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AP-42 Section Number: 1.8

Reference Number: 36

Title: Source Test Report for Particulate
Emissions Impingement Wet Scrubber
Boiler Number 5

March 1992

65W1-115509

**SOURCE TEST REPORT
for
PARTICULATE EMISSIONS**

**IMPINGEMENT WET SCRUBBER
BOILER NUMBER 5
BRYANT, FLORIDA**

MARCH 5, 1992

Prepared for:

**U.S. SUGAR CORPORATION
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REPORT CERTIFICATION

To the best of my knowledge, all applicable field and analytical procedures comply with Florida Department of Environmental Regulation requirements and all test data and plant operating data are true and correct.

Dagmar Neck
Dagmar Neck

3/30/1992
Date

1.0 INTRODUCTION

On March 5, 1992, Air Consulting and Engineering, Inc. (ACE), conducted particulate testing on the Wet Scrubber Outlet of Boiler 5 at Bryant Sugar Mill, located in Bryant, Florida.

Testing was performed to demonstrate compliance with the current Florida Department of Environmental Regulation (FDER) operating permit.

United States Environmental Protection Agency (EPA) Method 5 (particulate) was utilized for the emission testing.

Mr. Sterling Jordan of the FDER observed a portion of the testing.

Mr. Peter Barquin of U.S. Sugar Corporation (U.S. Sugar) served as project director and Mr. Augusto Blanchard coordinated testing and provided the scrubber data.

2.0 SUMMARY AND DISCUSSION OF RESULTS

Boiler Number 5 demonstrated compliance with the permit conditions.

Table 1 is a summary of the emission results.

Particulate emissions averaged 58.70 pounds per hour (lbs/Hr) and 0.109 pounds per million BTU (lbs/MMBTU) which is within the allowable emissions of 80.86 lbs/Hr and 0.15 lbs/MMBTU.

According to permit conditions the maximum allowable emission rate is 87.5 lbs/Hr.

No oil was used during compliance testing.

Complete emission summaries, field data sheets and laboratory data are presented in Appendices A, B, and C, respectively.

Production rate summaries are provided in Appendix D. This data was obtained from control room recordings of steam flow, temperature, and pressure as well as feed water temperature and pressure. Steam integrator readings were recorded at the beginning and end of each particulate run.

Table 1 Emission Summary
 Boiler Number 5
 U.S. Sugar Corporation - Bryant Mill
 Bryant, Florida
 March 5, 1992

Run Number	Time	<u>Particulate Emission</u>		<u>Allowable Particulate Emission</u>	
		lbs/Hr	lbs/MMBTU	lbs/Hr	lbs/MMBTU
1	0806-0908	60.76	0.114	80.12	0.15
2	0949-1051	58.05	0.109	80.18	0.15
3	1221-1323	58.70 57.30	0.109 0.104	80.86	0.15
AVERAGE	---	58.70	0.109 0.104	80.86	0.15

$$\text{lbs/MMBTU} = \frac{\text{lbs/Hr}}{\text{Fuel Heat Input (MMBTU/Hr)}}$$

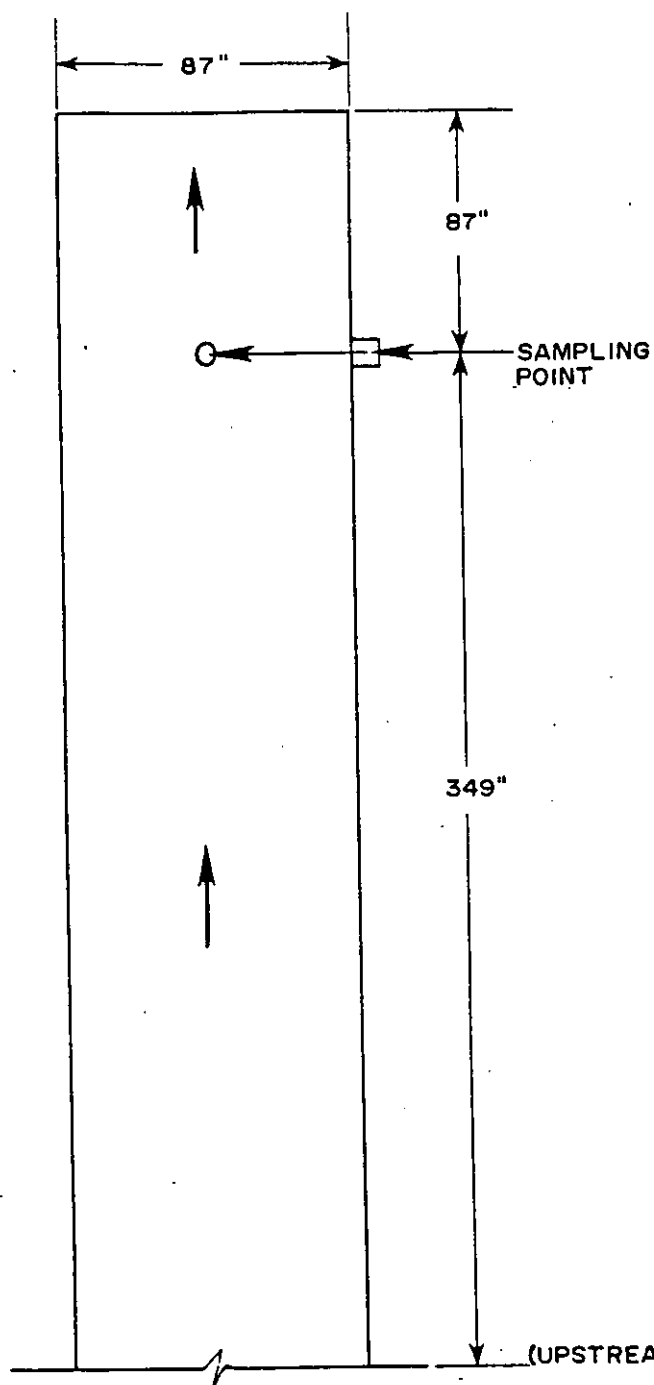
3.0 PROCESS DESCRIPTION AND OPERATION

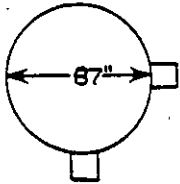
The Number 5 Boiler at U.S. Sugar's Bryant plant is a vibrating grate stoker design used primarily for bagasse fuel firing. Supplemental oil firing was not used during the emission test series. The boiler averaged 242,174 pounds per hour steam production over the three run test period.

Steam integrators and other production monitoring devices were rigorously calibrated prior to the production season.

4.0 SAMPLING POINT LOCATION

Figure 1 is a schematic of the exhaust stack with sampling point locations.



	
TRAVERSE POINT NUMBER	INCHES INSIDE STACK WALL
1	1.9
2	5.8
3	10.3
4	15.4
5	21.8
6	30.9
7	56.1
8	65.3
9	71.6
10	76.7
11	81.2
12	85.1

NOT TO SCALE

FIGURE 1.
SAMPLING POINT LOCATION
BRYANT-BOILER NO. 5
U.S. SUGAR CORPORATION
PAHOKEE, FLORIDA

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5.0 FIELD AND ANALYTICAL PROCEDURES

5.1 *Particulate Matter Sampling and Analysis--EPA Method 5 (Glass Probe)*

Particulate matter samples were collected by the particulate matter emission measurement method specified by the United States Environmental Protection Agency. A schematic diagram of the sampling train used is shown in Figure 2. All particulate matter captured from the nozzle to, and including, the filter was included in the calculation of the emission rate of particulate matter.

PREPARATION OF EQUIPMENT

1. **FILTERS** - Gelman type "A" filters were placed in a drying oven for two hours at 105 degrees C, removed and placed in a standard desiccator containing indicating silica gel, allowed to cool for two hours, and weighed to the nearest 0.1 mg. The filters were then re-desiccated for a minimum of six hours and weighed to a constant weight (less than 0.5 mg change from previous weighing). The average of the two constant weights was used as the tare weight.
2. **NOZZLE, FILTER HOLDER, AND SAMPLING PROBE** - The nozzle, filter holder, and sampling probe were washed vigorously with soapy water and brushes, rinsed with distilled water and acetone, and dried prior to the test program. All openings on the sampling equipment were sealed while in transit to the test site.
3. **IMPINGERS** - The Greenburg-Smith impingers were cleaned with a warm soapy water solution and brushes, rinsed with distilled water and acetone, and dried. The impingers were sealed tightly during transit.

TEST PROCEDURE

Prior to performing the actual particulate matter sample runs, certain stack and stack gas parameters were measured. These preliminary measurements

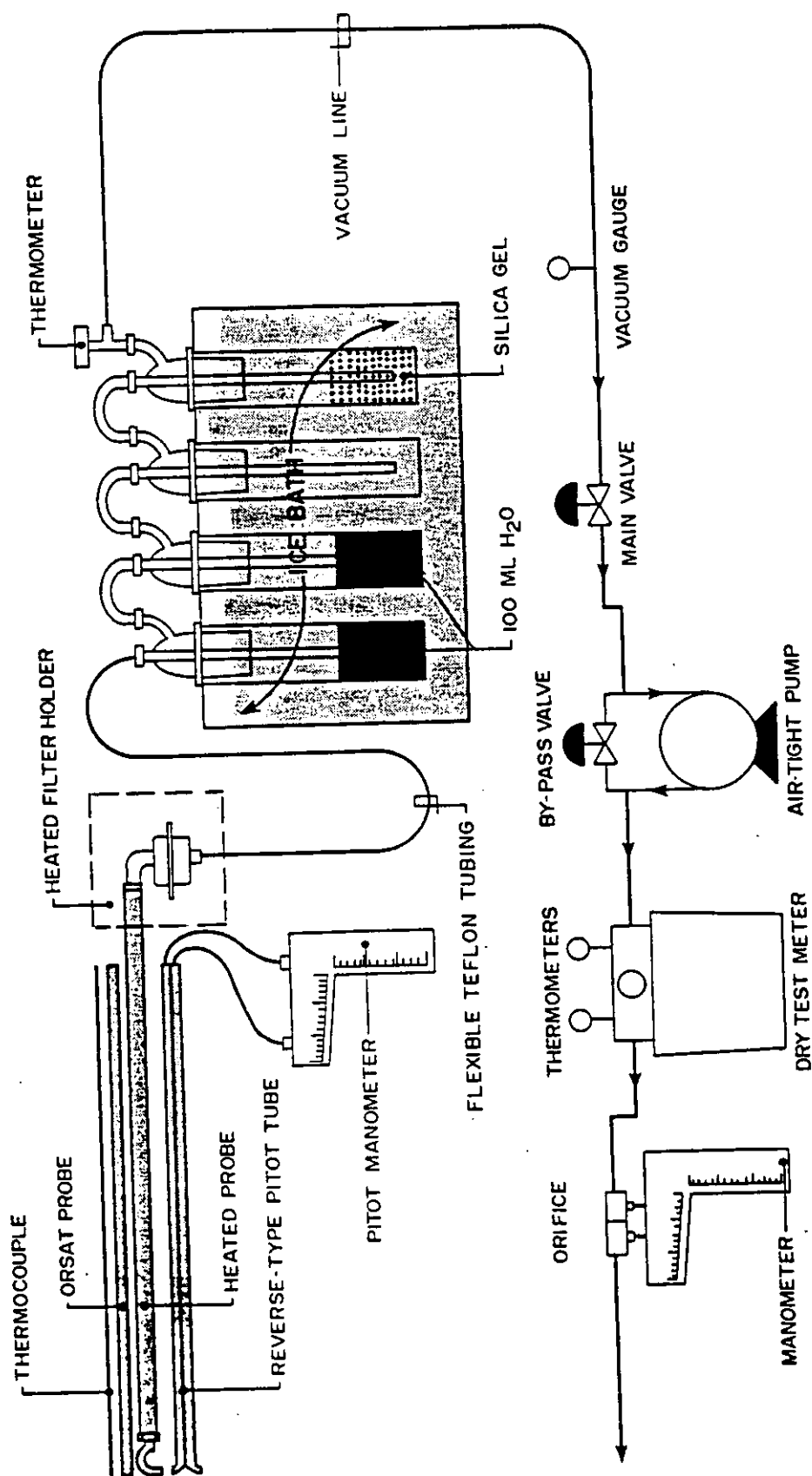


FIGURE 2
EPA METHOD 5 SAMPLING TRAIN

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included the average gas temperature, the stack gas velocity head, the stack gas moisture content, and the stack dimensions at the point where the tests were being performed. The stack gas temperature was determined by using a bi-metallic thermocouple and calibrated pyrometer. Velocity head measurements were made with calibrated type "S" pitot tube and an inclined manometer. Velocity head measurements of 0.05 inches H₂O or less were measured utilizing a micromanometer.

The sampling traverse points were selected so that a representative sample could be extracted from the gas stream. The traverse points were located in the center of equal areas, the number of which were dependent upon the distance upstream and downstream from flow disturbances.

Each particulate matter test run consisted of sampling for a specific amount of time at each traverse point. The type "S" pitot tube was connected to the sampling probe so that an instantaneous velocity head measurement could be made at each traverse point while making the test run. The stack gas temperature was also measured at each traverse point. Nomographs were used to calculate the isokinetic sampling rate at each traverse point during each test run.

The gases sampled passed through the following components: a stainless steel nozzle and glass probe; a glass fiber filter; two impingers each with 100 ml

of distilled deionized water; one impinger dry; one impinger with 200 grams of silica gel; a flexible sample line; an air-tight pump; a dry test meter; and a calibrated orifice. The second impinger had a standard tip, while the first, third, and fourth impingers had modified tips with a 0.5 inch I.D. opening.

Sample recovery was accomplished by the following procedures:

1. The pre-tared filter was removed from its holder and placed in Container 1 and sealed. (This is usually performed in the lab.)
2. All sample-exposed surfaces prior to the filter were washed with acetone and placed in Container 2, sealed and the liquid level marked.
3. The volume of water from the first three impingers was measured for the purpose of calculating the moisture in the stack gas and then discarded.
4. The used silica gel from the fourth impinger was transferred to the original tared container and sealed.

LABORATORY ANALYSIS

The three sample containers from each sample run were analyzed according to the following procedures:

1. The filter was dried at 105 degrees C for three hours, desiccated for a minimum of one hour, and weighed to the nearest 0.1 mg. A *minimum of two such weighings six hours apart was made to determine constant weight.*
2. The acetone from Container 2 was transferred to a tared beaker and evaporated to dryness at ambient temperature and pressure, desiccated for 24 hours, and weighed to the nearest 0.1 mg. A *minimum of two such weighings six hours apart were made to determine constant weight.*
3. The used silica gel in its tared container was weighed to the nearest 0.1 gram.

The total sample weight included the weight of material collected on the filter plus the weight of material collected in the nozzle, sampling probe, and front half of the filter holder.

DATA

The field data sheets, calculation sheets, and nomenclature definitions are included in the appendices of this report.

APPENDIX A
COMPLETE EMISSION DATA

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COMPLETE EMISSION DATA

PLANT: UNITED STATES SUGAR CORPORATION / BRYANT, FLORIDA
SOURCE: NUMBER 5 BOILER SCRUBBER OUTLET
DATE: 3-05-92

RUN NO.:	1	IMPINGER ml	232
BEGIN TIME:	806	SILICA GEL gms.	6.2
END TIME:	908	PERCENT O2	9.8
TOTAL RUN TIME:	60.00 min.	PERCENT CO2	10.8
BAROMETRIC PRESSURE:	29.90 "Hg	"F" FACTOR	
STACK PRESSURE:	29.90 "Hg.		
NOZZLE DIAMETER:	0.175 inches	PARTICULATE	
METER CORR. FACTOR:	1.009	-----	
FINAL METER:	65.615 cubic ft.	FILTER mg.	103.6
INITIAL METER:	31.737 cubic ft.	WASH mg.	8.6
STACK AREA:	41.283 sq. ft.		

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	DRIF. DIFF.	STACK TEMP.	METER TEMP.
1-1	1.500	1.225	0.840	161	68
1-2	2.400	1.549	1.340	160	68
1-3	2.500	1.581	1.400	160	68
1-4	2.000	1.414	1.120	162	68
1-5	2.300	1.517	1.290	162	69
1-6	2.000	1.414	1.120	162	70
1-7	2.000	1.414	1.120	162	71
1-8	1.500	1.225	0.840	162	72
1-9	1.800	1.342	1.010	163	72
1-10	1.500	1.225	0.840	163	72
1-11	1.500	1.225	0.840	166	73
1-12	1.500	1.225	0.840	163	74
2-1	1.100	1.049	0.620	157	75
2-2	1.100	1.049	0.620	160	76
2-3	1.100	1.049	0.620	160	76
2-4	1.300	1.140	0.730	161	77
2-5	1.300	1.140	0.730	162	78
2-6	1.500	1.225	0.840	162	78
2-7	3.000	1.732	1.680	162	79
2-8	3.000	1.732	1.680	162	80
2-9	3.500	1.871	1.960	163	81
2-10	3.500	1.871	1.960	163	82
2-11	2.500	1.581	1.400	163	83
2-12	3.000	1.732	1.680	162	83
AVERAGES	-----	1.397	1.130	162	75

RUN 1

NOZZLE AREA(SQ.FT.):	0.0001670		
AVG. VELOCITY HEAD	1.95 "H2O	VOL. FLOW ACFM	217733
AVG. STACK TEMP.:	162 F	VOL. FLOW SCFMD	138478
AVG. METER TEMP.:	75 F		
AVG. DRIFICE DIFFERENTIAL:---	1.13 "H2O	PARTICULATE DATA :	
METER STANDARD CUBIC FEET:---	33.825	-----	
% H2O VAPOR:	25.1	POUNDS PER HOUR:	60.759
GAS MOL. WT. DRY:	30.12	POUNDS PER SCF :	0.0000073
GAS MOL. WT. WET:	27.08	GRAINS/SCF:	0.051
% EXCESS AIR:	86.86	GRAINS/SCF @ 8% O2	0.059
AVG. STACK VEL.(FPS)-----	87.90	GRAINS/SCF @50% EA	0.064
MMBTU INPUT:	534.15	POUNDS PER MMBTU:	0.114
PERCENT ISO KINETIC :-----	100.62	LBS/MMBTU"F"FACTOR	0.000

NOZZLE AREA (FT.2)	$(D_n/12)^2 \times 3.141604$	0.000167
AVG. VELOCITY HEAD:	$(AVG. SQ. RT.)^2$	87.90
METER STND. FT3:	$(M_f - M_i) \times MCF \times (AVG. DRF. DIFF. / 13.6) / 29.92 \times (528 / (T_m + 460))$	33.825
PERCENT H2O:	$((IMP + SG) \times (((IMP + SG) \times .0474) + SCF) \times 100$	
Mw DRY:	$((O_2\% \times .32) + CO_2\% \times .44) + (100 - (O_2\% + CO_2\%) \times .28$	30.12
Mw WET:	$(Mw DRY \times (1 - \%H_2O / 100)) + \%H_2O \times 0.18$	27.08
% EXCESS AIR:	$\%O_2 / (((100 - (\%O_2 + \%CO_2)) \times .264) - \%O_2) \times 100$	86.86
STACK VEL. (FPS):	$85.49 \times .84 \times (AVG. SQ. RT. VEL. HD.) \times ((T_s + 460) / (P_s \times MwWET))^{.5}$	87.90
% ISOKINETIC:	$((T_s + 460) \times SCF \times 2992) / (528 \times FPS \times TIME \times A_n \times P_s \times 60 \times (1 - \%O_2 / 100)$	100.62
VOL. FLOW (ACFM):	$FPS \times 60 \times A_s$	217733
STND. FLOW (SCFMD):	$ACFM \times 528 / (T_s + 460) \times (1 - \%H_2O / 100) \times (P_s / 29.92)$	138478
PARTICULATE LB/HR:	$PROBE + FILTER \text{ mg.} / 453600 \times (SCFMD / SCF) \times 60$	60.759
PARTICULATE LB/SCF:	$PROBE + FILTER \text{ mg.} / 453600 / SCF$	0.0000073
GRAINS/SCF:	$LB/SCF \times 7000$	0.0512
GR/SCF @ 8% O2:	$(12.9 / (20.9 - \%O_2)) \times GR/SCF$	0.0592
GR/SCF @ 50% E.A.:	$GR/SCF \times ((100 + \%E.A.) / 150)$	0.0638
LB/MMBTU:	$(LB/HR) / (LB/MMBTUH)$	0.114
LB/MMBTU "F" FACTOR:	$LB/SCF \times "F" \text{ FACTOR} \times (20.9 / 20.9 - \%O_2)$	0.000

AIR CONSULTING AND ENGINEERING
COMPLETE EMISSION DATA

PLANT: UNITED STATES SUGAR CORPORATION / BRYANT, FLORIDA
SOURCE: NUMBER 5 BOILER SCRUBBER OUTLET
DATE: 3-05-92

RUN NO.: 2	IMPINGER ml	230
BEGIN TIME: 949	SILICA GEL gms.	11.0
END TIME: 1051	PERCENT O2	10.2
TOTAL RUN TIME: 60.00 min.	PERCENT CO2	10.3
BAROMETRIC PRESSURE: 29.90 "Hg	"F" FACTOR	
STACK PRESSURE: 29.90 "Hg.		
NOZZLE DIAMETER: 0.175 inches	PARTICULATE	
METER CORR. FACTOR: 1.009	-----	
FINAL METER: 100.953 cubic ft.	FILTER mg.	94.9
INITIAL METER: 65.922 cubic ft.	WASH mg.	10.9
STACK AREA: 41.283 sq. ft.		

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIF. DIFF.	STACK TEMP.	METER TEMP.
-----	-----	-----	-----	-----	-----
1-1	3.500	1.871	1.960	162	83
1-2	3.500	1.871	1.960	162	83
1-3	3.500	1.871	1.960	163	84
1-4	3.000	1.732	1.680	162	84
1-5	2.800	1.673	1.570	162	84
1-6	2.000	1.414	1.120	162	86
1-7	1.100	1.049	0.620	161	87
1-8	1.100	1.049	0.620	161	87
1-9	1.300	1.140	0.730	161	87
1-10	1.100	1.049	0.620	162	87
1-11	1.000	1.000	0.560	161	88
1-12	0.920	0.959	0.520	160	88
2-1	1.300	1.140	0.730	154	89
2-2	1.300	1.140	0.730	159	89
2-3	1.300	1.140	0.730	160	90
2-4	1.300	1.140	0.730	161	91
2-5	1.500	1.225	0.840	161	91
2-6	1.500	1.225	0.840	160	91
2-7	2.500	1.581	1.400	160	92
2-8	3.000	1.732	1.680	162	92
2-9	3.500	1.871	1.960	162	93
2-10	3.500	1.871	1.960	161	94
2-11	3.000	1.732	1.680	161	94
2-12	3.000	1.732	1.680	162	95
AVERAGES	-----	1.425	1.203	161	89

RUN 2

NOZZLE AREA(SQ.FT.): 0.0001670			
AVG. VELOCITY HEAD :-----	2.03 "H2O	VOL. FLOW ACFM :	222231
AVG. STACK TEMP.: -----	161 F	VOL. FLOW SCFMD :	141400
AVG. METER TEMP.: -----	89 F		
AVG. ORIFICE DIFFERENTIAL: ---	1.20 "H2O	PARTICULATE DATA :	
METER STANDARD CUBIC FEET: ---	34.090	-----	
% H2O VAPOR: ;-----	25.1	POUNDS PER HOUR:	58.047
GAS MOL. WT. DRY: -----	30.06	POUNDS PER SCF :	0.0000068
GAS MOL. WT. WET: -----	27.03	GRAINS/SCF:	0.048
% EXCESS AIR: -----	94.55	GRAINS/SCF @ 8% O2	0.058
AVG. STACK VEL.(FPS)-----	89.72	GRAINS/SCF @50% EA	0.062
MMBTU INPUT: -----	534.50	POUNDS PER MMBTU:	0.109
PERCENT ISO KINETIC :-----	99.31	LBS/MMBTU "F" FACTOR	0.000

NOZZLE AREA (FT. ²)	$(D_n/12)^2 \times 3.1416/4$	0.000167
AVG. VELOCITY HEAD:	$(AVG. SQ. RT.)^2/2$	89.72
METER STND. FT ³ :	$(M_f - M_i) \times MCF \times (AVG. ORF. DIFF. / 13.6) / 29.92 \times (528 / (T_m + 460))$	34.090
PERCENT H ₂ O:	$((IMP + SG) \times (((IMP + SG) \times 0.0474) + SCF) \times 100$	
Mw DRY:	$((O_2\% \times 32) + CO_2\% \times 44) + (100 - (O_2\% + CO_2\%) \times 28$	30.06
Mw WET:	$(Mw DRY \times (1 - \%H_2O/100)) + \%H_2O \times 0.18$	27.03
% EXCESS AIR:	$\%O_2 / (((100 - (\%O_2 + \%CO_2)) \times 0.264) - \%O_2) \times 100$	94.55
STACK VEL. (FPS):	$85.49 \times 0.84 \times (AVG. SQ. RT. VEL. HD.) \times ((T_s + 460) / (P_s \times MwWET)))^{1.5}$	89.72
% ISOKINETIC:	$((T_s + 460) \times SCF \times 2992) / (528 \times FPS \times TIME \times A_n \times P_s \times 60 \times (1 - \%O_2/100))$	99.31
VOL. FLOW (ACFM):	$FPS \times 60 \times A_s$	222231
STND. FLOW (SCFMD):	$ACFM \times 528 / (T_s + 460) \times (1 - \%H_2O/100) \times (P_s / 29.92)$	141400
PARTICULATE LB/HR:	$PROBE + FILTER \text{ mg.} / 453600 \times (SCFMD / SCF) \times 60$	58.047
PARTICULATE LB/SCF:	$PROBE + FILTER \text{ mg.} / 453600 / SCF$	0.0000068
GRAINS/SCF:	$LB/SCF \times 7000$	0.0479
GR/SCF @ 8% O ₂ :	$(12.9 / (20.9 - \%O_2)) \times GR/SCF$	0.0577
GR/SCF @ 50% E.A.:	$GR/SCF \times ((100 + \%E.A.) / 150)$	0.0621
LB/MMBTU:	$(LB/HR) / (LB/MMBTUH)$	0.109
LB/MMBTU "F" FACTOR:	$LB/SCF \times "F" \text{ FACTOR} \times (20.9 / 20.9 - \%O_2)$	0.000

COMPLETE EMISSION DATA

PLANT: UNITED STATES SUGAR CORPORATION / BRYANT, FLORIDA
 SOURCE: NUMBER 5 BOILER SCRUBBER OUTLET
 DATE: 3-05-92

RUN NO.:	3	IMPINGER ml	235
BEGIN TIME:	1221	SILICA GEL gms.	6.1
END TIME:	1323	PERCENT O2	10.0 <i>Avg</i>
TOTAL RUN TIME:	60.00 min.	PERCENT CO2	10.6 : 10.0
BAROMETRIC PRESSURE:	29.90 "Hg	"F" FACTOR	
STACK PRESSURE:	29.90 "Hg		
NOZZLE DIAMETER:	0.175 inches	PARTICULATE	
METER CORR. FACTOR:	1.009	-----	
FINAL METER:	136.604 cubic ft.	FILTER mg.	96.9
INITIAL METER:	101.335 cubic ft.	WASH mg.	8.1
STACK AREA:	41.283 sq. ft.		

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIF. DIFF.	STACK TEMP.	METER TEMP.
1-1	3.800	1.949	2.130	159	91
1-2	3.000	1.732	1.680	161	91
1-3	3.500	1.871	1.960	162	91
1-4	3.000	1.732	1.680	162	91
1-5	2.300	1.517	1.290	162	91
1-6	2.000	1.414	1.120	162	91
1-7	1.300	1.140	0.730	162	92
1-8	1.100	1.049	0.620	162	92
1-9	1.300	1.140	0.730	162	92
1-10	1.100	1.049	0.620	162	92
1-11	1.100	1.049	0.620	162	92
1-12	0.900	0.949	0.500	162	93
2-1	1.100	1.049	0.620	157	94
2-2	1.200	1.095	0.670	160	94
2-3	1.200	1.095	0.670	162	94
2-4	1.100	1.049	0.620	162	94
2-5	1.300	1.140	0.730	162	95
2-6	1.300	1.140	0.730	162	95
2-7	2.500	1.581	1.400	163	96
2-8	3.500	1.871	1.960	163	97
2-9	3.500	1.871	1.960	163	97
2-10	3.500	1.871	1.960	163	98
2-11	3.700	1.924	2.070	162	98
2-12	3.000	1.732	1.680	163	98
AVERAGES	-----	1.417	1.198	162	94

RUN 3

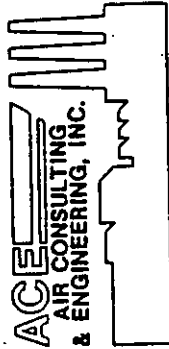
NOZZLE AREA(SQ.FT.):	0.0001670		
AVG. VELOCITY HEAD	2.01 "H2O	VOL. FLOW ACFM	220993
AVG. STACK TEMP.:	162 F <i>Avg = 162</i>	VOL. FLOW SCFMD	140327
AVG. METER TEMP.:	94 F	PARTICULATE DATA	<i>Avg = 140,068</i>
AVG. ORIFICE DIFFERENTIAL:	1.20 "H2O	-----	
METER STANDARD CUBIC FEET:	34.011		
% H2O VAPOR:	25.2	POUNDS PER HOUR:	57.304
GAS MOL. WT. DRY:	30.10	POUNDS PER SCF :	0.0000068
GAS MOL. WT. WET:	27.05	GRAINS/SCF:	0.048
% EXCESS AIR:	91.23	GRAINS/SCF @ 8% O2	0.056
AVG. STACK VEL.(FPS)	89.22	GRAINS/SCF @50% EA	0.061
MMBTU INPUT:	548.44	POUNDS PER MMBTU:	0.104
PERCENT ISOKINETIC	99.84	LBS/MMBTU "F" FACTOR	0.000

NOZZLE AREA (FT. ²)	$(D_n/12)!2 \times 3.141604$	0.000167
AVG. VELOCITY HEAD:	$(AVG. SQ. RT.)!2$	89.22
METER STND. FT3:	$(M_f - M_i) \times MCF \times (AVG. ORF. DIFF. /$ $13.6)) / 29.92) \times (528 / (T_m + 460))$	34.011
PERCENT H2O:	$((IMP + SG) \times (((IMP + SG) \times .0474) +$ $SCF) \times 100$	
Mw DRY:	$((O_2\% \times .32) + CO_2\% \times .44) + (100 - (O_2\% + CO_2$ $) \times .28$	30.10
Mw WET:	$(Mw DRY \times (1 - \%H_2O / 100)) + \%H_2O \times 0.18$	27.05
% EXCESS AIR:	$\%O_2 / (((100 - (\%O_2 + \%CO_2)) \times .264) - \%O_2) \times$ 100	91.23
STACK VEL. (FPS):	$85.49 \times .84 \times (AVG. SQ. RT. VEL. HD.) \times ((T_s$ $+ 460) / (P_s \times MwWET))!1.5$	89.22
% ISOKINETIC:	$((T_s + 460) \times SCF \times 2992) / (528 \times FPS \times TIME \times$ $A_n \times P_s \times 60 \times (1 - \%O_2 / 100)$	99.84
VOL. FLOW (ACFM):	$FPS \times 60 \times A_s$	220993
STND. FLOW (SCFMD):	$ACFM \times 528 / (T_s + 460) \times (1 - \%H_2O / 100) \times$ $(P_s / 29.92)$	140327
PARTICULATE LB/HR:	$PROBE + FILTER \text{ mg. } / 453600 \times (SCFMD /$ $SCF) \times 60$	57.304
PARTICULATE LB/SCF):	$PROBE + FILTER \text{ mg. } / 453600 / SCF$	0.0000068
GRAINS/SCF:	$LB/SCF \times 7000$	0.0476
GR/SCF @ 8% O2:	$(12.9 / (20.9 - \%O_2)) \times GR/SCF$	0.0564
GR/SCF @ 50% E.A.:	$GR/SCF \times ((100 + \%E.A.) / 150)$	0.0607
LB/MMBTU:	$(LB/HR) / (LB/MMBTUH)$	0.104
LB/MMBTU "F" FACTOR:	$LB/SCF \times "F" \text{ FACTOR} \times (20.9$ $/ 20.9 - \%O_2)$	0.000

APPENDIX B
FIELD DATA SHEETS

STACK SAMPLING FIELD DATA SHEET

PLANT USSC - Bryant
 SOURCE Boiler #5
 PLANT LOCATION Bryant
 TYPE OF SAMPLING TRAIN EPA-5
 TYPE OF SAMPLES P.M.
 DATE 03-05-93 RUN NO. 1
 TIME START 0806 TIME END 0908
 SAMPLE TIME 2.5 / 2.4 (min/pt) = 60 Total min
 ASSUMED MOISTURE 26 % FDA .74
 NOMOGRAPH C₁ .56 PITOT CORR. .84
 P_b 29.90 "Hg P_s 29.90 "Hg
 WEATHER ptly cldy TEMP 76 °F
 METER BOX NO. 6 H 1.91 Y
 NOZZLE CAL. .175 .175 .175 .175
 STACK DIMENSIONS 87"
 STACK AREA 41.283 ft² EFFECTIVE 41.283 ft²
 STACK HEIGHT ft
 STACK DIAMETER: UPSTRM. DNSTRM.
 PORT SIZE in. NIPPLE LENGTH in.
 U CORD LENGTH 200
 REMARKS: Observers: Sterling Jordan -
DER J Pt. Myers
David Brown -
HR5 / P. Brook County
Raisa Nepinsky -
HR5 / P. Brook County



2106 N.W. 67th PLACE, SUITES 9 & 10
 GAINESVILLE, FLORIDA 32606

TEST ID US05C1AS
 PAGE 1 OF 2

MAT'L PROCESSING RATE
 GAS METER READINGS: FINAL 065.615 ft³
 INITIAL 031.437 ft³
 NET 33.878 ft³
 FILTER NO. 1072 IMP. VOL. GAIN 232 ml.
 SIL GEL NO. 28 WT. GAIN 6.2 ml.
 TOTAL CONDENSATE 238.2 ml.

ORSAT

	1	2	3	4	AVG.
% CO ₂					10.8
% O ₂					9.7
% CO					
% N ₂					

F₀ = FO RANGE

ORSAT ANALYZER

LEAK CHECKS

PRE 0.00 cfm 15 "Hg POST 0.008 cfm 20 "Hg
 METER BOX/PUMP OK GAS SAMPLE SYST. OK
 ORSAT BAG OK
 PITOT TUBE NO. 90 PRE-TEST OK
 POST-TEST (+) 0.0006 / 15 H₂O/Sec
 POST-TEST (-) 0.0006 / 15 H₂O/Sec
 PYROMETER NO. ATK 3
 BOX OPERATOR Southwest PROBE HOLDER McDonald

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (FT. ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O") CALC. ACTUAL	STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LABY IMPINGER TEMP	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
1-1			033.24	1.50	.84 .84	161	256	49	68	4.0
2		0811	034.57	2.40	1.34 1.34	160	255	48	68	7.0
3			036.12	2.50	1.40 1.40	160	255	47	68	7.0
4		0816	037.61	2.00	1.12 1.12	162	254	47	68	6.0
5			039.13	2.30	1.29 1.29	162	265	48	69	7.0
6			040.42	2.00	1.12 1.12	162	265	49	70	7.0

STACK SAMPLING FIELD DATA SHEET

PLANT USSC - Bryant
 SOURCE Boiler #5
 PLANT LOCATION Bryant, Florida
 TYPE OF SAMPLING TRAIN EPA - S
 TYPE OF SAMPLES P.M
 DATE 03-05-92 RUN NO. 2
 TIME START 0949 TIME END 1051
 SAMPLE TIME 2.5 / 24 (min/pi) = 60 Total min
 ASSUMED MOISTURE 26 % FDA 74
 NOMOGRAPH C₁ 56 PITOT CORR. .84
 P_b 29.90 "Hg P_s 29.96 "Hg
 WEATHER MTLY CLDY TEMP 80 °F
 METER BOX NO. 6 H 1.91 Y 1.009
 NOZZLE CAL. .175 .175 .175
 STACK DIMENSIONS 87"
 STACK AREA 41.283 ft² EFFECTIVE 41.283 ft²
 STACK HEIGHT ft
 STACK DIAMETER: UPSTRM. DNSTRM.
 PORT SIZE in. NIPPLE LENGTH in.
 U CORD LENGTH in.
 REMARKS: sterling Jordan DER #1 Myers

DAVID BROWN > MRS. PHILMEDI CO
RAISA NEGINSKY



2106 N. W. 87th PLACE - SUITES 9 & 10
 GAINESVILLE, FLORIDA 32606

Permit Limit
 MAX 87.5 #/hr
 particulate
 on Boiler #5
 show this figure in the
 report

TEST ID US 85022AC
 PAGE 1 OF 3

MAT'L PROCESSING RATE
 GAS METER READINGS: FINAL 100.953 #3
 INITIAL 065.932 #3
 NET 35.031 #3
 FILTER NO. 1071 IMP. VOL. GAIN 230 ml.
 SIL GEL NO. 15 WT. GAIN 11.0 ml.
 TOTAL CONDENSATE 241 ml.

ORSAT

	1	2	3	4	AVG.
% CO ₂					10.25
% O ₂					10.25
% CO					
% N ₂					

F₀ = FO RANGE

ORSAT ANALYZER

LEAK CHECKS

PRE 0.005 cfm 15 "Hg POST 0.00 cfm 19 "Hg
 METER BOX/PUMP OK GAS SAMPLE SYST. OK
 ORSAT BAG OK
 PITOT TUBE NO. 90 PRE-TEST OK
 POST-TEST (+) 0.00 cfm 15 H₂O/sec
 POST-TEST (-) 0.00 cfm 15 H₂O/sec
 PYROMETER NO. ATK 3
 BOX OPERATOR Seath PROBE HOLDER McFarland

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O")		STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
			CALC.	ACTUAL					
1-1		3.50	1.96	1.96	162	227	48	83	10.0
2		3.50	1.96	1.96	162	228	48	83	10.0
3		3.50	1.96	1.96	163	230	48	84	10.0
4		3.00	1.68	1.68	162	241	51	84	10.0
5		3.20	1.57	1.57	162	240	51	84	9.0
6		3.00	1.12	1.12	162	251	52	86	7.0

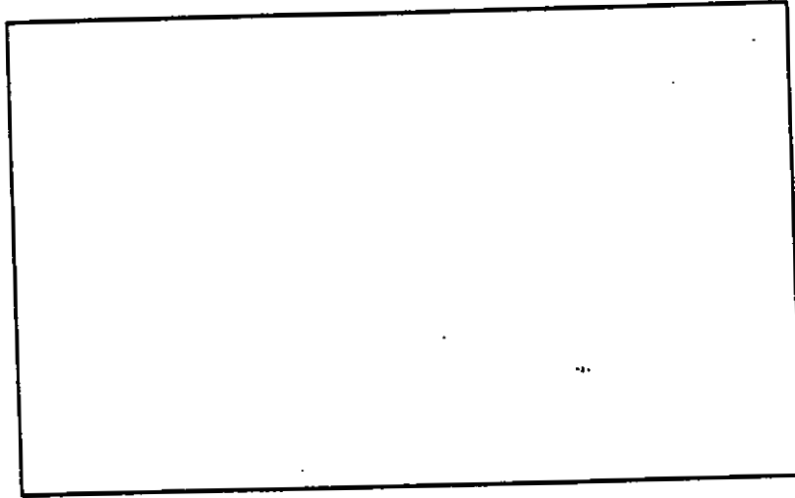
[illegible]

STACK SAMPLING FIELD DATA SHEET

PLANT USSC - Bryant
 SOURCE Boiler #5
 PLANT LOCATION Bryant
 TYPE OF SAMPLING TRAIN EPA-5
 TYPE OF SAMPLES AM
 DATE 03-05-92 RUN NO. 3
 TIME START 1221 TIME END 1323
 SAMPLE TIME 2.5 / 24 (min/pt) = 60 Total min
 ASSUMED MOISTURE 26 % FDA 44
 NOMOGRAPH 56 PITOT CORR. 184
 P_b 29.90 "Hg P_s 29.90 "Hg
 WEATHER Mstly cldy TEMP 85 °F
 METER BOX NO. 6 H 191 V 1.009
 NOZZLE CAL. 175 175 87
 STACK DIMENSIONS
 STACK AREA 41.283 m² EFFECTIVE 41.283 m²
 STACK HEIGHT ft
 STACK DIAMETER: UPSTRM. DNSTRM.
 PORT SIZE in NIPPLE LENGTH in
 U CORD LENGTH 200
 REMARKS:



2106 N.W. 67th PLACE - Suites 9 & 10
 GAINESVILLE, FLORIDA 32606



TEST ID USRS023AS
 PAGE 1 OF 2

MAT'L PROCESSING RATE
 GAS METER READINGS: FINAL 136604 m³
 INITIAL 101335 m³
 NET m³
 FILTER NO. 1070 IMP. VOL. GAIN 255 ml.
 SIL GEL NO. 129 WT. GAIN 6.1 ml.
 TOTAL CONDENSATE 241.1 ml.

ORSAT

	1	2	3	4	AVG.
% CO ₂					
% O ₂					
% CO					
% N ₂					

F₀ = FO RANGE =

ORSAT ANALYZER

LEAK CHECKS

PRE 0.018 cfm 20 "Hg POST 0.005 cfm 16 "Hg
 METER BOX/PUMP OK GAS SAMPLE SYST. OK
 ORSAT BAG OK
 PITOT TUBE NO. 90 PRE-TEST OK
 POST-TEST (+) 0.0006 "H₂O/sec
 POST-TEST (-) 0.0004 "H₂O/sec
 PYROMETER NO. AK3
 BOX OPERATOR Southland PROBE HOLDER McFarland

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL / COMMENTS	CLOCK TIME	GAS METER READING (FT ³)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O") CALC. ACTUAL	STACK GAS TEMP (°F)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg)
1-1			103.73	3.80	2.13 2.13	159	244	56	91	11.0
2		1326	105.11	3.00	1.68 1.68	161	238	54	91	8.0
3			107.05	3.50	1.96 1.96	162	238	56	91	10.0
4		1431	108.75	3.00	1.68 1.68	162	239	58	91	9.0
5			110.41	2.30	1.29 1.29	162	259	59	91	8.0
6		1536	111.81	2.00	1.12 1.12	162	273	58	91	7.0

[illegible]

APPENDIX C

LABORATORY ANALYSIS

AIR CONSULTING & ENGINEERING, inc.

PARTICULATE LAB DATA

SOURCE U.S. Sugar - Bryant SC

PROBE RINSE	RUN 1	RUN 2	RUN 3	BLANK
CONTAINER NUMBER	5-6	5-21	5-32	5-40A
TOTAL VOLUME (ml)	150	190	300	100
1st GROSS WEIGHT (g)	103.1438	104.3122	104.7335	110.154
2nd GROSS WEIGHT (g)	103.1438	104.3121	104.7331	110.154
AVERAGE GROSS WEIGHT (g)	103.1438	104.3121	104.7333	110.154
TARE WEIGHT (g)	103.1352	104.3012	104.725	110.154
SUB NET WEIGHT (g)	0.0086	0.009	0.0081	0.008
ACETONE BLANK (g)	-	-	-	-
TOTAL NET WEIGHT (mg)	8.6	10.9	8.1	8.0

NOTE: In no case should a blank residue >0.01 mg/g or 0.001% of the weight of acetone used be subtracted from the sample weight.

FILTER	RUN 1	RUN 2	RUN 3	BLANK
FILTER NUMBER	1072	1071	1070	1071
1st GROSS WEIGHT (g)	104.3122	104.3122	104.3122	104.3122
2nd GROSS WEIGHT (g)	104.3122	104.3122	104.3122	104.3122
AVERAGE GROSS WEIGHT (g)	104.3122	104.3122	104.3122	104.3122
TARE WEIGHT (g)	104.3122	104.3122	104.3122	104.3122
SUB NET WEIGHT (g)	0.0086	0.009	0.0081	0.008
TOTAL NET WEIGHT (mg)	8.6	10.9	8.1	8.0

DATE & TIME: 3-8-92 07:07
DATE & TIME: 3-8-92 16:11

TARE
BALANCE CHECK

SEE LAB BOOK

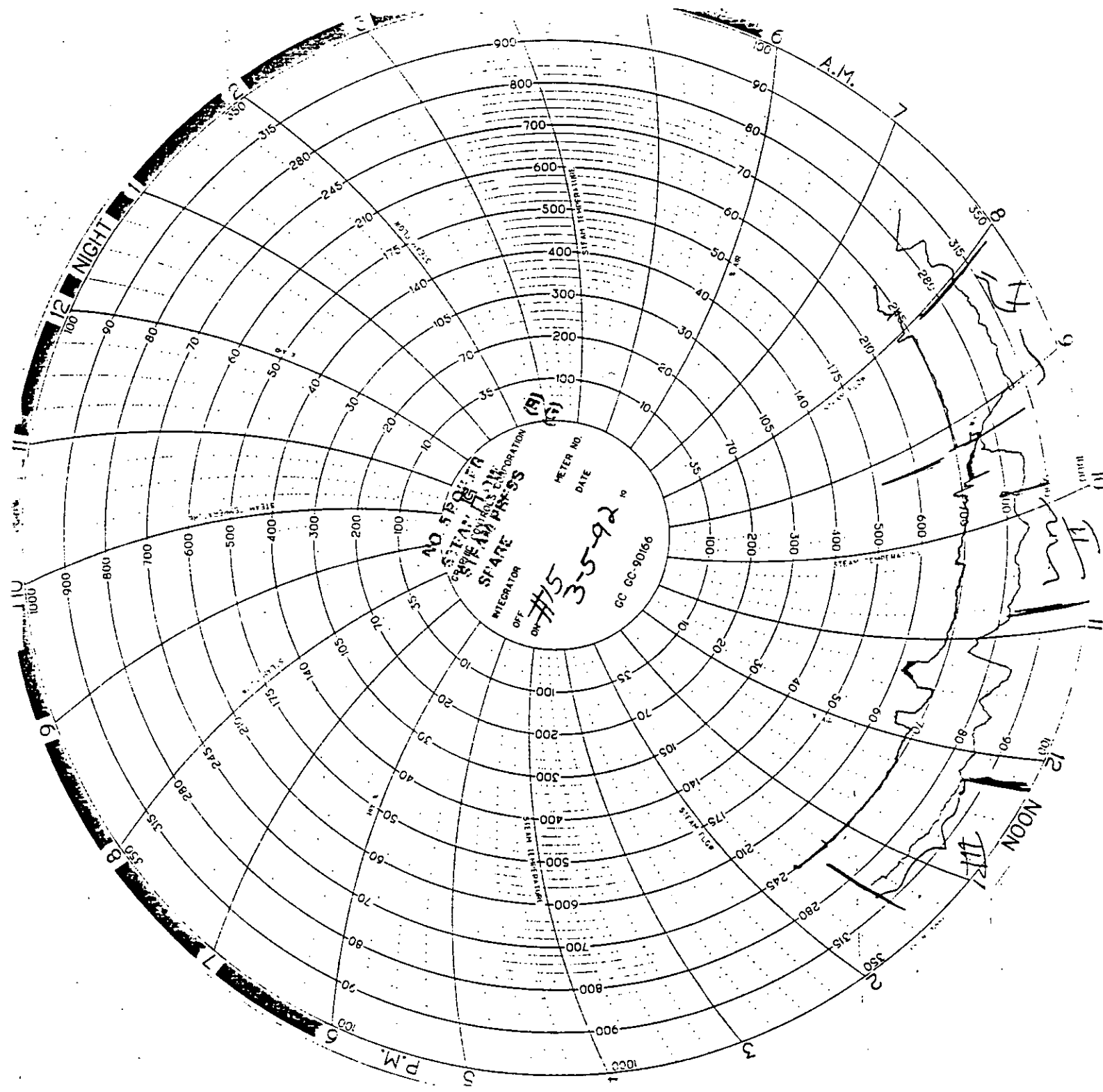
1st GROSS WEIGHT
BALANCE CHECK

0 ☒ 10.0g ☒
0.5g ☒ 100.0g ☒
%RH 69 DATE 3-8-92
Signature Christy L. Burk

2nd GROSS WEIGHT
BALANCE CHECK

0 ☒ 100g ☒
0.5g ☒ 100.0g ☒
%RH 76 DATE 3-19-92
Signature Christy L. Burk

APPENDIX D
PRODUCTION AND BOILER DATA



BRYANT BOILER No 5

DATE: 3-5-92

[illegible]

AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

PLANT: U. S. SUGAR CORPORATION DATE: 3-05-92
LOCATION: BRYANT, FLORIDA RUN NUMBER 1
SOURCE: NUMBER 5 BOILER, SCRUBBER OUTLET TIME: 0803-913

TIME INTERVAL----- 70 MINUTES

OIL:

FINAL OIL----- 0
BEGIN OIL----- 0
FACTOR----- 1

STEAM:

FINAL STEAM----- 868219
BEGIN STEAM----- 868139
FACTOR----- 3500
TEMPERATURE----- 900 DEGREES F
PRESSURE----- 856 PSIG
871 PSIA

FEEDWATER:

TEMPERATURE----- 260 DEGREES F
PRESSURE----- 1260 PSIG
1275 PSIA

HEAT INPUT:

STEAM----- 1452.7 BTU/LB
FEEDWATER----- 228.6 BTU/LB
NET STEAM----- 1224.1 BTU/LB
STEAM RATE----- 240000 LB/HR
BOILER EFFICIENCY----- 55.0 %
TOTAL FUEL HEAT INPUT----- 534.15 MMBTUH
STEAM CALIBRATION FACTOR----- 1.00

OIL----- 0.00 GPH
OIL----- 150000 BTU/GAL

TOTAL HEAT INPUT (OIL)----- 0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)----- 534.15 MMBTUH

ALLOWABLES:

ALLOWABLE EMISSION (OIL)----- 0.10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)----- 0.15 LB/MMBTU

TOTAL ALLOWABLE EMISSION----- 80.12 LB/HR
TOTAL ACTUAL EMISSION----- 60.76 LB/HR

TOTAL ALLOWABLE EMISSION----- 0.150 LB/MMBTU
TOTAL ACTUAL EMISSION----- 0.114 LB/MMBTU

•
•

BOILER NUMBER 5

OIL METER FACTOR — NO OIL —

SCRUBBER(S) PRESS DROP_____, ____

SCRUBBER(S) GPM _____, _____

SCRUBBER(S) H2O LEVEL _____, _____

PH(if applicable) _____

FINAL INTEGRATOR 868219

0803

0913

[illegible]

AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

PLANT: U. S. SUGAR CORPORATION DATE: 3-05-92
LOCATION: BRYANT, FLORIDA RUN NUMBER 2
SOURCE: NUMBER 5 BOILER, SCRUBBER OUTLET TIME: 0947-1057

TIME INTERVAL----- 70 MINUTES

OIL:

FINAL OIL----- 0
BEGIN OIL----- 0
FACTOR----- 1

STEAM:

FINAL STEAM----- 868340
BEGIN STEAM----- 868260
FACTOR----- 3500
TEMPERATURE----- 899 DEGREES F
PRESSURE----- 837 PSIG
852 PSIA

FEEDWATER:

TEMPERATURE----- 260 DEGREES F
PRESSURE----- 1260 PSIG
1275 PSIA

HEAT INPUT:

STEAM----- 1453.5 BTU/LB
FEEDWATER----- 228.6 BTU/LB
NET STEAM----- 1224.9 BTU/LB
STEAM RATE----- 240000 LB/HR
BOILER EFFICIENCY----- 55.0 %
TOTAL FUEL HEAT INPUT----- 534.50 MMBTUH
STEAM CALIBRATION FACTOR----- 1.00

OIL----- 0.00 GPH
OIL----- 150000 BTU/GAL

TOTAL HEAT INPUT (OIL)----- 0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)----- 534.50 MMBTUH

ALLOWABLES:

ALLOWABLE EMISSION (OIL)----- 0.10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)----- 0.15 LB/MMBTU

TOTAL ALLOWABLE EMISSION----- 80.18 LB/HR
TOTAL ACTUAL EMISSION----- 58.05 LB/HR

TOTAL ALLOWABLE EMISSION----- 0.150 LB/MMBTU
TOTAL ACTUAL EMISSION----- 0.109 LB/MMBTU

RE: RING - OF - WOOD
PER
PT. WYERS

[illegible]

AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

PLANT: U. S. SUGAR CORPORATION DATE: 3-05-92
LOCATION: BRYANT, FLORIDA RUN NUMBER 3
SOURCE: NUMBER 5 BOILER, SCRUBBER OUTLET TIME: 1220-1329

TIME INTERVAL----- 69 MINUTES

OIL:

FINAL OIL----- 0
BEGIN OIL----- 0
FACTOR----- 1

STEAM:

FINAL STEAM----- 868513
BEGIN STEAM----- 868432
FACTOR----- 3500
TEMPERATURE----- 900 DEGREES F
PRESSURE----- 850 PSIG
865 PSIA

FEEDWATER:

TEMPERATURE----- 260 DEGREES F
PRESSURE----- 1260 PSIG
1275 PSIA

HEAT INPUT:

STEAM----- 1452.2 BTU/LB
FEEDWATER----- 228.6 BTU/LB
NET STEAM----- 1223.6 BTU/LB
STEAM RATE----- 246522 LB/HR
BOILER EFFICIENCY----- 55.0 %
TOTAL FUEL HEAT INPUT----- 548.44 MMBTUH
STEAM CALIBRATION FACTOR----- 1.00

OIL----- 0.00 GPH
OIL----- 150000 BTU/GAL

TOTAL HEAT INPUT (OIL)----- 0.00 MMBTUH
TOTAL HEAT INPUT (NON-OIL)----- 548.44 MMBTUH

ALLOWABLES:

ALLOWABLE EMISSION (OIL)----- 0.10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)----- 0.15 LB/MMBTU

TOTAL ALLOWABLE EMISSION----- 82.27 LB/HR
TOTAL ACTUAL EMISSION----- 57.30 LB/HR

TOTAL ALLOWABLE EMISSION----- 0.150 LB/MMBTU
TOTAL ACTUAL EMISSION----- 0.104 LB/MMBTU

REV 1
539.03

45

BOILER NUMBER 5

OIL METER FACTOR NO OIL

SCRUBBER(S) PRESS. DROP____, ____

SCRUBBER(S) GPM _____, _____

SCRUBBER(S) H2O LEVEL _____, _____

Ph(if applicable) _____, _____

FINAL INTEGRATOR 868513

1220

1329

[illegible]

APPENDIX E

QUALITY ASSURANCE

STANDARD METER CALIBRATION
Meter Number 1040616

Air Consulting and Engineering, Inc. (ACE) uses a dry gas meter for the calibration standard. This meter has been calibrated against a wet test meter in triplicate. This data was used to generate a standard meter calibration curve (see next page). Field meter calibrations are corrected to this curve using the following formula:

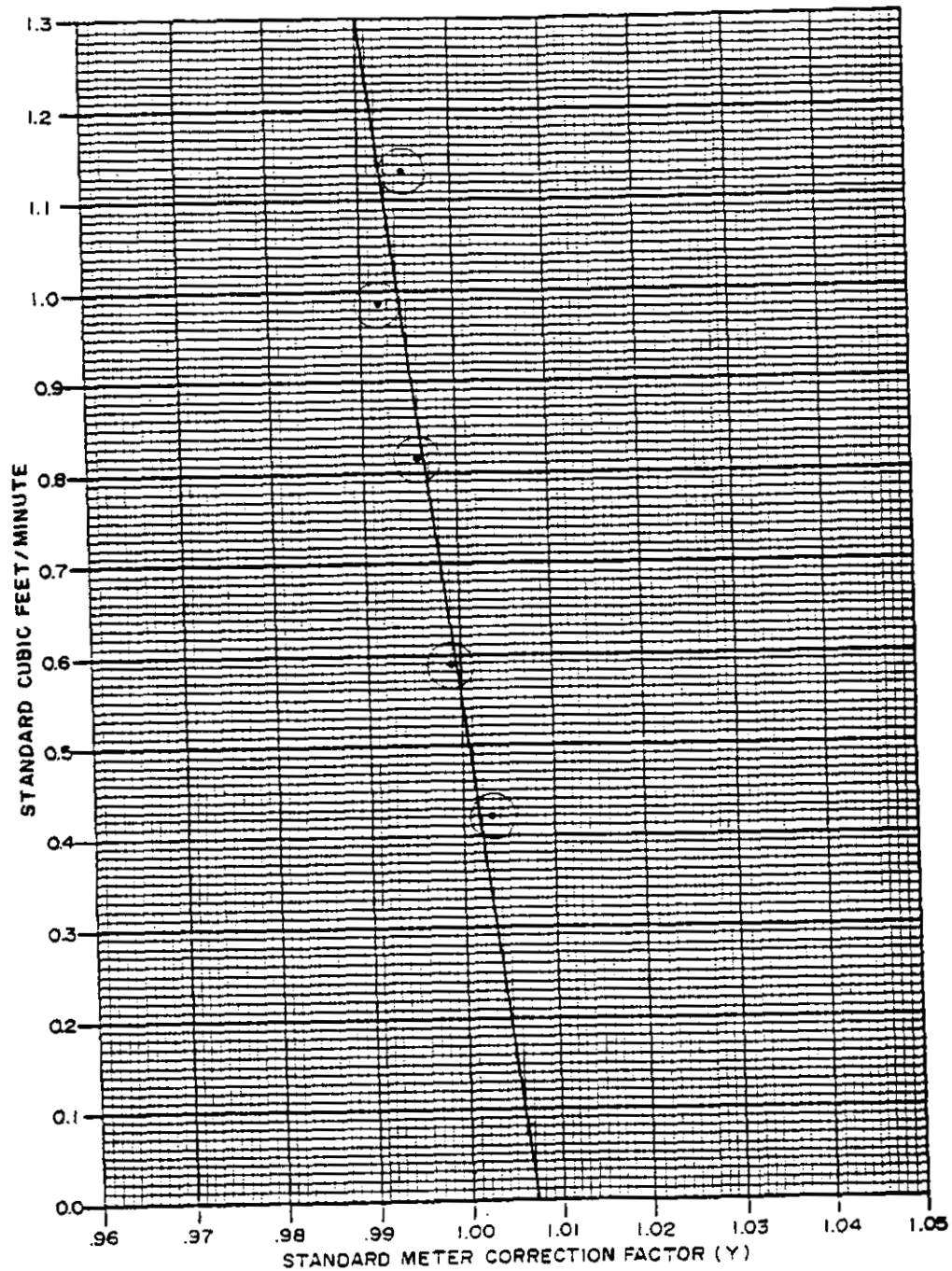
$$Y_a \times Y_s = Y$$

Y_a = actual ratio of field meter to standard meter

Y_s = ratio of standard meter to wet test meter at a given
flow rate (from Calibration Curve)

Y = corrected ratio of field meter

The dry standard meter was calibrated on June 11, 1991, and is checked and/or recalibrated at least annually.



STANDARD METER CALIBRATION
CURVE

JUNE 11, 1991

AIR CONSULTING
and
ENGINEERING

AIR CONSULTING & ENGINEERING STANDARD METER CALIBRATION

DATE 6-13-91 LEAK CHECK 0.000 CFM at 12 In. Hg.

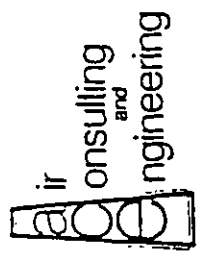
METER SERIAL NUMBER 1040616 BAROMETRIC PRESSURE 30.12 In. Hg.

STD GAS METER TEMPERATURE 74 °F/ASTM GLASS THERMOMETER TEMPERATURE 74 °F

WET ΔH	STD ΔH	GAS VOLUME, WET TEST METER			GAS VOLUME, STD GAS METER			TEMP. WET TEST METER (°F)	TEMP OF STD METER (°F)	TIME (Minutes)
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³			
-0.3	-0.60	6.012	11.553	5.511	0.003	5.500	5.497	74	74	13
-0.3	-0.60	1.553	7.032	5.479	5.500	10.979	5.479	75	75	13
-0.3	-0.60	7.032	12.509	5.477	10.979	16.450	5.471	75	75	13
-0.3	-0.96	2.853	8.143	5.290	16.804	22.127	5.323	75	76	9
-0.3	-0.96	8.143	13.430	5.287	22.127	27.442	5.315	75	76	9
-0.3	-0.96	3.430	8.703	5.273	27.442	32.753	5.311	75	77	9
-0.4	-1.6	9.252	14.995	5.743	33.311	39.123	5.812	76	78	7
-0.4	-1.6	4.995	10.713	5.718	39.123	44.909	5.786	76	78	7
-0.4	-1.6	0.713	6.145	5.732	44.909	50.707	5.798	76	78	7
-0.5	-2.1	6.941	12.917	5.976	51.214	57.292	6.078	76	78	6
-0.5	-2.1	2.917	8.898	5.981	57.292	63.375	6.083	76	78	6
-0.5	-2.1	8.898	14.813	5.975	63.375	69.452	6.077	76	78	6
-0.7	-2.7	5.278	10.988	5.710	69.452	75.663	5.797	76	78	5
-0.7	-2.7	0.988	6.708	5.720	75.663	81.474	5.811	76	78	5
-0.7	-2.7	6.708	12.386	5.678	81.474	87.247	5.773	76	78	5

CALIBRATED BY: W. F. Stabel

	Y	SCFM	Y	SCFM	Y	SCFM	Y	SCFM
Run 1	1.004	0.422	0.998	0.584	0.996	0.814	0.992	0.98E
Run 2	1.001	0.419	0.999	0.584	0.996	0.810	0.992	0.989
Run 3	1.003	0.419	0.999	0.582	0.996	0.812	0.992	0.988
Average	1.003	0.420	0.999	0.593	0.996	0.812	0.992	0.988
								1.131



air consulting
and
engineering

AIR CONSULTING & ENGINEERING

ANNUAL METER CALIBRATION

DATE 10-3-91 LEAK CHECK 0.500 CFM at 15 In. Hg.

METER BOX NUMBER 6 BAROMETRIC PRESSURE 29.94 In. Hg.

DRY GAS METER TEMPERATURE 82 °F / ASTM GLASS THERMOMETER TEMPERATURE 82 °F

ΔH_2	AVERAGE ΔH_D	GAS VOLUME, STANDARD METER			GAS VOLUME, DRY GAS METER			TEMP STD METER	TEMP OF DRY METER	TIME (Minutes)	TIMER
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³				
-0.08	0.5	65.936	72.128	6.192	550.514	556.690	6.176	81	82	16	16
-0.13	1.0	72.551	78.148	5.597	557.102	562.651	5.549	81	82	10	
-0.18	1.5	78.417	84.504	6.087	562.914	568.942	6.028	81	83	9	
-0.24	2.0	84.709	90.083	5.374	569.145	574.456	5.311	81	83	7	
-0.35	3.0	90.361	96.007	5.646	574.724	580.290	5.566	81	84	6	
-0.46	4.0	96.243	101.631	5.388	580.521	585.818	5.297	81	85	5	

DELTA H	Y _a	SCFM	Y _s	Y
1.909	1.003	0.378	1.004	1.007
1.825	1.008	0.547	1.001	1.009
1.871	1.010	0.661	1.000	1.009
1.937	1.011	0.750	0.998	1.009
1.930	1.013	0.919	0.996	1.008
1.959	1.015	1.052	0.994	1.008
MEAN:	1.905	1.010	0.999	1.009

CALIBRATED BY: H. F. Gabel

AIR CONSULTING & ENGINEERING, inc. POST TEST CALIBRATION

DATE 3-9-92 METER BOX NUMBER 6 LEAK CHECK 0.00 CFM at 20 in. Hg.
 CLIENT U.S. Sugar / Bryant SOURCE #2 Boiler THERMOCOUPLE NUMBER 48 PYROMETER NUMBER 48-3
 FLIGHT SERVICE Pb in. Hg. ACE BAROMETER Pb 29.87 in. Hg.
 ASTM GLASS THERMOMETER 157 °F / THERMOCOUPLE 156 °F ASTM GLASS THERMOMETER 20 °F / METER TEMP 20 °F

ΔHS	AVERAGE ΔHD	GAS VOLUME, STANDARD METER			GAS VOLUME, DRY GAS METER			TEMP STANDARD METER	TEMP OF DRY METER	TIME (Minutes)	MAX. VACUUM (in. Hg.)
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³				
2.8	1.9	764.376	771.800	7.424	307.640	315.155	7.515	77 28 77.5	79 83 81	10	20
2.8	1.9	771.800	774.287	7.487	315.155	322.768	7.613	77 29 77.5	83 86 84.5	10	20
2.75	1.9	779.287	786.766	7.479	322.268	330.399	7.631	79 80 77.5	86 89 87.5	10	20

CALIBRATED BY: Carolyn M. Farland

DELTA H
 1.954
 1.916
 1.916

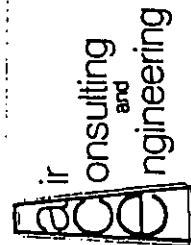
Ya
 0.990
 0.990
 0.990

SCFM
 0.728
 0.733
 0.731

Ys
 0.998
 0.998
 0.998

Y
 0.988
 0.988
 0.988

MEAN: 1.929 0.990 0.988



AIR CONSULTING & ENGINEERING, INC. PITOT TUBE CALIBRATION

DATE CALIBRATED 11-4-91 PITOT TUBE 90
 IS PITOT TUBE ASSEMBLY LEVEL YES ARE PITOT TUBE OPENINGS DAMAGED NO
 $\alpha_1 = 2.5^\circ (<10^\circ)$, $\alpha_2 = 1.0^\circ (<10^\circ)$, $\beta_1 = 2.5^\circ (<5^\circ)$, $\beta_2 = 1.0^\circ (<5^\circ)$
 $\gamma = 3.0^\circ$ $\theta = 2.0^\circ$ $A = 4.15 \text{ in.} = (P_a + P_b)$
 $z = A \sin \gamma = 0.060 \text{ in.} < 0.32 / < 1/8 \text{ in.}$
 $w = A \sin \theta = 0.040 \text{ in.} < 0.08 / < 1/32 \text{ in.}$
 $P_a \underline{0.575} \text{ in.}$ $P_b \underline{0.575} \text{ in.}$ $D_t \underline{.375}$
 WAS CALIBRATION REQUIRED NO

THERMOCOUPLE CALIBRATION

SOURCE (SPECIFY)	ASTM GLASS THERMOMETER WITH MERCURY (°F)	PYROMETER (°F)	DEGREE DIFFERENCE	PERCENT DIFFERENCE
ICE BATH	<u>36</u>	<u>36</u>	<u>0</u>	<u>0</u>
AMBIENT	<u>58</u>	<u>58</u>	<u>0</u>	<u>0</u>
HOT OVEN	<u>415</u>	<u>416</u>	<u>1</u>	<u>0.19</u>
CALIBRATED BY: <u>L.D. Carter</u> EPA $\left[\frac{(\text{REF. TEMP } ^\circ\text{F} + 460^\circ) - (\text{PYROMETER TEMP } ^\circ\text{F} + 460^\circ)}{\text{REF. TEMP } ^\circ\text{F} + 460^\circ} \right] 100 \leq 1.5\%$ FDER - MAXIMUM 5° DIFFERENCE				

AIR CONSULTING & ENGINEERING, INC. PYROMETER CALIBRATION

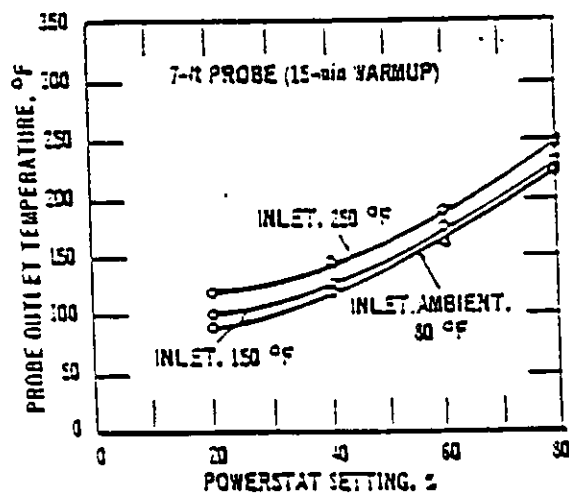
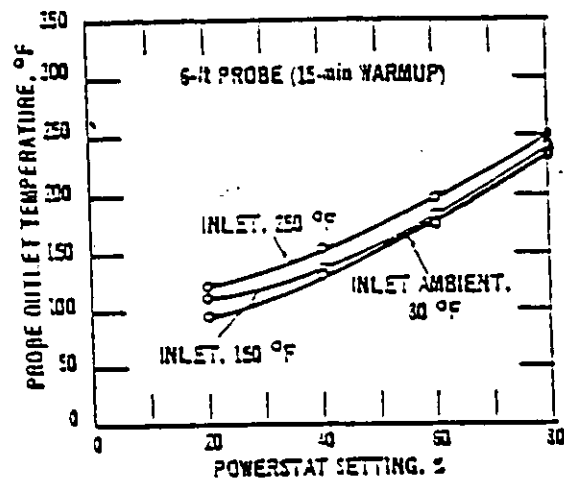
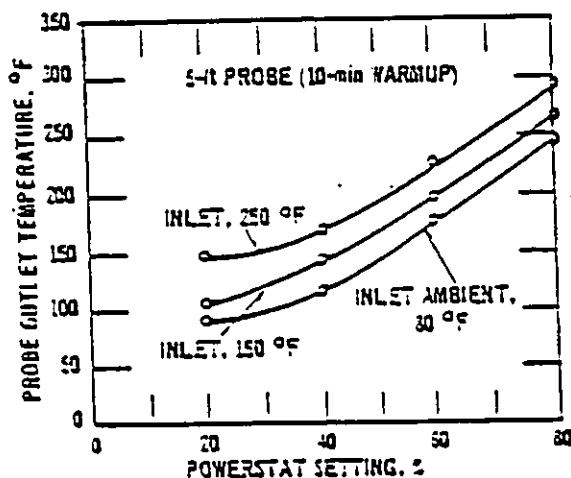
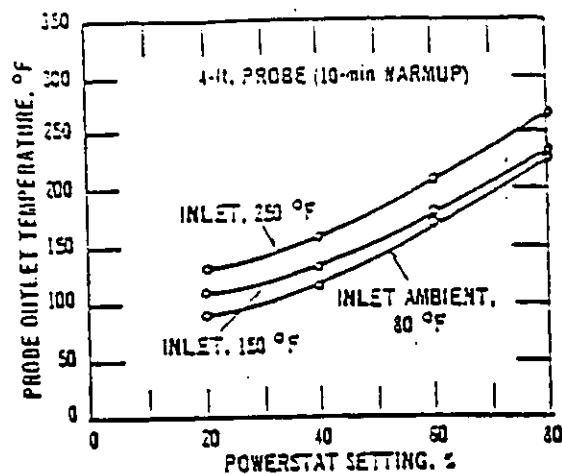
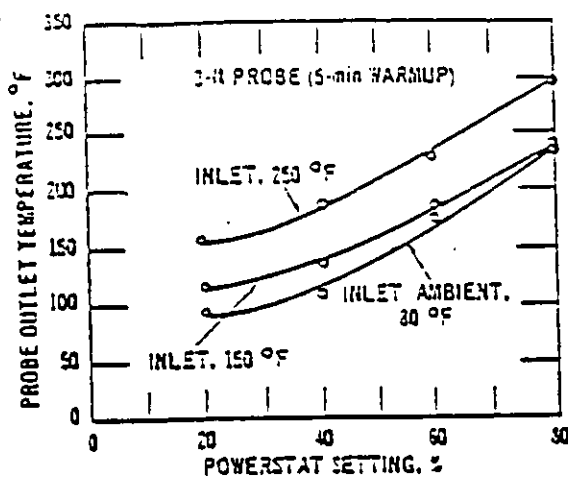
DATE 8-25-91 PYROMETER NUMBER Atkins #3

SOURCE (SPECIFY)	GLASS THERMOMETER WITH NBS MERCURY (°F)	PYROMETER (°F)	DEGREE DIFFERENCE	PERCENT DIFFERENCE
ICE BATH	<u>35</u>	<u>37</u>	<u>2</u>	<u>0.4</u>
AMBIENT	<u>88</u>	<u>89</u>	<u>1</u>	<u>0.2</u>
HOT OVEN	<u>345</u>	<u>348</u>	<u>3</u>	<u>0.5</u>

FDER - MAXIMUM 5° DIFFERENCE

EPA
$$\left[\frac{(\text{REF. TEMP } ^\circ\text{F} + 460^\circ) - (\text{PYROMETER TEMP } ^\circ\text{F} + 460^\circ)}{\text{REF. TEMP } ^\circ\text{F} + 460^\circ} \right] 100 \leq 1.5\%$$

CALIBRATED BY: S. L. Carter



NOTE: Flow rate held constant at 0.75; 50% change in flow rate has little effect on probe temperature.

Probe temperatures.

SAMPLE RECOVERY AND CHAIN OF CUSTODY

SAMPLE RECOVERY				
RUN NO.	CONTAINER NO.	LIQUID LEVEL MARKED	COLOR	COMMENTS
1	1072	-	DK. Black	
1	S-6	✓	clear	
2	1071	-	DK. Black	
2	S-21	✓	clear	
3	1070	-	DK. Black	
3	S-32	✓	clear	
ACETONE/ WATER BLANK (CIRCLE)	S-44A	✓	clear	
FILTER BLANK	1060	-	white	

RUN NO.	CONTAINER NO.	SILICA GEL		NET WT. (g)	COLOR
		FINAL WT. (g)	INIT. WT. (g)		
1	28	206.2	200.0	6.2	ok
2	15	211.0	200.0	11.0	ok
3	129	206.1	200.0	6.1	ok
			200.0		
			200.0		
			200.0		
			200.0		
			200.0		

APPENDIX F
PROJECT PARTICIPANTS

PROJECT PARTICIPANTS

AIR CONSULTING AND ENGINEERING, INC.

Stephen L. Neck, P.E.
Project Manager

Gerard Gauthreaux
Field Testing

Early McFarland
Field Testing

Christy Neck
Laboratory Analysis

Dagmar Neck
Report Preparation

Candace V. Taylor
Document Production

U.S. SUGAR CORPORATION

Peter Barquin
Project Director

Augusto Blanchard
Project Coordinator

FDER

Sterling Jordan
Test Observer

PALM BEACH COUNTY

Raisa Neginsky
Test Observer

David Brown
Test Observer