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# Hydrogen Cyanide, Hydrogen Fluoride and Diatomic Chlorine from a Portland Cement Plant

Buzzi Unicem USA, Inc. **Maryneal Cement Plant** Maryneal, TX

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TEST DATES: November 29-30, 2023

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Maryneal Cement Plant

202 CR 306

Maryneal, TX 79535

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#### 1. INTRODUCTION

The United States Environmental Protection Agency (US EPA) has directed the portland cement industry (SIC 3241) to conduct emissions testing as part of the US EPA Risk and Technology Review (RTR). This document provides the emission test results and supporting quality assurance/quality control (QA/QC) measures used to produce standardized data having known precision and accuracy. Collection of accurate, representative, and standardized data for facilities with low emissions is necessary especially in view of MACT standard setting procedures.

The Buzzi Unicem USA, Inc (Buzzi) facility in Maryneal, TX is a 1.1 million ton per year rated cement pyro-processing system. The plant operates one dry-process rotary kiln (Kiln #4) that has a preheater/precalciner (PH/PC). It consists of a ThyssenKrupp Industrial Solution PREPOL AS Calciner. An in-line raw mill provides kiln feed to the system.

The Maryneal facility kiln has a Selective Non-Catalytic Reduction System (SNCR) for NOx control, a Dry Sorbent Injection (DSI) system for acid gas control, and a baghouse to control particulate matter (PM). The gases from the kiln process exhaust out of a main kiln stack.

A more detailed description of the processes is provided in Section 2 of the RTR Sampling and Analytical Protocol reproduced in Appendix

The Buzzi retained DEECO Inc. (DEECO) to conduct emission tests for for hydrogen cyanide (HCN), hydrogen fluoride (HF), and diatomic chlorine (Cl<sub>2</sub>). All sampling runs were be one hour long. Concurrent measurements to determine volumetric flow rate were made.

A summary of the test results is shown in Table 1.1.

TABLE 1.1 SUMMARY OF HYDROGEN CYANIDE, HYDROGEN FLUORIDE, AND DIATOMIC CHLORINE EMISSIONS; BUZZI UNICEM USA, INC. MARYNEAL, TX FACILITY; NOVEMBER 29-30, 2023

Test Parameters	Main Stack Raw Mill On	Main Stack Raw Mill Off
Hydrogen Cyanide (FTIR) parts-per-million, dry basis corrected to 7% O <sub>2</sub> pounds-per-hour pounds-per-ton of clinker	13.1 9.6 0.070	15.4 10.6 0.082
Hydrogen Fluoride (FTIR) parts-per-million, dry basis corrected to $7\%~\rm O_2$ pounds-per-hour pounds-per-ton of clinker	<0.053 <0.029 <0.0002	<0.047 <0.024 <0.0002
Hydrogen Fluoride (Method 26A) parts-per-million, dry basis corrected to 7% O <sub>2</sub> pounds-per-hour pounds-per-ton of clinker	<0.31 <0.170 <0.0012	<0.34 <0.175 <0.0014
Diatomic Chlorine (Method 26A) parts-per-million, dry basis corrected to $7\%~\rm O_2$ pounds-per-hour pounds-per-ton of clinker	<0.06 <0.114 <0.0008	0.20 0.40 0.0031

The sampling and analytical procedures followed are summarized in Table 1.2 and discussed in detail in Section 3.

Testing was performed on the main stack under two conditions, Raw Mill On and Raw Mill Off. One Raw Mill On run was conducted on November 29, 2023. The remaining two Raw Mill On runs and three Raw Mill Off runs were conducted on November 30, 2023.

Sampling was conducted by personnel from DEECO, Inc. of Raleigh, North Carolina. All questions regarding sampling and analytical data should be directed to Dr. Scott Steinsberger of DEECO at (800) 733-3261. The field sampling was completed by Lee Harris, Gage Mayer, and Scott Steinsberger of DEECO.

The remainder of this document summarizes the results, procedures and quality control measures followed for this program. Section 2 contains tabulated air emission results for each parameter of interest. Section 3 summarizes the air emission sampling and analytical procedures performed by DEECO, with a brief description and/or reference to the applicable methodologies. Section 4 discusses the basic quality control elements in place for this program to assure the collection of representative, accurate air emission data.

The appendices provided in this document contain all of the necessary information to verify the reported results. Included as Appendices are: Appendix A - Emission Summary Tables; Appendix B - Field Data and CEM/FTIR Data; Appendix C - Ion Chromatography Analytical Report Data; Appendix D - Plant Process Data; Appendix E - Calibration Documents; Appendix F - Test Participants; Appendix G - RTR Sampling and Analytical Protocol

TABLE 1.2 SUMMARY OF SAMPLING AND ANALYTICAL PROTOCOLS FOR BUZZI UNICEM USA, INC. MARYNEAL, TX FACILITY

<b>Location and Frequency</b>	Test Parameter	Sampling Method	Sampling Procedure	Analysis Method	Analysis Procedure
Kiln Main Stack	Volumetric Flow Rate and cyclonic check	EPA Methods 1 and 2	Velocity and temperature traverses	EPA Methods 1 and 2	Manometer for differential pressure and thermocouple for temperature
	Oxygen and Carbon Dioxide and Stratification Check	EPA Method 3A	Continuous; extractive sample	EPA Method 3A	Paramagnetic for O <sub>2</sub> and NDIR for CO <sub>2</sub>
	Moisture	EPA Method 4	Condensation	EPA Method 4	Gravimetric
	Hydrogen Fluoride and Diatomic Chlorine (Cl <sub>2</sub> )	EPA Method 26A	Isokinetic integrated sample	EPA Method 26A	Ion chromatography
	Hydrogen Fluoride and Hydrogen Cyanide	EPA Method 320	Continuous; extractive sample	EPA Method 320	Fourier Transform Infrared (FTIR) Spectroscopy

# 2. SUMMARY OF RESULTS

Emissions sampling was conducted at the Buzzi facility located in Maryneal, TX Sampling was conducted for stack gas flow rate (EPA Methods 1 and 2), stack gas oxygen and carbon dioxide (EPA Method 3A), stack gas moisture (EPA Method 4), stack gas hydrogen fluoride and diatomic chlorine (EPA Method 26A) and stack gas hydrogen cyanide and hydrogen fluoride (EPA Method 320).

Testing was conducted on the main stack under two conditions; Raw Mill On and Raw Mill Off and the results are summarized in Tables 2.1 and 2.2, respectively.

TABLE 2.1 BUZZI UNICEM USA, INC. MARYNEAL, TX FACILITY; KILN MAIN STACK HYDROGEN CYANIDE, HYDROGEN FLUORIDE, AND DIATOMIC CHLORINE EMISSIONS; RAW MILL ON; NOVEMBER 29-30, 2023

		AW MILL ON	,	l ,
Test Parameter	Main Stack Raw Mill On Run 1	Main Stack Raw Mill On Run 2	Main Stack Raw Mill On Run 3	Main Stack Raw Mill On Average
Time	14:50-15:56	09:20-10:26	10:45-11:51	November 29-30, 2023
Flow Rate (dscfm)	256,850	244,700	251,600	251,050
Oxygen	10.7%	11.4%	11.7%	11.3%
Carbon Dioxide	16.9%	15.2%	14.9%	15.7%
Moisture	13.3%	14.0%	11.1%	12.8%
Hydrogen Cyanide (FTIR)				
ppm <sub>dry</sub> at 7% O <sub>2</sub>	13.8	13.1	12.4	13.1
pounds-per-hour	10.9	9.2	8.7	9.6
pounds-per-ton of clinker	0.073	0.069	0.067	0.070
Hydrogen Fluoride (FTIR)				
ppm <sub>dry</sub> at 7% O <sub>2</sub>	< 0.050	< 0.054	< 0.054	< 0.053
pounds-per-hour	< 0.030	<0.028	< 0.028	<0.029
pounds-per-ton of clinker	< 0.0002	< 0.0002	< 0.0002	< 0.0002
Hydrogen Fluoride (Method 26A)				
ppm <sub>dry</sub> at 7% O <sub>2</sub>	< 0.29	< 0.34	< 0.32	< 0.31
pounds-per-hour	<0.168	<0.178	< 0.163	<0.170
pounds-per-ton of clinker	< 0.0011	< 0.0013	< 0.0013	< 0.0012
Diatomic Chlorine (Method 26A)				
ppm <sub>dry</sub> at 7% O <sub>2</sub>	< 0.05	< 0.07	< 0.06	< 0.06
pounds-per-hour	< 0.105	<0.123	< 0.114	<0.114
pounds-per-ton of clinker	< 0.0007	< 0.0009	< 0.0009	< 0.0008

TABLE 2.2 BUZZI UNICEM USA, INC. MARYNEAL, TX FACILITY; KILN MAIN STACK HYDROGEN CYANIDE, HYDROGEN FLUORIDE, AND DIATOMIC CHLORINE EMISSIONS; RAW MILL OFF; NOVEMBER 30, 2023

	, , , , , , , , , , , , , , , , , , ,	AW MILL OF		l
Test Parameter	Main Stack Raw Mill Off Run 1	Main Stack Raw Mill Off Run 2	Main Stack Raw Mill Off Run 3	Main Stack Raw Mill Off Average
Time	14:05-15:11	15:39-16:45	17:25-18:31	November 30, 2023
Flow Rate (dscfm)	202,100	208,800	207,350	206,083
Oxygen	9.7%	9.9%	10.0%	9.9%
Carbon Dioxide	18.2%	17.9%	17.8%	18.0%
Moisture	14.7%	13.8%	14.2%	14.2%
Hydrogen Cyanide (FTIR)				
ppm <sub>dry</sub> at 7% O <sub>2</sub>	15.1	15.7	15.5	15.4
pounds-per-hour	10.4	10.9	10.6	10.6
pounds-per-ton of clinker	0.080	0.085	0.082	0.082
Hydrogen Fluoride (FTIR)				
ppm <sub>dry</sub> at 7% O <sub>2</sub>	< 0.047	< 0.047	< 0.048	< 0.047
pounds-per-hour	< 0.024	<0.024	<0.024	< 0.024
pounds-per-ton of clinker	< 0.0002	< 0.0002	< 0.0002	< 0.0002
Hydrogen Fluoride (Method 26A)				
ppm <sub>dry</sub> at 7% O <sub>2</sub>	< 0.34	< 0.34	< 0.35	< 0.34
pounds-per-hour	< 0.174	< 0.174	< 0.177	< 0.175
pounds-per-ton of clinker	< 0.0014	< 0.0014	< 0.0014	< 0.0014
Diatomic Chlorine (Method 26A)				
ppm <sub>dry</sub> at 7% O <sub>2</sub>	0.25	0.11	0.23	0.20
pounds-per-hour	0.49	0.23	0.47	0.40
pounds-per-ton of clinker	0.0038	0.0018	0.0036	0.0031

#### 3. SAMPLING AND ANALYTICAL PROCEDURES

Table 1.2 presents a summary of the overall sampling and analytical protocols used for the test program for the main stack at Buzzi's Maryneal, TX facility. All sampling and analytical methods employed for this test program were performed in accordance with the procedures outlined in the Reference Test Methods contained in the Code of Federal Regulations, Title 40, Part 60, Appendix A (40 CFR 60, Appendix A) and 40 CFR 63, Appendix A.

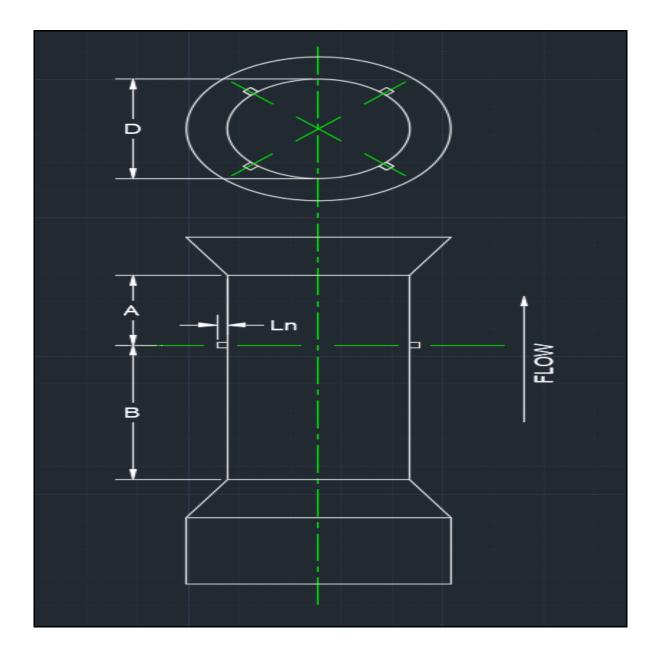
# 3.1 Sampling Point Determination - EPA Method 1

The main stack is a vertically-oriented circular stack with an inside diameter of 140.0" inside diameter. The stack gas sampling ports are located approximately 157'9" (approximately 13.4 duct diameters) above the ID fan breaching and approximately 48'3" (approximately 4.1 duct diameters) from the stack outlet.

The sampling location met the minimum specifications for selection of a measurement site as outlined in EPA Method 1. Cyclonic flow checks, as described in EPA Method 1 Section 2.4, using the Type-S pitot null procedure and angle measurements at the stack test location were conducted.

A twelve (12) point sampling traverse were made using 3 points in each of 4 sampling ports at the main stack. Each traverse was made at each sampling location using a type-S pitot tube in accordance with EPA Methods 2 procedures. The traverse point locations are provided in Appendix B. Gas temperatures were measured using calibrated Type K thermocouples and digital readout devices. All measurements were performed in accordance with the procedures in EPA Methods 2, and 26A.

A schematic of the main stack is provided in Figure 3-1.



Stack Diameter (D) = 140.0"
Distance to nearest upstream disturbance (A) = 579", 4.1 Duct Diameters
Distance to nearest downstream disturbance (B) = 1893", 13.4 Duct Diameters
Sampling Ports Available = 4Ports Diameter = 6"
Length of ports Ln = 6.25"

Figure 3.1 Schematic of the Main Stack Sampling Location

The number and location of the sampling or traverse points were determined according to the procedures outlined in EPA Method 1. The traverse point locations are provided in Appendix B. All points were at least 1.0 inches from the stack wall, per Method 1.

# 3.2 Flue Gas Velocity and Volumetric Flow Rate - EPA Method 2

The flue gas velocity and volumetric flow rate were determined according to the procedures outlined in EPA Method 2. Velocity measurements were using type S pitot tubes conforming to the calibration specifications outlined in EPA Method 2, Section 10.1. Each Type-S pitot tube, calibrated according to these standards, had an assigned coefficient. Differential pressures were measured with fluid manometers. Effluent gas temperatures were measured with chromel-alumel thermocouples equipped with digital readouts.

### 3.3 Outlet Flue Gas Composition - EPA Method 3A

Outlet flue gas analysis for oxygen  $(O_2)$  and carbon dioxide  $(CO_2)$  concentrations, and the calculation of percent excess air and flue gas dry molecular weight was performed in accordance with EPA Method 3A.

To evaluate the sampling location and points for FTIR and  $O_2$  sampling, a three-point  $O_2$  concentration stratification test on a line passing through the centroidal area at (for stacks is greater than 2.4 meters) at 0.4, 1.2 and 2.0 meters from the stack or duct wall. The procedures in Section 8.1.2 of Method 7E were followed, but oxygen will be used as parameter as allowed by fourth sentence in Section 8.1.2. The plant  $O_2$  CEMS was used as a control. A criteria of <5% variation from combined mean for each point was used as indication of non-stratification to allow single point sampling at the point closest to the mean.

Per EPA Method 3A for determining molecular weight, continuous extractive sampling will be obtain using the Method 320 sampling system described in Section 3.6.

A portion of the hot , wet gas sample was sent through a condensing system to remove the stack moisture. A portion of the moisture-free gas sample was sent to an  $O_2/CO_2$  analyzer.

Calibration procedures were be performed in accordance with EPA methodology. Analyzers were calibrated before and after each test and a calibration check between each test run.

The pretest calibrations consisted of the following steps:

- Internal (direct) calibration of each analyzer to adjust calibration and check linearity.
- External (through the entire sampling system) calibration to check the system bias on zero and span gases.

The post test calibration consisted of an external system bias calibration check.

The analyzer calibrated using a certified zero and span (mid or high range) gas. Zero and span

gases were directed to each analyzer through the appropriate plumbing, the calibration gas flow rates were adjusted to the correct flow rate and the analyzer was adjusted with the appropriate span pot.

After the analyzer was properly adjusted the linearity was checked using a low and high range calibration gas. The maximum allowable limit for linearity is 2% of the analyzer range and all analyzers were shown to be linear within these limits before proceding.

The external calibration bias check were performed by placing the CEM system in sampling mode and injecting a zero and span gas into the sample line at the probe exit. This check showed if there is any sampling system related bias, and also checks the integrity of the sample line.

#### 3.3.1 Calibration Gases

DEECO useed EPA Protocol and/or  $\pm 2\%$  NIST Traceable gases for calibration as required by the various reference methods employed in this test program. Calibration gases were selected from previous experience with similar sources and/or from information obtained from the facility engineer prior to sampling. In some cases if the gases that are selected are out of the optimum range of operation then no significant impact of data quality is expected due to the linear nature of the analyzers that were used.

Specific HCN gases were manufactured for this test program in the range of 50-100 ppm to provide spikes in the 5-10 ppm range, or lower; with an  $SF_6$  or appropriate tracer used to calculate the exact spike gas dilution ratio of 10% or less.

No audit gases from a federal or a state agency were provided.

# 3.3.2 Sampling Procedures

At the completion of the pretest calibration routine, the CEM system was ready for operation. No further adjustments of sample flow rates, analyzer zero or span adjustments, or other critical CEM operating parameters were made until testing and post test calibration were complete.

Each sampling run was one hour. At the completion for each test run, calibration gases were used to check between test runs. A zero and the upscale calibration gas closest to the actual emission concentrations were used for the pretest and post test calibrations.

#### 3.4 Flue Gas Moisture Content - EPA Method 4

The flue gas moisture content was determined in conjunction with the EPA Method 26A trains according to the sampling and analytical procedures outlined in EPA Method 4. (NOTE: In order to maintain isokinetic sampling, the sampling rate used may have been required to temporarily exceed the EPA Method 4-specified maximum sampling rate of 0.75 CFM, based on observed stack gas pitot readings.) The impingers were connected in series and contained reagents as described below. The impingers were contained in an ice bath in order to assure condensation of the moisture in the flue gas stream. Any moisture that is not condensed in the impingers was captured in the silica gel, therefore all moisture was weighed and entered into moisture content calculations.

# 3.5 Hydrogen Fluoride and Diatomic Chlorine - EPA Method 26A

Sampling and analytical procedures were those outlined in EPA Method 26A to determine primarily diatomic chlorine ( $\text{Cl}_2$ ) emissions and hydrogen fluoride (HF) emissions at main stack outlet sampling locations. Duplicate simultaneous trains (a.k.a "paired trains") for each test run were used to determine precision.

Sample was collected through a heated glass probe, followed by a heated Teflon filter, where stack gas HF and  $\text{Cl}_2$  were collected in a series of chilled impingers. The sampling train impingers contained 100 ml of 0.1N sulfuric acid in the first and second, an empty third impinger, 100 ml of 0.1N NaOH in the fourth and fifth and 200 grams of silica gel in the last impinger

Sampling was conducted isokinetically  $(\pm 10\%)$  with readings of flue gas parameters recorded at traverse points selected according to EPA Method 1. Leak-checks on the Method 26A sampling train were performed before and after each sampling run and optionally for any port change. The sampling train leak-checks and leakage rate (where applicable) were documented on the field test data sheet for each respective run. All leak checks were acceptable.

The glass button hook nozzle and probe liner was constructed of borosilicate glass. The filter holder will be constructed of borosilicate glass with a Teflon frit filter support and a sealing gasket. A PTFE-bonded glass fiber filter was used. The probe and filter housing were heated to above 248°F and not exceed an upper boundary of 273°F. Probe liners and filter holders were cleaned thoroughly prior to testing.

The Method 26A trains was operated isokinetically for a minimum of 60 minutes and collected a minimum of 1 dry, standard cubic meter (DSCM). Pretest preparations, preliminary determinations, and leak check procedures were those outlined in EPA Method 5.

After completion of sampling the train was leak checked and transferred to the sample recovery trailer. All leak checks were acceptable. The impingers were weighed to determine moisture gain in accordance with EPA Method 4.

Sample recovery involved quantitative recovery of the sulfuric acid impinger contents and the NaOH impinger contents into separate tare-weighed, precleaned polyethylene sample containers.

The nozzle, probe, filter and filter housing were not recovered.

The contents of sulfuric acid impingers, including the contents if any of the empty (2<sup>nd</sup> knockout or third) impinger were quantitatively transferred to the tare-weighed, precleaned polyethylene sample container, followed by three rinses with deionized (DI) water of the impingers and all connecting glassware (including the connecting glassware to the first impinger) placed in the same H<sub>2</sub>SO<sub>4</sub> container. The container was labeled and weighed to determine the final sample volume.

The contents NaOH impingers were quantitatively transferred to a second tare-weighed, precleaned polyethylene sample container, followed by three rinses with DI water of the impingers and all connecting glassware placed in the same NaOH container. The container was labeled and weighed to determine the final sample volume.

Sample recovery from each train included:

- 1. Container No. 1 Contents of H<sub>2</sub>SO<sub>4</sub> impingers and knockout impinger and, and DI rinse of impingers and connecting glassware; and
- 2. Container No. 2 Contents NaOH impingers, and DI rinse of impingers and connecting glassware.

Additional quality control consisted of collecting and analyzing a field blank train for every three test runs. The blank train was assembled from a used train, leak checked and sat for a period equal to the sampling time (i.e, 1-hr). The blank train data was to be used to determine the method detection limit for the test program target analytes (ie. The lowest number that could be detected), and compared to stack emissions.

Reagent blanks of 0.1 N H<sub>2</sub>SO<sub>4</sub>, 0.1N NaOH, and DI water were collected and archived for later analysis should there be any issues with the field blank train samples

The H<sub>2</sub>SO<sub>4</sub> impinger solutions were analyzed using ion chromatography techniques for fluoride ions (F) (EPA SW-9057). Duplicate analyses performed on the samples and field blanks. Precision was demonstrated by duplicate injection of each sample, the results of each individual analysis being within 5% of their mean to be acceptable.

The NaOH impinger solutions was treated with sodium thiosulfate to ensure complete conversion of hypochlorous acid (HClO) to chloride ions (Cl<sup>-</sup>). The resulting solution was analyzed using ion chromatography techniques for chloride ions (EPA SW-9057). Duplicate analyses was performed on the samples and field blanks. Precision was demonstrated by duplicate injection of each sample, the results of each individual analysis being within 5% of their mean to be acceptable

All EPA Method 26A HF/Cl<sub>2</sub> samples were analyzed by Element One of Wilmington NC. Refer to Section 1, Figure 1.1 of the RTR Sampling and Analytical Protocol for contact information.

For this test program, the relative deviation (RD) was to be calculated as described in EPA Method 30B between the Cl<sub>2</sub> concentrations measured with the paired trains. A criteria of a less than 10% relative deviation or 0.2 ppm absolute difference was required.

The absolute differences between the  $\mathrm{Cl}_2$  concentrations measured with the paired trains is summarized in Table 3.1. For each paired run,  $\mathrm{Cl}_2$  concentrations met the 0.2 ppm absolute difference criteria.

TABLE 3.1 PAIRED METHOD 26A SAMPLING TRAIN DIATOMIC CHLORINE CONCENTRATION COMPARISON RESULTS FOR THE KILN MAIN STACK; NOVEMBER 29-30, 2023

	, , , , ,	Train A Diatomic Chlorine	Train B Diatomic Chlorine	Absolute
Run	Time	Concentration (ppm,dry)	Concentration (ppm,dry)	Difference (ppm,dry)
November 29-30	, 2023; Main Stack;	Raw Mill On		
Run 1	14:50-15:56	< 0.037	< 0.037	0.000
Run 2	09:20-10:26	< 0.042	<0.049	0.006
Run 3	10:45-11:51	< 0.043	< 0.040	0.003
November 30, 20	23; Main Stack; Ra	w Mill Off		
Run 1	14:05-15:11	0.192	0.206	0.015
Run 2	15:39-16:45	0.085	0.093	0.008
Run 3	17:25-18:31	0.173	0.185	0.012

# 3.6 Hydrogen Cyanide and Hydrogen Fluoride - EPA Method 320

EPA Method 320 was performed to determine emissions of concentrations of HCN and HF. Three, 1-hour sampling runs were conducted under each representative process and control system operating conditions.

The gas sample was extracted from the stack through a glass-lined probe and filter heated to  $375^{\circ}$  F. For external calibration checks and analyte spikes, the gases were introduced in front of the heated filter. Any excess calibration gas was diverted through the sample probes into the source. Outflow of gas from the heated filter enclosure was transported through a Teflon sample line heated to  $375^{\circ}$  F. For these sources approximately 300' of sample line was required. The heated sample line was connected directly to the FTIR sample cell. Using heat-traced Teflon tubing the exit of the FTIR cell was connected to a sample pump with a heated stainless steel pump head. The pump discharge was directed to a proprietary chiller-type gas conditioner to remove moisture prior to delivery sample gas to the  $O_2/CO_2$  monitor.

The distribution of the gas sample to the monitors was accomplished using a panel equipped with valves and rotometers. The gas sample was then divided and directed to the  $O_2/CO_2$  analyzer.

FTIR sample cell was maintained at 191 °C and connected to a MKS Instruments Multigas 2030 Fourier Transform Infrared Spectrometer and Detector.

The FTIR spectrometer measured vapor phase organic or inorganic compounds which absorb energy in the mid-infrared spectral region, about 400 to 4000 cm $^{-1}$  (25 to 2.5  $\mu$ m). Continuous measurement were made by matching sample absorbance bands with bands in reference spectra, and comparing sample band intensities with reference band intensities.

The principle limitation to FTIR spectroscopy are the presence of interfering compounds that also absorb energy in the mid-infrared spectral region. In a cement kiln stack gas matrix, water vapor  $(H_2O)$  and carbon dioxide  $(CO_2)$  are the primary interferents that must be incorporated into the identification and quantitation method.

The FTIR software performs the computation for a single compound by subtracting all the other compounds (interferants and target) from the absorbance spectra and quantifies the single compound based on the remain absorbance. The FTIR software provides a Standard Error Calculation (SEC) value that is an indication of how well the identification and quantitation has been performed. A high SEC indicates that other interferants have not been accounted for in the analysis method, and a low SEC is indicative of greater confidence measurement.

The instrument is operated with a resolution of 0.5 cm<sup>-1</sup> with 4x zero filling. Beer-Norton Medium apodization is used with amplitude phase correction.

For this RTR test program, following specific QA/QC activities for EPA Method 320 were performed and are summarized in Table 3.2

#### 3.6.1 Laboratory QA/QC Activities Before Field Test Program

Before field testing occurs, the following QA/QC activities were conducted;

- Seven consecutive samples of dry nitrogen <u>through the sampling system</u> was acquired and used to calculate the standard deviation for each of the test program target analytes multiplied by a factor of 3. These data were considered representative of detection limits (DL) for this test program and were below the 0.5 ppm required DL for both HCN and HF;
- 2) From these seven dry nitrogen samples, the results for the Signal-to-Noise Ratio (SNR) @ 2500 cm<sup>-1</sup> was >2500, at 64 scans and the results for single beam intensity @ 2500 cm<sup>-1</sup> was >0.9; and
- 3) The HCN calibration gases was analyzed directly and the FTIR responses agreed with tag value within 5%

# 3.6.2 QA/QCActivities During Field Test Program

During the field test program, following QA/QC activities were be performed and criterium met;

- 1) On each test day prior to any testing, an instrument background was collected using dry nitrogen directed to the gas cell. The background was collected with at least 128 scans;
- 2) The probe, filter, sample line and all sample system components in contact with effluent were be maintained at or above 375°F or 191°C (consistent with FTIR calibration temperature) to avoid any possible "cold spots;"
- A system zero with all sampling system components at operating temperature was performed by injecting nitrogen at the sample probe and through sample filter and entire measurement system. After zero equilibration was been achieved, all measurement components will be quantified for at least 128 scans;
- 4) The sample probe was position at effluent measurement point and sampling was continue until equilibration of the measurement system has been achieved. At this point, the effluent concentrations was quantified with two consecutive 64-scan samples as the initial native concentration for the dynamic spike;
- 5) Analyte spiking was conducted for HCN before the first test run, and after each successive test run for a minimum of 4 spikes per test condition. These results will be used to determine accuracy and are summarized in Table 3.3;
- The spike gas injections was maintained at 10% or less of total sample volume. The spike gas concentration and flow rate was be selected to approximately double the native effluent concentration. Spike recovery results were within  $\pm 20\%$  of the expected value. An SF<sub>6</sub> tracer was used to calculate the exact spike gas dilution ratio of 10% or less;
- 7) After the dynamic spike, nitrogen was sent through the sampling system until all traces of spike gas are removed and lines are proven below DL for target analytes;

TABLE 3.2 FTIR PRETEST AND FIELD TEST QA/QC SUMMARY

TABLE 3.2   FTIR PR	EIESI ANI	D FIELD TES	T QA/QC SU	VIVIARY	
Spectrum	HCN	SF6	HF	SNR 2500	sBeam @2500
Seven consecutive samples	s of dry nitroge	n for detection li	mit		
SPC 000837.LAB	-0.051		-0.002	6223.51	1.42
SPC 000838.LAB	-0.032		-0.000	5809.30	1.42
SPC 000839.LAB	0.046		-0.017	3759.60	1.42
SPC 000840.LAB	-0.011		0.016	4373.66	1.42
SPC 000841.LAB	0.080		0.002	5347.95	1.42
SPC 000842.LAB	0.059		-0.012	5012.46	1.42
SPC000843.LAB	-0.029		-0.006	4706.13	1.42
Standard Deviation X 3	0.156		0.032		
Averages				5033.23	1.42
HCN Standard (CC76823	3; 199.1 ppm H	CN/10.0 ppm SF	6)		
SPC 003164.LAB	196.3	9.6			
SPC 003165.LAB	197.0	9.6			
SPC 003166.LAB	197.0	9.6			
SPC 003167.LAB	197.3	9.6			
<del></del>			-		
Averages	196.9	9.6			
HCN Standard (CC76822	2; 49.9 ppm HC	CN/5.0 ppm SF6)	_		
SPC 003173.LAB	49.91	4.85			
SPC 003174.LAB	49.93	4.85			
SPC 003175.LAB	49.82	4.85			
SPC003176.LAB	49.90	4.85			
Averages	49.89	4.85	1		
Residuals for Post HCN a	nalyte spike nat	ive scans	<u> </u>		
SPC_003269.LAB Concentration	0.65		0.00		
	8.65		-0.06		
MDC3	0.38		0.25		
MDC3%	4.4%		NA	_	
SPC_003270LAB					
Concentration	8.64		-0.02		
MDC3	0.47		0.24		
MDC3%	5.4%		NA		
Final SNR @ 2500 cm <sup>-1</sup> an	ıd single beam i	ntensity @ 2500	cm <sup>-1</sup>		
SPC 004198.LAB				3828.6	1.30

- The nitrogen purge was discontinued and the sampling system was allowed to equilibrate with stack gas before starting a test run. The first two consecutive 64-scan samples of a sample run was used for the final native concentration. Residual results for HCN and HF were verified to be less than 0.2-0.3 ppm for data acceptance, or less than 5% of the measured value, whichever was least restrictive.
- 9) The final SNR @ 2500 cm<sup>-1</sup>, at 64 scans, and the results for single beam intensity @ 2500 cm<sup>-1</sup> were verified to met the >2500 and >0.9 criterium; respectively.

TABLE 3.3 ETHYLENE CALIBRATION TRANSFER STANDARD (CTS) AND HYDROGEN CYANIDE ANALYTE SPIKING TEST RESULTS FOR THE KILN MAIN STACK; NOVEMBER 29-30, 2023

Run	Time	Average Native Hydrogen Cyanide Concentration (ppm,wet)	Spike plus Average Hydrogen Cyanide Native Concentration (ppm,wet)	Hydrogen Cyanide Spike Recovery	CTS Error
November 29,	2023; Main Stac	k Raw Mill On			
Pre Run 1	12:15-12:33	8.72	19.97	95.9%	-1.3%
Post Run 1	13:16-13:56	9.15	17.74	91.4%	-2.6%
November 30,	2023; Main Stac	k Raw Mill On			
Pre Run 2	09:08-09:24	7.66	10.95	92.3%	-2.1%
Post Run 2	10:27-10:39	7.56	11.36	91.7%	
Post Run 3	11:42-11:56	7.40	10.90	89.7%	-2.1%
November 30,	2023; Main Stac	k Raw Mill Off			
Pre Run 1	13:39-13:57	9.73	13.50	99.5%	-2.1%
Post Run 1	15:12-15:23	10.69	14.05	91.5%	
Post Run 2	16:46-16:58	10.87	14.40	94.2%	
Post Run 3	18:31-18:51	10.26	13.50	93.0%	-2.2%

# 4. QA/QC PROCEDURES AND RESULTS

The objective of a quality assurance/quality control (QA/QC) program is to assure that the precision and accuracy of all environmental data generated by DEECO for clients are commensurate with data quality objectives (DQO's). DQO's are based on a common understanding of the intended end use(s) of the data, the measurement process, and the availability of resources. Once DQO's are established, formally or informally, QC protocol can be defined for the measurements.

In this project, the final data user will be Holcim. The data quality objectives in this project are to generate scientifically sound data to be used for compliance purposes.

# 4.1 Sampling Equipment

All of the sampling equipment used was calibrated according to the procedures outlined in the <u>Quality Assurance Handbook for Air Pollution Measurement Systems</u>, Volume III, EPA-600/4-77-027b.

# 4.1.1 Manual Sampling Equipment Calibrations

For sampling Methods 1, 2, and 4 the procedures and equipment used to measure stack gas velocity and temperature measurements and the metering system used to maintain constant rate sampling conditions and to determine the sample gas volume were subjected to pretest and posttest calibrations and/or inspections as required by the appropriate EPA methods.

**Barometer** - Barometric pressure values were obtained from a calibrated barometer, verified by phone call to a local airport, and corrected for elevation to sample port level (0.01 inches Hg per 10 ft. elevation).

<u>Pitot Tubes</u> - Each pitot tube used in sampling meets the design specifications for type-S pitot tubes in EPA Method 2. Therefore, a maximum value baseline coefficient ( $C_p$ ) of 0.84 is assigned to each pitot tube. Calibration by the manufacturer for pitot face-opening alignment included measuring the external tubing diameter (dimension  $D_t$ ), the base-to-opening plane distance (dimensions  $P_a$  and  $P_b$ ), and the face opening misalignment angles, with all terms as described in EPA Method 2. Pitot tubes were visually inspected for structural integrity at the completion of each test. Inspection sheets for pitot tubes are included in Appendix E.

Calibration Meter and Metering System - The secondary reference meter equipment arrangement for calibration is shown in Figure 5.7 of EPA Method 5. The prescribed procedures were followed. A wet test meter with a 1 ft<sup>3</sup>/rev capacity and  $\pm$  1 percent accuracy is used as the primary calibrant. The dry gas meter's pump is run for a minimum of 5 minutes at a flow rate of 0.35 cfm to condition the interior surface of the wet test meter. Leak checks are performed and if satisfactory, triplicate runs at each of no less than five different flow rates are done. A calibration curve is prepared and the meter is recalibrated after 200 hours of operation or annually, whichever comes first.

The calibration set-up for the dry gas metering system using the secondary reference meter in lieu of the wet test meter is given in Figure 5.5 of EPA Method 5. A leak check of the metering system before calibration was performed as shown in Figure 5.4 of EPA Method 5. The metering systems's pump is operated for 5 minutes at an orifice manometer setting of 0.5 inches  $H_20$  to heat up the pump and system to stabilize the meter inlet and outlet temperatures. Values for the orifice setting (delta H), wet test meter volume  $(V_w)$ , corresponding dry test meter volume  $(V_d)$ , dry test meter inlet and outlet gas temperatures ( $t_{di}$  and  $t_{dn}$ ), and time are recorded for the initial calibration. Then the ratio of the wet test meter to the dry test meter (gamma) and the orifice pressure differential that equates to 0.75 cfm at standard conditions (delta H@) are calculated.

A post-test meter calibration was made on the dry gas meter used during the test to check its accuracy against the pre-test calibration. This was performed following EPA Method 5, Section 16.3 or a post-test calibration check was made using the average orifice setting obtained during each test run and setting the vacuum at the maximum value obtained during each test run. These test runs were made against DEECO's secondary reference dry gas meter which was calibrated against a wet test meter. The calibration data sheets for the dry gas meters are included in Appendix E.

<u>Thermocouples and Digital Indicators</u> - Thermocouples were calibrated by comparing them against an ASTM-3F mercury-in-glass thermometer at approximately 32°F (ice water), ambient temperature, and at approximately 220°F. Each thermocouple was calibrated against temperature ranges to which it is typically exposed during test conditions, and they agreed within 1.5 percent (expressed in °R) of the reference thermometer throughout the entire calibration range. Also, thermocouples were checked at ambient temperature at the test site to verify calibration. The calibration data sheets for the thermocouples are included in Appendix E.

<u>Pretest and Posttest Leak Checks of Sampling Trains</u> - Each Method 4 sampling train was subjected to pretest leak checks and posttest leak checks. For all sampling runs the posttest leak checks were acceptable (less than 4% of the sampling rate at the highest vacuum recorded during the test run).

# 4.2 Analytical QA/QC Results

Analytical measurements of precision and accuracy were made on stack gas samples, and are summarized in a separate report.

# Appendix A

**Emission Summary Tables** 

Company: Buzzi Unicem; Maryneal TX Source: Main Stack; Raw Mill On Job ID: 23-3315

Train Type: EPA Method 26A

	1A 11/29/23 1450-1556	1B 11/29/23 1450-1556	3A 11/30/23 920-1026	3B 11/30/23 920-1026	4A 11/30/23 1045-1151	4B 11/30/23 1045-1151	Average
Initial Meter Volume, ft <sup>3</sup>	861.672	971.583	936.456	43.246	988.879	95.369	
Final Meter Volume, ft <sup>3</sup>	917.275	1025.334	988.745	95.115	1040.834	147.364	
Intra-Port Volume and/or Leak Check Correction, ft3	0.000	0.000	0.000	0.000	0.000	0.000	
Total Sample Volume, cf	55.603	53.751	52.289	51.869	51.955	51.995	52.910
DGM Calibration Factor	0.975	0.985	0.975	0.985	0.975	0.985	0.980
Average DGM Temp, F	69.6	72.3	61.3	61.6	66.1	68.1	66.5
Average DGM delta H, "H2O	2.33	2.34	2.18	2.19	2.17	2.18	2.23
Barometric Pressure, "Hg	27.32	27.32	27.43	27.43	27.43	27.43	27.39
Corrected Sample Vol, dscf	49.631	48.225	47.586	47.662	46.850	47.189	47.857
Corrected Sample Vol, dscm	1.405	1.366	1.347	1.350	1.327	1.336	1.355
Sample Volume (at Stack Conditions), acf	83.169	81.562	82.682	82.814	78.949	78.996	81,362
Sample Volume (at Stack Conditions), acm	2.355	2.310	2.341	2.345	2.236	2.237	2.304
Oxygen, %	10.7	10.7	11.4	11.4	11.7	11.7	11.3
Carbon Dioxide, %	16.9	16.9	15.2	15.2	14.9	14.9	15.7
Nitrogen, %	72.4	72.4	73.4	73.4	73.4	73.4	73.1
Stack Gas Excess Air, %	127.2	127.2	142.9	142.9	152.4	152.4	140.8
Total Moisture Catch Weight, grams	155.3	162.7	164.1	164.6	128.4	120.7	137.9
Stack Gas Moisture, %	12.9	13.7	14.0	14.0	11.4	10.8	12.8
Stack Gas Dry Molecular Weight, lb/lbmole	31.13	31.13	30.89	30.89	30.85	30.85	30.96
Stack Gas Wet Molecular Weight, lb/lbmole	29.44	29.33	29.08	29.08	29.39	29.46	29.30
Average Stack Temp, F	242.4	242.4	262.0	262.0	261.4	261.5	255.3
Stack Static (Gauge) Pressure, "H2O	-0.67	-0.67	-0.67	-0.67	-0.67	-0.67	-0.67
Stack Gas Actual Pressure, "Hg	27.27	27.27	27.38	27.38	27.38	27.38	27.34
Average Sqrt delta P *	0.991	0.991	0.958	0.958	0.958	0.958	0.969
Pitot Tube Coefficient	0.85	0.85	0.85	0.85	0.85	0.85	0.85
Stack Gas Velocity, ft/second	67.36	67.48	66.29	66.29	65.91	65.84	66.53
Nozzle Inside Diameter, inches	0.250	0.250	0.250	0.250	0.250	0.250	
Total Sample Time, min	60	60	60	60	60	60	60
Isokinetic Rate, %	100.7	98.6	101.7	101.9	97.7	97.8	99.7
Stack Dimensions	140 in. ID	140 in. ID	140 in. ID	140 in. ID	140 in. ID	140 in. ID	
Stack Area, sq ft	106.90	106.90	106.90	106.90	106.90	106.90	106.90
Actual Stack Gas Flow Rate, acfm	432,000	432,800	425,200	425,200	422,700	422,300	426,700
Actual Stack Gas Flow Rate, acmm	12,233	12,256	12,040	12,040	11,970	11,958	12,083
Stack Gas Flow Rate, dscfm	257,800	255,900	244,700	244,700	250,900	252,300	251,100
Stack Gas Flow Rate, dscmm	7,300	7,246	6,929	6,929	7,105	7,144	7,109

Company: Buzzi Unicem; Maryneal TX Source: Main Stack; Raw Mill On Job ID: 23-3315 Train Type: EPA Method 26A

NOTE: Average INCLUDES Non-detect runs' results

"ND()" denotes values below detection limits

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Average	0.2445 0.181 0.261 0.139 0.217 0.314 0.167 0.170	0.164166667 0.121 0.176 0.093 0.041 0.060 0.032 0.014
		~~~~
4B 30-Nov-23 1045-1151	0.224 0.168 0.253 0.135 0.202 0.305 0.162 0.162 0.163	0.156 0.117 0.176 0.094 0.003 0.060 0.032 0.0110
4A 30-Nov-23 1045-1151	0.237 0.179 0.270 0.144 0.215 0.324 0.173 0.168	0.167 0.126 0.190 0.101 0.043 0.034 0.034
3B 30-Nov-23 920-1026	0.259 0.192 0.281 0.151 0.231 0.338 0.182 0.176	0.193 0.143 0.209 0.113 0.006 0.071 0.038 0.038
3A 30-Nov-23 920-1026	0.265 0.197 0.288 0.155 0.237 0.346 0.187 0.180	0.167 0.124 0.0181 0.0098 0.042 0.062 0.033 0.114
1B 11/29/23 1450-1556	0.254 0.186 0.253 0.132 0.224 0.305 0.159 0.178	0.148 0.108 0.148 0.077 0.000 0.050 0.026 0.104
1A 11/29/23 1450-1556	0.228 0.162 0.221 0.115 0.195 0.266 0.139 0.157	0.154 0.110 0.149 0.078 0.037 0.026 0.026
		2.
	Catch Wt, mg Conc., mg/dscm Conc., mg/dscm @ 7% O2 Conc., mg/dscm @ 12% CO2 Conc., ppmvd @ 7% O2 Conc., ppmvd @ 7% O2 Conc., ppmvd @ 12% CO2 Emission Rate, lb/hr Clinker Rates (tph and lbs/ton)	Catch Wt, mg Conc., mg/dscm Conc., mg/dscm @ 7% O2 ND Conc., mg/dscm @ 12% CO2 ND Conc., ppmvd Absolute Difference, ppmvd (<0.2 required) Conc., ppmvd @ 7% O2 Conc., ppmvd @ 12% CO2 ND Conc., ppmvd @ 12% CO2
	Hydrogen Fluoride	Chlorine

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill On

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	CO2% (40) 191	14.169	14.010	14.101	13.875	14.046	14.321	14.172	14.101	14.005	13.844	13.937	13.979	13,914	14.007	14.256	13.902	14.039	14.073	14.081	14.105	14.033	14.023	14,179	13.961	14.144	14.104	14.260	14.046	14.131	14.163	14.093	14,113	14.251	14.223	14,143	14.182	14.132	14.181	14.028	14.041	13.983	14.014	14.050	14.337	14.097	14.076	13.982	14.174	13.950	14.091	14.119	14.091	M26A Moisture
	H2O% (40) 191C	13.327	13.899	12.380	14.220	13.464	13.550	13.854	13.525	13.671	13.382	13.671	13.690	14.052	13.739	13.359	13.63/	13.696	13.674	13.394	13.748	13.303	13.694	13.027	14,545	13.315	13.644	13.509	14 010	13.791	13.489	13.562	13.585	13.616	13.704	13.753	13.818	13.654	13.361	13.892	13.798	13.976	13.670	14.167	13.426	13.935	13.865	13.801	13.373	14,096	14.139	13,489	13.687	13.3
	Ethylene (100,3000) 191C HZO% (40) 191C CO2% (40) 191C	3.326	3.302	3.250	3209	3.044	2.948	3.046	3.120	3.134	3.264	3,157	3.282	3.200	3.054	3.069	3.115	3.007	3.035	3.012	2.986	3.266	3.170	3.219	3.290	3.324	3.264	3.429	3.474	3.473	3.426	3.497	3.317	3.234	3.251	3.288	3.359	3.340	330	3.316	3.393	3.296	3.320	3.096	3.087	3 228	3.050	3.036	3.165	3.224	3.159	3.221	3.217	4.163
	SF6 (10) 191C	-0.016	-0.013	200	-0.010	-0.012	-0.010	-0.011	20.012	0000	0.013	-0.012	-0.011	-0.013	-0.012	0.012	-0.012	0.014	-0.008	-0.013	0.015	4000	-0.011	-0.012	-0.013	-0.012	-0.013	-0.012	-0.013	0012	0013	-0.015	-0.013	-0.012	6000	-0.013	-0.014	0.010	0.013	-0.011	-0.003	0.011	-0.012	-0.015	-0.014	-0.012	-0.012	-0.015	-0.014	0.030	0013	-0.014	-0.012	-0.084
	191C	-0.149	5 5 5 5	25.0	-0.150	-0.187	-0.195	-0.194 -0.194	9,50	0.140	-0.148	-0.156	-0.164	-0.151	-0.131	-0.182	0.142	0.198	-0.194	-0.199	-0.180	-0.17	9 6 6	-0.199	-0.125	0.15 6.15 6.15 6.15	0.155	-0.199	-0.149	0.145	9.0	-0.155	-0.203	-0.206	0.202	-0.208	-0.194	-0.176	-0.200	-0.145	-0.147	0.159	-0.208	-0.201	-0.223	102.0	-0.204	-0.209	-0.220	-0.192	-0.200	-0.227	0.032	0.030
	HCN PCA 191c R1 191c	8.594	0.630	8 283	8.565	8.866	8.389	8.753	8.843	8 807	8.946	8.897	9.062	8.680	8.627	8.533	8 473	8,599	8.754	8.789	8.619	8.895	8.665	8.820	8.523	8.835	8 550	8.504	8.507	8.603	8.682	8.799	8.752	8.747	8.804	9.119	8.815	8.963	8.877	8.680	8.703	8,798	8.569	8.724	8.729	8.92/	8.994	9.203	9.197	9.098	8.867	9.099	8.783	10.949
	Time	23 14:50:36.250		23 14-53-49-000	23 14:54:51.854			23 14:58:03.879	23 14(09)07,449	1/29/23 15:00:11:300	23 15:02:19.536	1/29/23 15:03:23:083	1/29/23 15:04:27,039	23 15:05:30.949		23 15:07:38.726	23 15:00:42:030 23 15:00:46:594	23 15:10:50.461				23 15:16:10:00				23 15:20:25.788		23 15-23.37.672	23 15:24-41.527	23 15:25:45.219	23 15:27:53:032	23 15:28:56.947	23 15:30:00.919	23 15:31:04.736	1/29/23 15:32:08:631	23 15:34:16.546	1/29/23 15:35:20.365	23 15:36:24.271				23 15:41:44.131				23 15:47:03:359				23 15:52:23.149			(actual)	
,	Date	11/29/23	11/20/23	11/20/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/20/	11/29/23	11/29/	11/29/	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/20/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/	11/29/23	11/29/23	11/29/	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/20/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	11/29/23	40 7%	256,850
Run 1	Spectrum	SPC_003397.LAB	SPC 003330.040	SPC_0034001AB		SPC_003402.LAB	- 1	SPC_003404.LAB	SPC_003405.LAB	SPC 003400. AB	SPC 003408.LAB	SPC_003409.LAB	SPC_003410.LAB	SPC_003411.LAB	SPC_003412.LAB	SPC_003413.LAB	SPC 0034151AB	SPC 003416.LAB		SPC_003418.LAB	SPC_003419.LAB	SPC_003424.AB		SPC_003423.LAB	SPC_003424.LAB	SPC_003425.LAB	SPC 003427.LAB	SPC_003428.LAB	SPC_003429.LAB	SPC_003430 LAB	SPC 003432 LAB	SPC_003433.LAB	SPC_003434.LAB	SPC_003435.LAB	SPC_003436.LAB	SPC_003438.LAB	SPC_003439.LAB	SPC_003440.LAB	SPC 0034421AB	1 I		SPC_003445.LAB	SPC 003447.LAB	SPC_003448.LAB	SPC003449.LAB	SPC 003451 AB	SPC_003452.LAB	SPC_003453 LAB	SPC_003454.LAB	SPC003455.LAB	SPC 003457.LAB	SPC_003458 LAB	Mill On Run 1	DSCFM

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill On

ć	>																																																								v
CO2% (40) 191	11 445	13 310	12.874	12.054	12 994	13.017	13.045	12.991	13.103	13.015	13.058	12.887	13.025	12.796	12.876	12.855	12.805	12 672	12.760	12.733	12.853	12.754	12,778	12.84/	12.814	12.762	12.863	12.840	12.777	12,844	12.770	12.729	12.938	12 709	12.770	12.820	12.576	12.726	12.579	12.470	12.353	12.149	12.290	12.264	12.236	12.152	12.219	12.179	12.267	12.054	12.151	12.116	12.146	12.198	12.642	MOSA Moisture	INSIDIA WOTA
2 H2O% (40) 1910	8 689	12.346	45.213	44.042	13.808	14,617	14.076	14,450	13.815	14.263	13.924	14.720	13.811	14.210	13.783	13.926	14,403	14.343	14.064	14.511	13.787	14.280	14.105	13,664	14.230	14.519	13.801	13.729	14,524	13.884	14.255	14.249	13.629	14.475	13.778	13.986	14.086	13.489	14.189	13.550	13.551	14.309	13.962	14.386	13.616	13.904	13.991	13.966	13.258	14.378	13,510	14.020	13,463	13.501	13.896	4	<u>?</u>
Fithlene (100 3000) 1910 H2O% (40) 1910 CO3% (40) 1910		2878	2838	2 840	2.971	2.883	2.938	2.884	2.957	2.946	2.917	2.855	2.912	2.886	2.942	2.846	2.910	2.892	2.994	2.934	3.024	2.976	2.940	2.878	3,000	3.018	3.018	2.954	3.010	3.002	3.020	3.073	3.221	3.301	3.350	3.365	3.330	3.386	3.297	3.349	3.314	3.330	3.262	3.271	3.273	3.200	3.136	3.151	3.217	3.155	3.120	3.172	3.172	3.176	3.076	3,233	370.0
SF6 (10) 1910	-0.007	-0.008	-0.007	2000	-0.007	-0.004	-0.007	-0.004	-0.008	-0.006	-0.004	-0.007	-0.008	-0.007	-0.006	-0.007	-0.00	-0.007	-0.006	-0.004	-0.007	-0.005	-0.008	0.00	90.00	-0.008	-0.007	-0.005	-0.006	-0.004	-0.008	-0.007	-0.004	0.00 400.00	-0.006	-0.007	-0.007	-0.004	-0.006	-0.004	-0.004	-0.010	0.003	0.008	-0.008	0,008	-0.003	-0.011	-0.010	-0.009	-0.00	-0.008	-0.005	-0.009	-0.007	20.012	
HF ppm (10) 1910	0.059	-0.205	0.185	-0.201	-0.213	-0.197	-0.217	-0.218	-0.215	-0.174	-0.180	-0.199	-0.189	-0.171	-0.392	-0.189	-0.135	-0.179	-0.192	-0.197	-0.226	-0.214	-0.209	-0.223	189	-0.209	-0.228	-0.214	-0.227	-0.171	-0.195	-0.195	0.191	-0.194	-0.194	-0.194	-0.177	-0.203	-0.188	-0.216	-0.209	-0.210	-0.202	-0.214	-0.212	-0.230	-0.23	-0.217	-0.225	-0.216	-0.220	-0.206	-0.212	-0.206	0.032	0.054	•
HCN PCA 1916 R1 1916	7.235	8.068	7.488	7 647	7.706	7.681	7.752	7.788	7.752	7.645	7.922	7.719	7.822	1,5,1	7.7.7	7.809	7 792	7.632	7.700	7.732	7.793	7.639	7.694	7.75	7.568	7.622	7.626	7.624	7.594	7.627	7.532	7.811	8.000	7.778	8.019	8.179	7.908	8.265	7.626	7.519	7.584	7.370	7.380	7.498	7.614	7.447	7.555	7.577	7.667	7.526	7.611	7.412	7.539	7.704	7.675	9 190	0.069
Time	30/23			_			_		1/30/23 09:29:11.312					1/50/23 (9:34:30.839	1/30/23 08:33:33:13								1/30/23 09:45:10.246	1/30/23 03:46:15.76/					1/30/23 09:53:41 109				1/30/23 09:57:56.739			•		1/30/23 10:04:20.159		-			1/30/23 10:11:47.486			1/30/23 10:14:59.247		•	•		1/30/23 10:21:22:813	•		1/30/23 10:25:38.231		11.4% (ppm,dry @/ % Oz) 44.700 (lbs/hr)	(Ibs/
Run 2 Spectrum Date	3666.LAB	LAB	003668.LAB	003669 LAB	003670.LAB	1003671.LAB	303672.LAB 1	003673.LAB 1	003674.LAB 1	103675.LAB 1		J03677.LAB 1		003691 AB 1	003660.LAB	003687.LAB	0036831AB	303684.LAB	003685.LAB 1	003686.LAB 1	303687.LAB 1	003688.LAB	SPC_0036891.AB 11/	003690.LAD	003692 ! AB 1	003693.LAB 1	303694.LAB 1	SPC_003695.LAB 11/	003697.LAB	003698.LAB 1	003699.LAB 1	003700.LAB	SPC_003/01.LAB 11/	003703.LAB 1	003704.LAB	003705.LAB 1	003706.LAB 1	SPC_003707.LAB 11/	303709.LAB	103710.LAB 1	_003711.LAB 1	03712.LAB 1	003714.LAB	003715.LAB 1	-	SPC_003/17.LAB 11/	003719.LAB 1	003720.LAB 1	003721.LAB	SPC_003722.LAB 11/ SPC_003722.LAB 11/	003724 I AB 17	003725.LAB 1	003726.LAB 1	77.LAB 1	kun 2	DSCFM 244	tons/hr) 1

Buzzi Unicern; Maryneal TX Main Stack, Raw Mill On Bung

CO2% (40) 191C	12.339	12.549	12.545	12.240	12.480	12.350	12.496	12.213	12.454	12.325	12.319	12.1/5	12.372	12.432	12.360	12.434	12.320	12.396	13.188	12.186	12.260	12 402	12 400	12.274	12.035	12.249	12.179	12.062	12.123	12.176	12.201	12.264	12.393	12.220	12.509	12.622	12,448	12.732	12.669	12.782	12./16	12.852	12.772	12.719	12.819	12,708	12.840	12.764	12.080	12.740	12.543	12.684	12.736	12.527	12.69/	12.666	12.460	12.463		M26A Moisture
Ethylene (100,3000) 191C H2O% (40) 191C CO2% (40) 191C	14.339	13,227	13.350	14.511	13.550	13.509	13.285	14.588	13.256	13.534	13.574	14.480	13.565	13.306	14.000	13.192	13.972	13.748	14.241	13.460	13 949	13 411	13.344	13.248	14.398	12.894	13.268	13.898	13.145	12.866	14,153	12.921	13.055	14.123	12.892	13.007	14.319	13.156	13.713	12.964	13.310	13.261	13.953	13.626	13.302	13.886	13.274	13.463	13.410	13.173	14.555	13.340	13.534	14.227	13.729	13.450	14,510	13.626		4 4
Ethylene (100,3000) 19	3.062	3.094	3,105	3.092	3.091	3.032	3.102	2.955	3.012	3.034	2.953	768.7	2.900	2.997	2.030	2,983	3.004	3.063	2000	2 940	3.040	2.956	3.058	2.989	2.867	2.932	2.865	2.853	2.858	2.929	2.793	2.783	2.877	2.881	2.896	2.838	2.826	2.871	2.768	2.877	2.038	2.913	2.960	2.854	2.897	2.943	3.012	2.916	2.913	2.839	2.792	2.823	2.831	2.761	2.749	2.7.30	2.649	2.915	4.954	3.603
SF6 (10) 191C	-0.005	-0.006	-0.005	-0.008	-0.004	-0.005	-0.005	0.009	-0.006	-0.008	-0.00	2000	-0.003	-0.004	0.00	0000	0000	000	800	-0.00	600 0-	-0.006	-0.006	-0.006	-0.008	-0.008	-0.006	-0.005	-0.007	9000	0000	500.0- 500.0-	-0.002	-0.011	-0.005	-0.005	-0.007	-0.006	-0.006	-0.006	600.0	0.008	-0.005	-0.004	-0.007	-0.006	-0.007	-0.003	0000	0.008	-0.006	-0.003	-0.006	-0.008	0,000	-0.004	-0.006	-0.006	0.011	-0.040
HF ppm (10) 191C	-0.199	-0.213	-0.218	-0.198	-0.217	-0.168	-0.226	-0.213	-0.201	-0.225	0.200	0.7.0	57.0	2.7.5	0.475	7.7.0	0.500	-0.5	-0.175	-0.164	-0.170	-0.159	-0.172	-0.186	-0.154	-0.194	-0.167	-0.164	-0.177	-C.168	-0.203	-0.222 -0.208	-0.220	-0.216	-0.217	-0.220	-0.203	-0.212	-0.215	-0.232	-0.220	-0.241	-0.207	-0.229	-0.237	-0.215	-0.231	-0.167	-0.100	-0.195	-0.166	-0.192	-0.166	-0.186	-0.193	0.185	-0.189	0.032	0.054	0.0002
HCN PCA 191c R1 191c	7,396	7.584	7.548	7.513	7.559	7.558	7.846	7.574	7.629	7.559	7.403	7.405	7.636	7 303	7.423	7.133	7 447	6.954	7 168	7 034	6.937	7.235	7.053	6.866	6.919	7.167	7.118	7.003	7.183	7.136	7.158	7 280	7.191	6.902	7,455	7.639	7.334	7.558	7.503	769.7	7.385	7.764	7,447	7.450	7.467	7.421	616./	087.7	7.118	7.424	7.136	7.167	7.048	1.1/3	7.210	886.9	6.925	7.308	12.419	8.703 0.067
te Time	11/30/23 10:46:06.396	11/30/23 10:47:10.302				-			11/30/23 10:54:37.561	11/30/23 10:33/41,463 11/30/23 10:66:46 407							- +-				_								11/30/23 11:16:59.489	11/30/23 11:18:03:314		- 4	. 4	•	-	_	_	- 1		11/30/23 11:28:46:645	٠,	_	_	11/30/23 11:35:05.819	Ψ-	11/30/23 11:37:13.665		11/30/23 11:38:21:416		11/30/23 11:42:33.378		4	11/30/23 11:45:44.866	1/30/23 11:46:48:116	11/30/23 11:47:33:006				7% (ppm,	(ibs/for clinker)
Run 3 Spectrum Date	3745.LAB	_003746.LAB	003747.LAB		003749.LAB	_003750.LAB	003751.LAB	003/52.LAB	003/33.LAB		003755.LAB		0037581 AB	0037501 AB	0037601 AB	0037613 48		003763.LAB	003764 LAB	003765.LAB	003766.LAB		003768.LAB	003769.LAB	003770.LAB	003771.LAB	003772.LAB	003773.LAB		0037761AB	0037771 AB	003778 I AB	003779.LAB	003780.LAB	_003781.LAB	003782.LAB	003783.LAB	003784.LAB	003785.LAB	SPC_003785.LAB 1	003788.LAB		003790.LAB					003795 LAB	003797 I AB	003798.LAB	003799.LAB	003800.LAB		003602.LAB	003804.LAB	003805.LAB	003806.LAB	Հսո 3		Clinker (tons/hr) 130

Company: Buzzi Unicem; Maryneal TX Source: Main Stack; Raw Mill Off Job ID: 23-3315 Train Type: EPA Method 26A

	5A 11/30/23 1405-1511	5B 11/30/23 1405-1511	6A 11/30/23 1539-1645	6B 11/30/23 1539-1645	7A 11/30/23 1725-1831	7B 11/30/23 1725-1831	Average
Initial Meter Volume, ft <sup>3</sup>	42.388	148.366	87.361	192.402	133.245	237.196	
Final Meter Volume, ft <sup>3</sup>	87.059	192.303	133.165	236.989	178.981	282.538	
Intra-Port Volume and/or Leak Check Correction, ft <sup>3</sup>	0.000	0.000	0.000	0.000	0.000	0.000	
Total Sample Volume, cf	44.671	43.937	45.804	44.587	45.736	45.342	45.013
DGM Calibration Factor	0.975	0.985	0.975	0.985	0.975	0.985	0.980
Average DGM Temp, F	78.0	82.3	78.1	81.3	78.1	82.3	80.0
Average DGM delta H, "H2O	1.48	1.46	1.51	1.51	1.52	1.54	1.50
Barometric Pressure, "Hg	27.43	27.43	27.43	27.43	27.43	27.43	27.43
Corrected Sample Vol, dscf	39.318	38.757	40.311	39.408	40.252	40.005	39.675
Corrected Sample Vol, dscm	1.113	1.097	1.141	1.116	1.140	1.133	1.123
Sample Volume (at Stack Conditions), acf	72.248	71.720	72.656	71.524	72.766	73.081	72.333
Sample Volume (at Stack Conditions), acm	2.046	2.031	2.057	2.025	2.061	2.069	2.048
Oxygen, %	9.7	9.7	9.9	9.9	10.0	10.0	9.9
Carbon Dioxide, %	18.2	18.2	17.9	17.9	17.8	17.8	18.0
Nitrogen, %	72.1	72.1	72.2	72.2	72.2	72.2	72.2
Stack Gas Excess Air, %	103.9	103.9	108.1	108.1	110.4	110.4	107.5
Total Moisture Catch Weight, grams	140.1	144.8	133.2	137.5	135.2	145.3	139.3
Stack Gas Moisture, %	14.4	15.0	13.5	14.1	13.7	14.6	14.2
Stack Gas Dry Molecular Weight, lb/lbmole	31.30	31.30	31.26	31.26	31.25	31.25	31.27
Stack Gas Wet Molecular Weight, lb/lbmole	29.38	29.31	29.47	29.39	29.43	29.31	29.38
Average Stack Temp, F	300.0	300.0	293.3	293.3	293.8	293.8	295.7
Stack Static (Gauge) Pressure, "H2O	-0.67	-0.67	-0.67	-0.67	-0.67	-0.67	-0.67
Stack Gas Actual Pressure, "Hg	27.38	27.38	27.38	27.38	27.38	27.38	27.38
Average Sqrt delta P *	0.822	0.822	0.838	0.838	0.835	0.835	0.832
Pitot Tube Coefficient	0.85	0.85	0.85	0.85	0.85	0.85	0.85
Stack Gas Velocity, ft/second	58.06	58.13	58.84	58.92	58.69	58.81	58.58
Nozzle Inside Diameter, inches	0.250	0.250	0.250	0.250	0.250	0.250	
Total Sample Time, min	60	60	60	60	60	60	60
Isokinetic Rate, %	101.5	100.6	100.7	99.0	101.1	101.3	100.7
Stack Dimensions	140 in. 1D	140 in. ID					
Stack Area, sq ft	106.90	106.90	106.90	106.90	106.90	106.90	106.90
Actual Stack Gas Flow Rate, acfm	372,400	372,800	377,400	377,900	376,400	377,200	375,700
Actual Stack Gas Flow Rate, acmm	10,545	10,557	10,687	10,701	10,659	10,681	10,638
Stack Gas Flow Rate, dscfm	202,700	201,500	209,400	208,200	208,200	206,500	206,100
Stack Gas Flow Rate, dscmm	5,740	5,706	5,930	5,896	5,896	5,847	5,836

Company: Buzzi Unicem; Maryneal TX Source: Main Stack; Raw Mill Off Job ID: 23-3315 Train Type: EPA Method 26A

"ND()" denotes values below detection limits

NOTE: Average INCLUDES Non-detect runs' results

		11/30/23	~		11/30/23		30-Nov	-23		30-Nov-23		30-1	00-23		20-1404-00		
		1405-151	_	_	405-1511		1539-1645	345		1539-1645		1725	725-1831		1725-1831		
Hydrogen Fluoride	Catch Wt, mg		~	) ND(	0.265	N		3	) ND	0.251	Z ~		251 )	ŊĎ	0.267	) ND(	
	Conc., mg/dscm		_	ΝĎ	0.242	N (		2	ND(	0.225	Z		220 )	) N	0.236	) ND(	
	Conc., mg/dscm @ 7% O2		_	ΝĎ	0.300	N (		0	ND(	0.284	Z		281 )	) N	0.301	) ND(	
	Conc., mg/dscm @ 12% CO2		_	N	0.159	N (		6	ND(	0.151	Z		148 )	N N	0.159	) ND(	
	Conc., ppmvd	ND( 0.263	_	N	0.290	) ND(	0.267		ND(	0.270	)QN (		0.265	N N	0.283	) ND(	
	Conc., ppmvd @ 7% O2		_	ND(	0.360	N (			ND(	0.342	Z (		338 )	ND N	0.361	) ND(	
	Conc., ppmvd @ 12% CO2		_	ΝĎ	0.192	N (		6	ND(	0.181	Z		178 )	) N	0.191	) ND(	
	Emission Rate, lb/hr		_	ΝĎ	0.182	N (		~ ~	ND(	0.175	Z		172 )	) N	0.182	) ND(	
	Clinker Rates (tph and lbs/ton)	128.90		ND	0.0014		•	0	ND	0.0014	_	•	8.90	ND N	0.0014	) ND(	
Chlorine	Catch Wt, mg	0.631			0.672		0.286	0		0.306		0	0.580		0.617		
	Conc., mg/dscm	0.567			0.613		0.25	_		0.274		0	209		0.545		
	Conc., mg/dscm @ 7% O2	0.704			0.760		0.31	2		0.346		0	649		0.694		
	Conc., mg/dscm @ 12% CO2	0.374			0.404		0.16	m		0.184		0	343		0.367		
	Conc., ppmvd	0.192			0.208		0.08	ıO		0.093		0	173		0.185		
	Absolute Difference, ppmvd (<0.2 required)				0.015					0.008					0.012		
	Conc., ppmvd @ 7% O2	0.239			0.258		0.10	_		0.118		0	220		0.236		
	Conc., ppmvd @ 12% CO2	0.127			0.137		0.05	_		0.062		0	116		0.125		
	Emission Rate, lb/hr	0.479			0.507		0.22	₹		0.239		0	452		0.477		
	Clinker Rates (tph and lbs/ton)	128.90			0.0038		128.9	0		0.0018		12	8.90		0.0036		

Company: Buzzi Unicem; Maryneal TX Source: Main Stack; Raw Mill Off Job ID: 23-3315 Train Type: EPA Method 26A

"ND()" denotes values below detection limits

NOTE: Average INCLUDES Non-detect runs' results

7B X0-Nov-23 725-1831 Average	0.267 ) ND( 0.255 0.236 ) ND( 0.227 0.301 ) ND( 0.286 0.159 ) ND( 0.152 0.283 ) ND( 0.152 0.361 ) ND( 0.273 0.191 ) ND( 0.182 0.182 ) ND( 0.175	0.517 0.515 0.460 0.694 0.578 0.457 0.367 0.158 0.109 0.126 0.109 0.126 0.105 0.477 0.438
71 30-Nc 1725-	ND( 0.02 ND( 0.02 ND( 0.03 ND(	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
7A 30-Nov-23 1725-1831	ND( 0.251 ND( 0.220 ND( 0.281 ND( 0.148 ND( 0.265 ND( 0.178 ND( 0.178	0.580 0.509 0.649 0.343 0.175 0.223 0.118 0.452
6B 30-Nov-23 1539-1645	0.251 ) (0.225 ) (0.225 ) (0.224 ) (0.270 ) (0.342 ) (0.175 ) (0.175 ) (0.0012 )	0.306 0.274 0.346 0.184 0.098 0.008 0.119 0.063 0.239
6A 30-Nov-23 1539-1645	0.253 ) ND( 0.222 ) ND( 0.280 ) ND( 0.149 ) ND( 0.267 ) ND( 0.337 ) ND( 0.179 ) ND( 0.174 ) ND( 0.174 ) ND(	0.286 0.251 0.317 0.168 0.086 0.058
30-N- 1539	N N N N N N N N N N N N N N N N N N N	
5B 11/30/23 1405-1511	ND( 0.265 ND( 0.242 ND( 0.300 ND( 0.159 ND( 0.192 ND( 0.192 ND( 0.192 ND( 0.012	0.672 0.613 0.760 0.210 0.016 0.016 0.139 0.139
5A 11/30/23 1405-1511	0.243 ) N 0.218 ) N 0.271 ) N 0.144 ) N 0.263 ) N 0.173 ) N 0.173 ) N 0.166 ) N 0.128.90	0.631 0.567 0.704 0.374 0.195 0.128 0.128 0.128
, t	02 ND( 02 ND( 5 CO2 ND( 2 ND( 202 ND( 1 lbs/ton)	02 5 CO2 mvd (<0.2 required) 2 2 5 C2 11 section
	Catch Wt, mg Conc., mg/dscm Conc., mg/dscm @ 7% O2 Conc., mg/dscm @ 12% CO2 Conc., ppmvd Conc., ppmvd @ 7% O2 Conc., ppmvd @ 12% CO2 Emission Rate, !b/hr Clinker Rates (mtph and lbs/ton)	Catch Wt, mg Conc., mg/dscm Conc., mg/dscm @ 7% O2 Conc., mg/dscm @ 12% CO2 Conc., ppmvd Absolute Difference, ppmvd (<0.2 required) Conc., ppmvd @ 7% O2 Conc., ppmvd @ 12% CO2
	Hydrogen Fluoride	Chlorine

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill Off

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4.25.25.30 4.31.40.282 4.31.40.282 4.31.40.282 4.32.43.180 4.35.55.890 4.35.55.890 4.35.55.890 4.35.55.890 4.35.55.890 4.35.55.890 4.35.50.800 4.45.115.54 4.45.30.241 4.45.50.623 4.45.50.623 4.45.50.623 4.45.50.623 4.45.50.623 4.45.50.623 4.45.50.633 4.45.50.633 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83 4.55.66.83	0.326 0.320 0.448 0.330 0.330 0.336 0.326 0.326 0.245 0.245 0.245 0.243	0.0184 0.0188 0.0188 0.0184 0.0173 0.0181 0.0183	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	3.145 3.116 3.102 3.094 3.095 3.107 3.130	15.502 14.955 15.110 15.562 15.315 15.250 15.180	14:340 14:340 14:866 14:866 14:940 14:835 14:835 14:837
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14.33.48, 100 14.33.48, 100 14.33.55, 890 14.36.59, 890 14.36.59, 890 14.39.07, 600 14.39.07, 600 14.42.19, 655 14.41.15, 482 14.42.19, 657 14.45.30, 824 14.46.34, 916 14.45.50, 628 14.45.50, 628 14.55.66, 281 14.55.66, 281 14.56.17, 348 14.56.17, 348 14	0.3478 0.313 0.314 0.326 0.326 0.326 0.326 0.236 0.245 0.245	0.1383 0.1384 0.1384 0.1384 0.1381 0.180	5.00 5.00 5.00 5.00 6.00 6.00 6.00 6.00	3.102 3.094 3.015 3.089 3.107 3.130	15.110 15.562 15.515 15.190	14.866 14.819 14.603 14.835 14.897
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4.36-55.999 4.36-59.999 4.36-59.707 4.39-07.600 4.40-11.655 4.44-13.907 4.44-13.209 4.44-13.30.001 4.44-13.30.001 4.44-13.30.001 4.44-13.30.001 4.47-13.80.13 4.47-13.80.13 4.45-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55-10.24 4.55	0.313 0.396 0.313 0.298 0.198 0.045 0.245 0.245	0.173 0.173 0.194 0.193 0.193	600.0 600.0 600.0 600.0 600.0 600.0	3.089 3.107 3.130	15.250 15.190	14.940 14.603 14.835 14.897
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14.38.03.770 14.39.07.500 14.40.11.655 14.41.15.482 14.42.19.673 14.42.23.209 14.42.23.209 14.45.30.824 14.45.30.824 14.55.50.50.570 14.55.50.234 14.55.50.234 14.55.50.234 14.55.50.234 14.55.50.234 14.55.50.234 14.55.17.848 14.55.17.848 14.55.17.848 14.55.17.848 14.55.17.848 14.55.17.848 14.55.17.848 14.55.17.848 14.55.17.848 14.55.17.848 14.55.17.848 15.00.25.563	0.100 0.326 0.298 0.198 0.245 0.245 0.282	5, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5, 5	0.00 0.00 0.00 0.00 0.00 0.00 0.00	3.130	15.180	14.897
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1445:31.061 1447:38.061 1447:38.024 1449:46.618 1449:46.618 1450:55.02 1450:62.24 1450:62.20 1450:62.20 1450:17.84 1456:17.848 1456:17.848 1456:17.848 1450:17.848 1450:17.848	0.282	-0.183	-0.006	3.091	15,417	14.732
14:46:34.916 14:7:38.824 14:49:46.618 14:49:46.618 14:50:50.570 14:51:54.426 14:55:66.281 14:55:66.281 14:55:66.281 14:55:10.104 14:55:11.788 14:50:12.816 15:00:23.365 15:00:23.365	0.230	-0.186	-0.010	3.012	15.105	14.831
14447.38.824 14484.27.78 144946.678 1450.50.570 1450.50.524 14.55.06.281 14.55.06.281 14.55.01.288 14.56.10.104 14.55.17.848 14.56.17.848 14.50.1.288 14.50.1.288 15.00.25.53		-0.189	600.0-	3.029	15.001	14.947
14-48-42.78 14-49-46.61 14-50-50.570 14-50-56.370 14-55-66.281 14-55-06.281 14-55-10.104 14-57-14.288 14-58-17.388 14-58-17.388 14-58-17.388 14-58-17.388 14-58-17.388 14-58-17.388 14-58-17.388 14-58-17.388 14-58-17.388 14-58-17.388 14-58-17.388 14-58-17.388 14-58-17.388	10.360	-0.190	-0.008	3.070	15.013	14.807
H44946618 H45950570 H4515428 H45268.382 H45506.281 H45506.281 H45817.014 H45817.848 H45817.848 H45817.848 H45817.848 H45817.848 H45817.846 H45817.846 H45817.846	10.319	-0.189	-0.008	2.996	15.236	14.868
14:50:50.570 14:51:54.426 14:52:63.82 14:55:06.281 14:55:06.281 14:57:14.298 14:57:14.298 14:59:27.381 15:00:25.653 15:07:29.688	10.282	-0.190	-0.010	3.001	14.946	14.878
1451:54.426 14:52:58.382 14:54:02.241 14:55:10.104 14:55:10.104 14:55:10.104 14:52:21.816 14:59:21.816 15:00:25.663 15:01:29.686	10.318	-0.186	-0.010	3.148	15.152	14.861
14:52:63.382 14:54:02.241 14:55:06.281 14:56:10.104 14:57:14.298 14:58:17.848 14:59:27.381 15:00:28:683 15:00:28:683 15:00:23:565	10.298	-0.197	600'0-	3.143	15.217	14,768
14:54:02.24 14:55:06.281 14:55:06.281 14:56:10.104 14:57:14.298 14:59:21.816 15:00:28.668 15:01:29.668 15:01:29.668	10.527	-0.180	-0.014	3.214	15.235	14.809
14:55:06.281 14:55:10.104 14:57:14.298 14:59:21.816 15:00:25.653 15:01:29.688 15:01:29.688	10.476	-0.189	-0.008	3.167	15.011	14,947
14:55:10.104 14:57:14.298 14:59:21.816 15:00:25.663 15:01:29.688 15:01:29.688	10.632	-0.185	-0.008	3.100	14.942	14.973
1455/14.298 14:58:17.848 14:59:21.816 15:00:25.853 15:01:29.868 15:03:35.853	10.525	-0.205	-0.011	3.208	14.899	15.101
14:58:17,848 14:59:21,816 15:00:25,653 15:01:29,668	10.446	-0.177	210.0-	3.128	15.196	14.880
15:00:25.653 15:00:25.653 15:01:29.668 15:02:33.505	10.250	0.200	0.00	3.225	15.114	14.842
15:01:29:668 15:02:33:505	2.337	-0.203	- 800 000 000 000 000 000 000 000 000 000	3.048	15.148	14.750
15:02:33.505	0.441	0 173	0.010	2 954	14 943	14.860
45:00:04	0.531	-0.182	-0.010	3.058	14.827	14.799
1/30/23 15:03:3/.361	10,589	-0.187	-0.008	3.041	15.016	14.820
15:04:41.368	10.463	-0.184	-0.012	2.991	14,959	14.709
15:05:45.202	10.697	-0.231	-0.012	2.986	15.176	14.973
15:06:49.416	0.516	-0.229	-0.010	3.043	15.223	14.910
15:08:07:985	10.424	-0.187	-0.008	3.062	14.959	14.830
11/30/23 15:09:11.851	0.606	-0.195	0.010	3.034	14.878	14.793
15:10:10:70:789	10.483	-0.230	010.0	3.052	14.903 204.446	14.853
(actual)	0.384	0.032	600.0-	3.145	15.165	14.866
, 02)	15.108 <	0.047	-0.014	4.576		
(lbs/hr)	0.352 <	0.024	-0.051	3.254	14.7	M26A Moisture
(lbs/ton clinker)	> 080	0.0002				

COC2%(40) 19
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1 9.9% 208,800 128.90 Buzzi Unicem; Maryneal TX Main Stack, Raw Mill Off Run 2 Spectrum

Spectrum

SpC\_004013.LA8

SPC\_00402.LA8

SPC\_00402.LA8

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SPC\_00402.LA8

SPC\_00403.LA8

SPC\_00403.LA8 Oxygen DSCFM Clinker (tons/hr)

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill Off

Run 3	Ose Ose Time	HCN PCA 1912 R1 1912	HE pom (10) 191C. SER	SER (10) 1910 Eth.	Phylone (100 2000) 104 Oct. Oct. (000)	770% /40) 1910	CO2% (40) 1810	
SPC_004118.LAB	11/30/23 17:26:09.022	10.517			3.276	14.933	14.473	
	11/30/23 17:27:12.780	10.549		-0.008	3.210	14.588	14.725	
	11/30/23 17:28:16:733	10.734	-0.241	0.009	3.220	14.704	14.6/4	
SPC 004122.LAB	11/30/23 17:30:24.453	10.611	-0.237	600.0-	3.293	14.866	14.580	
SPC_004123.LAB		10.873	-0.257	-0.008	3.229	14.558	14.705	
SPC 004124 AB		10.763	-0.246	-0.008	3.185	14.530	14.732	
SPC 004125.LAB	11/30/23 17:33:36.161	10.527		0.009	3.263	14.955	14.614	
SPC 004127.LAB		10.628	-0.252	0.011	3.182	14.391	14.733	
SPC_004128.LAB		10.788		-0.009	3.167	14,765	14.818	
SPC_004129.LAB	11/30/23 17:37:51.777	10.578	-0.241	-0.009	3.236	14.712	14.901	
SPC_004130.LAB	11/30/23 17:38:55.678	10.358		600.0-	3.378	14.988	14.579	
SPC_004131.LAB	11/30/23 17:39:59:580	10.293	-0.393	-0.009	3.368	14.906	14.539	
SPC 004133.LAB	11/30/23 17:42:07:595	10.584	-0.237	-0.00%	3.274	15.011	14.540	
SPC_0041341.AB	11/30/23 17:43:11.290	10.699		-0.007	3.262	14,491	14.691	
SPC_004135.LAB		10.431	-0.255	-0.008	3.233	14.868	14.636	
SPC_004136.LAB	11/30/23 17:45:19:096	10.514		-0.008	3.209	14.493	14.676	
SPC 004138.LAB		10.585	-0.204	-0.008	3.172	14.307	14.578	
SPC 004139.LAB		10.564		-0.009	3.051	15.012	14.525	
SPC_004140.LAB		10.548		-0.010	3.075	14.573	14.678	
SPC_004141.LAB	11/30/23 17:50:38.626	10.244		-0.008	3.229	14.941	14.579	
SPC 004143.LAB	11/30/23 17:52:46.426	10.116	-0.245	-0.010	3.280	14.821	14.468	
SPC_004144.LAB	11/30/23 17:53:50.521	10.485		-0.009	3.269	14.648	14.579	
SPC_004145.LAB		10.541		-0.006	3.245	14.697	14.593	
SPC_004146.LAB		10.558		-0.009	3.203	14.838	14.593	
SPC 004147.LAB	11/30/23 17:57:02:225	10.404		-0.008	3.286	14.980	14.414	
SPC 004149.LAB		10.405	-0.256	-0.009	3.293	14,832	14.572	
SPC_004150.LAB		10.384		-0.008	3.275	14.569	14.662	
SPC_004151.LAB		10.186		-0.008	3.350	15.102	14.622	
SPC_004152.LAB	11/30/23 18:02:21.552	10.296	-0.231	5000	3.332	14.519	14,642	
SPC_004154.LAB		10.112		-0.010	3.253	15.734	14.523	
SPC_004155.LAB	11/30/23	10.248		-0.010	3.307	14.929	14.713	
SPC_004156.LAB	11/30/23	10.432		-0.008	3,397	14.654	14.673	
SPC_004157.LAB	11/30/23 18:07:41.071	10.205	-0.237	-0.010	3.351	15.142	14.510	
SPC 004159.LAB	11/30/23	10.140		-0.007	3.313	14.675	14.656	
SPC 004160.LAB	•	10.399		-0.009	3.182	15.002	14.582	
SPC_004161.LAB	11/30/23 18:11:56.684	10.378	-0.229	-0.009	3.197	14.720	14.603	
SPC_0041631AB	11/30/23 18:14:04:490	10.303		-0.00%	3.103	14.398	14.612	
SPC_004164.LAB	•	10.250	-0.240	-0.011	3.229	14.724	14.676	
SPC_004165.LAB		10.429	-0.247	0.010	3.109	15.036	14.472	
SPC 004167.LAB	11/30/23 18:17:16:308	10.520		-0.00e	3.239	15.098	14.546	
SPC 004168.LAB	•	10.351	-0.247	-0.008	3.095	15.108	14.556	
SPC_004169.LAB	-	10.274	-0.249	-0.009	3.054	14.813	14.565	
SPC 0041711 AB	11/30/23 18:21:31.896	9.999	-0.244	-0.00/	3.210	14.584	14.620	
SPC 004172.LAB		10.145		-0.005	3.122	14.533	14.763	
SPC_004173.LAB		10.289	-0.246	-0.009	3.040	14.664	14.625	
SPC_0041/4.LAB	11/30/23 18:25:47.772	10.239	-0.251	-0.008	3.073	14.624	14.580	
1	•	10.296	-0.215	-0.006	3.001	14.670	14.523	
SPC_004177.LAB	•	10.222	-0.209	-0.010	3.093	15.188	14.477	
ı	-	10.323	-0.245	-0.007	3.046	14.659	14.748	
SPC_0041791.AB	11/30/23 18:31:07.393	10.394	-0.189	900.0-	3.109	14.757	14.556	
Oxygen	(mdd)	•	< 0.048	-0.013	4.779			
DSCFM	207,350 (lbs/hr)	•	< 0.024	-0.047	3.394	14.2	M26A Moisture	
Clinker (tons/hr)	128.90 (Ibs/ton clinker)	0.082	4.UU02					

Appendix B

Field Data and CEM/FTIR Data

# EPA Method 1 Traverse Point Location for Circular Ducts

Plant	Lone	Star Industries			Exam	pl	e For	
City	Maryn	eal	State	TX			ax	
Location		Main Kiln Stack			1	٦	Downstream	
Stack ID (	inches)	140						See Report Text
Nipple Le	ngth	6.25				•	Port Level	For Figure of Location
Nearest U	pstream	Disturbance (Bend	, ID FAN, etc)					
Distance (	(inches)	1893 T	ype of Disturbance		1 1	ļ		
Nearest D	ownstre	am Disturbance (Be	end, or Stack Out	let)	<u> </u>	,	Upstream	
Distance (	(inches)	579 T	ype of Disturbance					
Sampler		SCS D	pate 11/28/23		F Dins	iow ectio		
(Mark with a	ın "x")	ļ			Stack Sche	mai	ic (Draw by hand a	fter printing)
Particulat	e Traver	se? x	Yes	No				
						1		
Number o	f Travers	se Points Required	6					

Traverse Point	Fraction of Stack	Stack ID	Diameter Frac.	Nipple Length	Traverse Point Distance
Number	Internal Diam.	(Inches)	Stack ID	(Inches)	from outside Nipple
1	0.044	140	6.16	6.25	12 3/8 in.
2	0.146	140	20.44	6.25	26 3/4 in.
3	0.296	140	41.44	6.25	47 3/4 in.
4	0.704	140	98.56	6.25	104 3/4 in.
5	0.854	140	119.56	6.25	125 3/4 in.
6	0.956	140	133.84	6.25	140 1/8 in.
					-
					-

#### Cyclonic Flow Check Data Sheet

PLAN	T AND CITY		DATE,	SAMPLIN	G LOCATION		SAMPLE:	TYPE	RUN N	JMBER
Bug	1 May	neel TX	11/24/23	M	in Mac	k	Cyclonic Flo	w Check		
OPERATO	Barometric Pressure (Pb (In, Hg)	STATIC PRESS (in, H2O)	AMBIENT TEMP (deg. F)	STACK ID (In.)	PITOT Cp	DGM BOX No.	DGM delta H@	DGM CAL FACTOR (gamma)		PROBE ID NO
WYGM	77.32	40.67	50	MO	७.४५	M5.15	NA	NA		5B

#### EPA Method 2 Data

Run Time (24 hr)	Traverse Port Point	Pitot Delta P READING "H2O	STACK TEMP deg F	Absolute Angle at null (0) Delta P READING " H2O
	AL	0,90	241	- 5
	<u> </u>	0.95	249	3
	10	, ,	522	13
	2	1.0	243	4
	3	0.95	244	4
	î	(,0	742	2
	2	12.96	243	4
	3	0.90	240	.3
	01	0,98	240	5
	3	1.0	241	<u> </u>
Pitot Leak (	 Check			
Averages				

Average of Absolute Angle Readings must be < 20 degrees

		NOZZLE ER DIAMETER		K FACTOR	157	SAMPLE		E .	,	45	É			8	S	؈			9	7	e			Ø	B	5			
1 of 1	MOINIDER	NUMBER	,250	CONTENT %	3/3 5 31	6.	Sil Gel EXIT	(deg. F)	61		52			5.6	57	28			28	35	جر ه			57	50	50			
PAGE 1 of		NGTH TYPE	Fret:VC	O2 CONTENT	11 0/0	FII TER	OVEN	(deg. F)	246	3176	255			250	240	255			122	ੈ <del>/72</del>	252			252	757	452			<b>-</b>
JON OF	177	PROBE LENGTH AND LINER TYPE	9 2010 FT	CHECK (FINAL)	.00/ CU, FT	MOU	IN / OUT	(deg. F)	6.8	70	20			69	70	17			67	12	69			83	10	Ĩ.		AVE. TEMP.	
SAMO	SAIVITE	PITOT CP %	6.55 0,84	CHECK (INITIAL)	<u>⊢</u> 0	2	STACK	(deg. F)	5170	17176	682		INCHES HE	245	245	245		INCHES Hg	243	242	238		INCHES Hg	852	21:12	245		AVE. TEMP.	
ğ	20	STACK ID (In.)	140.00"	ORSAT NO.	EALED FAILED	7117	PROBE	(deg. F)	253	254	256		CU.FT @	255	255	256		000	156	255	253		/ @1	256	122	255			
	SAMPLING LOCATION	FILTER	XX	STACK PITOT NO.	SASSEN	MOOFE	delta H ORIFICE		1.2	2.2	2.2		+	. <b>6</b>	2,3	7.7		CU.FT @	5.0	2.3	2.7		CU.FT @	124	2.6	2.6		- AVE delta H	
A SHEET	SAINIFL	AMBIENT TEMP (dea. F)	2015	STACK THERM NO.	5 A	della D	VELOCITY	(In. H20)	0.90	20.0	0.93	End of Port	LEAK RATE:	2:	7.57	0.90	End of Port	LEAK RATE	176:0	9 9	24.9	End of Port	LEAK RATE:	0-1			End of Port	AVE SQRT delta P	
METHOD 26A FIELD DATA S	UNIC.	STATIC PRESSURE (in. Water)	1001	DGM CAL FACTOR (Y)	DITOT I FAK CHECK>		DGM	Vm (cu. ft.)	350,008	11,298	370.61	875.079	PT.0.27	975.079	930.19	934.98	199.5H	939.319	939319	993.34	398, 19	902.713	902,718	962.718	44.500	912.34	217.716	DGM	
D 26A		-0-	ATT 33	DGM H@	1.63		CLOCK TIMF	(24-HR)	1450			15 1505	100	1507	-		1522	ITIAL	762	1_		1539	INITIAL	11241			1556		_
METHC	-  ³ 		51.33	DGM BOX No.	M4-15	FLADSED	TEST	NIN)	0	5	10	15	AK CHECK? SU. FT)	15	20	25	30	AK CHECK? CU. FT)	30	35	40	45	AK CHECK? CU. FT)	45	50	55	09	TOTAL	60 Min.
	FLAN	OPERATOR		ASSUMED MOISTURE 1 (%)				Ö	A-1	2	က		INTRA-PORT L <u>EAK CHECK?</u> DGM VOLUME (CU. FT)	B-1	2	8		INTRA-PORT LEAK CHECK?  DGM VOLUME (CU. FT)  F	C-7	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)	D-1	2	3			

PlantSample Local Run No Filter Numbe	A ON	Mary Jain S Lain S -M2 Not Applicab	Aach 6A-TA	X,	Reco	ole Date 11 overy Date 16 overed by	1 29 /23		
			MO	ISTURE					
Impingers	l 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (knockout)	2 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	4 Optional Knockout (untipped)	5 100 ml 0.1N NaOH (untipped)	6 100 ml 0.1N NaOH (untipped)	Silica gel		
Final weight	/	842.4	784.5	648.9	757.4	742.9	920.6	g	
Initial weight		737.5	758.1	643.2	747.9	741.0	907.7	g	
Net weight		1049	26.4	5.7	3.5	1,9	12,9	g	
Description o	of impinger v	water	<u>Cle</u>		Total moist	$\frac{28}{3}$	W s	speril gel	l colo
		]	RECOVE	RED SA	MPLE				
H <sub>2</sub> SO <sub>4</sub> Imping container no.	ers and knoc	kout contents	and water rin	nse	====3)	Liquid le		/ · /	
NaOH Imping container no.	ers contents:	and water ring -M26A-I	se NaOH 13	•		Liquid le			
Samples store	d and locked							=	

		ZLE DIAMETER	K FACTOR	2.38	CAMBIE	TRAIN VAC	م. ع	প	3			- 1	0,	27	n			1	~ \	2	N			и	,	~	2				
1 of 1	I WOINIDER I	NUMBER 3.5%	CONTENT	او.۲		Sil Gel EXI	55	53	hS			141	24	24	Z.			XI.	£4	25	26			3	2.1	5.3	4.4				
PAGE 1 of	NO.	ENGTH ER TYPE	CONTENT	% =	EN TED	OVEN TEMP	746	349	Shd			Ġ	950	929	252				260	956	928			100	300	200	258				
- GA	17	PROBE LENGTH AND LINER TYPE	CHECK	Sol o	@ H	N/OUT TEMP	1. A.	43	4			011	70	73	44			c	43	£.	43			1010	6	i S	1		AVE. TEMP		
- T	M26A	PITOT Cp	C.47 0.84 LEAK CHECK	INITIAL)	£,	STACK	343	244	239		INCHES Hg	INCHES Hg	345	345	348		INCHES Hg	INCHES Hg	243	342	328		INCHES Hg	INCHES HE	Q >9	617	3HS		AVE. TEMP.		
		STACK ID (In.)	140.60 ORSAT	1	2	PROBE TEMP	256	256	256		0	00	456	963	\$2		@		16	\$7 7	35.5		8	3	3HG	3ME	She				
	NG LOCATION	FILTER	STACK PITOT	Ö	ASSED	delta H ORIFICE	) . ( 2) . (	. ct	c.		CU.FT @	1	6.	<u>ئ</u>	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		CU.FT @	- 1	Ç	8.3	2:3		CULFT	- 11	4.6	ع.ه	g.6		AVE delta H		
A SHEE	SAMPLI	AMBIENT TEMP (deg. F)	> 40 STACK THERM	NO.	FCK >	VELOCITY HEAD	(III. FZU)	6.	, 43	<b>End of Port</b>	LEAK RATE:		ب به	£	<b>9</b> 6.	End of Port	LEAK RATE:		Ţ	20	6.	End of Port	LEAK RATE:	,	0, 1	1.1	1.1	End of Port	AVE SQRT		
METHOD 26A FIELD DATA SH	1 24 (23	STATIC PRESSURE (in. Water)	DGM CAL	OR (Y)	EAK CH	DGM	04) 583	974 33		982.935			989.935	985.91	990.68	995.641			995.641	व्यवन स	1005.57	1009.782		- 11	1014 54	(0145x3	1030.08	1835.134	DGM VOLIME	1025.334	
D 26A	I Call Town	AMBIENT PRESS (In Ha)	24 32 DGM H@			CLOCK	_	_		15.08	INITIAL	FINAL	15.04	_		15:22	INITIAL	FINAL	15:04			45 18:38	INITIAL	щL	7.5		10	95,3			1
METHC	PLANI AND CITY	OR	M.W.U. DGM E BOX No.	MY - 21		ELAPSED TEST TIME	(MIIM)	טרט	10	15	EAK CHECK? (CU. FT)		15	20	25	30	EAK CHECK? (CU. FT)	,	30	35	40	45	EAK CHECK? (CU. FT)		45	20	55	09	TOTAL	60 Min.	
	PLAN	OPERATOR	ASSUMED MOISTURE	(%)		TRAVERSE PORT/ A /POINT	_	2	r (C)		INTRA-PORT LEAK CHECK? DGM.VOLUME (CU. FT)	,	B-1	2	3	8	INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		C-1	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		D-1	2	3				

Sample Locat Run No	tion Ma	Star -M2		_	Reco	very Date//	129/23	<u>-</u>							
			<u>MO</u>	<u>ISTURE</u>				1							
Impingers	1 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub>	2 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	4 Optional Knockout (untipped)	5 100 ml 0.1N NaOH (untipped)	6 100 ml 0.1N NaOH (untipped)	Silica gel								
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$															
	Recovery Date														
	Recovery Date														
Description o	(knockout)         (tipped)         (tipped)         (untipped)         (untipped)         (untipped)         (untipped)           Final weight         845.7         789.8         615.1         740.0         740.8         912.3         g           Initial weight         749.9         747.1         611.9         734.9         738.1         899.1         g           Net weight         95.8         42.7         3.2         5.1         2.7         13.2         g           Description of impinger water         Clean         350.0         Sil gel constitution         Sil gel constitution														
		]	RECOVE	RED SA	<b>MPLE</b>										
H <sub>2</sub> SO <sub>4</sub> Imping container no.	ers and knocl	cout contents	and water rin	<u>ise</u>											
NaOH Imping container no.				S		Liquid lev marked/se									
Samples store	d and locked							<u>.</u>							

Run Z Aborted Problem Process

		715	DIAMET	100	K FACT	78.2		SAMPL	(in. Fg	7	4	7			17	7															
<del>-</del>	NUMBER	NO77	NUMBER		- Laure	_	6.5	Sil Gel EXIT	(deg. F)	57	5,6	25	WHI IN		26									The State of the S							
PAGE 1 of	RUN NUMBER	2A ON	RTYPE		CONTENT			PILTER OVEN TEMP	(deg. F)	652	256	252			130	000								1 -1 -1 -1							
	TYPE	PROBE	AND LINER TYPE		CHECK	CU. FT	@	IN / OUT	(deg. F)	و و	50)	67			6.7	900		The same												AVE.	
	SAMPLE TYPE	M26A PITOT	පි	0.84	CHECK	0.00/ CU.FT	@_ (Чпнд	STACK	(deg. F)	21/2	2118	763		INCHES HG	7110	2			NCHES Ha	INCHES Hg					INCHES Hg	- INCIDES FIG				AVE.	
	NOI	STACK		071	ORSAT		FAILED	PROBE	(deg. F)	254	754	452		001	2576				(e) L	0					86	3)					
<u> </u>	SAMPLING LOCATION	FILTER	NUMBERS		STACK PITOT		PASSED	delta H ORIFICE	(In. H2O)	23	2.6	2.H		CU.FT @	-ci	22			CU.F	CU.FT					CU.FT @				DESCRIPTION OF	AVE delta H	
A	SAMPL	AMBIENT	TEMP (deg. F)	50	STACK THERM NO		Ol	VELOCITY HEAD	(In. H20)	1.7	- 1	0,	End of Port	LEAK RATE:	6.90	8.93		End of Port	LEAK RATE:					<b>End of Port</b>	LEAK RATE:				End of Port	AVE SQRT delta P	
METHOD 26A FIELD DAT	DATE	STATIC	PRESSURE (in. Water)	200	DGM CAL FACTOR (Y)	0.975	PIIOI LEAK CH	DGM	Vm (cu. ft.)	598,710	07379		C33 085	933.685	933.085												-			DGM	
<b>JD 26A</b>		AMBIENT	PRESS (In. Hg)	2522	H@W	1.63		CLOCK	_	23.9			16.35	INITIAL	1691				INITIAL	FINAL					INITIAL						
	2	-		なごう		W5-15	I EL ABOED	TEST			3	2	15	(CU. FT)	15	20	25	30	(CU. FT)		30	35	40	45	EAK CHECK? (CU. FT)	45	50	55	09	TOTAL	60 Min.
	PLAN	OPERATOR		20	ASSUMED MOISTURE (%)	2	TPAVEDOE	PORT/ /POINT	S. S.	H-T	2 2	2	TO CO	DGM VOLUME (CU. FT)	B-1	2	3		INTRA-PURT LEAK CHECK?  DGM VOLUME (CU. FT)		<u>-</u>	2	က		DGM VOLUME (CU. FT)	D-1	2	3			

		ZLE DIAMETER	CA 2520 K FACTOR	2.5.2	SAMPLE TRAIN VAC	(in. Hg)		ي(			r	7	7	State of State of		<b> </b>	7				B.	<b>6</b>	r			
1 MEER	6NJ	NOZZI NUMBER DI	CONTENT	6.5	Sil Gel EXITEMP	(deg. F)	200	48			30	10	is			hS	24	\$5			E	29	29			
PAGE 1 of 1	8A 6	3TH YPE	CONTENT	0/	PILTER OVEN	(deg. F)	25.7	256			752	253	250	To the last of the		283	823	1752			<b>122</b>	288	35.5			7
I VOE			CHECK	60 CU. FT	IN DGM	(deg. F)	S L	59			09	29	63			9	63	64			79	2	179		AVE. TEMP.	
			CHECK	(10   CU. FT	STAC	(deg. F)	762	192		INCHES Hg	262	062	202		INCHES Hg	263	263	55		INCHES Hg INCHES Hg	260	202	261		AVE. TEMP.	
Š	200	STACK ID (In.)	ORSAT	EACKING.	PROBE	(deg. F)	263	282		CU.FT @	h52	452	253		CU.FT @	253	752	257		CU.FT @	255	255	25.7			_
	MAGING COCATION	FILTER NUMBERS	STACK PITOT	NO. βαξάΕΝ		_	0,0	8.1		+	2.3	2.2	21		+	76	2.3	c,	1	+	4.3	2.3	272		T AVE delta H	
A SHEE	MAN	AMBIENT TEMP (deg. F)	STACK THERM	_ ~	delta P VELOCITY	(In. H20)	98.0 18.4	97.0	End of Port	LEAK RATE:	36.0	8,93	68.0	End of Port	LEAK RATE:	0,1	0.98	96.0	End of Port	LEAK RATE:	960	0.95	9.9H	End of Port	AVE SQRT delta P	
METHOD 26A FIELD DATA SI	-	STATIC PRESSURE (in. Water)	- 0.67 DGM CAL	O.975 DITOT FAKCHE	DGM	Vm (cu. ft.)	936,456	विनान विक	948,941		176.846	953.45	957.91	962.175		25.7 1.76	4 -	T0.1170	975.464		475.464	19.080	CR4.33	989 Jus	VOLUME	
DD 26A	MENTINES IX	AMBÍEŇT PRESS (In. Ha)	100000000000000000000000000000000000000	891	CLOCK	(24-HR)	0 CP C	10	15 1755	INITIAL	15/0987	20	25	0 0952	INITIAL	30 0854	35	40	5 1009	INITIAL	45 10 11	50	55	9201 09		7
METH	$\exists$	11,350	DGM BOX No.	M5-15	山	(MIN)				CU. FT)			2	3	EAK CHECK? (CU. FT)				4	LEAK CHECKS E (CU. FT)	4			9	TOTAL	60 Min.
	Ruzz: La	OPERATOR	ASSUMED I	(%)	TRAVERSE PORT/	NO.	A-1	7 8		INTRA-PORT L <u>EAK CHECK?</u> DGM VOLUME (CU. FT)	B-1	2	m		INTRA-PORT LEAK CHECK?  DGM VOLUME (CU. FT)  EINAL	7	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)	D-1	2	3			

PlantV Sample Loca Run No Filter Numbe	MN	Mais	stage Stage 26A-3A	<u> </u>	Reco	ple Date <u>lea</u> overy Date ut overed by	1 30/23	<u>.</u>	
			MC	<u>ISTURE</u>					
Impingers	1 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (knockout)	2 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	4 Optional Knockout (untipped)	5 100 ml 0.1N NaOH (untipped)	6 100 ml 0.1N NaOH (untipped)	Silica gel		
Final weight		831.8	812.3	652.5	759.7	731.0	934.1	g	
Initial weight		749.2	750.2	648.8	758.1	730.4	920.6	g	
Net weight								g	
Description o	of impinger v	vater	elea		Total moistu	50 	v S	spe il ge grar	l col
		ļ	RECOVE	RED SA	<b>MPLE</b>				
H <sub>2</sub> SO <sub>4</sub> Imping container no.	ers and knock	cout contents -M26A-H	and water rir	ise		Liquid lev marked/se			
NaOH Imping container no.	ers contents a	and water rins -M26A-N	se NaOH 3/			Liquid lev marked/se			
Samples stored	d and locked								

		ZLE		ZSO KEACTOR	YO LOW LA	B-38	SAMPLE	TRAIN	(in. Hg)	0	~~	5			~		No	\$			6	- II	20	^			3	ž	3					
1	ACINIDINIDERA A K	NI IMBER I DIA	752		CONTENT	16.5		Sil Gel EXII TEMP	(deg. F)	8	15	21			100	\ \ \{	23	44			1	2	22	3.5			53	24	200					
PAGE 1 of	KON	NGTH Y		Le m	CONTENT	=	FILTER	OVEN	(deg. F)	ક્રિક	250	426			200	454	22	SS.			6	\$53	953	3.4			754	259	カボル					
	YPE	PROBE LENG		24.	CHECK -	Boot OL	DGM Hg	IN / OUT	(deg. F)	25	2,	20			, ,	و و	19	53			4	6,9	50	63			77	100	1,7	2	AVE	TEMP.		
	SAMPLE	PITOT	90	0,520,84	CHECK (NITIAL)	DON CU. FT	9 BH.	STACK	(deg. F)	Page	406	261		INCHES Hg	INCHES HG	28.7	263	3,9%		INCHES Hg	INCHES Hg	K61	FF.	7	A Charles	INCHES Hg	7,0	260	1300	700	2/1/6	TEMP.		
		STACK	)		ORSAT	4		PROBE	(deg. F)	357	र्भुष	358		@		253	<b>453</b>	SS		0	l l	353	346	843		86	2 18 12	122	25.6	7.7			44.	G
_	NG LOCATION	ATTER I		NA	PITOT	50	ASSED	delta H ORIFICE	(In. H20)	2.0	3.0	8.1		CU.FT @	CU.F.	<del>ر</del> در	ج د	<del>[</del> 6		CU.FT @	11	A.4	7		S TOWER THE PERSON	CU.FT.®	77	ہے۔ ص	200	4		delta H		
오	SAMPLING	AMBIENT	(deg. F)	1 2%	STACK	W	^ C	VELOCITY	(In. H2O)	8	,8 <sub>4</sub>	2%	<b>End of Port</b>	LEAK RATE:		. 95	. બે ૩	b\$:	End of Port	LEAK RATE:		- 1	6	9	End of Port	LEAK RATE:	9	α \u	200	MIN 26 DOM	End of Port	AVE SOR		
FIELD DATA		1.5		64	DGM CAL FACTOR (V)	988	TOT LEAK CHE	DGM	0	43.146	4F . 33	51.34	55:33/			55, 33\	59.46	63.86	66. 18b			931 35 B	गुर्गा	Th.84	61.340		41 91. N	ا		2000	75, 117	DGM		
		AMBIENT	(Fr. Ha)	37.43	DGM H@	1.69	-	CLOCK	(24-HR)	9:30			56.16	INITIAL	FINAL	9.34			9:58	INITIA	FINAL	4.54			10:09	INITIAL	<u> </u>	10:11			0.00			1
METHOD 26A	<b>WCITY</b>	michm		March	DGM BOX No.	র	0.00	TEST	(MIN)	0	5	10	15	AK CHECK? CU. FT)	,	15	20	25	30	CH ET)		30	35	40	45	CU. FT)		45	20	55	09	TOTAL	60 Min.	
	PLANT	OPERATOR		TABL	MED	13%			NO.	A-1	2	8		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		B-1	2	က		INTRA-PORT LEAK CHECK?	DGINI VOLOINIE	5	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		0-1	2	က				Ē

Plant Sample Locar Run No Filter Number	MNC	Mary Mas -M2 Not Applicat	neal Stack CGA- 313		Reco	ole Date Ct / very Date Ct vered by	1 30 123	
			782.2 <u>mo</u>	ISTURE				
Impingers	1 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub>	2 100 ml / 0.1N H <sub>2</sub> SO <sub>4</sub>	13 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub>	4 Optional Knockout	5 100 ml 0.1N NaOH	6 100 ml 0.1N NaOH (untipped)	Silica gel	
Final weight	(knockout) /	(tipped)	(tipped)	(untipped)	(untipped)	747.0	925.1	g
Initial weight		755.0V	747.7	613.L	7459	7460	912.1	g
Net weight		110,3	35.2	2.3	2.9	40	13.0	g
Description o	lof impinger v	water <sub>=</sub>	cle		Fotal moistu			spent il gel colo grams
		]	RECOVE	RED SAI	MPLE			
H <sub>2</sub> SO <sub>4</sub> Imping container no.	ers and knock	cout contents -M26A-H	and water rin	ise 3	<del>.</del>	Liquid lev marked/se		
NaOH Imping container no.	ers contents a	and water rins	se NaOH 3	ß	#	Liquid lev marked/se		
Samples store	d and locked	v						š

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	1	NOZZLE JER DIAMETER	8521			S	KAIN		h	6	7			V	2)	Λ,	۵	The same of the sa		,	9 (	o.	و			7	7	٢		323			
1 NUMBER		NUMBER	3. 25	CONTENT	5 N		Sil Gel EXI	(deg. F)	25	56	8			0	9	24	9				ق	9	63			09	ق	63					
PAGE 1 of 1 RUN NUMBER	4A ON	NGIH X TYPE	362	O2 CONTENT	-	FILTER	OVEN	(deg. F)	222	2000	255			11-00	7 62	254	154			2	256	050	152			152	222	25.6				7	
YPF		AND LINER TYPE	51 gle	CHECK (FINAL)	# 100 CU. FT	DGM	IN/OUT	(deg. F)	9	୧୬	en			Į,	e e	27	6				9	7,0	0			20	2	69		AVE	TEMP.		
SAMPLE	M26A	PITOT Cp	0,84	CHECK (INITIAL)	. 00 CU. FT		STACK	(deg. F)	192	202	197		INCHES Hg	INCHES Hg	26.6	262	261		INCHES Hg	INCHES Hg	261	262	292		INCHES HE	600	100	000	2002	AVE	TEMP.		
NOL	2	STACK ID	041	ORSAT NO.	PAINED	1.7%	PROBE	(deg. F)	n52	25%	256		CU.FT @	1	220	157	284		CU.FT.@	0 1	252	256	223		CU.FT.®	065	מבח	0.50				7	
T	5	FILTER	N/A	STACK PITOT	NACKED I	USOF D	delta H	(In. H2O)	0,2	2,1	6.		\		7.7	2.7	2.1		COL	CO	2.3	2.3		7.7	+	4		200	- 100	AVE	ס		
A SHEET	12		AD C	STACK THERM	CHECK TO IV	delta P	VELOCITY	(In, H20)	550	0.55	920	End of Port	LEAK RATE:	10	0,94	10.0	0.8	End of Port	LEAK RATE:		86.0	0,49	76'0	End of Port	LEAK RATE:	960	700	70.0	End of Dor	AVE CODE	delta P		
FIELD DAT		mi.	5	DGM CAL FACTOR (Y)	10 10 10 10 10 10 10 10 10 10 10 10 10 1	2	DGM	Vm (cu. ft.)	988 879		997.47	1001.527			1001527	LL. 2901	Hp. 900	1014.335			1014.335	1018.95	1023.54	1627.161		171 171	20.00	20 700.		10.00.01	VOLUME		
METHOD 26A FIELD DATA S	282		(In. Hg)	DGM DGM BOX No. H@	MS-15 168	EI ADSED	TEST CLOCK	(MIN) (24-HR)	c	-	10	15 1100	5	FINAL	15 1107	20	25	30 1177	CK?		30 1119	35	40	45 1134	CHECK? FT) INITIAL	FINAL	40 I I OF	00 1	- 1	1 4 1 09	TOTAL	60 Min.	
ME	Ruzzi Unitem Mu	OPERATOR	- Hand	WED	(%)	TRAVERSH ELA				0	1 m		INTRA-PORT LEAK CHECK?		B-1	2	r (n)		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		7-	2	8		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		<u></u>	7	20		_ 4 <sub>1</sub> ,	Ó	

Sample Location  Run No. La Ord On -M26A- HA  Filter Number(s)  Not Applicable  MOISTURE  Sample Date 1/30/23  Recovery Date/1/30/23  Recovered by 56/														
Impingers 1 2 3 4 5 6														
50 ml 100 ml 100 ml Optional 100 ml 100 ml Silica gel 0.1N H <sub>2</sub> SO <sub>4</sub> 0.1N H <sub>2</sub> SO <sub>4</sub> 0.1N H <sub>2</sub> SO <sub>4</sub> Knockout 0.1N NaOH 0.1N NaOH														
(knockout) (tipped) (tipped) (untipped) (untipped) (untipped) (untipped)														
Final weight         (knockout)         (tipped)         (tipped)         (untipped)         (untipped)         (untipped)         (untipped)           Final weight         841.8         761.7         615.9         751.5         751.5         937.5         g           Initial weight         747.6         614.4         751.1         751.5         921.7         g           Net weight         94.6         14.1         1.5         0.9         0.0         17.8         g														
Final weight   841.8 761.7 615.9 751.5 751.5 935.5 g  Initial weight   747.7 747.6 614.4 751.1 751.5 921.7 g  Net weight   94.6 14.1 1.5 0.4 0.0 17.8 g														
Initial weight 747.7 747.6 614.4 751.1 751.5 921.7 g Net weight 94.6 14.1 1.7 0.4 0.0 17.8 g														
Initial weight 747.7 747.6 614.4 751.1 751.5 921.7 g  Net weight 94.6 14.1 1.7 0.4 0.0 17.8 g														
RECOVERED SAMPLE														
H <sub>2</sub> SO <sub>4</sub> Impingers and knockout contents and water rinse container no. MN 256A-H2SO4- 7A marked/sealed marked/sealed	<u></u>													
NaOH Impingers contents and water rinse container no. MN -M26A-NaOH +A marked/sealed marked/sealed	•													
Samples stored and locked	÷													

		ZLE DIAMETER	.287	K FACTOR	23	SAMPLE		(in. Hg)	~ "	200	3	NATURE OF THE PARTY OF THE PART		5	3	S				7	er er	~				<b>^</b> '	,	3			
1 of 1	S CONTRACT	NUMBER	Sec.	CO2 CONTENT	16.5		Sil Gel EXITEMP	(deg. F)	2	200	26			29	29	09				19	62	63				63	63	59			
PAGE 1 of	NOV	LENGTH IER TYPE	15.65	CONTENT		FII TER	JEMP TEMP	(deg. F)	25%	9276	497			75H	ASY.	द्ध				<b>3</b> 32	255	321				757	255	156			
ADE	1 1	PROBE LENGTH AND LINER TYPE	210	CHECK (FINAL)		2	IN/OUT	(deg. F)	25	\$ 1	8			99	67	89				98	64	S.				7	7	de l	September 1	AVE. TEMP.	
SAMDIET	66	PITOT	0.890.84	CHECK	ᄩ	Ē	STACK	(deg. F)	269	196	2,9		INCHES HO	862	192	200		INCHES Hg	INCHES Hg	Rbl	R.P.	4%		INCHES Hg	INCHES Hg	स्पर	ૠ	1981		AVE. TEMP.	
NO		X	(m)	ORSAT NO.			PROBE	(deg. F)	256	248	153		@@	255	J.S.J.	JH0		@	@	લુક્ત	RSA	É		0	<b>a</b>	35	7,57	hs&			<b></b>
T	30	FILTER	N.W.	STACK PITOT NO.	System .	ASSED I	delta H ORIFICE	(In. H2O)	٥٠٠/٥	2		N. P. L.	CU.FT @	2,2	ሌ ጭ	7.6		CU.FT @	CU.F	ካፖሪ	470	to the		CU.FT	- 1	43	Ç	4.00		AVE delta H	
A SHEET	I WIND	AMBIENT	(deg. r.) ∠ 74	STACK THERM NO	5 A	delta D	VELOCITY HEAD	(In. H2O)	.65	8 2		End of Port	LEAK RATE:	nø.	1	43.	End of Port	LEAK RATE:	2	86.	طها	P.	End of Port	LEAK RATE:		96.	`\	Hr.	End of Port	AVE SQRT delta P	
FIELD DATA	V 25 D2	STATIC PRESSURE	(In. water)	DGM CAL FACTOR (Y)	NES CALCUES ST				95.369	والخنص	103.65	10.7.624		10rt. 634	11.2 TH	06.91	131.091			180.141	125.06	129.86	ኒያዛ አናገ			134451	139.50	434 FB 143 34	李子	DGM	187-364
26A		AMBIENT	(D. Hg)	DGM H@	1.61		CLOCK	(24-HR)	40.0			11.00	INITIAL				11:17	INITIAL	FINAL	30 11:19			11,34	INITIAL	FINAL	11.36			N:51		
METHOD	5		7/ 100	/ DGM BOX No.	M5-31	EI APSEN			19:45 O	2	10	15	CU. FT)	15	20	25	30	SAK CHECK? (CU. FT)	,	30	35	40	45	EAK CHECK? (CU. FT)		45	50	55	09	TOTAL	60 Min.
	שועון	OPERATOR COM	(5000 M.	ASSUMED MOISTURE (%)	13	TRAVERSE	PORT/ /POINT	ON ON	A-1	2	က	Taga	DGM VOLUME (CU. FT)	B-1	2	3	TO N	INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		C-1	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		D-1	2	3			

PlantBU Sample Locat Run No Filter Numbe	tion				Reco	ole Date 11/ very Date 14 vered by	1 30 /23							
			MO	ISTURE										
Impingers	1 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (knockout) /	2 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	4 Optional Knockout (untipped)	5 100 ml 0.1N NaOH (untipped)	6 100 ml 0.1N NaOH (untipped)	Silica gel							
(knockout)         (tipped)         (tipped)         (untipped)         (untipped)         (untipped)         (untipped)           Final weight         839.4         741.8         665.7         753.1         742.7         936.7         g           Initial weight         747.6         733.6         665.3         753.2         747.7         970.1         g           Net weight         95.8         9.0         0.4         -0.1         6.0         16.6         g														
(knockout)         (tipped)         (tipped)         (untipped)         (untipped)         (untipped)         (untipped)           Final weight         839.4         741.8         665.7         753.1         742.7         730.1         g           Initial weight         75.8         8.0         0.4         -0.1         6.0         16.6         g           Description of impinger water         Clean         50         % spen														
(knockout)         (tipped)         (tipped)         (untipped)         (untipped)         (untipped)         (untipped)           Final weight         839.4         741.8         665.7         753.1         742.7         936.7         g           Initial weight         747.6         733.8         665.3         753.2         747.7         970.1         g           Net weight         95.8         9.0         0.4         -0.1         6.0         16.6         g														
Initial weight														
		]	RECOVE	RED SA	MPLE									
H <sub>2</sub> SO <sub>4</sub> Imping container no.						Liquid lev marked/se		? •						
NaOH Imping container no.	ers contents a	and water rins  -M26A-N	se NaOH 4[:	3	-	Liquid lev marked/se	1 /							
Samples store Remarks			) 					-						

ZLE	DIAMETER	K FACTOR	2.16	SAMPLE TRAIN VAC	K	1	7			W	a	W			6	ی	و			٥	٥	0			
	NUMBER -150 (750	CO2 CONTENT	2121	Sil Gel EXIT	20	29	8	New York		3	19	00	STATE OF THE REAL PROPERTY.		10	20	00	A STATE OF THE STA		29	633	62	31		
1 of	3 TYPE	CONTENT		OVEN TEMP	090	253	248				8 172	253			25%	259	254			252	152 1000	5/1/2			7
PAGE I PAGE PROBE LENGTH	AND LINE	CHECK (FINAL)	@ 10 "Hg	IN / OUT TEMP	17.1	28	و	STEPHEN STATE		12	111	40			19	8	F			8	~	82		AVE. TEMP.	
SAMPLE M26A PITOT	Cp	LEAK CHECK (INITIAL)	% 6.0.FT 6.1.FT	STAC	202	300	800		INCHES Hg	301	301	301		INCHES Hg	102	300	29.0		INCHES Hg	298	299	247		AVE. TEMP.	
$\Theta V$	(년)	ORSAT NO.	FAILED	PROBE TEMP	AC.	h52	254		CU.FT @	756	252	085		CU.FT.®	1557	127	152		CU.FT @	150	h52	780			7
NG LOCA OK OK FILTER	NUMBERS	STACK PITOT NO.	PASSED	delta H ORIFICE	(MI. 1120)	3	<u>6</u>		+	7,	۲,	۲,4		+	2	5	ř		1	Ĺ.	٥	÷		delta H	
A SHEET SAMPLING SAMPLING AMBIENT F	TEMP (deg. F)	STACK THERM NO.	8	VELGE	0.6%	0000	0.58	End of Port	LEAK RATE:	P.69.0	0.04	50,0	End of Port	LEAK RATE:	676	0.71	6.70	End of Port	LEAK RATE:	0.79	2L:0	89,0	End of Port	AVE SQR1 delta P	
METHOD 26A FIELD DATA SI RAND CITY DATE STATIC AMERICAL STATIC AMERICAL STATIC	PRESSURE (in. Water)	DGM CAL FACTOR (Y)	PITOT LEAK CHE	DGM READING	10.2%	46.02		52766		57-160	1495	10.00	(03.606	3 N	C. 2. CoO(a	67.55	71.37	75.144		75.149	79.18	43.21	47.059	DGM	
HOD 26A	PRESS (In. Hg)	DGM H@	40.1	CLOCK	0 1250	-	_	2 1420	INITIAL	15 1422		_	1/2/11	INITIAL	1430	-	_	45 1454	INITIAL	45 1456	0	2	0 [5]		7
METHC PLANT AND CITY PERATOR	<u> </u>	869	Marie	ELAPSED TEST TIME	(MIM)			15	EAK CHECK? (CU. FT)	7	20	25	3(	EAK CHECK? (CU. FT)	30	35	40	4	EAK CHECK? (CU. FT)		50	55	09	TOTAL	OO MIN.
PLANT BAZZA UN		ASSUMED MOISTURE (%)	14	TRAVERSE PORT/ /POINT		2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)	B-1	2	က	18	INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)	2	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)	D-1	2	3			

Plant	MN D	Mary Main ff -M2 Not Applicab		<u></u>	Reco	ole Date <u>[[]</u> very Date <u>[]</u> vered by	130 /23	-
			MO	ISTURE				
Impingers	l 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (knockout)	2 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	4 Optional Knockout (untipped)	5 100 ml 0.1N NaOH (untipped)	6 100 ml 0.1N NaOH (untipped)	Silica gel	
Final weight		859.6	768.9	747.4	762.7	9469	g	
Initial weight		756.3	7536	6439	746.6	763.2	934.2	g
Net weight	1	109.3	15.3	2.9	0.8	-0.5	12.3	g
Description o	of impinger v	water	cle		Total moist	60 _B/ ure =	· / 0	spent il gel color grams
		1	RECOVE	RED SA	MPLE			
H <sub>2</sub> SO <sub>4</sub> Imping container no.						Liquid lev marked/se		
NaOH Imping container no.				}		Liquid lev marked/se		
Samples store	d and locked	);						

	200	ZLE ZLE DIAMETER	4.6	180		363x Q.17	SAMPLE	TRAIN	(in. Hg)	ત્ય	ಡ	ત્હ			2	ر ۲ ر	8	7				rs	es!	~				8	CA.	3		(%)	
_	RUN NUMBER	N N SZ	282 (282	, vet	CONTENT	455	- The	Sil Gel EXIT	(deg. F)	09	58	09			٢	09	22	25				82	38	25				ķ	g,	09			
PAGE 1 of	RUN	LENGTH FR TYPE	0	w.Vc	CONTENT	**************************************	FILTER	OVEN	(deg. F)	253	255	256			0.00	3.7	245	96.96				S) X	255	78%	CHARLE WAS		11/10	M	ויי	2 49			
	YPE	PROBE LE	000	(June)	CHECK (FINAL)	CU. FT	DGM	IN / OUT	(deg. F)	748	49	8			6	PO	<b>6</b> 9	63	Section of the section of			83	Ж. Ж	22			6.3	000	24	35		AVE. TEMP.	
	SAMPLE	PITOT	5%	10.830.84	CHECK (INITIAL)	, 001 CU. FT	2	STACK	(deg. F)	303	300	399		INCHES Hg	INCHES Hg	301	201	300	A STATE OF THE STA	INCHES Hg	INCHES Hg	301	299	298		INCHES Hg	INCHES IN	228	299	253	A CONTRACTOR OF THE PARTY OF TH	AVE. TEMP.	
	NOI	SPACK	(ln.)	041	ORSAT NO.	FAILED	1 / 1155	PROBE	(deg. F)	8hB	346	SHE		0	(3)	אאמ	3Hb	483		8	(0)	254	E.	34W		000	9)	250	754	250			
_	ING LOCAT	A PREPARED	NOMICEIN	WA	STACK PITOT NO.	PASSED	MOOFE	delta H	(ln. H2O)	74	(-3	1.3		CU.FT	CU.F	(2)	1.5	1.3		CU.FT	CU.FT	د.	1.5	بن		CU.FT		7 7	- <u>}</u>	1.5		AVE delta H	
A SHEET	SAMPLIN	AMBIENT	(deg. F)	£	STACK THERM NO.	CK - > M	della	VELOCITY	(In. H2O)	. 63		. 58	End of Port	LEAK RATE:	D ()	20.	.64	ر ق ب	End of Port	LEAK RATE:		ص ۲ <u>۱</u>	7	90	End of Port	LEAK RATE:	5	<u>.</u>	۲. ج	.68	End of Port	AVE SQRT delta P	
FIELD DATA	DATE	STATIC PRESSIBE	(in. Water)	F.C)-1	DGM CAL FACTOR (Y)	PITOT I FAK CHECK	בריים בריים ביים	DGM	Vm (cu. ft.)	148.366	427.19	155.48	198 898		170 000	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	169.37	165.06	171.50H			MY1.504	14736	バルか	VED SEDS			(49:04)	18485	188:49	Lary 383	DGM VOLUME	(4.9-1) E.
26A		MIGANISTENT	(In. Hg)	27.48	DG H @⊗	١-بولا		CLOCK	(24-HR)				3,30	INITIAL	ᄪᆫ	176			F. 37	INITIAL	FINAL	lu: }9			H. 5H		니	06.M			17.73		_
METHOD	2.5			Man	BOX No.	1M5-31	щ	TEST	(MIN)	0	ည	10	15	SAK CHECK? CU. FT)		15	20	25	30	CU. FT)	`	30	35	40	45	CU. FT)		45	20	55	09	TOTAL	60 Min.
	PLANT	OPERATOR CAMP		(rus)	ASSUMED MOISTURE (%)	Z d	TRAVERSH	PORT/	NO.	A-1	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		B-1	2	က	5	INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		C-1	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		D-1	2	3			

Plant Bu Sample Locat Run No Filter Numbe	ion w	Mary Com S Off-M2 Not Applicab		χ 	Reco	ole Date [1] overy Date [4] overed by	130 123	-
			<u>MO</u>	ISTURE				=
Impingers	1 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (knockout)	2 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	4 Optional Knockout (untipped)	5 100 ml 0.1N NaOH (untipped)	6 100 ml 0.1N NaOH (untipped)	Silica gel (untipped)	
Final weight		668.9	768.1	614.1	757.7	737.2	937.0	g
Initial weight		760.9	7470	6125	755.7	737.1	9250	g
Net weight		108.0	21.1	1.6	2.0	0.1	12.0	g
Description o	f impinger v	water	Clèa		Total moist	$\frac{80}{\beta/\omega}$ are = 1	Sil	spent gel color rams
		]	RECOVE	RED SA	<b>MPLE</b>			
H <sub>2</sub> SO <sub>4</sub> Imping container no.	ers and knock	cout contents	and water rin	1 <u>se</u>	,	Liquid lev marked/se		č
NaOH Imping container no.	ers contents a	and water rins	se NaOH 51	3		Liquid lev marked/se		
Samples store	d and locked							

			ZLE DIAMETER	080	K FACTOR	2,16	1	TRAIN	(in. Hg)	20	0			60	(V)	2				(N)	60	W			3	8	3		æt.	
<u></u>	RUN NUMBER	出し	NUMBER DIA	250 250			- 65	Sil Gel EXIT	(deg. F)	200	3			[9]	02	61				62	3	6.1			55)	63	F)			
PAGE 1 of	RUN	GA D	100		CONTENT	_	0.1	TEMP TEMP	(deg. F.)		253			617	75CH	1.52	8		,	256	249	152			256	122	248	18 more 1		
	TYPE		AND LINER TYPE	2000	CHECK	00100	(a)	N OUT	(deg. F)	15	9			26	77	82			ļ	8	8	Ça.			18	40	80	- F	AVE. TEMP.	
	SAMPLE TYPE	M26A	PITOT CP, dO	12 CI-0 84	CHECK	ි [ලූ	(Hg	STACK	(deg. F)	257	293		INCHES Hg	252	293	750		INCHES Hg	INCHES Hg	794	293	293		INCHES Hg	293	2,6%	794		AVE. TEMP.	
	TION		S)	(In.)	ORSAT	CER	FAILED		(deg. r)	07/0	2417		CU.FT @	17117	248	245		CU.FT @	B	246	248	242		CU.FT @	245	241.	16D	STATE OF THE STATE		
<b>-</b>	ING LOCATION	55	FILTER	W/W	STACK PITOT	11 1/2	HASSED	delta H ORIFICE	(In. HZU)	Zvi	2.1		- CO.	2	۲.	(3		- O. S.	3	L	9	٥		- CC.	1.8	1.1	9.		AVE delta H	
'A SHEET	SAMPLING	Days year	AMBIENT	(deg. F)	STACK		FCK / 7	VELOCITY HEAD	(In. HZO)	5.67	180	End of Port	LEAK RATE:	07.0	0,00	) ()	End of Port	LEAK RATE:		0.79	0.75	072	End of Port	LEAK RATE:	H9:0	08.0	h1.0	End of Port	AVE SQRT delta P	
FIELD DATA		X	STATIC PRESSURE	(In. Water)	DGM CAL FACTOR (Y)	0.9.75	PILOI LEAK CHECK	DGM READING	VM (CU. II.)	1907 P	04.61	97.936		924.76	(O) (C)	105,39	108.815		,	104.515	112:81	116,1	120.734		H81_021	124.87	19.621	133.165	DGM	
3D 26A		PLO AND	AMBIENT	(In. Hg)	DGM H@	1.68		CLOCK	(Z4-HK)	5 5 5 1		1524	INITIAL				161	INITIAL	FINAL	1613		,	11,026	INITIAL	1630		_	1645		_
METHOD	E				DGM BOX No.	MS-13		TEST	7,54	5	10	15	SAK CHECK? CU. FT)	15	20	25	30	CU. FT)		30	35	40	45	CU. FT)	45	20	55	9	TOTAL	60 Min.
	回	ることにおいること	OPERAT	1000	5	14	HOUNTY CA	PORT/ /POINT	NO.	A-1	က		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)	B-1	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		<u>۲</u>	2	3		DGM VOLUME (CU. FT)	D-1	2	3			

Plant Book Sample Locat Run No Filter Number	MN.	Mary 1 Lain 6 Off-M2 Not Applicab		X -	Reco	ole Date <u>[1]</u> overy Date <u>[1]</u> overed by	13/23	
			MO	ISTURE				
Impingers	1 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (knockout)	2 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> / (tipped)	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	4 Optional Knockout (untipped)	5 100 ml 0.1N NaOH (untipped)	6 100 ml 0.1N NaOH (untipped)	Silica gel	
Final weight		860.3	767.0	619.3	770.1	748.4	950.Z	g
Initial weight		751.7	757.7	616.7	t71.7	747.7	757.4	g
Net weight	<u> </u>	108.6	9.3	2-6	0.4	1.0	11.3	g
Description o	of impinger v	water	He	<u>.</u>	Total moist	75   10   17	/W s	spent il gel colo grams
		]	RECOVE	RED SA	MPLE			
H <sub>2</sub> SO <sub>4</sub> Imping container no.	ers and knocl	kout contents -M26A-H	and water rir	lse L		Liquid lev marked/se		
NaOH Imping container no.	ers contents a	and water rins	se NaOH 6A			Liquid lev marked/se		
Samples store	d and locked	-						=

		7 E	DIAMETER		0.92		217	CAMBIE	TRAIN	(in. Hg)	Ü	2	R				N	(8	Ø				W	3	6			מ	4	դ				
<u></u>	RUN NUMBER	5 P. P.	NUMBER	USZ. 057.	-780	CONTENT	7.71		Sil Gel EXIT	(deg. F)	09	90	22				256	55	53				25	25	53			55	50	K				
PAGE 1 of	RUN	ENGTH	5 <u>≻</u>	1	10.23	CONTENT	-	E11 TEB	ON THE PERSON OF	(deg. F)	158	158	356				スケゲ	257	246				256	335	255			75.3	255	ગ્રજમ		\	7	
	TYPE	BORE	- 7	1	5,6	CHECK	CU. FT	BH. GA @	IN/OUT	(deg. F)	24	46	let.				83	83	S				89	æ	82			×	£2	83		AVE. TEMP		
	SAMPLE	MZbA	පි	26	0,37,084	CHECK (NITIAL)	ار اور	@ very	STACK	(deg. F)	393	hbE	394		INCHES Hg	NCHES Hg	293	3993	બ્લાર	The state of the s	INCHES Ha	INCHES Hg	294	343	394		INCHES Hg	SWS.	893	334		AVE. TEMP		
	NOL	120 100		(ln.)	041	ORSAT NO.	CEM	J FAILED.	PROBE	(deg. F)	750	Bulg	353		@ L:	CU.FT @	BE	250	353		@ L:	CU.FT.®	ر ا ا	454	25.4		CU.FT.®	157	755	255				
<b> </b>	SLOCAT	1861 12N	NUMBERS		WIT	PITOT	51	PASSED	delta H	(In. H2O)	<i>h</i> ']	(.3	<u>ن</u> ۔		CU.F	cu.F	192	7'	4.3		CU.F	CU.F	4.	<i>و</i> ۔ د	9		S.O.S.	8.1	, E.	-44		AVE delta H		
A SHEET	SAMPLIN	AMBIENT	TEMP	(deg. E)	500	THERM	54	CK	VELOCITY	(In. H20)	5.34	69.	57	End of Port	LEAK RATE:	Û	02,5	99.	09.	End of Port	LEAK RATE:		pt,	75	, T3	End of Port	LEAK RATE:	h 5	5	174	End of Port	AVE SQRT		
FIELD DATA	ш	/ 30 /23	PRESSURE	(in. Water)	19.67	CAL FACTOR (Y)		PITOT LEAK CHECK	DGM	Vm (cu. ft.)	192403	194,89	89,233	302.698			211d. 698	205.89	A19.37	21.1.16			313.136	217.06	990.068	734.839		ASU STA	7	23294	236.980	DGM	436.989	
		Mary near	PRESS	(In. Hg)	77.41	2 2 8 8 8 8	17	697	CLOCK	(24-HR)	15:39			15:24	INITIAL	FINAL	15:56			11.91	NITIAL	FINAL	16,(3)			16,26	INITIAL		2		SMS			
<b>METHOD 26A</b>	D C	5			$\geq$	BOX No.	12-5W	4000	TEST	WIN NIN	0	5	10	15	AK CHECK? CU. FT)	,	15	20	25	30	AK CHECK?	· · · · · · · ·	30	35	40	45	AK CHECK? CU. FT)	45	50	55	09	TOTAL	60 Min.	
	PLANT	UNIVITY TO THE	250		3000		F		PORT/	NO.	A-1	2	က		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		B-1	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		C-1	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)	1-0	2	က				

Plant Sample Local Run No Filter Number	19N 6	Mary OH -M2 Not Applicab	great 6A-6B	4x 	Reco	ole Date <u></u> very Date vered by	/ 31/23	<u> </u>				
			MO	ISTURE								
Impingers	1 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (knockout)	2 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	4 Optional Knockout (untipped)	5 100 ml 0.1N NaOH (untipped)	6 100 ml 0.1N NaOH (untipped)	Silica gel (untipped)					
Final weight		877.8	770.9	671.1	745.6	744.3	950,4	g				
Initial weight		771.2	7.56.7	668.2	745.6	744.2	9367	g				
Net weight	Net weight / 105.6 14.2 2.9 8.0 0.1 13.7 g											
Description o	Description of impinger water											
		]	RECOVE	RED SA	<b>MPLE</b>							
H <sub>2</sub> SO <sub>4</sub> Impingers and knockout contents and water rinse container no. MV Off-M26A-H2SO4- 013 marked/sealed												
NaOH Impingers contents and water rinse container no. MOH-M26A-NaOH 6B Liquid level marked/sealed												
Samples store	d and locked							•				

	Section of the second	ZLE DIAMETER	052	N TACLOR	2.16	SAMPLE	TRAIN	(in. Hg)	go	b	7			fv.	6	S	AL SECTION		,	9,	91	2			9	0	Ō			
-	RUN NUMBER	NUMBER 1	100	CONTENT %	177	3	Sil Gel EXITEMP	(deg. F)	65	00	20			62	62	29					20	2.1			00	19	OD	Section Section		
PAGE 1 of	RUN	ENGTH ER TYPE	105,5	CONTENT	20	EII TEB	TEMP	(deg. F)	752	181	256			25%	754	152				124	255	052			155	7582	255	The second	7	_
1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TYPE	PROBE LEN AND LINER	616	CHECK (FINAL)	100 CU FT		IN/OUT	(deg. F)	7	7	77			7	77	78			7	-  -	67	9			8	18	40		AVE. TEMP.	
	SAMPLE	PITOT CP 6/6	0.65 0.84	CHECK (INITIAL)	100 در <del>ا</del>	БL (3)	STACK	(deg. F)	193	H62	794		INCHES Hg	1NCHES FIG	29%	293		INCHES Hg	INCHES IN	7577	293	5/57		INCHES Hg	293	766	767		AVE. TEMP.	
	NOL	STACK ID (In.)	140.0	ORSAT NO.		- ALLE	PROBE			453	25.0		180	200	255	255		CU.FT.®		7227	952	hc2	× C. Luchas	CU.FT.@	155	222	952			
⊢	G LOCA	FILTER	CH	PITOT NO.	BARCEN !	ASSED	delta H ORIFICE	(In. H2O)	1,5	1.1	1.5		CUFT®	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	17.7	1.3		+	20.5	ئد	او.	5,		\	1.8	17	9.		AVE delta H	
ഗ	SAMPLIN	AMBIENT TEMP (dea. F)	00	THERM NO.	COUNTY IN	100 ct 100	VELOCITY HEAD	(In. H2O)	79.0	0.64	0.69	End of Port	LEAK RATE:	270	100	3	End of Port	LEAK RATE:	1	7.7	0.75	0/10	End of Port	LEAK RATE:	18:0	0.79	0.72	End of Port	AVE SQRT delta P	
FIELD DATA	DATE	STATIC STATIC PRESSURE (in. Water)	100	CAL FACTOR (Y)	BITOTAL EAK CHECK		DGM READING	Vm (cu. ft.)	2h2°521	127.21	146,54	143.916	Î	142919	77.70	151.07	124.811			12421	158.89	162.95	166.64		166 699	171.02	PT-4.98	178.981	DGM	
OD 26A	_	AMBIENT PRESS (In Ha)	27.43	File	997		CLOCK	(24-HR)	52L1  0	5	10	15 1740		15 1117.	1_	25	30 1757	INITIAL		30 1757	_	_	45 19 H	INITIAL FINAI	45 18 6	50	55	60 (4.5)		
METHOD	戶	32	15	E BOX No.	M5-13	DOOV DOOR	TEST TIME		1	2	3 1		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)					INTRA-PORT LEAK CHECK?  DGM VOLUME (CU. FT)	_		2	3	7	INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)		2			TOTAL	60 Min.
	PLA	OPERATOR	1/4	ASSUMED MOISTURE (%)	Σ	TOAVEDO	PORT/ /POINT	NO	A-1				INTRA-PORT LEAK CHI DGM VOLUME (CU. FT)	Ä.				INTRA-PORT DGM VOLUM		<u>7</u>				INTRA-PORT DGM VOLUM	D-1					

PlantSample Local Run No Filter Numbe	yn '	Man Man DH -M2 Not Applicab		<u>(</u> <u>=</u> —		ole Date [1] very Date [1] vered by	30 123 1131 123 365	5			
			MO	ISTURE				_			
Impingers	1 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (knockout)	2 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	4 Optional Knockout (untipped)	5 100 ml 0.1N NaOH (untipped)	6 100 ml 0.1N NaOH (untipped)	Silica gel				
Final weight	(	845.5	778.8	645.4	747.4	757.0	1642.3	g			
Initial weight		7429	7-61.4	643.4	747.0	751.4	1029.1	g			
Net weight / 102.6 17.4 2.0 6.4 -0.4 13.2 g											
Description o	of impinger v	water	'Cea		Total moistu	13		spent gel color rams			
		]	RECOVE	RED SA	MPLE						
H <sub>2</sub> SO <sub>4</sub> Imping container no.	ers and knoc MN O+	kout contents	and water rin	ise A		Liquid lev marked/se	vel ealed				
NaOH Impingers contents and water rinse container no. MOGG-M26A-NaOH 77  Liquid level marked/sealed											
Samples store Remarks											

		ZLE DIAMETER	162	-	,	7.1/				B	જ	2	THE REAL PROPERTY.		S	æ	CR				6	d	ન			ಳ	ત્ય	6			
_	RUN NUMBER	NUMBER	3/3 8	CONTENT	%	17.7		Sil Gel EXIT TEMP	(deg. F)	\$	25	2%			hs	24	25				55	52	29			28	B	00	S. C. C.		
PAGE 1 of	RUN	VGTH TYPE	sleece	CONTENT	%	2,8	FILTER	OVEN	(deg. F)	256	256	222			155	05E	<b>153</b>				356	454	253			જુહત	ASS	255			
	rype	PROBE LEN AND LINER	ŗ.	CHECK	<b>→</b>	@ 16 "Hg	DGM	IN / OUT TEMP	(deg. F)	80	18	83			8,3	83	<b>3</b> 3				83	83	83		ā)	83	83	83		AVE. TEMP.	
	MPLE	MZ6A PITOT Cp 66	0.95 0.84	SHECK SHECK	(INITIAL)	@ 10 "Ha		STACK	(deg. F)	345	295	294		INCHES Hg	343	345	<b>ઝ</b> વય		INCHES Hg	INCHES HG	44	જ્યુન	343		NCHES HG	ોશ 3	જીવન	294		AVE. TEMP.	
	NOI	STAN	(m.)	ORSAT	Ö	FALED		PROBE	(deg. F)	250	253	248		@@	dug 245	249	258		@(		250	340	35.5		@@ E	HAC	<b>353</b>	256			7-1
_	NG LOCAT	ALTHER NUMBERS	N/A	STACK	NO.	PASSED		delta H ORIFICE	(In. H2O)	ć	2	ú		CU.FT.®	3	1.4	1.3		CU.FT		<u> </u>	4.	, is		CU.FT CU.FT	Ø	8	<u>ي</u> نہ		AVE delta H	
(C)	SAMPLIN	AMBIENT	(deg. r)	STACK	ON	CK> II	ı	VELOCITY	(In. H2O)	4	ئ ج	.59	End of Port	LEAK RATE:	40	.65	09'	End of Port	LEAK RATE:	1	dit.	342	et.	End of Port	LEAK RATE:	18.	1000	85,	End of Port	AVE SQRT delta P	
FIELD DATA	100	7733	(In. water)	DGM	FACTOR (Y)	PITOT LEAK CHECK		DGM READING	Vm (cu. ft.)	333,196	2,0,0	244 . 13	244.755		SSLIPHE	251.43	255.11	258.330	Ī	- 11	258.330	263.23	ایک	964.956		269,956	243.85	277 .09	28 2538	(1)	383.534
26A		MAMBIENT	(BL) 1	DGM H@		<u>.</u>		CLOCK TIME	(24-HR)	35,71			04:E3	INITIAL	14.42			19:57	INITIAL	=1	17.50	65		18,14	INITIAL				18:31		
METHOD	PLANT AND CITY		AM CA	D DGM RE BOX No.		M5-31	山	TEST	(MIN)	0	5	10	15	CU. FT)	15	20	25	30	CU. FT)		30	35	40	45	CU. FT)	45	50	55	09	TOTAL	60 Min.
	PLANT	SPERATOR**	W (TOAK)	ASSUMED	(%)	<u> </u>	TRAVERSE	PORT/ /POINT	NO.	A-1	2	3		INTRA-PORT LEAK CHECK? DGM VOLUME (CU. FT)	B-1	2	3		INTRA-PORT LEAK CHECK?  DGM VOLUME (CU. FT)		<u>?</u>	2	က		DGM VOLUME (CU. FT)	D-1	2	3			

Plant Bc Sample Loca Run No. A Filter Number	ΛN	Mari Lain 1/2 Oft-M2 Not Applicab	Meal Stack 6A-7AB	TX -	Reco	ole Date <u>((/</u> very Date <u>/-</u> vered by	2/ / /23		
			<u>MO</u>	ISTURE					
Impingers  Final weight  Initial weight	l 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (knockout)	2 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped) \$53.b	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped) 7 89.3	4 Optional Knockout (untipped) 6 12.97 6 11.3	5 100 ml 0.1N NaOH (untipped) 748,4 744.6	6 100 ml 0.1N NaOH (untipped) 7 37.D 7 37.8	Silica gel (untipped) 982.1	g g	
Net weight		92.5	39,1	1.6	1.8	0.2	15.1	g	
Description o	of impinger v		RECOVE		Total moistu	$\frac{2}{13}$ $\text{are} = \frac{13}{1}$	w Si	spent Il gel colo grams	
H <sub>2</sub> SO <sub>4</sub> Imping container no.	ers and knock	cout contents 7-M26A-H	and water rin	<u>sse</u>		Liquid lev marked/se	,		
NaOH Impingers contents and water rinse container no. My Off-M26A-NaOH 713 Liquid level marked/sealed									
Samples store Remarks						_			

PlantSample Locate Run No Filter Number		Mary Warr OFF-M2 Not Applicab		TX =		ole Date <u>10</u> overy Date <sub>11</sub> overed by		
			<u>MO</u>	ISTURE				1
Impingers	l 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (knockout)	2 100 ml 0.1N H₂SO₄ (tipped)	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	4 Optional Knockout (untipped)	5 100 ml 0.1N NaOH (untipped)	6 100 ml 0.1N NaOH (untipped)	Silica gel (untipped)	
Final weight		7660	760.4	616.0	749.9		951.3	. g
Initial weight		766.2	760.4	618.1	760.0	752.8	950,2	g
Net weight				-				g
Description o	of impinger v	water	Cle	<u></u>			% S	
				,	Total moistu	ire =		grams
		<u>]</u>	RECOVE	RED SAI	MPLE			
H <sub>2</sub> SO <sub>4</sub> Imping container no.	ers and knock	cout contents  -M26A-H	and water rin	<u>sse</u>		Liquid lev marked/se		
NaOH Imping container no.	ers contents a	and water rins	ie VaOH FÜ	3		Liquid lev marked/se		
Samples stored	d and locked	train	61			_		

Plant P Sample Loca Run No. 1 Filter Numbe	NN '	Mais 57	rachi tacki 16A- FB	1×	Samp Reco Reco	ole Date <u>//</u> every Date <u>/</u> evered by	1 30 123 (1 30/23 569	<u>.</u> <u>.</u>
			<u>MC</u>	ISTURE				
Impingers	I 50 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (knockout)	2 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	3 100 ml 0.1N H <sub>2</sub> SO <sub>4</sub> (tipped)	4 Optional Knockout (untipped)	5 100 ml 0.1N NaOH (untipped)	6 100 ml 0.1N NaOH (untipped)	Silica gel (untipped)	
Final weight		750.9	752.6	613.0	741.7	744.7	9323	g
Initial weight		757.3	752.5	6129	749.5	741.7	932.2	. g
Net weight	/							g
Description o	of impinger v	water			Fotal moistu		<u> </u>	spent il gel colo grams
		<u>]</u>	RECOVE				,	Brains
H <sub>2</sub> SO <sub>4</sub> Imping container no.				ise		Liquid lev marked/se	1/	
NaOH Imping container no.	ers contents a	and water rins -M26A-N	se NaOH = [	3		Liquid lev marked/se	1/	
Samples stored		Time of the state	<del></del>	3 A	_			<b>-</b> .

Client: Buzzi Maryneal TX Test Location: Main Stack; Raw Mill On Date: Nov 29, 2023 Start Time: 14:50:05

Date: Nov 29, 2023	Sta
Run number 1	-
One Minute Average	98
•	
	(
	%

One Minute Average	S	
	O2 %,dry	CO2 %,dry
2:51:03 PM 2:52:03 PM	10.8 10.7	16.7
2:53:03 PM	10.7	16.8 16.6
2:54:03 PM	10.8	16.6
2:55:03 PM	10.8	16.7
2:56:03 PM	10.7	17.0
2:57:03 PM 2:58:03 PM	10.8 10.8	16.8 16.7
2:59:03 PM	10.8	16.7
3:00:03 PM	10.8	16.8
3:01:03 PM	10.8	16.3
3:02:03 PM 3:03:03 PM	10.8 10.8	16.5 16.6
3:04:03 PM	10.8	16.5
3:05:03 PM	10.8	16.7
3:06:03 PM	10.8	16.8
3:07:03 PM	10.8	16.7
3:08:03 PM 3:09:03 PM	10.8 10.8	16.5 16.6
3:10:03 PM	10.8	16.7
3:11:03 PM	10.8	16.6
3:12:03 PM	10.8	16.7
3:13:03 PM 3:14:03 PM	10.8 10.9	16.8 16.5
3:15:03 PM	10.9	16.5
3:16:03 PM	10.8	16.6
3:17:03 PM	10.8	16.7
3:18:03 PM 3:19:03 PM	10.8 10.8	16.8 16.7
3:20:03 PM	10.8	16.7
3:21:03 PM	10.7	16.7
3:22:03 PM	10.7	16.9
3:23:03 PM	10.7	16.9
3:24:03 PM 3:25:03 PM	10.7 10.7	16.7 16.9
3:26:03 PM	10.7	16.9
3:27:03 PM	10.7	16.8
3:28:03 PM	10.7	16.7
3:29:03 PM 3:30:03 PM	10.7 10.7	16.7 17.0
3:31:03 PM	10.7	16.9
3:32:03 PM	10.7	16.9
3:33:03 PM	10.7	16.8
3:34:03 PM 3:35:03 PM	10.7 10.8	16.9 16.8
3:36:03 PM	10.8	16.8
3:37:03 PM	10.7	16.8
3:38:03 PM	10.7	16.7
3:39:03 PM 3:40:03 PM	10.7 10.7	16.8 16.6
3:41:03 PM	10.7	16.7
3:42:03 PM	10.7	16.6
3:43:03 PM 3:44:03 PM	10.7	16.8
3:45:03 PM	10.7 10.7	16.8 17.0
3:46:03 PM	10.7	16.7
3:47:03 PM	10.8	16.7
3:48:03 PM	10.8	16.7
3:49:03 PM 3:50:03 PM	10.8 10.8	16.6 16.8
3:51:03 PM	10.8	16.8
3:52:03 PM	10.8	16.6
3:53:03 PM	10.8	16.9
3:54:03 PM 3:55:03 PM	10.8 10.8	16.7 16.8
3:56:03 PM	10.8	16.7
Run Avgs	10.8	16.7
Cal Gas	11.8	10.0
Initial Zero	0.0	0.2
Final Zero Initial cal.	0.2 11.8	0.3 10.0
Final Cal.	11.9	10.0
Corrected Average	10.7	16.9

Buzzi Unicen	Buzzi Unicem: Maryneal TX Main Stack: Raw	Main Stac	ck: Raw	Mill On	AND TO A TO		_	Novemb	November 29, 2023		)	Operator							
\\.					Run No.		No. 1 14:50-15:56	ľ	Run No.	Run No.				***	Run No.		Run No.		
	quar.		Internal	Sal Sal	Pre Run	Percent	Post Run	Percent	Percent	Pre Run	Percent	Post Run	Percent	Percent	Pre Run	Percent	Post Run	Percent	Percent
Cylinder ID Gas Type	Gas Type	Value	Response	Error	Bias Bias Bias Drift Bias	Bias	Bias	Bias	Drift	Bias	Bias	Bias Bias Drift Bias Bias Bias Drift	Bias	Drift	Bias	Bias	Bias	Bias	Drift
16000000	O2 Zero	Zero N2 0.0%	%0.0	0.00%	%0:0	%00.0	0.2% 0.91% 0.91%	0.91%	0.91%		on annual or			·		******			
EB0066680	O2 Mid	11.8%	12.0%	0.82%	11.8%	-0.91%	11.9% -0.46% 0.46%	-0.46%	0.46%		est trates					*******			
ALM056015	O2 Span	21.9%	21.9%	0.00%					TAXABET .							7,200,00			
- Paritimeter,	CO2 Zero			0.00%	0.2%	1.10%	0.3%	1.65%	0.55%					inagement.		y			<b></b>
EB0066680	CO2 Mid	10.0%	9.9%	-0.51%	10.0%	0.55%	10.0%	0.55%	0.00%					*******					
ALM055015	CO2 Span	18.2%	18.2%	0.17%					Angescoonsg-					-					

Client: Buzzi Maryneal TX Test Location: Main Stack; Raw Mill On Date: Nov 30, 2023 Start Time: 09:20:23 Run number 2 One Minute Averages

one minute in orașe	•	
	O2 %,dry	CO2 %,dry
9:21:21 AM 9:22:21 AM 9:23:21 AM 9:24:21 AM 9:25:21 AM 9:25:21 AM 9:26:21 AM 9:26:21 AM 9:27:21 AM 9:30:21 AM 9:30:21 AM 9:31:21 AM 9:32:21 AM 9:33:21 AM 9:35:21 AM 9:36:21 AM 9:40:21 AM 9:41:21 AM 9:41:21 AM 9:42:21 AM 9:42:21 AM 9:45:21 AM 9:45:21 AM 9:45:21 AM 9:55:21 AM 9:56:21 AM 10:00:21 AM 10:00:21 AM 10:01:21 AM 10:00:21 AM 10:01:21 AM 10:01:21 AM 10:01:21 AM 10:01:21 AM 10:01:21 AM 10:11:21 AM	11.2 11.2 11.2 11.3 11.3 11.3 11.3 11.3	15.4 15.3 15.4 15.4 15.4 15.4 15.4 15.3 15.1 15.1 15.1 15.1 15.1 15.1 15.1
Final Zero Initial cal. Final Cal.	0.1 11.9 12.0	0.1 9.8 9.8
Corrected Average	11.4	15.2

Client: Buzzi Maryneal TX Test Location: Main Stack; Raw Mill On Date: Nov 30, 2023 Start Time: 10:39:23 Run number 3 One Minute Averages

One windle Averages		
	O2 %,dry	CO2 %,dry
10:46:21 AM 10:47:21 AM 10:49:21 AM 10:50:21 AM 10:50:21 AM 10:50:21 AM 10:53:21 AM 10:53:21 AM 10:56:21 AM 10:56:21 AM 10:56:21 AM 10:56:21 AM 10:57:21 AM 10:59:21 AM 11:07:21 AM 11:07:	11.9 11.9 11.9 11.9 11.9 11.9 11.9 11.9	14.5 14.5 14.4 14.5 14.3 14.3 14.3 14.4 14.4 14.4 14.4 14.4
Cal Gas Initial Zero Final Zero	11.8 0.1 0.0	10.0 0.1 0.1
Initial cal. Final Cal.	12.0 11.9	9.8 9.8
Corrected Average	11.7	14.9

Buzzi Unicen	Buzzi Unicem; Maryneal TX Main Stack: Raw N	Main Stac	:K: Raw I	/⊪ On				Novemb	er 30, 2	023		Operator							
5					Run No.	2	09.20-10.26		*	du No.	3	10:45-11:51		-	Run No.				
******			Internal	Ö	Pre Run   Percent   Post Run   Percent   Pre Run	Percent	Post Run	Percent	Percent 8	Pre Run	Percent Post Run Percent Percent Pre Run	Post Run	Percent	Percent	Pre Run	Percent F	Percent Post Run Percent Percent	ercent F	ercent
Cylinder ID Gas Type	Gas Type	Value	Response	Error	Bias	Bias	Bias	Bias	onit O	Bias	Bias	Bias	Bias	Orift	Bias	Blas	Bias	Bias	Drift Drift
01177410	O2 Zero	Zero N2   0.0%	0.0%	0.00%	0.0%	0.00%	0.1%   0.46%   0.46%	0.46%		0.1%	0.46%	0.0%	0.00% -0.46%	-0.46%					Name of Street, Street
EB0068680	O2 Mid	11.8%	12.0%	0.82%	11.9%	-0.46%	12.0%	0.00% 0.46%	0.46%	12.0%	0.00%	11.9%	-0.46%	-0.46%		energy/series/	-		
ALM056015	O2 Span	21.9%	21.9%	0.00%		are date										******			
	CO2 Zero	Zero N2	0.0%	0.00%	0.0%	0.00%	0.1% 0.55% 0.55%	0.55%	0.55%	0.1%	0.55%	0.1%	0.55%	0.00%		enconnecta :			*********
EB0068680	CO2 Mid	10.0%	%6.6	-0.61%	9.8%	-0.55%	9.8%	-0.55%	0.00%	9.8%	-0.55%	%8.6	-0.55%	0.00%					*******
		***							water		beau			***	-	******			

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Client: Buzzi Maryneal TX Test Location: Main Stack Mill Off Date: Nov 30, 2023 Start Time: 13:58:53 Run number 4 One Minute Averages

	O2 %,dry	CO2 %,dry
2:05:51 PM 2:06:51 PM 2:07:51 PM 2:08:51 PM 2:09:51 PM 2:10:51 PM 2:11:51 PM 2:11:51 PM 2:13:51 PM 2:14:51 PM 2:15:51 PM 2:21:51 PM 2:22:51 PM 2:22:51 PM 2:22:51 PM 2:23:51 PM 2:23:51 PM 2:23:51 PM 2:23:51 PM 2:24:51 PM 2:25:51 PM 2:25:51 PM 2:25:51 PM 2:25:51 PM 2:33:51 PM 2:33:51 PM 2:33:51 PM 2:33:51 PM 2:33:51 PM 2:35:51 PM 2:45:51 PM 2:55:51 PM	9.9 9.8 9.8 9.7 9.6 9.7 9.6 9.7 9.6 9.7 9.6 9.7 9.7 9.8 9.7 9.8 9.7 9.8 9.7 9.8 9.7 9.8 9.7 9.8 9.7 9.8 9.7 9.8 9.8 9.7 9.8 9.8 9.7 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8	17.6 17.6 17.6 17.9 17.8 17.8 17.8 17.8 17.8 17.7 18.0 17.9 17.8 17.7 17.9 17.7 17.8 17.7 17.8 17.7 17.8 17.7 17.8 17.7 17.8 17.7 17.8 17.7 17.8 17.7 17.8 17.7 17.8 17.8
Final Zero Initial cal. Final Cal.	0.1 11.9 11.9	0.1 9.8 9.8
Corrected Average	9.7	18.2

Client: Buzzi Maryneal TX Test Location: Main Stack Mill Off Date: Nov 30, 2023 Start Time: 15:22:49 Run number 5 One Minute Averages

•		
	O2 %,dry	CO2 %,dry
3:39:47 PM 3:40:47 PM 3:41:47 PM 3:42:47 PM 3:43:47 PM 3:44:47 PM 3:45:47 PM 3:46:47 PM 3:46:47 PM 3:48:47 PM 3:49:47 PM 3:50:47 PM 3:55:47 PM 4:01:47 PM 4:10:47 PM 4:20:47 PM 4:21:47 PM 4:21:47 PM 4:23:47 PM 4:33:47 PM 4:43:47 PM 4:43:47 PM 4:43:47 PM	9.8 9.9 9.9 9.9 9.9 9.9 9.9 9.9	17.8 17.6 17.9 17.8 17.7 17.6 17.6 17.6 17.6 17.6 17.5 17.3 17.2 17.3 17.3 17.3 17.3 17.3 17.3 17.3 17.4 17.5 17.3 17.3 17.3 17.5 17.3 17.5 17.3 17.5 17.3 17.5 17.3 17.5 17.5 17.6 17.6 17.6 17.6 17.6 17.6 17.6 17.6
Final Zero Initial cal. Final Cal.	0.1 11.9 12.0	0.1 9.8 9.8
Corrected Average	99	179

Corrected Average 9.9 17.9

Client: Buzzi Maryneal TX
Test Location: Main Stack Mill Off
Date: Nov 30, 2023 Start Time: 16:57:03
Run number 6

One Minute Averages

	O2 %,dry	CO2 %,dry
5:26:01 PM 5:27:01 PM 5:28:01 PM 5:28:01 PM 5:30:01 PM 5:31:01 PM 5:33:01 PM 5:33:01 PM 5:35:01 PM 5:35:01 PM 5:35:01 PM 5:36:01 PM 5:36:01 PM 5:39:01 PM 5:40:01 PM 5:50:01 PM 5:50:01 PM 5:50:01 PM 5:50:01 PM 5:50:01 PM 6:50:01 PM 6:55:01 PM 6:55:01 PM 6:55:01 PM 6:00:01 PM	10.1 10.1 10.1 10.1 10.1 10.1 10.1 10.0 10.0 10.0 10.0 10.1 10.1 10.1 10.2 10.2	17.5 17.3 17.3 17.5 17.4 17.4 17.4 17.6 17.4 17.6 17.4 17.3 17.4 17.3 17.4 17.3 17.4 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.4 17.5 17.3 17.4 17.5 17.3 17.4 17.4 17.4 17.4 17.4 17.4 17.4 17.4
Final Zero Initial cal. Final Cal.	0.1 12.0 12.0	0.1 9.8 9.8
Corrected Average	10.0	17.8

Buzzi Unicen	Buzzi Unicem; Maryneal TX Main Stack: Raw	Main Stac	ck: Raw	VIII OF				Novem	November 30, 2023	023		Operator							
				-	Run No.		14:05-15:11			Run No.		15:39-16:45			Run No. 3		17:25-18:31	A STATE OF THE PARTY OF THE PAR	
Cvinder ID Gas Type	Gas Type	Value	Internal	Error E	Pre Run Bias	Percent	Percent Post Run Percent Pre Run Bias Bias Bias Drift Bias	Percent	Percent Drift	Pre Run Bias	Percent Bias	Post Run Percent Percent Pre Run Percent Post Run Percent Bias Bias Drift Bias Bias Bias Bias	Percent Bias	Percent 1	Pre Run Bias	Percent F Bias	Post Run Bias		Percent Doft
	O2 Zero	N2	0.0%	0.00%		0.46%	0.1%		0.00%	0.1%	0.46%		1 .	3	1	0.46%	0.1%		0.00%
EB0066680	O2 Mid	11.8% 12.0%	12.0%	0.82%	11.9%	-0.46%	11.9%	-0.46% 0.00%	MARKE	11.9%	-0.46%	12.0%	12.0% 0.00% 0.46% 12.0%	0.46%		0.00%	12.0%	0.00%	0.00%
ALM056015	O2 Span	21.9% 21.9%	21.9%	%00.0					wantit										
	CO2 Zero	Zero N2 0.0%	%0.0	0.00%	0.1%	0.55%	0.1%	0.55%	0.00%	0.1%	0.55%	0.1%	0.55%	0.00%	0.1%	0.55%	0.1%	0.55%	0.00%
EB006680	CO2 Mid	10.0%	%6.6	-0.61%	9.8%	-0.55%	9.8%	-0.55% 0.00%	0.00%	9.8%	-0.55%	9.8%	-0.55% 0.00%		9.8%	-0.55%	9.8%	-0.55%	0.00%
ALM056015	CO2 Span	18.2%	18.2%	0.17%					NA PROCES	-	Zuon					vredecisé (			

Buzzi Unicem Maryneal TX Main Stack; Mill On HCN Analyte Spikes

	Date	11/29/23	11/29/23
	Time	12:15-12:33	15:57-16:15
		Main Pre 1	Main Post 1
		HCN	HCN
Cs	Spike Direct, ppm	197.19	197.19
	SF6 Tracer Direct, ppm	9.58	9.58
SF6	Diluted SF6 Tracer, ppm	0.616	0.533
	Diluted SF6 Tracer, ppm	0.579	0.429
	Average Diluted SF6 Tracer, ppm	0.598	0.481
DF	Dilution Ratio	16.03	19.92
	Total, ppm	20.211	18.671
	Total, ppm	19.721	16.802
Ct	Average Total, ppm	19.966	17.737
	Pre Spike Native , ppm	8.868	9.151
	Pre Spike Native , ppm	8.704	8.908
	Post Spike Native , ppm	8.650	9.353
	Post Spike Native , ppm	8.642	9.180
Cn	Average Native, ppm	8.716	9.148
	Spike Recovery	95.9%	91.4%
	CTS Direct (CC426155)		
	Ethylene Expected (ppm)	75.47	75.47
	Ethylene Measured (ppm)	74.48	73.48
	CTS Error	-1.3%	-2.6%

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill On Pre Run 1 HCN Analyte Spike

Spectrum	Date	Time	HCN PCA 191c R1 191c	HF ppm (10) 191C	SF6 (10) 191C	
SPC003252.LAB	11/29/23	12:13:49.127	10.097	-0.043	0.032	
SPC003253.LAB	11/29/23	12:14:53.023	8.868	-0.052	-0.006	
SPC003254.LAB	11/29/23	12:15:56.935	8.704	-0.075	-0.010	
SPC003255.LAB	11/29/23	12:17:00.851	13.783	-0.080	0.306	
SPC003256.LAB	11/29/23	12:18:04.795	24.690	-0.072	0.868	
SPC003257.LAB	11/29/23	12:19:08.664	22.206	-0.093	0.730	
SPC003258.LAB	11/29/23	12:20:12.632	20.211	-0.063	0.616	
SPC003259.LAB	11/29/23	12:21:16.495	_19.721	-0.071	0.579	
SPC003260.LAB	11/29/23	12:22:20.410	21.800	-0.062	0.711	
SPC003261.LAB	11/29/23	12:23:24.329	44.831	-0.084	1.916	
SPC003262.LAB	11/29/23	12:24:28.549	10.093	-0.090	0.193	
SPC003263.LAB	11/29/23	12:25:32.136	0.235	-0.025	0.001	
SPC003264.LAB	11/29/23	12:26:36.375	0.237	-0.000	-0.004	
SPC003265.LAB	11/29/23	12:27:40.087	0.081	-0.012	-0.009	
SPC003266.LAB	11/29/23	12:28:44.166	0.794	-0.016	-0.007	
SPC003267.LAB	11/29/23	12:29:47.797	9.255	0.058	-0.010	
SPC003268.LAB	11/29/23	12:30:52.098	9.025	-0.036	-0.010	
SPC003269.LAB	11/29/23	12:31:55.611	8.650	-0.059	-0.013	
SPC003270.LAB	11/29/23	12:32:59.572	8.642	-0.018	-0.010	

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill On Post Run 1 HCN Analyte Spike HF ppm (10) 191C SF6 (10) 191C Spectrum Date Time HCN PCA 191c R1 191c SPC\_\_003459.LAB 11/29/23 15:56:38.579 11/29/23 15:57:42.450 11/29/23 15:58:46.356 -0.186 -0.008 9.151 SPC\_\_003460.LAB SPC\_\_003461.LAB 8.908 -0.195 -0.013 0.483 0.848 15.433 -0.158 SPC\_003462.LAB SPC\_003463.LAB SPC\_003464.LAB 11/29/23 15:59:50.268 11/29/23 16:00:54.215 11/29/23 16:01:58.082 24.154 12.849 -0.154 -0.186 0.211 24.883 -0.194 0.880 SPC\_003465.LAB 11/29/23 16:03:01.992 21.645 -0.195 0.688 SPC\_\_003466.LAB SPC\_\_003467.LAB -0.215 -0.214 11/29/23 16:04:05.903 11/29/23 16:05:09.802 0.533 18.671 0.429 16.802 SPC\_\_003468.LAB 11/29/23 16:06:13.717 15.668 -0.214 0.359 SPC\_\_003469.LAB 11/29/23 16:07:17.877 13.151 -0.097 -0.036 0.345 SPC\_003470.LAB SPC\_003471.LAB SPC\_003472.LAB 11/29/23 16:08:21.640 11/29/23 16:09:25.432 11/29/23 16:10:29.343 0.315 0.084 -0.025 -0.000 -0.008 -0.036 -0.009 -0.011 -0.011 -0.031 -0.103 SPC\_003473.LAB 11/29/23 16:11:33.434 3.554 SPC\_\_003474.LAB SPC\_\_003475.LAB SPC\_\_003476.LAB 11/29/23 16:12:37.253 11/29/23 16:13:41.122 9.649 9.353

9.180

11/29/23 16:14:45.034

-0.191

-0.213

-0.013

-0.013

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill On Post Run 1 CTS

Spectrum	Date	Time	HCN PCA 191c R1 191c	HF ppm (10) 191C	SF6 (10) 191C	Ethylene (100,3000) 191C
SPC003560.LAB SPC003561.LAB SPC003562.LAB	11/29/23 11/29/23	18:45:53.586 18:46:57.614 18:48:01.393	0.053 -0.226 -0.128	-0.013 -0.005 -0.007	-0.010 -0.013 -0.014	16.286 73.543 73.411
SPC003563.LAB	11/29/23	18:49:05.439	-0.316	-0.013	-0.020	53.814

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill On CTS and HCN Direct

C15 and mon bliect					
Spectrum	Date Time				Ethylene (100,3000) 191C
SPC003128.LAB	11/29/23 09:48:23.996	0.020	0.006	0.001	-0.072
SPC003129.LAB	11/29/23 09:49:27.908	0.134	-0.005	-0.001	-0.058
SPC003130.LAB	11/29/23 09:50:31.936	0.044	-0.008	0.003	-0.116
SPC003131BKG.LAB	11/29/23 09:53:26.078	0.000	0.000	0.000	0.000
SPC003132.LAB	11/29/23 09:54:36.458	0.000	0.000	0.001	-0.015
SPC003133.LAB	11/29/23 09:55:40.374	0.109	0.009	0.000	0.002
SPC003134.LAB	11/29/23 09:56:44.401	-0.042	-0.006	0.001	-0.051
SPC003135.LAB	11/29/23 09:57:48.181	-0.080	-0.006	0.000	-0.006
SPC003136.LAB	11/29/23 09:58:52.214	-0.022	0.049	-0.001	-0.033
SPC003137.LAB	11/29/23 09:59:56.406	0.006	0.033	0.001	-0.047
SPC003138.LAB	11/29/23 10:00:59.901	-0.032	0.047	0.002	-0.051
SPC003139.LAB	11/29/23 10:02:03.848	-0.090	0.127	-0.001	0.015
SPC003140.LAB	11/29/23 10:03:07.759	-0.001	0.125	-0.011	22.400
SPC003141.LAB	11/29/23 10:04:11.624	-0.293	0.061	-0.005	61.988
SPC003142.LAB	11/29/23 10:05:15.938	-0.165	0.060	-0.011	58.433
SPC003143.LAB	11/29/23 10:06:19.438	-0.142	0.062	-0.009	54.454
SPC003144.LAB	11/29/23 10:07:23.437	-0.070	0.009	-0.009	74.299
SPC003145.LAB	11/29/23 10:08:27.783	-0.180	0.010	-0.008	74.579
SPC003146.LAB	11/29/23 10:09:31.168	-0.255	0.004	-0.011	74.391
SPC003147.LAB	11/29/23 10:10:35.067	-0.286	-0.005	-0.008	74.456
SPC003148.LAB	11/29/23 10:11:39.102	-0.083	-0.001	-0.006	9.761
SPC003149.LAB	11/29/23 10:12:42.891	-0.151	-0.001	-0.005	0.481
SPC003150.LAB	11/29/23 10:13:46.799	-0.048	-0.009	-0.005	0.478
SPC 003151.LAB	11/29/23 10:14:50.845	-0.038	0.011	-0.007	0.442
SPC003152.LAB	11/29/23 10:15:54.666	-0.180	0.006	-0.004	0.467
SPC 003153.LAB	11/29/23 10:16:58.915	-0.100	-0.004	-0.006	0.497
SPC 003154.LAB	11/29/23 10:18:02.445	-0.007	0.002	-0.002	0.472
SPC 003155.LAB	11/29/23 10:19:06.462	10.754	0.013	1.172	0.663
SPC 003156.LAB	11/29/23 10:20:10.264	41.711	0.028	4.607	-0.076
SPC 003157.LAB	11/29/23 10:21:14.292	45.886	0.017	4.849	-0.279
SPC_003158.LAB	11/29/23 10:22:18.085	46.590	-0.006	4.851	-0.135
SPC 003159.LAB	11/29/23 10:23:21.995	46.739	0.016	4.856	-0.264
SPC 003160.LAB	11/29/23 10:24:25.960	47.320	0.003	4.860	-0.268
SPC 003161.LAB	11/29/23 10:25:29.819	37.078	0.008	4.848	-0.184
SPC 003162.LAB	11/29/23 10:26:33.849	28.421	0.018	4.624	-0.228
SPC 003163.LAB	11/29/23 10:32:14.551	195.980	0.011	9.583	-0.647
SPC 003164.LAB	11/29/23 10:33:18.264	196.278	-0.026	9.585	-0.465
SPC 003165.LAB	11/29/23 10:34:22.223	196.975	0.012	9.583	-0.523
SPC 003166.LAB	11/29/23 10:35:26.094	197.038	0.007	9.580	-0.445
SPC 003167.LAB	11/29/23 10:36:30.150	197.342	-0.007	9.580	-0.500
SPC 003168.LAB	11/29/23 10:37:34.119	170.976	-0.020	9.590	-0.601
SPC 003169.LAB	11/29/23 10:38:37.830	157.143	-0.019	9.064	-0.470
SPC003170.LAB	11/29/23 10:39:41.948	138.047	0.025	7.225	-0.339
SPC 003171.LAB	11/29/23 10:40:45.858	67.542	0.029	5.083	-0.220
SPC 003172.LAB	11/29/23 10:41:49.573	49.888	-0.000	4.852	-0.250
SPC 003173.LAB	11/29/23 10:42:53.522	49.909	0.003	4.847	-0.339
SPC 003174.LAB	11/29/23 10:43:57.490	49.927	0.006	4.851	-0.271
SPC 003175.LAB	11/29/23 10:45:01.307	49.815	0.013	4.849	-0.321
SPC_003176.LAB	11/29/23 10:46:05.212	49.899	0.005	4.848	-0.292
SPC003177.LAB	11/29/23 10:47:09.125	23.829	0.025	2.379	0.742

	Maryneal TX Main Stack; Raw Mill On and Off HCN Analyte Spikes							
	Raw Mill Status	o			JJO	#O	ЭĘ	#O
	Date	11/30/23	11/30/23		11/30/23		11/30/23	
			10:27-10:39	11:42-11:56	13:39-13:57		16:46-16:58	
			Main Post 2	Main Post 3	Main Pre 4		Main Post 5	ع ≥
လိ	Spike Direct, ppm	<b>HCN</b> 49.92	49.92	49.92	49.92	49.92	49.95	49.92
	. ppm		4.84	4.84	4.84		4.84	
SF6	Diluted SF6 Tracer, ppm	0.420	0.499	0.476	0.466	0.474	0.482	0.450
	Diluted SF6 Tracer, ppm	0.407	0.462	0.427	0.445	0.454	0.461	0.417
	Average Diluted SF6 Tracer, ppm	0.414	0.481	0.452	0.456	0.464	0.472	0.434
DF	Dilution Ratio	11.69	10.06	10.71	10.61	10.42	10.25	11.15
	Total, ppm	10.955	11.425	11.060	13.559	14.073	14.432	13.608
	Total, ppm	10.938	11.290	10.732	13.438	14.019	14.364	13.398
ၓ	Average Total, ppm	10.947	11.358	10.896	13.499	14.046	14.398	13.503
	Pre Spike Native , ppm	7.915	7.571	7.147	9.645	10.596	11.052	10.394
	Pre Spike Native , ppm	7.597	7.503	6.992	9.597	10.474	11.064	10.121
	Post Spike Native, ppm	7.488	7.750	7.687	9.886	10.950	10.615	10.319
	Post Spike Native, ppm	7.647	7.425	7.789	608.6	10.725	10.762	10.213
ວ	Average Native , ppm	7.662	7.562	7.404	9.734	10.686	10.873	10.262

Buzzi Unicem

93.0%

94.2%

91.5%

99.5%

89.7%

91.7%

92.3%

Spike Recovery

75.47 73.86 **-2.1%** 

75.47 73.85 **-2.1%** 

CTS Direct (CC426155)
Ethylene Expected (ppm)
Ethylene Measured (ppm)
CTS Error

75.47 73.81 **-2.2%** 

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill On Pre Run 2 HCN Analyte Spike

Spectrum	Date	Time	HCN PCA 191c R1 191c	HF ppm (10) 191C	SF6 (10) 191C
SPC003653.LAB	11/30/23	09:06:49.691	8.614	-0.076	-0.009
SPC003654.LAB	11/30/23	09:07:53.558	7.915	-0.159	-0.010
SPC003655.LAB	11/30/23	09:08:57.221	7.597	-0.165	-0.007
SPC003656.LAB	11/30/23	09:10:01.009	8.417	-0.179	0.165
SPC003657.LAB	11/30/23	09:11:05.018	12.389	-0.183	0.589
SPC003658.LAB	11/30/23	09:12:08.818	11.962	-0.164	0.535
SPC003659.LAB	11/30/23	09:13:12.721	10.955	-0.175	0.420
SPC003660.LAB	11/30/23	09:14:16.770	10.938	-0.154	0.407
SPC003661,LAB	11/30/23	09:15:20.779	9.460	-0.170	0.190
SPC003662.LAB	11/30/23	09:16:24.617	7.698	-0.166	-0.004
SPC003663.LAB	11/30/23	09:17:28.327	4.351	-0.088	0.147
SPC003664.LAB	11/30/23	09:18:32.432	0.178	-0.039	0.005
SPC003665.LAB	11/30/23	09:19:36.136	0.177	-0.020	0.003
SPC003666.LAB	11/30/23	09:20:40.096	7.235	-0.059	-0.007
SPC003667.LAB	11/30/23	09:21:43.959	8.068	-0.205	-0.008
SPC003668.LAB	11/30/23	09:22:47.875	7.488	-0.185	-0.007
SPC003669.LAB	11/30/23	09:23:51.774	7.647	-0.201	-0.007
SPC003670.LAB	11/30/23	09:24:55.773	7.706	-0.213	-0.007

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill On Post Run 2 HCN Analyte Spike

Date	Time	HCN PCA 191c R1 191c	HF ppm (10) 191C	SF6 (10) 191C
11/30/23	10:25:38.231	7.704	-0.206	-0.009
11/30/23	10:26:42.135	7.571	-0.229	-0.008
11/30/23	10:27:46.073	7.503	-0.192	-0.008
11/30/23	10:28:49.930	7.766	-0.208	-0.003
11/30/23	10:29:54.024	10.988	-0.187	0.441
11/30/23	10:30:57.740	11.425	-0.212	0.499
11/30/23	10:32:01.639	11.290	-0.218	0.462
11/30/23	10:33:05.541	9.417	-0.144	0.311
11/30/23	10:34:09.433	0.594	-0.077	0.010
11/30/23	10:35:13.378	0.077	-0.038	-0.002
11/30/23	10:36:17.244	0.564	-0.027	-0.003
11/30/23	10:37:21.148	7.939	-0.091	-0.006
11/30/23	10:38:25.052	7.750	-0.195	-0.004
11/30/23	10:39:28.962	7.425	-0.209	-0.004
	11/30/23 11/30/23 11/30/23 11/30/23 11/30/23 11/30/23 11/30/23 11/30/23 11/30/23 11/30/23 11/30/23 11/30/23	Date Time 11/30/23 10:25:38.231 11/30/23 10:26:42.135 11/30/23 10:27:46.073 11/30/23 10:28:49.930 11/30/23 10:29:54.024 11/30/23 10:30:57.740 11/30/23 10:32:01.639 11/30/23 10:33:05.541 11/30/23 10:35:13.378 11/30/23 10:36:17.244 11/30/23 10:37:21.148 11/30/23 10:38:25.052 11/30/23 10:39:28.962	11/30/23       10:25:38.231       7.704         11/30/23       10:26:42.135       7.571         11/30/23       10:27:46.073       7.503         11/30/23       10:28:49.930       7.766         11/30/23       10:29:54.024       10.988         11/30/23       10:30:57.740       11.425         11/30/23       10:32:01.639       11.290         11/30/23       10:33:05.541       9.417         11/30/23       10:35:13.378       0.077         11/30/23       10:35:13.378       0.077         11/30/23       10:37:21.148       7.939         11/30/23       10:38:25.052       7.750	11/30/23       10:25:38.231       7.704       -0.206         11/30/23       10:26:42.135       7.571       -0.229         11/30/23       10:27:46.073       7.503       -0.192         11/30/23       10:28:49.930       7.766       -0.208         11/30/23       10:29:54.024       10.988       -0.187         11/30/23       10:30:57.740       11.425       -0.212         11/30/23       10:32:01.639       11.290       -0.218         11/30/23       10:33:05.541       9.417       -0.144         11/30/23       10:34:09.433       0.594       -0.077         11/30/23       10:35:13.378       0.077       -0.038         11/30/23       10:36:17.244       0.564       -0.027         11/30/23       10:37:21.148       7.939       -0.091         11/30/23       10:38:25.052       7.750       -0.195

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill On

Post Run 3 CTS and		te Spike				
Spectrum	Date	Time	HCN PCA 191c R1 191c	HF ppm (10) 191C	SF6 (10) 191C	Ethylene (100,3000) 191C
SPC003807.LAB	44/20/22	11:52:08.233	7.147	-0.192	-0.003	2.744
SPC 003808.LAB		11:53:12.140				
_			6.992	-0.175	-0.007	2.751
SPC003809.LAB		11:54:16.171	7.978	-0.196	0.131	2.587
SPC003810.LAB		11:55:19.933	11.513	-0.200	0.545	2.416
SPC003811.LAB		11:56:24.218	11.060	-0.205	0.476	2.486
SPC003812.LAB	11/30/23	11:57:27.780	10.732	-0.194	0.427	2.562
SPC003813.LAB	11/30/23	11:58:31.979	8.274	-0.084	0.399	1.592
SPC003814.LAB	11/30/23	11:59:35.886	0.416	-0.038	0.008	0.033
SPC003815.LAB	11/30/23	12:00:39.432	0.172	-0.022	-0.008	-0.011
SPC003816.LAB	11/30/23	12:01:43.471	2.855	-0.046	-0.003	0.932
SPC003817.LAB	11/30/23	12:02:47.325	7.615	-0.093	-0.004	3.027
SPC003818.LAB	11/30/23	12:03:51.154	7.687	-0.165	-0.004	2.978
SPC003819.LAB	11/30/23	12:04:55.061	7.789	~0.215	-0.004	3.018
SPC003820.LAB	11/30/23	12:05:58.994	7.597	-0.216	-0.004	2.851
SPC003821.LAB	11/30/23	12:07:02.894	5.943	-0.114	-0.009	10.770
SPC003822.LAB	11/30/23	12:08:06.790	-0.016	-0.041	-0.005	72.292
SPC003823.LAB	11/30/23	12:09:11.005	-0.148	-0.026	-0.009	73.536
SPC003824.LAB	11/30/23	12:10:14.655	-0.142	-0.014	~0.011	73.864
SPC003825.LAB	11/30/23	12:11:18.662	-0.048	-0.005	-0.010	73.846
SPC003826.LAB	11/30/23	12:12:22.480	-0.065	-0.023	-0.007	74.133
SPC003827.LAB	11/30/23	12:13:26.274	0.736	~0.027	-0.010	67.215
SPC_003828.LAB	11/30/23	12:14:30.179	8.806	-0.096	-0.005	4.047

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill Off Pre Run 4 HCN Analyte Spike

Spectrum	Date	Time	HCN PCA 191c R1 191c	HF ppm (10) 191C	SF6 (10) 191C
SPC003907.LAB	11/30/23	13:39:29.055	9.645	-0.175	-0.010
SPC003908.LAB	11/30/23	13:40:32.962	9.598	~0.216	-0.009
SPC003909.LAB	11/30/23	13:41:36.858	10.329	-0.164	0.088
SPC003910.LAB	11/30/23	13:42:40.721	15.836	-0.196	0.847
SPC003911.LAB	11/30/23	13:43:44.629	11.759	-0.169	0.243
SPC003912.LAB	11/30/23	13:44:48.877	13.673	-0.167	0.493
SPC003913.LAB	11/30/23	13:45:52.430	13.559	-0.176	0.466
SPC003914.LAB	11/30/23	13:46:56.342	13.438	-0.193	0.445
SPC003915.LAB	11/30/23	13:48:00.291	13.321	-0.192	0.406
SPC003916.LAB	11/30/23	13:49:04.257	7.370	-0.110	0.130
SPC003917.LAB	11/30/23	13:50:08.144	0.968	-0.036	0.004
SPC003918.LAB	11/30/23	13:51:11.932	0.227	-0.020	-0.006
SPC003919.LAB	11/30/23	13:52:15.850	2.280	-0.026	-0.003
SPC003920.LAB	11/30/23	13:53:19.760	10.340	-0.137	~0.013
SPC003921.LAB	11/30/23	13:54:23.690	9.954	-0.172	-0.011
SPC003922.LAB	11/30/23	13:55:27.604	9.886	-0.165	-0.011
SPC003923.LAB	11/30/23	13:56:31.515	9.809	-0.171	-0.010
SPC 003924.LAB	11/30/23	13:57:35.413	10.067	-0.166	-0.012

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill Off Post Run 4 HCN Analyte Spike

Spectrum	Date	Time
SPC003994.LAB	11/30/23	15:12:23.934
SPC003995.LAB	11/30/23	15:13:27.573
SPC003996.LAB	11/30/23	15:14:31.355
SPC003997.LAB	11/30/23	15:15:35.688
SPC003998.LAB	11/30/23	15:16:39.508
SPC003999.LAB	11/30/23	15:17:43.316
SPC004000.LAB	11/30/23	15:18:47.034
SPC004001.LAB	11/30/23	15:19:50.926
SPC004002.LAB	11/30/23	15:20:54.773
SPC004003.LAB	11/30/23	15:21:58.704
SPC 004004.LA8	11/30/23	15:23:02.963

HCN PCA 191c R1 191c	HF ppm (10) 191C	SF6 (10) 191C
10.596	-0.196	-0.010
10.474	-0.205	-0.008
12.848	-0.185	0.347
14.073	-0.194	0.474
14.019	-0.182	0.454
13.169	-0.191	0.342
0.615	-0.059	0.025
0.148	-0.034	-0.000
7.417	-0.092	-0.005
10.950	-0.225	-0.011
10.725	-0.230	-0.011

Buzzi Unicem; Maryneaf TX Main Stack, Raw Mill Off Post Run 5 HCN Analyte Spike Spectrum Date SPC\_\_004081.LAB 11/30/23 SPC\_\_004082.LAB 11/30/23

Spectrum	Date	Time
SPC004081.LAB	11/30/23	16:45:48.064
SPC_004082.LAB	11/30/23	16:46:52.004
SPC004083.LAB	11/30/23	16:47:56.216
SPC004084.LAB	11/30/23	16:49:00.137
SPC004085.LAB	11/30/23	16:50:03.716
SPC_004086.LAB	11/30/23	16:51:07.575
SPC004087.LAB	11/30/23	16:52:11.596
SPC004088.LAB	11/30/23	16:53:15,366
SPC004089.LAB	11/30/23	16:54:19.328
SPC004090.LAB	11/30/23	16:55:23.562
SPC004091.LAB	11/30/23	16:56:27.199
SPC 004092.LAB	11/30/23	16:57:31.081

HCN PCA 191c R1 191c	_HF ppm (10) 191C	SF6 (10) 191C
11.052	-0.239	-0.011
11.064	-0.251	-0.008
11.960	-0.257	0.165
14.432	-0.201	0.482
14.364	-0.200	0.461
13.612	-0.204	0.349
3.280	-0.064	0.138
0.246	-0.015	0.002
4.999	-0.048	-0.006
11.376	-0.224	-0.010
10.615	-0.241	-0.009
10.762	-0.245	-0.008

Buzzi Unicem; Maryneal TX
Main Stack, Raw Mill Off
Post Run 6 HON Analyte Spike
Spectrum Date Time
SPC\_004179.LAB 11/30/23 18:31:07.393
SPC\_004181.LAB 11/30/23 18:32:10.845
SPC\_004181.LAB 11/30/23 18:33:14.8672
SPC\_004181.LAB 11/30/23 18:35:22.859
SPC\_004183.LAB 11/30/23 18:36:26.454
SPC\_004185.LAB 11/30/23 18:36:26.454
SPC\_004185.LAB 11/30/23 18:36:34.287
SPC\_004185.LAB 11/30/23 18:39:38.147
SPC\_004185.LAB 11/30/23 18:39:38.147
SPC\_004185.LAB 11/30/23 18:39:38.147
SPC\_004185.LAB 11/30/23 18:40:42.431
SPC\_004185.LAB 11/30/23 18:40:42.4916
SPC\_004195.LAB 11/30/23 18:46:57.717
SPC\_004195.LAB 11/30/23 18:46:57.717
SPC\_004195.LAB 11/30/23 18:46:01.566
SPC\_004194.LAB 11/30/23 18:47.05.662
SPC\_004194.LAB 11/30/23 18:47.05.662
SPC\_004194.LAB 11/30/23 18:47.05.662 -0.219 -0.203 -0.203 -0.194 -0.200 -0.049 13,398 0.417 2.852 0.626 0.228 -0.027 -0.014 0.008 -0.050 0.064 -0.003 -0.009 -0.009 -0.015 -0.002 0.003 0.075 2.211 -0.004 -0.016 0.005 0.510 SPC\_004189.LAB SPC\_004190.LAB SPC\_004191.LAB SPC\_004191.LAB SPC\_004193.LAB SPC\_004194.LAB SPC\_004196.LAB SPC\_004196.LAB SPC\_004196.LAB SPC\_004196.LAB -0.224 -0.202 -0.199 -0.098 -0.030 10.542 3.214 3.049 3.073 10.213 0.856 -0.055 11/30/23 18:45:01:506 11/30/23 18:47:05:662 11/30/23 18:49:09:361 11/30/23 18:50:17.158 11/30/23 18:51:21.066 0.139 -0.035 -0.015 -0.028 -0.013 -0.004 0.137 0.005 -0.086 10.430 73.788 0.005 0.082 -0.009 -0.008 73.840

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill On CTS and HCN Direct

Spectrum	Date	Time	HCN PCA 191c R1 191c	HF ppm (10) 191C	SF6 (10) 191C	Ethylene (100,3000) 191C
SPC003645.LAB	11/30/23	08:58:18.068	29.847	-0.013	2.882	-0.025
SPC003646.LAB	11/30/23	08:59:21.972	49.867	-0.030	4.835	-0.504
SPC003647.LAB	11/30/23	09:00:25.885	49.970	-0.015	4.835	-0.460
SPC003648,LAB	11/30/23	09:01:30.186	30.292	0.002	2.696	0.702

Buzzi Unicem; Maryneal TX Main Stack, Raw Mill On CTS and HCN Direct

C 12 and alon pirect						
Spectrum	Date	Time	HCN PCA 191c R1 191c	HF ppm (10) 191C	SF6 (10) 191C	Ethylene (100,3000) 191C
SPC003564BKG.LAB	11/30/23	07:24:27.085	0.000	0.000	0.000	0.000
SPC003565.LAB	11/30/23	07:25:37.733	0.014	-0.006	-0.001	-0.061
SPC003566.LAB	11/30/23	07:26:41.371	-0.080	0.006	-0.020	43.985
SPC003567.LAB	11/30/23	07:27:45.267	-0.228	0.009	-0.010	73.655
SPC003568.LAB	11/30/23	07:28:49.515	-0.229	-0.022	-0.011	73.784
SPC003569.LAB	11/30/23	07:29:53.185	0.009	-0.015	-0.012	73.918
SPC_003570.LAB	11/30/23	07:30:56.969	77.472	0.004	3.499	38.467
SPC_003571.LAB	11/30/23	07:32:00.868	193.908	-0.014	9.564	-0.537
SPC003572.LAB	11/30/23	07:33:04.768	195.330	-0.015	9.546	-0.325
SPC003573.LAB	11/30/23	07:34:08.677	196.749	0.007	9.535	-0.349
SPC003574.LAB	11/30/23	07:35:12.623	197.175	-0.016	9.567	-0.452
SPC003575.LAB	11/30/23	07:36:16.530	198.323	-0.017	9.561	-0.435
SPC003576.LAB	11/30/23	07:37:20.478	198.512	-0.012	9.541	-0.516
SPC003577.LAB	11/30/23	07:38:24.409	109.918	-0.035	4.944	4.122
SPC003578.LAB	11/30/23	07:39:28.420	0.306	-0.009	-0.005	0.478
SPC003579.LAB	11/30/23	07:40:32.184	0.162	-0.014	-0.002	0.488

# Appendix C

Ion Chromatography Analytical Report Data

# Deeco, Inc.

3404 Lake Woodard Drive Raleigh, NC 27604

Project No: 23-3315 Buzzi Unicem

Hydrogen Fluoride & Chlorine

EPA Method 26A Analysis

Analytical Report 41721



Element One, Inc.

6319-D Carolina Beach Rd., Wilmington, NC 28412 910-793-0128 FAX: 910-792-6853 e1lab@e1lab.com

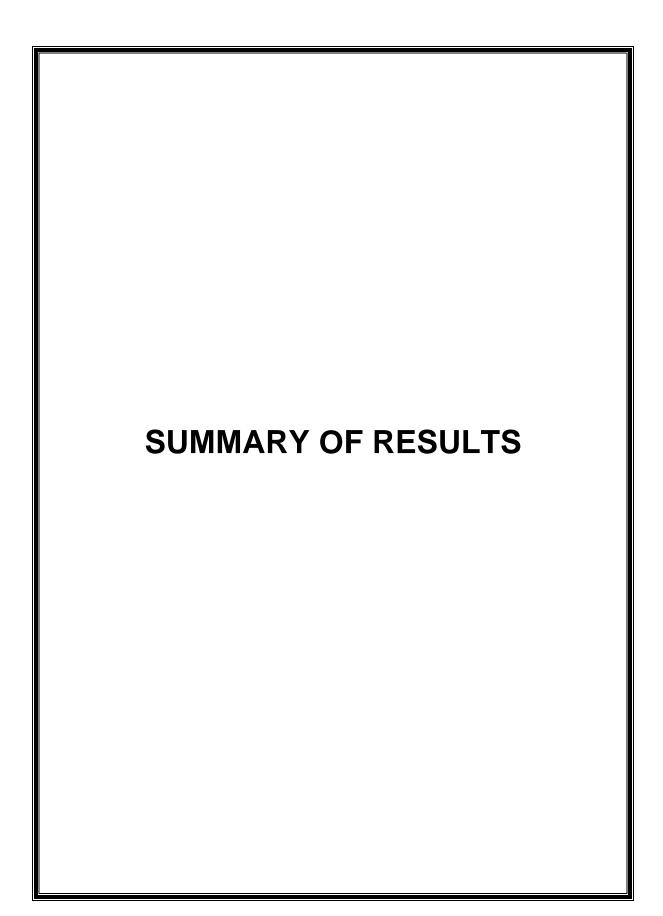
The following data for Analytical Report 41721 has been reviewed for completeness, accuracy, adherence to method protocol, and compliance with quality assurance guidelines.

Review by:

Katie Gattis, Quality Assurance Officer December 27, 2023

Report Reviewed and Finalized by:

Ken Smith, Laboratory Director December 27, 2023



# **Summary of Analysis**

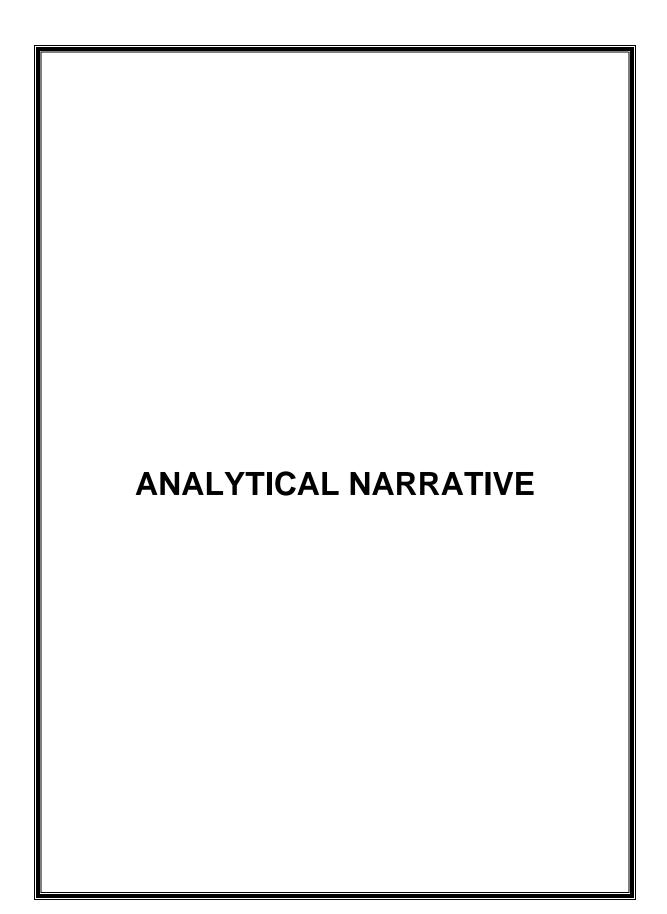
## **Summary of Method 26A Analysis**

	MN- M26A-R1A e41721-1	MN- M26A-R3A e41721-2	MN- M26A-R4A e41721-3
Element	Total mg	Total mg	Total mg
HF	< 0.228	< 0.265	< 0.237
Cl <sub>2</sub>	< 0.154	< 0.167	< 0.167
	MN-	MN-	MN-
	M26A-R5A e41721-4	M26A-R6A e41721-5	M26A-R7A e41721-6
Element	Total mg	Total mg	Total mg
HF	< 0.243	< 0.253	< 0.251
Cl <sub>2</sub>	0.631	0.286	0.580
	MN-	MN-	MN-
	M26A-R1B e41721-7	M26A-R3B e41721-8	M26A-R4B e41721-9
Element	Total mg	Total mg	Total mg
HF	< 0.254	< 0.259	< 0.224
Cl <sub>2</sub>	< 0.148	< 0.193	< 0.156
	MN-	MN-	MN-
	M26A-R5B e41721-10	M26A-R6B e41721-11	M26A-R7B e41721-12
Element	Total mg	Total mg	Total mg
HF	< 0.265	< 0.251	< 0.267
$Cl_2$	0.672	0.306	0.617

	MN- M26A-FBON e41721-13	MN- M26A-FBOFF e41721-14
Element	Total mg	Total mg
HF Cl <sub>2</sub>	< 0.202 < 0.157	< 0.21 < 0.178

### elementOne

Certification: NJ NELAP NC009 41721 Deeco M26A Report Packet Page 4 of 46



### **Element One Analytical Narrative**

Client:	Deeco, Inc.	Element One #:	41721
Client ID:	23-3315 Buzzi Unicem	Analyst:	LAW
Method:	M26A	Dates Received:	12.11.23
Analytes:	HF, Cl <sub>2</sub>	Dates Analyzed:	12.18-21.23

#### **Summary of Analysis**

The samples were prepared and analyzed according to Method 26A protocol. The samples were analyzed for fluoride and chloride on Metrohm 861/788 and 881/858 ion chromatograph systems.

#### **Detection Limits**

The Metrohm reporting limit was 0.1 µg/mL for fluoride and chloride.

#### **Analysis QA/QC**

Duplicate analyses relative percent difference (RPD), spike recovery and second source verification data are summarized in the Quality Control section. All QA/QC data was within the criteria of the method.

#### **Additional Comments**

The reported results have not been corrected for any blank values or spike recovery values. Due to the sample matrix, it was necessary to analyze all samples at a minimum five-fold dilution to reduce interferences and to preserve the anion column. The reported results relate only to the items tested or calibrated.



# **Summary of Quality Control Data**

## **Summary of Method 26A Duplicate Analysis RPD**

(Method 26A	QC limits:	<5% for RPD)
-------------	------------	--------------

	MN-	MN-	MN-
	M26A-R1A	M26A-R3A	M26A-R4A
Element	RPD	RPD	RPD
HF	NA	NA	NA
Cl <sub>2</sub>	NA	NA	NA
	MN-	MN-	MN-
	M26A-R5A	M26A-R6A	M26A-R7A
Element	RPD	RPD	RPD
HF	NA	NA	NA
Cl <sub>2</sub>	2.1%	0.0%	3.6%
	MN-	MN-	MN-
	M26A-R1B	M26A-R3B	M26A-R4B
Element	RPD	RPD 	RPD 
HF	NA	NA	NA
Cl <sub>2</sub>	NA	NA	NA
	MN-	MN-	MN-
	M26A-R5B	M26A-R6B	M26A-R7B
Element	RPD	RPD	RPD
HF	NA	NA	NA
Cl <sub>2</sub>	1.9%	1.0%	4.1%

	MN-	MN-
	M26A-FBON	M26A-FBOFF
Element	RPD	RPD 
HF	NA	NA
$Cl_2$	NA	NA

# **Summary of Quality Control Data**

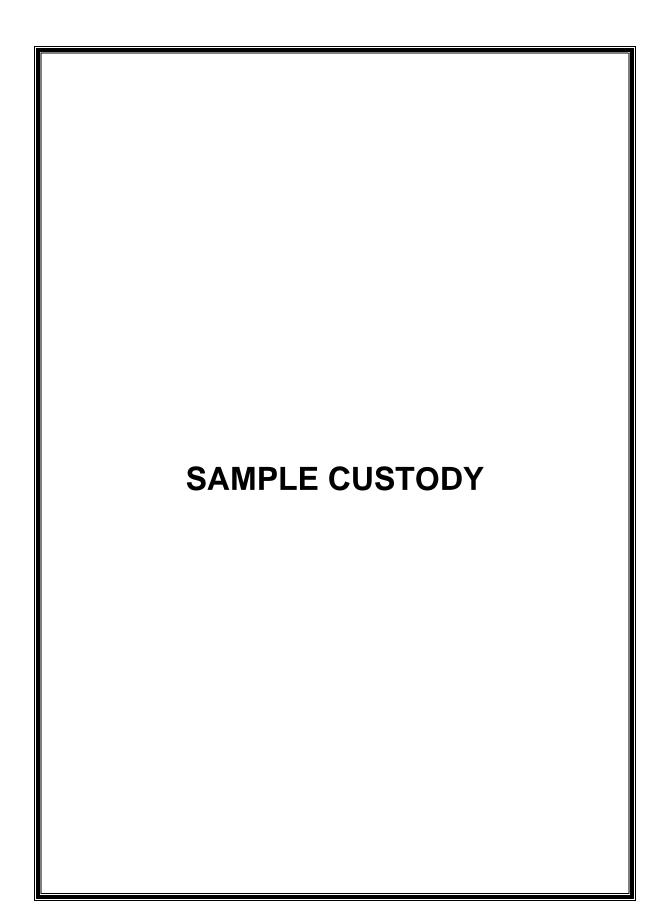
# Summary of Method 26A Spike Recoveries (Method 26A QC limits: 90-110% for Spike Recoveries)

	MN-	MN-
	M26A-R4A	M26A-R4B
Element	Recovery	Recovery
HF	108%	108%
Cl <sub>2</sub>	105%	100%
	RC-	RC-
	M26A-R3A	M26A-R3B
Element	Recovery	Recovery
HF	106%	106%
Cl <sub>2</sub>	101%	101%

#### **Second Source Calibration Verification**

(\*Laboratory QC limits: 90-110%)

	DL 0.1mg/L	*QC 5.0mg/L
Element	Recovery	Recovery
HF e41721 (1-14)	97%	101%
HF e41721 (15-28)	105%	100%
Cl <sub>2</sub> e41721 (1-14)	94%	107%
Cl <sub>2</sub> e41721 (15-28)	109%	102%



Relinquished by: (Signature)  Relinquished by: (Signature)  Relinquished by: (Signature)	Date/Time			_	Train:	Train: EPA Method 26
	ae ae	Plant Location: Maryneal TX			Project Name:	23-3315
		Received by: (Signature)		Date/Time		
		Received by: (Signature)		Date/Time	Comments	
	Date/Time R	Received by: (Signature)		Date/Time	Comments	
Field Sample Date C	Composite or Grab	Analysis Required	Sampling Train	Sample Description	Special Notes	Lab
MN-1A-H <sub>3</sub> SO <sub>4</sub> 11/29/23 C	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 434.0 mL	Element One
MN-1A-NaOH 11/29/23 C	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	Final Volume 308.5 mL Sodium thiosulfate NOT ADDED!	Element One
MN-1B-H <sub>3</sub> SO <sub>4</sub> 11/29/23 C	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>q</sub> and DI Rinses	Final Volume 483.5 mL	Element One
MN-1B-NaOH 11/29/23 C	Сопр.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	Final Volume 296.1 mL Sodium thiosulfate NOT ADDED!	Element One
MN-3A-H <sub>2</sub> SO <sub>4</sub> 11/30/23 C	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 504.1 mL	Element One
MN-3A-NaOH 11/30/23 C	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 333.1 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
MN-3B-H <sub>2</sub> SO <sub>4</sub> 11/30/23 C	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 492.8 mL	Element One
MN-3B-NaOH 11/30/23 C	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volums 325.2 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One

### elementOne

Certification: NJ NELAP NC009 41721 Deeco M26A Report Packet Page 13 of 46

			DEECO, Inc. 3404 Lake Woodard Dr. Raleigh, NC 27604 919-250-0285			Date: Lab: Train:	21/12/10/23  Lab: Element One  Train: EPA Method 26
Plant Name: Buzzi Unicem			Plant Location: Maryneal TX			Project Name:	23-3315
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time (2-//-λ.)	Comments	
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time	Comments	
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time Comments	Comments	
Field Sample No.	Date	Composite or Grab	Analysis Required	Sampling Train	Sample Description	Special Notes	Lab
MN-4A-H <sub>2</sub> SO <sub>4</sub>	£2/0£/11	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 447.4 mL	Element One
MN-4A-NaOH	11/30/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	Final Volume 333.6 mL Sodium thiosulfate NOT ADDED!	Element One
MN-4B-H <sub>2</sub> SO <sub>4</sub>	11/30/23	Сотр.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H₂SO₄ and DI Rinses	Final Volume 425.8 mL	Element One
MN-4B-NaOH	11/30/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	Final Volume 312.2 mL Sodium thiosulfate NOT ADDED!	Element One
MN-5A-H <sub>2</sub> SO <sub>4</sub>	11/30/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 461.7 mL	Element One
MN-5A-NaOH	11/30/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 333.8 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
MN-5B-H <sub>2</sub> SO <sub>4</sub>	11/30/23	Сотр.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 503.1 mL	Element One
MN-5B-NaOH	11/30/23	Сотр.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 358.9 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One

			DEECO, Ind 3404 Lake Woodard Dr. Raleigh, NC 27604 919-250-0285			Ud ( Date: Lab: Train:	4172人 Date: 12/10/23 Lab: Element One Train: EPA Method 26
Plant Name: Buzzi Unicem			Plant Location: Maryneal TX			Project Name:	23-3315
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time  2-(1-23	Comments	
Relinquished by: (Signature)		шв	Received by: (Signature)		Date/Time	Comments	
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time Comments	Comments	
Field Sample No.	Date	Composite or Grab	Analysis Required	Sampling Train	Sample Description	Special Notes	Lab
MN-6A-H <sub>2</sub> SO <sub>4</sub>	11/30/23	Сотр.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 479.8 mL	Element One
MN-6A-NaOH	11/30/23	Сотр.	Chloride ion as Chlorine (Cl.)	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 338.3 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
MN-6B-H <sub>2</sub> SO <sub>4</sub>	11/30/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 477.4 mL	Element One
MN-6B-NaOH	11/30/23	Сотр.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	Final Volume 311.5 mL Sodium thiosulfate NOT ADDED!	Element One
MN-7A-H <sub>2</sub> SO <sub>4</sub>	11/30/23	Сотр.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 476.5 mL	Element One
MN-7A-NaOH	11/30/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 352.3 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
MN-7B-H <sub>2</sub> SO <sub>4</sub>	11/30/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 507.1 mL	Element One
MN-7B-NaOH	11/30/23	Сотр.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 337.5 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One

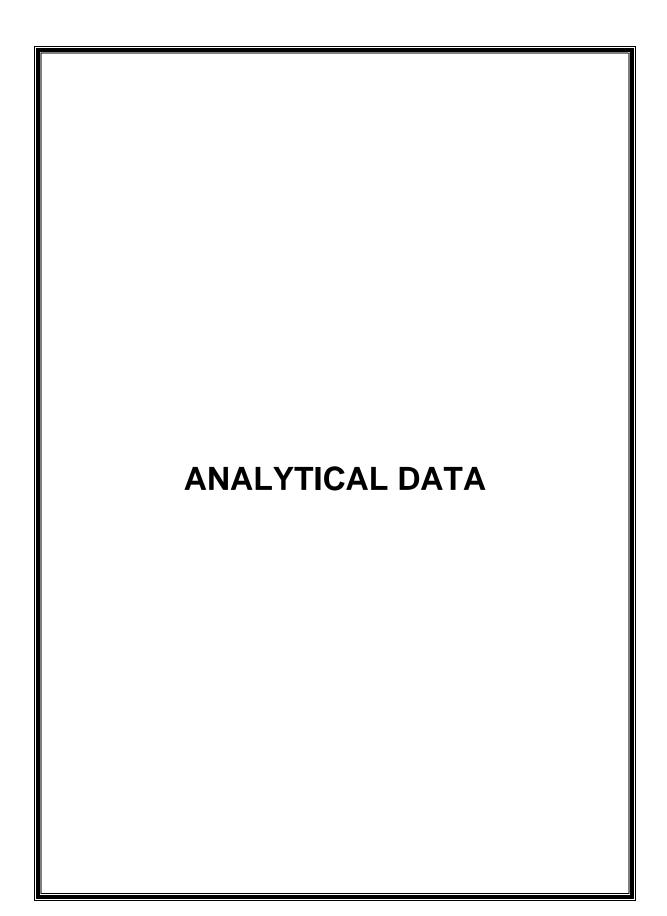
			DEECO, Ind 3404 Lake Woodard Dr. Raleigh, NC 27604 919-250-0285			HIT Date: Lab: Train: E	
Plant Name: Buzzi Unicem			Plant Location: Maryneal TX			Project Name:	23-3315
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time Comments	Comments }	
Relinquished by: (Signature)		Date/Thme	Date/Time Received by: (Signature)		Date/Time	Comments	
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time	Comments	
Field Sample No.	Date	Composite or Grab	Analysis Required	Sampling Train	Sample Description	Special Notes	Lab
MN-FBON-H <sub>2</sub> SO <sub>4</sub>	11/30/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 384.3 mL Element One	Element One
MN-FBON-NaOH	11/30/23	Сотр.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 313.8 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
MN-FBOFF-H <sub>2</sub> SO <sub>4</sub>	11/30/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 399.1 mL Element One	Element One
MN-FBOFF-NaOH	11/30/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 355.9 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One

			DEECO, Ind. 3404 Lake Woodard Dr. Raleigh, NC 27604 919-250-0285			└┤	
Plant Name: Buzzi Unicem			Plant Location: Festus MO			Project Name:	23-3317
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time	Comments	
Relinquished by: (Signature)		Date/Time	Received by: (Signature)			Comments	
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time Comments	Comments	
Field Sample No.	Date	Composite or Grab	Analysis Required	Sampling Train	Sample Description	Special Notes	Lab
RC-1A-H <sub>2</sub> SO <sub>6</sub>	12/05/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 422.6 mL	Element One
RC-1A-NaOH	12/05/23	Сотр.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 296.6 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
RC-1B-H <sub>2</sub> SO <sub>4</sub>	12/05/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 498.6 mL	Element One
RC-1B-NaOH	12/05/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	Final Volume 297.1 mL Sodium thiosulfate NOT ADDED!	Element One
RC-2A-H <sub>2</sub> SO <sub>4</sub>	12/05/23	Сотр.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 436.5 mL	Element One
RC-2A-NaOH	12/05/23	Comp.	Chloride ion as Chlorine (CL <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 339.0 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
RC-2B-H <sub>2</sub> SO <sub>4</sub>	12/05/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H₂SO₄ and DI Rinses	Final Volume 436.0 mL	Element One
RC-2B-NaOH	12/05/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 324.8 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One

,			DEECO, Inc. 3404 Lake Woodard Dr. Raleigh, NC 27604 919-250-0285			HITZ Date: Lab: Train:	
Plant Name: Buzzi Unicem			Plant Location: Festus MO			Project Name:	23-3317
Relinquished by: (Signature)	,	Date/Time	Date/Time Received by: (Signature)		Date/Time	Comments ?	
Relinquished by: (Signature)		Date/Time	Date/Time  Réceived by: (Signature)		Date/Time	Comments	
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time	Comments	
Field Sample No.	Date	Composite or Grab	Analysis Required	Sampling Train	Sample Description	Special Notes	Lab
RC-3A-H <sub>3</sub> SO <sub>4</sub>	12/06/23	Сотр.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 482.2 mL	Element One
RC-3A-NaOH	12/06/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 349.4 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
RC-3B-H <sub>2</sub> SO <sub>4</sub>	12/06/23	Сотр.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 469.8 mL	Element One
RC-3B-NaOH	12/06/23	Сотр.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 3343.6mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
RC-4A-H <sub>2</sub> SO <sub>4</sub>	12/06/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 432.0 mL Element One	Element One
RC-4A-NaOH	12/06/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 347.0 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
RC-4B-H <sub>3</sub> SO <sub>4</sub>	12/06/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 461.3 mL	Element One
RC-4B-NaOH	12/06/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 341.0 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One

			DEECO, Inc 3404 Lake Woodard Dr. Raleigh, NC 27604 919-250-0285			∠   ¬ Date: Lab: Train:	
Plant Name: Buzzi Unicem			Plant Location: Festus MO			Project Name:	23-3317
Relinquished by: (Signature)		Date/Time	Received by: (Signature)		Date/Time /2//-//	Comments	
Relinquished by: (Signature)		e e	Received by: (Signature)		Date/Time	Comments	
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time Comments	Comments	
Field Sample No.	Date	Composite or Grab	Analysis Required	Sampling Train	Sample Description	Special Notes	Lab
RC-5A-H <sub>2</sub> SO <sub>4</sub>	12/06/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 433.1 mL.	Element One
RC-5A-NaOH	12/06/23	Сотр.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	Final Volume 282.2 mL Sodium thiosulfate NOT ADDED!	Element One
RC-5B-H <sub>2</sub> SO <sub>4</sub>	12/06/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 463.3 mL	Element One
RC-5B-NaOH	12/06/23	Сотр.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	Final Volume 329.1 mL Sodium thiosulfate NOT ADDED!	Element One
RC-6A-H <sub>2</sub> SO <sub>4</sub>	12/06/23	Сопр.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 437.9 mL	Element One
RC-6A-NaOH	12/06/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 328.5 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
RC-6B-H <sub>2</sub> SO <sub>4</sub>	12/06/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 464.0 mL	Element One
RC-6B-NaOH	12/06/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26A	аОН	Final Volume 346.4 mL Sodium thiosulfate NOT ADDED!	Element One

			DEECO, Ind 3404 Lake Woodard Dr. Raleigh, NC 27604 919-250-0285			Date: Lab: Train:	U(172∫ ( Date: 12/10/23 Lab: Element One Train: EPA Method 26
Plant Name: Buzzi Unicem			Plant Location: Festus MO			Project Name:	23-3317
Relinquished by: (Signature)		Date/Time (2/1)	Date/Time Received by: (Signature)		Date/Time Comments  \langle \lambda_i \lambda_i \lambda_j	Comments	
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time Comments	Comments	
Relinquished by: (Signature)		Date/Time	Date/Time Received by: (Signature)		Date/Time	Comments	
Field Sample No.	Date	Composite or Grab	Analysis Required	Sampling Train	Sample Description	Special Notes	Lab
RC-FBON-H <sub>2</sub> SO <sub>4</sub>	12/06/23	Сошр.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 419.0 mL Element One	Element One
RC-FBON-NaOH	12/06/23	Comp.	Chloride ion as Chlorine (Cl <sub>2</sub> )	EPA Method 26a	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 341.0 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
RC-FBOFF-H <sub>2</sub> SO <sub>4</sub>	12/06/23	Comp.	Fluoride ion as Hydrogen Fluoride	EPA Method 26A	0.1N H <sub>2</sub> SO <sub>4</sub> and DI Rinses	Final Volume 420.7 mL	Element One
RC-FBOFF-NaOH	12/06/23	Comp.	Chloride ion as Chlorine (CL <sub>2</sub> )	EPA Method 26A	0.1N NaOH and DI Rinses	0.1N NaOH Final Volume 334.7 mL and DI Sodium thiosulfate Rinses NOT ADDED!	Element One
	12/06/23						
	12/06/23						



# **Analytical Calculations**

HF-

Total HX (mg) = [X Results (μg/mL)\*Dilution\*Beginning Vol (mL)]\*Correction Factor 1000

#### Where-

X Results= Raw sample concentration (ppm) — IC Data Sheet

Dilution= <u>Diluted Volume</u>—IC Run Sheet Aliquot

Beginning Volume--Sample Submission

1.053= Correction factor for hydrogen fluoride

Cl<sub>2</sub> -

Total  $X_2$  (mg) = X Results ( $\mu$ g/mL)\*Dilution\*Beginning Volume (mL) 1000

#### Where-

X Results= Raw sample concentration (ppm)—Cl2 IC Data Sheet

Dilution= <u>Diluted Volume</u>—IC Run Sheet Aliquot

Beginning Volume--Sample Submission

# **Analytical Calculations**

## Spike Recovery-

Spike (%) = (Spiked Result (
$$\mu$$
g/mL) – Sample Result ( $\mu$ g/mL)) X100  
Spike Amount ( $\mu$ g/mL)

### Where-

Spike Result = Raw sample concentration (ppm)--IC-Data Sheet

Sample Result = Raw sample concentration (ppm)--IC-Data Sheet

Spike Amount—IC-Data Sheet

## **Duplicate Analysis RPD-**

RPD (%) = (Duplicate Result ( $\mu$ g/mL) - Sample Result ( $\mu$ g/mL)) X100 Average (µg/mL)

#### Where-

Sample Result and Duplicate Results=Raw sample concentration (ppm)--IC-Data Sheet

Average= (<u>Duplicate + Sample Results)</u>
2

Client: Deeco, Ir Project No 23-3315 Volume Marked Y N	nc.						FORM			
Project No 23-3315  Volume Marked Y  (N)	nc.						Analys	is Due Da	te 12.20	0.23
Project No 23-3315  Volume Marked Y  (N)	nc.					QA/		ort Due Da		
Project No 23-3315  Volume Marked Y  (N)								Date Rec	12.11.	23
Y (N)								Time Rec	1100	
Y (N)	Volume L	nee		FH pH <	2	∠BH ph	1 > 8	R	ef. Method	ı:
	Y (N		N		N	(Y)	N	'	26A	
OI-I-I			-(	)	.,	0				
Sample Identification	n							,		
1 MN-M26A-R1A			7		26A-R1B		13	MN-M26A		
2 MN-M26A-R3A			8		26A-R3B		14	MN-M26A	-FBOFF	
3 MN-M26A-R4A			9		26A-R4B					
MN-M26A-R4A	Spike				26A-R4B S	pike				
4 MN-M26A-R5A			10		26A-R5B					
5 MN-M26A-R6A			11		26A-R6B					
6 MN-M26A-R7A			12		26A-R7B					
Analyeee Beaucata		nples 1-14		HF						
Analyses Requeste	Sam	ples 1-14		Cl <sub>2</sub>						
Runs/FB										
	pinger 1 bined Imp)	FH In	nping	er 2	FH Im	pinger 3	BH Imp (or Comb	pinger 4 pined Imp)	BH Imp	inger 5
Lab ID BV, ml	FV, ml	BV, ml		₹V, ml	BV, ml	FV, ml	BV, ml	FV, ml	BV, ml	FV, ml
1	434.0		$\perp$					801.5		
2	504.1							333.1		
3.S	449.4							333.W	-	-
4	461.7		_ [ _			_				
			_					353.8		
5	4718							355.8 355.3		
3	476.5							353.8 335.3 352.3		
5 3 7	476.5 483.5							353.8 335.3 352.3 296.\		
5 3 7 8	476.5 483.5 492.8							353.8 358.3 352.3 296.\ 3 <b>3</b> 5.2		
5 3 7 8 9.S	476.5 483.5 492.8 425.8							353.8 338.3 352.3 296.1 3 <b>2</b> 5.2 312.2		
5 6 7 8 9.S	476.5 483.5 492.8							353.8 338.3 352.3 296.\ 3 <b>2</b> 5.2 312.2 358.9		
5 6 7 8 9.S 10	476.5 483.5 492.8 425.8 503.1							353.8 335.3 352.3 296.1 3 <b>2</b> 5.2 312.2 358.9 311.5		
5 6 7 8 9.S 10 11	476.5 473.5 492.8 425.8 503.1 477.9 507.1							353.8 335.3 352.3 296.1 3 <b>2</b> 5.2 312.2 358.9 311.5 337.5		
5 6 7 8 9.S 10 11 12 13	476.5 483.5 492.8 425.8 503.1							353.8 335.3 352.3 296.1 3 <b>2</b> 5.2 312.2 358.9 311.5		

								QA	•	is Due Da ort Due Da		
Client	Deeco, I	nc.								Date Rec	12.11	.23
Projec	t No 23-3315									Time Rec	1100	
Volu	ume Marked	Volu	me Los	ss		FH pH	< 2	BH ph	1 > 8	R	ef. Method	t:
Υ	(N)	Υ	(N)	?	(	)	N	(Ý)	N	]	26A	
Samp	ole Identification	on										
15	RC-M26A-R1A				21	RC-M2	26A-R1B		27	RC-M26A	-FBON	
16	RC-M26A-R2A				22	RC-M2	26A-R2B		28	RC-M26A	-FBOFF	
17	RC-M26A-R3A				23	RC-M2	26A-R3B					
	RC-M26A-R3A	Spike				RC-M2	26A-R3B S	pike				
18	RC-M26A-R4A				24	RC-M2	26A-R4B					
	RC-M26A-R5A				25		26A-R5B					
20	RC-M26A-R6A				26	RC-M2	26A-R6B					
Analy	ses Requeste	d	Sample	es 15-28	3	HF						
			Sample	es 15-28	3	Cl <sub>2</sub>						
Runs	/FB											
		npinger 1 nbined Im		FH Im	ping	er 2	FH Imp	pinger 3		oinger 4 sined Imp)	BH Imp	inger 5
ab ID		FV,		BV, ml	F	V, ml	BV, ml	FV, ml	BV, ml	FV, ml	BV, ml	FV, ml
5		411	.(0							196.6		
6		45U.								3391-0		
7.S		482:								349.4		
8		932.								341.0		
9		433.	1							282.2		
0		437.								328.5		
1		498	1.1							297.1		
2		486e		-						324.8		
3.S		469	1.8							343.6		
		461	.3							341.0		
		4(13	.3							329.1		
4		464	.0							344.4		
24 25 26		-1001			-	_	-			341.0		
24		410	_		_		_	-				-
24 25 26 27		-	.0							334.7		
4 5 6 7 8 <b>Reag</b>	ent Blanks	410	.0							334.7		
4 5 6 7 8 <b>Reag</b>	) Fraction	410 410	.0	FV, ml					Notes	334.7		
4 5 6 7 8 <b>Reag</b>	0.1 N H <sub>2</sub>	410 410 504	.0	FV, ml					Notes	334.7		
24 25 26 27	) Fraction	410 410 504	.0	FV, ml					Notes	334.7		

### M26A-HF IC Data Sheet

Lab ID #: 41721 (1-14)

Client: Deeco

Column: IonPac AS14A

Date: 12.20.23

Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0 mM NaHCO<sub>3</sub>

Analyst: LAW

Flow Rate: 1.0 mL/min.

Detection Limit, (µg/ml): 0.10

F to HF factor: 1.053

w	
7/0	

Sample ID	F' μg/ml	Dilution	Final Vol, ml	HF, Total mg	Spike, µg/ml	Recovery/ RPD	File Name	Date Time
LRB	0.000	1	10	< 0.001			_2023-12-18_	12/18/2023 14:57
LRB	0.000	1	10	< 0.001		NA	_2023-12-18_	12/18/2023 15:16
LRB SPK	5.100	1	10	0.054	5.00	102%	_2023-12-18_	12/18/2023 15:34
LRB SPK	4.942	1	10	0.052	5.00	99%	_2023-12-18_	12/18/2023 15:53
41721-1	0.000	5	434.0	< 0.228			_2023-12-18_	12/18/2023 17:27
41721-1 DUP	0.000	5	434.0	< 0.228		NA	_2023-12-18_	12/18/2023 17:46
41721-2	0.000	5	504.1	< 0.265			_2023-12-18_	12/18/2023 20:34
41721-2 DUP	0.082	5	504.1	< 0.265		NA	_2023-12-18_	12/18/2023 20:53
41721-3	0.000	5	449.4	< 0.237			_2023-12-18_	12/18/2023 18:04
41721-3 DUP	0.000	5	449.4	< 0.237		NA	_2023-12-18_	12/18/2023 18:23
41731-3 SPK	5.429	5	449.4	12.84	5.00	109%	_2023-12-18_	12/18/2023 18:42
41721-3 SPK DUP	5.318	5	449.4	12.58	5.00	106%	_2023-12-18_	12/18/2023 19:00
41721-4	0.000	5	461.0	< 0.243			_2023-12-18_	12/18/2023 21:12
41721-4 DUP	0.000	5	461.7	< 0.243		NA	_2023-12-18_	12/18/2023 21:30
41721-5	0.000	5	479.8	< 0.253			_2023-12-18_	12/18/2023 21:49
41721-5 DUP	0.000	5	479.8	< 0.253		NA	_2023-12-18_	12/18/2023 22:08
41721-6	0.000	5	476.5	< 0.251			_2023-12-18_	12/18/2023 22:26
41721-6 DUP	0.000	5	476.5	< 0.251		NA	_2023-12-18_	12/18/2023 22:45
41721-7	0.000	5	483.5	< 0.254			_2023-12-18_	12/18/2023 23:04
41721-7 DUP	0.081	5	483.5	< 0.254		NA	_2023-12-18_	12/18/2023 23:23
41721-8	0.000	5	492.8	< 0.259			_2023-12-19_	12/19/2023 0:56
41721-8 DUP	0.079	5	492.8	< 0.259		NA	_2023-12-19_	12/19/2023 1:15
41721-9	0.073	. 5	425.8	< 0.224			_2023-12-19_	12/19/2023 1:34
41721-9 DUP	0.066	5	425.8	< 0.224		NA	_2023-12-19_	12/19/2023 1:53
41721-9 SPK	5.466	5	425.8	12.2	5.00	108%	_2023-12-19_	12/19/2023 2:11
41721-9 SPK DUP	5.459	5	425.8	12.2	5.00	108%	_2023-12-19_	12/19/2023 2:30
41721-10	0.097	5	503.1	< 0.265			_2023-12-19_	12/19/2023 2:49
41721-10 DUP	0.047	5	503.1	< 0.265		NA	_2023-12-19_	12/19/2023 3:07
41721-11	0.076	5	477.4	< 0.251			_2023-12-19_	12/19/2023 3:26
41721-11 DUP	0.073	5	477.4	< 0.251		NA	_2023-12-19_	12/19/2023 3:45
41721-12	0.094	5	507.1	< 0.267			_2023-12-19_	12/19/2023 5:19
41721-12 DUP	0.081	5	507.1	< 0.267		NA	_2023-12-19_	12/19/2023 5:37
41721-13 FB ON	0.000	5	384.3	< 0.202			_2023-12-19_	12/19/2023 5:56
41721-13 FB ON DUP	0.000	5	384.3	< 0.202		NA	_2023-12-19_	12/19/2023 6:15
41721-14 FB OFF	0.000	5	399.1	< 0.21			_2023-12-19_	12/19/2023 6:34
41721-14 FB OFF DUF	0.000	5	399.1	< 0.21		NA	_2023-12-19_	12/19/2023 6:52

elementOne

e 41721-HF

HF Data 1 of 2

Surk fach

M26A-HF IC Data Sheet

Lab ID #: 41721 (1-14)

Client: Deeco

Column: IonPac AS14A

Date: 12.20.23

Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0 mM NaHCO<sub>3</sub>

Analyst: LAW

Flow Rate: 1.0 mL/min.

Detection Limit, (µg/ml): 0.10

0 F to HF factor: 1.053

Standards	F µg/ml D	ilution	QC, µg/ml	% Relative Error	% Recovery	File Name	Date Time
0	0.000					_2023-12-18_	12/18/2023 11:12
0.1	0.102			2.0%	102%	_2023-12-18_	12/18/2023 11:31
1	0.962			-3.8%	96%	_2023-12-18_	12/18/2023 11:50
3	3.041			1.4%	101%	_2023-12-18_	12/18/2023 12:08
5	5.008			0.2%	100%	_2023-12-18_	12/18/2023 12:27
10	9.987			-0.1%	100%	_2023-12-18_	12/18/2023 12:46
0.1	0.110			10.0%	110%	_2023-12-19_	12/19/2023 8:45
1	0.932			-6.8%	93%	_2023-12-19_	12/19/2023 9:03
3	3.071			2.4%	102%	_2023-12-19_	12/19/2023 9:22
5	5.126			2.5%	103%	_2023-12-19_	12/19/2023 9:41
10	10.109			1.1%	101%	_2023-12-19_	12/19/2023 10:00
Correlation-	0.999788						
QC	5.028		5.00		101%	_2023-12-18_	12/18/2023 13:05
QC	4.832		5.00		97%	_2023-12-18_	12/18/2023 13:23
QC	4.819		5.00		96%	_2023-12-18_	12/18/2023 17:08
QC	5.178		5.00		104%	_2023-12-18_	12/18/2023 19:19
QC	4.933		5.00		99%	_2023-12-18_	12/18/2023 19:38
QC	5.176		5.00		104%	_2023-12-18_	12/18/2023 23:41
QC	5.199		5.00		104%	_2023-12-19_	12/19/2023 0:00
QC	10.104		5.00		202%	_2023-12-19_	12/19/2023 4:04
QC	5.117		5.00		102%	_2023-12-19_	12/19/2023 4:22
QC	5.089		5.00		102%	_2023-12-19_	12/19/2023 7:48
QC	5.084		5.00		102%	_2023-12-19_	12/19/2023 10:18
DL	0.097		0.10		97%	_2023-12-18_	12/18/2023 14:19
DL	0.110		0.10		110%	_2023-12-18_	12/18/2023 14:38
DL	0.105		0.10		105%	_2023-12-19_	12/19/2023 8:07
DL	0.110		0.10		110%	_2023-12-19_	12/19/2023 10:37
36738-5 QC DUP	6.651	1	6.96		101%	_2023-12-19_	12/19/2023 7:30
BLK	0.000					_2023-12-18_	12/18/2023 13:42
BLK	0.000					_2023-12-18_	12/18/2023 14:01
BLK	0.144					_2023-12-18_	12/18/2023 19:57
BLK	0.000					_2023-12-18_	12/18/2023 20:15
BLK	0.000					_2023-12-19_	12/19/2023 0:19
BLK	0.000					_2023-12-19_	12/19/2023 0:38
BLK	0.000					_2023-12-19_	12/19/2023 4:41
BLK	0.000					_2023-12-19_	12/19/2023 5:00
BLK	0.000					_2023-12-19_	12/19/2023 8:26
BLK	0.000					_2023-12-19_	12/19/2023 10:56

elementOne

HF Data 2 of 2

e 41721-HF

### IC Sample Sheet/Digestion Worksheet

Lab ID #:41721 (1-14)

Date: 12.1823

Column: IonPac AS14A

Instrument: % 1784

Analyst: Lwo

Conc. Eluent: 8:0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0mM NaHCO<sub>3</sub>

Lot# 141-871

Batch name: 12/823-417-21

10mL Conc. Eluent Diluted to FV=1L with filtered UPDI Regenerant: 100 mM H<sub>3</sub>PO<sub>4</sub>

Lot # 1011-103-2

Flow Rate: 1.0 mL/min.

Method: 300/26A

				1.0 mL/min. Results	Results	Method:	Wt (g) /
AS LOC.	Sample ID	Client	Analyte	(ug/mL)	(ug/mL)	Dilution	FV (mL)
	00			<u>GC</u>	MANI	R2	
2	G-(		1	BBC5US74	Symultherica	,9998	
3	[.5						
4	30						
ک	56						
Ь	10-0						
マ	Ó.						
8	€						
9	Blk						
10	BVL						
\	DC						
12	br.						
13	Les						
19	URB						
15	URBY						
/6	LREX						
17	41721-1	Decco	HF			. 2×	
18	-12	1					
19	-3						1
20_	-3 -3 b -34				_		
21	-34				5.429		
22	-3+D	レン	V		5318	U.	
23	6C					1	
24	G£.						
25	BK						

Manual integrations noted by M	
Curve IC Lot # \C\\-\84 \ Comments: \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	
Spike 50 uL from 1000 ug/mL Std. to 10mL sample Lot #s: IC ME Solution 230804-250 W IC NO2 Solution 2368942-250149	
QC: Spike 50 uL from 1000 ug/mL F, Cl, Br, and SO <sub>4</sub> Std. to 10mL sample; lot #'s listied above.	
QC: Spike 20 uL from 1000 ug/mL NO <sub>2</sub> , NO <sub>3</sub> , and PO <sub>4</sub> Std. to 10mL sample; lot #'s listed above.	
Submitted for QC- Date: Time: By: QC Review- Date: Time: By:	

### IC Sample Sheet/Digestion Worksheet

HF Lab ID #: 41721 (1-14)

Date: 121823

Column: IonPac AS14A

Instrument: 361 1788

Analyst: المنا

Conc. Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0mM NaHCO<sub>3</sub>

Conc. Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0mm Na<sub>1</sub>CO<sub>3</sub> 20... \ 10mL Conc. Eluent Diluted to FV=1L with filtered UPDI Regenerant: 100 mM H<sub>3</sub>PO<sub>4</sub> Lot # \C\\ -103 -2

Lot# 1011-821

Batch name: 121823-41 72 \

Flow Rate: 1.0 mL/min.

Method: 300/26A

AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)
26	BIK						
27	41721-2	Decco	HF			5×	
28	-2D	<u> </u>	1				
29	-4				~		
30	-4D -5 -5p						
31	-5						
32	-5p						
33	- b						
34	-60	1					
35	-2						
3.	-70	J				V	
37	G€						
38	GC						
39	Plk						
40	BIV						
41	41921 - 8	Deeco	HF			5×	
42	-8D		-		_	-	-
43	-9						
પવ	-9D_						
us	-9+				5466		
પદ્	91D				5459		
५२	-10						
48	-10D						
49	-11						
SD	-11 D						

Manual integrations noted by M		- 62		
Curve IC Lot #	_Comments:	pg 201)		
Spike 50 uL from 1000 ug/ml/ Std. to	) 10mL sample Lot #	s: IC ME Solution	IC NO/2 So	lution
QC: Spike 50 uL from 1000 ug/mL F				
QC: Spike 20 ul. from 1900 ug/m/L N	IO2, NO3, and PO4 S	Std. to 10mL sample; lo	xt #'s listed above	/
Submitted for QC- Date:	Time:	By: QC F	Review- Date:Tip	ne: By:
/			ζ ′	

		#F Lab ID #: 41721 (1-4)
elementOne	IC Sample Sheet/Digestion Worksheet	Lab ID#: 41721 (1-14)
Date: 12-1823 Analyst: しんい	Column: IonPac AS14A Conc. Eluent: 8.0 mM Na <sub>2</sub> CO <sub>3</sub> / 1.0mM NaHCO <sub>3</sub>	Instrument: 861   288 Lot# 101(-827

Batch name: 12|823-4|72\

10mL Conc. Eluent Diluted to FV=1L with filtered UPDI
Regenerant: 100 mM H₃PO₄

Flow Rate: 1.0 mL/min.

Method: 300/26A

AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)
51	€ 1000h						
52	Ge som	·					
53	BL						
SY	BIL						
<i>5</i> 5	41721-12	Decco	HF			5×	
56	-120		i		_	1	
54	-13 FBaN						
54	-13 FBUND						
59	- 14 PBOFF						
66	-14 FBGAFD	· 5			-		
10	36734-5-66				5/1/4	ĺΧ	TV=696
62	3-60				6-651	1×	
63	Œ						
64	DL						
65	BIL						
66	64						
67	1.0						
68	3-0						
69	5.6						
10	10:0						
71	EL.						
XL	DL						
23	BIL						
74							
15							

Manual integrations noted by M
Curve IC Lot #Comments:ps_3o(`)
Spike 50 uL from 1000 ug/ml/Std. to 10/nL sample Lot #'s: IC ME Solution
QC; Spike 50 uL from 1000/ug/mL F, Øl, Br, and SO <sub>4</sub> Std. to 10mL sample; lot #'s listied/above./
QC: Spike 20 uL from 10g/b ug/mL lybo, NO <sub>3</sub> , and PO <sub>4</sub> Std. to 10mL sample; lot #s listed above.
Submitted for QC- Date: Time: By: QC Review- Date: Time: By:
,

M26A-HF IC Data Sheet

Lab ID #: 41721 (15-28)

Client: Deeco

Column: IonPac AS14A

Date: 12.22.23

Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0 mM NaHCO<sub>3</sub>

Analyst: LAW

Flow Rate: 1.0 mL/min.

Detection Limit, (µg/ml): 0.10

F to HF factor: 1.053

						- %		
Sample ID	F' µg/ml	Dilution	Final Vol, ml	HF, Total mg	Spike, µg/ml	Recovery/ RPD	File Name	Date Time
LRB	0.000	1	10	< 0.001			_2023-12-19_	12/19/2023 21:14
LRB	0.000	1	10	< 0.001		NA	_2023-12-19_	12/19/2023 21:33
LRB SPK	5.044	1	10	0.053	5.00	101%	2023-12-19_	12/19/2023 21:52
LRB SPK	5.013	1	10	0.053	5.00	100%	2023-12-19	12/19/2023 22:10
41721-15	0.036	5	422.6	< 0.222			2023-12-19_	12/19/2023 22:29
41721-15 DUP	0.036	5	422.6	< 0.222		NA	2023-12-19	12/19/2023 22:48
41721-16	0.036	5	436.5	< 0.23			2023-12-20_	12/20/2023 1:36
41721-16 DUP	0.035	5	436.5	< 0.23		NA.	_2023-12-20_	12/20/2023 1:55
41721-17	0.032	5	482.2	< 0.254			_2023-12-19_	12/19/2023 23:07
41721-17 DUP	0.032	5	482.2	< 0.254		NA	_2023-12-19_	12/19/2023 23:25
41721-17 SPK	5.388	5	482.2	13.67	5.00	107%	_2023-12-19_	12/19/2023 23:44
41721-17 SPK DUP	5.234	5	482.2	13.28	5.00	104%	_2023-12-20_	12/20/2023 0:03
41721-18	0.033	5	432.0	< 0.227			_2023-12-20_	12/20/2023 2:14
41721-18 DUP	0.056	5	432.0	< 0.227		NA	_2023-12-20_	12/20/2023 2:33
41721-19	0.058	5	433.1	< 0.228			_2023-12-20_	12/20/2023 2:51
41721-19 DUP	0.066	5	433.1	< 0.228		NA	_2023-12-20_	12/20/2023 3:10
41721-20	0.050	5	437.9	< 0.23			_2023-12-20_	12/20/2023 3:29
41721-20 DUP	0.043	5	437.9	< 0.23		NA	_2023-12-20_	12/20/2023 3:48
41721-21	0.040	5	498.6	< 0.262			_2023-12-20_	12/20/2023 4:06
41721-21 DUP	0.048	5	498.6	< 0.262		NA	_2023-12-20_	12/20/2023 4:25
41721-22	0.094	5	436.0	< 0.229			_2023-12-20_	12/20/2023 5:59
41721-22 DUP	0.065	5	436.0	< 0.229		NA	_2023-12-20_	12/20/2023 6:17
41721-23	0.040	5	469.8	< 0.247			_2023-12-20_	12/20/2023 6:36
41721-23 DUP	0.039	5	469.8	< 0.247		NA	_2023-12-20_	12/20/2023 6:55
41721-23 SPK	5.355	5	469.8	13.24	5.00	106%	_2023-12-20_	12/20/2023 7:14
41721-23 SPK DUP	5.347	5	469.8	13.22	5.00	106%	_2023-12-20_	12/20/2023 7:32
41721-24	0.083	5	461.3	< 0.243			_2023-12-20_	12/20/2023 7:51
41721-24 DUP	0.037	5	461.3	< 0.243		NA	_2023-12-20_	12/20/2023 8:10
41721-25	0.077	5	463.3	< 0.244			_2023-12-20_	12/20/2023 8:29
41721-25 DUP	0.048	5	463.3	< 0.244		NA	_2023-12-20_	12/20/2023 8:47
41721-26	0.042	5	464.0	< 0.244			_2023-12-20_	12/20/2023 10:22
41721-26 DUP	0.000	5	464.0	< 0.244		NA	_2023-12-20_	12/20/2023 10:40
41721-27 FB ON	0.000	5	419.0	< 0.221			_2023-12-20_	12/20/2023 10:59
41721-27 FB ON DUP	0.000	5	419.0	< 0.221		NA	_2023-12-20_	12/20/2023 11:18
41721-28 FB OFF	0.000	5	420.7	< 0.221			_2023-12-20_	12/20/2023 11:36
41721-28 FB OFF DUP	0.000	5	420.7	< 0.221		NA	_2023-12-20_	12/20/2023 11:55

elementOne e 41721-HF

HF Data 1 of 2

elementOne

M26A-HF IC Data Sheet

Lab ID #: 41721 (15-28

Client: Deeco

Column: IonPac AS14A

Date: 12.22.23

Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0 mM NaHCO<sub>3</sub>

Analyst: LAW

Flow Rate: 1.0 mL/min.

Detection Limit, (µg/ml): 0.10

F to HF factor: 1.053

Standards	F µg/ml D	ilution	QC, µg/ml	% Relative Error	% Recovery	File Name	Date Time
0	0.000					_2023-12-19_	12/19/2023 17:29
0.1	0.104			4.0%	104%	2023-12-19	12/19/2023 17:48
1	0.934			-6.6%	93%	_2023-12-19_	12/19/2023 18:07
3	3.059			2.0%	102%	2023-12-19	12/19/2023 18:26
5	5.032			0.6%	101%	_2023-12-19_	12/19/2023 18:44
10	9.971			-0.3%	100%	_2023-12-19_	12/19/2023 19:03
0.1	0.105			5.0%	105%	_2023-12-20_	12/20/2023 13:48
1	0.927			-7.3%	93%	_2023-12-20_	12/20/2023 14:06
3	2.717			-9.4%	91%	_2023-12-20_	12/20/2023 14:25
5	5.119			2.4%	102%	_2023-12-20_	12/20/2023 14:44
10	10.251			2.5%	103%	_2023-12-20_	12/20/2023 15:03
Correlation-	0.999798						
QC	5.009		5.00		100%	_2023-12-19_	12/19/2023 19:22
QC	4.742		5.00		95%	_2023-12-19_	12/19/2023 19:41
QC	4.659		5.00		93%	_2023-12-20_	12/20/2023 0:22
QC	5.008		5.00		100%	_2023-12-20_	12/20/2023 0:40
QC	5.129		5.00		103%	_2023-12-20_	12/20/2023 4:44
QC	4.685		5.00		94%	_2023-12-20_	12/20/2023 5:03
QC	5.057		5.00		101%	_2023-12-20_	12/20/2023 9:06
QC	5.033		5.00		101%	_2023-12-20_	12/20/2023 9:25
QC	5.063		5.00		101%	_2023-12-20_	12/20/2023 12:51
QC	5.028		5.00		101%	_2023-12-20_	12/20/2023 15:21
DL	0.105		0.10		105%	_2023-12-19_	12/19/2023 20:37
DL	0.095		0.10		95%	_2023-12-19_	12/19/2023 20:55
DL	0.103		0.10		103%	_2023-12-20_	12/20/2023 13:10
DL	0.108		0.10		108%	_2023-12-20_	12/20/2023 15:40
36738-5 QC	6.720	1	6.96		102%	_2023-12-20_	12/20/2023 12:14
36738-5 QC DUP	6.765	1	6.96		102%	_2023-12-20_	12/20/2023 12:33
BLK	0.000					_2023-12-19_	12/19/2023 19:59
BLK	0.000					_2023-12-19_	12/19/2023 20:18
BLK	0.000					_2023-12-20_	12/20/2023 0:59
BLK	0.000					_2023-12-20_	12/20/2023 1:18
BLK	0.000					_2023-12-20_	12/20/2023 5:21
BLK	0.000					_2023-12-20_	12/20/2023 5:40
BLK	0.000					_2023-12-20_	12/20/2023 9:44
BLK	0.000					_2023-12-20_	12/20/2023 10:03
BLK	0.000					_2023-12-20_	12/20/2023 13:29
BLK	0.000					_2023-12-20_	12/20/2023 15:59

elementOne e 41721-HF

HF Data 2 of 2

Lab ID #: 41721 (15-28) elementOne IC Sample Sheet/Digestion Worksheet

Date: 12-19-23

Column: IonPac AS14A

Instrument: 861 (48%

Analyst: نسما

Batch name: 121913-41721

Conc. Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0mM NaHCO<sub>3</sub>

Lot# 1611 - 871

10mL Conc. Eluent Diluted to FV=1L with filtered UPDI Regenerant: 100 mM H<sub>3</sub>PO<sub>4</sub> Lot # f

Lot # 1011-87-104-2 Method: 300/26A

	,		1.0 mL/min.	Method: 300/26A			
AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)
1	0.0			04	MANE	RI	
2	61		F-	-	Signathrul	,9996	
3	1.0						
ч	5.0						
5	So						
6	100						
6	Θ(						
8	60(						7
9	BL						
10	31L						
11	Di						
12	DL						
13	LOB						
14	NB						
15	LRBH						
16	LRBY						
12	41721-15	Deeco	HF			5×	
18	-150		1.				
19	-17						
10	- 17D						
21	-17+				5.388		
12	-17+D				5.234	L	
23	Œ						
24	€.						
25	BL						

Manual integrations noted by M	1.67
Curve IC Lot # \CU-\64-4 Comments: P	410F3
Spike 50 uL from 1000 ug/ml. Std. to 10mL sample Lot #'s: IC N	ME Solution 2363029-250 W IC NO2 Solution 2308 942-250 W
QC: Spike 50 uL from 1000 ug/mL F, Cl, Br, and SO <sub>4</sub> Std. to 10	
QC: Spike 20 uL from 1000 ug/mL NO2, NO3, and PO4 Std. to 1	0mL sample; lot #s listed above.
Submitted for QC- Date: 122027 Time: 4137- By: 1	QC Review- Date: Time: By:

-			-	
$\alpha$	me	m	"	nο

## IC Sample Sheet/Digestion Worksheet

Lab ID #: 41724

Date: 1249-23

Column: IonPac AS14A

Instrument: 861 788

Analyst: ພລ

Conc. Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0mM NaHCO<sub>3</sub>

Lot# 1C11-87-1

Batch name: 12/927-41721

10mL Conc. Eluent Diluted to FV=1L with filtered UPDI Regenerant: 100 mM H<sub>3</sub>PO<sub>4</sub> Lot # LCL(-104-2

			Flow Rate:	Method:			
AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)
26	BlK						
27	41721-16	Deeco	HF			5×	
28	-16D	<u></u>					
24	-18						
30	-18D				<u>'</u>		
31	~19						
32	~19D						
33,	-20						
34	20 D				_		
35	-21				-		
36	-210	4	$\downarrow$			ال.	
37	₽ć						
38	GC						
39	BIŁ						
46	BIL						
વા	4/221-22	Decco	HE			5×	
42	-22D						
43	-23						
44	-23D				_		
45	-23+	1			5355		
Y6	-23+D				5342		
47	-24				_		
48	-24D						
49 50	-25 ·						
50	-2SD	<u> </u>	V				

Manual integrations noted by M
Curve IC Lot #
Spike 50 uL from 1000 ug/m/L Std. tg/10mL sample Lot/#s: IC ME SolutionIC/NO2 Solution
QC: Spike 50 uL from 1000 ug/mL/F, CI, Br, and SO <sub>4</sub> Std. to 10mL sample; lot #'s listled above/
QC: Spike 20 uL from 1000 ug/mL NO <sub>2</sub> , NO <sub>3</sub> , and PO <sub>4</sub> Std. to 10mL sample; lot #'s listed above.
Submitted for QC- Date: Time: By: QC Review- Date: / Time: By:

elementO	ne IC S	IC Sample Sheet/Digestion Worksheet Lab ID #: 41424							
An	Analyst: Conc. Eluent: 8.0 mM Na <sub>2</sub> CO <sub>3</sub> / 1.0mM NaHCO <sub>3</sub> Lot# \Cli- Batch name: 10mL Conc. Eluent Diluted to FV=1L with filtered UPDI Regenerant: 100 mM H <sub>3</sub> PO <sub>4</sub> Lot # \Cli-						-104-7 300/26A		
AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)		
51	Œ								
52	EK								
53	BIL								
34	8(1								
55	41721-26	Decer	HF		-	5×			
<u>56</u>	260	1							
57	-27FB0N				-				
58	-27 FB OND								
59	-28 FB OFF	-			_				
60	-28FBOFFD								
101	36738-5-QL				6.220	1×	TV=696		
62	5-G	1			6-965	d			
b3	(3)		-						
64	D								
65	PIL.								
66	0.1								
67	1-0-1								
69	3.0								
69	5-0								
30	6-01								
71	Œ								
72	TL.								
73	\$V~								
74									
15									
Manual integrations noted by M  Curve IC Lot #									

element∪ne

## M26A-Cl<sub>2</sub> IC Data Sheet

Lab ID #: 41721 (1-14)

Client: Deeco

Date: 12.20.23 Analyst: LAW Column: IonPac AS14A

Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0 mM NaHCO<sub>3</sub>

Flow Rate: 1.0 mL/min.

Detection Limit, (µg/ml): 0.10

Sample ID	Cl' µg/ml	Dilution	Final Vol, ml	Cl <sub>2</sub> , Total mg	Spike, µg/ml	% RPD/ Recovery	File Name	Date Time
LRB	-0.013	1	10	< 0.001			-2dc57c8e:18c7d19aefa:-7919	12/18/2023 20:14
LRB	-0.026	1	10	< 0.001		NA	-2dc57c8e:18c7d19aefa:-7917	12/18/2023 20:38
LRB SPK	10.086	1	10	0.101	5.00	202%	-2dc57c8e:18c7d19aefa:-7915	12/18/2023 21:01
LRB SPK	10.090	1	10	0.101	5.00	202%	-2dc57c8e:18c7d19aefa:-7913	12/18/2023 21:25
41721-1	0.013	5	308.5	< 0.154			-2dc57c8e:18c7d19aefa:-78f9	12/19/2023 2:30
41721-1 DUP	0.010	5	308.5	< 0.154		NA	-2dc57c8e:18c7d19aefa:-78f7	12/19/2023 2:54
41721-2	0.006	5	333.1	< 0.167			-2dc57c8e:18c7d19aefa:-78f5	12/19/2023 3:17
41721-2 DUP	-0.045	5	333.1	< 0.167		NA	-2dc57c8e:18c7d19aefa:-78f3	12/19/2023 3:41
41721-3	-0.010	5	333.6	< 0.167			-2dc57c8e:18c7d19aefa:-78f1	12/19/2023 4:04
41721-3 DUP	-0.028	5	333.6	< 0.167		NA	-2dc57c8e:18c7d19aefa:-78ef	12/19/2023 4:28
41721-3 SPK	5.285	5	333.6	8.8	5.00	106%	-2dc57c8e:18c7d19aefa:-78ed	12/19/2023 4:51
41721-3 SPK DUP	5.221	5	333.6	8.71	5.00	104%	-2dc57c8e:18c7d19aefa:-78eb	12/19/2023 5:15
41721-4	0.374	5	333.8	0.624			-2dc57c8e:18c7d19aefa:-78e1	12/19/2023 7:12
41721-4 DUP	0.382	5	333.8	0.638		2.1%	-2dc57c8e:18c7d19aefa:-78df	12/19/2023 7:36
41721-5	0.169	5	338.3	0.286			-2dc57c8e:18c7d19aefa:-784c	12/19/2023 7:59
41721-5 DUP	0.169	5	338.3	0.286		0.0%	-2dc57c8e:18c7d19aefa:-784a	12/19/2023 8:23
41721-6	0.323	5	352.3	0.569			-2dc57c8e:18c7d19aefa:-7848	12/19/2023 8:46
41721-6 DUP	0.335	5	352.3	0.590		3.6%	-2dc57c8e:18c7d19aefa:-7846	12/19/2023 9:10
41721-7	0.021	5	296.1	< 0.148			-2dc57c8e:18c7d19aefa:-7844	12/19/2023 9:33
41721-7 DUP	0.012	5	296.1	< 0.148		NA	-2dc57c8e:18c7d19aefa:-7842	12/19/2023 9:57
41721-8	-0.026	5	385.2	< 0.193			-2dc57c8e:18c7d19aefa:-77d9	12/19/2023 10:20
41721-8 DUP	-0.029	5	385.2	< 0.193		NA	-2dc57c8e:18c7d19aefa:-77d7	12/19/2023 10:44
41721-9	-0.035	5	312.2	< 0.156			-2dc57c8e:18c7d19aefa:-7704	12/19/2023 12:41
41721-9 DUP	-0.034	5	312.2	< 0.156		NA.	-2dc57c8e:18c7d19aefa:-7702	12/19/2023 13:04
41721-9 SPK	4.953	5	312.2	7.73	5.00	99%	-2dc57c8e:18c7d19aefa:-7700	12/19/2023 13:28
41721-9 SPK DUP	5.064	5	312.2	7.90	5.00	101%	-2dc57c8e:18c7d19aefa:-76fe	12/19/2023 13:51
41721-10	0.371	5	358.9	0.666			-2dc57c8e:18c7d19aefa:-74f7	12/19/2023 14:15
41721-10 DUP	0.378	5	358.9	0.678		1.9%	-2dc57c8e:18c7d19aefa:-74f5	12/19/2023 14:38
41721-11	0.197	5	311.5	0.307			-2dc57c8e:18c7d19aefa:-74f3	12/19/2023 15:02
41721-11 DUP	0.195	5	311.5	0.304		1.0%	-2dc57c8e:18c7d19aefa:-74f1	12/19/2023 15:25
41721-12	0.358	5	337.5	0.604			-2dc57c8e:18c7d19aefa:-74ef	12/19/2023 15:49
41721-12 DUP	0.373	5	337.5	0.629		4.1%	-2dc57c8e:18c7d19aefa:-74ed	12/19/2023 16:12
41721-13 FBON	0.008	5	313.8	< 0.157			-2dc57c8e:18c7d19aefa:-74e3	12/19/2023 18:10
41721-13 FBON DUP	0.039	5	313.8	< 0.157		NA	-2dc57c8e:18c7d19aefa:-74e1	12/19/2023 18:34
41721-14 FB OFF	0.070	5	355.9	< 0.178			-2dc57c8e:18c7d19aefa:-74df	12/19/2023 18:57
41721-14 FB OFF DU	0.084	5	355.9	< 0.178		NA	-2dc57c8e:18c7d19aefa:-74dd	12/19/2023 19:21

elementOne e 41721-Cl<sub>2</sub>

Cl<sub>2</sub>-Data 1 of 2

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element∪ne

## M26A-Cl<sub>2</sub> IC Data Sheet

Lab ID #: 41721 (1-14)

Client: Deeco

Date: 12.20.23 Analyst: LAW Column: IonPac AS14A

Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0 mM NaHCO<sub>3</sub>

Flow Rate: 1.0 mL/min.

Detection Limit, (µg/ml): 0.10

Standards	Cl <sup>-</sup> µg/ml	Dilution	QC µg/	%Kelative ml Error	% Recovery	File Name	Date Time
0	0.000					-2dc57c8e:18c7d19aefa:-7503	12/18/2023 15:32
0.1	0.107			7.0%	107%	-2dc57c8e:18c7d19aefa:-7501	12/18/2023 15:56
1	0.912			-8.8%	91%	-2dc57c8e:18c7d19aefa:-74ff	12/18/2023 16:19
3	2.980			-0.7%	99%	-2dc57c8e:18c7d19aefa:-74fd	12/18/2023 16:43
5	5.149			3.0%	103%	-2dc57c8e:18c7d19aefa:-74fb	12/18/2023 17:06
10	9.948			-0.5%	99%	-2dc57c8e:18c7d19aefa:-74f9	12/18/2023 17:30
0.1	0.107			7.0%	107%	-2dc57c8e:18c7d19aefa:-74d1	12/19/2023 21:42
1	1.014			1.4%	101%	-2dc57c8e:18c7d19aefa:-74cf	12/19/2023 22:05
3	3.097			3.2%	103%	-2dc57c8e:18c7d19aefa:-74cd	12/19/2023 22:29
5	5.162			3.2%	103%	-2dc57c8e:18c7d19aefa:-74cb	12/19/2023 22:52
10	9.782			-2.2%	98%	-2dc57c8e:18c7d19aefa:-74c9	12/19/2023 23:16
Correlation-	0.999771						
QC	5.336		5.00		107%	-2dc57c8e:18c7d19aefa:-7925	12/18/2023 17:53
QC	5.264		5.00		105%	-2dc57c8e:18c7d19aefa:-7923	12/18/2023 18:17
QC	5.208		5.00		104%	-2dc57c8e:18c7d19aefa:-7905	12/19/2023 0:09
QC	5.205		5.00		104%	-2dc57c8e:18c7d19aefa:-7903	12/19/2023 0:33
QC	5.256		5.00		105%	-2dc57c8e:18c7d19aefa:-78e9	12/19/2023 5:38
QC	5.322		5.00		106%	-2dc57c8e:18c7d19aefa:-78e7	12/19/2023 6:02
QC	5.319		5.00		106%	-2dc57c8e:18c7d19aefa:-770c	12/19/2023 11:07
QC	5.020		5.00		100%	-2dc57c8e:18c7d19aefa:-770a	12/19/2023 11:31
QC	5.365		5.00		107%	-2dc57c8e:18c7d19aefa:-74eb	12/19/2023 16:38
QC	5.406		5.00		108%	-2dc57c8e:18c7d19aefa:-74e9	12/19/2023 17:00
QC	5.310		5.00		106%	-2dc57c8e:18c7d19aefa:-74d7	12/19/2023 20:31
QC	5.366		5.00		107%	-2dc57c8e:18c7d19aefa:-74c7	12/19/23 23:39
DL	0.094		0.10		94%	-2dc57c8e:18c7d19aefa:-791d	12/18/2023 19:27
DL	0.090		0.10		90%	-2dc57c8e:18c7d19aefa:-791b	12/18/2023 19:51
DL	0.095		0.10		95%	-2dc57c8e:18c7d19aefa:-74d5	12/19/2023 20:55
DL	0.106		0.10		106%	-2dc57c8e:18c7d19aefa:-74c5	12/20/2023 0:03
40034-7 QC	3.938	20	78.0		101%	-2dc57c8e:18c7d19aefa:-74db	12/19/2023 19:44
40034-7 QC DUP	3.919	20	78.0		100%	-2dc57c8e:18c7d19aefa:-74d9	12/19/2023 20:08
BLK	0.000					-2dc57c8e:18c7d19aefa:-7921	12/18/2023 18:40
BLK	0.000					-2dc57c8e:18c7d19aefa:-791f	12/18/2023 19:04
BLK	0.000					-2dc57c8e:18c7d19aefa:-7901	12/19/2023 0:56
BLK	0.000					-2dc57c8e:18c7d19aefa:-78ff	12/19/2023 1:20
BLK	0.020					-2dc57c8e:18c7d19aefa:-78e5	12/19/2023 6:25
BLK	0.000					-2dc57c8e:18c7d19aefa:-78e3	12/19/2023 6:49
BLK	0.000					-2dc57c8e:18c7d19aefa:-7708	12/19/2023 11:54
BLK	0.000					-2dc57c8e:18c7d19aefa:-7706	12/19/2023 12:18
BLK	0.000					-2dc57c8e:18c7d19aefa:-74e7	12/19/2023 17:23
BLK	0.000					-2dc57c8e:18c7d19aefa:-74e5	12/19/2023 17:47
BLK	0.000					-2dc57c8e:18c7d19aefa:-74d3	12/19/2023 21:18
BLK .	0.000					-2dc57c8e:18c7d19aefa:-74c3	12/20/2023 0:26

elementOne e 41721-Cl<sub>2</sub>

Cl<sub>2</sub>-Data 2 of 2

41707

elementOne

### IC Sample Sheet/Digestion Worksheet

Lab ID #:

41721

Date: 1218.23

Column: IonPac AS14A

Instrument: % 1 \ & S

دىب :Analyst

Conc. Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0mM NaHCO<sub>3</sub>

Lot#1011-87-1

10mL Con

10mL Conc. Eluent Diluted to FV=1L with filtered UPDI

d UPDI

Batch name: \21823 - 41202 Re

Regenerant: 100mM H<sub>3</sub>PO<sub>4</sub> Flow Rate: 1.0 mL/min. Lot # IC(\-\03^Z Method: 26A NaOH

		wethou.	26A NaOH				
AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)
1	6.0			OC.	man	R2	
2	61		CI-	4308559	Raa	14972	
3	1.0						
Ч	3.0						
S	5,0						
م	10.0						
7	6E						
4	CC						
9	BlL						
10	BIL						
11	DL						
12	D						
13	LIEB						
19	Les						
ιŚ	LABY 1000	*					
الم	0001						
17	4407-1		C\7.		3,191	16×	
18	-10		1		3.192		
19	-3				6.162		
20	-3D				6.159		
21	-2+ 1	10 ppr			10.212		
12	-3+>)	54.	1		10.153	$\mathcal{L}$	
23			7				
24	GQ .						
25	Ble						

Manual integrations noted by M
Curve IC Lot # \(\(\)\\_\04-\\ Sodium Thiosulfate Lot #\(\)(1\)-73-\(\)\ Comments: \(\)\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\
Spike 50 uL from 1000 ug/mL Std. to 10mL sample Lot #'s: IC ME Solution Z353624-250 W/S
QC: Spike 50 uL from 1000 ug/mL Br Std. to 10mL sample; lot #'s listied above.
Submitted for QC- Date: \(\frac{2.2023}{2.000}\) Time: \(\frac{9.50}{9.000}\) By: \(\frac{10.000}{9.000}\) QC Review- Date: \(\frac{10.0000}{10.0000}\) Time: \(\frac{10.0000}{9.0000}\) By: \(\frac{10.0000}{9.0000}\)

41707 Lab ID #: 41721 elementOne IC Sample Sheet/Digestion Worksheet Date: 12.1823 Instrument:8%1 85 % Column: IonPac AS14A Lot# 141-87-1 Analyst: دس Conc. Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0mM NaHCO<sub>3</sub> 10mL Conc. Eluent Diluted to FV=1L with filtered UPDI Regenerant: 100mM H<sub>3</sub>PO<sub>4</sub> Lot # (C

Lot # (C) (-)63 - 2-Method: 26A NaOH Batch name: 121823-417-67 Flow Rate: 1.0 mL/min.

AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)
26	BOK						
27	41707-2		Clz		1,417	10×	
28	-ZD			,	1.472	1	
29	41221-1					5×	
30	-ID					1	
-31	-2						
32	-25						
33	-3				-		
34	-30						
35	-3+				5.285		
36	-3tp				5221	\ <u>\</u>	
37	OE.						
38	Gr.						
39	BlL						
40	BIK		0.1			<i>C</i>	
41	4121-9		Cl2		0.374	5×	
42	~4D		-		6382		
43	-4b -5 -Sp	-			6169		
	- 3D				6169		
45	-6D				6.323		
46							
48	-7 -70						
49	- 8						
28	48-					5	

Manual integra	£			
Curve IC Lot #	Sodium Thiosulfate Lot #	Comments:	8920F4	
Spike 50 uL from 1000 ug/mL Std/	to 10mL sample Lot #'s: IC ME Sol	ution		
QC: Spike 50 uL from 1000 ug/mL	Br Std. to 10m/L sample; lot/#s listic	ed above.		
Submitted for QC- Date:	Time: By:	QC Review- Date:	Time:	By:
- /	/ /			
/-	· /			

Ana	ne IC S Date: 12-18-23 alyst: LM ame: 121823-4180	e <b>t</b> M NaHCO <sub>3</sub> :1L with filtere	Lot # [ C   1-	3811858 871			
AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)
51	Œ						
52	60						
53	BIL						
59	BIC						
5.5	41221-9					5×	
56	-9D						
52	-9j				4953		
58	-9+D				3004		
59	-10				0.321		
le 6	-10D				0.328		
61	-11				0.197		
62	-IID				0.195		
63	-12				0.358		
64	-12D				6373	4	
65	Gr.						
طعا	GC						
67	BL						
83	BL						
69	41221-1398 FG	W				5×	
30	-1388 BPV	ND			-	1	
71	-14 FB666					1	
72	-14 FBOOFD					L.V.	
7,5	40034-7 - BC				3,938	20X	N=780
94	-7_GC				3,919	U	
75	Gt/				L		

Manual integra		/	-	- 00	
Curve IC Lot #	Sogium Thiosu	ulfate Lot #	Comments:	pg SAT	4
Spike 50 uL from 1000 ug/ml				, -	
QC: Spike 50 uL from 1000 u	g/mL Br Std. to 10mL:	sample; lot #'s listled	abøve.		
Submitted for QC- Date:	Time:	/By:,	C Review- Date:	Time:	By:
		/ /			
	,	' /			

elementOne IC Sample Sheet/Digestion Worksheet Lab ID #: 41707								
Date: 12 18 23								
AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)	
76	DC							
77	BIK							
76	0.1							
74	6.1							
86	3-0							
81	56							
82	10.0						,	
83	<u> </u>			<u> </u>				
84	DL							
	BII							
QC: Spike 50	Soo om 1000 ug/mL Std. to 10 uL from 1000 ug/mL Br St	f. to 10mL sary	Fs: IC ME Soluti ble; lot #'s listied	on /	_	4 854 By: By:		

881/858 Ion Chromatograph System

elementOne

### M26A-Cl2 IC Data Sheet

0.10

Lab ID #: 41721 (15-28)

Client: Deeco

Column: IonPac AS14A

Date: 12.22.23

Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0 mM NaHCO<sub>3</sub>

Analyst: LAW

Flow Rate: 1.0 mL/min. 1.000

Detection Limit, (µg/ml):

Dottootion Limit, (P.S.								
Sample ID	Cl' µg/ml	Dilution	Final Vol, ml	Cl <sub>2</sub> , Total mg	Spike, µg/ml	% RPD/ Recovery	File Name	Date Time
LRB	-0.003	1	10	< 0.001			-2dc57c8e:18c7d19aefa:-6f6d	12/20/2023 14:26
LRB	0.004	1	10	< 0.001		NA	-2dc57c8e:18c7d19aefa:-6f8b	12/20/2023 14:50
LRB SPK	5.137	1	10	0.051	5.00	103%	-2dc57c8e:18c7d19aefa:-6f69	12/20/2023 15:13
LRB SPK	5.242	1	10	0.052	5.00	105%	-2dc57c8e:18c7d19aefa:-6f67	12/20/2023 15:37
41721-15	-0.021	5	296.6	< 0.148			-2dc57c8e:18c7d19aefa:-6f65	12/20/2023 16:00
41721-15 DUP	0.020	5	296.6	< 0.148		NA	-2dc57c8e:18c7d19aefa:-6f63	12/20/2023 16:24
41721-16	0.008	5	339.0	< 0.17			-2dc57c8e:18c7d19aefa:-6f51	12/20/2023 19:55
41721-16 DUP	-0.013	5	339.0	< 0.17		NA	-2dc57c8e:18c7d19aefa:-6f4f	12/20/2023 20:19
41721-17	0.034	5	349.4	< 0.175			-2dc57c8e:18c7d19aefa:-6f61	12/20/2023 16:47
41721-17 DUP	0.016	5	349.4	< 0.175		NA	-2dc57c8e:18c7d19aefa:-6f5f	12/20/2023 17:11
41721-17 SPK	5.057	5	349.4	8.83	5.00	100%	-2dc57c8e:18c7d19aefa:-6f5d	12/20/2023 17:34
41721-17 SPK DUP	5.065	5	349.4	8.85	5.00	101%	-2dc57c8e:18c7d19aefa:-6f5b	12/20/2023 17:58
41721-18	0.023	5	347.0	< 0.174			-2dc57c8e:18c7d19aefa:-6f4d	12/20/2023 20:42
41721-18 DUP	0.037	5	347.0	< 0.174		NA	-2dc57c8e:18c7d19aefa:-6f4b	12/20/2023 21:06
41721-19	0.092	5	282.2	< 0.141			-2dc57c8e:18c7d19aefa:-6f49	12/20/2023 21:29
41721-19 DUP	0.090	5	282.2	< 0.141	- 1	AN GE	-2dc57c8e:18c7d19aefa:-6f47	12/20/2023 21:53
41721-20	0.058	5	328.5	< 0.164	(4	NA NA	-2dc57c8e:18c7d19aefa:-6f45	12/20/2023 22:16
41721-20 DUP	0.077	5	328.5	< 0.164	۷,	NA	-2dc57c8e:18c7d19aefa:-6f43	12/20/2023 22:40
41721-21	-0.029	5	297.1	< 0.149			-2dc57c8e:18c7d19aefa:-6dfe	12/20/2023 23:03
41721-21 DUP	-0.052	5	297.1	< 0.149		NA.	-2dc57c8e:18c7d19aefa:-6dfc	12/20/2023 23:27
41721-22	-0.016	5	324.8	< 0.162			-2dc57c8e:18c7d19aefa:-6df2	12/21/2023 1:24
41721-22 DUP	-0.016	5	324.8	< 0.162		NA	-2dc57c8e:18c7d19aefa:-6df0	12/21/2023 1:48
41721-23	-0.016	5	343.6	< 0.172			-2dc57c8e:18c7d19aefa:-6dee	12/21/2023 2:11
41721-23 DUP	-0.019	5	343.6	< 0.172		NA	-2dc57c8e:18c7d19aefa:-6dec	12/21/2023 2:35
41721-23 SPK	4.922	5	343.6	8.46	5.00	99%	-2dc57c8e:18c7d19aefa:-6dea	12/21/2023 2:58
41721-23 SPK DUP	5.125	5	343.6	8.80	5.00	103%	-2dc57c8e:18c7d19aefa:-6de8	12/21/2023 3:22
41721-24	-0.053	5	341.0	< 0.171			-2dc57c8e:18c7d19aefa:-6de6	
41721-24 DUP	0.011	5	341.0	< 0.171		NA	-2dc57c8e:18c7d19aefa:-6de4	
41721-25	-0.029	5	329.1	< 0.165			-2dc57c8e:18c7d19aefa:-6de2	12/21/2023 4:32
41721-25 DUP	-0.014	5	329.1	< 0.165		NA	-2dc57c8e:18c7d19aefa:-6de0	12/21/2023 4:56
41721-26	0.005	5	346.4	< 0.173			-2dc57c8e:18c7d19aefa:-6dd6	
41721-26 DUP	-0.011	5	346.4	< 0.173		NA	-2dc57c8e:18c7d19aefa:-6dd4	
41721-27 FB ON	-0.029	5	341.0	< 0.171			-2dc57c8e:18c7d19aefa:-6dd2	
41721-27 FB ON DUP	0.014	5	341.0	< 0.171		NA	-2dc57c8e:18c7d19aefa:-6dd0	
41721-28 FB OFF	0.055	5	334.7	< 0.167			-2dc57c8e:18c7d19aefa:-6dce	
41721-28 FB OFF DUP	0.019	5	334.7	< 0.167		NA	-2dc57c8e:18c7d19aefa:-6dcc	12/21/2023 8:50

elementOne e 41721-Cl<sub>2</sub>

Cl<sub>2</sub>-Data 1 of 2

complete.

881/858 Ion Chromatograph System

elementOne

## M26A-CI2 IC Data Sheet

Lab ID #: 41721 (15-28)

Client: Deeco

Column: IonPac AS14A

Date: 12.22.23

Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0 mM NaHCO<sub>3</sub>

Analyst: LAW

Flow Rate: 1.0 mL/min.

1.000

Detection Limit, (µg/ml): 0.10

Standards	Cl' µg/ml	Dilution	QC µg/ml	%Relative Error	% Recovery	File Name	Date Time
0	0.000					-2dc57c8e:18c7d19aefa:-6d07	12/20/2023 9:44
0.1	0.106			6.0%	106%	-2dc57c8e:18c7d19aefa:-6d05	12/20/2023 10:08
1	0.924			-7.6%	92%	-2dc57c8e:18c7d19aefa:-6d03	12/20/2023 10:32
3	2.989			-0.4%	100%	-2dc57c8e:18c7d19aefa:-6d01	12/20/2023 10:55
5	5.131			2.6%	103%	-2dc57c8e:18c7d19aefa:-6cff	12/20/2023 11:19
10	9.949			-0.5%	99%	-2dc57c8e:18c7d19aefa:-6cfd	12/20/2023 11:42
0.1	0.109			9.0%	109%	-2dc57c8e:18c7d19aefa:-6cf5	12/21/2023 11:11
1	0.969			-3.1%	97%	-2dc57c8e:18c7d19aefa:-6cf3	12/21/2023 11:35
3	2.949			-1.7%	98%	-2dc57c8e:18c7d19aefa:-6cf1	12/21/2023 11:58
5	5.140			2.8%	103%	-2dc57c8e:18c7d19aefa:-6cef	12/21/2023 12:22
10	10.294			2.9%	103%	-2dc57c8e:18c7d19aefa:-6ced	12/21/2023 12:45
Correlation-	0.999798						
QC	5.110		5.00		102%	-2dc57c8e:18c7d19aefa:-6f79	12/20/2023 12:08
QC	5.181		5.00		104%	-2dc57c8e:18c7d19aefa:-6f77	12/20/2023 12:29
QC	5.149		5.00		103%	-2dc57c8e:18c7d19aefa:-6f59	12/20/2023 18:21
QC	5.114		5.00		102%	-2dc57c8e:18c7d19aefa:-6f57	12/20/2023 18:45
QC	5.105		5.00		102%	-2dc57c8e:18c7d19aefa:-6dfa	12/20/2023 23:50
QC	5.208		5.00		104%	-2dc57c8e:18c7d19aefa:-6df8	12/21/2023 0:14
QC	5.092		5.00		102%	-2dc57c8e:18c7d19aefa:-6dde	12/21/2023 5:19
QC	5.149		5.00		103%	-2dc57c8e:18c7d19aefa:-6ddc	12/21/2023 5:43
QC	5.157		5.00		103%	-2dc57c8e:18c7d19aefa:-6cfb	12/21/2023 10:01
QC	5.230		5.00		105%	-2dc57c8e:18c7d19aefa:-6ceb	12/21/2023 13:09
DL	0.109		0.10		109%	-2dc57c8e:18c7d19aefa:-6f71	12/20/2023 13:39
DL	0.100		0.10		100%	-2dc57c8e:18c7d19aefa:-6f6f	12/20/2023 14:03
DL	0.094		0.10		94%	-2dc57c8e:18c7d19aefa:-6cf9	12/21/2023 10:24
40034-7 QC	3.801	20	78.0		97%	-2dc57c8e:18c7d19aefa:-6dca	12/21/2023 9:14
40034-7 QC DUP	3.844	20	78.0		99%	-2dc57c8e:18c7d19aefa:-6dc8	12/21/2023 9:37
BLK	0.000					-2dc57c8e:18c7d19aefa:-6f75	12/20/2023 12:53
BLK	0.000					-2dc57c8e:18c7d19aefa:-6f73	12/20/2023 13:16
BLK	0.000					-2dc57c8e:18c7d19aefa:-6f55	12/20/2023 19:08
BLK	0.000					-2dc57c8e:18c7d19aefa:-6f53	12/20/2023 19:32
BLK	0.000					-2dc57c8e:18c7d19aefa:-6df6	12/21/2023 0:37
BLK	0.000					-2dc57c8e:18c7d19aefa:-6df4	12/21/2023 1:01
BLK	-0.039					-2dc57c8e:18c7d19aefa:-8dda	12/21/2023 6:06
BLK	0.000					-2dc57c8e:18c7d19aefa:-6dd8	12/21/2023 6:30
BLK	0.000					-2dc57c8e:18c7d19aefa:-6cf7	12/21/2023 10:48
BLK	0.000					-2dc57c8e:18c7d19aefa:-6ce7	12/21/2023 13:56

elementOne e 41721-Cl<sub>2</sub>

Cl<sub>2</sub>-Data 2 of 2

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	ne		

## IC Sample Sheet/Digestion Worksheet

Lab ID #: 41721 (15-28)

Date: 124923 Analyst: W

Column: IonPac AS14A

Instrument: 881) 45く Lot# 1011 — 8チィ

Conc. Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0mM NaHCO<sub>3</sub>

10mL Conc. Eluent Diluted to FV=1L with filtered UPDI Regenerant: 100mM H<sub>3</sub>PO<sub>4</sub> Lot # \C\(-\IOU\-Z\) Batch name: | 23023-41221

Flow Rate: 1.0 mL/min.

Datorria	Flow Rate: 1.0 mL/min.						Method: 26A NaOH		
AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)		
1	0.0			GC_	MANG	<u>g2</u>			
2	61		CI-	4308559	RICCA	.499298			
3	1.0								
Ч	3.0								
S	50								
6	10-0								
7	Œ								
8	GC.								
9	BIL								
(0	BIL								
l,	DL								
12	DL								
(3	UES								
14	LLB								
15	UBY								
lω	URF								
17	41221-15	heeco	Ch			ξX			
18	-15								
19	-12								
lo	-170				_				
21	-17+				5.052				
22	-17+D	J			5.065				
25	Œ								
24	Œ								
25	BK								

Manual integrations noted by M	
Curve IC Lot # 1(1/-105-1 Sodium Thiosulfate Lot # 1(1/-23-4 Comments: 90, 10 F 5	
Spike 50 uL from 1000 ug/mL Std. to 10mL sample Lot #'s: IC ME Solution 230107.9-250 by	
QC: Spike 50 uL from 1000 ug/mL Br Std. to 10mL sample; lot #'s listled above.	
Submitted for QC- Date: 22123 Time: 328 By: QC Review- Date: Time: By:	_

-1	le i	~~	_	mi	5	۱n.	_

## IC Sample Sheet/Digestion Worksheet

Lab ID #: 41721 (15-28)

Date: 12:923 Analyst: いい

Column: IonPac AS14A

Instrument: 881 \ 858 Lot# \ \ C\ I\ ~84-

Conc. Eluent: 8.0 mM Na<sub>2</sub>CO<sub>3</sub>/ 1.0mM NaHCO<sub>3</sub>

10mL Conc. Eluent Diluted to FV=1L with filtered UPDI Regenerant: 100mM H₃PO₄ Lot # I

Batch name: 12H923-41721

Lot # 1011-104-2 Method: 26A NaOH

Datonine	121925-417	Z) Rege	v Rate: 1.0 ml			Method:	26A NaOH
AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)
26	BIK						
27	41221-16	Deeco	Cl2			5×	
28	CO1-						
29	-18						
36	-19D				~		
31	-19						
32	-19D						
33	-20						
34	-200						
35	-2.1						
36	-21D		1		_		
37	O(						
38	æ						
39	8lK						
40	BIL						
٧١	41221-22	Deeco	C)2.			5×	
42	-22D	-				1	
43	-23						
44	-23 D						
45	-23+				4922		
46	-23+0				5.125		
uz	-24				_		
48	-240						
49	-25						
56	-25 P	V	レ			V	

Manual integra	_			_	()	
Curve IC Lot #	Sodium Thiosulfate Lot #_		_Comments:	PG 20	# 5	
Spike 50 uL from 1000 ug/mL Std	to 10mL sample Lot #'s: IC I	ME Solution		10		
QC: Spike 50 uL from 1000 ug/ŋɗ	. Br Std. to 10mL sample; lot	#'s listied above.	/			
Submitted for QC- Date:	Time: By:	QC Review	w- Date:	Time:	By:	_

							41221 (15-2	
elementO	Date: 12,49,23	Column: IonPac AS14A Conc. Eluent: 8.0 mM Na <sub>2</sub> CO <sub>3</sub> / 1.0mM NaHCO <sub>3</sub>					*81/858 -871	
	Analyst: Conc. Eluent: 8.0 mM Na <sub>2</sub> CO <sub>3</sub> / 1.0mM NaHCO <sub>3</sub> 10mL Conc. Eluent Diluted to FV=1L with filtere Regenerant: 100mM H <sub>3</sub> PO <sub>4</sub> Flow Rate: 1.0 mL/min.							
AS LOC.	Sample ID	Client	Analyte	Results (ug/mL)	Results (ug/mL)	Dilution	Wt (g) / FV (mL)	
51	Œ.							
52	60							
53	PIL							
54	BIK							
55	41721-26	Deeco	Clz			5>		
ط5	-260	_	+			1		
57	-27 FBON							
5%	-27 FB OND				<u>~</u>			
59	_28 AB OH-				-	<u> </u>		
60	-28 FB OFFD	4				A.		
6/	100347 - 65				3.801	20×	TV=78.0	
9	7_G(		<u> </u>		384H	1		
- 63	OL				-	-		
64	Dr.					<del>                                     </del>	<u> </u>	
65	BIL					-		
<u>66</u>	0.4							
67 68	30							
69	50							
70	0.01					-		
71	Œ					-		
72	DC							
73	BIX							
\-								

Manual integra	_ ,		$\sim$
Curve IC Lot #	Sodium Thiosulfate Lot #	Comments:/	po 30t.2
Spike 50 uL from 1000 ug/grlL Std.:	to 10mL sample Lot #'s: IC ME S	olution	1)
QC: Spike 50 uL from 1900 ug/mL	Br Std. to 10mL/sample; lot #'s lis	tied above.	
Submitted for QC- Date:	Time: By:	QC Review- Date;	Time: By:
2	/	/	
	/	/	

Appendix D

**Plant Process Data** 

Buzzi Unicem Maryneal TX Kiln	Kiin4: CUNKER_PR
4 Main Stack Mili	OD (TNHR)
On Run 1	Expression
Date/Time	Value
11/29/2023 14:50	150.9
11/29/2023 14:51	150.9 151.0
11/29/2023 14:52	150.9
11/29/2023 14:54	150.9
11/29/2023 14:55	150.9
11/29/2023 14:56	151.0
11/29/2023 14:57	150.9
11/29/2023 14:58 11/29/2023 14:59	150.9 150.9
11/29/2023 15:00	150.9
11/29/2023 15:01	150.9
11/29/2023 15:02	150.9
11/29/2023 15:03	150.9
11/29/2023 15:04	151.0 150.9
11/29/2023 15:06	150.9
11/29/2023 15:07	150.9
11/29/2023 15:08	150.9
11/29/2023 15:09	150.9
11/29/2023 15:10	150.9
11/29/2023 15:11	151.0 150.9
11/29/2023 15:12 11/29/2023 15:13	150.9
11/29/2023 15:14	150.9
11/29/2023 15:15	150.9
11/29/2023 15:16	150.9
11/29/2023 15:17	150.8
11/29/2023 15:18	150.9 150.9
11/29/2023 15:20	151.0
11/29/2023 15:21	150.9
11/29/2023 15:22	150.9
11/29/2023 15:23	150.9
11/29/2023 15:24 11/29/2023 15:25	150.9 150.9
11/29/2023 15:26	150.9
11/29/2023 15:27	150.9
11/29/2023 15:28	150.9
11/29/2023 15:29	150.9
11/29/2023 15:30	150.9 150.9
11/29/2023 15:31 11/29/2023 15:32	150.9
11/29/2023 15:33	150.9
11/29/2023 15:34	150.9
11/29/2023 15:35	150.9
11/29/2023 15:36	150.9
11/29/2023 15:37 11/29/2023 15:38	151.0 150.9
11/29/2023 15:39	150.9
11/29/2023 15:40	150.9
11/29/2023 15:41	150.9
11/29/2023 15:42	151.0
11/29/2023 15:43	150.9
11/29/2023 15:44 11/29/2023 15:45	150.9 150.9
11/29/2023 15:46	151.0
11/29/2023 15:47	150.9
11/29/2023 15:48	151.0
11/29/2023 15:49	150.9
11/29/2023 15:50 11/29/2023 15:51	151.0
11/29/2023 15:52	150.9 150.9
11/29/2023 15:53	150.9
11/29/2023 15:54	150.9
11/29/2023 15:55	150.9
11/29/2023 15:56	150.9

Buzzi Unicem	Klin4:
Maryneal TX Kiin	CLINKER_PR
4 Main Stack Mill	OD (TNHR)
On Run 2	Expression
Date/Time	Value
11/30/2023 09:20	138.3
11/30/2023 09:21	138.4
Control of the Contro	
11/30/2023 09:22	138.3
11/30/2023 09:23	138.2
11/30/2023 09:24	138.2
11/30/2023 09:25	138.3
CONTRACTOR PROPERTY CONTRACTOR CONTRACTOR CONTRACTOR	
11/30/2023 09:26	138.3
11/30/2023 09:27	138.2
11/30/2023 09:28	135.7
11/30/2023 09:29	135.0
11/30/2023 09:30	135.1
11/30/2023 09:31	135.2
11/30/2023 09:32	135.1
11/30/2023 09:33	135.2
paging appropriate and appropriate to a	
11/30/2023 09:34	135.1
11/30/2023 09:35	135.2
11/30/2023 09:36	135.1
11/30/2023 09:37	135.0
Contract Contract Page Avenue Contract	
11/30/2023 09:38	135.1
11/30/2023 09:39	135.2
11/30/2023 09:40	135.1
11/30/2023 09:41	135.1
CONTROL PROGRAMMENT AND ADDRESS OF THE PARTY	135.1
11/30/2023 09:42	
11/30/2023 09:43	135.1
11/30/2023 09:44	135.1
11/30/2023 09:45	135.1
0.00 00000000 1000000000000000000000000	
11/30/2023 09:46	135.1
11/30/2023 09:47	135.1
11/30/2023 09:48	135.1
11/30/2023 09:49	135.1
Constitution of the Consti	135.0
11/30/2023 09:50	
11/30/2023 09:51	135.1
11/30/2023 09.52	135.1
11/30/2023 09:53	135.1
11/30/2023 09:54	135.1
***************************************	
11/30/2023 09:55	135.2
11/30/2023 09:56	135.2
11/30/2023 09:57	135.0
11/30/2023 09:58	135.1
NAMES OF THE PROPERTY OF THE P	
11/30/2023 09:59	135.1
11/30/2023 10:00	133.0
11/30/2023 10:01	128.9
11/30/2023 10:02	129.0
11/30/2023 10:03	128.9
11/30/2023 10:04	128.9
11/30/2023 10:05	128.9
11/30/2023 10:06	128.9
11/30/2023 10:07	
11/30/2023 10:08	128.9
11/30/2023 10:09	128.9
11/30/2023 10:10	128.9
11/30/2023 10:11	129.0
11/30/2023 10:12	1
11/30/2023 10:13	128.9
11/30/2023 10:14	128.9
11/30/2023 10:15	128.9
11/30/2023 10:16	128.9
11/30/2023 10:17	128.9
11/30/2023 10:18	128.9
Contract process Applicate VI Contract processing	128.9
11/30/2023 10:19	
11/30/2023 10:20	128.9
11/30/2023 10:21	128.9
11/30/2023 10:22	128.9
11/30/2023 10:23	128.9
11/30/2023 10:24	128.9
West Control of the C	
11/30/2023 10:25	128.9
11/30/2023 10:26	128.9

	Kiin4:
	CLINKER_PR
	OD (TNHR)
Date/Time	Expression Value
11/30/2023 10:45	129.0
11/30/2023 10:46	128.9
11/30/2023 10:47	128.9 129.0
11/30/2023 10:49	128.9
11/30/2023 10:50	128.9
11/30/2023 10:51	128.9
11/30/2023 10:52	129.0 128.9
11/30/2023 10:54	128.9
11/30/2023 10:55	129.0
11/30/2023 10:56	128.9
11/30/2023 10:57 11/30/2023 10:58	128.9 128.9
11/30/2023 10:59	128.9
11/30/2023 11:00	128.9
11/30/2023 11:01	128.9
11/30/2023 11:02	128.9 128.9
11/30/2023 11:04	128.9
11/30/2023 11:05	128.9
11/30/2023 11:06	128.9
11/30/2023 11:07 11/30/2023 11:08	128.9 128.9
11/30/2023 11:09	128.9
11/30/2023 11:10	128.9
11/30/2023 11:11	129.0
11/30/2023 11:12	128.9 128.9
11/30/2023 11:14	128.9
11/30/2023 11:15	128.9
11/30/2023 11:16	128.9 129.0
11/30/2023 11:18	128.9
11/30/2023 11:19	132.0
11/30/2023 11:20	132.1
11/30/2023 11:21 11/30/2023 11:22	132.0 132.0
11/30/2023 11:23	131.9
11/30/2023 11:24	132.0
11/30/2023 11:25 11/30/2023 11:26	132.0 132.0
11/30/2023 11:27	
11/30/2023 11:28	131.9
11/30/2023 11:29	131.9
11/30/2023 11:30 11/30/2023 11:31	131.9 132.1
11/30/2023 11:32	132.0
11/30/2023 11:33	131.9
11/30/2023 11:34 11/30/2023 11:35	132.0 132.1
11/30/2023 11:35	4
11/30/2023 11:37	132.0
11/30/2023 11:38	
11/30/2023 11:39 11/30/2023 11:40	
11/30/2023 11:41	131.9
11/30/2023 11:42	132.1
11/30/2023 11:43	131.9
11/30/2023 11:44 11/30/2023 11:45	1
11/30/2023 11:46	
11/30/2023 11:47	131.9
11/30/2023 11:48 11/30/2023 11:49	
11/30/2023 11:50	131.9
11/30/2023 11:51	
Average	130.4

**************************************	
5 6 6 6 6	
Maria Caracteria	129_A
Buzzi Unicem	Kiin4:
Maryneal TX Kiin	CLINKER PR
0.0000000000000000000000000000000000000	200000000000000000000000000000000000000
4 Main Stack Mill	OD (TNHR)
On Run 3	Expression
Data Mina	
Date/Time	Value
11/30/2023 10:45	129.0
11/30/2023 10:46	128.9
11/20/2022 10/47	128.9
11/30/2023 10:47	120.5
11/30/2023 10:48	129.0
11/30/2023 10:49	128.9
11/30/2023 10:50	128.9
a country of the published of the development	***************************************
11/30/2023 10:51	128.9
14 00 0000 10.00	129.0
11/30/2023 10:52	129.0
11/30/2023 10:53	128.9
Control of the Contro	
11/30/2023 10:54	128.9
11/30/2023 10:55	129.0
AN EXPLORED CONTRACT CONTRACT OF THE	<del></del>
11/30/2023 10:56	128.9
Contract of Contract of the Contract of the Contract	128.9
TO THE RESERVE OF THE PARTY OF	
11/30/2023 10:58	128.9
AN ACCOUNT OF A STATE AND ADDRESS OF THE	
11/30/2023 10:59	128.9
11/30/2023 11:00	128.9
Control of the Contro	
11/30/2023 11:01	128.9
11/20/2013 11/02	1200
11/30/2023 11:02	128.9
11/30/2023 11:03	128.9
11/30/2023 11:04	128.9
11/30/2023 11:05	128.9
Contract Con	
11/30/2023 11:06	128.9
11/30/2023 11:07	128.9
TTI JOILLORD ALLOY	120.5
11/30/2023 11:08	128.9
West 2005/00/00/00/00/00/00/00	120.0
11/30/2023 11:09	128.9
11/30/2023 11:10	128.9
***************************************	
11/30/2023 11:11	129.0
11/30/2023 11:12	128.9
A PRODUCT OF THE PROPERTY OF T	
11/30/2023 11:13	128.9
11/20/2003 11:14	128.9
11/30/2023 11:14	120.9
11/30/2023 11:15	128.9
11/30/2023 11:16	128.9
11/30/2023 11:17	129.0
11/30/2023 11:18	128.9
11/30/2023 11:19	132.0
AND SECURITION OF THE PARTY OF	
11/30/2023 11:20	132.1
11/20/2022 11/21	1220
11/30/2023 11:21	132.0
11/30/2023 11:22	132.0
11/30/2023 11:23	131.9
11/30/2023 11:24	132.0
	•
11/30/2023 11:25	132.0
11/30/2023 11:26	132.0
L-REMARKS MANAGEMENT	
11/30/2023 11:27	
11/30/2023 11:27	132.0
11/30/2023 11:27 11/30/2023 11:28	132.0 131.9
11/30/2023 11:27	132.0 131.9
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29	132.0 131.9 131.9
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30	132.0 131.9 131.9 131.9
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30	132.0 131.9 131.9
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31	132.0 131.9 131.9 131.9 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:31	132.0 131.9 131.9 131.9 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:31	132.0 131.9 131.9 131.9 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33	132.0 131.9 131.9 131.9 132.1 132.0 131.9
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:31	132.0 131.9 131.9 131.9 132.1 132.0
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:34	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:34	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:34	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:39 11/30/2023 11:31 11/30/2023 11:31 11/30/2023 11:33 11/30/2023 11:34 11/30/2023 11:35	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:36	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0 132.0 132.1 132.0 132.0
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:34 11/30/2023 11:35	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0 132.1 132.0
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:31 11/30/2023 11:33 11/30/2023 11:34 11/30/2023 11:35 11/30/2023 11:36	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0 132.1 132.0 132.1 132.0 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:33 11/30/2023 11:33 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:38 11/30/2023 11:38	132.0 131.9 131.9 131.9 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:31 11/30/2023 11:33 11/30/2023 11:34 11/30/2023 11:35 11/30/2023 11:36	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0 132.1 132.0 132.1 132.0 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:29 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:38 11/30/2023 11:38 11/30/2023 11:38	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:38 11/30/2023 11:38 11/30/2023 11:38 11/30/2023 11:38	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:38 11/30/2023 11:38 11/30/2023 11:38 11/30/2023 11:38	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:31 11/30/2023 11:33 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:38 11/30/2023 11:38 11/30/2023 11:38 11/30/2023 11:41 11/30/2023 11:41	132.0 131.9 131.9 132.1 132.0 131.9 132.0 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:32 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:39 11/30/2023 11:40 11/30/2023 11:41 11/30/2023 11:41	132.0 131.9 131.9 131.9 132.1 132.0 131.9 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:32 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:39 11/30/2023 11:40 11/30/2023 11:41 11/30/2023 11:41	132.0 131.9 131.9 132.1 132.0 131.9 132.0 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:32 11/30/2023 11:31 11/30/2023 11:33 11/30/2023 11:33 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:38 11/30/2023 11:38 11/30/2023 11:41 11/30/2023 11:41 11/30/2023 11:41 11/30/2023 11:42	132.0 131.9 131.9 131.9 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:32 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:39 11/30/2023 11:40 11/30/2023 11:41 11/30/2023 11:41	132.0 131.9 131.9 132.1 132.0 131.9 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:39 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:34 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:31 11/30/2023 11:41 11/30/2023 11:41 11/30/2023 11:41 11/30/2023 11:44 11/30/2023 11:44	132.0 131.9 131.9 131.9 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.1 132.0 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:32 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:34 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:39 11/30/2023 11:41 11/30/2023 11:41 11/30/2023 11:41 11/30/2023 11:43	132.0 131.9 131.9 131.9 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.1 132.0 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:39 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:34 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:31 11/30/2023 11:41 11/30/2023 11:41 11/30/2023 11:41 11/30/2023 11:44 11/30/2023 11:44	132.0 131.9 131.9 131.9 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.1 132.0 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:32 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:34 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:38 11/30/2023 11:39 11/30/2023 11:41 11/30/2023 11:41 11/30/2023 11:43 11/30/2023 11:43 11/30/2023 11:44 11/30/2023 11:45 11/30/2023 11:45	132.0 131.9 131.9 131.9 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 131.9 132.1 131.9 131.9 131.9
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:31 11/30/2023 11:33 11/30/2023 11:34 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:38 11/30/2023 11:40 11/30/2023 11:41 11/30/2023 11:43 11/30/2023 11:43 11/30/2023 11:44 11/30/2023 11:45 11/30/2023 11:46	132.0 131.9 131.9 131.9 132.1 132.0 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.1 131.9 132.1 131.9 132.1 131.9 132.1 131.9 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:32 11/30/2023 11:31 11/30/2023 11:32 11/30/2023 11:33 11/30/2023 11:34 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:38 11/30/2023 11:39 11/30/2023 11:41 11/30/2023 11:41 11/30/2023 11:43 11/30/2023 11:43 11/30/2023 11:44 11/30/2023 11:45 11/30/2023 11:45	132.0 131.9 131.9 131.9 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 131.9 132.1 131.9 131.9 131.9
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:31 11/30/2023 11:33 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:35 11/30/2023 11:39 11/30/2023 11:40 11/30/2023 11:41 11/30/2023 11:45 11/30/2023 11:45 11/30/2023 11:45 11/30/2023 11:46	132.0 131.9 131.9 131.9 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.1 132.1 131.9 132.1 131.9 132.1 131.9 132.1 131.9 132.1 131.9 132.1
11/30/2023 11:27 11/30/2023 11:28 11/30/2023 11:28 11/30/2023 11:30 11/30/2023 11:31 11/30/2023 11:31 11/30/2023 11:33 11/30/2023 11:34 11/30/2023 11:35 11/30/2023 11:36 11/30/2023 11:38 11/30/2023 11:40 11/30/2023 11:41 11/30/2023 11:43 11/30/2023 11:43 11/30/2023 11:44 11/30/2023 11:45 11/30/2023 11:46	132.0 131.9 131.9 131.9 132.1 132.0 132.0 132.1 132.0 132.1 132.0 132.1 132.0 132.1 132.1 131.9 132.1 131.9 132.1 131.9 132.1 131.9 132.1

11/30/202 Average

Buzzi Unicem	Kiln4:
Maryneal TX Kiln	CLINKER_PR
4 Main Stack Mill Off Run 1	OD (TNHR) Expression
Date/Time	Value
11/30/2023 14:05 11/30/2023 14:06	128.9 129.0
11/30/2023 14:07	128.9
11/30/2023 14:08	128.9
11/30/2023 14:09	128.9 128.9
11/30/2023 14:11	129.0
11/30/2023 14:12 11/30/2023 14:13	128.8 128.9
11/30/2023 14:14	128.9
11/30/2023 14:15	128.8
11/30/2023 14:16 11/30/2023 14:17	128.9 128.9
11/30/2023 14:18	128.9
11/30/2023 14:19	128.9
11/30/2023 14:20	128.9
11/30/2023 14:22	129.0
11/30/2023 14:23	128.9
11/30/2023 14:24 11/30/2023 14:25	128.9
11/30/2023 14:26	128.9
11/30/2023 14:27	128.9
11/30/2023 14:28 11/30/2023 14:29	128.9 128.9
11/30/2023 14:30	128.9
11/30/2023 14:31	129.0
11/30/2023 14:32 11/30/2023 14:33	129.0 129.0
11/30/2023 14:34	128.9
11/30/2023 14:35	128.9
11/30/2023 14:36	129.0 128.9
11/30/2023 14:38	129.0
11/30/2023 14:39	128.9 128.9
11/30/2023 14:40	128.9
11/30/2023 14:42	128.9
11/30/2023 14:43	128.9 128.9
11/30/2023 14:45	128.9
11/30/2023 14:46	129.0
11/30/2023 14:47 11/30/2023 14:48	128.9 128.9
11/30/2023 14:49	128.9
11/30/2023 14:50	129.0
11/30/2023 14:51 11/30/2023 14:52	128.9 129.0
11/30/2023 14:53	129.0
11/30/2023 14:54	128.9
11/30/2023 14:55 11/30/2023 14:56	128.9 128.9
11/30/2023 14:57	128.9
11/30/2023 14:58	128.9
11/30/2023 14:59	129.0 128.9
11/30/2023 15:01	128.9
11/30/2023 15:02	2000
11/30/2023 15:03 11/30/2023 15:04	128.9 128.9
11/30/2023 15:05	
11/30/2023 15:06	1
11/30/2023 15:07 11/30/2023 15:08	128.9 129.0
11/30/2023 15:09	128.9
11/30/2023 15:10	
11/30/2023 15:11	128.9

	Contract and advisory of the
Buzzi Unicem	Kiln4:
Maryneal TX Kiln	CLINKER_PR
4 Main Stack Mill	OD (TNHR)
Off Run 2	Expression
PASSES CONTRACTOR CONTRACTOR	
Date/Time	Value
11/30/2023 15:39	129.0
11/30/2023 15:40	128.9
11/30/2023 15:41	128.9
CONTROL SECTION CONTROL SECTIO	
11/30/2023 15:42	128.9
11/30/2023 15:43	128.9
11/30/2023 15:44	128.9
11/30/2023 15:45	128.9
11/30/2023 15:46	128.9
11/30/2023 15:47	128.9
11/30/2023 15:48	129.0
11/30/2023 15:49	128.9
11/30/2023 15:50	129.0
11/30/2023 15:51	128.9
11/30/2023 15:52	128.9
V/000000000000000000000000000000000000	
11/30/2023 15:53	128.9
11/30/2023 15:54	128.9
11/30/2023 15:55	128.9
11/30/2023 15:56	1
and the Color of t	
11/30/2023 15:57	128.9
11/30/2023 15:58	128.9
11/30/2023 15:59	129.0
11/30/2023 16:00	129.0
Crossock William Communication	
11/30/2023 16:01	128.9
11/30/2023 16:02	129.0
11/30/2023 16:03	128.9
11/30/2023 16:04	128.9
SACRETIAN REPORTED TO TAKE THE PROPERTY OF THE	
11/30/2023 16:05	128.9
11/30/2023 16:06	129.0
11/30/2023 16:07	128.9
11/30/2023 16:08	129.0
11/30/2023 16:09	128.9
TAXABATTA CINCIPATAN ACADA SANARA MARALANA	128.9
11/30/2023 16:10	
11/30/2023 16:11	129.0
11/30/2023 16:12	128.9
11/30/2023 16:13	128.9
11/30/2023 16:14	128.9
11/30/2023 16:15	128.9
CONTRACTOR OF THE PARTY OF THE	128.9
11/30/2023 16:16	
11/30/2023 16:17	129.0
11/30/2023 16:18	128.9
11/30/2023 16:19	129.0
11/30/2023 16:20	128.9
11/30/2023-16:21	
11/30/2023 16:22	128.9
11/30/2023 16:23	128.9
11/30/2023 16:24	129.0
11/30/2023 16:25	
11/30/2023 16:26	
Accesses to access the second contract of	128.9
11/30/2023 16:27	128.9
11/30/2023 16:28	128.9
11/30/2023 16:29	128.9
11/30/2023 16:30	129.0
11/30/2023 16:31	128.9
91000000000000000000000000000000000000	
11/30/2023 16:32	129.0
11/30/2023 16:33	129.0
11/30/2023 16:34	128.9
11/30/2023 16:35	129.0
11/30/2023 16:36	128.9
	128.9
11/30/2023 16:37	
11/30/2023 16:38	128.9
11/30/2023 16:39	129.0
11/30/2023 16/40	129.0
11/30/2023 16:41	128.9
11/30/2023 16:42	128.9
11/30/2023 16:43	128.9
11/30/2023 16:44	128.9
11/30/2023 16:45	128.9
Average	128 9

Buzzi Unicem	Kiln4:
Maryneal TX Kiin	CLINKER PR
4 Main Stack: Mill Off Run 3	OD (TNHR) Expression
Date/Time	Value
11/30/2023 17:25	128.9
11/30/2023 17:26	128.9
11/30/2023 17:27	128.9
11/30/2023 17:28	128.9
11/30/2023 17:29	128.9
11/30/2023 17:30	128.9
11/30/2023 17:31	128.9
11/30/2023 17:32 11/30/2023 17:33	128.9 128.9
11/30/2023 17:34	128.9
11/30/2023 17:35	129.0
11/30/2023 17:36	128.9
11/30/2023 17:37	128.9
11/30/2023 17:38	128.9
11/30/2023 17:39	129.0
11/30/2023 17:40	128.9
11/30/2023 17/41	128.9
11/30/2023 17:42	129.0
11/30/2023 17:43	128.9 128.9
11/30/2023 17:45	128.9
11/30/2023 17:46	129.0
11/30/2023 17:47	128.9
11/30/2023 17:48	129.0
11/30/2023 17:49	129.0
11/30/2023 17:50	129.0
11/30/2023 17:51	129.0
11/30/2023 17:52	128.9
11/30/2023 17:53	128.9 129.0
11/30/2023 17:55	128.9
11/30/2023 17:56	128.9
11/30/2023 17:57	128.9
11/30/2023 17:58	128.9
11/30/2023 17:59	128.9
11/30/2023 18:00	128.9
11/30/2023 18:01	129.0
11/30/2023 18:02 11/30/2023 18:03	128.9 128.9
11/30/2023 18:04	128.9
11/30/2023 18:05	128.9
11/30/2023 18:06	129.0
11/30/2023 18:07	128.9
11/30/2023 18:08	128.9
11/30/2023 18:09	129.0
11/30/2023 18:10	128.9
11/30/2023 18:11	128.9
11/30/2023 18:12	128.9 128.9
11/30/2023 18:13	128.9
11/30/2023 18:15	128.9
11/30/2023 18:16	128.9
11/30/2023 18:17	128.9
11/30/2023 18:18	128.9
11/30/2023 18:19	129.0
11/30/2023 18:20	128.9
11/30/2023 18:21	128.9
11/30/2023 18:22 11/30/2023 18:23	128.9
11/30/2023 18:23	129.0 128.9
11/30/2023 18:25	128.9
11/30/2023 18:26	128.9
11/30/2023 18:27	129.0
11/30/2023 18:28	128.9
11/30/2023 18:29	128.9
11/30/2023 18:30	128.9
11/30/2023 18:31	128.9 128.9
Average	1784

Appendix E

**Calibration Documents** 

Pitot	Tube	Insp	ection	Sheet	

PITOT I	ube Inspection Sheet		
	_	Date	01/03/23
	O Level	Tube Assembly Level?	Yes
		Ports Damaged?	No
	Bullseye Level	-10 deg < a1 < +10 deg	2
4		-10 deg < a2 < +10 deg	1
		-5 deg < B1 < +5 deg	1
	a1	-5 deg < B2 < +5 deg	1
	8	Y (gamma)	1
	**** <del> </del>	0 (theta)	1
	$\Box$	A (alpha)	0.951
	77-B1	$Z = A (\sin y) < 0.125$ "?	yes
	$\Rightarrow$	W = A (sin 0) < 0.031"?	yes
	B2	Pa =	0.475
		Pb =	0.476
		Tube Diameter (Dt) =	0.376
		Pa = Pb +- 0.063"?	yes
	<b>,</b>		
		(1.05 x Dt)?	0.3948
		(1.50 x Dt)?	0.564
	Fa A	(1.05 x Dt)< P < (1.50 x Dt)?	yes
	Pb		
	Eligible for Default Pitot Calibratio	n Factor (Cp = 0.84)?	Yes

Thermocouple Calibration

Type of Reference Thermometer?	Mercury	Date	01/03/23
Barometeric Pressure?	29.5	2 Ambient Temperature?	68

Source	Reference Temp, F	Thermocouple Temp, F	Absolute Temp Difference
cold air	37	38	-0.20%
medium air	215	215	0.00%
hot air	325	325	0.00%

### Windtunnel Calibration

Pitot Reading	Reference (0.99)	5A S-Type Pitot	Ср
ΔΡ1	0.31	0.44	0.84
$\Delta P_2$	0.31	0.43	0.85
$\Delta P_3$	0.31	0.43	0.85
Average Pitot Tube Calibration Factor>			0.85

Thermocouple Calibration Check (EPA ALT-011 Procedure), performed on 1/3/23

The mide duple damplation officer (LFA ALT-OTT Frocedure), performed on 170/20					
Source	Ref. Temp. F	Thermocouple Temp. F	± 2 deg F?		
Ambient	68	66.9	Yes		

	Pitot	Tube	Inspection	Sheet
--	-------	------	------------	-------

PILOLI	ube Inspection Sheet	***	
	_	Date	01/03/23
	O Level	Tube Assembly Level?	Yes
		Ports Damaged?	No
	Buliseye Level	-10 deg < a1 < +10 deg	1
		-10 deg < a2 < +10 deg	2
		-5 deg < B1 < +5 deg	1
	ai	-5 deg < B2 < +5 deg	2
	8a2	Y (gamma)	1
	₹	0 (theta)	1
		A (alpha)	0.94
	81	Z = A (sin y) < 0.125"?	yes
		W = A (sin 0) < 0.031"?	yes
	B2	Pa =	0.47
		Pb =	0.47
		Tube Diameter (Dt) =	0.376
		Pa = Pb +- 0.063 <u>"</u> ?	yes
700		(1.05 x Dt)?	0.3948
P Paris a cucha cu	4	(1.50 x Dt)?	0.564
Phonore statution and	Pa		
Addition soons to document	Pb A	(1.05 x Dt)< P < (1.50 x Dt)?	yes
		u.	
	Eligible for Default Pitot Calibration	Factor (Cp = 0.84)?	Yes

Thermocouple Calibration

mornio o o apio o ambration			
Type of Reference Thermometer?	Mercury	Date	01/03/23
Barometeric Pressure?	29.52	Ambient Temperature?	69.9

Source	Reference Temp, F	Thermocouple Temp, F	Absolute Temp Difference
cold air	37	38	-0.20%
medium air	215	215	0.00%
hot air	325	324	0.13%

**Windtunnel Calibration** 

Pitot Reading	Reference (0.99)	5B S-Type Pitot	Ср
ΔP <sub>1</sub>	0.31	0.44	0.84
ΔP <sub>2</sub>	0.31	0.43	0.85
ΔP <sub>3</sub>	0.31	0.44	0.84
	0.84		

Thermocouple Calibration Check (E)	A ALI-UII FIOL	sudre), periorified off traiza		
Source	Ref. Temp. F	Thermocouple Temp. F	± 2 deg F?	
Ambient	69.9	69.4	Yes	

# MET

METHO	)D 5 D(	RY GAS N	IETER C	METHOD 5 DRY GAS METER CALIBRATION USING CRITICAL ORI	USING C	RITICAL OF	RIFICES						Quality - Sen	Quality - Service - Reliability	100 m	VICE BY CONTROL OF			
	(5 (8) (4)	Select three c Record barom Run at tested necessary to a Record data a	ritical orifices netric pressur vacuum (fron schieve a min nd informatio	Select three critical orifices to calibrate the dry gas meter which bracket the expected operating range. Record barometric pressure before and after calibration procedure.  Run at tested vacuum (from Orifice Calibration Report), for a period of time necessary to achieve a minimum total volume of 5 cubic feet.  Record data and information in the GREEM cells, YELLOW cells are calculated.	gas meter whii salibration proco (Report), for a of 5 cubic feet. Ils, YELLOW or	ch bracket the exedure. period of time	pected ope	rating rang	a)				ENVIR	ONMEN	ENVIRONMENTAL SUPPLY COMPANY	LY COM	PANY		
METER	DATE:	12/28/21 M5-15		MEYER SERIAL#: CRITICAL ORIFICE SET SERIAL#:	METER SERIAL#: CE SET SERIAL#:	MS-15	â	BAROMETRIC PRESSURE (In Hg):	PRESSI	JRE (in Hg	INITIAE 30.03	FINAL. 30.03	AVG (P <sub>bar)</sub> 30.03		IF.	IF Y VARIATION EXCEEDS 2.00%, ORIFICE SHOULD BE RECALIBRATED	KCEEDS 2.00%,		
		ž	TESTED					TEME	TEMPERATURES °F	tes %		ELAPSED					<b>/</b> ▼		
ORIFICE #	%CN #	FACTOR (AVG)	VACUUM (in Ha)	DGW	DGM READINGS (FT3)	T³) NET (V=)	AMBIENT	DGM INLET		DGM OUTLET INITIAL FINAL	T DGM	TIME (MIN)	DGM AH	(1) V (STD)	(2) V (STD)	(£) >	Y VARIATION (%)	, and a	
	-	0 3283				000					] _				-				] [
12	- ~	0000				0.000											- , _ ,		Т
	en					0.000					•								_
	<u></u>	0.4094	85	353.924	359.213	5.289	75	62	65 6	62 62	62.75	10.00	0.8	5.3733	AVG =	0.989		1.62	_
<u>ক</u>	~	0.4094	18	359.213	364.553	5.340	9/	9 9	9 99	62 63		10.00	9.0	5,4122	5.3119	0.981		1.62	
	J					0.000					•			,	AVG =	0.985	1.09		
	_	0.5047	18	364.553	371.213	6.660	92	99	70 6	63 65	99	10.00	1.3	6.7325	6.5483	0.973		1.72	
<u>0</u>	24 6	0.5047	48	371.213	377.910	6.697	9/	70	72 6	65 66	68.25	10.00	£.	6.7411	6.5483	0.971		1.72	
	_					2000			-	-	•				AVG=	0.972	-0.29		7
ļ	<u></u>	0.6426	18	377.910	386.465	8.555	11	2	74 6	89 99	69.5	10.00	2.1	8.6078	8.3298	0.968		1.71	
73	7 6	0.6426	18	386.465	395.066	8.601	#	24	22	68 69	71.5	10.00	2.1	8.6215	8.3298	996.0		1.71	
	., L									$\left\{ \ \right\}$	, ] [				AVG≈	0.967	-0.81		٦ [
	——— <u>—</u>	0.8587				0.000					•								
32	7					0.000					0								
	<u></u>					0.000			-		•								
T SNICH	JITIGO DE	STATE OF TAX	200.00	I ISBN THE CRITICAL ADICIDES AS AS AS A STATE OF THE ABOVE											AVG =				

USING THE CRITICAL ORIFICES AS CALIBRATION STANDARDS:
The following equations are used to calculate the standard volumes of air passed through the DGM, Vm (std), and the critical orifice, Vcr (std), and the DGM calibration factor, Y. These equations are automatically calculated in the

 $Vm_{(sd)} = K_1 * Vm * Pbar + (\Delta H^-13.6)$ 

€

= Net volume of gas sample passed through DGM, corrected to standard conditions K<sub>1</sub> = 17.64 °R/in. Hg (English), 0.3858 °K/mm Hg (Metric)

T<sub>m</sub> = Absolute DGM avg. temperature (°R · English, °K - Metric)

■ Volume of gas sample passed through the critical oritice, corrected to standard conditions

T<sub>somb</sub> = Absolute ambient temperature (PR - English, PK - Metric)

1.68 AVERAGE AH@ =

0.975

AVERAGE DRY GAS METER CALIBRATION FACTOR, Y =

@ 0 F @ 500 F @ 1000 F 0 496 1000 (per manufacturer procedure) Potentiometer Check, °F

Avg Absolute Difference =

0.1%

K' = Average K' factor from Critical Orifice Calibration

DGM calibration factor

 $Y = \frac{V_C \xi_{sap}}{V m_{trap}}$ 

3

 $Vcr_{(v,t)} = K^* * \frac{Pbar * \Theta}{\sqrt{Tamb}}$ 

3

# METHOD 5 DRY GAS METER CALIBRATION USING CRITICAL ORIFICES

**ENVIRONMENTAL SUPPLY COMPANY** 

- Select three critical orifices to calibrate the dry gas meter which bracket the expected operating range.
   Record barometric pressure before and after calibration procedure.
   Run at tested vacuum (from Orifice Calibration Report), for a period of time
- necessary to achieve a minimum total volume of 5 cubic feet.

		CEEDS 2.00%,	CALIBRATED	_*	>-	VARIATION (%)	ָ   		J			1			2.83				-0.87				-1.96	1	I.		
		IF Y VARIATION EXCEEDS 2.00%,	ORIFICE SHOULD BE RECALIBRATED		(3)	Υ						1.017	1.008		1.012	0.979	0.973		0.976	0.966	0.964		0.965				
		F Y	ORIFICE		(2)	Ver (STD)					AVG =	5.3499	5.3499		AVG =	6.5890	6.5953		AVG =	8.3973	8.3973		AVG =				AVG =
					ε	V <sub>m</sub> (STD)						5.2584	5.3100			6.7289	6.7798			8,6894	8.7089						
	AVG (Pbw)	29,99			DGM AH	(in H <sub>2</sub> O)						0.86	0.86			1.3	1.3			2.1	2.1						
	FINAL	29.99		ELAPSED	TIME (MIN)	θ						10.00	10.00			10.00	10.00			10.00	10.00						
	INITIAL	29.99			DGM	AVG		0	0	0		69	69.25	0		70	70.25	0		70.75	72	0		0	0	0	
	_	(in Hg):		ų	DGM OUTLET	FINAL						69	69			70	70			70	70						
		BAROMETRIC PRESSURE (in Hg):		TEMPERATURES ºF		INITIAL FINAL INITIAL FINAL			_			69	69			69	69			69	70						
		ETRIC PR		TEMPER	DGM INLET	AL FINA!			-			69	70			71	72	_		74	76					_	
		BAROM				IN IN						69	8			70	70			70	72						
ģ					AMBIENT							67	67			89	67			67	49						
ens are calculate		M5-21	14315		r³)	%ET (Vm)		0.000	0.000	0.000		5.244	5.298	0.000		6.716	6.770	0.000		8.668	8.708	0.000		0.000	0.000	0.000	
ils, YELLOW CR		METER SERIAL #:	SET SERIAL #:		DGM READINGS (FT3)	FINAL						63.745	69.109			75.825	82.595			91.263	99.971						
<ol> <li>Kecord data and information in the GREEN cells, YELLOW cells are calculated.</li> </ol>		Ā	CRITICAL ORIFICE SET SERIAL #:		םפו	INITIAL						58.501	63.811			69.109	75.825			82.595	91.263						
nd knformation i			2	TESTED	VACUUM	(jn Kg)	   					18	18			18	18			18	18						
Record data ar		12 8 22	M5-21	ž	FACTOR	(AVG)		0.3283				0.4094	0.4094			0.5047	0.5047			0.6426	0.6426			0.8587			
4	L	DATE	METER PART #:			# NO&	]		~	m	. '	₹~	~	m		_	7	ю	. '	<del></del>	~	e	. '	-	7	ო	
			METER			ORIFICE # RUN #			7				15				9				23				32		

1.69 1.69 1.69 1.68 1.68 1.68

USING THE CRITICAL ORIFICES AS CALIBRATION STANDARDS:
The following equations are used to calculate the standard volumes of air passed through the DGM, Vm (std), and the critical orifice, Vcr (std), and the DGM calibration factor, Y. These equations are automatically calculated in the

 $Vm_{(sd)} = K_1 * Vm * Pbar + (\Delta H \cdot 13.6)$ €

 $Vcr_{(u,v)} = K^* * \frac{Pbar * \Theta}{\sqrt{Tamb}}$ 

8

= Net volume of gas sample passed through DGM, corrected to standard conditions K<sub>1</sub> = 17.64 °R/in. Hg (English), 0.3858 °K/mm Hg (Metric)

T.m. = Absolute DGM avg. temperature ("R - English, "K - Metric)

 Volume of gas sample passed through the critical oritice, corrected to standard conditions Tans = Absolute ambient temperature (9R - English, 9K - Metric)

1000 (per manufacturer procedure) Potentiometer Check, "F

@ 500 F @ 1000 F

@ 0 F

0.985

AVERAGE DRY GAS METER CALIBRATION FACTOR, Y =

1.69

AVERAGE AH@ =

0.1%

Avg Absolute Difference =

K' = Average K' factor from Critical Orifice Calibration DGM calibration factor

 $\gamma = \frac{V_{CQ_{stab}}}{V_{M_{stab}}}$ 

ල

Company: Buzzi Unicem; Maryneal TX Source: Main Stack; Raw Mill Off Job ID: 23-3315 Train Type: EPA Method 26A

Alt-009 Alternate Post Test Calibration Data

o Arcanara I ost i est Campiano I Data	 م	ű	8.4	g	7.4	78		
	11/30/23	11/30/23	30-Nov-23	30-Nov-23	30-Nov-23	30-Nov-23	M5-15	M5-21
	1405-1511	1405-1511	1539-1645	1539-1645	1725-1831	1725-1831	Averages	Averages
۳۸	44.671	43.937	45.804	44.587	45.736	45.342		
πL	538	542.3	538.1	541.3	538.1	542.3		
Pb	27.43	27.43	27.43	27.43	27.43	27.43		
Havg	1.48	1.46	1.51	1.51	1.52	1.54		
@H	1.68	1.69	1.68	1.69	1.68	1.69		
Md	31.3	31.3	31.26	31.26	31.248	31.248		
(Havg)^0.5	1.2135534	1.20637998	1.22591897	1.22591897	1.22999959	1.23974091		
Run Time, Min	09	09	09	09	09	09		
Calculated Gamma (Yqa)	0.956	0.967	0.942	0.968	0.947	0.963	0.948	0.966
Meter Gamma	0.975	0.985	0.975	0.985	0.975	0.985	0.975	0.985
% difference from Actual Y	1.99%	1.85%	3.37%	1.75%	2.89%	2.19%	2.75%	1.93%





### CERTIFICATE OF ANALYSIS

**Grade of Product: EPA Protocol** 

Part Number:

E04NI77E15A3796

Reference Number: 122-401833216-1

Cylinder Number:

EB0066680

Cylinder Volume:

151.1 CF

Laboratory:

124 - Durham (SAP) - NC

Cylinder Pressure:

2015 PSIG

PGVP Number:

B22020

Valve Outlet:

590

Gas Code:

Certification Date:

Jun 23, 2020

CO,CO2,O2,BALN **Expiration Date:** Jun 23, 2028

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals

		ANALYTICAL	L RESULTS		
Component	Requested Concentration	Actual Concent <u>ration</u>	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON MONOXIDE	65.00 PPM	63,68 PPM	G1	+/- 0.5% NIST Traceable	06/23/2020
CARBON DIOXIDE	10.00 %	10.01 %	G1	+/- 0.6% NIST Traceable	06/22/2020
OXYGEN	12.00 %	11.82 %	G1	+/- 0.9% NIST Traceable	06/22/2020
NITROGEN	Balance				

			CALIBRATION STANDARDS		
Туре	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	09010213	KAL004779	98.48 PPM CARBON MONOXIDE/NITROGEN	+/- 0.5%	Oct 16, 2024
NTRM	13060638	CC414571	13,359 % CARBON DIOXIDE/NITROGEN	+/- 0.6%	May 14, 2025
NTRM	98051109	SG9168283BAL	9.507 % OXYGEN/NITROGEN	+/- 0.7%	Oct 06, 2021

	ANALYTICAL EQUIPMEN	Γ
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA510 CO2 2L6YXWY0	Nondispersive Infrared (NDIR)	May 28, 2020
Horiba VIA510 CO 1G46EA07	Nondispersive Infrared (NDIR)	Jun 18, 2020
Horiba MPA510 O2 41499150042	Paramagnetic	May 28, 2020

Triad Data Available Upon Request



Approved for Release



**Airgas Specialty Gases** Airgas USA LLC 630 United Drive Durham, NC 27713 Airgas.com

### **CERTIFICATE OF ANALYSIS**

### **Grade of Product: EPA PROTOCOL STANDARD**

Part Number:

E04NI59E15A38X3

Reference Number: 122-402389885-1A

Cylinder Number:

ALM-056015

Cylinder Volume:

143.7 CF

Laboratory:

124 - Durham (SAP) - NC

Cylinder Pressure:

2016 PSIG

PGVP Number:

B22022

Valve Outlet:

590 Mar 28, 2022

Gas Code:

CO,CO2,O2,BALN

Certification Date:

Expiration Date: Mar 28, 2030

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a mole/mole basis unless otherwise noted.

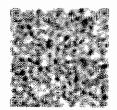
Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

		ANALYTICAI	LRESULTS		
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON MONOXIDE	120.0 PPM	116.5 PPM	G1	+/- 0.3% NIST Traceable	03/28/2022
CARBON DIOXIDE	18.00 %	18.17 %	G1	+/- 0.7% NIST Traceable	03/28/2022
OXYGEN	22.00 %	21.90 %	G1	+/- 0.5% NIST Traceable	03/28/2022
NITROGEN	Balance				

		•	CALIBRATION STANDARDS		
Туре	Lot ID	Cylinder No	Concentration	Uncertainty	<b>Expiration Date</b>
NTRM	13010207	KAL003102	246.9 PPM CARBON MONOXIDE/NITROGEN	+/- 0.2%	Oct 16, 2024
NTRM	12061508	CC354696	19.87 % CARBON DIOXIDE/NITROGEN	+/- 0.6%	Jan 11, 2024
NTRM	08010220	K013155	23,20 % OXYGEN/NITROGEN	+/- 0.4%	Jun 01, 2024

	ANALYTICAL EQUIPME	NT
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VA-5001 CO2 BF89GV17	Nondispersive Infrared (NDIR)	Mar 01, 2022
Horiba VIA510 CO RS2EGL6K	Nondispersive Infrared (NDIR)	Mar 01, 2022
Siemens Oxymat 61 M3299 O2	Paramagnetic	Mar 01, 2022

Triad Data Available Upon Request



Approved for Release



Airgas Specialty Gases Airgas USA LLC 630 United Drive Durham, NC 27713 Airgas.com

122-402705571-1

### CERTIFICATE OF ANALYSIS

### **Grade of Product: CERTIFIED STANDARD-SPEC**

Part Number:

Cylinder Number:

Laboratory:

Analysis Date: Lot Number:

X02NI99C15A54F5

CC426155 124 - Durham (SAP) - NC

Mar 28, 2023

122-402705571-1

Expiration Date: Mar 28, 2031

Reference Number:

Cylinder Volume:

144.0 CF Cylinder Pressure: 2015 PSIG

Valve Outlet: 350

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T.

	Al	NALYTICAL RESULTS	
Component	Req Conc	Actual Concentration (Mole %)	Analytical Uncertainty
ETHYLENE NITROGEN	75.00 PPM Balance	75.47 PPM	+/- 2%

Gas Mixture reference materials.





Approved for Release



### CERTIFICATE OF ACCURACY: GMACS-c Calibration Standard

CUSTOMER INFORMATION

AIRGAS SPECIALTY GASES

Work Order #: 160-402845895-1

Customer: DEECO Inc.

**Exploratory Products Group** 

Sales Order #: 1123601913

Address 1: 3404 Lake Woodard Road

6141 Easton Road

PO#: 7100179560

Address 2:

Plumsteadville, PA 18949

City / State / Zip: Raleigh, NC 27604

PRODUCT INFORMATION

COMPOSITION

CONCENTRATION

UNCERTAINTY (Abs)

UNCERTAINTY (Rel)

Hydrogen Cyanide Sulfur Hexafluoride 199.1 PPM 10.0 PPM

5.7 PPM 0.07 PPM 2.9 % 0.7 %

Nitrogen

Balance

CYLINDER #: CC768233

AIRGAS PART #: X03NI99C15AC0Y6

CYLINDER TYPE: 150A Aluminum

8-Sep-2023 CERTIFICATION DATE:

CGA: 350 SS

EXPIRATION DATE:

8-Mar-2024

CYLINDER PRESSURE: 2000 psig

MIXTURE DEW POINT: N/A

CERTIFICATION DATA

BLENDING PROCESS: GravStat™ Gravimetry

CONCENTRATION

UNCERTAINTY (Abs)

UNCERTAINTY (Rel)

Hydrogen Cyanide Ifur Hexafluoride

COMPONENT

200.40 PPM 10.01 PPM

3.0 PPM 0.07 PPM 1.5 % 0.7 %

CONFIRMING ANALYSIS: FTIR Spectroscopy

INSTRUMENT / MODEL:

CAI Model 700 FTIR

COMPONENT

CONCENTRATION

UNCERTAINTY (Abs)

**UNCERTAINTY (Rel)** 

Hydrogen Cyanide

197.9 PPM

4.9 PPM

2.5 %

REFERENCE STANDARD: GMPS-c 200 PPM Hydrogen Cyanide

CYLINDER NUMBER:

CC768217

EXPIRATION DATE: 2/27/2024

COMPONENT

CONCENTRATION

**UNCERTAINTY (Abs)** 

UNCERTAINTY (Rel)

Hydrogen Cyanide

197.1 PPM

4.8 PPM

2.4 %

CALIBRATION CURVE DATA

Curve Order

Correlation

Slope (X2)

Slope (X)

Intercept

Point-to-Point Matching Std

Linear / Direct Ratio

N/A

N/A

N/A

N/A

INTERLOCK STATISTICS

CONCENTRATION

**UNCERTAINTY (Abs)** 

**UNCERTAINTY (Rel)** 

**BLEND RESULT:** ANALYSIS RESULT: 200.40 PPM 197.9 PPM

3.0 PPM 4.9 PPM 1.5 % 2.5 %

INTERLOCK RESULT:

199.1 PPM

5.7 PPM

2.9 %

COMMENTS / SPECIAL INSTRUCTIONS

- A GMACS-c ("Candidate GMACS") is made and certified according to the EPA GMACS Procedure (Alt-114) found at: https://cfpub.epa.gov

2. Do not use this standard if pressure is less than 200 psig.

Do not use or store this product at or below the stated dew point.

APPROVED BY:

**BOB GRASMEDER** 



### CERTIFICATE OF ACCURACY: GMACS-c Calibration Standard

CUSTOMER INFORMATION

AIRGAS SPECIALTY GASES

**Exploratory Products Group** 

6141 Easton Road

Plumsteadville, PA 18949

Work Order #: 160-402845897-1

Sales Order #: 1123601913

PO#: 7100179560

Customer: DEECO Inc.

Address 1: 3404 Lake Woodard Road

Address 2:

City / State / Zip: Raleigh, NC 27604

PRODUCT INFORMATION

COMPOSITION Hydrogen Cyanide

Sulfur Hexafluoride

Nitrogen

CONCENTRATION 49.9 PPM

> 5.0 PPM Balance

UNCERTAINTY (Abs)

2.3 PPM 0.07 PPM **UNCERTAINTY (Rel)** 

4.6 %

1.3 %

CYLINDER #: CC768222

CYLINDER TYPE: 150A Aluminum

CGA: 350 SS

CYLINDER PRESSURE: 2000 psig

AIRGAS PART #: X03NI99C15AC0W8

CERTIFICATION DATE: 7-Sep-2023 EXPIRATION DATE: 7-Mar-2024

MIXTURE DEW POINT: N/A

CERTIFICATION DATA

BLENDING PROCESS: GravStat™ Gravimetry

COMPONENT Hydrogen Cyanide lfur Hexafluoride CONCENTRATION

50.02 PPM

5.02 PPM

**UNCERTAINTY (Abs)** 

0.9 PPM 0.07 PPM UNCERTAINTY (Rel)

1.8 % 1.3 %

CONFIRMING ANALYSIS: FTIR Spectroscopy

INSTRUMENT / MODEL: CAI Model 700 FTIR

COMPONENT Hydrogen Cyanide CONCENTRATION

49.8 PPM

UNCERTAINTY (Abs) 2.1 PPM

UNCERTAINTY (Rel)

4.2 %

REFERENCE STANDARD: GMPS-c 50 PPM Hydrogen Cyanide

CYLINDER NUMBER: CC768196

EXPIRATION DATE: 2/29/2024

**COMPONENT** 

CONCENTRATION

UNCERTAINTY (Abs)

UNCERTAINTY (Rel)

Hydrogen Cyanide

48.9 PPM

1.7 PPM

3.4 %

**CALIBRATION CURVE DATA** 

Curve Order

Correlation

Slope (X2)

Slope (X)

Intercept

Point-to-Point Matching Std

Linear / Direct Ratio

N/A

N/A

N/A

N/A

INTERLOCK STATISTICS

CONCENTRATION

**UNCERTAINTY (Abs)** 0.9 PPM

UNCERTAINTY (Rel) 1.8 %

BLEND RESULT: **ANALYSIS RESULT:** INTERLOCK RESULT: 50.02 PPM 49.8 PPM 49.9 PPM

2.1 PPM 2.3 PPM 4.2 % 4.6 %

COMMENTS / SPECIAL INSTRUCTIONS

A GMACS-c ("Candidate GMACS") is made and certified according to the EPA GMACS Procedure (Alt-114) found at: https://cfpub.epa.gov

之. Do not use this standard if pressure is less than 200 psig.

3. Do not use or store this product at or below the stated dew point.

APPROVED BY		

**BOB GRASMEDER** 

Client: Buzzi Maryneal TX

Test Location: Main Stack; Stratification Check Date: Nov 29, 2023 Start Time: 14:50:05

Run number 1

One Minute Averages

	Reference	Plant
	02	02
	%,dry	%,dry
2:51:03 PM	10.8	11.5
2:52:03 PM	10.7	11.4
2:53:03 PM	10.8	11.4
2:54:03 PM	10.8	11.4
2:55:03 PM	10.8	11.5
2:56:03 PM	10.7	11.5
Point A	10.8	11.4
2:57:03 PM	10.8	11.5
2:58:03 PM	10.8	11.5
2:59:03 PM	10.8	11.4
3:00:03 PM	10.8	11.5
3:01:03 PM	10.8	11.4
3:02:03 PM	10.8	11.5
Point B	10.8	11.5
3:03:03 PM	10.8	11.5
3:04:03 PM	10.8	11.4
3:05:03 PM	10.8	11.4
3:06:03 PM	10.8	11.5
3:07:03 PM	10.8	11.3
3:08:03 PM	10.8	11.4
Point C	10.8	11.4
Average	10.8	11.4

Date/Time	Kiln4: O2 (PCT) Raw Value
11/29/2023 14:50	11.45
11/29/2023 14:51	11.43
11/29/2023 14:52	11.42
11/29/2023 14:53	11.40
11/29/2023 14:54	11.45
11/29/2023 14:55	11.45
11/29/2023 14:56	11.47
11/29/2023 14:57	11.50
11/29/2023 14:58	11.36
11/29/2023 14:59	11.45
11/29/2023 15:00	11.40
11/29/2023 15:01	11.53
11/29/2023 15:02	11.48
11/29/2023 15:03	11.40
11/29/2023 15:04	11.43
11/29/2023 15:05	11.50
11/29/2023 15:06	11.31
11/29/2023 15:07	11.42

Buzzi Unicem, Maryneal TX Main Stack

Pretest							
Spectrum	Date Time	HCN PCA 191c R1 191c	SF6 (10) 191C	Ethylene (100,3000) 191C HF ppm (10) 191C	HF ppm (10) 191C	SNR 2500	sBeam @ 2500
SPC_000830BKG.LAB	11/14/23 06:57:22.688	0.000	0.000	0.000	0.000	NaN	1.41
SPC_000831.LAB	11/14/23 06:58:33.020	-0.004	-0.001	-0.037	0.011	6779.16	1.42
SPC_000832BKG.LAB	11/14/23 07:01:13.650	0.000	0.000	0.000	0.000	5353.34	1.42
SPC_000833.LAB	11/14/23 07:02:24.028	-0.064	0.003	-0.062	0.018	5553.53	1.42
SPC_000834.LAB	11/14/23 07:03:28.036	-0.154	-0.000	0.013	2000	4837.84	1.42
SPC_000835.LAB	11/14/23 07:04:32.104	0.035	0.001	-0.014	0.003	5479.59	1.42
SPC_000836BKG.LAB	11/14/23 07:07:39.052	0.000	0.000	0.000	0.000	5734.58	1.42
SPC_000837.LAB	11/14/23 07:08:49.639	-0.051	-0.001	-0.019	-0.002	6223.51	1.42
SPC000838.LAB	11/14/23 07:09:53.338	-0.032	-0.003	0.027	-0.000	5809.30	1.42
SPC_000839.LAB	11/14/23 07:10:57.234	0.046	-0.000	-0.014	-0.017	3759.60	1.42
SPC_000840.LAB	11/14/23 07:12:01.138	-0.011	-0.001	-0.102	0.016	4373.66	1.42
SPC_000841.LAB	11/14/23 07:13:05.164	0.080	-0.001	-0.068	0.002	5347.95	1.42
SPC_000842.LAB	11/14/23 07:14:08.941	0.059	-0.001	-0.051	-0.012	5012.46	1.42
SPC_000843.LAB	11/14/23 07:15:12.843	-0.029	-0.002	-0.084	-0.006	4706.13	1.42
	Standard Deviation x 3	0.156	0.002		0.032		
	Averages					5033.23	1.42
SPC_003144.LAB	11/29/23 10:07:23.437	-0.070	600.0-	73.818	0.009	3771.37	1.25
SPC_003145.LAB	11/29/23 10:08:27.783	-0.180	-0.008	74.579	0.010	4602.22	1.25
SPC_003146.LAB	11/29/23 10:09:31.168	-0.255	-0.011	74.391	0.004	3362.83	1.25
SPC_003147.LAB	11/29/23 10:10:35.067	-0.286	-0.016	74.456	-0.005	3721.81	1.25
Ethylene Calibration Transfer Standard (CC426155; 75.47 ppm)	tandard (CC426155; 75.47 ppr	(u		74.475			
SPC_003163.LAB	11/29/23 10:32:14.551	195.980	9.583	-0.647	-0.007	NaN	1.25
SPC003164.LAB	11/29/23 10:33:18.264	196.278	9.585	-0.465	-0.017	4782.81	1.25
SPC003165.LAB	11/29/23 10:34:22.223	196.975	9.583	-0.523	-0.015	5254.76	1.25
SPC_003166.LAB	11/29/23 10:35:26.094	197.038	9.580	-0.445	-0.014	5634.48	1.25
SPC_003167.LAB	11/29/23 10:36:30.150	197.342	9.580	-0.500	-0.009	5809.63	1.25
HCN Standard (CC768233; 199.1 ppm HCN/10.0 ppm SF6)	1 ppm HCN/10.0 ppm SF6)	196.908	9.582				
SPC_003172.LAB	11/29/23 10:41:49.573	49.888	4.852	-0.442	-0.014	4728.10	1.25
SPC_003173.LAB	11/29/23 10:42:53.522	49.909	4.847	-0.380	-0.005	4092.51	1.25
SPC_003174.LAB	11/29/23 10:43:57.490	49.927	4.851	-0.391	-0.016	3563.85	1.25
SPC_003175.LAB	11/29/23 10:45:01.307	49.815	4.849	-0.423	-0.020	4533.18	1.25
SPC_003176.LAB	11/29/23 10:46:05.212	49.899	4.848	-0.380	-0.004	3854.17	1.25
HCN Standard (CC768222; 49.9 ppm HCN/5.0 ppm SF6)	ppm HCN/5.0 ppm SF6)	49.887	4.849				

## Analysis Validation Report

Sample Filename: F:\Maryneal\November 29\SPC\_003269.LAB

Filename for noise: F:\Midlothian on Renta\November 14\SPC\_000837.LAB Interferences Filenames: C:\Midlothian on Renta\November 15\SPC\_001463.LAB C:\Midlothian on Renta\November 15\SPC\_001464.LAB C:\Midlothian on Renta\November 15\SPC\_001466.LAB C:\Midlothian on Renta\November 15\SPC\_001466.LAB C:\Midlothian on Renta\November 15\SPC\_001466.LAB C:\Midlothian on Renta\November 15\SPC\_001467.LAB C:\Midlothian on Renta\November 15\SPC\_001469.LAB C:\Midlothian on Renta\November 15\SPC\_001469.LAB C:\Midlothian on Renta\November 15\SPC\_001469.LAB C:\Midlothian on Renta\November 15\SPC\_001469.LAB

Recipe path: C:\OLT\recipes\Cement Testing R3.MGRCP

Comment Good Close to DL Check it!	e to DL	₩ ************************************	≅ X ъ≠	, 773	e to DL 1	e to DL	e to DL	e to DL	e to DL	关证	e to DL	e to DL	注:	e to DL	e to DL	e to DL	e to DL
Good Close	Close Good Good	000 G	0000	9000	Soo Goog	Close	Close	Close		Chec	Close	Close	Chec	Clos	Close	Close	Clos
Span	1 1 1	1 1 1	, , ,	,		, ,	ı		, 1		t		,	,	ŧ	ı	
gma Range 0-200 0.02 0-10 0-10	0-3000 0-40 0-40	0-100 0-1000 0-3000	0-300 0-500 0-1	0-70	0-1000 0-250	0-100	0-150	0-2000	0-3000	0-3000	0-1000	0-1000	0-100	0-200	0-20	0-10	0-150
Sigma - 0.02	0.11	0.02 0.12 0.07		0.09	0.08	0.14	0.01	0.68	0.12	0.11	0.05	0.06	0.01	0.11	0.01	0.05	0.23
	0.75	0.01	_ ' c	0.04	0.35	0.3	0.01	1.78	0.09	0.27	90.0	0.3	0	0.22	0.25	0.03	0.44
. CL ~ 0.17 - 0.22 0.01 -	1.55 0.28 - 0.27 -	0.41 0.82 2.62	3.23	0.75	0 8 7	0.72	0.31	4.15	11.91	6.25	1.58	3.81	0.14	<del>-</del>	0.29	0.33	1.14
. DL .	1.08	0.06	<u>n</u> c	0.33	0.59	0.72	0.05	3.81	0.44	0.61	0.21	0.49	0.02	0.54	0.29	0.17	1.14
OCU . 0.46 - 0.45 0.02 -	3.11 0.33 -	1.05 2.17 5.69	2.23 10.18 - 0	1.32	2.63 3.15	0.89	0.35	6.36	24.41	12.24	2.29	5.01	0.23	1.36	0.16	0.55	0.41
	3.11 0.33 0.25								_		_					_	
MAU F 0.34 0.07	0.29	0.28	0.43	0.24	0.38	0.14	0.03	1.12	2.25	1.81	0.37	0.5	0.02	0.22	0.05	0.16	0.04
MDC1 0.28 0.04	0.01	0.15	0.2	0.2	0.35	0.12	0.02	0.88	1.19	<u>~</u>	0.31	0.43	0.02	0.2	0.05	0.14	0.03
_	0.33	0.05	0.00	0.28	0.23	0.42	0.04	2.03	0.35	0.34	0.15	0.19	0.02	0.32	0.04	0.14	0.7
	0.17 - 0.18 -	0.58 1.13 4.15	6.4 6.99	1.09	2.41 1.19	0.75	0.34	5 2	12.94	7.43	1.89	4.28	0.17	1.22	0.15	0.48	0.38
Conc N 8.65 -0.06	2.92 13.76 13.46	1.23 12.1 129.08	161.72	5.44	2.22 4.96	1.17	-0.1	0.16	2.21	4.45	0.62	1.78	0.61	1.17	0.02	8.0	-3.51
Gas calibration Name HCN (200) PCA 191C 191C HF PPM (10) 191C SF6 (10) 191C	ETHYLENE (100,3000) 191C H2O% (40) 191C CO2% (40) 191C	HCL PPM (100) 191C SO2 (1000) 191C NO (350,3000) 191C	CO (500) 191C (10F2) CO (500) 191C (10F2) CO% (1) 191C (20F2)	FORMALDEHYDE (70) 191C	ACE I ALDEHYDE (1000) 191C CH4 (250) 191C (10F2)	PROPANE (100) 191C HBR (100) 180C	NO2 (150) 191C (10F2)	NO2 (2000) 191C (20F2)	NH3 (3000) 191C (20F2)	CH4 (3000) 191C (20F2)	ACETYLENE (1000) 191C	PROPYLENE (200,1000) 191C	COS (100) 150C	ETHANE (500) 191C	H2SO4 (50) 150C	MEOH (10) 191C	SO3 (150) 191C

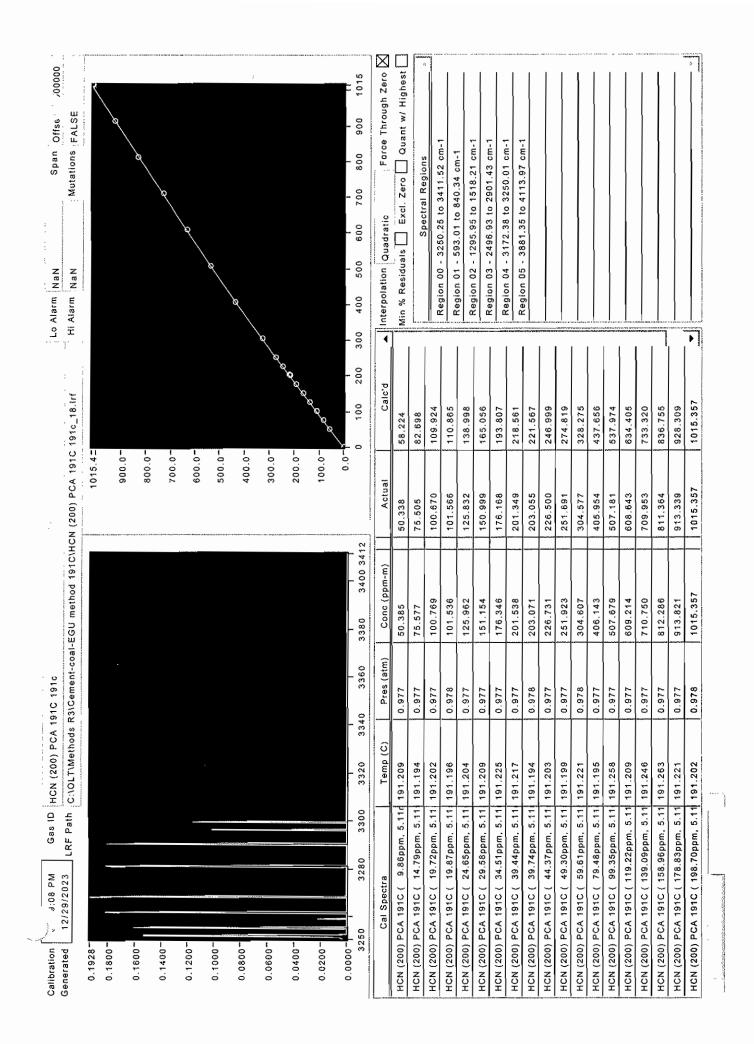
## Analysis Validation Report

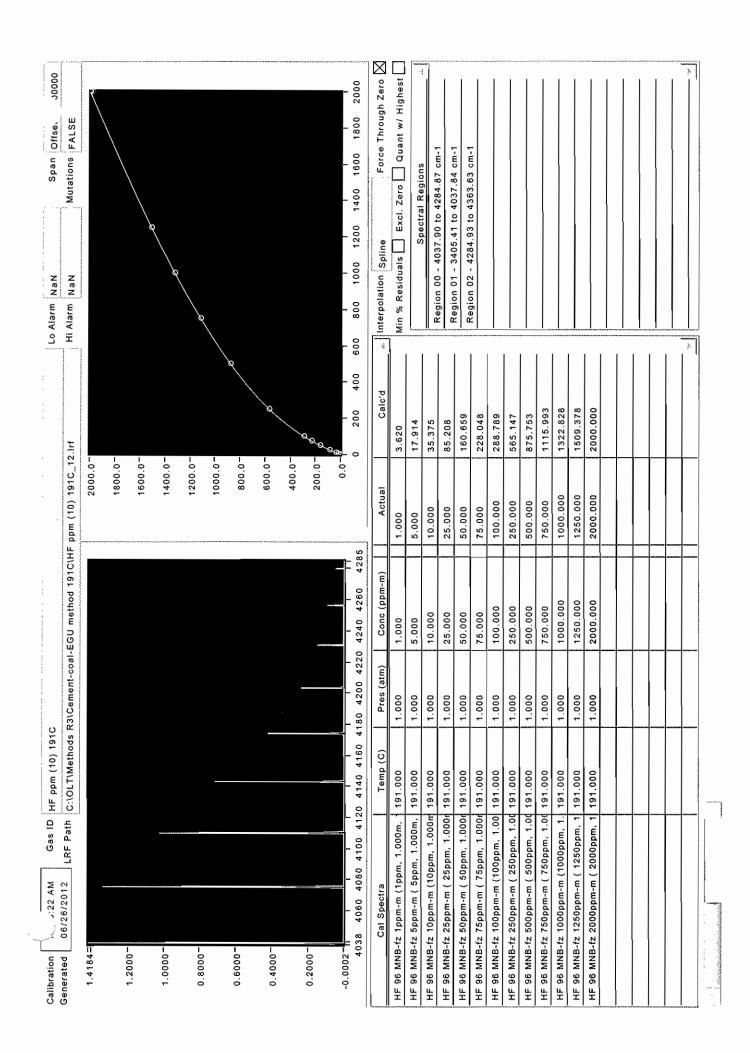
Sample Filename: F:\Marynea\\November 29\SPC\_003270.LAB

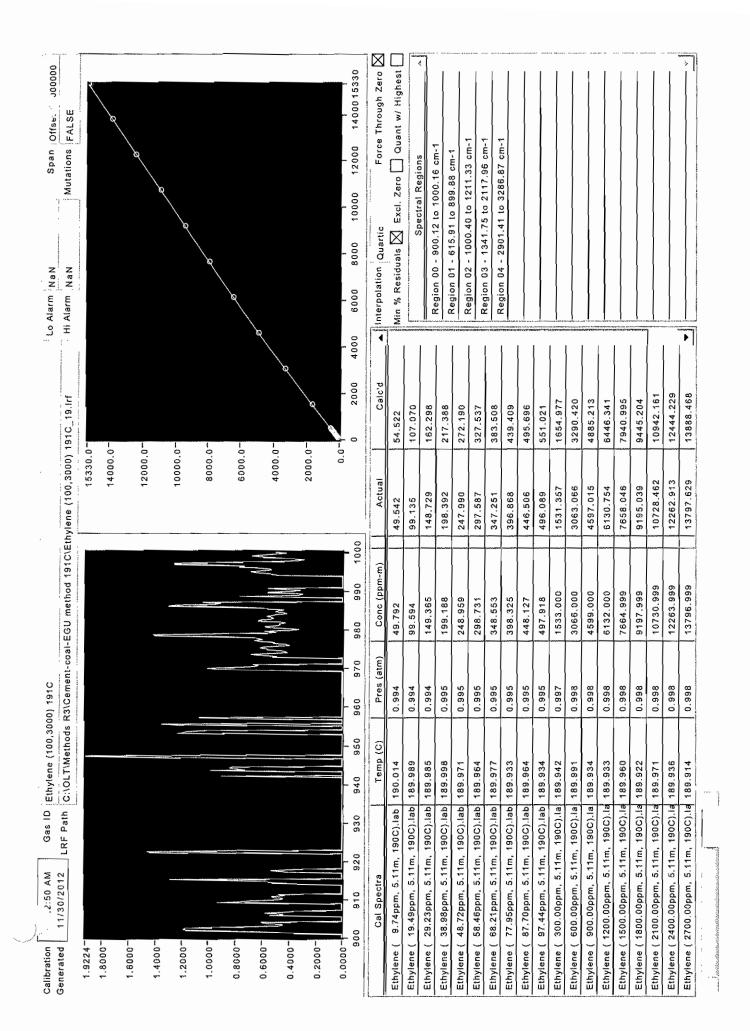
Filename for noise: F:\Midlothian on Renta\November 14\SPC\_000837.LAB Interferences Filenames: C:\Midlothian on Renta\November 15\SPC\_001463.LAB C:\Midlothian on Renta\November 15\SPC\_001464.LAB C:\Midlothian on Renta\November 15\SPC\_001465.LAB C:\Midlothian on Renta\November 15\SPC\_001466.LAB C:\Midlothian on Renta\November 15\SPC\_001466.LAB C:\Midlothian on Renta\November 15\SPC\_001466.LAB C:\Midlothian on Renta\November 15\SPC\_001468.LAB C:\Midlothian on Renta\November 15\SPC\_001469.LAB C:\Midlothian on Renta\November 15\SPC\_001469.LAB C:\Midlothian on Renta\November 15\SPC\_001469.LAB

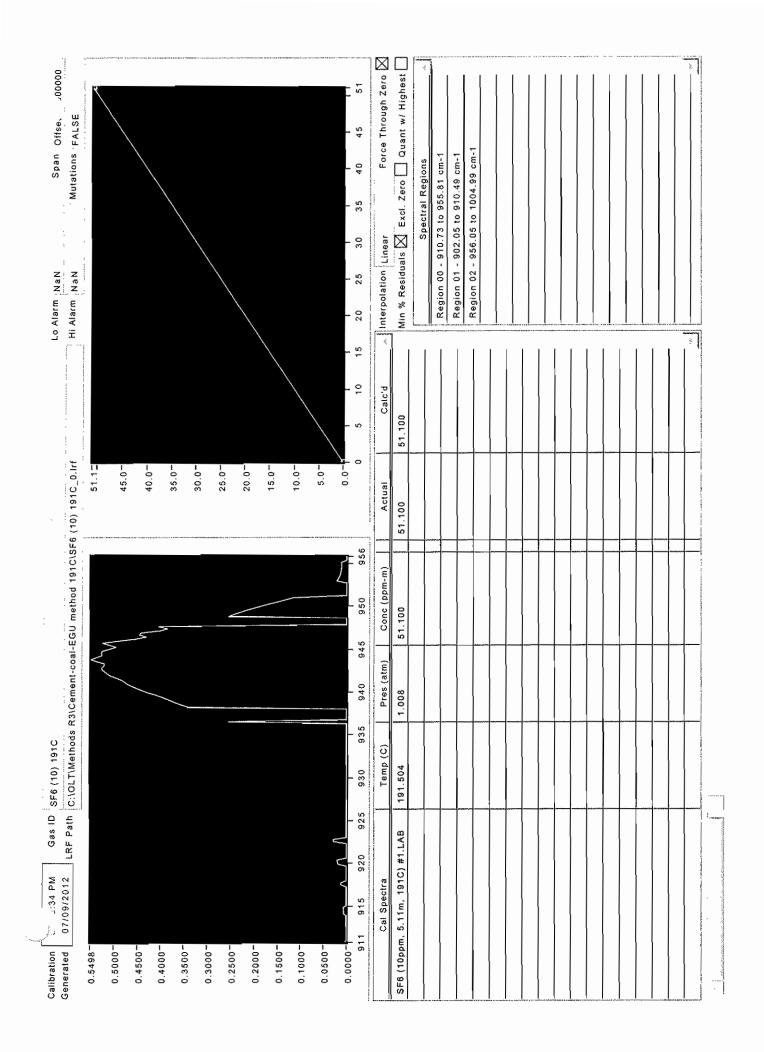
Recipe path: C:\OLT\recipes\Cement Testing R3.MGRCP

~ Bias Sigma Range Span Comment			- 0-10 -	0.75 0.11 0-3000 - Close to DL	- 0-40 -	- 0-40 -	0.02 0-100 -	0.12 0-1000 -	0.23 0.07 0-3000 - Good	0.01 0-300 -	- 0-500 -	0 0-1	- 07-0 60.0	0.08 0-1000	0.02 0-250 -	0.14 0-100 -	0.06 0-100	0.01 0-150 -	0.68 0-2000 -	0.02 0-300 -	0.12 0-3000 -	0.11 0-3000 -	0.05 0-1000 -	0.06 0-1000 -	0.01 0-100 -	0.11 0-500 -	0.01 0-50	0.05 0-10
~ C	0.18	0.21				0.27			2.75																			
~ DF	,	3 0.07	•	1.08	•	-			0.45		1																	
OCC	0.57	0.43	0.02	3.14	0.33	0.26	96.0	2.18	5.76	2.3	10.49	0	1.32	2.62	3.14	0.88	10.15	0.35	6.29	0.2	24.45	12.43	2.3	5.08	0.23	1.36	0.17	0.54
FMU*R OC	0.57	0.43	0.02	3.14	0.33	0.26	0.96	2.18	5.76	2.3	10.49	0	1.32	2.62	3.14	0.88	10.15	0.35	6.29	0.2	24.45	12.43	2.3	5.08	0.23	1.36	0.17	0.54
MAU	0.34	0.07	0	0.29	0.02	0.02	0.28	0.27	0.35	0.2	0.43	0	0.24	0.38	0.7	0.14	1.39	0.03	1.12	0.05	2.25	1.81	0.37	0.5	0.02	0.22	0.05	0.16
MDC1	0.28	0.04	0	0.17	0.01	0.01	0.15	0.14	0.26	0.12	0.2	0	0.2	0.35	0.26	0.12	0.68	0.02	0.88	0.04	1.19	1.1	0.31	0.43	0.05	0.2	0.05	0.14
MDC2		0.05		0.33			0.05	0.37	0.22	0.03		0	0.28	0.23	0.05	0.42	0.17	0.04	2.03	0.05	0.35	0.34	0.15	0.19	0.02	0.32	0.04	0.14
	0.47 -	0.24	0.02 -	1.8	0.17 -	0.19 -	0.52	1.13	4.2	1.36	5.15 -	0	1.09	2.41	1.19	0.74	4.99	0.34	4.94	0.17	12.96	7.55	1.9	4.33	0.17	1.21	0.15	0.47
	8.64	-0.02	-0.01	2.89	13.67	13.62	1.13	10.37	135.44	1.07	168.94	0.02	5.24	2.21	4.83	1.2	-0.02	-0.09	<b>0</b> .1	0.33	1.62	4.36	0.54	1.51	0.61	1.24	0.02	0.78
Gas calibration Name	HCN (200) PCA 191C 191C	HF PPM (10) 191C	SF6 (10) 191C	ETHYLENE (100,3000) 191C	H2O% (40) 191C	CO2% (40) 191C	HCL PPM (100) 191C	SO2 (1000) 191C	NO (350,3000) 191C	NH3 (300) 191C (10F2)	CO (500) 191C (10F2)	CO% (1) 191C (20F2)	FORMALDEHYDE (70) 191C	ACETALDEHYDE (1000) 191C	CH4 (250) 191C (10F2)	PROPANE (100) 191C	HBR (100) 180C	NO2 (150) 191C (10F2)	NO2 (2000) 191C (20F2)	N2O (100,200,300) 191C	NH3 (3000) 191C (20F2)	CH4 (3000) 191C (20F2)	ACETYLENE (1000) 191C	PROPYLENE (200,1000) 191C	COS (100) 150C	ETHANE (500) 191C	H2SO4 (50) 150C	MEOH (10) 191C









Appendix F

**Test Participants** 

Scott Steinsberger Project Manager and FTIR Operator

Lee Harris Sample Recovery Technician

Gage Mayer Sampling Technician

Antonio Pineda Buzzi Plant Contact

### Appendix G

**RTR Sampling and Analytical Protocol** 



### PROTOCOL TO PERFORM A SAMPLING AND ANALYTICAL TESTING PROGRAM AS PART OF THE US EPA RISK AND TECHNOLOGY REVIEW

at Buzzi Unicem USA, Inc. Maryneal Cement Plant 202 CR 306 Maryneal, TX 79535

Submitted By: DEECO, INC. 3404 Lake Woodard Road Raleigh, NC 27604

October 10, 2023

**Copy #1** 

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### 1.1 SUMMARY OF TEST PROGRAM

The United States Environmental Protection Agency (US EPA) has directed the portland cement industry (SIC 3241) to conduct emissions testing as part of the US EPA Risk and Technology Review (RTR). This document provides the overall test program approach and specifies minimum sample collection procedures, data quality objectives, and quality assurance/quality control measures to be used by the source testing firms selected by the cement companies performing tests. The test program is designed to be a comprehensive and robust test of each facility. The quality assurance and quality control (QA/QC) measures are designed to produce standardized data having known precision and accuracy. Collection of accurate, representative, and standardized data for facilities with low emissions is necessary especially in view of MACT standard setting procedures.

1.0 INTRODUCTION

Cement kiln pyro-processing systems located throughout the US are included in the RTR request. Individual facilities have a wide range of kiln system configurations and air pollution control (APC) trains. Site-specific considerations will be required to capture emissions profiles for the target analytes that represent the extent of control or possible emissions increases from these controls.

### 1.2 PLANT NAME, ADDRESS, AND CONTACT

Buzzi Unicem USA, Inc. Maryneal Cement Plant 202 CR 306 Maryneal, TX 79535

Antonio Pineda

Office: 610-882-5038 Mobile: 610-704-3592

E-Mail Antonio.Pineda@buzziunicemusa.com

### 1.3 PROCESS OF INTEREST

Maryneal is a 1.1 million ton per year rated cement pyro-processing system. The plant operates one dry-process rotary kiln (Kiln #4) that has a preheater/precalciner (PH/PC). It consists of a ThyssenKrupp Industrial Solution PREPOL AS Calciner. An in-line raw mill provides kiln feed to the system. The gases from the kiln process exhaust out of a main kiln stack.

### 1.4 AIR POLLUTION CONTROL EQUIPMENT

The Maryneal facility kiln has a Selective Non-Catalytic Reduction System (SNCR) for NOx control, a Dry Sorbent Injection (DSI) system for acid gas control, and a baghouse to control particulate matter (PM).

### 1.5 EMISSION POINTS AND SAMPLING LOCATIONS

The Kiln Stack will be the only location sampled for the RTR program. Details of this sampling location are provided in Section 4.

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### 1.6 POLLUTANTS TO BE MEASURED

Emission testing will be conducted for hydrogen cyanide (HCN), hydrogen fluoride (HF), and diatomic chlorine (Cl<sub>2</sub>). Concurrent measurements to determine volumetric flow rate will be made. The sampling and analytical procedures to be followed are discussed in detail in Section 5.

### 1.7 EXPECTED TEST DATES

The test is currently scheduled for the week of November 27, 2023. A detailed test schedule is provided in Table 3-1.

### 1.8 TEST PROGRAM ORGANIZATION

The test program organizational chart is presented in Figure 1.1.

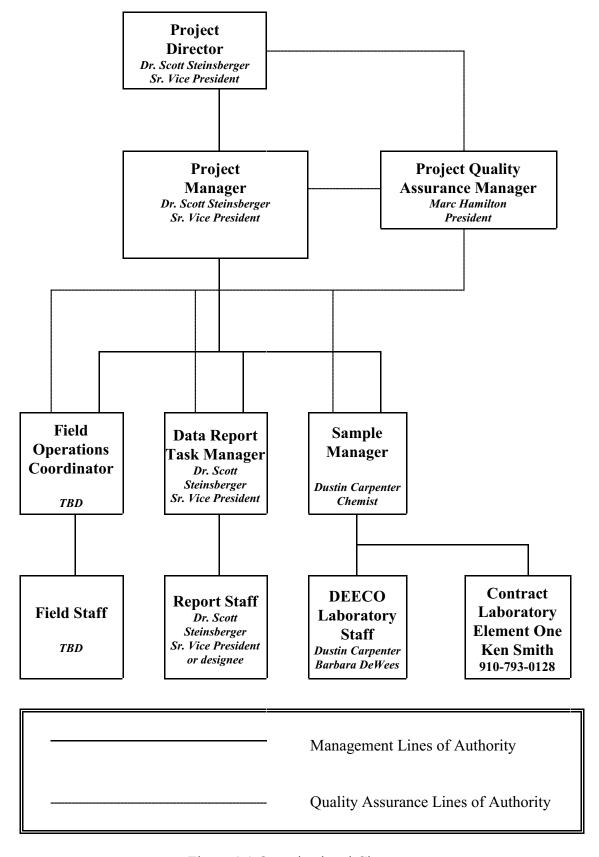


Figure 1.1 Organizational Chart

### 2.0 SOURCE DESCRIPTION

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### 2.1 PROCESS DESCRIPTION

Buzzi Unicem's Maryneal plant operates one dry-process, rotary kiln with a preheater/precalciner (PH/PC) to produce portland cement at their facility in Maryneal, TX.

Kiln feed is introduced at the top of the kiln's preheater tower, while fuel is introduced at the burning zone or discharge end of the rotary kiln. Fuel is also introduced at the calciner burner located toward the bottom of the preheater tower. Natural gas and petroleum coke are used as the fuels in the production process. Exhaust gases from the kiln are drafted into a common duct with an induced-draft fan and ultimately vent to a baghouse.

The raw mill at the facility is an in-line mill (as defined in 40 CFR 63.1341) since a portion of the exhaust gases from the kiln system is used for processing raw materials in the mill. In the mill, raw materials are combined and ground. Kiln exhaust gas is used to dry the materials during grinding, which provides for greater fuel efficiency in the kiln system. Prepared feed is can either be stored in silos or directly fed to the kiln system.

In addition to the main baghouse and stack, exhaust gases from the clinker cooling process vent to three clinker cooler baghouses. Two of the clinker cooler baghouses vent to a combined common stack and the other to a single exhaust stack.

Stack gases from the kiln system are mainly composed of combustion products, carbon dioxide from calcination, excess air, and particulate matter. To remove the PM, exhaust gases from the kiln are routed through a fabric filter dust collector (i.e., the main baghouse. Once cleaned, the exhaust gases from the baghouse discharge to the atmosphere through a single exhaust stack.

### 2.2 CONTROL EQUIPMENT DESCRIPTION

Airflows from the kiln are routed through a fabric filter dust collection (i.e., the main baghouse). Once cleaned, the exhaust gases from the baghouse discharge to the atmosphere through a single exhaust stack. The system uses lime injection and SNCR for additional emissions control.

A schematic of the Maryneal process, including control equipment is shown below in Figure 2.1.

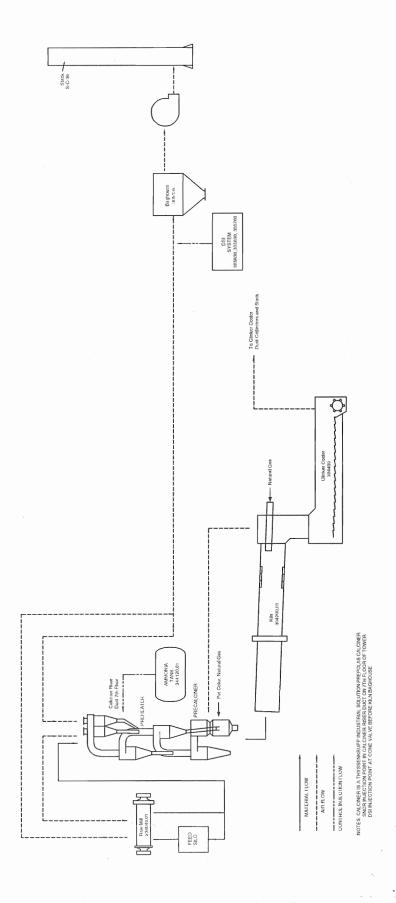


Figure 2.1 Maryneal Process Schematic

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### 3.1 OBJECTIVES

An air emissions sampling and analytical program will be conducted on the Kiln Stack at the Buzzi Unicem USA Inc. cement facility located in Maryneal TX. All testing will be performed following accepted EPA methodology. The test program is to provide a standardized data set to the EPA and the cement industry so that reliable facility inter-comparisons of emissions can be made.

All testing will be performed in strict accordance with specifications stipulated in 40 CFR 60, Appendix A for flow rate following EPA Method 1, 2, 3A, and 4 and hydrogen fluoride (HF) and diatomic chlorine (Cl<sub>2</sub>) following EPA Method 26A and in 40 CFR 63, Appendix A for hydrogen cyanide (HCN) and (HF) following EPA Method 320. All sampling runs will be one hour long.

Testing will be conducted under representative process and control system operating conditions. This facility has an inline raw mill and testing will be performed while operating in the "Mill On" and "Mill Off" conditions.

### 3.2 TEST MATRIX

Table 3-1 presents the sampling and analytical matrix and proposed test schedule.

TABLE 3-1 PROGRAM OUTLINE AND TENTATIVE TEST SCHEDULE FOR BUZZI UNICEM USA, INC, MARYNEAL TX

Sampling Location	No. of runs									
Day 1										
Stack	Arrive o	on-site and set up	test equipment							
Day 2 (Ra	w Mill	On or Off, depe	ending on productio	n)						
Stack	3	O <sub>2</sub> /CO <sub>2</sub>	EPA Method 3A	60	Paramagnetic (O2) NDIR (CO2)	DEECO				
	3	HF and Cl <sub>2</sub>	EPA Method 26A <sup>1</sup>	60	Ion Chromatograph	Element One				
	3	DEECO								
Day 3 (Ra	w Mill	On or Off, depe	ending on productio	n)						
Stack	3 O <sub>2</sub> /CO <sub>2</sub>		EPA Method 3A	60	Paramagnetic (O2) NDIR (CO2)	DEECO				
	3	HF and Cl <sub>2</sub>	EPA Method 26A <sup>1</sup>	60	Ion Chromatograph	Element One				
	3	HCN and HF	EPA Method 320	60	FTIR (Method 320)	DEECO				
Day 4 Cor	ntingen	cy Day/Demobil	ization							

<sup>&</sup>lt;sup>1</sup> Stack gas flow rate and moisture measurement may be taken from concurrent Method 26A isokinetic sampling trains.

### 3.3 TEST COORDINATION

Mr. Antonio Pineda, Corporate Environmental Engineer, will serve as the test coordinator and will be responsible for:

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- 1. Scheduling the start of all testing
- 2. Principal contact with the agency officials concerning the tests
- 3. Principal contact with DEECO concerning the tests
- 4. Recording the process data during the testing
- 5. Providing copies of any field test data to the agency

If there is a temporary equipment malfunction in the middle of a test, radio contact will be made with the test crew in order to delay the test. When problems have been corrected, the test will continue from the point where it was delayed. If the malfunction or upset condition results in an extended test delay, then the affected test run(s) may be aborted and a new run(s) conducted when the malfunction has been corrected or process upset cleared. Any samples or field data from aborted runs may be discarded.

### 4.0 SAMPLING LOCATION DESCRIPTIONS

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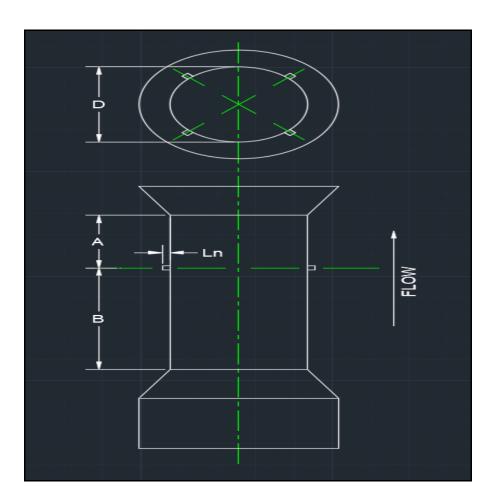
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### 4.1 SAMPLING LOCATION DESCRIPTION

The measurement site for the Kiln Stack is located in a vertically-oriented round duct. The duct has an inside diameter of 141.25". The nearest upstream disturbance is a duct breaching (from the ID fan) located about 579 inches (~4.1 diameters) from the sampling ports. The nearest downstream disturbance is the stack outlet at about 1893 inches (~13.4 diameters) from the sampling ports.

This sampling location meets the minimum specifications for selection of a measurement site as outlined in EPA Method 1. Four (4) test ports are located at equidistant positions (every 90°) around the duct. A schematic of the stack sampling location is shown in Figure 4.1. Cyclonic flow checks, as described in EPA Method 1 Section 2.4, using the Type-S pitot null procedure and angle measurements will be conducted at the Kiln Stack test location.

For the Kiln Stack, a total of 24 velocity/isokinetic traverse points will be used, with six points on each of the four ports. An S-type pitot tube is used in accordance with EPA Method 2 to measure the flue gas velocity. Gas temperatures are measured using calibrated Type K thermocouples and digital readout devices. These measurements are performed in accordance with the procedures in EPA Methods 2, 5, and 26A.



Stack Diameter (D) = 141.25"
Distance to nearest upstream disturbance (A) = 579", 4.1 Duct Diameters Distance to nearest downstream disturbance (B) = 1893", 13.4 Duct Diameters Sampling Ports Available = 4
Ports Diameter = 6"
Length of ports Ln = 6.25"

Figure 4.1 Schematic of Kiln Stack Sampling Location

### 5.0 SAMPLING AND ANALYTICAL PROCEDURES

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This section contains a brief description of the sampling and analytical procedures for each method that will be employed during the test program. All equipment, procedures, and quality assurance measures necessary for completion of the test program will meet or exceed the specifications of the appropriate methods. Any deviations from the methods to ensure quality representativeness of the results are also discussed.

### 5.1 TEST METHODS

The methods for the test program are described below, and apply to all process operating conditions (e.g. where there is an inline raw mill, testing will be performed while operating in the "Mill On" and "Mill Off" conditions). Table 3-1 outlines expected operating conditions for this test.

### 5.1.1 SAMPLING POINT DETERMINATION - EPA METHOD 1

The number and location of the sampling or traverse points will be determined according to the procedures outlined in EPA Method 1. The sample location will be inspected to insure EPA Method 1 criteria is met. All points will be at least 1.0 inches from the stack wall, per Method 1.

### 5.1.2 FLUE GAS VELOCITY AND VOLUMETRIC FLOW RATE - EPA METHOD 2

The flue gas velocity and volumetric flow rate will be determined according to the procedures outlined in EPA Method 2. Velocity measurements will be made using type S pitot tubes conforming to the calibration specifications outlined in EPA Method 2, Section 10.1. Each Type-S pitot tube, calibrated according to these standards, will have an assigned coefficient. Differential pressures will be measured with Magnehelic gauges of appropriate range or with fluid manometers. Effluent gas temperatures will be measured with chromel-alumel thermocouples equipped with digital readouts.

### 5.1.3 OUTLET FLUE GAS COMPOSITION - EPA METHOD 3A

Outlet flue gas analysis for oxygen  $(O_2)$  and carbon dioxide  $(CO_2)$  concentrations, and the calculation of percent excess air and flue gas dry molecular weight will be performed in accordance with EPA Method 3A.

To evaluate the sampling location and points for FTIR and  $O_2$  sampling, a three-point  $O_2$  concentration stratification test on a line passing through the centroidal area at 16.7, 50.0 and 83.3 percent of the measurement line (or for stacks is greater than 2.4 meters (7.8 ft) at 0.4, 1.2 and 2.0 meters from the stack or duct wall). The procedures in Section 8.1.2 of Method 7E will be followed, but oxygen will be used as parameter as allowed by fourth sentence in Section 8.1.2. The plant  $O_2$  CEMS as a control. A criteria of <5% variation from combined mean for each point will be used as indication of non-stratification and allowing single point sampling at the point closest to the mean. Otherwise, sampling for equal periods at the three test points during test run will be conducted.

Per EPA Method 3A for determining molecular weight, integrated sampling will be obtain using the Method 320 sampling system described in Section 5.1.6.

A portion of the hot, wet gas sample will be sent through a condensing system to remove the stack moisture, A portion of the moisture-free gas sample will be snt to a CAI Model 200  $O_2$  (or equivalent) analyzer measures using the paramagnetic technique. An oxygen molecule, because of its

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sp3 electron orbital distribution, has an unpaired electron and hence displays a magnetic orientation. Since other elements that display this magnetic phenomenon are not common gasses at normal temperatures, the paramagnetic measurement technique is virtually specific for oxygen. The sample gas flows through a detection cell located in a very strong magnetic field. The concentration of  $O_2$  gas present induces a pressure differential in the detector cell. The amount of differential pressure is proportional to the concentration of  $O_2$  gas present.

Calibration procedures will be performed in accordance with EPA methodology. Analyzers will be calibrated before and after each test and a calibration check between each test run.

The pretest calibrations will consist of the following steps:

- Internal (direct) calibration of each analyzer to adjust calibration and check linearity.
- External (through the entire sampling system) calibration to check the system bias on zero and span gases.

The post test calibration will consist of an external system bias calibration check.

The analyzer will be as calibrated using a certified zero and span (mid or high range) gas. Zero and span gases were directed to each analyzer through the appropriate plumbing, the calibration gas flow rates will be adjusted to the correct flow rate and the analyzer will be adjusted with the appropriate span pot.

After the analyzer is properly adjusted the linearity will be checked using a low and high range calibration gas. The maximum allowable limit for linearity is 2% of the analyzer range. All analyzers will be shown to be linear within these limits before proceding.

The external calibration bias check will be performed by placing the CEM system in sampling mode and injecting a zero and span gas into the sample line at the probe exit. This check shows if there is any sampling system related bias, and also checks the integrity of the sample line.

 $\underline{\textbf{5.1.3.1}}$  Calibration Gases-DEECO will use EPA Protocol and/or  $\pm 2\%$  NIST Traceable gases for calibration as required by the various reference methods employed in this test program. Calibration gases will be selected from previous experience with similar sources and/or from information obtained from the facility engineer prior to sampling. In some cases if the gases that are selected are out of the optimum range of operation then no significant impact of data quality is expected due to the linear nature of the analyzers that were used.

Audit gases, if available from a federal or a state agency, will be analyzed.

<u>5.1.3.2 Sampling Procedures</u>-At the completion of the pretest calibration routine, the CEM system will be ready for operation. No further adjustments of sample flow rates, analyzer zero or span adjustments, or other critical CEM operating parameters will be made until testing and post test calibration were complete.

Each sampling run will be one hour. At the completion for each test run, calibration gases will be used to check between test runs. A zero and the upscale calibration gas closest to the actual emission concentrations will be used for the pretest and post test calibrations.

## 5.1.4 FLUE GAS MOISTURE CONTENT - EPA METHOD 4

The flue gas moisture content will be determined in conjunction with the EPA Method 26A trains according to the sampling and analytical procedures outlined in EPA Method 4. (NOTE: In order to maintain isokinetic sampling, the sampling rate used may be required to temporarily exceed the EPA Method 4-specified maximum sampling rate of 0.75 CFM, based on observed stack gas pitot readings.) The impingers will be connected in series and will contain reagents as described below. The impingers will be contained in an ice bath in order to assure condensation of the moisture in the flue gas stream. Any moisture that is not condensed in the impingers is captured in the silica gel, therefore all moisture can be weighed and entered into moisture content calculations.

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#### 5.1.5 HYDROGEN FLUORIDE AND DIATOMIC CHLORINE - EPA METHOD 26A

Sampling and analytical procedures will be similar to those outlined in EPA Method 26A to determine primarily diatomic chlorine ( $\text{Cl}_2$ ) emissions and hydrogen fluoride (HF) emissions at main stack outlet sampling locations. Duplicate simultaneous trains (a.k.a "paired trains") for each test run will be used to determine precision.

Sample is collected through a heated glass probe, followed by a heated quartz fiber filter, where stack gas HF and  $\text{Cl}_2$  are collected in a series of chilled impingers. The sampling train impingers will contain 50 ml of 0.1N sulfuric acid in the first impinger (optional should high moisture warrant a modified short stem), 100 ml of 0.1N sulfuric acid in the second and third, a fourth empty impinger, 100 ml of 0.1N NaOH in the fifth and sixth and 200 grams of silica gel in the last impinger. (**NOTE**: For plants with scrubbers, the optional cyclone may be used since the gas stream may be saturated with moisture.)

Sampling will be conducted isokinetically  $(\pm 10\%)$  with readings of flue gas parameters recorded at traverse points selected according to EPA Method 1. Leak-checks on the Method 26A sampling train will be are performed before and after each sampling run and optionally for any port change. In the event that any portion of the train needed to be disassembled and reassembled (i.e., due to filter or resin changes), leak-checks are performed. The sampling train leak-checks and leakage rate (where applicable) are documented on the field test data sheet for each respective run. All leak checks will be acceptable.

The glass button hook nozzle and probe liner will be constructed of borosilicate glass or quartz. The filter holder will be constructed of borosilicate glass with a Teflon frit filter support and a sealing gasket. A heated quartz fiber filter, for sources above 210°C, or PTFE-bonded glass fiber filter will be used. The probe and filter housing will heated to above 248°F and not exceed an upper boundary of 273°F. Probe liners and filter holders will be cleaned thoroughly prior to testing.

The Method 26A trains will be operated isokinetically for a minimum of 60 minutes and collect a minimum of 1 dry, standard cubic meter (DSCM). Pretest preparations, preliminary determinations, and leak check procedures will be those outlined in EPA Method 5.

After completion of sampling the train will be leak checked and transferred to the sample recovery trailer. All leak checks will be acceptable. The impingers will be weighed to determine moisture gain in accordance with EPA Method 4.

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Sample recovery will involve quantitative recovery of the sulfuric acid impinger contents and the NaOH impinger contents into separate tare-weighed, precleaned polyethylene sample containers. The nozzle, probe, filter and filter housing will not be recovered.

The contents of sulfuric acid impingers, including the contents if any of the empty ( $2^{nd}$  knockout or fourth) impinger will be quantitatively transferred to the tare-weighed, precleaned polyethylene sample container, followed by three rinses with deionized (DI) water of the impingers and all connecting glassware (including the connecting glassware to the first impinger) placed in the same  $H_2SO_4$  container. The container will be labeled and weighed to determine the final sample volume. The liquid level will be marked on the sample container.

The contents NaOH impingers will be quantitatively transferred to a second tare-weighed, precleaned polyethylene sample container, followed by three rinses with DI water of the impingers and all connecting glassware placed in the same NaOH container. The container will be labeled and weighed to determine the final sample volume. The liquid level will be marked on the sample container

Sample recovery from each train will include:

- 1. Container No. 1 Contents 1<sup>st</sup> knockout, H<sub>2</sub>SO<sub>4</sub> impingers, and 2<sup>nd</sup> knockout and, and DI rinse of impingers and connecting glassware; and
- 2. Container No. 2 Contents NaOH impingers, and DI rinse of impingers and connecting glassware.

Additional quality control consists of collecting and analyzing a field blank train for every three test runs. The blank train is to be assembled from a used train, leak checked and sit for a period equal to the sampling time (i.e, 1-hr). The blank train data will be used to determine the method detection limit for the test program target analytes (ie. The lowest number that could be detected), and compared to stack emissions.

Reagent blanks of  $0.1 \text{ N}\text{ H}_2\text{SO}_4$ , 0.1N NaOH, and DI water will be collected and archived for later analysis should there be any issues with the field blank train samples

The  $H_2SO_4$  impinger solutions will be analyzed using ion chromatography techniques for fluoride ions (F) (EPA SW-9057). Duplicate analyses will be performed on the samples and a reagent blank. Precision will be demonstrated by duplicate injection of each sample, the results of each individual analysis must be within 5% of their mean to be acceptable. If the precision criteria is not met, analysis of the sample is repeated until consecutive injections meet the criteria.

The NaOH impinger solutions will be treated with sodium thiosulfate to ensure complete conversion of hypochlorous acid (HClO) to chloride ions (Cl<sup>-</sup>). The resulting solution will be analyzed using ion chromatography techniques for chloride ions (EPA SW-9057). Duplicate analyses will be performed on the samples and a reagent blank. Precision will be demonstrated by duplicate injection of each sample, the results of each individual analysis must be within 5% of their mean to be acceptable. If the precision criteria is not met, analysis of the sample is repeated until consecutive injections meet the criteria.

All EPA Method 26A HF/Cl<sub>2</sub> samples will be analyzed by Element One of Wilmington NC. Refer to Section 1, Figure 1.1 for contact information.

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The relative deviation (RD)will be calculated as described in EPA Method 30B between the Cl<sub>2</sub> concentrations measured with the paired trains.

#### 5.1.6 HYDROGEN CYANIDE AND HYDROGEN FLUORIDE - EPA METHOD 320

EPA Method 320 will be performed to determine emissions of concentrations of HCN and HF. Three, 1-hour sampling runs will be conducted under representative process and control system operating conditions.

The gas sample will be extracted from the stack through a glass-lined probe and filter heated to  $375^{\circ}$  F. For external calibration checks and analyte spikes, the gases will be introduced in front of the heated filter. Any excess calibration gas will be diverted through the sample probes into the source. Outflow of gas from the heated filter enclosure was transported through a Teflon sample line heated to  $375^{\circ}$  F. For this source approximately 100' of sample line will be required. The heated sample line will be connected directly to the FTIR sample cell. Using heat-traced Teflon tubing the exit of the FTIR cell will be connected to a sample pump with a heated stainless steel pump head. The pump discharge will be directed to a proprietary chiller-type gas conditioner to remove moisture prior to delivery sample gas to the  $O_2/CO_2$  monitors.

The distribution of the gas sample to the monitors will be accomplished using a panel equipped with valves and rotometers. The gas sample was then divided and directed to the analyzers.

FTIR sample cell will be maintained at 191°C and connected to a MKS Instruments Multigas 2030 Fourier Transform Infrared Spectrometer and Detector.

The FTIR spectrometer will measure vapor phase organic or inorganic compounds which absorb energy in the mid-infrared spectral region, about  $400 \text{ to } 4000 \text{ cm}^{-1}$  (25 to 2.5  $\mu m$ ). Continuous measurement will be made by matching sample absorbance bands with bands in reference spectra, and comparing sample band intensities with reference band intensities.

The principle limitation to FTIR spectroscopy are the presence of interfering compounds that also absorb energy in the mid-infrared spectral region. In a cement kiln stack gas matrix, water vapor  $(H_2O)$  and carbon dioxide  $(CO_2)$  are the primary interferents that must be incorporated into the identification and quantitation method.

The FTIR software performs the computation for a single compound by subtracting all the other compounds (interferants and target) from the absorbance spectra and quantifies the single compound based on the remain absorbance. The FTIR software provides a Standard Error Calculation (SEC) value that is an indication of how well the identification and quantitation has been performed. A high SEC indicates that other interferants have not been accounted for in the analysis method, and a low SEC is indicative of greater confidence measurement.

The instrument is operated with a resolution of 0.5 cm<sup>-1</sup> with 4x zero filling. Beer-Norton Medium apodization is used with amplitude phase correction.

For this RTR test program, following specific QA/QC activities for EPA Method 320 will be performed and criterium met.

# **5.1.6.1** Laboratory QA/QC Activities Before Field Test Program- Before field testing occurs, the following QA/QC activities will be conducted;

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- Seven consecutive samples of dry nitrogen <u>through the sampling system</u> will be acquired and used to calculate the standard deviation for each of the test program target analytes multiplied by a factor of 3. These data will be considered representative of detection limits for this test program and are to be compared to the 0.5 ppm required DL;
- 2) From these seven dry nitrogen samples, the results for the Signal-to-Noise Ratio (SNR) @ 2500 cm<sup>-1</sup> should be >2500, at 64 scans and the results for single beam intensity @ 2500 cm<sup>-1</sup> should be >0.9; and
- Upon receipt of HCN calibration gases a direct analysis will be performed to verify FTIR response agrees with tag value within 5%. Analysis results will be reported to PCA to assess need for modified reference spectra and/or change to direct analysis criterion:

# <u>5.1.6.2 QA/QCActivities During Field Test Program</u>- During the field test program, following QA/QC activities will be performed and criterium met;

- 1) On each test day prior to any testing, an instrument background will be collected using dry nitrogen directed to the gas cell. The background will be collected with at least 128 scans;
- The probe, filter, sample line and all sample system components in contact with effluent will be maintained at or above 375°F or 191°C (consistent with FTIR calibration temperature) to avoid any possible "cold spots;"
- 3) Heated sample lines will be ≤100 feet wherever possible, and not longer than 200 feet, without prior approval for unusual test circumstances;
- 4) A system zero with all sampling system components at operating temperature will be performed by injecting nitrogen at the sample probe and through sample filter and entire measurement system. After zero equilibration has been achieved, all measurement components will be quantified for at least 128 scans;
- Ambient air will be sampled until equilibration of the measurement system has been achieved and all measurement components will be quantify for at least 128 scans;
- The sample probe will be position at effluent measurement point and sampling will continue until equilibration of the measurement system has been achieved. At this point, the effluent concentrations will be quantified with two consecutive 64-scan samples as the initial native concentration for the dynamic spike;
- Analyte spiking will be conducted for HCN before the first test run, and after each successive test run for a minimum of 4 spikes per test condition. (Additional spikes would be required before and after corrective action for the sampling or analysis system and/or before and after removing the sampling system from the stack.) These results will determine accuracy;
- 8) The spike gas injections will be maintained at 10% or less of total sample volume. The spike gas concentration and flow rate will be selected to approximately double the native effluent concentration, or the spike will be conducted to add 3-4 ppm to native concentration, whichever results in greater spiked concentration. Spike recovery results will be within  $\pm 20\%$  of the expected value or  $\pm 0.5$  ppm, whichever is least restrictive. (Specific HCN gases will be manufactured for this test program in the range of 50-100 ppm to provide spikes in the 5-10 ppm range, or lower. An SF<sub>6</sub> or appropriate tracer will be used to calculate the exact spike gas dilution ratio of 10% or less;)
- 9) After the dynamic spike, nitrogen will be sent through the sampling system until all traces of spike gas are removed and lines are proven below DL for target analytes;

The nitrogen purge will be discontinued and the sampling system will be allowed to equilibrate with stack gas before starting a test run. The first two consecutive 64-scan samples of a sample run will be used for the final native concentration. Residual results for HCN and HF will be verified to be less than 0.2-0.3 ppm for data acceptance, or less than 5% of the measured value, whichever is least restrictive. Calculate the standard deviation for each of the test program target analytes for seven consecutive sample spectra from Run 1, multiplied by a factor of 3. These data will be compared to the pre-test system nitrogen standard deviation results and also included in the facility test report;

The SNR @ 2500 cm<sup>-1</sup>, at 64 scans, and the results for single beam intensity @ 2500 cm<sup>-1</sup> will be verified to met the >2500 and >0.9 criterium; respectively. The analyte spiking for HCN and subsequent system nitrogen injection will be conducted after each test run. Continue sequence until at least three valid runs per test condition are completed.

# 6.0 QUALITY ASSURANCE/QUALITY CONTROL ACTIVITIES

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# 6.1 QA/QC PROCEDURES

The QA/QC procedures for this RTR test program are summarized in Table 6-1.

TABLE 6-1 QA/QC PROCEDURES AND REQUIREMENTS

Target			
Analyte	Test Method	Detection Limit	QA/QC
HCN	EPA Method 320	0.5 ppm	Increase scans if needed to achieve detection limits. Increasing to 400 from relative 64 (gives a 2.5 S/N advantage).  HCN spiking before and after each run by adding 10% or less spike to approximately double the native effluent concentration, or conduct spike to add 3-4 ppm to native concentration, whichever results in greater spiked concentration.
			Spike recovery results shall be within $\pm 20\%$ of the expected value or $\pm 0.5$ ppm, whichever is least restrictive
			5% pre-to-post run calibration transfer standard (CTS) requirement
HF		0.2-0.3 ppm	Rely on CTS (5%), HCN and tracer gas responses to validate HF FTIR data
Cl <sub>2</sub>	EPA Method 26A	$\sim 0.07 \text{ mg/m}^3$ ( $\sim 0.2 \text{ ppm}$ )	Duplicate Simultaneous Trains; Collect minimum of 1 dscm for each sample train. Acceptance criteria for paired samples: 10% Relative Deviation or 0.2 ppm absolute difference, whichever is least restrictive. Insert dry impinger between acid and base impingers
Effluent Flow Rate	EPA Methods 1-4	Not Applicable	As per M26A isokinetic testing or separately by Methods 1-3. FTIR measurements for $\rm H_2O$ . Wind Tunnel calibrated pitot tube having a Cp of 0.84 or less is required for all flow measurements. Compare preliminary velocity traverse measurements and sample run flow rate measurements to installed certified flow rate monitor. Investigate and resolve differences greater than 10% of average flow rate.
$\mathrm{O}_2$	EPA Method 3A	Not Applicable	Analyte concentrations corrected @ $7\%$ O <sub>2</sub> Span is 10%, 15%, or 20% (for co-mingled stacks only) Acceptance criteria are 0.2% O <sub>2</sub> difference for analyzer calibration error, and 0.3% O <sub>2</sub> for system bias checks, and zero and upscale drift checks.

### 6.2 SAMPLE IDENTIFICATION AND CUSTODY

Sample custody procedures for this program are based on EPA recommended procedures. Since samples will be analyzed by one or more laboratories as well as in the field, the custody procedures emphasize careful documentation of sample collection and field analytical data and the use of chain of custody records for samples being transported. The procedures which will be used are discussed below.

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The project manager will be responsible for ensuring that proper custody and documentation procedures are followed for the field sampling and field analytical efforts. He will be assisted in this effort by key sampling personnel involved in sampling recovery.

Samples will be collected, transported, and stored in clean containers which are constructed of materials inert to the analytical matrix such as glass jars. Only containers which allow air tight seals will be used. Amber glass jars will be employed when containers are needed to inhibit photochemical reactions.

All sampling data, including information regarding sampling times, locations, and any specific considerations associated with sample acquisition will be recorded on preformatted data sheets. All samples will be given unique, identifying alphanumeric sample codes which will serve to track samples from the field to the laboratory.

Samples will be stored for transport from the lab to the field to the lab in storage boxes constructed in a fashion which minimizes movement and thus prevents breakage of containers. For example, boxes used for transporting glass containers will have foam inserts with form-fitting cutouts. Sample transport boxes will be locked except when in use. Vans containing equipment and samples will be locked whenever they are left unattended.

A daily activity log will be maintained by the project supervisor. This will be an informal log used to record various types of information, such as minor problems which arise, sketches of sampling locations, names and phone numbers of plant contacts. daily activity summaries, etc.

This section provides information regarding the organization of the sampling and analytical program. The following details the key positions and their responsibilities. Once personnel have been assigned to these positions, their qualifications will be provided as an addendum.

The organization of the project team, including QA functions, is shown in the project organization chart (see Figure 1.1).

## 7.0 SAMPLE CUSTODY

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Sample custody procedures for this program are based on EPA recommended procedures. Since samples will be analyzed by one or more laboratories as well as in the field, the custody procedures emphasize careful documentation of sample collection and field analytical data and the use of chain of custody records for samples being transported. The procedures which will be used are discussed below.

#### 7.1 FIELD SAMPLING OPERATIONS

The project manager will be responsible for ensuring that proper custody and documentation procedures are followed for the field sampling and field analytical efforts. He will be assisted in this effort by key sampling personnel involved in sampling recovery.

Samples will be collected, transported, and stored in clean containers which are constructed of materials inert to the analytical matrix such as glass jars. Only containers which allow air tight seals will be used. Amber glass jars will be employed when containers are needed to inhibit photochemical reactions.

All sampling data, including information regarding sampling times, locations, and any specific considerations associated with sample acquisition will be recorded on preformatted data sheets. All samples will be given unique, identifying alphanumeric sample codes which will serve to track samples from the field to the laboratory.

Samples will be stored for transport from the lab to the field to the lab in storage boxes constructed in a fashion which minimizes movement and thus prevents breakage of containers. For example, boxes used for transporting glass containers will have foam inserts with form-fitting cutouts. Sample transport boxes will be locked except when in use. Vans containing equipment and samples will be locked whenever they are left unattended.

A daily activity log will be maintained by the project supervisor. This will be an informal log used to record various types of information, such as minor problems which arise, sketches of sampling locations, names and phone numbers of plant contacts. daily activity summaries, etc.

#### 7.2 ANALYTICAL OPERATIONS

Analytical operations will be performed on-site in the laboratory as well as in the remote laboratories. Samples analyzed by outside laboratories are transported with a Change of Custody form. This form will list sample identifications, analytical parameters, sample matrices, anticipated date of results, and other relevant information necessary to ensure the appropriate analyses are performed and to document the progress of the samples.

# 8.0 INTERNAL QUALITY CONTROL CHECKS

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Specific quality control (QC) procedures will be followed to ensure the continuous production of useful and valid data throughout the course of this test program. The QC checks and procedures described in this section represent an integral part of the overall sampling and analytical scheme. Strict adherence to prescribed procedures is quite often the most applicable QC check. A discussion of both the sampling and analytical QC checks that will be utilized during this program is presented below.

# 8.1 EQUIPMENT INSPECTION AND MAINTENANCE

Each item of field test equipment will be assigned a unique, permanent identification number. An effective preventative maintenance program is necessary to ensure data quality. Each item of equipment returning from the field will be inspected before it is returned to storage. During the course of these inspections, items are cleaned, repaired, reconditioned, and recalibrated where necessary.

Each item of equipment transported to the field for this test program will be inspected again before being packed to detect equipment problems which may originate during periods of storage. This minimizes lost time on the job site due to equipment failure.

Occasional equipment failure in the field is unavoidable despite the most rigorous inspection and maintenance procedures. For this reason, replacement equipment for all critical sampling train components will be transported to the job site.

# **8.2 EQUIPMENT CALIBRATION**

New items for which calibration is required will be calibrated before initial field use. Equipment whose calibration status may change with use or time will be inspected in the field before testing begins and again upon return form each field use. When an item of equipment is found to be out of calibration, it will be repaired and recalibrated or retired from service. All equipment will be periodically recalibrated in full, regardless of the outcome of these regular inspections.

Calibrations will be conducted in a manner, and at a frequency, which meets or exceeds U.S. EPA specifications. The calibration procedures outlined in the EPA Methods will be followed. When these methods are inapplicable, methods such as those prescribed by the American Society for Testing Materials (ASTM) will be used.

Data obtained during calibrations will be recorded on standardized forms, which will be checked for completeness and accuracy by the quality assurance manager. Data reduction and subsequent calculations will be performed using computer facilities. Calculations will be checked at least twice for accuracy. Copies of calibration forms will be included in the test or projects reports.

Emissions sampling equipment requiring calibration includes pitot tubes, pressure gauges, thermometers, dry gas meters and barometers. The following sections elaborate on the calibration procedures to be followed for these items of equipment.

**A: Pitot Tubes.** All Type S pitot tubes used, whether separate or attached to a sampling probe, will be constructed in-house or by a third-party vendor. Each new pitot will be calibrated in accordance with Section 10.1 of EPA Method 2. Each Type-S pitot tube, calibrated according to these standards, will have an assigned coefficient. This coefficient should not change as long as the pitot tube is not damaged.

Each pitot tube will be inspected visually upon return from the field. If a cursory inspection indicates damage or raises doubt that the pitot remains in accordance with the EPA geometry standards, the pitot tube will be refurbished as needed and recalibrated.

- **B:** Differential Pressure Gauge. All meter consoles used are equipped with 10-inch water column (W.C.) inclined-vertical manometers. Fluid manometers do not require calibration other than leak checks. Manometers will be leak checked in the field prior to each test series, and again upon return from the field.
- **C: Impinger Thermometer.** Prior to the start of testing, the thermometer used to monitor the temperature of the gas leaving the last impinger will be compared with a mercury-in-glass thermometer which meets ASTM E-1 No. 63F specifications. The impinger thermometer is adjusted if necessary until is agrees within 2°F of the reference thermometer. If the thermometer is not adjustable, it is labeled with a correction factor.
- **D: Dry Gas Meter Thermometer.** The thermometer used to measure the temperature of the metered gas sample will be checked prior to each field trip against an ASTM mercury-in-glass thermometer. The dry gas meter thermometer is acceptable if the values agree within  $\pm$  5.4°F. Thermometers not meeting this requirements will be adjusted or labeled with a correction factor.
- **E:** Flue Gas Temperature Sensor. All thermocouples employed for the measurement of flue gas temperature are calibrated upon receipt. Initial calibrations will be performed at three points (ice bath, boiling water, and hot oil). An ASTM mercury-inglass thermometer will be used as a reference. The thermocouple is acceptable if the agreement is within 1.5 percent (absolute) at each of the three calibration points.

Before and after each field use, the reading from the flue gas thermocouple-potentiometer combination will be compared with an ASTM mercury-in-glass reference thermometer at ambient conditions. If the two agree within  $\pm$  1.5 percent (absolute), the thermocouple and potentiometer are considered to be in proper working order.

**F: Dry Gas Meter and Orifice.** Two procedures will be used to calibrate the dry gas meter and orifice simultaneously. The full calibration will be a complete laboratory procedure used to obtain the calibration factor of the dry gas meter. Full calibrations will be performed over a wide range of orifice settings. A simpler procedure, the posttest calibration, will be designed to check whether the calibration factor has changed.

A dry gas meter that is calibrated annually against a spirometer or a set of calibrated critical orifices will be used as a transfer standard. During the annual calibration, triplicate calibration runs will be performed at seven flow rates ranging from 0.25 to 1.40 cfm.

G: Dry Gas Meter. Each metering system receives a full calibration at the time of purchase and a post-test calibration after each field use. If the calibration factor,  $\gamma$ , deviates by less than five percent from the initial value, the test data are acceptable.

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If  $\gamma$  deviates by more than 5 percent, the meter is recalibrated and the meter coefficient (initial or recalibrated) that yields the lowest sample volume for the test runs is used.

EPA Method 5 requires another full calibration anytime the post-test calibration check indicates that  $\gamma$  changed by more than 5 percent. Standard practice is to adjust and recalibrate the dry gas meter anytime  $\gamma$  is found to be outside the range of 0.96 to 1.04. Post-test calibrations will be performed after each field test series per EPA Method 5, section 16.3 procedures.

- **H: Orifice.** An orifice calibration factor will be calculated for each flow setting during a full calibration. If the range of values does not vary by more than 0.20 in H<sub>2</sub>O over a range of 0.4 to 4.0 in H<sub>2</sub>O, the arithmetic average of the values obtained during the calibration is used.
- **I: Barometer.** Each field barometer will be adjusted before each test series to agree within  $\pm$  0.1 inches of a reference aneroid barometer. The reference barometer will be checked against the station pressure value (corrected for elevation difference) reported by the National Weather Service.

# 8.3 SAMPLING QUALITY CONTROL PROCEDURES

The following pretest QC checks will be conducted:

- All sampling equipment will be thoroughly checked to ensure clean and operable components.
- Equipment will be inspected for possible damage from shipment.
- The oil manometer or Magnehelic gauge used to measure pressure across the Type S pitot tube will be leveled and zeroed.
- The number and location of the sampling traverse points will be checked before taking measurements.
- The temperature measurement system will be visually checked for damage and operability by measuring the ambient temperature prior to each traverse.

In addition to the general QC procedures listed above, QC procedures specific to each sampling method will also be incorporated into the sampling scheme. These methods and specific procedures are discussed below.

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**A:** Sampling Train QC checks. The following QC procedures will be emphasized:

# Prior to Start of Tests

- Keep all cleaned glassware and sample train components sealed until train assembly.
- Assemble the sampling trains in an environment free from uncontrolled dust.
- Visually inspect each sampling train for proper assembly.
- Perform pretest calculations to determine the proper sampling nozzle size.

### Prior to Each Test Run

- Visually inspect the sampling nozzle.
- Visually inspect the Type S pitot tube.
- Leak check each leg of the Type S pitot tube.
- Leak check the entire sampling train.

## **During Each Test Run**

- Readings of temperature and differential pressure will be taken at each transverse point.
- All sampling data and calculations will be recorded on preformatted data sheets.
- All calibration data forms will be reviewed for completeness and accuracy.
- Any unusual occurrences will be noted during each run on the appropriate data form.
- The project supervisor will review sampling data sheets daily during testing.
- Properly maintain the roll and pitch axis of the Type S pitot tube and the sampling nozzle.
- Leak check the train before and after any move from one sampling port to another during a run (at DEECO's option) or if a filter change takes place.
- Conduct additional leak checks if the sampling time exceeds 4 hours.
- Maintain the probe, filter, and impingers at the proper temperatures.
- Maintain ice in the ice bath at all times.
- Make proper readings of the dry gas meter, delta P and delta H, temperature, and pump vacuum during sampling at each traverse point.
- Maintain isokinetic sampling within  $\pm$  10% of 100%.

#### After Each Test Run

- Visually inspect the sampling nozzle.
- Visually inspect the Type S pitot tube.
- Leak check each leg of the Type S pitot tube.
- Leak check the entire sampling train.

## **B:** QC for Volumetric air flow rate determinations

**Flue Gas Velocity.** Data required to determine the flue gas velocity will be collected using the methodology specified in EPA Method 2. Quality control procedures are as follows.

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- Visually inspect the Type S pitot tube before and after sampling.
- Leak check both legs of the pitot tube before and after sampling.
- Check the number and location of the sampling traverse points before taking measurements.

**Flue Gas Molecular Weight.** In the event that that integrated bag samples are to be used for determination of flue gas molecular weight, EPA Method 3 will be the sampling technique specified. Quality control will focus on the following procedures:

- The sampling train will be leak checked before and after each run.
- A constant sampling rate will be used in withdrawing a sample.
- The sampling train will be purged prior to sample collection.
- The sampling port will be properly sealed to prevent air in-leakage.

**Moisture Content.** The moisture content of the gas stream will be determined using the technique specified in EPA Method 4. The following QC checks will be performed:

- The sampling train will be leak checked before and after each run.
- Ice will be maintained in the ice bath throughout each run to insure an exit temperature (after the silica gel impinger) of  $\leq 67^{\circ}F$ .

#### 8.4 ANALYTICAL QUALITY CONTROL PROCEDURES

All analyses for this program will be performed using accepted laboratory procedures in accordance with the specified analytical protocols. Adherence to prescribed QC procedures will ensure data of consistent and measurable quality. Analytical QC will focus upon the use of control standards to provide a measure of analytical precision and accuracy. Also, specific acceptance criteria are defined for various analytical operations including calibrations, control standard analyses, drift checks, blanks, etc. The following general QC procedures will be incorporated into the analytical effort:

- The on-site project manager will review all analytical data and QC data on a daily basis for completeness and acceptability.
- Analytical QC data will be tabulated using the appropriate charts and forms on a daily basis
- Copies of the QC data tabulation will be submitted to the quality assurance manager following the completion of the test program.
- All hard copy raw data (i.e., chromatograms, computer printouts, etc.) will be maintained in organized files.

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Specific analytical QC procedures for the Orsat analyzer (if used) are listed below.

- The analyzer will be leveled and the fluid levels zeroed prior to use.
- The analyzer will be leak checked prior to use.
- The analyzer will be thoroughly purged with sample prior to use.
- The analyzer will be checked by analyzing an ambient air sample.

## EPA Method 26A Sample Analysis QC Checks are listed below.

- Calibration curve consisting of 4 calibration levels that bracket the expected sample range. Dilute samples as necessary to reach the calibration range;
- Duplicate analysis of calibration standards, before and after sample analysis, with duplicate injections being within 5% of their mean;
- Duplicate analysis of reagent blanks, quality control samples and field samples with duplicate injections being within 5% of their mean;
- Matrix spike samples may be prepared and analyzed. Matrix spike recoveries should be 90-110%
- A field blank will be carried through the procedure and analyzed with the field samples.
- An audit sample will be analyzed for if available from two or more independent, Approved Audit Sample Providers no less than 60 days prior to the test effort.

# 9.0 REPORTING AND DATA REDUCTION REQUIREMENTS

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#### 9.1 DATA REPORTING

The reporting units for HCN, HF, and  $\text{Cl}_2$  will be in parts-per-million by volume, wet basis (ppm<sub>v,d</sub>), parts-per-million by volume, dry corrected to 7% oxygen (ppm<sub>v,d</sub>@7%O<sub>2</sub>), pounds-per-hour (lbs/hr), and pounds-per-ton of clinker (lbs/ton). Additional supporting data for  $\text{CO}_2$ ,  $\text{O}_2$ , and  $\text{H}_2\text{O}$  concentrations and volumetric flow rates (actual cubic feet-per-minute, wet,standard cubic feet-per-minute, and dry,standard cubic feet-per-minute) will be reported. The clinker production, in short tons-per-hour (TPH) will be reported.

Any data that is not acceptable because of technical difficulties will be indicated, and an explanation of the technical problem will be given. All related QC and calibration data will be in the final report.

#### 9.2 REPORT CONTENTS

Copies of the test report will be submitted after the test series has been completed. Results reported will include, but not be limited to emission rates and concentrations of gaseous pollutants, and process sample determinations, any liquid stream constituents determinations, and any other type of data requested. This report will also include a list of all personnel present during testing, summary results, descriptions of test procedures used, a description of the source and its operation during testing, test locations drawings, example calculations, raw field data, and equipment calibrations.

## 9.3 DATA REDUCTION

Care will be exercised to ensure hand recorded data is written accurately and legibly. Additionally, the use of prepared data recording forms, conveniently formatted, is an important aid to verify that all necessary data items are recorded. The collected field and laboratory data will be reviewed by the analyst and the Project Manager.

The Project Manager will reduce and validate all of the sampling and analytical data that is collected. The sampling data will include flow measurements, calibrations, etc. Each laboratory will reduce all analytical results prior to their submission to the Project Manager. The analytical data will be used to determine concentrations and emission rates of the compounds of interest.

Data reduction follows guidelines published in EPA Reference Methods, where applicable, and by guideline documents where EPA Reference Methods are not available. Validated computer programs will be used to calculate all reported values.

#### 9.4 DATA VALIDATION

A second technical review of the data will be performed and documented by a qualified scientist other than the one who performed the actual analyses. The second reviewer will include evidence (e.g., check marks, recalculations, etc.) that show which data points were checked. Finally, the second reviewer will sign and date the cover page of the data packet or the record that was reviewed.

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In-situ measurements will be validated by demonstrated acceptable post-test leak checks and calibration verifications according to the referenced method used.

Analysis data may be validated according to defined criteria by a secondary reviewer or by the analyst. At a minimum and if applicable, analysis data will be validated according to the following criteria (additional method-specific criteria or project requirements may apply):

- Sampling records complete and traceable
- All appropriate QC samples included with the analytical batch and reported with the sample results
- Routine tuning, calibration and inspection of analytical instrumentation documented and performed prior to analyses
- Initial and continuing calibration criteria met
- Method/reagent blanks confirm no background contamination
- Surrogate recoveries within criteria
- Qualitative sample results (e.g., retention times, mass spectra, isotopic ratios) consistent with standard data
- Sample data within the calibrated range of the instrument
- Chromatograms or other raw data consistent with computer-generated quantitation reports
- Accuracy of intermediate data manipulations, transcribed numbers and/or final reported results verified
- Reference standards, instrumentation, sample identification, analysts, methodology, and sequence of processing clearly identified and traceable in the project records
- Lost data or corrective actions documented (e.g., loss of sample, reanalysis, redilutions, additional cleanup steps, alternative calculations etc.)
- Data that does not meet the validation requirements flagged accordingly
- Data reported in the correct units (e.g., "ppm" should not be used without specifying volume or mass units; "ug/g" are preferred units for data reporting)

### 10.0 PLANT ENTRY AND SAFETY

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#### 10.1 SAFETY RESPONSIBILITIES

The Project Manager is responsible for ensuring compliance with plant entry, health, and safety requirements. The Facility Contact (refer to Section 1.2) as the authority to impose or waive facility restrictions. The Project Manager has the authority to negotiate with facility person any deviations from the facility restrictions.

### 10.2 SAFETY PROGRAM

DEECO has a comprehensive health and safety program that satisfies Federal OSHA and MSHA requirements. The basic elements include: (1) written policies and procedures, (2) routine training of employees and supervisors, (3) medical monitoring, (4) use of personal protection equipment, (5) hazard communication, (6) pre-mobilization meetings with Holcim personnel and DEECO test team personnel, and (7) routine surveillance of the on-going test work.

## 10.3 SAFETY REQUIREMENTS

All test personnel will adhere to the following standard safety and precautionary measures as follows:

- 1) Confine activities to test area only;
- 2) Wear hard hats at all times on-site, except inside sample recovery trailers and mobile CEM laboratory;
- 3) Wear protective shoes or boots in test area:
- 4) Wear protective glasses or goggles at the outlet test sites, and other areas as designated;
- 5) Have readily available first aid equipment and fire extinguishers.

Before or on the first day on-site, the Project Manager will fill out the Emergency Response Procedure form and provide copies to be posted at each test site.