company 900 Gifco Road Midlothian, TX 76065	Mr. Francisco Pinto Manager of Community and Environmental Affairs (972) 723-7231 francisco.pinto@ashgrove.com
Test Company Representative	Mostardi Platt 7715 Commercial Way, Suite 155 Henderson, NV 89011	Mr. Richard J. Sollars II Regional Manager (630) 993-2100 rsollars@mp-mail.com

2.0 TEST REQUIREMENTS

Testing was performed at the Kiln 3 stack. The following table presents a list of the parameters tested, the applicable methodologies utilized, and average test results:

Source	Parameter Tested	Test Results	Method/Regulation Citation
Kiln 3 Stack	Hydrogen Fluoride (HF)	≤ 0.20 ppmvw	USEPA Method 320, 40CFR63, Appendix A
		≤ 0.35 ppmvd @7% O ₂	
		≤ 0.21 lb/hr	
		≤ 0.0019 lb/ton clinker	
	HF ¹	≤ 0.12 ppmvd	Method 26A, 40CFR60, Appendix A
		≤ 0.13 ppmvd @7% O ₂	
		≤ 0.08 lb/hr	
		≤ 0.0007 lb/ton clinker	
	Chlorine (Cl ₂) ¹	≤ 0.04 ppmvd	USEPA Method 26A, 40CFR60, Appendix A
		≤ 0.04 ppmvd @7% O ₂	
		≤ 0.08 lb/hr	
		≤ 0.0007 lb/ton clinker	
	Hydrogen Cyanide (HCN)	≤ 0.21 ppmvw	USEPA Method 320, 40CFR63, Appendix A
		≤ 0.37 ppmvd @7% O ₂	
≤ 0.30 lb/hr			
≤ 0.0027 lb/ton clinker			
Oxygen (O ₂)	8.1 % (dry)	USEPA Method 3A, 40CFR60, Appendix A	
Carbon Dioxide (CO ₂)	15.4 % (dry)	USEPA Method 320, 40CFR63, Appendix A	
Moisture (H ₂ O)	37.6 %	USEPA Method 320, 40CFR63, Appendix A	
Cyclonic Flow Determination	PASS	USEPA Method 1, 40CFR60, Appendix A, Section 11.4	
Three-point O ₂ Stratification Determination	< 5 %	USEPA Method 3A, 40CFR60, Appendix A and Method 7E, Section 8.1.2	

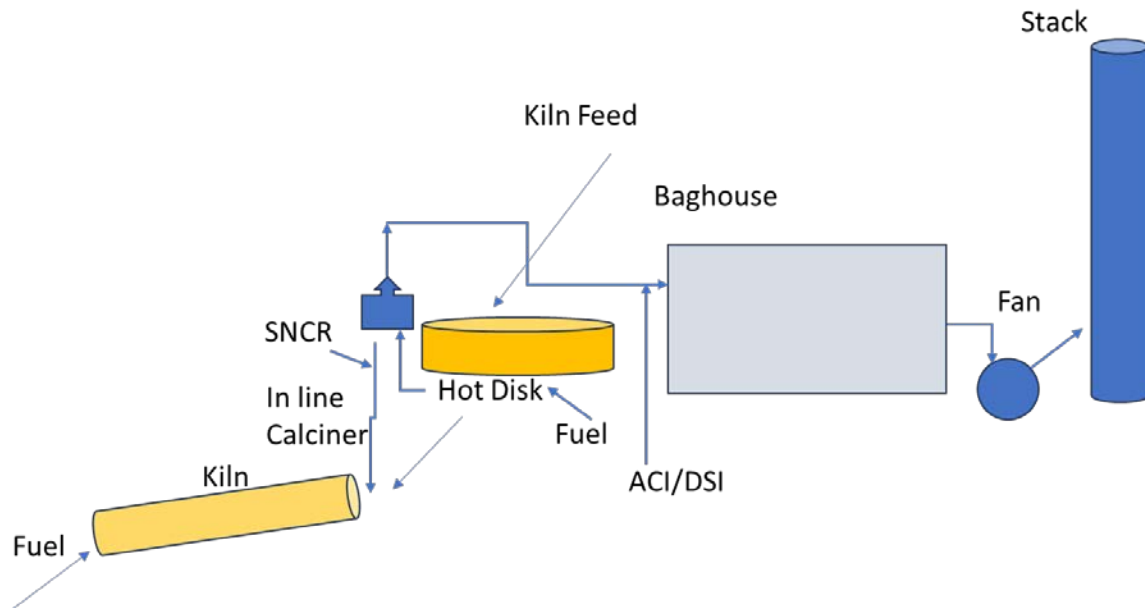
¹ HF and Cl₂ Method 26A results are reported as the average from Train A and Train B.

3.0 QA SPECIFICATIONS AND PROCESS DIAGRAM

Table 3-1 QA/QC Specifications

Parameter	Method	QA/QC Specification	Acceptance Criteria	Actual Result
HCN	320	Method Detection Limit	0.5 ppm	0.2 ppmvw
		SNR	>2500 at 64 scans	3459 (Run 1 Average)
		S Beam	>0.9	1.184 (Run 1 Average)
		Direct HCN Analysis	±5% of tag value	-4.9%
		Dynamic Spike Analysis	≤10% of total sample volume	8.8%
			Spike gas ~twice native concentration or 3-4 ppm addition to native concentration	+3.7 ppm
			≤±20% of expected value or ≤±0.5 ppm, whichever is less restrictive	≤±20% of expected value
Residuals	≤±0.3 ppm, or ≤±5% of measured value, whichever is less restrictive	≤±0.3 ppm		
Cl ₂	26A	Method Detection Limit	300 µg	150 µg
		Paired Train Agreement	≤10% Relative Deviation or ≤0.2 ppm, whichever is less restrictive.	≤10% Relative Deviation

Table 3-2 Process Flow Diagram



4.0 TEST PROCEDURES

All testing, sampling, analytical, and calibration procedures used for this test program were performed as described in the Title 40, *Code of Federal Regulations*, Part 60, Appendix A (40CFR60), Methods 1, 2, 3A, 4, 26A, and 40CFR63, Appendix A, Method 320; and the latest revisions thereof. Where applicable, the *Quality Assurance Handbook for Air Pollution Measurement Systems*, Volume III, Stationary Source Specific Methods, United States Environmental Protection Agency (USEPA) 600/R-94/038c, September 1994 was used to supplement procedures in addition to the appended “Draft General Test Plan”.

4.1 Method 1 Sample and Velocity Traverse Determination

Sample points for testing are determined using USEPA Test Method 1, 40CFR60, Appendix A. The characteristics of the measurement location is summarized below.

Sample Point Selection

Test Location	Stack Diameter	Port Length	Upstream Diameters	Downstream Diameters	Test Parameter	Number of Sampling Points
Kiln 3 Stack	11.502 Feet	7.0 Inches	16.8 Diameters	7.4 Diameters	HF/Cl ₂ (26A)	12
					O ₂ (3A)	3 (stratification)
					HCN/HF/CO ₂ (320/3A)	1

A cyclonic flow check was performed in accordance with Section 11.4, which demonstrated it meets the criteria of an average value of less than 20° and therefore is considered to be a suitable testing location for flow rate measurements.

4.2 Method 2 Volumetric Flow Rate Determination

The gas velocity and volumetric flowrate were determined using Method 2, 40CFR60, Appendix A, as an integrated part of the HF/Cl₂ sampling system.

Velocity pressures were determined by traversing the duct with wind tunnel calibrated S-type pitot tube. Temperatures were measured using K-type thermocouples with calibrated digital temperature indicators. The molecular weight and moisture content of the gases were also determined to permit the calculation of the volumetric flowrate.

4.3 Method 3A Oxygen (O₂) and Carbon Dioxide (CO₂) Determination

O₂ and CO₂ concentrations were determined in accordance with Method 3A, 40CFR60, Appendix A and Method 320, 40CFR63, Appendix A, respectively. A Servomex analyzer was used to determine O₂ concentrations while the MKS 2030 analyzer was used to determine CO₂ concentrations. The O₂ instrument has a paramagnetic detector and operates in a nominal range of 0-25%.

A list of calibration gases used and the results of all calibration and other required quality assurance checks are found in the appendix of this report. Copies of calibration gas certifications are also appended.

4.4 Method 26A Hydrogen Fluoride (HF) and Chlorine (Cl₂) Determination

HF and Cl₂ concentrations and emission rates were determined in accordance with Method 26A, 40CFR60, Appendix A. Paired sampling trains were used to collect the samples. A total of twelve (12) test points were sampled per run on the Kiln 3 stack. The sample was extracted isokinetically from the gas stream and passed through dilute sulfuric acid (0.1N H₂SO₄). HF was collected in the dilute acid. Cl₂ was collected in the dilute sodium hydroxide (0.1N NaOH) solution. The sample train consisted of a Teflon coated nozzle, a heated borosilicate glass probe liner, a Teflon® filter placed on the outlet of the glass probe liner, and six impingers. The first two impingers contained the 0.1N H₂SO₄, the third remained empty (and was recovered with the first two impingers), the fourth and fifth impingers contained the 0.1N NaOH, while the sixth impinger contained silica gel to absorb any remaining moisture. A de-ionized water rinse was performed on each set of impingers, and samples were stored in Nalgene sample containers for transport. The 0.1N H₂SO₄ impinger catch samples were analyzed for HF while the 0.1N NaOH impinger catch samples were analyzed for Cl₂. A method detection limit (MDL) of 150 µg was determined for both HF and Cl₂ using the "Definition and Procedure for the Determination of the Method Detection Limit, Revision 2". All equipment used was calibrated in accordance with the specifications of the method. Calibration data is appended.

Hand recorded field data sheets were reviewed and scans are retained on the Mostardi Platt network. Copies of this data is available upon request.

4.5 Method 320 Speciated Flue Gas Concentration Determinations

The sampling procedures for HCN and HF were performed in accordance with USEPA Method 320, 40CFR63, Appendix A. Data was continuously recorded with a data logging system throughout sampling, with brief interruption to properly label reference spectra.

The average gas effluent concentrations were determined from the average gas concentration displayed by the MKS 2030 analyzer.

All sampling system components were heated to 375°F +/- 25°F, including: stainless steel sample probe, stainless steel calibration tee, in line glass fiber particulate filter, Teflon® sample line, heated head sample pump, and FTIR detector cell. The sample pump distributes the gas sample to the instrument at a steady sample flow rate (+/- 10%). All components of the sampling system are constructed of stainless steel, glass, or Teflon®.

FTIR technology works on the principle that most gases absorb infrared light. This is true for all compounds except for homonuclear diatomic molecules and noble gases such as: N₂, O₂, H₂, He, Ne, and Ar. Vibrations, stretches, bends, and rotations within the bonds of a molecule determine the infrared absorption distinctiveness. The absorption creates a "fingerprint" which is unique for each given compound. The quantity of infrared light absorbed is proportional to the gas concentration. Most compounds have absorbencies at different infrared frequencies, thus allowing the simultaneous analysis of multiple compounds at one time. The FTIR software compares each sample spectrum to a user-selected list of calibration references and concentration data is generated.

FTIR data was collected using an MKS MultiGas 2030 FTIR spectrometer. Data was generated at 0.5 cm⁻¹. Each Spectra was derived from the coaddition of 62-64 scans with a new data point generated approximately every minute. HCN analyte spiking assured the ability of the FTIR to quantify HCN in the presence of effluent gas. All analyte spikes were introduced using an instrument grade stainless steel rotameter. All QA/QC procedures were within the acceptance criteria allowance of the applicable methodology and the "General Test Plan."

5.0 TEST RESULTS SUMMARIES

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Test Location: Kiln 3
Test Method: 26A - Combined Results

	Source Condition	Normal	Normal	Normal	
	Date	1/4/24	1/4/24	1/4/24	
	Start Time	10:50	12:25	14:17	
	End Time	12:03	13:39	15:30	
	Run 1	Run 2	Run 3	Average	
Stack Conditions					
Average Gas Velocity, ft/sec	79.233	78.922	79.352	79.169	
Gas Volumetric Flow Rate, acfm	493,963	492,023	494,699	493,562	
Gas Volumetric Flow Rate, dscfm	207,668	207,610	211,366	208,881	
Gas Volumetric Flow Rate, scfm	321,977	325,496	323,879	323,784	
Average %CO ₂ by volume, dry basis	14.9	15.4	16.0	15.4	
Average %O ₂ by volume, dry basis	8.4	8.1	7.8	8.1	
Clinker Production, ton/hr	107.5	110.4	110.4	109.4	
Chlorine (Cl₂) Emissions					
ppm	≤ 0.04	≤ 0.04	≤ 0.04	≤ 0.04	
ppm@7%O ₂	≤ 0.04	≤ 0.04	≤ 0.04	≤ 0.04	
lb/hr	≤ 0.08	≤ 0.08	≤ 0.08	≤ 0.08	
lb/ton	≤ 0.0007	≤ 0.0007	≤ 0.0007	≤ 0.0007	
Hydrogen Fluoride (HF) Emissions					
ppm	≤ 0.12	≤ 0.12	≤ 0.12	≤ 0.12	
ppm@7%O ₂	≤ 0.14	≤ 0.13	≤ 0.13	≤ 0.13	
lb/hr	≤ 0.08	≤ 0.08	≤ 0.08	≤ 0.08	
lb/ton	≤ 0.0007	≤ 0.0007	≤ 0.0007	≤ 0.0007	

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Test Location: Kiln 3
 Test Method: 26A - A Train

	Source Condition	Normal	Normal	Normal				
	Date	1/4/24	1/4/24	1/4/24				
	Start Time	10:50	12:25	14:17				
	End Time	12:03	13:39	15:30				
		Run 1A	Run 2A	Run 3A	Average			
Stack Conditions								
Average Gas Temperature, °F		327.6	316.6	324.3	322.8			
Flue Gas Moisture, percent by volume		35.0%	35.9%	33.4%	34.8%			
Average Flue Pressure, in. Hg		29.11	29.11	29.11	29.11			
Gas Sample Volume, dscf		51,756	52,792	52,855	52,468			
Average Gas Velocity, ft/sec		79.154	79.275	79.643	79.357			
Gas Volumetric Flow Rate, acfm		493,471	494,222	496,517	494,737			
Gas Volumetric Flow Rate, dscfm		209,334	209,428	216,521	211,761			
Gas Volumetric Flow Rate, scfm		321,826	326,881	325,189	324,632			
Average %CO ₂ by volume, dry basis		14.9	15.4	16.0	15.4			
Average %O ₂ by volume, dry basis		8.4	8.1	7.8	8.1			
Isokinetic Variance		99.5	101.4	98.2	99.7			
Chlorine (Cl₂) Emissions								
ug of sample collected	≤	150.00	≤	150.00	≤	150.00	≤	150.00
ppm	≤	0.04	≤	0.03	≤	0.03	≤	0.03
Hydrogen Fluoride (HF) Emissions								
ug of sample collected	≤	150.00	≤	150.00	≤	150.00	≤	150.00
ppm	≤	0.12	≤	0.12	≤	0.12	≤	0.12

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Test Location: Kiln 3
 Test Method: 26A - B Train

Source Condition	Normal	Normal	Normal	
Date	1/4/24	1/4/24	1/4/24	
Start Time	10:50	12:25	14:17	
End Time	12:03	13:39	15:30	
	Run 1B	Run 2B	Run 3B	Average
Stack Conditions				
Average Gas Temperature, °F	328.4	316.3	324.8	323.2
Flue Gas Moisture, percent by volume	36.0%	36.5%	36.1%	36.2%
Average Flue Pressure, in. Hg	29.11	29.11	29.11	29.11
Gas Sample Volume, dscf	50.909	51.635	51.627	51.390
Average Gas Velocity, ft/sec	79.312	78.569	79.060	78.980
Gas Volumetric Flow Rate, acfm	494,455	489,823	492,881	492,386
Gas Volumetric Flow Rate, dscfm	206,001	205,792	206,210	206,001
Gas Volumetric Flow Rate, scfm	322,127	324,111	322,568	322,935
Average %CO ₂ by volume, dry basis	14.9	15.4	16.0	15.4
Average %O ₂ by volume, dry basis	8.4	8.1	7.8	8.1
Isokinetic Variance	99.4	101.0	100.7	100.4

Chlorine (Cl₂) Emissions				
ug of sample collected	≤ 150.00	≤ 150.00	≤ 150.00	≤ 150.00
ppm	≤ 0.04	≤ 0.04	≤ 0.04	≤ 0.04

Hydrogen Fluoride (HF) Emissions				
ug of sample collected	≤ 150.00	≤ 150.00	≤ 150.00	≤ 150.00
ppm	≤ 0.13	≤ 0.12	≤ 0.12	≤ 0.12

Ash Grove Cement Company Midlothian Cement Plant Kiln 3 Stack Normal Operations/>90% Production Reference Method Test Data									
Test No.	Date	Start Time	End Time	O ₂ % (dry)	Moisture %	HCN ppmvw	HCN ppmvd @ 7% O ₂	HF ppmvw	HF ppmvd @ 7% O ₂
1	1/4/2024	10:50	11:49	8.4	39.1%	≤ 0.21	≤ 0.38	0.23	0.41
2	1/4/2024	12:25	13:24	8.1	37.0%	≤ 0.20	≤ 0.35	≤ 0.21	≤ 0.37
3	1/4/2024	14:17	15:16	7.8	36.6%	≤ 0.22	≤ 0.37	≤ 0.17	≤ 0.28
Average				8.1	37.6%	≤ 0.21	≤ 0.37	≤ 0.20	≤ 0.35


Test No.	Date	Start Time	End Time	Volumetric Flow, DSCFM	Clinker Production, ton/hr	HCN lb/hr	HCN lb/ton	HF lb/hr	HF lb/ton
1	1/4/2024	10:50	11:49	207,668	107.5	≤ 0.30	≤ 0.0028	0.24	0.0022
2	1/4/2024	12:25	13:24	207,610	110.4	≤ 0.28	≤ 0.0026	≤ 0.22	≤ 0.0020
3	1/4/2024	14:17	15:16	211,366	110.4	≤ 0.31	≤ 0.0028	≤ 0.18	≤ 0.0016
Average				208,881	109.4	≤ 0.30	≤ 0.0027	≤ 0.21	≤ 0.0019

6.0 CERTIFICATION

Mostardi Platt is pleased to have been of service to Ash Grove Cement Company. If you have any questions regarding this test report, please do not hesitate to contact us at 630-993-2100.

As project manager, I hereby certify that this test report represents a true and accurate summary of emissions test results and the methodologies employed to obtain those results, and the test program was performed in accordance with the methods specified in this test report.

MOSTARDI PLATT



Aaron Benninghoff

Project Manager



Chet A. Gutwein

Quality Assurance

APPENDICES

Appendix A – Plant Operating Data

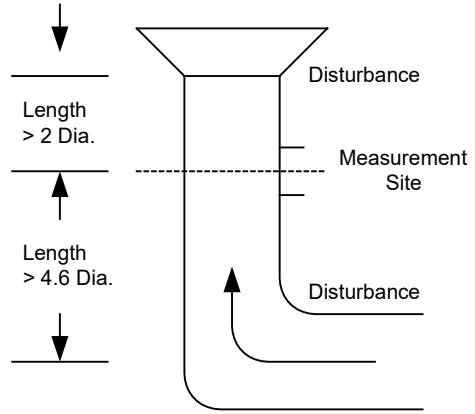
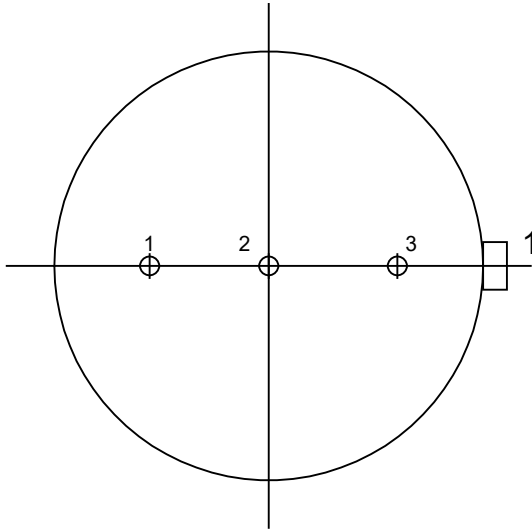
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1/4/2024 10:59	105.7
1/4/2024 11:00	105.6
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1/4/2024 11:02	106.2
1/4/2024 11:03	106.3
1/4/2024 11:04	106.3
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1/4/2024 11:26	103.6
1/4/2024 11:27	105.2
1/4/2024 11:28	106
1/4/2024 11:29	106.9
1/4/2024 11:30	107.3
1/4/2024 11:31	101.6
1/4/2024 11:32	106.1
1/4/2024 11:33	105.9
1/4/2024 11:34	106.2
1/4/2024 11:35	106.1
1/4/2024 11:36	106.2
1/4/2024 11:37	106.1
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1/4/2024 11:42	111.3
1/4/2024 11:43	111.1
1/4/2024 11:44	110.8
1/4/2024 11:45	110.6
1/4/2024 11:46	110.5
1/4/2024 11:47	110.5
1/4/2024 11:48	110.6
1/4/2024 11:49	110.4
1/4/2024 11:50	110.5
1/4/2024 11:51	110.5
1/4/2024 11:52	110.4
1/4/2024 11:53	110.5
1/4/2024 11:54	110.4
1/4/2024 11:55	109.2
1/4/2024 11:56	109.5
1/4/2024 11:57	109.8
1/4/2024 11:58	110.1
1/4/2024 11:59	110.3
1/4/2024 12:00	110.3
1/4/2024 12:01	110.2
1/4/2024 12:02	110.5
1/4/2024 12:03	110.5
Average	107.5

Date/Time	KILN: CLINKER (TNHR) Expression Value
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1/4/2024 12:27	110.4
1/4/2024 12:28	110.4
1/4/2024 12:29	110.4
1/4/2024 12:30	110.3
1/4/2024 12:31	108.6
1/4/2024 12:32	109.4
1/4/2024 12:33	109.8
1/4/2024 12:34	110.1
1/4/2024 12:35	110.2
1/4/2024 12:36	110.2
1/4/2024 12:37	110.3
1/4/2024 12:38	110.4
1/4/2024 12:39	110.5
1/4/2024 12:40	110.4
1/4/2024 12:41	110.4
1/4/2024 12:42	110.5
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1/4/2024 12:44	110.4
1/4/2024 12:45	110.4
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1/4/2024 12:47	110.6
1/4/2024 12:48	110.5
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1/4/2024 12:50	110.6
1/4/2024 12:51	110.5
1/4/2024 12:52	110.6
1/4/2024 12:53	110.4
1/4/2024 12:54	110.5
1/4/2024 12:55	110.4
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1/4/2024 13:01	111
1/4/2024 13:02	110.8
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1/4/2024 13:05	110.5
1/4/2024 13:06	110.5
1/4/2024 13:07	110.5
1/4/2024 13:08	110.5
1/4/2024 13:09	110.5
1/4/2024 13:10	110.4
1/4/2024 13:11	110.4
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1/4/2024 13:13	110.4
1/4/2024 13:14	110.4
1/4/2024 13:15	110.4
1/4/2024 13:16	110.5
1/4/2024 13:17	110.4
1/4/2024 13:18	110.4
1/4/2024 13:19	110.4
1/4/2024 13:20	110.4
1/4/2024 13:21	110.5
1/4/2024 13:22	110.4
1/4/2024 13:23	110.4
1/4/2024 13:24	110.4
1/4/2024 13:25	110.4
1/4/2024 13:26	110.4
1/4/2024 13:27	110.4
1/4/2024 13:28	110.4
1/4/2024 13:29	110.4
1/4/2024 13:30	110.4
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1/4/2024 13:32	110.5
1/4/2024 13:33	110.5
1/4/2024 13:34	110.5
1/4/2024 13:35	110.4
1/4/2024 13:36	110.5
1/4/2024 13:37	110.4
1/4/2024 13:38	110.5
1/4/2024 13:39	110.4
Average	110.4

Date/Time	KILN: CLINKER (TNHR) Expression Value
1/4/2024 14:17	110.4
1/4/2024 14:18	110.5
1/4/2024 14:19	110.5
1/4/2024 14:20	110.4
1/4/2024 14:21	110.4
1/4/2024 14:22	110.4
1/4/2024 14:23	110.4
1/4/2024 14:24	110.4
1/4/2024 14:25	110.4
1/4/2024 14:26	110.5
1/4/2024 14:27	110.4
1/4/2024 14:28	110.4
1/4/2024 14:29	110.5
1/4/2024 14:30	110.5
1/4/2024 14:31	110.4
1/4/2024 14:32	110.4
1/4/2024 14:33	110.5
1/4/2024 14:34	110.5
1/4/2024 14:35	110.4
1/4/2024 14:36	110.5
1/4/2024 14:37	110.4
1/4/2024 14:38	110.4
1/4/2024 14:39	110.4
1/4/2024 14:40	110.5
1/4/2024 14:41	110.4
1/4/2024 14:42	110.4
1/4/2024 14:43	110.5
1/4/2024 14:44	110.4
1/4/2024 14:45	110.4
1/4/2024 14:46	110.4
1/4/2024 14:47	110.4
1/4/2024 14:48	110.4
1/4/2024 14:49	110.4
1/4/2024 14:50	110.5
1/4/2024 14:51	110.4
1/4/2024 14:52	110.4
1/4/2024 14:53	110.4
1/4/2024 14:54	110.4
1/4/2024 14:55	110.5
1/4/2024 14:56	110.4
1/4/2024 14:57	110.4
1/4/2024 14:58	110.4
1/4/2024 14:59	110.4
1/4/2024 15:00	110.4
1/4/2024 15:01	110.4
1/4/2024 15:02	110.3
1/4/2024 15:03	110.5
1/4/2024 15:04	110.5
1/4/2024 15:05	110.5
1/4/2024 15:06	110.4
1/4/2024 15:07	110.5
1/4/2024 15:08	110.4
1/4/2024 15:09	110.5
1/4/2024 15:10	110.4
1/4/2024 15:11	110.4
1/4/2024 15:12	110.5
1/4/2024 15:13	110.4
1/4/2024 15:14	110.5
1/4/2024 15:15	110.4
1/4/2024 15:16	110.3
1/4/2024 15:17	110.4
1/4/2024 15:18	110.4
1/4/2024 15:19	110.5
1/4/2024 15:20	110.4
1/4/2024 15:21	110.5
1/4/2024 15:22	110.4
1/4/2024 15:23	110.4
1/4/2024 15:24	110.4
1/4/2024 15:25	110.4
1/4/2024 15:26	110.4
1/4/2024 15:27	110.4
1/4/2024 15:28	110.4
1/4/2024 15:29	110.5
1/4/2024 15:30	110.4
Average	110.4

Appendix B – Test Section Diagrams

STRATIFICATION TEST FOR ROUND DUCTS



Job: Ash Grove Cement Company
Midlothian Cement Plant
Midlothian, Texas

Test Location: Kiln 3 Stack

Stack Diameter: 11.50 Feet

Stack Area: 103.91 Square Feet

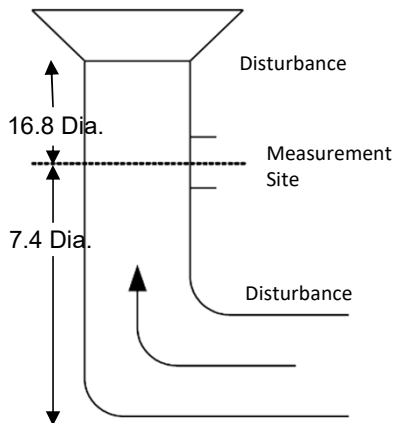
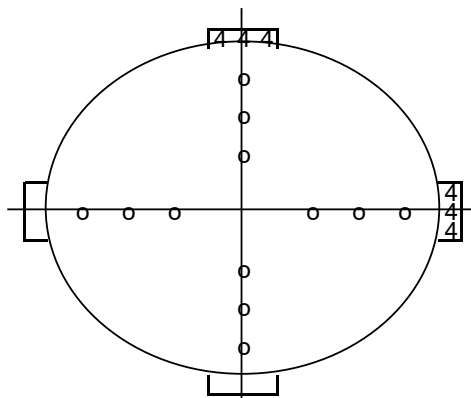
No. Sample Points: 3

Port Length: 7.0 Inches

Distance from Inside Wall
To Traverse Point:

1. 83.3 % of diameter
2. 50.0 % of diameter
3. 16.7 % of diameter

EQUAL AREA TRAVERSE FOR ROUND DUCTS



Client: Ash Grove Cement Company

Facility: Midlothian Cement Plant

Test Location: Kiln 3

Date: 01/04/24

Diameter (Feet): 11.502

Port Length (In): 7.00

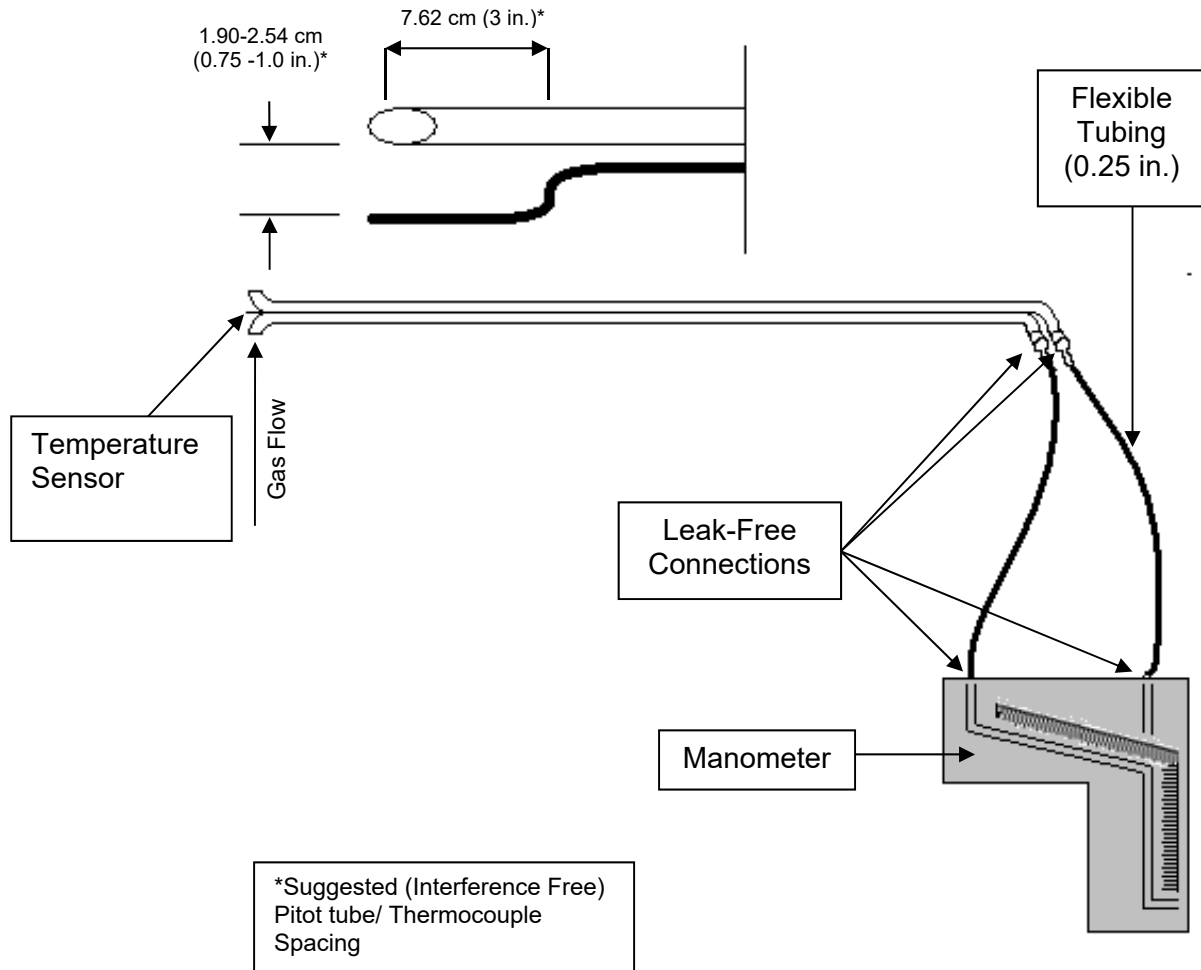
Ports Sampled: 4

Points/Port: 3

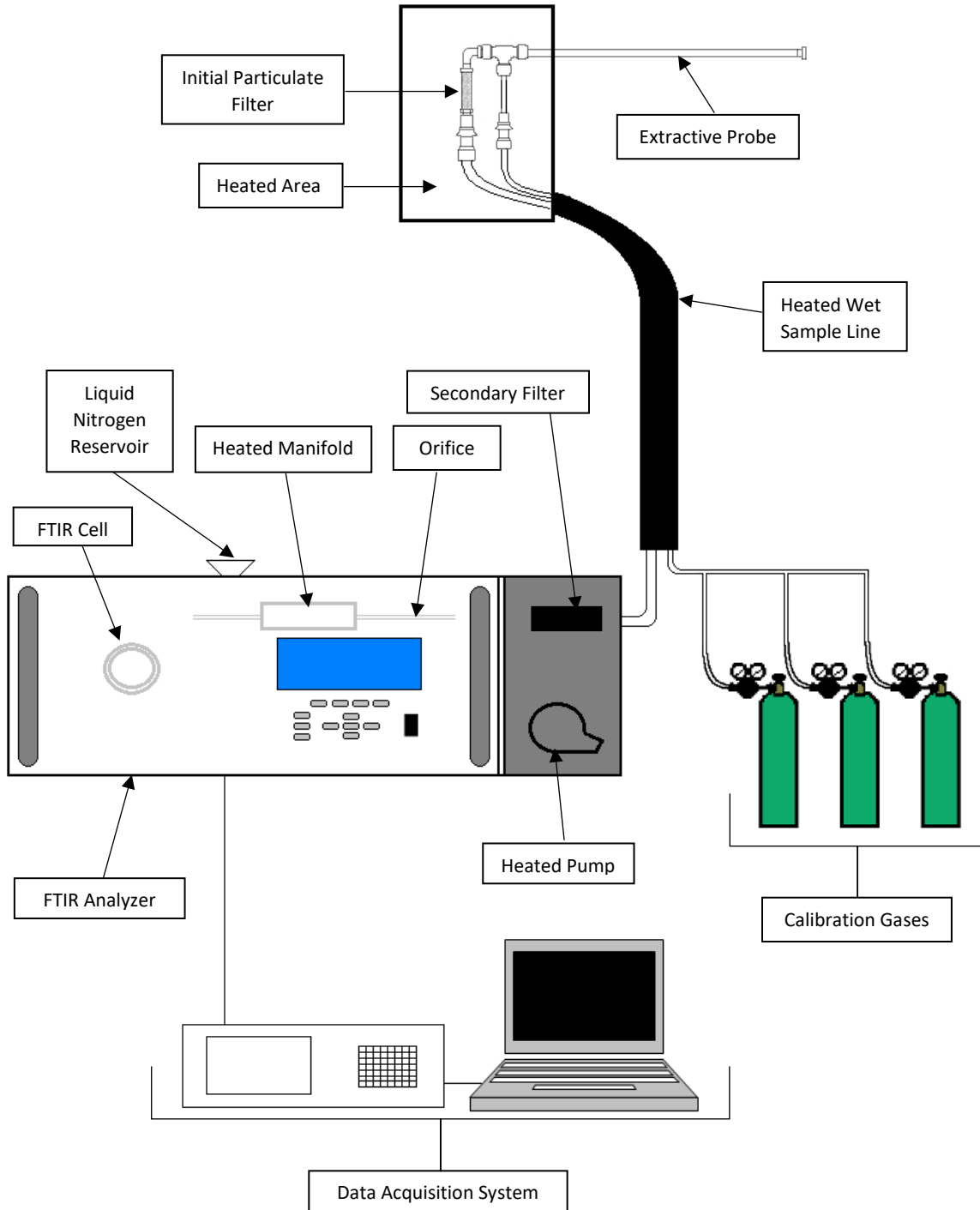
	Point Markings	
	From inside wall (in.)	% of Diameter
1	6.07	4.40
2	20.15	14.60
3	40.86	29.60

Appendix C – Sample Train Diagrams

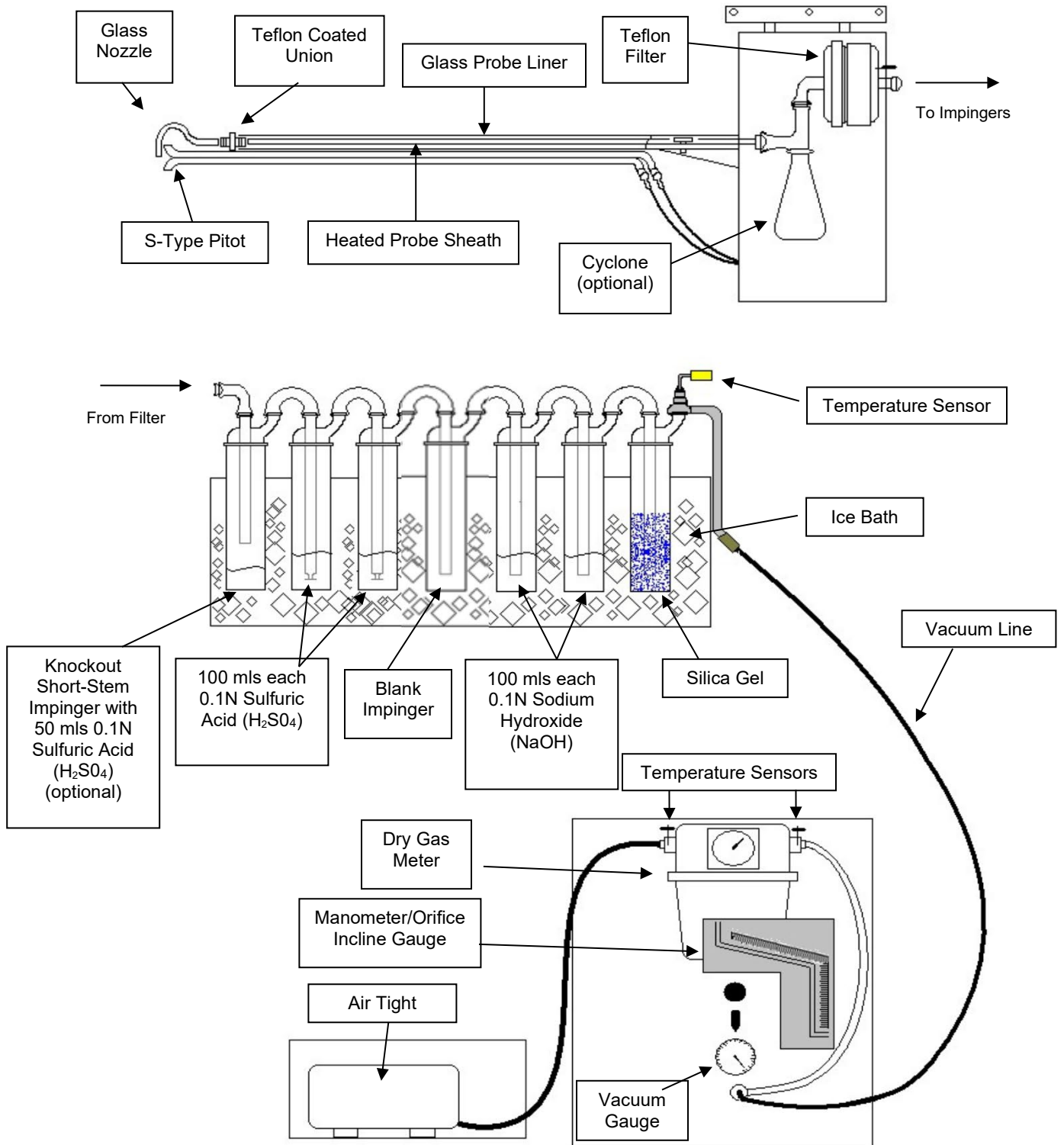
USEPA Method 2 – Type S Pitot Tube Manometer Assembly



USEPA Method 320 – Vapor Phase Organic and Inorganic Emissions by Extractive Fourier Transform Infrared (FTIR) Spectroscopy Sample Train Diagram



USEPA Method 26A – HF and Cl₂ Sample Train Diagram



Appendix D – Calculation Nomenclature and Formulas

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Project #: M235102
Test Location: Kiln 3 Stack
Date: 1/4/24

Sample Calculations

$$(8.63\% - 0.36\%) \times \frac{\text{O2 \% (dry)} \quad 11.95\%}{12.11\% - 0.36\%} = 8.42\%$$

$$C_{\text{gas}} = (C - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0}$$

where:

C_{gas} = Effluent gas concentration, dry basis, ppm or %

C = Average gas concentration indicated by gas analyzer, dry basis, ppm or %

C_0 = Average of initial and final system calibration bias check responses for the zero gas, ppm or %

C_{m} = Average of initial and final system calibration bias check responses for the upscale calibration gas, ppm or %

C_{ma} = Actual concentration of the upscale calibration gas, ppm or %

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Project #: M235102
 Test Location: Kiln 3 Stack
 Date: 1/4/24

FTIR Sample Calculations

Direct Recovery % of Calibration Transfer Standard

$$DR_{cts} = \frac{D_{cts}}{C_{ma}} \times 100$$

$$C_{ma} = \underline{100.4}$$

$$D_{cts} = \underline{99.9}$$

$$DR_{cts} = \underline{99.5\%}$$

Recovery % with Calibration Transfer Standard System Purge

$$R_{cts} = \frac{Sys_{cts}}{D_{cts}} \times 100$$

$$Sys_{cts} = \underline{97.1}$$

$$D_{cts} = \underline{99.9}$$

$$R_{cts} = \underline{97\%}$$

Direct Recovery % of Analyte Spike Gas

SF6

$$DR_{sf6} = \frac{D_{sf6}}{C_{ma}} \times 100$$

$$C_{ma} = \underline{5.0}$$

$$D_{sf6} = \underline{5.0}$$

$$DR_{sf6} = \underline{101\%}$$

HCN

$$DR_{asg} = \frac{D_{asg}}{C_{ma}} \times 100$$

$$C_{ma} = \underline{49.3}$$

$$D_{asg} = \underline{46.9}$$

$$DR_{asg} = \underline{95.1\%}$$

Dilution Factor for Analyte Spiking

$$DF = \frac{Spk_{sf6}}{D_{sf6}}$$

$$Spk_{sf6} = \underline{0.400}$$

$$D_{sf6} = \underline{5.036}$$

$$DF = \underline{0.079}$$

Recovery % for Analyte Spike With HCN

$$R_x = \frac{Spk_x}{(N_x \times (1-DF) + D_{asg} \times DF)}$$

$$Spk_x = \underline{2.8}$$

$$N_x = \underline{-0.7}$$

$$DF = \underline{0.079}$$

$$D_{asg} = \underline{46.9}$$

$$R_x = \underline{90.2} \%$$

where:

- DR_{cts} = Recovery % of the calibration transfer standard directly to the analyzer
- C_{ma} = certified concentration of calibration gas, ppm
- D_{cts} = Concentration of the calibration transfer standard gas directly to the analyzer, ppm
- R_{cts} = Recovery % of the calibration transfer standard through the sampling system
- Sys_{cts} = Concentration of the calibration transfer standard gas through the system, ppm
- DF = Dilution Factor of analyte spike gas
- Spk_{sf6} = SF6 concentration in effluent during spiking
- Spk_x = Analyte concentration in effluent during spiking
- D_{asg} = Concentration of the analyte spike gas directly to the analyzer, ppm
- D_{sf6} = Concentration of the SF6 directly to the analyzer, ppm
- R_x = Recovery % of the analyte spike gas
- N_x = Native effluent (HCN) concentration prior to analyte spike

MOSTARDI PLATT

Moisture Calculations

$$V_{wc(std)} = \frac{(V_f - V_i)\rho_w RT_{std}}{P_{std}M_w} = 0.04707(V_f - V_i)$$

$$V_{wsg(std)} = \frac{(W_f - W_i)\rho_w RT_{std}}{P_{std}M_w} = 0.04715(W_f - W_i)$$

$$V_{m(std)} = 17.64 V_m Y \frac{P_{bar} + \frac{\Delta H}{13.6}}{T_m}$$

$$B_{ws} = \frac{V_{wc(std)} + V_{wsg(std)}}{V_{wc(std)} + V_{wsg(std)} + V_{m(std)}}$$

Where:

B_{ws} = Water vapor in gas stream, proportion by volume

M_w = Molecular weight of water, 18.015 lb/lb-mole

P_{bar} = Barometric pressure at the testing site, in. Hg

P_{std} = Standard absolute pressure, 29.92 in. Hg

R = Ideal gas constant, $0.048137 \text{ (in. Hg)(ft}^3\text{)/(g-mole)(}^\circ\text{R)} =$
 $[21.8348 \text{ (in. Hg)(ft}^3\text{)/(lb-mole)(}^\circ\text{R)}]/453.592 \text{ g-mole/lb-mole}$

T_m = Absolute average dry gas meter temperature, $^\circ\text{R}$

T_{std} = Standard absolute temperature, 528 $^\circ\text{R}$

V_f = Final volume of condenser water, ml

V_i = Initial volume of condenser water, ml

V_m = Dry gas volume measured by dry gas meter, dcf

$V_{m(std)}$ = Dry gas volume measured by dry gas meter, corrected to standard conditions, scf

$V_{wc(std)}$ = Volume of condensed water vapor, corrected to standard conditions, scf

$V_{wsg(std)}$ = Volume of water vapor collected in silica gel, corrected to standard conditions, scf

W_f = Final weight of silica gel, g

W_i = Initial weight of silica gel, g

Y = Dry gas meter calibration factor

ΔH = Average pressure exerted on dry gas meter outlet by gas sample bag, in. H_2O

ρ_w = Density of water, 0.9982 g/ml

13.6 = Specific gravity of mercury (Hg)

17.64 = T_{std}/P_{std}

0.04707 = ft^3/ml 0.04715 = ft^3/g

MOSTARDI PLATT

Volumetric Flow Nomenclature

- A = Cross-sectional area of stack or duct, ft²
- B_{ws} = Water vapor in gas stream, proportion by volume
- C_p = Pitot tube coefficient, dimensionless
- M_d = Dry molecular weight of gas, lb/lb-mole
- M_s = Molecular weight of gas, wet basis, lb/lb-mole
- M_w = Molecular weight of water, 18.0 lb/lb-mole
- P_{bar} = Barometric pressure at testing site, in. Hg
- P_g = Static pressure of gas, in. Hg (in. H₂O/13.6)
- DH = Static pressure of gas, in. H₂O
- P_s = Absolute pressure of gas, in. Hg = P_{bar} + P_g
- P_{std} = Standard absolute pressure, 29.92 in. Hg
- A_{cfm} = Actual volumetric gas flow rate
- Sc_{fm} = Volumetric gas flow rate, corrected to standard conditions
- D_{scfm} = Standard volumetric flow rate, corrected to dry conditions
- R = Ideal gas constant, 21.85 in. Hg-ft³/°R-lb-mole
- T_s = Average stack gas temperature, °F
- T_m = Average dry gas meter temperature, °F
- T_{std} = Standard absolute temperature, 528°R
- v_s = Gas velocity, ft/sec
- V_{m(std)} = Volume of gas sampled, corrected to standard conditions, scf
- V_{w(std)} = Volume of water vapor in gas sample, corrected to standard conditions, scf
- V_{lc} = Volume of liquid collected
- Y = Dry gas meter calibration factor
- Δp = Velocity head of gas, in. H₂O
- K₁ = 17.647 °R/in. Hg
- %EA = Percent excess air
- %CO₂ = Percent carbon dioxide by volume, dry basis
- %O₂ = Percent oxygen by volume, dry basis
- %N₂ = Percent nitrogen by volume, dry basis
- 0.264 = Ratio of O₂ to N₂ in air, v/v
- 0.28 = Molecular weight of N₂ or CO, divided by 100
- 0.32 = Molecular weight of O₂ divided by 100
- 0.44 = Molecular weight of CO₂ divided by 100
- 13.6 = Specific gravity of mercury (Hg)

MOSTARDI PLATT

Volumetric Air Flow Calculations

$$Vm (std) = 17.647 \times Vm \times \left[\frac{(P_{bar} + \left[\frac{DH}{13.6} \right])}{(460 + Tm)} \right] \times Y$$

$$Vw (std) = 0.0471 \times Vlc$$

$$Bws = \left[\frac{Vw (std)}{Vw (std) + Vm (std)} \right]$$

$$Md = (0.44 \times \%CO_2) + (0.32 \times \%O_2) + [0.28 \times (100 - \%CO_2 - \%O_2)]$$

$$Ms = Md \times (1 - Bws) + (18 \times Bws)$$

$$Vs = \sqrt{\frac{(Ts + 460)}{Ms \times Ps}} \times \sqrt{DP} \times Cp \times 85.49$$

$$Acfm = Vs \times Area (of\ stack\ or\ duct) \times 60$$

$$Scfm = Acfm \times 17.647 \times \left[\frac{Ps}{(460 + Ts)} \right]$$

$$Scfh = Scfm \times 60 \frac{min}{hr}$$

$$Dscfm = Scfm \times (1 - Bws)$$

MOSTARDI PLATT

Isokinetic Calculation Formulas

$$1. V_{w(\text{std})} = V_{lc} \left(\frac{\rho_w}{M_w} \right) \left(\frac{RT_{\text{std}}}{P_{\text{std}}} \right) = K_2 V_{lc}$$

$$2. V_{m(\text{std})} = V_m Y \left(\frac{T_{\text{std}}}{T_m} \right) \left(\frac{(P_{\text{bar}} + (\frac{\Delta H}{13.6}))}{P_{\text{std}}} \right) = K_1 V_m Y \frac{(P_{\text{bar}} + (\frac{\Delta H}{13.6}))}{T_m}$$

$$3. B_{ws} = \frac{V_{w(\text{std})}}{(V_{m(\text{std})} + V_{w(\text{std})})}$$

$$4. M_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2)$$

$$5. M_s = M_d(1 - B_{ws}) + 18.0(B_{ws})$$

$$6. C_a = \frac{m_a}{V_a \rho_a}$$

$$7. W_a = C_a V_{aw} \rho_a$$

$$8. C_{acf} = 15.43 K_i \left(\frac{m_n P_s}{(V_{w(\text{std})} + V_{m(\text{std})}) T_s} \right)$$

$$9. C_s = (15.43 \text{ grains/gram}) (m_n / V_{m(\text{std})})$$

$$10. v_s = K_p C_p \sqrt{\frac{\Delta P T_s}{P_s M_s}}$$

$$11. Q_{acfm} = v_s A (60_{\text{sec/min}})$$

$$12. Q_{sd} = (3600_{\text{sec/hr}}) (1 - B_{ws}) v_s \left(\frac{T_{\text{std}} P_s}{T_s P_{\text{std}}} \right) A$$

$$13. E \text{ (emission rate, lbs/hr)} = Q_{sd} (C_s / 7000 \text{ grains/lb})$$

$$14. IKV = \frac{T_s V_{m(\text{std})} P_{\text{std}}}{T_{\text{std}} v_s \theta A_n P_s 60(1 - B_{ws})} = K_4 \frac{T_s V_{m(\text{std})}}{P_s v_s A_n \theta (1 - B_{ws})}$$

$$15. \%EA = \left(\frac{\%O_2 - (0.5 \%CO)}{0.264 \%N_2 - (\%O_2 - 0.5 \%CO)} \right) \times 100$$

MOSTARDI PLATT

Isokinetic Nomenclature

- A = Cross-sectional area of stack or duct, square feet
A_n = Cross-sectional area of nozzle, square feet
B_{ws} = Water vapor in gas stream, by volume
C_a = Acetone blank residue concentration, g/g
C_{act} = Concentration of particulate matter in gas stream at actual conditions, gr/acf
C_p = Pitot tube coefficient
C_s = Concentration of particulate matter in gas stream, dry basis, corrected to standard conditions, gr/dscf
IKV = Isokinetic sampling variance, must be 90.0 % ≤ IKV ≤ 110.0%
M_d = Dry molecular weight of gas, lb/lb-mole
M_s = Molecular weight of gas, wet basis, lb/lb-mole
M_w = Molecular weight of water, 18.0 lb/lb-mole
m_a = Mass of residue of acetone after evaporation, grams
P_{bar} = Barometric pressure at testing site, inches mercury
P_g = Static pressure of gas, inches mercury (inches water/13.6)
P_s = Absolute pressure of gas, inches mercury = P_{bar} + P_g
P_{std} = Standard absolute pressure, 29.92 inches mercury
Q_{acfm} = Actual volumetric gas flow rate, acfm
Q_{sd} = Dry volumetric gas flow rate corrected to standard conditions, dscfh
R = Ideal gas constant, 21.85 inches mercury cubic foot/°R-lb-mole
T_m = Dry gas meter temperature, °R
T_s = Gas temperature, °R
T_{std} = Absolute temperature, 528°R
V_a = Volume of acetone blank, ml
V_{aw} = Volume of acetone used in wash, ml
W_a = Weight of residue in acetone wash, grams
m_n = Total amount of particulate matter collected, grams
V_{1c} = Total volume of liquid collected in impingers and silica gel, ml
V_m = Volume of gas sample as measured by dry gas meter, dcf
V_{m(std)} = Volume of gas sample measured by dry gas meter, corrected to standard conditions, dscf
V_s = Gas velocity, ft/sec
V_{w(std)} = Volume of water vapor in gas sample, corrected to standard conditions, scf
Y = Dry gas meter calibration factor
ΔH = Average pressure differential across the orifice meter, inches water
Δp = Velocity head of gas, inches water
ρ_a = Density of acetone, 0.7855 g/ml (average)
ρ_w = Density of water, 0.002201 lb/ml
θ = Total sampling time, minutes
K₁ = 17.647 °R/in. Hg
K₂ = 0.04707 ft³/ml
K₄ = 0.09450/100 = 0.000945
K_p = Pitot tube constant, $85.49 \frac{ft}{sec} \left[\frac{(lb/lb-mole)(in. Hg)}{(^{\circ}R)(in. H_2O)} \right]^{1/2}$
%EA = Percent excess air
%CO₂ = Percent carbon dioxide by volume, dry basis
%O₂ = Percent oxygen by volume, dry basis
%CO = Percent carbon monoxide by volume, dry basis
%N₂ = Percent nitrogen by volume, dry basis
0.264 = Ratio of O₂ to N₂ in air, v/v
28 = Molecular weight of N₂ or CO
32 = Molecular weight of O₂
44 = Molecular weight of CO₂
13.6 = Specific gravity of mercury (Hg)

MOSTARDI PLATT

Calculations for Hydrogen Fluoride By Method 26 or 26A

Concentration

$$\frac{\text{lbs HF}}{\text{dscf}} = \frac{\mu\text{g HF in sample}}{4.536 \times 10^8 \times \text{dscf}}$$

where:

$$4.536 \times 10^8 = \mu\text{g/lb}$$

dscf = Volume of gas sampled

$$\mu\text{g/lb HF} = \mu\text{g F} \times \frac{20.008}{19.000}$$

Parts Per Million

$$\text{ppm HF} = \frac{\text{lbs HF}}{\text{dscf}} \div \frac{20.008}{385 \times 10^6}$$

where:

385 = Volume of 1 lb mole of gas at 68°F and 29.92 in. Hg

106 = Conversion of ppm v/v

Emission Rate

$$\text{lbs HF /dscf} \times \text{dscfm} \times 60 \text{ min/hr} = \text{lbs/hr HF}$$

MOSTARDI PLATT

Pollutant Concentration Correction 7% for Percent Oxygen

$$C_{adj} = C_d \frac{20.9 - 7\%}{20.9 - \%O_2}$$

where:

C_{adj} = Pollutant concentration corrected to percent O_2

20.9 - 7% = Percent O_2 , the defined O_2 correction value, percent

20.9 = Percent O_2 in air

$\%O_2$ = Measured O_2 concentration dry basis, percent

C_d = Pollutant concentration measured, dry basis, ppm.

Appendix E- Laboratory Sample Analysis

Chain-of-Custody Form

Project Number: M235102			Date Results Required:			
Client: Ash Grove Midlothian			TAT Required:			
Plant/Test Location: Main Kiln Stack			Project Supervisor: Aaron Benninghoff			
PO#:						
Sample Number	Sample Date	Sample Point Identification	# of Confs	Sub Lab	Analysis Required	Volume, mls
001	1/4/24	#1A KILN M26A H2SO4 Part 1	1		HF	602.7
002	1/4/24	#1A KILN M26A H2SO4 Part 2	1		HF	292.1
003	1/4/24	#1A KILN M26A NaOH	1		Cl2	380.9
004	1/4/24	#1B KILN H2SO4 Part 1	1		HF	587.2
005	1/4/24	#1B KILN M26A H2SO4 Part 2	1		HF	319.0
006	1/4/24	#1B KILN M26A NaOH	1		Cl2	435.2
007	1/4/24	#2A KILN M26A H2SO4 Part 1	1		HF	577.9
008	1/4/24	#2A KILN M26A H2SO4 Part 2	1		HF	478.4
009	1/4/24	#2A KILN M26A NaOH	1		Cl2	394.2
010	1/4/24	#2B KILN M26A H2SO4 Part 1	1		HF	540.3
011	1/4/24	#2B KILN M26A H2SO4 Part 2	1		HF	410.0
012	1/4/24	#2B KILN M26A NaOH	1		Cl2	453.6
013	1/4/24	#3A KILN M26A H2SO4 Part 1	1		HF	580.7
014	1/4/24	#3A KILN H2SO4 Part 2	1		HF	360.0
015	1/4/24	#3A KILN M26A NaOH	1		Cl2	365.7
016	1/4/24	#3B KILN M26A H2SO4 Part 1	1		HF	564.5
017	1/4/24	#3B KILN M26A H2SO4 Part 2	1		HF	433.2
018	1/4/24	#3B KILN M26A NaOH	1		Cl2	423.5
019	1/4/24	A Train Blank H2SO4	1		HF	383.0
020	1/4/24	A Train Blank NaOH	1		Cl2	352.7
021	1/4/24	DI Reagent Blank	1		HF/Cl2	117.2
Delivered to Lab by: Date/Time:		Received by: Date/Time:		Processed by: Date/Time:		

Appendix F - Reference Method Test Data

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Test Location: Kiln 3
Project #: M235102
Test Method: 26A
Test Engineer: CLC1
Test Technician: BRD1

	<u>Run 1A</u>	<u>Run 2A</u>	<u>Run 3A</u>
Temp ID:	CM28	CM28	CM28
Meter ID:	CM28	CM28	CM28
Pitot ID:	P-1278	P-1278	P-1278
Nozzle Diameter (Inches):	0.281	0.281	0.281
Meter Calibration Date:	12/8/2023	12/8/2023	12/8/2023
Meter Calibration Factor (Y):	0.984	0.984	0.984
Meter Orifice Setting (Delta H):	1.878	1.878	1.878
Nozzle Kit ID Number and Material:	Glass 11	Glass 11	Glass 11

Leak Checks

Pre Pitot Leak Check	0.0	@	4.0	"H ₂ O	0.0	@	3.8	"H ₂ O	0.0	@	4.1	"H ₂ O
Post Pitot Leak Check	0.0	@	4.2	"H ₂ O	0.0	@	4.0	"H ₂ O	0.0	@	3.8	"H ₂ O
Pre Nozzle Leak Check	0.0000	@	13	"Hg	0.0000	@	15	"Hg	0.0000	@	13	"Hg
Post Nozzle Leak Check	0.0000	@	12	"Hg	0.0000	@	10	"Hg	0.0000	@	10	"Hg

Pitot Tube Coefficient: 0.832
 Probe Length (Feet): 5.0
 Probe Liner Material: Glass
 Sample Plane: Horizontal
 Port Length (Inches): 7.00
 Port Size (Diameter, Inches): 6.00
 Port Type: Flange
 Duct Shape: Circular
 Diameter (Feet): 11.502
 Duct Area (Square Feet): 103.905
 Upstream Diameters: 16.8
 Downstream Diameters: 7.4
 Number of Ports Sampled: 4
 Number of Points per Port: 3
 Minutes per Point: 5.0
 Minutes per Reading: 5.0
 Total Number of Traverse Points: 12
 Test Length (Minutes): 60
 Train Type: Anderson Box
 Source Condition: Normal
 Diluent Model/Serial Number: Servomex 1440 and MKS 2030
 Moisture Balance ID: D-01
 # of Runs: 3

Run 1A - Method 26A

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Test Location: Kiln 3
 Source Condition: Normal

Date: 1/4/24
 Start Time: 10:50
 End Time: 12:03

DRY GAS METER CONDITIONS

STACK CONDITIONS

ΔH: 2.28 in. H₂O
 Meter Temperature, Tm: 61.3 °F
 Sqrt ΔP: 1.097 in. H₂O
 Stack Temperature, Ts: 327.6 °F
 Meter Volume, Vm: 52.749 ft³
 Meter Volume, Vmstd: 51.756 dscf
 Meter Volume, Vwstd: 27.813 wscf
 Isokinetic Variance: 99.5 %I
 Test Length: 60.00 in mins.
 Nozzle Diameter: 0.281 in inches
 Barometric Pressure: 29.29 in Hg

Static Pressure -2.50 in. H₂O
 Flue Pressure (Ps): 29.11 in. Hg. abs.
 Carbon Dioxide: 14.91 %
 Oxygen: 8.42 %
 Nitrogen: 76.67 %
 Gas Weight dry, Md: 30.722 lb/lb mole
 Gas Weight wet, Ms: 26.275 lb/lb mole
 Excess Air: 71.230 %
 Gas Velocity, Vs: 79.154 fps
 Volumetric Flow: 493,471 acfm
 Volumetric Flow: 209,334 dscfm
 Volumetric Flow: 321,826 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3623.4 ml Silica Initial Wt. 849.5 grams
 Final Impinger Content: 4193.9 ml Silica Final Wt. 869.5 grams
 Impinger Difference: 570.5 ml Silica Difference: 20.0 grams
 Total Water Gain: 590.5 Moisture, Bws: 0.350

Port- Point No.	Clock Time	Velocity	Orifice	Actual	Stack	Meter Temp		Pump	Probe	Filter	Impinger
		Head Δp in. H ₂ O	ΔH in. H ₂ O	Meter Vol. ft ³	Temp °F	Inlet °F	Outlet °F	Vacuum "Hg	Temp °F	Exit Temp °F	Exit Temp °F
1-1	10:50:00	1.40	2.60	23.056	331	57	59	5	255	260	60
1-2	10:55:00	1.30	2.40	27.690	330	57	59	5	252	259	57
1-3	11:00:00	1.00	1.80	32.130	329	57	59	6	252	260	60
	11:05:00			36.211							
2-1	11:09:00	1.40	2.60	36.211	329	58	60	7	250	260	61
2-2	11:14:00	1.20	2.50	40.950	328	58	60	7	251	260	62
2-3	11:19:00	1.00	1.80	45.320	327	60	62	7	252	259	62
	11:24:00			49.317							
3-1	11:29:00	1.40	2.60	49.317	330	60	62	7	251	259	59
3-2	11:34:00	1.20	2.30	54.230	328	62	64	7	250	261	58
3-3	11:39:00	1.00	1.90	58.610	327	64	64	7	250	259	59
	11:44:00			62.582							
4-1	11:48:00	1.40	2.60	62.582	326	64	65	7	254	262	57
4-2	11:53:00	1.20	2.30	67.320	324	64	66	7	257	261	57
4-3	11:58:00	1.00	1.90	71.770	322	64	67	7	260	259	57
	12:03:00			75.805							

Total 1:00:00 52.749 60.4 62.3
 Average 2.28 327.6 61.3 7
 Min 1.80 322.0 57.0 5
 Max 2.60 331.0 67.0 7

Impinger Weight Sheet - Run 1A

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Test Location: Kiln 3
Project #: M235102
Date: 1/4/2024
Test Method: 26A
Weighed/Measured By: WAP
Balance ID: D-01

Scale Calibration Check Date: 1/3/2024
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	1,005.6	780.8	224.8
0.1N H2SO4	971.5	738.6	232.9
Empty	685.8	610.1	75.7
0.1N NaOH	779.3	749.3	30.0
0.1N NaOH	751.7	744.6	7.1
Silica Gel	869.5	849.5	20.0

<u>4,193.9</u> Liquid Final	<u>3,623.4</u> Liquid Initial	<u>570.5</u> Liquid Gain
<u>869.5</u> Silica Final	<u>849.5</u> Silica Initial	<u>20.0</u> Silica Gain

Run 2A - Method 26A

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Test Location: Kiln 3
 Source Condition: Normal

Date: 1/4/24
 Start Time: 12:25
 End Time: 13:39

DRY GAS METER CONDITIONS			STACK CONDITIONS		
ΔH:	2.35	In. H ₂ O	Static Pressure	-2.50	in. H ₂ O
Meter Temperature, Tm:	72.6	°F	Flue Pressure (Ps):	29.11	in. Hg. abs.
Sqrt ΔP:	1.104	In. H ₂ O	Carbon Dioxide:	15.44	%
Stack Temperature, Ts:	316.6	°F	Oxygen:	8.14	%
Meter Volume, Vm:	54.956	ft ³	Nitrogen:	76.4	%
Meter Volume, Vmstd:	52.792	dscf	Gas Weight dry, Md:	30.796	lb/lb mole
Meter Volume, Vwstd:	29.607	wscf	Gas Weight wet, Ms:	26.198	lb/lb mole
Isokinetic Variance:	101.4	%I	Excess Air:	67.637	%
Test Length:	60.00	in mins.	Gas Velocity, Vs:	79.275	fps
Nozzle Diameter:	0.281	in inches	Volumetric Flow:	494,222	acfm
Barometric Pressure:	29.29	in Hg	Volumetric Flow:	209,428	dscfm
			Volumetric Flow:	326,881	scfm

MOISTURE DETERMINATION

Initial Impinger Content:	3621.7	ml	Silica Initial Wt.	862.2	grams
Final Impinger Content:	4232.5	ml	Silica Final Wt.	880.0	grams
Impinger Difference:	610.8	ml	Silica Difference:	17.8	grams
Total Water Gain:	628.6		Moisture, Bws:	0.359	

Port-Point No.	Clock Time	Velocity	Orifice	Actual	Stack	Meter Temp		Pump	Probe	Filter	Impinger
		Head Δp in. H ₂ O	ΔH in. H ₂ O	Meter Vol. ft ³	Temp °F	Inlet °F	Outlet °F	Vacuum "Hg	Temp °F	Exit Temp °F	Exit Temp °F
1-1	12:25:00	1.40	2.70	76.541	320	70	71	5	258	260	50
1-2	12:30:00	1.20	2.30	81.420	319	70	71	5	257	260	51
1-3	12:35:00	1.00	1.90	85.980	318	71	72	5	260	259	52
	12:40:00			90.012							
2-1	12:45:00	1.40	2.70	90.012	318	72	72	5	260	258	51
2-2	12:50:00	1.20	2.30	94.940	317	73	72	5	261	261	51
2-3	12:55:00	1.10	2.20	99.620	318	74	72	5	258	259	52
	13:00:00			103.861							
3-1	13:04:00	1.40	2.70	103.861	316	75	72	5	256	262	52
3-2	13:09:00	1.30	2.50	108.810	315	75	72	5	261	261	53
3-3	13:14:00	1.00	1.90	113.520	314	75	72	5	260	259	54
	13:19:00			117.713							
4-1	13:24:00	1.40	2.70	117.713	316	75	72	5	260	257	56
4-2	13:29:00	1.30	2.40	122.730	315	75	72	5	258	260	58
4-3	13:34:00	1.00	1.90	127.480	313	75	72	5	259	261	59
	13:39:00			131.497							

Total	1:00:00			54.956		73.3	71.8				
Average			2.35		316.6	72.6		5			
Min			1.90		313.0	70.0		5			
Max			2.70		320.0	75.0		5			

Impinger Weight Sheet - Run 2A

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Test Location: Kiln 3
Project #: M235102
Date: 1/4/2024
Test Method: 26A
Weighed/Measured By: WAP
Balance ID: D-01

Scale Calibration Check Date: 1/3/2024
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	901.2	735.7	165.5
0.1N H2SO4	937.6	747.2	190.4
Empty	888.4	643.2	245.2
0.1N NaOH	744.7	738.3	6.4
0.1N NaOH	760.6	757.3	3.3
Silica Gel	880.0	862.2	17.8

<u>4,232.5</u>	<u>3,621.7</u>	<u>610.8</u>
Liquid Final	Liquid Initial	Liquid Gain
<u>880.0</u>	<u>862.2</u>	<u>17.8</u>
Silica Final	Silica Initial	Silica Gain

Run 3A - Method 26A

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Test Location: Kiln 3
 Source Condition: Normal

Date: 1/4/24
 Start Time: 14:17
 End Time: 15:30

DRY GAS METER CONDITIONS

ΔH: 2.32 in. H₂O
 Meter Temperature, Tm: 74.2 °F
 Sqrt ΔP: 1.112 in. H₂O
 Stack Temperature, Ts: 324.3 °F
 Meter Volume, Vm: 55.194 ft³
 Meter Volume, Vmstd: 52.855 dscf
 Meter Volume, Vwstd: 26.527 wscf
 Isokinetic Variance: 98.2 %I

 Test Length: 60.00 in mins.
 Nozzle Diameter: 0.281 in inches
 Barometric Pressure: 29.29 in Hg

STACK CONDITIONS

Static Pressure -2.50 in. H₂O
 Flue Pressure (Ps): 29.11 in. Hg. abs.
 Carbon Dioxide: 15.97 %
 Oxygen: 7.82 %
 Nitrogen: 76.21 %
 Gas Weight dry, Md: 30.868 lb/lb mole
 Gas Weight wet, Ms: 26.568 lb/lb mole
 Excess Air: 63.580 %
 Gas Velocity, Vs: 79.643 fps
 Volumetric Flow: 496,517 acfm
 Volumetric Flow: 216,521 dscfm
 Volumetric Flow: 325,189 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3634.2 ml Silica Initial Wt. 874.7 grams
 Final Impinger Content: 4176.9 ml Silica Final Wt. 895.2 grams
 Impinger Difference: 542.7 ml Silica Difference: 20.5 grams

 Total Water Gain: 563.2 Moisture, Bws: 0.334

Port-Point No.	Clock Time	Velocity	Orifice	Actual	Stack	Meter Temp		Pump	Probe	Filter	Impinger
		Head Δp in. H ₂ O	ΔH in. H ₂ O	Meter Vol. ft ³	Temp °F	Inlet °F	Outlet °F	Vacuum "Hg	Temp °F	Exit Temp °F	Exit Temp °F
1-1	14:17:00	1.40	2.70	32.410	315	75	72	5	258	260	60
1-2	14:22:00	1.30	2.30	37.410	317	75	72	5	258	260	61
1-3	14:27:00	1.00	1.90	42.180	318	75	72	5	259	261	62
	14:32:00			46.292							
2-1	14:36:00	1.40	2.70	46.292	322	75	72	5	260	259	62
2-2	14:41:00	1.30	2.30	51.210	324	75	72	5	259	261	62
2-3	14:46:00	1.10	2.10	55.980	320	76	72	5	260	260	63
	14:51:00			60.213							
3-1	14:55:00	1.40	2.70	60.213	328	76	72	5	261	260	63
3-2	15:00:00	1.30	2.30	65.015	330	77	72	5	259	260	63
3-3	15:05:00	1.00	1.90	69.950	331	77	72	5	261	260	63
	15:10:00			73.931							
4-1	15:15:00	1.40	2.70	73.931	330	77	73	5	258	260	63
4-2	15:20:00	1.30	2.30	78.810	329	78	73	5	260	259	64
4-3	15:25:00	1.00	1.90	83.530	327	78	73	5	261	260	63
	15:30:00			87.604							

Total 1:00:00 55.194 76.2 72.3
 Average 2.32 324.3 74.2 5
 Min 1.90 315.0 72.0 5
 Max 2.70 331.0 78.0 5

Impinger Weight Sheet - Run 3A

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Test Location: Kiln 3
Project #: M235102
Date: 1/4/2024
Test Method: 26A
Weighed/Measured By: WAP
Balance ID: D-01

Scale Calibration Check Date: 1/4/2024
Scale Calibration Check (see QS-6.05C for procedure)

must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	1,039.2	783.2	256.0
0.1N H2SO4	994.3	740.4	253.9
Empty	635.8	613.6	22.2
0.1N NaOH	758.6	750.0	8.6
0.1N NaOH	749.0	747.0	2.0
Silica Gel	895.2	874.7	20.5

<u>4,176.9</u> Liquid Final	<u>3,634.2</u> Liquid Initial	<u>542.7</u> Liquid Gain
<u>895.2</u> Silica Final	<u>874.7</u> Silica Initial	<u>20.5</u> Silica Gain

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Test Location: Kiln 3
Project #: M235102
Test Method: 26A
Test Engineer: JVC
Test Technician: BRD1

	<u>Run 1B</u>	<u>Run 2B</u>	<u>Run 3B</u>
Temp ID:	CM44	CM44	CM44
Meter ID:	CM44	CM44	CM44
Pitot ID:	P-1279	P-1279	P-1279
Filter ID:	B	B	B
Nozzle Diameter (Inches):	0.281	0.281	0.281
Meter Calibration Date:	12/11/2023	12/11/2023	12/11/2023
Meter Calibration Factor (Y):	0.994	0.994	0.994
Meter Orifice Setting (Delta H):	1.801	1.801	1.801
Nozzle Kit ID Number and Material:	Glass #32	Glass #32	Glass #32

Leak Checks

Pre Pitot Leak Check	0.0 @ 4.0 "H ₂ O	0.0 @ 4.5 "H ₂ O	0.0 @ 5.0 "H ₂ O
Post Pitot Leak Check	0.0 @ 4.5 "H ₂ O	0.0 @ 3.5 "H ₂ O	0.0 @ 4.0 "H ₂ O
Pre Nozzle Leak Check	0.0000 @ 11 "Hg	0.0050 @ 20 "Hg	0.0100 @ 20 "Hg
Post Nozzle Leak Check	0.0000 @ 17 "Hg	0.0050 @ 19 "Hg	0.0100 @ 16 "Hg

Pitot Tube Coefficient: 0.833
 Probe Length (Feet): 5.0
 Probe Liner Material: Glass
 Sample Plane: Horizontal
 Port Length (Inches): 7.00
 Port Size (Diameter, Inches): 6.00
 Port Type: Flange
 Duct Shape: Circular
 Diameter (Feet): 11.502
 Duct Area (Square Feet): 103.905
 Upstream Diameters: 16.8
 Downstream Diameters: 7.4
 Number of Ports Sampled: 4
 Number of Points per Port: 3
 Minutes per Point: 5.0
 Minutes per Reading: 5.0
 Total Number of Traverse Points: 12
 Test Length (Minutes): 60
 Train Type: Anderson Box
 Source Condition: Normal
 Diluent Model/Serial Number: Servomex 1440 and MKS 2030
 Moisture Balance ID: D-01
 # of Runs: 3

Run 1B - Method 26A

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Test Location: Kiln 3
 Source Condition: Normal

Date: 1/4/24
 Start Time: 10:50
 End Time: 12:03

DRY GAS METER CONDITIONS

STACK CONDITIONS

ΔH: 2.31 in. H₂O
 Meter Temperature, Tm: 56.0 °F
 Sqrt ΔP: 1.094 in. H₂O
 Stack Temperature, Ts: 328.4 °F
 Meter Volume, Vm: 50.834 ft³
 Meter Volume, Vmstd: 50.909 dscf
 Meter Volume, Vwstd: 28.698 wscf
 Isokinetic Variance: 99.4 %I
 Test Length: 60.00 in mins.
 Nozzle Diameter: 0.281 in inches
 Barometric Pressure: 29.29 in Hg

Static Pressure -2.50 in. H₂O
 Flue Pressure (Ps): 29.11 in. Hg. abs.
 Carbon Dioxide: 14.91 %
 Oxygen: 8.42 %
 Nitrogen: 76.67 %
 Gas Weight dry, Md: 30.722 lb/lb mole
 Gas Weight wet, Ms: 26.136 lb/lb mole
 Excess Air: 71.230 %
 Gas Velocity, Vs: 79.312 fps
 Volumetric Flow: 494,455 acfm
 Volumetric Flow: 206,001 dscfm
 Volumetric Flow: 322,127 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3582.1 ml Silica Initial Wt. 897.8 grams
 Final Impinger Content: 4174.3 ml Silica Final Wt. 914.9 grams
 Impinger Difference: 592.2 ml Silica Difference: 17.1 grams
 Total Water Gain: 609.3 Moisture, Bws: 0.360

Port- Point No.	Clock Time	Velocity	Orifice	Actual	Stack	Meter Temp		Pump	Probe	Filter	Impinger
		Head Δp in. H ₂ O	ΔH in. H ₂ O	Meter Vol. ft ³	Temp °F	Inlet °F	Outlet °F	Vacuum "Hg	Temp °F	Exit Temp °F	Exit Temp °F
1-1	10:50:00	1.30	2.50	40.651	331	53	53	5	260	259	55
1-2	10:55:00	1.10	2.10	45.110	330	54	54	5	264	261	55
1-3	11:00:00	0.98	1.90	49.190	328	54	54	5	262	257	56
	11:05:00			52.850							
2-1	11:09:00	1.40	2.70	52.850	329	55	55	6	256	258	56
2-2	11:14:00	1.30	2.50	57.480	331	56	56	5	259	260	57
2-3	11:19:00	0.95	1.80	61.880	333	56	56	5	259	257	57
	11:24:00			65.564							
3-1	11:29:00	1.40	2.70	65.564	332	56	56	6	260	262	59
3-2	11:34:00	1.20	2.30	70.220	329	56	56	5	261	260	61
3-3	11:39:00	1.00	1.90	74.440	327	56	56	5	258	260	62
	11:44:00			78.246							
4-1	11:48:00	1.40	2.70	78.246	324	58	58	7	263	259	64
4-2	11:53:00	1.30	2.50	82.810	324	59	59	6	259	258	64
4-3	11:58:00	1.10	2.10	87.390	323	59	59	5	258	259	65
	12:03:00			91.485							

Total 1:00:00 50.834 56.0 56.0
 Average 2.31 328.4 56.0 5
 Min 1.80 323.0 53.0 5
 Max 2.70 333.0 59.0 7

Impinger Weight Sheet - Run 1B

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Test Location: Kiln 3
Project #: M235102
Date: 1/4/2024
Test Method: 26A
Weighed/Measured By: WAP
Balance ID: D-01

Scale Calibration Check Date: 1/3/2024
Scale Calibration Check (see QS-6.05C for procedure)
 must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	871.3	778.4	92.9
0.1N H2SO4	903.1	710.0	193.1
Empty	834.7	612.8	221.9
0.1N NaOH	818.7	745.5	73.2
0.1N NaOH	746.5	735.4	11.1
Silica Gel	914.9	897.8	17.1

<u>4,174.3</u>	<u>3,582.1</u>	<u>592.2</u>
Liquid Final	Liquid Initial	Liquid Gain
<u>914.9</u>	<u>897.8</u>	<u>17.1</u>
Silica Final	Silica Initial	Silica Gain

Run 2B - Method 26A

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Test Location: Kiln 3
 Source Condition: Normal

Date: 1/4/24
 Start Time: 12:25
 End Time: 13:39

DRY GAS METER CONDITIONS				STACK CONDITIONS			
ΔH:	2.37	In. H ₂ O		Static Pressure	-2.50	in. H ₂ O	
Meter Temperature, Tm:	60.4	°F		Flue Pressure (Ps):	29.11	in. Hg. abs.	
Sqrt ΔP:	1.092	In. H ₂ O		Carbon Dioxide:	15.44	%	
Stack Temperature, Ts:	316.3	°F		Oxygen:	8.14	%	
Meter Volume, Vm:	51.993	ft ³		Nitrogen:	76.4	%	
Meter Volume, Vmstd:	51.635	dscf		Gas Weight dry, Md:	30.796	lb/lb mole	
Meter Volume, Vwstd:	29.687	wscf		Gas Weight wet, Ms:	26.125	lb/lb mole	
Isokinetic Variance:	101.0	%I		Excess Air:	67.637	%	
Test Length:	60.00	in mins.		Gas Velocity, Vs:	78.569	fps	
Nozzle Diameter:	0.281	in inches		Volumetric Flow:	489,823	acfm	
Barometric Pressure:	29.29	in Hg		Volumetric Flow:	205,792	dscfm	
				Volumetric Flow:	324,111	scfm	

MOISTURE DETERMINATION

Initial Impinger Content:	3330.1	ml	Silica Initial Wt.	784.7	grams
Final Impinger Content:	3943.9	ml	Silica Final Wt.	801.2	grams
Impinger Difference:	613.8	ml	Silica Difference:	16.5	grams
Total Water Gain:	630.3		Moisture, Bws:	0.365	

Port-Point No.	Clock Time	Velocity	Orifice	Actual	Stack	Meter Temp		Pump	Probe	Filter	Impinger
		Head Δp in. H ₂ O	ΔH in. H ₂ O	Meter Vol. ft ³	Temp °F	Inlet °F	Outlet °F	Vacuum "Hg	Temp °F	Exit Temp °F	Exit Temp °F
1-1	12:25:00	1.30	2.50	94.221	319	59	59	4	260	258	57
1-2	12:30:00	1.30	2.50	98.610	318	59	59	4	260	265	58
1-3	12:35:00	1.10	2.20	103.220	316	59	59	4	260	261	58
	12:40:00			107.338							
2-1	12:45:00	1.40	2.70	107.338	317	59	59	4	255	264	58
2-2	12:50:00	1.30	2.60	112.050	319	60	60	4	260	259	59
2-3	12:55:00	1.00	2.00	116.580	317	61	61	4	257	261	59
	13:00:00			120.543							
3-1	13:04:00	1.30	2.60	120.543	312	61	61	5	259	257	61
3-2	13:09:00	1.20	2.40	125.140	317	62	62	4	260	262	62
3-3	13:14:00	0.96	1.90	129.490	314	62	62	4	258	259	62
	13:19:00			133.424							
4-1	13:24:00	1.30	2.60	133.424	316	61	61	5	260	264	64
4-2	13:29:00	1.20	2.40	137.890	316	61	61	4	255	261	63
4-3	13:34:00	1.00	2.00	142.380	314	61	61	4	260	261	64
	13:39:00			146.214							

Total	1:00:00			51.993		60.4	60.4				
Average			2.37		316.3	60.4		4			
Min			1.90		312.0	59.0		4			
Max			2.70		319.0	62.0		5			

Impinger Weight Sheet - Run 2B

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Test Location: Kiln 3
Project #: M235102
Date: 1/4/2024
Test Method: 26A
Weighed/Measured By: WAP
Balance ID: D-01

Scale Calibration Check Date: 1/3/2024
Scale Calibration Check (see QS-6.05C for procedure)

must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	864.6	690.5	174.1
0.1N H2SO4	772.1	614.1	158.0
Empty	790.8	605.3	185.5
0.1N NaOH	818.4	732.4	86.0
0.1N NaOH	698.0	687.8	10.2
Silica Gel	801.2	784.7	16.5

<u>3,943.9</u> Liquid Final	<u>3,330.1</u> Liquid Initial	<u>613.8</u> Liquid Gain
<u>801.2</u> Silica Final	<u>784.7</u> Silica Initial	<u>16.5</u> Silica Gain

Run 3B - Method 26A

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Test Location: Kiln 3
 Source Condition: Normal

Date: 1/4/24
 Start Time: 14:17
 End Time: 15:30

DRY GAS METER CONDITIONS				STACK CONDITIONS			
ΔH:	2.40	In. H ₂ O		Static Pressure	-2.50	in. H ₂ O	
Meter Temperature, Tm:	61.6	°F		Flue Pressure (Ps):	29.11	in. Hg. abs.	
Sqrt ΔP:	1.095	In. H ₂ O		Carbon Dioxide:	15.97	%	
Stack Temperature, Ts:	324.8	°F		Oxygen:	7.82	%	
Meter Volume, Vm:	52.097	ft ³		Nitrogen:	76.21	%	
Meter Volume, Vmstd:	51.627	dscf		Gas Weight dry, Md:	30.868	lb/lb mole	
Meter Volume, Vwstd:	29.131	wscf		Gas Weight wet, Ms:	26.226	lb/lb mole	
Isokinetic Variance:	100.7	%I		Excess Air:	63.580	%	
Test Length:	60.00	in mins.		Gas Velocity, Vs:	79.060	fps	
Nozzle Diameter:	0.281	in inches		Volumetric Flow:	492,881	acfm	
Barometric Pressure:	29.29	in Hg		Volumetric Flow:	206,210	dscfm	
				Volumetric Flow:	322,568	scfm	

MOISTURE DETERMINATION

Initial Impinger Content:	3606.0	ml	Silica Initial Wt.	873.7	grams
Final Impinger Content:	4208.2	ml	Silica Final Wt.	890.0	grams
Impinger Difference:	602.2	ml	Silica Difference:	16.3	grams
Total Water Gain:	618.5		Moisture, Bws:	0.361	

Port-Point No.	Clock Time	Velocity	Orifice	Actual	Stack	Meter Temp		Pump	Probe	Filter	Impinger
		Head Δp in. H ₂ O	ΔH in. H ₂ O	Meter Vol. ft ³	Temp °F	Inlet °F	Outlet °F	Vacuum "Hg	Temp °F	Exit Temp °F	Exit Temp °F
1-1	14:17:00	1.30	2.60	46.694	315	61	61	5	259	258	56
1-2	14:22:00	1.10	2.20	51.270	317	61	61	5	260	265	57
1-3	14:27:00	0.94	1.90	55.470	314	61	61	4	262	263	57
	14:32:00			59.346							
2-1	14:36:00	1.40	2.80	59.346	323	61	61	6	260	258	58
2-2	14:41:00	1.20	2.40	64.110	326	62	62	5	262	255	58
2-3	14:46:00	1.10	2.20	68.300	324	62	62	5	263	257	60
	14:51:00			72.489							
3-1	14:55:00	1.40	2.70	72.489	333	61	61	6	259	262	62
3-2	15:00:00	1.30	2.60	77.210	330	62	62	5	262	264	63
3-3	15:05:00	1.00	2.00	81.690	327	62	62	4	264	260	63
	15:10:00			85.683							
4-1	15:15:00	1.30	2.60	85.683	331	62	62	6	264	261	63
4-2	15:20:00	1.30	2.60	90.150	330	62	62	5	262	263	64
4-3	15:25:00	1.10	2.20	94.640	328	62	62	5	262	262	65
	15:30:00			98.791							
Total	1:00:00			52.097		61.6	61.6				
Average			2.40		324.8	61.6		5			
Min			1.90		314.0	61.0		4			
Max			2.80		333.0	62.0		6			

Impinger Weight Sheet - Run 3B

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Test Location: Kiln 3
Project #: M235102
Date: 1/4/2024
Test Method: 26A
Weighed/Measured By: WAP
Balance ID: D-01

Scale Calibration Check Date: 1/4/2024
Scale Calibration Check (see QS-6.05C for procedure)

must be within $\pm 0.5g$ of certified mass

<u>Certified Weight, grams</u>	<u>Result, grams</u>
250	<u>250.0</u>
500	<u>500.0</u>
750	<u>750.0</u>

IMPINGER CONTENTS	FINAL MLS / GRAMS	INITIAL MLS / GRAMS	GAIN MLS / GRAMS
0.1N H2SO4	928.6	781.6	147.0
0.1N H2SO4	887.2	716.8	170.4
Empty	821.3	616.6	204.7
0.1N NaOH	793.1	752.4	40.7
0.1N NaOH	778.0	738.6	39.4
Silica Gel	890.0	873.7	16.3

<u>4,208.2</u> Liquid Final	<u>3,606.0</u> Liquid Initial	<u>602.2</u> Liquid Gain
<u>890.0</u> Silica Final	<u>873.7</u> Silica Initial	<u>16.3</u> Silica Gain

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Project #: M235102
 Test Location: Kiln 3 Stack
 Date: 1/4/24

Run 1

Spectrum	Time	FTIR Data					Cell Temp	Pressure	Analyzer Data O2 % (dry)
		H2O %	CO2 % (wet)	HCN ppmvw	HF ppmvw				
RUN1_0927.LAB	10:50	81.06	2.89	≤ 0.20	0.40	191.26	1.00	8.82	
RUN1_0928.LAB	10:51	64.96	5.24	≤ 0.20	0.41	191.27	1.02	8.82	
RUN1_0929.LAB	10:52	59.03	6.04	≤ 0.20	0.31	191.27	1.02	8.87	
RUN1_0930.LAB	10:53	49.36	7.38	≤ 0.20	0.25	191.27	1.03	8.84	
RUN1_0931.LAB	10:54	45.87	7.89	0.28	0.24	191.27	1.03	8.77	
RUN1_0932.LAB	10:55	42.97	8.42	≤ 0.20	0.23	191.26	1.03	8.74	
RUN1_0933.LAB	10:56	41.73	8.64	≤ 0.20	0.17	191.26	1.04	8.67	
RUN1_0934.LAB	10:57	39.83	8.91	≤ 0.20	0.15	191.26	1.04	8.60	
RUN1_0935.LAB	10:58	39.51	9.06	0.22	0.16	191.27	1.04	8.48	
RUN1_0936.LAB	10:59	39.81	9.29	≤ 0.20	0.18	191.26	1.04	8.40	
RUN1_0937.LAB	11:00	38.97	9.26	≤ 0.20	0.21	191.26	1.04	8.31	
RUN1_0938.LAB	11:01	39.01	9.13	0.23	0.23	191.27	1.04	8.35	
RUN1_0939.LAB	11:02	38.15	9.29	0.25	0.17	191.27	1.04	8.31	
RUN1_0940.LAB	11:03	38.44	9.19	0.20	0.16	191.27	1.04	8.50	
RUN1_0941.LAB	11:04	37.36	9.10	0.25	0.19	191.27	1.04	8.85	
RUN1_0942.LAB	11:05	36.52	8.96	≤ 0.20	0.15	191.26	1.04	9.16	
RUN1_0943.LAB	11:06	36.22	9.00	0.23	0.27	191.26	1.04	9.11	
RUN1_0944.LAB	11:07	39.52	8.61	≤ 0.20	0.16	191.26	1.03	9.03	
RUN1_0945.LAB	11:08	36.81	9.21	≤ 0.20	0.11	191.26	1.04	8.85	
RUN1_0946.LAB	11:09	35.26	9.50	0.20	0.11	191.27	1.04	8.77	
RUN1_0947.LAB	11:10	38.89	8.94	≤ 0.20	0.23	191.27	1.03	8.75	
RUN1_0948.LAB	11:11	35.28	9.56	≤ 0.20	0.19	191.26	1.04	8.51	
RUN1_0949.LAB	11:12	37.76	9.36	≤ 0.20	0.23	191.27	1.03	8.37	
RUN1_0950.LAB	11:13	37.10	9.60	0.35	0.23	191.26	1.03	8.41	
RUN1_0951.LAB	11:14	34.44	9.85	≤ 0.20	0.23	191.26	1.04	8.35	
RUN1_0952.LAB	11:15	33.81	9.74	≤ 0.20	0.17	191.27	1.04	8.63	
RUN1_0953.LAB	11:16	38.22	8.67	≤ 0.20	0.19	191.27	1.03	9.23	
RUN1_0954.LAB	11:17	33.79	9.28	≤ 0.20	0.19	191.27	1.04	9.34	
RUN1_0955.LAB	11:18	37.61	8.89	≤ 0.20	0.26	191.27	1.04	9.25	
RUN1_0956.LAB	11:19	36.62	9.13	≤ 0.20	0.13	191.27	1.03	9.09	
RUN1_0957.LAB	11:20	34.36	9.79	≤ 0.20	0.17	191.27	1.04	8.88	
RUN1_0958.LAB	11:21	38.06	9.27	≤ 0.20	0.35	191.26	1.03	8.66	
RUN1_0959.LAB	11:22	35.40	9.51	≤ 0.20	0.22	191.26	1.04	8.55	
RUN1_0960.LAB	11:23	37.01	9.49	0.21	0.25	191.27	1.03	8.50	
RUN1_0961.LAB	11:24	36.31	9.41	≤ 0.20	0.28	191.26	1.03	8.62	
RUN1_0962.LAB	11:25	37.52	9.42	≤ 0.20	0.28	191.26	1.03	8.64	
RUN1_0963.LAB	11:26	36.32	9.42	≤ 0.20	0.27	191.26	1.03	8.64	
RUN1_0964.LAB	11:27	34.39	9.67	≤ 0.20	0.18	191.26	1.04	8.69	
RUN1_0965.LAB	11:28	37.56	9.14	≤ 0.20	0.26	191.27	1.03	8.75	
RUN1_0966.LAB	11:29	37.10	9.44	≤ 0.20	0.19	191.27	1.03	8.70	
RUN1_0967.LAB	11:30	35.41	9.71	≤ 0.20	0.21	191.27	1.03	8.65	
RUN1_0968.LAB	11:31	37.10	9.41	≤ 0.20	0.28	191.27	1.03	8.65	
RUN1_0969.LAB	11:32	37.36	9.44	≤ 0.20	0.23	191.26	1.03	8.59	
RUN1_0970.LAB	11:33	35.25	9.68	≤ 0.20	0.28	191.30	1.04	8.60	
RUN1_0971.LAB	11:34	39.70	9.14	≤ 0.20	0.35	191.27	1.03	8.56	
RUN1_0972.LAB	11:35	35.01	10.05	0.23	0.17	191.26	1.04	8.43	
RUN1_0973.LAB	11:36	37.49	9.59	≤ 0.20	0.26	191.26	1.03	8.35	
RUN1_0974.LAB	11:37	37.90	9.74	≤ 0.20	0.19	191.28	1.03	8.31	
RUN1_0975.LAB	11:38	35.30	10.00	≤ 0.20	0.21	191.26	1.03	8.21	
RUN1_0976.LAB	11:39	39.26	9.26	≤ 0.20	0.27	191.26	1.03	8.41	
RUN1_0977.LAB	11:40	34.80	9.83	≤ 0.20	0.20	191.26	1.03	8.49	
RUN1_0978.LAB	11:41	36.77	9.60	≤ 0.20	0.20	191.26	1.03	8.51	
RUN1_0979.LAB	11:42	35.84	9.83	≤ 0.20	0.29	191.26	1.03	8.41	
RUN1_0980.LAB	11:43	36.77	9.70	≤ 0.20	0.31	191.26	1.03	8.43	
RUN1_0981.LAB	11:44	38.36	9.53	≤ 0.20	0.23	191.26	1.03	8.36	
RUN1_0982.LAB	11:45	35.77	9.72	0.37	0.21	191.26	1.04	8.45	
RUN1_0983.LAB	11:46	37.65	9.51	≤ 0.20	0.22	191.26	1.03	8.50	
RUN1_0984.LAB	11:47	36.76	9.72	≤ 0.20	0.27	191.26	1.03	8.42	
RUN1_0985.LAB	11:48	35.33	9.76	≤ 0.20	0.16	191.27	1.03	8.38	
RUN1_0986.LAB	11:49	38.69	9.40	≤ 0.20	0.24	191.26	1.03	8.50	
Average		39.07	9.09	≤ 0.21	0.23	191.27	1.03	8.63	

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Project #: M235102
 Test Location: Kiln 3 Stack
 Date: 1/4/24

Run 2

Spectrum	Time	FTIR Data					Cell Temp	Pressure	Analyzer Data O2 % (dry)
		H2O %	CO2 % (wet)	HCN ppmvw	HF ppmvw				
RUN 2_1078.LAB	12:25	30.81	10.6	≤ 0.20	0.16	-0.1	-0.55	7.97	
RUN 2_1079.LAB	12:26	38.06	9.6	≤ 0.20	0.17	-0.4	-0.61	8.12	
RUN 2_1080.LAB	12:27	37.13	9.9	≤ 0.20	0.31	-0.5	-0.61	8.43	
RUN 2_1081.LAB	12:28	33.77	10.4	≤ 0.20	0.22	-0.4	-0.54	8.57	
RUN 2_1082.LAB	12:29	38.71	9.5	≤ 0.20	0.18	-0.5	-0.73	8.61	
RUN 2_1083.LAB	12:30	34.10	10.2	≤ 0.20	0.10	-0.4	-0.46	8.54	
RUN 2_1084.LAB	12:31	39.90	9.2	≤ 0.20	0.30	-0.6	-0.69	8.47	
RUN 2_1085.LAB	12:32	37.85	9.4	≤ 0.20	0.29	-0.6	-0.70	8.29	
RUN 2_1086.LAB	12:33	36.21	9.6	≤ 0.20	0.16	-0.5	-0.55	8.12	
RUN 2_1087.LAB	12:34	35.91	9.8	≤ 0.20	0.27	-0.4	-0.62	7.99	
RUN 2_1088.LAB	12:35	35.89	9.9	≤ 0.20	0.23	-0.4	-0.52	7.91	
RUN 2_1089.LAB	12:36	39.38	9.4	≤ 0.20	0.27	-0.5	-0.58	8.08	
RUN 2_1090.LAB	12:37	35.65	10.3	≤ 0.20	0.15	-0.4	-0.61	8.14	
RUN 2_1091.LAB	12:38	39.25	9.7	≤ 0.20	0.29	-0.6	-0.55	8.12	
RUN 2_1092.LAB	12:39	35.40	10.1	≤ 0.20	0.31	-0.5	-0.79	8.13	
RUN 2_1093.LAB	12:40	37.79	9.7	≤ 0.20	0.17	-0.4	-0.66	8.29	
RUN 2_1094.LAB	12:41	35.73	10.0	≤ 0.20	0.19	-0.4	-0.71	8.31	
RUN 2_1095.LAB	12:42	35.55	9.9	≤ 0.20	0.21	-0.5	-0.62	8.17	
RUN 2_1096.LAB	12:43	38.37	9.5	≤ 0.20	0.26	-0.5	-0.69	8.17	
RUN 2_1097.LAB	12:44	38.10	9.5	≤ 0.20	0.24	-0.5	-0.68	8.29	
RUN 2_1098.LAB	12:45	36.29	9.8	≤ 0.20	0.29	-0.4	-0.74	8.45	
RUN 2_1099.LAB	12:46	37.20	9.8	≤ 0.20	0.23	-0.4	-0.67	8.48	
RUN 2_1100.LAB	12:47	38.55	9.4	≤ 0.20	0.22	-0.4	-0.56	8.51	
RUN 2_1101.LAB	12:48	38.42	9.4	≤ 0.20	0.26	-0.5	-0.72	8.47	
RUN 2_1102.LAB	12:49	35.68	9.8	≤ 0.20	0.21	-0.5	-0.55	8.48	
RUN 2_1103.LAB	12:50	39.18	9.2	≤ 0.20	0.25	-0.5	-0.53	8.37	
RUN 2_1104.LAB	12:51	35.44	9.8	≤ 0.20	0.17	-0.5	-0.71	8.36	
RUN 2_1105.LAB	12:52	37.84	9.4	0.23	0.26	-0.5	-0.78	8.30	
RUN 2_1106.LAB	12:53	36.19	9.7	≤ 0.20	0.21	-0.4	-0.55	8.19	
RUN 2_1107.LAB	12:54	37.80	9.5	≤ 0.20	0.17	-0.5	-0.58	8.08	
RUN 2_1108.LAB	12:55	35.05	10.0	≤ 0.20	0.15	-0.4	-0.62	8.09	
RUN 2_1109.LAB	12:56	37.65	9.6	≤ 0.20	0.16	-0.5	-0.77	8.13	
RUN 2_1110.LAB	12:57	40.11	9.4	≤ 0.20	0.37	-0.5	-0.44	8.11	
RUN 2_1111.LAB	12:58	35.39	10.1	≤ 0.20	0.15	-0.4	-0.60	8.09	
RUN 2_1112.LAB	12:59	37.78	9.7	≤ 0.20	0.22	-0.4	-0.67	8.30	
RUN 2_1113.LAB	13:00	37.78	9.6	≤ 0.20	0.30	-0.5	-0.68	8.43	
RUN 2_1114.LAB	13:01	35.00	10.1	≤ 0.20	0.14	-0.4	-0.58	8.51	
RUN 2_1115.LAB	13:02	38.53	9.5	≤ 0.20	0.27	-0.4	-0.76	8.34	
RUN 2_1116.LAB	13:03	35.50	9.8	0.23	0.17	-0.5	-0.63	8.15	
RUN 2_1117.LAB	13:04	38.33	9.3	≤ 0.20	0.31	-0.4	-0.64	8.06	
RUN 2_1118.LAB	13:05	37.97	9.5	≤ 0.20	0.27	-0.4	-0.56	8.00	
RUN 2_1119.LAB	13:06	35.30	10.2	≤ 0.20	≤ 0.10	-0.5	-0.60	7.98	
RUN 2_1120.LAB	13:07	37.75	9.8	≤ 0.20	0.23	-0.3	-0.62	8.12	
RUN 2_1121.LAB	13:08	35.90	10.1	≤ 0.20	0.25	-0.4	-0.50	8.15	
RUN 2_1122.LAB	13:09	41.13	9.3	0.35	0.15	-0.5	-0.57	8.16	
RUN 2_1123.LAB	13:10	35.58	10.0	0.21	0.15	-0.3	-0.60	8.45	
RUN 2_1124.LAB	13:11	38.50	9.5	≤ 0.20	0.20	-0.6	-0.78	8.62	
RUN 2_1125.LAB	13:12	36.70	9.9	≤ 0.20	0.28	-0.5	-0.60	8.51	
RUN 2_1126.LAB	13:13	36.72	9.7	≤ 0.20	0.16	-0.4	-0.70	8.44	
RUN 2_1127.LAB	13:14	35.31	9.7	≤ 0.20	0.15	-0.4	-0.44	8.31	
RUN 2_1128.LAB	13:15	35.43	9.8	≤ 0.20	0.15	-0.4	-0.58	8.33	
RUN 2_1129.LAB	13:16	41.77	8.9	≤ 0.20	0.24	-0.5	-0.54	8.31	
RUN 2_1130.LAB	13:17	35.50	10.0	≤ 0.20	0.14	-0.4	-0.45	8.25	
RUN 2_1131.LAB	13:18	38.28	9.5	≤ 0.20	0.20	-0.4	-0.57	8.24	
RUN 2_1132.LAB	13:19	34.65	10.1	≤ 0.20	0.14	-0.4	-0.68	8.33	
RUN 2_1133.LAB	13:20	38.03	9.6	≤ 0.20	0.18	-0.5	-0.62	8.34	
RUN 2_1134.LAB	13:21	37.35	9.8	≤ 0.20	0.12	-0.4	-0.66	8.29	
RUN 2_1135.LAB	13:22	37.12	9.6	0.23	0.19	-0.5	-0.69	8.30	
RUN 2_1136.LAB	13:23	37.80	9.6	≤ 0.20	0.24	-0.4	-0.78	8.28	
RUN 2_1137.LAB	13:24	36.71	9.8	≤ 0.20	0.27	-0.4	-0.76	8.32	
Average		37.02	9.73	≤ 0.20	≤ 0.21	-0.44	-0.62	8.27	

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Project #: M235102
 Test Location: Kiln 3 Stack
 Date: 1/4/24

Run 3

Spectrum	Time	FTIR Data					Cell Temp	Pressure	Analyzer Data O2 % (dry)
		H2O %	CO2 % (wet)	HCN ppmvw	HF ppmvw				
RUN 3_1315.LAB	14:17	38.46	9.6	≤ 0.20	0.14	191.26	1.03	8.20	
RUN 3_1316.LAB	14:18	38.64	9.7	≤ 0.20	0.27	191.26	1.03	8.15	
RUN 3_1317.LAB	14:19	36.27	10.0	≤ 0.20	0.13	191.26	1.04	8.15	
RUN 3_1318.LAB	14:20	37.05	9.8	≤ 0.20	≤ 0.10	191.26	1.03	8.15	
RUN 3_1319.LAB	14:21	35.61	10.1	≤ 0.20	0.13	191.26	1.04	8.11	
RUN 3_1320.LAB	14:22	38.50	9.7	≤ 0.20	0.24	191.26	1.03	8.05	
RUN 3_1321.LAB	14:23	37.66	9.8	0.36	0.13	191.26	1.03	7.99	
RUN 3_1322.LAB	14:24	35.87	10.1	0.26	0.18	191.26	1.04	8.05	
RUN 3_1323.LAB	14:25	38.73	9.6	≤ 0.20	≤ 0.10	191.26	1.03	8.21	
RUN 3_1324.LAB	14:26	34.19	10.7	≤ 0.20	≤ 0.10	191.26	1.03	7.91	
RUN 3_1325.LAB	14:27	39.33	9.8	0.43	0.17	191.27	1.03	7.80	
RUN 3_1326.LAB	14:28	35.36	10.6	0.26	0.21	191.27	1.04	7.81	
RUN 3_1327.LAB	14:29	37.08	10.0	≤ 0.20	0.11	191.26	1.03	7.87	
RUN 3_1328.LAB	14:30	34.66	10.4	≤ 0.20	0.14	191.26	1.03	7.91	
RUN 3_1329.LAB	14:31	39.28	9.9	≤ 0.20	≤ 0.10	191.25	1.03	7.83	
RUN 3_1330.LAB	14:32	35.71	10.5	0.21	0.18	191.26	1.04	7.88	
RUN 3_1331.LAB	14:33	37.77	10.0	≤ 0.20	0.16	191.26	1.03	8.00	
RUN 3_1332.LAB	14:34	34.68	10.3	≤ 0.20	0.14	191.26	1.03	8.11	
RUN 3_1333.LAB	14:35	34.20	10.4	≤ 0.20	≤ 0.10	191.26	1.04	8.10	
RUN 3_1334.LAB	14:36	40.20	9.3	≤ 0.20	0.31	191.26	1.03	8.16	
RUN 3_1335.LAB	14:37	35.01	10.4	≤ 0.20	0.12	191.26	1.03	8.11	
RUN 3_1336.LAB	14:38	36.46	10.0	≤ 0.20	≤ 0.10	191.26	1.03	8.17	
RUN 3_1337.LAB	14:39	34.60	10.2	≤ 0.20	≤ 0.10	191.33	1.04	8.13	
RUN 3_1338.LAB	14:40	38.01	10.0	≤ 0.20	0.20	191.28	1.03	7.96	
RUN 3_1339.LAB	14:41	36.11	10.4	0.20	0.13	191.26	1.03	7.70	
RUN 3_1340.LAB	14:42	34.88	10.6	0.24	0.11	191.27	1.04	7.72	
RUN 3_1341.LAB	14:43	34.30	10.7	≤ 0.20	0.17	191.26	1.04	7.72	
RUN 3_1342.LAB	14:44	39.67	9.7	0.23	0.16	191.26	1.03	7.81	
RUN 3_1343.LAB	14:45	34.54	10.5	≤ 0.20	0.19	191.26	1.04	7.88	
RUN 3_1344.LAB	14:46	36.63	10.1	0.29	0.16	191.26	1.03	7.91	
RUN 3_1345.LAB	14:47	36.63	10.2	0.32	≤ 0.10	191.25	1.03	7.96	
RUN 3_1346.LAB	14:48	36.19	10.2	0.43	≤ 0.10	191.26	1.03	7.86	
RUN 3_1347.LAB	14:49	35.60	10.2	≤ 0.20	0.15	191.26	1.03	7.95	
RUN 3_1348.LAB	14:50	36.01	10.2	≤ 0.20	0.19	191.26	1.03	7.96	
RUN 3_1349.LAB	14:51	35.65	10.2	≤ 0.20	≤ 0.10	191.26	1.03	8.01	
RUN 3_1350.LAB	14:52	36.93	9.9	≤ 0.20	0.21	191.26	1.03	8.07	
RUN 3_1351.LAB	14:53	36.76	10.0	≤ 0.20	0.13	191.26	1.03	8.19	
RUN 3_1352.LAB	14:54	34.34	10.7	≤ 0.20	0.12	191.26	1.03	7.84	
RUN 3_1353.LAB	14:55	39.24	9.9	≤ 0.20	≤ 0.10	191.26	1.03	7.74	
RUN 3_1354.LAB	14:56	36.68	10.3	0.24	0.13	191.26	1.03	7.70	
RUN 3_1355.LAB	14:57	34.01	10.5	0.24	0.15	191.26	1.03	7.75	
RUN 3_1356.LAB	14:58	39.63	9.7	≤ 0.20	0.16	191.26	1.03	7.80	
RUN 3_1357.LAB	14:59	35.02	10.5	≤ 0.20	≤ 0.10	191.26	1.04	7.76	
RUN 3_1358.LAB	15:00	37.48	10.1	≤ 0.20	≤ 0.10	191.26	1.03	7.64	
RUN 3_1359.LAB	15:01	37.15	10.3	≤ 0.20	≤ 0.10	191.26	1.03	7.65	
RUN 3_1360.LAB	15:02	34.68	10.6	≤ 0.20	≤ 0.10	191.26	1.04	7.93	
RUN 3_1361.LAB	15:03	37.66	9.9	≤ 0.20	≤ 0.10	191.26	1.03	7.92	
RUN 3_1362.LAB	15:04	35.12	10.3	≤ 0.20	0.15	191.26	1.03	8.20	
RUN 3_1363.LAB	15:05	37.33	10.0	≤ 0.20	≤ 0.10	191.26	1.03	8.17	
RUN 3_1364.LAB	15:06	34.95	10.4	≤ 0.20	0.22	191.25	1.03	8.10	
RUN 3_1365.LAB	15:07	40.40	9.4	0.26	0.35	191.26	1.03	8.15	
RUN 3_1366.LAB	15:08	37.06	9.9	0.30	0.33	191.26	1.03	8.12	
RUN 3_1367.LAB	15:09	34.92	10.3	≤ 0.20	0.20	191.26	1.03	7.99	
RUN 3_1368.LAB	15:10	38.18	10.0	0.21	0.29	191.26	1.03	7.91	
RUN 3_1369.LAB	15:11	35.07	10.6	≤ 0.20	0.29	191.26	1.03	7.73	
RUN 3_1370.LAB	15:12	37.08	10.3	0.20	0.32	191.25	1.03	7.62	
RUN 3_1371.LAB	15:13	39.58	9.9	0.22	0.39	191.26	1.03	7.62	
RUN 3_1372.LAB	15:14	34.43	10.5	≤ 0.20	0.21	191.26	1.03	7.72	
RUN 3_1373.LAB	15:15	34.66	10.3	≤ 0.20	0.27	191.26	1.03	8.05	
RUN 3_1374.LAB	15:16	38.29	9.5	≤ 0.20	0.32	191.27	1.03	8.26	
Average		36.60	10.12	≤ 0.22	≤ 0.17	191.26	1.03	7.95	

Method 1 and 2 Cyclonic Flow Check Data

Project Number M235102
Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Location: Kiln 3
Pitot ID: P-1279
Pitot Coefficient: 0.833
Probe Length: 5

Source Condition: Normal
Run No.: 1
Date: 1/3/2024
Start Time: 15:05
End Time: 15:15
RM Testers: JVC/BRD1
Port Length: 7.00




Port	Point	DP (in. H ₂ O)	Sqrt. DP	Temp (°F)	Yaw Angle (°)	DP (in. H ₂ O) at Null Point Angle	Velocity (V)	Port	Point	DP (in. H ₂ O)	Sqrt. DP	Temp (°F)	Yaw Angle (°)	DP (in. H ₂ O) at Null Point Angle	Velocity (V)
A	1	1.40	1.1832	339.0	4.0	0.00	85.85	C	1	1.40	1.1832	336.0	9.0	0.00	85.69
A	2	1.20	1.0954	332.0	6.0	0.00	79.14	C	2	1.20	1.0954	337.0	12.0	0.00	79.39
A	3	0.98	0.9899	335.0	7.0	0.00	71.65	C	3	1.10	1.0488	338.0	4.0	0.00	76.05
B	1	1.40	1.1832	327.0	8.0	0.00	85.21	D	1	1.40	1.1832	334.0	6.0	0.00	85.59
B	2	1.30	1.1402	335.0	10.0	0.00	82.52	D	2	1.30	1.1402	336.0	8.0	0.00	82.58
B	3	1.00	1.0000	337.0	5.0	0.00	72.47	D	3	0.97	0.9849	337.0	3.0	0.00	71.37




Average Yaw Angle 6.8 °

Stratification Test Results Summary
Ash Grove Cement Company
Midlothian Cement Plant
Kiln 3 Stack
January 4, 2024

Number of Ports Sampled: 1
Number of Points per Port: 3
Total Number of Traverse Points: 3

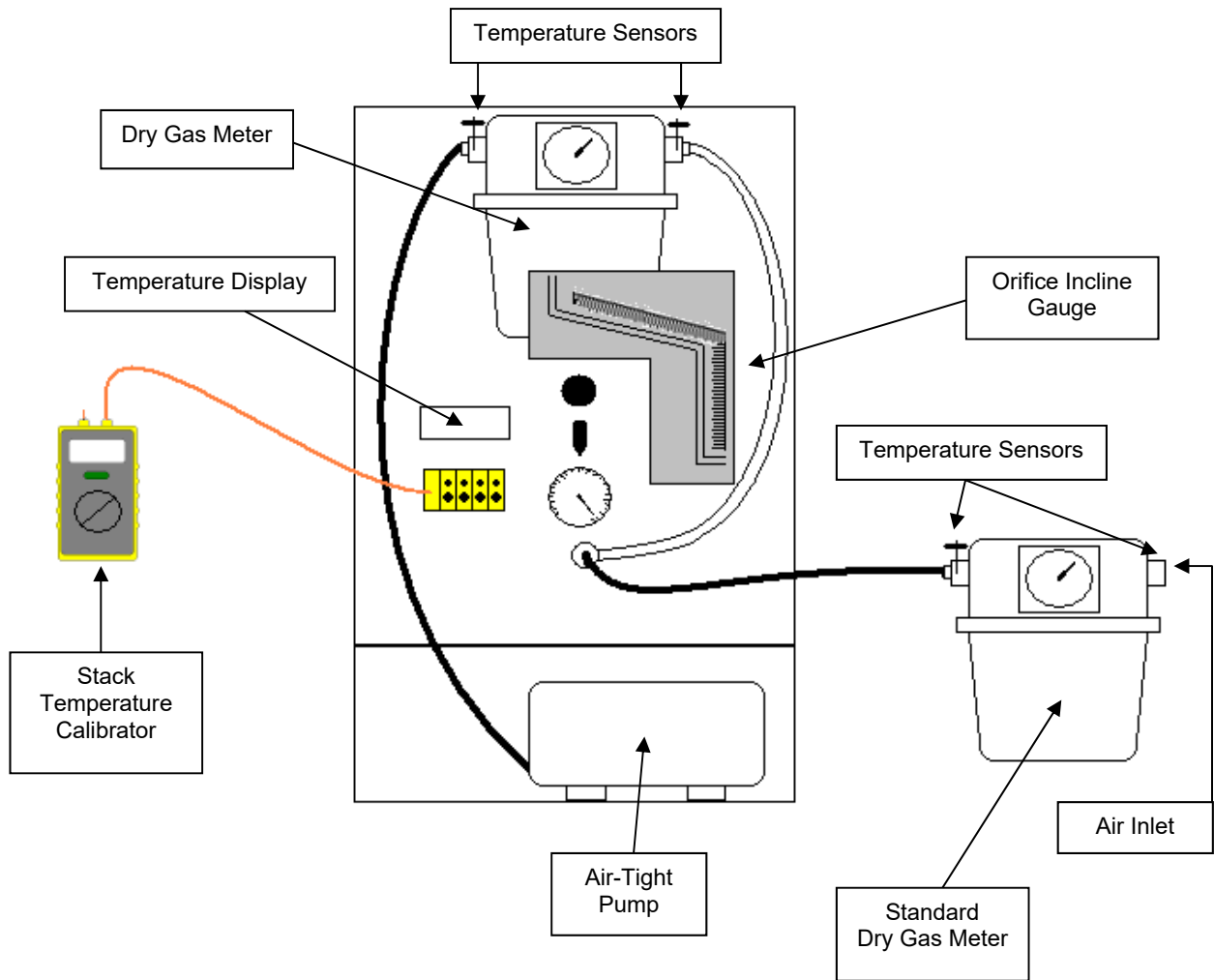
Port No.	Point No.	Time	O ₂ %	Actual % Difference O ₂ %	Mean Difference O ₂ %
1	1	10:50	8.70	0.46	0.04
	2	11:00	8.73	0.11	0.01
	3	11:10	8.79	0.57	0.05
Average			8.74		

One point traverse (<5% difference) 
Three point traverse (0.4, 1.2, and 2.0 meters), <10% difference 
Twelve point traverse (Method 1 points) >10% difference 

One point traverse (<0.3% mean difference) 
Three point traverse (0.4, 1.2, and 2.0 meters), < 0.5% mean difference for O₂ 
Twelve point traverse (Method 1 points) >0.5% mean difference for O₂ 

Appendix G - Calibration Data

Dry Gas Meter/Control Module Calibration Diagram



Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM28
 Standard Meter No. 18654513
 Standard Meter (Y) 1.00630

Date: December 8, 2023
 Calibrated By: DCS
 Barometric Pressure: 24.60

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		57.185	101.169	65	70	70					
Initial		52.124	95.968	65	70	69					
Difference	1 0.20	5.061	5.201	65	70	70	70	19	10	0.987	1.908
Final		62.280	106.441	67	73	71					
Initial		57.185	101.169	65	70	70					
Difference	2 0.50	5.095	5.272	66	72	71	71	12	0	0.980	1.848
Final		67.284	111.601	68	74	72					
Initial		62.280	106.441	67	73	71					
Difference	3 0.70	5.004	5.160	68	74	72	73	10	10	0.983	1.931
Final		72.382	116.871	69	76	73					
Initial		67.284	111.601	68	74	72					
Difference	4 0.90	5.098	5.270	69	75	73	74	9	10	0.980	1.947
Final		77.722	122.374	69	78	74					
Initial		72.382	116.871	69	76	73					
Difference	5 1.20	5.340	5.503	69	77	74	75	8	15	0.985	1.915
Final		52.124	95.968	64	70	69					
Initial		46.850	90.574	65	68	70					
Difference	6 2.00	5.274	5.394	65	69	70	69	6	0	0.987	1.721

Average 0.984 1.878

Stack Temperature Sensor Calibration			
Temperature ID :	170198981	Name :	DCS
Ambient Temperature, °F :	63.7	Date :	December 8, 2023

Temperature Calibrator			
Model # :	CL23A	Certification Date:	October 19, 2023
Serial # :	T-314718	Expiration Date:	October 19, 2024

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

Reference Source Temperature (°F)	Test Thermometer Temperature (°F)	Temperature Difference %
0	0	0.0
250	248	0.3
600	596	0.4
1200	1196	0.2

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM28
 Standard Meter No. 18654513
 Standard Meter (Y) 1.00630

Date: January 8, 2024
 Calibrated By: PJC1
 Barometric Pressure: 24.64

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		408.818	466.380	69	71	71					
Initial		403.508	461.020	69	71	71					
Difference	1 0.20	5.310	5.360	69	71	71	71	18	0	1.000	1.546
Final		414.394	471.972	69	73	72					
Initial		408.818	466.380	69	71	71					
Difference	2 0.50	5.576	5.592	69	72	72	72	12	0	1.007	1.556
Final		419.843	477.466	69	72	72					
Initial		414.394	471.972	69	73	72					
Difference	3 0.70	5.449	5.494	69	73	72	72	10	0	1.002	1.582
Final		424.913	482.503	68	72	72					
Initial		419.843	477.466	69	72	72					
Difference	4 0.90	5.070	5.037	69	72	72	72	9	0	1.017	1.901
Final		430.222	487.878	68	73	71					
Initial		424.913	482.503	68	72	72					
Difference	5 1.20	5.309	5.375	68	73	72	72	8	0	0.998	1.823
Final		403.508	461.020	69	71	71					
Initial		398.348	455.826	69	71	71					
Difference	6 2.00	5.160	5.194	69	71	71	71	6	0	0.998	1.819

Average **1.004** **1.705**

Stack Temperature Sensor Calibration			
Temperature ID :	CM28	Name :	PJC1
Ambient Temperature, °F :	70.2	Date :	January 8, 2024

Temperature Calibrator			
Model # :	CL23A	Certification Date:	October 19, 2023
Serial # :	T-314718	Expiration Date:	October 18, 2024

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

Reference Source Temperature (°F)	Test Thermometer Temperature (°F)	Temperature Difference %
0	0	0.0
250	248	0.3
600	596	0.4
1200	1197	0.2

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM44
 Standard Meter No. 15788714
 Standard Meter (Y) 0.98570

Date: December 8, 2023
 Calibrated By: DCS
 Barometric Pressure: 24.60

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		235.191	613.064	72	70	70					
Initial		229.915	607.829	69	68	68					
Difference	1 0.20	5.276	5.235	71	69	69	69	18	31	0.990	1.747
Final		240.612	618.410	71	71	71					
Initial		235.191	613.064	71	71	71					
Difference	2 0.50	5.421	5.346	71	71	71	71	12	1	0.998	1.739
Final		245.956	623.773	72	72	72					
Initial		240.612	618.410	71	71	71					
Difference	3 0.70	5.344	5.363	72	72	72	72	10	22	0.980	1.866
Final		262.898	640.323	73	73	73					
Initial		257.511	635.027	73	73	73					
Difference	4 0.90	5.387	5.296	73	73	73	73	9	0	1.000	1.785
Final		257.511	635.027	73	73	73					
Initial		251.943	629.549	72	72	72					
Difference	5 1.20	5.568	5.478	73	73	73	73	8	16	0.998	1.877
Final		229.915	607.829	69	68	68					
Initial		224.144	602.180	69	67	67					
Difference	6 2.00	5.771	5.649	69	68	68	68	6	30	0.998	1.794

Average **0.994** **1.801**

Stack Temperature Sensor Calibration			
Temperature ID :	170198981	Name :	DCS
Ambient Temperature, °F :	63.7	Date :	December 8, 2023

Temperature Calibrator			
Model # :	CL23A	Certification Date:	October 19, 2023
Serial # :	T-314718	Expiration Date:	October 19, 2024

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

Reference Source Temperature (°F)	Test Thermometer Temperature (°F)	Temperature Difference %
0	0	0.0
250	249	0.1
600	597	0.3
1200	1197	0.2

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM44
 Standard Meter No. 18654513
 Standard Meter (Y) 1.00630

Date: January 9, 2024
 Calibrated By: PJC1
 Barometric Pressure: 24.54

Run Number	Orifice Setting in H ₂ O Chg (H)	Standard Meter Gas Volume vr	Dry Gas Meter Gas Volume vd	Standard Meter Temp. F° tr	Dry Gas Meter Inlet Temp. F° tdi	Dry Gas Meter Outlet Temp. F° tdo	Dry Gas Meter Avg. Temp. F° td	Time Min	Time Sec	Y	Chg (H)
Final		441.479	810.254	70	69	69					
Initial		436.387	805.136	69	68	68					
Difference	1 0.20	5.092	5.118	70	69	69	69	18	0	0.999	1.700
Final		446.620	815.420	70	70	70					
Initial		441.479	810.254	70	69	69					
Difference	2 0.50	5.141	5.166	70	70	70	70	12	0	0.999	1.853
Final		451.781	820.597	70	71	71					
Initial		446.620	815.420	70	70	70					
Difference	3 0.70	5.161	5.177	70	71	71	71	10	0	1.002	1.784
Final		457.093	825.938	70	71	71					
Initial		451.781	820.597	70	71	71					
Difference	4 0.90	5.312	5.341	70	71	71	71	9	3	1.000	1.771
Final		462.516	831.405	70	72	72					
Initial		457.093	825.938	70	71	71					
Difference	5 1.20	5.423	5.467	70	72	72	72	8	0	0.997	1.769
Final		436.387	805.136	69	68	68					
Initial		431.061	799.815	69	68	68					
Difference	6 2.00	5.326	5.321	69	68	68	68	6	12	0.999	1.841

Average 0.999 1.786

Stack Temperature Sensor Calibration			
Temperature ID :	CM44	Name :	PJC1
Ambient Temperature, °F :	72.4	Date :	January 9, 2024

Temperature Calibrator			
Model # :	CL23A	Certification Date:	October 19, 2023
Serial # :	T-314718	Expiration Date:	October 18, 2024

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

Reference Source Temperature (°F)	Test Thermometer Temperature (°F)	Temperature Difference %
0	0	0.0
250	249	0.1
600	597	0.3
1200	1197	0.2

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

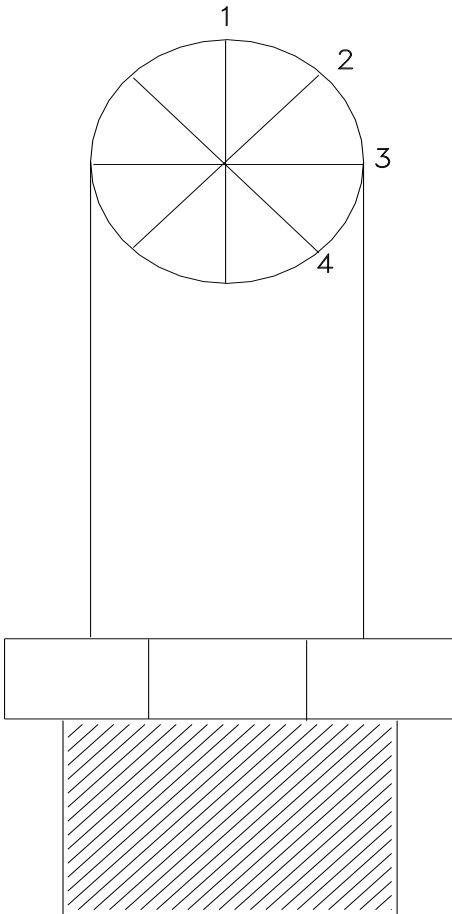
Nozzle Calibration

Date: 10/13/2023

Nozzle ID No.: 899

Analyst: EOS

Material/Type: Glass



0.280 1

0.282 2

0.281 3

0.282 4

Valid Data

Average
<u>0.281</u>

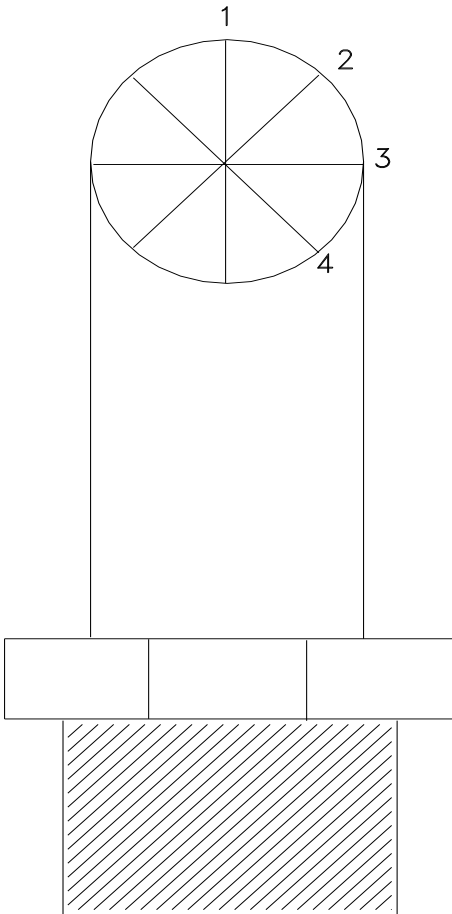
Nozzle Calibration

Date: 4/25/2023

Nozzle ID No.: 981

Analyst: WAP

Material/Type: Glass



0.281 1

0.281 2

0.281 3

0.281 4



Average
<u>0.281</u>

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Project #: M235102
Test Location: Kiln 3 Stack
Date: 1/4/2024
Operator: AWB
Operating Condition: Normal Operations > 90% Production

Sample System: FTIR
Probe Length: 5.0 ft
Probe Type: FTIR
Sample Plane: Horizontal
Port Length: 7 in.
Port Size (diameter): 6 in.
Port Type: Flange
Duct Shape: Circular
Diameter: 11.502 ft

Duct Area: 103.91 Sq. Ft.
Upstream Diameters: 16.80 Minimum Upstream Distance 5.8 Feet
Downstream Diameters: 7.40 Minimum Downstream Distance 23.0 Feet
Number of Ports Sampled: 1 Ideal Upstream Distance 23.0 Feet
Number of Points per Port: 1 Ideal Downstream Distance 92.0 Feet
Total Number of Traverse Points: 1

Calibration Gases

Type	Setting	Cylinder ID	Cylinder Value	Analyzer Response	Difference, % of Span	Expiration Date	Mid cylinder % of high cylinder	Final Bottle Pressure, PSI
O2 % (dry)	Zero	Zero Nitrogen	0.0	-0.03	0.14%	N/A		>500
	Mid	EB0162460	11.95	11.72	1.04%	7/19/2031	54.29%	>500
	High	EB0162461	22.01	22.18	-0.77%	11/9/2031		>500

Type	Compound	Cylinder ID	Cylinder Value	Expiration Date	Final Bottle Pressure, PSI
Zero Gas	Nitrogen	Zero Nitrogen	0.0	N/A	>500
Calibration Transfer Standard	Ethylene	EB0091181	100.4	7/10/2026	>500
Analyte Spike Gas	HCN	CC768228	49.30	3/11/2024	>500
	SF6		5.009		

Response Time Data

Type	RM Analyzer Make/Model	RM Analyzer s/n	Analyzer Span	RM Gas Span
O2 % (dry)	Servomex	01440D1/4385	25	22.01
HF ppmvw	MKS 2030	19088195	10	N/A
HCN ppmvw	MKS 2030	19088196	200	N/A

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Project #: M235102
Diluent: O2 %

Test Location: Kiln 3 Stack
Date: 1/4/24
Operator: AWB
O2 % Correction: 7

O2 % (dry) Correction Data

Run #	Cma	Precal	Postcal	Pre zero	Post zero	Co	Cm	C	Cgas	Span Bias	Span Drift	Zero Bias	Zero Drift
1	11.95	12.17	12.04	0.40	0.32	0.36	12.11	8.63	8.4	-1.45	-0.59	-1.59	-0.36
2	11.95	12.04	11.96	0.32	0.32	0.32	12.00	8.27	8.1	-1.09	-0.36	-1.59	0.00
3	11.95	11.96	11.97	0.32	0.34	0.33	11.97	7.95	7.8	-1.14	0.05	-1.68	0.09

Concentration of Cal Gas C = Average value of test Co=Average Pre and Post Zero
 erage Pre and Post Span Cgas = Corrected gas value of test

Calibration Corrected and Calculated Data

Run #	Run Date	Start Time	End Time	Moisture %	O2 % (dry)	CO2 % (wet)	CO2 % (dry)	HCN ppmvw	HCN ppmvd @ 7% O2	HF ppmvw	HF ppmvd @ 7% O2
1	1/4/24	10:50	11:49	39.07%	8.42	9.09	14.91	0.20	0.37	0.36	0.67
2	1/4/24	12:25	13:24	37.02%	8.14	9.73	15.44	0.20	0.35	0.38	0.66
3	1/4/24	14:17	15:16	36.60%	7.82	10.12	15.97	0.20	0.34	0.31	0.52

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Test Location: Kiln 3 Stack
Date: 1/4/24
Project #: M235102

<u>Time</u>	<u>O2 % (dry)</u>	
7:28	-0.03	iz
7:29	-0.03	
7:31	22.18	ih
7:32	22.21	
7:34	11.72	im
7:35	11.74	
10:10	0.41	
10:11	0.40	z
10:16	12.17	m
10:17	12.19	

Client: Ash Grove Cement Company
Facility: Midlothian Cement Plant
Project #: M235102
Test Location: Kiln 3 Stack
Date: 1/4/24

Post 1/Pre 2			Post 2/Pre 3		
<u>Time</u>	<u>O2 % (dry)</u>		<u>Time</u>	<u>O2 % (dry)</u>	
12:09	0.33		13:56	0.32	z
12:10	0.32	z	13:57	0.31	
12:18	12.04	m	13:59	11.96	m
12:19	12.06		14:00	12.01	

Post 3		
<u>Time</u>	<u>O2 % (dry)</u>	
15:39	0.34	z
15:40	0.32	
15:43	11.97	m
15:44	11.99	

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Project #: M235102
 Operating Condition: Normal Operations > 90% Production

Test Location: Kiln 3 Stack
 Date: 1/4/2024
 Operator: AWB
 FTIR s/n: 19088195

System Leak Check: 0.0 mL/min

Nitrogen (Zero) Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
N2 DIRECT_0001.LAB	1/4/24	7:40:30	0.6	0.1	0.1	191.2	1.12	-0.9	0.6	0.074
N2 DIRECT_0002.LAB	1/4/24	7:40:38	0.0	0.0	0.0	191.2	1.31	0.4	0.2	-0.034
N2 DIRECT_0003.LAB	1/4/24	7:40:46	0.0	0.0	0.0	191.3	1.31	0.8	0.0	-0.064
N2 DIRECT_0004.LAB	1/4/24	7:40:54	0.0	0.0	0.0	191.2	1.31	0.7	0.0	0.012
N2 DIRECT_0005.LAB	1/4/24	7:41:02	-0.1	0.0	0.1	191.2	1.31	-2.2	0.1	0.017
N2 DIRECT_0006.LAB	1/4/24	7:41:10	-0.1	0.0	0.0	191.3	1.31	-0.9	0.3	-0.070
N2 DIRECT_0007.LAB	1/4/24	7:41:18	0.0	0.0	0.0	191.3	1.31	0.2	0.2	0.002
N2 DIRECT_0008.LAB	1/4/24	7:41:26	0.1	0.0	0.0	191.2	1.31	0.2	0.2	-0.006
N2 DIRECT_0009.LAB	1/4/24	7:41:34	0.0	0.0	0.0	191.3	1.31	1.3	0.2	-0.015

Calibration Transfer Standard (CTS), Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
CTS DIRECT_0023.LAB	1/4/24	7:48:31	0.0	0.0	0.0	191.3	1.02	99.5	0.2	-0.018	99.1%
CTS DIRECT_0024.LAB	1/4/24	7:48:39	0.0	0.0	0.0	191.3	1.02	99.5	0.6	-0.012	99.1%
CTS DIRECT_0025.LAB	1/4/24	7:48:47	0.0	0.0	0.0	191.3	1.01	100.2	0.4	-0.009	99.8%
CTS DIRECT_0026.LAB	1/4/24	7:48:55	0.0	0.0	0.0	191.3	1.02	100.1	0.5	-0.011	99.7%
CTS DIRECT_0027.LAB	1/4/24	7:49:03	0.0	0.0	0.0	191.3	1.02	100.1	0.4	-0.014	99.7%
CTS DIRECT_0028.LAB	1/4/24	7:49:11	0.0	0.0	0.1	191.3	1.02	100.1	0.6	-0.012	99.7%
CTS DIRECT_0029.LAB	1/4/24	7:49:19	0.0	0.0	0.0	191.3	1.02	100.1	0.5	-0.018	99.7%
Average											99.9

Analyte Spike Gas (HCN) Direct to FTIR

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % HCN		
HCN DIRECT_0033.LAB	1/4/24	7:50:55	0.0	0.0	0.0	191.3	1.02	0.0	47.0	5.029	95.2%		
HCN DIRECT_0034.LAB	1/4/24	7:51:03	0.0	0.0	0.0	191.3	1.03	-0.1	46.7	5.031	94.7%		
HCN DIRECT_0035.LAB	1/4/24	7:51:11	0.0	0.0	-0.1	191.3	1.03	-0.1	46.8	5.034	95.0%		
HCN DIRECT_0036.LAB	1/4/24	7:51:19	0.0	0.0	0.0	191.3	1.03	0.2	47.0	5.036	95.3%		
HCN DIRECT_0037.LAB	1/4/24	7:51:27	0.0	0.0	0.0	191.3	1.03	0.0	46.8	5.040	95.0%		
HCN DIRECT_0038.LAB	1/4/24	7:51:35	0.0	0.0	0.0	191.3	1.03	0.2	47.0	5.035	95.4%		
HCN DIRECT_0039.LAB	1/4/24	7:51:43	0.0	0.0	0.0	191.3	1.03	0.0	46.7	5.045	94.8%		
HCN DIRECT_0040.LAB	1/4/24	7:51:51	0.0	0.0	0.0	191.3	1.03	0.0	47.1	5.041	95.5%		
Average											46.9	5.036	95.1%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
CTS REMOTE_0744.LAB	1/4/24	10:06:12	2.8	0.0	0.0	191.4	1.05	96.2	0.0	-0.013	95.8%
CTS REMOTE_0745.LAB	1/4/24	10:06:20	2.4	0.0	0.0	191.3	1.05	96.5	0.0	-0.020	96.1%
CTS REMOTE_0746.LAB	1/4/24	10:06:28	2.1	0.0	-0.1	191.3	1.05	97.1	0.2	-0.012	96.7%
CTS REMOTE_0747.LAB	1/4/24	10:06:36	1.8	0.0	0.0	191.5	1.05	97.5	0.1	-0.014	97.1%
CTS REMOTE_0748.LAB	1/4/24	10:06:44	1.5	0.0	0.0	191.4	1.05	97.8	-0.2	-0.005	97.4%
CTS REMOTE_0749.LAB	1/4/24	10:06:52	1.4	0.0	0.0	191.3	1.05	97.8	-0.3	-0.017	97.4%
CTS REMOTE_0750.LAB	1/4/24	10:07:00	1.3	0.0	0.0	191.3	1.05	98.1	-0.4	-0.020	97.7%
CTS REMOTE_0751.LAB	1/4/24	10:07:08	1.3	0.0	0.0	191.3	1.05	97.9	-0.2	-0.011	97.5%

Response Time Test

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Response Time (sec)
CTS REMOTE_0777.LAB	1/4/24	10:12:50	0.5	0.0	-0.1	191.3	1.04	0.1	-0.5	-0.003	-
CTS REMOTE_0778.LAB	1/4/24	10:12:57	5.2	3.8	0.1	191.3	1.04	0.4	0.3	-0.010	15
CTS REMOTE_0779.LAB	1/4/24	10:13:04	12.1	4.4	0.1	191.3	1.04	19.1	-0.1	-0.020	23
CTS REMOTE_0780.LAB	1/4/24	10:13:11	5.2	0.1	0.1	191.3	1.04	92.0	0.3	-0.016	-
CTS REMOTE_0781.LAB	1/4/24	10:13:18	3.8	0.0	0.0	191.3	1.04	95.0	0.0	-0.020	-
CTS REMOTE_0782.LAB	1/4/24	10:13:25	2.5	0.0	0.0	191.3	1.05	96.2	0.2	-0.019	-
CTS REMOTE_0783.LAB	1/4/24	10:13:32	1.7	0.0	0.0	191.3	1.05	97.3	0.1	-0.013	-
CTS REMOTE_0784.LAB	1/4/24	10:13:39	1.3	0.0	0.1	191.3	1.04	97.4	-0.2	-0.020	-
CTS REMOTE_0785.LAB	1/4/24	10:13:46	1.2	0.0	-0.1	191.3	1.05	97.6	-0.4	-0.012	-

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Project #: M235102
 Operating Condition: Normal Operations > 90% Production

Test Location: Kiln 3 Stack
 Date: 1/4/2024
 Operator: AWB
 FTIR s/n: 19088195

Pre 1 Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
NATIVE REMOTE_0825.LAB	1/4/24	10:21:15	30.4	9.8	0.4	191.3	1.04	0.5	-0.4	-0.006
NATIVE REMOTE_0826.LAB	1/4/24	10:21:23	39.2	8.6	0.4	191.3	1.03	0.0	-0.8	-0.014
NATIVE REMOTE_0827.LAB	1/4/24	10:21:31	49.7	7.2	0.6	191.3	1.02	-0.2	-0.9	-0.009
									-0.7	-0.009

Pre 1 Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
SPIKE REMOTE_0904.LAB	1/4/24	10:32:48	31.1	8.6	0.2	191.3	1.04	0.5	2.8	0.400	0.079	90.2%
SPIKE REMOTE_0905.LAB	1/4/24	10:32:56	31.1	8.6	0.3	191.3	1.04	0.4	3.0	0.439	0.087	86.1%
SPIKE REMOTE_0906.LAB	1/4/24	10:33:04	31.2	8.5	0.3	191.3	1.04	0.5	2.8	0.437	0.087	82.0%
SPIKE REMOTE_0907.LAB	1/4/24	10:33:12	31.6	8.5	0.3	191.3	1.04	0.4	3.0	0.448	0.089	85.6%
SPIKE REMOTE_0908.LAB	1/4/24	10:33:20	31.4	8.6	0.3	191.3	1.04	0.4	3.0	0.450	0.089	85.1%
SPIKE REMOTE_0909.LAB	1/4/24	10:33:28	30.6	8.8	0.3	191.3	1.04	0.4	3.0	0.447	0.089	85.0%
SPIKE REMOTE_0910.LAB	1/4/24	10:33:36	30.2	9.0	0.2	191.3	1.04	0.6	3.0	0.447	0.089	84.5%
SPIKE REMOTE_0911.LAB	1/4/24	10:33:44	30.0	9.0	0.3	191.3	1.04	0.4	2.9	0.450	0.089	82.3%

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN1_0984.LAB	1/4/24	11:59:57	36.8	9.7	0.4	191.3	1.03	0.5	-1.2	-0.006
RUN1_0985.LAB	1/4/24	12:00:58	35.3	9.8	0.3	191.3	1.03	0.5	-0.9	-0.007
RUN1_0986.LAB	1/4/24	12:01:59	38.7	9.4	0.4	191.3	1.03	0.4	-1.1	-0.008
									-1.1	-0.007

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST R1 SPIKE_1003.LAB	1/4/24	12:05:46	32.9	9.1	0.4	191.3	1.03	0.6	2.7	0.424	0.084	92.1%
POST R1 SPIKE_1004.LAB	1/4/24	12:05:54	32.6	9.1	0.3	191.3	1.03	0.5	2.6	0.451	0.090	80.6%
POST R1 SPIKE_1005.LAB	1/4/24	12:06:02	32.2	9.1	0.3	191.3	1.04	0.4	2.6	0.451	0.090	81.8%
POST R1 SPIKE_1006.LAB	1/4/24	12:06:10	32.0	9.2	0.6	191.3	1.03	0.4	2.7	0.462	0.092	82.2%
POST R1 SPIKE_1007.LAB	1/4/24	12:06:18	32.1	9.0	0.3	191.3	1.04	0.5	2.6	0.495	0.098	71.3%
POST R1 SPIKE_1008.LAB	1/4/24	12:06:26	34.1	8.7	0.0	191.3	1.04	0.4	3.3	0.484	0.096	93.4%
POST R1 SPIKE_1009.LAB	1/4/24	12:06:34	43.5	7.5	0.4	191.3	1.03	0.0	2.5	0.429	0.085	83.4%
POST R1 SPIKE_1010.LAB	1/4/24	12:06:42	43.1	7.3	0.5	191.3	1.03	0.2	3.0	0.493	0.098	83.6%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST R1 CTS_1033.LAB	1/4/24	12:10:20	3.3	0.0	-0.1	191.3	1.05	95.7	0.2	-0.015	95.3%
POST R1 CTS_1034.LAB	1/4/24	12:10:27	3.1	0.0	-0.2	191.3	1.05	96.0	0.3	-0.014	95.7%
POST R1 CTS_1035.LAB	1/4/24	12:10:34	2.9	0.0	0.2	191.3	1.04	96.4	0.1	-0.012	96.0%
POST R1 CTS_1036.LAB	1/4/24	12:10:41	2.6	0.0	0.0	191.3	1.04	96.9	0.4	-0.011	96.5%
POST R1 CTS_1037.LAB	1/4/24	12:10:48	2.3	0.0	-0.1	191.3	1.04	97.3	0.0	-0.012	96.9%
POST R1 CTS_1038.LAB	1/4/24	12:10:55	2.0	0.0	0.1	191.3	1.05	97.0	0.1	-0.019	96.6%
POST R1 CTS_1039.LAB	1/4/24	12:11:02	1.9	0.0	-0.1	191.3	1.04	97.5	0.0	-0.012	97.1%
POST R1 CTS_1040.LAB	1/4/24	12:11:09	1.7	0.0	0.0	191.3	1.05	97.3	-0.4	-0.012	96.9%

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Project #: M235102
 Operating Condition: Normal Operations > 90% Production

Test Location: Kiln 3 Stack
 Date: 1/4/2024
 Operator: AWB
 FTIR s/n: 19088195

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN 2_1152.LAB	1/4/24	13:36:00	38.2	9.7	0.3	191.3	1.03	0.6	-2.5	-0.007
RUN 2_1153.LAB	1/4/24	13:37:00	37.7	9.6	0.3	191.3	1.03	0.5	-2.2	-0.005
RUN 2_1154.LAB	1/4/24	13:38:00	37.2	9.7	0.3	191.3	1.03	0.6	-2.5	-0.005
									-2.4	-0.006

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST 2 SPIKE_1191.LAB	1/4/24	13:46:54	31.9	9.2	0.3	191.3	1.03	0.6	1.4	0.419	0.083	79.9%
POST 2 SPIKE_1192.LAB	1/4/24	13:47:02	32.5	9.2	0.2	191.3	1.03	0.8	1.7	0.418	0.083	102.4%
POST 2 SPIKE_1194.LAB	1/4/24	13:47:10	46.3	7.2	0.3	191.3	1.02	0.2	1.1	0.384	0.076	82.0%
POST 2 SPIKE_1203.LAB	1/4/24	13:47:18	33.0	8.7	0.3	191.3	1.03	0.7	1.7	0.485	0.096	74.4%
POST 2 SPIKE_1207.LAB	1/4/24	13:47:26	32.4	9.4	0.2	191.3	1.04	0.7	1.5	0.414	0.082	89.5%
POST 2 SPIKE_1211.LAB	1/4/24	13:47:34	32.0	9.1	0.3	191.3	1.04	0.5	1.5	0.458	0.091	71.2%
POST 2 SPIKE_1215.LAB	1/4/24	13:47:42	32.3	9.0	0.2	191.3	1.03	0.6	1.5	0.449	0.089	74.1%
POST 2 SPIKE_1216.LAB	1/4/24	13:47:50	34.4	8.9	0.0	191.3	1.03	0.4	1.6	0.438	0.087	82.2%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST 2 CTS_1268.LAB	1/4/24	13:54:59 PM	3.1	0.0	-0.2	191.3	1.05	96.0	-0.9	-0.009	96.0%
POST 2 CTS_1269.LAB	1/4/24	13:55:07 PM	2.9	0.0	-0.1	191.3	1.05	96.1	-0.9	-0.011	96.1%
POST 2 CTS_1270.LAB	1/4/24	13:54:59 PM	2.6	0.0	0.1	191.3	1.05	97.1	-0.9	-0.012	97.1%
POST 2 CTS_1271.LAB	1/4/24	13:55:07 PM	2.2	0.0	-0.1	191.3	1.05	97.1	-0.9	-0.018	97.2%
POST 2 CTS_1272.LAB	1/4/24	13:54:59 PM	2.1	0.0	0.0	191.3	1.05	97.2	-0.9	-0.019	97.2%
POST 2 CTS_1273.LAB	1/4/24	13:55:07 PM	1.9	0.0	0.0	191.3	1.05	97.5	-1.4	-0.020	97.6%
POST 2 CTS_1274.LAB	1/4/24	13:54:59 PM	1.9	0.0	-0.2	191.3	1.05	97.5	-1.0	-0.013	97.5%
POST 2 CTS_1275.LAB	1/4/24	13:55:07 PM	1.8	0.0	-0.1	191.3	1.05	97.6	-1.5	-0.016	97.6%

Native Effluent Prior to Analyte Spike

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
RUN 3_1385.LAB	1/4/24	15:27:00	38.0	9.4	0.3	191.3	1.03	0.6	-2.5	-0.005
RUN 3_1386.LAB	1/4/24	15:28:00	35.2	10.0	0.2	191.3	1.03	0.8	-2.4	-0.006
RUN 3_1387.LAB	1/4/24	15:29:00	38.7	10.1	0.3	191.3	1.03	0.6	-2.5	-0.006
									-2.5	-0.006

Effluent Spike Using Analyte

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Dilution Factor	Recovery % HCN
POST R3 SPIKE_1408.LAB	1/4/24	15:34:48	31.2	9.4	0.2	191.3	1.04	0.6	2.1	0.499	0.099	86.9%
POST R3 SPIKE_1409.LAB	1/4/24	15:34:56	31.4	9.5	0.2	191.2	1.04	0.6	2.0	0.486	0.096	88.7%
POST R3 SPIKE_1410.LAB	1/4/24	15:35:04	32.7	9.2	0.4	191.3	1.04	0.7	2.0	0.476	0.095	89.8%
POST R3 SPIKE_1411.LAB	1/4/24	15:35:12	33.1	9.0	0.1	191.3	1.03	0.8	2.0	0.494	0.098	83.6%
POST R3 SPIKE_1412.LAB	1/4/24	15:35:20	32.4	9.1	0.2	191.3	1.04	0.7	2.1	0.481	0.095	94.7%
POST R3 SPIKE_1413.LAB	1/4/24	15:35:28	32.0	9.2	0.2	191.3	1.04	0.7	2.1	0.484	0.096	91.3%
POST R3 SPIKE_1414.LAB	1/4/24	15:35:36	32.1	9.2	0.2	191.3	1.04	0.7	1.9	0.487	0.097	82.5%
POST R3 SPIKE_1415.LAB	1/4/24	15:35:44	33.1	9.1	0.2	191.3	1.04	0.7	2.0	0.488	0.097	84.6%

CTS, System Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST R3 CTS_1443.LAB	1/4/24	15:40:36	2.5	0.0	-0.1	191.3	1.05	96.3	-1.3	-0.020	96.4%
POST R3 CTS_1444.LAB	1/4/24	15:40:44	2.5	0.0	-0.1	191.3	1.05	97.1	-0.7	-0.011	97.1%
POST R3 CTS_1445.LAB	1/4/24	15:40:52	2.4	0.0	-0.1	191.3	1.05	96.7	-0.7	-0.013	96.8%
POST R3 CTS_1446.LAB	1/4/24	15:41:00	2.3	0.0	-0.2	191.2	1.05	96.8	-1.2	-0.014	96.9%
POST R3 CTS_1447.LAB	1/4/24	15:41:08	2.1	0.0	-0.1	191.3	1.05	97.1	-0.6	-0.009	97.1%
POST R3 CTS_1448.LAB	1/4/24	15:41:16	2.0	0.0	0.0	191.3	1.05	97.2	-1.4	-0.022	97.2%
POST R3 CTS_1449.LAB	1/4/24	15:41:24	1.9	0.0	-0.2	191.3	1.04	97.7	-0.9	-0.016	97.7%
POST R3 CTS_1450.LAB	1/4/24	15:41:32	1.8	0.0	-0.2	191.3	1.05	97.2	-1.5	-0.019	97.3%

Client: Ash Grove Cement Company
 Facility: Midlothian Cement Plant
 Project #: M235102
 Operating Condition: Normal Operations > 90% Production

Test Location: Kiln 3 Stack
 Date: 1/4/2024
 Operator: AWB
 FTIR s/n: 19088195

Post Test CTS, Direct Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet	Recovery % Ethylene
POST R3 CTS_1489.LAB	1/4/24	15:50:00	0.8	0.0	0.0	191.3	1.11	99.6	-1.6	-0.019	99.6%
POST R3 CTS_1490.LAB	1/4/24	15:50:08	0.6	0.0	0.1	191.3	1.07	99.7	-1.6	-0.023	99.8%
POST R3 CTS_1491.LAB	1/4/24	15:50:16	0.4	0.0	0.0	191.3	1.07	99.6	-1.2	-0.020	99.6%
POST R3 CTS_1492.LAB	1/4/24	15:50:24	0.4	0.0	0.2	191.3	1.07	99.3	-1.2	-0.016	99.3%
POST R3 CTS_1493.LAB	1/4/24	15:50:32	0.3	0.0	-0.1	191.6	1.07	99.6	-1.8	-0.015	99.6%
POST R3 CTS_1494.LAB	1/4/24	15:50:40	0.2	0.0	0.1	191.3	1.07	99.6	-1.4	-0.018	99.6%
POST R3 CTS_1495.LAB	1/4/24	15:50:48	0.2	0.0	0.1	191.3	1.07	99.4	-1.3	-0.017	99.5%
POST R3 CTS_1496.LAB	1/4/24	15:50:56	0.2	0.0	0.1	191.3	1.07	99.6	-1.2	-0.022	99.7%
Average								99.5			

Post Test N2, Direct Purge

Spectrum	Date	Time	H2O% %v	CO2 %v wet	HF ppmv wet	FTIR Gas Cell Temperature deg C	FTIR Gas Cell Pressure atm	Ethylene ppmv wet	HCN ppmv wet	SF6 ppmv wet
POST R3 N2_1498.LAB	1/4/24	15:54:07	0.0	0.0	0.0	191.3	1.05	0.1	-1.1	-0.003
POST R3 N2_1499.LAB	1/4/24	15:56:13	0.0	0.0	0.0	191.3	1.05	0.1	-1.0	-0.002
POST R3 N2_1500.LAB	1/4/24	15:58:18	0.0	0.0	0.0	191.3	1.05	0.1	-0.9	-0.004

Zero Gas and In-Stack Detection Limit Study
Ash Grove Cement Company
Midlothian Cement Plant
Kiln 3 Stack
1/4/2024

Time	DL summary - zero gas		Time	DL summary - in stack	
	HF ppm (10) 191C	HCN (100) 191C		HF ppm (10) 191C	HCN (100) 191C
7:41:02 AM	0.06	-0.09	10:16:09 AM	-0.01	-0.36
7:41:10 AM	0.05	0.08	10:16:16 AM	-0.02	-0.25
7:41:18 AM	0.00	0.10	10:16:23 AM	0.00	-0.23
7:41:26 AM	0.01	-0.07	10:16:30 AM	0.00	-0.26
7:41:34 AM	0.00	-0.12	10:16:37 AM	-0.03	-0.40
7:41:42 AM	0.01	-0.06	10:16:44 AM	-0.08	-0.40
			10:16:51 AM	0.01	-0.27
Standard Deviation	0.02	0.08	Standard Deviation	0.03	0.07
3x = DL	0.07	0.25	3x = DL	0.08	0.20

Appendix H - Gas Cylinder Certifications

CERTIFICATE OF ANALYSIS

Grade of Product: EPA PROTOCOL STANDARD

Part Number: E03NI78E15A1066	Reference Number: 153-402794083-1
Cylinder Number: EB0162460	Cylinder Volume: 151.1 CF
Laboratory: 124 - Tooele (SAP) - UT	Cylinder Pressure: 2015 PSIG
PGVP Number: B72023	Valve Outlet: 590
Gas Code: CO2,O2,BALN	Certification Date: Jul 19, 2023

Expiration Date: Jul 19, 2031

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	10.00 %	9.897 %	G1	+/- 0.8% NIST Traceable	07/19/2023
OXYGEN	12.00 %	11.95 %	G1	+/- 0.9% NIST Traceable	07/19/2023
NITROGEN	Balance				

CALIBRATION STANDARDS

Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	13060405	CC411744	7.489 % CARBON DIOXIDE/NITROGEN	0.6%	May 14, 2025
NTRM	98051010	SG9161286BAL	12.05 % OXYGEN/NITROGEN	0.7%	Dec 14, 2023

ANALYTICAL EQUIPMENT

Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA-510 SV4MEUTJ CO2	CO2 NDIR (Dixon)	Jun 28, 2023
Horiba MPA-510 W603MM58 O2	O2 Paramagnetic (DIXON)	Jun 29, 2023

Triad Data Available Upon Request



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: EPA PROTOCOL STANDARD

Part Number: E03NI59E15A3452	Reference Number: 153-402886633-1
Cylinder Number: EB0162461	Cylinder Volume: 159.0 CF
Laboratory: 124 - Tooele (SAP) - UT	Cylinder Pressure: 2015 PSIG
PGVP Number: B72023	Valve Outlet: 590
Gas Code: CO2,O2,BALN	Certification Date: Nov 09, 2023

Expiration Date: Nov 09, 2031

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	19.00 %	18.64 %	G1	+/- 0.8% NIST Traceable	11/09/2023
OXYGEN	22.00 %	22.01 %	G1	+/- 0.5% NIST Traceable	11/09/2023
NITROGEN	Balance				

CALIBRATION STANDARDS

Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	13060802	CC415397	24.04 % CARBON DIOXIDE/NITROGEN	0.6%	Dec 11, 2025
NTRM	09061434	CC282492	22.53 % OXYGEN/NITROGEN	0.4%	May 13, 2025

ANALYTICAL EQUIPMENT

Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA-510 SV4MEUTJ CO2	CO2 NDIR (Dixon)	Oct 17, 2023
Horiba MPA-510 W603MM58 O2	O2 Paramagnetic (DIXON)	Oct 17, 2023

Triad Data Available Upon Request



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: CERTIFIED STANDARD-SPEC

Part Number:	X02NI99C15A1268	Reference Number:	153-402780689-1
Cylinder Number:	EB0091181	Cylinder Volume:	144.0 CF
Laboratory:	124 - Tooele (SAP) - UT	Cylinder Pressure:	2015 PSIG
Analysis Date:	Jul 10, 2023	Valve Outlet:	350
Lot Number:	153-402780689-1		

Expiration Date: Jul 10, 2026

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

Component	Req Conc	Actual Concentration (Mole %)	Analytical Uncertainty
ETHYLENE	100.0 PPM	100.4 PPM	+/- 2%
NITROGEN	Balance		



Signature on file

CERTIFICATE OF ANALYSIS

Grade of Product: CERTIFIED STANDARD-SPEC

Customer:	MOSTARDI PLATT	Reference Number:	160-402841639-1
Part Number:	X03NI99C15AC0W8	Cylinder Volume:	144.4 CF
Cylinder Number:	CC768228	Cylinder Pressure:	2015 PSIG
Laboratory:	124 - Plumsteadville - PA	Valve Outlet:	350SS
Analysis Date:	Sep 11, 2023		
Lot Number:	160-402841639-1		

Expiration Date: Mar 11, 2024

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

Component	Req Conc	Actual Concentration (Mole %)	Analytical Uncertainty
SULFUR HEXAFLUORIDE	5.000 PPM	5.009 PPM	+/- 5%
HYDROGEN CYANIDE	50.00 PPM	49.30 PPM	+/- 5%
NITROGEN	Balance		



Signature on file

END OF THE REPORT