

# Section 114 Information Collection Request Emissions Test Report

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CalPortland Company, Inc.  
Redding Cement Plant  
EPA Registry ID: 110070385909  
15390 Wonderland Blvd.  
Redding, CA 96003  
Report No. M234605A





**Section 114 Information Collection Request  
Emissions Test Report**

**CalPortland Company, Inc.  
Redding Cement Plant  
EPA Registry ID: 110070385909  
15390 Wonderland Blvd.  
Redding, CA 96003**

**Report Submittal Date:  
February 14, 2024**

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Mostardi Platt

**Report No. M234605A**

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## 1.0 INTRODUCTION

Mostardi Platt conducted an air emissions test program for CalPortland Company, Inc. at the Redding Cement Plant located in Redding, California. All testing was performed as described in the *Code of Federal Regulations*, Title 40, Part 60, Appendix A (40CFR60), Methods 1, 2, 3A, 4, 26A, and 40CFR63, Appendix A, (40CFR63) Method 320.

This test program was completed to satisfy the requirements of the United States Environmental Protection Agency (USEPA) Section 114 Information Collection Request for Portland Cement Manufacturing facilities.

The identification of individuals associated with the test program is summarized below:

| <b>Location</b>             | <b>Address</b>  | <b>Contact</b>  |
|-----------------------------|---|---|
| Test Coordinator            | CalPortland Company<br>15390 Wonderland Blvd.<br>Redding, CA 96003      | Meghan Way<br>Environmental Manager<br>(530) 806-1569<br><a href="mailto:mway@calportland.com">mway@calportland.com</a>           |
| Test Company Representative | Mostardi Platt<br>7715 Commercial Way, Suite 155<br>Henderson, NV 89011 | Mr. Richard J. Sollars II<br>Regional Manager<br>(630) 993-2100<br><a href="mailto:rsollars@mp-mail.com">rsollars@mp-mail.com</a> |

## 2.0 TEST REQUIREMENTS

Testing was performed at the kiln stack. The following table presents a list of the parameters tested, the applicable methodologies utilized, and average test results:

| Source  | Parameter Tested                         | Test Results  | Method/Regulation Citation               |
|---|--|---|--|
| Kiln Stack<br>Mill On                                   | Hydrogen Fluoride (HF)                   | ≤ 0.10 ppmvw  | USEPA Method 320,<br>40CFR63, Appendix A |
|   |  | ≤ 0.19 ppmvd @7% O <sub>2</sub>   |  |
|   |  | ≤ 0.05 lb/hr  |  |
|   |  | ≤ 0.0006 lb/ton clinker   |  |
|   | HF <sup>1</sup>                          | ≤ 0.13 ppmvd  | Method 26A,<br>40CFR60, Appendix A       |
|   |  | ≤ 0.15 ppmvd @7% O <sub>2</sub>   |  |
|   |  | ≤ 0.12 lb/hr  |  |
|   |  | ≤ 0.0005 lb/ton clinker   |  |
|   | Chlorine (Cl <sub>2</sub> ) <sup>1</sup> | ≤ 0.04 ppmvd  | USEPA Method 26A,<br>40CFR60, Appendix A |
|   |  | ≤ 0.05 ppmvd @7% O <sub>2</sub>   |  |
|   |  | ≤ 0.13 lb/hr  |  |
|   |  | ≤ 0.0005 lb/ton clinker   |  |
|   | Hydrogen Cyanide (HCN)                   | 0.78 ppmvw  | USEPA Method 320,<br>40CFR63, Appendix A |
|   |  | 1.47 ppmvd @7% O <sub>2</sub>   |  |
| 0.49 lb/hr  |  |   |  |
| 0.0064 lb/ton clinker                                   |  |   |  |
| Oxygen (O <sub>2</sub> )                                | 12.5 % (dry)                             | USEPA Method 3A,<br>40CFR60, Appendix A                                 |  |
| Carbon Dioxide (CO <sub>2</sub> )                       | 13.7 % (dry)                             | USEPA Method 320,<br>40CFR63, Appendix A                                |  |
| Moisture (H <sub>2</sub> O)                             | 11.6 %                                   | USEPA Method 320,<br>40CFR63, Appendix A                                |  |
| Cyclonic Flow Determination                             | PASS                                     | USEPA Method 1, 40CFR60,<br>Appendix A, Section 11.4                    |  |
| Three-point O <sub>2</sub> Stratification Determination | < 5 %                                    | USEPA Method 3A,<br>40CFR60, Appendix A and<br>Method 7E, Section 8.1.2 |  |

<sup>1</sup> HF and Cl<sub>2</sub> Method 26A results are reported as the average from Train A and Train B.

| Source  | Parameter Tested                         | Test Results  | Method/Regulation Citation               |
|---|--|---|--|
| Kiln Stack<br>Mill Off                                  | Hydrogen Fluoride (HF)                   | ≤ 0.10 ppmvw  | USEPA Method 320,<br>40CFR63, Appendix A |
|   |  | ≤ 0.16 ppmvd @7% O <sub>2</sub>   |  |
|   |  | ≤ 0.04 lb/hr  |  |
|   |  | ≤ 0.0005 lb/ton clinker   |  |
|   | HF <sup>2</sup>                          | ≤ 0.10 ppmvd  | Method 26A,<br>40CFR60, Appendix A       |
|   |  | ≤ 0.14 ppmvd @7% O <sub>2</sub>   |  |
|   |  | ≤ 0.04 lb/hr  |  |
|   |  | ≤ 0.0005 lb/ton clinker   |  |
|   | Chlorine (Cl <sub>2</sub> ) <sup>1</sup> | ≤ 0.03 ppmvd  | USEPA Method 26A,<br>40CFR60, Appendix A |
|   |  | ≤ 0.04 ppmvd @7% O <sub>2</sub>   |  |
|   |  | ≤ 0.04 lb/hr  |  |
|   |  | ≤ 0.0005 lb/ton clinker   |  |
|   | Hydrogen Cyanide (HCN)                   | 0.91 ppmvw  | USEPA Method 320,<br>40CFR63, Appendix A |
|   |  | 1.49 ppmvd @7% O <sub>2</sub>   |  |
| 0.53 lb/hr  |  |   |  |
| 0.0067 lb/ton clinker                                   |  |   |  |
| Oxygen (O <sub>2</sub> )                                | 11.2 % (dry)                             | USEPA Method 3A,<br>40CFR60, Appendix A                                 |  |
| Carbon Dioxide (CO <sub>2</sub> )                       | 16.2 % (dry)                             | USEPA Method 320,<br>40CFR63, Appendix A                                |  |
| Moisture (H <sub>2</sub> O)                             | 12.2 %                                   | USEPA Method 320,<br>40CFR63, Appendix A                                |  |
| Cyclonic Flow Determination                             | PASS                                     | USEPA Method 1, 40CFR60,<br>Appendix A, Section 11.4                    |  |
| Three-point O <sub>2</sub> Stratification Determination | < 5 %                                    | USEPA Method 3A,<br>40CFR60, Appendix A and<br>Method 7E, Section 8.1.2 |  |

<sup>2</sup> HF and Cl<sub>2</sub> Method 26A results are reported as the average from Train A and Train B.

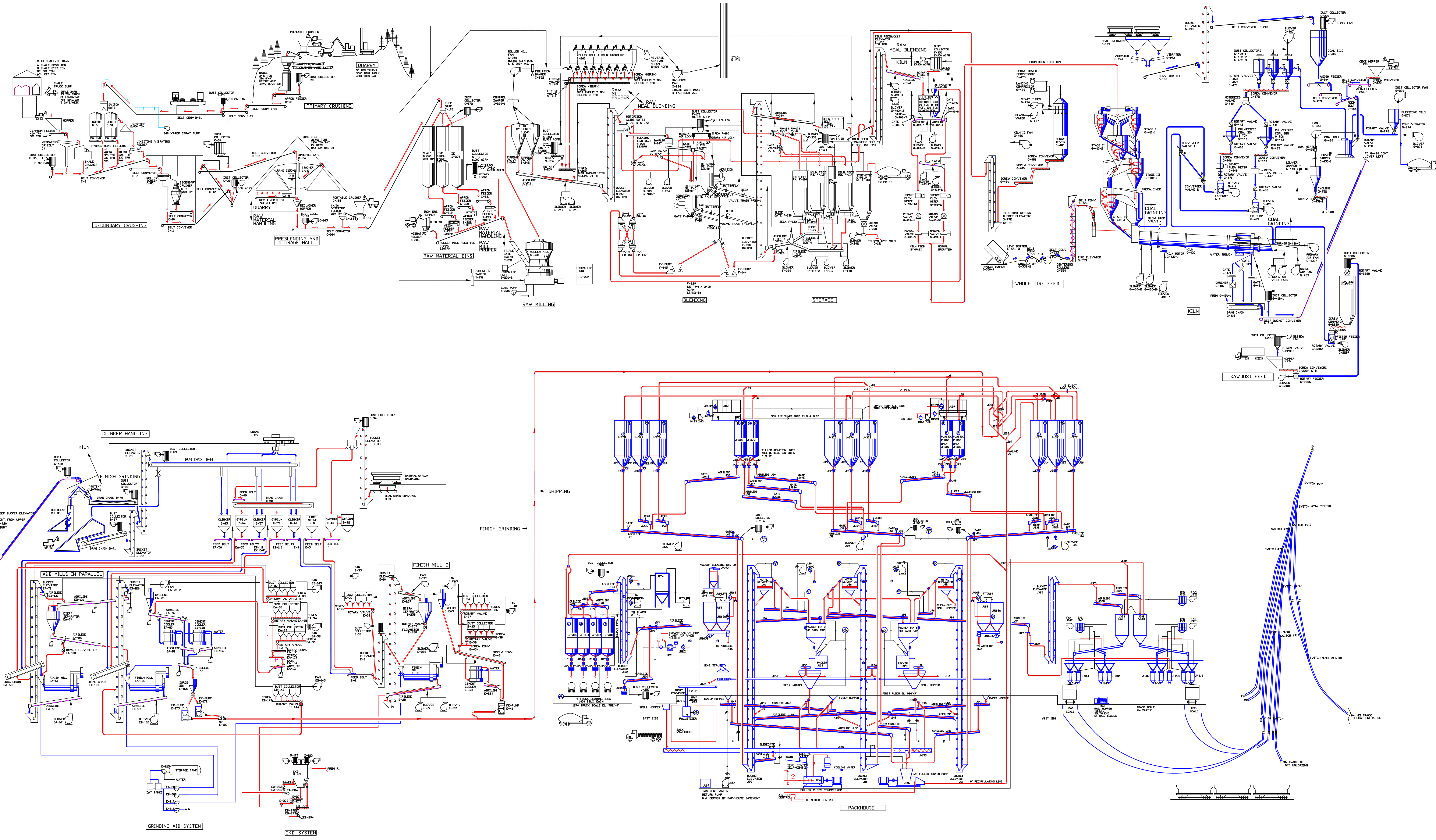
## 3.0 QA SPECIFICATIONS AND PROCESS DIAGRAM

### 3-1 QA/QC Specifications

| Parameter       | Method  | QA/QC Specification    | Acceptance Criteria   | Actual Result           |
|-----------------|---|------------------------|---|-------------------------|
| HCN             | 320   | Method Detection Limit | 0.5 ppm   | 0.1 ppmvw               |
|                 |   | SNR                    | >2500 at 64 scans   | 6951 (Run 1 Average)    |
|                 |   | S Beam                 | >0.9  | 1.314 (Run 1 Average)   |
|                 |   | Direct HCN Analysis    | ±5% of tag value  | 1.6%                    |
|                 |   | Dynamic Spike Analysis | ≤10% of total sample volume   | 7.6%                    |
|                 |   |                        | Spike gas ~twice native concentration or 3-4 ppm addition to native concentration | +3.5 ppm                |
|                 |   |                        | ≤±20% of expected value or ≤±0.5 ppm, whichever is less restrictive               | <20%                    |
| Residuals       | ≤±0.3 ppm, or ≤±5% of measured value, whichever is less restrictive | 0.2 ppmvw              |   |                         |
| Cl <sub>2</sub> | 26A   | Detection Limit        | 300 µg  | 150 µg                  |
|                 |   | Paired Train Agreement | ≤10% Relative Deviation or ≤0.2 ppm, whichever is less restrictive.               | ≤10% Relative Deviation |

### 3-2 Process Description and Process Flow Diagram

The facility is located at 15390 Wonderland Blvd. in Redding, California. Limestone, shale, and other rawmaterials are sent from the quarry to be crushed into smaller pieces for processing. The raw material is milled then sent through the preheater tower in preparation of the rotary kiln. In the kiln, coal, coke, and other fuels are added for combustion; natural gas is used for startup heat. The milled blend is exposed to extreme temperatures in the kiln, transforming into a mineral compound called clinker. Clinker is sent to the contiguous satellite cooler tubes to quench before finish milling. With the addition of gypsum, finish mills grind clinker into Portland cement. Product is stored and then shipped from the facility.



PLOT DATE  
7-26-22

Project No. M234605A  
Main KILN Stack

|     |          |      |    |       |      |    |
|-----|----------|------|----|-------|------|----|
| NO. | REVISION | DATE | BY | SCALE | DATE | BY |
| 3   |          |      |    |       |      |    |
| 2   |          |      |    |       |      |    |

DRAWN: K SMITH  
CHK: CJK  
APPV: SCALENONE



REDDING  
PLANT FLOW DIAGRAM  
SHEET 1 OF 1  
15390 WONDERLAND BLVD  
REDDING CA 96001  
100-F-101 R1  
REV. 1

## 4.0 TEST PROCEDURES

All testing, sampling, analytical, and calibration procedures used for this test program were performed as described in the Title 40, *Code of Federal Regulations*, Part 60, Appendix A (40CFR60), Methods 1, 2, 3A, 4, 26A, and 40CFR63, Appendix A, Method 320; and the latest revisions thereof. Where applicable, the *Quality Assurance Handbook for Air Pollution Measurement Systems*, Volume III, Stationary Source Specific Methods, United States Environmental Protection Agency (USEPA) 600/R-94/038c, September 1994 was used to supplement procedures in addition to the appended "Draft General Test Plan".

### 4.1 Method 1 Sample and Velocity Traverse Determination

Sample points for testing are determined using USEPA Test Method 1, 40CFR60, Appendix A. The characteristics of the measurement location is summarized below.

#### Sample Point Selection

| Test Location | Stack Diameter | Upstream Diameters | Downstream Diameters | Test Parameter                  | Number of Sampling Points |
|---------------|----------------|--------------------|----------------------|---------------------------------|---------------------------|
| Main Kiln     | 7.0 Feet       | 16.0               | 11.0                 | HF/Cl <sub>2</sub> (26A)        | 12                        |
|               |                |                    |                      | O <sub>2</sub> (3A)             | 3 (stratification)        |
|               |                |                    |                      | HCN/HF/CO <sub>2</sub> (320/3A) | 1                         |

A cyclonic flow check was performed in accordance with Section 11.4, which demonstrated it meets the criteria of an average value of less than 20° and therefore is considered to be a suitable testing location for flow rate measurements.

### 4.2 Method 2 Volumetric Flow Rate Determination

The gas velocity and volumetric flowrate were determined using Method 2, 40CFR60, Appendix A, as an integrated part of the HF/Cl<sub>2</sub> sampling system.

Velocity pressures were determined by traversing the duct with wind tunnel calibrated S-type pitot tube. Temperatures were measured using K-type thermocouples with calibrated digital temperature indicators. The molecular weight and moisture content of the gases were also determined to permit the calculation of the volumetric flowrate.

### 4.3 Method 3A Oxygen (O<sub>2</sub>) and Carbon Dioxide (CO<sub>2</sub>) Determination

O<sub>2</sub> and CO<sub>2</sub> concentrations were determined in accordance with Method 3A, 40CFR60, Appendix A and Method 320, 40CFR63, Appendix A, respectively. A Servomex analyzer was used to determine O<sub>2</sub> concentrations while the MKS 2030 analyzer was used to determine CO<sub>2</sub> concentrations. The O<sub>2</sub> instrument has a paramagnetic detector and operates in a nominal range of 0-25%.

A list of calibration gases used and the results of all calibration and other required quality assurance checks are found in the appendix of this report. Copies of calibration gas certifications are also appended.

#### **4.4 Method 26A Hydrogen Fluoride (HF) and Chlorine (Cl<sub>2</sub>) Determination**

HF and Cl<sub>2</sub> concentrations and emission rates were determined in accordance with Method 26A, 40CFR60, Appendix A. Paired sampling trains were used to collect the samples. A total of twelve (12) test points were sampled per run on the kiln stack. The sample was extracted isokinetically from the gas stream and passed through dilute sulfuric acid (0.1N H<sub>2</sub>SO<sub>4</sub>). HF was collected in the dilute acid. Cl<sub>2</sub> was collected in the dilute sodium hydroxide (0.1N NaOH) solution. The sample train consisted of a Teflon coated nozzle, a heated borosilicate glass probe liner, a Teflon® filter placed on the outlet of the glass probe liner, and six impingers. The first two impingers contained the 0.1N H<sub>2</sub>SO<sub>4</sub>, the third remained empty (and was recovered with the first two impingers), the fourth and fifth impingers contained the 0.1N NaOH, while the sixth impinger contained silica gel to absorb any remaining moisture. A de-ionized water rinse was performed on each set of impingers, and samples were stored in Nalgene sample containers for transport. The 0.1N H<sub>2</sub>SO<sub>4</sub> impinger catch samples were analyzed for HF while the 0.1N NaOH impinger catch samples were analyzed for Cl<sub>2</sub>. A method detection limit (MDL) of 150 µg was determined for both HF and Cl<sub>2</sub> using the "Definition and Procedure for the Determination of the Method Detection Limit, Revision 2". All equipment used was calibrated in accordance with the specifications of the method. Calibration data is appended.

Hand recorded field data sheets were reviewed and scans are retained on the Mostardi Platt network. Copies of this data is available upon request.

#### **4.5 Method 320 Speciated Flue Gas Concentration Determinations**

The sampling procedures for HCN and HF were performed in accordance with USEPA Method 320, 40CFR63, Appendix A. Data was continuously recorded with a data logging system throughout sampling, with brief interruption to properly label reference spectra.

The average gas effluent concentrations were determined from the average gas concentration displayed by the MKS 2030 analyzer. The Method 320 sampling system vaporizes water droplets similar to Method 26A. The difference is that Method 320 is an extractive method that calculates concentration based on compounds continuously flowing through the FTIR gas cell where the Method 26A captures water vapor in an impinger train. Calculating Method 320 concentrations on a dry basis uses the water vapor contained in the FTIR gas cell. In order to calculate lb/hr, the dry FTIR concentration is used in combination with the dry stack gas volumetric flow rate.

All sampling system components were heated to 375°F +/- 25°F, including: stainless steel sample probe, stainless steel calibration tee, in line glass fiber particulate filter, Teflon® sample line, heated head sample pump, and FTIR detector cell. The sample pump distributes the gas sample to the instrument at a steady sample flow rate (+/- 10%). All components of the sampling system are constructed of stainless steel, glass, or Teflon®.

FTIR technology works on the principle that most gases absorb infrared light. This is true for all compounds except for homonuclear diatomic molecules and noble gases such as: N<sub>2</sub>, O<sub>2</sub>, H<sub>2</sub>, He, Ne, and Ar. Vibrations, stretches, bends, and rotations within the bonds of a molecule determine the infrared absorption distinctiveness. The absorption creates a "fingerprint" which is

unique for each given compound. The quantity of infrared light absorbed is proportional to the gas concentration. Most compounds have absorbencies at different infrared frequencies, thus allowing the simultaneous analysis of multiple compounds at one time. The FTIR software compares each sample spectrum to a user-selected list of calibration references and concentration data is generated.

FTIR data was collected using an MKS MultiGas 2030 FTIR spectrometer. Data was generated at  $0.5 \text{ cm}^{-1}$ . Each Spectra was derived from the coaddition of 62-64 scans with a new data point generated approximately every minute. HCN analyte spiking assured the ability of the FTIR to quantify HCN in the presence of effluent gas. All analyte spikes were introduced using an instrument grade stainless steel rotameter. All QA/QC procedures were within the acceptance criteria allowance of the applicable methodology and the "General Test Plan."

## 5.0 TEST RESULTS SUMMARIES

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Test Method:** 26A Combined

| Source Condition                              | Mill On  | Mill On  | Mill On  |          |
|---|----------|----------|----------|----------|
| Date  | 11/14/23 | 11/14/23 | 11/14/23 |          |
| Start Time                                    | 8:00     | 9:25     | 10:50    |          |
| End Time                                      | 9:05     | 10:29    | 11:55    |          |
|   | Run 1    | Run 2    | Run 3    | Average  |
| <b>Stack Conditions</b>                       |          |          |          |          |
| Average Gas Velocity, ft/sec                  | 87.514   | 87.232   | 86.414   | 87.053   |
| Gas Volumetric Flow Rate, acfm                | 202,076  | 201,424  | 199,535  | 201,011  |
| Gas Volumetric Flow Rate, dscfm               | 133,876  | 133,465  | 132,493  | 133,278  |
| Gas Volumetric Flow Rate, scfm                | 150,470  | 150,211  | 148,848  | 149,843  |
| Average %CO <sub>2</sub> by volume, dry basis | 13.4     | 13.7     | 13.8     | 13.6     |
| Average %O <sub>2</sub> by volume, dry basis  | 12.7     | 12.5     | 12.5     | 12.6     |
| Clinker production, ton/hr                    | 77.2     | 77.2     | 78.3     | 77.6     |
| <b>Chloride (Cl<sub>2</sub>) Emissions</b>    |          |          |          |          |
| ppm   | ≤ 0.03   | ≤ 0.03   | ≤ 0.03   | ≤ 0.03   |
| ppm@7%O <sub>2</sub>                          | ≤ 0.04   | ≤ 0.04   | ≤ 0.04   | ≤ 0.04   |
| lb/hr   | ≤ 0.04   | ≤ 0.04   | ≤ 0.04   | ≤ 0.04   |
| lb/ton of clinker                             | ≤ 0.0005 | ≤ 0.0005 | ≤ 0.0005 | ≤ 0.0005 |
| <b>Hydrogen Fluoride (HF) Emissions</b>       |          |          |          |          |
| ppm   | ≤ 0.09   | ≤ 0.09   | ≤ 0.09   | ≤ 0.09   |
| ppm@7%O <sub>2</sub>                          | ≤ 0.15   | ≤ 0.15   | ≤ 0.15   | ≤ 0.15   |
| lb/hr   | ≤ 0.04   | ≤ 0.04   | ≤ 0.04   | ≤ 0.04   |
| lb/ton of clinker                             | ≤ 0.0005 | ≤ 0.0005 | ≤ 0.0005 | ≤ 0.0005 |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Test Method: 26A

|   | Source Condition<br>Date | Mill On<br>11/14/23 | Mill On<br>11/14/23 | Mill On<br>11/14/23 |         |        |   |        |
|---|--------------------------|---------------------|---------------------|---------------------|---------|--------|---|--------|
|   | Start Time               | 8:00                | 9:25                | 10:50               |         |        |   |        |
|   | End Time                 | 9:05                | 10:29               | 11:55               |         |        |   |        |
|   |                          | Run 1A              | Run 2A              | Run 3A              | Average |        |   |        |
| <b>Stack Conditions</b>                       |                          |                     |                     |                     |         |        |   |        |
| Average Gas Temperature, °F                   |                          | 231.4               | 230.2               | 229.7               | 230.4   |        |   |        |
| Flue Gas Moisture, percent by volume          |                          | 11.0%               | 11.4%               | 11.1%               | 11.2%   |        |   |        |
| Average Flue Pressure, in. Hg                 |                          | 29.17               | 29.17               | 29.17               | 29.17   |        |   |        |
| Gas Sample Volume, dscf                       |                          | 71.022              | 70.778              | 70.239              | 70.680  |        |   |        |
| Average Gas Velocity, ft/sec                  |                          | 87.486              | 87.073              | 86.208              | 86.922  |        |   |        |
| Gas Volumetric Flow Rate, acfm                |                          | 202,011             | 201,058             | 199,061             | 200,710 |        |   |        |
| Gas Volumetric Flow Rate, dscfm               |                          | 133,928             | 132,811             | 132,060             | 132,933 |        |   |        |
| Gas Volumetric Flow Rate, scfm                |                          | 150,404             | 149,966             | 148,584             | 149,651 |        |   |        |
| Average %CO <sub>2</sub> by volume, dry basis |                          | 13.4                | 13.7                | 13.8                | 13.6    |        |   |        |
| Average %O <sub>2</sub> by volume, dry basis  |                          | 12.7                | 12.5                | 12.5                | 12.6    |        |   |        |
| Isokinetic Variance                           |                          | 102.3               | 102.8               | 102.6               | 102.6   |        |   |        |
| <b>Chloride (Cl<sub>2</sub>) Emissions</b>    |                          |                     |                     |                     |         |        |   |        |
| ug of sample collected                        | ≤                        | 150.00              | ≤                   | 150.00              | ≤       | 150.00 | ≤ | 150.00 |
| ppm   | ≤                        | 0.03                | ≤                   | 0.03                | ≤       | 0.03   | ≤ | 0.03   |
| <b>Hydrogen Fluoride (HF) Emissions</b>       |                          |                     |                     |                     |         |        |   |        |
| ug of sample collected                        | ≤                        | 150.00              | ≤                   | 150.00              | ≤       | 150.00 | ≤ | 150.00 |
| ppm   | ≤                        | 0.09                | ≤                   | 0.09                | ≤       | 0.09   | ≤ | 0.09   |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Test Method: 26A

| Source Condition                              | Mill On  | Mill On  | Mill On  |          |
|---|----------|----------|----------|----------|
| Date  | 11/14/23 | 11/14/23 | 11/14/23 |          |
| Start Time                                    | 8:00     | 9:25     | 10:50    |          |
| End Time                                      | 9:05     | 10:29    | 11:55    |          |
|   | Run 1B   | Run 2B   | Run 3B   | Average  |
| <b>Stack Conditions</b>                       |          |          |          |          |
| Average Gas Temperature, °F                   | 231.3    | 230.4    | 230.5    | 230.7    |
| Flue Gas Moisture, percent by volume          | 11.1%    | 10.9%    | 10.9%    | 11.0%    |
| Average Flue Pressure, in. Hg                 | 29.17    | 29.17    | 29.17    | 29.17    |
| Gas Sample Volume, dscf                       | 73.356   | 73.501   | 72.840   | 73.232   |
| Average Gas Velocity, ft/sec                  | 87.542   | 87.390   | 86.619   | 87.184   |
| Gas Volumetric Flow Rate, acfm                | 202,140  | 201,789  | 200,009  | 201,313  |
| Gas Volumetric Flow Rate, dscfm               | 133,824  | 134,118  | 132,926  | 133,623  |
| Gas Volumetric Flow Rate, scfm                | 150,536  | 150,456  | 149,111  | 150,034  |
| Average %CO <sub>2</sub> by volume, dry basis | 13.4     | 13.7     | 13.8     | 13.6     |
| Average %O <sub>2</sub> by volume, dry basis  | 12.7     | 12.5     | 12.5     | 12.6     |
| Isokinetic Variance                           | 102.4    | 102.4    | 102.3    | 102.4    |
| <b>Chloride (Cl<sub>2</sub>) Emissions</b>    |          |          |          |          |
| ug of sample collected                        | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 |
| ppm   | ≤ 0.02   | ≤ 0.02   | ≤ 0.03   | ≤ 0.02   |
| <b>Hydrogen Fluoride (HF) Emissions</b>       |          |          |          |          |
| ug of sample collected                        | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 |
| ppm   | ≤ 0.09   | ≤ 0.09   | ≤ 0.09   | ≤ 0.09   |

**CalPortland Company, Inc.**  
**Redding Cement Plant**  
**Main Kiln Stack**  
**Reference Method Test Data**  
**Mill On**

| Test No.       | Date       | Start Time | End Time | O2 % (dry)  | Moisture %   | HCN ppmvw   | HCN ppmvd @ 7% O2 | HF ppmvw      | HF ppmvd @ 7% O2 |
|----------------|------------|------------|----------|-------------|--------------|-------------|-------------------|---------------|------------------|
| 1              | 11/14/2023 | 8:00       | 8:59     | 12.7        | 11.7%        | 0.76        | 1.45              | ≤ 0.10        | ≤ 0.19           |
| 2              | 11/14/2023 | 9:25       | 10:24    | 12.5        | 11.5%        | 0.78        | 1.46              | ≤ 0.10        | ≤ 0.19           |
| 3              | 11/14/2023 | 10:50      | 11:49    | 12.5        | 11.5%        | 0.80        | 1.49              | ≤ 0.10        | ≤ 0.19           |
| <b>Average</b> |            |            |          | <b>12.5</b> | <b>11.6%</b> | <b>0.78</b> | <b>1.47</b>       | <b>≤ 0.10</b> | <b>≤ 0.19</b>    |

| Test No.       | Date       | Start Time | End Time | Volumetric Flow, DSCFM | Clinker Production, ton/hr | HCN lb/hr   | HCN lb/ton    | HF lb/hr      | HF lb/ton       |
|----------------|------------|------------|----------|------------------------|----------------------------|-------------|---------------|---------------|-----------------|
| 1              | 11/14/2023 | 8:00       | 8:59     | 133,876                | 77.2                       | 0.49        | 0.0063        | ≤ 0.05        | ≤ 0.0006        |
| 2              | 11/14/2023 | 9:25       | 10:24    | 133,465                | 77.2                       | 0.50        | 0.0064        | ≤ 0.05        | ≤ 0.0006        |
| 3              | 11/14/2023 | 10:50      | 11:49    | 132,493                | 78.3                       | 0.50        | 0.0064        | ≤ 0.05        | ≤ 0.0006        |
| <b>Average</b> |            |            |          | <b>133,278</b>         | <b>77.6</b>                | <b>0.49</b> | <b>0.0064</b> | <b>≤ 0.05</b> | <b>≤ 0.0006</b> |

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Test Method:** 26A Combined

|   | Source Condition | Mill Off | Mill Off | Mill Off |         |        |
|---|------------------|----------|----------|----------|---------|--------|
|   | Date             | 11/14/23 | 11/14/23 | 11/14/23 |         |        |
|   | Start Time       | 12:50    | 14:15    | 15:40    |         |        |
|   | End Time         | 13:55    | 15:19    | 16:44    |         |        |
|   |                  | Run 1    | Run 2    | Run 3    | Average |        |
| <b>Stack Conditions</b>                       |                  |          |          |          |         |        |
| Average Gas Velocity, ft/sec                  |                  | 85.762   | 86.028   | 84.657   | 85.482  |        |
| Gas Volumetric Flow Rate, acfm                |                  | 198,029  | 198,644  | 195,479  | 197,384 |        |
| Gas Volumetric Flow Rate, dscfm               |                  | 122,230  | 121,094  | 119,754  | 121,026 |        |
| Gas Volumetric Flow Rate, scfm                |                  | 137,807  | 136,316  | 134,967  | 136,363 |        |
| Average %CO <sub>2</sub> by volume, dry basis |                  | 16.2     | 16.2     | 16.1     | 16.2    |        |
| Average %O <sub>2</sub> by volume, dry basis  |                  | 11.2     | 11.2     | 11.3     | 11.2    |        |
| Clinker production, ton/hr                    |                  | 78.3     | 78.3     | 78.3     | 78.3    |        |
| <b>Chloride (Cl<sub>2</sub>) Emissions</b>    |                  |          |          |          |         |        |
| ppm   | ≤                | 0.03     | ≤        | 0.03     | ≤       | 0.03   |
| ppm@7%O <sub>2</sub>                          | ≤                | 0.04     | ≤        | 0.04     | ≤       | 0.04   |
| lb/hr   | ≤                | 0.04     | ≤        | 0.04     | ≤       | 0.04   |
| lb/ton of clinker                             | ≤                | 0.0005   | ≤        | 0.0005   | ≤       | 0.0005 |
| <b>Hydrogen Fluoride (HF) Emissions</b>       |                  |          |          |          |         |        |
| ppm   | ≤                | 0.10     | ≤        | 0.10     | ≤       | 0.10   |
| ppm@7%O <sub>2</sub>                          | ≤                | 0.14     | ≤        | 0.14     | ≤       | 0.14   |
| lb/hr   | ≤                | 0.04     | ≤        | 0.04     | ≤       | 0.04   |
| lb/ton of clinker                             | ≤                | 0.0005   | ≤        | 0.0005   | ≤       | 0.0005 |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Test Method: 26A

|   | Source Condition | Mill Off | Mill Off | Mill Off |  |
|---|------------------|----------|----------|----------|--|
|   | Date             | 11/14/23 | 11/14/23 | 11/14/23 |  |
|   | Start Time       | 12:50    | 14:15    | 15:40    |  |
|   | End Time         | 13:55    | 15:19    | 16:44    |  |
|   | Run 1A           | Run 2A   | Run 3A   | Average  |  |
| <b>Stack Conditions</b>                       |                  |          |          |          |  |
| Average Gas Temperature, °F                   | 279.5            | 291.3    | 285.4    | 285.4    |  |
| Flue Gas Moisture, percent by volume          | 11.4%            | 10.9%    | 11.0%    | 11.1%    |  |
| Average Flue Pressure, in. Hg                 | 29.17            | 29.17    | 29.17    | 29.17    |  |
| Gas Sample Volume, dscf                       | 65.240           | 64.262   | 63.758   | 64.420   |  |
| Average Gas Velocity, ft/sec                  | 85.662           | 85.633   | 84.289   | 85.195   |  |
| Gas Volumetric Flow Rate, acfm                | 197,799          | 197,734  | 194,630  | 196,721  |  |
| Gas Volumetric Flow Rate, dscfm               | 121,966          | 120,665  | 119,595  | 120,742  |  |
| Gas Volumetric Flow Rate, scfm                | 137,693          | 135,479  | 134,411  | 135,861  |  |
| Average %CO <sub>2</sub> by volume, dry basis | 16.2             | 16.2     | 16.1     | 16.2     |  |
| Average %O <sub>2</sub> by volume, dry basis  | 11.2             | 11.2     | 11.3     | 11.2     |  |
| Isokinetic Variance                           | 103.2            | 102.7    | 102.8    | 102.9    |  |
| <b>Chloride (Cl<sub>2</sub>) Emissions</b>    |                  |          |          |          |  |
| ug of sample collected                        | ≤ 150.00         | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 |  |
| ppm   | ≤ 0.03           | ≤ 0.03   | ≤ 0.03   | ≤ 0.03   |  |
| <b>Hydrogen Fluoride (HF) Emissions</b>       |                  |          |          |          |  |
| ug of sample collected                        | ≤ 150.00         | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 |  |
| ppm   | ≤ 0.10           | ≤ 0.10   | ≤ 0.10   | ≤ 0.10   |  |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Test Method: 26A

|   | Source Condition | Mill Off | Mill Off | Mill Off |  |
|---|------------------|----------|----------|----------|--|
|   | Date             | 11/14/23 | 11/14/23 | 11/14/23 |  |
|   | Start Time       | 12:50    | 14:15    | 15:40    |  |
|   | End Time         | 13:55    | 15:19    | 16:44    |  |
|   | Run 1B           | Run 2B   | Run 3B   | Average  |  |
| <b>Stack Conditions</b>                       |                  |          |          |          |  |
| Average Gas Temperature, °F                   | 280.0            | 289.0    | 285.8    | 284.9    |  |
| Flue Gas Moisture, percent by volume          | 11.2%            | 11.4%    | 11.5%    | 11.4%    |  |
| Average Flue Pressure, in. Hg                 | 29.17            | 29.17    | 29.17    | 29.17    |  |
| Gas Sample Volume, dscf                       | 67.577           | 67.305   | 66.317   | 67.066   |  |
| Average Gas Velocity, ft/sec                  | 85.861           | 86.422   | 85.024   | 85.769   |  |
| Gas Volumetric Flow Rate, acfm                | 198,259          | 199,554  | 196,327  | 198,047  |  |
| Gas Volumetric Flow Rate, dscfm               | 122,493          | 121,522  | 119,912  | 121,309  |  |
| Gas Volumetric Flow Rate, scfm                | 137,920          | 137,152  | 135,523  | 136,865  |  |
| Average %CO <sub>2</sub> by volume, dry basis | 16.2             | 16.2     | 16.1     | 16.2     |  |
| Average %O <sub>2</sub> by volume, dry basis  | 11.2             | 11.2     | 11.3     | 11.2     |  |
| Isokinetic Variance                           | 103.0            | 103.4    | 103.3    | 103.2    |  |
| <b>Chloride (Cl<sub>2</sub>) Emissions</b>    |                  |          |          |          |  |
| ug of sample collected                        | ≤ 150.00         | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 |  |
| ppm   | ≤ 0.03           | ≤ 0.03   | ≤ 0.03   | ≤ 0.03   |  |
| <b>Hydrogen Fluoride (HF) Emissions</b>       |                  |          |          |          |  |
| ug of sample collected                        | ≤ 150.00         | ≤ 150.00 | ≤ 150.00 | ≤ 150.00 |  |
| ppm   | ≤ 0.09           | ≤ 0.10   | ≤ 0.10   | ≤ 0.10   |  |

CalPortland Company, Inc.  
 Redding Cement Plant  
 Main Kiln Stack  
 Reference Method Test Data  
 Mill Off

| Test No.       | Date       | Start Time | End Time | O2 % (dry)  | Moisture %   | HCN ppmvw   | HCN ppmvd @ 7% O2 | HF ppmvw      | HF ppmvd @ 7% O2 |
|----------------|------------|------------|----------|-------------|--------------|-------------|-------------------|---------------|------------------|
| 1              | 11/14/2023 | 12:50      | 13:49    | 11.2        | 12.2%        | 0.83        | 1.34              | ≤ 0.10        | ≤ 0.16           |
| 2              | 11/14/2023 | 14:15      | 15:14    | 11.2        | 12.4%        | 0.89        | 1.45              | ≤ 0.10        | ≤ 0.16           |
| 3              | 11/14/2023 | 15:40      | 16:39    | 11.3        | 12.0%        | 1.01        | 1.67              | ≤ 0.10        | ≤ 0.17           |
| <b>Average</b> |            |            |          | <b>11.2</b> | <b>12.2%</b> | <b>0.91</b> | <b>1.49</b>       | <b>≤ 0.10</b> | <b>≤ 0.16</b>    |

| Test No.       | Date       | Start Time | End Time | Volumetric Flow, DSCFM | Clinker Production, ton/hr | HCN lb/hr   | HCN lb/ton    | HF lb/hr      | HF lb/ton       |
|----------------|------------|------------|----------|------------------------|----------------------------|-------------|---------------|---------------|-----------------|
| 1              | 11/14/2023 | 12:50      | 13:49    | 122,230                | 78.3                       | 0.48        | 0.0062        | ≤ 0.04        | ≤ 0.0006        |
| 2              | 11/14/2023 | 14:15      | 15:14    | 121,094                | 78.3                       | 0.52        | 0.0066        | ≤ 0.04        | ≤ 0.0006        |
| 3              | 11/14/2023 | 15:40      | 16:39    | 119,754                | 78.3                       | 0.58        | 0.0074        | ≤ 0.04        | ≤ 0.0005        |
| <b>Average</b> |            |            |          | <b>121,026</b>         | <b>78.3</b>                | <b>0.53</b> | <b>0.0067</b> | <b>≤ 0.04</b> | <b>≤ 0.0006</b> |

## 6.0 CERTIFICATION

Mostardi Platt is pleased to have been of service to CalPortland Company, Inc. If you have any questions regarding this test report, please do not hesitate to contact us at 630-993-2100.

As project manager, I hereby certify that this test report represents a true and accurate summary of emissions test results and the methodologies employed to obtain those results, and the test program was performed in accordance with the methods specified in this test report.

MOSTARDI PLATT



Richard J. Sollars II

Project Manager



Chet A. Gutwein

Quality Assurance

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## APPENDICES

## Appendix A – Plant Operating Data

| Date/Time        | KILN:<br>CLINKER_PROD<br>(TNHR)<br>1-Minute Block<br>Average<br>Expression<br>Value |
|------------------|---|
| 11/14/2023 08:00 | 77.20   |
| 11/14/2023 08:01 | 77.20   |
| 11/14/2023 08:02 | 77.20   |
| 11/14/2023 08:03 | 77.20   |
| 11/14/2023 08:04 | 77.20   |
| 11/14/2023 08:05 | 77.20   |
| 11/14/2023 08:06 | 77.20   |
| 11/14/2023 08:07 | 77.20   |
| 11/14/2023 08:08 | 77.20   |
| 11/14/2023 08:09 | 77.20   |
| 11/14/2023 08:10 | 77.20   |
| 11/14/2023 08:11 | 77.20   |
| 11/14/2023 08:12 | 77.20   |
| 11/14/2023 08:13 | 77.20   |
| 11/14/2023 08:14 | 77.20   |
| 11/14/2023 08:15 | 77.20   |
| 11/14/2023 08:16 | 77.14   |
| 11/14/2023 08:17 | 77.20   |
| 11/14/2023 08:18 | 77.20   |
| 11/14/2023 08:19 | 77.20   |
| 11/14/2023 08:20 | 77.20   |
| 11/14/2023 08:21 | 77.20   |
| 11/14/2023 08:22 | 77.20   |
| 11/14/2023 08:23 | 77.20   |
| 11/14/2023 08:24 | 77.20   |
| 11/14/2023 08:25 | 77.20   |
| 11/14/2023 08:26 | 77.20   |
| 11/14/2023 08:27 | 77.14   |
| 11/14/2023 08:28 | 77.20   |
| 11/14/2023 08:29 | 77.20   |
| 11/14/2023 08:30 | 77.20   |
| 11/14/2023 08:31 | 77.20   |
| 11/14/2023 08:32 | 77.20   |
| 11/14/2023 08:33 | 77.20   |
| 11/14/2023 08:34 | 77.20   |
| 11/14/2023 08:35 | 77.20   |
| 11/14/2023 08:36 | 77.20   |
| 11/14/2023 08:37 | 77.20   |
| 11/14/2023 08:38 | 77.20   |
| 11/14/2023 08:39 | 77.20   |
| 11/14/2023 08:40 | 77.20   |
| 11/14/2023 08:41 | 77.20   |
| 11/14/2023 08:42 | 77.20   |
| 11/14/2023 08:43 | 77.20   |
| 11/14/2023 08:44 | 77.20   |
| 11/14/2023 08:45 | 77.20   |
| 11/14/2023 08:46 | 77.20   |
| 11/14/2023 08:47 | 77.20   |
| 11/14/2023 08:48 | 77.20   |
| 11/14/2023 08:49 | 77.20   |
| 11/14/2023 08:50 | 77.20   |
| 11/14/2023 08:51 | 77.20   |
| 11/14/2023 08:52 | 77.20   |
| 11/14/2023 08:53 | 77.20   |
| 11/14/2023 08:54 | 77.20   |
| 11/14/2023 08:55 | 77.20   |
| 11/14/2023 08:56 | 77.20   |
| 11/14/2023 08:57 | 77.20   |
| 11/14/2023 08:58 | 77.20   |
| 11/14/2023 08:59 | 77.20   |
| Average          | 77.20   |

| Date/Time        | KILN:<br>CLINKER_PROD<br>(TNHR)<br>1-Minute Block<br>Average<br>Expression<br>Value |
|------------------|---|
| 11/14/2023 09:25 | 77.20   |
| 11/14/2023 09:26 | 77.20   |
| 11/14/2023 09:27 | 77.20   |
| 11/14/2023 09:28 | 77.20   |
| 11/14/2023 09:29 | 77.14   |
| 11/14/2023 09:30 | 77.20   |
| 11/14/2023 09:31 | 77.20   |
| 11/14/2023 09:32 | 77.20   |
| 11/14/2023 09:33 | 77.20   |
| 11/14/2023 09:34 | 77.20   |
| 11/14/2023 09:35 | 77.20   |
| 11/14/2023 09:36 | 77.20   |
| 11/14/2023 09:37 | 77.20   |
| 11/14/2023 09:38 | 77.20   |
| 11/14/2023 09:39 | 77.20   |
| 11/14/2023 09:40 | 77.14   |
| 11/14/2023 09:41 | 77.20   |
| 11/14/2023 09:42 | 77.20   |
| 11/14/2023 09:43 | 77.20   |
| 11/14/2023 09:44 | 77.20   |
| 11/14/2023 09:45 | 77.20   |
| 11/14/2023 09:46 | 77.20   |
| 11/14/2023 09:47 | 77.20   |
| 11/14/2023 09:48 | 77.20   |
| 11/14/2023 09:49 | 77.20   |
| 11/14/2023 09:50 | 77.20   |
| 11/14/2023 09:51 | 77.20   |
| 11/14/2023 09:52 | 77.20   |
| 11/14/2023 09:53 | 77.20   |
| 11/14/2023 09:54 | 77.20   |
| 11/14/2023 09:55 | 77.20   |
| 11/14/2023 09:56 | 77.20   |
| 11/14/2023 09:57 | 77.20   |
| 11/14/2023 09:58 | 77.20   |
| 11/14/2023 09:59 | 77.20   |
| 11/14/2023 10:00 | 77.20   |
| 11/14/2023 10:01 | 77.20   |
| 11/14/2023 10:02 | 77.20   |
| 11/14/2023 10:03 | 77.20   |
| 11/14/2023 10:04 | 77.20   |
| 11/14/2023 10:05 | 77.20   |
| 11/14/2023 10:06 | 77.20   |
| 11/14/2023 10:07 | 77.20   |
| 11/14/2023 10:08 | 77.20   |
| 11/14/2023 10:09 | 77.20   |
| 11/14/2023 10:10 | 77.20   |
| 11/14/2023 10:11 | 77.20   |
| 11/14/2023 10:12 | 77.20   |
| 11/14/2023 10:13 | 77.20   |
| 11/14/2023 10:14 | 77.20   |
| 11/14/2023 10:15 | 77.20   |
| 11/14/2023 10:16 | 77.20   |
| 11/14/2023 10:17 | 77.20   |
| 11/14/2023 10:18 | 77.20   |
| 11/14/2023 10:19 | 77.20   |
| 11/14/2023 10:20 | 77.20   |
| 11/14/2023 10:21 | 77.20   |
| 11/14/2023 10:22 | 77.14   |
| 11/14/2023 10:23 | 77.20   |
| 11/14/2023 10:24 | 77.37   |
| Average          | 77.20   |

| Date/Time        | KILN:<br>CLINKER_PROD<br>(TNHR)<br>1-Minute Block<br>Average<br>Expression<br>Value |
|------------------|---|
| 11/14/2023 10:50 | 78.32   |
| 11/14/2023 10:51 | 78.32   |
| 11/14/2023 10:52 | 78.32   |
| 11/14/2023 10:53 | 78.38   |
| 11/14/2023 10:54 | 78.32   |
| 11/14/2023 10:55 | 78.32   |
| 11/14/2023 10:56 | 78.32   |
| 11/14/2023 10:57 | 78.32   |
| 11/14/2023 10:58 | 78.32   |
| 11/14/2023 10:59 | 78.32   |
| 11/14/2023 11:00 | 78.32   |
| 11/14/2023 11:01 | 78.32   |
| 11/14/2023 11:02 | 78.32   |
| 11/14/2023 11:03 | 78.32   |
| 11/14/2023 11:04 | 78.32   |
| 11/14/2023 11:05 | 78.32   |
| 11/14/2023 11:06 | 78.32   |
| 11/14/2023 11:07 | 78.32   |
| 11/14/2023 11:08 | 78.32   |
| 11/14/2023 11:09 | 78.32   |
| 11/14/2023 11:10 | 78.32   |
| 11/14/2023 11:11 | 78.32   |
| 11/14/2023 11:12 | 78.38   |
| 11/14/2023 11:13 | 78.32   |
| 11/14/2023 11:14 | 78.32   |
| 11/14/2023 11:15 | 78.38   |
| 11/14/2023 11:16 | 78.32   |
| 11/14/2023 11:17 | 78.32   |
| 11/14/2023 11:18 | 78.32   |
| 11/14/2023 11:19 | 78.32   |
| 11/14/2023 11:20 | 78.32   |
| 11/14/2023 11:21 | 78.32   |
| 11/14/2023 11:22 | 78.32   |
| 11/14/2023 11:23 | 78.32   |
| 11/14/2023 11:24 | 78.32   |
| 11/14/2023 11:25 | 78.32   |
| 11/14/2023 11:26 | 78.32   |
| 11/14/2023 11:27 | 78.38   |
| 11/14/2023 11:28 | 78.32   |
| 11/14/2023 11:29 | 78.32   |
| 11/14/2023 11:30 | 78.32   |
| 11/14/2023 11:31 | 78.32   |
| 11/14/2023 11:32 | 78.32   |
| 11/14/2023 11:33 | 78.32   |
| 11/14/2023 11:34 | 78.32   |
| 11/14/2023 11:35 | 78.32   |
| 11/14/2023 11:36 | 78.38   |
| 11/14/2023 11:37 | 78.32   |
| 11/14/2023 11:38 | 78.32   |
| 11/14/2023 11:39 | 78.32   |
| 11/14/2023 11:40 | 78.32   |
| 11/14/2023 11:41 | 78.32   |
| 11/14/2023 11:42 | 78.32   |
| 11/14/2023 11:43 | 78.32   |
| 11/14/2023 11:44 | 78.32   |
| 11/14/2023 11:45 | 78.32   |
| 11/14/2023 11:46 | 78.32   |
| 11/14/2023 11:47 | 78.32   |
| 11/14/2023 11:48 | 78.32   |
| 11/14/2023 11:49 | 78.32   |
| Average          | 78.33   |

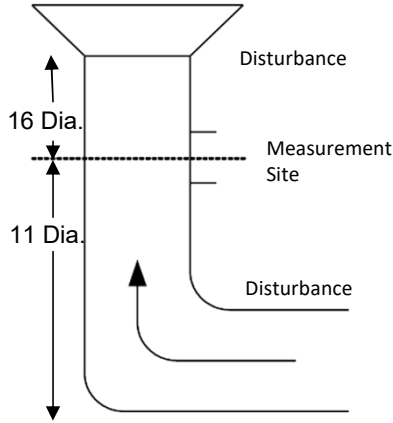
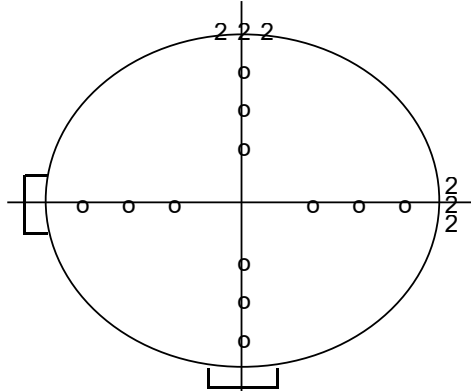
| Date/Time        | KILN:<br>CLINKER_PROD<br>(TNHR)<br>1-Minute Block<br>Average<br>Expression<br>Value |
|------------------|---|
| 11/14/2023 12:50 | 78.32   |
| 11/14/2023 12:51 | 78.32   |
| 11/14/2023 12:52 | 78.32   |
| 11/14/2023 12:53 | 78.32   |
| 11/14/2023 12:54 | 78.32   |
| 11/14/2023 12:55 | 78.32   |
| 11/14/2023 12:56 | 78.32   |
| 11/14/2023 12:57 | 78.32   |
| 11/14/2023 12:58 | 78.32   |
| 11/14/2023 12:59 | 78.32   |
| 11/14/2023 13:00 | 78.32   |
| 11/14/2023 13:01 | 78.32   |
| 11/14/2023 13:02 | 78.32   |
| 11/14/2023 13:03 | 78.32   |
| 11/14/2023 13:04 | 78.32   |
| 11/14/2023 13:05 | 78.32   |
| 11/14/2023 13:06 | 78.32   |
| 11/14/2023 13:07 | 78.32   |
| 11/14/2023 13:08 | 78.32   |
| 11/14/2023 13:09 | 78.32   |
| 11/14/2023 13:10 | 78.32   |
| 11/14/2023 13:11 | 78.32   |
| 11/14/2023 13:12 | 78.32   |
| 11/14/2023 13:13 | 78.32   |
| 11/14/2023 13:14 | 78.32   |
| 11/14/2023 13:15 | 78.32   |
| 11/14/2023 13:16 | 78.32   |
| 11/14/2023 13:17 | 78.32   |
| 11/14/2023 13:18 | 78.32   |
| 11/14/2023 13:19 | 78.32   |
| 11/14/2023 13:20 | 78.32   |
| 11/14/2023 13:21 | 78.32   |
| 11/14/2023 13:22 | 78.32   |
| 11/14/2023 13:23 | 78.32   |
| 11/14/2023 13:24 | 78.32   |
| 11/14/2023 13:25 | 78.38   |
| 11/14/2023 13:26 | 78.32   |
| 11/14/2023 13:27 | 78.32   |
| 11/14/2023 13:28 | 78.32   |
| 11/14/2023 13:29 | 78.32   |
| 11/14/2023 13:30 | 78.32   |
| 11/14/2023 13:31 | 78.32   |
| 11/14/2023 13:32 | 78.32   |
| 11/14/2023 13:32 | 78.32   |
| 11/14/2023 13:33 | 78.32   |
| 11/14/2023 13:34 | 78.32   |
| 11/14/2023 13:35 | 78.32   |
| 11/14/2023 13:36 | 78.32   |
| 11/14/2023 13:37 | 78.32   |
| 11/14/2023 13:38 | 78.32   |
| 11/14/2023 13:39 | 78.32   |
| 11/14/2023 13:40 | 78.32   |
| 11/14/2023 13:41 | 78.32   |
| 11/14/2023 13:42 | 78.32   |
| 11/14/2023 13:43 | 78.32   |
| 11/14/2023 13:44 | 78.32   |
| 11/14/2023 13:45 | 78.32   |
| 11/14/2023 13:46 | 78.32   |
| 11/14/2023 13:47 | 78.32   |
| 11/14/2023 13:48 | 78.32   |
| 11/14/2023 13:49 | 78.32   |
| Average          | 78.32   |

| Date/Time        | KILN:<br>CLINKER_PROD<br>(TNHR)<br>1-Minute Block<br>Average<br>Expression<br>Value |
|------------------|---|
| 11/14/2023 14:15 | 78.32   |
| 11/14/2023 14:16 | 78.32   |
| 11/14/2023 14:17 | 78.32   |
| 11/14/2023 14:18 | 78.32   |
| 11/14/2023 14:19 | 78.32   |
| 11/14/2023 14:20 | 78.32   |
| 11/14/2023 14:21 | 78.32   |
| 11/14/2023 14:22 | 78.32   |
| 11/14/2023 14:23 | 78.32   |
| 11/14/2023 14:24 | 78.32   |
| 11/14/2023 14:25 | 78.32   |
| 11/14/2023 14:26 | 78.38   |
| 11/14/2023 14:27 | 78.32   |
| 11/14/2023 14:28 | 78.32   |
| 11/14/2023 14:29 | 78.32   |
| 11/14/2023 14:30 | 78.32   |
| 11/14/2023 14:31 | 78.32   |
| 11/14/2023 14:32 | 78.32   |
| 11/14/2023 14:33 | 78.32   |
| 11/14/2023 14:34 | 78.32   |
| 11/14/2023 14:35 | 78.32   |
| 11/14/2023 14:36 | 78.32   |
| 11/14/2023 14:37 | 78.32   |
| 11/14/2023 14:38 | 78.32   |
| 11/14/2023 14:39 | 78.32   |
| 11/14/2023 14:40 | 78.32   |
| 11/14/2023 14:41 | 78.32   |
| 11/14/2023 14:42 | 78.32   |
| 11/14/2023 14:43 | 78.32   |
| 11/14/2023 14:44 | 78.32   |
| 11/14/2023 14:45 | 78.32   |
| 11/14/2023 14:46 | 78.32   |
| 11/14/2023 14:47 | 78.32   |
| 11/14/2023 14:48 | 78.32   |
| 11/14/2023 14:49 | 78.32   |
| 11/14/2023 14:50 | 78.32   |
| 11/14/2023 14:51 | 78.32   |
| 11/14/2023 14:52 | 78.32   |
| 11/14/2023 14:53 | 78.32   |
| 11/14/2023 14:54 | 78.32   |
| 11/14/2023 14:55 | 78.32   |
| 11/14/2023 14:56 | 78.32   |
| 11/14/2023 14:57 | 78.32   |
| 11/14/2023 14:58 | 78.32   |
| 11/14/2023 14:59 | 78.32   |
| 11/14/2023 15:00 | 78.32   |
| 11/14/2023 15:01 | 78.32   |
| 11/14/2023 15:02 | 78.32   |
| 11/14/2023 15:03 | 78.32   |
| 11/14/2023 15:04 | 78.32   |
| 11/14/2023 15:05 | 78.32   |
| 11/14/2023 15:06 | 78.32   |
| 11/14/2023 15:07 | 78.32   |
| 11/14/2023 15:08 | 78.32   |
| 11/14/2023 15:09 | 78.32   |
| 11/14/2023 15:10 | 78.32   |
| 11/14/2023 15:11 | 78.32   |
| 11/14/2023 15:12 | 78.32   |
| 11/14/2023 15:13 | 78.32   |
| 11/14/2023 15:14 | 78.32   |
| Average          | 78.32   |

| Date/Time        | KILN:<br>CLINKER_PROD<br>(TNHR)<br>1-Minute Block<br>Average<br>Expression<br>Value |
|------------------|---|
| 11/14/2023 15:40 | 78.32   |
| 11/14/2023 15:41 | 78.32   |
| 11/14/2023 15:42 | 78.32   |
| 11/14/2023 15:43 | 78.32   |
| 11/14/2023 15:44 | 78.32   |
| 11/14/2023 15:45 | 78.32   |
| 11/14/2023 15:46 | 78.32   |
| 11/14/2023 15:47 | 78.32   |
| 11/14/2023 15:48 | 78.32   |
| 11/14/2023 15:49 | 78.38   |
| 11/14/2023 15:50 | 78.32   |
| 11/14/2023 15:51 | 78.32   |
| 11/14/2023 15:52 | 78.32   |
| 11/14/2023 15:53 | 78.32   |
| 11/14/2023 15:54 | 78.32   |
| 11/14/2023 15:55 | 78.32   |
| 11/14/2023 15:56 | 78.32   |
| 11/14/2023 15:57 | 78.32   |
| 11/14/2023 15:58 | 78.32   |
| 11/14/2023 15:59 | 78.32   |
| 11/14/2023 16:00 | 78.32   |
| 11/14/2023 16:01 | 78.32   |
| 11/14/2023 16:02 | 78.32   |
| 11/14/2023 16:03 | 78.32   |
| 11/14/2023 16:04 | 78.32   |
| 11/14/2023 16:05 | 78.32   |
| 11/14/2023 16:06 | 78.32   |
| 11/14/2023 16:07 | 78.32   |
| 11/14/2023 16:08 | 78.32   |
| 11/14/2023 16:09 | 78.32   |
| 11/14/2023 16:10 | 78.32   |
| 11/14/2023 16:11 | 78.32   |
| 11/14/2023 16:12 | 78.32   |
| 11/14/2023 16:13 | 78.32   |
| 11/14/2023 16:14 | 78.32   |
| 11/14/2023 16:15 | 78.32   |
| 11/14/2023 16:16 | 78.32   |
| 11/14/2023 16:17 | 78.32   |
| 11/14/2023 16:18 | 78.32   |
| 11/14/2023 16:19 | 78.32   |
| 11/14/2023 16:20 | 78.32   |
| 11/14/2023 16:21 | 78.32   |
| 11/14/2023 16:22 | 78.32   |
| 11/14/2023 16:23 | 78.32   |
| 11/14/2023 16:24 | 78.32   |
| 11/14/2023 16:25 | 78.32   |
| 11/14/2023 16:26 | 78.38   |
| 11/14/2023 16:27 | 78.32   |
| 11/14/2023 16:28 | 78.32   |
| 11/14/2023 16:29 | 78.32   |
| 11/14/2023 16:30 | 78.32   |
| 11/14/2023 16:31 | 78.32   |
| 11/14/2023 16:32 | 78.32   |
| 11/14/2023 16:33 | 78.32   |
| 11/14/2023 16:34 | 78.32   |
| 11/14/2023 16:35 | 78.32   |
| 11/14/2023 16:36 | 78.32   |
| 11/14/2023 16:37 | 78.32   |
| 11/14/2023 16:38 | 78.32   |
| 11/14/2023 16:39 | 78.32   |
| Average          | 78.32   |

## Appendix B – Test Section Diagrams

# EQUAL AREA TRAVERSE FOR ROUND DUCTS



**Client:** CalPortland Company, Inc.

**Facility:** Redding Cement Plant

**Test Location:** Kiln Stack

**Date:** 11/14/23

**Diameter (Feet):** 7.000

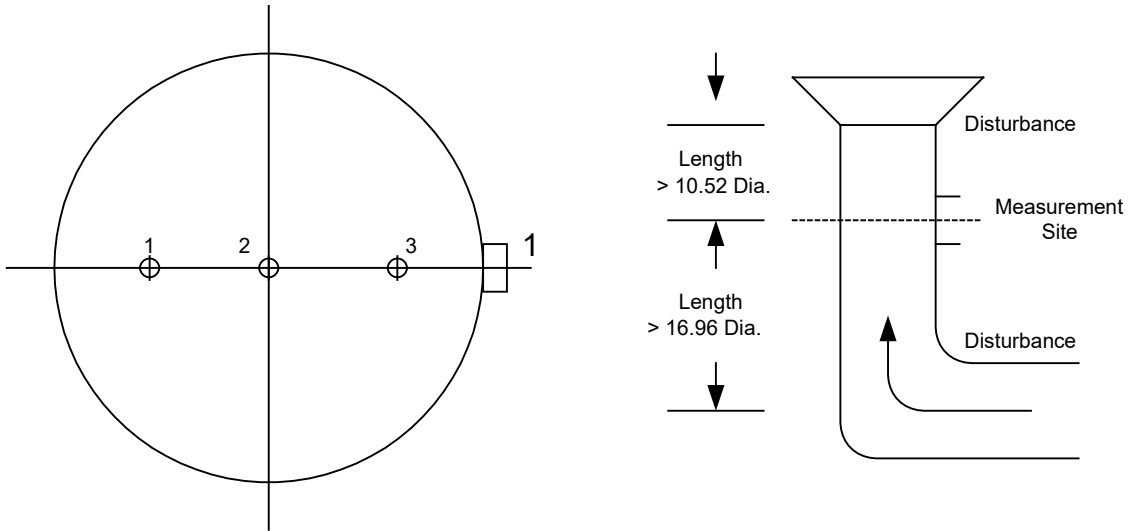
**Port Length (In):** 12.00

**Ports Sampled:** 2

**Points/Port:** 6

|   | <b>Point Markings</b>         |                      |
|---|-------------------------------|----------------------|
|   | <b>From inside wall (in.)</b> | <b>% of Diameter</b> |
| 1 | 3.70                          | 4.40                 |
| 2 | 12.26                         | 14.60                |
| 3 | 24.86                         | 29.60                |
| 4 | 59.14                         | 70.40                |
| 5 | 71.74                         | 85.40                |
| 6 | 80.30                         | 95.60                |

# GASEOUS TRAVERSE FOR ROUND DUCTS (Stratification)



Job: CalPortland Redding

Test Location: Main Kiln Stack

Stack Diameter: 7.0 Feet

Stack Area: 38.485 Square Feet

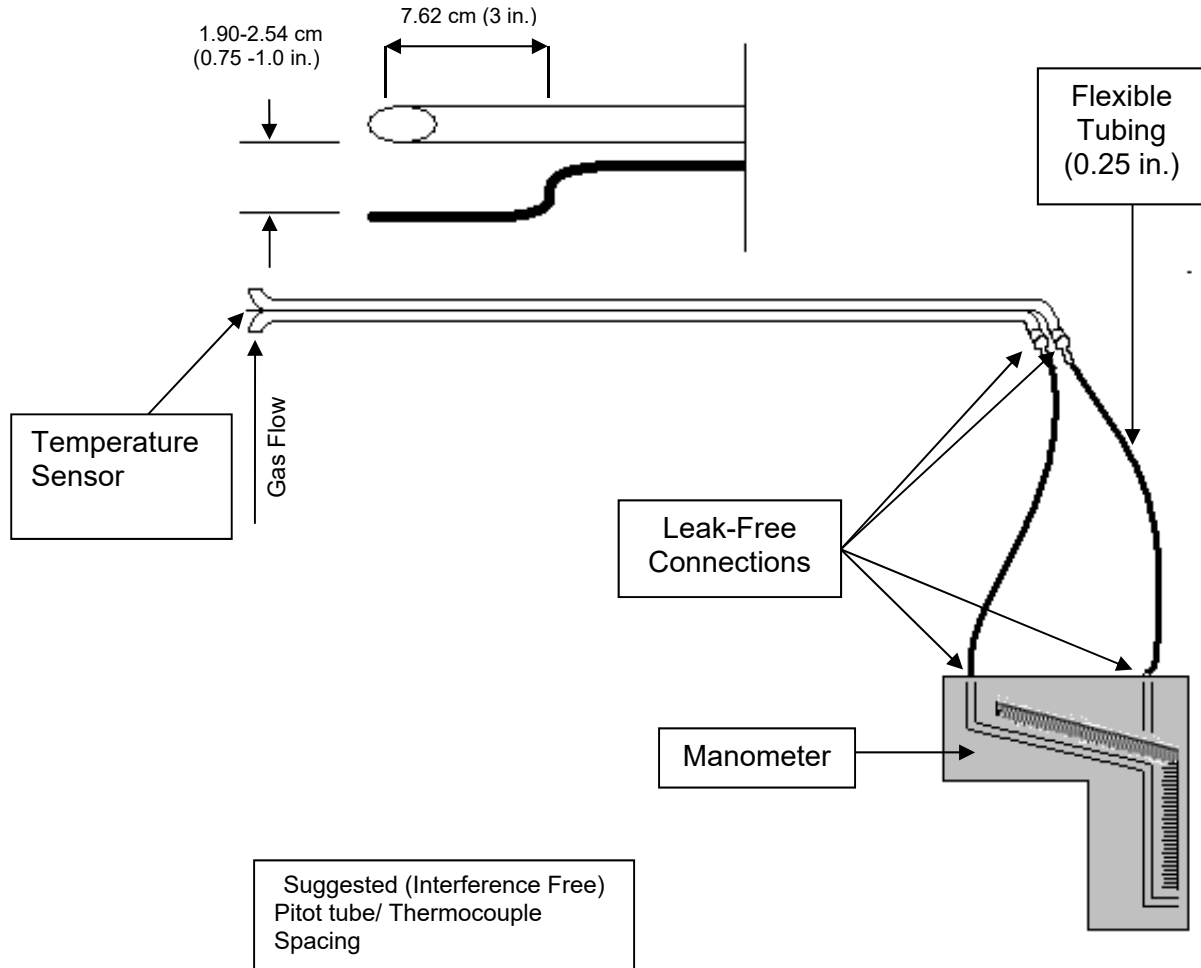
No. Sample Points: 3

Distance from Inside Wall  
To Traverse Point:

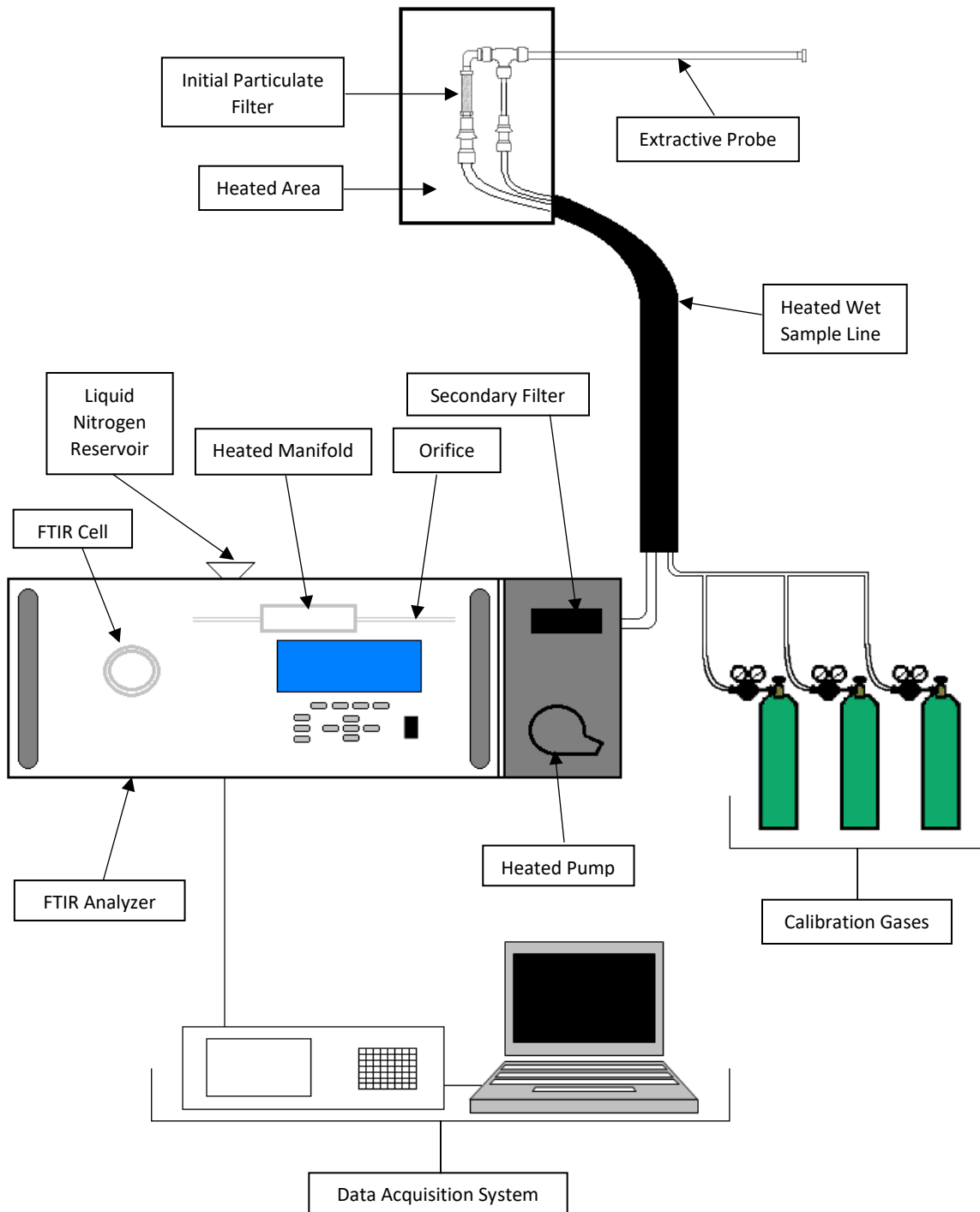
1. 83.3 % of diameter
2. 50.0 % of diameter
3. 16.7 % of diameter

## Appendix C – Sample Train Diagrams

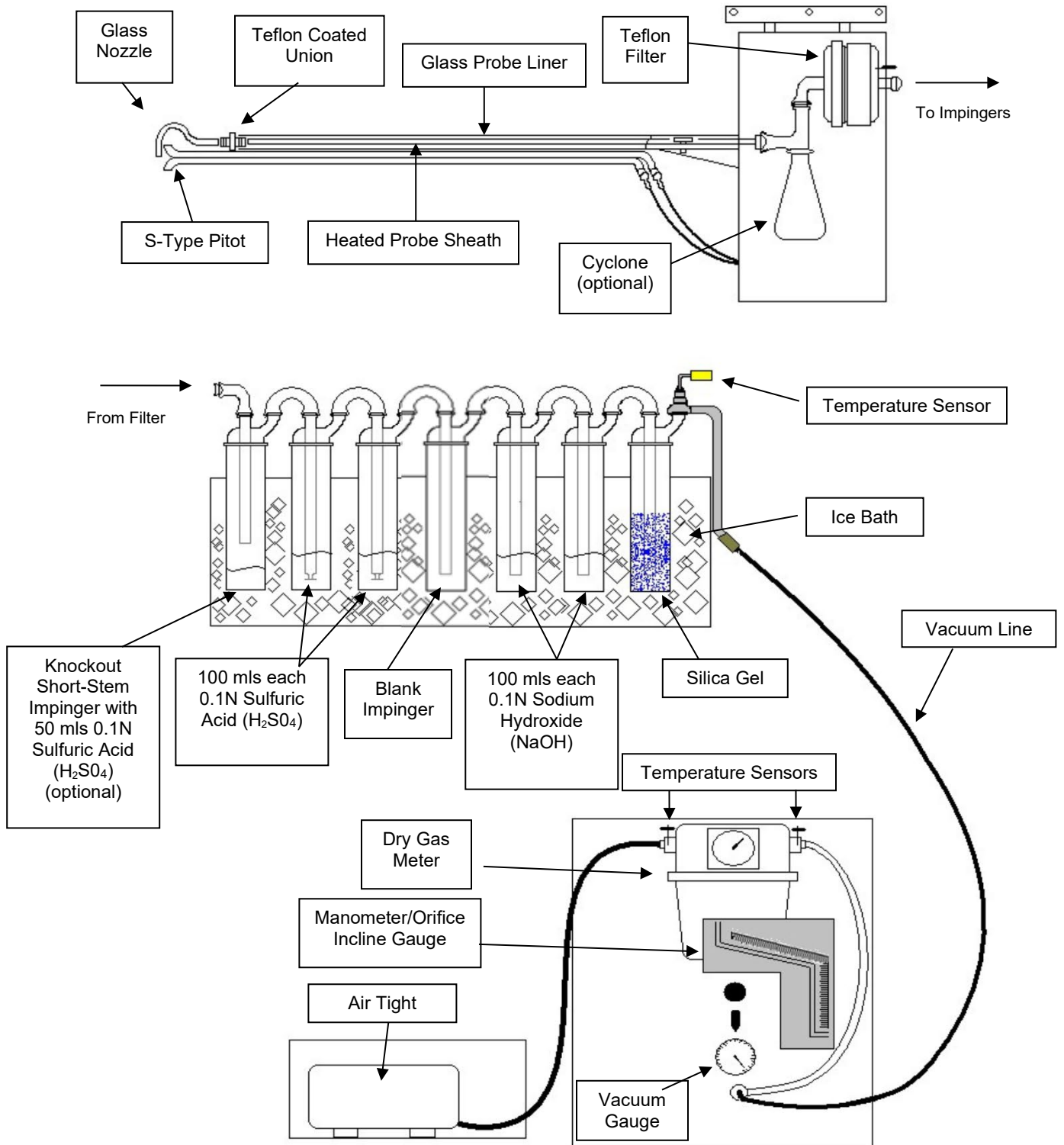
# USEPA Method 2 – Type S Pitot Tube Manometer Assembly



# USEPA Method 320 – Vapor Phase Organic and Inorganic Emissions by Extractive Fourier Transform Infrared (FTIR) Spectroscopy Sample Train Diagram



# USEPA Method 26A – HF and Cl<sub>2</sub> Sample Train Diagram



## Appendix D – Calculation Nomenclature and Formulas

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Project #:** M234605  
**Test Location:** Main Kiln Stack  
**Date:** 11/14/23

### **Sample Calculations**

$$(12.59\% - 0.01\%) \times \frac{\text{O2 \% (dry)} \quad 11.18\%}{11.12\% - 0.01\%} = 12.66\%$$

$$C_{\text{gas}} = (C - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0}$$

where:

$C_{\text{gas}}$  = Effluent gas concentration, dry basis, ppm or %

$C$  = Average gas concentration indicated by gas analyzer, dry basis, ppm or %

$C_0$  = Average of initial and final system calibration bias check responses for the zero gas, ppm or %

$C_{\text{m}}$  = Average of initial and final system calibration bias check responses for the upscale calibration gas, ppm or %

$C_{\text{ma}}$  = Actual concentration of the upscale calibration gas, ppm or %

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Run:** 1  
**Date:** 11/14/2023  
**Method:** 26A  
**Source Condition:** Mill On

**Dry Molecular Weight**

$$Md = 0.44 \times (\%CO_2) + 0.32 \times (\%O_2) + 0.28 \times \%N_2$$

$$\%CO_2 = \frac{13.4}{\quad} \qquad \%O_2 = \frac{12.7}{\quad} \qquad \%N_2 = \frac{73.9}{\quad}$$

$$Md = \frac{30.652}{\quad}$$

**Wet Molecular Weight**

$$Ms = Md \times (1 - Bws) + (18.0 \times Bws)$$

$$Md = \frac{30.652}{\quad} \qquad Bws = \frac{0.110}{\quad}$$

$$Ms = \frac{29.266}{\quad}$$

**Meter Volume at Standard Conditions**

$$Vm(std) = 17.647 \times Y \times Vm \times \frac{(Pbar + DH/13.6)}{Tm}$$

$$Y = \frac{0.992}{\quad} \qquad DH = \frac{4.2}{\quad} \qquad Vm = \frac{70.975}{\quad} \qquad Tm = \frac{56.8}{\quad} \qquad Pbar = \frac{29.2}{\quad}$$

$$Vm(std) = \frac{71.022}{\quad}$$

**Volume of Water Vapor Condensed**

$$Vw(std) = 0.0471 \times (\text{net H}_2\text{O gain})$$

$$\text{Net H}_2\text{O} = \frac{185.5}{\quad}$$

$$Vw(std) = \frac{8.737}{\quad}$$

**Moisture Content**

$$Bws = \frac{Vw(std)}{Vw(std) + Vm(std)}$$

$$Vw(std) = \frac{8.737}{\quad} \qquad Vm(std) = \frac{71.022}{\quad}$$

$$Bws = \frac{0.110}{\quad}$$

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Run: 1  
 Date: 11/14/2023  
 Method: 26A  
 Source Condition: Mill On

**Average Duct Velocity**

$$V_s = 85.49 \times C_p \times \text{Sqrt DP (avg)} \times (T_s \text{ (avg)} + 460 / (P_s \times M_s))^{1/2}$$

|                             |  |   |
|-----------------------------|--|---|
| $C_p = \frac{0.820}{29.17}$ | $T_s \text{ (avg)} = \frac{231.4}{29.266}$ | $\text{Sqrt DP (avg)} = \frac{1.387}{}$ |
| $P_s = \frac{29.17}{}$      | $M_s = \frac{29.266}{}$                    |   |
| $V_s = \frac{87.486}{}$     |  |   |

**Volumetric Flow Rate (Actual Basis)**

$$Q = V_s \times A \times 60$$

|                         |                       |
|-------------------------|-----------------------|
| $V_s = \frac{87.486}{}$ | $A = \frac{38.485}{}$ |
| $Q = \frac{202,011}{}$  |                       |

**Volumetric Flow Rate (Standard Basis)**

$$Q_{std} = 17.647 \times Q \times \frac{P_s}{T_s \text{ (avg)} + 460}$$

|                              |                        |                                      |
|------------------------------|------------------------|--------------------------------------|
| $Q = \frac{202,011}{}$       | $P_s = \frac{29.17}{}$ | $T_s \text{ (avg)} = \frac{231.4}{}$ |
| $Q_{std} = \frac{150,404}{}$ |                        |                                      |

**Volumetric Flow Rate (Standard Dry Basis)**

$$Q_{std}(\text{dry}) = Q_{std} \times (1 - B_{ws})$$

|  |                           |
|--|---------------------------|
| $Q_{std} = \frac{150,404}{}$             | $B_{ws} = \frac{0.110}{}$ |
| $Q_{std}(\text{dry}) = \frac{133,928}{}$ |                           |

**Isokinetic Variation:**

$$\%ISO = \frac{0.0945 \times (T_s + 460) \times V_m(\text{std})}{V_s \times \theta \times A_n \times P_s \times (1 - B_{ws})}$$

|                            |                                     |                         |
|----------------------------|-------------------------------------|-------------------------|
| $T_s = \frac{231.4}{}$     | $V_m(\text{std}) = \frac{71.022}{}$ | $V_s = \frac{87.486}{}$ |
| $A_n = \frac{0.0003327}{}$ | $\theta = \frac{60}{}$              | $P_s = \frac{29.17}{}$  |
| $B_{ws} = \frac{0.110}{}$  |                                     |                         |
| $\%ISO = \frac{102.3}{}$   |                                     |                         |

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Run:** 1  
**Date:** 11/14/2023  
**Method:** 26A  
**Source Condition:** Mill On

**Chloride (Cl2) Concentration:**

$$\text{mg/m}^3 = \frac{\text{mg of Chloride (Cl2)}}{\text{Vm(std)} \times 0.02832 \text{ m}^3/\text{ft}^3}$$

$$\text{mg} = \underline{0.15} \quad \text{Vm(std)} = \underline{71.022}$$

$$\text{mg/m}^3 = \underline{0.07}$$

**Chloride (Cl2) Emission Rate:**

$$\text{lb of Chloride (Cl2)} = \frac{\mu\text{g of sample} \times 10^{-6} \text{ grams}/\mu\text{g}}{453.6 \text{ grams/lb}}$$

$$\text{Emission Rate lb/hr} = \frac{\text{lb of Chloride (Cl2)}}{\text{Vm(std)}} \times \text{dscfm} \times 60 \text{ min/hr}$$

$$\text{lb of Chloride (Cl2)} = \underline{3.31\text{E-}10} \quad \text{dscfm} = \underline{133,928}$$

$$\text{Emission Rate lb/hr} = \underline{0.0374}$$

$$\text{Emission Rate lb/ton} = \frac{\text{lb/hr of Chloride (Cl2)}}{\text{clinker production ton/hr}}$$

$$\text{lb/hr of Chloride (Cl2)} = \underline{0.0374} \quad \text{clinker ton/hr} = \underline{77.2}$$

$$\text{Emission Rate lb/ton} = \underline{0.0005}$$

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Test Location: Main Kiln Stack  
 Date: 11/14/23

### FTIR Sample Calculations

#### Direct Recovery % of Calibration Transfer Standard

$$DR_{cts} = \frac{D_{cts}}{Cma} \times 100$$

$$Cma = \underline{101.4}$$

$$D_{cts} = \underline{101.3}$$

$$DR_{cts} = \underline{99.9\%}$$

#### Recovery % with Calibration Transfer Standard System Purge

$$R_{cts} = \frac{Sys_{cts}}{D_{cts}} \times 100$$

$$Sys_{cts} = \underline{101.2}$$

$$D_{cts} = \underline{101.3}$$

$$R_{cts} = \underline{100\%}$$

#### Direct Recovery % of Analyte Spike Gas

SF6

$$DR_{sf6} = \frac{D_{sf6}}{Cma} \times 100$$

$$Cma = \underline{5.0}$$

$$D_{sf6} = \underline{5.0}$$

$$DR_{sf6} = \underline{99\%}$$

HCN

$$DR_{asg} = \frac{D_{asg}}{Cma} \times 100$$

$$Cma = \underline{49.6}$$

$$D_{asg} = \underline{50.3}$$

$$DR_{asg} = \underline{101.6\%}$$

#### Dilution Factor for Analyte Spiking

$$DF = \frac{Spk_{sf6}}{D_{sf6}}$$

$$Spk_{sf6} = \underline{0.317}$$

$$D_{sf6} = \underline{4.955}$$

$$DF = \underline{0.064}$$

#### Recovery % for Analyte Spike With HCN

$$R_x = \frac{Spk_x}{(N_x \times (1-DF) + D_{asg} \times DF)}$$

$$Spk_x = \underline{3.9}$$

$$N_x = \underline{0.9}$$

$$DF = \underline{0.064}$$

$$D_{asg} = \underline{50.3}$$

$$R_x = \underline{95.6} \%$$

#### where:

- DR<sub>cts</sub> = Recovery % of the calibration transfer standard directly to the analyzer
- Cma = certified concentration of calibration gas, ppm
- D<sub>cts</sub> = Concentration of the calibration transfer standard gas directly to the analyzer, ppm
- R<sub>cts</sub> = Recovery % of the calibration transfer standard through the sampling system
- Sys<sub>cts</sub> = Concentration of the calibration transfer standard gas through the system, ppm
- DF = Dilution Factor of analyte spike gas
- Spk<sub>sf6</sub> = SF6 concentration in effluent during spiking
- Spk<sub>x</sub> = Analyte concentration in effluent during spiking
- D<sub>asg</sub> = Concentration of the analyte spike gas directly to the analyzer, ppm
- D<sub>sf6</sub> = Concentration of the SF6 directly to the analyzer, ppm
- R<sub>x</sub> = Recovery % of the analyte spike gas
- N<sub>x</sub> = Native effluent (HCN) concentration prior to analyte spike

# MOSTARDI PLATT

## Volumetric Flow Nomenclature

- A = Cross-sectional area of stack or duct, ft<sup>2</sup>
- B<sub>ws</sub> = Water vapor in gas stream, proportion by volume
- C<sub>p</sub> = Pitot tube coefficient, dimensionless
- M<sub>d</sub> = Dry molecular weight of gas, lb/lb-mole
- M<sub>s</sub> = Molecular weight of gas, wet basis, lb/lb-mole
- M<sub>w</sub> = Molecular weight of water, 18.0 lb/lb-mole
- P<sub>bar</sub> = Barometric pressure at testing site, in. Hg
- P<sub>g</sub> = Static pressure of gas, in. Hg (in. H<sub>2</sub>O/13.6)
- DH = Static pressure of gas, in. H<sub>2</sub>O
- P<sub>s</sub> = Absolute pressure of gas, in. Hg = P<sub>bar</sub> + P<sub>g</sub>
- P<sub>std</sub> = Standard absolute pressure, 29.92 in. Hg
- A<sub>cfm</sub> = Actual volumetric gas flow rate
- Sc<sub>fm</sub> = Volumetric gas flow rate, corrected to standard conditions
- D<sub>scfm</sub> = Standard volumetric flow rate, corrected to dry conditions
- R = Ideal gas constant, 21.85 in. Hg-ft<sup>3</sup>/°R-lb-mole
- T<sub>s</sub> = Average stack gas temperature, °F
- T<sub>m</sub> = Average dry gas meter temperature, °F
- T<sub>std</sub> = Standard absolute temperature, 528°R
- v<sub>s</sub> = Gas velocity, ft/sec
- V<sub>m(std)</sub> = Volume of gas sampled, corrected to standard conditions, scf
- V<sub>w(std)</sub> = Volume of water vapor in gas sample, corrected to standard conditions, scf
- V<sub>lc</sub> = Volume of liquid collected
- Y = Dry gas meter calibration factor
- Δp = Velocity head of gas, in. H<sub>2</sub>O
- K<sub>1</sub> = 17.647 °R/in. Hg
- %EA = Percent excess air
- %CO<sub>2</sub> = Percent carbon dioxide by volume, dry basis
- %O<sub>2</sub> = Percent oxygen by volume, dry basis
- %N<sub>2</sub> = Percent nitrogen by volume, dry basis
- 0.264 = Ratio of O<sub>2</sub> to N<sub>2</sub> in air, v/v
- 0.28 = Molecular weight of N<sub>2</sub> or CO, divided by 100
- 0.32 = Molecular weight of O<sub>2</sub> divided by 100
- 0.44 = Molecular weight of CO<sub>2</sub> divided by 100
- 13.6 = Specific gravity of mercury (Hg)

# MOSTARDI PLATT

## Volumetric Air Flow Calculations

$$Vm (std) = 17.647 \times Vm \times \left[ \frac{(P_{bar} + \left[ \frac{DH}{13.6} \right])}{(460 + Tm)} \right] \times Y$$

$$Vw (std) = 0.0471 \times Vlc$$

$$Bws = \left[ \frac{Vw (std)}{Vw (std) + Vm (std)} \right]$$

$$Md = (0.44 \times \%CO_2) + (0.32 \times \%O_2) + [0.28 \times (100 - \%CO_2 - \%O_2)]$$

$$Ms = Md \times (1 - Bws) + (18 \times Bws)$$

$$Vs = \sqrt{\frac{(Ts + 460)}{Ms \times Ps}} \times \sqrt{DP} \times Cp \times 85.49$$

$$Acfm = Vs \times Area (of\ stack\ or\ duct) \times 60$$

$$Scfm = Acfm \times 17.647 \times \left[ \frac{Ps}{(460 + Ts)} \right]$$

$$Scfh = Scfm \times 60 \frac{min}{hr}$$

$$Dscfm = Scfm \times (1 - Bws)$$

## MOSTARDI PLATT

### Isokinetic Calculation Formulas

$$1. V_{w(std)} = V_{lc} \left( \frac{\rho_w}{M_w} \right) \left( \frac{RT_{std}}{P_{std}} \right) = K_2 V_{lc}$$

$$2. V_{m(std)} = V_m Y \left( \frac{T_{std}}{T_m} \right) \left( \frac{(P_{bar} + (\frac{\Delta H}{13.6}))}{P_{std}} \right) = K_1 V_m Y \frac{(P_{bar} + (\frac{\Delta H}{13.6}))}{T_m}$$

$$3. B_{ws} = \frac{V_{w(std)}}{(V_{m(std)} + V_{w(std)})}$$

$$4. M_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2)$$

$$5. M_s = M_d(1 - B_{ws}) + 18.0(B_{ws})$$

$$6. C_a = \frac{m_a}{V_a \rho_a}$$

$$7. W_a = C_a V_{aw} \rho_a$$

$$8. C_{acf} = 15.43 K_i \left( \frac{m_n P_s}{(V_{w(std)} + V_{m(std)}) T_s} \right)$$

$$9. C_s = (15.43 \text{ grains/gram}) (m_n / V_{m(std)})$$

$$10. v_s = K_p C_p \sqrt{\frac{\Delta P T_s}{P_s M_s}}$$

$$11. Q_{acfm} = v_s A (60_{\text{sec/min}})$$

$$12. Q_{sd} = (3600_{\text{sec/hr}}) (1 - B_{ws}) v_s \left( \frac{T_{std} P_s}{T_s P_{std}} \right) A$$

$$13. E \text{ (emission rate, lbs/hr)} = Q_{std} (C_s / 7000 \text{ grains/lb})$$

$$14. IKV = \frac{T_s V_{m(std)} P_{std}}{T_{std} v_s \theta A_n P_s 60(1 - B_{ws})} = K_4 \frac{T_s V_{m(std)}}{P_s v_s A_n \theta (1 - B_{ws})}$$

$$15. \%EA = \left( \frac{\%O_2 - (0.5 \%CO)}{0.264 \%N_2 - (\%O_2 - 0.5 \%CO)} \right) \times 100$$

# MOSTARDI PLATT

## Isokinetic Nomenclature

- A = Cross-sectional area of stack or duct, square feet  
A<sub>n</sub> = Cross-sectional area of nozzle, square feet  
B<sub>ws</sub> = Water vapor in gas stream, by volume  
C<sub>a</sub> = Acetone blank residue concentration, g/g  
C<sub>act</sub> = Concentration of particulate matter in gas stream at actual conditions, gr/acf  
C<sub>p</sub> = Pitot tube coefficient  
C<sub>s</sub> = Concentration of particulate matter in gas stream, dry basis, corrected to standard conditions, gr/dscf  
IKV = Isokinetic sampling variance, must be 90.0 % ≤ IKV ≤ 110.0%  
M<sub>d</sub> = Dry molecular weight of gas, lb/lb-mole  
M<sub>s</sub> = Molecular weight of gas, wet basis, lb/lb-mole  
M<sub>w</sub> = Molecular weight of water, 18.0 lb/lb-mole  
m<sub>a</sub> = Mass of residue of acetone after evaporation, grams  
P<sub>bar</sub> = Barometric pressure at testing site, inches mercury  
P<sub>g</sub> = Static pressure of gas, inches mercury (inches water/13.6)  
P<sub>s</sub> = Absolute pressure of gas, inches mercury = P<sub>bar</sub> + P<sub>g</sub>  
P<sub>std</sub> = Standard absolute pressure, 29.92 inches mercury  
Q<sub>acfm</sub> = Actual volumetric gas flow rate, acfm  
Q<sub>sd</sub> = Dry volumetric gas flow rate corrected to standard conditions, dscfh  
R = Ideal gas constant, 21.85 inches mercury cubic foot/°R-lb-mole  
T<sub>m</sub> = Dry gas meter temperature, °R  
T<sub>s</sub> = Gas temperature, °R  
T<sub>std</sub> = Absolute temperature, 528°R  
V<sub>a</sub> = Volume of acetone blank, ml  
V<sub>aw</sub> = Volume of acetone used in wash, ml  
W<sub>a</sub> = Weight of residue in acetone wash, grams  
m<sub>n</sub> = Total amount of particulate matter collected, grams  
V<sub>1c</sub> = Total volume of liquid collected in impingers and silica gel, ml  
V<sub>m</sub> = Volume of gas sample as measured by dry gas meter, dcf  
V<sub>m(std)</sub> = Volume of gas sample measured by dry gas meter, corrected to standard conditions, dscf  
V<sub>s</sub> = Gas velocity, ft/sec  
V<sub>w(std)</sub> = Volume of water vapor in gas sample, corrected to standard conditions, scf  
Y = Dry gas meter calibration factor  
ΔH = Average pressure differential across the orifice meter, inches water  
Δp = Velocity head of gas, inches water  
ρ<sub>a</sub> = Density of acetone, 0.7855 g/ml (average)  
ρ<sub>w</sub> = Density of water, 0.002201 lb/ml  
θ = Total sampling time, minutes  
K<sub>1</sub> = 17.647 °R/in. Hg  
K<sub>2</sub> = 0.04707 ft<sup>3</sup>/ml  
K<sub>4</sub> = 0.09450/100 = 0.000945  
K<sub>p</sub> = Pitot tube constant,  $85.49 \frac{ft}{sec} \left[ \frac{(lb/lb-mole)(in. Hg)}{(^{\circ}R)(in. H_2O)} \right]^{1/2}$   
%EA = Percent excess air  
%CO<sub>2</sub> = Percent carbon dioxide by volume, dry basis  
%O<sub>2</sub> = Percent oxygen by volume, dry basis  
%CO = Percent carbon monoxide by volume, dry basis  
%N<sub>2</sub> = Percent nitrogen by volume, dry basis  
0.264 = Ratio of O<sub>2</sub> to N<sub>2</sub> in air, v/v  
28 = Molecular weight of N<sub>2</sub> or CO  
32 = Molecular weight of O<sub>2</sub>  
44 = Molecular weight of CO<sub>2</sub>  
13.6 = Specific gravity of mercury (Hg)

# MOSTARDI PLATT

## Calculations for Hydrogen Fluoride By Method 26 or 26A

### Concentration

$$\frac{\text{lbs HF}}{\text{dscf}} = \frac{\mu\text{g HF in sample}}{4.536 \times 10^8 \times \text{dscf}}$$

where:

$$4.536 \times 10^8 = \mu\text{g/lb}$$

dscf = Volume of gas sampled

$$\mu\text{g/lb HF} = \mu\text{g F} \times \frac{20.008}{19.000}$$

### Parts Per Million

$$\text{ppm HF} = \frac{\text{lbs HF}}{\text{dscf}} \div \frac{20.008}{385 \times 10^6}$$

where:

385 = Volume of 1 lb mole of gas at 68°F and 29.92 in. Hg

106 = Conversion of ppm v/v

### Emission Rate

$$\text{lbs HF /dscf} \times \text{dscfm} \times 60 \text{ min/hr} = \text{lbs/hr HF}$$

## MOSTARDI PLATT

### Pollutant Concentration Correction 7% for Percent Oxygen

$$C_{adj} = C_d \frac{20.9 - 7\%}{20.9 - \%O_2}$$

where:

$C_{adj}$  = Pollutant concentration corrected to percent  $O_2$

$20.9 - 7\%$  = Percent  $O_2$ , the defined  $O_2$  correction value, percent

$20.9$  = Percent  $O_2$  in air

$\%O_2$  = Measured  $O_2$  concentration dry basis, percent

$C_d$  = Pollutant concentration measured, dry basis, ppm.

## Appendix E- Laboratory Sample Analysis

| Chain-of-Custody Form           |             |                             |            |                            |                         |             |
|---------------------------------|-------------|-----------------------------|------------|----------------------------|-------------------------|-------------|
| Project Number: M234605         |             |                             |            | Date Results Required:     |                         |             |
| Client: CalPortland – Redding   |             |                             |            | TAT Required:              |                         |             |
| Plant/Test Location: Kiln Stack |             |                             |            | Project Supervisor: Rich S |                         |             |
| Sample Number                   | Sample Date | Sample Point Identification | # of Conts | Sub Lab                    | Analysis Required       | Volume, mls |
| 001                             | 11/14/23    | #1A 26A Mill off 0.1N H2SO4 | 1          |                            | M26A (HF)               |             |
| 002                             | 11/14/23    | #1A 26A Mill off 0.1N NaOH  | 1          |                            | M26A (Cl <sub>2</sub> ) |             |
| 003                             | 11/14/23    | #2A 26A Mill off 0.1N H2SO4 | 1          |                            | M26A (HF)               |             |
| 004                             | 11/14/23    | #2A 26A Mill off 0.1N NaOH  | 1          |                            | M26A (Cl <sub>2</sub> ) |             |
| 005                             | 11/14/23    | #3A 26A Mill off 0.1N H2SO4 | 1          |                            | M26A (HF)               |             |
| 006                             | 11/14/23    | #3A 26A Mill off 0.1N NaOH  | 1          |                            | M26A (Cl <sub>2</sub> ) |             |
| 007                             | 11/14/23    | #1B 26A Mill off 0.1N H2SO4 | 1          |                            | M26A (HF)               |             |
| 008                             | 11/14/23    | #1B 26A Mill off 0.1N NaOH  | 1          |                            | M26A (Cl <sub>2</sub> ) |             |
| 009                             | 11/14/23    | #2B 26A Mill off 0.1N H2SO4 | 1          |                            | M26A (HF)               |             |
| 010                             | 11/14/23    | #2B 26A Mill off 0.1N NaOH  | 1          |                            | M26A (Cl <sub>2</sub> ) |             |
| 011                             | 11/14/23    | #3B 26A Mill off 0.1N H2SO4 | 1          |                            | M26A (HF)               |             |
| 012                             | 11/14/23    | #3B 26A Mill off 0.1N NaOH  | 1          |                            | M26A (Cl <sub>2</sub> ) |             |
| 013                             | 11/14/23    | #1A 26A Mill on 0.1N H2SO4  | 1          |                            | M26A (HF)               |             |
| 014                             | 11/14/23    | #1A 26A Mill on 0.1N NaOH   | 1          |                            | M26A (Cl <sub>2</sub> ) |             |
| 015                             | 11/14/23    | #2A 26A Mill on 0.1N H2SO4  | 1          |                            | M26A (HF)               |             |
| 016                             | 11/14/23    | #2A 26A Mill on 0.1N NaOH   | 1          |                            | M26A (Cl <sub>2</sub> ) |             |
| 017                             | 11/14/23    | #3A 26A Mill on 0.1N H2SO4  | 1          |                            | M26A (HF)               |             |
| 018                             | 11/14/23    | #3A 26A Mill on 0.1N NaOH   | 1          |                            | M26A (Cl <sub>2</sub> ) |             |
| 019                             | 11/14/23    | #1B 26A Mill on 0.1N H2SO4  | 1          |                            | M26A (HF)               |             |
| 020                             | 11/14/23    | #1B 26A Mill on 0.1N NaOH   | 1          |                            | M26A (Cl <sub>2</sub> ) |             |
| 021                             | 11/14/23    | #2B 26A Mill on 0.1N H2SO4  | 1          |                            | M26A (HF)               |             |
| 022                             | 11/14/23    | #2B 26A Mill on 0.1N NaOH   | 1          |                            | M26A (Cl <sub>2</sub> ) |             |
| 023                             | 11/14/23    | #3B 26A Mill on 0.1N H2SO4  | 1          |                            | M26A (HF)               |             |
| 024                             | 11/14/23    | #3B 26A Mill on 0.1N NaOH   | 1          |                            | M26A (Cl <sub>2</sub> ) |             |

|                                    |          |                                |   |                               |                                |  |
|------------------------------------|----------|--------------------------------|---|-------------------------------|--------------------------------|--|
| 025                                | 11/14/23 | A Train Field Blank 0.1N H2SO4 | 1 |                               | M26A (HF)                      |  |
| 026                                | 11/14/23 | A Train Field Blank 0.1N NaOH  | 1 |                               | M26A (Cl <sub>2</sub> )        |  |
| 027                                | 11/14/23 | B Train Field Blank 0.1N H2SO4 | 1 |                               | M26A (HF)                      |  |
| 028                                | 11/14/23 | B Train Field Blank 0.1N NaOH  | 1 |                               | M26A (Cl <sub>2</sub> )        |  |
| 029                                | 11/14/23 | 0.1N H2SO4 Reagent Blank       | 1 |                               | M26A (HF)                      |  |
| 030                                | 11/14/23 | 0.1N NaOH Reagent Blank        | 1 |                               | M26A (Cl <sub>2</sub> )        |  |
| 031                                | 11/14/23 | DI Water Reagent Blank         | 1 |                               | M26A (HF and Cl <sub>2</sub> ) |  |
| Delivered to Lab by:<br>Date/Time: |          | Received by:      Date/Time:   |   | Processed by:      Date/Time: |                                |  |

Laboratory Notes:

### Kiln-Mill On

|  |   |
|--|---|
| Client: CalPortland<br>Facility: Redding<br>Test Location: Kiln-Mill On<br>Project Number: M234605<br>Method: 26A<br>Date Samples Received: 11/21/2023 | Analysis Date: 12/5/2023<br>Analysis Location: Elmhurst<br>Analyst: JMG |
|--|---|

#### Train A

| Sampling Date        |       | 11/14/2023    | 11/14/2023       | 11/14/2023    | 11/14/2023        |     |     |
|----------------------|-------|---------------|------------------|---------------|-------------------|-----|-----|
|                      | UNITS | M26A DI Blank | M26A H2SO4 Blank | M26A H2SO4-R1 | M26A H2SO4-R1 Dup | RDL | MDL |
| Sulfuric Acid Volume | ml    | 200           | 200              | 406           | 406               |     |     |
| Hydrofluoric Acid    | ug    | <150          | <150             | <150          | <150              | 150 | 15  |

| Sampling Date        |       | 11/14/2023     | 11/14/2023     | 11/14/2023    |  |     |     |
|----------------------|-------|----------------|----------------|---------------|--|-----|-----|
|                      | UNITS | M26A- H2SO4 R2 | M26A- H2SO4 R3 | Field Blank A |  | RDL | MDL |
| Sulfuric Acid Volume | ml    | 379            | 424            | 294           |  |     |     |
| Hydrofluoric Acid    | ug    | <150           | <150           | <150          |  | 150 | 15  |

#### Train B

| Sampling Date        |       | 11/14/2023    | 11/14/2023       | 11/14/2023    | 11/14/2023        |     |     |
|----------------------|-------|---------------|------------------|---------------|-------------------|-----|-----|
|                      | UNITS | M26A DI Blank | M26A H2SO4 Blank | M26A H2SO4-R1 | M26A H2SO4-R1 Dup | RDL | MDL |
| Sulfuric Acid Volume | ml    | 200           | 200              | 415           | 415               |     |     |
| Hydrofluoric Acid    | ug    | <150          | <150             | <150          | <150              | 150 | 15  |

| Sampling Date        |       | 11/14/2023     | 11/14/2023     | 11/14/2023    |  |     |     |
|----------------------|-------|----------------|----------------|---------------|--|-----|-----|
|                      | UNITS | M26A- H2SO4 R2 | M26A- H2SO4 R3 | Field Blank B |  | RDL | MDL |
| Sulfuric Acid Volume | ml    | 447            | 423            | 294           |  |     |     |
| Hydrofluoric Acid    | ug    | <150           | <150           | <150          |  | 150 | 15  |





### Kiln-Mill On

|  |   |
|--|---|
| Client: CalPortland<br>Facility: Redding<br>Test Location: Kiln-Mill On<br>Project Number: M234605<br>Method: 26A<br>Date Samples Received: 11/21/2023 | Analysis Date: 12/5/2023<br>Analysis Location: Elmhurst<br>Analyst: JMG |
|--|---|

#### Train A

| Sampling Date           |       | 11/14/2023    | 11/14/2023      | 11/14/2023   | 11/14/2023       |     |     |
|-------------------------|-------|---------------|-----------------|--------------|------------------|-----|-----|
|                         | UNITS | M26A DI Blank | M26A NaOH Blank | M26A NaOH-R1 | M26A NaOH-R1 Dup | RDL | MDL |
| Sodium Hydroxide Volume | ml    | 200           | 200             | 264          | 264              |     |     |
| Chlorine                | ug    | <150          | <150            | <150         | <150             | 150 | 15  |

| Sampling Date           |       | 11/14/2023    | 11/14/2023    | 11/14/2023    |     |     |
|-------------------------|-------|---------------|---------------|---------------|-----|-----|
|                         | UNITS | M26A- NaOH R2 | M26A- NaOH R3 | Train A Blank | RDL | MDL |
| Sodium Hydroxide Volume | ml    | 265           | 275           | 279           |     |     |
| Chlorine                | ug    | <150          | <150          | <150          | 150 | 15  |

#### Train B

| Sampling Date           |       | 11/14/2023    | 11/14/2023      | 11/14/2023   | 11/14/2023       |     |     |
|-------------------------|-------|---------------|-----------------|--------------|------------------|-----|-----|
|                         | UNITS | M26A DI Blank | M26A NaOH Blank | M26A NaOH-R1 | M26A NaOH-R1 Dup | RDL | MDL |
| Sodium Hydroxide Volume | ml    | 200           | 200             | 269          | 269              |     |     |
| Chlorine                | ug    | <150          | <150            | <150         | <150             | 150 | 15  |

| Sampling Date           |       | 11/14/2023    | 11/14/2023    | 11/14/2023    |     |     |
|-------------------------|-------|---------------|---------------|---------------|-----|-----|
|                         | UNITS | M26A- NaOH R2 | M26A- NaOH R3 | Train B Blank | RDL | MDL |
| Sodium Hydroxide Volume | ml    | 287           | 241           | 279           |     |     |
| Chlorine                | ug    | <150          | <150          | <150          | 150 | 15  |

|                               |                      |                           |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
|-------------------------------|----------------------|---------------------------|-------------------------|----------------------------------|------------------------------|------------------------|-----------------|----------------------|-----------------------|-----------------------|--|--|--|--|--|--|--|--|--|-------------|
| <b>Client:</b>                | CalPortland          | <b>Analysis Date:</b>     | 12/6/2023               |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| <b>Facility:</b>              | Redding              | <b>Analysis Location:</b> | Elmhurst Lab            |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| <b>Test Location:</b>         | Kiln-Mill On         | <b>Analyst:</b>           | JMG                     |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| <b>Project Number:</b>        | M234605              |                           |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| <b>Method:</b>                | 26A                  |                           |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| <b>Date Samples Received:</b> | 11/21/2023           |                           |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
|                               |                      |                           |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| <b>Standard ppm Cl</b>        | <b>Area</b>          | <b>Response Factor</b>    | <b>Calculated Value</b> | <b>Slope of Regression Curve</b> |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 1                             | 0.1264               | 0.1264                    | 0.97                    | 0.1308                           |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 2                             | 0.2504               | 0.1252                    | 1.92                    |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 5                             | 0.6542               | 0.1308                    | 5.00                    | Response Factor Ave              |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 8                             | 1.0781               | 0.1348                    | 8.25                    | 0.1307                           |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 10                            | 1.3636               | 0.1364                    | 10.43                   |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| <b>Lot Number</b>             | Ricca 8209004        |                           |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
|                               | <b>R<sup>2</sup></b> | <b>0.9997</b>             |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
|                               |                      |                           |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| <b>Sample Number</b>          | <b>Sample Date</b>   | <b>Sample ID</b>          | <b>Sample Area</b>      | <b>PPM Cl</b>                    | <b>PPM X Dilution Factor</b> | <b>Dilution Factor</b> | <b>Total ml</b> | <b>mg Cl in soln</b> | <b>ug Cl2 in soln</b> | <b>ug Cl2 in soln</b> |  |  |  |  |  |  |  |  |  |             |
| 031                           | 11/14/2023           | DI Reagent Blank          | 0.0025                  | 0.0191                           | 0.0191                       | 1                      | 200             | 0.0038               |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 031                           | 11/14/2023           | DI Reagent Blank          | 0.0005                  | 0.0038                           | 0.0038                       | 1                      | 200             | 0.0008               |                       | 0.0023                |  |  |  |  |  |  |  |  |  | 2.294394956 |
| 030                           | 11/14/2023           | NaOH Reagent Blank        | 0.0103                  | 0.0788                           | 0.0788                       | 1                      | 200             | 0.0158               |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 030                           | 11/14/2023           | NaOH Reagent Blank        | 0.0107                  | 0.0818                           | 0.0818                       | 1                      | 200             | 0.0164               |                       | 0.0161                |  |  |  |  |  |  |  |  |  | 16.06076469 |
| 014                           | 11/14/2023           | Test 1A NaOH Imp          | 0.0024                  | 0.0184                           | 0.0184                       | 1                      | 264             | 0.0048               |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 014                           | 11/14/2023           | Test 1A NaOH Imp          | 0.0029                  | 0.0222                           | 0.0222                       | 1                      | 264             | 0.0059               |                       | 0.0054                |  |  |  |  |  |  |  |  |  | 5.350529038 |
| 014                           | 11/14/2023           | Test 1A NaOH Imp          | 0.0035                  | 0.0268                           | 0.0268                       | 1                      | 264             | 0.0071               |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 014                           | 11/14/2023           | Test 1A NaOH Imp          | 0.0034                  | 0.0260                           | 0.0260                       | 1                      | 264             | 0.0069               |                       | 0.0070                |  |  |  |  |  |  |  |  |  | 6.965783087 |
| 016                           | 11/14/2023           | Test 2A NaOH Imp          | 0.0015                  | 0.0115                           | 0.0115                       | 1                      | 265             | 0.0030               |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 016                           | 11/14/2023           | Test 2A NaOH Imp          | 0.0010                  | 0.0076                           | 0.0076                       | 1                      | 265             | 0.0020               |                       | 0.0025                |  |  |  |  |  |  |  |  |  | 2.533394431 |
| 018                           | 11/14/2023           | Test 3A NaOH Imp          | 0.0049                  | 0.0375                           | 0.0375                       | 1                      | 275             | 0.0103               |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 018                           | 11/14/2023           | Test 3A NaOH Imp          | 0.0035                  | 0.0268                           | 0.0268                       | 1                      | 275             | 0.0074               |                       | 0.0088                |  |  |  |  |  |  |  |  |  | 8.833420582 |
| 026                           | 11/14/2023           | Train Blank               | 0.0163                  | 0.1247                           | 0.1247                       | 1                      | 279             | 0.0348               |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 026                           | 11/14/2023           | Train Blank               | 0.0157                  | 0.1201                           | 0.1201                       | 1                      | 279             | 0.0335               |                       | 0.0341                |  |  |  |  |  |  |  |  |  | 34.14059695 |
|                               |                      |                           |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
|                               |                      | Run 1 H2SO4 Spike W/ 2ppm | 0.1235                  | 0.9445                           |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
|                               |                      | Run 1 H2SO4 Spike W/ 2ppm | 0.1221                  | 0.9338                           |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
|                               |                      |                           |                         |                                  | <b>Expected Value</b>        | <b>% Difference</b>    |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
|                               |                      |                           |                         |                                  | 0.9677                       | 2.94%                  |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
|                               |                      |                           |                         |                                  | 0.9677                       |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| <b>CCV ppm Cl</b>             | <b>Area</b>          | <b>PPM Cl</b>             |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 5 ppm ICV                     | 0.6732               | 5.1486                    |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 5 ppm CCV                     | 0.6685               | 5.1127                    |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 5 ppm CCV                     | 0.6758               | 5.1685                    |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
|                               |                      |                           |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| <b>Standard ppm Cl</b>        | <b>Area</b>          | <b>Difference</b>         |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 1                             | 0.1378               | 4.14%                     |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 2                             | 0.2611               | 2.05%                     |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 5                             | 0.6899               | 2.59%                     |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 8                             | 1.0936               | 0.71%                     |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |
| 10                            | 1.3713               | 0.28%                     |                         |                                  |                              |                        |                 |                      |                       |                       |  |  |  |  |  |  |  |  |  |             |

|                               |                      |                           |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
|-------------------------------|----------------------|---------------------------|-------------------------|----------------------------------|------------------------------|------------------------|-----------------|----------------------|---------------------------|-----------------------|--|--|--|--|
| <b>Client:</b>                | CalPortland          | <b>Analysis Date:</b>     | 12/6/2023               |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| <b>Facility:</b>              | Redding              | <b>Analysis Location:</b> | Elmhurst Lab            |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| <b>Test Location:</b>         | Kiln-Mill On         | <b>Analyst:</b>           | JMG                     |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| <b>Project Number:</b>        | M234605              |                           |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| <b>Method:</b>                | 26A                  |                           |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| <b>Date Samples Received:</b> | 11/21/2023           |                           |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
|                               |                      |                           |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
|                               |                      |                           |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| <b>Standard ppm Cl</b>        | <b>Area</b>          | <b>Response Factor</b>    | <b>Calculated Value</b> | <b>Slope of Regression Curve</b> |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 1                             | 0.1264               | 0.1264                    | 0.97                    | 0.1308                           |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 2                             | 0.2504               | 0.1252                    | 1.92                    |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 5                             | 0.6542               | 0.1308                    | 5.00                    | <b>Response Factor Ave</b>       |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 8                             | 1.0781               | 0.1348                    | 8.25                    | 0.1307                           |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 10                            | 1.3636               | 0.1364                    | 10.43                   |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| Lot Number                    | Ricca 8209004        |                           |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
|                               | <b>R<sup>2</sup></b> | <b>0.9997</b>             |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
|                               |                      |                           |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| <b>Sample Number</b>          | <b>Sample Date</b>   | <b>Sample ID</b>          | <b>Sample Area</b>      | <b>PPM Cl</b>                    | <b>PPM X Dilution Factor</b> | <b>Dilution Factor</b> | <b>Total ml</b> | <b>mg Cl in soln</b> | <b>mg Cl2 in soln avg</b> | <b>ug Cl2 in soln</b> |  |  |  |  |
| 031                           | 11/14/2023           | DI Reagent Blank          | 0.0025                  | 0.0191                           | 0.0191                       | 1                      | 200             | 0.0038               |                           |                       |  |  |  |  |
| 031                           | 11/14/2023           | DI Reagent Blank          | 0.0005                  | 0.0038                           | 0.0038                       | 1                      | 200             | 0.0008               | 0.0023                    | 2.294394956           |  |  |  |  |
| 030                           | 11/14/2023           | NaOH Reagent Blank        | 0.0103                  | 0.0788                           | 0.0788                       | 1                      | 200             | 0.0158               |                           |                       |  |  |  |  |
| 030                           | 11/14/2023           | NaOH Reagent Blank        | 0.0107                  | 0.0818                           | 0.0818                       | 1                      | 200             | 0.0164               | 0.0161                    | 16.06076469           |  |  |  |  |
| 020                           | 11/14/2023           | Test 1B NaOH Imp          | 0.0045                  | 0.0344                           | 0.0344                       | 1                      | 269             | 0.0093               |                           |                       |  |  |  |  |
| 020                           | 11/14/2023           | Test 1B NaOH Imp          | 0.0050                  | 0.0382                           | 0.0382                       | 1                      | 269             | 0.0103               | 0.0098                    | 9.772210518           |  |  |  |  |
| 020                           | 11/14/2023           | Test 1B NaOH Imp          | 0.0046                  | 0.0352                           | 0.0352                       | 1                      | 269             | 0.0095               |                           |                       |  |  |  |  |
| 020                           | 11/14/2023           | Test 1B NaOH Imp          | 0.0038                  | 0.0291                           | 0.0291                       | 1                      | 269             | 0.0078               | 0.0086                    | 8.640691405           |  |  |  |  |
| 022                           | 11/14/2023           | Test 2B NaOH Imp          | 0.0067                  | 0.0512                           | 0.0512                       | 1                      | 287             | 0.0147               |                           |                       |  |  |  |  |
| 022                           | 11/14/2023           | Test 2B NaOH Imp          | 0.0058                  | 0.0444                           | 0.0444                       | 1                      | 287             | 0.0127               | 0.0137                    | 13.71856984           |  |  |  |  |
| 024                           | 11/14/2023           | Test 3B NaOH Imp          | 0.0009                  | 0.0069                           | 0.0069                       | 1                      | 241             | 0.0017               |                           |                       |  |  |  |  |
| 024                           | 11/14/2023           | Test 3B NaOH Imp          | 0.0009                  | 0.0069                           | 0.0069                       | 1                      | 241             | 0.0017               | 0.0017                    | 1.658847553           |  |  |  |  |
| 028                           | 11/14/2023           | Train B Train Blank       | 0.0163                  | 0.1247                           | 0.1247                       | 1                      | 279             | 0.0348               |                           |                       |  |  |  |  |
| 028                           | 11/14/2023           | Train B Train Blank       | 0.0157                  | 0.1201                           | 0.1201                       | 1                      | 279             | 0.0335               | 0.0341                    | 34.14059695           |  |  |  |  |
| <b>CCV ppm Cl</b>             | <b>Area</b>          | <b>PPM Cl</b>             |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 5 ppm ICV                     | 0.6732               | 5.1486                    |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 5 ppm CCV                     | 0.6685               | 5.1127                    |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 5 ppm CCV                     | 0.6758               | 5.1685                    |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
|                               |                      |                           |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| <b>Standard ppm Cl</b>        | <b>Area</b>          | <b>Difference</b>         |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 1                             | 0.1378               | 4.14%                     |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 2                             | 0.2611               | 2.05%                     |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 5                             | 0.6899               | 2.59%                     |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 8                             | 1.0936               | 0.71%                     |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |
| 10                            | 1.3713               | 0.28%                     |                         |                                  |                              |                        |                 |                      |                           |                       |  |  |  |  |

### Kiln-Mill Off

|   |   |
|---|---|
| Client: CalPortland<br>Facility: Redding<br>Test Location: Kiln-Mill Off<br>Project Number: M234605<br>Method: 26A<br>Date Samples Received: 11/21/2023 | Analysis Date: 12/5/2023<br>Analysis Location: Elmhurst<br>Analyst: JMG |
|---|---|

#### Train A

| Sampling Date        |       | 11/14/2023    | 11/14/2023       | 11/14/2023    | 11/14/2023        |     |     |
|----------------------|-------|---------------|------------------|---------------|-------------------|-----|-----|
|                      | UNITS | M26A DI Blank | M26A H2SO4 Blank | M26A H2SO4-R1 | M26A H2SO4-R1 Dup | RDL | MDL |
| Sulfuric Acid Volume | ml    | 200           | 200              | 404           | 404               |     |     |
| Hydrofluoric Acid    | ug    | <150          | <150             | <150          | <150              | 150 | 15  |

| Sampling Date        |       | 11/14/2023     | 11/14/2023     | 11/14/2023    |     |     |
|----------------------|-------|----------------|----------------|---------------|-----|-----|
|                      | UNITS | M26A- H2SO4 R2 | M26A- H2SO4 R3 | Field Blank A | RDL | MDL |
| Sulfuric Acid Volume | ml    | 421            | 380            | 294           |     |     |
| Hydrofluoric Acid    | ug    | <150           | <150           | <150          | 150 | 15  |

#### Train B

| Sampling Date        |       | 11/14/2023    | 11/14/2023       | 11/14/2023    | 11/14/2023        |     |     |
|----------------------|-------|---------------|------------------|---------------|-------------------|-----|-----|
|                      | UNITS | M26A DI Blank | M26A H2SO4 Blank | M26A H2SO4-R1 | M26A H2SO4-R1 Dup | RDL | MDL |
| Sulfuric Acid Volume | ml    | 200           | 200              | 421           | 421               |     |     |
| Hydrofluoric Acid    | ug    | <150          | <150             | <150          | <150              | 150 | 15  |

| Sampling Date        |       | 11/14/2023     | 11/14/2023     | 11/14/2023    |     |     |
|----------------------|-------|----------------|----------------|---------------|-----|-----|
|                      | UNITS | M26A- H2SO4 R2 | M26A- H2SO4 R3 | Field Blank B | RDL | MDL |
| Sulfuric Acid Volume | ml    | 396            | 356            | 294           |     |     |
| Hydrofluoric Acid    | ug    | <150           | <150           | <150          | 150 | 15  |





### Kiln-Mill Off

|   |   |
|---|---|
| Client: CalPortland<br>Facility: Redding<br>Test Location: Kiln-Mill Off<br>Project Number: M234605<br>Method: 26A<br>Date Samples Received: 11/21/2023 | Analysis Date: 12/5/2023<br>Analysis Location: Elmhurst<br>Analyst: JMG |
|---|---|

#### Train A

| Sampling Date           |       | 11/14/2023    | 11/14/2023      | 11/14/2023   | 11/14/2023       |     |     |
|-------------------------|-------|---------------|-----------------|--------------|------------------|-----|-----|
|                         | UNITS | M26A DI Blank | M26A NaOH Blank | M26A NaOH-R1 | M26A NaOH-R1 Dup | RDL | MDL |
| Sodium Hydroxide Volume | ml    | 200           | 200             | 278          | 278              |     |     |
| Chlorine                | ug    | <150          | <150            | <150         | <150             | 150 | 15  |

| Sampling Date           |       | 11/14/2023    | 11/14/2023    | 11/14/2023    |     |     |
|-------------------------|-------|---------------|---------------|---------------|-----|-----|
|                         | UNITS | M26A- NaOH R2 | M26A- NaOH R3 | Train A Blank | RDL | MDL |
| Sodium Hydroxide Volume | ml    | 255           | 276           | 279           |     |     |
| Chlorine                | ug    | <150          | <150          | <150          | 150 | 15  |

#### Train B

| Sampling Date           |       | 11/14/2023    | 11/14/2023      | 11/14/2023   | 11/14/2023       |     |     |
|-------------------------|-------|---------------|-----------------|--------------|------------------|-----|-----|
|                         | UNITS | M26A DI Blank | M26A NaOH Blank | M26A NaOH-R1 | M26A NaOH-R1 Dup | RDL | MDL |
| Sodium Hydroxide Volume | ml    | 200           | 200             | 274          | 274              |     |     |
| Chlorine                | ug    | <150          | <150            | <150         | <150             | 150 | 15  |

| Sampling Date           |       | 11/14/2023    | 11/14/2023    | 11/14/2023    |     |     |
|-------------------------|-------|---------------|---------------|---------------|-----|-----|
|                         | UNITS | M26A- NaOH R2 | M26A- NaOH R3 | Train B Blank | RDL | MDL |
| Sodium Hydroxide Volume | ml    | 255           | 277           | 279           |     |     |
| Chlorine                | ug    | <150          | <150          | <150          | 150 | 15  |





## Appendix F - Reference Method Test Data

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Test Method:** 26A  
**Test Engineer:** TRY  
**Test Technician:** KLJ

|                                    | <u>Run 1A</u> | <u>Run 2A</u> | <u>Run 3A</u> |
|------------------------------------|---------------|---------------|---------------|
| Temp ID:                           | CM45          | CM45          | CM45          |
| Meter ID:                          | CM45          | CM45          | CM45          |
| Pitot ID:                          | S8-031A       | S8-031A       | S8-031A       |
| Nozzle Diameter (Inches):          | 0.247         | 0.247         | 0.247         |
| Meter Calibration Date:            | 10/25/2023    | 10/25/2023    | 10/25/2023    |
| Meter Calibration Factor (Y):      | 0.992         | 0.992         | 0.992         |
| Meter Orifice Setting (Delta H):   | 1.729         | 1.729         | 1.729         |
| Nozzle Kit ID Number and Material: | Glass         | Glass         | Glass         |

**Leak Checks**

|                        |        |   |     |                   |        |   |     |                   |        |   |     |                   |
|------------------------|--------|---|-----|-------------------|--------|---|-----|-------------------|--------|---|-----|-------------------|
| Pre Pitot Leak Check   | 0.0    | @ | 3.5 | "H <sub>2</sub> O | 0.0    | @ | 4.0 | "H <sub>2</sub> O | 0.0    | @ | 4.5 | "H <sub>2</sub> O |
| Post Pitot Leak Check  | 0.0    | @ | 4.2 | "H <sub>2</sub> O | 0.0    | @ | 5.2 | "H <sub>2</sub> O | 0.0    | @ | 5.0 | "H <sub>2</sub> O |
| Pre Nozzle Leak Check  | 0.0000 | @ | 13  | "Hg               | 0.0000 | @ | 16  | "Hg               | 0.0000 | @ | 16  | "Hg               |
| Post Nozzle Leak Check | 0.0000 | @ | 10  | "Hg               | 0.0000 | @ | 12  | "Hg               | 0.0000 | @ | 10  | "Hg               |

Pitot Tube Coefficient: 0.820  
 Probe Length (Feet): 8.0  
 Probe Liner Material: Glass  
 Sample Plane: Horizontal  
 Port Length (Inches): 12.00  
 Port Size (Diameter, Inches): 4.00  
 Port Type: Nipple  
 Duct Shape: Circular  
 Diameter (Feet): 7  
  
 Duct Area (Square Feet): 38.485  
  
 Upstream Diameters: 16.0  
 Downstream Diameters: 11.0  
 Number of Ports Sampled: 2  
 Number of Points per Port: 6  
 Minutes per Point: 5.0  
 Minutes per Reading: 5.0  
 Total Number of Traverse Points: 12  
 Test Length (Minutes): 60  
 Train Type: Anderson Box  
 Source Condition: Mill On  
 Diluent Model/Serial Number: CAI 700/221018  
 Moisture Balance ID: LV3  
 # of Runs: 3



### Impinger Weight Sheet - Run 1A

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | 250.0                |
| 500                            | 500.0                |
| 750                            | 750.0                |

| IMPINGER CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4        | 794.1                | 746.5                  | 47.6                |
| 0.1N H2SO4        | 819.2                | 744.5                  | 74.7                |
| Empty             | 684.8                | 655.5                  | 29.3                |
| 0.1N NaOH         | 707.5                | 694.1                  | 13.4                |
| 0.1N NaOH         | 718.8                | 715.1                  | 3.7                 |
| Silica Gel        | 902.4                | 885.6                  | 16.8                |

|                     |                       |                    |
|---------------------|-----------------------|--------------------|
| 3,724.4             | 3,555.7               | 168.7              |
| <b>Liquid Final</b> | <b>Liquid Initial</b> | <b>Liquid Gain</b> |
| 902.4               | 885.6                 | 16.8               |
| <b>Silica Final</b> | <b>Silica Initial</b> | <b>Silica Gain</b> |

Run 2A - Method 26A

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Source Condition: Mill On

Date: 11/14/23  
 Start Time: 9:25  
 End Time: 10:29

DRY GAS METER CONDITIONS

ΔH: 4.21 in. H<sub>2</sub>O  
 Meter Temperature, Tm: 60.5 °F  
 Sqrt ΔP: 1.381 in. H<sub>2</sub>O  
 Stack Temperature, Ts: 230.2 °F  
 Meter Volume, Vm: 71.242 ft<sup>3</sup>  
 Meter Volume, Vmstd: 70.778 dscf  
 Meter Volume, Vwstd: 9.142 wscf  
 Isokinetic Variance: 102.8 %I  
 Test Length: 60.00 in mins.  
 Nozzle Diameter: 0.247 in inches  
 Barometric Pressure: 29.23 in Hg

STACK CONDITIONS

Static Pressure -0.80 in. H<sub>2</sub>O  
 Flue Pressure (Ps): 29.17 in. Hg. abs.  
 Carbon Dioxide: 13.70 %  
 Oxygen: 12.50 %  
 Nitrogen: 73.8 %  
 Gas Weight dry, Md: 30.692 lb/lb mole  
 Gas Weight wet, Ms: 29.240 lb/lb mole  
 Excess Air: --- %  
 Gas Velocity, Vs: 87.073 fps  
 Volumetric Flow: 201,058 acfm  
 Volumetric Flow: 132,811 dscfm  
 Volumetric Flow: 149,966 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3566.1 ml Silica Initial Wt. 893.9 grams  
 Final Impinger Content: 3736.8 ml Silica Final Wt. 917.3 grams  
 Impinger Difference: 170.7 ml Silica Difference: 23.4 grams  
 Total Water Gain: 194.1 Moisture, Bws: 0.114

| Port-Point No. | Clock Time | Velocity                     | Orifice                 | Actual                     | Stack   | Meter Temp |           | Pump       | Probe   | Filter       | Impinger     |
|----------------|------------|------------------------------|-------------------------|----------------------------|---------|------------|-----------|------------|---------|--------------|--------------|
|                |            | Head Δp in. H <sub>2</sub> O | ΔH in. H <sub>2</sub> O | Meter Vol. ft <sup>3</sup> | Temp °F | Inlet °F   | Outlet °F | Vacuum "Hg | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1            | 9:25:00    | 2.10                         | 4.60                    | 77.581                     | 229     | 59         | 57        | 6          | 256     | 256          | 54           |
| 1-2            | 9:30:00    | 1.90                         | 4.20                    | 83.790                     | 230     | 60         | 59        | 6          | 254     | 254          | 53           |
| 1-3            | 9:35:00    | 2.00                         | 4.40                    | 89.700                     | 230     | 61         | 59        | 5          | 256     | 255          | 54           |
| 1-4            | 9:40:00    | 1.80                         | 3.90                    | 95.780                     | 232     | 61         | 58        | 6          | 255     | 256          | 52           |
| 1-5            | 9:45:00    | 1.80                         | 4.00                    | 101.530                    | 231     | 60         | 60        | 6          | 253     | 256          | 53           |
| 1-6            | 9:50:00    | 1.90                         | 4.20                    | 107.290                    | 230     | 60         | 60        | 6          | 254     | 256          | 55           |
|                | 9:55:00    |                              |                         | 113.209                    |         |            |           |            |         |              |              |
| 2-1            | 9:59:00    | 1.80                         | 4.00                    | 113.209                    | 230     | 62         | 60        | 7          | 253     | 254          | 57           |
| 2-2            | 10:04:00   | 1.80                         | 4.00                    | 118.980                    | 229     | 61         | 61        | 7          | 254     | 255          | 58           |
| 2-3            | 10:09:00   | 1.90                         | 4.20                    | 124.760                    | 230     | 62         | 60        | 5          | 256     | 255          | 61           |
| 2-4            | 10:14:00   | 2.10                         | 4.60                    | 130.700                    | 230     | 62         | 62        | 5          | 257     | 257          | 58           |
| 2-5            | 10:19:00   | 2.00                         | 4.40                    | 136.950                    | 231     | 63         | 62        | 5          | 251     | 253          | 56           |
| 2-6            | 10:24:00   | 1.80                         | 4.00                    | 143.050                    | 230     | 62         | 61        | 6          | 254     | 254          | 53           |
|                | 10:29:00   |                              |                         | 148.823                    |         |            |           |            |         |              |              |

Total 1:00:00 71.242 61.1 59.9  
 Average 4.21 230.2 60.5 6  
 Min 3.90 229.0 57.0 5  
 Max 4.60 232.0 63.0 7

### Impinger Weight Sheet - Run 2A

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | 250.0                |
| 500                            | 500.0                |
| 750                            | 750.0                |

| IMPINGER CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4        | 795.5                | 765.5                  | 30.0                |
| 0.1N H2SO4        | 735.6                | 663.8                  | 71.8                |
| Empty             | 683.6                | 648.2                  | 35.4                |
| 0.1N NaOH         | 777.5                | 754.9                  | 22.6                |
| 0.1N NaOH         | 744.6                | 733.7                  | 10.9                |
| Silica Gel        | 917.3                | 893.9                  | 23.4                |

|                                       |   |                                    |
|---------------------------------------|---|------------------------------------|
| <u>3,736.8</u><br><b>Liquid Final</b> | <u>3,566.1</u><br><b>Liquid Initial</b> | <u>170.7</u><br><b>Liquid Gain</b> |
| <u>917.3</u><br><b>Silica Final</b>   | <u>893.9</u><br><b>Silica Initial</b>   | <u>23.4</u><br><b>Silica Gain</b>  |

Run 3A - Method 26A

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Source Condition: Mill On

Date: 11/14/23  
 Start Time: 10:50  
 End Time: 11:55

DRY GAS METER CONDITIONS

ΔH: 4.11 in. H<sub>2</sub>O  
 Meter Temperature, Tm: 63.4 °F  
 Sqrt ΔP: 1.369 in. H<sub>2</sub>O  
 Stack Temperature, Ts: 229.7 °F  
 Meter Volume, Vm: 71.113 ft<sup>3</sup>  
 Meter Volume, Vmstd: 70.239 dscf  
 Meter Volume, Vwstd: 8.789 wscf  
 Isokinetic Variance: 102.6 %I  
  
 Test Length: 60.00 in mins.  
 Nozzle Diameter: 0.247 in inches  
 Barometric Pressure: 29.23 in Hg

STACK CONDITIONS

Static Pressure -0.80 in. H<sub>2</sub>O  
 Flue Pressure (Ps): 29.17 in. Hg. abs.  
 Carbon Dioxide: 13.80 %  
 Oxygen: 12.50 %  
 Nitrogen: 73.7 %  
 Gas Weight dry, Md: 30.708 lb/lb mole  
 Gas Weight wet, Ms: 29.295 lb/lb mole  
 Excess Air: --- %  
 Gas Velocity, Vs: 86.208 fps  
 Volumetric Flow: 199,061 acfm  
 Volumetric Flow: 132,060 dscfm  
 Volumetric Flow: 148,584 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3569.7 ml Silica Initial Wt. 881.1 grams  
 Final Impinger Content: 3737.4 ml Silica Final Wt. 900.0 grams  
 Impinger Difference: 167.7 ml Silica Difference: 18.9 grams  
  
 Total Water Gain: 186.6 Moisture, Bws: 0.111

| Port-Point No. | Clock Time | Velocity                     | Orifice                 | Actual                     | Stack   | Meter Temp |           | Pump       | Probe   | Filter       | Impinger     |
|----------------|------------|------------------------------|-------------------------|----------------------------|---------|------------|-----------|------------|---------|--------------|--------------|
|                |            | Head Δp in. H <sub>2</sub> O | ΔH in. H <sub>2</sub> O | Meter Vol. ft <sup>3</sup> | Temp °F | Inlet °F   | Outlet °F | Vacuum "Hg | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1            | 10:50:00   | 1.90                         | 4.20                    | 49.325                     | 230     | 64         | 62        | 6          | 253     | 255          | 53           |
| 1-2            | 10:55:00   | 2.10                         | 4.10                    | 55.290                     | 229     | 63         | 62        | 5          | 255     | 254          | 51           |
| 1-3            | 11:00:00   | 1.80                         | 4.00                    | 61.550                     | 230     | 63         | 62        | 6          | 252     | 257          | 52           |
| 1-4            | 11:05:00   | 2.00                         | 4.40                    | 67.350                     | 230     | 63         | 63        | 6          | 254     | 256          | 52           |
| 1-5            | 11:10:00   | 1.80                         | 4.00                    | 73.460                     | 229     | 64         | 62        | 6          | 256     | 252          | 54           |
| 1-6            | 11:15:00   | 1.90                         | 4.20                    | 79.270                     | 229     | 64         | 63        | 6          | 254     | 251          | 57           |
|                | 11:20:00   |                              |                         | 85.242                     |         |            |           |            |         |              |              |
| 2-1            | 11:25:00   | 1.80                         | 4.00                    | 85.242                     | 229     | 65         | 62        | 6          | 255     | 256          | 59           |
| 2-2            | 11:30:00   | 1.80                         | 4.00                    | 91.050                     | 230     | 66         | 62        | 5          | 253     | 254          | 61           |
| 2-3            | 11:35:00   | 1.90                         | 4.20                    | 96.860                     | 230     | 65         | 63        | 6          | 254     | 255          | 60           |
| 2-4            | 11:40:00   | 1.90                         | 4.20                    | 102.840                    | 231     | 65         | 63        | 6          | 256     | 257          | 58           |
| 2-5            | 11:45:00   | 1.80                         | 4.00                    | 108.810                    | 230     | 64         | 63        | 7          | 255     | 256          | 54           |
| 2-6            | 11:50:00   | 1.80                         | 4.00                    | 114.620                    | 229     | 65         | 64        | 6          | 257     | 253          | 56           |
|                | 11:55:00   |                              |                         | 120.438                    |         |            |           |            |         |              |              |

Total 1:00:00 71.113 64.3 62.6  
 Average 4.11 229.7 63.4 6  
 Min 4.00 229.0 62.0 5  
 Max 4.40 231.0 66.0 7

### Impinger Weight Sheet - Run 3A

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | <u>250.0</u>         |
| 500                            | <u>500.0</u>         |
| 750                            | <u>750.0</u>         |

| IMPINGER CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4        | 822.3                | 740.0                  | 82.3                |
| 0.1N H2SO4        | 815.4                | 754.2                  | 61.2                |
| Empty             | 669.5                | 654.2                  | 15.3                |
| 0.1N NaOH         | 729.3                | 720.7                  | 8.6                 |
| 0.1N NaOH         | 700.9                | 700.6                  | 0.3                 |
| Silica Gel        | 900.0                | 881.1                  | 18.9                |

|                                       |   |                                    |
|---------------------------------------|---|------------------------------------|
| <u>3,737.4</u><br><b>Liquid Final</b> | <u>3,569.7</u><br><b>Liquid Initial</b> | <u>167.7</u><br><b>Liquid Gain</b> |
| <u>900.0</u><br><b>Silica Final</b>   | <u>881.1</u><br><b>Silica Initial</b>   | <u>18.9</u><br><b>Silica Gain</b>  |

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Test Method:** 26A  
**Test Engineer:** CLC  
**Test Technician:** KLJ

|                                    | <u>Run 1B</u> | <u>Run 2B</u> | <u>Run 3B</u> |
|------------------------------------|---------------|---------------|---------------|
| Temp ID:                           | CM18          | CM18          | CM18          |
| Meter ID:                          | CM18          | CM18          | CM18          |
| Pitot ID:                          | S8-032A       | S8-032A       | S8-032A       |
| Nozzle Diameter (Inches):          | 0.251         | 0.251         | 0.251         |
| Meter Calibration Date:            | 10/17/2023    | 10/17/2023    | 10/17/2023    |
| Meter Calibration Factor (Y):      | 0.987         | 0.987         | 0.987         |
| Meter Orifice Setting (Delta H):   | 1.533         | 1.533         | 1.533         |
| Nozzle Kit ID Number and Material: | Glass         | Glass         | Glass         |

**Leak Checks**

|                        |        |   |     |                   |        |   |     |                   |        |   |     |                   |
|------------------------|--------|---|-----|-------------------|--------|---|-----|-------------------|--------|---|-----|-------------------|
| Pre Pitot Leak Check   | 0.0    | @ | 3.2 | "H <sub>2</sub> O | 0.0    | @ | 4.3 | "H <sub>2</sub> O | 0.0    | @ | 4.3 | "H <sub>2</sub> O |
| Post Pitot Leak Check  | 0.0    | @ | 3.5 | "H <sub>2</sub> O | 0.0    | @ | 4.2 | "H <sub>2</sub> O | 0.0    | @ | 3.8 | "H <sub>2</sub> O |
| Pre Nozzle Leak Check  | 0.0000 | @ | 15  | "Hg               | 0.0000 | @ | 14  | "Hg               | 0.0000 | @ | 13  | "Hg               |
| Post Nozzle Leak Check | 0.0000 | @ | 16  | "Hg               | 0.0000 | @ | 8   | "Hg               | 0.0000 | @ | 16  | "Hg               |

Pitot Tube Coefficient: 0.822  
 Probe Length (Feet): 8.0  
 Probe Liner Material: Glass  
 Sample Plane: Horizontal  
 Port Length (Inches): 12.00  
 Port Size (Diameter, Inches): 4.00  
 Port Type: Nipple  
 Duct Shape: Circular  
 Diameter (Feet): 7  
 Duct Area (Square Feet): 38.485  
 Upstream Diameters: 16.0  
 Downstream Diameters: 11.0  
 Number of Ports Sampled: 2  
 Number of Points per Port: 6  
 Minutes per Point: 5.0  
 Minutes per Reading: 5.0  
 Total Number of Traverse Points: 12  
 Test Length (Minutes): 60  
 Train Type: Anderson Box  
 Source Condition: Mill On  
 Diluent Model/Serial Number: CAI 700/221018  
 Moisture Balance ID: LV3  
 # of Runs: 3

Run 1B - Method 26A

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Source Condition: Mill On

Date: 11/14/23  
 Start Time: 8:00  
 End Time: 9:05

DRY GAS METER CONDITIONS

STACK CONDITIONS

ΔH: 4.03 in. H<sub>2</sub>O  
 Meter Temperature, Tm: 60.0 °F  
 Sqrt ΔP: 1.384 in. H<sub>2</sub>O  
 Stack Temperature, Ts: 231.3 °F  
 Meter Volume, Vm: 74.178 ft<sup>3</sup>  
 Meter Volume, Vmstd: 73.356 dscf  
 Meter Volume, Vwstd: 9.161 wscf  
 Isokinetic Variance: 102.4 %I  
 Test Length: 60.00 in mins.  
 Nozzle Diameter: 0.251 in inches  
 Barometric Pressure: 29.23 in Hg

Static Pressure -0.80 in. H<sub>2</sub>O  
 Flue Pressure (Ps): 29.17 in. Hg. abs.  
 Carbon Dioxide: 13.40 %  
 Oxygen: 12.70 %  
 Nitrogen: 73.90 %  
 Gas Weight dry, Md: 30.652 lb/lb mole  
 Gas Weight wet, Ms: 29.247 lb/lb mole  
 Excess Air: --- %  
 Gas Velocity, Vs: 87.542 fps  
 Volumetric Flow: 202,140 acfm  
 Volumetric Flow: 133,824 dscfm  
 Volumetric Flow: 150,536 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3513.0 ml Silica Initial Wt. 859.1 grams  
 Final Impinger Content: 3686.1 ml Silica Final Wt. 880.5 grams  
 Impinger Difference: 173.1 ml Silica Difference: 21.4 grams  
 Total Water Gain: 194.5 Moisture, Bws: 0.111

| Port-Point No. | Clock Time | Velocity                        | Orifice                    | Actual                        | Stack      | Meter Temp  |              | Pump          | Probe      | Filter          | Impinger        |
|----------------|------------|---------------------------------|----------------------------|-------------------------------|------------|-------------|--------------|---------------|------------|-----------------|-----------------|
|                |            | Head Δp<br>in. H <sub>2</sub> O | ΔH<br>in. H <sub>2</sub> O | Meter Vol.<br>ft <sup>3</sup> | Temp<br>°F | Inlet<br>°F | Outlet<br>°F | Vacuum<br>"Hg | Temp<br>°F | Exit Temp<br>°F | Exit Temp<br>°F |
| 1-1            | 8:00:00    | 2.10                            | 4.40                       | 44.126                        | 232        | 58          | 57           | 5             | 253        | 251             | 55              |
| 1-2            | 8:05:00    | 2.00                            | 4.20                       | 50.570                        | 232        | 58          | 57           | 5             | 252        | 250             | 41              |
| 1-3            | 8:10:00    | 1.80                            | 3.80                       | 56.860                        | 232        | 60          | 58           | 5             | 252        | 251             | 48              |
| 1-4            | 8:15:00    | 2.00                            | 4.20                       | 62.840                        | 232        | 62          | 58           | 7             | 252        | 251             | 55              |
| 1-5            | 8:20:00    | 1.90                            | 4.00                       | 69.160                        | 231        | 63          | 58           | 7             | 252        | 251             | 56              |
| 1-6            | 8:25:00    | 1.80                            | 3.80                       | 75.330                        | 230        | 63          | 58           | 7             | 251        | 252             | 58              |
|                | 8:30:00    |                                 |                            | 81.307                        |            |             |              |               |            |                 |                 |
| 2-1            | 8:35:00    | 1.80                            | 3.80                       | 81.307                        | 232        | 62          | 58           | 7             | 251        | 252             | 58              |
| 2-2            | 8:40:00    | 1.90                            | 4.00                       | 87.560                        | 232        | 62          | 58           | 7             | 251        | 250             | 59              |
| 2-3            | 8:45:00    | 1.90                            | 4.00                       | 93.450                        | 231        | 63          | 58           | 7             | 251        | 250             | 59              |
| 2-4            | 8:50:00    | 1.80                            | 3.80                       | 99.600                        | 231        | 63          | 60           | 6             | 255        | 253             | 58              |
| 2-5            | 8:55:00    | 2.00                            | 4.20                       | 105.450                       | 230        | 63          | 59           | 5             | 253        | 254             | 57              |
| 2-6            | 9:00:00    | 2.00                            | 4.20                       | 111.900                       | 230        | 64          | 61           | 6             | 254        | 251             | 60              |
|                | 9:05:00    |                                 |                            | 118.304                       |            |             |              |               |            |                 |                 |
| Total          | 1:00:00    |                                 |                            | 74.178                        |            | 61.8        | 58.3         |               |            |                 |                 |
| Average        |            |                                 | 4.03                       |                               | 231.3      | 60.0        |              | 6             |            |                 |                 |
| Min            |            |                                 | 3.80                       |                               | 230.0      | 57.0        |              | 5             |            |                 |                 |
| Max            |            |                                 | 4.40                       |                               | 232.0      | 64.0        |              | 7             |            |                 |                 |

### Impinger Weight Sheet - Run 1B

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | <u>250.0</u>         |
| 500                            | <u>500.0</u>         |
| 750                            | <u>750.0</u>         |

| IMPINGER<br>CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|----------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4           | 775.0                | 709.0                  | 66.0                |
| 0.1N H2SO4           | 811.5                | 740.5                  | 71.0                |
| Empty                | 642.8                | 627.9                  | 14.9                |
| 0.1N NaOH            | 696.8                | 683.4                  | 13.4                |
| 0.1N NaOH            | 760.0                | 752.2                  | 7.8                 |
| Silica Gel           | 880.5                | 859.1                  | 21.4                |

|                                       |   |                                    |
|---------------------------------------|---|------------------------------------|
| <u>3,686.1</u><br><b>Liquid Final</b> | <u>3,513.0</u><br><b>Liquid Initial</b> | <u>173.1</u><br><b>Liquid Gain</b> |
| <u>880.5</u><br><b>Silica Final</b>   | <u>859.1</u><br><b>Silica Initial</b>   | <u>21.4</u><br><b>Silica Gain</b>  |

Run 2B - Method 26A

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Source Condition: Mill On

Date: 11/14/23  
 Start Time: 9:25  
 End Time: 10:29

DRY GAS METER CONDITIONS

ΔH: 4.08 in. H<sub>2</sub>O  
 Meter Temperature, Tm: 65.0 °F  
 Sqrt ΔP: 1.384 in. H<sub>2</sub>O  
 Stack Temperature, Ts: 230.4 °F  
 Meter Volume, Vm: 75.030 ft<sup>3</sup>  
 Meter Volume, Vmstd: 73.501 dscf  
 Meter Volume, Vwstd: 8.954 wscf  
 Isokinetic Variance: 102.4 %I  
 Test Length: 60.00 in mins.  
 Nozzle Diameter: 0.251 in inches  
 Barometric Pressure: 29.23 in Hg

STACK CONDITIONS

Static Pressure -0.80 in. H<sub>2</sub>O  
 Flue Pressure (Ps): 29.17 in. Hg. abs.  
 Carbon Dioxide: 13.70 %  
 Oxygen: 12.50 %  
 Nitrogen: 73.8 %  
 Gas Weight dry, Md: 30.692 lb/lb mole  
 Gas Weight wet, Ms: 29.314 lb/lb mole  
 Excess Air: --- %  
 Gas Velocity, Vs: 87.390 fps  
 Volumetric Flow: 201,789 acfm  
 Volumetric Flow: 134,118 dscfm  
 Volumetric Flow: 150,456 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3629.4 ml Silica Initial Wt. 869.4 grams  
 Final Impinger Content: 3800.5 ml Silica Final Wt. 888.4 grams  
 Impinger Difference: 171.1 ml Silica Difference: 19.0 grams  
 Total Water Gain: 190.1 Moisture, Bws: 0.109

| Port-Point No. | Clock Time | Velocity                     | Orifice                 | Actual                     | Stack   | Meter Temp |           | Pump       | Probe   | Filter       | Impinger     |
|----------------|------------|------------------------------|-------------------------|----------------------------|---------|------------|-----------|------------|---------|--------------|--------------|
|                |            | Head Δp in. H <sub>2</sub> O | ΔH in. H <sub>2</sub> O | Meter Vol. ft <sup>3</sup> | Temp °F | Inlet °F   | Outlet °F | Vacuum "Hg | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1            | 9:25:00    | 2.10                         | 4.45                    | 18.870                     | 230     | 62         | 60        | 5          | 251     | 250          | 55           |
| 1-2            | 9:30:00    | 1.80                         | 3.80                    | 25.350                     | 230     | 64         | 61        | 5          | 250     | 250          | 56           |
| 1-3            | 9:35:00    | 2.00                         | 4.20                    | 31.350                     | 230     | 66         | 61        | 5          | 252     | 250          | 56           |
| 1-4            | 9:40:00    | 1.90                         | 4.00                    | 37.700                     | 230     | 68         | 62        | 5          | 251     | 251          | 57           |
| 1-5            | 9:45:00    | 1.80                         | 3.80                    | 43.950                     | 231     | 68         | 62        | 5          | 251     | 250          | 58           |
| 1-6            | 9:50:00    | 2.00                         | 4.30                    | 50.500                     | 231     | 68         | 62        | 5          | 250     | 250          | 60           |
|                | 9:55:00    |                              |                         | 56.448                     |         |            |           |            |         |              |              |
| 2-1            | 9:59:00    | 1.90                         | 4.00                    | 56.448                     | 230     | 68         | 62        | 5          | 251     | 250          | 60           |
| 2-2            | 10:04:00   | 1.80                         | 3.90                    | 62.620                     | 230     | 69         | 63        | 5          | 251     | 250          | 61           |
| 2-3            | 10:09:00   | 1.80                         | 3.90                    | 68.750                     | 231     | 69         | 63        | 5          | 250     | 250          | 61           |
| 2-4            | 10:14:00   | 2.00                         | 4.30                    | 74.820                     | 231     | 70         | 64        | 5          | 251     | 250          | 62           |
| 2-5            | 10:19:00   | 2.00                         | 4.30                    | 81.200                     | 230     | 70         | 64        | 5          | 251     | 251          | 62           |
| 2-6            | 10:24:00   | 1.90                         | 4.00                    | 87.620                     | 231     | 71         | 64        | 5          | 250     | 250          | 63           |
|                | 10:29:00   |                              |                         | 93.900                     |         |            |           |            |         |              |              |

Total 1:00:00 75.030 67.8 62.3  
 Average 4.08 230.4 65.0 5  
 Min 3.80 230.0 60.0 5  
 Max 4.45 231.0 71.0 5

### Impinger Weight Sheet - Run 2B

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | <u>250.0</u>         |
| 500                            | <u>500.0</u>         |
| 750                            | <u>750.0</u>         |

| IMPINGER<br>CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|----------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4           | 805.5                | 754.3                  | 51.2                |
| 0.1N H2SO4           | 802.4                | 754.2                  | 48.2                |
| Empty                | 681.5                | 645.4                  | 36.1                |
| 0.1N NaOH            | 769.5                | 744.7                  | 24.8                |
| 0.1N NaOH            | 741.6                | 730.8                  | 10.8                |
| Silica Gel           | 888.4                | 869.4                  | 19.0                |

|                                       |   |                                    |
|---------------------------------------|---|------------------------------------|
| <u>3,800.5</u><br><b>Liquid Final</b> | <u>3,629.4</u><br><b>Liquid Initial</b> | <u>171.1</u><br><b>Liquid Gain</b> |
| <u>888.4</u><br><b>Silica Final</b>   | <u>869.4</u><br><b>Silica Initial</b>   | <u>19.0</u><br><b>Silica Gain</b>  |

Run 3B - Method 26A

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Source Condition: Mill On

Date: 11/14/23  
 Start Time: 10:50  
 End Time: 11:55

DRY GAS METER CONDITIONS

ΔH: 4.02 in. H<sub>2</sub>O  
 Meter Temperature, Tm: 65.0 °F  
 Sqrt ΔP: 1.372 in. H<sub>2</sub>O  
 Stack Temperature, Ts: 230.5 °F  
 Meter Volume, Vm: 74.355 ft<sup>3</sup>  
 Meter Volume, Vmstd: 72.840 dscf  
 Meter Volume, Vwstd: 8.869 wscf  
 Isokinetic Variance: 102.3 %I  
 Test Length: 60.00 in mins.  
 Nozzle Diameter: 0.251 in inches  
 Barometric Pressure: 29.23 in Hg

STACK CONDITIONS

Static Pressure -0.80 in. H<sub>2</sub>O  
 Flue Pressure (Ps): 29.17 in. Hg. abs.  
 Carbon Dioxide: 13.80 %  
 Oxygen: 12.50 %  
 Nitrogen: 73.7 %  
 Gas Weight dry, Md: 30.708 lb/lb mole  
 Gas Weight wet, Ms: 29.329 lb/lb mole  
 Excess Air: --- %  
 Gas Velocity, Vs: 86.619 fps  
 Volumetric Flow: 200,009 acfm  
 Volumetric Flow: 132,926 dscfm  
 Volumetric Flow: 149,111 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3510.3 ml Silica Initial Wt. 880.0 grams  
 Final Impinger Content: 3682.7 ml Silica Final Wt. 895.9 grams  
 Impinger Difference: 172.4 ml Silica Difference: 15.9 grams  
 Total Water Gain: 188.3 Moisture, Bws: 0.109

| Port-Point No. | Clock Time | Velocity                     | Orifice                 | Actual                     | Stack   | Meter Temp |           | Pump       | Probe   | Filter       | Impinger     |
|----------------|------------|------------------------------|-------------------------|----------------------------|---------|------------|-----------|------------|---------|--------------|--------------|
|                |            | Head Δp in. H <sub>2</sub> O | ΔH in. H <sub>2</sub> O | Meter Vol. ft <sup>3</sup> | Temp °F | Inlet °F   | Outlet °F | Vacuum "Hg | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1            | 10:50:00   | 1.80                         | 3.80                    | 94.365                     | 230     | 62         | 62        | 5          | 250     | 251          | 41           |
| 1-2            | 10:55:00   | 2.00                         | 4.30                    | 100.350                    | 230     | 64         | 62        | 5          | 250     | 250          | 44           |
| 1-3            | 11:00:00   | 1.90                         | 4.00                    | 106.756                    | 230     | 66         | 63        | 6          | 251     | 250          | 46           |
| 1-4            | 11:05:00   | 1.90                         | 4.00                    | 112.980                    | 231     | 67         | 63        | 7          | 251     | 251          | 48           |
| 1-5            | 11:10:00   | 2.00                         | 4.30                    | 119.200                    | 231     | 67         | 63        | 7          | 252     | 251          | 49           |
| 1-6            | 11:15:00   | 1.80                         | 3.90                    | 125.580                    | 231     | 68         | 64        | 7          | 251     | 251          | 50           |
|                | 11:20:00   |                              |                         | 131.660                    |         |            |           |            |         |              |              |
| 2-1            | 11:25:00   | 1.90                         | 4.00                    | 131.660                    | 230     | 66         | 63        | 5          | 250     | 250          | 51           |
| 2-2            | 11:30:00   | 1.80                         | 3.85                    | 137.880                    | 230     | 66         | 63        | 6          | 251     | 250          | 52           |
| 2-3            | 11:35:00   | 1.80                         | 3.85                    | 143.940                    | 231     | 67         | 64        | 7          | 251     | 251          | 54           |
| 2-4            | 11:40:00   | 2.00                         | 4.30                    | 150.000                    | 231     | 68         | 64        | 7          | 250     | 250          | 55           |
| 2-5            | 11:45:00   | 1.80                         | 3.80                    | 156.400                    | 230     | 69         | 64        | 7          | 251     | 250          | 56           |
| 2-6            | 11:50:00   | 1.90                         | 4.10                    | 162.450                    | 231     | 69         | 65        | 7          | 251     | 251          | 58           |
|                | 11:55:00   |                              |                         | 168.720                    |         |            |           |            |         |              |              |
| Total          | 1:00:00    |                              |                         | 74.355                     |         | 66.6       | 63.3      | 5.0        |         |              |              |
| Average        |            |                              | 4.02                    |                            | 230.5   | 65.0       |           | 6          |         |              |              |
| Min            |            |                              | 3.80                    |                            | 230.0   | 62.0       |           | 5          |         |              |              |
| Max            |            |                              | 4.30                    |                            | 231.0   | 69.0       |           | 7          |         |              |              |

### Impinger Weight Sheet - Run 3B

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | 250.0                |
| 500                            | 500.0                |
| 750                            | 750.0                |

| IMPINGER CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4        | 797.3                | 706.3                  | 91.0                |
| 0.1N H2SO4        | 802.8                | 751.6                  | 51.2                |
| Empty             | 638.0                | 629.2                  | 8.8                 |
| 0.1N NaOH         | 674.6                | 661.6                  | 13.0                |
| 0.1N NaOH         | 770.0                | 761.6                  | 8.4                 |
| Silica Gel        | 895.9                | 880.0                  | 15.9                |

|                     |                       |                    |
|---------------------|-----------------------|--------------------|
| 3,682.7             | 3,510.3               | 172.4              |
| <b>Liquid Final</b> | <b>Liquid Initial</b> | <b>Liquid Gain</b> |
| 895.9               | 880.0                 | 15.9               |
| <b>Silica Final</b> | <b>Silica Initial</b> | <b>Silica Gain</b> |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Test Location: Main Kiln Stack  
 Date: 11/14/23

Run 1

| Spectrum        | Time | FTIR Data    |              |             |             |               | Analyzer Data |              |
|-----------------|------|--------------|--------------|-------------|-------------|---------------|---------------|--------------|
|                 |      | H2O %        | CO2 % (wet)  | HCN ppmvw   | HF ppmvw    | Cell Temp     | Pressure      | O2 % (dry)   |
| RUN1_000201.LAB | 8:00 | 11.64        | 11.81        | 0.85        | 0.10        | 191.29        | 0.98          | 12.56        |
| RUN1_000202.LAB | 8:01 | 11.53        | 11.69        | 0.88        | 0.10        | 191.18        | 0.98          | 12.62        |
| RUN1_000203.LAB | 8:02 | 11.78        | 11.93        | 0.84        | 0.10        | 191.03        | 0.98          | 12.56        |
| RUN1_000204.LAB | 8:03 | 11.64        | 11.79        | 0.82        | 0.10        | 190.90        | 0.98          | 12.67        |
| RUN1_000205.LAB | 8:04 | 11.55        | 11.70        | 0.88        | 0.10        | 190.77        | 0.98          | 12.72        |
| RUN1_000206.LAB | 8:05 | 11.67        | 11.71        | 0.85        | 0.10        | 190.70        | 0.98          | 12.69        |
| RUN1_000207.LAB | 8:06 | 11.87        | 12.01        | 0.78        | 0.10        | 190.66        | 0.98          | 12.60        |
| RUN1_000208.LAB | 8:07 | 11.43        | 11.97        | 0.86        | 0.10        | 190.36        | 0.98          | 12.58        |
| RUN1_000209.LAB | 8:08 | 11.79        | 11.99        | 0.85        | 0.10        | 190.07        | 0.98          | 12.63        |
| RUN1_000210.LAB | 8:09 | 11.76        | 12.07        | 0.90        | 0.10        | 189.97        | 0.98          | 12.53        |
| RUN1_000211.LAB | 8:10 | 11.98        | 12.11        | 0.67        | 0.10        | 190.32        | 0.98          | 12.49        |
| RUN1_000212.LAB | 8:11 | 11.75        | 11.92        | 0.81        | 0.10        | 190.99        | 0.98          | 12.55        |
| RUN1_000213.LAB | 8:12 | 11.81        | 11.98        | 0.82        | 0.10        | 191.31        | 0.98          | 12.60        |
| RUN1_000214.LAB | 8:13 | 11.94        | 11.92        | 0.75        | 0.10        | 191.28        | 0.98          | 12.65        |
| RUN1_000215.LAB | 8:14 | 11.92        | 11.78        | 0.71        | 0.10        | 191.09        | 0.98          | 12.61        |
| RUN1_000216.LAB | 8:15 | 11.84        | 11.65        | 0.83        | 0.10        | 190.98        | 0.98          | 12.73        |
| RUN1_000217.LAB | 8:16 | 11.84        | 11.61        | 0.74        | 0.10        | 190.86        | 0.98          | 12.77        |
| RUN1_000218.LAB | 8:17 | 11.52        | 11.49        | 0.77        | 0.10        | 190.69        | 0.98          | 12.79        |
| RUN1_000219.LAB | 8:18 | 11.36        | 11.60        | 0.83        | 0.10        | 190.65        | 0.98          | 12.84        |
| RUN1_000220.LAB | 8:19 | 11.88        | 11.97        | 0.66        | 0.10        | 190.62        | 0.98          | 12.78        |
| RUN1_000221.LAB | 8:20 | 11.59        | 12.08        | 0.81        | 0.10        | 190.32        | 0.98          | 12.58        |
| RUN1_000222.LAB | 8:21 | 11.58        | 12.03        | 0.74        | 0.10        | 190.06        | 0.98          | 12.54        |
| RUN1_000223.LAB | 8:22 | 11.40        | 12.10        | 0.78        | 0.10        | 190.00        | 0.98          | 12.51        |
| RUN1_000224.LAB | 8:23 | 10.92        | 11.76        | 0.80        | 0.10        | 190.43        | 0.98          | 12.50        |
| RUN1_000225.LAB | 8:24 | 10.98        | 11.50        | 0.80        | 0.10        | 191.05        | 0.98          | 12.75        |
| RUN1_000226.LAB | 8:25 | 11.10        | 11.73        | 0.81        | 0.10        | 191.29        | 0.98          | 12.83        |
| RUN1_000227.LAB | 8:26 | 11.00        | 11.93        | 0.83        | 0.10        | 191.25        | 0.98          | 12.78        |
| RUN1_000228.LAB | 8:27 | 10.82        | 11.88        | 0.84        | 0.10        | 191.08        | 0.98          | 12.69        |
| RUN1_000229.LAB | 8:28 | 10.78        | 11.94        | 0.81        | 0.10        | 190.82        | 0.98          | 12.70        |
| RUN1_000230.LAB | 8:29 | 10.81        | 12.33        | 0.78        | 0.10        | 190.71        | 0.98          | 12.60        |
| RUN1_000231.LAB | 8:30 | 10.83        | 12.47        | 0.82        | 0.10        | 190.57        | 0.98          | 12.56        |
| RUN1_000232.LAB | 8:31 | 10.99        | 12.50        | 0.82        | 0.10        | 190.53        | 0.98          | 12.42        |
| RUN1_000233.LAB | 8:32 | 11.25        | 12.37        | 0.83        | 0.10        | 190.38        | 0.98          | 12.37        |
| RUN1_000234.LAB | 8:33 | 11.31        | 12.14        | 0.84        | 0.10        | 190.18        | 0.98          | 12.34        |
| RUN1_000235.LAB | 8:34 | 11.31        | 11.93        | 0.78        | 0.10        | 190.07        | 0.98          | 12.40        |
| RUN1_000236.LAB | 8:35 | 11.42        | 11.97        | 0.68        | 0.10        | 190.08        | 0.98          | 12.53        |
| RUN1_000237.LAB | 8:36 | 11.48        | 12.19        | 0.80        | 0.10        | 190.66        | 0.98          | 12.58        |
| RUN1_000238.LAB | 8:37 | 11.27        | 12.07        | 0.82        | 0.10        | 191.16        | 0.98          | 12.55        |
| RUN1_000239.LAB | 8:38 | 12.16        | 11.82        | 0.69        | 0.10        | 191.33        | 0.98          | 12.49        |
| RUN1_000240.LAB | 8:39 | 11.71        | 11.99        | 0.78        | 0.10        | 191.18        | 0.98          | 12.62        |
| RUN1_000241.LAB | 8:40 | 11.82        | 12.10        | 0.73        | 0.10        | 190.99        | 0.98          | 12.65        |
| RUN1_000242.LAB | 8:41 | 11.76        | 12.07        | 0.79        | 0.10        | 190.86        | 0.98          | 12.59        |
| RUN1_000243.LAB | 8:42 | 12.19        | 12.11        | 0.76        | 0.10        | 190.81        | 0.98          | 12.50        |
| RUN1_000244.LAB | 8:43 | 12.15        | 12.01        | 0.65        | 0.10        | 190.74        | 0.98          | 12.50        |
| RUN1_000245.LAB | 8:44 | 11.86        | 12.02        | 0.70        | 0.10        | 190.66        | 0.98          | 12.43        |
| RUN1_000246.LAB | 8:45 | 11.81        | 12.00        | 0.60        | 0.10        | 190.47        | 0.98          | 12.52        |
| RUN1_000247.LAB | 8:46 | 12.05        | 11.76        | 0.62        | 0.10        | 190.16        | 0.98          | 12.53        |
| RUN1_000248.LAB | 8:47 | 11.84        | 11.46        | 0.65        | 0.10        | 190.02        | 0.98          | 12.52        |
| RUN1_000249.LAB | 8:48 | 11.60        | 11.49        | 0.73        | 0.10        | 190.15        | 0.98          | 12.60        |
| RUN1_000250.LAB | 8:49 | 12.23        | 11.93        | 0.60        | 0.10        | 190.80        | 0.98          | 12.76        |
| RUN1_000251.LAB | 8:50 | 12.42        | 12.01        | 0.70        | 0.10        | 191.20        | 0.98          | 12.74        |
| RUN1_000252.LAB | 8:51 | 11.99        | 11.29        | 0.70        | 0.10        | 191.30        | 0.98          | 12.41        |
| RUN1_000253.LAB | 8:52 | 11.88        | 10.99        | 0.66        | 0.10        | 190.96        | 0.98          | 12.17        |
| RUN1_000254.LAB | 8:53 | 11.94        | 10.98        | 0.63        | 0.10        | 190.52        | 0.98          | 12.54        |
| RUN1_000255.LAB | 8:54 | 12.06        | 11.11        | 0.59        | 0.10        | 190.19        | 0.98          | 12.91        |
| RUN1_000256.LAB | 8:55 | 12.34        | 11.43        | 0.60        | 0.10        | 190.07        | 0.98          | 12.91        |
| RUN1_000257.LAB | 8:56 | 12.42        | 11.83        | 0.63        | 0.10        | 190.30        | 0.98          | 12.71        |
| RUN1_000258.LAB | 8:57 | 12.48        | 12.33        | 0.72        | 0.10        | 190.93        | 0.98          | 12.51        |
| RUN1_000259.LAB | 8:58 | 11.87        | 11.84        | 0.78        | 0.10        | 191.31        | 0.98          | 12.34        |
| RUN1_000260.LAB | 8:59 | 11.78        | 11.67        | 0.83        | 0.10        | 191.35        | 0.98          | 12.11        |
| <b>Average</b>  |      | <b>11.66</b> | <b>11.86</b> | <b>0.76</b> | <b>0.10</b> | <b>190.71</b> | <b>0.98</b>   | <b>12.59</b> |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Test Location: Main Kiln Stack  
 Date: 11/14/23

Run 2

| Spectrum        | Time  | FTIR Data    |              |             |             |               | Analyzer Data |              |
|-----------------|-------|--------------|--------------|-------------|-------------|---------------|---------------|--------------|
|                 |       | H2O %        | CO2 % (wet)  | HCN ppmvw   | HF ppmvw    | Cell Temp     | Pressure      | O2 % (dry)   |
| RUN2_000334.LAB | 9:25  | 11.95        | 12.5         | 0.65        | 0.10        | 190.4         | 0.98          | 12.29        |
| RUN2_000335.LAB | 9:26  | 12.25        | 12.2         | 0.65        | 0.10        | 190.1         | 0.98          | 12.33        |
| RUN2_000336.LAB | 9:27  | 12.21        | 12.0         | 0.60        | 0.10        | 190.0         | 0.98          | 12.40        |
| RUN2_000337.LAB | 9:28  | 11.79        | 12.1         | 0.73        | 0.10        | 190.4         | 0.98          | 12.44        |
| RUN2_000338.LAB | 9:29  | 11.86        | 11.9         | 0.63        | 0.10        | 191.0         | 0.98          | 12.42        |
| RUN2_000339.LAB | 9:30  | 11.59        | 12.0         | 0.83        | 0.10        | 191.2         | 0.98          | 12.48        |
| RUN2_000340.LAB | 9:31  | 11.62        | 11.9         | 0.78        | 0.10        | 191.2         | 0.98          | 12.54        |
| RUN2_000341.LAB | 9:32  | 11.36        | 11.9         | 0.88        | 0.10        | 191.1         | 0.98          | 12.57        |
| RUN2_000342.LAB | 9:33  | 11.36        | 11.9         | 0.84        | 0.10        | 190.9         | 0.98          | 12.53        |
| RUN2_000343.LAB | 9:34  | 11.31        | 11.8         | 0.76        | 0.10        | 190.8         | 0.98          | 12.58        |
| RUN2_000344.LAB | 9:35  | 11.24        | 11.9         | 0.77        | 0.10        | 190.7         | 0.98          | 12.58        |
| RUN2_000345.LAB | 9:36  | 11.08        | 12.1         | 0.77        | 0.10        | 190.6         | 0.98          | 12.54        |
| RUN2_000346.LAB | 9:37  | 11.30        | 12.2         | 0.80        | 0.10        | 190.6         | 0.98          | 12.51        |
| RUN2_000347.LAB | 9:38  | 10.88        | 12.3         | 0.82        | 0.10        | 190.5         | 0.98          | 12.46        |
| RUN2_000348.LAB | 9:39  | 10.96        | 12.3         | 0.80        | 0.10        | 190.3         | 0.98          | 12.40        |
| RUN2_000349.LAB | 9:40  | 11.44        | 12.3         | 0.79        | 0.10        | 190.1         | 0.98          | 12.33        |
| RUN2_000350.LAB | 9:41  | 11.50        | 12.3         | 0.75        | 0.10        | 190.0         | 0.98          | 12.34        |
| RUN2_000351.LAB | 9:42  | 11.18        | 12.4         | 0.81        | 0.10        | 190.2         | 0.98          | 12.37        |
| RUN2_000352.LAB | 9:43  | 11.66        | 12.0         | 0.86        | 0.10        | 190.9         | 0.98          | 12.36        |
| RUN2_000353.LAB | 9:44  | 11.57        | 11.7         | 0.77        | 0.10        | 191.3         | 0.98          | 12.47        |
| RUN2_000354.LAB | 9:45  | 11.07        | 11.6         | 0.86        | 0.10        | 191.3         | 0.98          | 12.59        |
| RUN2_000355.LAB | 9:46  | 11.21        | 11.7         | 0.83        | 0.10        | 191.2         | 0.98          | 12.74        |
| RUN2_000356.LAB | 9:47  | 11.85        | 12.0         | 0.70        | 0.10        | 191.0         | 0.98          | 12.66        |
| RUN2_000357.LAB | 9:48  | 11.61        | 12.2         | 0.80        | 0.10        | 190.9         | 0.98          | 12.42        |
| RUN2_000358.LAB | 9:49  | 11.63        | 12.1         | 0.82        | 0.10        | 190.8         | 0.98          | 12.28        |
| RUN2_000359.LAB | 9:50  | 11.81        | 12.2         | 0.76        | 0.10        | 190.7         | 0.98          | 12.34        |
| RUN2_000360.LAB | 9:51  | 11.39        | 12.5         | 0.77        | 0.10        | 190.5         | 0.98          | 12.31        |
| RUN2_000361.LAB | 9:52  | 11.48        | 12.6         | 0.80        | 0.10        | 190.3         | 0.98          | 12.22        |
| RUN2_000362.LAB | 9:53  | 11.72        | 12.4         | 0.69        | 0.10        | 190.1         | 0.98          | 12.25        |
| RUN2_000363.LAB | 9:54  | 12.03        | 12.3         | 0.62        | 0.10        | 190.1         | 0.98          | 12.18        |
| RUN2_000364.LAB | 9:55  | 11.50        | 12.5         | 0.84        | 0.10        | 190.4         | 0.98          | 12.30        |
| RUN2_000365.LAB | 9:56  | 11.27        | 12.4         | 0.86        | 0.10        | 190.9         | 0.98          | 12.34        |
| RUN2_000366.LAB | 9:57  | 11.71        | 12.1         | 0.81        | 0.10        | 191.2         | 0.98          | 12.27        |
| RUN2_000367.LAB | 9:58  | 11.35        | 12.1         | 0.84        | 0.10        | 191.2         | 0.98          | 12.31        |
| RUN2_000368.LAB | 9:59  | 11.22        | 12.0         | 0.83        | 0.10        | 191.1         | 0.98          | 12.42        |
| RUN2_000369.LAB | 10:00 | 11.45        | 11.9         | 0.77        | 0.10        | 190.9         | 0.98          | 12.44        |
| RUN2_000370.LAB | 10:01 | 11.03        | 12.0         | 0.85        | 0.10        | 190.8         | 0.98          | 12.47        |
| RUN2_000371.LAB | 10:02 | 10.84        | 12.1         | 0.84        | 0.10        | 190.7         | 0.98          | 12.57        |
| RUN2_000372.LAB | 10:03 | 11.22        | 12.1         | 0.81        | 0.10        | 190.5         | 0.98          | 12.57        |
| RUN2_000373.LAB | 10:04 | 11.58        | 12.1         | 0.68        | 0.10        | 190.2         | 0.98          | 12.53        |
| RUN2_000374.LAB | 10:05 | 11.17        | 12.2         | 0.73        | 0.10        | 190.1         | 0.98          | 12.48        |
| RUN2_000375.LAB | 10:06 | 11.28        | 12.2         | 0.79        | 0.10        | 190.2         | 0.98          | 12.42        |
| RUN2_000376.LAB | 10:07 | 11.52        | 12.4         | 0.86        | 0.10        | 190.8         | 0.98          | 12.38        |
| RUN2_000377.LAB | 10:08 | 11.68        | 12.5         | 0.77        | 0.10        | 191.2         | 0.98          | 12.39        |
| RUN2_000378.LAB | 10:09 | 11.57        | 12.2         | 0.85        | 0.10        | 191.3         | 0.98          | 12.36        |
| RUN2_000379.LAB | 10:10 | 11.55        | 12.2         | 0.82        | 0.10        | 191.2         | 0.98          | 12.23        |
| RUN2_000380.LAB | 10:11 | 11.25        | 12.3         | 0.87        | 0.10        | 191.1         | 0.98          | 12.28        |
| RUN2_000381.LAB | 10:12 | 11.62        | 12.1         | 0.81        | 0.10        | 191.0         | 0.98          | 12.37        |
| RUN2_000382.LAB | 10:13 | 11.04        | 12.2         | 0.83        | 0.10        | 190.8         | 0.98          | 12.31        |
| RUN2_000383.LAB | 10:14 | 11.63        | 12.1         | 0.80        | 0.10        | 190.5         | 0.98          | 12.41        |
| RUN2_000384.LAB | 10:15 | 11.72        | 12.2         | 0.77        | 0.10        | 190.2         | 0.98          | 12.44        |
| RUN2_000385.LAB | 10:16 | 11.72        | 12.3         | 0.77        | 0.10        | 190.2         | 0.98          | 12.34        |
| RUN2_000386.LAB | 10:17 | 11.54        | 12.2         | 0.83        | 0.10        | 190.8         | 0.98          | 12.32        |
| RUN2_000387.LAB | 10:18 | 12.03        | 12.2         | 0.78        | 0.10        | 191.2         | 0.98          | 12.30        |
| RUN2_000388.LAB | 10:19 | 12.31        | 12.2         | 0.75        | 0.10        | 191.3         | 0.98          | 12.21        |
| RUN2_000389.LAB | 10:20 | 12.35        | 12.2         | 0.73        | 0.10        | 191.2         | 0.98          | 12.29        |
| RUN2_000390.LAB | 10:21 | 11.82        | 12.5         | 0.81        | 0.10        | 191.0         | 0.98          | 12.26        |
| RUN2_000391.LAB | 10:22 | 12.38        | 12.4         | 0.71        | 0.10        | 190.9         | 0.98          | 12.22        |
| RUN2_000392.LAB | 10:23 | 11.95        | 12.4         | 0.71        | 0.10        | 190.8         | 0.98          | 12.20        |
| RUN2_000393.LAB | 10:24 | 11.75        | 12.3         | 0.82        | 0.10        | 190.7         | 0.98          | 12.13        |
| <b>Average</b>  |       | <b>11.55</b> | <b>12.16</b> | <b>0.78</b> | <b>0.10</b> | <b>190.73</b> | <b>0.98</b>   | <b>12.39</b> |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Test Location: Main Kiln Stack  
 Date: 11/14/23

Run 3

| Spectrum        | Time  | FTIR Data    |              |             |             |               | Analyzer Data |              |
|-----------------|-------|--------------|--------------|-------------|-------------|---------------|---------------|--------------|
|                 |       | H2O %        | CO2 % (wet)  | HCN ppmvw   | HF ppmvw    | Cell Temp     | Pressure      | O2 % (dry)   |
| RUN3_000453.LAB | 10:50 | 11.74        | 12.2         | 0.74        | 0.10        | 190.2         | 0.98          | 12.27        |
| RUN3_000454.LAB | 10:51 | 11.39        | 12.4         | 0.77        | 0.10        | 190.1         | 0.98          | 12.24        |
| RUN3_000455.LAB | 10:52 | 11.47        | 12.4         | 0.84        | 0.10        | 190.3         | 0.98          | 12.23        |
| RUN3_000456.LAB | 10:53 | 11.67        | 12.3         | 0.80        | 0.10        | 190.9         | 0.98          | 12.32        |
| RUN3_000457.LAB | 10:54 | 11.67        | 12.1         | 0.80        | 0.10        | 191.3         | 0.98          | 12.45        |
| RUN3_000458.LAB | 10:55 | 11.05        | 12.1         | 0.90        | 0.10        | 191.3         | 0.98          | 12.49        |
| RUN3_000459.LAB | 10:56 | 11.22        | 11.7         | 0.85        | 0.10        | 191.1         | 0.98          | 12.68        |
| RUN3_000460.LAB | 10:57 | 11.17        | 11.7         | 0.87        | 0.10        | 191.0         | 0.98          | 12.65        |
| RUN3_000461.LAB | 10:58 | 11.04        | 11.8         | 0.85        | 0.10        | 190.9         | 0.98          | 12.61        |
| RUN3_000462.LAB | 10:59 | 10.82        | 11.9         | 0.86        | 0.10        | 190.8         | 0.98          | 12.62        |
| RUN3_000463.LAB | 11:00 | 11.13        | 12.0         | 0.82        | 0.10        | 190.7         | 0.98          | 12.58        |
| RUN3_000464.LAB | 11:01 | 10.79        | 12.2         | 0.85        | 0.10        | 190.5         | 0.98          | 12.46        |
| RUN3_000465.LAB | 11:02 | 11.36        | 12.2         | 0.83        | 0.10        | 190.5         | 0.97          | 12.46        |
| RUN3_000466.LAB | 11:03 | 10.75        | 12.2         | 0.84        | 0.10        | 190.5         | 0.98          | 12.46        |
| RUN3_000467.LAB | 11:04 | 10.24        | 12.2         | 0.85        | 0.10        | 190.3         | 0.98          | 12.47        |
| RUN3_000468.LAB | 11:05 | 10.60        | 12.2         | 0.86        | 0.10        | 190.1         | 0.98          | 12.45        |
| RUN3_000469.LAB | 11:06 | 11.15        | 12.3         | 0.76        | 0.10        | 190.1         | 0.98          | 12.45        |
| RUN3_000470.LAB | 11:07 | 12.26        | 12.4         | 0.63        | 0.10        | 190.5         | 0.97          | 12.27        |
| RUN3_000471.LAB | 11:08 | 12.10        | 12.4         | 0.73        | 0.10        | 191.1         | 0.97          | 12.20        |
| RUN3_000472.LAB | 11:09 | 12.63        | 12.2         | 0.73        | 0.10        | 191.3         | 0.97          | 12.34        |
| RUN3_000473.LAB | 11:10 | 12.46        | 12.1         | 0.76        | 0.10        | 191.3         | 0.97          | 12.40        |
| RUN3_000474.LAB | 11:11 | 12.41        | 12.1         | 0.73        | 0.10        | 191.1         | 0.97          | 12.45        |
| RUN3_000475.LAB | 11:12 | 12.89        | 11.9         | 0.71        | 0.10        | 191.0         | 0.97          | 12.44        |
| RUN3_000476.LAB | 11:13 | 12.32        | 12.1         | 0.73        | 0.10        | 190.9         | 0.97          | 12.45        |
| RUN3_000477.LAB | 11:14 | 12.18        | 12.0         | 0.71        | 0.10        | 190.9         | 0.98          | 12.38        |
| RUN3_000478.LAB | 11:15 | 11.67        | 12.0         | 0.87        | 0.10        | 190.8         | 0.98          | 12.46        |
| RUN3_000479.LAB | 11:16 | 11.30        | 12.0         | 0.83        | 0.10        | 190.7         | 0.98          | 12.55        |
| RUN3_000480.LAB | 11:17 | 11.03        | 12.0         | 0.79        | 0.10        | 190.7         | 0.98          | 12.58        |
| RUN3_000481.LAB | 11:18 | 10.94        | 12.0         | 0.91        | 0.10        | 190.7         | 0.98          | 12.60        |
| RUN3_000482.LAB | 11:19 | 11.00        | 12.0         | 0.85        | 0.10        | 190.6         | 0.98          | 12.54        |
| RUN3_000483.LAB | 11:20 | 10.61        | 12.1         | 0.86        | 0.10        | 190.6         | 0.98          | 12.55        |
| RUN3_000484.LAB | 11:21 | 10.57        | 12.4         | 0.86        | 0.10        | 190.6         | 0.98          | 12.56        |
| RUN3_000485.LAB | 11:22 | 10.61        | 12.4         | 0.88        | 0.10        | 190.6         | 0.97          | 12.44        |
| RUN3_000486.LAB | 11:23 | 10.63        | 12.4         | 0.85        | 0.10        | 190.5         | 0.98          | 12.44        |
| RUN3_000487.LAB | 11:24 | 10.54        | 12.5         | 0.87        | 0.10        | 190.6         | 0.98          | 12.44        |
| RUN3_000488.LAB | 11:25 | 10.49        | 12.4         | 0.91        | 0.10        | 190.5         | 0.97          | 12.37        |
| RUN3_000489.LAB | 11:26 | 10.74        | 12.4         | 0.84        | 0.10        | 190.6         | 0.97          | 12.38        |
| RUN3_000490.LAB | 11:27 | 10.89        | 12.6         | 0.86        | 0.10        | 190.6         | 0.97          | 12.41        |
| RUN3_000491.LAB | 11:28 | 11.21        | 12.3         | 0.83        | 0.10        | 190.5         | 0.97          | 12.29        |
| RUN3_000492.LAB | 11:29 | 11.37        | 12.4         | 0.90        | 0.10        | 190.5         | 0.97          | 12.35        |
| RUN3_000493.LAB | 11:30 | 11.29        | 12.4         | 0.82        | 0.10        | 190.5         | 0.97          | 12.29        |
| RUN3_000494.LAB | 11:31 | 11.48        | 12.5         | 0.84        | 0.10        | 190.5         | 0.97          | 12.25        |
| RUN3_000495.LAB | 11:32 | 11.79        | 12.4         | 0.80        | 0.10        | 190.5         | 0.97          | 12.16        |
| RUN3_000496.LAB | 11:33 | 11.87        | 12.4         | 0.67        | 0.10        | 190.6         | 0.97          | 12.19        |
| RUN3_000497.LAB | 11:34 | 11.86        | 12.5         | 0.74        | 0.10        | 190.6         | 0.97          | 12.30        |
| RUN3_000498.LAB | 11:35 | 11.86        | 12.1         | 0.70        | 0.10        | 190.6         | 0.97          | 12.32        |
| RUN3_000499.LAB | 11:36 | 12.12        | 12.0         | 0.69        | 0.10        | 190.6         | 0.97          | 12.31        |
| RUN3_000500.LAB | 11:37 | 12.12        | 12.2         | 0.74        | 0.10        | 190.6         | 0.97          | 12.45        |
| RUN3_000501.LAB | 11:38 | 12.13        | 12.4         | 0.71        | 0.10        | 190.6         | 0.97          | 12.40        |
| RUN3_000502.LAB | 11:39 | 11.87        | 12.6         | 0.77        | 0.10        | 190.6         | 0.97          | 12.31        |
| RUN3_000503.LAB | 11:40 | 11.80        | 12.6         | 0.80        | 0.10        | 190.6         | 0.97          | 12.20        |
| RUN3_000504.LAB | 11:41 | 11.83        | 12.4         | 0.81        | 0.10        | 190.6         | 0.97          | 12.14        |
| RUN3_000505.LAB | 11:42 | 11.92        | 12.6         | 0.71        | 0.10        | 190.6         | 0.97          | 12.23        |
| RUN3_000506.LAB | 11:43 | 12.04        | 12.3         | 0.70        | 0.10        | 190.6         | 0.97          | 12.27        |
| RUN3_000507.LAB | 11:44 | 11.97        | 12.3         | 0.71        | 0.10        | 190.6         | 0.97          | 12.20        |
| RUN3_000508.LAB | 11:45 | 11.78        | 12.2         | 0.65        | 0.10        | 190.6         | 0.97          | 12.29        |
| RUN3_000509.LAB | 11:46 | 11.88        | 12.3         | 0.71        | 0.10        | 190.6         | 0.97          | 12.32        |
| RUN3_000510.LAB | 11:47 | 11.70        | 12.1         | 0.85        | 0.10        | 190.7         | 0.97          | 12.35        |
| RUN3_000511.LAB | 11:48 | 11.42        | 12.0         | 0.90        | 0.10        | 190.7         | 0.97          | 12.33        |
| RUN3_000512.LAB | 11:49 | 11.49        | 12.3         | 0.86        | 0.10        | 190.8         | 0.97          | 12.36        |
| <b>Average</b>  |       | <b>11.47</b> | <b>12.23</b> | <b>0.80</b> | <b>0.10</b> | <b>190.66</b> | <b>0.97</b>   | <b>12.39</b> |

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Test Method:** 26A  
**Test Engineer:** TRY  
**Test Technician:** CLC

|                                    | <u>Run 1A</u> | <u>Run 2A</u> | <u>Run 3A</u> |
|------------------------------------|---------------|---------------|---------------|
| Temp ID:                           | CM45          | CM45          | CM45          |
| Meter ID:                          | CM45          | CM45          | CM45          |
| Pitot ID:                          | S8-031A       | S8-031A       | S8-031A       |
| Nozzle Diameter (Inches):          | 0.247         | 0.247         | 0.247         |
| Meter Calibration Date:            | 10/25/2023    | 10/25/2023    | 10/25/2023    |
| Meter Calibration Factor (Y):      | 0.992         | 0.992         | 0.992         |
| Meter Orifice Setting (Delta H):   | 1.729         | 1.729         | 1.729         |
| Nozzle Kit ID Number and Material: | Glass         | Glass         | Glass         |

**Leak Checks**

|                        |        |   |     |                   |        |   |     |                   |        |   |     |                   |
|------------------------|--------|---|-----|-------------------|--------|---|-----|-------------------|--------|---|-----|-------------------|
| Pre Pitot Leak Check   | 0.0    | @ | 3.8 | "H <sub>2</sub> O | 0.0    | @ | 4.6 | "H <sub>2</sub> O | 0.0    | @ | 4.8 | "H <sub>2</sub> O |
| Post Pitot Leak Check  | 0.0    | @ | 4.6 | "H <sub>2</sub> O | 0.0    | @ | 5.2 | "H <sub>2</sub> O | 0.0    | @ | 5.6 | "H <sub>2</sub> O |
| Pre Nozzle Leak Check  | 0.0000 | @ | 15  | "Hg               | 0.0000 | @ | 18  | "Hg               | 0.0000 | @ | 15  | "Hg               |
| Post Nozzle Leak Check | 0.0000 | @ | 11  | "Hg               | 0.0000 | @ | 12  | "Hg               | 0.0000 | @ | 10  | "Hg               |

Pitot Tube Coefficient: 0.820  
 Probe Length (Feet): 8.0  
 Probe Liner Material: Glass  
 Sample Plane: Horizontal  
 Port Length (Inches): 12.00  
 Port Size (Diameter, Inches): 4.00  
 Port Type: Nipple  
 Duct Shape: Circular  
 Diameter (Feet): 7  
  
 Duct Area (Square Feet): 38.485  
  
 Upstream Diameters: 16.0  
 Downstream Diameters: 11.0  
 Number of Ports Sampled: 4  
 Number of Points per Port: 3  
 Minutes per Point: 5.0  
 Minutes per Reading: 5.0  
 Total Number of Traverse Points: 12  
 Test Length (Minutes): 60  
 Train Type: Anderson Box  
 Source Condition: Mill Off  
 Diluent Model/Serial Number: CAI 700/221018  
 Moisture Balance ID: LV3  
 # of Runs: 3

Run 1A - Method 26A

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Source Condition: Mill Off

Date: 11/14/23  
 Start Time: 12:50  
 End Time: 13:55

DRY GAS METER CONDITIONS

STACK CONDITIONS

ΔH: 3.58 in. H<sub>2</sub>O  
 Meter Temperature, Tm: 70.1 °F  
 Sqrt ΔP: 1.319 in. H<sub>2</sub>O  
 Stack Temperature, Ts: 279.5 °F  
 Meter Volume, Vm: 66.982 ft<sup>3</sup>  
 Meter Volume, Vmstd: 65.240 dscf  
 Meter Volume, Vwstd: 8.412 wscf  
 Isokinetic Variance: 103.2 %I  
 Test Length: 60.00 in mins.  
 Nozzle Diameter: 0.247 in inches  
 Barometric Pressure: 29.23 in Hg

Static Pressure -0.80 in. H<sub>2</sub>O  
 Flue Pressure (Ps): 29.17 in. Hg. abs.  
 Carbon Dioxide: 16.20 %  
 Oxygen: 11.20 %  
 Nitrogen: 72.60 %  
 Gas Weight dry, Md: 31.040 lb/lb mole  
 Gas Weight wet, Ms: 29.551 lb/lb mole  
 Excess Air: --- %  
 Gas Velocity, Vs: 85.662 fps  
 Volumetric Flow: 197,799 acfm  
 Volumetric Flow: 121,966 dscfm  
 Volumetric Flow: 137,693 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3572.1 ml Silica Initial Wt. 896.2 grams  
 Final Impinger Content: 3729.9 ml Silica Final Wt. 917.0 grams  
 Impinger Difference: 157.8 ml Silica Difference: 20.8 grams  
 Total Water Gain: 178.6 Moisture, Bws: 0.114

| Port-Point No. | Clock Time | Velocity                        | Orifice                    | Actual                        | Stack      | Meter Temp  |              | Pump          | Probe      | Filter          | Impinger        |
|----------------|------------|---------------------------------|----------------------------|-------------------------------|------------|-------------|--------------|---------------|------------|-----------------|-----------------|
|                |            | Head Δp<br>in. H <sub>2</sub> O | ΔH<br>in. H <sub>2</sub> O | Meter Vol.<br>ft <sup>3</sup> | Temp<br>°F | Inlet<br>°F | Outlet<br>°F | Vacuum<br>"Hg | Temp<br>°F | Exit Temp<br>°F | Exit Temp<br>°F |
| 1-1            | 12:50:00   | 1.70                            | 3.10                       | 21.270                        | 278        | 67          | 65           | 6             | 253        | 255             | 60              |
| 1-2            | 12:55:00   | 1.70                            | 3.50                       | 26.750                        | 279        | 67          | 65           | 6             | 255        | 257             | 58              |
| 1-3            | 13:00:00   | 1.80                            | 3.30                       | 32.230                        | 277        | 66          | 66           | 7             | 256        | 254             | 57              |
| 1-4            | 13:05:00   | 1.60                            | 3.30                       | 37.870                        | 278        | 67          | 66           | 6             | 254        | 256             | 54              |
| 1-5            | 13:10:00   | 1.80                            | 3.80                       | 43.190                        | 277        | 68          | 66           | 7             | 255        | 251             | 56              |
| 1-6            | 13:15:00   | 1.90                            | 4.00                       | 48.840                        | 277        | 68          | 65           | 5             | 253        | 253             | 58              |
|                | 13:20:00   |                                 |                            | 54.648                        |            |             |              |               |            |                 |                 |
| 2-1            | 13:25:00   | 1.80                            | 3.80                       | 54.648                        | 281        | 74          | 72           | 6             | 253        | 254             | 61              |
| 2-2            | 13:30:00   | 1.60                            | 3.30                       | 60.350                        | 282        | 73          | 73           | 5             | 252        | 253             | 58              |
| 2-3            | 13:35:00   | 1.70                            | 3.60                       | 65.720                        | 282        | 75          | 73           | 5             | 255        | 254             | 59              |
| 2-4            | 13:40:00   | 1.70                            | 3.60                       | 71.270                        | 281        | 75          | 73           | 5             | 254        | 255             | 59              |
| 2-5            | 13:45:00   | 1.80                            | 3.80                       | 76.820                        | 280        | 74          | 74           | 6             | 257        | 255             | 60              |
| 2-6            | 13:50:00   | 1.80                            | 3.80                       | 82.530                        | 282        | 76          | 74           | 6             | 256        | 254             | 58              |
|                | 13:55:00   |                                 |                            | 88.252                        |            |             |              |               |            |                 |                 |
| Total          | 1:00:00    |                                 |                            | 66.982                        |            | 70.8        | 69.3         |               |            |                 |                 |
| Average        |            |                                 | 3.58                       |                               | 279.5      | 70.1        |              | 6             |            |                 |                 |
| Min            |            |                                 | 3.10                       |                               | 277.0      | 65.0        |              | 5             |            |                 |                 |
| Max            |            |                                 | 4.00                       |                               | 282.0      | 76.0        |              | 7             |            |                 |                 |

### Impinger Weight Sheet - Run 1A

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | <u>250.0</u>         |
| 500                            | <u>500.0</u>         |
| 750                            | <u>750.0</u>         |

| IMPINGER CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4        | 807.3                | 769.0                  | 38.3                |
| 0.1N H2SO4        | 725.0                | 660.0                  | 65.0                |
| Empty             | 676.9                | 648.0                  | 28.9                |
| 0.1N NaOH         | 776.3                | 757.1                  | 19.2                |
| 0.1N NaOH         | 744.4                | 738.0                  | 6.4                 |
| Silica Gel        | 917.0                | 896.2                  | 20.8                |

|                                       |   |                                    |
|---------------------------------------|---|------------------------------------|
| <u>3,729.9</u><br><b>Liquid Final</b> | <u>3,572.1</u><br><b>Liquid Initial</b> | <u>157.8</u><br><b>Liquid Gain</b> |
| <u>917.0</u><br><b>Silica Final</b>   | <u>896.2</u><br><b>Silica Initial</b>   | <u>20.8</u><br><b>Silica Gain</b>  |

Run 2A - Method 26A

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Source Condition: Mill Off

Date: 11/14/23  
 Start Time: 14:15  
 End Time: 15:19

DRY GAS METER CONDITIONS

ΔH: 3.61 in. H<sub>2</sub>O  
 Meter Temperature, Tm: 76.5 °F  
 Sqrt ΔP: 1.310 in. H<sub>2</sub>O  
 Stack Temperature, Ts: 291.3 °F  
 Meter Volume, Vm: 66.766 ft<sup>3</sup>  
 Meter Volume, Vmstd: 64.262 dscf  
 Meter Volume, Vwstd: 7.889 wscf  
 Isokinetic Variance: 102.7 %I  
 Test Length: 60.00 in mins.  
 Nozzle Diameter: 0.247 in inches  
 Barometric Pressure: 29.23 in Hg

STACK CONDITIONS

Static Pressure -0.80 in. H<sub>2</sub>O  
 Flue Pressure (Ps): 29.17 in. Hg. abs.  
 Carbon Dioxide: 16.20 %  
 Oxygen: 11.20 %  
 Nitrogen: 72.6 %  
 Gas Weight dry, Md: 31.040 lb/lb mole  
 Gas Weight wet, Ms: 29.614 lb/lb mole  
 Excess Air: --- %  
 Gas Velocity, Vs: 85.633 fps  
 Volumetric Flow: 197,734 acfm  
 Volumetric Flow: 120,665 dscfm  
 Volumetric Flow: 135,479 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3559.1 ml Silica Initial Wt. 878.1 grams  
 Final Impinger Content: 3704.7 ml Silica Final Wt. 900.0 grams  
 Impinger Difference: 145.6 ml Silica Difference: 21.9 grams  
 Total Water Gain: 167.5 Moisture, Bws: 0.109

| Port-Point No. | Clock Time | Velocity                     | Orifice                 | Actual Meter Vol. ft <sup>3</sup> | Stack Temp °F | Meter Temp |           | Pump Vacuum "Hg | Probe Temp °F | Filter Exit Temp °F | Impinger Exit Temp °F |
|----------------|------------|------------------------------|-------------------------|-----------------------------------|---------------|------------|-----------|-----------------|---------------|---------------------|-----------------------|
|                |            | Head Δp in. H <sub>2</sub> O | ΔH in. H <sub>2</sub> O |                                   |               | Inlet °F   | Outlet °F |                 |               |                     |                       |
| 1-1            | 14:15:00   | 1.80                         | 3.70                    | 89.128                            | 294           | 76         | 74        | 6               | 259           | 254                 | 60                    |
| 1-2            | 14:20:00   | 1.70                         | 3.50                    | 94.800                            | 295           | 76         | 75        | 5               | 256           | 258                 | 62                    |
| 1-3            | 14:25:00   | 1.70                         | 3.70                    | 100.320                           | 294           | 75         | 75        | 7               | 257           | 257                 | 60                    |
| 1-4            | 14:30:00   | 1.70                         | 3.30                    | 105.830                           | 294           | 76         | 76        | 7               | 255           | 253                 | 59                    |
| 1-5            | 14:35:00   | 1.80                         | 3.50                    | 111.350                           | 293           | 77         | 76        | 6               | 254           | 255                 | 57                    |
| 1-6            | 14:40:00   | 1.60                         | 3.90                    | 117.050                           | 294           | 78         | 75        | 6               | 255           | 255                 | 57                    |
|                | 14:45:00   |                              |                         | 122.404                           |               |            |           |                 |               |                     |                       |
| 2-1            | 14:49:00   | 1.80                         | 3.80                    | 122.404                           | 290           | 78         | 76        | 6               | 254           | 254                 | 61                    |
| 2-2            | 14:54:00   | 1.60                         | 3.40                    | 128.110                           | 287           | 79         | 77        | 6               | 256           | 257                 | 57                    |
| 2-3            | 14:59:00   | 1.70                         | 3.60                    | 133.520                           | 289           | 78         | 76        | 5               | 255           | 254                 | 56                    |
| 2-4            | 15:04:00   | 1.80                         | 3.80                    | 139.070                           | 287           | 77         | 76        | 6               | 255           | 256                 | 54                    |
| 2-5            | 15:09:00   | 1.60                         | 3.30                    | 144.780                           | 289           | 78         | 77        | 7               | 254           | 253                 | 52                    |
| 2-6            | 15:14:00   | 1.80                         | 3.80                    | 150.180                           | 290           | 77         | 77        | 6               | 252           | 255                 | 53                    |
|                | 15:19:00   |                              |                         | 155.894                           |               |            |           |                 |               |                     |                       |

Total 1:00:00 66.766 77.1 75.8  
 Average 3.61 291.3 76.5 6  
 Min 3.30 287.0 74.0 5  
 Max 3.90 295.0 79.0 7

### Impinger Weight Sheet - Run 2A

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | <u>250.0</u>         |
| 500                            | <u>500.0</u>         |
| 750                            | <u>750.0</u>         |

| IMPINGER CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4        | 812.7                | 747.8                  | 64.9                |
| 0.1N H2SO4        | 805.3                | 745.0                  | 60.3                |
| Empty             | 670.4                | 655.4                  | 15.0                |
| 0.1N NaOH         | 712.4                | 707.2                  | 5.2                 |
| 0.1N NaOH         | 703.9                | 703.7                  | 0.2                 |
| Silica Gel        | 900.0                | 878.1                  | 21.9                |

|                                       |   |                                    |
|---------------------------------------|---|------------------------------------|
| <u>3,704.7</u><br><b>Liquid Final</b> | <u>3,559.1</u><br><b>Liquid Initial</b> | <u>145.6</u><br><b>Liquid Gain</b> |
| <u>900.0</u><br><b>Silica Final</b>   | <u>878.1</u><br><b>Silica Initial</b>   | <u>21.9</u><br><b>Silica Gain</b>  |

Run 3A - Method 26A

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Source Condition: Mill Off

Date: 11/14/23  
 Start Time: 15:40  
 End Time: 16:44

DRY GAS METER CONDITIONS

ΔH: 3.53 in. H<sub>2</sub>O  
 Meter Temperature, Tm: 75.5 °F  
 Sqrt ΔP: 1.294 in. H<sub>2</sub>O  
 Stack Temperature, Ts: 285.4 °F  
 Meter Volume, Vm: 66.138 ft<sup>3</sup>  
 Meter Volume, Vmstd: 63.758 dscf  
 Meter Volume, Vwstd: 7.899 wscf  
 Isokinetic Variance: 102.8 %I  
  
 Test Length: 60.00 in mins.  
 Nozzle Diameter: 0.247 in inches  
 Barometric Pressure: 29.23 in Hg

STACK CONDITIONS

Static Pressure -0.80 in. H<sub>2</sub>O  
 Flue Pressure (Ps): 29.17 in. Hg. abs.  
 Carbon Dioxide: 16.10 %  
 Oxygen: 11.30 %  
 Nitrogen: 72.6 %  
 Gas Weight dry, Md: 31.028 lb/lb mole  
 Gas Weight wet, Ms: 29.592 lb/lb mole  
 Excess Air: --- %  
 Gas Velocity, Vs: 84.289 fps  
 Volumetric Flow: 194,630 acfm  
 Volumetric Flow: 119,595 dscfm  
 Volumetric Flow: 134,411 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3576.0 ml Silica Initial Wt. 917.0 grams  
 Final Impinger Content: 3725.0 ml Silica Final Wt. 935.7 grams  
 Impinger Difference: 149.0 ml Silica Difference: 18.7 grams  
  
 Total Water Gain: 167.7 Moisture, Bws: 0.110

| Port-Point No. | Clock Time | Velocity                     | Orifice                 | Actual                     | Stack   | Meter Temp |           | Pump       | Probe   | Filter       | Impinger     |
|----------------|------------|------------------------------|-------------------------|----------------------------|---------|------------|-----------|------------|---------|--------------|--------------|
|                |            | Head Δp in. H <sub>2</sub> O | ΔH in. H <sub>2</sub> O | Meter Vol. ft <sup>3</sup> | Temp °F | Inlet °F   | Outlet °F | Vacuum "Hg | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1            | 15:40:00   | 1.70                         | 3.60                    | 56.870                     | 285     | 76         | 75        | 5          | 258     | 256          | 58           |
| 1-2            | 15:45:00   | 1.60                         | 3.30                    | 62.430                     | 286     | 75         | 74        | 6          | 256     | 253          | 60           |
| 1-3            | 15:50:00   | 1.80                         | 3.80                    | 67.800                     | 285     | 75         | 74        | 5          | 255     | 252          | 61           |
| 1-4            | 15:55:00   | 1.60                         | 3.40                    | 73.510                     | 285     | 75         | 74        | 5          | 256     | 254          | 60           |
| 1-5            | 16:00:00   | 1.70                         | 3.60                    | 78.890                     | 284     | 76         | 75        | 6          | 254     | 255          | 58           |
| 1-6            | 16:05:00   | 1.70                         | 3.60                    | 84.460                     | 286     | 75         | 75        | 6          | 254     | 257          | 55           |
|                | 16:10:00   |                              |                         | 90.011                     |         |            |           |            |         |              |              |
| 2-1            | 16:14:00   | 1.60                         | 3.30                    | 90.011                     | 285     | 76         | 75        | 6          | 259     | 254          | 56           |
| 2-2            | 16:19:00   | 1.80                         | 3.80                    | 95.400                     | 286     | 77         | 76        | 6          | 256     | 256          | 54           |
| 2-3            | 16:24:00   | 1.60                         | 3.30                    | 101.120                    | 286     | 76         | 75        | 5          | 257     | 254          | 53           |
| 2-4            | 16:29:00   | 1.70                         | 3.60                    | 106.490                    | 285     | 76         | 76        | 7          | 253     | 253          | 52           |
| 2-5            | 16:34:00   | 1.70                         | 3.60                    | 112.050                    | 286     | 77         | 76        | 7          | 256     | 255          | 54           |
| 2-6            | 16:39:00   | 1.60                         | 3.40                    | 117.620                    | 286     | 77         | 76        | 7          | 254     | 257          | 57           |
|                | 16:44:00   |                              |                         | 123.008                    |         |            |           |            |         |              |              |

Total 1:00:00 66.138 75.9 75.1  
 Average 3.53 285.4 75.5 6  
 Min 3.30 284.0 74.0 5  
 Max 3.80 286.0 77.0 7

### Impinger Weight Sheet - Run 3A

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | <u>250.0</u>         |
| 500                            | <u>500.0</u>         |
| 750                            | <u>750.0</u>         |

| IMPINGER<br>CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|----------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4           | 802.0                | 767.6                  | 34.4                |
| 0.1N H2SO4           | 726.0                | 670.4                  | 55.6                |
| Empty                | 680.0                | 648.6                  | 31.4                |
| 0.1N NaOH            | 754.5                | 735.1                  | 19.4                |
| 0.1N NaOH            | 762.5                | 754.3                  | 8.2                 |
| Silica Gel           | 935.7                | 917.0                  | 18.7                |

|                                       |   |                                    |
|---------------------------------------|---|------------------------------------|
| <u>3,725.0</u><br><b>Liquid Final</b> | <u>3,576.0</u><br><b>Liquid Initial</b> | <u>149.0</u><br><b>Liquid Gain</b> |
| <u>935.7</u><br><b>Silica Final</b>   | <u>917.0</u><br><b>Silica Initial</b>   | <u>18.7</u><br><b>Silica Gain</b>  |

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Test Method:** 26A  
**Test Engineer:** CLC  
**Test Technician:** KLJ

|                                    | <u>Run 1B</u> | <u>Run 2B</u> | <u>Run 3B</u> |
|------------------------------------|---------------|---------------|---------------|
| Temp ID:                           | CM18          | CM18          | CM18          |
| Meter ID:                          | CM18          | CM18          | CM18          |
| Pitot ID:                          | S8-032A       | S8-032A       | S8-032A       |
| Nozzle Diameter (Inches):          | 0.251         | 0.251         | 0.251         |
| Meter Calibration Date:            | 10/17/2023    | 10/17/2023    | 10/17/2023    |
| Meter Calibration Factor (Y):      | 0.987         | 0.987         | 0.987         |
| Meter Orifice Setting (Delta H):   | 1.533         | 1.533         | 1.533         |
| Nozzle Kit ID Number and Material: | Glass         | Glass         | Glass         |

**Leak Checks**

|                        |        |   |     |                   |        |   |     |                   |        |   |     |                   |
|------------------------|--------|---|-----|-------------------|--------|---|-----|-------------------|--------|---|-----|-------------------|
| Pre Pitot Leak Check   | 0.0    | @ | 4.0 | "H <sub>2</sub> O | 0.0    | @ | 4.2 | "H <sub>2</sub> O | 0.0    | @ | 4.5 | "H <sub>2</sub> O |
| Post Pitot Leak Check  | 0.0    | @ | 3.8 | "H <sub>2</sub> O | 0.0    | @ | 4.0 | "H <sub>2</sub> O | 0.0    | @ | 4.0 | "H <sub>2</sub> O |
| Pre Nozzle Leak Check  | 0.0000 | @ | 14  | "Hg               | 0.0000 | @ | 14  | "Hg               | 0.0000 | @ | 15  | "Hg               |
| Post Nozzle Leak Check | 0.0000 | @ | 10  | "Hg               | 0.0000 | @ | 10  | "Hg               | 0.0000 | @ | 12  | "Hg               |

Pitot Tube Coefficient: 0.822  
 Probe Length (Feet): 8.0  
 Probe Liner Material: Glass  
 Sample Plane: Horizontal  
 Port Length (Inches): 12.00  
 Port Size (Diameter, Inches): 4.00  
 Port Type: Nipple  
 Duct Shape: Circular  
 Diameter (Feet): 7  
  
 Duct Area (Square Feet): 38.485  
  
 Upstream Diameters: 16.0  
 Downstream Diameters: 11.0  
 Number of Ports Sampled: 4  
 Number of Points per Port: 3  
 Minutes per Point: 5.0  
 Minutes per Reading: 5.0  
 Total Number of Traverse Points: 12  
 Test Length (Minutes): 60  
 Train Type: Anderson Box  
 Source Condition: Mill Off  
 Diluent Model/Serial Number: CAI 700/221018  
 Moisture Balance ID: LV3  
 # of Runs: 3

Run 1B - Method 26A

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Source Condition: Mill Off

Date: 11/14/23  
 Start Time: 12:50  
 End Time: 13:55

DRY GAS METER CONDITIONS

STACK CONDITIONS

ΔH: 3.50 in. H<sub>2</sub>O  
 Meter Temperature, Tm: 72.6 °F  
 Sqrt ΔP: 1.319 in. H<sub>2</sub>O  
 Stack Temperature, Ts: 280.0 °F  
 Meter Volume, Vm: 70.080 ft<sup>3</sup>  
 Meter Volume, Vmstd: 67.577 dscf  
 Meter Volume, Vwstd: 8.511 wscf  
 Isokinetic Variance: 103.0 %I  
 Test Length: 60.00 in mins.  
 Nozzle Diameter: 0.251 in inches  
 Barometric Pressure: 29.23 in Hg

Static Pressure -0.80 in. H<sub>2</sub>O  
 Flue Pressure (Ps): 29.17 in. Hg. abs.  
 Carbon Dioxide: 16.20 %  
 Oxygen: 11.20 %  
 Nitrogen: 72.60 %  
 Gas Weight dry, Md: 31.040 lb/lb mole  
 Gas Weight wet, Ms: 29.581 lb/lb mole  
 Excess Air: --- %  
 Gas Velocity, Vs: 85.861 fps  
 Volumetric Flow: 198,259 acfm  
 Volumetric Flow: 122,493 dscfm  
 Volumetric Flow: 137,920 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3619.5 ml Silica Initial Wt. 887.7 grams  
 Final Impinger Content: 3788.6 ml Silica Final Wt. 899.3 grams  
 Impinger Difference: 169.1 ml Silica Difference: 11.6 grams  
 Total Water Gain: 180.7 Moisture, Bws: 0.112

| Port-<br>Point No. | Clock<br>Time | Velocity                        | Orifice                    | Actual                        | Stack      | Meter Temp  |              | Pump          | Probe      | Filter          | Impinger        |
|--------------------|---------------|---------------------------------|----------------------------|-------------------------------|------------|-------------|--------------|---------------|------------|-----------------|-----------------|
|                    |               | Head Δp<br>in. H <sub>2</sub> O | ΔH<br>in. H <sub>2</sub> O | Meter Vol.<br>ft <sup>3</sup> | Temp<br>°F | Inlet<br>°F | Outlet<br>°F | Vacuum<br>"Hg | Temp<br>°F | Exit Temp<br>°F | Exit Temp<br>°F |
| 1-1                | 12:50:00      | 1.80                            | 3.60                       | 69.650                        | 279        | 70          | 68           | 5             | 250        | 250             | 54              |
| 1-2                | 12:55:00      | 1.70                            | 3.40                       | 75.550                        | 280        | 74          | 68           | 5             | 250        | 250             | 55              |
| 1-3                | 13:00:00      | 1.70                            | 3.40                       | 81.300                        | 279        | 76          | 68           | 5             | 250        | 250             | 55              |
| 1-4                | 13:05:00      | 1.70                            | 3.40                       | 87.080                        | 279        | 76          | 68           | 5             | 251        | 251             | 56              |
| 1-5                | 13:10:00      | 1.80                            | 3.60                       | 92.840                        | 279        | 77          | 69           | 5             | 251        | 250             | 57              |
| 1-6                | 13:15:00      | 1.90                            | 3.80                       | 98.790                        | 280        | 77          | 69           | 5             | 250        | 250             | 58              |
|                    | 13:20:00      |                                 |                            | 104.900                       |            |             |              |               |            |                 |                 |
| 2-1                | 13:25:00      | 1.70                            | 3.40                       | 104.900                       | 280        | 77          | 69           | 5             | 251        | 250             | 58              |
| 2-2                | 13:30:00      | 1.70                            | 3.40                       | 110.680                       | 281        | 77          | 69           | 5             | 250        | 250             | 58              |
| 2-3                | 13:35:00      | 1.80                            | 3.65                       | 116.500                       | 281        | 78          | 69           | 5             | 251        | 250             | 59              |
| 2-4                | 13:40:00      | 1.60                            | 3.25                       | 122.400                       | 280        | 78          | 69           | 5             | 252        | 250             | 60              |
| 2-5                | 13:45:00      | 1.70                            | 3.50                       | 127.990                       | 281        | 78          | 70           | 5             | 251        | 251             | 62              |
| 2-6                | 13:50:00      | 1.80                            | 3.60                       | 133.780                       | 281        | 79          | 70           | 5             | 251        | 251             | 62              |
|                    | 13:55:00      |                                 |                            | 139.730                       |            |             |              |               |            |                 |                 |
| Total              | 1:00:00       |                                 |                            | 70.080                        |            | 76.4        | 68.8         |               |            |                 |                 |
| Average            |               |                                 | 3.50                       |                               | 280.0      | 72.6        |              | 5             |            |                 |                 |
| Min                |               |                                 | 3.25                       |                               | 279.0      | 68.0        |              | 5             |            |                 |                 |
| Max                |               |                                 | 3.80                       |                               | 281.0      | 79.0        |              | 5             |            |                 |                 |

### Impinger Weight Sheet - Run 1B

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | <u>250.0</u>         |
| 500                            | <u>500.0</u>         |
| 750                            | <u>750.0</u>         |

| IMPINGER<br>CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|----------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4           | 808.9                | 765.5                  | 43.4                |
| 0.1N H2SO4           | 800.5                | 728.5                  | 72.0                |
| Empty                | 677.1                | 646.3                  | 30.8                |
| 0.1N NaOH            | 763.1                | 743.9                  | 19.2                |
| 0.1N NaOH            | 739.0                | 735.3                  | 3.7                 |
| Silica Gel           | 899.3                | 887.7                  | 11.6                |

|                                       |   |                                    |
|---------------------------------------|---|------------------------------------|
| <u>3,788.6</u><br><b>Liquid Final</b> | <u>3,619.5</u><br><b>Liquid Initial</b> | <u>169.1</u><br><b>Liquid Gain</b> |
| <u>899.3</u><br><b>Silica Final</b>   | <u>887.7</u><br><b>Silica Initial</b>   | <u>11.6</u><br><b>Silica Gain</b>  |

Run 2B - Method 26A

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Source Condition: Mill Off

Date: 11/14/23  
 Start Time: 14:15  
 End Time: 15:19

DRY GAS METER CONDITIONS

ΔH: 3.44 in. H<sub>2</sub>O  
 Meter Temperature, Tm: 75.0 °F  
 Sqrt ΔP: 1.319 in. H<sub>2</sub>O  
 Stack Temperature, Ts: 289.0 °F  
 Meter Volume, Vm: 70.115 ft<sup>3</sup>  
 Meter Volume, Vmstd: 67.305 dscf  
 Meter Volume, Vwstd: 8.657 wscf  
 Isokinetic Variance: 103.4 %I  
 Test Length: 60.00 in mins.  
 Nozzle Diameter: 0.251 in inches  
 Barometric Pressure: 29.23 in Hg

STACK CONDITIONS

Static Pressure -0.80 in. H<sub>2</sub>O  
 Flue Pressure (Ps): 29.17 in. Hg. abs.  
 Carbon Dioxide: 16.20 %  
 Oxygen: 11.20 %  
 Nitrogen: 72.6 %  
 Gas Weight dry, Md: 31.040 lb/lb mole  
 Gas Weight wet, Ms: 29.554 lb/lb mole  
 Excess Air: --- %  
 Gas Velocity, Vs: 86.422 fps  
 Volumetric Flow: 199,554 acfm  
 Volumetric Flow: 121,522 dscfm  
 Volumetric Flow: 137,152 scfm

MOISTURE DETERMINATION

Initial Impinger Content: 3521.5 ml Silica Initial Wt. 890.9 grams  
 Final Impinger Content: 3686.2 ml Silica Final Wt. 910.0 grams  
 Impinger Difference: 164.7 ml Silica Difference: 19.1 grams  
 Total Water Gain: 183.8 Moisture, Bws: 0.114

| Port-Point No. | Clock Time | Velocity                     | Orifice                 | Actual                     | Stack   | Meter Temp |           | Pump       | Probe   | Filter       | Impinger     |
|----------------|------------|------------------------------|-------------------------|----------------------------|---------|------------|-----------|------------|---------|--------------|--------------|
|                |            | Head Δp in. H <sub>2</sub> O | ΔH in. H <sub>2</sub> O | Meter Vol. ft <sup>3</sup> | Temp °F | Inlet °F   | Outlet °F | Vacuum "Hg | Temp °F | Exit Temp °F | Exit Temp °F |
| 1-1            | 14:15:00   | 1.90                         | 3.80                    | 40.835                     | 284     | 74         | 73        | 7          | 250     | 250          | 47           |
| 1-2            | 14:20:00   | 1.80                         | 3.65                    | 46.880                     | 290     | 74         | 73        | 7          | 250     | 250          | 48           |
| 1-3            | 14:25:00   | 1.70                         | 3.50                    | 52.870                     | 291     | 75         | 73        | 7          | 251     | 250          | 50           |
| 1-4            | 14:30:00   | 1.70                         | 3.50                    | 58.660                     | 290     | 76         | 74        | 7          | 251     | 250          | 51           |
| 1-5            | 14:35:00   | 1.80                         | 3.65                    | 64.450                     | 287     | 76         | 74        | 7          | 251     | 251          | 52           |
| 1-6            | 14:40:00   | 1.70                         | 3.50                    | 70.400                     | 288     | 78         | 74        | 7          | 252     | 251          | 54           |
|                | 14:45:00   |                              |                         | 76.210                     |         |            |           |            |         |              |              |
| 2-1            | 14:49:00   | 1.70                         | 3.40                    | 76.210                     | 290     | 75         | 73        | 7          | 251     | 250          | 51           |
| 2-2            | 14:54:00   | 1.80                         | 3.60                    | 81.960                     | 288     | 76         | 74        | 7          | 251     | 251          | 53           |
| 2-3            | 14:59:00   | 1.70                         | 3.40                    | 87.880                     | 289     | 76         | 74        | 7          | 250     | 250          | 54           |
| 2-4            | 15:04:00   | 1.70                         | 3.40                    | 93.650                     | 290     | 77         | 74        | 7          | 251     | 250          | 56           |
| 2-5            | 15:09:00   | 1.80                         | 3.60                    | 99.410                     | 291     | 78         | 74        | 7          | 250     | 251          | 58           |
| 2-6            | 15:14:00   | 1.60                         | 2.25                    | 105.350                    | 290     | 79         | 75        | 7          | 250     | 250          | 60           |
|                | 15:19:00   |                              |                         | 110.950                    |         |            |           |            |         |              |              |

Total 1:00:00 70.115 76.2 73.8  
 Average 3.44 289.0 75.0 7  
 Min 2.25 284.0 73.0 7  
 Max 3.80 291.0 79.0 7

### Impinger Weight Sheet - Run 2B

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | <u>250.0</u>         |
| 500                            | <u>500.0</u>         |
| 750                            | <u>750.0</u>         |

| IMPINGER<br>CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|----------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4           | 799.6                | 714.1                  | 85.5                |
| 0.1N H2SO4           | 791.4                | 735.1                  | 56.3                |
| Empty                | 639.4                | 630.0                  | 9.4                 |
| 0.1N NaOH            | 690.3                | 680.0                  | 10.3                |
| 0.1N NaOH            | 765.5                | 762.3                  | 3.2                 |
| Silica Gel           | 910.0                | 890.9                  | 19.1                |

|                                       |   |                                    |
|---------------------------------------|---|------------------------------------|
| <u>3,686.2</u><br><b>Liquid Final</b> | <u>3,521.5</u><br><b>Liquid Initial</b> | <u>164.7</u><br><b>Liquid Gain</b> |
| <u>910.0</u><br><b>Silica Final</b>   | <u>890.9</u><br><b>Silica Initial</b>   | <u>19.1</u><br><b>Silica Gain</b>  |

Run 3B - Method 26A

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Test Location: Kiln Stack  
 Source Condition: Mill Off

Date: 11/14/23  
 Start Time: 15:40  
 End Time: 16:44

| DRY GAS METER CONDITIONS |        |                      |  | STACK CONDITIONS    |         |                      |  |
|--------------------------|--------|----------------------|--|---------------------|---------|----------------------|--|
| ΔH:                      | 3.38   | In. H <sub>2</sub> O |  | Static Pressure     | -0.80   | in. H <sub>2</sub> O |  |
| Meter Temperature, Tm:   | 74.4   | °F                   |  | Flue Pressure (Ps): | 29.17   | in. Hg. abs.         |  |
| Sqrt ΔP:                 | 1.300  | In. H <sub>2</sub> O |  | Carbon Dioxide:     | 16.10   | %                    |  |
| Stack Temperature, Ts:   | 285.8  | °F                   |  | Oxygen:             | 11.30   | %                    |  |
| Meter Volume, Vm:        | 69.025 | ft <sup>3</sup>      |  | Nitrogen:           | 72.6    | %                    |  |
| Meter Volume, Vmstd:     | 66.317 | dscf                 |  | Gas Weight dry, Md: | 31.028  | lb/lb mole           |  |
| Meter Volume, Vwstd:     | 8.633  | wscf                 |  | Gas Weight wet, Ms: | 29.527  | lb/lb mole           |  |
| Isokinetic Variance:     | 103.3  | %I                   |  | Excess Air:         | ---     | %                    |  |
| Test Length:             | 60.00  | in mins.             |  | Gas Velocity, Vs:   | 85.024  | fps                  |  |
| Nozzle Diameter:         | 0.251  | in inches            |  | Volumetric Flow:    | 196,327 | acfm                 |  |
| Barometric Pressure:     | 29.23  | in Hg                |  | Volumetric Flow:    | 119,912 | dscfm                |  |
|                          |        |                      |  | Volumetric Flow:    | 135,523 | scfm                 |  |

MOISTURE DETERMINATION

|                           |        |    |                    |       |       |
|---------------------------|--------|----|--------------------|-------|-------|
| Initial Impinger Content: | 3627.4 | ml | Silica Initial Wt. | 899.3 | grams |
| Final Impinger Content:   | 3801.6 | ml | Silica Final Wt.   | 908.4 | grams |
| Impinger Difference:      | 174.2  | ml | Silica Difference: | 9.1   | grams |
| Total Water Gain:         | 183.3  |    | Moisture, Bws:     | 0.115 |       |

| Port-Point No. | Clock Time | Velocity                        | Orifice                    | Actual                        | Stack      | Meter Temp  |              | Pump          | Probe      | Filter          | Impinger        |
|----------------|------------|---------------------------------|----------------------------|-------------------------------|------------|-------------|--------------|---------------|------------|-----------------|-----------------|
|                |            | Head Δp<br>in. H <sub>2</sub> O | ΔH<br>in. H <sub>2</sub> O | Meter Vol.<br>ft <sup>3</sup> | Temp<br>°F | Inlet<br>°F | Outlet<br>°F | Vacuum<br>"Hg | Temp<br>°F | Exit Temp<br>°F | Exit Temp<br>°F |
| 1-1            | 15:40:00   | 1.80                            | 3.60                       | 11.485                        | 285        | 74          | 72           | 5             | 250        | 250             | 54              |
| 1-2            | 15:45:00   | 1.60                            | 3.20                       | 17.400                        | 286        | 74          | 72           | 5             | 251        | 250             | 54              |
| 1-3            | 15:50:00   | 1.70                            | 3.40                       | 22.980                        | 285        | 75          | 72           | 5             | 251        | 251             | 56              |
| 1-4            | 15:55:00   | 1.70                            | 3.40                       | 28.750                        | 286        | 76          | 73           | 5             | 250        | 250             | 56              |
| 1-5            | 16:00:00   | 1.80                            | 3.60                       | 34.500                        | 285        | 76          | 73           | 5             | 251        | 251             | 57              |
| 1-6            | 16:05:00   | 1.60                            | 3.20                       | 40.450                        | 287        | 77          | 73           | 5             | 251        | 250             | 58              |
|                | 16:10:00   |                                 |                            | 46.050                        |            |             |              |               |            |                 |                 |
| 2-1            | 16:14:00   | 1.70                            | 3.40                       | 46.050                        | 285        | 75          | 72           | 5             | 250        | 250             | 57              |
| 2-2            | 16:19:00   | 1.60                            | 3.20                       | 51.810                        | 285        | 76          | 72           | 5             | 251        | 250             | 58              |
| 2-3            | 16:24:00   | 1.70                            | 3.40                       | 57.400                        | 286        | 77          | 73           | 5             | 251        | 250             | 59              |
| 2-4            | 16:29:00   | 1.80                            | 3.60                       | 63.200                        | 286        | 77          | 73           | 5             | 250        | 250             | 59              |
| 2-5            | 16:34:00   | 1.60                            | 3.20                       | 69.100                        | 287        | 78          | 73           | 5             | 251        | 251             | 60              |
| 2-6            | 16:39:00   | 1.70                            | 3.40                       | 74.720                        | 286        | 79          | 74           | 5             | 252        | 251             | 60              |
|                | 16:44:00   |                                 |                            | 80.510                        |            |             |              |               |            |                 |                 |

|         |         |  |      |        |       |      |      |   |  |  |  |
|---------|---------|--|------|--------|-------|------|------|---|--|--|--|
| Total   | 1:00:00 |  |      | 69.025 |       | 76.2 | 72.7 |   |  |  |  |
| Average |         |  | 3.38 |        | 285.8 | 74.4 |      | 5 |  |  |  |
| Min     |         |  | 3.20 |        | 285.0 | 72.0 |      | 5 |  |  |  |
| Max     |         |  | 3.60 |        | 287.0 | 79.0 |      | 5 |  |  |  |

### Impinger Weight Sheet - Run 3B

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Kiln Stack  
**Project #:** M234605  
**Date:** 11/14/2023  
**Test Method:** 26A  
**Weighed/Measured By:** KLJ  
**Balance ID:** LV3

**Scale Calibration Check Date:** 11/14/2023  
**Scale Calibration Check (see QS-6.05C for procedure)**  
 must be within  $\pm 0.5g$  of certified mass  

| <u>Certified Weight, grams</u> | <u>Result, grams</u> |
|--------------------------------|----------------------|
| 250                            | 250.0                |
| 500                            | 500.0                |
| 750                            | 750.0                |

| IMPINGER CONTENTS | FINAL<br>MLS / GRAMS | INITIAL<br>MLS / GRAMS | GAIN<br>MLS / GRAMS |
|-------------------|----------------------|------------------------|---------------------|
| 0.1N H2SO4        | 832.2                | 745.9                  | 86.3                |
| 0.1N H2SO4        | 793.5                | 750.5                  | 43.0                |
| Empty             | 668.6                | 646.5                  | 22.1                |
| 0.1N NaOH         | 760.0                | 744.5                  | 15.5                |
| 0.1N NaOH         | 747.3                | 740.0                  | 7.3                 |
| Silica Gel        | 908.4                | 899.3                  | 9.1                 |

|                     |                       |                    |
|---------------------|-----------------------|--------------------|
| 3,801.6             | 3,627.4               | 174.2              |
| <b>Liquid Final</b> | <b>Liquid Initial</b> | <b>Liquid Gain</b> |
| 908.4               | 899.3                 | 9.1                |
| <b>Silica Final</b> | <b>Silica Initial</b> | <b>Silica Gain</b> |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Test Location: Main Kiln Stack  
 Date: 11/14/23

Run 1

| Spectrum              | Time  | FTIR Data    |              |             |             |               | Cell Temp   | Pressure     | Analyzer Data<br>O2 % (dry) |
|-----------------------|-------|--------------|--------------|-------------|-------------|---------------|-------------|--------------|-----------------------------|
|                       |       | H2O %        | CO2 % (wet)  | HCN ppmvw   | HF ppmvw    |               |             |              |                             |
| MILLOFF_R1_000627.LAB | 12:50 | 12.04        | 14.44        | 0.81        | 0.10        | 190.64        | 0.97        | 11.00        |                             |
| MILLOFF_R1_000628.LAB | 12:51 | 11.91        | 14.18        | 0.81        | 0.10        | 190.64        | 0.97        | 11.03        |                             |
| MILLOFF_R1_000629.LAB | 12:52 | 11.84        | 13.85        | 0.87        | 0.10        | 190.65        | 0.97        | 11.22        |                             |
| MILLOFF_R1_000630.LAB | 12:53 | 11.96        | 13.93        | 0.80        | 0.10        | 190.64        | 0.97        | 11.24        |                             |
| MILLOFF_R1_000631.LAB | 12:54 | 12.10        | 14.04        | 0.80        | 0.10        | 190.64        | 0.97        | 11.11        |                             |
| MILLOFF_R1_000632.LAB | 12:55 | 12.15        | 14.07        | 0.76        | 0.10        | 190.64        | 0.97        | 11.05        |                             |
| MILLOFF_R1_000633.LAB | 12:56 | 12.16        | 14.16        | 0.88        | 0.10        | 190.69        | 0.97        | 11.04        |                             |
| MILLOFF_R1_000634.LAB | 12:57 | 12.08        | 14.18        | 0.83        | 0.10        | 190.77        | 0.97        | 11.11        |                             |
| MILLOFF_R1_000635.LAB | 12:58 | 12.06        | 14.01        | 0.86        | 0.10        | 190.95        | 0.97        | 11.13        |                             |
| MILLOFF_R1_000636.LAB | 12:59 | 12.14        | 13.96        | 0.77        | 0.10        | 191.02        | 0.97        | 11.19        |                             |
| MILLOFF_R1_000637.LAB | 13:00 | 12.10        | 13.84        | 0.82        | 0.10        | 191.04        | 0.97        | 11.25        |                             |
| MILLOFF_R1_000638.LAB | 13:01 | 12.10        | 13.92        | 0.88        | 0.10        | 190.94        | 0.97        | 11.17        |                             |
| MILLOFF_R1_000639.LAB | 13:02 | 12.17        | 14.11        | 0.80        | 0.10        | 190.92        | 0.97        | 11.09        |                             |
| MILLOFF_R1_000640.LAB | 13:03 | 12.06        | 13.97        | 0.78        | 0.10        | 190.86        | 0.97        | 11.12        |                             |
| MILLOFF_R1_000641.LAB | 13:04 | 12.00        | 14.14        | 0.82        | 0.10        | 190.86        | 0.97        | 11.23        |                             |
| MILLOFF_R1_000642.LAB | 13:05 | 12.07        | 14.30        | 0.80        | 0.10        | 190.80        | 0.97        | 11.23        |                             |
| MILLOFF_R1_000643.LAB | 13:06 | 12.12        | 14.15        | 0.82        | 0.10        | 190.76        | 0.97        | 11.11        |                             |
| MILLOFF_R1_000644.LAB | 13:07 | 12.15        | 14.21        | 0.79        | 0.10        | 190.76        | 0.97        | 11.12        |                             |
| MILLOFF_R1_000645.LAB | 13:08 | 12.17        | 14.28        | 0.80        | 0.10        | 190.76        | 0.97        | 11.05        |                             |
| MILLOFF_R1_000646.LAB | 13:09 | 12.12        | 14.25        | 0.84        | 0.10        | 190.75        | 0.97        | 11.00        |                             |
| MILLOFF_R1_000647.LAB | 13:10 | 12.22        | 14.22        | 0.80        | 0.10        | 190.71        | 0.97        | 11.15        |                             |
| MILLOFF_R1_000648.LAB | 13:11 | 12.23        | 13.89        | 0.80        | 0.10        | 190.64        | 0.97        | 11.15        |                             |
| MILLOFF_R1_000649.LAB | 13:12 | 12.16        | 14.07        | 0.74        | 0.10        | 190.67        | 0.97        | 11.20        |                             |
| MILLOFF_R1_000650.LAB | 13:13 | 12.17        | 14.16        | 0.79        | 0.10        | 190.73        | 0.97        | 11.15        |                             |
| MILLOFF_R1_000651.LAB | 13:14 | 12.18        | 14.37        | 0.80        | 0.10        | 190.75        | 0.97        | 11.10        |                             |
| MILLOFF_R1_000652.LAB | 13:15 | 12.17        | 14.40        | 0.78        | 0.10        | 190.94        | 0.97        | 11.05        |                             |
| MILLOFF_R1_000653.LAB | 13:16 | 12.21        | 14.24        | 0.83        | 0.10        | 191.17        | 0.97        | 10.89        |                             |
| MILLOFF_R1_000654.LAB | 13:17 | 12.18        | 14.26        | 0.81        | 0.10        | 191.20        | 0.97        | 11.07        |                             |
| MILLOFF_R1_000655.LAB | 13:18 | 12.15        | 14.27        | 0.84        | 0.10        | 191.09        | 0.97        | 11.09        |                             |
| MILLOFF_R1_000656.LAB | 13:19 | 12.20        | 14.29        | 0.78        | 0.10        | 190.91        | 0.97        | 10.99        |                             |
| MILLOFF_R1_000657.LAB | 13:20 | 12.13        | 14.02        | 0.79        | 0.10        | 190.83        | 0.97        | 11.04        |                             |
| MILLOFF_R1_000658.LAB | 13:21 | 12.18        | 14.08        | 0.80        | 0.10        | 190.73        | 0.97        | 11.07        |                             |
| MILLOFF_R1_000659.LAB | 13:22 | 12.17        | 14.17        | 0.81        | 0.10        | 190.74        | 0.97        | 11.17        |                             |
| MILLOFF_R1_000660.LAB | 13:23 | 12.17        | 14.30        | 0.86        | 0.10        | 190.71        | 0.97        | 11.10        |                             |
| MILLOFF_R1_000661.LAB | 13:24 | 12.20        | 14.24        | 0.80        | 0.10        | 190.70        | 0.97        | 11.12        |                             |
| MILLOFF_R1_000662.LAB | 13:25 | 12.15        | 13.99        | 0.84        | 0.10        | 190.65        | 0.97        | 11.04        |                             |
| MILLOFF_R1_000663.LAB | 13:26 | 12.21        | 14.09        | 0.80        | 0.10        | 190.59        | 0.97        | 11.06        |                             |
| MILLOFF_R1_000664.LAB | 13:27 | 12.10        | 13.99        | 0.78        | 0.10        | 190.58        | 0.97        | 11.20        |                             |
| MILLOFF_R1_000665.LAB | 13:28 | 12.10        | 13.97        | 0.78        | 0.10        | 190.60        | 0.97        | 11.16        |                             |
| MILLOFF_R1_000666.LAB | 13:29 | 12.22        | 14.06        | 0.82        | 0.10        | 190.73        | 0.97        | 11.24        |                             |
| MILLOFF_R1_000667.LAB | 13:30 | 12.22        | 14.28        | 0.79        | 0.10        | 190.75        | 0.97        | 11.26        |                             |
| MILLOFF_R1_000668.LAB | 13:31 | 12.11        | 14.11        | 0.82        | 0.10        | 190.71        | 0.97        | 11.15        |                             |
| MILLOFF_R1_000669.LAB | 13:32 | 12.18        | 14.12        | 0.86        | 0.10        | 190.68        | 0.97        | 11.06        |                             |
| MILLOFF_R1_000670.LAB | 13:33 | 12.34        | 14.27        | 0.85        | 0.10        | 190.72        | 0.97        | 11.17        |                             |
| MILLOFF_R1_000671.LAB | 13:34 | 12.31        | 14.26        | 0.86        | 0.10        | 190.74        | 0.97        | 11.19        |                             |
| MILLOFF_R1_000672.LAB | 13:35 | 12.36        | 14.41        | 0.87        | 0.10        | 190.70        | 0.97        | 11.09        |                             |
| MILLOFF_R1_000673.LAB | 13:36 | 12.39        | 14.49        | 0.92        | 0.10        | 190.69        | 0.97        | 11.04        |                             |
| MILLOFF_R1_000674.LAB | 13:37 | 12.30        | 14.55        | 0.80        | 0.10        | 190.66        | 0.97        | 10.91        |                             |
| MILLOFF_R1_000675.LAB | 13:38 | 12.38        | 14.75        | 0.88        | 0.10        | 190.69        | 0.97        | 10.91        |                             |
| MILLOFF_R1_000676.LAB | 13:39 | 12.48        | 14.54        | 0.86        | 0.10        | 190.71        | 0.97        | 10.94        |                             |
| MILLOFF_R1_000677.LAB | 13:40 | 12.50        | 14.23        | 0.87        | 0.10        | 190.68        | 0.97        | 10.88        |                             |
| MILLOFF_R1_000678.LAB | 13:41 | 12.40        | 14.13        | 0.85        | 0.10        | 190.62        | 0.97        | 10.86        |                             |
| MILLOFF_R1_000679.LAB | 13:42 | 12.37        | 14.36        | 0.92        | 0.10        | 190.63        | 0.97        | 10.98        |                             |
| MILLOFF_R1_000680.LAB | 13:43 | 12.44        | 14.52        | 0.90        | 0.10        | 190.53        | 0.97        | 10.96        |                             |
| MILLOFF_R1_000681.LAB | 13:44 | 12.45        | 14.42        | 0.87        | 0.10        | 190.59        | 0.97        | 10.91        |                             |
| MILLOFF_R1_000682.LAB | 13:45 | 12.32        | 14.36        | 0.88        | 0.10        | 190.72        | 0.97        | 10.84        |                             |
| MILLOFF_R1_000683.LAB | 13:46 | 12.40        | 14.38        | 0.90        | 0.10        | 190.74        | 0.97        | 10.81        |                             |
| MILLOFF_R1_000684.LAB | 13:47 | 12.47        | 14.24        | 0.83        | 0.10        | 190.79        | 0.97        | 10.81        |                             |
| MILLOFF_R1_000685.LAB | 13:48 | 12.44        | 14.11        | 0.80        | 0.10        | 190.79        | 0.97        | 10.94        |                             |
| MILLOFF_R1_000686.LAB | 13:49 | 12.39        | 13.95        | 0.85        | 0.10        | 190.76        | 0.97        | 10.98        |                             |
| <b>Average</b>        |       | <b>12.20</b> | <b>14.19</b> | <b>0.83</b> | <b>0.10</b> | <b>190.76</b> | <b>0.97</b> | <b>11.07</b> |                             |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Test Location: Main Kiln Stack  
 Date: 11/14/23

Run 2

| Spectrum              | Time  | FTIR Data    |              |             |             |               | Cell Temp   | Pressure     | Analyzer Data<br>O2 % (dry) |
|-----------------------|-------|--------------|--------------|-------------|-------------|---------------|-------------|--------------|-----------------------------|
|                       |       | H2O %        | CO2 % (wet)  | HCN ppmvw   | HF ppmvw    |               |             |              |                             |
| MILLOFF_R2_000754.LAB | 14:15 | 12.39        | 14.2         | 0.84        | 0.10        | 190.7         | 0.97        | 11.07        |                             |
| MILLOFF_R2_000755.LAB | 14:16 | 12.35        | 14.4         | 0.84        | 0.10        | 190.7         | 0.97        | 11.17        |                             |
| MILLOFF_R2_000756.LAB | 14:17 | 12.25        | 14.5         | 0.85        | 0.10        | 190.9         | 0.97        | 11.06        |                             |
| MILLOFF_R2_000757.LAB | 14:18 | 12.17        | 14.5         | 0.89        | 0.10        | 191.0         | 0.97        | 11.28        |                             |
| MILLOFF_R2_000758.LAB | 14:19 | 12.19        | 14.3         | 0.79        | 0.10        | 191.0         | 0.97        | 11.49        |                             |
| MILLOFF_R2_000759.LAB | 14:20 | 12.20        | 14.1         | 0.89        | 0.10        | 190.9         | 0.97        | 11.33        |                             |
| MILLOFF_R2_000760.LAB | 14:21 | 12.54        | 14.2         | 0.86        | 0.10        | 190.8         | 0.97        | 10.88        |                             |
| MILLOFF_R2_000761.LAB | 14:22 | 12.74        | 14.3         | 0.84        | 0.10        | 190.8         | 0.97        | 10.87        |                             |
| MILLOFF_R2_000762.LAB | 14:23 | 12.41        | 13.6         | 0.81        | 0.10        | 190.7         | 0.97        | 11.41        |                             |
| MILLOFF_R2_000763.LAB | 14:24 | 12.08        | 13.1         | 0.85        | 0.10        | 190.7         | 0.97        | 11.60        |                             |
| MILLOFF_R2_000764.LAB | 14:25 | 12.40        | 13.4         | 0.84        | 0.10        | 190.7         | 0.97        | 11.17        |                             |
| MILLOFF_R2_000765.LAB | 14:26 | 12.81        | 14.1         | 0.91        | 0.10        | 190.8         | 0.97        | 10.65        |                             |
| MILLOFF_R2_000766.LAB | 14:27 | 12.62        | 14.1         | 0.86        | 0.10        | 190.8         | 0.97        | 10.89        |                             |
| MILLOFF_R2_000767.LAB | 14:28 | 12.36        | 13.8         | 0.83        | 0.10        | 190.8         | 0.97        | 11.28        |                             |
| MILLOFF_R2_000768.LAB | 14:29 | 12.37        | 14.0         | 0.87        | 0.10        | 190.7         | 0.97        | 11.22        |                             |
| MILLOFF_R2_000769.LAB | 14:30 | 12.35        | 14.3         | 0.90        | 0.10        | 190.6         | 0.97        | 11.22        |                             |
| MILLOFF_R2_000770.LAB | 14:31 | 12.35        | 14.6         | 0.89        | 0.10        | 190.6         | 0.97        | 11.11        |                             |
| MILLOFF_R2_000771.LAB | 14:32 | 12.50        | 14.6         | 0.89        | 0.10        | 190.7         | 0.97        | 11.06        |                             |
| MILLOFF_R2_000772.LAB | 14:33 | 12.56        | 15.0         | 0.85        | 0.10        | 190.7         | 0.97        | 10.88        |                             |
| MILLOFF_R2_000773.LAB | 14:34 | 12.57        | 15.0         | 0.86        | 0.10        | 190.8         | 0.97        | 10.84        |                             |
| MILLOFF_R2_000774.LAB | 14:35 | 12.55        | 14.9         | 0.88        | 0.10        | 190.8         | 0.97        | 10.72        |                             |
| MILLOFF_R2_000775.LAB | 14:36 | 12.63        | 14.6         | 0.83        | 0.10        | 190.7         | 0.97        | 10.92        |                             |
| MILLOFF_R2_000776.LAB | 14:37 | 12.63        | 14.6         | 0.88        | 0.10        | 190.7         | 0.97        | 11.07        |                             |
| MILLOFF_R2_000777.LAB | 14:38 | 12.64        | 14.7         | 0.90        | 0.10        | 190.6         | 0.97        | 10.90        |                             |
| MILLOFF_R2_000778.LAB | 14:39 | 12.51        | 14.4         | 0.96        | 0.10        | 190.7         | 0.97        | 10.91        |                             |
| MILLOFF_R2_000779.LAB | 14:40 | 12.43        | 14.3         | 0.86        | 0.10        | 190.7         | 0.97        | 11.09        |                             |
| MILLOFF_R2_000780.LAB | 14:41 | 12.31        | 14.1         | 0.87        | 0.10        | 190.7         | 0.97        | 11.12        |                             |
| MILLOFF_R2_000781.LAB | 14:42 | 12.24        | 14.3         | 0.89        | 0.10        | 190.6         | 0.97        | 11.19        |                             |
| MILLOFF_R2_000782.LAB | 14:43 | 12.29        | 14.2         | 0.91        | 0.10        | 190.6         | 0.97        | 11.12        |                             |
| MILLOFF_R2_000783.LAB | 14:44 | 12.33        | 14.3         | 0.92        | 0.10        | 190.6         | 0.97        | 11.02        |                             |
| MILLOFF_R2_000784.LAB | 14:45 | 12.49        | 14.5         | 0.90        | 0.10        | 190.6         | 0.97        | 10.94        |                             |
| MILLOFF_R2_000785.LAB | 14:46 | 12.31        | 13.9         | 0.90        | 0.10        | 190.6         | 0.97        | 10.95        |                             |
| MILLOFF_R2_000786.LAB | 14:47 | 12.25        | 13.4         | 0.86        | 0.10        | 190.6         | 0.97        | 11.59        |                             |
| MILLOFF_R2_000787.LAB | 14:48 | 12.23        | 13.4         | 0.90        | 0.10        | 190.7         | 0.97        | 11.80        |                             |
| MILLOFF_R2_000788.LAB | 14:49 | 12.25        | 13.2         | 0.87        | 0.10        | 190.6         | 0.97        | 11.85        |                             |
| MILLOFF_R2_000789.LAB | 14:50 | 12.34        | 13.9         | 0.84        | 0.10        | 190.7         | 0.97        | 11.78        |                             |
| MILLOFF_R2_000790.LAB | 14:51 | 12.28        | 13.8         | 0.91        | 0.10        | 190.7         | 0.97        | 11.16        |                             |
| MILLOFF_R2_000791.LAB | 14:52 | 12.21        | 14.0         | 0.86        | 0.10        | 190.7         | 0.97        | 11.25        |                             |
| MILLOFF_R2_000792.LAB | 14:53 | 12.31        | 14.1         | 0.85        | 0.10        | 190.7         | 0.97        | 11.24        |                             |
| MILLOFF_R2_000793.LAB | 14:54 | 12.24        | 14.2         | 0.83        | 0.10        | 190.7         | 0.97        | 11.11        |                             |
| MILLOFF_R2_000794.LAB | 14:55 | 12.26        | 14.1         | 0.90        | 0.10        | 190.6         | 0.97        | 11.10        |                             |
| MILLOFF_R2_000795.LAB | 14:56 | 12.47        | 14.2         | 0.93        | 0.10        | 190.6         | 0.97        | 11.06        |                             |
| MILLOFF_R2_000796.LAB | 14:57 | 12.57        | 14.4         | 0.94        | 0.10        | 190.6         | 0.97        | 11.02        |                             |
| MILLOFF_R2_000797.LAB | 14:58 | 12.53        | 14.3         | 0.93        | 0.10        | 190.6         | 0.97        | 10.99        |                             |
| MILLOFF_R2_000798.LAB | 14:59 | 12.44        | 14.2         | 0.89        | 0.10        | 190.6         | 0.97        | 11.00        |                             |
| MILLOFF_R2_000799.LAB | 15:00 | 12.50        | 14.2         | 0.97        | 0.10        | 190.7         | 0.97        | 10.92        |                             |
| MILLOFF_R2_000800.LAB | 15:01 | 12.51        | 14.0         | 0.92        | 0.10        | 190.6         | 0.97        | 11.05        |                             |
| MILLOFF_R2_000801.LAB | 15:02 | 12.49        | 14.3         | 0.90        | 0.10        | 190.6         | 0.97        | 11.18        |                             |
| MILLOFF_R2_000802.LAB | 15:03 | 12.57        | 14.5         | 1.02        | 0.10        | 190.6         | 0.97        | 10.88        |                             |
| MILLOFF_R2_000803.LAB | 15:04 | 12.46        | 14.3         | 0.95        | 0.10        | 190.6         | 0.97        | 10.97        |                             |
| MILLOFF_R2_000804.LAB | 15:05 | 12.57        | 14.4         | 0.87        | 0.10        | 190.7         | 0.97        | 11.04        |                             |
| MILLOFF_R2_000805.LAB | 15:06 | 12.59        | 14.5         | 0.99        | 0.10        | 190.8         | 0.97        | 11.01        |                             |
| MILLOFF_R2_000806.LAB | 15:07 | 12.56        | 14.4         | 0.95        | 0.10        | 190.9         | 0.97        | 10.93        |                             |
| MILLOFF_R2_000807.LAB | 15:08 | 12.57        | 14.5         | 0.96        | 0.10        | 190.9         | 0.97        | 10.94        |                             |
| MILLOFF_R2_000808.LAB | 15:09 | 12.36        | 14.2         | 0.93        | 0.10        | 190.9         | 0.97        | 10.94        |                             |
| MILLOFF_R2_000809.LAB | 15:10 | 12.35        | 14.1         | 0.86        | 0.10        | 190.8         | 0.97        | 10.94        |                             |
| MILLOFF_R2_000810.LAB | 15:11 | 12.43        | 14.2         | 0.94        | 0.10        | 190.7         | 0.97        | 11.10        |                             |
| MILLOFF_R2_000811.LAB | 15:12 | 12.35        | 14.2         | 0.88        | 0.10        | 190.7         | 0.97        | 11.15        |                             |
| MILLOFF_R2_000812.LAB | 15:13 | 12.36        | 14.2         | 0.89        | 0.10        | 190.7         | 0.97        | 11.04        |                             |
| MILLOFF_R2_000813.LAB | 15:14 | 12.34        | 14.3         | 0.95        | 0.10        | 190.8         | 0.97        | 11.10        |                             |
| <b>Average</b>        |       | <b>12.42</b> | <b>14.21</b> | <b>0.89</b> | <b>0.10</b> | <b>190.72</b> | <b>0.97</b> | <b>11.11</b> |                             |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Test Location: Main Kiln Stack  
 Date: 11/14/23

Run 3

| Spectrum              | Time  | FTIR Data    |              |             |             |               | Cell Temp   | Pressure     | Analyzer Data<br>O2 % (dry) |
|-----------------------|-------|--------------|--------------|-------------|-------------|---------------|-------------|--------------|-----------------------------|
|                       |       | H2O %        | CO2 % (wet)  | HCN ppmvw   | HF ppmvw    |               |             |              |                             |
| MILLOFF_R3_000894.LAB | 15:40 | 12.03        | 14.5         | 0.92        | 0.10        | 190.2         | 0.97        | 11.01        |                             |
| MILLOFF_R3_000895.LAB | 15:41 | 12.05        | 14.9         | 1.00        | 0.10        | 190.5         | 0.97        | 10.82        |                             |
| MILLOFF_R3_000896.LAB | 15:42 | 12.03        | 14.9         | 0.95        | 0.10        | 191.0         | 0.97        | 10.86        |                             |
| MILLOFF_R3_000897.LAB | 15:43 | 12.08        | 14.6         | 1.00        | 0.10        | 191.1         | 0.97        | 11.00        |                             |
| MILLOFF_R3_000898.LAB | 15:44 | 12.06        | 14.2         | 0.91        | 0.10        | 191.1         | 0.97        | 11.17        |                             |
| MILLOFF_R3_000899.LAB | 15:45 | 12.07        | 14.1         | 0.93        | 0.10        | 191.1         | 0.97        | 11.21        |                             |
| MILLOFF_R3_000900.LAB | 15:46 | 12.11        | 13.9         | 0.97        | 0.10        | 191.1         | 0.97        | 11.24        |                             |
| MILLOFF_R3_000901.LAB | 15:47 | 12.10        | 13.9         | 0.90        | 0.10        | 191.1         | 0.97        | 11.33        |                             |
| MILLOFF_R3_000902.LAB | 15:48 | 12.00        | 13.8         | 0.97        | 0.10        | 191.1         | 0.97        | 11.38        |                             |
| MILLOFF_R3_000903.LAB | 15:49 | 12.07        | 14.0         | 0.96        | 0.10        | 191.1         | 0.97        | 11.32        |                             |
| MILLOFF_R3_000904.LAB | 15:50 | 12.11        | 14.1         | 0.97        | 0.10        | 191.1         | 0.97        | 11.25        |                             |
| MILLOFF_R3_000905.LAB | 15:51 | 12.02        | 14.1         | 0.95        | 0.10        | 191.1         | 0.97        | 11.31        |                             |
| MILLOFF_R3_000906.LAB | 15:52 | 12.05        | 13.9         | 0.96        | 0.10        | 191.0         | 0.97        | 11.33        |                             |
| MILLOFF_R3_000907.LAB | 15:53 | 12.10        | 14.0         | 0.91        | 0.10        | 190.9         | 0.97        | 11.45        |                             |
| MILLOFF_R3_000908.LAB | 15:54 | 11.94        | 14.2         | 0.99        | 0.10        | 190.9         | 0.97        | 11.28        |                             |
| MILLOFF_R3_000909.LAB | 15:55 | 11.92        | 14.1         | 0.94        | 0.10        | 190.9         | 0.97        | 11.18        |                             |
| MILLOFF_R3_000910.LAB | 15:56 | 11.95        | 14.1         | 0.98        | 0.10        | 190.8         | 0.97        | 11.29        |                             |
| MILLOFF_R3_000911.LAB | 15:57 | 12.10        | 14.2         | 0.91        | 0.10        | 190.8         | 0.97        | 11.26        |                             |
| MILLOFF_R3_000912.LAB | 15:58 | 12.04        | 14.2         | 1.00        | 0.10        | 190.8         | 0.97        | 11.20        |                             |
| MILLOFF_R3_000913.LAB | 15:59 | 12.02        | 14.0         | 0.98        | 0.10        | 190.8         | 0.97        | 11.22        |                             |
| MILLOFF_R3_000914.LAB | 16:00 | 11.91        | 13.8         | 1.03        | 0.10        | 190.7         | 0.97        | 11.32        |                             |
| MILLOFF_R3_000915.LAB | 16:01 | 11.70        | 13.7         | 1.06        | 0.10        | 190.6         | 0.97        | 11.49        |                             |
| MILLOFF_R3_000916.LAB | 16:02 | 11.64        | 13.8         | 1.03        | 0.10        | 190.6         | 0.97        | 11.55        |                             |
| MILLOFF_R3_000917.LAB | 16:03 | 11.72        | 13.8         | 1.04        | 0.10        | 190.6         | 0.97        | 11.55        |                             |
| MILLOFF_R3_000918.LAB | 16:04 | 11.77        | 13.8         | 1.05        | 0.10        | 190.6         | 0.97        | 11.46        |                             |
| MILLOFF_R3_000919.LAB | 16:05 | 11.84        | 13.9         | 1.08        | 0.10        | 190.6         | 0.97        | 11.46        |                             |
| MILLOFF_R3_000920.LAB | 16:06 | 11.87        | 14.0         | 1.03        | 0.10        | 190.6         | 0.97        | 11.35        |                             |
| MILLOFF_R3_000921.LAB | 16:07 | 11.89        | 14.3         | 0.96        | 0.10        | 190.7         | 0.97        | 11.35        |                             |
| MILLOFF_R3_000922.LAB | 16:08 | 11.86        | 14.4         | 1.04        | 0.10        | 190.7         | 0.97        | 11.24        |                             |
| MILLOFF_R3_000923.LAB | 16:09 | 11.83        | 14.3         | 1.10        | 0.10        | 190.7         | 0.97        | 11.23        |                             |
| MILLOFF_R3_000924.LAB | 16:10 | 11.94        | 14.4         | 0.96        | 0.10        | 190.7         | 0.97        | 11.18        |                             |
| MILLOFF_R3_000925.LAB | 16:11 | 11.87        | 14.1         | 1.03        | 0.10        | 190.7         | 0.97        | 11.27        |                             |
| MILLOFF_R3_000926.LAB | 16:12 | 11.91        | 14.2         | 1.08        | 0.10        | 190.7         | 0.97        | 11.32        |                             |
| MILLOFF_R3_000927.LAB | 16:13 | 11.93        | 14.3         | 0.99        | 0.10        | 190.6         | 0.97        | 11.18        |                             |
| MILLOFF_R3_000928.LAB | 16:14 | 11.86        | 14.4         | 1.07        | 0.10        | 190.6         | 0.97        | 11.19        |                             |
| MILLOFF_R3_000929.LAB | 16:15 | 12.44        | 14.5         | 0.97        | 0.10        | 190.6         | 0.97        | 11.19        |                             |
| MILLOFF_R3_000930.LAB | 16:16 | 12.01        | 14.5         | 1.10        | 0.10        | 190.6         | 0.97        | 10.95        |                             |
| MILLOFF_R3_000931.LAB | 16:17 | 12.12        | 14.2         | 1.03        | 0.10        | 190.6         | 0.97        | 11.01        |                             |
| MILLOFF_R3_000932.LAB | 16:18 | 11.78        | 13.8         | 1.10        | 0.10        | 190.7         | 0.97        | 11.08        |                             |
| MILLOFF_R3_000933.LAB | 16:19 | 11.54        | 13.4         | 1.04        | 0.10        | 190.7         | 0.97        | 11.22        |                             |
| MILLOFF_R3_000934.LAB | 16:20 | 11.94        | 13.1         | 0.96        | 0.10        | 190.7         | 0.97        | 11.59        |                             |
| MILLOFF_R3_000935.LAB | 16:21 | 11.88        | 13.8         | 0.98        | 0.10        | 190.6         | 0.97        | 11.81        |                             |
| MILLOFF_R3_000936.LAB | 16:22 | 12.22        | 13.7         | 0.99        | 0.10        | 190.7         | 0.97        | 11.67        |                             |
| MILLOFF_R3_000937.LAB | 16:23 | 11.63        | 12.9         | 1.05        | 0.10        | 190.7         | 0.97        | 10.95        |                             |
| MILLOFF_R3_000938.LAB | 16:24 | 11.68        | 13.4         | 1.04        | 0.10        | 190.7         | 0.97        | 11.19        |                             |
| MILLOFF_R3_000939.LAB | 16:25 | 11.93        | 13.5         | 1.01        | 0.10        | 190.7         | 0.97        | 11.84        |                             |
| MILLOFF_R3_000940.LAB | 16:26 | 12.00        | 13.6         | 0.98        | 0.10        | 190.7         | 0.97        | 11.55        |                             |
| MILLOFF_R3_000941.LAB | 16:27 | 12.25        | 13.8         | 1.02        | 0.10        | 190.7         | 0.97        | 11.42        |                             |
| MILLOFF_R3_000942.LAB | 16:28 | 11.88        | 14.1         | 1.02        | 0.10        | 190.7         | 0.97        | 11.49        |                             |
| MILLOFF_R3_000943.LAB | 16:29 | 11.78        | 14.3         | 1.06        | 0.10        | 190.7         | 0.97        | 11.53        |                             |
| MILLOFF_R3_000944.LAB | 16:30 | 11.96        | 14.5         | 1.06        | 0.10        | 190.7         | 0.97        | 11.43        |                             |
| MILLOFF_R3_000945.LAB | 16:31 | 12.38        | 14.9         | 1.06        | 0.10        | 190.7         | 0.97        | 11.22        |                             |
| MILLOFF_R3_000946.LAB | 16:32 | 12.12        | 14.9         | 1.04        | 0.10        | 190.7         | 0.97        | 11.17        |                             |
| MILLOFF_R3_000947.LAB | 16:33 | 11.99        | 15.0         | 1.03        | 0.10        | 190.7         | 0.97        | 10.97        |                             |
| MILLOFF_R3_000948.LAB | 16:34 | 12.00        | 15.0         | 1.04        | 0.10        | 190.7         | 0.97        | 10.86        |                             |
| MILLOFF_R3_000949.LAB | 16:35 | 12.09        | 15.0         | 1.04        | 0.10        | 190.8         | 0.97        | 10.92        |                             |
| MILLOFF_R3_000950.LAB | 16:36 | 12.37        | 14.8         | 1.05        | 0.10        | 190.8         | 0.97        | 11.00        |                             |
| MILLOFF_R3_000951.LAB | 16:37 | 12.34        | 14.7         | 1.10        | 0.10        | 190.8         | 0.97        | 10.97        |                             |
| MILLOFF_R3_000952.LAB | 16:38 | 12.26        | 14.4         | 1.07        | 0.10        | 190.9         | 0.97        | 10.92        |                             |
| MILLOFF_R3_000953.LAB | 16:39 | 11.99        | 14.3         | 1.08        | 0.10        | 191.0         | 0.97        | 11.01        |                             |
| <b>Average</b>        |       | <b>11.98</b> | <b>14.15</b> | <b>1.01</b> | <b>0.10</b> | <b>190.78</b> | <b>0.97</b> | <b>11.25</b> |                             |

**Method 1 and 2 Cyclonic Flow Check Data**

**Project Number:** M234605  
**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Location:** Kiln Stack  
**Pitot ID:** S8-031A  
**Pitot Coefficient:** 0.820  
**Probe Length:** 8

**Source Condition:** Mill On  
**Run No.:** 1  
**Date:** 11/14/2023  
**Start Time:** 7:20  
**End Time:** 7:40  
**RM Testers:** TRY/CLC  
**Port Length:** 12.00




| Port | Point | DP (in. H <sub>2</sub> O) | Sqrt. DP | Temp (°F) | Yaw Angle (°) | DP (in. H <sub>2</sub> O) at Null Point Angle | Velocity (V) | Port | Point | DP (in. H <sub>2</sub> O) | Sqrt. DP | Temp (°F) | Yaw Angle (°) | DP (in. H <sub>2</sub> O) at Null Point Angle | Velocity (V) |
|------|-------|---------------------------|----------|-----------|---------------|---|--------------|------|-------|---------------------------|----------|-----------|---------------|---|--------------|
| A    | 1     | 1.90                      | 1.3784   | 229.0     | 3.0           | 0.00  | 86.81        | B    | 1     | 2.20                      | 1.4832   | 231.0     | 3.0           | 0.00  | 93.54        |
| A    | 2     | 2.00                      | 1.4142   | 230.0     | 2.0           | 0.00  | 89.13        | B    | 2     | 1.90                      | 1.3784   | 232.0     | 4.0           | 0.00  | 87.00        |
| A    | 3     | 1.80                      | 1.3416   | 230.0     | 3.0           | 0.00  | 84.55        | B    | 3     | 2.00                      | 1.4142   | 233.0     | 3.0           | 0.00  | 89.32        |
| A    | 4     | 1.80                      | 1.3416   | 232.0     | 4.0           | 0.00  | 84.68        | B    | 4     | 1.90                      | 1.3784   | 233.0     | 3.0           | 0.00  | 87.06        |
| A    | 5     | 2.10                      | 1.4491   | 232.0     | 3.0           | 0.00  | 91.46        | B    | 5     | 1.80                      | 1.3416   | 233.0     | 4.0           | 0.00  | 84.74        |
| A    | 6     | 1.90                      | 1.3784   | 232.0     | 4.0           | 0.00  | 87.00        | B    | 6     | 1.80                      | 1.3416   | 232.0     | 2.0           | 0.00  | 84.68        |




Average Yaw Angle      3.2 °

**Stratification Test Results Summary**  
**CalPortland Company, Inc.**  
**Redding Cement Plant**  
**Main Kiln Stack**  
**November 14, 2023**

**Number of Ports Sampled:** 1  
**Number of Points per Port:** 3  
**Total Number of Traverse Points:** 3

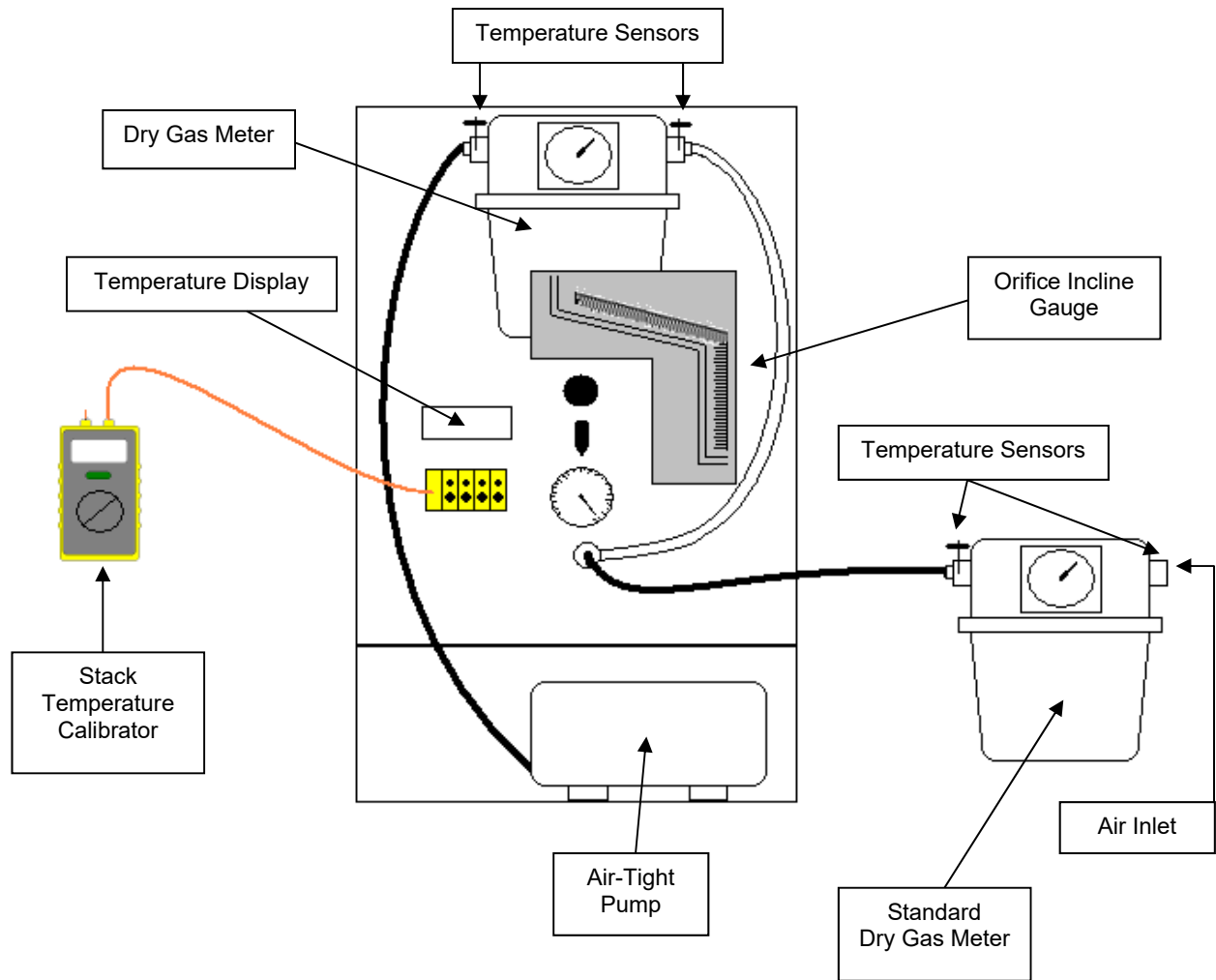
| Port No.       | Point No. | Time | O <sub>2</sub> % | Actual % Difference O <sub>2</sub> % | Mean Difference O <sub>2</sub> % |
|----------------|-----------|------|------------------|--------------------------------------|----------------------------------|
| 1              | 1         | 7:41 | 12.42            | 1.19                                 | 0.15                             |
|                | 2         | 7:45 | 12.71            | 1.11                                 | 0.14                             |
|                | 3         | 7:49 | 12.58            | 0.08                                 | 0.01                             |
| <b>Average</b> |           |      | <b>12.57</b>     |                                      |                                  |

One point traverse (<5% difference)   
Three point traverse (0.4, 1.2, and 2.0 meters), <10% difference   
Twelve point traverse (Method 1 points) >10% difference 

One point traverse (<0.3% mean difference)   
Three point traverse (0.4, 1.2, and 2.0 meters), < 0.5% mean difference for O<sub>2</sub>   
Twelve point traverse (Method 1 points) >0.5% mean difference for O<sub>2</sub> 

**Appendix G - Calibration Data**

# Dry Gas Meter/Control Module Calibration Diagram



Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM54  
 Standard Meter No. 18654530  
 Standard Meter (Y) 0.99730

Date: October 17, 2023  
 Calibrated By: IB  
 Barometric Pressure: 27.90

| Run Number | Orifice Setting in H <sub>2</sub> O Chg (H) | Standard Meter Gas Volume vr | Dry Gas Meter Gas Volume vd | Standard Meter Temp. F° tr | Dry Gas Meter Inlet Temp. F° tdi | Dry Gas Meter Outlet Temp. F° tdo | Dry Gas Meter Avg. Temp. F° td | Time Min | Time Sec | Y     | Chg (H) |
|------------|---|------------------------------|-----------------------------|----------------------------|----------------------------------|-----------------------------------|--------------------------------|----------|----------|-------|---------|
| Final      |   | 63.100                       | 78.370                      | 70                         | 71                               | 71                                |                                |          |          |       |         |
| Initial    |   | 57.720                       | 72.920                      | 70                         | 70                               | 70                                |                                |          |          |       |         |
| Difference | 1   0.20                                    | 5.380                        | 5.450                       | 70                         | 71                               | 71                                | 71                             | 18       | 0        | 0.985 | 1.361   |
| Final      |   | 68.591                       | 83.944                      | 71                         | 72                               | 72                                |                                |          |          |       |         |
| Initial    |   | 63.100                       | 78.370                      | 70                         | 71                               | 71                                |                                |          |          |       |         |
| Difference | 2   0.50                                    | 5.491                        | 5.574                       | 71                         | 72                               | 72                                | 72                             | 12       | 3        | 0.983 | 1.464   |
| Final      |   | 74.004                       | 89.414                      | 72                         | 73                               | 73                                |                                |          |          |       |         |
| Initial    |   | 68.591                       | 83.944                      | 71                         | 72                               | 72                                |                                |          |          |       |         |
| Difference | 3   0.70                                    | 5.413                        | 5.470                       | 72                         | 73                               | 73                                | 73                             | 10       | 1        | 0.987 | 1.460   |
| Final      |   | 79.380                       | 94.860                      | 72                         | 74                               | 74                                |                                |          |          |       |         |
| Initial    |   | 74.004                       | 89.414                      | 72                         | 73                               | 73                                |                                |          |          |       |         |
| Difference | 4   0.90                                    | 5.376                        | 5.446                       | 72                         | 74                               | 74                                | 74                             | 9        | 0        | 0.985 | 1.536   |
| Final      |   | 84.655                       | 100.184                     | 72                         | 74                               | 74                                |                                |          |          |       |         |
| Initial    |   | 79.380                       | 94.860                      | 72                         | 74                               | 74                                |                                |          |          |       |         |
| Difference | 5   1.20                                    | 5.275                        | 5.324                       | 72                         | 74                               | 74                                | 74                             | 8        | 0        | 0.989 | 1.679   |
| Final      |   | 57.720                       | 72.920                      | 70                         | 70                               | 70                                |                                |          |          |       |         |
| Initial    |   | 52.640                       | 67.840                      | 69                         | 69                               | 69                                |                                |          |          |       |         |
| Difference | 6   2.00                                    | 5.080                        | 5.080                       | 70                         | 70                               | 70                                | 70                             | 6        | 0        | 0.992 | 1.696   |

Average 0.987 1.533

**Stack Temperature Sensor Calibration**

Meter Box # : CM 18 Name : IB

Ambient Temperature : 73.4 °F Date : October 17, 2023

Calibrator Model # : CL940A

Serial # : 526

Date Of Certification : December 28, 2022

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

| <b>Reference Source Temperature (°F)</b> | <b>Test Thermometer Temperature (°F)</b> | <b>Temperature Difference %</b> |
|--|--|---------------------------------|
| 0  | -1                                       | 0.2                             |
| 250                                      | 248                                      | 0.3                             |
| 600                                      | 597                                      | 0.3                             |
| 1200                                     | 1199                                     | 0.1                             |

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM18  
 Standard Meter No. 18654530  
 Standard Meter (Y) 0.99730

Date: December 7, 2023  
 Calibrated By: DV  
 Barometric Pressure: 28.16

| Run Number | Orifice Setting in H <sub>2</sub> O Chg (H) | Standard Meter Gas Volume vr | Dry Gas Meter Gas Volume vd | Standard Meter Temp. F° tr | Dry Gas Meter Inlet Temp. F° tdi | Dry Gas Meter Outlet Temp. F° tdo | Dry Gas Meter Avg. Temp. F° td | Time Min | Time Sec | Y     | Chg (H) |
|------------|---|------------------------------|-----------------------------|----------------------------|----------------------------------|-----------------------------------|--------------------------------|----------|----------|-------|---------|
| Final      |   | 37.180                       | 61.955                      | 65                         | 69                               | 68                                |                                |          |          |       |         |
| Initial    |   | 32.123                       | 56.846                      | 65                         | 68                               | 66                                |                                |          |          |       |         |
| Difference | 1   0.20                                    | 5.057                        | 5.109                       | 65                         | 69                               | 67                                | 68                             | 18       | 21       | 0.992 | 1.564   |
| Final      |   | 32.123                       | 56.846                      | 65                         | 68                               | 66                                |                                |          |          |       |         |
| Initial    |   | 26.765                       | 51.410                      | 64                         | 67                               | 65                                |                                |          |          |       |         |
| Difference | 2   0.50                                    | 5.358                        | 5.436                       | 65                         | 68                               | 66                                | 67                             | 12       | 12       | 0.985 | 1.541   |
| Final      |   | 26.765                       | 51.410                      | 64                         | 67                               | 65                                |                                |          |          |       |         |
| Initial    |   | 21.369                       | 46.097                      | 63                         | 65                               | 64                                |                                |          |          |       |         |
| Difference | 3   0.70                                    | 5.396                        | 5.313                       | 64                         | 66                               | 65                                | 65                             | 10       | 2        | 1.014 | 1.436   |
| Final      |   | 21.369                       | 46.097                      | 63                         | 65                               | 64                                |                                |          |          |       |         |
| Initial    |   | 15.896                       | 40.585                      | 63                         | 64                               | 63                                |                                |          |          |       |         |
| Difference | 4   0.90                                    | 5.473                        | 5.512                       | 63                         | 65                               | 64                                | 64                             | 9        | 0        | 0.990 | 1.445   |
| Final      |   | 42.896                       | 67.822                      | 65                         | 70                               | 68                                |                                |          |          |       |         |
| Initial    |   | 37.449                       | 62.323                      | 65                         | 69                               | 68                                |                                |          |          |       |         |
| Difference | 5   1.20                                    | 5.447                        | 5.499                       | 65                         | 70                               | 68                                | 69                             | 8        | 17       | 0.992 | 1.645   |
| Final      |   | 10.794                       | 35.460                      | 63                         | 63                               | 63                                |                                |          |          |       |         |
| Initial    |   | 5.348                        | 30.047                      | 62                         | 63                               | 63                                |                                |          |          |       |         |
| Difference | 6   2.00                                    | 5.446                        | 5.413                       | 63                         | 63                               | 63                                | 63                             | 6        | 4        | 0.999 | 1.473   |

Average **0.995** **1.517**

| <b>Stack Temperature Sensor Calibration</b> |        |        |           |
|---|--------|--------|-----------|
| Temperature ID :                            | 100770 | Name : | DV        |
| Ambient Temperature, °F :                   | 67.8   | Date : | 12/7/2023 |

| <b>Temperature Calibrator</b> |        |                     |                   |
|-------------------------------|--------|---------------------|-------------------|
| Model # :                     | CL940A | Certification Date: | December 28, 2022 |
| Serial # :                    | 526    | Expiration Date:    | December 29, 2023 |

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

| <b>Reference Source Temperature (°F)</b> | <b>Test Thermometer Temperature (°F)</b> | <b>Temperature Difference %</b> |
|--|--|---------------------------------|
| 0  | -1                                       | 0.2                             |
| 250                                      | 248                                      | 0.3                             |
| 600                                      | 597                                      | 0.3                             |
| 1200                                     | 1199                                     | 0.1                             |

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM45  
 Standard Meter No. 18654530  
 Standard Meter (Y) 0.99730

Date: October 25, 2023  
 Calibrated By: ER  
 Barometric Pressure: 28.07

| Run Number | Orifice Setting in H <sub>2</sub> O Chg (H) | Standard Meter Gas Volume vr | Dry Gas Meter Gas Volume vd | Standard Meter Temp. F° tr | Dry Gas Meter Inlet Temp. F° tdi | Dry Gas Meter Outlet Temp. F° tdo | Dry Gas Meter Avg. Temp. F° td | Time Min | Time Sec | Y     | Chg (H) |
|------------|---|------------------------------|-----------------------------|----------------------------|----------------------------------|-----------------------------------|--------------------------------|----------|----------|-------|---------|
| Final      |   | 55.157                       | 83.483                      | 71                         | 70                               | 70                                |                                |          |          |       |         |
| Initial    |   | 50.075                       | 78.368                      | 70                         | 69                               | 69                                |                                |          |          |       |         |
| Difference | 1   0.20                                    | 5.082                        | 5.115                       | 71                         | 70                               | 70                                | 70                             | 18       | 10       | 0.988 | 1.550   |
| Final      |   | 60.156                       | 88.610                      | 71                         | 72                               | 72                                |                                |          |          |       |         |
| Initial    |   | 55.107                       | 83.583                      | 71                         | 70                               | 70                                |                                |          |          |       |         |
| Difference | 2   0.50                                    | 5.049                        | 5.027                       | 71                         | 71                               | 71                                | 71                             | 12       | 5        | 1.000 | 1.735   |
| Final      |   | 65.214                       | 93.743                      | 72                         | 73                               | 73                                |                                |          |          |       |         |
| Initial    |   | 60.156                       | 88.610                      | 71                         | 72                               | 72                                |                                |          |          |       |         |
| Difference | 3   0.70                                    | 5.058                        | 5.133                       | 72                         | 73                               | 73                                | 73                             | 10       | 12       | 0.983 | 1.723   |
| Final      |   | 70.351                       | 98.824                      | 73                         | 74                               | 74                                |                                |          |          |       |         |
| Initial    |   | 65.214                       | 93.743                      | 72                         | 73                               | 73                                |                                |          |          |       |         |
| Difference | 4   0.90                                    | 5.137                        | 5.081                       | 73                         | 74                               | 74                                | 74                             | 9        | 15       | 1.008 | 1.770   |
| Final      |   | 50.175                       | 78.368                      | 70                         | 69                               | 69                                |                                |          |          |       |         |
| Initial    |   | 45.061                       | 73.232                      | 69                         | 69                               | 69                                |                                |          |          |       |         |
| Difference | 5   1.20                                    | 5.114                        | 5.136                       | 70                         | 69                               | 69                                | 69                             | 8        | 3        | 0.989 | 1.798   |
| Final      |   | 39.305                       | 67.255                      | 68                         | 68                               | 68                                |                                |          |          |       |         |
| Initial    |   | 34.281                       | 62.201                      | 68                         | 67                               | 67                                |                                |          |          |       |         |
| Difference | 6   2.00                                    | 5.024                        | 5.054                       | 68                         | 68                               | 68                                | 68                             | 6        | 8        | 0.985 | 1.797   |

Average                      **0.992**                      **1.729**

| <b>Stack Temperature Sensor Calibration</b> |        |        |            |
|---|--------|--------|------------|
| Temperature ID :                            | 100769 | Name : | ER         |
| Ambient Temperature, °F :                   | 69     | Date : | 10/25/2023 |

| <b>Temperature Calibrator</b> |          |                     |            |
|-------------------------------|----------|---------------------|------------|
| Model # :                     | CL23A    | Certification Date: | May 1,2023 |
| Serial # :                    | T-285668 | Expiration Date:    | May 2,2024 |

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

| <b>Reference Source Temperature (°F)</b> | <b>Test Thermometer Temperature (°F)</b> | <b>Temperature Difference %</b> |
|--|--|---------------------------------|
| 0  | 1  | 0.2                             |
| 250                                      | 252                                      | 0.3                             |
| 600                                      | 601                                      | 0.1                             |
| 1200                                     | 1204                                     | 0.2                             |

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Meter Box Calibration

Dry Gas Meter Calibration Data

Dry Gas Meter No. CM45  
 Standard Meter No. 18654530  
 Standard Meter (Y) 0.99730

Date: December 8, 2023  
 Calibrated By: ER  
 Barometric Pressure: 28.27

| Run Number | Orifice Setting in H <sub>2</sub> O Chg (H) | Standard Meter Gas Volume vr | Dry Gas Meter Gas Volume vd | Standard Meter Temp. F° tr | Dry Gas Meter Inlet Temp. F° tdi | Dry Gas Meter Outlet Temp. F° tdo | Dry Gas Meter Avg. Temp. F° td | Time Min | Time Sec | Y     | Chg (H) |
|------------|---|------------------------------|-----------------------------|----------------------------|----------------------------------|-----------------------------------|--------------------------------|----------|----------|-------|---------|
| Final      |   | 52.925                       | 41.165                      | 61                         | 63                               | 63                                |                                |          |          |       |         |
| Initial    |   | 47.906                       | 36.110                      | 61                         | 62                               | 62                                |                                |          |          |       |         |
| Difference | 1   0.20                                    | 5.019                        | 5.055                       | 61                         | 63                               | 63                                | 63                             | 18       | 15       | 0.993 | 1.556   |
| Final      |   | 57.944                       | 46.214                      | 61                         | 63                               | 63                                |                                |          |          |       |         |
| Initial    |   | 52.925                       | 41.165                      | 61                         | 63                               | 63                                |                                |          |          |       |         |
| Difference | 2   0.50                                    | 5.019                        | 5.049                       | 61                         | 63                               | 63                                | 63                             | 12       | 5        | 0.994 | 1.704   |
| Final      |   | 62.985                       | 51.262                      | 62                         | 64                               | 64                                |                                |          |          |       |         |
| Initial    |   | 57.944                       | 46.214                      | 61                         | 63                               | 63                                |                                |          |          |       |         |
| Difference | 3   0.70                                    | 5.041                        | 5.048                       | 62                         | 64                               | 64                                | 64                             | 10       | 10       | 0.998 | 1.676   |
| Final      |   | 68.012                       | 56.366                      | 62                         | 64                               | 64                                |                                |          |          |       |         |
| Initial    |   | 62.985                       | 51.262                      | 62                         | 64                               | 64                                |                                |          |          |       |         |
| Difference | 4   0.90                                    | 5.027                        | 5.104                       | 62                         | 64                               | 64                                | 64                             | 9        | 5        | 0.984 | 1.731   |
| Final      |   | 73.052                       | 61.450                      | 62                         | 64                               | 64                                |                                |          |          |       |         |
| Initial    |   | 68.012                       | 56.366                      | 62                         | 64                               | 64                                |                                |          |          |       |         |
| Difference | 5   1.20                                    | 5.040                        | 5.084                       | 62                         | 64                               | 64                                | 64                             | 8        | 5        | 0.989 | 1.818   |
| Final      |   | 47.906                       | 36.110                      | 61                         | 62                               | 62                                |                                |          |          |       |         |
| Initial    |   | 42.897                       | 31.050                      | 61                         | 63                               | 63                                |                                |          |          |       |         |
| Difference | 6   2.00                                    | 5.009                        | 5.060                       | 61                         | 63                               | 63                                | 63                             | 6        | 5        | 0.985 | 1.736   |

Average **0.990** **1.704**

**Stack Temperature Sensor Calibration**

Meter Box # : CM45 Name : ER

Ambient Temperature : 62.3 °F Date : December 8, 2023

Calibrator Model # : CL940

Serial # : 526

Date Of Certification : December 28, 2022

Primary Standards Directly Traceable National Institute of Standards and Technology (NIST)

| <b>Reference Source Temperature (°F)</b> | <b>Test Thermometer Temperature (°F)</b> | <b>Temperature Difference %</b> |
|--|--|---------------------------------|
| 0  | 1  | 0.2                             |
| 250                                      | 251                                      | 0.1                             |
| 600                                      | 600                                      | 0.0                             |
| 1200                                     | 1204                                     | 0.2                             |

$$\frac{(\text{Ref. Temp., } ^\circ\text{F} + 460) - (\text{Test Therm. Temp., } ^\circ\text{F} + 460)}{\text{Ref. Temp., } ^\circ\text{F} + 460} * 100 \leq 1.5 \%$$

Ref. Temp., °F + 460



# Airflow Sciences Corporation

## Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation  
 Wind Tunnel Location: Livonia, MI  
 Probe Type: S-Type Pitot  
 Probe ID: S8-031-A  
 Probe Calibration Date: 07/10/17  
 Test Point Location: center  
 Ambient Temperature (°F): 77.8  
 Barometric Pressure ("Hg): 29.23

| Repetition                         | Nominal Low Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |               | Calculated C <sub>p</sub> |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
|                                    |                                     | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (°) |                           |
| 1                                  | 60                                  | 0.81                                  | 77.8             | 1.18                   | 0             | 0.82                      |
| 2                                  | 60                                  | 0.80                                  | 77.8             | 1.18                   | 0             | 0.82                      |
| 3                                  | 60                                  | 0.81                                  | 77.8             | 1.18                   | 0             | 0.82                      |
| Average (C <sub>p(avg-low)</sub> ) |                                     |                                       |                  |                        |               | 0.82                      |

| Repetition                          | Nominal High Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |                 | Calculated C <sub>p</sub> |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
|                                     |                                      | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (deg) |                           |
| 1                                   | 90                                   | 1.81                                  | 77.8             | 2.63                   | 0               | 0.82                      |
| 2                                   | 90                                   | 1.81                                  | 77.8             | 2.62                   | 0               | 0.82                      |
| 3                                   | 90                                   | 1.81                                  | 77.8             | 2.63                   | 0               | 0.82                      |
| Average (C <sub>p(avg-high)</sub> ) |                                      |                                       |                  |                        |                 | 0.82                      |

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.49\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C<sub>p</sub> values shall be within +/- 3 %.  
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

|                              |
|------------------------------|
| <b>C<sub>p</sub> = 0.820</b> |
|------------------------------|



# Airflow Sciences Corporation

## Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation  
 Wind Tunnel Location: Livonia, MI  
 Probe Type: S-Type Pitot  
 Probe ID: S8-031-B  
 Probe Calibration Date: 07/10/17  
 Test Point Location: center  
 Ambient Temperature (°F): 77.5  
 Barometric Pressure ("Hg): 29.23

| Repetition                         | Nominal Low Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |               | Calculated C <sub>p</sub> |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
|                                    |                                     | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (°) |                           |
| 1                                  | 60                                  | 0.81                                  | 77.5             | 1.19                   | 0             | 0.82                      |
| 2                                  | 60                                  | 0.81                                  | 77.5             | 1.19                   | 0             | 0.82                      |
| 3                                  | 60                                  | 0.81                                  | 77.5             | 1.19                   | 0             | 0.82                      |
| Average (C <sub>p(avg-low)</sub> ) |                                     |                                       |                  |                        |               | 0.82                      |

| Repetition                          | Nominal High Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |                 | Calculated C <sub>p</sub> |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
|                                     |                                      | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (deg) |                           |
| 1                                   | 90                                   | 1.81                                  | 77.5             | 2.65                   | 0               | 0.82                      |
| 2                                   | 90                                   | 1.81                                  | 77.5             | 2.64                   | 0               | 0.82                      |
| 3                                   | 90                                   | 1.81                                  | 77.5             | 2.64                   | 0               | 0.82                      |
| Average (C <sub>p(avg-high)</sub> ) |                                      |                                       |                  |                        |                 | 0.82                      |

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.55\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C<sub>p</sub> values shall be within +/- 3 %.  
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

|                              |
|------------------------------|
| <b>C<sub>p</sub> = 0.818</b> |
|------------------------------|



# Airflow Sciences Corporation

## Probe Calibration for Method 2

### Data Collection and Analysis

Date: 6/8/2017  
 Temperature (°F): 72.2  
 Pressure ("Hg): 29.33  
 Personnel: wgj  
 Probe: S8-031-A

| Wind Tunnel Target DP [I.W.C] | Wind Tunnel Actual DP [I.W.C] | S-Probe DP [I.W.C.] | $C_p$ | $C_{p(avg)}$ | $C_p - C_{p(avg)}$ | $\sigma_{max}$ |      |
|-------------------------------|-------------------------------|---------------------|-------|--------------|--------------------|----------------|------|
| 0.81                          | 0.81                          | 1.19                | 0.818 | 0.818        | 0.000              | 0.001          | Pass |
| 0.81                          | 0.81                          | 1.19                | 0.818 |              | 0.000              |                |      |
| 0.81                          | 0.81                          | 1.19                | 0.817 |              | -0.001             |                |      |
| 1.81                          | 1.82                          | 2.63                | 0.823 | 0.822        | 0.001              | 0.001          | Pass |
| 1.81                          | 1.82                          | 2.64                | 0.822 |              | 0.000              |                |      |
| 1.81                          | 1.81                          | 2.64                | 0.820 |              | -0.001             |                |      |



# Airflow Sciences Corporation

## Probe Calibration for Method 2

### Data Collection and Analysis

Date: 6/8/2017  
 Temperature (°F): 72.0  
 Pressure ("Hg): 29.33  
 Personnel: wgj  
 Probe: S8-031-B

| Wind Tunnel Target DP [I.W.C] | Wind Tunnel Actual DP [I.W.C] | S-Probe DP [I.W.C.] | $C_p$ | $C_{p(avg)}$ | $C_p - C_{p(avg)}$ | $\sigma_{max}$ |      |
|-------------------------------|-------------------------------|---------------------|-------|--------------|--------------------|----------------|------|
| 0.81                          | 0.81                          | 1.19                | 0.817 | 0.816        | 0.000              | 0.001          | Pass |
| 0.81                          | 0.81                          | 1.19                | 0.817 |              | 0.000              |                |      |
| 0.81                          | 0.81                          | 1.19                | 0.816 |              | -0.001             |                |      |
| 1.81                          | 1.82                          | 2.65                | 0.820 | 0.820        | 0.000              | 0.000          | Pass |
| 1.81                          | 1.82                          | 2.65                | 0.820 |              | 0.000              |                |      |
| 1.81                          | 1.82                          | 2.64                | 0.820 |              | 0.000              |                |      |



# Airflow Sciences Corporation

## Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation  
 Wind Tunnel Location: Livonia, MI  
 Probe Type: S-Type Pitot  
 Probe ID: S8-031-A  
 Probe Calibration Date: 06/08/17  
 Test Point Location: center  
 Ambient Temperature (°F): 72.2  
 Barometric Pressure ("Hg): 29.33

| Repetition                         | Nominal Low Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |               | Calculated C <sub>p</sub> |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
|                                    |                                     | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (°) |                           |
| 1                                  | 60                                  | 0.81                                  | 72.2             | 1.19                   | 0             | 0.82                      |
| 2                                  | 60                                  | 0.81                                  | 72.2             | 1.19                   | 0             | 0.82                      |
| 3                                  | 60                                  | 0.81                                  | 72.2             | 1.19                   | 0             | 0.82                      |
| Average (C <sub>p(avg-low)</sub> ) |                                     |                                       |                  |                        |               | 0.82                      |

| Repetition                          | Nominal High Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |                 | Calculated C <sub>p</sub> |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
|                                     |                                      | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (deg) |                           |
| 1                                   | 90                                   | 1.82                                  | 72.2             | 2.63                   | 0               | 0.82                      |
| 2                                   | 90                                   | 1.82                                  | 72.2             | 2.64                   | 0               | 0.82                      |
| 3                                   | 90                                   | 1.81                                  | 72.2             | 2.64                   | 0               | 0.82                      |
| Average (C <sub>p(avg-high)</sub> ) |                                      |                                       |                  |                        |                 | 0.82                      |

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.51\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C<sub>p</sub> values shall be within +/- 3%.  
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

**C<sub>p</sub> = 0.820**



# Airflow Sciences Corporation

## Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation  
 Wind Tunnel Location: Livonia, MI  
 Probe Type: S-Type Pitot  
 Probe ID: S8-031-B  
 Probe Calibration Date: 06/08/17  
 Test Point Location: center  
 Ambient Temperature (°F): 72.0  
 Barometric Pressure ("Hg): 29.33

| Repetition                         | Nominal Low Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |               | Calculated C <sub>p</sub> |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
|                                    |                                     | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (°) |                           |
| 1                                  | 60                                  | 0.81                                  | 72.0             | 1.19                   | 0             | 0.82                      |
| 2                                  | 60                                  | 0.81                                  | 72.0             | 1.19                   | 0             | 0.82                      |
| 3                                  | 60                                  | 0.81                                  | 72.0             | 1.19                   | 0             | 0.82                      |
| Average (C <sub>p(avg-low)</sub> ) |                                     |                                       |                  |                        |               | 0.82                      |

| Repetition                          | Nominal High Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |                 | Calculated C <sub>p</sub> |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
|                                     |                                      | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (deg) |                           |
| 1                                   | 90                                   | 1.82                                  | 72.0             | 2.65                   | 0               | 0.82                      |
| 2                                   | 90                                   | 1.82                                  | 72.0             | 2.65                   | 0               | 0.82                      |
| 3                                   | 90                                   | 1.82                                  | 72.0             | 2.64                   | 0               | 0.82                      |
| Average (C <sub>p(avg-high)</sub> ) |                                      |                                       |                  |                        |                 | 0.82                      |

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.45\%}} \quad \text{Pass}$$

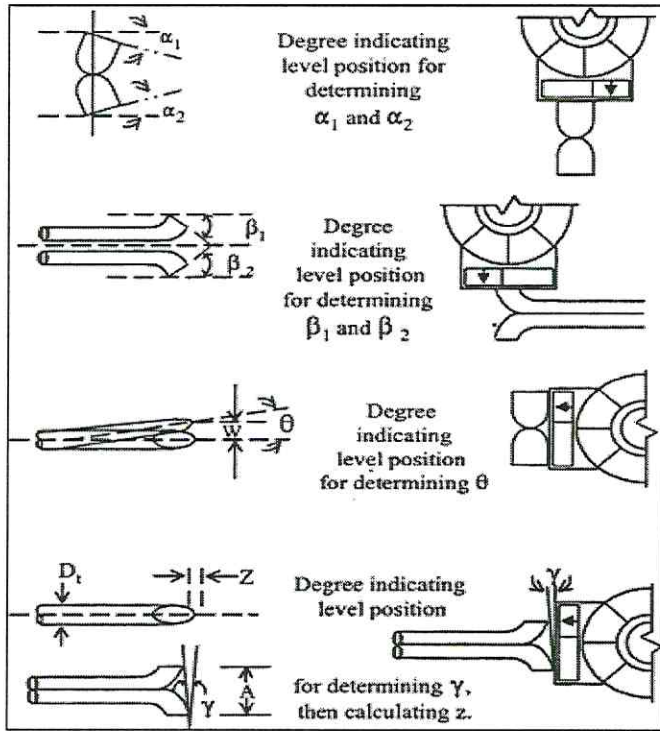
Note: (1) The percent difference between the low and high velocity setting C<sub>p</sub> values shall be within +/- 3 %.  
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

|                              |
|------------------------------|
| <b>C<sub>p</sub> = 0.818</b> |
|------------------------------|

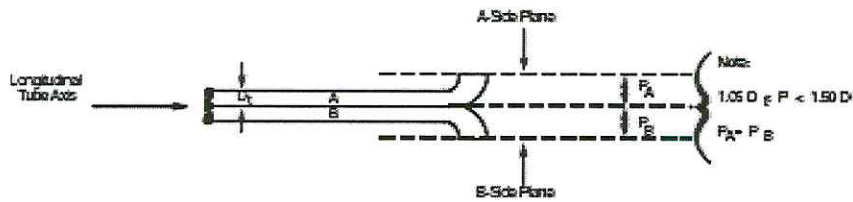


# Airflow Sciences Corporation

## Probe Inspection for Method 2



|            |           |      |
|------------|-----------|------|
| $\alpha_1$ | 0.8 (°)   | Pass |
| $\alpha_2$ | 0.3 (°)   | Pass |
| $\beta_1$  | 0.3 (°)   | Pass |
| $\beta_2$  | 1.1 (°)   | Pass |
| $D_t$      | 0.375 (") | Pass |
| $P_a$      | 0.459 (") | Pass |
| $P_b$      | 0.459 (") | Pass |
| $z$        | <0.02 (") | Pass |
| $w$        | 0.005 (") | Pass |



### Certification

I certify that Type S probe ID **S8-031** meets or exceeds all specifications, criteria, and applicable design features.

Certified by:                     Craig Rood                    

Date:                     6/8/2017



# Airflow Sciences Corporation

## Probe Calibration for Method 2

Data Collection and Analysis

Date: 8/31/2017  
Temperature (°F): 73.7  
Pressure ("Hg): 29.43  
Personnel: wgj  
Probe: S8-032-A

| Wind Tunnel Target DP [I.W.C.] | Wind Tunnel Actual DP [I.W.C.] | S-Probe DP [I.W.C.] | $C_p$ | $C_{p(avg)}$ | $C_p - C_{p(avg)}$ | $\sigma_{max}$ |      |
|--------------------------------|--------------------------------|---------------------|-------|--------------|--------------------|----------------|------|
| 0.81                           | 0.81                           | 1.18                | 0.820 | 0.821        | 0.000              | 0.000          | Pass |
| 0.81                           | 0.81                           | 1.18                | 0.821 |              | 0.000              |                |      |
| 0.81                           | 0.81                           | 1.18                | 0.821 |              | 0.000              |                |      |
| 1.81                           | 1.82                           | 2.62                | 0.825 | 0.824        | 0.000              | 0.000          | Pass |
| 1.81                           | 1.82                           | 2.63                | 0.824 |              | 0.000              |                |      |
| 1.81                           | 1.82                           | 2.63                | 0.824 |              | 0.000              |                |      |



# Airflow Sciences Corporation

## Probe Calibration for Method 2

Data Collection and Analysis

Date: 8/31/2017  
Temperature (°F): 74.5  
Pressure ("Hg): 29.43  
Personnel: wgj  
Probe: S8-032-B

| Wind Tunnel Target DP [I.W.C.] | Wind Tunnel Actual DP [I.W.C.] | S-Probe DP [I.W.C.] | C <sub>p</sub> | C <sub>p(avg)</sub> | C <sub>p</sub> -C <sub>p(avg)</sub> | σ <sub>max</sub> |      |
|--------------------------------|--------------------------------|---------------------|----------------|---------------------|-------------------------------------|------------------|------|
| 0.81                           | 0.81                           | 1.19                | 0.819          | 0.819               | 0.000                               | 0.000            | Pass |
| 0.81                           | 0.81                           | 1.19                | 0.819          |                     | 0.000                               |                  |      |
| 0.81                           | 0.81                           | 1.19                | 0.820          |                     | 0.000                               |                  |      |
| 1.81                           | 1.81                           | 2.63                | 0.823          | 0.823               | 0.000                               | 0.000            | Pass |
| 1.81                           | 1.82                           | 2.63                | 0.823          |                     | 0.000                               |                  |      |
| 1.81                           | 1.82                           | 2.63                | 0.823          |                     | 0.000                               |                  |      |

# Airflow Sciences Corporation

## Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation  
 Wind Tunnel Location: Livonia, MI  
 Probe Type: S-Type Pitot  
 Probe ID: S8-032-A  
 Probe Calibration Date: 08/31/17  
 Test Point Location: center  
 Ambient Temperature (°F): 73.7  
 Barometric Pressure ("Hg): 29.43

| Repetition                         | Nominal Low Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |               | Calculated C <sub>p</sub> |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
|                                    |                                     | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (°) |                           |
| 1                                  | 60                                  | 0.81                                  | 73.7             | 1.18                   | 0             | 0.82                      |
| 2                                  | 60                                  | 0.81                                  | 73.7             | 1.18                   | 0             | 0.82                      |
| 3                                  | 60                                  | 0.81                                  | 73.7             | 1.18                   | 0             | 0.82                      |
| Average (C <sub>p(avg-low)</sub> ) |                                     |                                       |                  |                        |               | 0.82                      |

| Repetition                          | Nominal High Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |                 | Calculated C <sub>p</sub> |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
|                                     |                                      | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (deg) |                           |
| 1                                   | 90                                   | 1.82                                  | 73.7             | 2.62                   | 0               | 0.82                      |
| 2                                   | 90                                   | 1.82                                  | 73.7             | 2.63                   | 0               | 0.82                      |
| 3                                   | 90                                   | 1.82                                  | 73.7             | 2.63                   | 0               | 0.82                      |
| Average (C <sub>p(avg-high)</sub> ) |                                      |                                       |                  |                        |                 | 0.82                      |

$$\text{\% Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.46\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C<sub>p</sub> values shall be within +/- 3 %.  
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

**C<sub>p</sub> = 0.822**



# Airflow Sciences Corporation

## Probe Calibration for Method 2

Wind Tunnel Facility: Airflow Sciences Corporation  
 Wind Tunnel Location: Livonia, MI  
 Probe Type: S-Type Pitot  
 Probe ID: S8-032-B  
 Probe Calibration Date: 08/31/17  
 Test Point Location: center  
 Ambient Temperature (°F): 74.5  
 Barometric Pressure ("Hg): 29.43

| Repetition                         | Nominal Low Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |               | Calculated C <sub>p</sub> |
|------------------------------------|-------------------------------------|---------------------------------------|------------------|------------------------|---------------|---------------------------|
|                                    |                                     | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (°) |                           |
| 1                                  | 60                                  | 0.81                                  | 74.5             | 1.19                   | 0             | 0.82                      |
| 2                                  | 60                                  | 0.81                                  | 74.5             | 1.19                   | 0             | 0.82                      |
| 3                                  | 60                                  | 0.81                                  | 74.5             | 1.19                   | 0             | 0.82                      |
| Average (C <sub>p(avg-low)</sub> ) |                                     |                                       |                  |                        |               | 0.82                      |

| Repetition                          | Nominal High Velocity Setting (ft/s) | Calibration Pitot                     |                  | Tested Probe           |                 | Calculated C <sub>p</sub> |
|-------------------------------------|--------------------------------------|---------------------------------------|------------------|------------------------|-----------------|---------------------------|
|                                     |                                      | DP <sub>std</sub> ("H <sub>2</sub> O) | Temperature (°F) | DP ("H <sub>2</sub> O) | Yaw Angle (deg) |                           |
| 1                                   | 90                                   | 1.81                                  | 74.5             | 2.63                   | 0               | 0.82                      |
| 2                                   | 90                                   | 1.82                                  | 74.5             | 2.63                   | 0               | 0.82                      |
| 3                                   | 90                                   | 1.82                                  | 74.5             | 2.63                   | 0               | 0.82                      |
| Average (C <sub>p(avg-high)</sub> ) |                                      |                                       |                  |                        |                 | 0.82                      |

$$\% \text{ Difference} = \frac{C_{p(\text{avg-low})} - C_{p(\text{avg-high})}}{C_{p(\text{avg-low})}} \times 100\% = \underline{\underline{-0.43\%}} \quad \text{Pass}$$

Note: (1) The percent difference between the low and high velocity setting C<sub>p</sub> values shall be within +/- 3 %.  
 (2) If calibrating a 3-D probe for this method, the pitch angle setting must be 0°.

**C<sub>p</sub> = 0.821**



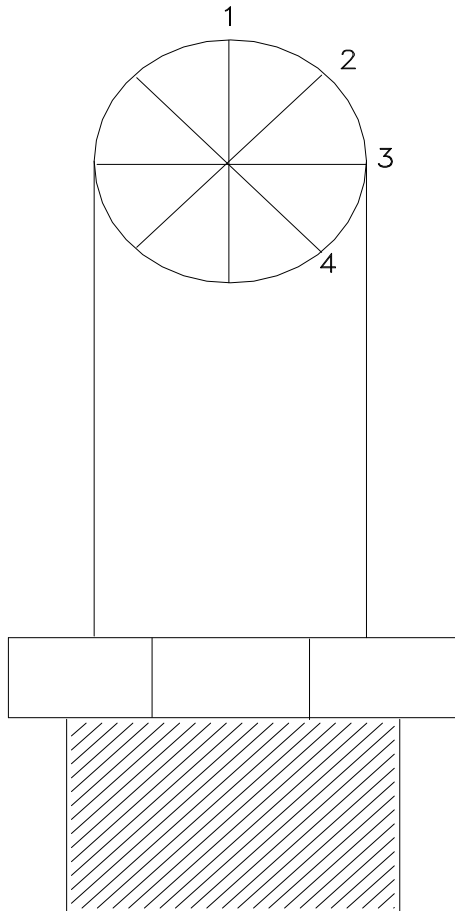
# Nozzle Calibration

Date: 7/14/2023

Nozzle ID No.: 954

Analyst: RB

Material/Type: Glass



|       |   |
|-------|---|
| 0.251 | 1 |
| 0.251 | 2 |
| 0.251 | 3 |
| 0.250 | 4 |

**Valid Data**

|                |
|----------------|
| <b>Average</b> |
| <u>0.251</u>   |

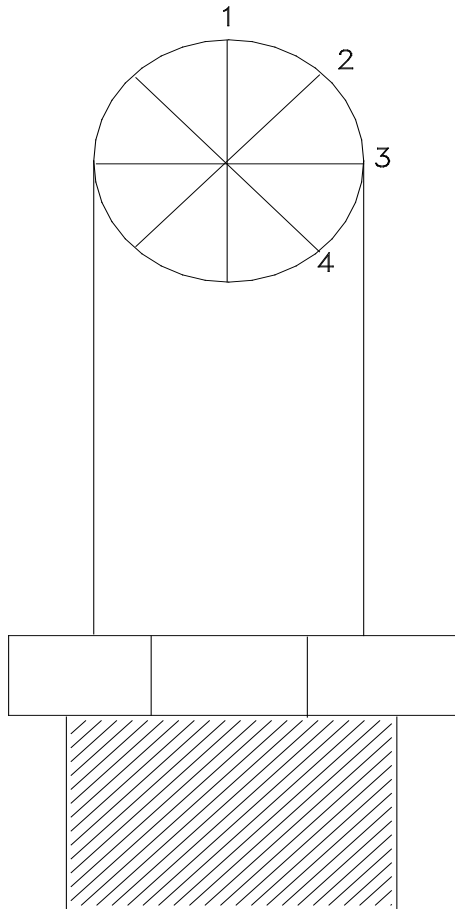
# Nozzle Calibration

Date: 12/4/2020

Nozzle ID No.: 667

Analyst: EWB

Material/Type: Glass



|       |   |
|-------|---|
| 0.247 | 1 |
| 0.247 | 2 |
| 0.248 | 3 |
| 0.246 | 4 |

**Valid Data**

|                |
|----------------|
| <b>Average</b> |
| 0.247          |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Test Location: Main Kiln Stack  
 Date: 11/14/2023  
 Operator: R. Sollars  
 Operating Condition Mill On

Sample System: FTIR  
 Probe Length: 8.0 ft  
 Probe Type: FTIR  
 Sample Plane: Vertical  
 Port Length: 12 in.  
 Port Size (diameter): 4 in.  
 Port Type: Flange  
 Duct Shape: Circular  
 Diameter: 7 ft  
 Duct Area: 38.48 Sq. Ft.  
 Upstream Diameters: 16.00 Minimum Upstream Distance 3.5 Feet  
 Downstream Diameters: 11.00 Minimum Downstream Distance 14.0 Feet  
 Number of Ports Sampled: 1 Ideal Upstream Distance 14.0 Feet  
 Number of Points per Port: 1 Ideal Downstream Distance 56.0 Feet  
 Total Number of Traverse Points: 1

**Calibration Gases**

| Type       | Setting | Cylinder ID   | Cylinder Value | Analyzer Response | Difference, % of Span | Expiration Date | Mid cylinder % of high cylinder | Final Bottle Pressure, PSI |
|------------|---------|---------------|----------------|-------------------|-----------------------|-----------------|---------------------------------|----------------------------|
| O2 % (dry) | Zero    | Zero Nitrogen | 0.0            | -0.07             | 0.32%                 | N/A             |                                 | 1300                       |
|            | Mid     | EB0075029     | 11.18          | 11.15             | 0.14%                 | 9/7/2031        | 50.54%                          | 1600                       |
|            | High    | CC308342      | 22.12          | 21.97             | 0.68%                 | 5/25/2031       |                                 | 1800                       |

| Type                          | Compound | Cylinder ID   | Cylinder Value | Expiration Date | Final Bottle Pressure, PSI |
|-------------------------------|----------|---------------|----------------|-----------------|----------------------------|
| Zero Gas                      | Nitrogen | Zero Nitrogen | 0.0            | N/A             | 1300                       |
| Calibration Transfer Standard | Ethylene | AAL072815     | 101.4          | 9/5/2031        | 1700                       |
| Analyte Spike Gas             | HCN      | CC768241      | 49.55          | 3/11/2024       | 1800                       |
|                               | SF6      |               | 5.001          |                 |                            |

**Response Time Data**

| Type       | RM Analyzer Make/Model | RM Analyzer s/in | Analyzer Span | RM Gas Span |
|------------|------------------------|------------------|---------------|-------------|
| O2 % (dry) | CAI 700                | 221018           | 25            | 22.12       |
| HF ppmvw   | MKS 2030               | 110161896        | 10            | N/A         |
| HCN ppmvw  | MKS 2030               | 110161896        | 200           | N/A         |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Diluent: O2 %

Test Location: Main Kiln Stack  
 Date: 11/14/23  
 Operator: R. Sollars  
 O2 % Correction: 7

O2 % (dry) Correction Data

| Run # | Cma   | Precal | Postcal | Pre zero | Post zero | Co   | Cm    | C     | Cgas | Span Bias | Span Drift | Zero Bias | Zero Drift |
|-------|-------|--------|---------|----------|-----------|------|-------|-------|------|-----------|------------|-----------|------------|
| 1     | 11.18 | 11.13  | 11.11   | 0.01     | 0.00      | 0.01 | 11.12 | 12.59 | 12.7 | 0.18      | -0.09      | -0.32     | -0.05      |
| 2     | 11.18 | 11.11  | 11.11   | 0.00     | 0.00      | 0.00 | 11.11 | 12.39 | 12.5 | 0.18      | 0.00       | -0.32     | 0.00       |
| 3     | 11.18 | 11.11  | 11.10   | 0.00     | 0.01      | 0.01 | 11.11 | 12.39 | 12.5 | 0.23      | -0.05      | -0.36     | 0.05       |

Concentration of Cal Gas C = Average value of test Co=Average Pre and Post Zero  
 erage Pre and Post Span Cgas = Corrected gas value of test

Calibration Corrected and Calculated Data

| Run # | Run Date | Start Time | End Time | Moisture % | O2 % (dry) | CO2 % (wet) | CO2 % (dry) | HCN ppmvw | HCN ppmvd @ 7% O2 | HF ppmvw | HF ppmvd @ 7% O2 |
|-------|----------|------------|----------|------------|------------|-------------|-------------|-----------|-------------------|----------|------------------|
| 1     | 11/14/23 | 8:00       | 8:59     | 11.66%     | 12.66      | 11.86       | 13.43       | 0.76      | 1.45              | 0.10     | 0.19             |
| 2     | 11/14/23 | 9:25       | 10:24    | 11.55%     | 12.47      | 12.16       | 13.75       | 0.78      | 1.46              | 0.10     | 0.19             |
| 3     | 11/14/23 | 10:50      | 11:49    | 11.47%     | 12.48      | 12.23       | 13.81       | 0.80      | 1.49              | 0.10     | 0.19             |

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Main Kiln Stack  
**Date:** 11/14/23  
**Project #:** M234605

**Linearity Cal/Pre 1 Cal**

| <u>Time</u> | <u>O2 % (dry)</u> |    |
|-------------|-------------------|----|
| 6:52        | 0.01              |    |
| 6:53        | -0.07             | iz |
| 6:54        | -0.07             |    |
| 6:55        | 2.72              |    |
| 6:56        | 6.14              |    |
| 6:57        | 5.68              |    |
| 6:58        | 9.83              |    |
| 6:59        | 4.55              |    |
| 7:00        | 5.53              |    |
| 7:01        | 20.83             |    |
| 7:02        | 21.96             |    |
| 7:03        | 21.97             | ih |
| 7:04        | 16.70             |    |
| 7:05        | 11.11             |    |
| 7:06        | 11.10             |    |
| 7:07        | 11.15             | im |
| 7:08        | 18.80             |    |
| 7:09        | 15.94             |    |
| 7:10        | 0.05              |    |
| 7:11        | 6.15              |    |
| 7:12        | 20.73             |    |
| 7:13        | 20.77             |    |
| 7:14        | 20.78             |    |
| 7:15        | 20.78             |    |
| 7:16        | 15.71             |    |
| 7:17        | 12.01             |    |
| 7:18        | 12.42             |    |
| 7:19        | 12.47             |    |
| 7:20        | 12.41             |    |
| 7:21        | 12.27             |    |
| 7:22        | 10.82             |    |
| 7:23        | 11.05             |    |
| 7:24        | 11.19             |    |
| 7:25        | 11.36             |    |
| 7:26        | 10.71             |    |
| 7:27        | 8.81              |    |
| 7:28        | 0.04              |    |
| 7:29        | 0.01              | z  |
| 7:30        | 3.44              |    |
| 7:31        | 10.83             |    |
| 7:32        | 11.12             |    |
| 7:33        | 11.13             |    |
| 7:34        | 11.13             | m  |

**Client:** CalPortland Company, Inc.

**Facility:** Redding Cement Plant

**Project #:** M234605

**Test Location:** Main Kiln Stack

**Date:** 11/14/23

| <b>Post 1/Pre 2</b> |                   |   | <b>Post 2/Pre 3</b> |                   |   |
|---------------------|-------------------|---|---------------------|-------------------|---|
| <u>Time</u>         | <u>O2 % (dry)</u> |   | <u>Time</u>         | <u>O2 % (dry)</u> |   |
| 9:10                | 10.26             |   | 10:37               | 8.31              |   |
| 9:11                | 1.94              |   | 10:38               | 11.10             |   |
| 9:12                | 0.01              |   | 10:39               | 11.11             | m |
| 9:13                | 0.00              | z | 10:40               | 10.55             |   |
| 9:14                | 10.12             |   | 10:41               | 0.05              |   |
| 9:15                | 11.10             |   | 10:42               | 0.00              | z |
| 9:16                | 11.11             | m | 10:43               | 2.15              |   |
| 9:17                | 6.67              |   | 10:44               | 12.24             |   |
|                     |                   |   | 10:45               | 12.25             |   |

| <b>Post 3</b> |                   |   |
|---------------|-------------------|---|
| <u>Time</u>   | <u>O2 % (dry)</u> |   |
| 11:58         | 11.43             |   |
| 11:59         | 11.21             |   |
| 12:00         | 5.59              |   |
| 12:01         | 0.04              |   |
| 12:02         | 0.01              | z |
| 12:03         | 6.00              |   |
| 12:04         | 11.08             |   |
| 12:05         | 11.10             | m |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Test Location: Main Kiln Stack  
 Date: 11/14/2023  
 Operator: R. Sollars  
 Operating Condition Mill Off

Sample System: FTIR  
 Probe Length: 8.0 ft  
 Probe Type: FTIR  
 Sample Plane: Vertical  
 Port Length: 12 in.  
 Port Size (diameter): 4 in.  
 Port Type: Flange  
 Duct Shape: Circular  
 Diameter: 7 ft  
 Duct Area: 38.48 Sq. Ft.  
 Upstream Diameters: 16.00 Minimum Upstream Distance 3.5 Feet  
 Downstream Diameters: 11.00 Minimum Downstream Distance 14.0 Feet  
 Number of Ports Sampled: 1 Ideal Upstream Distance 14.0 Feet  
 Number of Points per Port: 1 Ideal Downstream Distance 56.0 Feet  
 Total Number of Traverse Points: 1

**Calibration Gases**

| Type       | Setting | Cylinder ID   | Cylinder Value | Analyzer Response | Difference, % of Span | Expiration Date | Mid cylinder % of high cylinder | Final Bottle Pressure, PSI |
|------------|---------|---------------|----------------|-------------------|-----------------------|-----------------|---------------------------------|----------------------------|
| O2 % (dry) | Zero    | Zero Nitrogen | 0.0            | -0.07             | 0.32%                 | N/A             |                                 | 1300                       |
|            | Mid     | EB0075029     | 11.18          | 11.15             | 0.14%                 | 9/7/2031        | 50.54%                          | 1600                       |
|            | High    | CC308342      | 22.12          | 21.97             | 0.68%                 | 5/25/2031       |                                 | 1800                       |

| Type                          | Compound | Cylinder ID   | Cylinder Value | Expiration Date | Final Bottle Pressure, PSI |
|-------------------------------|----------|---------------|----------------|-----------------|----------------------------|
| Zero Gas                      | Nitrogen | Zero Nitrogen | 0.0            | N/A             | 1300                       |
| Calibration Transfer Standard | Ethylene | AAL072815     | 101.4          | 9/5/2031        | 1700                       |
| Analyte Spike Gas             | HCN      | CC768241      | 49.55          | 3/11/2024       | 1800                       |
|                               | SF6      |               | 5.001          |                 |                            |

**Response Time Data**

| Type       | RM Analyzer Make/Model | RM Analyzer s/n | Analyzer Span | RM Gas Span |
|------------|------------------------|-----------------|---------------|-------------|
| O2 % (dry) | CAL 700                | 221018          | 25            | 22.12       |
| HF ppmvw   | MKS 2030               | 110161896       | 10            | N/A         |
| HCN ppmvw  | MKS 2030               | 110161896       | 200           | N/A         |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Diluent: O2 %

Test Location: Main Kiln Stack  
 Date: 11/14/23  
 Operator: R. Sollars  
 O2 % Correction: 7

O2 % (dry) Correction Data

| Run # | Cma   | Precal | Postcal | Pre zero | Post zero | Co   | Cm    | C     | Cgas | Span Bias | Span Drift | Zero Bias | Zero Drift |
|-------|-------|--------|---------|----------|-----------|------|-------|-------|------|-----------|------------|-----------|------------|
| 1     | 11.18 | 11.10  | 11.10   | 0.01     | -0.01     | 0.00 | 11.10 | 11.07 | 11.2 | 0.23      | 0.00       | -0.27     | -0.09      |
| 2     | 11.18 | 11.10  | 11.10   | -0.01    | 0.01      | 0.00 | 11.10 | 11.11 | 11.2 | 0.23      | 0.00       | -0.36     | 0.09       |
| 3     | 11.18 | 11.10  | 11.10   | 0.01     | 0.01      | 0.01 | 11.10 | 11.25 | 11.3 | 0.23      | 0.00       | -0.36     | 0.00       |

Concentration of Cal Gas C = Average value of test Co=Average Pre and Post Zero  
 erage Pre and Post Span Cgas = Corrected gas value of test

Calibration Corrected and Calculated Data

| Run # | Run Date | Start Time | End Time | Moisture % | O2 % (dry) | CO2 % (wet) | CO2 % (dry) | HCN ppmvw | HCN ppmvd @ 7% O2 | HF ppmvw | HF ppmvd @ 7% O2 |
|-------|----------|------------|----------|------------|------------|-------------|-------------|-----------|-------------------|----------|------------------|
| 1     | 11/14/23 | 12:50      | 13:49    | 12.20%     | 11.15      | 14.19       | 16.16       | 0.83      | 1.34              | 0.10     | 0.16             |
| 2     | 11/14/23 | 14:15      | 15:14    | 12.42%     | 11.19      | 14.21       | 16.22       | 0.89      | 1.45              | 0.10     | 0.16             |
| 3     | 11/14/23 | 15:40      | 16:39    | 11.98%     | 11.33      | 14.15       | 16.08       | 1.01      | 1.67              | 0.10     | 0.17             |

**Client:** CalPortland Company, Inc.  
**Facility:** Redding Cement Plant  
**Test Location:** Main Kiln Stack  
**Date:** 11/14/23  
**Project #:** M234605

**Linearity Cal/Pre 1 Cal**

| <u>Time</u> | <u>O2 % (dry)</u> |    |
|-------------|-------------------|----|
| 6:52        | 0.01              |    |
| 6:53        | -0.07             | iz |
| 6:54        | -0.07             |    |
| 6:55        | 2.72              |    |
| 6:56        | 6.14              |    |
| 6:57        | 5.68              |    |
| 6:58        | 9.83              |    |
| 6:59        | 4.55              |    |
| 7:00        | 5.53              |    |
| 7:01        | 20.83             |    |
| 7:02        | 21.96             |    |
| 7:03        | 21.97             | ih |
| 7:04        | 16.70             |    |
| 7:05        | 11.11             |    |
| 7:06        | 11.10             |    |
| 7:07        | 11.15             | im |
| 7:08        | 18.80             |    |
| 7:09        | 15.94             |    |
| 7:10        | 0.05              |    |
| 7:11        | 6.15              |    |
| 7:12        | 20.73             |    |
| 7:13        | 20.77             |    |
| 7:14        | 20.78             |    |
| 7:15        | 20.78             |    |
| 7:16        | 15.71             |    |
| 7:17        | 12.01             |    |
| 7:18        | 12.42             |    |
| 7:19        | 12.47             |    |
| 7:20        | 12.41             |    |
| 7:21        | 12.27             |    |
| 7:22        | 10.82             |    |
| 7:23        | 11.05             |    |
| 7:24        | 11.19             |    |
| 7:25        | 11.36             |    |
| 7:26        | 10.71             |    |
| 7:27        | 8.81              |    |
| 7:28        | 0.04              |    |
| 7:29        | 0.01              |    |
| 7:30        | 3.44              |    |
| 7:31        | 10.83             |    |
| 7:32        | 11.12             |    |
| 7:33        | 11.13             |    |
| 7:34        | 11.13             |    |
| 11:58       | 11.43             |    |
| 11:59       | 11.21             |    |
| 12:00       | 5.59              |    |

**Client:** CalPortland Company, Inc.

**Facility:** Redding Cement Plant

**Project #:** M234605

**Test Location:** Main Kiln Stack

**Date:** 11/14/23

| <b>Post 1/Pre 2</b> |                   |   | <b>Post 2/Pre 3</b> |                   |   |
|---------------------|-------------------|---|---------------------|-------------------|---|
| <u>Time</u>         | <u>O2 % (dry)</u> |   | <u>Time</u>         | <u>O2 % (dry)</u> |   |
| 14:02               | 4.72              |   | 15:25               | 10.33             |   |
| 14:03               | 11.08             |   | 15:26               | 6.63              |   |
| 14:04               | 11.10             | m | 15:27               | 0.03              |   |
| 14:05               | 10.65             |   | 15:28               | 0.01              | z |
| 14:06               | 0.11              |   | 15:29               | 7.45              |   |
| 14:07               | 0.00              |   | 15:30               | 11.07             |   |
| 14:08               | -0.01             | z | 15:31               | 11.10             | m |

| <b>Post 3</b> |                   |   |
|---------------|-------------------|---|
| <u>Time</u>   | <u>O2 % (dry)</u> |   |
| 16:47         | 10.54             |   |
| 16:48         | 9.19              |   |
| 16:49         | 2.11              |   |
| 16:50         | 0.02              |   |
| 16:51         | 0.01              | z |
| 16:52         | 8.45              |   |
| 16:53         | 11.09             |   |
| 16:54         | 11.10             | m |

**Appendix H - FTIR QA/QC**

## Method 320 FTIR Detector Multi-Gas Determination QA/QC

FTIR data was collected using an MKS MultiGas 2030 FTIR spectrometer.

The FTIR was equipped with a temperature-controlled, 5.11 meter multi-pass gas cell maintained at 191°C. Gas flows and sampling system pressures were monitored using a rotameter and pressure transducer. All data was collected at 0.5 cm<sup>-1</sup> resolution. Each spectrum was derived from the coaddition of 64 scans, with a new data point generated approximately every one minute. Analyzer data for each run is presented in the Reference Method Test Data appendix.

| SAMPLING SYSTEM PARAMETERS |                               |                          |                                       |                        |
|----------------------------|-------------------------------|--------------------------|---------------------------------------|------------------------|
| MKS Serial #               | Sampling Line                 | Probe Assembly           | Particulate Filter Media              | Operating Temperatures |
| 110161896                  | 100' 3/8" dia., heated Teflon | Heated 12', 3/8" dia. SS | 0.01µ heated borosilicate glass fiber | 191°C                  |

QA/QC procedures followed US EPA Method 320 guidelines. See below for QA/QC procedure details and list of calibration gas standards. All calibration gases were introduced to the analyzer and the sampling system using an instrument grade stainless steel rotameter. All QA/QC procedures were within the acceptance criteria allowance of the applicable EPA methodology. Detailed FTIR QA/QC data follow the narrative portion of this appendix.

| FTIR QA/QC Procedures                            |   |                         |  |                            |                              |        |
|--|---|-------------------------|--|----------------------------|------------------------------|--------|
| QA/QC Specification                              | Purpose   | Calibration Gas Analyte | Delivery   | Frequency                  | Acceptance Criteria          | Result |
| M320: Zero                                       | Verify that the FTIR is free of contaminants & zero the FTIR  | Nitrogen (zero)         | Direct to FTIR                                     | pre/post test              | < MDL or Noise               | Pass   |
| M320: Calibration Transfer Standard (CTS) Direct | Verify FTIR stability, confirm optical path length  | Ethylene                | Direct to FTIR                                     | pretest                    | +/- 5% cert. value           | Pass   |
| M320: Analyte Direct                             | Verify FTIR calibration   | HCN, SF <sub>6</sub>    | Direct to FTIR                                     | Pretest                    | +/- 5% cert. value           | Pass   |
| M320: CTS Response                               | Verify system stability, recovery, response time  | Ethylene                | Sampling System                                    | Daily, pre/post test       | +/- 5% of Direct Measurement | Pass   |
| M320: Zero Response                              | Verify system is free of contaminants, system bias  | Nitrogen (zero)         | Sampling System                                    | pretest                    | Bias correct data            | Pass   |
| M320: Analyte Spike                              | Verify system ability to deliver and quantify analyte of interest in the presence of other effluent gases | HCN, SF <sub>6</sub>    | Dynamic Addition to Sampling System, 1:10 effluent | Throughout testing – daily | +/- 20% theoretical recovery | Pass   |

Note: The determined concentrations from direct analyses were used in all system/spike recovery calculations.

| CALIBRATION GAS STANDARDS |                     |        |               |                                |
|---------------------------|---------------------|--------|---------------|--------------------------------|
| Components                | Concentration (ppm) | Vendor | Cylinder #    | Standard Type                  |
| Ethylene                  | 101.4               | Airgas | AAL072815     | Primary +/- 1%                 |
| HCN/SF <sub>6</sub>       | 49.55/5.001         | Airgas | CC768241      | Certified Standard-Spec +/- 5% |
| Nitrogen                  | Zero Gas            | Airgas | Zero Nitrogen | UHP Grade                      |

### Analyte Spiking

HCN spiking was performed prior to testing to verify the ability of the sampling system to quantitatively deliver a sample containing HCN from the base of the probe to the FTIR. Analyte spiking assures the ability of the FTIR sampling system to recover acid gases in the presence of effluent gas.

As part of the spiking procedure, samples were measured to determine native HCN concentrations to be used in the spike recovery calculations. The analyte spiking gases contained a low concentration of sulfur hexafluoride (SF<sub>6</sub>). The determined SF<sub>6</sub> concentration in the spiked sample was used to calculate the dilution factor of the spike and thus used to calculate the concentration of the spiked HCN. The spike target dilution ratio was 1:10 or less.

The following equation illustrates the percent recovery calculation.

$$DF = \frac{SF_6(spik)}{SF_6(direct)} \quad (\text{Sec. 9.2.3 (3) USEPA Method 320})$$

$$CS = DF * Spike(dir) + Unspike(1 - DF) \quad (\text{Sec. 9.2.3 (4) USEPA Method 320})$$

DF = Dilution factor of the spike gas

SF<sub>6(dir)</sub> = SF<sub>6</sub> concentration measured directly in undiluted spike gas

SF<sub>6(spik)</sub> = Diluted SF<sub>6</sub> concentration measured in a spiked sample

Spike<sub>dir</sub> = Concentration of the analyte in the spike standard measure by the FTIR directly

CS = Expected concentration of the spiked samples

Unspike = Native concentration of analytes in unspiked samples

### Post Collection Data Validation

As part of the data validation procedure, reference spectra are manually fit to that of the sample spectra and a concentration is determined. The reference spectra are scaled to match the peak amplitude of the sample, thus providing a scale factor. The scale factor multiplied by the reference spectra concentration is used to determine the concentration value for the sample spectra. Sample pressure and temperature corrections are then applied to compute the final sample concentration. The manually calculated results are then compared with the software-generated results. The data is then validated if the two concentrations are within ± 20% agreement. If there is a difference greater than ± 20% the spectra are reviewed for possible spectra interferences or any other possible causes leading to incorrectly quantified data.

### **Detection Limit**

The detection limit of each analyte was calculated following Annex A2 of ASTM D6348-12 procedure using spectra that contained similar amounts of moisture.

| <b>FTIR DETECTION LIMITS</b> |                                   |                             |                                 |
|------------------------------|-----------------------------------|-----------------------------|---------------------------------|
| <b>Analyte</b>               | <b>Detection Limit (ppmv wet)</b> | <b>Detection Limit (%v)</b> | <b>Detection Limit (%v wet)</b> |
| <b>Hydrogen Cyanide</b>      | 0.2                               | —                           | —                               |
| <b>Hydrogen Fluoride</b>     | 0.1                               |                             |                                 |
| <b>Water</b>                 | —                                 | <b>0.1</b>                  | <b>N/A</b>                      |
| <b>Carbon Dioxide</b>        | —                                 | <b>N/A</b>                  | <b>0.1</b>                      |

Copies of gas cylinder certifications are appended. All concentration data were recorded on a wet, volume basis. HCN spiking was performed prior to testing to confirm the measurement system's ability to deliver and quantify HCN. The sample and data collection followed the procedures outlined in Methods 320.

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Operating Condition: Mill On

Test Location: Main Kiln Stack  
 Date: 11/14/2023  
 Operator: R. Sollars  
 FTIR s/n: 110161896

System Leak Check: 0.0 mL/min

**Nitrogen (Zero) Direct to FTIR**

| Spectrum             | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|----------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| N2_DIR_000006.LAB    | 11/14/23 | 6:52:09 | 0.0        | 0.0           | 0.0            | 191.0                              | 0.97                          | 0.0                  | -0.1            | -0.008          |
| N2_DIR_0000078KG.LAB | 11/14/23 | 6:54:23 | 0.0        | 0.0           | 0.0            | 190.6                              | 0.97                          | 0.0                  | 0.0             | 0.000           |
| N2_DIR_000008.LAB    | 11/14/23 | 6:54:37 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | 0.0                  | -0.1            | 0.002           |
| N2_DIR_000009.LAB    | 11/14/23 | 6:54:45 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | -0.1                 | -0.1            | 0.001           |
| N2_DIR_000010.LAB    | 11/14/23 | 6:54:53 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | -0.1                 | 0.0             | -0.001          |
| N2_DIR_000011.LAB    | 11/14/23 | 6:55:01 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | -0.2                 | 0.0             | 0.003           |
| N2_DIR_000012.LAB    | 11/14/23 | 6:55:09 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | -0.2                 | -0.1            | 0.002           |
| N2_DIR_000013.LAB    | 11/14/23 | 6:55:17 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | -0.2                 | 0.0             | 0.001           |
| N2_DIR_000014.LAB    | 11/14/23 | 6:55:24 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | 0.0                  | 0.1             | -0.003          |

**Calibration Transfer Standard (CTS), Direct to FTIR**

| Spectrum           | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|--------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| CTS_DIR_000020.LAB | 11/14/23 | 6:56:53 | 0.0        | 0.0           | 0.0            | 190.1                              | 0.97                          | 101.2                | 0.1             | -0.022          | 99.8%                  |
| CTS_DIR_000021.LAB | 11/14/23 | 6:57:01 | 0.0        | 0.0           | 0.0            | 190.1                              | 0.97                          | 101.2                | -0.1            | -0.021          | 99.8%                  |
| CTS_DIR_000022.LAB | 11/14/23 | 6:57:08 | 0.0        | 0.0           | 0.0            | 190.1                              | 0.97                          | 101.5                | 0.0             | -0.020          | 100.1%                 |
| CTS_DIR_000023.LAB | 11/14/23 | 6:57:16 | 0.0        | 0.0           | 0.0            | 190.0                              | 0.97                          | 101.3                | 0.0             | -0.028          | 99.9%                  |
| CTS_DIR_000024.LAB | 11/14/23 | 6:57:24 | 0.0        | 0.0           | 0.0            | 190.0                              | 0.97                          | 101.4                | 0.0             | -0.023          | 100.0%                 |
| CTS_DIR_000025.LAB | 11/14/23 | 6:57:32 | 0.0        | 0.0           | 0.0            | 190.0                              | 0.97                          | 101.2                | 0.0             | -0.023          | 99.8%                  |
| CTS_DIR_000026.LAB | 11/14/23 | 6:57:40 | 0.0        | 0.0           | 0.0            | 189.9                              | 0.97                          | 101.3                | 0.2             | -0.020          | 99.9%                  |
| Average            |          |         |            |               |                |                                    |                               |                      |                 |                 |                        |
|                    |          |         |            |               |                |                                    |                               | 101.3                |                 |                 | 99.9%                  |

**Analyte Spike Gas (HCN) Direct to FTIR**

| Spectrum               | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>HCN |
|------------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|-------------------|
| 49.6HCN_DIR_000029.LAB | 11/14/23 | 6:59:08 | 0.0        | 0.0           | 0.0            | 190.1                              | 0.97                          | -0.2                 | 50.3            | 4.957           | 101.4%            |
| 49.6HCN_DIR_000030.LAB | 11/14/23 | 6:59:16 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 0.1                  | 50.4            | 4.968           | 101.8%            |
| 49.6HCN_DIR_000031.LAB | 11/14/23 | 6:59:24 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | -0.1                 | 50.1            | 4.941           | 101.1%            |
| 49.6HCN_DIR_000032.LAB | 11/14/23 | 6:59:32 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | 0.0                  | 50.5            | 4.961           | 101.8%            |
| 49.6HCN_DIR_000033.LAB | 11/14/23 | 6:59:40 | 0.0        | 0.0           | 0.0            | 190.5                              | 0.97                          | -0.4                 | 50.3            | 4.959           | 101.5%            |
| 49.6HCN_DIR_000034.LAB | 11/14/23 | 6:59:48 | 0.0        | 0.0           | 0.0            | 190.6                              | 0.97                          | -0.1                 | 50.4            | 4.949           | 101.8%            |
| 49.6HCN_DIR_000035.LAB | 11/14/23 | 6:59:55 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | -0.2                 | 50.3            | 4.951           | 101.5%            |
| 49.6HCN_DIR_000036.LAB | 11/14/23 | 7:00:03 | 0.0        | 0.0           | 0.0            | 190.8                              | 0.97                          | -0.2                 | 50.4            | 4.957           | 101.7%            |
| Average                |          |         |            |               |                |                                    |                               |                      |                 |                 |                   |
|                        |          |         |            |               |                |                                    |                               | 50.3                 | 4.955           | 101.6%          |                   |

**CTS, System Purge**

| Spectrum          | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|-------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| CTS_RT_000044.LAB | 11/14/23 | 7:09:52 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | 100.9                | -0.1            | -0.028          | 99.5%                  |
| CTS_RT_000045.LAB | 11/14/23 | 7:10:00 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.1                | 0.0             | -0.024          | 99.7%                  |
| CTS_RT_000046.LAB | 11/14/23 | 7:10:08 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | 101.2                | 0.0             | -0.027          | 99.9%                  |
| CTS_RT_000047.LAB | 11/14/23 | 7:10:16 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.3                | -0.1            | -0.026          | 100.0%                 |
| CTS_RT_000048.LAB | 11/14/23 | 7:10:24 | 0.0        | 0.0           | 0.1            | 190.2                              | 0.97                          | 101.2                | -0.3            | -0.018          | 99.9%                  |
| CTS_RT_000049.LAB | 11/14/23 | 7:10:32 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.4                | 0.0             | -0.021          | 100.1%                 |
| CTS_RT_000050.LAB | 11/14/23 | 7:10:39 | 0.0        | 0.0           | 0.1            | 190.1                              | 0.97                          | 101.3                | -0.1            | -0.020          | 100.0%                 |
| CTS_RT_000051.LAB | 11/14/23 | 7:10:47 | 0.0        | 0.0           | 0.0            | 190.1                              | 0.97                          | 101.3                | -0.1            | -0.027          | 100.0%                 |

**Response Time Test**

| Spectrum          | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Response Time (sec) |
|-------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|---------------------|
| CTS_RT_000041.LAB | 11/14/23 | 7:09:29 | 0.9        | 0.0           | 0.0            | 190.4                              | 0.97                          | 0.0                  | -0.2            | -0.003          | -                   |
| CTS_RT_000042.LAB | 11/14/23 | 7:09:37 | 0.7        | 0.6           | 0.0            | 190.4                              | 0.97                          | 25.6                 | 0.0             | -0.024          | 15.89               |
| CTS_RT_000043.LAB | 11/14/23 | 7:09:44 | 0.1        | 0.0           | 0.0            | 190.3                              | 0.97                          | 99.9                 | 0.0             | -0.025          | 23.89               |
| CTS_RT_000044.LAB | 11/14/23 | 7:09:52 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | 100.9                | -0.1            | -0.028          |                     |
| CTS_RT_000045.LAB | 11/14/23 | 7:10:00 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.1                | 0.0             | -0.024          |                     |
| CTS_RT_000046.LAB | 11/14/23 | 7:10:08 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | 101.2                | 0.0             | -0.027          |                     |
| CTS_RT_000047.LAB | 11/14/23 | 7:10:16 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.3                | -0.1            | -0.026          |                     |
| CTS_RT_000048.LAB | 11/14/23 | 7:10:24 | 0.0        | 0.0           | 0.1            | 190.2                              | 0.97                          | 101.2                | -0.3            | -0.018          |                     |
| CTS_RT_000049.LAB | 11/14/23 | 7:10:32 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.4                | 0.0             | -0.021          |                     |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Operating Condition: Mill On

Test Location: Main Kiln Stack  
 Date: 11/14/2023  
 Operator: R. Sollars  
 FTIR s/n: 110161896

Pre 1 Native Effluent Prior to Analyte Spike

| Spectrum                 | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|--------------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| AMBIENT_STACK_000124.LAB | 11/14/23 | 7:21:16 | 11.1       | 12.2          | -0.2           | 190.8                              | 0.97                          | 0.7                  | 0.7             | -0.007          |
| AMBIENT_STACK_000125.LAB | 11/14/23 | 7:21:24 | 11.1       | 12.3          | -0.2           | 190.7                              | 0.97                          | 0.7                  | 0.9             | 0.001           |
| AMBIENT_STACK_000126.LAB | 11/14/23 | 7:21:31 | 11.1       | 12.4          | -0.2           | 190.7                              | 0.97                          | 0.8                  | 1.0             | -0.007          |
|                          |          |         |            |               |                |                                    |                               |                      | 0.9             | -0.004          |

Pre 1 Effluent Spike Using Analyte

| Spectrum            | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Dilution<br>Factor | Recovery %<br>HCN |
|---------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| PRE1_SPK_000145.LAB | 11/14/23 | 7:25:12 | 10.7       | 11.9          | -0.2           | 190.1                              | 0.97                          | 0.7                  | 3.9             | 0.317           | 0.064              | 95.6%             |
| PRE1_SPK_000146.LAB | 11/14/23 | 7:25:20 | 10.7       | 11.8          | -0.2           | 190.0                              | 0.97                          | 0.8                  | 3.9             | 0.316           | 0.064              | 97.8%             |
| PRE1_SPK_000147.LAB | 11/14/23 | 7:25:28 | 10.8       | 11.8          | -0.2           | 190.0                              | 0.97                          | 0.7                  | 3.7             | 0.312           | 0.063              | 92.8%             |
| PRE1_SPK_000148.LAB | 11/14/23 | 7:25:35 | 10.7       | 11.8          | -0.2           | 189.9                              | 0.97                          | 0.6                  | 3.7             | 0.324           | 0.065              | 89.9%             |
| PRE1_SPK_000149.LAB | 11/14/23 | 7:25:43 | 11.0       | 11.8          | -0.2           | 189.9                              | 0.97                          | 0.6                  | 3.6             | 0.313           | 0.063              | 90.7%             |
| PRE1_SPK_000150.LAB | 11/14/23 | 7:25:51 | 11.1       | 11.8          | -0.2           | 189.9                              | 0.97                          | 0.8                  | 3.7             | 0.316           | 0.064              | 91.3%             |
| PRE1_SPK_000151.LAB | 11/14/23 | 7:25:59 | 11.0       | 11.7          | -0.2           | 189.9                              | 0.97                          | 0.7                  | 3.7             | 0.303           | 0.061              | 95.2%             |
| PRE1_SPK_000152.LAB | 11/14/23 | 7:26:07 | 11.1       | 11.7          | -0.2           | 190.0                              | 0.97                          | 0.6                  | 3.7             | 0.309           | 0.062              | 94.6%             |

Native Effluent Prior to Analyte Spike

| Spectrum        | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|-----------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| RUN1_000261.LAB | 11/14/23 | 9:03:30 | 11.5       | 11.8          | -0.2           | 191.3                              | 0.98                          | 0.7                  | 0.8             | -0.001          |
| RUN1_000262.LAB | 11/14/23 | 9:04:33 | 11.8       | 11.8          | -0.2           | 191.2                              | 0.98                          | 0.7                  | 0.8             | -0.002          |
| RUN1_000263.LAB | 11/14/23 | 9:05:36 | 12.1       | 11.9          | -0.2           | 191.1                              | 0.98                          | 0.8                  | 0.8             | -0.003          |
|                 |          |         |            |               |                |                                    |                               |                      | 0.8             | -0.002          |

Effluent Spike Using Analyte

| Spectrum             | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Dilution<br>Factor | Recovery %<br>HCN |
|----------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST1_SPK_000282.LAB | 11/14/23 | 9:09:16 | 10.6       | 11.6          | -0.2           | 190.6                              | 0.98                          | 0.5                  | 4.8             | 0.421           | 0.085              | 95.6%             |
| POST1_SPK_000283.LAB | 11/14/23 | 9:09:24 | 10.7       | 11.6          | -0.2           | 190.6                              | 0.98                          | 0.8                  | 4.8             | 0.417           | 0.084              | 95.9%             |
| POST1_SPK_000284.LAB | 11/14/23 | 9:09:32 | 10.6       | 11.7          | -0.2           | 190.5                              | 0.98                          | 0.5                  | 4.8             | 0.415           | 0.084              | 96.9%             |
| POST1_SPK_000285.LAB | 11/14/23 | 9:09:39 | 10.7       | 11.8          | -0.2           | 190.5                              | 0.98                          | 0.7                  | 4.9             | 0.418           | 0.084              | 98.6%             |
| POST1_SPK_000286.LAB | 11/14/23 | 9:09:47 | 10.7       | 11.8          | -0.2           | 190.5                              | 0.98                          | 0.7                  | 4.7             | 0.415           | 0.084              | 95.0%             |
| POST1_SPK_000287.LAB | 11/14/23 | 9:09:55 | 10.6       | 11.6          | -0.2           | 190.5                              | 0.98                          | 0.7                  | 5.0             | 0.411           | 0.083              | 100.6%            |
| POST1_SPK_000288.LAB | 11/14/23 | 9:10:03 | 10.6       | 11.4          | -0.2           | 190.5                              | 0.98                          | 0.6                  | 4.7             | 0.419           | 0.085              | 93.4%             |
| POST1_SPK_000289.LAB | 11/14/23 | 9:10:11 | 10.6       | 11.3          | -0.2           | 190.5                              | 0.98                          | 0.8                  | 4.7             | 0.418           | 0.084              | 95.0%             |

CTS, System Purge

| Spectrum             | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|----------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST1_CTS_000299.LAB | 11/14/23 | 9:12:20 | 0.4        | 0.0           | 0.0            | 190.3                              | 0.98                          | 100.1                | 0.1             | -0.024          | 98.9%                  |
| POST1_CTS_000300.LAB | 11/14/23 | 9:12:28 | 0.3        | 0.0           | 0.0            | 190.3                              | 0.98                          | 100.5                | 0.0             | -0.028          | 99.2%                  |
| POST1_CTS_000301.LAB | 11/14/23 | 9:12:36 | 0.3        | 0.0           | 0.0            | 190.2                              | 0.98                          | 100.6                | 0.1             | -0.024          | 99.3%                  |
| POST1_CTS_000302.LAB | 11/14/23 | 9:12:44 | 0.3        | 0.0           | 0.0            | 190.2                              | 0.98                          | 100.7                | 0.3             | -0.019          | 99.4%                  |
| POST1_CTS_000303.LAB | 11/14/23 | 9:12:51 | 0.2        | 0.0           | 0.0            | 190.2                              | 0.98                          | 100.8                | 0.1             | -0.023          | 99.5%                  |
| POST1_CTS_000304.LAB | 11/14/23 | 9:12:59 | 0.2        | 0.0           | 0.0            | 190.1                              | 0.98                          | 100.7                | 0.0             | -0.030          | 99.4%                  |
| POST1_CTS_000305.LAB | 11/14/23 | 9:13:07 | 0.2        | 0.0           | 0.0            | 190.1                              | 0.98                          | 100.6                | -0.1            | -0.024          | 99.3%                  |
| POST1_CTS_000306.LAB | 11/14/23 | 9:13:15 | 0.2        | 0.0           | 0.0            | 190.1                              | 0.98                          | 100.3                | -0.1            | -0.026          | 99.0%                  |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Operating Condition: Mill On

Test Location: Main Kiln Stack  
 Date: 11/14/2023  
 Operator: R. Sollars  
 FTIR s/n: 110161896

Native Effluent Prior to Analyte Spike

| Spectrum        | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|-----------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| RUN2_000393.LAB | 11/14/23 | 10:27:42 | 11.8       | 12.3          | -0.2           | 190.7                              | 0.98                          | 0.8                  | 0.8             | 0.001           |
| RUN2_000394.LAB | 11/14/23 | 10:28:45 | 12.0       | 12.1          | -0.3           | 190.7                              | 0.98                          | 0.9                  | 0.7             | 0.000           |
| RUN2_000395.LAB | 11/14/23 | 10:29:48 | 11.5       | 12.0          | -0.2           | 190.6                              | 0.98                          | 0.8                  | 0.8             | -0.003          |
|                 |          |          |            |               |                |                                    |                               |                      | <b>0.8</b>      | <b>-0.001</b>   |

Effluent Spike Using Analyte

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Dilution<br>Factor | Recovery %<br>HCN |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST1_SPK_000405.LAB | 11/14/23 | 10:32:58 | 10.4       | 11.2          | -0.2           | 190.5                              | 0.98                          | 0.8                  | 4.5             | 0.393           | 0.079              | 95.8%             |
| POST1_SPK_000406.LAB | 11/14/23 | 10:33:06 | 10.7       | 11.1          | -0.3           | 190.5                              | 0.98                          | 0.7                  | 4.5             | 0.394           | 0.079              | 96.3%             |
| POST1_SPK_000407.LAB | 11/14/23 | 10:33:14 | 10.6       | 11.1          | -0.2           | 190.5                              | 0.98                          | 0.7                  | 4.6             | 0.395           | 0.080              | 96.5%             |
| POST1_SPK_000408.LAB | 11/14/23 | 10:33:22 | 10.5       | 11.1          | -0.2           | 190.5                              | 0.98                          | 0.6                  | 4.3             | 0.396           | 0.080              | 91.6%             |
| POST1_SPK_000409.LAB | 11/14/23 | 10:33:30 | 10.4       | 11.1          | -0.2           | 190.4                              | 0.98                          | 0.7                  | 4.5             | 0.386           | 0.078              | 98.2%             |
| POST1_SPK_000410.LAB | 11/14/23 | 10:33:38 | 10.4       | 11.2          | -0.2           | 190.3                              | 0.98                          | 0.5                  | 4.6             | 0.393           | 0.079              | 97.1%             |
| POST1_SPK_000411.LAB | 11/14/23 | 10:33:45 | 10.4       | 11.2          | -0.2           | 190.3                              | 0.98                          | 0.6                  | 4.4             | 0.397           | 0.080              | 92.4%             |
| POST1_SPK_000412.LAB | 11/14/23 | 10:33:54 | 10.4       | 11.4          | -0.2           | 190.3                              | 0.98                          | 0.7                  | 4.7             | 0.393           | 0.079              | 99.0%             |

CTS, System Purge

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST1_CTS_000420.LAB | 11/14/23 | 10:35:45 | 0.7        | 0.0           | 0.0            | 189.9                              | 0.98                          | 100.0                | 0.1             | -0.018          | 98.8%                  |
| POST1_CTS_000421.LAB | 11/14/23 | 10:35:53 | 0.6        | 0.0           | 0.0            | 189.9                              | 0.98                          | 100.1                | 0.2             | -0.016          | 98.8%                  |
| POST1_CTS_000422.LAB | 11/14/23 | 10:36:01 | 0.6        | 0.0           | 0.0            | 189.9                              | 0.98                          | 100.2                | 0.1             | -0.023          | 99.0%                  |
| POST1_CTS_000423.LAB | 11/14/23 | 10:36:09 | 0.5        | 0.0           | 0.0            | 190.0                              | 0.98                          | 100.5                | 0.0             | -0.025          | 99.2%                  |
| POST1_CTS_000424.LAB | 11/14/23 | 10:36:17 | 0.5        | 0.0           | 0.0            | 190.1                              | 0.98                          | 100.3                | 0.1             | -0.018          | 99.0%                  |
| POST1_CTS_000425.LAB | 11/14/23 | 10:36:24 | 0.4        | 0.0           | 0.0            | 190.1                              | 0.98                          | 100.2                | -0.1            | -0.019          | 98.9%                  |
| POST1_CTS_000426.LAB | 11/14/23 | 10:36:32 | 0.4        | 0.0           | 0.0            | 190.3                              | 0.98                          | 100.3                | 0.2             | -0.025          | 99.1%                  |
| POST1_CTS_000427.LAB | 11/14/23 | 10:36:40 | 0.3        | 0.0           | 0.0            | 190.3                              | 0.98                          | 100.6                | 0.0             | -0.016          | 99.3%                  |

Native Effluent Prior to Analyte Spike

| Spectrum        | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|-----------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| RUN3_000513.LAB | 11/14/23 | 11:53:08 | 11.4       | 12.1          | -0.2           | 190.8                              | 0.97                          | 0.9                  | 0.8             | -0.002          |
| RUN3_000514.LAB | 11/14/23 | 11:54:10 | 11.4       | 12.3          | -0.3           | 190.8                              | 0.97                          | 0.9                  | 0.9             | -0.001          |
| RUN3_000515.LAB | 11/14/23 | 11:55:13 | 11.4       | 12.2          | -0.2           | 190.7                              | 0.97                          | 0.9                  | 0.9             | 0.000           |
|                 |          |          |            |               |                |                                    |                               |                      | <b>0.9</b>      | <b>-0.001</b>   |

Effluent Spike Using Analyte

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Dilution<br>Factor | Recovery %<br>HCN |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST3_SPK_000534.LAB | 11/14/23 | 11:58:43 | 10.3       | 11.6          | -0.2           | 190.6                              | 0.97                          | 0.9                  | 4.5             | 0.409           | 0.083              | 90.3%             |
| POST3_SPK_000535.LAB | 11/14/23 | 11:58:51 | 10.4       | 11.6          | -0.2           | 190.6                              | 0.97                          | 0.9                  | 4.6             | 0.403           | 0.081              | 94.5%             |
| POST3_SPK_000536.LAB | 11/14/23 | 11:58:58 | 10.4       | 11.6          | -0.3           | 190.6                              | 0.97                          | 0.8                  | 4.6             | 0.400           | 0.081              | 95.1%             |
| POST3_SPK_000537.LAB | 11/14/23 | 11:59:06 | 10.4       | 11.5          | -0.2           | 190.6                              | 0.97                          | 1.0                  | 4.7             | 0.399           | 0.080              | 97.4%             |
| POST3_SPK_000538.LAB | 11/14/23 | 11:59:14 | 10.4       | 11.5          | -0.2           | 190.6                              | 0.97                          | 0.9                  | 4.7             | 0.399           | 0.081              | 96.4%             |
| POST3_SPK_000539.LAB | 11/14/23 | 11:59:22 | 10.4       | 11.5          | -0.2           | 190.6                              | 0.97                          | 0.7                  | 4.7             | 0.399           | 0.081              | 97.2%             |
| POST3_SPK_000540.LAB | 11/14/23 | 11:59:30 | 10.3       | 11.5          | -0.2           | 190.6                              | 0.97                          | 0.7                  | 4.8             | 0.395           | 0.080              | 99.0%             |
| POST3_SPK_000541.LAB | 11/14/23 | 11:59:38 | 10.4       | 11.4          | -0.2           | 190.6                              | 0.97                          | 0.9                  | 4.6             | 0.406           | 0.082              | 93.6%             |

CTS, System Purge

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST3_CTS_000554.LAB | 11/14/23 | 12:02:03 | 0.1        | 0.0           | -0.1           | 190.6                              | 0.97                          | 100.6                | 0.0             | -0.021          | 99.3%                  |
| POST3_CTS_000555.LAB | 11/14/23 | 12:02:11 | 0.0        | 0.0           | 0.0            | 190.6                              | 0.97                          | 100.8                | 0.2             | -0.027          | 99.5%                  |
| POST3_CTS_000556.LAB | 11/14/23 | 12:02:19 | 0.1        | 0.0           | 0.0            | 190.6                              | 0.97                          | 100.8                | 0.0             | -0.018          | 99.5%                  |
| POST3_CTS_000557.LAB | 11/14/23 | 12:02:27 | 0.1        | 0.0           | 0.0            | 190.6                              | 0.97                          | 101.0                | 0.2             | -0.020          | 99.7%                  |
| POST3_CTS_000558.LAB | 11/14/23 | 12:02:34 | 0.0        | 0.0           | 0.1            | 190.6                              | 0.97                          | 100.8                | 0.1             | -0.026          | 99.5%                  |
| POST3_CTS_000559.LAB | 11/14/23 | 12:02:42 | 0.0        | 0.0           | 0.0            | 190.6                              | 0.97                          | 100.6                | 0.0             | -0.028          | 99.4%                  |
| POST3_CTS_000560.LAB | 11/14/23 | 12:02:50 | 0.0        | 0.0           | 0.0            | 190.6                              | 0.97                          | 100.9                | 0.2             | -0.029          | 99.6%                  |
| POST3_CTS_000561.LAB | 11/14/23 | 12:02:58 | 0.0        | 0.0           | 0.0            | 190.6                              | 0.97                          | 101.2                | 0.0             | -0.019          | 99.9%                  |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Operating Condition: Mill On

Test Location: Main Kiln Stack  
 Date: 11/14/2023  
 Operator: R. Sollars  
 FTIR s/n: 110161896

Post Test CTS, Direct Purge

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST3_CTS_000981.LAB | 11/14/23 | 16:50:15 | 0.5        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.7                | 0.2             | -0.018          | 99.5%                  |
| POST3_CTS_000982.LAB | 11/14/23 | 16:50:23 | 0.5        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.6                | 0.1             | -0.013          | 99.3%                  |
| POST3_CTS_000983.LAB | 11/14/23 | 16:50:30 | 0.4        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.8                | 0.4             | -0.015          | 99.5%                  |
| POST3_CTS_000984.LAB | 11/14/23 | 16:50:38 | 0.3        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.6                | 0.1             | -0.021          | 99.4%                  |
| POST3_CTS_000985.LAB | 11/14/23 | 16:50:46 | 0.3        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.8                | 0.2             | -0.025          | 99.5%                  |
| POST3_CTS_000986.LAB | 11/14/23 | 16:50:54 | 0.3        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.8                | 0.2             | -0.024          | 99.5%                  |
| POST3_CTS_000987.LAB | 11/14/23 | 16:51:02 | 0.2        | 0.0           | 0.0            | 190.4                              | 0.97                          | 100.6                | 0.1             | -0.015          | 99.4%                  |
| POST3_CTS_000988.LAB | 11/14/23 | 16:51:10 | 0.2        | 0.0           | 0.0            | 190.5                              | 0.97                          | 101.2                | 0.1             | -0.023          | 99.9%                  |
| Average              |          |          |            |               |                |                                    |                               | 100.8                |                 |                 |                        |

Post Test N2, Direct Purge

| Spectrum           | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|--------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| CTS_DIR_001020.LAB | 11/14/23 | 17:01:32 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.8                | 0.1             | -0.023          |
| CTS_DIR_001021.LAB | 11/14/23 | 17:01:40 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.8                | 0.0             | -0.019          |
| CTS_DIR_001022.LAB | 11/14/23 | 17:01:48 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.8                | 0.2             | -0.024          |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Operating Condition: Mill Off

Test Location: Main Kiln Stack  
 Date: 11/14/2023  
 Operator: R. Sollars  
 FTIR s/n: 110161896

System Leak Check: 0.0 mL/min

**Nitrogen (Zero) Direct to FTIR**

| Spectrum             | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|----------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| N2_DIR_000006.LAB    | 11/14/23 | 6:52:09 | 0.0        | 0.0           | 0.0            | 191.0                              | 0.97                          | 0.0                  | -0.1            | -0.008          |
| N2_DIR_0000078KG.LAB | 11/14/23 | 6:54:23 | 0.0        | 0.0           | 0.0            | 190.6                              | 0.97                          | 0.0                  | 0.0             | 0.000           |
| N2_DIR_000008.LAB    | 11/14/23 | 6:54:37 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | 0.0                  | -0.1            | 0.002           |
| N2_DIR_000009.LAB    | 11/14/23 | 6:54:45 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | -0.1                 | -0.1            | 0.001           |
| N2_DIR_000010.LAB    | 11/14/23 | 6:54:53 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | -0.1                 | 0.0             | -0.001          |
| N2_DIR_000011.LAB    | 11/14/23 | 6:55:01 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | -0.2                 | 0.0             | 0.003           |
| N2_DIR_000012.LAB    | 11/14/23 | 6:55:09 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | -0.2                 | -0.1            | 0.002           |
| N2_DIR_000013.LAB    | 11/14/23 | 6:55:17 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | -0.2                 | 0.0             | 0.001           |
| N2_DIR_000014.LAB    | 11/14/23 | 6:55:24 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | 0.0                  | 0.1             | -0.003          |

**Calibration Transfer Standard (CTS), Direct to FTIR**

| Spectrum           | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|--------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| CTS_DIR_000020.LAB | 11/14/23 | 6:56:53 | 0.0        | 0.0           | 0.0            | 190.1                              | 0.97                          | 101.2                | 0.1             | -0.022          | 99.8%                  |
| CTS_DIR_000021.LAB | 11/14/23 | 6:57:01 | 0.0        | 0.0           | 0.0            | 190.1                              | 0.97                          | 101.2                | -0.1            | -0.021          | 99.8%                  |
| CTS_DIR_000022.LAB | 11/14/23 | 6:57:08 | 0.0        | 0.0           | 0.0            | 190.1                              | 0.97                          | 101.5                | 0.0             | -0.020          | 100.1%                 |
| CTS_DIR_000023.LAB | 11/14/23 | 6:57:16 | 0.0        | 0.0           | 0.0            | 190.0                              | 0.97                          | 101.3                | 0.0             | -0.028          | 99.9%                  |
| CTS_DIR_000024.LAB | 11/14/23 | 6:57:24 | 0.0        | 0.0           | 0.0            | 190.0                              | 0.97                          | 101.4                | 0.0             | -0.023          | 100.0%                 |
| CTS_DIR_000025.LAB | 11/14/23 | 6:57:32 | 0.0        | 0.0           | 0.0            | 190.0                              | 0.97                          | 101.2                | 0.0             | -0.023          | 99.8%                  |
| CTS_DIR_000026.LAB | 11/14/23 | 6:57:40 | 0.0        | 0.0           | 0.0            | 189.9                              | 0.97                          | 101.3                | 0.2             | -0.020          | 99.9%                  |
| Average            |          |         |            |               |                |                                    |                               |                      |                 |                 | 99.9%                  |

**Analyte Spike Gas (HCN) Direct to FTIR**

| Spectrum               | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>HCN |
|------------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|-------------------|
| 49.6HCN_DIR_000029.LAB | 11/14/23 | 6:59:08 | 0.0        | 0.0           | 0.0            | 190.1                              | 0.97                          | -0.2                 | 50.3            | 4.957           | 101.4%            |
| 49.6HCN_DIR_000030.LAB | 11/14/23 | 6:59:16 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 0.1                  | 50.4            | 4.968           | 101.8%            |
| 49.6HCN_DIR_000031.LAB | 11/14/23 | 6:59:24 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | -0.1                 | 50.1            | 4.941           | 101.1%            |
| 49.6HCN_DIR_000032.LAB | 11/14/23 | 6:59:32 | 0.0        | 0.0           | 0.0            | 190.4                              | 0.97                          | 0.0                  | 50.5            | 4.961           | 101.8%            |
| 49.6HCN_DIR_000033.LAB | 11/14/23 | 6:59:40 | 0.0        | 0.0           | 0.0            | 190.5                              | 0.97                          | -0.4                 | 50.3            | 4.959           | 101.5%            |
| 49.6HCN_DIR_000034.LAB | 11/14/23 | 6:59:48 | 0.0        | 0.0           | 0.0            | 190.6                              | 0.97                          | -0.1                 | 50.4            | 4.949           | 101.8%            |
| 49.6HCN_DIR_000035.LAB | 11/14/23 | 6:59:55 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | -0.2                 | 50.3            | 4.951           | 101.5%            |
| 49.6HCN_DIR_000036.LAB | 11/14/23 | 7:00:03 | 0.0        | 0.0           | 0.0            | 190.8                              | 0.97                          | -0.2                 | 50.4            | 4.957           | 101.7%            |
| Average                |          |         |            |               |                |                                    |                               |                      |                 |                 | 101.6%            |

**CTS, System Purge**

| Spectrum          | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|-------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| CTS_RT_000044.LAB | 11/14/23 | 7:09:52 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | 100.9                | -0.1            | -0.028          | 99.5%                  |
| CTS_RT_000045.LAB | 11/14/23 | 7:10:00 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.1                | 0.0             | -0.024          | 99.7%                  |
| CTS_RT_000046.LAB | 11/14/23 | 7:10:08 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | 101.2                | 0.0             | -0.027          | 99.9%                  |
| CTS_RT_000047.LAB | 11/14/23 | 7:10:16 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.3                | -0.1            | -0.026          | 100.0%                 |
| CTS_RT_000048.LAB | 11/14/23 | 7:10:24 | 0.0        | 0.0           | 0.1            | 190.2                              | 0.97                          | 101.2                | -0.3            | -0.018          | 99.9%                  |
| CTS_RT_000049.LAB | 11/14/23 | 7:10:32 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.4                | 0.0             | -0.021          | 100.1%                 |
| CTS_RT_000050.LAB | 11/14/23 | 7:10:39 | 0.0        | 0.0           | 0.1            | 190.1                              | 0.97                          | 101.3                | -0.1            | -0.020          | 100.0%                 |
| CTS_RT_000051.LAB | 11/14/23 | 7:10:47 | 0.0        | 0.0           | 0.0            | 190.1                              | 0.97                          | 101.3                | -0.1            | -0.027          | 100.0%                 |

**Response Time Test**

| Spectrum          | Date     | Time    | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Response Time (sec) |
|-------------------|----------|---------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|---------------------|
| CTS_RT_000041.LAB | 11/14/23 | 7:09:29 | 0.9        | 0.0           | 0.0            | 190.4                              | 0.97                          | 0.0                  | -0.2            | -0.003          | -                   |
| CTS_RT_000042.LAB | 11/14/23 | 7:09:37 | 0.7        | 0.6           | 0.0            | 190.4                              | 0.97                          | 25.6                 | 0.0             | -0.024          | 15.89               |
| CTS_RT_000043.LAB | 11/14/23 | 7:09:44 | 0.1        | 0.0           | 0.0            | 190.3                              | 0.97                          | 99.9                 | 0.0             | -0.025          | 23.89               |
| CTS_RT_000044.LAB | 11/14/23 | 7:09:52 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | 100.9                | -0.1            | -0.028          |                     |
| CTS_RT_000045.LAB | 11/14/23 | 7:10:00 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.1                | 0.0             | -0.024          |                     |
| CTS_RT_000046.LAB | 11/14/23 | 7:10:08 | 0.0        | 0.0           | 0.0            | 190.3                              | 0.97                          | 101.2                | 0.0             | -0.027          |                     |
| CTS_RT_000047.LAB | 11/14/23 | 7:10:16 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.3                | -0.1            | -0.026          |                     |
| CTS_RT_000048.LAB | 11/14/23 | 7:10:24 | 0.0        | 0.0           | 0.1            | 190.2                              | 0.97                          | 101.2                | -0.3            | -0.018          |                     |
| CTS_RT_000049.LAB | 11/14/23 | 7:10:32 | 0.0        | 0.0           | 0.0            | 190.2                              | 0.97                          | 101.4                | 0.0             | -0.021          |                     |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Operating Condition: Mill Off

Test Location: Main Kiln Stack  
 Date: 11/14/2023  
 Operator: R. Sollars  
 FTIR s/n: 110161896

Pre 1 Native Effluent Prior to Analyte Spike

| Spectrum        | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|-----------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| RUN3_000513.LAB | 11/14/23 | 11:53:08 | 11.4       | 12.1          | -0.2           | 190.8                              | 0.97                          | 0.9                  | 0.8             | -0.002          |
| RUN3_000514.LAB | 11/14/23 | 11:54:10 | 11.4       | 12.3          | -0.3           | 190.8                              | 0.97                          | 0.9                  | 0.9             | -0.001          |
| RUN3_000515.LAB | 11/14/23 | 11:55:13 | 11.4       | 12.2          | -0.2           | 190.7                              | 0.97                          | 0.9                  | 0.9             | 0.000           |
|                 |          |          |            |               |                |                                    |                               |                      | <b>0.9</b>      | <b>-0.001</b>   |

Pre 1 Effluent Spike Using Analyte

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Dilution<br>Factor | Recovery %<br>HCN |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST3_SPK_000533.LAB | 11/14/23 | 11:58:35 | 10.3       | 11.6          | -0.2           | 190.6                              | 0.97                          | 0.7                  | 4.5             | 0.396           | <b>0.080</b>       | <b>93.6%</b>      |
| POST3_SPK_000534.LAB | 11/14/23 | 11:58:43 | 10.3       | 11.6          | -0.2           | 190.6                              | 0.97                          | 0.9                  | 4.5             | 0.409           | <b>0.083</b>       | <b>90.3%</b>      |
| POST3_SPK_000535.LAB | 11/14/23 | 11:58:51 | 10.4       | 11.6          | -0.2           | 190.6                              | 0.97                          | 0.9                  | 4.6             | 0.403           | <b>0.081</b>       | <b>94.5%</b>      |
| POST3_SPK_000536.LAB | 11/14/23 | 11:58:58 | 10.4       | 11.6          | -0.3           | 190.6                              | 0.97                          | 0.8                  | 4.6             | 0.400           | <b>0.081</b>       | <b>95.1%</b>      |
| POST3_SPK_000537.LAB | 11/14/23 | 11:59:06 | 10.4       | 11.5          | -0.2           | 190.6                              | 0.97                          | 1.0                  | 4.7             | 0.399           | <b>0.080</b>       | <b>97.4%</b>      |
| POST3_SPK_000538.LAB | 11/14/23 | 11:59:14 | 10.4       | 11.5          | -0.2           | 190.6                              | 0.97                          | 0.9                  | 4.7             | 0.399           | <b>0.081</b>       | <b>96.4%</b>      |
| POST3_SPK_000539.LAB | 11/14/23 | 11:59:22 | 10.4       | 11.5          | -0.2           | 190.6                              | 0.97                          | 0.7                  | 4.7             | 0.399           | <b>0.081</b>       | <b>97.2%</b>      |
| POST3_SPK_000540.LAB | 11/14/23 | 11:59:30 | 10.3       | 11.5          | -0.2           | 190.6                              | 0.97                          | 0.7                  | 4.8             | 0.395           | <b>0.080</b>       | <b>99.0%</b>      |

Native Effluent Prior to Analyte Spike

| Spectrum              | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|-----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| MILLOFF_R1_000686.LAB | 11/14/23 | 13:52:40 | 12.4       | 13.9          | -0.2           | 190.8                              | 0.97                          | 1.1                  | 0.8             | 0.004           |
| MILLOFF_R1_000687.LAB | 11/14/23 | 13:53:43 | 12.5       | 14.1          | -0.2           | 190.7                              | 0.97                          | 1.1                  | 0.8             | 0.003           |
| MILLOFF_R1_000688.LAB | 11/14/23 | 13:54:46 | 12.4       | 14.0          | -0.2           | 190.7                              | 0.97                          | 1.1                  | 0.9             | 0.004           |
|                       |          |          |            |               |                |                                    |                               |                      | <b>0.8</b>      | <b>0.004</b>    |

Effluent Spike Using Analyte

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Dilution<br>Factor | Recovery %<br>HCN |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST1_SPK_000702.LAB | 11/14/23 | 13:58:09 | 11.4       | 13.4          | -0.2           | 190.5                              | 0.97                          | 1.0                  | 4.5             | 0.384           | <b>0.078</b>       | <b>96.0%</b>      |
| POST1_SPK_000703.LAB | 11/14/23 | 13:58:17 | 11.4       | 13.5          | -0.2           | 190.6                              | 0.97                          | 1.1                  | 4.5             | 0.383           | <b>0.077</b>       | <b>96.1%</b>      |
| POST1_SPK_000704.LAB | 11/14/23 | 13:58:25 | 11.4       | 13.4          | -0.2           | 190.5                              | 0.97                          | 0.9                  | 4.5             | 0.382           | <b>0.077</b>       | <b>97.0%</b>      |
| POST1_SPK_000705.LAB | 11/14/23 | 13:58:33 | 11.4       | 13.3          | -0.2           | 190.5                              | 0.97                          | 1.2                  | 4.5             | 0.391           | <b>0.079</b>       | <b>94.5%</b>      |
| POST1_SPK_000706.LAB | 11/14/23 | 13:58:41 | 11.4       | 13.4          | -0.2           | 190.6                              | 0.97                          | 1.1                  | 4.5             | 0.408           | <b>0.082</b>       | <b>91.8%</b>      |
| POST1_SPK_000707.LAB | 11/14/23 | 13:58:49 | 11.5       | 13.5          | -0.2           | 190.6                              | 0.97                          | 0.9                  | 4.7             | 0.394           | <b>0.080</b>       | <b>98.7%</b>      |
| POST1_SPK_000708.LAB | 11/14/23 | 13:58:57 | 11.6       | 13.5          | -0.2           | 190.6                              | 0.97                          | 0.9                  | 4.6             | 0.397           | <b>0.080</b>       | <b>95.2%</b>      |
| POST1_SPK_000709.LAB | 11/14/23 | 13:59:04 | 11.7       | 13.5          | -0.3           | 190.6                              | 0.97                          | 1.0                  | 4.5             | 0.403           | <b>0.081</b>       | <b>93.2%</b>      |

CTS, System Purge

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST1_CTS_000715.LAB | 11/14/23 | 14:00:50 | 0.1        | 0.0           | 0.0            | 190.7                              | 0.97                          | 101.1                | 0.0             | -0.016          | <b>99.8%</b>           |
| POST1_CTS_000716.LAB | 11/14/23 | 14:00:58 | 0.1        | 0.0           | 0.1            | 190.7                              | 0.97                          | 101.0                | -0.1            | -0.022          | <b>99.7%</b>           |
| POST1_CTS_000717.LAB | 11/14/23 | 14:01:06 | 0.1        | 0.0           | 0.0            | 190.7                              | 0.97                          | 101.0                | 0.2             | -0.025          | <b>99.7%</b>           |
| POST1_CTS_000718.LAB | 11/14/23 | 14:01:14 | 0.1        | 0.0           | 0.0            | 190.7                              | 0.97                          | 101.0                | 0.0             | -0.019          | <b>99.7%</b>           |
| POST1_CTS_000719.LAB | 11/14/23 | 14:01:22 | 0.1        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.8                | 0.3             | -0.023          | <b>99.6%</b>           |
| POST1_CTS_000720.LAB | 11/14/23 | 14:01:30 | 0.1        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.8                | 0.1             | -0.025          | <b>99.5%</b>           |
| POST1_CTS_000721.LAB | 11/14/23 | 14:01:38 | 0.1        | 0.0           | 0.0            | 190.7                              | 0.97                          | 101.2                | 0.1             | -0.015          | <b>99.9%</b>           |
| POST1_CTS_000722.LAB | 11/14/23 | 14:01:45 | 0.1        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.6                | 0.1             | -0.018          | <b>99.4%</b>           |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Operating Condition: Mill Off

Test Location: Main Kiln Stack  
 Date: 11/14/2023  
 Operator: R. Sollars  
 FTIR s/n: 110161896

Native Effluent Prior to Analyte Spike

| Spectrum              | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|-----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| MILLOFF_R2_000814.LAB | 11/14/23 | 15:17:54 | 12.2       | 14.1          | -0.2           | 191.1                              | 0.97                          | 1.2                  | 1.0             | 0.004           |
| MILLOFF_R2_000815.LAB | 11/14/23 | 15:18:57 | 12.3       | 14.0          | -0.2           | 191.2                              | 0.97                          | 1.2                  | 0.9             | 0.001           |
| MILLOFF_R2_000816.LAB | 11/14/23 | 15:20:00 | 12.3       | 14.1          | -0.2           | 191.2                              | 0.97                          | 1.2                  | 1.0             | 0.006           |
|                       |          |          |            |               |                |                                    |                               |                      | <b>1.0</b>      | <b>0.004</b>    |

Effluent Spike Using Analyte

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Dilution<br>Factor | Recovery %<br>HCN |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST2_SPK_000840.LAB | 11/14/23 | 15:24:31 | 11.2       | 13.2          | -0.3           | 190.7                              | 0.97                          | 1.1                  | 4.4             | 0.351           | 0.071              | 98.4%             |
| POST2_SPK_000841.LAB | 11/14/23 | 15:24:39 | 11.2       | 13.2          | -0.2           | 190.7                              | 0.97                          | 1.2                  | 4.4             | 0.354           | 0.071              | 97.3%             |
| POST2_SPK_000842.LAB | 11/14/23 | 15:24:47 | 11.1       | 13.0          | -0.2           | 190.7                              | 0.97                          | 1.1                  | 4.2             | 0.352           | 0.071              | 92.8%             |
| POST2_SPK_000843.LAB | 11/14/23 | 15:24:55 | 11.1       | 12.8          | -0.2           | 190.7                              | 0.97                          | 1.2                  | 4.3             | 0.358           | 0.072              | 94.1%             |
| POST2_SPK_000844.LAB | 11/14/23 | 15:25:03 | 11.2       | 13.0          | -0.2           | 190.7                              | 0.97                          | 1.0                  | 4.5             | 0.352           | 0.071              | 101.1%            |
| POST2_SPK_000845.LAB | 11/14/23 | 15:25:10 | 11.4       | 13.1          | -0.2           | 190.7                              | 0.97                          | 1.0                  | 4.3             | 0.352           | 0.071              | 95.6%             |
| POST2_SPK_000846.LAB | 11/14/23 | 15:25:18 | 11.4       | 13.2          | -0.2           | 190.7                              | 0.97                          | 1.0                  | 4.4             | 0.359           | 0.072              | 96.4%             |
| POST2_SPK_000847.LAB | 11/14/23 | 15:25:26 | 11.4       | 13.1          | -0.2           | 190.7                              | 0.97                          | 1.2                  | 4.3             | 0.355           | 0.072              | 95.9%             |

CTS, System Purge

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST2_CTS_000855.LAB | 11/14/23 | 15:27:20 | 0.1        | 0.0           | 0.0            | 190.6                              | 0.97                          | 101.1                | 0.1             | -0.027          | 99.8%                  |
| POST2_CTS_000856.LAB | 11/14/23 | 15:27:29 | 0.1        | 0.0           | 0.0            | 190.6                              | 0.97                          | 101.3                | 0.0             | -0.017          | 100.0%                 |
| POST2_CTS_000857.LAB | 11/14/23 | 15:27:36 | 0.1        | 0.0           | 0.0            | 190.5                              | 0.97                          | 101.0                | 0.2             | -0.023          | 99.7%                  |
| POST2_CTS_000858.LAB | 11/14/23 | 15:27:44 | 0.1        | 0.0           | 0.0            | 190.5                              | 0.97                          | 101.0                | 0.1             | -0.024          | 99.7%                  |
| POST2_CTS_000859.LAB | 11/14/23 | 15:27:52 | 0.1        | 0.0           | 0.0            | 190.5                              | 0.97                          | 101.1                | 0.2             | -0.025          | 99.8%                  |
| POST2_CTS_000860.LAB | 11/14/23 | 15:28:00 | 0.1        | 0.0           | 0.0            | 190.5                              | 0.97                          | 101.1                | 0.1             | -0.013          | 99.8%                  |
| POST2_CTS_000861.LAB | 11/14/23 | 15:28:07 | 0.1        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.8                | 0.2             | -0.026          | 99.5%                  |
| POST2_CTS_000862.LAB | 11/14/23 | 15:28:15 | 0.1        | 0.0           | 0.1            | 190.5                              | 0.97                          | 101.2                | 0.1             | -0.019          | 99.9%                  |

Native Effluent Prior to Analyte Spike

| Spectrum              | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|-----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| MILLOFF_R3_000953.LAB | 11/14/23 | 16:42:30 | 12.0       | 14.3          | -0.2           | 191.0                              | 0.97                          | 1.4                  | 1.1             | -0.001          |
| MILLOFF_R3_000954.LAB | 11/14/23 | 16:43:33 | 11.9       | 14.0          | -0.2           | 191.1                              | 0.97                          | 1.4                  | 1.1             | 0.002           |
| MILLOFF_R3_000955.LAB | 11/14/23 | 16:44:35 | 11.7       | 13.8          | -0.2           | 190.9                              | 0.97                          | 1.4                  | 1.0             | 0.002           |
|                       |          |          |            |               |                |                                    |                               |                      | <b>1.1</b>      | <b>0.001</b>    |

Effluent Spike Using Analyte

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Dilution<br>Factor | Recovery %<br>HCN |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|--------------------|-------------------|
| POST3_SPK_000961.LAB | 11/14/23 | 16:46:35 | 10.7       | 12.9          | -0.3           | 190.7                              | 0.97                          | 1.5                  | 4.1             | 0.315           | 0.064              | 98.1%             |
| POST3_SPK_000962.LAB | 11/14/23 | 16:46:43 | 10.6       | 12.8          | -0.2           | 190.7                              | 0.97                          | 1.3                  | 4.1             | 0.310           | 0.063              | 97.8%             |
| POST3_SPK_000963.LAB | 11/14/23 | 16:46:50 | 10.8       | 12.9          | -0.2           | 190.7                              | 0.97                          | 1.3                  | 4.3             | 0.325           | 0.066              | 99.4%             |
| POST3_SPK_000964.LAB | 11/14/23 | 16:46:58 | 10.7       | 13.0          | -0.2           | 190.7                              | 0.97                          | 1.2                  | 4.3             | 0.326           | 0.066              | 100.1%            |
| POST3_SPK_000965.LAB | 11/14/23 | 16:47:07 | 10.8       | 13.2          | -0.2           | 190.6                              | 0.97                          | 1.4                  | 4.2             | 0.327           | 0.066              | 96.6%             |
| POST3_SPK_000966.LAB | 11/14/23 | 16:47:14 | 10.9       | 13.1          | -0.2           | 190.6                              | 0.97                          | 1.4                  | 4.2             | 0.332           | 0.067              | 95.4%             |
| POST3_SPK_000967.LAB | 11/14/23 | 16:47:22 | 10.9       | 13.1          | -0.2           | 190.6                              | 0.97                          | 1.3                  | 4.4             | 0.325           | 0.066              | 102.3%            |
| POST3_SPK_000968.LAB | 11/14/23 | 16:47:30 | 10.9       | 13.2          | -0.2           | 190.5                              | 0.97                          | 1.3                  | 4.0             | 0.306           | 0.062              | 97.7%             |

CTS, System Purge

| Spectrum             | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|----------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| POST3_CTS_000981.LAB | 11/14/23 | 16:50:15 | 0.5        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.7                | 0.2             | -0.018          | 99.3%                  |
| POST3_CTS_000982.LAB | 11/14/23 | 16:50:23 | 0.5        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.6                | 0.1             | -0.013          | 99.5%                  |
| POST3_CTS_000983.LAB | 11/14/23 | 16:50:30 | 0.4        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.8                | 0.4             | -0.015          | 99.5%                  |
| POST3_CTS_000984.LAB | 11/14/23 | 16:50:38 | 0.3        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.6                | 0.1             | -0.021          | 99.4%                  |
| POST3_CTS_000985.LAB | 11/14/23 | 16:50:46 | 0.3        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.8                | 0.2             | -0.025          | 99.5%                  |
| POST3_CTS_000986.LAB | 11/14/23 | 16:50:54 | 0.3        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.8                | 0.2             | -0.024          | 99.5%                  |
| POST3_CTS_000987.LAB | 11/14/23 | 16:51:02 | 0.2        | 0.0           | 0.0            | 190.5                              | 0.97                          | 100.6                | 0.1             | -0.015          | 99.4%                  |
| POST3_CTS_000988.LAB | 11/14/23 | 16:51:10 | 0.2        | 0.0           | 0.0            | 190.5                              | 0.97                          | 101.2                | 0.1             | -0.023          | 99.9%                  |

Client: CalPortland Company, Inc.  
 Facility: Redding Cement Plant  
 Project #: M234605  
 Operating Condition: Mill Off

Test Location: Main Kiln Stack  
 Date: 11/14/2023  
 Operator: R. Sollars  
 FTIR s/n: 110161896

Post Test CTS, Direct Purge

| Spectrum           | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet | Recovery %<br>Ethylene |
|--------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|------------------------|
| CTS_DIR_001020.LAB | 11/14/23 | 17:01:32 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.8                | 0.1             | -0.023          | 99.5%                  |
| CTS_DIR_001021.LAB | 11/14/23 | 17:01:40 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.8                | 0.0             | -0.019          | 99.5%                  |
| CTS_DIR_001022.LAB | 11/14/23 | 17:01:48 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.8                | 0.2             | -0.024          | 99.5%                  |
| CTS_DIR_001023.LAB | 11/14/23 | 17:01:56 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | 101.0                | 0.1             | -0.026          | 99.7%                  |
| CTS_DIR_001024.LAB | 11/14/23 | 17:02:04 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.8                | 0.1             | -0.026          | 99.5%                  |
| CTS_DIR_001025.LAB | 11/14/23 | 17:02:11 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.5                | 0.1             | -0.026          | 99.3%                  |
| CTS_DIR_001026.LAB | 11/14/23 | 17:02:19 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.9                | 0.0             | -0.029          | 99.6%                  |
| CTS_DIR_001027.LAB | 11/14/23 | 17:02:27 | 0.0        | 0.0           | 0.0            | 190.7                              | 0.97                          | 100.9                | 0.1             | -0.025          | 99.7%                  |
| Average            |          |          |            |               |                |                                    |                               | 100.8                |                 |                 |                        |

Post Test N2, Direct Purge

| Spectrum          | Date     | Time     | H2O%<br>%v | CO2<br>%v wet | HF<br>ppmv wet | FTIR Gas Cell Temperature<br>deg C | FTIR Gas Cell Pressure<br>atm | Ethylene<br>ppmv wet | HCN<br>ppmv wet | SF6<br>ppmv wet |
|-------------------|----------|----------|------------|---------------|----------------|------------------------------------|-------------------------------|----------------------|-----------------|-----------------|
| N2_DIR_001031.LAB | 11/14/23 | 17:05:55 | 0.0        | 0.0           | 0.0            | 190.6                              | 0.97                          | 0.1                  | 0.0             | 0.000           |
| N2_DIR_001032.LAB | 11/14/23 | 17:08:01 | 0.0        | 0.0           | 0.0            | 190.5                              | 0.97                          | 0.1                  | 0.0             | -0.001          |
| N2_DIR_001033.LAB | 11/14/23 | 17:10:07 | 0.0        | 0.0           | 0.0            | 190.6                              | 0.97                          | 0.1                  | 0.0             | -0.002          |

| Time                      | DL summary - zero gas |                | Time                      | DL summary - in stack |                |
|---------------------------|-----------------------|----------------|---------------------------|-----------------------|----------------|
|                           | HF ppm (10) 191C      | HCN (100) 191C |                           | HF ppm (10) 191C      | HCN (100) 191C |
| 6:54:45 AM                | 0.02                  | -0.08          | 7:39:43 AM                | -0.16                 | 0.79           |
| 6:54:53 AM                | 0.02                  | -0.03          | 7:40:46 AM                | -0.20                 | 0.77           |
| 6:55:01 AM                | 0.04                  | -0.03          | 7:41:49 AM                | -0.21                 | 0.78           |
| 6:55:09 AM                | -0.03                 | -0.06          | 7:42:52 AM                | -0.18                 | 0.76           |
| 6:55:17 AM                | 0.00                  | -0.01          | 7:43:55 AM                | -0.20                 | 0.79           |
| 6:55:24 AM                | 0.04                  | 0.11           | 7:44:57 AM                | -0.21                 | 0.72           |
| 6:55:33 AM                | 0.03                  | -0.13          | 7:46:00 AM                | -0.21                 | 0.74           |
| <b>Standard Deviation</b> | <b>0.02</b>           | <b>0.07</b>    | <b>Standard Deviation</b> | <b>0.02</b>           | <b>0.02</b>    |
| <b>3x = DL</b>            | <b>0.07</b>           | <b>0.21</b>    | <b>3x = DL</b>            | <b>0.05</b>           | <b>0.07</b>    |

## Appendix I - Gas Cylinder Certifications

# CERTIFICATE OF ANALYSIS

## Grade of Product: EPA PROTOCOL STANDARD

|  |                                  |
|--|----------------------------------|
| Part Number: E03NI56E15A1055             | Reference Number: 48-402752988-1 |
| Cylinder Number: CC308342                | Cylinder Volume: 162.0 CF        |
| Laboratory: 124 - Los Angeles (SAP) - CA | Cylinder Pressure: 2015 PSIG     |
| PGVP Number: B32023                      | Valve Outlet: 590                |
| Gas Code: CO2,O2,BALN                    | Certification Date: May 25, 2023 |

**Expiration Date: May 25, 2031**

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

### ANALYTICAL RESULTS

| Component      | Requested Concentration | Actual Concentration | Protocol Method | Total Relative Uncertainty | Assay Dates |
|----------------|-------------------------|----------------------|-----------------|----------------------------|-------------|
| CARBON DIOXIDE | 22.00 %                 | 22.58 %              | G1              | +/- 0.6% NIST Traceable    | 05/25/2023  |
| OXYGEN         | 22.00 %                 | 22.12 %              | G1              | +/- 1.1% NIST Traceable    | 05/25/2023  |
| NITROGEN       | Balance                 |                      |                 |                            |             |

### CALIBRATION STANDARDS

| Type | Lot ID   | Cylinder No | Concentration                   | Uncertainty | Expiration Date |
|------|----------|-------------|---------------------------------|-------------|-----------------|
| NTRM | 12061520 | CC354777    | 19.87 % CARBON DIOXIDE/NITROGEN | +/- 0.6%    | Jan 11, 2024    |
| NTRM | 08010228 | K016648     | 23.20 % OXYGEN/NITROGEN         | +/- 0.2%    | Jun 01, 2024    |

### ANALYTICAL EQUIPMENT

| Instrument/Make/Model | Analytical Principle | Last Multipoint Calibration |
|-----------------------|----------------------|-----------------------------|
| SIEMENS 6E CO2        | NDIR                 | Apr 26, 2023                |
| SIEMENS OXYMAT 6      | PARAMAGNETIC         | May 22, 2023                |

Triad Data Available Upon Request



Signature on file

# CERTIFICATE OF ANALYSIS

## Grade of Product: EPA PROTOCOL STANDARD

|  |                                  |
|--|----------------------------------|
| Part Number: E03NI78E15A0225             | Reference Number: 48-402834276-1 |
| Cylinder Number: EB0075029               | Cylinder Volume: 152.0 CF        |
| Laboratory: 124 - Los Angeles (SAP) - CA | Cylinder Pressure: 2015 PSIG     |
| PGVP Number: B32023                      | Valve Outlet: 590                |
| Gas Code: CO2,O2,BALN                    | Certification Date: Sep 07, 2023 |

**Expiration Date: Sep 07, 2031**

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted. The results relate only to the items tested. The report shall not be reproduced except in full without approval of the laboratory. Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

### ANALYTICAL RESULTS

| Component      | Requested Concentration | Actual Concentration | Protocol Method | Total Relative Uncertainty | Assay Dates |
|----------------|-------------------------|----------------------|-----------------|----------------------------|-------------|
| CARBON DIOXIDE | 11.00 %                 | 11.15 %              | G1              | +/- 0.6% NIST Traceable    | 09/07/2023  |
| OXYGEN         | 11.00 %                 | 11.18 %              | G1              | +/- 1.4% NIST Traceable    | 09/07/2023  |
| NITROGEN       | Balance                 |                      |                 |                            |             |

### CALIBRATION STANDARDS

| Type | Lot ID   | Cylinder No  | Concentration                   | Uncertainty | Expiration Date |
|------|----------|--------------|---------------------------------|-------------|-----------------|
| NTRM | 08010611 | K005428      | 13.94 % CARBON DIOXIDE/NITROGEN | +/- 0.6%    | Jan 30, 2024    |
| NTRM | 98051002 | SG9150866BAL | 12.05 % OXYGEN/NITROGEN         | +/- 0.7%    | Dec 14, 2023    |

### ANALYTICAL EQUIPMENT

| Instrument/Make/Model | Analytical Principle | Last Multipoint Calibration |
|-----------------------|----------------------|-----------------------------|
| SIEMENS 6E CO2        | NDIR                 | Aug 21, 2023                |
| SIEMENS OXYMAT 6      | PARAMAGNETIC         | Aug 18, 2023                |

Triad Data Available Upon Request



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Signature on file

## CERTIFICATE OF ANALYSIS

### Grade of Product: CERTIFIED STANDARD-SPEC

|                  |                              |                    |                |
|------------------|------------------------------|--------------------|----------------|
| Part Number:     | X02NI99C15A1268              | Reference Number:  | 48-402834277-1 |
| Cylinder Number: | AAL072815                    | Cylinder Volume:   | 144.0 CF       |
| Laboratory:      | 124 - Los Angeles (SAP) - CA | Cylinder Pressure: | 2015 PSIG      |
| Analysis Date:   | Sep 05, 2023                 | Valve Outlet:      | 350            |
| Lot Number:      | 48-402834277-1               |                    |                |

**Expiration Date: Sep 05, 2031**

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Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

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### ANALYTICAL RESULTS

| Component | Req Conc  | Actual Concentration<br>(Mole %) | Analytical<br>Uncertainty |
|-----------|-----------|----------------------------------|---------------------------|
| ETHYLENE  | 100.0 PPM | 101.4 PPM                        | +/- 2%                    |
| NITROGEN  | Balance   |                                  |                           |

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Signature on file

## CERTIFICATE OF ANALYSIS

### Grade of Product: CERTIFIED STANDARD-SPEC

|                  |                           |                    |                 |
|------------------|---------------------------|--------------------|-----------------|
| Customer:        | MOSTARDI PLATT            | Reference Number:  | 160-402841635-1 |
| Part Number:     | X03NI99C15AC0W8           | Cylinder Volume:   | 144.4 CF        |
| Cylinder Number: | CC768241                  | Cylinder Pressure: | 2015 PSIG       |
| Laboratory:      | 124 - Plumsteadville - PA | Valve Outlet:      | 350SS           |
| Analysis Date:   | Sep 11, 2023              |                    |                 |
| Lot Number:      | 160-402841635-1           |                    |                 |

**Expiration Date: Mar 11, 2024**

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

### ANALYTICAL RESULTS

| Component           | Req Conc  | Actual Concentration<br>(Mole %) | Analytical<br>Uncertainty |
|---------------------|-----------|----------------------------------|---------------------------|
| SULFUR HEXAFLUORIDE | 5.000 PPM | 5.001 PPM                        | +/- 1.3%                  |
| HYDROGEN CYANIDE    | 50.00 PPM | 49.55 PPM                        | +/- 5%                    |
| NITROGEN            | Balance   |                                  |                           |



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Signature on file

END OF THE REPORT