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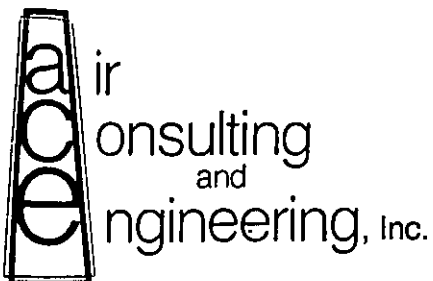
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AP-42 Section Number: 1.8

Reference Number: 18

Title: Source Test Report for Particulate
Emissions Twin Impingement Wet
Scrubber Number 4 Boiler: Atlantic
Sugar Association

November 1990



Ref-5

OSWI-ASA 3

SOURCE TEST REPORT
for
PARTICULATE EMISSIONS
IMPINGEMENT WET SCRUBBER
NUMBER 4 BOILER

ATANTIC SUGAR ASSOCIATION
BELLE GLADE, FLORIDA

NOVEMBER 29, 1990

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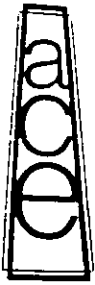
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REPORT CERTIFICATION

To the best of my knowledge, all applicable field and analytical procedures comply with Florida Department of Environmental Regulation requirements and all test data and plant operating data are true and correct.

Stephen L. Neck
Stephen L. Neck, P.E.

State of Florida
Registration No. 20020

December 22, 1990
Date

1.0 INTRODUCTION

Personnel from Air Consulting and Engineering, INC. (ACEI) performed annual source emission compliance testing for the Atlantic Sugar Association on November 29, 1990. Testing was performed at the Number 4 Boiler wet scrubber outlet.

Testing was designed to fulfill "specific conditions" of the current Florida Department of Environmental Regulation (FDER) operating permit.

Three United States Environmental Protection Agency (USEPA) Method 5 particulate matter (PM) test runs were conducted while the plant was documented to be operating within 10% of permitted production.

Mr. Frank Kleeman served as test coordinator and certified production rates. ACEI performed this work under subcontract to Kleeman Engineering, Inc.

Mr. Sherril Culliver of the Florida Department of Environmental Regulation (FDER) witnessed a portion of the testing.

2.0 SUMMARY and DISCUSSION of RESULTS

Results of the emission testing are provided in Table 1. Complete emission data are located in the report appendices.

The source was found to be operating within full compliance of permit conditions. Stack emissions averaged 44.02 pounds per hour (LB/HR) and 0.198 pounds per million btu (LB/MMBTU) heat input against a "process rate" basis allowable emission of 0.290 LB/MMBTU. Permit conditions limit emissions to 0.10 LB/MMBTU from oil and 0.290 LB/MMBTU from residue firing. No oil was used during compliance testing.

Production rate summaries are provided in Appendix A. These data were taken from control room recordings of steam flow, temperature, and pressure as well as feedwater temperature and pressure (Appendix E). Residue integrator and oil meter readings were recorded at the beginning and end of each particulate test run by Mr. Frank Kleeman.

TABLE 1
EMISSION SUMMARY
ATLANTIC SUGAR ASSOCIATION
NUMBER 4 BOILER
NOVEMBER 29, 1990

RUN NUMBER	TIME	ACTUAL EMISSIONS		ALLOWABLE EMISSIONS	
		LB/HR	LB/MMBTU	LB/HR	LB/MMBTU
1	0845-0946 61	42.21	0.199	61.50	0.290
2	1100-1201 61	44.18	0.196	65.32	0.290
3	1315-1416 61	45.67	0.200	66.08	0.290
AVERAGES	-----	44.02	0.198	64.30	0.290

3.0 PROCESS DESCRIPTION AND OPERATION

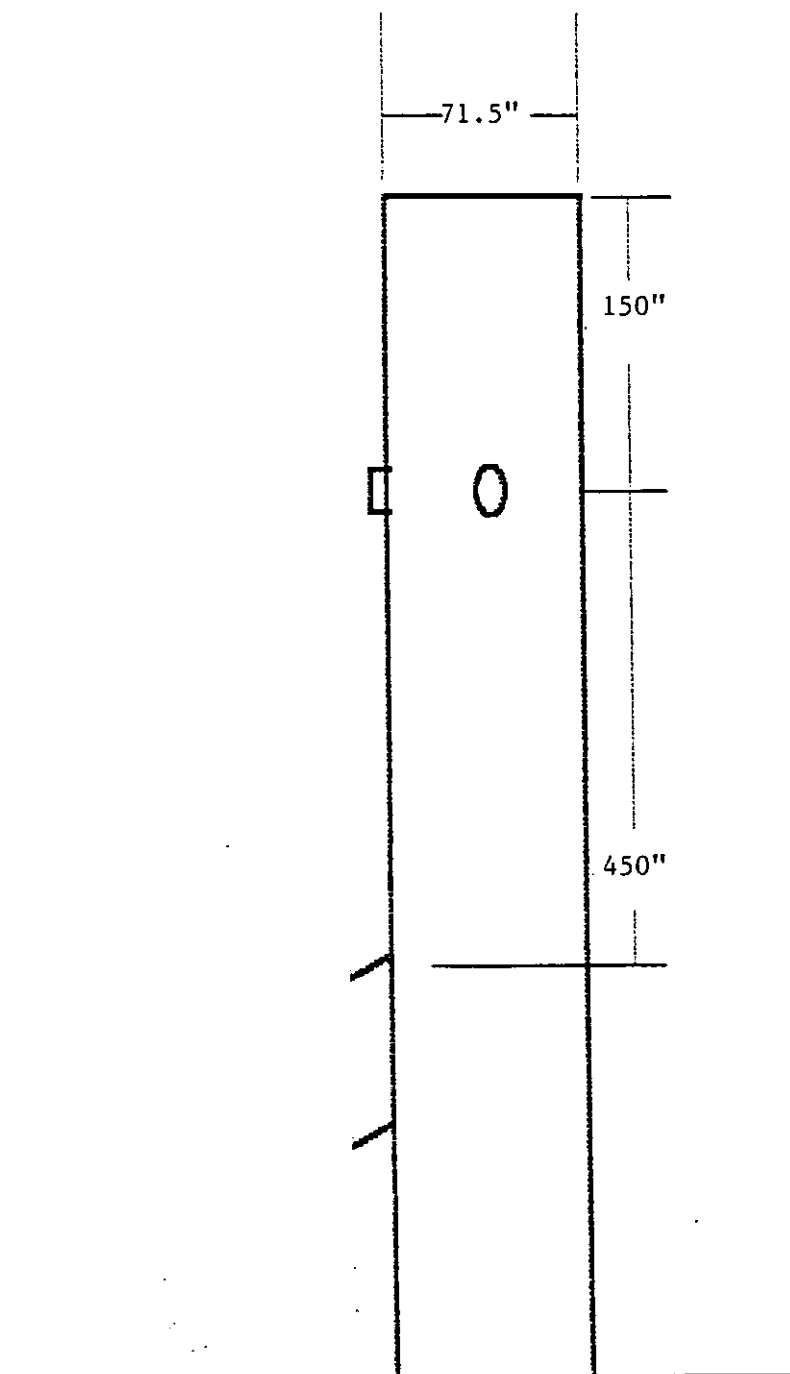
The Number 4 Boiler at the Atlantic Sugar Association is a spreader stoker design used primarily for residue fuel firing. Supplemental oil firing may also be utilized but was not used during the emission test series. The boiler averaged 113,933 pounds per hour steam production over the three run test period.

Oil meters, steam integrators, and other production monitoring devices were rigorously calibrated prior to the production season.

4.0 SAMPLING POINT LOCATION

The sampling point location consists of a scrubber outlet stack 71.5" in diameter. The stack has two sample ports 90 degrees apart. The ports were located 405" from an upstream disturbance and 150" from the outlet.

Twenty test points were sampled for each test run. The traverse points were located as shown in Figure 1. The stack configuration is such that there is no reason to evaluate the presence of cyclonic flow.



TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL
1	1.8
2	5.8
3	10.5
4	16.2
5	24.4
6	47.1
7	55.3
8	61
9	65.7
10	69.7

FIGURE 1.
SAMPLING POINT LOCATION

5.0 FIELD and ANALYTICAL PROCEDURES- USEPA METHOD 5

Particulate matter samples were collected by the emission measurement method specified by the United States Environmental Protection Agency. A schematic diagram of the sampling train used is provided in Figure 2. All particulate matter captured from the nozzle to and including the filter was included in the calculation of the emission rate of particulate matter.

PREPARATION OF EQUIPMENT

1. FILTERS- Gelman type "A" glass fiber filters were placed in a drying oven for two hours at 105 degrees C, removed and placed in a standard desiccator containing indicating silica gel, allowed to cool for two hours, and weighed to the nearest 0.1 mg. The filters were then re-desiccated for a minimum of six hours and weighed to a constant weight (less than 0.5 mg change from previous weighing). The average of the two constant weights was used as the tare value.
2. NOZZLE, FILTER HOLDER, AND SAMPLING PROBE - The nozzle, filter holder, and sampling probe were washed vigorously with soapy water and brushes, rinsed with distilled water and acetone, and dried prior to the test program. All openings on the equipment were sealed while in transit to the test site.
3. IMPINGERS - The Greenburg-Smith impingers were cleaned, rinsed, and dried as in 2. The impingers were also sealed during transit.

TEST PROCEDURE

Prior to performing the actual particulate matter sample runs, certain stack and stack gas parameters were measured. These preliminary measurements included the average gas temperature, the stack gas velocity head, the stack gas moisture content, and the dimensions at the point where the tests were to be performed. The stack temperature was determined using a bi-metallic thermocouple and calibrated

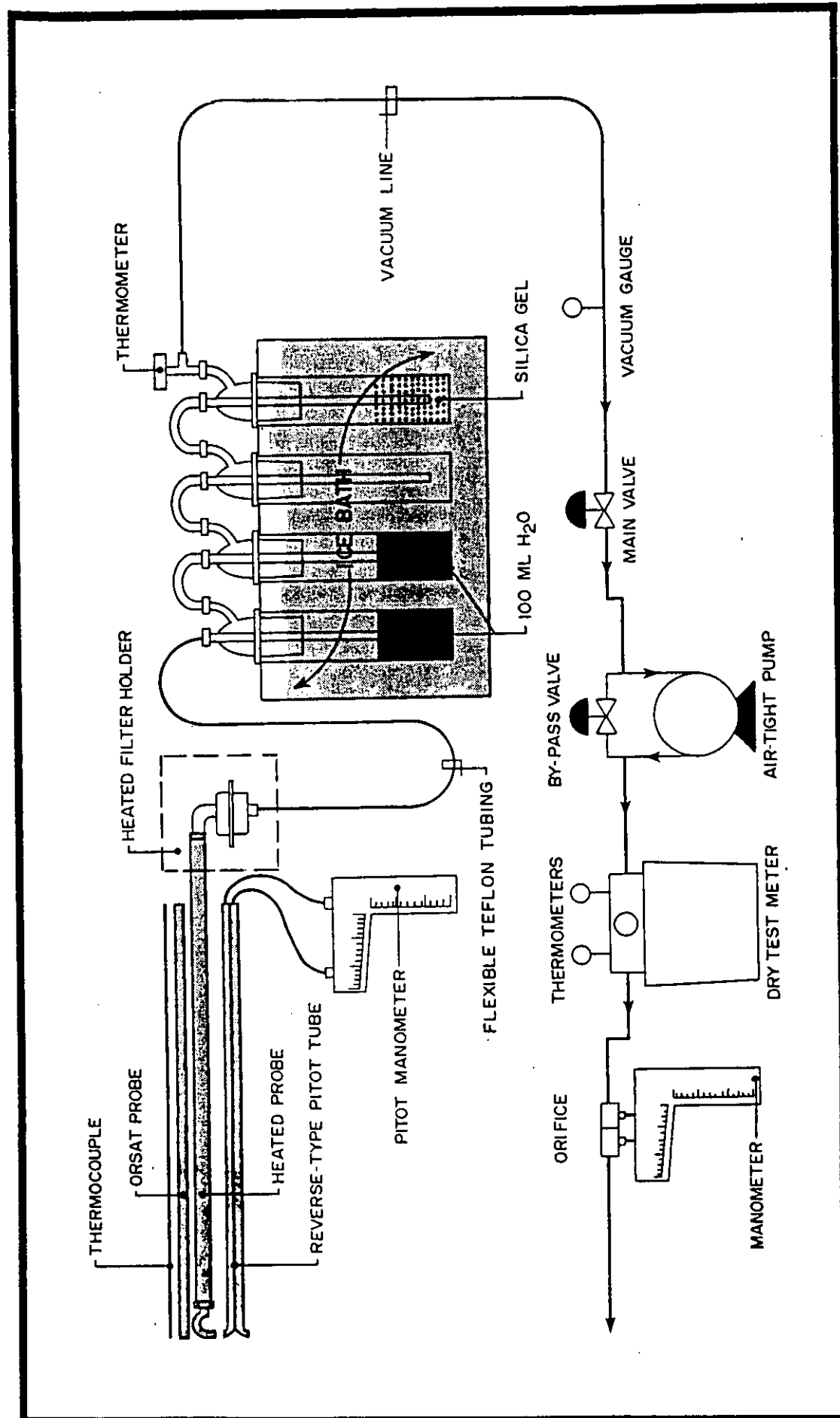


FIGURE 1.1
 EPA METHOD 5 SAMPLING TRAIN

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pyrometer. Velocity head measurements were made with a calibrated type "s" pitot tube and an inclined manometer. Velocity head measurements of 0.05 inches H₂O or less were measured using a micromonometer.

The sampling traverse points were selected so that a representative sample could be extracted from the gas stream. The traverse points were located in the center of equal areas, the number of which were dependent upon the distance upstream or downstream from flow disturbances. USEPA Methods 1 and 2 were utilized for this task.

Each particulate matter test run consisted of sampling for a specific amount of time at each point. The type "s" pitot tube was connected to the sampling probe so that an instantaneous velocity head measurement could be made at each traverse point while conducting the test run. The stack gas temperature was also measured at each traverse point. Together with assumed moisture and orsat knowledge as well as known nozzle area, calculations of "isokinetic" (equal energy or velocity) were quickly made and effected for each traverse point during the test run.

The gases sampled passed through the following components: a stainless steel nozzle and glass probe; a glass fiber filter; two impingers charged with 100 ml of distilled water each; one dry impinger; one impinger with 200 grams of silica gel desiccant; a flexible length of tubing; a leak free pump; a calibrated dry gas meter; and, finally, a calibrated flow orifice.

Sample recovery was accomplished in the following manner:

1. The pre-tared filter was removed from its holder and placed in Container 1 and sealed. (This is usually performed in the lab).
2. All sample-exposed surfaces prior to the filter were washed with acetone and placed in Container 2. The container was then sealed and the liquid level marked.
3. The volume of water from the first three impingers was measured for the purpose of calculating the moisture content of the stack gases, then discarded.
4. The silica gel from the fourth impinger was transferred to the original tared container and sealed.

LABORATORY ANALYSIS

The three sample containers from each sample run were analyzed according to the following procedures:

1. The filter was either dried for two hours at 105 degrees C or desiccated for 24 hours at ambient temperature. Following desiccation, the filter was weighed to the nearest 0.1 mg. A minimum of two such weighings six hours apart were made with a variance of less than 0.5 mg.
2. The acetone from Container 2 was transferred to a tared beaker, evaporated to dryness, and weighed in the same manner as above.
3. The used silica gel in its tared container was weighed to the nearest 0.1 gram.

The total sample weight included the weight gains from Sample Containers 1 and 2.

DATA

All relevent field and lab data sheets as well as emission calculations are provided in the report appendices.

APPENDIX A
COMPLETE EMISSION DATA
AND
SAMPLE CALCULATIONS

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Complete Emission Data

PLANT: ATLANTIC SUGAR ASSOCIATION	DATE: 11-29-90
LOCATION: BELLE GLADE, FLORIDA	RUN NUMBER 1
SOURCE: NUMBER 4 SCRUBBER OUTLET	TIME: 0845-0945

TIME INTERVAL----- 60 MINUTES

OIL:

FINAL OIL-----	0
BEGIN OIL-----	0
FACTOR-----	1

STEAM:

FINAL STEAM-----	9548
BEGIN STEAM-----	8457
FACTOR-----	100
TEMPERATURE-----	543 DEGREES F
PRESSURE-----	234 PSIG
	249 PSIA

FEEDWATER:

TEMPERATURE-----	250 DEGREES F
PRESSURE-----	350 PSIG
	365 PSIA

HEAT INPUT:

STEAM-----	1287.5 BTU/LB
FEEDWATER-----	218.4 BTU/LB
NET STEAM-----	1069.0 BTU/LB
STEAM RATE-----	109100 LB/HR
BOILER EFFICIENCY-----	55.0 %
TOTAL FUEL HEAT INPUT-----	212.05 MMBTUH
STEAM CALIBRATION FACTOR-----	1.00

OIL-----	0.00 GPH
OIL-----	150000 BTU/GAL

TOTAL HEAT INPUT (OIL)-----	0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)-----	212.05 MMBTUH

ALLOWABLES:

ALLOWABLE EMISSION (OIL)-----	.10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)-----	.29 LB/MMBTU
TOTAL ALLOWABLE EMISSION-----	61.50 LB/HR
TOTAL ACTUAL EMISSION-----	42.21 LB/HR
TOTAL ALLOWABLE EMISSION-----	0.290 LB/MMBTU
TOTAL ACTUAL EMISSION-----	0.199 LB/MMBTU

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Complete Emission Results

Plant:	ATLANTIC SUGAR ASSOCIATION	Date:	11-29-90
Location:	BELLE GLADE, FLORIDA	Run 1	From 0845 - 0946
Stack:	NUMBER 4 BOILER		

Y Factor	0.994	Nozzle Diameter	0.230 In.
Total Time	60.00 Min	Nozzle Area	0.000289 Ft ²
Stack Area	27.883 Ft ²	Barometric Pressure	30.40 In Hg
Stack Temperature	173.6 °F	Meter Temperature	74.9 °F
Stack Pressure	30.40 In Hg	Meter Orifice Diff	1.716 In H2O
Stack Avg √ Vel Head	0.989 In H2O	Meter Volume	39.492 CF
		Condensate Vol	292.80 ml

1. Volume Water Vapor Sampled	13.782	SCF
2. Volume Standard Dry Gas Sampled	39.518	SCF
3. Total Standard Sample Volume	53.300	SCF
4. Percent Moisture	25.900	
5. Percent Dry Air	74.100	
6. Molecular Weight of Dry Flue Gas	29.860	
7. Molecular Weight of Wet Flue Gas	26.788	
8. Specific Gravity Flue Gas	0.93	
9. Percent Oxygen [O2]	10.50	
10. Percent Carbon Dioxide [CO2]	9.00	
11. Percent Excess Air	97.656	
12. Velocity of Flue Gas	62.646	FPS
13. Actual Volumetric Flow Rate	104805.1	ACFM
14. Dry Volumetric Flow Rate	77660.6	ACFMD
15. Standard Volumetric Flow Rate	65755.4	SCFMD
16. Emission Concentration	0.0749	gr/SCF
17. Emission Concentration	0.0470	gr/ACF
18. Emission Rate	42.21	lbs/Hr
19. Percent Isokinetic	96.8	

Probe/Nozzle Wash	21.4	mg
Filter	170.4	mg
Total	191.8	mg

Plant: ATLANTIC SUGAR ASSOCIATION
Date: 11-29-90
Stack: NUMBER 4 BOILER
Run Number: 1

Average SQR Velocity Head = 0.989

Velocity Head Inputs:

0.7800	0.7400	1.1000	1.1000	1.1000	1.1500	1.1000
1.1500	1.1500	1.0500	0.6100	0.8000	0.8000	0.8300
0.8700	0.9700	1.0000	1.1000	1.1500	1.1500	

Average Orifice Pressure = 1.716

Orifice Pressure Inputs:

1.2500	1.2000	1.7500	1.7500	1.7500	1.9000	1.8500
2.1000	2.1000	1.9000	1.1000	1.4400	1.4400	1.5000
1.5500	1.7500	1.8000	2.0000	2.1000	2.1000	

Average Stack Temperature = 173.6

Stack Temperature Inputs:

169	171	172	175	177	176	176
176	176	173	170	172	171	172
172	172	177	176	174	175	

Average Meter Temperature = 74.9

Meter Temperature Inputs:

68	69	70	70	71	72	73
73	74	75	76	76	76	77
78	79	79	80	80	81	

Plant: ATLANTIC SUGAR ASSOCIATION
 Date: 11-29-90
 Stack: NUMBER 4 BOILER

Vwv Volume Water Vapor Sampled

$$Vwv = 0.04707 \times 292.8 = 13.782 \text{ SCF}$$

VMstd Volume Standard Dry Gas Sampled

$$VMstd = 17.64 \times 39.492 \times 0.994 \times [30.40 + (1.716 / 13.6)] / (74.9 + 460) = 39.518 \text{ SCF}$$

Vt Total Standard Sample Volume

$$Vt = 13.782 + 39.518 = 53.300 \text{ SCF}$$

$$W \text{ Percent Water} = (13.782 / 53.300) \times 100 = 25.9 \%$$

$$FDA \text{ Percent Dry Air} = (1 - 0.259) \times 100 = 74.1 \%$$

Md Molecular Weight of Dry Stack Gas

$$Md = (0.44 \times 9.00 \%CO_2) + (0.32 \times 10.50 \%O_2) + [0.28 \times (80.50 \%N_2 + 0.00 \%CO)] = 29.860$$

Ms Molecular Weight of Wet Stack Gas

$$Ms = (29.860 \times 0.741) + (18 \times 0.259) = 26.788$$

SG Specific Gravity Stack Gas

$$SG = 26.788 / 28.84 = 0.93$$

Ea Percent Excess Air

$$Ea = ((10.5 \%O_2) - (0 \%CO / 2)) \times 100$$

$$Ea = \frac{[(0.264 \times (80.5 \%N_2)) - (10.5 \%O_2) - (0 \%CO / 2)]}{97.656}$$

Vs Velocity of Stack

$$Vs = (85.49 \times 0.84 \times 0.989) \times \sqrt{(173.6 + 460) / (30.40 \times 26.788)} \\ Vs = 62.646$$

Qa Actual Volumetric Flow

$$Qa = (27.883 \times 62.646 \times 60) = 104805.1 \text{ ACFM}$$

Qd Dry Volumetric Flow

$$Qd = (104805.1 \times 0.741) = 77660.6 \text{ ACFMD}$$

Qsd Standard Volumetric Flow

$$Qsd = 104805.1 \times 0.741 \times [528 / (173.6 + 460)] \times (30.40 / 29.92) = 65755.4 \text{ SCFMD}$$

Plant: ATLANTIC SUGAR ASSOCIATION
Date: 11-29-90
Stack: NUMBER 4 BOILER

ESTP Emission Rate

$$\text{gr/SCF} = [0.01543 \times (21.4 + 170.4)] / (39.518)$$
$$\text{gr/SCF} = 0.0749$$

Lbs/Hr Emission Rate

$$\text{Lbs/Hr} = 0.0749 / 7000 \times 65755.4 \times 60 = 42.21$$

I Percent Isokinetic

$$I = 100 \times (173.6 + 460) \times [(0.002669 \times 292.8) + (39.492 \times 0.994 / (74.9 + 460)) \times (30.40 + (1.716 / 13.6))] / (60 \times 60 \times 62.646 \times 30.40 \times 0.000289)$$
$$I = 96.8 \%$$

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Complete Emission Data

PLANT: ATLANTIC SUGAR ASSOCIATION	DATE: 11-29-90
LOCATION: BELLE GLADE, FLORIDA	RUN NUMBER 2
SOURCE: NUMBER 4 SCRUBBER OUTLET	TIME: 1100-1200

TIME INTERVAL----- 60 MINUTES

OIL:

FINAL OIL-----	0
BEGIN OIL	0
FACTOR-----	1

STEAM:

FINAL STEAM-----	2058
BEGIN STEAM	902
FACTOR-----	100
TEMPERATURE	550 DEGREES F
PRESSURE-----	252 PSIG
	267 PSIA

FEEDWATER:

TEMPERATURE-----	250 DEGREES F
PRESSURE	350 PSIG
	365 PSIA

HEAT INPUT:

STEAM-----	1290.1 BTU/LB
FEEDWATER	218.4 BTU/LB
NET STEAM-----	1071.6 BTU/LB
STEAM RATE	115600 LB/HR
BOILER EFFICIENCY-----	55.0 %
TOTAL FUEL HEAT INPUT	225.24 MMBTUH
STEAM CALIBRATION FACTOR-----	1.00

OIL-----	0.00 GPH
OIL	150000 BTU/GAL

TOTAL HEAT INPUT (OIL)-----	0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)	225.24 MMBTUH

ALLOWABLES:

ALLOWABLE EMISSION (OIL)-----	.10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)	.29 LB/MMBTU

TOTAL ALLOWABLE EMISSION-----	65.32 LB/HR
TOTAL ACTUAL EMISSION	44.18 LB/HR

TOTAL ALLOWABLE EMISSION-----	0.290 LB/MMBTU
TOTAL ACTUAL EMISSION	0.196 LB/MMBTU

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Complete Emission Results

Plant:	ATLANTIC SUGAR ASSOCIATION	Date:	11-29-90
Location:	BELLE GLADE, FLORIDA	Run	2
Stack:	NUMBER 4 BOILER	From	1100 - 1201

Y Factor	0.994	Nozzle Diameter	0.230 In
Total Time	60.00 Min	Nozzle Area	0.000289 Ft ²
Stack Area	27.883 Ft ²	Barometric Pressure	30.40 In Hg
Stack Temperature	176.3 °F	Meter Temperature	80.5 °F
Stack Pressure	30.39 In Hg	Meter Orifice Diff	1.999 In H ₂ O
Stack Avg √ Vel Head	1.023 In H ₂ O	Meter Volume	42.375 CF
		Condensate Vol	328.40 ml

1. Volume Water Vapor Sampled	15.458	SCF
2. Volume Standard Dry Gas Sampled	41.992	SCF
3. Total Standard Sample Volume	57.450	SCF
4. Percent Moisture	26.900	
5. Percent Dry Air	73.100	
6. Molecular Weight of Dry Flue Gas	29.916	
7. Molecular Weight of Wet Flue Gas	26.711	
8. Specific Gravity Flue Gas	0.93	
9. Percent Oxygen [O ₂]	9.50	
10. Percent Carbon Dioxide [CO ₂]	9.60	
11. Percent Excess Air	80.117	
12. Velocity of Flue Gas	65.042	FPS
13. Actual Volumetric Flow Rate	108813.2	ACFM
14. Dry Volumetric Flow Rate	79542.4	ACFMD
15. Standard Volumetric Flow Rate	67046.2	SCFMD
16. Emission Concentration	0.0769	gr/SCF
17. Emission Concentration	0.0474	gr/ACF
18. Emission Rate	44.18	lbs/Hr
19. Percent Isokinetic	100.9	

Probe/Nozzle Wash	15.7	mg
Filter	193.5	mg
Total	209.2	mg

Plant: ATLANTIC SUGAR ASSOCIATION
Date: 11-29-90
Stack: NUMBER 4 BOILER
Run Number: 2

Average SQR Velocity Head = 1.023

Velocity Head Inputs:

0.9700	0.9500	1.1000	1.1500	1.1500	1.1500	1.1500
1.1500	1.1500	1.1000	0.6800	0.7800	0.8800	0.9800
0.9800	1.1000	1.1500	1.1500	1.1500	1.1500	

Average Orifice Pressure = 1.999

Orifice Pressure Inputs:

1.8000	1.8000	2.0500	2.2000	2.2000	2.2000	2.2000
2.2000	2.2000	2.1000	1.3000	1.5000	1.7000	1.8600
1.8600	2.1000	2.2000	2.2000	2.1000	2.2000	

Average Stack Temperature = 176.3

Stack Temperature Inputs:

170	173	174	176	176	178	177
176	177	178	175	176	177	178
178	179	178	174	177	178	

Average Meter Temperature = 80.5

Meter Temperature Inputs:

75	75	76	77	77	78	79
79	80	80	82	82	82	83
83	84	84	84	85	85	

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Complete Emission Data

PLANT:	ATLANTIC SUGAR ASSOCIATION	DATE:	11-29-90
LOCATION:	BELLE GLADE, FLORIDA	RUN NUMBER	3
SOURCE:	NUMBER 4 SCRUBBER OUTLET	TIME:	1315-1415

TIME INTERVAL----- 60 MINUTES

OIL:

FINAL OIL-----	0
BEGIN OIL	0
FACTOR-----	1

STEAM:

FINAL STEAM-----	4683
BEGIN STEAM	3512
FACTOR-----	100
TEMPERATURE	547 DEGREES F
PRESSURE-----	244 PSIG
	259 PSIA

FEEDWATER:

TEMPERATURE-----	250 DEGREES F
PRESSURE	350 PSIG
	365 PSIA

HEAT INPUT:

STEAM-----	1288.8 BTU/LB
FEEDWATER	218.5 BTU/LB
NET STEAM-----	1070.3 BTU/LB
STEAM RATE	117100 LB/HR
BOILER EFFICIENCY-----	55.0 %
TOTAL FUEL HEAT INPUT	227.88 MMBTUH
STEAM CALIBRATION FACTOR-----	1.00
OIL-----	0.00 GPH
OIL	150000 BTU/GAL

TOTAL HEAT INPUT (OIL)-----	0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)	227.88 MMBTUH

ALLOWABLES:

ALLOWABLE EMISSION (OIL)-----	.10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)	.29 LB/MMBTU
TOTAL ALLOWABLE EMISSION-----	66.08 LB/HR
TOTAL ACTUAL EMISSION	45.67 LB/HR
TOTAL ALLOWABLE EMISSION-----	0.290 LB/MMBTU
TOTAL ACTUAL EMISSION	0.200 LB/MMBTU

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Complete Emission Results

Plant: ATLANTIC SUGAR ASSOCIATION
 Location: BELLE GLADE, FLORIDA Date: 11-29-90
 Stack: NUMBER 4 BOILER Run 3 From 1315 - 1416

Y Factor	0.994	Nozzle Diameter	0.230 In
Total Time	60.00 Min	Nozzle Area	0.000289 Ft ²
Stack Area	27.889 Ft ²	Barometric Pressure	30.40 In Hg
Stack Temperature	178.9 °F	Meter Temperature	83.6 °F
Stack Pressure	30.39 In Hg	Meter Orifice Diff	1.887 In H ₂ O
Stack Avg √ Vel Head	0.997 In H ₂ O	Meter Volume	41.127 CF
		Condensate Vol	316.40 ml

1. Volume Water Vapor Sampled	14.893	SCF
2. Volume Standard Dry Gas Sampled	40.512	SCF
3. Total Standard Sample Volume	55.405	SCF
4. Percent Moisture	26.900	
5. Percent Dry Air	73.100	
6. Molecular Weight of Dry Flue Gas	29.916	
7. Molecular Weight of Wet Flue Gas	26.711	
8. Specific Gravity Flue Gas	0.93	
9. Percent Oxygen [O ₂]	9.50	
10. Percent Carbon Dioxide [CO ₂]	9.60	
11. Percent Excess Air	80.117	
12. Velocity of Flue Gas	63.518	FPS
13. Actual Volumetric Flow Rate	106287.0	ACFM
14. Dry Volumetric Flow Rate	77695.8	ACFMD
15. Standard Volumetric Flow Rate	65218.0	SCFMD
16. Emission Concentration	0.0817	gr/SCF
17. Emission Concentration	0.0501	gr/ACF
18. Emission Rate	45.67	lbs/Hr
19. Percent Isokinetic	100.1	

Probe/Nozzle Wash	17.5	mg
Filter	197.0	mg
Total	214.5	mg

Avg O₂ = 9.8

T_{amb} = 172

Flow = 66,000

Input = 222

Plant: ATLANTIC SUGAR ASSOCIATION
Date: 11-29-90
Stack: NUMBER 4 BOILER
Run Number: 3

Average SQR Velocity Head = 0.997

Velocity Head Inputs:

0.9300	0.9700	1.0000	1.1000	1.1000	1.0000	1.0000
1.0000	1.0000	1.0000	0.6300	0.7400	0.8500	0.9300
0.9500	1.1000	1.1000	1.2000	1.2000	1.2000	

Average Orifice Pressure = 1.887

Orifice Pressure Inputs:

1.7500	1.8500	1.9000	2.1000	2.0000	1.9000	1.9000
1.9000	1.9000	1.9000	1.2000	1.4000	1.6000	1.7500
1.8000	2.0000	2.0000	2.3000	2.3000	2.3000	

Average Stack Temperature = 178.9

Stack Temperature Inputs:

176	178	177	179	180	181	180
179	182	180	177	177	178	177
180	180	181	179	178	179	

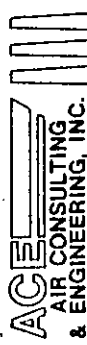
Average Meter Temperature = 83.6

Meter Temperature Inputs:

78	78	79	79	80	81	82
82	83	84	85	85	86	86
86	87	87	88	88	88	

APPENDIX B
FIELD DATA SHEETS

STACK SAMPLING FIELD DATA SHEET



2106 N. W. 67th PLACE - SUITES 9 & 10
GAINESVILLE, FLORIDA 32606

PLANT ATLANTIC SUGAR ASSOCIATED
SOURCE NO. 4 BOLLER

PLANT LOCATION BELLE GLADE, FL.

TYPE OF SAMPLING TRAIN EPA-5

TYPE OF SAMPLES PM

DATE 11-29-90 RUN NO. 1

TIME START 0845 TIME END 0946

SAMPLE TIME 20 (min/pt) = 60 Total min

ASSUMED MOISTURE 28 % FDA 72

NOMOGRAPH C₁ 1.68 PITOT CORR. 284

P_b 30.4 "Hg P_s 30.25 "Hg

WEATHER CLEAR TEMP. °F

METER BOX NO. 1 H 2.05 V 0.994

NOZZLE CAL. 230 230 230 = 230

STACK DIMENSIONS 71.5

STACK AREA 27.883 ft² EFFECTIVE 11.2

STACK HEIGHT ft.

STACK DIAMETER: UPSTRM. DNSTRM.

PORT SIZE in. NIPPLE LENGTH in.

U CORD LENGTH 125

REMARKS: 109100 lbs 543°F

234 PSI

PM 250°F-350

TEST ID _____

PAGE _____ OF _____

MAT'L PROCESSING RATE _____

GAS METER READINGS: FINAL 216.470 ft³

INITIAL 116.978 ft³

NET _____ ft³

FILTER NO. 2876 IMP. VOL. GAIN 285 ml.

SIL GEL NO. 25 WT. GAIN 7.8 ml.

TOTAL CONDENSATE 292.8 ml.

ORSAT

	1	2	3	4	AVG.
% CO ₂					<u>9.0</u>
% O ₂					<u>10.5</u>
% CO					
% N ₂					

F₀ = _____ F₀ RANGE = _____

ORSAT ANALYZER _____

LEAK CHECKS _____

PRE 0.02 cfm 19 "Hg POST 0.000 cfm 25 "Hg

METER BOX/PUMP _____ GAS SAMPLE SYST. _____

ORSAT BAG _____

PITOT TUBE NO. 1601 PRE-TEST 0.1K

POST-TEST (+) 3.8 / 15 H₂O/Sec

POST-TEST (-) 4.1 / 15 H₂O/Sec

PYROMETER NO. _____

BOX OPERATOR NEEK PROBE HOLDER CEMNO

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (FT ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O") CALC. ACTUAL	STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP (°F)	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
1-1		0848	178.75	.78	1.25 1.25	169	251	50	68	6.0
2		0853	180.45	.74	1.2 1.2	171	252	46	69	6
3		0854	182.42	1.1	1.75 1.75	172	253	44	70	8
4		0859	184.40	1.1	1.75 1.75	175	251	44	70	8.5
5		0900	186.43	1.1	1.75 1.75	177	251	44	71	9
6		0905	188.52	1.15	1.9 1.9	176	248	50	72	10

5780
4074
170.6
17.1

41.37

[illegible]

STACK SAMPLING FIELD DATA SHEET



2106 N. W. 67th PLACE, SUITES 9 & 10
GAINESVILLE, FLORIDA 32606

TEST ID _____
PAGE _____ OF _____

PLANT ATLANTIC SUGAR ASSOCIATION
SOURCE No. 4 BOILER

PLANT LOCATION BEULIE GLADE, FLORIDA
TYPE OF SAMPLING TRAIN FPA-5

TYPE OF SAMPLES P.M.

DATE 11-29-90 RUN NO. 2

TIME START 10:00 TIME END 12:01

SAMPLE TIME 20, 3 (min/pt) = 60 Total min

ASSUMED MOISTURE 26 % FDA 74

NOMOGRAPH 1.85 PITOT CORR. .84

P_b 30.4 "Hg P_s 30.39 "Hg

WEATHER CLEAR TEMP °F

METER BOX NO. 1 H 205 V 994

NOZZLE CAL. _____ = 230

STACK DIMENSIONS _____

STACK AREA 27.883 ft² EFFECTIVE _____ ft²

STACK HEIGHT 2 ft

STACK DIAMETER: UPSTRM. _____ DNSTRM. _____

PORT SIZE _____ in. NIPPLE LENGTH _____ in.

U CORD LENGTH 125

REMARKS: _____

MAT'L PROCESSING RATE _____

GAS METER READINGS: FINAL 257.130 ft³

INITIAL 216.753 ft³

NET _____ ft³

FILTER NO. 2877 IMP. VOL. GAIN 320 ml.

SIL GEL NO. 14 WT. GAIN 8.4 ml.

TOTAL CONDENSATE 328.4 ml.

ORSAT

	1	2	3	4	AVG.
% CO ₂					<u>9.6</u>
% O ₂					<u>9.5</u>
% CO					
% N ₂					

F₀ = _____ F₀ RANGE = _____

ORSAT ANALYZER _____

LEAK CHECKS _____

PRE 0.00 cfm 24 "Hg POST 0.000 cfm 24 "Hg

METER BOX/PUMP _____ GAS SAMPLE SYST. _____

ORSAT BAG _____

PITOT TUBE NO. 1601 PRE-TEST 0.4

POST-TEST (+) 4.6 / 13 H₂O/Sec

POST-TEST (-) 3.3 / 15 H₂O/Sec

PYROMETER NO. 1

BOX OPERATOR NECK PROBE HOLDER GERARD

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (FT ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O") CALC. ACTUAL	STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP (°F)	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
1-1		1103	218.85	.97	1.8 1.8	170	240	57	75	7
2		1106	220.88	.95	1.8 1.8	173	234	57	75	7
3		1109	223.03	1.1	2.05 2.05	174	230	56	76	8.5
4		1112	225.22	1.65	2.2 2.2	176	227	56	79	10
5		1115	227.43	1.15	2.2 2.2	176	225	58	77	10
6		1118	229.61	1.15	2.2 2.2	178	230	59	78	10

6050
14075
147.5
19.8

ACE
AIR CONSULTING
& ENGINEERING, INC.

000289

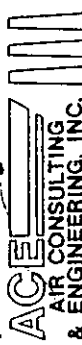
932-63

[illegible]

STACK SAMPLING FIELD DATA SHEET

PLANT ATLANTIC SUGAR ASSOCIATION
 SOURCE No. 4 Boiler
 PLANT LOCATION BEZEL GULF, FLORIDA
 TYPE OF SAMPLING TRAIN EPA-5
 TYPE OF SAMPLES P.M.
 DATE 11-29-90 RUN NO. 3
 TIME START 1315 TIME END 1416
 SAMPLE TIME 2013 (min/pt) = 60 Total min
 ASSUMED MOISTURE 26 % FDA 74
 NOMOGRAPH C₁ 1.9 PITOT CORR. .84
 P_b 30.4 "Hg P_s 30.39 "Hg
 WEATHER CLEAR TEMP. 85 °F
 METER BOX NO. 1 H 2.05 Y 205.734
 NOZZLE CAL. 71.5 = 2.30

STACK DIMENSIONS 71.5
 STACK AREA 27.889 ft² EFFECTIVE ft²
 STACK HEIGHT ft
 STACK DIAMETER: UPSTRM. DNSTRM.
 PORT SIZE in. NIPPLE LENGTH in.
 U CORD LENGTH 125
 REMARKS:



2106 N. W. 67th PLACE · Suites 9 & 10
 GAINESVILLE, FLORIDA 32606

MAT'L PROCESSING RATE
 GAS METER READINGS: FINAL 301.874 ft³
 260.747 INITIAL 260.747 ft³
 NET ft³
 FILTER NO. 2878 IMP. VOL. GAIN 310 ml.
 SIL GEL NO. 604 WT. GAIN 604 ml.
 TOTAL CONDENSATE 316.4 ml.

ORSAT

	1	2	3	4	AVG.
% CO ₂					9.6
% O ₂					9.5
% CO					
% N ₂					

F₀ = F₀ RANGE =

ORSAT ANALYZER

LEAK CHECKS

PRE 0.00 cfm 23 "Hg POST 0.000 cfm 26 "Hg
 METER BOX/PUMP GAS SAMPLE SYST.
 ORSAT BAG PRE-TEST 0.1
 PITOT TUBE NO. 1601 5.3 / 15 H₂O/Sec
 POST-TEST (+) 3.0 / 15 H₂O/Sec
 POST-TEST (-) /
 PYROMETER NO.
 BOX OPERATOR NOTES PROBE HOLDER CONDARD

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (FT ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O") CALC. ACTUAL	STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP (°F)	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
1-1		1318	262.70	.93	1.75 1.75	176	238	57	78	7.0
2		1321	264.64	.97	1.85 1.85	178	237	57	78	7.5
3		1324	266.83	1.00	1.9 1.9	177	234	50	79	8
4		1327	269.0	1.1	2.1 2.1	179	229	57	79	9
5		1330	271.1	1.1	2.0 2.0	180	228	51	80	9
6		1333	273.2	1.0	1.9 1.9	181	234	57	81	9

[illegible]

APPENDIX C
LABORATORY ANALYSES

AIR CONSULTING & ENGINEERING, inc.

PARTICULATE LAB DATA

SOURCE

ASA No. 4 Boiler

PROBE RINSE	RUN 1	RUN 2	RUN 3	BLANK
CONTAINER NUMBER	S-1	S-6	S-23	S-33
TOTAL VOLUME (ml)	200	205	200	100
1st GROSS WEIGHT (g)	106.6278	103.1510	103.1069	100.7617
2nd GROSS WEIGHT (g)	106.6278	103.1512	103.1069	100.7615
AVERAGE GROSS WEIGHT (g)	106.6278	103.1511	103.1069	100.7616
TARE WEIGHT (g)	106.6063	103.1354	103.0894	100.7604
SUB NET WEIGHT (g)	0.0215	0.0157	0.0175	0.012
ACETONE BLANK (g)				
TOTAL NET WEIGHT (mg)	21.5	15.7	17.5	1.2

NOTE: In no case should a blank residue >0.01 mg/g or 0.001% of the weight of acetone used be subtracted from the sample weight.

FILTER	RUN 1	RUN 2	RUN 3	BLANK
FILTER NUMBER	2876	2877	2878	2839
1st GROSS WEIGHT (g)	0.5751	0.6010	0.6024	0.4078
2nd GROSS WEIGHT (g)	0.5750	0.6010	0.6021	0.4073
AVERAGE GROSS WEIGHT (g)	0.5751	0.6010	0.6023	0.4075
TARE WEIGHT (g)	0.4047	0.4075	0.4053	0.4081
SUB NET WEIGHT (g)	0.1704	0.1935	0.1970	0.0006
TOTAL NET WEIGHT (mg)	170.4	193.5	197.0	

TARE
BALANCE CHECK

SEE LAB BOOK

1st GROSS WEIGHT
BALANCE CHECK

0 0.0000 10.0g
0.5g 0.5001 100.0g 100.0000
%RH 46 DATE 12-3
Signature S. J. N. L.

2nd GROSS WEIGHT
BALANCE CHECK

0 0.0000 100g
0.5g 0.5000 100.0g 100.0000
%RH 46 DATE 12-4
Signature S. J. N. L.

AIR CONSULTING AND ENGINEERING, Inc.

SAMPLE RECOVERY AND CHAIN OF CUSTODY

PLANT NAME ASA TEST DATE 11-29-90
SOURCE NAME No. 4 BOILER SAMPLE RECOVERED BY SEN
TYPE OF SAMPLE pm PARTICULATE ANALYSES BY SEN

SAMPLE RECOVERY

RUN NO.	CONTAINER NO.	LIQUID LEVEL MARKED	COLOR	COMMENTS
1 PW	S-1	✓	.BLACKEN	
FIL	2876		BLACK	
2 PW	S-6	✓	"	
FIL	2877		"	
3 PW	S-23	✓	"	
FIL	2878		"	
(CIRCLE) ACETONE / WATER BLANK	S-33			
FILTER BLANK	2839			

SILICA GEL

RUN NO.	CONTAINER NO.	FINAL WT. (g)	INIT. WT. (g)	NET WT. (g)	COLOR
1	25	207.8	200.0	7.8	OK
2	14	208.4	200.0	8.4	"
3	42	206.4	200.0	6.4	"
			200.0		
			200.0		
			200.0		
			200.0		
			200.0		

APPENDIX D
QUALITY ASSURANCE
AND
CHAIN OF CUSTODY

AIR CONSULTING & ENGINEERING, inc.

POST TEST CALIBRATION

DATE 12-22-90 METER BOX NUMBER 1 LEAK CHECK 0.00 CFM at 22 in. Hg.
 CLIENT ATLANTIC SUGAR + S.G. Co-op SOURCE VAR 100-3 THERMOCOUPLE NUMBER 1601 PYROMETER NUMBER 1
 FLIGHT SERVICE Pb 30.11 in. Hg. ACE BAROMETER Pb 30.11 in. Hg.
 ASTM GLASS THERMOMETER 149 OF / THERMOCOUPLE 150 OF ASTM GLASS THERMOMETER 68 OF / METER TEMP 68 OF

Δ HS	AVERAGE Δ HD	GAS VOLUME, STANDARD METER			GAS VOLUME, DRY GAS METER			TEMP STANDARD METER	TEMP OF DRY METER	TIME (Minutes)	MAX. VACUUM In. Hg.
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³				
126	2.1	452.500	493.960	41.46	290.053	331.598	41.545	71 73	69 76	55	21
119	1.5	493.960	509.942	15.982	331.598	347.654	16.056	73 75	76 78	25	22
132	2.7	509.942	569.500	59.558	347.654	406.880	59.226	75 76	78 82	101	20

DELTA H
 2.068
 2.052
 4.341

Ys
 0.993
 0.995
 0.998

Y
 0.987
 0.992
 1.005

SCFM
 0.753
 0.636
 0.585

Ya
 0.994
 0.997
 1.007

CALIBRATED BY:

S. J. Decker

MEAN:

2.820

0.995

0.995

0.998

1.000

2.820

MEAN:

 air consulting and engineering

STANDARD METER CALIBRATION
Meter Number 1040616

Air Consulting and Engineering, Inc. (ACE) uses a dry gas meter for the calibration standard. This meter has been calibrated against a wet test meter in triplicate. This data was used to generate a standard meter calibration curve (see next page). Field meter calibrations are corrected to this curve using the following formula:

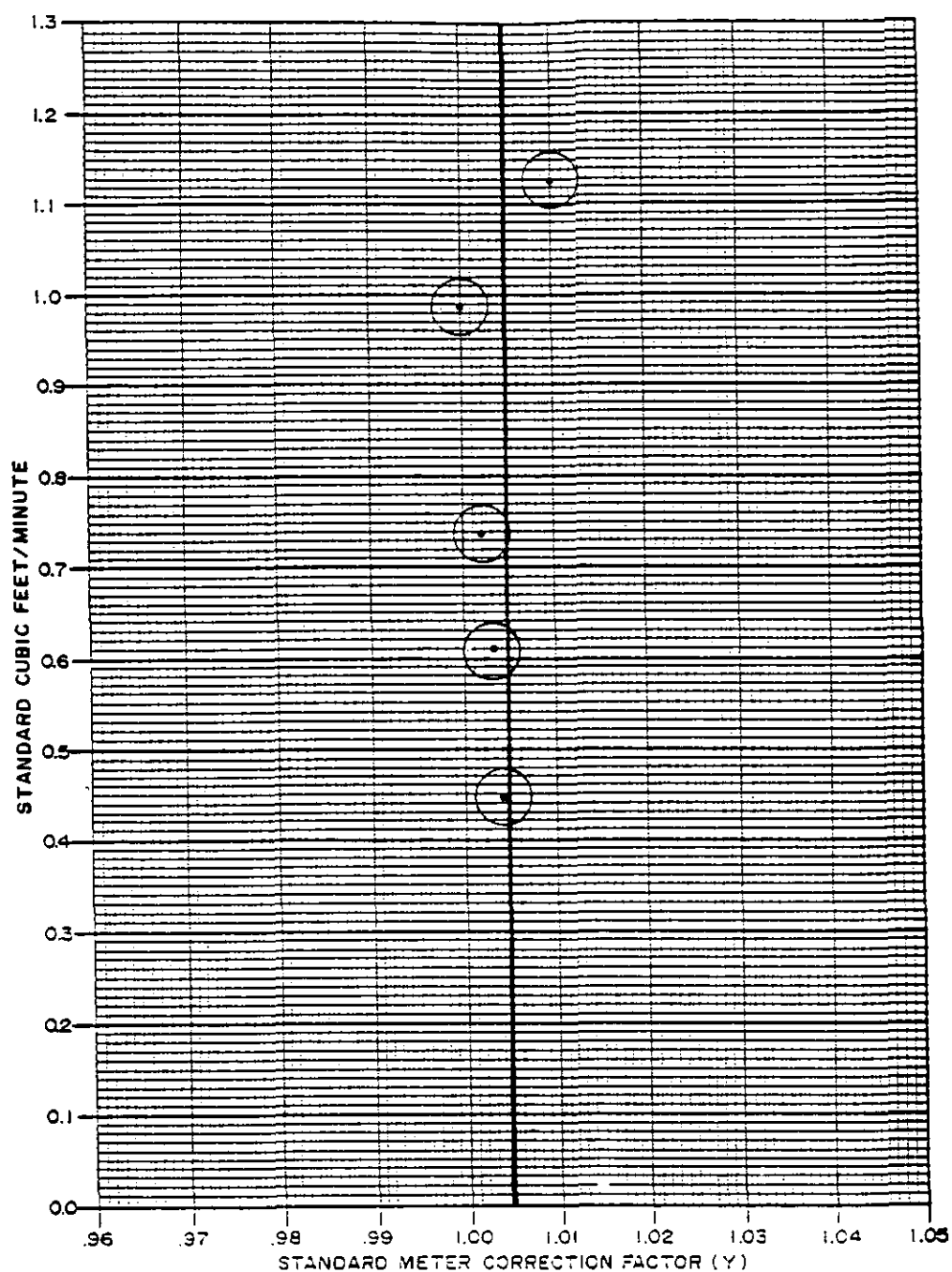
$$Y_a \times Y_s = Y$$

Y_a = actual ratio of field meter to standard meter

Y_s = ratio of standard meter to wet test meter at a given
flow rate (from Calibration Curve)

Y = corrected ratio of field meter

The dry standard meter was calibrated on November 23, 1990, and is checked and/or recalibrated at least annually.



STANDARD METER CALIBRATION CURVE
METER SERIAL NO. 1040616 (SOUTH)
NOVEMBER 23, 1990

AIR CONSULTING
and
ENGINEERING

AIR CONSULTING & ENGINEERING

STANDARD METER CALIBRATION

DATE 11-23-90 LEAK CHECK 0.000 CFM at 12 in. Hg.

METER SERIAL NUMBER 1040616 (South)

BAROMETRIC PRESSURE 30.07 in. Hg.

STD GAS METER TEMPERATURE 67 °F/ASTM GLASS THERMOMETER TEMPERATURE 69 °F

WET ΔH	STD ΔH	GAS VOLUME, WET TEST METER			GAS VOLUME, STD GAS METER			TEMP OF STD. METER (°F)	TIME (Minutes)
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³		
0.1	-1.1	0.000	5.333	5.333	272.003	277.309	5.306	70	12
0.1	-1.1	5.333	10.664	5.331	277.309	282.600	5.291	70	12
0.1	-1.1	10.664	15.982	5.318	282.600	287.877	5.277	70	12
0.3	-1.9	0.000	5.490	5.490	288.149	293.623	5.474	70	9
0.3	-1.9	5.490	12.799	7.309	293.623	300.898	7.275	70	12
0.3	-1.9	12.799	18.278	5.479	300.898	306.359	5.461	70	9
0.4	-2.5	0.000	5.160	5.160	306.712	311.863	5.151	70	7
0.4	-2.5	5.160	10.321	5.161	311.863	317.017	5.154	70	7
0.4	-2.5	10.321	15.488	5.167	317.017	322.173	5.156	70	7
0.5	-3.7	0.000	7.481	7.481	322.562	330.068	7.506	70	8
0.5	-3.7	7.481	14.039	6.558	330.068	336.655	6.587	70	7
0.5	-3.7	14.039	19.619	5.610	336.655	342.278	5.623	70	6
0.7	-5.3	0.000	5.639	5.639	342.618	348.279	5.631	70	5
0.7	-5.3	5.639	11.268	5.629	348.279	353.889	5.610	70	5
0.7	-5.3	11.268	16.889	5.621	353.889	359.498	5.609	70	5

CALIBRATED BY: A. F. Stahel

	Y	SCFM	Y	SCFM	Y	SCFM	Y	SCFM	Y	SCFM
Run 1	1.002	0.445	1.002	0.611	1.002	0.738	1.000	0.986	1.009	1.129
Run 2	1.005	0.445	1.004	0.610	1.002	0.738	0.999	0.986	1.011	1.127
Run 3	1.005	0.444	1.002	0.610	1.003	0.739	1.001	0.986	1.010	1.126
Average	1.004	0.444	1.003	0.610	1.002	0.738	1.000	0.986	1.010	1.127

 Air Consulting and Engineering

AIR CONSULTING & ENGINEERING, INC. PYROMETER CALIBRATION

DATE 7-10-90

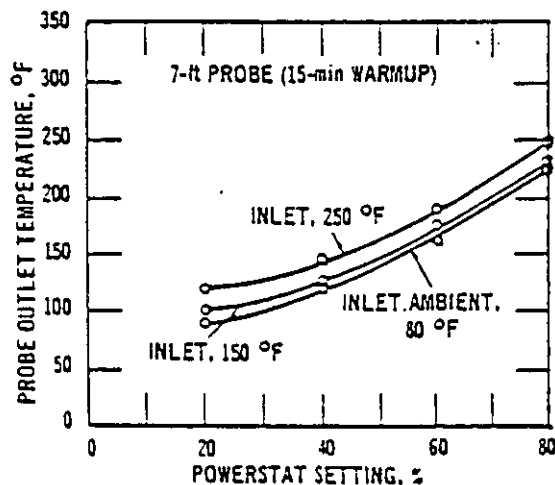
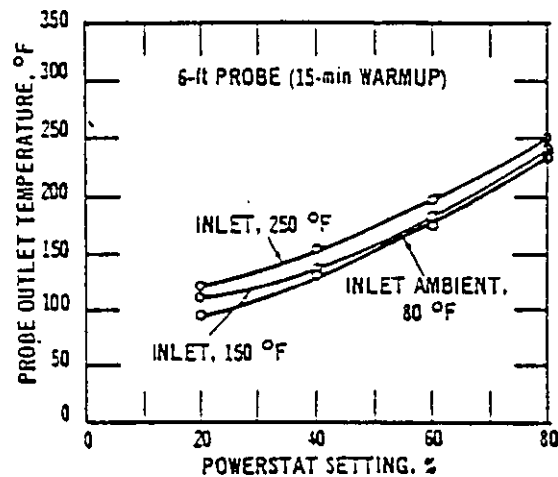
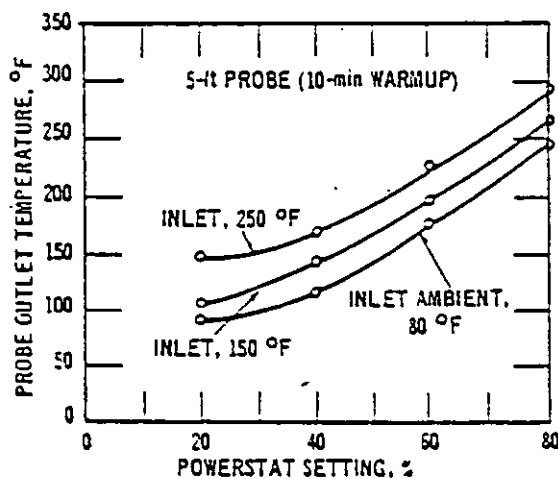
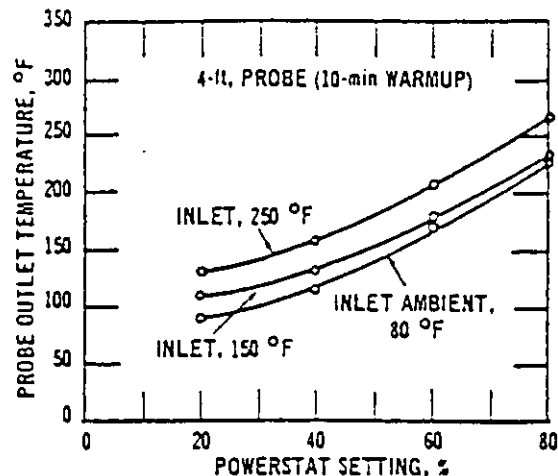
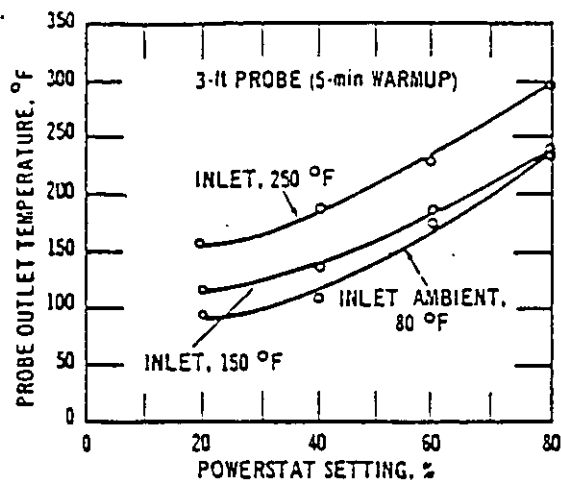
PYROMETER NUMBER METER BOX #1

SOURCE (SPECIFY)	GLASS THERMOMETER WITH NBS MERCURY (°F)	PYROMETER (°F)	DEGREE DIFFERENCE	PERCENT DIFFERENCE
ICE BATH	<u>32°</u>	<u>33°</u>	<u>1</u>	<u>.2%</u>
AMBIENT	<u>94°</u>	<u>96°</u>	<u>2</u>	<u>.4%</u>
HOT OVEN	<u>800°</u>	<u>800°</u>	<u>0</u>	<u>0</u>

FDER - MAXIMUM 5° DIFFERENCE

$$\text{EPA} \left[\frac{(\text{REF. TEMP. } ^\circ\text{F} + 460^\circ) - (\text{PYROMETER TEMP. } ^\circ\text{F} + 460^\circ)}{\text{REF. TEMP. } ^\circ\text{F} + 460^\circ} \right] 100 \leq 1.5\%$$

CALIBRATED BY: 



NOTE: Flow rate held constant at 0.75; 50% change in flow rate has little effect on probe temperature.

Probe temperatures.

AIR CONSULTING & ENGINEERING, INC.

PITOT TUBE CALIBRATION

DATE CALIBRATED 9-25-90

PITOT TUBE 1601

IS PITOT TUBE ASSEMBLY LEVEL YES

ARE PITOT TUBE OPENINGS DAMAGED NO

$\alpha_1 = 0^\circ (<10^\circ)$, $\alpha_2 = 1.5^\circ (<10^\circ)$, $\beta_1 = 1^\circ (<5^\circ)$, $\beta_2 = 2^\circ (<5^\circ)$

$\gamma = 1.5^\circ$, $\theta = 1^\circ$, $A = 1.179$ in. = $(P_a + P_b)$

$z = A \sin \gamma = 0.031$ in., $<0.32 / <1/8$ in.

$w = A \sin \theta = 0.021$ in., $<0.08 / <1/32$ in.

P_a 0.5895 in. P_b 0.5895 in. D_1 0.375

WAS CALIBRATION REQUIRED NO

THERMOCOUPLE CALIBRATION

SOURCE (SPECIFY)	ASTM GLASS THERMOMETER WITH MERCURY (°F)	PYROMETER (°F)	DEGREE DIFFERENCE	PERCENT DIFFERENCE
------------------	--	----------------	-------------------	--------------------

ICE BATH

AMBIENT

HOT OVEN

CALIBRATED BY: _____

FDER - MAXIMUM 5° DIFFERENCE

EPA $\left[\frac{(\text{REF. TEMP. } ^\circ\text{F} + 460^\circ) - (\text{PYROMETER TEMP. } ^\circ\text{F} + 460^\circ)}{\text{REF. TEMP. } ^\circ\text{F} + 460^\circ} \right] 100 \leq 1.5\%$

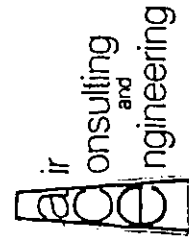
AIR CONSULTING & ENGINEERING, inc.

POST TEST CALIBRATION

DATE 11-27-90 METER BOX NUMBER 1 LEAK CHECK 0.00 CFM at 24 in. Hg.
 CLIENT ASA/SCGCOF SOURCE No 3 & No. 4 Boilers THERMOCOUPLE NUMBER 1601 PYROMETER NUMBER 1
 FLIGHT SERVICE Pb — in. Hg. ACE BAROMETER Pb — in. Hg. No. 1 Boilers & No. 2 Boilers
 ASTM GLASS THERMOMETER 173 °F / THERMOCOUPLE 173 °F ASTM GLASS THERMOMETER 73 °F / METER TEMP 74 °F

ΔHS	AVERAGE ΔHD	GAS VOLUME, STANDARD METER			GAS VOLUME, DRY GAS METER			TEMP. OF DRY METER	TIME (Minutes)	MAX. VACUUM in. Hg.
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³			
-15	1.3	374.714	382.073	7.359	979.100	986.776	7.676	73 73	84 85	13.0 15.0
-15	1.3	382.073	389.951	7.878	986.776	994.981	8.205	73 73	85 87	14.0 15
-15	1.3	390.000	397.812 397.812	7.812	995.033	1003.188	8.155	73 73	87 87	14.0 15

CALIBRATED BY: Stephen J. Nuel



$$Y_1 = 0.976$$

$$Y_2 = 0.980$$

$$Y_3 = 0.980$$

$$Y_{AVG} = 0.98$$

603
618
634

AIR CONSULTING & ENGINEERING

ANNUAL METER CALIBRATION

DATE 6-7-90 LEAK CHECK 0.000 CFM at 12 In. Hg.METER BOX NUMBER 1BAROMETRIC PRESSURE 30.02 In. Hg.DRY GAS METER TEMPERATURE 89 °F/ASTM GLASS THERMOMETER TEMPERATURE 90 °F

Δ HIS	AVERAGE Δ H/D	GAS VOLUME, STANDARD METER			GAS VOLUME, DRY GAS METER			TEMP STD METER	TEMP OF DRY METER	TIME (Minutes)	TIMER
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³				
-07	0.5	206.539	214.496	7.957	719.311	727.244	7.933	85	85	21	21
-15	1.25	215.308	221.239	5.931	728.042	733.952	5.910	85	86	10	
-22	2.0	221.610	227.578	5.968	734.320	740.265	5.945	85	87	8	
-32	2.75	228.029	233.291	5.262	740.708	745.940	5.232	86	88	6	
-40	3.5	233.668	239.592	5.924	746.315	752.205	5.890	87	90	6	
-50	4.25	240.117	245.527	5.410	752.724	758.112	5.388	87	91	5	

DELTA H	Y _a	SCFM	Y _s	Y
2.004	1.002	0.368	1.004	1.006
2.041	1.002	0.577	0.998	1.000
2.061	1.003	0.725	0.993	0.996
2.054	1.003	0.851	0.989	0.992
2.063	1.003	0.956	0.985	0.988
2.082	1.001	1.048	0.983	0.984
MEAN:				
2.051	1.002		0.992	0.994

CALIBRATED BY: H. F. Rabel

APPENDIX E
PRODUCTION RATE
CERTIFICATION

BOILER DATA SHEET

COMPANY ATLANTIC SUGAR ASSN.

REPORTED BY

Frank Cleman

DATE NOVEMBER 29, 1990

INTEGRATOR FACTOR $\times 100$

BOILER NO. 4

FUEL OIL USED No Oil

TIME	INTEGRATOR	LOG SCALE STEAM		TEMP.	FEED WATER	
		FLOW $\times 1460$	PRESSURE		TEMP.	PRESSURE
RUN 1 845	8457	85	235	555	250	350
900	8731	85	260	550	250	350
915	9023	95	225	530	250	350
930	9279	75	205	530	250	350
945	9548	75	245	545	250	350
60 MIN.	1091		234	543	250	350 AVG.
	$1091 \times 100 = 109,100 \text{ LBS/HR}$					
RUN 2 1100	0902	75	260	550	250	350
1115	1181	93	235	555	250	350
1130	1465	90	265	560	250	350
1145	1767	92	250	535	250	350
1200	2058	90	250	550	250	350
60 MIN.	1156		252	550	250	350 AVG.
	$1156 \times 100 = 115,600 \text{ LBS/HR}$					
RUN 3 1250/15	3512	92	250	550	250	350
130	3810	85	235	545	250	350
145	4092	91	250	550	250	350
200	4387	90	240	545	250	350
215	4683	92	245	545	250	350
60 MIN.	1171		244	547	250	350 AVG.
	$1171 \times 100 = 117,100 \text{ LBS/HR}$					

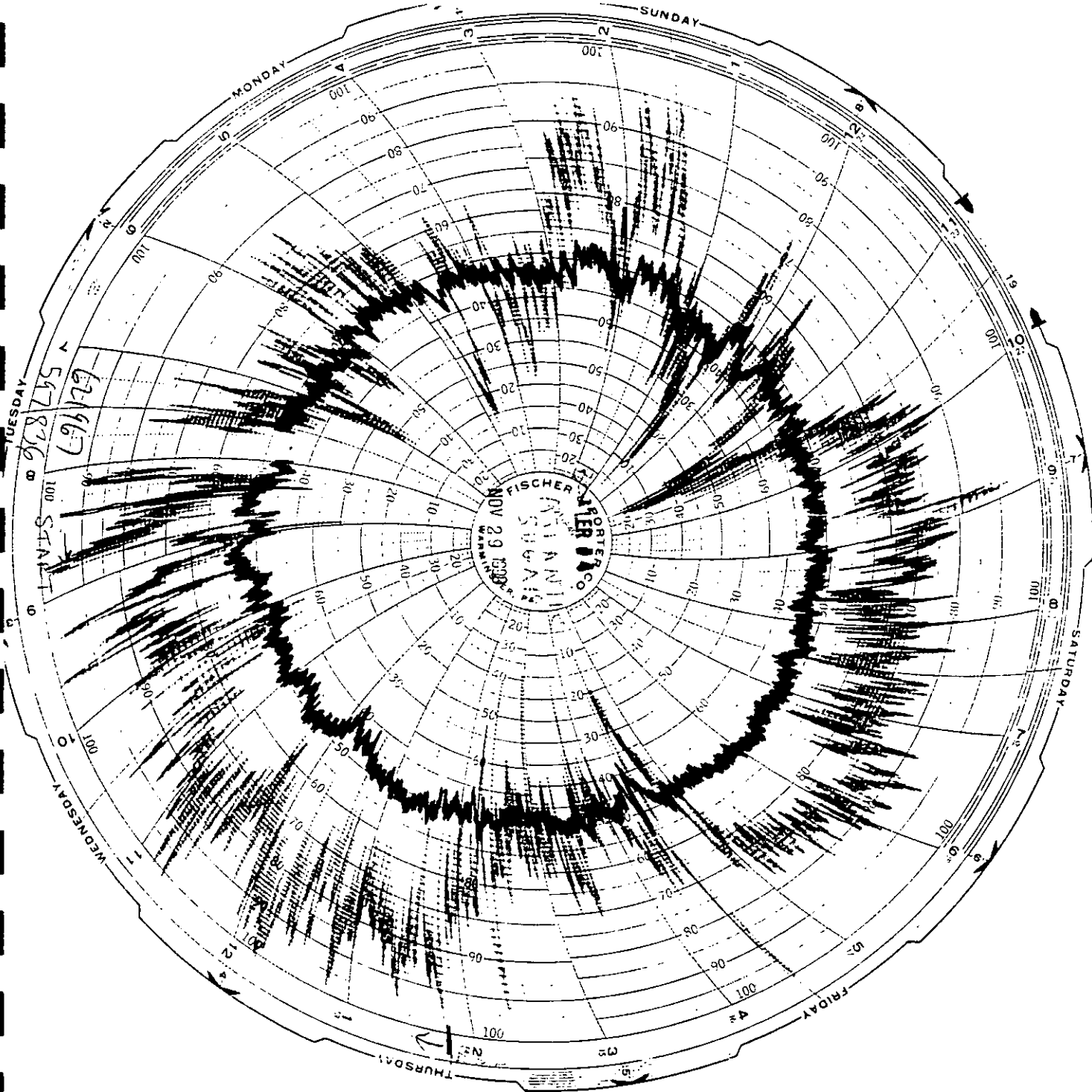
PROCESS DATA

INSTALLATION Boiler #4COMPANY ATLANTIC SUGAR ASSN.DATE NOVEMBER 29, 1990TYPE OF INSTALLATION BAGASSE BOILERTYPE OF MATERIAL PROCESSED STEAMTYPE OF FUEL USED BAGASSETYPE OF POLLUTION CONTROL SYSTEM WET SCRUBBER

	NORMAL	RUN 1	RUN 2	RUN 3
SCRUBBER WATER FLOW (GPM)	<u>350</u>	<u>325</u>	<u>370</u>	<u>345</u>
PRESSURE DROP (INCHES)	<u>4.0</u>	<u>3.2</u>	<u>3.6</u>	<u>3.5</u>

REPORTED BY

Frank Kleeman



APPENDIX F
PROJECT PARTICIPANTS

PROJECT PARTICIPANTS

ACEI:

STEPHEN L. NECK, P.E.

FIELD TESTING
REPORT PREPARATION

GERARD GAUTHREUX

FIELD TESTING

KLEEMAN ENGINEERING, INC

FRANK S. KLEEMAN, P.E.

PROJECT COORDINATOR

FDER

SHERRILL C. CULLIVER

Ref 5

INPUT SHEET - REV:09/13/83 - PAGE 2 OF 2

ENTER THE FOLLOWING:

	RUN1	RUN2	RUN3
1. H2O COLLECTED (ONLY VOL. MEASURED), ML:			
2. H2O COLLECTED (WEIGHED PART ONLY), GM:	358.0	268.2	264.0
3. M'N PARTICULATE WEIGHT, GM:	1790	1162.6	1913
4. V'M VOLUME METERED, CF:	47.336	31.314	32.19
5. Y DRY GAS METER CAL FACTOR:	1.001	1.001	1.001
6. RDP AVG SDR DELTA P (WHEN SAMPLING):	.70	.60	.67
7. DH AVG DELTA H, IN H2O:	3.03	1.23	1.33
8. T'M AVG METER TEMP, DEG F:	86.5	84.4	86.5
9. T'S AVG STACK TEMP, DEG F:	153.5	156.7	156
10. P'S* STACK PRESS, *IN (14.0):	30.30	30.18	30.19
11. P'B BAROMETRIC PRESS, IN HG:	30.09	30.10	30.10
13. D'N ACTUAL NOZZLE DIAMETER, IN.:	3.05	2.50	2.50
14. T ACTUAL SAMPLE TIME, MIN:	60	60	60
15. C'P PITOT TUBE COEFFICIENT:	.84	.84	.84
OPTION ENTRIES:	251.4	254.7	256.1
17. ORSAT/FYRITE - %CO2:		254.06	
18. ORSAT/FYRITE - %O2:			
20. ORSAT/FYRITE (FOR C'S @ 50% E.A.) - %CO:			
19. SPECIFIC M'D ENTRIES:			
23. CYCLONIC (10-20 DEG) - AVG COS(YAW):			
26. CYC. (>20) - AVG(SDR D.P X COS(YAW)):			
24. PROCESS WT SOURCE - T/HR:			
22. LB/TON REGULATED - T/HR:			
27. LB/* REGULATED (* AS DEFINED) - */HR:			
23. LAM&CYC(200) VAL(SAMPLE PTS/TOT PTS):			

AP

UNITED STATES SUGAR CORPORATION

Post Office Drawer 1207 Clewiston, Florida 33440
Telephone: (813) 983-8121 Telex: 510-952-7753

February 8, 1991

RECEIVED
FEB 13 1991

Mr. David Knowles
Florida Department of Environmental
Regulation
2269 Bay Street
Fort Myers, Fl. 33901-2896

Division of Environmental Engineering
**PALM BEACH COUNTY
HEALTH DEPARTMENT**

RE: Palm Beach County AP
USSC Bryant Blr. #1
Annual Compliance Test

Dear Mr. Knowles:

We are enclosing copy of annual Compliance Stack Test report on Boiler No. 1 at our Bryant mill.

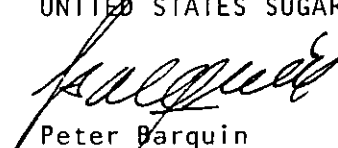
This test was performed by Air Consulting & Engineering, Inc. on January 8, 1991.

Also enclosed is a certification of calibration of steam recorders by our Mr. Fernando Llorens, Supervisor of our Process Controls and Instrumentation.

By copy of this letter we are also forwarding one copy of this test to Palm Beach County Health Department.

Sincerely,

UNITED STATES SUGAR CORPORATION



Peter Barquin
Administrative Assistant
to Senior Vice President
Sugar Houses

*Francis Capobianco
Bouynton Lake No.*

58 Parford

Dept. -ESE

UNITED STATES SUGAR CORPORATION

Post Office Drawer 1207 Clewiston, Florida 33440
Telephone: (813) 983-8121 Telex: 510-952-7753

February 8, 1991

TO WHOM IT MAY CONCERN:

This is to certify that the steam flow recorder of Boiler No. 1
at the Bryant Sugar House was recently calibrated under my supervision
and found to be within specifications.

Sincerely,

UNITED STATES SUGAR CORPORATION

A handwritten signature in dark ink, appearing to read "Fernando Z. Llorens". The signature is fluid and cursive, with the first and last names being more prominent.

Fernando Z. Llorens
Supervisor, Process Controls
and Instrumentation

DATE 03/22/91 FLORIDA DEPARTMENT OF ENVIRONMENTAL REGULATION
 PARTICULATE STACK TEST VERIFICATION
 DER METHOD 5

FACILITY NAME: ATLANTIC SUGAR

APIS #

COMPANY CONDUCTING TEST: ACE

TEST DATE 11 29 90

SOURCE DESCRIPTION: BOILER 4

STACK TEST DATA SUMMATION

		RUN1	RUN2	RUN3
1.H2O	(VOL.MEAS.),ML	292.8	328.4	316.4
2.H2O	(MASS MEAS.),GM	0	0	0
3.M'N	PARTICULATE WEIGHT, GM	.1918	.2092	.2145
4.V'M	VOLUME METERED,CF	39.492	42.375	41.127
5.Y	DRY GAS MTR. CALIB.FCTR.	.994	.994	.994
6.RDP	AVG SQR D.P-SAMPLING	.989	1.023	.997
7.DH	AVG DELTA H,IN.H2O	1.716	1.99	1.887
8.T'M	AVG MTR. TEMP,DEG.F	74.9	80.5	83.6
9.T'S	AVG STACK TEMP,DEG.F	173	176.3	178.9
10.P'S	STACK PRESS,' 'HG(ABS)	30.4	30.4	30.4
11.P'B	BAROMETRIC PRESS,' 'HG	30.4	30.4	30.4
13.D'N	ACTUAL NOZZLE DIAM,IN	.23	.23	.23
14.T	ACTUAL SAMPLE TIME,MIN	60	60	60
15.C'P	PITOT TUBE COEFFICIENT	.84	.84	.84
23.S/T	VALUE:SAMPLE PTS/TOT PTS	1	1	1

RUN	VOLUME SAMPLED DSCF	MOISTURE CONTENT PERCENT	STACK VEL FPS	FLOW RATE DSCF/H	PERCENT ISO- KINETIC	ACTUAL EMISS LB/HR	ACTUAL EMISS LB/MBTU	ALLOW EMISS LB/MBTU
1	39.52	25.86	62.49	3,939,857	96.96	42.15	0.191	0.290
2	41.99	26.91	64.96	4,016,602	101.06	44.11	0.200	0.290
3	40.51	26.88	63.43	3,907,744	100.22	45.61	0.206	0.290
MEAN	40.67	26.55	63.63	3,954,734	99.41	43.96	0.199	0.290

SUMMARY

GENERAL:

REVIEWED BY AS
ACTUAL A 'S = 27.883 SQ FT
LAMINAR FLOW ASSUMED (<10 DEG YAW) (OR <20 DER)
ACTUAL EMISS BASED ON HEAT INPUT = 221 MBTU/HR
ALL REQUIRED LEAK TESTS ACCEPTABLE
ASSUMED M 'D=30.0 (COMBUSTION GASES)

COMMENT.....

RUN 1 :

ACTUAL A 'N = .0002885 SQ FT

COMMENT.....

RUN 2 :

ACTUAL A 'N = .0002885 SQ FT

COMMENT.....

RUN 3 :

ACTUAL A 'N = .0002885 SQ FT

COMMENT.....

Stack area
27.883

ACE
11-29-90

INPUT SHEET - REV:09/10/83 - PAGE 2 OF 2

ENTER THE FOLLOWING:

	RUN1	RUN2	RUN3
1. H2O COLLECTED (ONLY VOL. MEASURED), ML:	292.80	328.40	316.40
2. H2O COLLECTED (WEIGHED PART ONLY), GM:	—	—	—
3. M'N PARTICULATE WEIGHT, GM:	1918	2092	2145
4. V'M VOLUME METERED, CF:	39.492	42.375	41.127
5. Y DRY GAS METER CAL FACTOR:	994	994	994
6. RDP AVG SDR DELTA P (WHEN SAMPLING):	989	1023	997
7. DH AVG DELTA H, IN H2O:	1.712	1.99	1.887
8. T'M AVG METER TEMP, DEG F:	74.9	80.5	83.6
9. T'S AVG STACK TEMP, DEG F:	173	176.3	178.9
10. P'S* STACK PRESS, *IN(.....):	30.40	30.40	30.40
11. P'B BAROMETRIC PRESS, IN HG:	30.40	30.40	30.40
12. D'N ACTUAL NOZZLE DIAMETER, IN.:	230	230	230
14. T ACTUAL SAMPLE TIME, MIN:	60	60	60
15. C'P PITOT TUBE COEFFICIENT:	84	84	84
OPTION ENTRIES:	MBTU 212.05	225.24	227.88
17. ORSAT/FYRITE - %CO2:			
18. ORSAT/FYRITE - %O2:			
20. ORSAT/FYRITE (FOR C'S @ 50% E.A.)-%CO:			
19. SPECIFIC M'D ENTRIES:			
23. CYCLONIC (10-20 DEG) - AVG COS(YAW):			
26. CYC.(>20) - AVG(SDR D.P X COS(YAW)):			
24. PROCESS WT SOURCE - T/HR:			
22. LB/TON REGULATED - T/HR:			
27. LB/* REGULATED (* AS DEFINED) - */HR:			
29. LAM&CYCC(20) - VAL(SAMPLE PTS/TOT PTS):			