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AP-42 Section Number: 1.8

Reference Number: 16

Title: Source Test Report for Particulate
Emissions Twin Impingement Wet
Scrubber Number 4 Boiler: Talisman
Sugar Corporation

February 1991

SOURCE TEST REPORT
for
PARTICULATE EMISSIONS

TWIN IMPINGEMENT WET SCRUBBER
NUMBER 4 BOILER

TALISMAN SUGAR CORPORATION
SOUTH BAY, FLORIDA

FEBRUARY 11. 1991

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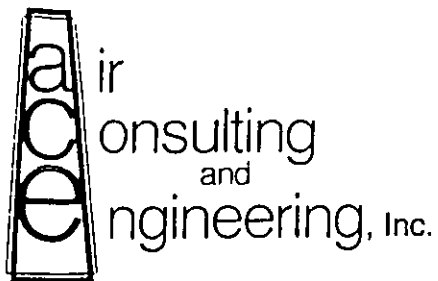
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REPORT CERTIFICATION

To the best of my knowledge, all applicable field and analytical procedures comply with Florida Department of Environmental Regulation requirements and all test data and plant operating data are true and correct.

Stephen L. Neck
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State of Florida
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3-23-91
Date

2nd SUBMITTAL

SEAL

1.0 INTRODUCTION

Personnel from Air Consulting and Engineering, INC. (ACEI) performed annual source emission compliance testing for the Talisman Sugar Corporation in South Bay, Florida on February 11, 1991. Testing was performed at the Number 4 Boiler wet scrubber outlets.

Testing was designed to fulfill "specific conditions" of the current Florida Department of Environmental Regulation (FDER) operating permit.

Four United States Environmental Protection Agency (USEPA) Method 5 particulate matter (PM) test runs were conducted while the plant was documented to be operating within 10% of permitted production.

Mr. Frank Kleeman served as test coordinator and certified production rates. ACEI performed this work under subcontract to Kleeman Engineering, Inc.

Mr. Ken Tucker of the Florida Department of Environmental Regulation (FDER) witnessed most of the testing.

2.0 SUMMARY and DISCUSSION of RESULTS

Results of the emission testing are provided in Table 1. Complete emission data are located in the report appendices.

The source was found to be operating within full compliance of permit conditions. Stack emissions averaged 64.55 pounds per hour (LB/HR) and 0.271 pounds per million btu (LB/MMBTU) heat input against a "process rate" basis allowable emission of 0.300 LB/MMBTU. Permit conditions limit emissions to 0.10 LB/MMBTU from oil and 0.300 LB/MMBTU from bagasse firing. No oil was used during compliance testing.

Production rate summaries are provided in Appendix A. These data were taken from control room recordings of steam flow, temperature, and pressure as well as feedwater temperature and pressure (Appendix E). Steam integrator readings were recorded at the beginning and end of each particulate test run by Mr. Frank Kleeman.

Due to a cracked filter holder, the final leak check for test Run 3 was excessive. This test result has been excluded from the emission averages.

TABLE 1
EMISSION SUMMARY
TALISMAN SUGAR CORPORATION
NUMBER 4 BOILER
FEBRUARY 11, 1991

RUN NUMBER	TIME	ACTUAL EMISSIONS		ALLOWABLE EMISSIONS	
		LB/HR	LB/MMBTU	LB/HR	LB/MMBTU
1	0835-1014 39	62.79	0.265	71.20	0.300
2	1110-1246	63.84	0.259	73.86	0.300
3	1345-1521 36	26.64	0.110	72.36	0.300
4	1700-1839 39	67.01	0.289	69.51	0.300
AVERAGES	----- 58	64.55	0.271	71.52	0.300

* RUN 3 NOT INCLUDED

3.0 PROCESS DESCRIPTION AND OPERATION

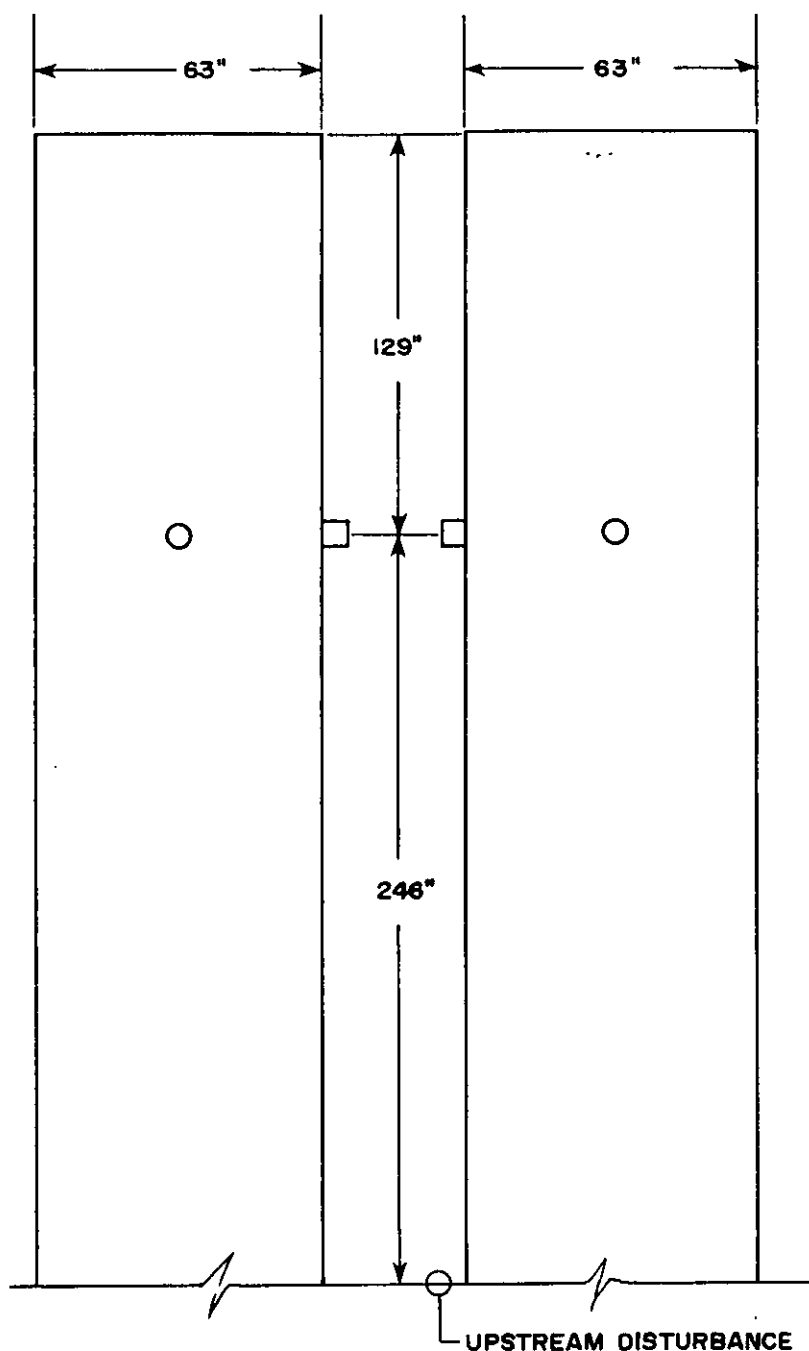
The Number 4 Boiler at the Talisman Sugar Corporation is a traveling grate stoker design used primarily for bagasse fuel firing. Supplemental oil firing may also be utilized but was not used during the emission test series.

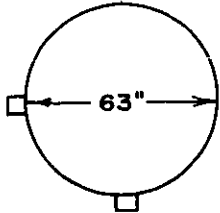
The boiler averaged 122,201 pounds per hour steam production over the Run Numbers 1, 2 and 4 test period.

Oil meters, steam integrators, and other production monitoring devices were rigorously calibrated prior to the production season.

4.0 SAMPLING POINT LOCATION

The sampling point location and outlet duct schematic are provided in Figure 1.



	
TRAVERSE POINT NUMBER	INCHES INSIDE STACK WALL
1	1.3
2	4.2
3	7.4
4	11.2
5	15.8
6	22.4
7	40.6
8	47.3
9	51.8
10	55.6
11	58.8
12	61.7

NOTE: NOT TO SCALE

**FIGURE 1.
SAMPLING POINT LOCATION
BOILER NO. 4
TALISMAN SUGAR CORPORATION
SOUTH BAY, FLORIDA**

**AIR CONSULTING
and
ENGINEERING**

5.0 FIELD and ANALYTICAL PROCEDURES- USEPA METHOD 5

Particulate matter samples were collected by the emission measurement method specified by the United States Environmental Protection Agency. A schematic diagram of the sampling train used is provided in Figure 2. All particulate matter captured from the nozzle to and including the filter was included in the calculation of the emission rate of particulate matter.

PREPARATION OF EQUIPMENT

1. FILTERS- Gelman type "A" glass fiber filters were placed in a drying oven for two hours at 105 degrees C, removed and placed in a standard desiccator containing indicating silica gel, allowed to cool for two hours, and weighed to the nearest 0.1 mg. The filters were then re-desiccated for a minimum of six hours and weighed to a constant weight (less than 0.5 mg change from previous weighing). The average of the two constant weights was used as the tare value.
2. NOZZLE, FILTER HOLDER, AND SAMPLING PROBE - The nozzle, filter holder, and sampling probe were washed vigorously with soapy water and brushes, rinsed with distilled water and acetone, and dried prior to the test program. All openings on the equipment were sealed while in transit to the test site.
3. IMPINGERS - The Greenburg-Smith impingers were cleaned, rinsed, and dried as in 2. The impingers were also sealed during transit.

TEST PROCEDURE

Prior to performing the actual particulate matter sample runs, certain stack and stack gas parameters were measured. These preliminary measurements included the average gas temperature, the stack gas velocity head, the stack gas moisture content, and the dimensions at the point where the tests were to be performed. The stack temperature was determined using a bi-metallic thermocouple and calibrated

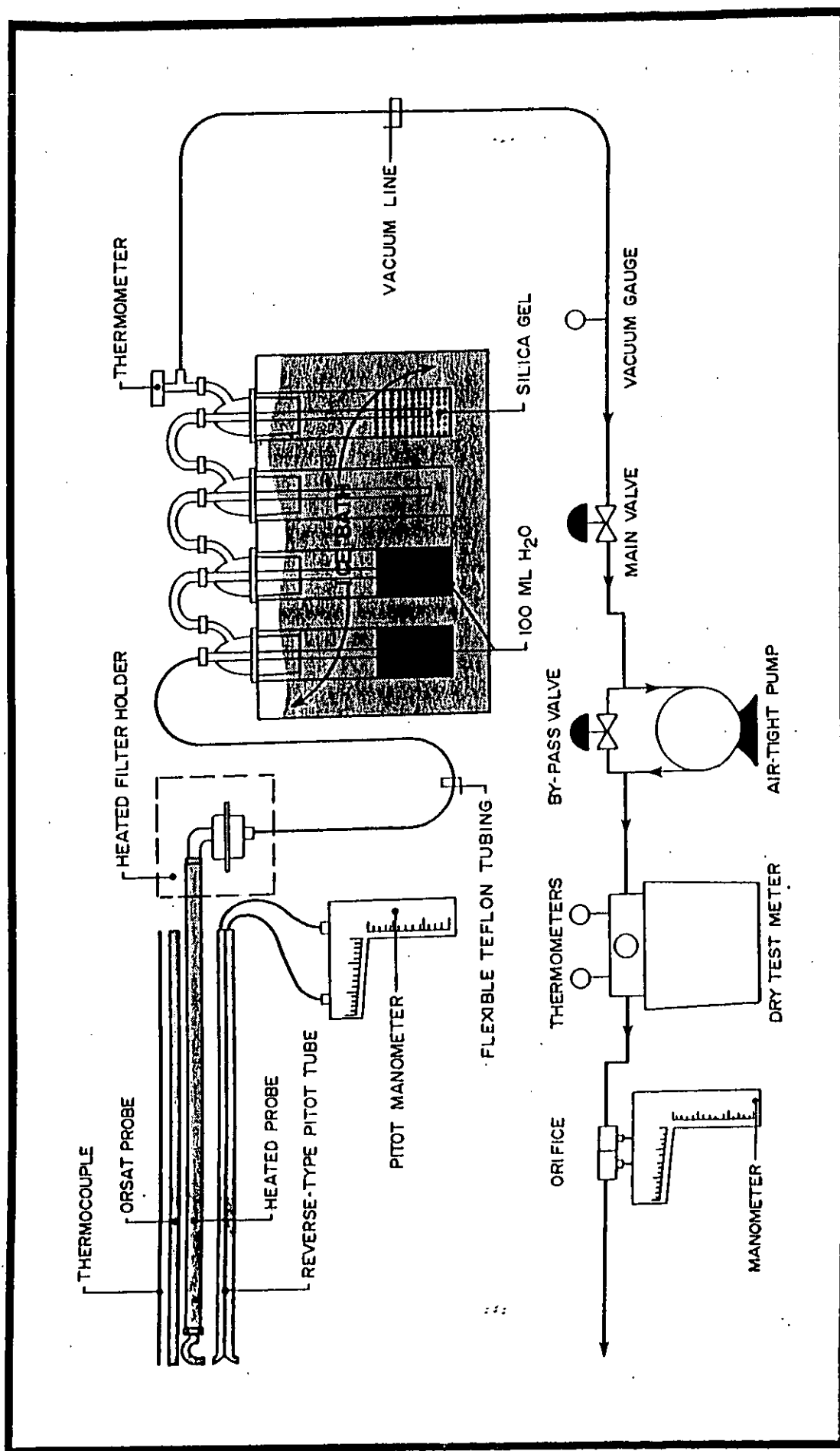


FIGURE 2
EPA METHOD 5 SAMPLING TRAIN

pyrometer. Velocity head measurements were made with a calibrated type "s" pitot tube and an inclined manometer. Velocity head measurements of 0.05 inches H₂O or less were measured using a micromonometer.

The sampling traverse points were selected so that a representative sample could be extracted from the gas stream. The traverse points were located in the center of equal areas, the number of which were dependent upon the distance upstream or downstream from flow disturbances. USEPA Methods 1 and 2 were utilized for this task.

Each particulate matter test run consisted of sampling for a specific amount of time at each point. The type "s" pitot tube was connected to the sampling probe so that an instantaneous velocity head measurement could be made at each traverse point while conducting the test run. The stack gas temperature was also measured at each traverse point. Together with assumed moisture and orsat knowledge as well as known nozzle area, calculations of "isokinetic" (equal energy or velocity) were quickly made and effected for each traverse point during the test run.

The gases sampled passed through the following components: a stainless steel nozzle and glass probe; a glass fiber filter; two impingers charged with 100 ml of distilled water each; one dry impinger; one impinger with 200 grams of silica gel desiccant; a flexible length of tubing; a leak free pump; a calibrated dry gas meter; and, finally, a calibrated flow orifice.

Sample recovery was accomplished in the following manner:

1. The pre-tared filter was removed from its holder and placed in Container 1 and sealed. (This is usually performed in the lab).
2. All sample-exposed surfaces prior to the filter were washed with acetone and placed in Container 2. The container was then sealed and the liquid level marked.
3. The volume of water from the first three impingers was measured for the purpose of calculating the moisture content of the stack gases, then discarded.
4. The silica gel from the fourth impinger was transferred to the original tared container and sealed.

LABORATORY ANALYSIS

The three sample containers from each sampler run were analyzed according to the following procedures:

1. The filter was either dried for two hours at 105 degrees C or desiccated for 24 hours at ambient temperature. Following desiccation, the filter was weighed to the nearest 0.1 mg. A minimum of two such weighings six hours apart were made with a variance of less than 0.5 mg.
2. The acetone from Container 2 was transferred to a tared beaker, evaporated to dryness, and weighed in the same manner as above.
3. The used silica gel in its tared container was weighed to the nearest 0.1 gram.

The total sample weight included the weight gains from Sample Containers 1 and 2.

DATA

All relevant field and lab data sheets as well as emission calculations are provided in the report appendices.

APPENDIX A
COMPLETE EMISSION DATA
AND
SAMPLE CALCULATIONS

AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

PLANT: TALISMAN SUGAR CORPORATION DATE: 2-11-91
LOCATION: SOUTH BAY, FLORIDA RUN NUMBER 1
SOURCE: NUMBER 4 BOILER, SCRUBBER OUTLET TIME: 0835-1011

TIME INTERVAL----- 96 MINUTES

OIL:

FINAL OIL----- 0
BEGIN OIL----- 0
FACTOR----- 1

STEAM:

FINAL STEAM----- 5738
BEGIN STEAM----- 3785
FACTOR----- 100
TEMPERATURE----- 575 DEGREES F
PRESSURE----- 285 PSIG
300 PSIA

FEEDWATER:

TEMPERATURE----- 260 DEGREES F
PRESSURE----- 420 PSIG
435 PSIA

HEAT INPUT:

STEAM----- 1298.1 BTU/LB
FEEDWATER----- 228.6 BTU/LB
NET STEAM----- 1069.5 BTU/LB
STEAM RATE----- 122063 LB/HR
BOILER EFFICIENCY----- 55.0 %
TOTAL FUEL HEAT INPUT----- 237.35 MMBTUH
STEAM CALIBRATION FACTOR----- 1.00

OIL----- 0.00 GPH
OIL----- 150000 BTU/GAL

TOTAL HEAT INPUT (OIL)----- 0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)----- 237.35 MMBTUH

ALLOWABLES:

ALLOWABLE EMISSION (OIL)----- .10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)----- .30 LB/MMBTU

TOTAL ALLOWABLE EMISSION----- 71.20 LB/HR
TOTAL ACTUAL EMISSION----- 60.91 LB/HR

TOTAL ALLOWABLE EMISSION----- 0.300 LB/MMBTU
TOTAL ACTUAL EMISSION----- 0.257 LB/MMBTU

AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

PLANT:	TALISMAN SUGAR CORPORATION	DATE:	2-11-91
LOCATION:	SOUTH BAY, FLORIDA	RUN NUMBER	2
SOURCE:	NUMBER 4 BOILER, SCRUBBER OUTLET	TIME:	1110-1246

TIME INTERVAL----- 96 MINUTES

OIL:

FINAL OIL-----	0
BEGIN OIL-----	0
FACTOR-----	1

STEAM:

FINAL STEAM-----	8983
BEGIN STEAM-----	6960
FACTOR-----	100
TEMPERATURE-----	572 DEGREES F
PRESSURE-----	281 PSIG
	296 PSIA

FEEDWATER:

TEMPERATURE-----	260 DEGREES F
PRESSURE-----	435 PSIG
	450 PSIA

HEAT INPUT:

STEAM-----	1299.6 BTU/LB
FEEDWATER-----	228.6 BTU/LB
NET STEAM-----	1071.0 BTU/LB
STEAM RATE-----	126438 LB/HR
BOILER EFFICIENCY-----	55.0 %
TOTAL FUEL HEAT INPUT-----	246.20 MMBTUH
STEAM CALIBRATION FACTOR-----	1.00

OIL-----	0.00 GPH
OIL-----	150000 BTU/GAL

TOTAL HEAT INPUT (OIL)-----	0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)-----	246.20 MMBTUH

ALLOWABLES:

ALLOWABLE EMISSION (OIL)-----	.10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)-----	.30 LB/MMBTU
TOTAL ALLOWABLE EMISSION-----	73.86 LB/HR
TOTAL ACTUAL EMISSION-----	62.00 LB/HR
TOTAL ALLOWABLE EMISSION-----	0.300 LB/MMBTU
TOTAL ACTUAL EMISSION-----	0.252 LB/MMBTU

AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

PLANT: TALISMAN SUGAR CORPORATION DATE: 2-11-91
LOCATION: SOUTH BAY, FLORIDA RUN NUMBER 3
SOURCE: NUMBER 4 BOILER, SCRUBBER OUTLET TIME: 1345-1521

TIME INTERVAL----- 96 MINUTES

OIL:

FINAL OIL----- 0
BEGIN OIL----- 0
FACTOR----- 1

STEAM:

FINAL STEAM----- 92166
BEGIN STEAM----- 90191
FACTOR----- 100
TEMPERATURE----- 579 DEGREES F
PRESSURE----- 282 PSIG
297 PSIA

FEEDWATER:

TEMPERATURE----- 260 DEGREES F
PRESSURE----- 440 PSIG
455 PSIA

HEAT INPUT:

STEAM----- 1303.4 BTU/LB
FEEDWATER----- 228.6 BTU/LB
NET STEAM----- 1074.8 BTU/LB
STEAM RATE----- 123438 LB/HR
BOILER EFFICIENCY----- 55.0 %
TOTAL FUEL HEAT INPUT----- 241.21 MMBTUH
STEAM CALIBRATION FACTOR----- 1.00

OIL----- 0.00 GPH
OIL----- 150000 BTU/GAL

TOTAL HEAT INPUT (OIL)----- 0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)----- 241.21 MMBTUH

ALLOWABLES:

ALLOWABLE EMISSION (OIL)----- .10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)----- .30 LB/MMBTU

TOTAL ALLOWABLE EMISSION----- 72.36 LB/HR
TOTAL ACTUAL EMISSION----- 25.14 LB/HR

TOTAL ALLOWABLE EMISSION----- 0.300 LB/MMBTU
TOTAL ACTUAL EMISSION----- 0.104 LB/MMBTU

AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

PLANT: TALISMAN SUGAR CORPORATION	DATE: 2-11-91
LOCATION: SOUTH BAY, FLORIDA	RUN NUMBER 4
SOURCE: NUMBER 4 BOILER, SCRUBBER OUTLET	TIME: 1700-1838

TIME INTERVAL----- 98 MINUTES

OIL:

FINAL OIL-----	0
BEGIN OIL-----	0
FACTOR-----	1

STEAM:

FINAL STEAM-----	996119
BEGIN STEAM-----	994190
FACTOR-----	100
TEMPERATURE-----	585 DEGREES F
PRESSURE-----	270 PSIG
	285 PSIA

FEEDWATER:

TEMPERATURE-----	260 DEGREES F
PRESSURE-----	450 PSIG
	465 PSIA

HEAT INPUT:

STEAM-----	1307.6 BTU/LB
FEEDWATER-----	228.6 BTU/LB
NET STEAM-----	1079.0 BTU/LB
STEAM RATE-----	1181.02 LB/HR
BOILER EFFICIENCY-----	55.0 %
TOTAL FUEL HEAT INPUT-----	231.69 MMBTUH
STEAM CALIBRATION FACTOR-----	1.00

OIL-----	0.00 GPH
OIL	150000 BTU/GAL

TOTAL HEAT INPUT (OIL)-----	0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)	231.69 MMBTUH

ALLOWABLES:

ALLOWABLE EMISSION (OIL)-----	.10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)	.30 LB/MMBTU
TOTAL ALLOWABLE EMISSION-----	69.51 LB/HR
TOTAL ACTUAL EMISSION	64.79 LB/HR
TOTAL ALLOWABLE EMISSION-----	0.300 LB/MMBTU
TOTAL ACTUAL EMISSION	0.280 LB/MMBTU

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AIR CONSULTING and ENGINEERING
COMPLETE EMISSION DATA

PLANT: TALISMAN SUGAR CORPORATION
SOURCE: NUMBER 4 BOILER
DATE: 2-11-91

RUN NO.:	1	IMPINGER ml	235
BEGIN TIME:	0835	SILICA GEL gms.	12.8
END TIME:	1014	PERCENT O2	7.50
TOTAL RUN TIME:	96.00 min.	PERCENT CO2	12.70
BAROMETRIC PRESSURE:	30.00 "Hg	"F" FACTOR	0
STACK PRESSURE:	30.00 "Hg.		
NOZZLE DIAMETER:	.205 inches	PARTICULATE	
METER CORR. FACTOR:	.994	-----	
FINAL METER:	355.379 cubic ft.	FILTER mg.	217.8
INITIAL METER:	325.555 cubic ft.	WASH mg.	9.2
STACK AREA:	43.295 sq. ft.		

STACK 1 DATA INPUTS

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIF. DIFF.	STACK TEMP.	METER TEMP.
-----	-----	-----	-----	-----	-----
1-1	.550	0.742	.520	154	5
1-2	.700	0.837	.660	153	5
1-3	.710	0.843	.660	154	5
1-4	.660	0.812	.620	154	5
1-5	.410	0.640	.390	155	5
1-6	.240	0.490	.230	155	5
1-7	.310	0.557	.290	154	5
1-8	.400	0.632	.380	154	5
1-9	.420	0.648	.400	157	5
1-10	.440	0.663	.410	155	5
1-11	.520	0.721	.490	150	5
1-12	.480	0.693	.450	150	5
2-1	.140	0.374	.130	155	5
2-2	.140	0.374	.130	154	5
2-3	.160	0.400	.140	154	5
2-4	.120	0.346	.110	154	6
2-5	.160	0.400	.140	155	6
2-6	.180	0.424	.170	155	6
2-7	.280	0.529	.260	155	6
2-8	.430	0.656	.400	154	6
2-9	.560	0.748	.530	155	6
2-10	.620	0.787	.580	154	6
2-11	.650	0.806	.550	154	6
2-12	.620	0.787	.580	150	6
AVERAGES	0.413	0.621	0.384	154	5

EMISSION RESULTS

NOZZLE DIA. (SQ.FT.):	0.0002295		
AVG. VELOCITY HEAD	:-----	0.36 "H2O	VOL. FLOW ACFM : 9818
AVG. STACK TEMP.:	-----	154 F	VOL. FLOW SCFMD : 6075
AVG. METER TEMP.:	-----	65 F	
AVG. ORIFICE DIFFERENTIAL:	---	0.37 "H2O	PARTICULATE DATA :
METER STANDARD CUBIC FEET:	---	29.946	-----
% H2O VAPOR:	:-----	28.2	POUNDS PER HOUR: 60.91
GAS MOL. WT. DRY:	-----	30.33	POUNDS PER SCF : 0.000016
GAS MOL. WT. WET:	-----	26.85	GRAINS/SCF: 0.11
% EXCESS AIR:	-----	55.28	GRAINS/SCF @ 8% O2 0.11
AVG. STACK VEL. (FPS)	-----	37.80	GRAINS/SCF @50% EA 0.12
MMBTU INPUT:	-----	237.35	POUNDS PER MMBTU: 0.25
PERCENT ISOKINETIC	:-----	96.85	

RUN 1 (cont.)

STACK 2 DATA INPUTS

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIFICE DIFF.	STACK TEMP.	METER TEMP.
1-1	.380	0.616	.360	153	66
1-2	.380	0.616	.360	154	67
1-3	.310	0.557	.290	154	67
1-4	.370	0.608	.350	154	68
1-5	.390	0.624	.370	154	68
1-6	.350	0.592	.330	155	69
1-7	.270	0.520	.250	155	69
1-8	.250	0.500	.230	155	70
1-9	.310	0.557	.290	155	70
1-10	.310	0.557	.290	155	71
1-11	.320	0.566	.300	154	71
1-12	.320	0.566	.300	155	72
2-1	.220	0.469	.210	155	72
2-2	.220	0.469	.210	154	73
2-3	.220	0.469	.210	155	73
2-4	.250	0.500	.250	155	73
2-5	.250	0.500	.250	155	74
2-6	.220	0.469	.250	155	74
2-7	.420	0.648	.420	155	75
2-8	.460	0.678	.460	155	75
2-9	.530	0.728	.580	155	75
2-10	.550	0.742	.600	154	76
2-11	.560	0.748	.600	155	76
2-12	.520	0.721	.600	154	76
AVERAGES	0.349	0.584	0.348	155	72

SAMPLE CALCULATIONS - RUN 1

NOZZLE AREA (FT.2)	$(D_n/12)!2 \times 3.1416/4$	0.000229
AVG. VELOCITY HEAD:	$(AVG.SQ.RT.)!2$	38.96
METER STND. FT3:	$(M_f-M_i) \times MCF \times (AVG.ORF.DIFF./13.6))/29.92) \times (528/(T_m+460))$	29.950
PERCENT H2O:	$((IMP+SG) \times ((IMP+SG) \times .0474) + SCF) \times 100$	
Mw DRY:	$((O_2\% \times .32) + CO_2\% \times .44) + (100 - (O_2\% + CO_2\%)) \times .28$	30.33
Mw WET:	$(Mw DRY \times (1 - \%H_2O/100)) + \%H_2O \times .18$	26.85
% EXCESS AIR:	$\%O_2 / (((100 - (\%O_2 + \%CO_2)) \times .264) - \%O_2) \times 100$	55.28
STACK VEL. (FPS):	$85.49 \times .84 \times (AVG.SQ.RT.VEL.HD.) \times ((Ts + 460)/(Ps \times MwWET))! .5$	38.96
% ISOKINETIC:	$((Ts + 460) \times SCF \times 2992) / (528 \times FPS \times TIME \times A_n \times Ps \times 60 \times (1 - \%O_2/100))$	94.06
VOL. FLOW (ACFM):	$FPS \times 60 \times A_s$	101206
STND. FLOW (SCFMD):	$ACFM \times 528 / (Ts + 460) \times (1 - \%H_2O/100) \times (Ps/29.92)$	62652
PARTICULATE LB/HR:	$PROBE + FILTER \text{ mg.} / 453600 \times (SCFMD / SCF) \times 60$	62.813
PARTICULATE LB/SCF):	$PROBE + FILTER \text{ mg.} / 453600 / SCF$	0.0000167
GRAINS/SCF:	$LB/SCF \times 7000$	0.1170
GR/SCF @ 8% O2:	$(12.9 / (20.9 - \%O_2)) \times GR/SCF$	0.1126
GR/SCF @ 50% E.A.:	$GR/SCF \times ((100 + \%E.A.) / 150)$	0.1211
LB/MMBTU:	$(LB/HR) / (LB/MMBTUH)$	0.000
LB/MMBTU "F" FACTOR:	$LB/SCF \times "F" \text{ FACTOR} \times (20.9 / 20.9 - \%O_2)$	0.000

NOTE: THESE ARE EXAMPLE CALCULATIONS,
 DERIVED SOLUTIONS FOR THIS CASE
 DIFFER FROM ACTUAL SOLUTIONS DUE
 TO DIFFERENCES IN INPUT DATA.

AIR CONSULTING and ENGINEERING
COMPLETE EMISSION DATA

PLANT: TALISMAN SUGAR CORPORATION
SOURCE: NUMBER 4 BOILER
DATE: 2-11-91

RUN NO.:	2	IMPINGER ml	305
BEGIN TIME:	1110	SILICA GEL gms.	12.8
END TIME:	1251	PERCENT O2	7.70
TOTAL RUN TIME:	96.00 min.	PERCENT CO2	12.50
BAROMETRIC PRESSURE:	30.00 "Hg	"F" FACTOR	0
STACK PRESSURE:	30.00 "Hg.		
NOZZLE DIAMETER:	.230 inches	PARTICULATE	
METER CORR. FACTOR:	.994	-----	
FINAL METER:	393.410 cubic ft.	FILTER mg.	274.8
INITIAL METER:	355.640 cubic ft.	WASH mg.	21.3
STACK AREA:	43.295 sq. ft.		

STACK 1 DATA INPUTS

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIF. DIFF.	STACK TEMP.	METER TEMP.
-----	-----	-----	-----	-----	-----
1-1	.640	0.800	1.100	153	7
1-2	.660	0.812	1.120	153	7
1-3	.690	0.831	1.170	154	7
1-4	.550	0.742	.940	153	7
1-5	.500	0.707	.850	154	7
1-6	.380	0.616	.650	154	7
1-7	.280	0.529	.480	154	7
1-8	.380	0.616	.650	154	7
1-9	.430	0.656	.730	154	7
1-10	.250	0.500	.420	154	7
1-11	.490	0.700	.830	154	7
1-12	.490	0.700	.830	155	7
2-1	.130	0.361	.220	154	8
2-2	.150	0.387	.240	153	8
2-3	.150	0.387	.240	154	8
2-4	.140	0.374	.240	154	8
2-5	.150	0.387	.240	155	8
2-6	.160	0.400	.270	154	8
2-7	.200	0.447	.340	155	8
2-8	.330	0.574	.560	154	8
2-9	.330	0.574	.560	154	8
2-10	.580	0.762	1.000	154	8
2-11	.600	0.775	1.000	154	8
2-12	.580	0.762	1.000	150	8
AVERAGES	0.385	0.600	0.653	154	7

EMISSION RESULTS

NOZZLE DIA. (SQ. FT.):	0.0002889		
AVG. VELOCITY HEAD :	0.34 "H2O	VOL. FLOW ACFM :	9512
AVG. STACK TEMP.:	154 F	VOL. FLOW SCFMD :	5812
AVG. METER TEMP.:	82 F		
AVG. ORIFICE DIFFERENTIAL:---	0.60 "H2O	PARTICULATE DATA :	
METER STANDARD CUBIC FEET:---	36.721	-----	
% H2O VAPOR:	29.1	POUNDS PER HOUR:	61.99
GAS MOL. WT. DRY:	30.31	POUNDS PER SCF :	0.000017
GAS MOL. WT. WET:	26.72	GRAINS/SCF:	0.12
% EXCESS AIR:	57.60	GRAINS/SCF @ 8% O2	0.12
AVG. STACK VEL. (FPS)-----	36.62	GRAINS/SCF @ 50% EA	0.13
MMBTU INPUT:	246.20	POUNDS PER MMBTU:	0.25
PERCENT ISOKINETIC :-----	98.61		

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIFICE DIFF.	STACK TEMP.	METER TEMP.
1-1	.310	0.557	.530	153	83
1-2	.350	0.592	.600	153	83
1-3	.330	0.574	.560	154	84
1-4	.340	0.583	.580	154	84
1-5	.360	0.600	.610	154	85
1-6	.360	0.600	.610	155	85
1-7	.240	0.490	.400	155	85
1-8	.220	0.469	.370	154	85
1-9	.240	0.490	.400	154	85
1-10	.280	0.529	.480	155	85
1-11	.320	0.566	.540	154	85
1-12	.320	0.566	.540	154	86
2-1	.240	0.490	.400	154	86
2-2	.240	0.490	.400	154	86
2-3	.240	0.490	.400	155	86
2-4	.230	0.480	.390	155	86
2-5	.230	0.480	.390	155	86
2-6	.210	0.458	.350	155	86
2-7	.330	0.574	.560	155	86
2-8	.430	0.656	.730	154	86
2-9	.470	0.686	.800	155	86
2-10	.530	0.728	.900	154	86
2-11	.530	0.728	.900	155	86
2-12	.480	0.693	.820	153	86
AVERAGES	0.326	0.565	0.553	154	85

AIR CONSULTING and ENGINEERING
COMPLETE EMISSION DATA

PLANT: TALISMAN SUGAR CORPORATION
SOURCE: NUMBER 4 BOILER
DATE: 2-11-91

RUN NO.:	3	IMPINGER ml	100
BEGIN TIME:	1345	SILICA GEL gms.	7.0
END TIME:	1535	PERCENT O2	7.70
TOTAL RUN TIME:	96.00 min.	PERCENT CO2	12.70
BAROMETRIC PRESSURE:	30.00 "Hg	"F" FACTOR	0
STACK PRESSURE:	30.00 "Hg.		
NOZZLE DIAMETER:	.230 inches	PARTICULATE	
METER CORR. FACTOR:	.994	-----	
FINAL METER:	434.586 cubic ft.	FILTER mg.	102.6
INITIAL METER:	393.761 cubic ft.	WASH mg.	4.4
STACK AREA:	43.295 sq. ft.		

STACK 1 DATA INPUTS

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIF. DIFF.	STACK TEMP.	METER TEMP.
-----	-----	-----	-----	-----	-----
1-1	.760	0.872	1.350	155	8
1-2	.760	0.872	1.350	155	8
1-3	.760	0.872	1.350	155	8
1-4	.700	0.837	1.260	158	8
1-5	.650	0.806	1.170	156	8
1-6	.280	0.529	.500	156	8
1-7	.280	0.529	.500	154	8
1-8	.320	0.566	.580	157	8
1-9	.420	0.648	.760	155	8
1-10	.520	0.721	.940	154	8
1-11	.460	0.678	.820	155	8
1-12	.460	0.678	.820	155	8
2-1	.100	0.316	.180	156	8
2-2	.050	0.224	.090	155	8
2-3	.080	0.283	.140	156	8
2-4	.140	0.374	.250	156	8
2-5	.130	0.361	.230	155	8
2-6	.190	0.436	.340	155	8
2-7	.270	0.520	.490	156	8
2-8	.420	0.648	.760	156	8
2-9	.470	0.686	.850	156	8
2-10	.570	0.755	1.000	156	9
2-11	.620	0.787	1.100	156	9
2-12	.620	0.787	1.100	155	9
AVERAGES	0.418	0.616	0.747	156	8

EMISSION RESULTS

NOZZLE DIA. (SQ.FT.):	0.0002889		
AVG. VELOCITY HEAD	:-----	0.34 "H2O	VOL. FLOW ACFM : 9131
AVG. STACK TEMP.:	-----	155 F	VOL. FLOW SCFMD : 6956
AVG. METER TEMP.:	-----	89 F	
AVG. ORIFICE DIFFERENTIAL:	---	0.65 "H2O	PARTICULATE DATA :
METER STANDARD CUBIC FEET:	---	39.160	-----
% H2O VAPOR:	:-----	11.5	POUNDS PER HOUR: 25.14
GAS MOL. WT. DRY:	-----	30.34	POUNDS PER SCF : 0.000006
GAS MOL. WT. WET:	-----	28.92	GRAINS/SCF: 0.04
% EXCESS AIR:	-----	57.83	GRAINS/SCF @ 8% O2 0.04
AVG. STACK VEL. (FPS)	-----	35.15	GRAINS/SCF @50% EA 0.04
MMBTU INPUT:	-----	241.21	POUNDS PER MMBTU: 0.10
PERCENT ISOKINETIC	:-----	87.87	

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIFICE DIFF.	STACK TEMP.	METER TEMP.
1-1	.300	0.548	.540	155	91
1-2	.300	0.548	.540	154	91
1-3	.360	0.600	.650	156	91
1-4	.320	0.566	.580	155	91
1-5	.420	0.648	.760	155	91
1-6	.400	0.632	.720	155	92
1-7	.230	0.480	.410	155	92
1-8	.210	0.458	.380	154	92
1-9	.240	0.490	.380	154	92
1-10	.260	0.510	.470	154	92
1-11	.260	0.510	.470	155	92
1-12	.290	0.539	.520	155	93
2-1	.210	0.458	.380	154	93
2-2	.220	0.469	.400	154	93
2-3	.220	0.469	.400	155	93
2-4	.220	0.469	.400	158	93
2-5	.200	0.447	.360	155	93
2-6	.200	0.447	.360	156	93
2-7	.320	0.566	.580	155	93
2-8	.420	0.648	.760	155	93
2-9	.420	0.648	.760	155	93
2-10	.360	0.600	.650	155	93
2-11	.480	0.693	.860	155	93
2-12	.460	0.678	.830	155	93
AVERAGES	0.305	0.547	0.548	155	92

AIR CONSULTING and ENGINEERING
COMPLETE EMISSION DATA

PLANT: TALISMAN SUGAR CORPORATION
SOURCE: NUMBER 4 BOILER
DATE: 2-11-91

RUN NO.:	4	IMPINGER ml	315
BEGIN TIME:	1700	SILICA GEL gms.	7.3
END TIME:	1839	PERCENT O2	7.40
TOTAL RUN TIME:	96.00 min.	PERCENT CO2	12.70
BAROMETRIC PRESSURE:	30.00 "Hg	"F" FACTOR	0
STACK PRESSURE:	30.00 "Hg.		AVG 12.9
NOZZLE DIAMETER:	.230 inches	PARTICULATE	-7.5
METER CORR. FACTOR:	.994	-----	
FINAL METER:	475.547 cubic ft.	FILTER mg.	300.8
INITIAL METER:	434.832 cubic ft.	WASH mg.	16.8
STACK AREA:	43.295 sq. ft.		

STACK 1 DATA INPUTS

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIF. DIFF.	STACK TEMP.	METER TEMP.
1-1	.720	0.849	1.300	156	8
1-2	.750	0.866	1.350	155	8
1-3	.700	0.837	1.260	156	8
1-4	.520	0.721	.940	156	8
1-5	.400	0.632	.720	156	8
1-6	.250	0.500	.450	156	8
1-7	.240	0.490	.450	156	8
1-8	.330	0.574	.600	157	8
1-9	.350	0.592	.630	157	8
1-10	.400	0.632	.720	157	8
1-11	.460	0.678	.830	154	8
1-12	.460	0.678	.830	154	8
2-1	.130	0.361	.230	156	8
2-2	.130	0.361	.230	155	8
2-3	.200	0.447	.360	156	8
2-4	.200	0.447	.360	157	8
2-5	.220	0.469	.400	157	8
2-6	.160	0.400	.290	157	8
2-7	.280	0.529	.500	156	8
2-8	.460	0.678	.830	157	8
2-9	.550	0.742	1.000	157	8
2-10	.630	0.794	1.150	157	8
2-11	.730	0.854	1.300	156	8
2-12	.700	0.837	1.250	156	8
AVERAGES	0.415	0.624	0.749	156	8

EMISSION RESULTS

NOZZLE DIA. (SQ.FT.):	0.0002889		
AVG. VELOCITY HEAD	:-----	0.36 "H2O	VOL. FLOW ACFM : 9830
AVG. STACK TEMP.:	-----	156 F	VOL. FLOW SCFMD : 6089
AVG. METER TEMP.:	-----	84 F	
AVG. ORIFICE DIFFERENTIAL:	---	0.69 "H2O	PARTICULATE DATA : <i>AVG 12.14</i>
METER STANDARD CUBIC FEET:	---	39.482	<i>5992</i>
% H2O VAPOR:	:-----	27.9	POUNDS PER HOUR: 64.79
GAS MOL. WT. DRY:	-----	30.33	POUNDS PER SCF : 0.000017
GAS MOL. WT. WET:	-----	26.88	GRAINS/SCF: 0.12
% EXCESS AIR:	-----	54.04	GRAINS/SCF @ 8% O2 0.11
AVG. STACK VEL. (FPS)	-----	37.84	GRAINS/SCF @50% EA 0.12
MMBTU INPUT:	-----	231.69	POUNDS PER MMBTU: 0.28
PERCENT ISOKINETIC	:-----	101.21	

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIFICE DIFF.	STACK TEMP.	METER TEMP.
1-1	.250	0.500	.450	156	85
1-2	.310	0.557	.560	156	85
1-3	.330	0.574	.600	155	85
1-4	.360	0.600	.650	155	85
1-5	.360	0.600	.650	155	85
1-6	.380	0.616	.680	155	85
1-7	.260	0.510	.470	156	85
1-8	.260	0.510	.470	156	85
1-9	.280	0.529	.500	156	86
1-10	.320	0.566	.580	156	86
1-11	.320	0.566	.580	156	86
1-12	.350	0.592	.630	156	86
2-1	.220	0.469	.400	156	85
2-2	.220	0.469	.400	156	85
2-3	.250	0.500	.450	156	86
2-4	.250	0.500	.450	156	85
2-5	.220	0.469	.400	156	85
2-6	.220	0.469	.400	156	85
2-7	.400	0.632	.720	156	85
2-8	.530	0.728	.950	156	85
2-9	.570	0.755	1.000	156	85
2-10	.570	0.755	1.000	156	86
2-11	.570	0.755	1.000	156	86
2-12	.570	0.755	1.000	156	87
AVERAGES	0.349	0.582	0.625	156	85

Aug 1, 2, 4
= 155

APPENDIX B
FIELD DATA SHEETS

STACK SAMPLING FIELD DATA SHEET



2106 N. W. 67th PLACE - Suites 9 & 10
GAINESVILLE, FLORIDA 32606

TEST ID _____
PAGE 1 OF 2

PLANT TALSMAN SUGAR CORPORATION

SOURCE NUMBER 4 BOILER

PLANT LOCATION SOUTH BAY PLANT

TYPE OF SAMPLING TRAIN EPA-15

TYPE OF SAMPLES PARTICULATES

DATE 2-11-91 RUN NO. 1

TIME START 0835 TIME END 1014

SAMPLE TIME 48 (min/pt) = 96 Total min

ASSUMED MOISTURE 30 % FDA 7

NOMOGRAPH C₁ 94 PITOT CORR. 84

P_b 30.0 "Hg P_s 30.0 "Hg

WEATHER CLEAR TEMP _____ °F

METER BOX NO. 1 H 2.05 V 994

NOZZLE CAL. 205 205 1205 = 205

STACK DIMENSIONS 6.3" x 2

STACK AREA 43.295 ft² EFFECTIVE _____ ft²

STACK HEIGHT _____ ft.

STACK DIAMETER: UPSTRM. _____ DNSTRM. _____

PORT SIZE _____ in. NIPPLE LENGTH _____ in.

U CORD LENGTH 425 125

REMARKS: TAL4611

TSC461

MAT'L PROCESSING RATE _____

GAS METER READINGS: FINAL 355 379 ft³

INITIAL 323 583 ft³

NET _____ ft³

FILTER NO. 4003 IMP. VOL. GAIN 235 ml.

SIL GEL NO. 50 WT. GAIN 12.8 ml.

TOTAL CONDENSATE 247.8 ml.

ORSAT _____

% CO₂ _____

% O₂ _____

% CO _____

% N₂ _____

F₀ = _____ F₀ RANGE = _____

ORSAT ANALYZER _____

LEAK CHECKS _____

PRE 0.00 cfm 25 "Hg POST 0.000 cfm 15 "Hg

METER BOX/PUMP _____ GAS SAMPLE SYST. _____

ORSAT BAG _____

PITOT TUBE NO. 1601 PRE-TEST OK

POST-TEST (+) 3.5 15 H₂O/Sec

POST-TEST (-) 4.4 15 H₂O/Sec

PYROMETER NO. 1

BOX OPERATOR ALAN PROBE HOLDER CELANO

7.5 237.97
7.5
2.9 6
2.3
1.6366
14112
02254
68.434 16/142
Ken Bryson
Jeff

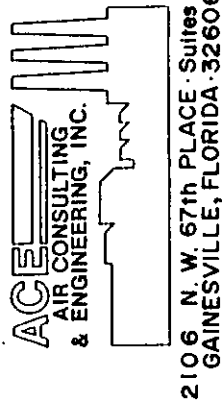
62.71 237.35 205

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (FT ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O")		STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP (°F)	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
					CALC.	ACTUAL					
N-1-1		0837	326.3	.55	.52	.52	154	270	46	51	3.0
2		0839	327.05	.70	.66	.66	153	273	42	51	4.0
3		41	327.90	.71	.66	.66	154	273	43	51	4.0
4		43	328.7	.66	.62	.62	154	271	41	52	4.0
5		45	329.3	.41	.39	.39	155	270	42	52	3.0
6		0847	329.8	.24	.23	.23	155	275	44	53	3.0

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (ft. ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O)		STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP (°F)	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
					CALC.	ACTUAL					
N-1-7		0849	330.32	1.31	.29	.29	154	274	45	54	3.5
8		51	330.94	1.40	.38	.38	154	270	45	54	4
9		53	331.6	1.42	.40	.40	157	270	45	54	4
10		55	332.24	1.44	.41	.41	155	274	45	55	4
11		57	332.95	1.52	.49	.49	150	267	45	56	5
12		0857	333.66	1.48	.45	.45	150	267	45	57	4.5
N-2-1		0901	334.07	1.14	.13	.13	155	264	46	58	2.5
2		03	334.47	1.14	.13	.13	154	268	47	58	3
3		05	334.86	1.16	.14	.14	154	268	47	59	3
4		07	335.18	1.13	.11	.11	154	273	48	60	3
5		09	335.57	1.16	.14	.14	155	273	48	61	3.5
6		11	336.00	1.18	.17	.17	155	273	48	61	3.5
7		13	336.54	1.28	.26	.26	155	268	47	62	4
8		15	337.16	1.43	.40	.40	154	267	47	63	5
9		17	337.95	1.56	.53	.53	155	270	47	63	5
10		19	338.75	1.62	.58	.58	154	270	46	64	5.5
11		21	339.54	1.65	.61	.61	154	270	46	65	6
12		0923	340. -	1.62	.58	.58	150	270	46	65	6
S-1-1		0927	340.9	1.38	.36	.36	153	271	47	66	5
2		29	341.52	1.38	.36	.36	154	270	47	67	5
3		31	342.1	1.35	.29	.29	154	270	47	67	4.5
4		33	342.7	1.37	.35	.35	154	270	47	68	5
5		35	343.44	1.39	.37	.37	154	271	47	68	5.5
6		37	343.94	1.35	.33	.33	155	271	47	69	5.5
7		39	344.49	1.34	.25	.25	155	269	47	69	5.0

STACK SAMPLING FIELD DATA SHEET

PLANT Thalassman Sugar Corp.
 SOURCE NUMBER 4 BOILER
 PLANT LOCATION SOUTH BAY FLORIDA
 TYPE OF SAMPLING TRAIN EPA-5
 TYPE OF SAMPLES PM
 DATE 2-11-91 RUN NO. 2
 TIME START 110 TIME END 1251
 SAMPLE TIME 48 (min/pt) = 76 Total min
 ASSUMED MOISTURE 28 % FDA 72
 NOMOGRAPH CLEAR PITOT CORR.
 P_b 30.00 "Hg P_s 30.00 "Hg
 WEATHER CLEAR TEMP 99 °F
 METER BOX NO. 1 H. 99 V. 2.05
 NOZZLE CAL. 1230 230 230 230
 STACK DIMENSIONS _____
 STACK AREA _____ ft² EFFECTIVE _____ ft²
 STACK HEIGHT _____ ft.
 STACK DIAMETER: UPSTRM. _____ DNSTRM. _____
 PORT SIZE _____ in. NIPPLE LENGTH _____ in.
 U CORD LENGTH _____
 REMARKS: _____



8.0
 8.2
 7.4
 7.5
 6284
 4014
 2770
 65.742
 246.22 m4

TR-4 C-11

TEST ID 7
 PAGE 1 OF 3

MAT'L PROCESSING RATE _____
 GAS METER READINGS: FINAL 393.410 ft³
 INITIAL 355.640 ft³
 NET _____ ft³
 FILTER NO. 2879 IMP. VOL. GAIN 305 ml.
 SIL GEL NO. 18 WT. GAIN 8.8 ml.
 TOTAL CONDENSATE 3638 ml.

	1	2	3	4	AVG.
% CO ₂					<u>12.3</u>
% O ₂					<u>2.7</u>
% CO					
% N ₂					

F₀ = _____ F₀ RANGE = _____
 ORSAT ANALYZER _____
 LEAK CHECKS _____
 PRE 000 cfm 20 "Hg POST 0.00 cfm 27 "Hg
 METER BOX/PUMP _____ GAS SAMPLE SYST. _____
 ORSAT BAG _____
 PITOT TUBE NO. 1601 PRE-TEST 0.15
 POST-TEST (+) 4.3 / 15 H₂O/Sec
 POST-TEST (-) 6.3 / 15 H₂O/Sec
 PYROMETER NO. _____
 BOX OPERATOR Neck PROBE HOLDER GeM40

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (FT ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O")		STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP (°F)	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
					CALC.	ACTUAL					
N-1-1			356.83	1.64	1.1	1.1	153	280	-	74	6
2	* STOP FOR	1116	357.86	1.66	1.12	1.12	153	255	53	75	5
3	Box Temp	1118	358.95	1.67	1.17	1.17	154	247	50	75	5.5
4		20	360.00	1.55	1.94	1.94	153	243	50	75	5
5		22	360.95	1.50	1.85	1.85	154	245	50	75	5
6		24	361.75	1.38	1.65	1.65	154	243	51	75	5

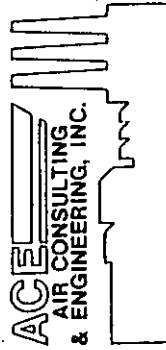
63.844 246.20 759

467

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (ft ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O")		STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP (°F)	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIL ("Hg)
					CALC.	ACTUAL					
N-1-7		1126	362.5	1.28	.48	.48	154	245	53	76	4.5
8		28	363.3	1.38	.65	.65	154	251	54	77	5.0
9		30	364.2	1.43	.73	.73	154	257	54	77	5.0
10		32	364.9	1.25	.42	.42	154	258	54	78	5.0
11		34	365.8	1.49	.83	.83	154	253	55	79	6.5
12		1136	366.72	1.49	.83	.83	155	256	55	79	6.5
N-2-1		1139	367.22	1.13	.22	.22	154	252	56	80	4.0
2		41	367.7	1.15	.24	.24	153	250	56	80	4.0
3		43	368.25	1.15	.24	.24	154	250	56	80	4
4		45	368.8	1.14	.24	.24	154	245	57	81	4.5
5		47	369.31	1.15	.24	.24	155	247	57	81	4.5
6		49	369.85	1.16	.27	.27	154	248	57	81	4.5
7		51	370.47	1.20	.34	.34	155	243	57	82	5
8		53	371.22	1.33	.56	.56	154	242	57	82	6
9		55	372.00	1.33	.56	.56	154	246	57	82	6.5
10		57	373.00	1.58	1.0	1.0	154	252	57	82	8.5
11		57	374.00	1.60	1.0	1.0	154	256	52	83	8.5
12		1201	375.0	1.58	1.0	1.0	154	263	57	83	8.5
S-1-1		1204	375.73	1.31	.53	.53	153	257	57	83	7.0
2		06	376.55	1.35	.60	.60	153	254	58	83	7.0
3		08	377.30	1.33	.56	.56	154	246	58	84	7.0
4		10	378.1	1.34	.58	.58	154	243	58	84	7.5
5		12	378.9	1.26	.61	.61	154	244	58	85	8
6		14	379.7	1.36	.61	.61	155	244	59	85	8
7		16	380.35	1.24	.46	.46	155	242	59	85	7.5

[illegible]

STACK SAMPLING FIELD DATA SHEET



2106 N. W. 67th PLACE, Suites 9 & 10
GAINESVILLE, FLORIDA 32606

PLANT Thurman Sugar Corporation
SOURCE NUMBER 4 BOLLER
PLANT LOCATION SOUTH BAY, FL.

TYPE OF SAMPLING TRAIN PM
TYPE OF SAMPLES LEAF
DATE 2-11-91 RUN NO. 3
TIME START 1345 TIME END 1535
SAMPLE TIME 48.2 (min/pt) = 96 Total min

ASSUMED MOISTURE 30 % FDA
NOMOGRAPH 1.8 PITOT CORR. .84
 P_b 30.0 "Hg P_s 30.0 "Hg
WEATHER CLEAR TEMP 89.4 °F
METER BOX NO. 1 H 2.05 Y. 994

NOZZLE CAL. 6.3"Ø x 2
STACK DIMENSIONS 6.3"Ø x 2
STACK AREA ft² EFFECTIVE ft²

STACK HEIGHT ft.
STACK DIAMETER: UPSTRM. DNSTRM.
PORT SIZE in. NIPPLE LENGTH in.
U CORD LENGTH ft.

REMARKS:

TEST ID 3
PAGE 1 OF 3

MAT'L PROCESSING RATE
GAS METER READINGS: FINAL 434.586 ft³
INITIAL 393.761 ft³
NET 40.825 ft³
FILTER NO. 2880 IMP. VOL. GAIN 100 ml.
SIL GEL NO. 110 WT. GAIN 2.0 ml.
TOTAL CONDENSATE 307.0 ml.

ORSAT

	1	2	3	4	AVG.
% CO ₂					
% O ₂					
% CO					
% N ₂					

F₀ = FO RANGE = FO

ORSAT ANALYZER

PEAK CHECKS

PRE 0.00 cfm 27 "Hg POST cfm "Hg
METER BOX/PUMP GAS SAMPLE SYST.

ORSAT BAG PITOT TUBE NO. 1601 PRE-TEST H₂O/Sec

POST-TEST (+) H₂O/Sec

POST-TEST (-) H₂O/Sec

PYROMETER NO. NECK PROBE HOLDER

BOX OPERATOR CELANO

241.62 mm BTU
5100
4041
1059

26.041 241.21

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (FT³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O") CALC. ACTUAL	STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP F	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
N-1-1		1347	394.96	.76	1.35 1.35	261	155	61	89	45
2		49	396.16	.76	1.35 1.35	261	155	55	83	5
3		51	396.4	.76	1.35 1.35	267	155	51	83	5
4		53	399	.70	1.26 1.26	267	158	51	83	5
5		55	—	.63	1.17 1.17	—	156	50	84	—
6		57	—	.28	1.0 1.0	—	156	58	85	—

73 2402

AIR CONSULTING
& ENGINEERING, INC.

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (ft ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O")		STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP (°F)	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
					CALC.	ACTUAL					
N-1-7		1459	—	.128	.150	.20	154	261	50	85	4
8		1601	402.3	.32	.1576	.576	157.8	260	50	85	4
9		1603	—	.142	.76	.76	155	258	51	86	4.5
10		1605	408.0	.152	.194	.94	154	260	50	87	5
11		1418	405.1	.46	.182	.82	155	260	50	87	4.5
12		1420	405.93	.46	.182	.82	155	260	50	87	4.5
N-2-1		1423	—	.10	.18	.18	156	271	51	87	2
2		25	—	.05	.09	.09	155	271	51	87	2
3		27	402	.08	.14	.14	156	276	52	87	2
4		29	407.6	.14	.25	.25	156	269	53	88	3
5		31	408	.13	.23	.23	155	270	53	88	3
6		33	409.27	.14	.34	.34	155	273	54	88	3
7		35	410.14	.14	.49	.49	156	274	55	88	3
8		37	411.07	.42	.76	.76	156	273	54	89	4
9		39	412.08	.47	.95	.85	156	271	53	89	4.5
10		41	413.10	.57	1.0	1.0	156	274	53	90	4.5
11		43	414.27	.62	1.1	1.1	156	267	52	90	5
12		1445	415.1	.62	1.1	1.1	155	267	52	90	5
S-1-1		1448	416.22	.30	.54	.54	155	265	54	91	3.5
2		50	417.03	.30	.54	.54	154	269	53	91	3.5
3		52	417.9	.36	.61	.61	156	270	54	91	4
4		54	418.76	.32	.58	.58	155	269	53	91	3.5
5		56	419.70	.42	.76	.76	155	269	53	91	4.5
6		58	420.61	.40	.72	.72	155	269	53	92	4
7		1500	421.3	.23	.41	.41	155	265	54	92	3

WIP
9000

[illegible]

STACK SAMPLING FIELD DATA SHEET

PLANT TALAMON SUGAR CORP.
 SOURCE NUMBER 4 BOILER
 PLANT LOCATION 5047th BAY FL.
 TYPE OF SAMPLING TRAIN EPA-5
 TYPE OF SAMPLES PM
 DATE 2-11-91 RUN NO. 4
 TIME START 1700 TIME END 1839
 SAMPLE TIME 48.2 (min/pi) = 96 Total min
 ASSUMED MOISTURE 30 % FDA
 NOMOGRAPH C₁ 6.8 PITOT CORR. .84
 P_b 30.0 "Hg P_s 30.0 "Hg
 WEATHER CLOUDY TEMP. °F
 METER BOX NO. 1 H₂O Y 1994
 NOZZLE CAL. 6.3"Ø x 2
 STACK DIMENSIONS 6.3"Ø x 2
 STACK AREA 11.2 EFFECTIVE 11.2
 STACK HEIGHT 11
 STACK DIAMETER: UPSTRM. DNSTRM.
 PORT SIZE in. NIPPLE LENGTH in.
 U CORD LENGTH ft
 REMARKS:



2106 N. W. 67th PLACE SUITES 9 & 10
 GAINESVILLE, FLORIDA 32606

7.5
 7.5
 7.2
 7.3
 7038
 4030
 3008
 247.64 man

TEST ID 4
 PAGE 1 OF 3

MAT'L PROCESSING RATE
 GAS METER READINGS: FINAL 4781847 ft³
 INITIAL 434832 ft³
 NET 44356 ft³
 FILTER NO. 2881 IMP. VOL. GAIN 315 ml.
 SIL GEL NO. 51 WT. GAIN 7.3 ml.
 TOTAL CONDENSATE mi.

ORSAT

	1	2	3	4	AVG.
% CO ₂					12.7
% O ₂					7.4
% CO					
% N ₂					

F₀ = FO RANGE =

ORSAT ANALYZER

LEAK CHECKS

PRE 0.00 cfm 15 "Hg POST 12 cfm 0000 Hg
 METER BOX/PUMP GAS SAMPLE SYST.
 ORSAT BAG 1601 PRE-TEST 0.6
 PITOT TUBE NO. 47115 H₂O/Sec
 POST-TEST (+) 3.7115 H₂O/Sec
 POST-TEST (-) 1
 PYROMETER NO. 1
 BOX OPERATOR PROBE HOLDER

229 07.40 231.69

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (FT ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O)		STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP (°F)	DRY GAS METER TEMP. (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
					CALC.	ACTUAL					
1-1		1702	435.87	1.70	1.3	1.3	156	244	55	80	5
2		04	437.0	1.75	1.35	1.35	155	244	55	80	5
3		06	438.15	1.70	1.26	1.26	156	244	53	80	5
4		08	439-	1.52	1.24	1.24	156	247	53	80	5
5		10	440.25	1.40	1.72	1.72	156	287	53	80	5
6		12	440.96	1.25	1.45	1.45	156	252	53	80	5



TEST ID

PAGE

2 OF 3

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (ft ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O)		STACK GAS TEMP. (°F)	SAMPLE BOX TEMP. (°F)	LAST IMPINGING TEMP. (°F)	DRY GAS METER TEMP. (°F)	VACUUM ON SAMPLE TRAIL ("Hg)
					CALC.	ACTUAL					
N-1-7		1714	446.65	.27	.45	.45	156	250	55	80	40
Y		1716	442.2	.33	.6	.6	157	250	56	80	570
9		18	443.3	.35	.63	.63	157	241	56	80	5.0
10		20	444.2	.40	.72	.72	157	238	56	81	6
11		22	445.12	.46	.83	.83	154	236	57	81	6
12		1724	446.63	.46	.83	.83	154	238	57	82	6
N-2-1		1727	446.54	.13	.23	.23	156	257	58	82	4
2		1729	447.06	.13	.23	.23	155	255	58	82	4
3		1731	447.73	.20	.36	.36	156	247	56	82	5
4		33	448.4	.20	.36	.36	157	235	56	83	5
5		35	449.1	.22	.40	.40	157	233	55	83	5.5
6		37	449.7	.16	.29	.29	157	229	54	83	5.0
7		39	450.45	.28	.50	.50	156	235	55	83	6.0
8		41	451.40	.46	.83	.83	157	246	53	84	7
9		43	452.4	.55	1.0	1.0	157	256	53	84	8
10		45	453.52	.63	1.15	1.15	157	258	53	84	9.5
11		47	454.70	.73	1.3	1.3	156	260	52	84	10.5
12		1749	455.87	.70	1.25	1.25	156	260	82	85	10
S-1-1		1752	456.2	.25	.45	.45	156	255	52	85	6.5
2		54	457.32	.31	.56	.56	156	257	52	85	7.5
3		56	458.14	.33	.6	.6	155	252	53	85	7.5
4		58	458.96	.36	.65	.65	155	247	53	85	8
5		1800	459.8	.36	.65	.65	155	246	54	85	8
6		02	460.6	.38	.68	.68	155	250	53	85	8.5
7		04	461.33	.26	.47	.47	156	250	53	85	7

APPENDIX C
LABORATORY ANALYSES

AIR CONSULTING & ENGINEERING, INC.

PARTICULATE LAB DATA

SOURCE TALISMAN STEEL CORP. #4 POWER

PROBE RINSE	RUN 1	RUN 2	RUN 3	BLANK 4	(2/11/91)
CONTAINER NUMBER	175	200	150	175	
TOTAL VOLUME (ml)					
1st GROSS WEIGHT (g)	103.5823	104.7396	104.7396	106.1853	DATE & TIME: 2/19/91-1330
2nd GROSS WEIGHT (g)	103.5828	104.7394	104.7391	106.1858	DATE & TIME: 2/20/91-
AVERAGE GROSS WEIGHT (g)	103.5826	104.7394	104.7394	106.1856	12H = 46 1300
TARE WEIGHT (g)	103.5734	104.7255	104.7255	106.1688	
SUB NET WEIGHT (g)	0.0092	0.0213	0.0044	0.0168	
ACETONE BLANK (g)	-	-	-	-	
TOTAL NET WEIGHT (mg)	92	213	44	168	

NOTE: In no case should a blank residue >0.01 mg/g or 0.001% of the weight of acetone used be subtracted from the sample weight.

FILTER	RUN 1	RUN 2	RUN 3	BLANK 4	
FILTER NUMBER	24203	2879	2880	2881	0115
1st GROSS WEIGHT (g)	0.6291	0.6764	0.5066	0.7038	DATE & TIME: 2/19/91
2nd GROSS WEIGHT (g)	0.6289	0.6760	0.5068	0.7038	DATE & TIME: 2/19/91
AVERAGE GROSS WEIGHT (g)	0.6290	0.6762	0.5067	0.7038	1330
TARE WEIGHT (g)	0.4912	0.4614	0.4041	0.4030	
SUB NET WEIGHT (g)	0.2178	0.2748	0.1026	0.3008	
TOTAL NET WEIGHT (mg)	217.8	274.8	102.6	300.8	

TARE
BALANCE CHECK1st GROSS WEIGHT
BALANCE CHECK2nd GROSS WEIGHT
BALANCE CHECK

SEE LAB BOOK

0 10.0g

0.5g 100.0g

%RH 46 DATE 2/19/91

Signature

0 10.0g

0.5g 100.0g

%RH 40 DATE 2/19

Signature C. H. H.

AIR CONSULTING & ENGINEERING, inc.

PARTICULATE LAB DATA

SOURCE TALLISMAN SLAGAZ CORP. - #4 DOLLER

PROBE RINSE	RUN ☒	RUN ☐	RUN ☐	2/1/91
CONTAINER NUMBER				BLANK
TOTAL VOLUME (ml)				100
1st GROSS WEIGHT (g)				105.4473
2nd GROSS WEIGHT (g)				
AVERAGE GROSS WEIGHT (g)				
TARE WEIGHT (g)				105.4462
SUB NET WEIGHT (g)				
ACETONE BLANK (g)				
TOTAL NET WEIGHT (mg)				

NOTE: In no case should a blank residue >0.01 mg/g or 0.001% of the weight of acetone used be subtracted from the sample weight.

FILTER	RUN ☐	RUN ☐	RUN ☐	BLANK
FILTER NUMBER				3082
1st GROSS WEIGHT (g)				0.4014
2nd GROSS WEIGHT (g)				0.4014
AVERAGE GROSS WEIGHT (g)				0.4014
TARE WEIGHT (g)				0.0001
SUB NET WEIGHT (g)				0.4
TOTAL NET WEIGHT (mg)				

TARE
BALANCE CHECK1st GROSS WEIGHT
BALANCE CHECK2nd GROSS WEIGHT
BALANCE CHECK

SEE LAB BOOK

0 _____ 10.0g _____
 0.5g _____ 100.0g _____
 % RH _____ DATE _____
 Signature _____

0 _____ 10.0g _____
 0.5g _____ 100.0g _____
 % RH _____ DATE _____
 Signature _____

APPENDIX D
QUALITY ASSURANCE
AND
CHAIN OF CUSTODY

AIR CONSULTING AND ENGINEERING, Inc.

SAMPLE RECOVERY AND CHAIN OF CUSTODY

PLANT NAME TALISMAN SUGAR CORP. TEST DATE 2/11/91
 SOURCE NAME No. 4 BOILER SAMPLE RECOVERED BY C. HODGE
 TYPE OF SAMPLE PART. PARTICULATE ANALYSES BY _____

SAMPLE RECOVERY

RUN NO.	CONTAINER NO.	LIQUID LEVEL MARKED	COLOR	COMMENTS
1	S-14	✓	MED	
1	4003	-	BLK	
2	S-25	✓	"	
2	2879	-	"	
3	S-32	✓	"	
3	2880	-	"	
4	S-35	✓	"	
4	2881	-	"	
ACETONE / WATER BLANK (CIRCLE)		✓	CLEAR	
FILTER BLANK		-	WH.	

SILICA GEL

RUN NO.	CONTAINER NO.	FINAL WT. (g)	INIT. WT. (g)	NET WT. (g)	COLOR
1	50	212.2	200.0	12.2	PINK
2	18	208.8	200.0	8.8	"
3	16	207.0	200.0	7.0	"
4	51	207.3	200.0	7.3	"
			200.0		
			200.0		
			200.0		
			200.0		

STANDARD METER CALIBRATION
Meter Number 1040616

Air Consulting and Engineering, Inc. (ACE) uses a dry gas meter for the calibration standard. This meter has been calibrated against a wet test meter in triplicate. This data was used to generate a standard meter calibration curve (see next page). Field meter calibrations are corrected to this curve using the following formula:

$$Y_a \times Y_s = Y$$

Y_a = actual ratio of field meter to standard meter

Y_s = ratio of standard meter to wet test meter at a given
flow rate (from Calibration Curve)

Y = corrected ratio of field meter

The dry standard meter was calibrated on November 23, 1990, and is checked and/or recalibrated at least annually.

AIR CONSULTING & ENGINEERING

STANDARD METER CALIBRATION

DATE 11-23-90 LEAK CHECK 0.000 CFM at 12 in. Hg.

METER SERIAL NUMBER 1040616(Santa)

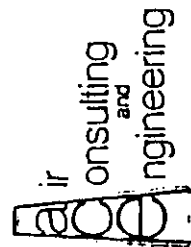
BAROMETRIC PRESSURE 30.07 in. Hg.

STD GAS METER TEMPERATURE 67 °F/ASTM GLASS THERMOMETER TEMPERATURE 69 °F

WET ΔH	STD ΔH	GAS VOLUME, WET TEST METER			GAS VOLUME, STD GAS METER			TEMP OF STD. METER (°F)	TIME (Minutes)
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³		
-0.1	-1.1	0.020	5.333	5.333	272.003	277.309	5.306	70	67
-0.1	-1.1	5.333	10.664	5.331	277.309	282.600	5.291	70	67
-0.1	-1.1	10.664	15.982	5.318	282.600	287.877	5.277	70	67
-0.3	-1.9	0.000	5.490	5.490	288.149	293.623	5.474	70	67
-0.3	-1.9	5.490	12.799	7.309	293.623	300.898	7.275	70	67
-0.3	-1.9	12.799	18.278	5.479	300.898	306.359	5.461	70	67
-0.4	-2.5	0.000	5.160	5.160	306.712	311.863	5.151	70	67
-0.4	-2.5	5.160	10.321	5.161	311.863	317.017	5.154	70	67
-0.4	-2.5	10.321	15.488	5.167	317.017	322.173	5.156	70	67
-0.5	-3.7	0.000	7.481	7.481	322.562	330.068	7.506	70	67
-0.5	-3.7	7.481	14.039	6.558	330.068	336.655	6.587	70	67
-0.5	-3.7	14.039	19.649	5.610	336.655	342.278	5.623	70	67
-0.7	-5.3	0.000	5.639	5.639	342.648	348.279	5.631	70	67
-0.7	-5.3	5.639	11.268	5.629	348.279	353.889	5.610	70	67
-0.7	-5.3	11.268	16.889	5.621	353.889	359.498	5.609	70	67

CALIBRATED BY: A. F. Galad

Y	SCFM	Y	SCFM	Y	SCFM	Y	SCFM
Run 1	1.002	0.445	1.002	0.611	0.738	1.000	0.986
Run 2	1.005	0.445	1.004	0.610	0.738	0.999	0.986
Run 3	1.005	0.444	1.002	0.610	0.739	1.001	0.986
Average	1.004	0.444	1.003	0.610	0.739	1.000	0.986



1,127

1,010

0.986

1,000

0.738

1.002

0.610

0.739

1.000

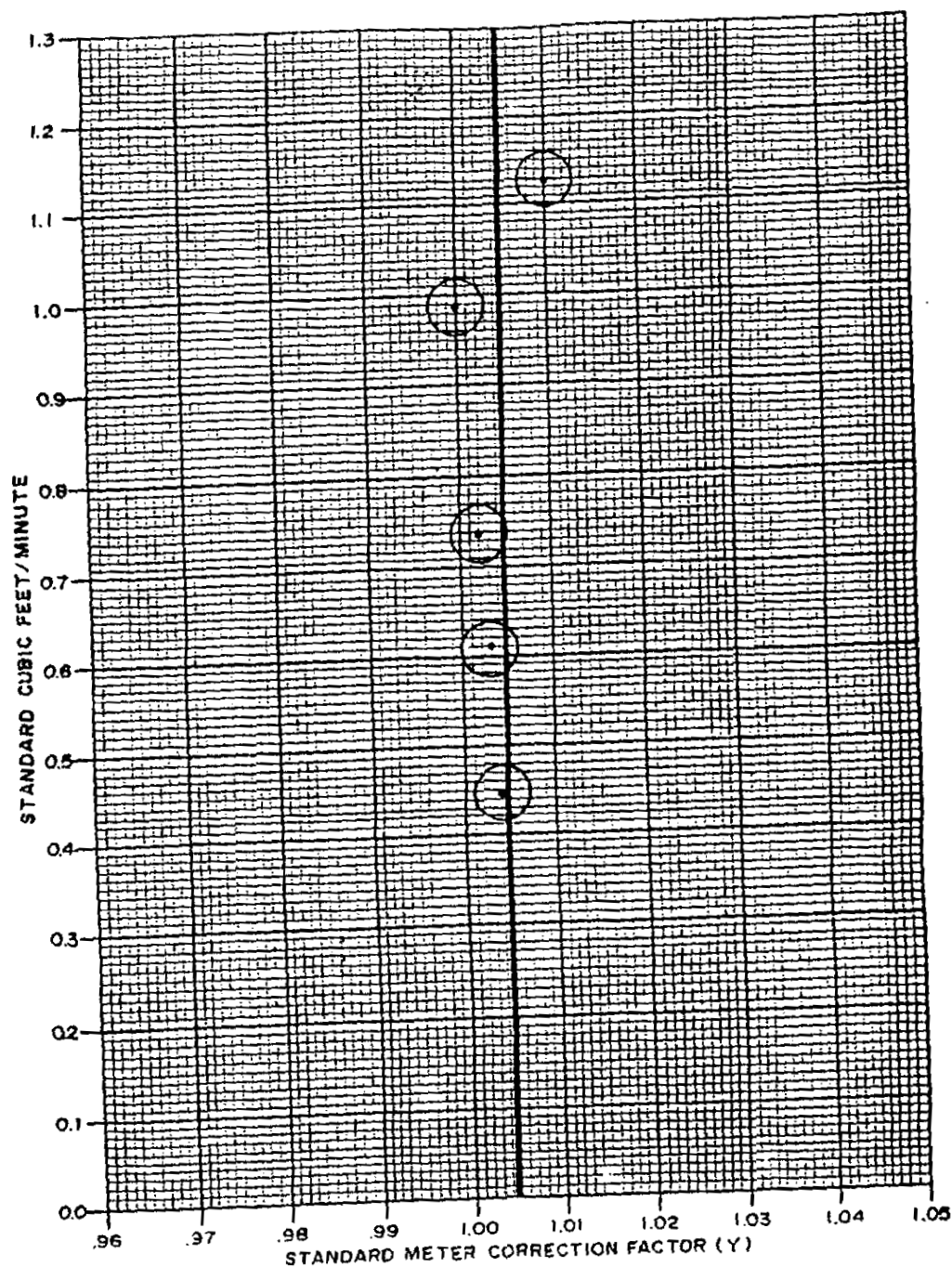
0.986

1,126

1,010

0.986

1,127



STANDARD METER CALIBRATION CURVE
METER SERIAL NO. 1040616 (SOUTH)
NOVEMBER 23, 1990

AIR CONSULTING
and
ENGINEERING

AIR CONSULTING & ENGINEERING, inc.

POST TEST CALIBRATION

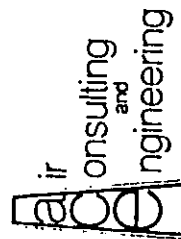
DATE 2-11-91 METER BOX NUMBER 1 LEAK CHECK 0.000 CFM at 29 in. Hg.
 CLIENT U.S. SUGAR / TALLSMA SOURCE VARIOUS THERMOCOUPLE NUMBER 3611601 PYROMETER NUMBER 601
 FLIGHT SERVICE Pb 30.11 in. Hg. ACE BAROMETER Pb 30.1 in. Hg.
 ASTM GLASS THERMOMETER 160 of / THERMOCOUPLE 160 of / ASTM GLASS THERMOMETER 64 of / METER TEMP 64 of

Δ HS	AVERAGE Δ HD	GAS VOLUME, STANDARD METER			GAS VOLUME, DRY GAS METER			TEMP. STANDARD METER	TEMP. OF DRY METER	TIME (Minutes)	MAX. VACUUM in. Hg.
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³				
-5	2.1	513.835	508.00	5.835	193.300	199.452	6.152	64 59	64	8	21
-5	2.1	513.835	522.560	8.725	199.817	209.013	9.196	59	66	12	21
-5	2.1	522.560	513.835	7.993	209.013	217.471	8.458	59	68	11	21

CALIBRATED BY: Stephen A. Neal RUN NUMBER 1

STANDARD M.C.F.	DELTA Ha	M.C.F.
1.005	2.135	0.959
1.005	2.140	0.963
1.005	2.135	0.963
1.005	2.137	0.962

SCFM
0.75
0.74
0.74
0.74



AVERAGES

AIR CONSULTING & ENGINEERING

ANNUAL METER CALIBRATION

DATE 6-7-90

LEAK CHECK 0.000 CFM at 12 in. Hg.

METER BOX NUMBER 1

BAROMETRIC PRESSURE 30.02 in. Hg.

DRY GAS METER TEMPERATURE 89 °F/ASTM GLASS THERMOMETER TEMPERATURE 90 °F

ΔHS	AVERAGE ΔHD	GAS VOLUME, STANDARD METER			GAS VOLUME, DRY GAS METER			TEMP. STD. METER	TEMP. OF DRY METER	TIME (Minutes)	TIMER
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³				
-07	0.5	206.539	214.496	7.957	719.311	727.244	7.933	85	85	21	21
-15	1.25	215.308	224.239	5.931	728.042	733.952	5.910	85	86	10	
-22	2.0	224.610	227.578	5.968	734.320	740.265	5.945	85	87	8	
-32	2.75	228.029	233.291	5.262	740.708	745.940	5.232	86	88	6	
-40	3.5	233.668	239.592	5.924	746.315	752.205	5.890	87	90	6	
-50	4.25	240.117	245.527	5.410	752.724	758.112	5.388	87	91	5	

DELTA H	Y _a	SCFM	Y _s	Y
2.004	1.002	0.368	1.004	1.006
2.041	1.002	0.577	0.998	1.000
2.061	1.003	0.725	0.993	0.996
2.054	1.003	0.851	0.989	0.992
2.063	1.003	0.956	0.985	0.988
2.082	1.001	1.048	0.983	0.984
MEAN:	2.051	1.002	0.992	0.994

CALIBRATED BY: H. F. Gabel



air
onsulting
and
engineering

PITOT TUBE CALIBRATION MEASUREMENTS

DATE CALIBRATED 4-9-90 PITOT TUBE 70

Pitot tube assembly level? ✓ Yes No

Pitot tube openings damaged? Yes (explain below) ✓ No

$\alpha_1 = \underline{2}^\circ (<10^\circ)$, $\alpha_2 = \underline{0}^\circ (<10^\circ)$, $\beta_1 = \underline{2}^\circ (<5^\circ)$,

$\beta_2 = \underline{1}^\circ (<5^\circ)$

$\gamma = \underline{3}^\circ$, $\theta = \underline{3}^\circ$, $A = \underline{0.869}$ in. = (Pa + Pb)

$z = A \sin \gamma = \underline{0.045}$ in.; <0.32 / $<1/8$ in.

$w = A \sin \theta = \underline{0.045}$ in.; <0.08 / $<1/32$ in.

$P_a = \underline{460}$ in. $P_b = \underline{409}$ in. $D_c = \underline{375}$

Calibration required? Yes ✓ No

THERMOCOUPLE CALIBRATION

Date 4-9-90 Thermocouple No. 70

Source (Specify)	ASTM Glass Thermometer With Mercury ($^\circ\text{F}$)	Pyrometer ($^\circ\text{F}$)	Degree Difference	% Difference
Ambient	72	72	0	0.00
Ice Bath	36	38	2	0.38
Oven	311	310	1	0.19

FDER - Maximum 5° difference

EPA $\left[\frac{(\text{Ref. temp. } ^\circ\text{F} + 460) - (\text{Pyrometer temp. } ^\circ\text{F} + 460)}{\text{Ref. temp. } ^\circ\text{F} + 460} \right] 100 \leq 1.5\%$

Calibrated by J. L. Carter

AIR CONSULTING & ENGINEERING, INC. PYROMETER CALIBRATION

DATE 7-10-90

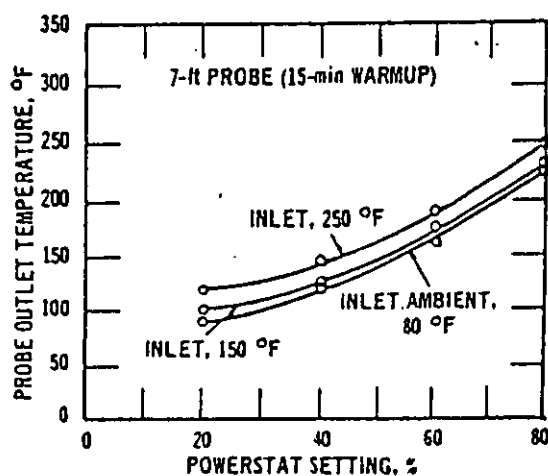
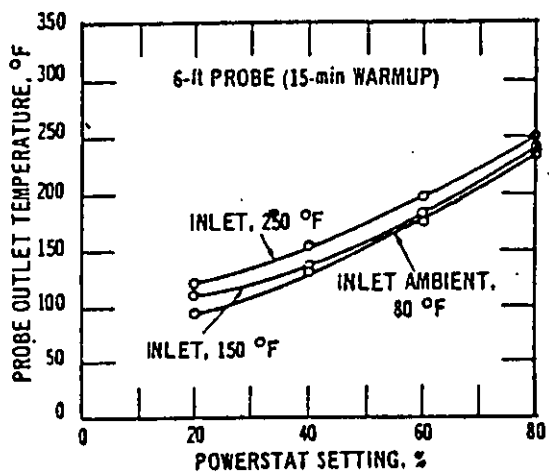
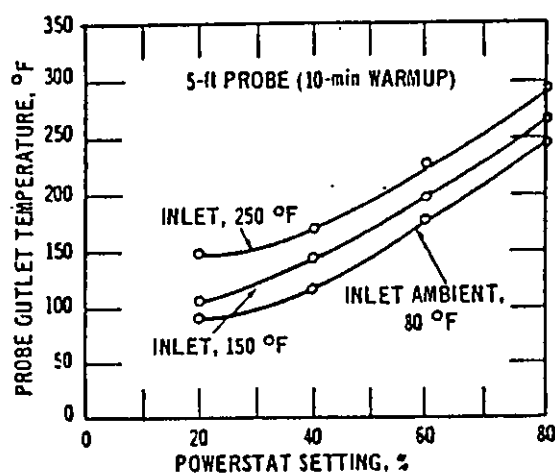
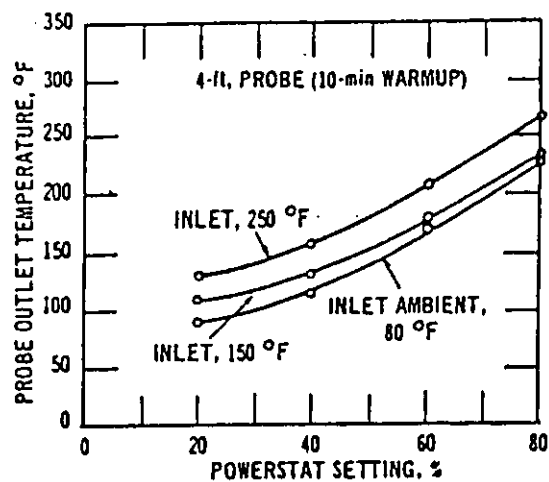
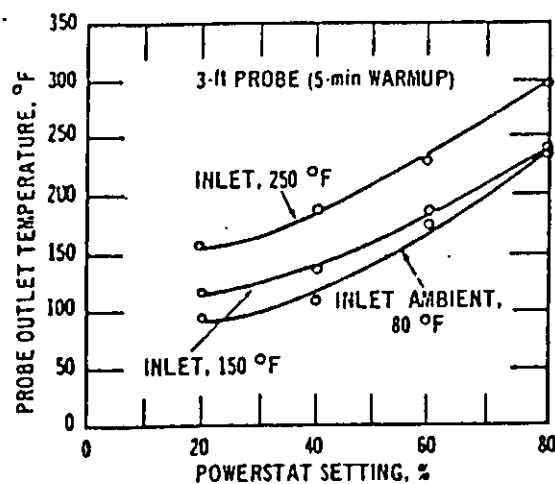
PYROMETER NUMBER METER BOX #1

SOURCE (SPECIFY)	GLASS THERMOMETER WITH NBS MERCURY (°F)	PYROMETER (°F)	DEGREE DIFFERENCE	PERCENT DIFFERENCE
ICE BATH	<u>32°</u>	<u>33°</u>	<u>1</u>	<u>.2%</u>
AMBIENT	<u>94°</u>	<u>96°</u>	<u>2</u>	<u>.4%</u>
HOT OVEN	<u>800°</u>	<u>800°</u>	<u>0</u>	<u>0</u>

FDER - MAXIMUM 5° DIFFERENCE

EPA
$$\left[\frac{(\text{REF. TEMP. } ^\circ\text{F} + 460^\circ) - (\text{PYROMETER TEMP. } ^\circ\text{F} + 460^\circ)}{\text{REF. TEMP. } ^\circ\text{F} + 460^\circ} \right] 100 \leq 1.5\%$$

CALIBRATED BY: 



NOTE: Flow rate held constant at 0.75; 50% change in flow rate has little effect on probe temperature.

Probe temperatures.

APPENDIX E
PRODUCTION RATE
CERTIFICATION

BOILER DATA SHEET

COMPANY TALISMAN SUGAR

REPORTED BY FRANK KLEEMAN

DATE 2-11-91

INTEGRATOR FACTOR X 100

BOILER NO. 4

FUEL OIL USED No Oil

FEED WATER

	TIME	INTEGRATOR	LOG SCALE STEAM FLOW X 100	TEMP. PRESSURE	TEMP.	TEMP.	PRESSURE
RUN 1	8:35	83785	82	287	572	260	420
	9:00	4304	80	287	573	260	420
	9:30	4914	85	286	573	260	420
	10:11	5238	84	280	578	260	420
.6 HRS.	96 MIN.	1953		285	575	260	420 AV
		1953 X 100	122,060	LBS/HR			
		1.6					
RUN 2	11:10	6960	82	280	577	260	420
	11:40	7619	85	285	565	260	440
	12:10	8244	84	275	570	260	440
	12:46	8983	82	285	576	260	440
.6 HRS.	96 MIN.	2023		281	572	260	435 AV
		2023 X 100	126,440	LBS/HR			
		1.6					
RUN 3	1:45	90191	80	285	580	260	440
MILL DOWN	2:05 20 MIN.	0586395	82	280	575	260	440
	2:15	0799	87	275	570	260	440
	2:45	1437	84	280	585	260	440
	3:15	2056	82	288	582	260	440
	3:31 76 MIN.	23791580	82	285	580	260	440
.6 HRS.	96 MIN.	1975		282	579	260	440 AV
		1975 X 100	123,440	LBS/HR			
		1.6					

110

BOILER NUMBER 4

OIL METER FACTOR 100

STEAM INTEGRATOR FACTOR_____

SCRUBBER(S) PRESS.DROP____, ____

SCRUBBER(S) GPM _____

OPERATOR SIGNATURE _____

SCRUBBER(S) H2O LEVEL _____, _____

Ph(if applicable) _____, _____

INITIAL INTEGRATOR 994190

FINAL INTEGRATOR 996119

[illegible]

PROCESS DATA

INSTALLATION

Boiler 4

COMPANY TALISMAN SUGAR CORP.

DATE 2-11-91

TYPE OF INSTALLATION BAGASSE BOILER

TYPE OF MATERIAL PROCESSED STEAM

TYPE OF FUEL USED BAGASSE

TYPE OF POLLUTION CONTROL SYSTEM DRY COLLECTOR + DUAL VENTURI W/ SCRUBBER

	NORMAL	RUN 1	RUN 2	RUN 3
SCRUBBER WATER FLOW (GPM)	<u>1200</u>	<u>1200</u>	<u>1200</u>	<u>1200</u>
PRESSURE DROP (INCHES)	<u>12</u>	<u>12.0</u>	<u>11.5</u>	<u>11.5</u>

REPORTED BY FRANK KLEEMAN

Run 4

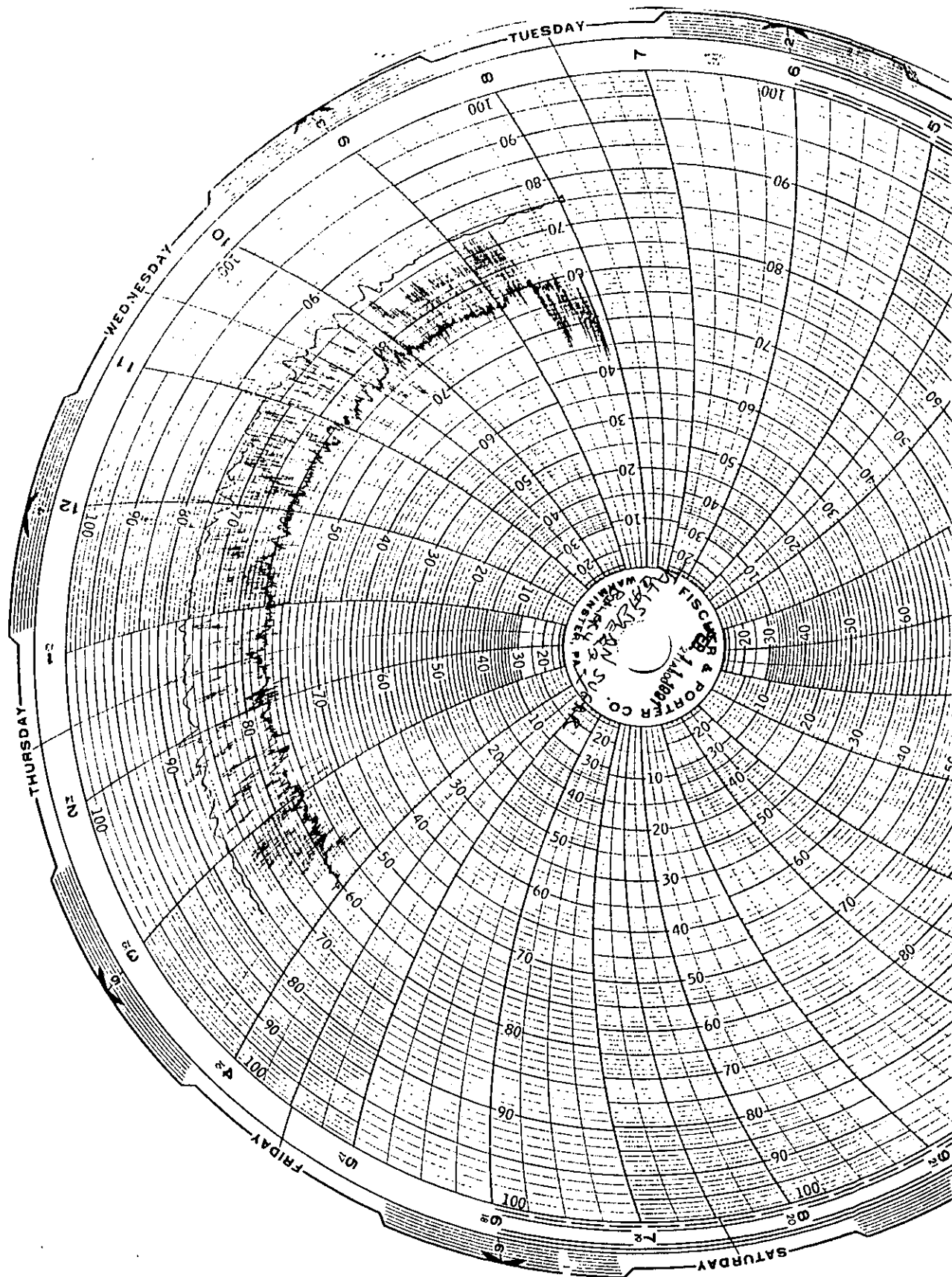
GPM

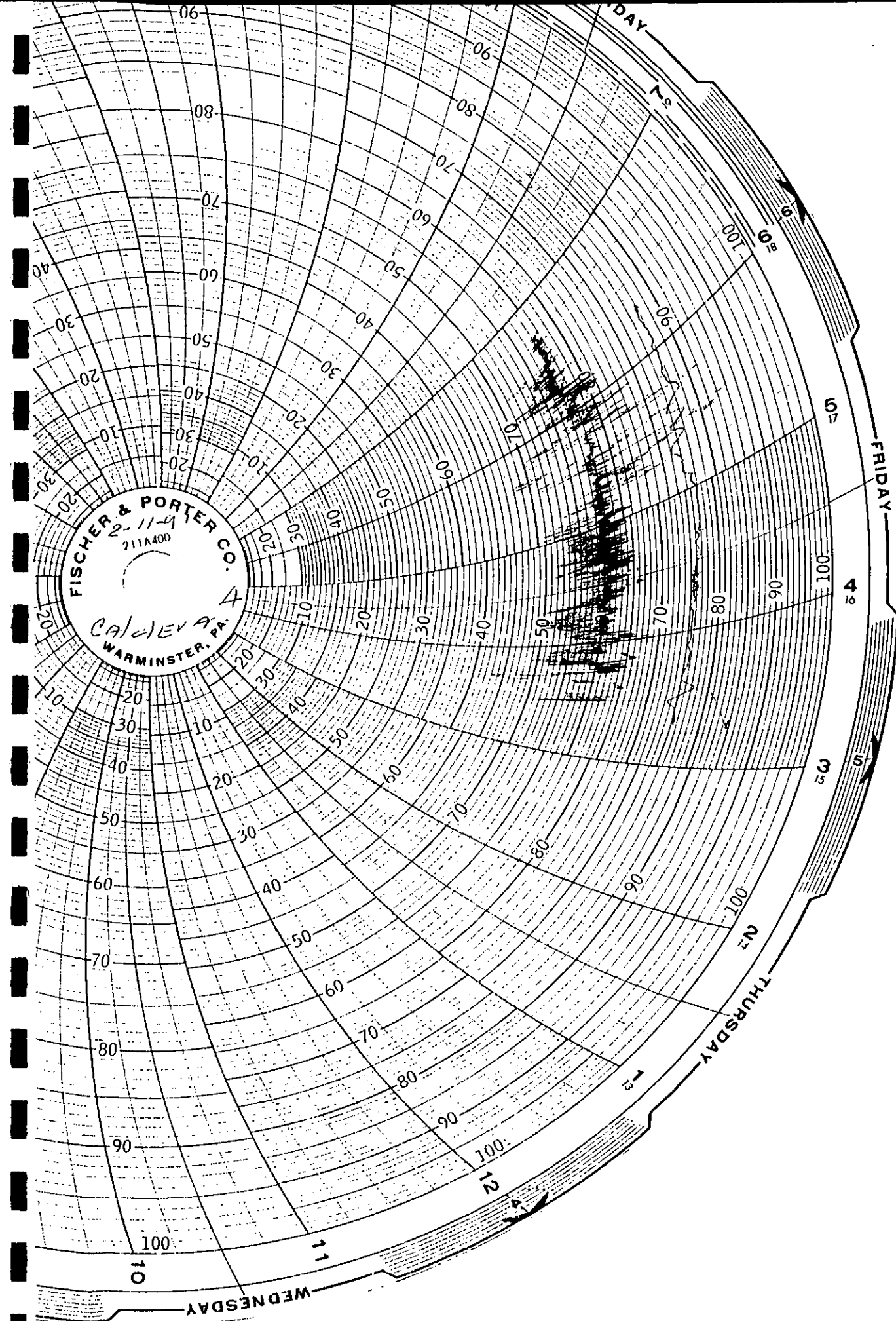
1200

ΔP

11.5"

S. L. Neuk





APPENDIX F
PROJECT PARTICIPANTS

PROJECT PARTICIPANTS

ACEI:

STEPHEN L. NECK, P.E.

FIELD TESTING
REPORT PREPARATION

GERARD GAUTHREUX

FIELD TESTING

KLEEMAN ENGINEERING, INC

FRANK S. KLEEMAN, P.E.

PROJECT COORDINATOR

FDER

KEN TUCKER

TEST OBSERVER

TSC

ANGELO ARCHBOLD

TEST COORDINATOR

DATE ../../.. FLORIDA DEPARTMENT OF ENVIRONMENTAL REGULATION
 PARTICULATE STACK TEST VERIFICATION
 DER METHOD 5

FACILITY NAME: TALISMAN SUGAR CORP.

APIS #

COMPANY CONDUCTING TEST: KLEEMAN

TEST DATE 2 11 91

SOURCE DESCRIPTION: BOILER

STACK TEST DATA SUMMATION

	RUN1	RUN2	RUN3
1.H2O (VOL.MEAS.),ML	235	305	315
2.H2O (MASS MEAS.),GM	12.8	12.8	7.3
3.M'N PARTICULATE WEIGHT, GM	.227	.296	.3176
4.V'M VOLUME METERED,CF	29.824	37.77	40.715
5.Y DRY GAS MTR. CALIB.FCTR.	.994	.994	.994
6.RDP AVG SQR D.P-SAMPLING	.621	.6	.624
7.DH AVG DELTA H,IN.H2O	.384	.653	.749
8.T'M AVG MTR. TEMP,DEG.F	65	82	84
9.T'S AVG STACK TEMP,DEG.F	154	154	156
0.P'S STACK PRESS,"HG(ABS)	30	30	30
1.P'B BAROMETRIC PRESS,"HG	30	30	30
3.D'N ACTUAL NOZZLE DIAM,IN	.205	.23	.23
4.T ACTUAL SAMPLE TIME,MIN	96	96	96
5.C'P PITOT TUBE COEFFICIENT	.84	.84	.84
3.S/T VALUE:SAMPLE PTS/TOT PTS	1	1	1

UN	VOLUME SAMPLED DSCF	MOISTURE CONTENT PERCENT	STACK VEL FPS	FLOW RATE DSCF/H	PERCENT ISO- KINETIC	ACTUAL EMISS LB/HR	ACTUAL EMISS LB/MBTU	ALLOW EMISS LB/MBTU
1	29.91	27.85	39.07	3,787,307	93.26	63.36	0.262	0.300
2	36.72	27.85	37.75	3,659,235	94.13	65.03	0.269	0.300
3	39.44	27.78	39.32	3,802,475	97.31	67.49	0.279	0.300
EAN	35.36	27.83	38.72	3,749,672	94.90	65.29	0.270	0.300

SUMMARY

GENERAL:

REVIEWED BY AS
ACTUAL A 'S = 43.295 SQ FT
LAMINAR FLOW ASSUMED (<10 DEG YAW) (OR <20 DER)
ACTUAL EMISS BASED ON HEAT INPUT = 241.58 MBTU/HR
ALL REQUIRED LEAK TESTS ACCEPTABLE
ASSUMED M 'D=30.0 (COMBUSTION GASES)

COMMENT.....

RUN 1 :

ACTUAL A 'N = .0002292 SQ FT
OVERSATURATED CONDITIONS: SATURATION MOISTURE ASSUMED/GIVEN PG.1

COMMENT.....

RUN 2 :

ACTUAL A 'N = .0002885 SQ FT
OVERSATURATED CONDITIONS: SATURATION MOISTURE ASSUMED/GIVEN PG.1

COMMENT.....

RUN 3 :

ACTUAL A 'N = .0002885 SQ FT

COMMENT.....

2-11-91

Boiler #4

ACG

Area 43.295

Ref 3

INPUT SHEET - REV:09/10/80 - PAGE 2 OF 2

ENTER THE FOLLOWING:

	RUN1	RUN2	RUN3
1. H2O COLLECTED (ONLY VOL. MEASURED), ML:	235	305	315
2. H2O COLLECTED (WEIGHED PART ONLY), GM:	12.8	12.8	7.3
3. M'N PARTICULATE WEIGHT, GM:	227	296	317.6
4. V'M VOLUME METERED, CF:	29.824	37.77	40.715
5. Y DRY GAS METER CAL FACTOR:	1.994	1.994	1.994
6. RDP AVG SOR DELTA P (WHEN SAMPLING):	1.621	1.600	1.624
7. DH AVG DELTA H, IN H2O:	1.384	1.653	1.749
8. T'M AVG METER TEMP, DEG F:	65	82	84
9. T'S AVG STACK TEMP, DEG F:	154	154	156
10. P'S* STACK PRESS, *IN(.....):	30.00	30.00	30.00
11. P'B BAROMETRIC PRESS, IN HG:	30.00	30.00	30.00
12. D'N ACTUAL NOZZLE DIAMETER, IN.:	2.05	2.30	2.30
13. T ACTUAL SAMPLE TIME, MIN:	96	96	96
14. C'P PITOT TUBE COEFFICIENT:	1.84	1.84	1.84
OPTION ENTRIES:	237.35	246.20	241.21
17. ORSAT/FYRITE - %CO2:			
18. ORSAT/FYRITE - %O2:			
20. ORSAT/FYRITE (FOR C'S @ 50% E.A.) - %CO:			
19. SPECIFIC M'D ENTRIES:			
23. CYCLONIC (10-20 DEG) - AVG COS(YAW):			
26. CYC. (>20) - AVG[SQR D.P X COS(YAW)]:			
24. PROCESS WT SOURCE - T/HR:			
22. LB/TON REGULATED - T/HR:			
27. LB/* REGULATED (* AS DEFINED) - */HR:			
23. LAM&CYC(20) - VAL(SAMPLE PTS/TOT PTS):			

241.58