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RESULTS OF THE SEPTEMBER 10 AND 11, 1991
MERCURY REMOVAL TESTS ON THE UNITS 1 & 2,
AND UNIT 3 SCRUBBER SYSTEMS AT THE NSP
SHERCO PLANT IN BECKER, MINNESOTA

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RESULTS OF THE SEPTEMBER 10 AND 11, 1991
MERCURY REMOVAL TESTS ON THE UNITS 1 & 2,
AND UNIT 3 SCRUBBER SYSTEMS AT THE NSP
SHERCO PLANT IN BECKER, MINNESOTA

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Report Number 1-3409
October 30, 1991
SP/slp

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ABBREVIATIONS

ACFM	actual cubic feet per minute
cc (ml)	cubic centimeter (milliliter)
DSCFM	standard cubic foot of dry gas per minute
DSML	dry standard milliliter
DEG-F (°F)	degrees Fahrenheit
DIA.	diameter
FP	finished product for plant
FT/SEC	feet per second
g	gram
GPM	gallons per minute
GR/ACF	grains per actual cubic foot
GR/DSCF	grains per dry standard cubic foot
g/dscm	grams per dry standard cubic meter
HP	horsepower
HRS	hours
IN.	inches
IN.HG.	inches of mercury
IN.WC.	inches of water
LB	pound
LB/DSCF	pounds per dry standard cubic foot
LB/HR	pounds per hour
LB/10 ⁶ BTU	pounds per million British Thermal Units heat input
LB/MMBTU	pounds per million British Thermal Units heat input
LTPD	long tons per day
MW	megawatt
mg/Nm ³	milligrams per dry standard cubic meter
ug/Nm ³	micrograms per dry standard cubic meter
microns (um)	micrometer
MIN.	minutes
ng	nanograms
ohm-cm	ohm-centimeter
PM	particulate matter
PPH	pounds per hour
PPM	parts per million
ppmC	parts per million carbon
ppm.d	parts per million, dry
ppm.w	parts per million, wet
ppt	parts per trillion
PSI	pounds per square inch
SQ.FT.	square feet
TPD	tons per day
ug	micrograms
v/v	percent by volume
w/w	percent by weight
<	≤ (when following a number)

Standard conditions are defined as 68 °F (20 °C) and 29.92 IN. of mercury pressure.

Jeff Cole, RTI, says this is a dry bottom boiler, according to the UDI/EEI database. Jeff has been working with the NSP data for five years and, therefore, I am taking his word on this.

Jj

1 INTRODUCTION

On September 10 and 11, 1991, Interpoll Laboratories personnel conducted mercury removal tests on the Units 1 & 2 Scrubber System, and the Unit 3 Scrubber System at the Northern States Power (NSP) Sherburne County Generating Station located in Becker, Minnesota. On-site testing was performed by D. Van Hoeve, E. Brennan, G. Hove and R. Aschenbach. Coordination between testing activities and plant operation was provided by Bob Catron of NSP. The tests were not witnessed by a member of the Minnesota Pollution Control Agency.

Units 1 & 2 are identical Combustion Engineering 750 megawatt boilers which came on line in 1976. During the test, both boilers were fired with 70% Wyoming and 30% Montana pulverized subbituminous coal. Emissions are controlled by a wet fgd scrubbing system which consists of twelve individual rod venturi scrubber spray towers. Cleaned flue gas is exhausted to the atmosphere by a 600-foot radial steel-lined concrete stack common to Units 1 & 2.

The Unit 3 is a Babcock and Wilcox 860 megawatt boiler which came on line in 1987. The boiler is fired with pulverized subbituminous coal (100% Montana (Westmoreland) coal). Particulate and sulfur dioxide emissions are controlled by a dry scrubber consisting of a spray dryer absorber (SDA) and baghouse. Scrubbed flue gas is exhausted to the atmosphere by a 650-foot high radial brick-lined concrete stack.

Evaluations were performed in accordance with EPA Methods 1 - 4 and 101A, CFR Title 40, Part 60, Appendix A (revised July 1, 1990). Previous data collected at this site was used to select the appropriate nozzle diameter required for isokinetic sample withdrawal. An Interpoll Labs sampling train which meets or exceeds specifications in the above-cited reference was used to collect mercury samples by means of a heated glass-lined probe. The collected samples were analyzed by cold vapor atomic absorption (CV/AA).

An integrated flue gas sample was extracted simultaneously with each mercury sample using a specially designed gas sampling system. Integrated flue gas samples were collected in 44-liter Tedlar bags housed in a protective aluminum container. After sampling was complete, the bags were sealed and returned to the laboratory for Orsat analysis. Prior to sampling, the Tedlar bags are leak checked at 15 IN.HG. vacuum with an in-line rotameter. Bags with any detectable inleakage are discarded.

Testing at the Inlet to the Units 1 & 2 Scrubber System was performed at six of twelve scrubber modules (Modules 101, 104, 107, 201, 204, and 207). Testing was conducted from a horizontal row of 6 ports on each of the module inlets. Two inlets were sampled during each of the three test runs. A 24-point traverse was used to isokinetically collect representative mercury samples from each of the module inlets. Each point was sampled for 2.5 minutes for a total of 60 minutes per module, two modules were tested per run for a total of 120 minutes per run.

Testing at the Units 1 and 2 Common Stack was conducted from four test ports on the Stack oriented at 90 degrees. These test ports are located seven stack diameters downstream of the breaching inlet and eleven diameters upstream of the stack exit. A 16-point traverse was used to isokinetically extract representative mercury samples. Each traverse point was sampled eight minutes to give a total sampling time of 128 minutes per run.

Testing at the Inlet to the Unit 3 Scrubber System was conducted from a horizontal row of two test ports. A 24-point traverse was used to isokinetically extract representative mercury samples. Each traverse point was sampled for five minutes for a total of 120 minutes per run.

Testing at the Unit 3 Stack was conducted from four test ports oriented at 90 degrees. These test ports are located seven stack diameters downstream of the breaching inlet and eleven diameters upstream of the stack outlet. A 16-point traverse was used to isokinetically

extract representative mercury samples. Each traverse point was sampled eight minutes to give a total sampling time of 128 minutes per run.

The important results of the test are summarized in Section 2. Detailed results are presented in Section 3. Field data and all other supporting information are presented in the appendices.

The Units 1 & 2 mercury test results are summarized in Table 1. The mercury concentration and mass rate for the Units 1 & 2 Wet Scrubber Inlet averaged 11.6 ug/Nm³ and 0.135 LB/HR respectively. The Scrubber Inlet mass rate was computed using the volumetric flow measured at the Stack (corrected for dilution), since this site is not plagued with large scale turbulence. The average concentration and mass rate at the Stack was 4.2 ug/Nm³ and 0.053 LB/HR respectively. The mercury removal efficiency of this scrubber system was then computed from the Inlet and Stack mass rates. The average removal efficiency was 59.3%.

The Unit 3 mercury results are summarized in Table 2. The mercury concentration and mass rate for the Unit 3 Dry Scrubber Inlet averaged 13.4 ug/Nm³ and .092 LB/HR respectively. The Scrubber Inlet mass rate was computed in an analogous manner to Units 1 & 2. The average concentration and mass rate for the Unit 3 Stack was 5.9 ug/Nm³ and .042 LB/HR respectively. The average mercury removal efficiency of this scrubber system was 54.5%.

Summary of the Emission Factors for the Mercury Determinations
 Conducted September 10 and 11, 1991 on Units 1 & 2 and Unit 3 at the
 NSP Sherburne County Plant in Becker, Minnesota.

Run	Concentration (ug/Nm ³)		Oxygen (%v/v.d)		Emission Factor (LB/10 ⁶ BTU)	
	(Inlet)	(Stack)	(Inlet)	(Stack)	(Inlet)	(Stack)
(Units 1 & 2)						
1	8.8	3.4	9.40	7.20	9.76X10 ⁻⁶	3.17X10 ⁻⁶
2	13.9	2.0	8.20	7.10	1.40X10 ⁻⁵	1.85X10 ⁻⁶
3	12.1	7.3	7.80	7.10	1.18X10 ⁻⁵	6.75X10 ⁻⁶
(Unit 3)						
1	11.3	5.3	6.70	6.30	1.02X10 ⁻⁵	4.63X10 ⁻⁶
2	14.7	6.0	5.60	6.20	1.23X10 ⁻⁵	5.21X10 ⁻⁶
3	14.1	6.4	7.00	6.00	1.29X10 ⁻⁵	5.48X10 ⁻⁶

Table 1. Summary of the Results of the September 10, 1991 Mercury Test on the Units 1 & 2 Wet Scrubber System at the NSP Sherburne County Generating Station.

Run	Concentration (ug/Nm ³)		Mass Rate (LB/HR)		Removal Eff. (%, w/w)
	Inlet	Stack	Inlet	Stack	
1	8.8	3.4	0.102	0.042	58.3
2	13.9	2.0	0.163	0.025	84.4
3	12.1	7.3	0.139	0.090	35.1
Avg.	11.6	4.2	0.135	0.053	59.3

Table 2. Summary of the Results of the September 11, 1991 Mercury Test on the Unit 3 Dry Scrubber System at the NSP Sherburne County Generating Station.

Run	Concentration (ug/Nm ³)		Mass Rate (LB/HR)		Removal Eff. (%, w/w)
	Inlet	Stack	Inlet	Stack	
1	11.3	5.3	0.081	0.038	52.8
2	14.7	6.0	0.105	0.043	59.4
3	14.1	6.4	0.091	0.044	51.4
Avg.	13.4	5.9	0.092	0.042	54.5

Table 3 presents mercury mass rates based on coal analyses. One sample of Units 1 & 2 coal and one sample of Unit 3 coal were analyzed for mercury content. Potential mercury mass rates from the Units 1 & 2 and Unit 3 boilers were computed based on the results of these coal analyses and the coal feed rates reported in the Plant logs (Appendix E). In the case of Unit 3 the coal did not contain a measurable quantity of mercury at a detection limit of 0.02 mg/Kg. This detection limit was used in computing the potential mass rate. It is important to note that an additional source of mercury exists for Unit 3, the lime additive used in the fgd scrubber. Lime from this scrubber was analyzed previously (March 1990) and found to contain 0.07 mg/Kg mercury. At an average lime feed rate of 4.0 LB/HR the lime contributes 0.001 LB/HR mercury for a total of 0.021 LB/HR. Excellent correlation is seen to exist between the potential mass rates calculated from the feed and the mass rates measured at the Scrubber Inlets (boiler outlets) for Units 1 & 2, the results for Unit 3 do not compare as well. The cause of the poor correlation for Unit 3 was investigated and no source for the discrepancy was determined.

No difficulties were encountered in the field or in the laboratory evaluation of the samples. On the basis of this fact and a complete review of the entire data and results, it is our opinion that the results as qualified above are accurate and closely reflect the actual values which existed at the time the test was performed.

Table 3. Summary of Potential Mercury Mass Rates from the Units 1&2, and Unit 3 Boilers at the Northern States Power, Sherburne County Generating Station.

Run	Coal Feed		Potential Mass Rate
	(TPH)	(LB/HR)	(LB/HR)
(Units 1&2)			
1	764	1528000	0.138
2	775	1550000	0.140
3	766	1532000	0.138
Avg.			0.138
(Unit 3)			
1	490	980000	0.020
2	494	988000	0.020
3	503	1006000	0.020
Avg.			0.020

3 RESULTS

The results of all field and laboratory evaluations are presented in this section. Gas composition (Orsat and moisture) are presented first followed by the computer printout of the mercury results. Preliminary measurements including test port locations are given in the appendices.

The results have been calculated on an IBM PC Computer using programs written in Extended BASIC specifically for source testing calculations. EPA-published equations have been used as the basis of the calculation techniques in these programs.

3.1 Results of Orsat and Moisture Analyses

Interpoll Labs Report No. 1-3409
Northern States Power Company
Becker, Minnesota

Test No. 1
Units 1 & 2 Scrubber Inlets

Results of Orsat & Moisture Analyses-----Methods 3 & 4(%v/v)

Date of run	Run 1 09-10-91	Run 2 09-10-91	Run 3 09-10-91
-------------	-------------------	-------------------	-------------------

Dry basis (orsat)

carbon dioxide.....	10.30	11.30	11.70
oxygen.....	9.40	8.20	7.80
carbon monoxide.....	0.00	0.00	0.00
nitrogen.....	80.30	80.50	80.50

Wet basis (orsat)

carbon dioxide.....	9.48	10.20	10.60
oxygen.....	8.65	7.41	7.07
carbon monoxide.....	0.00	0.00	0.00
nitrogen.....	73.91	72.70	72.96
water vapor.....	7.96	9.69	9.36

Dry molecular weight.....	30.02	30.14	30.18
Wet molecular weight.....	29.07	28.96	29.04
Specific gravity.....	1.004	1.000	1.003
Water mass flow.....(LB/HR)	0.00	0.00	0.00

Test No. 1
Units 1 & 2 Stack

Results of Orsat & Moisture Analyses-----Methods 3 & 4(%v/v)

	Run 1	Run 2	Run 3
Date of run	09-10-91	09-10-91	09-10-91

Dry basis (orsat)

carbon dioxide.....	12.20	12.40	12.40
oxygen.....	7.20	7.10	7.10
carbon monoxide.....	0.00	0.00	0.00
nitrogen.....	80.60	80.50	80.50

Wet basis (orsat)

carbon dioxide.....	10.46	10.56	10.53
oxygen.....	6.17	6.05	6.03
carbon monoxide.....	0.00	0.00	0.00
nitrogen.....	69.10	68.54	68.34
water vapor.....	14.27	14.86	15.11

Dry molecular weight.....	30.24	30.27	30.27
Wet molecular weight.....	28.49	28.45	28.41
Specific gravity.....	0.984	0.983	0.981
Water mass flow.....(LB/HR)	0.00	0.00	0.00

Interpoll Labs Report No. 1-3409
Northern States Power Company
Becker, Minnesota

Test No. 2
Unit 3 Scrubber Inlet

Results of Orsat & Moisture Analyses-----Methods 3 & 4(t/v/v)

Date of run	Run 1 09-11-91	Run 2 09-11-91	Run 3 09-11-91
Dry basis (orsat)			
carbon dioxide.....	12.60	13.60	12.40
oxygen.....	6.70	5.60	7.00
carbon monoxide.....	0.00	0.00	0.00
nitrogen.....	80.70	80.80	80.60
Wet basis (orsat)			
carbon dioxide.....	11.27	12.13	11.33
oxygen.....	5.99	4.99	6.40
carbon monoxide.....	0.00	0.00	0.00
nitrogen.....	72.20	72.07	73.67
water vapor.....	10.53	10.81	8.60
Dry molecular weight.....	30.28	30.40	30.26
Wet molecular weight.....	28.99	29.06	29.21
Specific gravity.....	1.001	1.004	1.009
Water mass flow.....(LB/HR)	0.00	0.00	0.00

Test No. 2
Unit 3 Stack

Results of Orsat & Moisture Analyses-----Methods 3 & 4(lv/v)

Date of run	Run 1 09-11-91	Run 2 09-11-91	Run 3 09-11-91
-------------	-------------------	-------------------	-------------------

Dry basis (orsat)

carbon dioxide.....	13.00	13.10	13.30
oxygen.....	6.30	6.20	6.00
carbon monoxide.....	0.00	0.00	0.00
nitrogen.....	80.70	80.70	80.70

Wet basis (orsat)

carbon dioxide.....	11.17	11.17	11.39
oxygen.....	5.41	5.28	5.14
carbon monoxide.....	0.00	0.00	0.00
nitrogen.....	69.35	68.78	69.12
water vapor.....	14.07	14.77	14.34

Dry molecular weight.....	30.33	30.34	30.37
Wet molecular weight.....	28.60	28.52	28.59
Specific gravity.....	0.988	0.985	0.988
Water mass flow.....(LB/HR)	0.00	0.00	0.00

3.2 Results of Mercury Sampling

Interpoll Labs Report No. 1-3409
Northern States Power Company
Becker, Minnesota

Test No. 1
Units 1 & 2 Scrubber Inlets

Results of Multi-Metal Modified Method 5 (4M5) Sampling.....

	Run 1	Run 2	Run 3
Date of run	09-10-91	09-10-91	09-10-91
Time run start/end.....(HRS)	0815-1030	1105-1340	1420-1643
Static pressure.....(IN.WC)	11.88	11.88	11.88
Cross sectional area (SQ.FT)	76.50	76.50	76.50
Pitot tube coefficient.....	0.840	0.840	0.840
Water in sample gas			
condenser.....(ML)	0.0	0.0	0.0
impingers.....(GRAMS)	94.0	113.0	99.0
desiccant.....(GRAMS)	13.0	15.0	11.0
total.....(GRAMS)	107.0	124.0	110.0
Gas meter coefficient.....	0.9990	0.9990	0.9990
Barometric pressure..(IN.HG)	29.20	29.20	29.20
Avg. orif.pres.drop..(IN.WC)	0.87	0.81	0.64
Avg. gas meter temp..(DEF-F)	86.2	84.0	87.3
Volume through gas meter....			
at meter conditions...(CF)	61.81	59.34	53.31
standard conditions.(DSCF)	58.35	56.24	50.20
standard conditions...(NM ³)	1.652	1.593	1.422
Total sampling time....(MIN)	120.00	120.00	120.00
Nozzle diameter.....(IN)	.187	.187	.187
Avg.stack gas temp ..(DEG-F)	287	290	282
Volumetric flow rate.....			
actual.....(ACFM)	323056	305628	274396
dry standard.....(DSCFM)	211365	195395	177838
Isokinetic variation.....(%)	92.3	96.3	94.4

Interpoll Labs Report No. 1-3409
Northern States Power Company
Becker, Minnesota

Test No. 1
Units 1 & 2 Stack

Results of Multi-Metal Modified Method 5 (4M5) Sampling.....

	Run 1	Run 2	Run 3
Date of run	09-10-91	09-10-91	09-10-91
Time run start/end.....(HRS)	0815-1032	1105-1344	1420-1639
Static pressure.....(IN.WC)	-1.35	-1.35	-1.35
Cross sectional area (SQ.FT)	829.58	829.58	829.58
Pitot tube coefficient.....	0.840	0.840	0.840
Water in sample gas			
condenser.....(ML)	0.0	0.0	0.0
impingers.....(GRAMS)	297.0	330.0	340.0
desiccant.....(GRAMS)	36.0	24.0	15.0
total.....(GRAMS)	333.0	345.0	355.0
Gas meter coefficient.....	1.0058	1.0058	1.0058
Barometric pressure..(IN.HG)	28.77	28.77	28.77
Avg. orif.pres.drop..(IN.WC)	1.87	1.92	1.86
Avg. gas meter temp..(DEG-F)	79.8	80.2	81.7
Volume through gas meter....			
at meter conditions...(CF)	99.30	100.73	99.33
standard conditions.(DSCF)	94.35	95.65	94.04
standard conditions..(NM ³)	2.672	2.708	2.663
Total sampling time....(MIN)	128.00	128.00	128.00
Nozzle diameter.....(IN)	.184	.184	.184
Avg.stack gas temp ..(DEG-F)	182	181	181
Volumetric flow rate.....			
actual.....(ACFM)	4932744	5021238	4946260
dry standard.....(DSCFM)	3334932	3376641	3313486
Isokinetic variation.....(%)	99.4	99.5	99.7

Interpoll Labs Report No. 1-3409
Northern States Power Company
Becker, Minnesota

Test No. 2
Unit 3 Scrubber Inlet

Results of Multi-Metal Modified Method 5 (4M5) Sampling.....

	Run 1	Run 2	Run 3
Date of run	09-11-91	09-11-91	09-11-91
Time run start/end.....(HRS)	0835-1042	1130-1336	1430-1635
Static pressure.....(IN.WC)	-17.00	-17.00	-17.00
Cross sectional area (SQ.FT)	1092.00	1092.00	1092.00
Pitot tube coefficient.....	0.840	0.840	0.840
Water in sample gas			
condenser.....(ML)	0.0	0.0	0.0
impingers.....(GRAMS)	190.0	109.0	83.0
desiccant.....(GRAMS)	6.0	6.0	5.0
total.....(GRAMS)	196.0	114.0	88.0
Gas meter coefficient.....	1.0066	1.0066	1.0066
Barometric pressure..(IN.HG)	29.04	29.04	29.04
Avg. orif.pres.drop..(IN.WC)	1.45	0.46	0.46
Avg. gas meter temp..(DEF-F)	80.9	84.2	85.9
Volume through gas meter....			
at meter conditions...(CF)	82.08	47.17	46.63
standard conditions.(DSCF)	78.53	44.75	44.10
standard conditions..(NM ³)	2.224	1.267	1.249
Total sampling time....(MIN)	120.00	120.00	120.00
Nozzle diameter.....(IN)	.251	.187	.187
Avg.stack gas temp ..(DEG-F)	268	275	279
Volumetric flow rate.....			
actual.....(ACFM)	3467717	3583209	3583699
dry standard.....(DSCFM)	2089932	2131208	2174653
Isokinetic variation.....(%)	99.6	100.2	96.8

Test No. 2
Unit 3 Stack

Results of Multi-Metal Modified Method 5 (4M5) Sampling.....

	Run 1	Run 2	Run 3
Date of run	09-11-91	09-11-91	09-11-91
Time run start/end.....(HRS)	0835-1054	1130-1346	1422-1632
Static pressure.....(IN.WC)	-0.46	-0.46	-0.46
Cross sectional area (SQ.FT)	683.49	683.49	683.49
Pitot tube coefficient.....	0.840	0.840	0.840
Water in sample gas			
condenser.....(ML)	0.0	0.0	0.0
impingers.....(GRAMS)	363.0	226.0	209.0
desiccant.....(GRAMS)	41.0	17.0	17.0
total.....(GRAMS)	404.0	243.0	226.0
Gas meter coefficient.....	1.0058	1.0058	1.0058
Barometric pressure..(IN.HG)	28.84	28.84	28.84
Avg. orif.pres.drop..(IN.WC)	2.84	0.92	0.86
Avg. gas meter temp..(DEG-F)	83.1	81.1	90.5
Volume through gas meter....			
at meter conditions...(CF)	122.59	69.76	68.31
standard conditions.(DSCF)	116.34	66.12	63.63
standard conditions..(NM ³)	3.294	1.872	1.802
Total sampling time....(MIN)	128.00	128.00	128.00
Nozzle diameter.....(IN)	.245	.184	.184
Avg.stack gas temp ..(DEG-F)	170	170	170
Volumetric flow rate.....			
actual.....(ACFM)	2754722	2773921	2680020
dry standard.....(DSCFM)	1909745	1908275	1850934
Isokinetic variation.....(%)	99.4	100.3	99.5

4 RESULTS OF FUEL ANALYSIS

INTERPOLL LABORATORIES, INC.
(612) 786-6020

NSP/Sherco
Laboratory Log No. 4201

Results of Mercury Analysis

Laboratory			Mercury, ¹
Log No.	Sample Identification	Sample Type	(mg/Kg)
4201-55	Test 1 Composite, Units 1 & 2	Coal	0.09
4201-56	Test 2 Composite, Unit 3	Coal	< 0.02

¹Digestion by ASTM Method D3684-78; analysis by EPA SW-846 Method 7470.

APPENDIX A

SAMPLING TRAIN CALIBRATION DATA

UNITS
1+2

EPA Method 5 Gas Metering System
Quality Control Check Data Sheet

Job N.S.P. SHILO STATION

Date 9/9/91

Operator D. BRENNAN

Module No. 2

Instructions: Operate the control module at a flow rate equal to ΔH for 10 minutes before attaching the umbilical. Record the following data:

Bar press 28.84 in. Hg. $\Delta H =$.999 ΔH 1.90 in. W.C.

ΔH
1.90

Time (min)	Volume (CF)	Meter Temp. (°F)	
		Inlet	Outlet
0.5	(721.00)	88	79
2.5	722.92	89	79
5.0	724.86	93	80
7.5	726.80	95	81
10	728.72	96	82
15	$V_m = 7.72$	Avg (t_m) = 86.875°F	

Calculate Y_{en} as follows:

$$Y_{en} = \frac{1.786}{P V_m} \left[\frac{(t_m + 460)}{F_b} \right]^{0.5}$$

$$Y_{en} = \frac{1.786}{(.999)(7.72)} \left[\frac{546.875}{(28.84)} \right]^{0.5}$$

$$Y_{en} = \underline{1.008}$$

If Y_{en} is not within the range of 0.97 to 1.03, "the volume metering system should be investigated before beginning."

BOX 9
B-13

CFR Title 40, Part 60, Appendix A, Method 5, Section 4.4.1

EPA Method 5 Gas Metering System
Quality Control Check Data Sheet

Job SHERCO-NSP Date 9-11
Operator DVH Module No. 3

Instructions: Operate the control module at a flow rate equal to Q_{H2} for 10 minutes before attaching the umbilical. Record the following data:

Bar press 28.84 in. Hg. $\psi = \underline{1.0058}$ in. H₂O 1.82 in. W.C.

Time (min)	Volume (CF)	Meter Temp. (°F)	
		Inlet	Outlet
0.5	(560.9)		
2.5	562.82	83	85
5.0	564.77	86	83
7.5	566.70	86	83
10	568.64	86	83
	V _m = <u>7.74</u>	Avg (t _m) = <u>84.38</u> °F	

Calculate Y_{en} as follows:

$$Y_{en} = \frac{1.786}{\psi V_m} \left[\frac{(t_m + 460)}{P_b} \right]^{0.5}$$

$$Y_{en} = \frac{1.786}{(1.0058)(7.74)} \left[\frac{(84.38) + 460}{(28.84)} \right]^{0.5}$$

$$Y_{en} = \underline{.996}$$

If Y_{en} is not within the range of 0.97 to 1.03, "the volume metering system should be investigated before beginning."

CFR Title 40, Part 60, Appendix A, Method 5, Section 4.4.1

EPA Method 5 Gas Metering System
Quality Control Check Data Sheet

Job NSP SHERCO (SCRUBBER FAULT) ^{WIT} #3 Date 11 Sept 91
Operator Bob Module No. 9

Instructions: Operate the control module at a flow rate equal to CH₄ for 10 minutes before attaching the umbilical. Record the following data:

Bar press 29.04 in. Hg. $\tau = 1.0066$ CH₄ 1.75 in. W.C.

Time (min)	Volume (CF)	Meter Temp. (°F)	
		Inlet	Outlet
	956.00		
2.5	957.88	72.0	72.0
5.0	959.78	74.6	72.6
7.5	961.69	76.4	73.0
10	963.58	77.8	73.2
	V _m = 7.58	Avg (t _m) = 73.95 °F	

Calculate Y_{en} as follows:

$$Y_{en} = \frac{1.786}{\tau V_m} \left[\frac{(t_m + 460)}{P_b} \right]^{0.5}$$

$$Y_{en} = \frac{2346752}{(1.0066)(7.58)} \left[\frac{(73.95) + 460}{(29.04)} \right]^{0.5}$$

4.3038723

7.630028

$$Y_{en} = 1.0037$$

18.386708

If Y_{en} is not within the range of 0.97 to 1.03, "the volume metering system should be investigated before beginning."

CFR Title 40, Part 60, Appendix A, Method 5, Section 4.4.1

Interpoll Laboratories, Inc.
(612) 786-6020

Meter Box Calibration and Usage Status

Date of Report: October 14, 1991

Meter Box No. : 2 (Rockwell) Dry Test Meter Serial No. 964549)

Date of Last Calibration: July 8, 1991

Calibration Technician: D. VanHoeve

Wet Test Meter No.: American Meter AL-20

Date of Use	Report No.	Initial Meter		Final Meter		Volume/Job (cu. ft.)	Total Volume* (cu. ft.)
		Reading		Reading			
July 12, 1991	1-3347	149.10		292.50		143.40	143.40
July 15, 1991	1-3352	293.00		429.15		136.15	279.55
September 6, 1991	1-3405	434.00		715.87		281.87	561.42
September 9, 1991	1-3409	721.00		904.91		183.91	745.33

* Total volume through meter since last calibration.

Interpoll Laboratories, Inc.

(612) 786-6020

Meter Box Calibration and Usage Status

Date of Report: October 14, 1991

Meter Box No. : 3 (Rockwell) Dry Test Meter Serial No. 35303)

Date of Last Calibration: August 23, 1991

Calibration Technician: E. Trowbridge

Wet Test Meter No.: American Meter AL-20

Date of Use	Report No.	Initial Meter Reading	Final Meter Reading	Volume/Job (cu. ft.)	Total Volume* (cu. ft.)
September 10, 1991	1-3409	234.60	830.00	595.40	595.40

* Total volume through meter since last calibration.

Interpoll Laboratories, Inc.
(612) 786-6020

Meter Box Calibration and Usage Status

Date of Report: October 14, 1991

Meter Box No. : 9 (Rockwell Dry Test Meter Serial No. 949230)

Date of Last Calibration: August 14, 1991

Calibration Technician: E. Trowbridge

Wet Test Meter No.: American Meter AL-20

Date of Use	Report No.	Initial Meter		Final Meter		Volume/Job (cu. ft.)	Total Volume* (cu. ft.)
		Reading		Reading			
August 28-29, 1991	1-3397	615.70		825.05		209.35	209.35
September 4, 1991	1-3401	827.30		953.58		126.28	335.63
September 11, 1991	1-3409	956.00		1141.36		185.36	520.99

* Total volume through meter since last calibration.

2

Control Module No.

METER CALIBRATION SHEET

Bar. Press. 29.22 in. Hg

EPA METHOD 5

Hot Test Water No. AL-20

Technician D. Van Hoever

[illegible]

Positive leak check performed by DA
 Water was in tolerance ☒
 Water was not in tolerance ☐; readjusted linkage
 Water was not in tolerance ☐; changed dry test meters

Approved by Daniel H. Reyer Date 7/8/91

• Based on AL-20 wet test meter calibration in August 1989 against Bell Prover (NBS Traceable) - Carl Poe Co.

S0102RR 5/90

Bar. Press. 29.20 in. Hg

Technician

INTERPOLL LABORATORIES, INC.
METER CALIBRATION SHEET

EPA METHOD 5

Positive leak check performed by 51
 Water was in tolerance ☒
 Water was not in tolerance ☐: readjusted linkage
 Water was not in tolerance ☐: changed dry test meters

Approved by Daniel H. Ryan Date 8/23/71

* Based on AL-20 wet test meter calibration in August 1909 against Bell Prover (NBS Traceable) - Carl Poe Co

Technician

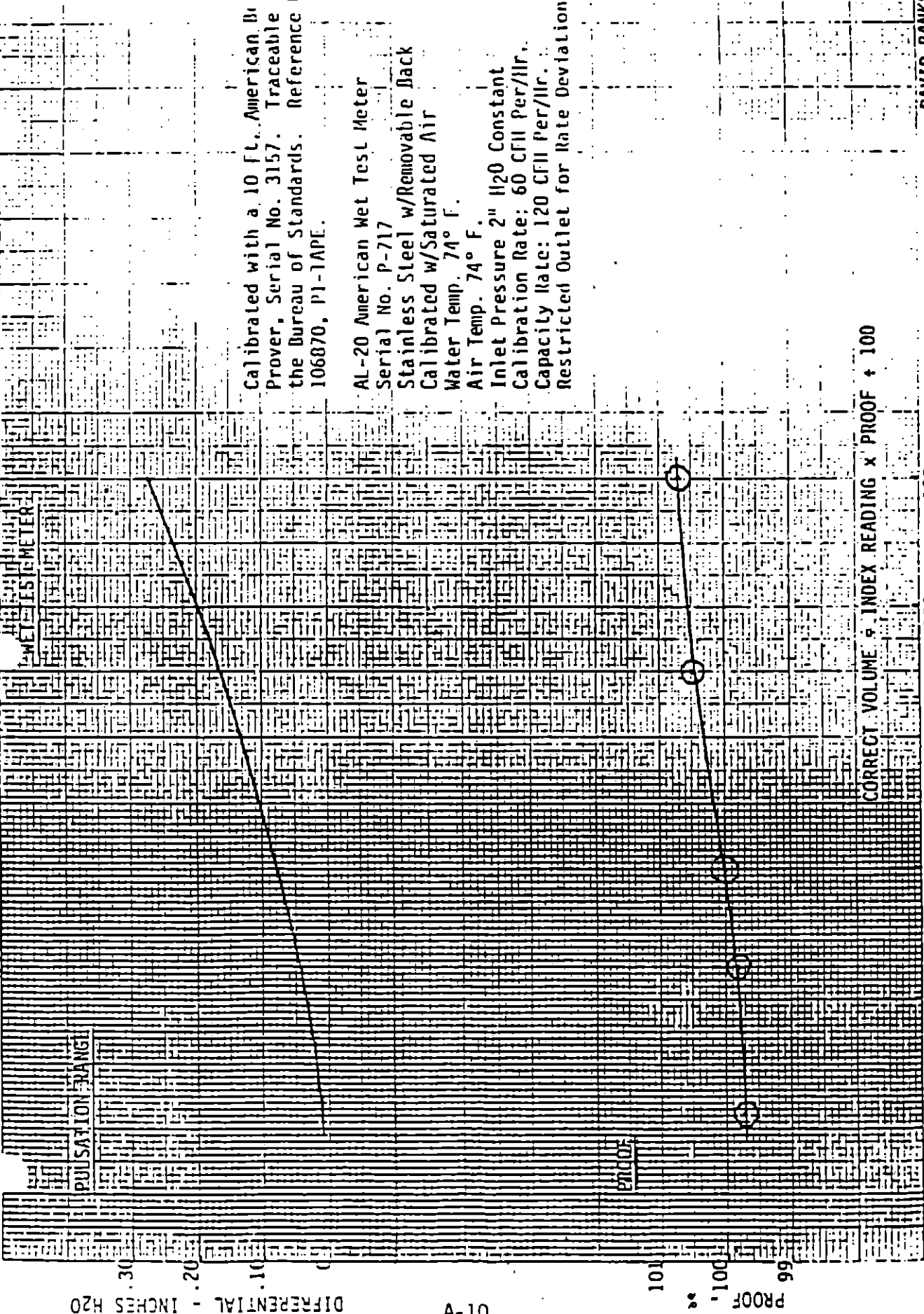
A-9

DIFFERENTIAL PROOF AND PROOF CALIBRATION CURVES

WET TEST METER

DIFFERENTIAL - INCHES H₂O

PULSATION RANGE



Calibrated with a 10 ft. American Bull Prover, Serial No. 3157. Traceable to the Bureau of Standards. Reference is 106870, P1-TAPE.

AL-20 American Wet Test Meter

Serial No. P-717

Stainless Steel w/Removable Back

Calibrated w/Saturated Air

Water Temp. 74° F.

Air Temp. 74° F.

Inlet Pressure 2" H₂O Constant

Calibration Rate: 60 CFH Per/Hr.

Capacity Rate: 120 CFH Per/Hr.

Restricted Outlet for Rate Deviation

DAVID BANKS

AUGUST 1989

FEET AIR

CUBIC FEET AIR

120

100

80

60

40

20

Interpoll Laboratories, Inc.

(612) 786-6020

Nozzle Calibration

Data Sheet

Date of Calibration: 9-10-91

Nozzle Number 2-1

Technician: Duke Brennan

The nozzle is rotated in 60 degree increments and the diameter at each point is measured to the nearest 0.001 inch. The observed readings and average are shown below.

Position	Diameter (inches)
1	.187
2	.189
3	.186
Average:	.187

Nozzle Calibration
Data Sheet

Date of Calibration: 9-10-91

Nozzle Number 1-3

Technician: Duane VanHoeve

The nozzle is rotated in 60 degree increments and the diameter at each point is measured to the nearest 0.001 inch. The observed readings and average are shown below.

Position	Diameter (inches)
1	.187
2	.186
3	.180
Average:	.184

Interpoll Laboratories, Inc.

(612) 786-6020

Nozzle Calibration

Data Sheet

Date of Calibration: 9-11-91

Nozzle Number 7-2

Technician: Duke Brennan

The nozzle is rotated in 60 degree increments and the diameter at each point is measured to the nearest 0.001 inch. The observed readings and average are shown below.

Position	Diameter (inches)
1	.188
2	.186
3	.187
Average:	.187

Nozzle Calibration

Data Sheet

Date of Calibration: 9-11-91

Nozzle Number 7-3

Technician: Duke Brennan

The nozzle is rotated in 60 degree increments and the diameter at each point is measured to the nearest 0.001 inch. The observed readings and average are shown below.

Position	Diameter (inches)
1	.251
2	.251
3	.251
Average:	.251

Interpoll Laboratories, Inc.

(612) 786-6020

Nozzle Calibration

Data Sheet

Date of Calibration: 9-11-91

Nozzle Number 1-4

Technician: Duane Van Hoever

The nozzle is rotated in 60 degree increments and the diameter at each point is measured to the nearest 0.001 inch. The observed readings and average are shown below.

Position	Diameter (inches)
1	.245
2	.243
3	.247
Average:	.245

Temperature Measurement Device
Calibration Sheet

Unit under test:

Vendor Atkins
 Model 39658-K Serial Number PDT-3
 Range -112-1999 °F Thermocouple Type K
 Date of Calibration 6-6-91 Technician Mark Koehler

Method of Calibration:

- ☐ Comparison against ASTM mercury in glass thermometer using a thermostatted and insulated aluminum block designed to provide uniform temperature. The temperature is adjusted by adjusting the voltage on the block heater cartridge.
- ☒ Omega Model CL-300 Type K Thermocouple Simulator which provides 22 precise temperature equivalent millivolt signals. The CL-300 is cold junction compensated. Calibration accuracy is $\pm 0.1\%$ of span (2100 °F) ± 1 degree (for negative temperatures add ± 2 degrees. The CL-300 simulates exactly the millivoltage of a Type K thermocouple at the indicated temperature.

Desired Temp (°F) Nominal	Temperature of Standard or Simulated Temp (°F)	Response of Unit Under Test (°F)	Deviation	
			Δt (°F)	(%)
0	0	-0.04	.04	.01
100	100	96.5	3.5	.63
200	200	199.4	.6	.09
300	300	297	3	.39
400	400	393	7	.81
500	500	492	8	.83
600	600	594	6	.57
700	700	693	7	.60
800	800	797	3	.24
900	900	898	2	.15
1000	1000	1001	1	.07
1100	1100	1103	3	.19
1200	1200	1208	8	.48
1300	1300	1307	7	.40
1400	1400	1409	9	.48
1500	1500	1505	5	.26
1600	1600	1604	4	.19
1700	1700	1698	2	.10
1800	1800	1794	6	.27
1900	1900	1884	16	.68
2000	2000	1977	23	.93
2100				
Averages:			5.91	0.40

OF = off scale response by unit under test (°F)
 $\% \text{ dev} = 100 \Delta t / (460 + t)$

- ☒ Unit in tolerance
☐ Unit was not in tolerance; recalibrated - See new calibration sheet.

Interpoll Laboratories, Inc.

Temperature Measurement Device
Calibration Sheet

Unit under test:

Vendor FLUKA
 Model 51 Serial Number POT #15
 Range -328 - 2498 °F °F Thermocouple Type K
 Date of Calibration 7-17-91 Technician STEVE LAMBERT

Method of Calibration:

- ☐ Comparison against ASTM mercury in glass thermometer using a thermostatted and insulated aluminum block designed to provide uniform temperature. The temperature is adjusted by adjusting the voltage on the block heater cartridge.
- ☒ Omega Model CL-300 Type K Thermocouple Simulator which provides 22 precise temperature equivalent millivolt signals. The CL-300 is cold junction compensated. Calibration accuracy is $\pm 0.1\%$ of span (2100 °F) ± 1 degree (for negative temperatures add ± 2 degrees. The CL-300 simulates exactly the millivoltage of a Type K thermocouple at the indicated temperature.

Desired Temp (°F) Nominal	Temperature of Standard or Simulated Temp (°F)	Response of Unit Under Test (°F)	Deviation	
			Δt (°F)	(%)
0	0	1.6	1.6	0.35
100	100	98.2	1.8	0.32
200	200	200.6	0.6	0.09
300	300	299.4	0.6	0.08
400	400	397.8	2.2	0.20
500	500	498.6	1.4	0.15
600	600	600.6	0.6	0.06
700	700	698.6	1.4	0.12
800	800	800.6	0.6	0.05
900	900	898.8	1.2	0.09
1000	1000	1000.2	0.2	0.01
1100	1100	1099.8	0.2	0.01
1200	1200	1202.4	2.4	0.14
1300	1300	1299.2	0.8	0.05
1400	1400	1402.6	2.6	0.14
1500	1500	1500.0	0.0	0.00
1600	1600	1601.2	1.2	0.05
1700	1700	1699.8	0.2	0.01
1800	1800	1801.2	1.2	0.05
1900	1900	1899.0	1.0	0.04
2000	2000	2001.0	1.0	0.04
2100	2100	2098.2	1.8	0.07
Averages:			1.12	0.09

OF = off scale response by unit under test (°F)
 % dev = $100 \Delta t / (460 + t)$

- ☒ Unit in tolerance
☐ Unit was not in tolerance; recalibrated - See new calibration sheet.

S-Type Pitot Tube Inspection SheetPitot No. 23-6Pitot tube dimensions:

1. External tubing diameter (D_t) 313 IN.
2. Base to Side A opening plane (P_A) 464 IN.
3. Base to Side B opening plane (P_B) 465 IN.

Alignment:

4. $\alpha_1 < 10^\circ$ 0
5. $\alpha_2 < 10^\circ$ 0
6. $\beta_1 < 5^\circ$ 2
7. $\beta_2 < 5^\circ$ 2
8. $Z < .125"$.03
9. $W < .0625"$.03

Distance from Pitot to Probe Components:

10. Pitot to 0.500 IN. nozzle 758 IN.
11. Pitot to probe sheath 3.00 IN.
12. Pitot to thermocouple (parallel to probe) 3.00 IN.
13. Pitot to thermocouple (perpendicular to probe) 762 IN.

☒ Meets all EPA design criteria thus $C_p = 0.84$

☐ Does not meet EPA design criteria - thus calibrate in wind tunnel
 $C_p =$ _____

Date of Inspection:

2-12-91

Inspected by:

[Signature]

CFR Title 40 Part 60 Appendix A Method 2

INTERPOLL LABORATORIES
(612)786-6020
Stack Sampling Department - QA
Aneroid Barometer Calibration Sheet

Date 7/8/91
 Technician Duane Van Hoever
 Mercury Column Barometer No. 1
 Aneroid Barometer No. Ultimeter Series 1 # 8C1216

Actual Mercury Barometer Read	Ambient Temp.	Temperature Correction Factor	Adjusted Mercury Barometer Read	Initial Aneroid Barometer Read	Difference (Pba-Pbm)
29.27	70	.11	29.16	29.17	-.01

Has this barometer shown any consistent problems with calibration? Yes/No. If yes, explain. No

Has problem been alleviated? Yes/No. How? _____

***Note**

Aneroid barometers will be calibrated periodically against a mercury column barometer. The aneroid barometer to be calibrated should be placed in close proximity to the mercury barometer and left to equilibrate for 20-30 minutes before calibrating. Aneroid barometer will be calibrated to the adjusted mercury barometer readings.

S-312

INTERPOLL LABORATORIES
(612)786-6020
Stack Sampling Department - QA
Aneroid Barometer Calibration Sheet

Date 7-17-71
Technician STEVE LONNIG
Mercury Column Barometer No. N/A-1
Aneroid Barometer No. S/N 560209

Actual Mercury Barometer Read	Ambient Temp.	Temperature Correction Factor	Adjusted Mercury Barometer Read	Initial Aneroid Barometer Read	Difference (P _{ba} -P _{bm})
29.13	86	0.150	28.98	29.08	0.10
LATELURE		-0.001	28.98	29.08	0.10

Has this barometer shown any consistent problems with calibration? Yes/No. If yes, explain. NO

Has problem been alleviated? Yes/No. How? N/A

***Note**

Aneroid barometers will be calibrated periodically against a mercury column barometer. The aneroid barometer to be calibrated should be placed in close proximity to the mercury barometer and left to equilibrate for 20-30 minutes before calibrating. Aneroid barometer will be calibrated to the adjusted mercury barometer readings.

S-312

APPENDIX B

LOCATION OF TEST PORTS

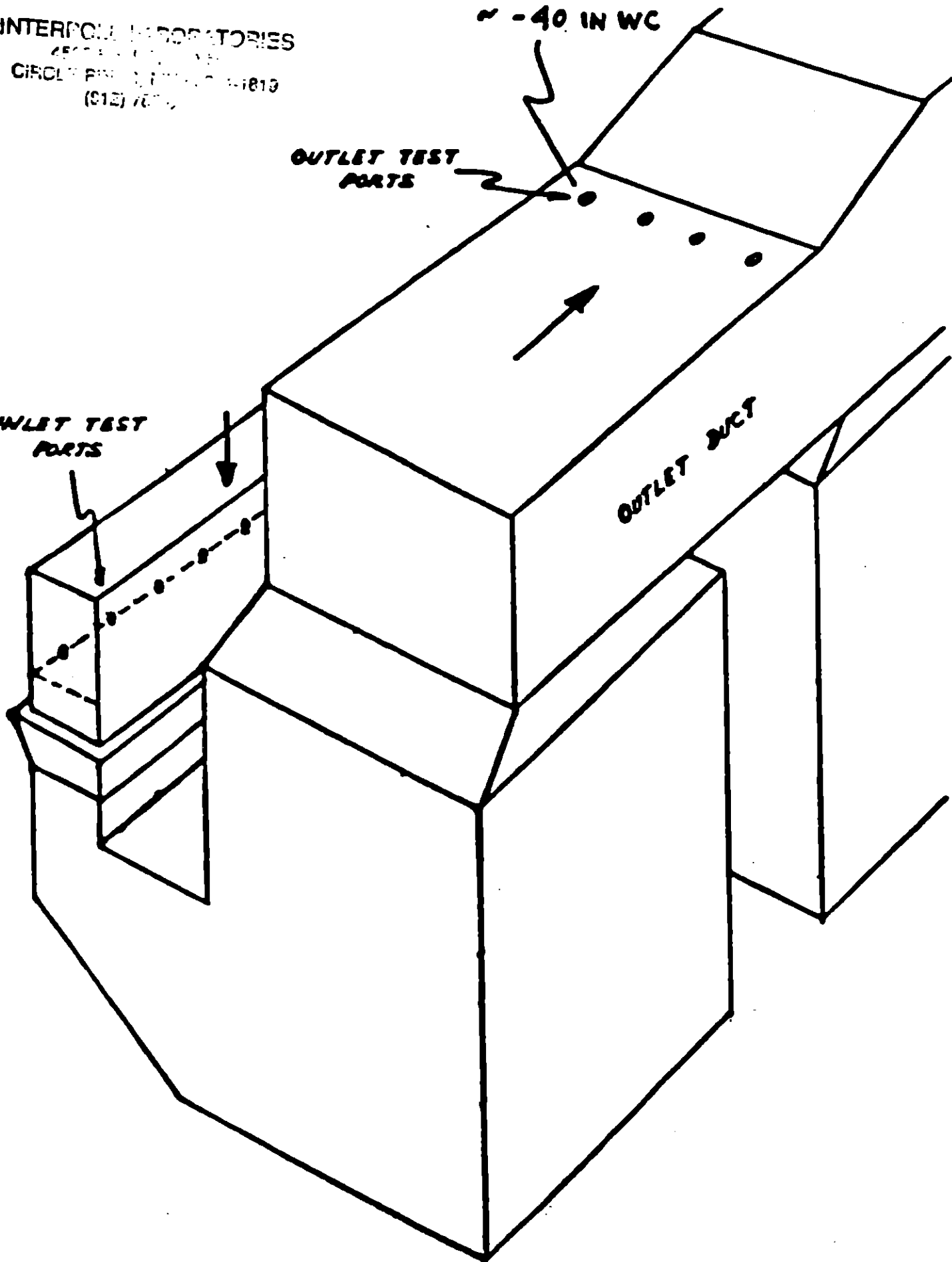
INTERPOL LABORATORIES
4500 E. 17TH AVE.
CIRCLE PIN 111819
(91E) 7070

~ -40 IN WC

OUTLET TEST
PORTS

INLET TEST
PORTS

OUTLET DUCT



EPA Method 1 Specification

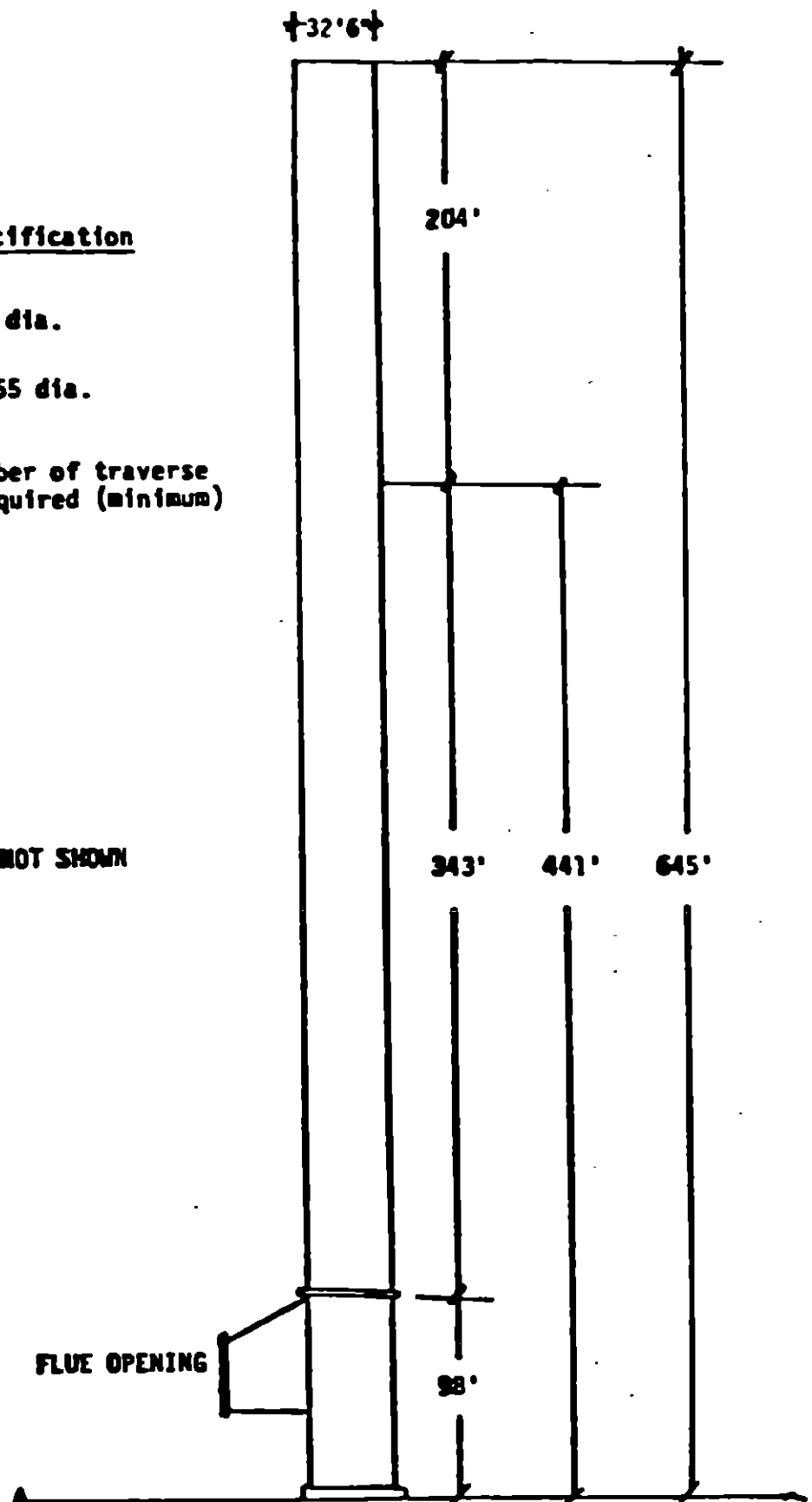
$$A = \frac{204}{32.5} = 6.28 \text{ dia.}$$

$$B = \frac{343}{32.5} = 10.55 \text{ dia.}$$

MN = Total number of traverse
points required (minimum)

MN = 12

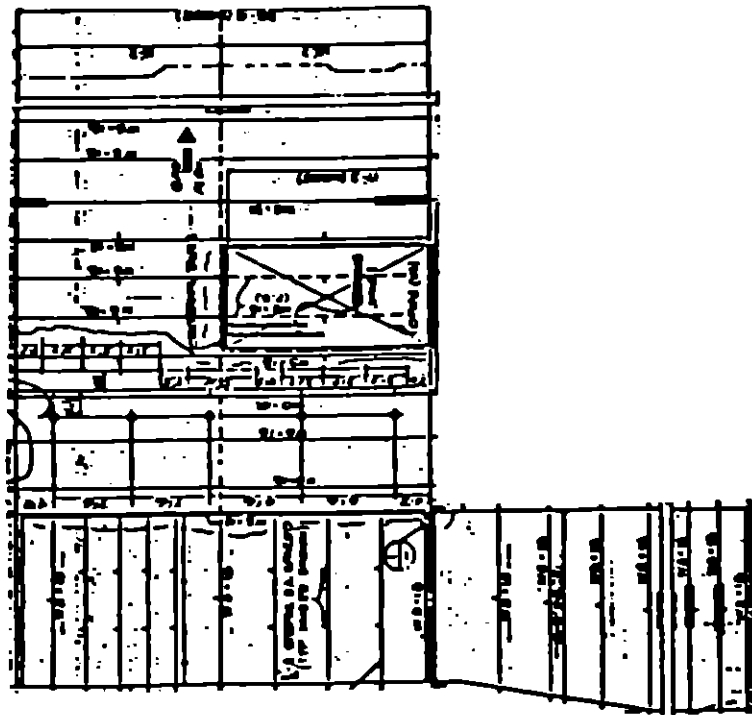
OUTER COLUMN NOT SHOWN



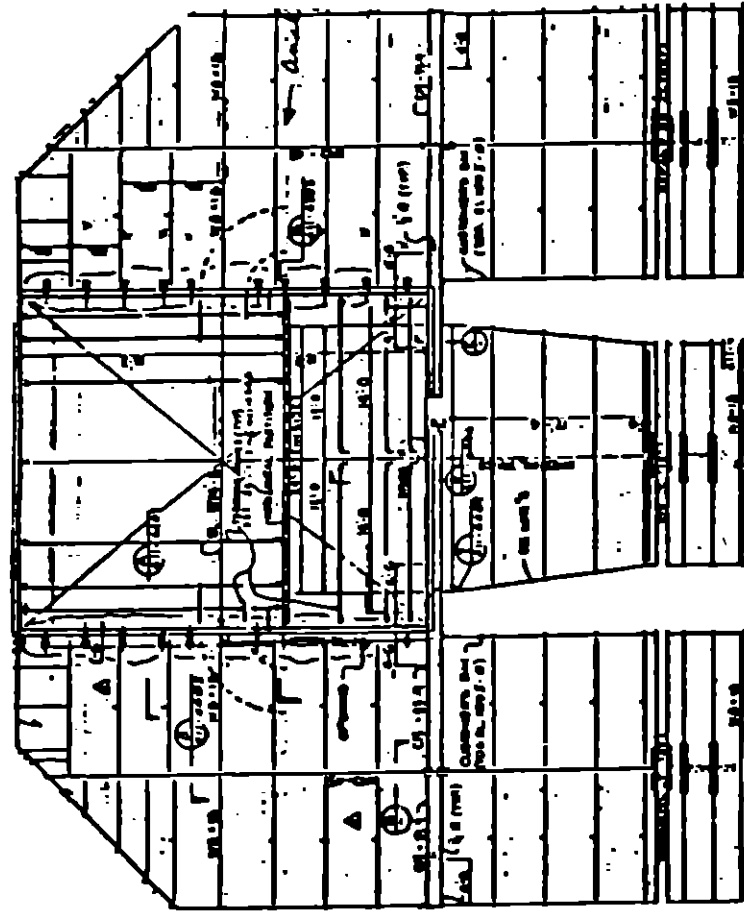
RSP SHERBURNE COUNTY GENERATING PLANT
UNITS 1&2 STACK

INTERPOLL INC.

NOT TO SCALE



SIDE ELEVATION

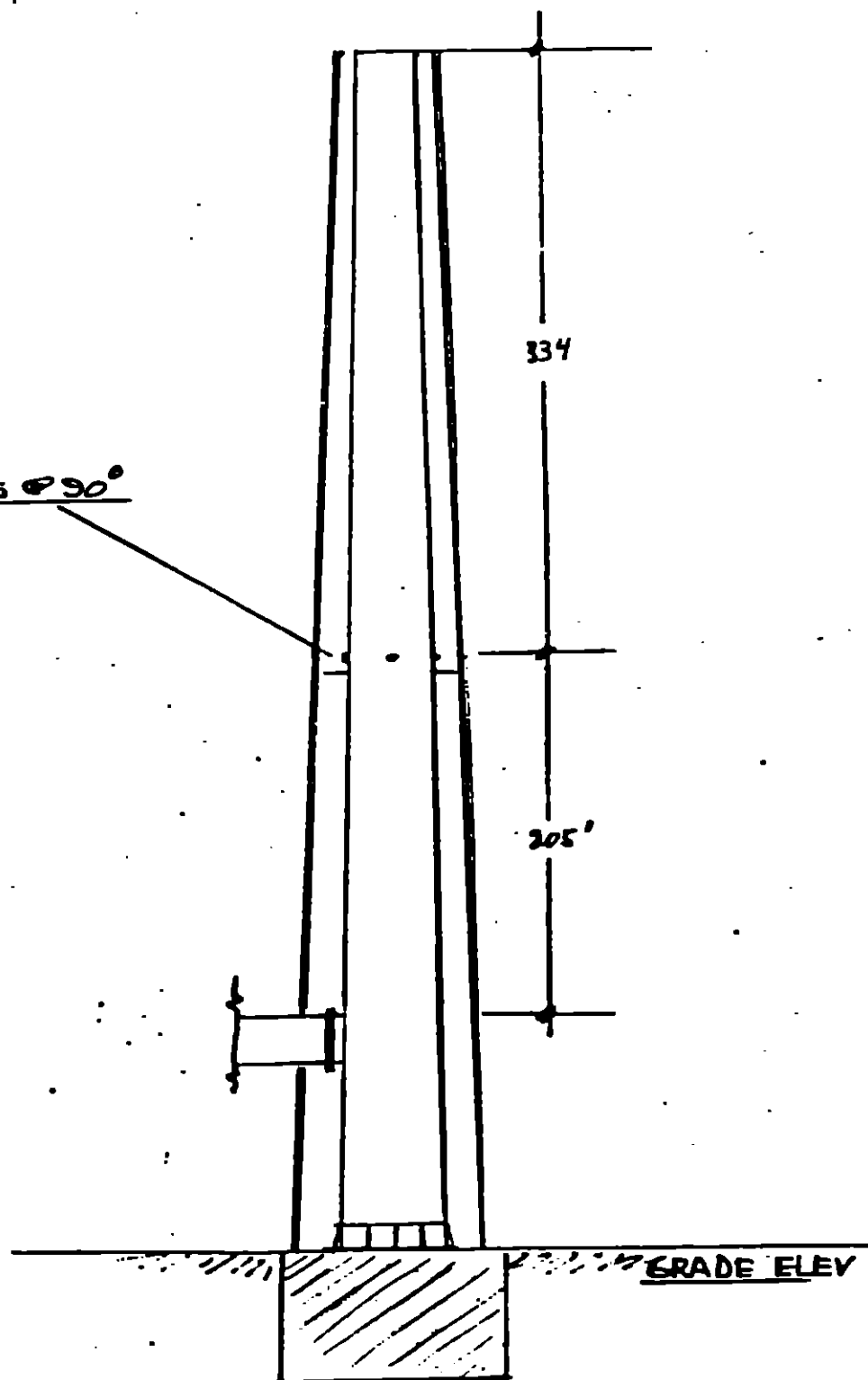


FRONT ELEVATION

NSP SHERCO UNIT 3 AIR HEATER OUTLET TEST SITE

NSP SHERCO UNIT 3

FOUR PORTS @ 90°
D_s = 29'-6"



LP 11/87
REV 3/88

NOT TO SCALE

APPENDIX C

FIELD DATA SHEETS



interpoll

INTERPOLL LABORATORIES, INC.
4500 BALL ROAD N.E.
CIRCLE PINES, MINNESOTA 55014-1819
TEL: 612/786-6020
FAX: 612/786-7854

May 27, 1992

Northern States Power Company
414 Nicollet Mall
Minneapolis, Minnesota 55401-1927

Attention: Patricia Boyce

Dear Patti:

Enclosed please find three (3) copies of the requested revised or corrected pages from Interpoll Laboratories Report No. 1-3409 entitled "Results of the September 10 and 11, 1991 Mercury Removal Tests on the Units 1 & 2, and Unit 3 Scrubber Systems at the NSP Sherco Plant in Becker, Minnesota". In addition, one complete copy of this report has also been enclosed as you requested.

If you have any questions, please call.

Sincerely,

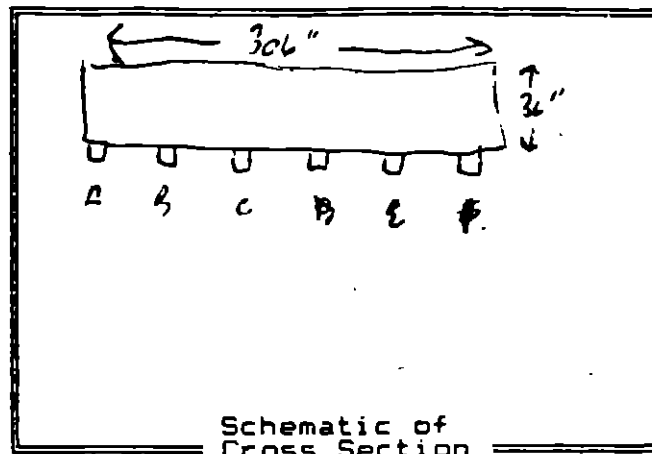
INTERPOLL LABORATORIES, INC.

Daniel Gespen,
Manager
Field Testing Support Group

DD:kce

INTERPOL LABORATORIES EPA METHOD 2 FIELD DATA SHEET

Job U.S.P. SHED
 Source 1" SCHURTER FILTERS
 Test — Run — Date 9/16/91
 Stack dimen. 2" x 306" IN.
 Dry bulb — °F Wet bulb — °F
 Manometer: ☒ Reg. ☐ Exp. ☐ Elec.
 Barometric pressure 29.84 in Hg
 Static pressure 11.88 in WC
 Operators D.B.
 Pitot No. 23-C Cp .84



Traverse Point No.	Fraction of Diameter	Distance from Stack Wall (in)	Distance from End of Port (in)	Velocity Pressure (in WC)	Temperature of gas (°F)
		Port length:	in.	Time start:	hrs
1	1			.70	
	2			.63	
	3			.63	
2	4			1.0?	
3	5			.85	
	6			.92	
4	7			1.3	
	8			1.1	
5	9			1.5	
	10			1.5	
6	11			.75	
	12			1.3	
	13				
	14				
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	98				
	99				
	100				
Temp. meas. tool & S/N: <u>PDT-15</u>				Time end:	hrs

R or nothing = reg. manometer; S = expanded; E = electronic S-392.1

INTERFOLL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job: N.S.P. SHERLO
 Source: SCRUBBER TALETS
 Method: 101A Filter holder: N/A

Date: 9/10/91 Test: 1 Run: 1
 No. of traverse points: 48
 Filter type: N/A

Sample Train Leak Check:

Pretest: { 0.02 cfm at 15 in. Hg. (vac) ☒
 Posttest: { .00 cfm at 10 in. Hg. (vac) ☒

Particulate Catch Data:

No.s of filters used: _____ Recovery solvent(s) _____

NONE ☐ acetone
☒ other(s) 7% KMnO₄
K₂O H₂SO₄

No. of probe wash bottles: _____
 Sample recovered by: _____

Condensate Data:

Item	Weight (g)		
	Final	Tare	Difference
Impinger No. 1	644	550	94.0
Impinger No. 2			
Impinger No. 3			
Condenser			
Desiccant	1350	1337	13.0
Total			107.0

Integrated Gas Sampling Data:

Bag Pump No. B-13 Box No. 9 Bag No. 1
 Bag Material: 5-layer Aluminized Tedlar Size: 44 L
 Pretest leak check: .00 cc/min at 15 in. Hg.
 Time start: 815 (HRS) Time end: 1030 (HRS)
 Sampling rate: 200 cc/min Operator: D.B.
 S/N of O₂ Analyzer used to monitor train outlet: 8

CF-023

INTERPOL LABORATORIES EPA METHOD 5 FIELD DATA SHEET

Job No. 542020 Operator DB Pitot No. 23-6 CP 84
 Source SAUBERK TALETS (2005104) Motor Box No. 2 Bar. Press. 29.42 in Hg H₂O
 Date 9/10/91 Collector Code: 999 L₉₂ IN MC Nozzle No. 187 IN.

Transfer Point No.	Sampling Time (min)	Sample Volume (L)	Velocity Head (in H ₂ O)	Orifice Meter (in H ₂ O)	Dob. Vol. (L)	VAC. in Hg	Temperature (°F)						Oxygen (%)
							Stack	Probe	Duct	Inlet	Gas/In	Gas/Duct	
A-1													
1	2.5	729.20	.98	.72	730.39	3.5	312	290	240	70	76	6.6	
2	5.0	730.36	.76	.54	731.12	3.0	309			79	78	6.7	
3	7.5	731.41	.90	.64	731.51	3.5	310			80	77	6.5	
4	10.0	732.52	.93	.66	731.47	4.0	310			81	77	6.5	
B-1													
1	12.5	733.662	.92	.66	731.80	4.0	310			84	78	6.5	
2	15.0	734.77	.79	.55	735.85	3.5	307			84	78	6.3	
3	17.5	735.92	.79	.55	737.06	4.0	310			86	78	6.4	
4	20.0	737.02	1.05	.75	738.05	3.0	310			87	78	6.1	
C-1													
1	22.5	738.061	.70	.50	739.27	4.0	306			87	79	6.5	
2	25.0	739.30	1.05	.76	740.42	4.0	310			88	79	6.3	
3	27.5	740.45	.94	.68	741.62	4.0	311			89	80	6.5	
4	30.0	741.63	1.03	.74	742.87	4.0	311			90	80	6.8	
D-1													
1	32.5	742.891	1.1	.79	743.76	3.0	305			89	80	7.0	
2	35.0	743.79	.55	.40	744.95	4.0	307			89	80	7.5	
3	37.5	744.98	1.0	.72	746.36	4.5	306			90	81	7.4	
4	40.0	746.36	1.4	1.02	747.78	4.5	307			92	80	7.3	
E-1													
1	42.5	747.788	1.4	1.02	748.36	4.5	304			90	81	8.1	
2	45.0	748.40	.25	.18	749.29	2.0	300			91	81	7.8	
3	47.5	749.72	1.2	.88	751.08	4.0	297			92	82	7.6	
4	50.0	751.08	1.3	.96	752.09	4.5	297			93	81	7.6	
F-1													
1	52.5	752.572	1.6	1.18	754.06	5.0	295			92	82	7.7	
2	55.0	754.10	1.5	1.11	755.45	4.5	286			92	82	7.6	
3	57.5	755.49	1.3	.97	756.08	3.5	283			93	83	7.8	
4	60.0	756.50	.72	.54	757.93	5.0	282			92	83	7.7	
Total													
Σ =		V ₀ =	Σ H =		Σ V ₀ =		Σ V ₀ =		Σ V ₀ =		Σ V ₀ =		

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110 H₂O
110 H₂O
110 H₂O

Transfer Point No.	Sampling Time (min)	Sample Volume (cc)	Velocity Head (in WC)	Drilled Meter (in WC)	Dep. Vol. (cc)	VAC. in Hg	Temperature (°F)				Case/Del	Dyecon (cc/v)	
							Stack	Probe	Oven	Insp.			
6-1	920	757.903	.68	.52	758.94	3.0	275			47	90	83	7.8
2	2.5	758.92	.88	.67	760.09	3.5	268			47	91	83	6.4
3	5.0	760.06	1.35	1.04	761.52	5.0	267			47	92	82	6.3
4	7.5	761.49	1.6	1.22	763.07	5.0	270			47	93	83	6.1
H-1	10.0	763.063	1.7	1.32	764.18	5.5	262			48	93	83	6.2
2	12.5	764.71	1.4	1.07	766.14	5.0	270			48	93	83	6.3
3	15.0	766.17	1.5	1.15	767.64	5.0	272			49	94	84	6.4
4	17.5	767.64	1.15	.88	768.96	4.0	272			49	93	85	6.6
5	20.0	768.938	1.65	1.28	770.54	5.0	265			49	94	84	6.8
T-1	22.5	770.55	1.4	1.07	772.00	5.0	272			49	94	84	6.7
2	25.0	772.00	1.78	.59	773.09	3.5	273			50	94	84	8.2
3	27.5	773.07	2.0	1.53	774.80	6.0	273			50	93	84	8.0
4	30.0	774.802	1.5	1.16	776.33	5.5	266			50	94	84	6.6
5-1	32.5	776.36	1.25	.96	777.71	4.5	268			50	94	84	6.9
2	35.0	777.75	1.25	.81	778.98	4.0	269			50	94	84	6.9
3	37.5	778.99	1.05	.96	780.35	4.5	269			51	94	84	6.4
4	40.0	780.33	1.25	.96	781.79	4.5	264			51	94	85	6.0
6-1	42.5	781.81	1.35	1.05	783.26	4.5	268			51	94	85	6.3
2	45.0	783.17	1.3	1.00	784.49	4.0	271			52	94	85	6.2
3	47.5	784.46	1.1	.84	785.79	3.5	270			52	94	84	6.1
4	50.0	785.405	.53	.40	786.91	5.5	263			52	94	84	6.5
L-1	52.5	786.93	1.5	1.16	788.34	4.5	272			53	94	85	6.2
2	55.0	788.33	1.35	1.03	789.68	4.0	275			53	94	86	5.9
3	57.5	789.66	1.2	.92	791.00	4.0	276			53	95	85	
4	60.0	791.006	1.15	.87									
1030													
9 = 120 V = 61.806 PM = 97													AV = 96.2

S-0037R

INTERPOL LABORATORIES EPA METHOD 5 FIELD DATA SHEET

Job ASD SHRACO Operator BG Pilot No. 73-C Cp. 84
Source SCARBOROUGH TOWNSHIP MOORE Motor Bar No. 1000 Bar. Press. 1000 IN. HG. 1000
Date 9/10/79 1001 1 2 Recorder Code 1997 Model No. 1000 1000 1000

Transfered Print No.	Sampling Time (min)	Sample Volume (cc)	Velocity Head (in.Hg)	Drifted Motor (in.Hg)	D.B. Vol. (cc)	VAC. in.Hg	Temperatures (°F)					Oxygen (%v/v)	
							Stack	Probe	Oven	Logg.	Cool'n		Cool/Dri
RECORD	1105	791.403	75	92	792.64	4	260	RECORD	RECORD	RECORD	RECORD	RECORD	RECORD
A-1	2.5	792.64	.75	.92	792.64	4	260			47	83	82	6.8
2	5.0	793.77	.85	.66	793.77	4	262			47	83	82	6.8
3	7.5	794.94	.93	.74	794.97	4	267			47	83	82	6.9
4	10.0	796.18	1.00	.79	796.22	4	268			47	82	82	7.2
B-1	12.5	797.44	1.36	1.03	797.44	4	265			47	83	80	7.0
2	15.0	798.835	.94	.74	798.84	5	271			48	84	81	7.0
3	17.5	800.06	1.00	.79	800.08	4	273			48	85	81	6.6
4	20.0	801.34	1.10	.87	801.38	4	273			48	85	81	7.5
C-1	22.5	802.54	.75	.59	802.54	4	269			47	87	80	6.8
2	25.0	803.88	1.30	1.03	803.86	4	273			47	87	81	6.6
3	27.5	805.14	1.10	.86	805.18	5	277			48	88	81	6.4
4	30.0	806.47	1.20	.94	806.54	5	276			48	90	81	6.0
D-1	32.5	808.15	1.50	1.21	808.08	6	261			46	90	82	5.8
2	35.0	809.39	1.10	.87	809.39	6	274			48	90	81	5.6
3	37.5	810.66	1.10	.86	810.64	5	278			48	90	81	5.5
4	40.0	812.11	1.40	1.11	812.17	5	269			48	92	81	7.3
E-1	42.5	813.62	1.50	1.19	813.70	6	272			48	91	81	6.0
2	45.0	815.09	1.40	1.12	815.19	6	268			48	91	82	5.7
3	47.5	816.44	1.15	.92	816.53	6	270			48	92	82	5.7
4	50.0	817.74	1.10	.88	817.85	6	267			48	92	82	5.7
F-1	52.5	819.20	1.20	.96	819.22	5	265			48	91	82	6.6
2	55.0	820.68	1.25	1.01	820.63	6	261			48	92	82	8.0
3	57.5	821.93	1.05	.86	821.93	7	254			47	92	82	7.8
4	60.0	823.55	1.65	1.35	823.56	6	254			47	92	82	7.0
RECORD	1205												

INTERFOLL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job N-5-2 5/18/60
 Source SAVRES
 Method 1012
 Filter holder: —
 Date 9/16/91 Test 1 Run 2
 No. of traverse points 48
 Filter type: —

Sample Train Leak Checks

Pretest: (0.02 cfm at 15 in. Hg. (vac) ☒
 Posttest: (00 cfm at 12 in. Hg. (vac) ☒

Particulate Catch Data:

No.s of filters used: _____
 Recovery solvent(s) _____

☐ acetone
☒ other(s) 4% KMNO₄
10% H₂SO₄
 No. of probe wash bottles: 1
 Sample recovered by: 2.8.

Condensate Data:

Item			Total
Weight (g)	Final	Tare	
Impinger No. 1	657	544	113
Impinger No. 2			
Impinger No. 3			
Condenser			
Desiccant			
	1519	1504	15
			128

Integrated Gas Sampling Data:

Bag Pump No. 8-13 Box No. 9 Bag No. 2
 Bag Material: 5-layer Aluminized Tedlar Size: 44 L
 Pretest leak check: .00 cc/min at 15 in. Hg.
 Time start: 1105 (HRS) Time end: 840 (HRS)
 Sampling rate: 200 cc/min Operator: 2.8.
 S/N of Oz Analyzer used to monitor train outlet: 8

CF-023

S-0046RR

C-5

INTERFOLL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job N.S.P. 5H260 Date 9/10/91 Test 1 Run 3
 Source SC000822 EN0215 100.25 (20.4.27) No. of traverse points 48
 Method 101A Filter holder: _____ Filter type: _____

Sample Train Leak Checks

Pretest: ☒ 0.02 cfm at 15 in. Hg. (vac) ☒
 Posttest: ☒ .00 cfm at 11 in. Hg. (vac) ☒

Particulate Catch Data:

No. of filters used: _____
 Recovery solvent(s) _____
☐ acetone ☐ other(s) _____
 No. of probe wash bottles: _____
 Sample recovered by: _____
4% KMNO₄
10% H₂SO₄

Condensate Data:

Item			Weight (g)
Impinger No. 1	646	547	
Impinger No. 2			
Impinger No. 3			
Condenser			
Desiccant		1385	
	1530	1519	11
Total			110

Integrated Gas Sampling Data:

Bag Pump No. 8-13 Box No. 9 Bag No. 3
 Bag Material: 5-layer Aluminized Tedlar Size: 44 L
 Pretest leak check: .00 cc/min at 15 in. Hg.
 Time start: 1420 (HRS) Time end: 1643 (HRS)
 Sampling rate: 200 cc/min Operator: B.B.
 S/N of O₂ Analyzer used to monitor train outlet: 8

CF-023

C-8

S-0046RR

5-215

INTERPOL LABORATORIES EPA METHOD 5 FIELD DATA SHEET

Job No. 2512 SHREK Operator B.A. Pilot No. 23-C CP 81
Source SHREK 215 SHREK 215 Motor No. 2-999 110 IN UC Bar. Press. 29.70 IN HG H2O
Date 7/10/71 1971 Non DE Chamber Feed. 1 Nozzle No. 1 Weir No. 1 IN.

Transfer Point No.	Sampling Time (min)	Sample Volume (cc)	Velocity Head (in H ₂ O)	Orifice Meter (in H ₂ O)	Obs. Vel. (ft/s)	VAC. (in Hg)	Temperatures (°F)						Oxygen (cc/v)
							Stack	Probe	Oven	Inlet	Gas In	Gas Out	
6-1	1240	823.70	.58	1.73	824.03	5	205			47	80	80	4.3
2	2.5	824.75	.74	.55	825.67	5	315			47	82	80	4.2
3	5.0	825.67	.54	.40	826.54	5	320			47	83	80	3.8
4	7.5	826.54	.62	.46	827.50	5	320			47	84	80	3.6
H-1	10.0	827.50	.90	.67	828.44	5	315			47	84	80	3.4
2	12.5	828.44	.90	.67	829.38	5	315			48	85	80	3.4
3	15.0	829.38	.83	.62	830.33	5	315			47	86	80	3.3
4	17.5	830.33	.83	.62	831.28	5	315			47	87	80	3.5
I-1	20.0	831.28	.83	.62	832.23	5	316			47	87	80	3.5
2	22.5	832.23	1.4	1.05	833.18	7	312			47	87	80	3.1
3	25.0	833.18	1.3	.96	834.13	7	320			48	87	80	3.0
4	27.5	834.13	.83	.61	835.08	5	318			47	88	80	3.0
J-1	30.0	835.08	.95	.71	836.03	6	316			47	88	81	3.1
2	32.5	836.03	1.25	.93	837.98	6	316			47	88	81	3.2
3	35.0	837.98	1.05	.78	839.22	6	315			47	88	81	3.2
4	37.5	839.22	.98	.73	840.42	6	315			48	88	81	3.2
K-1	40.0	840.42	1.10	.82	841.41	6	315			48	88	81	3.2
2	42.5	841.41	1.35	1.01	842.39	8	316			48	87	80	3.6
3	45.0	842.39	1.50	1.13	843.38	8	309			47	88	81	3.4
4	47.5	843.38	1.35	1.02	844.37	8	310			48	88	81	3.2
L-1	50.0	844.37	1.10	.83	845.36	8	308			47	88	81	3.0
2	52.5	845.36	1.40	1.04	846.35	9	307			47	88	81	3.4
3	55.0	846.35	.53	.46	847.34	5	307			47	88	81	3.4
4	57.5	847.34	.10	.07	848.33	3	300			47	87	81	3.5
M-1	60.0	848.33	.40	.30	849.32	5	302			47	87	81	3.4
(13410)													
V = 59.33 ft													
M = 81													
Avg. = 84.0													

INTERPOL LABORATORIES EPA METHOD 3 FIELD DATA SHEET

Job AL-3-P. SHERCO
 Source SEWAGE PLANT
 Date 8/12/91

Operator D.B.
 Water Box No. 3
 Gasoline 8.3

Probe 999
 Inlet MC
 Outlet MC

Pilot No. 23-C CP 84
 Bar. Press. 20.10 IN HG
 Nozzle No. 213 IN.

Transfer Point No.	Sampling Time (min)	Sample Volume (cc)	Velocity Head (in H ₂ O)	Orifice Meter (in H ₂ O)	Dep. Val. (ft)	VAC. in Hg	Temperature (°F)					Dye	
							Stack	Probe	Oven	Inlet	Case/Del		
A-1	14.20	851.60	.56	.43	852.55	5	273			47	82	80	5.8
2	2 1/2	852.54	.56	.43	853.46	5	275			47	82	80	5.7
3	5.0	853.43	.56	.43	854.31	5	274			47	83	80	5.8
4	7.5	854.30	.48	.37	855.30	5	270			47	84	80	6.0
B-1	10.0	855.30	.65	.50	856.30	8	275			47	85	81	5.6
2	12.5	856.32	.67	.51	857.28	7	272			48	85	81	5.1
3	15.0	857.28	.63	.48	858.37	7	273			48	86	80	5.1
4	17.5	858.38	.79	.61	859.54	7	274			48	88	80	5.1
C-1	20.0	859.52	.95	.73	860.68	11	271			47	87	81	6.3
2	22.5	860.67	.82	.63	861.73	9	260			47	88	81	4.9
3	25.0	861.72	.71	.54	862.83	8	273			47	87	81	4.8
4	27.5	862.81	.80	.62	864.01	9	270			48	87	81	5.0
D-1	30.0	864.00	.92	.71	865.24	5	269			47	87	80	6.0
2	32.5	865.25	.99	.77	866.29	4	273			48	88	81	4.8
3	35.0	866.29	.74	.57	867.28	4	276			48	88	81	4.4
4	37.5	867.27	.65	.50	868.36	4	275			48	88	81	4.4
E-1	40.0	868.33	.77	.59	869.29	4	274			47	88	82	4.7
2	42.5	869.29	.57	.44	870.21	4	276			47	89	82	4.4
3	45.0	870.00	.54	.43	871.27	4	277			47	89	83	4.2
4	47.5	871.25	.73	.56	872.15	5	276			48	89	82	4.5
F-1	50.0	872.17	.51	.39	873.45	4	269			48	88	82	4.6
2	52.5	872.79	.27	.21	874.15	4	260			48	88	82	6.9
3	55.0	873.43	.28	.22	875.35	4	264			47	88	82	5.4
4	57.5	874.33	.53	.41	875.35	4	273			47	89	82	5.0
5	60.0	875.34	.65	.50		4							
Σ =													
V =													
H =													
Avg. =													

S-0037R

Disc 1 of 2

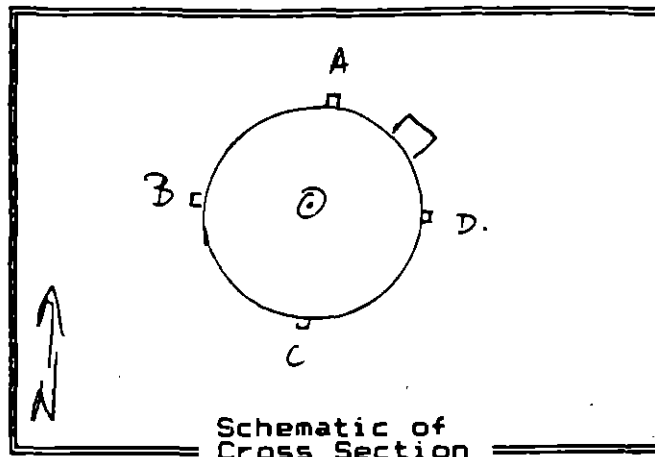
INTERPOL LABORATORIES EPA METHOD 5 FIELD DATA SHEET

Job N.S.P. SH200Source SH200Operator DBMotor Box No. 2Pilot No. 23-CCor. Press. 75.70 inHgMotor No. 83 in.

Injection Point No.	Sampling Time (min)	Sample Volume (cc)	Velocity Head (inHg)	Orifice Meter (inHg)	Dep. Vol. (cc)	VAC. inHg	Temperature (°F)					Oxygen (cc/vol)	
							Stack	Probe	Duct	Leaky	Gas In		Gas Out
6-1	2.5	875.35	1.15	.85	876.64	6	302			47	87	82	7.0
2	5.0	877.86	1.05	.78	877.88	5	302			47	88	82	7.2
3	7.5	879.08	1.05	.78	879.12	5	300			47	88	82	6.2
4	10.0	880.36	1.05	.78	880.36	6	298			48	89	82	5.5
H-1	12.5	881.56	.99	.74	881.56	5	300			47	91	83	4.9
2	15.0	882.76	.98	.73	882.77	5	298			47	92	83	4.5
3	17.5	883.88	.83	.64	883.89	5	280			46	93	84	4.1
4	20.0	884.95	.75	.56	884.95	5	299			47	95	84	4.0
I-1	22.5	886.38	1.35	1.02	886.36	6	298			47	95	84	3.9
2	25.0	887.70	1.20	.90	887.70	6	305			48	95	85	4.0
3	27.5	888.82	.85	.63	888.82	5	306			48	97	85	3.8
4	30.0	889.80	.64	.48	889.80	4	295			47	98	85	3.6
J-1	32.5	891.20	1.30	.98	891.20	6	300			47	98	85	6.5
2	35.0	892.30	.81	.61	892.30	5	299			48	98	86	6.2
3	37.5	893.52	1.05	.80	893.52	5	289			47	98	87	3.7
4	40.0	894.62	.73	.56	894.62	5	285			48	98	87	4.3
K-1	42.5	896.09	1.40	1.08	896.09	6	282			47	99	87	4.2
2	45.0	897.32	.98	.76	897.32	6	282			48	100	88	3.8
3	47.5	898.52	.96	.74	898.54	5	285			47	100	88	3.7
4	50.0	899.72	.92	.71	899.73	5	285			48	100	87	3.8
L-1	52.5	901.21	1.40	1.10	901.21	6	275			47	100	88	3.9
2	55.0	902.55	1.20	.93	902.57	6	285			48	100	89	4.6
3	57.5	903.65	.78	.60	903.66	5	287			48	101	90	5.2
4	60.0	904.91	1.00	.77	904.91	5	286			48	102	90	4.8
	164.3												
V ₀ = 53.31													
V ₀ = 120													
D = 1.0													
P = 0.0													
Avg. = 97.3													

INTERPOLL LABORATORIES EPA METHOD 2 FIELD DATA SHEET

Job N.S.P. SHERLO
Source UNITS 1 & 2 Stack
Test 1 Run 0 Date 9/10/91
Stack dimen. 390 IN.
Dry bulb °F Wet bulb °F
Manometer: ☒ Reg. ☐ Exp. ☐ Elec.
Barometric pressure 28.77 in Hg
Static pressure -1.35 in WC
Operators D. VanHoever & Gary Howe
Pitot No. V24-12 Cp .84

[illegible]

R or nothing= reg. manometer; S= expanded; E = electronic S-392.1

INTERFOLL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job N.S.D. SHERCO
 Source Units #1 & 2 Stack
 Method 5-1014 Filter holder: NA

Date 9/10/91 Test 1 Run 1
 No. of traverse points 16
 Filter type: none

Sample Train Leak Check:

Pretest: (0.02 cfm at 15 in. Hg. (vac) ☒
 Posttest: 0 cfm at 5 in. Hg. (vac) ☒

Particulate Catch Data:

No.s of filters used: Recovery solvent(s)

☐ acetone
☒ other(s) KMNO₄ & 6N HCL

No. of probe wash bottles: 1
 Sample recovered by: DWH

Condensate Data:

Item	Weight (g)		
	Final	Tare	Difference
Impinger No. 1			
Impinger No. 2	547	250	297
Impinger No. 3			
Condenser			
Desiccant	1540	1504	36
Total			373

Integrated Gas Sampling Data:

Bag Pump No. B12 Box No. _____ Bag No. 1
 Bag Material: 5-layer Aluminized Tedlar Size: 44 L
 Pretest leak check: 0 cc/min at 14 in. Hg.
 Time start: 0820 (HRS) Time end: 1032 (HRS)
 Sampling rate: 200 cc/min Operator: DWH
 S/N of O₂ Analyzer used to monitor train outlet: 11

CF-023

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WSP SURCO

Job NSP SURCO
Source UNITS 23 STICK
Date 8-10-91 1001 AM

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CP 14M9 H2O 11.1N.

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INTERFOLL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job N.S.P. Sherco Date 9/10/91 Test 1 Run 2
 Source Units 1 & 2 Stack No. of traverse points 16
 Method 101 A Filter holder: NA Filter type: NA

Sample Train Leak Check:

Pretest: (0.02 cfm at 15 in. Hg. (vac) ☒
 Posttest: 0 cfm at 10 in. Hg. (vac) ☒

Particulate Catch Data:

No.s of filters used: Recovery solvent(s)

☐ acetone
☒ other(s) KMNO₄ & 6N HCL

No. of probe wash bottles: 1
 Sample recovered by: DVA

Condensate Data:

Item	Weight (g)		
	Final	Tare	Difference
Impinger No. 1			
Impinger No. 2	<u>580</u>	<u>250</u>	<u>330</u>
Impinger No. 3			
Condenser			
Desiccant	<u>1412</u>	<u>1388</u>	<u>24</u>
Total			<u>354</u>

Integrated Gas Sampling Data: B

Bag Pump No. B12 Box No. _____ Bag No. 2

Bag Material: 5-layer Aluminized Tedlar Size: 44 L

Pretest leak check: 0 cc/min at 16 in. Hg.

Time start: 1110 (HRS) Time end: 1344 (HRS)

Sampling rate: 200 cc/min Operator: DVA

S/N of O₂ Analyzer used to monitor train outlet: 11

CF-023

N.S.P. SHELD

Source: Nov 22, 1961 1001 2
 Date: 9/10/61 1001 2

[illegible]

PUBLISHED BY
 THE
 PUBLISHERS
 100 N. 1st St.
 ST. LOUIS, MO.
 1914

[illegible]

Inversion Point No.	Sampling Time (min)	Sample Volume (cc)	Velocity Head (in H ₂ O)	Differential Pressure (in H ₂ O)	Dens. Vol. (cc)	VAC. in Hg	Temperature (°F)						Avg. =
							Stack	Probe	Duct	Inlet	Gas In	Gas Out	
A	105	341.80	2.50	1.90	443	6	182	N/A	N/A		75	75	7.5
A	4	344.87	2.75	2.07	819	6	182				77	75	7.3
A	8	348.13	2.60	1.96	137	6	182				80	76	7.3
B	12	351.39	2.60	1.96	456	6	180			53	82	77	7.4
B	16	354.57	2.60	1.96	767	55	180				83	77	7.4
B	20	357.71	2.45	1.87	0.78	55	180				83	77	7.3
B	24	360.80	2.30	1.75	3.77	5	180			55	82	78	7.4
C	28	363.84	2.30	1.76	6.81	5	180				85	78	7.3
C	32	366.98	2.25	1.91	9.96	5	190			60	86	79	7.3
C	36	369.95	2.20	1.99	3.18	5	180			58	85	78	7.3
C	40	373.28	2.20	2.06	6.45	5	181				86	78	7.2
D	44	376.52	2.25	1.91	9.61	5	180			55	85	78	7.3
D	48	379.72	2.20	1.98	2.82	5	181				85	78	7.3
D	52	382.92	2.25	1.91	5.96	5	181				87	81	7.3
D	56	385.95	2.25	1.91	9.12	5	181				87	81	7.3
E	60	389.26	2.20	1.84	2.22	5.5	181			55	87	81	7.3
E	64	392.32	2.20	1.84	5.22	6.0	181				87	81	7.3
F	68	395.38	2.20	2.07	8.61	6.0	180				87	81	7.3
F	72	398.50	2.20	2.07	1.89	6.0	181			54	87	81	7.3
G	76	401.85	2.20	1.96	5.06	6	180				87	81	7.3
G	80	405.09	2.20	1.96	8.19	6	180				87	81	7.3
H	84	408.15	2.25	1.90	1.38	6	180			54	87	81	7.3
H	88	411.32	2.20	1.98	4.58	6	181				87	81	7.3
I	92	414.44	2.20	1.98	7.44	6	181				87	81	7.3
I	96	417	2.20	1.98	7.44	6	181				87	81	7.3

INTERPOL LABORATORIES EPA METHOD 5 FIELD DATA SHEET

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Run

Operator
Meter Bar
Counter

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Order No.

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INTERPOL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job NSP. SHERCO Date 9/10/91 Test 1 Run 3
 Source Units 1 & 2 Stack No. of traverse points 16
 Method 101A Filter holder: none Filter type: none

Sample Train Leak Checks:

Pretest: (0.02 cfm at 15 in. Hg. (vac) ☒
 Posttest: 0 cfm at 8 in. Hg. (vac) ☒

Particulate Catch Data:

No.s of filters used: _____ Recovery solvent(s) _____

_____ ☐ acetone _____
 _____ ☒ other(s) _____

No. of probe wash bottles: 1
 Sample recovered by: DCH

Condensate Data:

Item	Weight (g)		
	Final	Tare	Difference
Impinger No. 1			
Impinger No. 2	590	250	340
Impinger No. 3			
Condenser			
Desiccant	1519	1504	15
Total			355

Integrated Gas Sampling Data:

Bag Pump No. B12 Box No. _____ Bag No. 3
 Bag Material: 5-layer Aluminized Tedlar Size: 44 L
 Pretest leak check: 0 cc/min at 14 in. Hg.
 Time start: _____ (HRS) Time end: _____ (HRS)
 Sampling rate: 200 cc/min Operator: DCH
 S/N of O₂ Analyzer used to monitor train outlet: 11

CF-023

Job NSP SHERCO
 Sub UNIT 5 1st STAGE
 Date 10/1/56 Run 3
 Operator _____ IN DE _____
 Meter Box No. _____ HU _____
 Counter Code: _____ T.D.S. _____
 Pitot No. _____ CP _____
 Bar. Press. 25.0 in Hg H2O
 Nozzle No. 1-3 Nozzle Dia. 189 in.

[illegible]

NSP 57/ERCD

Job NSP SH/ERCO
Source UNIT 102 STACK
Date 2-20-41 1001 Run 3

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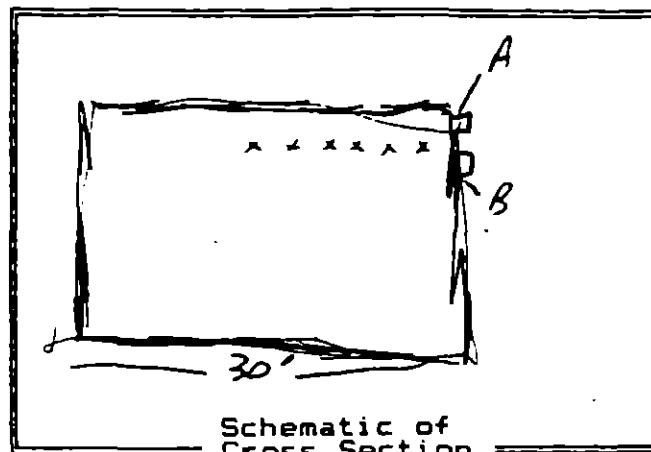
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02H

Transfer Point No.	Supplying Pipe (in)	Sample Volume (cf)	Velocity Head (in WC)	Drifted Meter (in WC)	Dis. Vol. (cf)	VAC. in Hg	Temperatures (°F)					Dewpon (Kv/v)	
							Stack	Probe	Oven	Leaky	Carbide		Gas/Dut
4	100	520.79	2.3	1.76	0.56	6	180				87	81	7.4
4	100	523.04	2.45	1.88	3.70	6	181			54	87	81	7.4
3	108	526.89	2.5	1.92	6.86	6	181				87	81	7.4
3	112	529.89	2.3	1.76	9.88	6	180				87	81	7.2
2	116	532.00	2.5	1.92	3.04	6	180			54	87	81	7.2
2	120	536.05	2.3	1.77	6.08	6	180				87	81	7.2
1	124	539.09	2.4	1.84	9.18	6	182				87	81	7.3
1	128	542.06	2.2	1.69	2.14	6	182			55	87	82	7.3
	1637												
											</		

Job N.S.P. SHERLO
Source UNIT 3 SCUBBLE INLET
Test 2 Run Date 9/11/91
Stack dimen. 360" X 436.8" IN.
Dry bulb °F Wet bulb °F
Manometer: ☐ Reg. ☐ Exp. ☐ Elec.
Barometric pressure 29.04 in Hg
Static pressure -17.0 in WC
Operators D.B. & B.A.
Pitot No. TEFWND
LINE 2 PRESS Cp 84

[illegible]

R or nothing= req. manometer; S= expanded; E = electronic S-392.1

INTERFOLL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job NSP SHORCO
 Source UNIT #3 SEWAGE TREAT
 Method 101A Filter holder: N/A

Date 9/11/91 Test 2 Run 1
 No. of traverse points 12
 Filter type: N/A

Sample Train Leak Check:

Pretest: (0.02 cfm at 15 in. Hg. (vac)
 Posttest: .003 cfm at 22 in. Hg. (vac)

Particulate Catch Data:

No.s of filters used: _____ Recovery solvent(s) _____

0

☐ acetone
☒ other(s) HNO₃ + HCL
+ 5% H₂O

No. of probe wash bottles: _____
 Sample recovered by: _____

Condensate Data:

Item	Weight (g)		
	Final	Tare	Difference
Impinger No. 1	<u>710</u>	<u>520</u>	<u>190.0</u>
Impinger No. 2			
Impinger No. 3			
Condenser			
Desiccant	<u>1392</u>	<u>1386</u>	<u>6.0</u>
Total			<u>(196.0)</u>

Integrated Gas Sampling Data:

Bag Pump No. B13 Box No. 26 Bag No. 1

Bag Material: 5-layer Aluminized Tedlar Size: 44 L

Pretest leak check: .00 cc/min at 15 in. Hg.

Time start: 835 (HRS) Time end: 1042 (HRS)

Sampling rate: 200 cc/min Operator: D.B.

S/N of O₂ Analyzer used to monitor train outlet: 4

CF-023

INTERFOLL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job N.S.P. SHERLD Date 9/11/91 Test 2 Run 2
 Source UNIT #3 SCRUBBER INLET No. of traverse points 12
 Method 101 A Filter holder: N/A Filter type: N/A

Sample Train Leak Checks:

Pretest: { 0.02 cfm at 15 in. Hg. (vac) ☒
 Posttest: { .00 cfm at 10 in. Hg. (vac) ☒

Particulate Catch Data:

No.s of filters used: _____ Recovery solvent(s) _____

0 ☐ acetone _____
☐ other(s) _____

No. of probe wash bottles: _____
 Sample recovered by: _____

Condensate Data:

Item	Weight (g)		
	Final	Tare	Difference
Impinger No. 1	648	539	109
Impinger No. 2			
Impinger No. 3			
Condenser			
Desiccant		1366	
	1458	1452	6.0
Total			115.0

Integrated Gas Sampling Data:

Bag Pump No. B-13 Box No. 26 Bag No. 2
 Bag Material: 5-layer Aluminized Tedlar Size: 44 L
 Pretest leak check: .00 cc/min at 15 in. Hg.
 Time start: 1130 (HRS) Time end: 1336 (HRS)
 Sampling rate: 200 cc/min Operator: D.B.
 S/N of O₂ Analyzer used to monitor train outlet: 4

CF-023

S-0046RR

INTERFOLL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job USP SHERCO
 Source UNIT #3 SCRUBBER INLET
 Method 10/A Filter holder: —

Date 9-11-91 Test 2 Run 3
 No. of traverse points 12
 Filter type: N/A

Sample Train Leak Checks:

Pretest: { 0.02 cfm at 15 in. Hg. (vac)

Posttest: { .00 cfm at 8 in. Hg. (vac)

Particulate Catch Data:

No.s of filters used: Recovery solvent(s)

 ☐ acetone
 ☐ other(s)

No. of probe wash bottles:

Sample recovered by:

Condensate Data:

Item	Weight(g)		
	Final	Tare	Difference
Impinger No. 1		539	
Impinger No. 2	622	539	83
Impinger No. 3			
Condenser			
Desiccant		738	
	1495	1490	5.0
Total			88.0

Integrated Gas Sampling Data:

Bag Pump No. B13 Box No. 24 Bag No. 3

Bag Material: 5-layer Aluminized Tedlar Size: 44 L

Pretest leak check: .00 cc/min at 15 in. Hg.

Time start: 1430 (HRS) Time end: 1635 (HRS)

Sampling rate: 200 cc/min Operator: D.R.

S/N of O₂ Analyzer used to monitor train outlet: 4

CF-023

INTERPOL LABORATORIES EPA METHOD 3 FIELD DATA SHEET

Job U.S.P. SHERLO
 Source UNIT 3 SHERMAN STREET
 Date 9/11/91 1991

Operator D.B. + B.A.
 Motor Box No. 9
 Generator Serial 1001

Stack Probe
 Temp. 7.75 in UC
 Date 10/26

Pilot No. 29.04
 Bar. Press. 29.04
 Nozzle No. 7-2

Temp. 15
 Wind Speed 84
 Humidity 82
 Direction 163

Transfer Point No.	Sampling Time (min)	Sample Volume (cc)	Velocity Head (in UC)	Drifted Motor (in UC)	Dep. Vol. (cc)	VAC. in Hg	Temperature (°F)				Oxygen (cc/vol)
							Stack	Probe	Oven	Temp.	
B-1-1	1430	94.73									
	5	95.96	.55	.39	98.95	2.0	285			83	5.3
	10	97.80	.56	.39	99.78	2.0	283			81	5.1
	15	99.64	.57	.40	99.62	2.0	283			86	5.0
	20	101.49	.58	.41	101.48	2.0	284			86	4.9
	25	103.23	.52	.37	103.25	2.0	284			86	5.3
	30	104.97	.49	.35	104.96	2.0	282			87	5.0
	35	107.19	.84	.60	107.21	3.0	280			88	4.9
	40	109.48	.87	.62	109.51	3.0	280			89	5.1
	45	111.59	.74	.53	111.63	2.5	277			89	5.0
A-1-1	50	113.75	.75	.54	113.79	2.5	276			89	4.9
	55	115.93	.78	.56	115.96	2.5	272			89	5.1
	60	118.115	.77	.56	118.13	2.5	272			89	4.8
	5	120.17	.71	.50	120.20	2.0	283			88	5.2
	10	122.25	.70	.47	122.26	2.0	286			88	5.1
	15	124.37	.74	.52	124.37	2.0	284			89	5.1
	20	126.24	.57	.41	126.23	2.0	278			90	5.2
	25	128.11	.58	.41	128.11	2.0	279			89	5.0
	30	129.74	.55	.39	129.74	2.0	280			90	5.0
	35	131.35	.32	.23	131.34	2.0	278			90	5.0
S-1	40	133.25	.60	.43	133.26	2.0	277			88	5.0
	45	135.38	.75	.54	135.40	2.0	274			90	5.1
	50	137.51	.73	.53	137.52	2.0	273			90	4.9
	55	139.55	.66	.44	139.54	2.0	270			90	5.1
	60	141.36	.53	.38	141.35	2.0	268			90	5.1
	1635										
							Avg. = 85.9				
							V ₀ = 44.63				
							θ = 120				



A hand-drawn schematic diagram of a cross-section. It features a large circle with a smaller circle in the center. Four small squares are positioned around the perimeter of the large circle, labeled A, B, C, and D. A rectangular base is attached to the bottom of the large circle. The entire diagram is enclosed in a rectangular frame.

R or nothing= reg. manometer; S= expanded; E = electronic S-392.1

INTERPOLL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job NSP SHERCO Date 9/11/91 Test 2 Run 1
 Source Unit #3 Stack No. of traverse points 16
 Method 10LA Filter holder: none Filter type: NA

Sample Train Leak Check:

Pretest: (0.02 cfm at 15 in. Hg. (vac) ~~X~~
 Posttest: 0 cfm at 10 in. Hg. (vac) ~~X~~

Particulate Catch Data:

No.s of filters used: _____ Recovery solvent(s) _____

_____ ☐ acetone
 _____ ☒ other(s) KMNO₄ 6N HCL

No. of probe wash bottles: 1
 Sample recovered by: DUT

Condensate Data:

Item	Weight (g)		
	Final	Tare	Difference
Impinger No. 1			
Impinger No. 2	613	250	363
Impinger No. 3			
Condenser			
Desiccant	1525	1484	41
Total			404

Integrated Gas Sampling Data:

Bag Pump No. B12 Box No. 2 Bag No. 1
 Bag Material: 5-layer Aluminized Tedlar Size: 44 L
 Pretest leak check: 0 cc/min at 15 in. Hg.
 Time start: 0840 (HRS) Time end: 1054 (HRS)
 Sampling rate: 200 cc/min Operator: DUT
 S/N of O₂ Analyzer used to monitor train outlet: 11

CF-023

U.S.P. SHERCO

Job _____
Source _____
Date 9/10/11 8 AM L

Operator 2044 64
Meter Box No. 4
Counter Unit 1
1.053

Pilot No. 624-127
Ber. Price. 25.85
Noble No. 1-127

55

[illegible]

INTERFOLL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job N.S.P. Sherco
 Source Unit #3 Stack
 Method 10/A Filter holder: NA

Date 9/11/91 Test 2 Run 2
 No. of traverse points 16
 Filter type: NA

Sample Train Leak Check:

Pretest: (0.02 cfm at 15 in. Hg. (vac) ~~✓~~
 Posttest: 0 cfm at 7 in. Hg. (vac) ~~✓~~

Particulate Catch Data:

No.s of filters used: Recovery solvent(s)

☐ acetone
☒ other(s) KmNO₃ & 6 N HCl

No. of probe wash bottles: 1
 Sample recovered by: Duff

Condensate Data:

Item	Weight (g)		
	Final	Tare	Difference
Impinger No. 1		250	
Impinger No. 2	476		226
Impinger No. 3			
Condenser			
Desiccant	1441	1427	17
Total			243

Integrated Gas Sampling Data:

Bag Pump No. B₁₂ Box No. 2 Bag No. 2

Bag Material: 5-layer Aluminized Tedlar Size: 44 L

Pretest leak check: 0 cc/min at 14 in. Hg.

Time start: 1134 (HRS) Time end: 1346 (HRS)

Sampling rate: 200 cc/min Operator: Duff

S/N of O₂ Analyzer used to monitor train outlet: 11

CF-025

77

Shirley
57 ACK

[illegible]

INTERPOL LABORATORIES EPA METHOD 5/17 SAMPLE LOG SHEET

Job N.S.P. Sherco Date 9/11/91 Test 2 Run 3
 Source Unit #3 Stack No. of traverse points 16
 Method LOLA Filter holder: NA Filter type: NA

Sample Train Leak Check:

Pretest: (0.02 cfm at 15 in. Hg. (vac) ☒
 Posttest: 0 cfm at 7 in. Hg. (vac) ☒

Particulate Catch Data:

No.s of filters used: _____ Recovery solvent(s) _____

_____ ☐ acetone
☒ other(s) KMNO₄ & 6 N HCL

No. of probe wash bottles: _____
 Sample recovered by: _____

Condensate Data:

Item	Weight (g)		
	Final	Tare	Difference
Impinger No. 1			
Impinger No. 2	459	250	209
Impinger No. 3			
Condenser			
Desiccant	1507	1490	17
Total			226

Integrated Gas Sampling Data:

Bag Pump No. B12 Box No. 2 Bag No. 3
 Bag Material: 5-layer Aluminized Tedlar Size: 44 L
 Pretest leak check: 0 cc/min at 14 in. Hg.
 Time start: 1425 (HRS) Time end: 1632 (HRS)
 Sampling rate: 200 cc/min Operator: DWH
 S/N of O₂ Analyzer used to monitor train outlet: 11

CF-023

INTERPOL LABORATORIES EPA METHOD 5 FIELD DATA SHEET

JOB N2P SHERO

SOURCE 14112 STACK

DATE 9-11-91

OPERATORS

MOTOR BOX NO.

CORRELATOR SERIAL

VH CH

IN DE

NOZZLE NO.

PILOT NO.

BAR. PRESS.

NOZZLE DIA.

V-27-14 CP

84

Transfered Point No.	Sampling Time (min)	Sample Volume (cc)	Velocity Head (in H ₂ O)	Orifice Meter (in H ₂ O)	Dep. Vel. (ft)	VAC. in Hg	Temperature (°F)					Dewpoint (°F)	
							Stack	Probe	Dry	Wet	Coat/Dry		
4	1422	761.69	1.2	.94	3.89	2.5	172			51	79	77	7.3
4	4	763.19	1.1	.85	5.99	2.5	171				83	78	5.8
3	8	765.99	1.1	.86	8.11	2.0	170				83	78	5.7
3	12	768.11	1.1	.86	0.22	2.0	170			52	86	79	5.7
2	16	770.17	1.2	.94	2.43	2.5	171				89	80	5.7
2	20	772.43	1.2	.94	4.66	2.5	170				91	81	5.8
1	24	774.56	1.1	.86	6.79	2.5	170				92	82	5.5
1	28	776.79	1.05	.83	8.88	2.5	170				97	81	5.6
4	32	778.88	1.1	.86	1.01	2.5	170			52	92	83	5.7
4	36	781.01	1.05	.83	3.10	2.0	171				93	84	5.7
3	40	783.10	1.1	.87	5.24	2.0	170				94	84	5.7
3	44	785.19	1.1	.87	7.39	2.5	170				95	85	5.6
3	48	787.39	1.1	.87	9.54	2.0	170			51	95	85	5.6
2	52	789.45	1.1	.87	1.64	2.0	171				96	86	5.7
2	56	791.61	1.05	.83	3.69	2.0	170				97	87	5.6
1	60	793.65	1.0	.80	5.75	2.5	170				98	88	5.6
1	64	795.75	1.1	.88	7.91	2.0	170			51	97	88	5.5
4	68	797.91	1.1	.88	0.07	2.5	171				98	89	5.6
4	72	800.10	1.1	.88	2.24	3.0	171				99	89	5.6
3	76	802.24	1.1	.88	4.40	2.0	170				99	90	5.7
3	80	804.42	1.1	.88	6.67	2.0	170			52	99	90	5.6
2	84	806.58	1.2	.96	8.93	2.0	171				99	90	5.7
2	88	808.90	1.1	.88	1.00	2.0	171				99	90	5.7
1	92	810.99	1.1	.88	3.06		171				99	91	
1	96	813.01	1.0	.80									
VA =											Avg. =		

APPENDIX D

INTERPOLL LABORATORIES ANALYTICAL DATA

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Interpoll Laboratories
(612) 786-6020

EPA Method 3 Data Reporting Sheet
Orsat Analysis

Job NSP/Shecco
Team Leader DA
Date Submitted 9-11-91
Test No. 1
Date of Analysis 9-11-91

Source Scrubber Inlet
Test Site Modules
Date of Test 9-11-91
No. of Runs Completed 3
Technician R. G. G.

Test/ Run	Sample Log Number and Type	No. of An.	Buret Readings (ml)			Conc. CO ₂ %v/v Dry	Conc. O ₂ %v/v Dry	F _o
			Zero Pt.	After CO ₂	After O ₂			
1/1	4201-13 B B F	1	0.00	10.30	19.70	10.30	9.40	1.12
		2	0.00	10.30	19.70	10.30	9.40	1.12
		Avg				10.30	9.40	
1/2	-14 B B F	1	0.00	11.30	19.50	11.30	8.20	1.12
		2	0.00	11.30	19.50	11.30	8.20	1.12
		Avg				11.30	8.20	
1/3	-15 B B F	1	0.00	11.70	19.50	11.70	7.80	1.12
		2	0.00	11.70	19.50	11.70	7.80	1.12
		Avg				11.70	7.80	
	B B F	1						
		2						
		Avg						
	B B F	1						
		2						
		Avg						
	B B F	1						
		2						
		Avg						
	B B F	1						
		2						
		Avg						
	B B F	1						
		2						
		Avg						
	B B F	1						
		2						
		Avg						

- ☒ Ambient Air QA Check
☒ Orsat Analyzer System Leak Check
☒ F_o Within EPA M-3 Guidelines
for fuel type.

Where $F_o = \frac{20.9 - O_2}{CO_2}$

EPA Method 3 Guidelines	
Fuel Type	F _o Range
Coal:	
Anthracite/Lignite	1.016-1.130
Bituminous	1.083-1.250
Oil:	
Distillate	1.260-1.413
Residual	1.210-1.370
Gas:	
Natural	1.600-1.936
Propane	1.434-1.586
Butane	1.405-1.553
Head/loss	1.000-1.170

F=Flask (250 cc all glass)
RETAINED BY EPA (5-1-1992)

EPA Method 3 Data Reporting Sheet
Orsat Analysis

Job NSP/Sharco
Team Leader DVT
Date Submitted 9-11-91
Test No. 1
Date of Analysis 9-11-91

Source Units 1&2
Test Site Stack
Date of Test 9-10-91
No. of Runs Completed 3
Technician A. G. G. G.

Test/ Run	Sample Log Number and Type	No. of An.	Buret Readings (ml)			Conc. CO ₂ %v/v Dry	Conc. O ₂ %v/v Dry	F _o
			Zero Pt.	After CO ₂	After O ₂			
1/1	4201-24 B B F	1	0.00	12.20	19.40	12.20	7.20	1.12
		2	0.00	12.20	19.40	12.20	7.20	1.12
		Avg				12.20	7.20	
1/2	-25 B B F	1	0.00	12.40	19.50	12.40	7.10	1.11
		2	0.00	12.40	19.50	12.40	7.10	1.11
		Avg				12.40	7.10	
1/3	-26 B B F	1	0.00	12.40	19.50	12.40	7.10	1.11
		2	0.00	12.40	19.50	12.40	7.10	1.11
		Avg				12.40	7.10	
	B B F	1						
		2						
		Avg						
	B B F	1						
		2						
		Avg						
	B B F	1						
		2						
		Avg						
	B B F	1						
		2						
		Avg						
	B B F	1						
		2						
		Avg						
	B B F	1						
		2						
		Avg						

- ☒ Ambient Air QA Check
☐ Orsat Analyzer System Leak Check
☒ F_o Within EPA M-3 Guidelines
for fuel type.

Where $F_o = \frac{20.9 - O_2}{CO_2}$

F=Flask (250 cc all glass)
B=Tedlar Bag (5-layer)

EPA Method 3 Guidelines	
Fuel Type	F _o Range
Coal:	
Anthracite/Lignite	1.016-1.130
Bituminous	1.083-1.250
Oil:	
Distillate	1.260-1.413
Residual	1.210-1.370
Gas:	
Natural	1.600-1.836
Propane	1.434-1.596
Butane	1.405-1.553
Wood/Wood Bark	1.000-1.150

Interpoll Laboratories
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EPA Method 3 Data Reporting Sheet
Orsat Analysis

Job NSP/Sherco
Team Leader OB
Date Submitted 9-12-91
Test No. 1
Date of Analysis 9-12-91

Source Unit #3
Test Site Scrubber Inlet
Date of Test 9-11-91
No. of Runs Completed 1
Technician R. Gibson

Test/ Run	Sample Log Number and Type	No. of An.	Buret Readings (ml)			Conc. CO ₂ %v/v Dry	Conc. O ₂ %v/v Dry	F ₀
			Zero Pt.	After CO ₂	After O ₂			
2/1	4201-37 ☒ B ☐ F	1	0.00	12.60	19.30	12.60	6.70	1.13
		2	0.00	12.60	19.30	12.60	6.70	1.13
		Avg				12.60	6.70	
2/2	-38 ☒ B ☐ F	1	0.00	13.60	19.20	13.60	5.60	1.13
		2	0.00	13.60	19.20	13.60	5.60	1.13
		Avg				13.60	5.60	
2/3	-39 ☒ B ☐ F	1	0.00	12.40	19.40	12.40	7.00	1.12
		2	0.00	12.40	19.40	12.40	7.00	1.12
		Avg				12.40	7.00	
	☐ B ☐ F	1						
		2						
		Avg						
	☐ B ☐ F	1						
		2						
		Avg						
	☐ B ☐ F	1						
		2						
		Avg						
	☐ B ☐ F	1						
		2						
		Avg						
	☐ B ☐ F	1						
		2						
		Avg						
	☐ B ☐ F	1						
		2						
		Avg						

- ☒ Ambient Air QA Check
☒ Orsat Analyzer System Leak Check
☒ F₀ Within EPA M-3 Guidelines
for fuel type.

Where $F_0 = \frac{20.9 - O_2}{CO_2}$

EPA Method 3 Guidelines	
Fuel Type	F ₀ Range
Coal:	
Anthracite/Lignite	1.016-1.130
Bituminous	1.083-1.250
Oil:	
Distillate	1.260-1.413
Residual	1.210-1.370
Gas:	
Natural	1.600-1.936
Propane	1.434-1.596
Butane	1.405-1.557

EPA Method 3 Data Reporting Sheet
Orsat Analysis

Job NSP/Shecco
Team Leader DUH
Date Submitted 9-12-91
Test No. 2
Date of Analysis 9-12-91

Source Unit #3
Test Site Stack
Date of Test 9-11-91
No. of Runs Completed 3
Technician LC/Don

Test/ Run	Sample Log Number and Type	No. of An.	Buret Readings (ml)			Conc. CO ₂	Conc. O ₂	F _o
			Zero Pt.	After CO ₂	After O ₂	%v/v Dry	%v/v Dry	
2/1	4201-49 ☒ B ☐ F	1	0.00	13.00	19.30	13.00	6.30	1.12
		2	0.00	13.00	19.30	13.00	6.30	1.12
		Avg				13.00	6.30	
2/2	-50 ☒ B ☐ F	1	0.00	13.10	19.30	13.10	6.20	1.12
		2	0.00	13.10	19.30	13.10	6.20	1.12
		Avg				13.10	6.20	
2/3	-51 ☒ B ☐ F	1	0.00	13.30	19.30	13.30	6.00	1.12
		2	0.00	13.30	19.30	13.30	6.00	1.12
		Avg				13.30	6.00	
	☐ B ☐ F	1						
		2						
		Avg						
	☐ B ☐ F	1						
		2						
		Avg						
	☐ B ☐ F	1						
		2						
		Avg						
	☐ B ☐ F	1						
		2						
		Avg						
	☐ B ☐ F	1						
		2						
		Avg						
	☐ B ☐ F	1						
		2						
		Avg						

- ☒ Ambient Air QA Check
☒ Orsat Analyzer System Leak Check
☐ F_o Within EPA M-3 Guidelines
for fuel type.

Where $F_o = \frac{20.9 - O_2}{CO_2}$

F=Flask (250 cc all glass)
B=Tedlar Bag (5-layer)

EPA Method 3 Guidelines	
Fuel Type	F _o Range
Coal:	
Anthracite/Lignite	1.016-1.150
Bituminous	1.083-1.250
Oil:	
Distillate	1.260-1.415
Residual	1.210-1.370
Gas:	
Natural	1.600-1.856
Propane	1.434-1.586
Butane	1.405-1.553
Wood/Wood Bark	1.000-1.100

INTERPOLL LABORATORIES, INC.
(612)786-6020

NSP/Sherco
Laboratory Log No. 4201

Results of Mercury Analysis

Test: 1
Source: Units 1 & 2 Scrubber Inlet
Sample Type: Method 101A Sampling Train

		Total Mass in Sample (ug)			
		Field			
Method		Blank	Run 1	Run 2	Run 3
(Log No.)		(4201-09)	(4201-10)	(4201-11)	(4201-12)
Mercury	SW-846, 7470	< 0.1	14.5	22.1	17.2

Test: 1
Source: Units 1 & 2 Stack
Sample Type: Method 101A Sampling Train

		Total Mass in Sample (ug)			
		Field			
Method		Blank	Run 1	Run 2	Run 3
(Log No.)		(4201-27)	(4201-28)	(4201-29)	(4201-30)
Mercury	SW-846, 7470	1.34	10.4	6.79	20.7

INTERPOLL LABORATORIES, INC.
(612)786-6020

NSP/Sherco
Laboratory Log No. 4201

Results of Mercury Analysis

Test: 2
Source: Unit 3 Scrubber Inlet
Sample Type: Method 101A Sampling Train

		Total Mass in Sample (ug)		
Method		Run 1	Run 2	Run 3
(Log No.)		(4201-40)	(4201-41)	(4201-42)
Mercury	SW-846, 7470	25.2	18.6	17.6

Test: 2
Source: Unit 3 Stack
Sample Type: Method 101A Sampling Train

		Total Mass in Sample (ug)		
Method		Run 1	Run 2	Run 3
(Log No.)		(4201-52)	(4201-53)	(4201-54)
Mercury	SW-846, 7470	18.9	12.5	12.8

Interpoll Laboratories
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Chain of Custody
Sample Deposition Sheet

Job N.S.P. SHERCO Source SCRUBBLE INLETS
Team Leader D. BRENNAN Test Site MOBILE (101-104)(107-201)(204-207)
Date Submitted 9/10/91 Date of Test 9/10/91
Test No. #1 2WS (1-3) No. of Runs Completed 3

No. of Samples	Type of Sample	Analysis Required	Comments
4	Probe Wash: ☐ Acetone ☐ D.I. Water	☐ As per EPA M-5 ☐ Other _____	
	Filter: ☐ 4" G.F. ☐ S.S. Thimble ☐ 2.5" G.F. ☐ 47 mm G.F.	☐ As per EPA M-5 ☐ As per EPA M-17 ☐ Other _____	
4 ² / ₃ (1) + 6 RINSES + 1 BLANK	Impinger Catch: ☐ D.I. Water ^{10/20} ☐ 3% H ₂ O ₂ ^{H₂SO₄} ☐ 4MS Hg Only + ☐ 4MS Metals (148) ☐ 1.0 N NaOH ☒ Other <u>KMNO₄</u>	☐ MN Protocol ☐ W1 Protocol ☐ EPA M-6 or 8 ☐ Acid Gases ☐ Formaldehyde ☐ Metals ☒ Other <u>MERCURY</u>	<u>IMPINGER + RINSE</u> <u>RULE FOR EACH</u> <u>RUN</u>
3	Integrated Gas sample	☒ As per EPA M-3 ☐ As per EPA M-10 ☐ Other _____	
	Oxides of Nitrogen (NO _x)	☐ As per EPA M-7A ☐ Other _____	Date _____ Time (HRS) _____
	☐ Fuel Sample ☐ Aggregate	☐ Attached fuel Form #S-0167RRR	
	Particle Size	☐ X-Ray Sedigraph ☐ Bahco Method ☐ Other _____	
	Audit Samples ☐ Sulfur Dioxide ☐ Oxides of Nit. ☐ Other _____	☐ As per EPA M-6 ☐ As per EPA M-7A ☐ Other _____	

Source Information

- 1) Type of Source: ☒ Boiler ☐ Asphalt Plant ☐ Incinerator ☐ Dryer
☐ Other _____
- 2) Fuel: ☒ Coal ☐ Wood ☐ Gas ☐ Oil ☐ RDF ☐ Other _____
- 3) Is sample combustible? ☒ No ☐ Yes
- 4) Does sample need special handling? ☒ No ☐ Yes If yes, explain _____

Interpoll Laboratories
(612) 796-6020

Chain of Custody
Sample Deposition Sheet

Job NSP SHERCO Source Units 1 & 2
Team Leader DWA Test Site Stack
Date Submitted 9/10/91 Date of Test 9/10/91
Test No. 1 No. of Runs Completed 3

No. of Samples	Type of Sample	Analysis Required	Comments
4	Probe Wash: ☐ Acetone ☐ D.I. Water	☐ As per EPA M-5 ☒ Other <u>KMNO₄ & 6N HCL RINSE</u>	
	Filter: ☐ 4" G.F. ☐ S.S. Thimble ☐ 2.5" G.F. ☐ 47 mm G.F.	☐ As per EPA M-5 ☐ As per EPA M-17 ☐ Other _____	
4	Impinger Catch: ☐ D.I. Water ☐ 3% H ₂ O ₂ ☒ 4MS Hg Only ☐ 4MS Metals ☐ 1.0 N NaOH ☐ Other _____	☐ MN Protocol ☐ WI Protocol ☐ EPA M-6 or 8 ☐ Acid Gases ☐ Formaldehyde ☐ Metals ☒ Other <u>Hg Method</u>	<u>TOT A</u>
3	Integrated Gas sample	☒ As per EPA M-3 ☐ As per EPA M-10 ☐ Other _____	
	Oxides of Nitrogen (NO _x)	☐ As per EPA M-7A ☐ Other _____	Date _____ Time (HRS) _____
	☐ Fuel Sample ☐ Aggregate	☐ Attached fuel Form #S-0163RRR	
	Particle Size	☐ X-Ray Sedigraph ☐ Bahco Method ☐ Other _____	
	Audit Samples ☐ Sulfur Dioxide ☐ Oxides of Nit. ☐ Other _____	☐ As per EPA M-6 ☐ As per EPA M-7A ☐ Other _____	

Source Information

- 1) Type of Source: ☒ Boiler ☐ Asphalt Plant ☐ Incinerator ☐ Dryer
☐ Other _____
- 2) Fuel: ☒ Coal ☐ Wood ☐ Gas ☐ Oil ☐ RDF ☐ Other _____
- 3) Is sample combustible? ☒ No ☐ Yes
- 4) Does sample need special handling? ☒ No ☐ Yes If yes, explain _____

S-279RRRR

Interpoll Laboratories
(612) 796-6020

Chain of Custody
Sample Deposition Sheet

Job N.S.P. SHERRO Source UNIT #3 SCRUBBER TALET
Team Leader D. BRENNAN Test Site SCRUBBER IN
Date Submitted 9/11/91 Date of Test 9/11/91
Test No. 2 (RUNS 1-3) No. of Runs Completed 3

No. of Samples	Type of Sample	Analysis Required	Comments
3	Probe Wash: <u>16.5% H₂O₂</u> ☐ Acetone <u>rinse</u> ☐ D.I. Water	☐ As per EPA M-5 ☒ Other <u>MERCURY</u>	
0	Filter: ☐ 4" G.F. ☐ S.S. Thimble ☐ 2.5" G.F. ☐ 47 mm G.F.	☐ As per EPA M-5 ☐ As per EPA M-17 ☐ Other	
3	Impinger Catch: ☐ D.I. Water ☐ 3% H ₂ O ₂ ☐ 4MS Hg Only ☐ 4MS Metals ☐ 1.0 N NaOH ☒ Other <u>KMNO₄ (4%)</u> <u>(10% H₂SO₄)</u>	☐ MN Protocol ☐ WI Protocol ☐ EPA M-6 or 8 ☐ Acid Gases ☐ Formaldehyde ☐ Metals ☒ Other <u>MERCURY</u>	
3	Integrated Gas sample	☒ As per EPA M-3 ☐ As per EPA M-10 ☐ Other	
—	Oxides of Nitrogen (NO _x)	☐ As per EPA M-7A ☐ Other	Date _____ Time (HRS) _____
—	☐ Fuel Sample ☐ Aggregate	☐ Attached fuel Form #S-0163RRR	
—	Particle Size	☐ X-Ray Sedigraph ☐ Bahco Method ☐ Other	
—	Audit Samples ☐ Sulfur Dioxide ☐ Oxides of Nit. ☐ Other	☐ As per EPA M-6 ☐ As per EPA M-7A ☐ Other	

Source Information

- 1) Type of Source: ☒ Boiler ☐ Asphalt Plant ☐ Incinerator ☐ Dryer
☐ Other
- 2) Fuel: ☒ Coal ☐ Wood ☐ Gas ☐ Oil ☐ RDF ☐ Other
- 3) Is sample combustible? ☒ No ☐ Yes
- 4) Does sample need special handling? ☒ No ☐ Yes If yes, explain

Interpoll Laboratories
(612) 786-6020

Chain of Custody
Sample Deposition Sheet

Job N.S.P. SHERLO Source Unit #3
Team Leader DH Test Site Stack
Date Submitted 9/11/91 Date of Test 9/11/91
Test No. 2 No. of Runs Completed 3

No. of Samples	Type of Sample	Analysis Required	Comments
3	Probe Wash: ☐ Acetone ☐ D.I. Water	☐ As per EPA M-5 ☒ Other <u>Hg</u>	
	Filter: ☐ 4" G.F. ☐ S.S. Thimble ☐ 2.5" G.F. ☐ 47 mm G.F.	☐ As per EPA M-5 ☐ As per EPA M-17 ☐ Other _____	
3	Impinger Catch: ☐ D.I. Water ☐ 3% H ₂ O ₂ ☐ 4MS Hg Only ☒ 4MS Metals ☐ 1.0 N NaOH ☐ Other _____	☐ MN Protocol ☐ WI Protocol ☐ EPA M-6 or 8 ☐ Acid Gases ☐ Formaldehyde ☐ Metals ☒ Other <u>Hg 10/a</u>	
3	Integrated Gas sample	☒ As per EPA M-3 ☐ As per EPA M-10 ☐ Other _____	
	Oxides of Nitrogen (NO _x)	☐ As per EPA M-7A ☐ Other _____	Date _____ Time (HRS) _____
2	☒ Fuel Sample ☐ Aggregate	☐ Attached fuel Form #S-0153RRR	<u>Mercury</u> <u>ASTM D 3684</u>
	Particle Size	☐ X-Ray Sedigraph ☐ Bahco Method ☐ Other _____	<u>As per proposal</u>
	Audit Samples ☐ Sulfur Dioxide ☐ Oxides of Nit. ☐ Other _____	☐ As per EPA M-6 ☐ As per EPA M-7A ☐ Other _____	

Source Information

- 1) Type of Source: ☒ Boiler ☐ Asphalt Plant ☐ Incinerator ☐ Dryer
☐ Other _____
- 2) Fuel: ☒ Coal ☐ Wood ☐ Gas ☐ Oil ☐ RDF ☐ Other _____
- 3) Is sample combustible? ☒ No ☐ Yes
- 4) Does sample need special handling? ☒ No ☐ Yes If yes, explain _____

S-278RRRR

APPENDIX E

UNITS 1,2 & 3 TREND LOGS

1030.30	*****	10	34.7	29.19	5495	-43.99L	1966.9	2427	386.3	92.7	378	3.26
1035.30	*****	10	35.7	29.19	5422	-42.00	968.4	2422	394.3	90.6	370	3.22
1040.30	*****	10	35.4	29.19	5433	-42.90	973.8	2437	394.2	90.5	377	3.37
1045.30	*****	10	35.1	29.19	5440	-44.25L	970.6	2426	384.4	86.3	379	3.27
1050.30	*****	10	35.8	29.19	5480	-43.39	973.5	2431	379.9	85.4	380	3.28
1055.30	*****	10	35.7	29.20	5377	-42.48	972.9	2427	382.3	85.4	372	3.08
1100.30	*****	10	35.7	29.20	5377	-43.46	975.2	2437	380.4	90.4	379	3.28
1105.30	*****	10	35.8	29.19	5474	-44.20L	971.1	2431	380.4	90.4	379	3.17
1110.30	*****	10	36.5	29.20	5494	-44.06L	973.1	2430	397.4	95.5	381	3.25
1115.30	*****	10	35.6	29.20	5390	-42.69	973.2	2432	BA703	BA705	FC340	BA706
1115.30 10/SE/91 SHERCO UNIT #1 TREND LOG # 33 CAT SCRUBBER TEST SPECIAL LOG												
1115.30	*****	10	35.5	29.20	5415	-43.27	972.9	2432	406.6	92.0	378	3.25
1120.30	*****	10	36.0	29.20	5452	-43.95	970.0	2424	406.6	92.0	382	3.23

TIME 11:28:00 DATE 23/AU/91

ERROR NUMBER= 304; SET TIME

REGISTER CONTENTS

L=718B T=50A0 X=0008 B=744A E=0003 A=0000

1125.30 10/SE/91 SHERCO UNIT #1 TREND LOG # 33

CAT SCRUBBER TEST SPECIAL LOG

GE704	BP704	SC702	BP701	BP703	BT889	SF702	MC346	MC307	BA704	BA703	BA705	FC340	BA706
BC302	SC302	SC302	BP701	BP703	BT889	SF702	MC346	MC307	BA704	BA703	BA705	FC340	BA706
1125.30	686.5	2663	652.1	-22.21	183.4	4510	356.3	2430	112.6	405.3	96.3	377	3.13
1130.30	690.6	2663	651.2	-21.75	183.6	4546	367.6	2429	108.8	412.0	88.2	381	3.28
1135.30	688.4	2664	652.8	-21.73	183.3	4513	385.1	2432	108.9	414.3	88.1	376	3.10
1140.30	695.4	2667	650.6	-22.10	183.4	4534	373.6	2433	123.8	424.2	103.9	379	3.32
1145.30	682.6	2655	652.6	-21.86	183.0	4477	373.7	2425	123.8	424.2	103.8	384	3.25
1150.30	692.6	2669	652.6	-21.35	183.4	4561	384.8	2437	118.1	437.8	98.6	382	3.19
1155.30	683.2	2657	652.1	-22.00	183.0	4482	372.8	2425	123.3	414.7	105.6	388	3.21
1200.30	692.4	2670	652.5	-21.78	183.3	4559	372.6	2436	123.3	414.8	105.6	384	3.24
1205.30	686.1	2660	652.4	-21.38	182.9	4506	394.4	2429	124.7	421.2	102.8	385	3.08
1210.30	692.1	2668	652.2	-22.49	183.1	4567	386.0	2434	124.6	436.3	107.0	381	3.21
1215.30	680.1	2653	652.9	-21.69	183.0	4463	386.9	2424	124.8	431.9	107.0	393	3.28
1220.30	686.4	2655	652.1	-21.64	183.2	4539	401.3	2423	122.2	430.9	107.7	394	3.34
1225.30	691.5	2674	654.6	-22.29	183.4	4549	401.5	2441	122.3	430.8	108.3	383	3.07
1230.30	680.5	2648	648.0	-22.34	183.6	4466	394.8	2421	124.1	449.1	111.0	399	3.36
1235.30	700.4	2680	653.0	-22.01	183.4	4606	393.6	2441	126.3	448.7	108.9	378	3.12
1240.30	686.9	2657	647.5	-22.31	183.3	4505	393.3	2424	126.2	448.8	108.9	387	3.18
1245.30	690.4	2669	650.8	-21.57	182.9	4550	379.2	2435	122.5	422.8	106.1	384	3.25
1250.30	683.4	2654	649.9	-21.87	183.3	4489	392.8	2422	126.1	424.3	103.9	391	3.30
1255.30	687.6	2664	652.2	-21.89	183.2	4535	387.3	2431	126.2	419.8	103.9	389	3.32
1300.30	692.3	2669	651.9	-21.77	183.4	4562	402.5	2436	130.9	461.4	113.1	382	3.15
1305.30	682.4	12652	680.9	-21.97	183.2	4490	402.6	2421	131.1	461.4	113.0	390	3.26

[illegible]

1525.30	12678	649.1	22.36	183.8	4562	446.3	133.9	470.3	119.2	379	3.14
1530.30	10	39.0	29.15	5440	-45.04L	959.6	2439				
1535.30	2666	646.8	-22.53	184.1	4508	419.4	124.3	442.1	108.1	387	3.16
1540.30	10	37.2	29.15	5476	-45.14L	951.1	2424				
1545.30	2663	646.0	-22.66	183.6	4524	422.4	124.4	438.1	108.2	384	3.23
1550.30	10	37.6	29.15	5510	-45.40L	955.9	2430				
1555.30	2666	646.9	-22.54	183.9	4520	414.8	128.4	482.1	111.4	382	3.18
1560.30	10	38.4	29.15	5461	-45.33L	952.6	2432				
1565.30	2666	647.4	-22.13	183.4	4532	414.8	128.5	482.1	105.6	383	3.23
1570.30	10	38.0	29.15	5440	-44.87L	951.8	2432				
1575.30	2667	643.1	-22.59	183.9	4518	418.2	121.5	480.7	107.6	380	3.19
1580.30	10	37.7	29.13	5493	-45.37L	952.9	2432				
1585.30	2663	640.1	-22.54	183.4	4522	397.5	123.5	422.4	112.2	384	3.31
1590.30	10	39.2	29.15	5476	-45.51L	949.2	2429				
1595.30	2677	643.5	-21.92	183.3	4573	397.3	123.4	422.4	112.3	374	3.25
1600.30	10	38.3	29.13	5425	-44.06L	954.8	2440				
1605.30	2653	643.8	-21.89	182.9	4466	390.5	117.8	435.1	102.6	384	3.27
1610.30	10	38.3	29.15	5467	-44.30L	953.8	2421				
1615.30	2669	645.2	-21.44	183.2	4531	404.3	129.1	442.4	115.5	377	3.19
1620.30	10	37.5	29.13	5447	-43.36	960.1	2435				
1625.30	2659	645.6	-22.05	183.1	4526	411.4	129.2	441.9	115.5	379	3.27
1630.30	10	37.8	29.13	5472	-44.30L	958.3	2425				
1635.30	2662	646.5	-21.39	183.6	4522	413.9	123.1	456.3	103.7	379	3.16
1640.30	10	37.5	29.13	5372	-43.35	962.2	2429				
1645.30	2668	646.9	-21.73	183.3	4526	414.1	123.2	456.3	104.3	378	3.28
1650.30	10	37.5	29.13	5425	-43.79	960.4	2436				

0820.18	302	695.8	10	38.0	29.15	185.0	455.6	379.2	72.3	418.6	95.1	387	3.20
0820.18	360	695.8	10	37.7	29.15	185.3	456.0	382.4	74.5	427.5	96.4	386	3.32
0825.18	341	694.1	10	37.5	29.15	185.4	457.5	379.8	77.0	421.8	96.5	386	3.17
0830.18	353	698.8	10	35.9	29.16	185.3	458.7	379.9	77.0	421.9	96.5	386	3.33
0835.18	10/SE/91 SHERCO UNIT #2 TREND LOG # 33	GE704	BP704	BP704	BP704	BP704	BP704	BP704	BP704	BP704	BP704	BP704	BP704
0835.18	354	696.0	10	36.1	29.15	184.4	456.7	386.9	79.8	416.9	107.4	386	3.29
0840.18	379	695.5	10	36.2	29.07	185.1	458.9	366.0	88.9	414.3	102.7	385	3.21
0845.18	411	695.3	10	36.6	29.18	181.6	456.1	366.0	88.9	414.3	102.8	388	3.18
0850.18	397	694.7	10	36.3	29.16	185.3	456.7	366.9	84.2	394.3	103.4	388	3.23
0855.18	381	696.6	10	36.2	29.16	184.2	456.3	364.7	83.7	394.4	105.4	337	3.21
0900.18	359	695.2	10	35.8	29.16	185.4	456.4	362.1	84.8	384.7	105.2	376	3.24
0905.18	374	696.2	10	36.2	29.16	184.9	455.4	353.4	81.3	394.4	103.8	389	3.19
0910.18	390	694.2	10	35.8	29.16	184.6	457.0	353.4	81.3	394.3	103.8	380	3.24
0915.18	354	691.5	10	35.9	29.16	185.2	454.3	354.4	80.5	382.3	96.1	387	3.22
0920.18	390	692.0	10	36.0	29.16	185.7	457.2	339.0	80.8	381.5	102.7	385	3.27
0925.18	370	696.6	10	35.8	29.16	185.1	456.2	339.0	80.8	381.5	102.7	387	3.16
0930.18	356	696.8	10	35.6	29.16	185.4	456.3	349.3	82.6	377.6	94.5	383	3.21
0935.18	375	691.7	10	36.2	29.16	185.4	457.8	350.8	82.6	376.9	100.0	383	3.24
0940.18	368	694.9	10	36.2	29.16	185.3	459.7	350.5	83.3	360.7	101.4	390	3.19
0945.18	378	696.0	10	36.3	29.16	181.6	457.8	346.4	81.6	385.9	99.6	383	3.38
0950.18	338	695.9	10	35.7	29.16	185.1	456.1	346.3	81.6	385.8	99.6	379	3.06
0955.18	10/SE/91 SHERCO UNIT #2 TREND LOG # 33	GE704	BP704	BP704	BP704	BP704	BP704	BP704	BP704	BP704	BP704	BP704	BP704
0955.18	375	695.6	10	35.6	29.16	185.2	457.2	348.1	85.8	379.9	106.8	389	3.25
1000.18	379	695.4	10	36.0	29.16	184.6	456.7	366.6	93.3	401.8	108.5	387	3.22
1005.18	379	695.9	10	36.0	29.16	184.6	456.7	366.6	93.3	401.8	108.5	387	3.22
1010.18	379	695.7	10	36.0	29.16	184.6	456.7	366.6	93.3	401.8	108.5	387	3.22

1030.18	346	10	34.9	29.18	-43.84L	185.6	4567	364.9	94.3	403.4	108.6	383	3.17																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
1035.18	359	10	35.8	29.18	-44.06L	185.0	4590	364.9	94.3	403.4	108.6	385	3.26																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
1040.18	381	10	35.6	29.18	-43.08	185.0	4559	356.8	95.6	401.8	111.0	385	3.19																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
1045.18	359	10	35.3	29.18	-43.73	185.0	4574	370.6	97.3	413.8	109.6	389	3.24																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
1050.18	354	10	36.0	29.18	-43.32	184.7	4573	370.6	97.3	413.9	109.7	384	3.28																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
1055.18	327	10	35.9	29.18	-43.77	185.8	4563	369.7	103.5	407.4	114.3	383	3.20																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
1100.18	350	10	35.8	29.18	-43.70	184.7	4580	384.7	99.2	414.7	108.3	385	3.20																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
1105.18	366	10	36.0	29.18	-43.42	185.5	4568	388.0	102.5	410.1	108.4	386	3.26																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
1110.18	347	10	36.6	29.18	-44.42L	185.4	4573	387.9	99.6	419.8	113.6	383	3.26																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																						
1115.18	372	10	35.8	29.18	-44.14L	CAT SCRUBBER TEST SPECIAL LOG								BA703	BA705	FC340	BA706																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
1115.18	10/SE/91 SHERCO UNIT #2 TREND LOG # 33	GE704	BP704	BP703	BP701	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702	BP702

1240.18	332	10	36.0	29.18	-43.49	414.9	114.8	462.6	129.3	395	3.22
	695.6	2682	660.2	-24.34L	185.0	4561					
1245.18	407	10	36.2	29.17	-43.27	454.4	117.5	460.4	131.3	386	3.18
	695.9	2689	659.7	-25.10L	185.7	4566					
1250.18	362	10	37.1	29.17	-44.18L	454.4	117.5	460.4	131.3	389	3.19
	696.3	2687	656.8	-24.81L	185.1	4561					
1255.18	388	10	36.5	29.16	-44.12L	449.4	117.7	464.6	134.1	387	3.12
	698.0	2684	656.8	-24.49L	185.4	4567					
1300.18	399	10	35.2	29.16	-45.00L	441.1	120.5	502.8	139.7	388	3.26
	697.3	2683	657.2	-24.86L	185.3	4563					
1305.18	380	10	35.2	29.16	-45.47L	437.6	116.0	507.5	132.0	392	3.21
	696.4	2682	655.2	-24.07L	185.3	4567					
1310.18	402	10	35.5	29.16	-43.92L	449.6	110.3	478.2	126.3	388	3.22
	695.6	2683	655.4	-23.89L	185.7	4560					
1315.18	390	10	35.1	29.16	-44.20L	449.6	110.3	478.2	128.3	384	3.25
	696.4	2686	654.9	-23.86	186.0	4569					
1320.18	439	10	34.6	29.16	-43.49	450.9	119.1	479.6	136.8	388	3.19
	694.8	2682	654.9	-23.66	185.0	4557					
1325.18	447	10	34.8	29.15	-43.27	440.2	113.6	470.7	127.7	394	3.25
	691.9	2673	654.9	-23.77	186.3	4541					
1330.18	422	10	34.7	29.15	-43.39	440.3	113.6	470.7	127.6	390	3.27
	697.5	2688	656.3	-23.61	185.6	4570					
1335.18	428	10	34.8	29.15	-43.08	433.9	120.4	484.4	128.2	392	3.14
	692.3	2676	655.2	-23.93	184.7	4543					
1340.18	407	10	36.0	29.15	-42.79	451.3	125.8	492.9	136.4	389	3.27
	696.4	2687	656.7	-23.68	185.6	4575					
1345.18	441	10	35.9	29.14	-42.43	447.9	122.2	490.3	137.8	384	3.12
	692.8	2682	656.4	-23.88	185.3	4562					
1350.18	371	10	36.3	29.15	-43.21	440.4	123.6	489.1	131.6	387	3.26
	696.9	2688	656.9	-23.68	184.8	4577					
1355.18	413	10	36.1	29.15	-42.67						
	692.8	2681	657.6	-23.70L	184.7	4552	140.2	489.1	131.7	387	3.16
1400.18	417	10	36.3	29.15	-42.82	442.7	118.2	477.7	131.7	393	3.22
	695.3	2681	657.4	-23.53	185.6	4569					
1405.18	464	10	36.3	29.15	-42.81	453.6	129.1	938.1	140.1	395	3.23
	693.9	2676	658.1	-23.72L	184.6	4550					
1410.18	439	10	37.9	29.13	-42.50	453.7	129.1	938.0	140.0	383	3.23
	695.4	2689	658.9	-24.15L	185.3	4563					
1415.18	425	10	37.2	29.15	-43.54	456.3	120.6	960.3	133.2	392	3.22
	694.4	2677	657.7	-23.87L	184.8	4553					
1420.18	410	10	36.8	29.14	-43.18	456.2	124.7	485.4	138.8	384	3.23
	696.1	2685	659.8	-24.18L	185.7	4564					
1425.18	401	10	36.3	29.13	-43.54	447.1	122.4	477.7	136.6	389	3.20
	694.7	2679	658.1	-24.09L	185.3	4560					
1430.18	436	10	36.4	29.15	-43.46	464.8	123.8	498.2	142.0	385	3.27
	695.4	2688	660.6	-24.15L	185.3	4566					
1435.18	420	10	36.4	29.14	-43.51	464.7	123.8	498.2	142.0	390	3.19
	695.3	2676	658.6	-24.32L	185.6	4556					
1440.18	419	10	37.2	29.15	-43.04	424.8	124.6	479.2	138.0	390	3.25
	696.4	2679	660.1	-24.17L	185.4	4558					
1445.18	386	10	37.1	29.14	-43.33	459.1	128.4	481.4	142.3	387	3.18
	696.4	2678	660.4	-24.35L	184.7	4566					

CAT SCRUBBER TEST SPECIAL LOG

10/SE/91 SHERCO UNIT #2 TREND LOG # 33

BT889 SF702 BA702 BA703 BA705

GE704 BF704 BT892 BF703

FC340

BA706

FC340

BA706

1500.18	390	2676	660.6	-24.34L	184.6	4867	442.9	120.9	471.9	136.9	390	3.19
1505.18	424	10	37.2	29.13	-43.24	185.0	4854	449.4	472.5	135.1	387	3.25
1510.18	386	10	37.9	29.12	-43.46	185.6	4864	427.7	474.3	133.2	394	3.22
1515.18	421	10	37.0	29.13	-43.54	185.6	4866	427.6	474.3	133.3	391	3.31
1515.18	10/SE/91 SHERCO UNIT #2 TREND LOG # 33	GE704	BP704	B1892	BP703	CAT SCRUBBER TEST	SPECIAL LOG	BA702	BA704	BA705	FC340	BA706
1515.18	SC301	SC302	BA707	2P701	185.6	4866	427.6	120.8	474.3	133.3	391	3.31
1520.18	385	10	36.7	29.13	-44.18L	184.8	4862	429.5	470.1	129.3	393	3.21
1525.18	403	10	37.1	29.13	-43.29	185.6	4862	425.6	470.1	137.6	399	3.21
1530.18	413	10	38.6	29.13	-44.27L	186.6	4879	425.6	470.1	137.6	392	3.23
1535.18	336	10	37.6	29.13	-44.77L	185.9	4852	432.6	458.1	125.1	391	3.12
1540.18	541	10	37.7	29.13	-42.41	184.4	4463	418.6	456.3	123.7	366	3.34
1545.18	523	10	38.5	29.13	-40.81	185.3	4461	417.3	450.3	126.4	374	3.16
1550.18	611H	10	38.2	29.13	-39.97	183.4	4458	431.9	455.4	122.6	376	3.34
1555.18	525	10	37.8	29.12	-40.14	183.9	4420	431.9	455.4	122.6	381	3.22
1600.18	579H	10	39.5	29.12	-41.18	184.6	4466	421.8	502.8	125.1	374	3.29
1605.18	587	10	38.5	29.12	-41.76	184.4	4402	408.3	460.2	123.8	387	3.12
1610.18	553	10	38.4	29.13	-41.11	183.6	4464	408.3	460.2	123.8	376	3.37
1615.18	568	10	37.6	29.11	-39.86	183.6	4466	411.9	458.9	121.3	370	3.20
1620.18	537	10	37.8	29.12	-40.65	184.6	4463	402.6	480.9	121.3	366	3.28
1625.18	584	10	37.7	29.12	-40.05	185.2	4438	407.1	456.0	121.0	371	3.22
1630.18	592H	10	37.7	29.12	-40.00	185.3	4438	394.5	444.5	122.1	376	3.27
1635.18	590H	10	37.9	29.12	-39.83	185.4	4429	394.5	444.4	122.1	368	3.21
1640.18	588	10	38.2	29.12	-39.55	185.7	4441	399.1	449.4	124.6	375	3.15
1645.18	593H	10	39.1	29.11	-38.61	185.7	4441	399.1	449.4	124.6	375	3.15
1645.18	10/SE/91 SHERCO UNIT #2 TREND LOG # 33	GE704	BP704	B1892	BP703	CAT SCRUBBER TEST	SPECIAL LOG	BA702	BA704	BA705	FC340	BA706
1645.18	SC301	SC302	BA707	2P701	185.4	4429	394.5	102.2	444.4	122.1	368	3.21
1645.18	614.9	2669	655.8	-22.30	-39.55	185.7	4441	399.1	449.4	124.6	375	3.15
1645.18	588	10	38.2	29.12	-39.55	185.7	4441	399.1	449.4	124.6	375	3.15
1645.18	615.1	2664	653.9	-22.08	-38.61	185.7	4441	399.1	449.4	124.6	375	3.15
1645.18	593H	10	39.1	29.11	-38.61	185.7	4441	399.1	449.4	124.6	375	3.15

UNIT 2 DATA SHEETS

53.06 11/SE/91 LOG 16 STACK COMPLIANCE TREND LOG
 GE504 MM 3 GENERATOR GROSS MEGAWATTS
 MC514 DEGREE F MAIN STEAM TEMPERATURE
 BP502 PSI G 31 STEAM DRUM PRESSURE
 DC524 KLB/HR TOTAL BOILER AIR FLOW
 SC571 SPRAY ABSORBERS SPRAYING

KLB/HR BOILER SUPRHTR OUILET STEAM FLOW
 PSIG MAIN STEAM STOP VLV INLET PRESS
 TONS/HR COAL FLOW TOTAL
 PERCENT MAX1 AVERAGE FLUE GAS O2
 DEGREE F SPRAY ABSORBERS INLET TEMP

TIME	GE504	MC526	MC514	MP525	BP502	LC502	DC524	DC566	SC571	SC572
0755.36	873.9	6167.6	992.3	2509.6	2741.4	499.492	8562	3.476	6	270.23
0800.36	879.4	6212.8	1000.3	2527.1	2756.0	487.412	8593	3.434	6	271.34
0805.36	873.4	6176.3	1001.6	2534.8	2762.6	482.152	8328	3.293	6	269.84
0810.36	871.4	6132.7	998.5	2519.6	2748.6	487.315	8373	3.251	6	270.00
0815.36	878.1	6130.3	997.9	2516.4	2744.4	491.485	8487	3.292	6	270.53
0820.36	879.4	6169.7	999.3	2520.0	2751.0	489.677	8569	3.445	6	271.31
0825.36	874.2	6085.7	1000.8	2519.6	2747.3	487.057	8389	3.177	5	271.80
0830.36	874.7	6194.0	1002.7	2517.1	2743.9	493.459	8628	3.436	6	272.98
0835.36	878.3	6111.8	1006.8	2526.8	2755.2	485.044	8459	3.338	6	272.63
0840.36	874.8	6123.3	1004.1	2526.5	2755.2	485.812	8501	3.415	6	272.69
0845.36	872.9	6103.5	1006.8	2521.1	2751.4	486.439	8505	3.478	6	272.59
0850.36	875.0	6130.5	1008.2	2520.8	2751.4	489.977	8570	3.485	6	272.83
SC508	IN WC SPRAY ABSORBERS DIFF PRESS									
JC504	IN WC 32 FABRIC FILTER DIFF PRESS									
JC516	IN WC 33 FABRIC FILTER DIFF PRESS									
DA505	PERCENT STACK OPACITY									
YC501	IN HG BAROMETRIC PRESSURE									

FAB FLTR COMPARTMENTS IN SERVICE
 31 FABRIC FILTER DIFF PRESS
 FLUE GAS TO STACK TEMP
 AMBIENT AIR TEMPERATURE

TIME	SC508	JC520	JC504	JC509	JC516	DC546	DA505	YT501	YC501
0755.36	3.63	44	3.9	4.1	3.9	168	0.573	88.2	29.167
0800.36	3.63	44	3.9	4.1	4.0	168	0.660	58.3	29.167
0805.36	3.55	44	3.7	3.9	3.8	168	0.608	58.2	29.167
0810.36	3.39	45	3.6	3.9	3.8	167	0.469	58.2	29.167
0815.36	3.59	44	3.8	4.0	3.8	167	0.486	58.0	29.167
0820.36	3.77	45	3.8	3.8	3.8	168	0.573	58.2	29.172
0825.36	3.50	44	4.0	4.1	3.9	167	0.586	58.2	29.155
0830.36	4.38	44	4.0	3.9	4.0	169	0.556	58.2	29.172
0835.36	3.77	44	3.9	4.0	4.0	170	0.573	58.2	29.174
0840.36	3.68	44	4.0	4.1	4.1	170	0.573	58.0	29.154
0845.36	3.68	44	3.9	4.0	4.0	170	0.566	58.0	29.172
0850.36	4.02	45	3.9	3.9	4.0	170	0.660	57.7	29.154

53.00 1/5/57 16 300K COM LIAISON IREND LUG
 GE504 MW 3 GENERATOR GROSS MEGAWATTS
 MC514 DEGREE F MAIN STEAM TEMPERATURE
 BP502 PSIG 31 STEAM DRUM PRESSURE
 DC524 KLBS/HR TOTAL BOILER AIR FLOW
 SC671 SPRAY ABSORBERS SPRAYING

KLBS/HR BOILER SUPRHR OUTLET STEAM FLOW
 PSIG MAIN STEAM STOP VLV INLET PRESS
 TONS/HR COAL FLOW TOTAL
 PERCENT MAX1 AVERAGE FLUE GAS O2
 DEGREE F SPRAY ABSORBERS INLET TEMP

TIME	GE504	MC526	MC514	MP525	BP502	LC502	DC524	DC566	SC571	SC572
0855.36	878.0	6079.5	1008.1	2532.4	2758.5	484.745	8527	3.361	6	273.25
0900.36	872.6	6168.6	1005.3	2525.7	2755.2	486.514	8436	3.339	6	272.36
0905.36	875.4	6141.3	1006.1	2516.0	2745.1	490.871	8495	3.290	6	272.34
0910.36	880.1	6169.7	1006.1	2529.7	2759.3	487.562	8513	3.282	6	271.64
0915.36	873.4	6182.4	1004.0	2529.7	2756.4	485.325	8424	3.242	6	270.77
0920.36	876.1	6186.6	1003.3	2519.7	2749.8	488.910	8491	3.233	6	270.47
0925.36	885.4	6193.0	1004.0	2516.4	2750.6	494.675	8772	3.423	6	270.28
0930.36	886.8	6163.6	1002.7	2530.4	2764.0	488.007	8534	3.248	6	269.38
0935.36	876.9	6183.0	1001.3	2524.2	2756.4	485.877	8440	3.297	6	269.27
0940.36	884.9	6213.9	1003.2	2514.1	2746.4	498.607	8486	3.085	6	269.95
0945.36	887.5	6192.9	1004.6	2527.0	2760.2	489.271	8593	3.380	6	270.34
0950.36	886.0	6277.0	1004.3	2527.4	2760.2	491.905	8583	3.367	6	270.09

IN MC SPRAY ABSORBERS DIFF PRESS
 JC508 32 FABRIC FILTER DIFF PRESS
 JC504 33 FABRIC FILTER DIFF PRESS
 JC516 IN MC
 DA505 IN MC
 YC501 PERCENT STACK OPACITY
 IN HG BAROMETRIC PRESSURE

FAB FLTH COMPARTMENTS IN SERVICE
 31 FABRIC FILTER DIFF PRESS
 FLUE GAS TO STACK TEMP
 AMBIENT AIR TEMPERATURE

TIME	SC508	JC520	JC504	JC509	JC516	DC546	DA505	YT501	YC501
0855.36	3.57	45	3.9	4.1	4.0	169	0.556	57.8	29.171
0900.36	3.74	44	4.3	4.0	4.0	169	0.660	58.2	29.171
0905.36	3.69	45	3.8	4.0	4.0	169	0.625	57.8	29.156
0910.36	3.88	43	3.9	4.2	4.1	168	0.677	58.1	29.157
0915.36	3.54	44	3.9	4.2	4.1	168	0.660	58.1	29.168
0920.36	3.61	44	3.9	4.2	4.1	168	0.660	58.1	29.153
0925.36	3.88	44	4.1	4.2	4.1	168	0.660	58.2	29.153
0930.36	3.74	48	3.9	3.8	3.8	168	0.556	58.1	29.153
0935.36	3.51	44	3.9	3.8	3.9	168	0.660	58.2	29.152
0940.36	3.56	45	4.0	4.0	3.9	168	0.556	58.2	29.152
0945.36	3.77	44	4.2	4.1	4.2	168	0.556	58.2	29.159
0950.36	3.76	44	4.0	4.1	4.1	168	0.469	58.2	29.156

3.06 11/SE/91 LOG 16 STACK COMPLIANCE TREND LOG

GE504	MM	3 GENERATOR GROSS MEGAWATTS	MC526	KLBS/HR	BOILER SUPPHIR OUILET STEAM FLOW
MC514	DEGREE F	MAIN STEAM TEMPERATURE	MP525	PSIG	MAIN STEAM STOP VLV INLET PRESS
BP502	PSIG	31 STEAM DRUM PRESSURE	LC502	TONS/HR	COAL FLOW TOTAL
DC524	KLBS/HR	TOTAL BOILER AIR FLOW	DC566	PERCENT	MAX1 AVERAGE FLUE GAS O2
SC571		SPRAY ABSORBERS SPRAYING	SC572	DEGREE F	SPRAY ABSORBERS INLET TEMP

TIME	GE504	MC526	MC514	MP525	BP502	LC502	DC524	DC566	SC571	SC572
1955.36	884.8	6192.8	1005.0	2522.8	2757.3	489.908	8694	3.531	6	271.13
1000.36	885.4	6208.2	1005.6	2529.8	2764.0	486.519	8651	3.594	6	271.44
1005.36	881.5	6219.5	1001.4	2519.4	2750.3	494.741	8521	3.351	6	270.03
1010.36	881.1	6237.4	1003.3	2515.8	2750.3	492.588	8562	3.343	6	272.22
1015.36	887.1	6282.3	1009.3	2526.3	2760.7	494.226	8518	3.245	6	271.80
1020.36	885.4	6201.0	1004.0	2523.2	2757.3	490.965	8590	3.356	6	271.56
1025.36	884.2	6270.3	1004.6	2522.5	2754.0	490.089	8659	3.378	6	272.80
1030.36	887.9	6233.3	1003.7	2526.8	2761.0	491.105	8550	3.296	6	271.81
1035.36	886.7	6211.4	999.7	2523.2	2757.9	491.202	8495	3.180	6	271.80
1040.36	885.1	6210.6	999.7	2516.8	2748.1	498.527	8533	3.420	6	271.94
1045.36	886.9	6204.4	997.3	2513.1	2748.1	495.358	8712	3.578	6	272.88
1050.36	888.4	6200.1	998.0	2516.4	2752.2	495.364	8580	3.464	6	272.98
SC508	IN WC SPRAY ABSORBERS DIFF PRESS									
JC504	IN WC 32 FABRIC FILTER DIFF PRESS									
JC516	IN WC 33 FABRIC FILTER DIFF PRESS									
DA505	PERCENT STACK OPACITY									
YC501	IN HG BAROMETRIC PRESSURE									

FAB FLTR COMPARTMENTS IN SERVICE
31 FABRIC FILTER DIFF PRESS
FLUE GAS TO STACK TEMP
AMBIENT AIR TEMPERATURE

TIME	SC508	JC520	JC504	JC509	JC516	DC546	DA505	YT501	YC501
1955.36	3.69	43	4.2	4.2	4.2	168	0.799	58.2	29.132
1000.36	3.49	44	4.1	4.3	4.3	168	0.451	58.4	29.152
1005.36	3.79	44	3.9	4.3	4.1	168	0.469	58.4	29.129
1010.36	3.84	45	3.9	4.1	4.2	168	0.608	58.4	29.129
1015.36	3.62	45	3.9	4.1	4.0	168	0.431	58.5	29.129
1020.36	3.65	44	4.1	4.3	4.2	168	0.434	58.4	29.129
1025.36	3.63	45	3.9	4.2	4.1	168	0.451	58.5	29.129
1030.36	3.64	43	4.1	4.3	4.2	168	0.451	59.0	29.129
1035.36	3.56	44	3.9	4.0	4.6	168	0.486	59.0	29.113
1040.36	3.63	43	4.0	4.6	4.0	168	0.590	59.0	29.117
1045.36	3.76	44	4.1	4.1	4.1	168	0.469	58.7	29.134
1050.36	4.09	44	3.9	3.8	4.0	168	0.573	59.0	29.134

3.06 11/SE/91 LUG 16 STACK COMPLIANCE INEND LUG
GE504 MM 3 GENERATOR GROSS MEGAWATTS
MC514 DEGREE F MAIN STEAM TEMPERATURE
BP502 PSIG 31 STEAM DRUM PRESSURE
DC524 KLBS/HR TOTAL BOILER AIR FLOW
SC571 SPRAY ABSORBERS SPRAYING

MC526 KLBS/HR BOILER SUPRHTR OUTLET STEAM FLOW
MP526 PSIG MAIN STEAM STOP VLV INLET PRESS
LC502 TONS/HR COAL FLOW TOTAL
DC566 PERCENT MAX1 AVERAGE FLUE GAS O2
SC572 DEGREE F SPRAY ABSORBERS INLET TEMP

TIME
055.36
100.36
105.36
110.36
115.36
120.36
125.36
130.36
135.36
140.36
145.36
150.36
SC508
JC504
JC516
DA505
YC501
GE504
887.3
887.1
881.8
882.7
886.2
887.1
887.3
891.6
890.3
888.9
889.7
892.0
IN MC
IN MC
IN MC
PERCENT
IN HG
MC526
6204.3
6320.4
6272.7
6251.7
6279.1
6290.6
6234.5
6255.4
6217.0
6276.1
6232.7
6228.9
SPRAY ABSORBERS DIFF PRESS
32 FABRIC FILTER DIFF PRESS
33 FABRIC FILTER DIFF PRESS
STACK OPACITY
BAROMETRIC PRESSURE
MC514
1000.1
998.8
989.8
991.4
993.7
994.3
997.1
999.9
997.2
1001.2
1002.1
1002.7
MP525
2519.7
2533.0
2519.2
2514.5
2522.0
2520.1
2516.1
2523.6
2520.0
2520.0
2523.5
2530.5
JC509
JC546
YC501
4.0
3.7
3.9
3.9
3.9
4.0
4.0
3.9
4.0
4.2
4.1
4.2
4.0
4.3
4.1
4.3
4.2
4.1
4.3
4.1
4.4
4.2
4.2

BP502
2755.5
2768.9
2754.3
2754.3
2761.5
2758.1
2754.9
2761.9
2755.2
2758.6
2762.4
2769.0
LC502
492.949
492.888
489.930
493.234
493.726
495.560
494.910
492.078
497.422
497.132
495.958
492.654
JC520
JC509
DC546
YC501
4.1
4.0
4.2
4.1
4.1
4.3
4.1
4.0
4.1
4.0
4.1
4.2
4.0
4.3
4.1
4.3
4.2
4.1
4.3
4.1
4.4
4.2
4.2
DA508
0.503
0.469
0.469
0.469
0.556
0.451
0.538
0.573
0.538
0.451
0.469
0.856
YC501
29.114
29.123
29.122
29.122
29.122
29.122
29.123
29.123
29.123
29.123
29.123
29.126

TIME
055.36
100.36
105.36
110.36
115.36
120.36
125.36
130.36
135.36
140.36
145.36
150.36
SC508
3.84
3.49
3.64
3.62
3.63
3.74
3.74
3.52
3.97
3.82
3.53
3.83
JC520
44
45
44
44
43
44
44
44
45
44
45
43
JC509
4.0
4.0
4.3
4.3
4.1
4.3
4.2
4.1
4.3
4.4
4.2
4.4
JC504
4.0
3.7
3.9
3.9
3.9
4.0
4.0
3.9
4.0
4.2
4.1
4.2
DA508
0.503
0.469
0.469
0.469
0.556
0.451
0.538
0.573
0.538
0.451
0.469
0.856
YC501
29.114
29.123
29.122
29.122
29.122
29.122
29.123
29.123
29.123
29.123
29.123
29.126

IN MC
DEGREE F
DEGREE F
FAB FLTR COMPANIMENTS IN SERVICE
31 FABRIC FILTER DIFF PRESS
FLUE GAS TO STACK TEMP
AMBIENT AIR TEMPERATURE
DA508
0.503
0.469
0.469
0.469
0.556
0.451
0.538
0.573
0.538
0.451
0.469
0.856
YC501
29.114
29.123
29.122
29.122
29.122
29.122
29.123
29.123
29.123
29.123
29.123
29.126

1253.06 11/SE/91 LOG 16 STACK COMPLIANCE TREND LOG
 GE504 MW 3 GENERATOR GROSS MEGAWATTS
 MC514 DEGREE F MAIN STEAM TEMPERATURE
 BP502 PSIG 31 STEAM DRUM PRESSURE
 DC524 KLBS/HR TOTAL BOILER AIR FLOW
 SC571 SPRAY ABSORBERS SPRAYING

TIME	GE504	MC526	MC514	MP525	BP502	LC502	DC524	DC566	SC571	SC572
1155.36	889.5	6329.6	1002.3	2527.3	2768.6	494.834	8647	3.372	6	276.98
1200.36	890.3	6249.1	1000.8	2520.9	2762.0	492.125	8655	3.422	6	276.28
1205.36	893.6	6294.1	1003.6	2523.1	2765.6	498.560	8714	3.465	6	277.47
1210.36	893.0	6226.0	1006.4	2526.5	2765.1	490.398	8737	3.515	6	276.88
1215.36	893.3	6204.0	1005.2	2519.8	2758.6	494.928	8755	3.556	6	276.19
1220.36	893.6	6180.6	1002.6	2515.3	2758.2	496.331	8707	3.428	6	275.92
1225.36	895.5	6199.1	1007.6	2525.5	2763.1	496.908	8753	3.520	6	277.19
1230.36	895.7	6235.4	1008.1	2526.0	2766.5	494.193	8683	3.444	6	277.09
1235.36	891.9	6267.1	1007.7	2522.3	2759.9	494.619	8708	3.478	6	277.48
1240.36	892.5	6161.0	1011.4	2525.6	2763.1	495.083	8834	3.672	6	277.19
1245.36	892.2	6276.1	1009.1	2530.2	2769.8	493.903	8673	3.441	6	276.97
1250.36	889.5	6222.1	1007.9	2526.5	2763.1	490.510	8660	3.343	*****	*****

SC508 IN MC SPRAY ABSORBERS DIFF PRESS
 JC504 IN MC 32 FABRIC FILTER DIFF PRESS
 JC516 IN MC 33 FABRIC FILTER DIFF PRESS
 DA505 PERCENT STACK OPACITY
 YC501 IN HG BAROMETRIC PRESSURE

TIME	SC508	JC520	JC504	JC509	JC516	DC546	DA505	Y1501	YC501
1155.36	3.85	44	4.1	4.1	3.9	168	0.469	59.7	29.125
1200.36	3.86	44	4.0	4.2	4.1	168	0.556	60.0	29.125
1205.36	3.64	44	4.1	4.2	4.1	169	0.556	60.0	29.125
1210.36	4.08	44	4.0	4.0	4.1	169	0.469	60.0	29.125
1215.36	3.99	45	4.0	4.1	4.1	168	0.451	60.1	29.125
1220.36	3.78	45	4.0	4.2	4.1	168	0.486	60.1	29.109
1225.36	3.90	44	4.3	4.3	4.4	169	0.469	60.1	29.099
1230.36	3.97	44	4.0	4.1	4.2	169	0.365	60.1	29.102
1235.36	3.87	43	4.1	4.3	4.3	169	0.469	60.2	29.102
1240.36	4.04	44	4.3	4.5	4.5	169	0.365	60.4	29.102
1245.36	3.83	44	4.1	4.2	4.3	169	0.538	60.3	29.102
1250.36	*****	*****	*****	*****	*****	*****	*****	60.4	29.102

FAB FLTH COMPARTMENTS IN SERVICE
 31 FABRIC FILTER DIFF PRESS
 FLUE GAS TO STACK TEMP
 AMBIENT AIR TEMPERATURE

353.06 11/SE/91 LOG 16 STACK COMPLIANCE TREND LOG
GE504 MW 3 GENERATOR GROSS MEGAWATTS
MC514 DEGREE F MAIN STEAM TEMPERATURE
BP502 PSIG 31 STEAM DRUM PRESSURE
DC524 KLBS/HR TOTAL BOILER AIR FLOW
SC571 SPRAY ABSORBERS SPRAYING

KLBS/HR BOILER SUPRMR OUTLET STEAM FLOW
PSIG MAIN STEAM STOP VLV INLET PRESS
TONS/HR COAL FLOW TOTAL
PERCENT MAX1 AVERAGE FLUE GAS O2
DEGREE F SPIRAY ABSORBERS INLET TEMP

TIME	GE504	MC526	MC514	MP525	BP502	LC502	DC524	DC566	SC571	SC572
1255.36	889.7	6192.1	1008.1	2526.4	2763.1	491.180	8616	3.369	*****	*****
1300.36	888.9	6273.1	1008.1	2526.6	2766.5	488.040	8613	3.453	*****	*****
1305.36	886.3	6289.1	1008.1	2523.2	2769.7	492.308	8734	3.618	6	276.82
1310.36	887.5	6238.8	1006.8	2521.6	2756.5	496.083	8745	3.488	6	277.22
1315.36	888.2	6244.6	1006.3	2525.2	2769.8	491.212	8609	3.317	6	276.75
1320.36	889.9	6224.4	1003.3	2522.3	2756.5	493.356	8642	3.346	6	276.38
1325.36	888.0	6250.8	1001.9	2518.2	2763.2	492.668	8623	3.404	6	276.48
1330.36	888.9	6206.8	1003.3	2518.0	2763.2	494.137	8636	3.509	6	277.22
1335.36	888.3	6267.5	1002.8	2522.0	2767.3	492.696	8636	3.436	6	277.39
1340.36	888.3	6260.7	1001.4	2515.5	2760.5	495.335	8660	3.385	6	277.63
1345.36	889.5	6195.9	1001.4	2513.8	2760.5	496.184	8675	3.244	6	277.91
1350.36	889.2	6207.1	1002.3	2514.1	2747.3	497.217	8606	3.204	6	279.03

IN MC SPRAY ABSORBERS DIFF PRESS
IN MC 32 FABRIC FILTER DIFF PRESS
IN MC 33 FABRIC FILTER DIFF PRESS
PERCENT STACK OPACITY
IN HG BAROMETRIC PRESSURE

FAB FLTR COMPARTMENTS IN SERVICE
31 FABRIC FILTER DIFF PRESS
FLUE GAS TO STACK TEMP
AMBIENT AIR TEMPERATURE

TIME	SC508	JC520	JC504	JC509	JC516	DC546	DA508	YT501	YC501
1255.36	*****	*****	*****	*****	*****	*****	*****	60.6	29.102
1300.36	*****	*****	*****	*****	*****	*****	*****	60.8	29.102
1305.36	3.90	44	4.1	4.0	4.1	169	0.469	60.7	29.102
1310.36	3.64	44	4.2	4.3	4.2	169	0.660	60.9	29.102
1315.36	3.63	44	4.0	4.2	4.1	169	0.586	60.9	29.086
1320.36	3.68	44	4.1	4.1	4.2	169	0.538	61.2	29.086
1325.36	3.62	44	4.1	4.1	4.2	169	0.838	61.1	29.086
1330.36	3.73	44	4.0	4.1	4.2	169	0.660	61.0	29.086
1335.36	3.84	45	4.0	4.1	4.1	169	0.856	61.2	29.070
1340.36	3.66	45	4.0	4.1	4.1	169	0.608	60.9	29.084
1345.36	3.70	44	4.3	4.3	4.3	169	0.556	61.3	29.084
1350.36	3.55	45	4.0	4.2	4.2	169	0.642	61.3	29.084

153.06 11/SE/91 LOG 16 STACK COMPLIANCE TREND LOG
 GE504 MW 3 GENERATOR GROSS MEGAWATTS
 MC514 DEGREE F MAIN STEAM TEMPERATURE
 BP502 PSIG 31 STEAM DRUM PRESSURE
 DC524 KLBS/HR TOTAL BOILER AIR FLOW
 SC571 SPRAY ABSORBERS SPRAYING

TIME	GE504	MC526	MC514	MP525	BP502	LC502	DC524	DC566	SC571	SC572
1355.36	890.1	6219.4	1004.2	2514.9	2750.6	499.448	8647	3.141	6	278.56
1400.36	890.8	6186.7	1005.3	2521.6	2753.9	495.635	8635	3.260	6	279.46
1405.36	888.9	6223.0	1007.0	2514.5	2750.5	501.205	8647	3.359	6	279.59
1410.36	892.8	6218.5	1010.1	2524.9	2757.5	499.974	8629	3.424	6	279.36
1415.36	890.8	6218.2	1005.7	2521.7	2757.2	497.779	8743	3.612	6	279.56
1420.36	889.0	6256.6	1004.0	2519.5	2754.7	499.130	8735	3.563	6	278.91
1425.36	890.2	6246.2	1006.6	2522.7	2754.7	500.788	8793	3.620	6	278.69
1430.36	892.5	6211.7	1002.7	2532.3	2768.1	490.735	8691	3.509	6	277.81
1435.36	886.8	6273.4	992.6	2625.7	2761.8	497.493	8639	3.452	6	277.59
1440.36	882.4	6312.2	991.8	2615.0	2761.8	500.660	8688	3.375	6	277.28
1445.36	885.9	6244.1	992.5	2618.3	2755.7	501.250	8757	3.606	6	277.92
1450.36	885.3	6271.3	992.5	2522.0	2759.1	500.271	8704	3.598	6	277.77

IN MC SPRAY ABSORBERS DIFF PRESS JC520
 IN MC 32 FABRIC FILTER DIFF PRESS JC509
 IN MC 33 FABRIC FILTER DIFF PRESS DC546
 PERCENT STACK OPACITY YT501
 IN HG BAROMETRIC PRESSURE

KLBS/HR BOILER SUPRHR OUTLET STEAM FLOW
 PSIG MAIN STEAM STOP VLV INLET PRESS
 TONS/HR COAL FLOW TOTAL
 PERCENT MAXI AVERAGE FLUE GAS O2
 DEGREE F SPRAY ABSORBERS INLET TEMP

FAB FLTR COMPARTMENTS IN SERVICE
 31 FABRIC FILTER DIFF PRESS
 FLUE GAS TO STACK TEMP
 AMBIENT AIR TEMPERATURE

TIME	SC508	JC520	JC504	JC509	JC516	DC546	DA505	YT501	YC501
1355.36	3.84	43	4.0	4.4	4.2	169	0.660	61.0	29.084
1400.36	3.78	44	4.1	4.3	4.3	169	0.538	61.0	29.084
1405.36	3.83	44	4.1	4.5	4.2	169	0.660	60.9	29.084
1410.36	3.66	44	4.0	4.3	4.1	169	0.660	61.1	29.084
1415.36	3.86	45	4.1	4.0	4.0	169	0.556	61.3	29.066
1420.36	4.19	44	4.2	4.0	4.1	169	0.660	61.2	29.066
1425.36	3.89	45	4.0	3.9	4.1	170	0.660	60.9	29.066
1430.36	3.76	44	4.2	4.2	4.2	169	0.660	61.4	29.051
1435.36	3.47	44	4.1	4.1	4.1	169	0.694	61.4	29.051
1440.36	3.84	43	4.0	4.2	4.2	169	0.764	61.2	29.051
1445.36	3.93	44	4.1	4.2	4.3	169	0.799	61.4	29.051
1450.36	3.85	44	3.9	4.2	4.2	169	0.746	61.6	29.037

TIME	DATE	LOG	STACK COMPLIANCE	INERT LOG	UNIT	PARAMETER	VALUE	UNIT	DESCRIPTION
1553.06	11/SE/91	LOG 10	STACK COMPLIANCE	INERT LOG	GE504	3 GENERATOR GROSS MEGAWATTS	MC526	KLBS/HR	BOILER SUPRTHR OUTLET STEAM FLOW
					MC514	DEGREE F MAIN STEAM TEMPERATURE	MP526	PSIG	MAIN STEAM STOP VLV INLET PRESS
					BP502	31 STEAM DRUM PRESSURE	LC502	TONS/HR	COAL FLOW TOTAL
					DC524	TOTAL BOILER AIR FLOW	DC566	PERCENT	MAX1 AVERAGE FLUE GAS O2
					SC571	SPRAY ABSORBERS SPRAYING	SC572	DEGREE F	SPRAY ABSORBERS INLET TEMP

TIME	GE504	MC526	MC514	MP525	BP502	LC502	DC524	DC566	SC571	SC572
1455.36	885.4	6290.9	993.1	2521.9	2759.2	500.584	8679	3.506	6	277.84
1500.36	882.9	6245.1	992.5	2511.1	2749.1	503.814	8758	3.462	6	278.44
1505.36	888.2	6271.6	999.9	2521.0	2756.5	502.990	8662	3.289	6	278.06
1510.36	890.7	6197.7	1001.4	2521.9	2764.2	501.271	8683	3.351	6	277.98
1515.36	899.6	6210.7	1001.5	2519.0	2757.6	502.937	8762	3.490	6	278.56
1520.36	893.9	6231.6	1002.9	2518.9	2757.2	506.510	8740	3.403	6	278.00
1525.36	890.5	6194.4	1002.8	2518.3	2756.7	502.915	8672	3.420	6	278.39
1530.36	890.6	6183.7	1002.2	2518.2	2756.8	502.622	8815	3.505	6	279.48
1535.36	893.7	6242.9	1002.4	2522.0	2760.2	506.489	8758	3.463	6	279.11
1540.36	895.4	6221.2	1002.4	2518.2	2756.8	506.740	8799	3.527	6	279.66
1545.36	897.3	6216.8	1003.7	2518.3	2760.0	508.169	8762	3.429	6	279.56
1550.36	897.9	6217.5	1005.0	2521.1	2762.6	507.158	8820	3.519	6	281.22
SC508	IN WC	SPRAY ABSORBERS	DIFF PRESS	JC520				FAB FLTR COMPARTMENTS	IN SERVICE	
JC504	IN WC	32 FABRIC FILTER	DIFF PRESS	JC509			IN WC	31 FABRIC FILTER	DIFF PRESS	
JC516	IN WC	33 FABRIC FILTER	DIFF PRESS	DC546			DEGREE F	FLUE GAS TO STACK	TEMP	
DA505	PERCENT	STACK OPACITY		YT501			DEGREE F	AMBIENT AIR	TEMPERATURE	
YC501	IN HG	BARIOMETRIC	PRESSURE							

TIME	SC508	JC520	JC604	JC509	JC516	DC546	DA505	Y1501	YC501
1455.36	3.83	44	3.9	4.1	4.1	169	0.660	61.4	29.053
1500.36	4.09	45	4.0	4.1	4.2	170	0.660	61.1	29.038
1505.36	3.87	44	4.0	4.3	4.3	170	0.677	61.4	29.038
1510.36	3.92	45	4.0	4.1	4.2	169	0.556	61.6	29.038
1515.36	3.79	43	4.1	4.2	4.3	170	0.660	61.8	29.038
1520.36	3.89	44	4.2	4.2	4.5	170	0.642	61.6	29.038
1525.36	4.14	44	4.2	4.7	4.1	170	0.764	61.9	29.038
1530.36	3.87	44	4.2	4.1	4.1	170	0.469	61.5	29.033
1535.36	3.81	44	4.1	4.1	4.1	170	0.764	61.7	29.026
1540.36	3.71	45	4.3	4.2	4.2	170	0.694	61.8	29.026
1545.36	3.93	45	4.1	4.2	4.2	170	0.660	61.5	29.025
1550.36	3.82	44	5.0	4.5	4.4	170	0.660	61.8	29.025

1638.06 11/SE/91 LOG 16 STACK COMPLIANCE TREND LOG
 GE504 MW 3 GENERATOR GROSS MEGAWATTS
 MC514 DEGREE F MAIN STEAM TEMPERATURE
 BP502 PSIG 31 STEAM DRUM PRESSURE
 DC524 KLBS/HR TOTAL BOILER AIR FLOW
 SC571 SPRAY ABSORBERS SPRAYING

TIME	GE504	MC526	MC514	MP525	BP502	LC502	DC524	DC566	SC571	SC572
1540.36	896.4	6221.2	1002.4	2518.2	2766.8	506.740	8799	3.527	6	279.66
1545.36	897.3	6216.8	1003.7	2519.3	2760.0	508.169	8762	3.429	6	279.56
1550.36	897.9	6217.5	1005.0	2521.1	2762.6	507.158	8820	3.519	6	281.22
1555.36	895.2	6201.1	1004.8	2529.4	2769.3	500.938	8737	3.417	6	280.75
1600.36	888.5	6305.4	1008.5	2532.4	2769.3	498.504	8729	3.487	6	280.44
1605.36	887.1	6223.4	1008.2	2524.5	2762.2	504.247	8703	3.450	6	280.00
1610.36	886.6	6247.9	1006.0	2528.1	2765.5	499.655	8654	3.441	6	279.42
1615.36	883.6	6257.8	1006.6	2521.9	2758.8	501.429	8685	3.450	6	279.28
1620.36	884.4	6223.0	1006.6	2525.2	2758.8	503.339	8750	3.543	6	278.69
1625.36	885.5	6210.2	1007.1	2521.6	2758.1	502.725	8716	3.574	6	278.83
1630.36	883.4	6198.7	1006.1	2525.4	2758.1	499.277	8766	3.620	6	278.78
1635.36	884.0	6219.8	1004.8	2522.1	2754.7	502.815	8712	3.541	6	278.75

IN MC SPRAY ABSORBERS DIFF PRESS
 JC508 32 FABRIC FILTER DIFF PRESS
 JC504 33 FABRIC FILTER DIFF PRESS
 JC516 33 FABRIC FILTER DIFF PRESS
 DA505 PERCENT STACK OPACITY
 YC501 IN HG BAROMETRIC PRESSURE

TIME	SC508	JC520	JC504	JC509	JC516	DC546	DA505	YT501	YC501
1540.36	3.71	45	4.3	4.2	4.2	170	0.694	61.8	29.026
1545.36	3.93	45	4.1	4.2	4.2	170	0.660	61.5	29.025
1550.36	3.82	44	5.0	4.5	4.4	170	0.660	61.8	29.025
1555.36	3.88	44	4.1	4.4	4.3	170	0.712	61.8	29.025
1600.36	3.73	43	4.1	4.3	4.3	170	0.660	61.6	29.025
1605.36	3.92	44	4.2	4.4	4.6	170	0.556	61.9	29.025
1610.36	3.57	44	4.1	4.4	4.2	170	0.746	62.0	29.025
1615.36	3.86	44	4.0	4.2	4.2	169	0.660	62.0	29.024
1620.36	3.93	45	4.1	4.2	4.3	169	0.677	61.9	29.009
1625.36	3.88	44	4.3	4.4	4.2	169	0.573	61.8	29.010
1630.36	3.70	45	4.1	4.2	4.2	169	0.660	61.4	29.009
1635.36	3.88	44	4.4	4.4	4.0	169	0.660	61.5	29.009

FAB FLTR COMPARTMENTS IN SERVICE
 31 FABRIC FILTER DIFF PRESS
 FLUE GAS TO STACK TEMP
 AMBIENT AIR TEMPERATURE

APPENDIX F

PROCEDURES

METHOD 101A—DETERMINATION OF PARTICULATE AND GASEOUS MERCURY EMISSIONS FROM SEWAGE SLUDGE INCINERATORS METH. 101A

Introduction

This method is similar to Method 101, except acidic potassium permanganate solution is used instead of acidic iodine monochloride for collection.

1. Applicability and Principle

1.1 Applicability. This method applies to the determination of particulate and gaseous mercury (Hg) emissions from sewage sludge incinerators and other sources as specified in the regulations.

1.2 Principle. Particulate and gaseous Hg emissions are withdrawn isokinetically from the source and collected in acidic potassium permanganate (KMnO_4) solution. The Hg collected (in the mercuric form) is reduced to elemental Hg, which is then aerated from the solution into an optical cell and measured by atomic absorption spectrophotometry.

2. Range and Sensitivity

2.1 Range. After initial dilution, the range of this method is 20 to 800 ng Hg/ml. The upper limit can be extended by further dilution of the sample.

2.2 Sensitivity. The sensitivity of the method depends on the recorder/spectrophotometer combination selected.

3. Interfering Agents

3.1 Sampling. Excessive oxidizable organic matter in the stack gas prematurely depletes the KMnO_4 solution and thereby prevents further collection of Hg.

3.2 Analysis. Condensation of water vapor on the optical cell windows causes a positive interference.

4. Precision

Based on eight paired-train tests, the within-laboratory standard deviation was estimated to be 4.8 μg Hg/ml in the concentration range of 50 to 130 μg Hg/m³.

5. Apparatus

5.1 Sampling Train and Sample Recovery. Same as Method 101, Sections 5.1 and 5.2, respectively, except for the following variations:

5.1.1 Probe Liner. Same as Method 101, Section 5.1.2, except that if a filter is used ahead of the impingers, the tester must use the probe heating system to minimize the condensation of gaseous Hg.

5.1.2 Filter Holder (Optional). Borosilicate glass with a rigid stainless-steel wire-screen filter support (do not use glass frit supports) and a silicone rubber or Teflon gasket, designed to provide a positive seal against leakage from outside or around the filter. The filter holder must be equipped with a filter heating system capable of

maintaining a temperature around the filter holder of $120 \pm 14^\circ\text{C}$ ($248 \pm 25^\circ\text{F}$) during sampling to minimize both water and gaseous Hg condensation. The tester may use a filter in cases where the stream contains large quantities of particulate matter.

5.2 Analysis. The apparatus needed for analysis is the same as Method 101, Sections 5.3 and 5.4, except as follows:

5.2.1 Volumetric Pipets. Class A: 1-, 2-, 3-, 4-, 5-, 10-, and 20-ml.

5.2.2 Graduated Cylinder. 25-ml.

5.2.3 Steam Bath.

6. Reagents

Use ACS reagent-grade chemicals or equivalent, unless otherwise specified.

6.1 Sampling and Recovery. The reagents used in sampling and recovery are as follows:

6.1.1 Water. Deionized distilled, meeting ASTM Specifications for Type I Reagent Water—ASTM Test Method D1193-77 (incorporated by reference—see § 61.18). If high concentrations of organic matter are not expected to be present, the analyst may eliminate the KMnO_4 test for oxidizable organic matter. Use this water in all dilutions and solution preparations.

6.1.2 Nitric Acid (HNO_3), 50 Percent (V/V). Mix equal volumes of concentrated HNO_3 and deionized distilled water, being careful to slowly add the acid to the water.

6.1.3 Silica Gel. Indicating type, 6- to 16-mesh. If previously used, dry at 175°C (350°F) for 2 hr. The tester may use new silica gel as received.

6.1.4 Filter (Optional). Glass fiber filter, without organic binder, exhibiting at least 99.95 percent efficiency on 0.3 μm dioctyl phthalate smoke particles. The tester may use the filter in cases where the gas stream contains large quantities of particulate matter, but he should analyze blank filters for Hg content.

6.1.5 Sulfuric Acid (H_2SO_4), 10 Percent (V/V). Add and mix 100 ml of concentrated H_2SO_4 with 900 ml of deionized distilled water.

6.1.6 Absorbing Solution, 4 Percent KMnO_4 (W/V). Prepare fresh daily. Dissolve 40 g of KMnO_4 in sufficient 10 percent H_2SO_4 to make 1 liter. Prepare and store in glass bottles to prevent degradation.

6.2 Analysis. The reagents needed for analysis are listed below:

6.2.1 Tin (II) Solution. Prepare fresh daily and keep sealed when not being used. Completely dissolve 20 g of tin (II) chloride (or 25 g of tin (II) sulfate) crystals (Baker Analyzed reagent grade or any other brand that will give a clear solution) in 25 ml of concentrated HCl . Dilute to 250 ml with deionized distilled water. Do not substitute HNO_3 , H_2SO_4 , or other strong acids for the HCl .

6.2.2 Sodium Chloride-Hydroxylamine Solution. Dissolve 12 g of sodium chloride and 12 g of hydroxylamine sulfate (or 12 g of hydroxylamine hydrochloride) in deionized distilled water and dilute to 100 ml.

6.2.3 Hydrochloric Acid (HCl), 8 N. Dilute 67 ml of concentrated HCl to 100 ml with deionized distilled water (slowly add the HCl to the water).

6.2.4 Nitric Acid, 15 Percent (V/V). Dilute 15 ml of concentrated HNO₃ to 100 ml with deionized distilled water.

6.2.5 Mercury Stock Solution, 1 mg Hg/ml. Prepare and store all mercury standard solutions in borosilicate glass containers. Completely dissolve 0.1354 g of mercury (II) chloride in 75 ml of deionized distilled water. Add 100 ml of concentrated HNO₃ and adjust the volume to exactly 100 ml with deionized distilled water. Mix thoroughly. This solution is stable for at least 1 month.

6.2.6 Intermediate Mercury Standard Solution, 10 µg Hg/ml. Prepare fresh weekly. Pipet 5.0 ml of the mercury stock solution (Section 6.2.5) into a 500-ml volumetric flask and add 20 ml of 15 percent HNO₃ solution. Adjust the volume to exactly 500 ml with deionized distilled water. Thoroughly mix the solution.

6.2.7 Working Mercury Standard Solution, 200 ng Hg/ml. Prepare fresh daily. Pipet 5.0 ml from the "Intermediate Mercury Standard Solution" (Section 6.2.6) into a 250-ml volumetric flask. Add 5 ml of 4 percent KMnO₄ absorbing solution and 5 ml of 15 percent HNO₃. Adjust the volume to exactly 250 ml with deionized distilled water. Mix thoroughly.

6.2.8 Potassium Permanganate, 5 Percent (W/V). Dissolve 5 g of KMnO₄ in deionized distilled water and dilute to 100 ml.

6.2.9 Filter. Whatman No. 40 or equivalent.

7. Procedure

7.1 Sampling. The sampling procedure is the same as Method 101, except for changes due to the use of KMnO₄ instead of ICl absorbing solution and the possible use of a filter. These changes are as follows:

7.1.1 Preliminary Determinations. The preliminary determinations are the same as those given in Method 101, section 7.1.2, except for the absorbing solution depletion sign. In this method, high oxidizable organic content may make it impossible to sample for the desired minimum time. This problem is indicated by the complete bleaching of the purple color of the KMnO₄ solution. In these cases, the tester may divide the sample run into two or more subruns to insure that the absorbing solution would not be depleted. In cases where an excess of water condensation is encountered, collect two runs to make one sample.

7.1.2 Preparation of Sampling Train. The preparation of the sampling train is the same as that given in Method 101, section 7.1.3, except for the cleaning of the glassware (probe, filter holder (if used), impingers, and connectors) and the charging of the first three impingers. In this method, clean all the glass components by rinsing with 50 percent HNO₃, tap water, 8 N HCl, tap water, and finally deionized distilled water. Then place 50 ml of 4 percent KMnO₄ in the first impinger and 100 ml in each of the second and third impingers.

If a filter is used, use a pair of tweezers to place the filter in the filter holder. Be sure to center the filter and place the gasket in proper position to prevent the sample gas stream from by-passing the filter. Check the filter for tears after assembly is completed. Be sure also to set the filter heating system at the desired operating temperature after the sampling train has been assembled.

7.1.3 Sampling Train Operation. In addition to the procedure given in Method 101, section 7.1.5, maintain a temperature around the filter (if applicable) of 120°±14° C (248°±25° F).

7.2 Sample Recovery. Begin proper clean-up procedure as soon as the probe is removed from the stack at the end of the sampling period. Allow the probe to cool. When it can be safely handled, wipe off any external particulate matter near the tip of the probe nozzle and place a cap over it. Do not cap off the probe tip tightly while the sampling train is cooling because the resultant vacuum would draw liquid out from the impingers.

Before moving the sample train to the cleanup site, remove the probe from the train, wipe off the silicone grease, and cap the open outlet of the probe. Be careful not to lose any condensate that might be present. Wipe off the silicone grease from the impinger. Use either ground-glass stoppers, plastic caps, or serum caps to close these openings.

Transfer the probe, impinger assembly, and (if applicable) filter assembly to a cleanup area that is clean, protected from the wind, and free of Hg contamination. The ambient air in laboratories located in the immediate vicinity of Hg-using facilities is not normally free of Hg contamination.

Inspect the train before and during assembly, and note any abnormal conditions. Treat the sample as follows:

7.2.1 Container No. 1 (Impinger, Probe, and Filter Holder). Use a graduated cylinder, measure the liquid in the first three impingers to within ±1 ml. Record the volume of liquid present (e.g., see Figure 5-3 of Method 5 in part 60 of 40 CFR). This information is needed to calculate the moisture content of the effluent gas. (Use only graduated cylinder and glass storage bottles that

have been precleaned as in section 7.1.2.) Place the contents of the first three impingers into a 1000-ml glass sample bottle.

(NOTE: If a filter is used, remove the filter from its holder, as outlined under "Container No. 3" below.)

Taking care that dust on the outside of the probe or other exterior surfaces does not get into the sample, quantitatively recover the Hg (and any condensate) from the probe nozzle, probe fitting, probe liner and front half of the filter holder (if applicable) as follows: Rinse these components with a total of 250 to 400 ml of fresh 4 percent KMnO_4 solution; add all washings to the 1000-ml glass sample bottle; remove any residual brown deposits on the glassware using the minimum amount of 8 N HCl required; and add this HCl rinse to this sample container.

After all washings have been collected in the sample container, tighten the lid on the container to prevent leakage during shipment to the laboratory. Mark the height of the fluid level to determine whether leakage occurs during transport. Label the container to clearly identify its contents.

7.2.2. Container No. 2 (Silica Gel). Note the color of the indicating silica gel to determine whether it has been completely spent and make a notation of its condition. Transfer the silica gel from its impinger to its original container and seal. The tester may use as aids a funnel to pour the silica gel and a rubber policeman to remove the silica gel from the impinger. It is not necessary to remove the small amount of particles that may adhere to the impinger wall and are difficult to remove. Since the gain in weight is to be used for moisture calculations, do not use any water or other liquids to transfer the silica gel. If a balance is available in the field, weigh the spent silica gel (or silica gel plus impinger) to the nearest 0.5 g; record this weight.

7.2.3. Container No. 3 (Filter). If a filter was used, carefully remove it from the filter holder, place it in a 100-ml glass sample bottle, and add 20 to 40 ml of 4 percent KMnO_4 . If it is necessary to fold the filter, be sure that the particulate cake is inside the fold. Carefully transfer to the 150-ml sample bottle any particulate matter and filter fibers that adhere to the filter holder gasket by using a dry Nylon bristle brush and a sharp-edged blade. Seal the container. Label the container to clearly identify its contents. Mark the height of the fluid level to determine whether leakage occurs during transport.

7.2.4. Container No. 4 (Filter Blank). If a filter was used, treat an unused filter from the same filter lot used for sampling in the same manner as Container No. 3.

7.2.5. Container No. 5 (Absorbing Solution Blank). For a blank, place 500 ml of 4

percent KMnO_4 absorbing solution in a 1000-ml sample bottle. Seal the container.

7.3 Sample preparation. Check liquid level in each container to see if liquid was lost during transport. If a noticeable amount of leakage occurred, either void the sample or use methods subject to the approval of the Administrator to account for the losses. Then follow the procedures below.

7.3.1. Containers No. 3 and No. 4 (Filter and Filter Blank). If a filter was used, place the contents, including the filter, of Containers No. 3 and No. 4 in separate 250-ml beakers and heat the beakers on a steam bath until most of the liquid has evaporated. Do not take to dryness. Add 20 ml of concentrated HNO_3 to the beakers, cover them with a glass, and heat on a hot plate at 70° C for 2 hours. Remove from the hot plate and filter the solution through Whatman No. 40 filter paper. Save the filtrate for Hg analysis. Discard the filter.

7.3.2. Container No. 1 (Impingers, Probe, and Filter Holder). Filter the contents of Container No. 1 through Whatman 40 filter paper to remove the brown MnO_2 precipitate. Wash the filter with 50 ml of 4 percent KMnO_4 absorbing solution and add this wash to the filtrate. Discard the filter. Combine the filtrates from Containers No. 1 and No. 3 (if applicable), and dilute to a known volume with deionized distilled water. Mix thoroughly.

7.3.3. Container No. 5 (Absorbing Solution Blank). Treat this container as described in section 7.3.2. Combine this filtrate with the filtrate with Container No. 4 and dilute to a known volume with deionized distilled water. Mix thoroughly.

7.4 Analysis. Calibrate the spectrophotometer and recorder and prepare the calibration curve as described in sections 8.1 and 8.2. Then repeat the procedure used to establish the calibration curve with appropriately sized aliquots (1 to 10 ml) of the samples (from sections 7.3.2 and 7.3.3) until two consecutive peak heights agree within ± 3 percent of their average value. If the 10-ml sample is below the detectable limit, use a larger aliquot (up to 20 ml), but decrease the volume of water added to the aeration cell accordingly to prevent the solution volume from exceeding the capacity of the aeration bottle. If the peak maximum of a 1.0-ml aliquot is off scale, further dilute the original sample to bring the Hg concentration into the calibration range of the spectrophotometer. If the Hg content of the absorbing solution and filter blank is below the working range of the analytical method, use zero for the blank.

Run a blank and standard at least after every five samples to check the spectrophotometer calibration; recalibrate as necessary.

It is also recommended that at least one sample from each stack test be checked by the Method of Standard Additions to confirm that matrix effects have not interfered in the analysis.

8. Calibration and Standards

The calibration and standards are the same as Method 101, Section 8, except for the following variations:

8.1 Optical Cell Heating System Calibration. Same as Method 101, Section 8.2, except use a 25-ml graduated cylinder to add 25 ml of deionized distilled water to the bottle section of the aeration cell.

8.2 Spectrophotometer and Recorder Calibration. The mercury response may be measured by either peak height or peak area. (NOTE: The temperature of the solution affects the rate at which elemental Hg is released from a solution and, consequently, it affects the shape of the absorption curve (area) and the point of maximum absorbance (peak height). To obtain reproducible results, all solutions must be brought to room temperature before use.) Set the spectrophotometer wave length at 253.7 nm and make certain the optical cell is at the minimum temperature that will prevent water condensation.

Then set the recorder scale as follows: Using a 25-ml graduated cylinder, add 25 ml of deionized distilled water to the aeration cell bottle and pipet 5.0 ml of the working mercury standard solution into the aeration cell. (NOTE: Always add the Hg-containing solution to the aeration cell after the 25 ml of deionized distilled water.) Place a Teflon-coated stirring bar in the bottle. Add 5 ml of the 4 percent KMnO₄ absorbing solution followed by 5 ml of 15 percent HNO₃ and 5 ml of 5 percent KMnO₄ to the aeration bottle and mix well. Now, attach the bottle section to the bubbler section of the aeration cell and make certain that (1) the aeration cell exit arm stopcock (Figure 101-3 of Method 101) is closed (so that Hg will not prematurely enter the optical cell when the reducing agent is being added) and (2) there is no flow through the bubbler. Add 5 ml of sodium chloride hydroxylamine in 1-ml increments until the solution is colorless. Now add 5 ml of tin (II) solution to the aeration bottle through the side arm, and immediately stopper the side arm. Stir the solution for 15 seconds, turn on the recorder, open the aeration cell exit arm stopcock, and immediately initiate aeration with continued stirring. Determine the maximum absorbance of the standard and set this value to read 90 percent of the recorder full scale.

9. Calculations

9.1 Dry Gas Volume, Volume of Water Vapor and Moisture Content, Stack Gas Velocity, Isokinetic Variation and Acceptable Results, and Determination of Compliance. Same as Method 101, sections 9.1, 9.2, 9.3,

9.6, and 9.7, respectively, except use data obtained from this test.

9.2 Total Mercury. For each source sample, correct the average maximum absorbance of the two consecutive samples whose peak heights agreed within ± 3 percent of their average for the contribution of the field blank. Then calculate the total Hg content in μg in each sample. Correct for any dilutions made to bring the sample into the working range of the spectrophotometer.

9.3 Mercury Emission Rate. Calculate the Hg emission rate R in g/day for continuous operations using Equation 101A-1. For cyclic operations, use only the time per day each stack is in operation. The total Hg emission rate from a source will be the summation of results from all stacks.

$$R = K \frac{m_{\text{Hg}} v_s A_s (86,400 \times 10^{-9})}{(V_{\text{std}} + V_{\text{std}})(T_s/P_s)}$$

Eq. 101A-1

Where:

m_{Hg} = Total Hg content in each sample, μg .

v_s = Average stack gas velocity, m/sec (fps).

A_s = Stack cross-sectional area, $\text{m}^2 (\text{ft}^2)$.

86,400 = Conversion factor, sec/day.

10^{-6} = Conversion factor, g/ μg .

V_{std} = Dry gas sample volume at standard conditions, corrected for leakage (if any), $\text{m}^3 (\text{ft}^3)$.

V_{std} = Volume of water vapor at standard conditions, $\text{m}^3 (\text{ft}^3)$.

T_s = Absolute average stack gas temperature, $^\circ\text{K} (^\circ\text{R})$.

P_s = Absolute stack gas pressure, mm Hg (in. Hg).

K = 0.3858 $^\circ\text{K}/\text{mm Hg}$ for metric units.

= 17.64 $^\circ\text{R}/\text{in. Hg}$ for English units.

10. Bibliography

1. Same as Method 101, Section 10.

2. Mitchell, W. J., M. R. Midgett, J. C. Suggs, and D. Albrinck. Test Methods to Determine the Mercury Emissions from Sludge Incineration Plants. U.S. Environmental Protection Agency, Research Triangle Park, North Carolina. Publication No. EPA-600/4-79-058. September 1979.

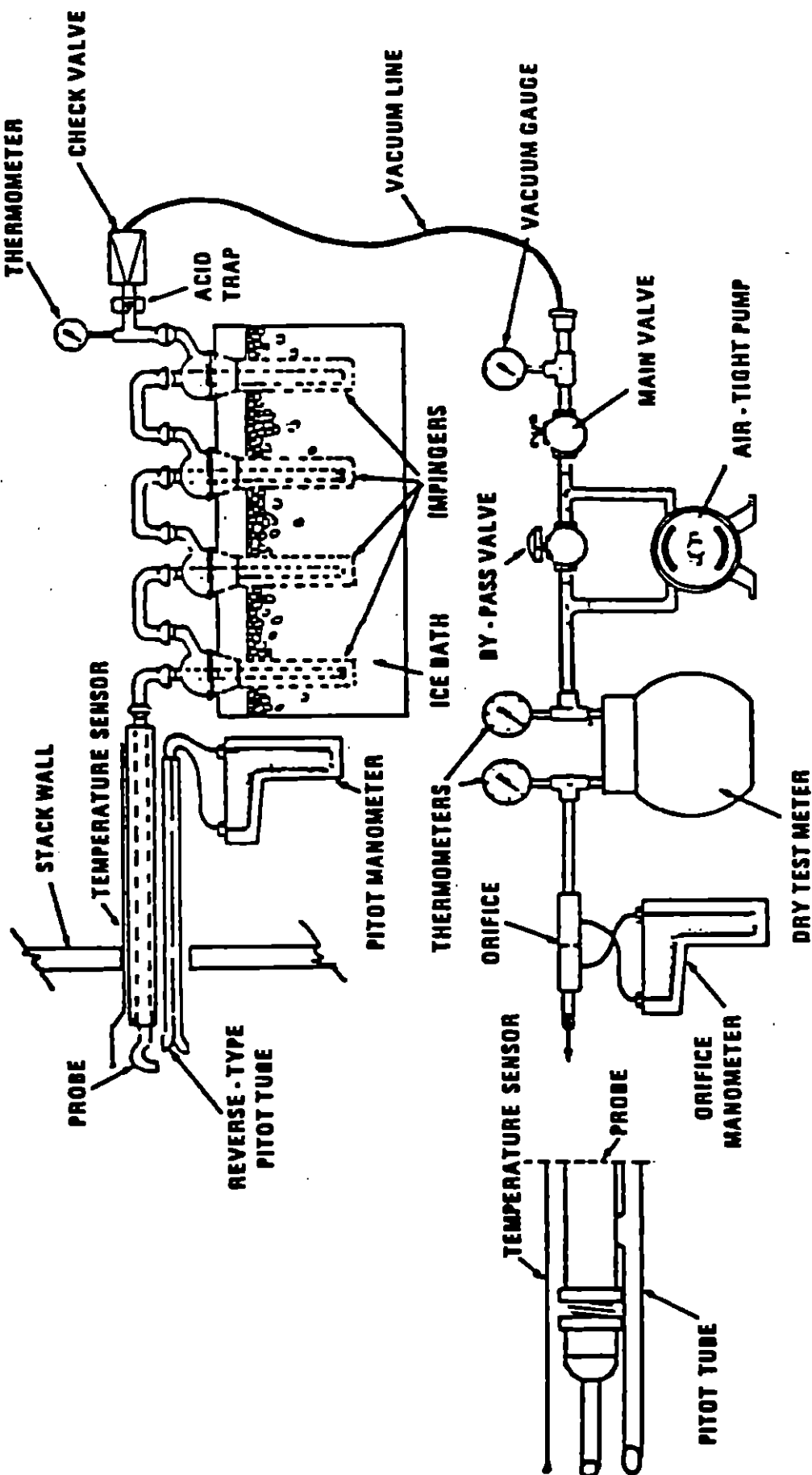


Figure 101-1 Mercury sampling train.

APPENDIX G

CALCULATION EQUATIONS

CALCULATION EQUATIONS

METHOD 2

$$\bar{V}_s = 95.48 C_p (\sqrt{\Delta p})_{avg} \sqrt{\frac{T_{s(avg)}}{P_s M_s}}$$

$$Q_{s,d} = 60(1 - B_{ws}) \bar{V}_s A \left(\frac{528}{T_{s(avg)}}\right) \left(\frac{P_s}{29.92}\right)$$

$$Q_a = 60 \bar{V}_s A$$

$$\dot{m}_g = \frac{4.995 Q_{s,d} G_d}{1 - B_{ws}}$$

$$RH^* = 100 (vp_{twb} 0.0003641 P_s (T_{db} - T_{wb}))/vp_{tdb}$$

$$B_{ws}^* = RH(vp_{tdb})/P_s$$

$$= \frac{4.585 \times 10^{-2} P_s M_s}{T_s (avg)}$$

*Alternate equations for calculating moisture content from wet bulb and dry bulb data.

SYMBOLS

A	= Cross sectional area of stack, SQ. FT.
A_n	= Cross sectional area of nozzle, SQ. FT.
B_{ws}	= Water vapor in gas stream, proportion by volume
C_p	= Pitot tube coefficient, dimensionless
C_a	= Concentration of particulate matter in stack gas, wet basis, GR/ACF
C_s	= Concentration of particulate matter in stack gas, dry basis, corrected to standard conditions, GR/DSCF
EA	= Excess air, percent by volume
γ	= Dry test meter correction factor, dimensionless
G_d	= Specific gravity (relative to air), dimensionless
I	= Isokinetic variation, percent by volume
M_d	= Molecular weight of stack gas, dry basis, g/g - mole.
$\dot{m}_g$	= Mass flow of wet flue gas, LB/HR
$\dot{m}_p$	= Particulate mass flow, LB/HR
M_s	= Molecular weight of stack gas, wet basis, g/g, mole.
M_p	= Total amount of particulate matter collected, g
P_{bar}	= Atmospheric pressure, IN. HG. (uncompensated)
P_g	= Stack static gas pressure, IN. WC.

P_s	= Absolute pressure of stack gas, IN.HG.
P_{std}	= Standard absolute pressure, 29.92 IN. HG.
A_a	= Actual volumetric stack gas flow rate, ACFM
$Q_{s,d}$	= Dry volumetric stack gas flow rate corrected to standard conditions, DSCFM
RH	= Relative humidity, %
T_{db}	= Dry bulb temperature of stack gas, °F
T_{wb}	= Wet bulb temperature of stack gas, °F
$T_m(avg)$	= Absolute average dry gas meter temperature, °R
$T_s(avg)$	= Absolute average stack temperature, °F
T_{std}	= Standard absolute temperature, 528 °F (68 °F)
θ	= Total sampling time, min.
V_{lc}	= Total volume of liquid collected in impingers and silica gel, ml
V_m	= Volume of gas sample as measured by dry gas meter, CF
$V_m(std)$	= Volume of gas sample measured by the dry gas meter corrected to standard conditions, DSCF
$V_w(std)$	= Volume of water vapor in the gas sample corrected to standard conditions, SCF
$\bar{V}_s$	= Average actual stack gas velocity, FT/SEC
$v_{p_{tdb}}$	= Vapor pressure at T_{db} , IN. HG.

- $v_{p_{twb}}$ = Vapor pressure at T_{wb} , IN. HG
- $\overline{\Delta H}$ = Average pressure differential across the orifice
meter, IN. WC.
- ΔP = Velocity pressure of stack gas, IN. WC.
- γ = Dry test meter correction coefficient, dimensionless
- ρ = Actual gas density, LB/ACF

CALCULATION EQUATIONS

METHOD 3

$$\%EA = \frac{100(\%O_2 - .5\% CO)}{0.264\% N_2 - \%O_2 + 0.5\% CO}$$

$$M_d = 0.44(\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)$$

$$M_s = M_d (1 - B_{ws}) + 0.18 B_{ws}$$

$$B_{ws} = \frac{V_{w(std)}}{V_{w(std)} + V_{m(std)}}$$

CALCULATION EQUATIONS

METHOD 5

$$V_{m(std)} = 17.65 V_m \gamma \left(\frac{P_{bar} + \overline{\Delta H}/13.6}{T_{m(avg)}} \right)$$

$$V_{w(std)} = 0.0472 V_{Is}$$

$$B_{ws} = \frac{V_{w(std)}}{V_{w(std)} + V_{m(std)}}$$

$$I = 0.0944 \left(\frac{T_{s(avg)} V_{m(std)}}{P_s V_s A_n \theta (1 - B_{ws})} \right)$$

$$C_s = \frac{15.43 M_p}{V_{m(std)}}$$

$$C_a = \frac{272.3 M_p P_s}{T_{s(avg)} (V_{w(std)} + V_{m(std)})}$$

$$(\dot{m}_p)_1 = 8.5714 \times 10^{-3} C_s Q_{s,d}$$

$$(\dot{m}_p)_2 = \frac{1.3228 \times 10^{-1} M_p A}{\theta A_n}$$

$$\dot{m}_p = \frac{(\dot{m}_p)_1 + (\dot{m}_p)_2}{2}$$

SYMBOLS

A	= Cross sectional area of stack, SQ. FT.
A_n	= Cross sectional area of nozzle, SQ. FT.
B_{ws}	= Water vapor in gas stream, proportion by volume
C_p	= Pitot tube coefficient, dimensionless
C_a	= Concentration of particulate matter in stack gas, wet basis, GR/ACF
C_s	= Concentration of particulate matter in stack gas, dry basis, corrected to standard conditions, GR/DSCF
EA	= Excess air, percent by volume
γ	= Dry test meter correction factor, dimensionless
G_d	= Specific gravity (relative to air), dimensionless
I	= Isokinetic variation, percent by volume
M_d	= Molecular weight of stack gas, dry basis, g/g - mole.
$\dot{m}_g$	= Mass flow of wet flue gas, LB/HR
$\dot{m}_p$	= Particulate mass flow, LB/HR
M_s	= Molecular weight of stack gas, wet basis, g/g, mole.
M_p	= Total amount of particulate matter collected, g
P_{bar}	= Atmospheric pressure, IN. HG. (uncompensated)
P_g	= Stack static gas pressure, IN. WC.

P_s	= Absolute pressure of stack gas, IN.HG.
P_{std}	= Standard absolute pressure, 29.92 IN. HG.
A_a	= Actual volumetric stack gas flow rate, ACFM
$Q_{s,d}$	= Dry volumetric stack gas flow rate corrected to standard conditions, DSCFM
RH	= Relative humidity, %
T_{db}	= Dry bulb temperature of stack gas, °F
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$\bar{V}_s$	= Average actual stack gas velocity, FT/SEC
$v_{p_{tdb}}$	= Vapor pressure at T_{db} , IN. HG.

$v_{p_{twb}}$ = Vapor pressure at T_{wb} , IN. HG

$\overline{\Delta H}$ = Average pressure differential across the orifice meter, IN. WC.

ΔP = Velocity pressure of stack gas, IN. WC.

γ = Dry test meter correction coefficient, dimensionless

ρ = Actual gas density, LB/ACF

Mercury Mass Balance

NSP - SHERCO

Units 1&2

Run	Coal Feed TPH	LB/HR	Potential Hg Emission Rate LB/HR
1	764	1528000	0.138
2	775	1550000	0.140
3	766	1532000	0.136

Unit 3

Run	Coal Feed TPH	LB/HR	Potential Hg Emission Rate LB/HR
1	490	980000	0.0882
2	494	988000	0.0889
3	503	1006000	0.0905

Mercury in Coal Sample

0.09 ug/kg 9.00E-08 lb/lb