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AP-42 Section Number: 1.8

Reference Number: 41

Title: Source Test Report for Particulate Emissions Twin Impingement Wet Scrubbers Boiler Number 3

November 1991

OSWI-SCGC12

**SOURCE TEST REPORT
for
PARTICULATE EMISSIONS**

**TWIN IMPINGEMENT WET SCRUBBERS
BOILER NUMBER 3**

NOVEMBER 21, 1991

Prepared for:

**SUGAR CANE GROWERS
COOPERATIVE OF FLORIDA
AIRPORT ROAD
BELLE GLADE, FLORIDA 33430-0666**

Prepared by:

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REPORT CERTIFICATION

To the best of my knowledge, all applicable field and analytical procedures comply with Florida Department of Environmental Regulation requirements and all test data and plant operating data are true and correct.

Dagmar Neck
Dagmar Neck

12/30/91
Date

1.0 INTRODUCTION

On November 21, 1991, Air Consulting and Engineering, Inc. (ACE), conducted particulate emission testing on the Wet Scrubber Outlet of Boiler 3 at Sugar Cane Growers Cooperative of Florida (Sugar Cane Growers) located in Belle Glade, Florida.

Testing was performed to demonstrate compliance with the current Florida Department of Environmental Regulation (FDER) operating permit.

United States Environmental Protection Agency (EPA) Method 5 was utilized for the emission testing.

Mr. Ken Tucker and Mr. Sterling Jordan of the FDER observed a portion of the testing.

Mr. Blas Marin of Sugar Cane Growers coordinated testing and provided production data.

2.0 SUMMARY AND DISCUSSION OF RESULTS

Boiler Number 3 demonstrated compliance with the permit conditions.

Table 1 is a summary of the emission results and flue gas parameters.

Particulate emissions averaged 35.53 pounds per hour (lbs/Hr) and 0.181 pounds per million BTU (lbs/MMBTU) which is within the allowable emissions of 45.78 lbs/Hr and 0.233 lbs/MMBTU.

Complete emission summaries, field data sheets and laboratory data are presented in Appendices A, B, and C, respectively.

Production rate summaries are provided in Appendix D. This data was obtained from control room recordings of steam flow, temperature, and pressure as well as feed water temperature and pressure. Residue integrator and oil meter readings were recorded at the beginning and end of each particulate run.

Table 1 Emission Summary
Boiler Number 3
Sugar Cane Growers Cooperative of Florida
Belle Glade, Florida
November 21, 1991

Run Number	Flow Rate SCFMD	Stack Temp. °F	Stack Moisture %	Particulate Emissions		Allowable Emissions	
				lbs/Hr	lbs/MMBTU	lbs/Hr	lbs/MMBTU
1	58456	149	28.0	40.43	0.211	46.12	0.241
2	55686	157	27.1	30.79	0.159	44.16	0.228
3	54050	157	27.1	35.36	0.174	47.06	0.231
AVERAGE	56064	154	27.4	35.53	0.181	45.78	0.233

3.0 PROCESS DESCRIPTION AND OPERATION

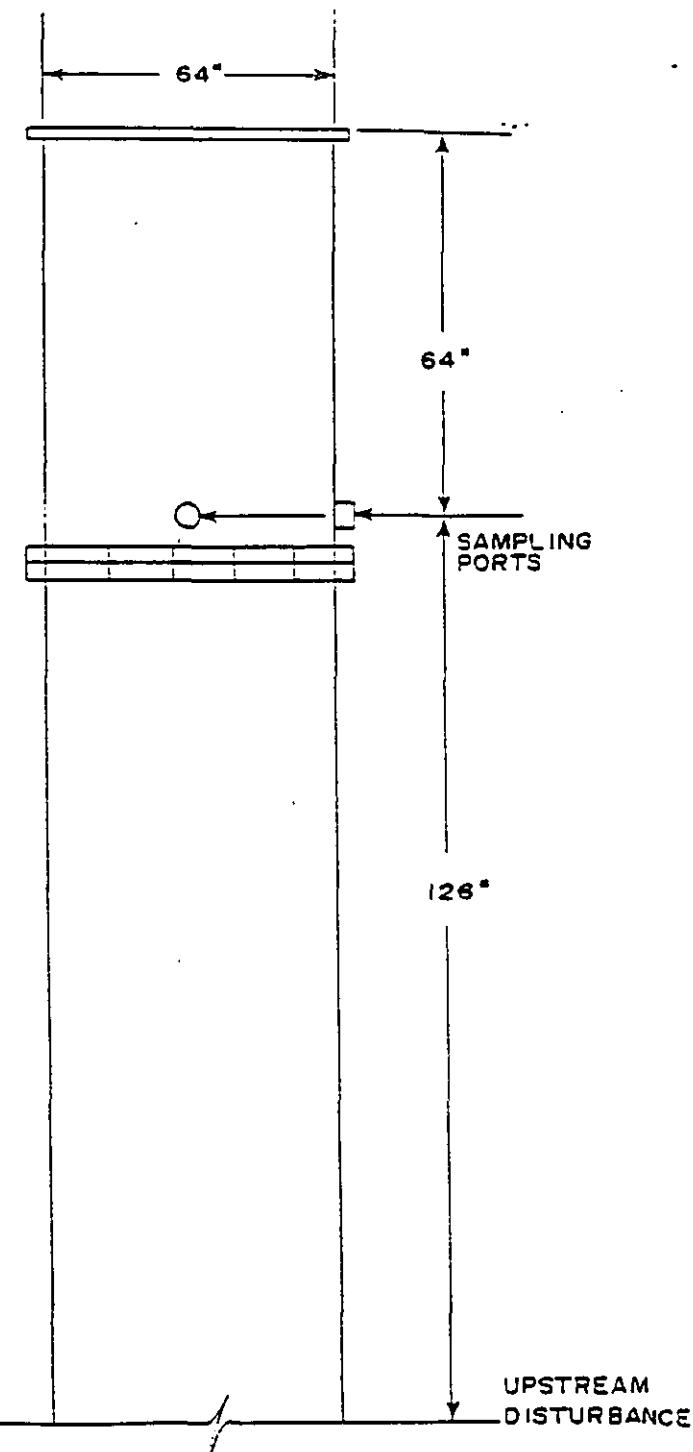
The Number 3 Boiler at Sugar Cane Growers is a spreader stoker design used primarily for residue fuel firing. Supplemental oil firing was also utilized for the emission test. The boiler averaged 102,676 lbs/Hr steam production over the three run test period.

Oil meters, steam integrators, and other production monitoring devices were rigorously calibrated prior to the production season.

4.0 SAMPLING POINT LOCATION

The sampling point location (Figure 1) consists of dual scrubber outlet stacks, each 64" in diameter. Each stack has two sample ports 90 degrees apart. The ports on the south stack are located 126 from an upstream disturbance and 64" from the outlet.

Twenty-four test points were sampled on each stack for each test run. The traverse were located as shown below. The stack configuration is such that there was no reason to evaluate the presence of cyclonic flow.



NOTE: NOT TO SCALE

FIGURE I.
SAMPLING POINT LOCATION
BOILER NO. 3
SUGARCAKE GROWERS COOP OF FLORIDA

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5.0 FIELD AND ANALYTICAL PROCEDURES

5.1 *Particulate Matter Sampling and Analysis--EPA Method 5 (Glass Probe)*

Particulate matter samples were collected by the particulate matter emission measurement method specified by the United States Environmental Protection Agency. A schematic diagram of the sampling train used is shown in Figure 2. All particulate matter captured from the nozzle to, and including, the filter was included in the calculation of the emission rate of particulate matter.

PREPARATION OF EQUIPMENT

1. **FILTERS** - Gelman type "A" filters were placed in a drying oven for two hours at 105 degrees C, removed and placed in a standard desiccator containing indicating silica gel, allowed to cool for two hours, and weighed to the nearest 0.1 mg. The filters were then re-desiccated for a minimum of six hours and weighed to a constant weight (less than 0.5 mg change from previous weighing). The average of the two constant weights was used as the tare weight.
2. **NOZZLE, FILTER HOLDER, AND SAMPLING PROBE** - The nozzle, filter holder, and sampling probe were washed vigorously with soapy water and brushes, rinsed with distilled water and acetone, and dried prior to the test program. All openings on the sampling equipment were sealed while in transit to the test site.
3. **IMPINGERS** - The Greenburg-Smith impingers were cleaned with a warm soapy water solution and brushes, rinsed with distilled water and acetone, and dried. The impingers were sealed tightly during transit.

TEST PROCEDURE

Prior to performing the actual particulate matter sample runs, certain stack and stack gas parameters were measured. These preliminary measurements

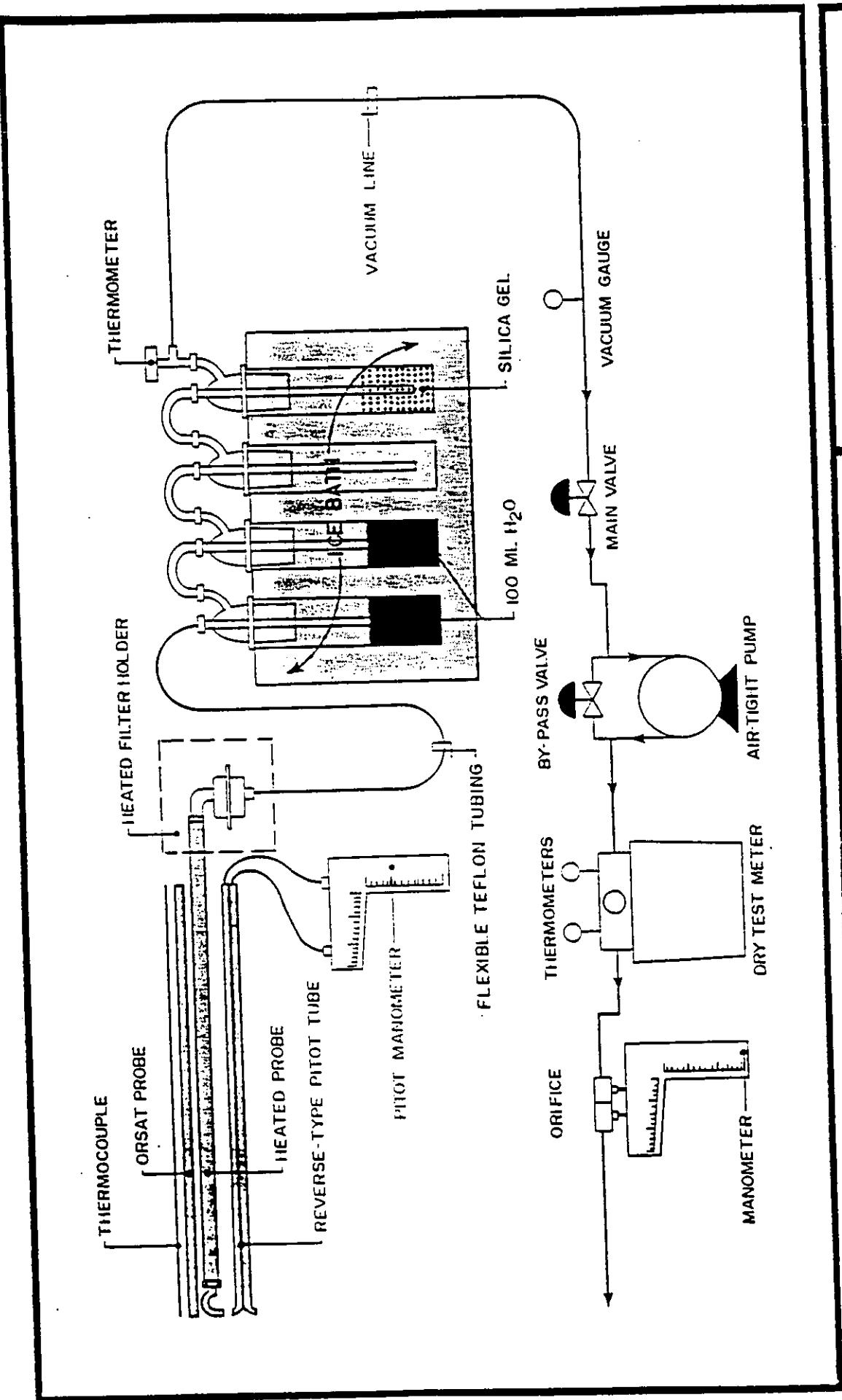


FIGURE 1
EPA METHOD 5 SAMPLING TRAIN

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included the average gas temperature, the stack gas velocity head, the stack gas moisture content, and the stack dimensions at the point where the tests were being performed. The stack gas temperature was determined by using a bi-metallic thermocouple and calibrated pyrometer. Velocity head measurements were made with calibrated type "S" pitot tube and an inclined manometer. Velocity head measurements of 0.05 inches H_2O or less were measured utilizing a micromanometer.

The sampling traverse points were selected so that a representative sample could be extracted from the gas stream. The traverse points were located in the center of equal areas, the number of which were dependent upon the distance upstream and downstream from flow disturbances.

Each particulate matter test run consisted of sampling for a specific amount of time at each traverse point. The type "S" pitot tube was connected to the sampling probe so that an instantaneous velocity head measurement could be made at each traverse point while making the test run. The stack gas temperature was also measured at each traverse point. Nomographs were used to calculate the isokinetic sampling rate at each traverse point during each test run.

The gases sampled passed through the following components: a stainless steel nozzle and glass probe; a glass fiber filter; two impingers each with 100 ml

of distilled deionized water; one impinger dry; one impinger with 200 grams of silica gel; a flexible sample line; an air-tight pump; a dry test meter; and a calibrated orifice. The second impinger had a standard tip, while the first, third, and fourth impingers had modified tips with a 0.5 inch I.D. opening.

Sample recovery was accomplished by the following procedures:

1. The pre-tared filter was removed from its holder and placed in Container 1 and sealed. (This is usually performed in the lab.)
2. All sample-exposed surfaces prior to the filter were washed with acetone and placed in Container 2, sealed and the liquid level marked.
3. The volume of water from the first three impingers was measured for the purpose of calculating the moisture in the stack gas and then discarded.
4. The used silica gel from the fourth impinger was transferred to the original tared container and sealed.

LABORATORY ANALYSIS

The three sample containers from each sample run were analyzed according to the following procedures:

1. The filter was dried at 105 degrees C for three hours, desiccated for a minimum of one hour, and weighed to the nearest 0.1 mg. A minimum of two such weighings six hours apart was made to determine constant weight.
2. The acetone from Container 2 was transferred to a tared beaker and evaporated to dryness at ambient temperature and pressure, desiccated for 24 hours, and weighed to the nearest 0.1 mg. A minimum of two such weighings six hours apart were made to determine constant weight.
3. The used silica gel in its tared container was weighed to the nearest 0.1 gram.

The total sample weight included the weight of material collected on the filter plus the weight of material collected in the nozzle, sampling probe, and front half of the filter holder.

DATA

The field data sheets, calculation sheets, and nomenclature definitions are included in the appendices of this report.

APPENDIX A
COMPLETE EMISSION DATA

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COMPLETE EMISSION DATA

PLANT: SUGAR CANE GROWERS COOPERATIVE OF FLORIDA
SOURCE: NUMBER 3 BOILER SCRUBBER OUTLET
DATE: 11-21-91

RUN NO.:	1	IMPIINGER ml	278
BEGIN TIME:	819	SILICA GEL gms.	9.6
END TIME:	922	PERCENT O2	10.2
TOTAL RUN TIME:	60.00 min.	PERCENT CO2	10.0
BAROMETRIC PRESSURE:	30.30 "Hg	"F" FACTOR	N/A
STACK PRESSURE:	30.30 "Hg		
NOZZLE DIAMETER:	.202 inches	PARTICULATE	
METER CORR. FACTOR:	1.004		
FINAL METER:	804.610 cubic ft.	FILTER mg.	113.1
INITIAL METER:	769.470 cubic ft.	WASH mg.	71.0
STACK AREA:	22.340 sq. ft.		

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	DRIF. DIFF.	STACK TEMP.	METER TEMP.
1-1	1.400	1.183	1.540	156	76
1-2	1.400	1.183	1.540	156	76
1-3	1.400	1.183	1.540	156	76
1-4	1.400	1.183	1.540	164	76
1-5	1.350	1.162	1.490	158	76
1-6	.850	0.922	.940	132	76
1-7	.870	0.933	.960	163	76
1-8	1.200	1.095	1.820	140	76
1-9	1.350	1.162	1.490	125	76
1-10	1.400	1.183	1.540	127	76
1-11	1.550	1.245	1.710	125	78
1-12	1.550	1.245	1.710	127	78
2-1	1.700	1.304	1.870	155	78
2-2	1.500	1.225	1.650	157	78
2-3	1.350	1.162	1.490	159	78
2-4	1.300	1.140	1.430	155	78
2-5	1.200	1.095	1.320	157	78
2-6	1.000	1.000	1.100	147	78
2-7	.790	0.889	.870	161	78
2-8	.850	0.922	.940	146	78
2-9	.850	0.975	1.05	155	78
2-10	1.100	1.049	1.210	160	78
2-11	1.100	1.049	1.210	140	78
2-12	1.100	1.049	1.210	149	78
AVERAGES	-----	1.106	1.375	149	78
		RUN 1			

NOZZLE AREA(SQ.FT.):	0.0002226	VOL. FLOW ACFM :	92416
Avg. VELOCITY HEAD :	1.22 "H2O	VOL. FLOW SCFMD :	58456
Avg. STACK TEMP. :	149 F		
Avg. METER TEMP. :	78 F		
Avg. DRIFICE DIFFERENTIAL:	1.37 "H2O	PARTICULATE DATA :	
METER STANDARD CUBIC FEET:	35.206		
% H2O VAPOR:	28.0	POUNDS PER HOUR:	40,434
GAS MOL. WT. DRY:	30.01	POUNDS PER SCF :	0.00000115
GAS MOL. WT. WET:	26.65	GRAINS/SCF :	0.081
% EXCESS AIR:	94.87	GRAINS/SCF @ 8% O2	0.098
Avg. STACK VEL. (FPS):	68.95	GRAINS/SCF @50% EA	0.105
MMBTU INPUT:	31.32	POUNDS PER MMBTU:	0.211
PERCENT ISOKINETIC :	100.76	LBS/MMBTU" F" FACTOR	0.000

SAMPLE CALCULATIONS - RUN 1

NOZZLE AREA (FT.2)	$(Dn/12)^2 \times 3.1416/4$	0.000223
Avg. Velocity Head:	$(AVG. SG. RT.)^2$	68.95
METER STND. FT3:	$(Mf-Mi) \times MCF \times (AVG. DRF. DIFF. / 13.6) / 29.92 \times (528 / (Tm+460))$	35.206
PERCENT H2O:	$((IMP+SG) \times (((IMP+SG) \times .0474) + SCF) \times 100$	
Mw DRY:	$((O2\% \times .32) + CO2\% \times .44) + (100 - (O2\% + CO2\%) \times .28$	30.01
Mw WET:	$(Mw DRY \times (1 - \%H2O/100)) + \%H2O \times .18$	26.65
% EXCESS AIR:	$\%O2 / (((100 - (\%O2 + \%CO2)) \times .264) - \%O2) \times 100$	94.87
STACK VEL. (FPS):	$65.49 \times .84 \times (AVG. SG. RT. VEL. HD.) \times ((Ts + 460) / (Ps \times MwWET))^{1.5}$	68.95
% ISOKINETIC:	$((Ts + 460) \times SCF \times 2992) / (528 \times FPS \times TIME \times An \times Ps \times 60 \times (1 - \%O2/100))$	100.76
VOL. FLOW (ACFM):	$FPS \times 60 \times An$	92416
STND. FLOW(SCFMD):	$ACFM \times 528 / (Ts + 460) \times (1 - \%H2O/100) \times (Ps / 29.92)$	58456
PARTICULATE LB/HR:	$PROBE + FILTER \text{ mg.} / 453600 \times (SCFMD / SCF) \times 60$	40.434
PARTICULATE LB/SCF:	$PROBE + FILTER \text{ mg.} / 453600 / SCF$	0.0000115
GRAINS/SCF:	$LB/SCF \times 7000$	0.0807
GR/SCF @ 8% O2:	$(12.9 / (20.9 - \%O2)) \times GR/SCF$	0.0977
GR/SCF @ 50% E.A.:	$GR/SCF \times ((100 + \%E.A.) / 150)$	0.1048
LB/MMBTU:	$(LB/HR) / (LB/MMBTUH)$	0.211
LB/MMBTU "F" FACTOR:	$LB/SCF \times "F" \text{ FACTOR} \times (20.9 / (20.9 - \%O2))$	0.000

AIR CONSULTING and ENGINEERING
COMPLETE EMISSION DATA

PLANT: SUGAR CANE GROWERS COOPERATIVE OF FLORIDA
SOURCE: NUMBER 3 BOILER SCRUBBER OUTLET
DATE: 11-21-81

RUN NO.:	2	IMPIINGER ml	241
BEGIN TIME:	1026	SILICA GEL cms.	7.4
END TIME:	1129	PERCENT O2	10.0
TOTAL RUN TIME:	60.00 min.	PERCENT CO2	10.0
BAROMETRIC PRESSURE:	30.30 "Hg	"F" FACTOR	N/A
STACK PRESSURE:	30.30 "Hg		
NOZZLE DIAMETER:	.202 inches	PARTICULATE	
METER CORR. FACTOR:	1.004		
FINAL METER:	836,560 cubic ft.	FILTER mg.	77.1
INITIAL METER:	604,810 cubic ft.	WASH mg.	55.6
STACK AREA:	22,340 sq. ft.		

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIF. DIFF.	STACK TEMP.	METER TEMP.
1-1	1.600	1.1268	1.600	154	78
1-2	1.620	1.1273	1.620	154	78
1-3	1.350	1.1182	1.350	152	78
1-4	1.200	1.095	1.200	154	78
1-5	1.160	1.049	1.160	153	78
1-6	1.900	0.949	1.900	153	78
1-7	1.600	0.775	1.600	155	78
1-8	1.730	0.884	1.730	160	78
1-9	1.870	0.933	1.870	160	78
1-10	1.910	0.954	1.910	154	75
1-11	1.930	0.964	1.930	154	75
1-12	1.930	0.964	1.930	154	75
2-1	1.400	1.1138	1.400	154	81
2-2	1.350	1.1162	1.350	157	81
2-3	1.350	1.1162	1.350	151	81
2-4	1.200	1.095	1.200	163	81
2-5	1.150	1.072	1.150	155	81
2-6	1.730	0.884	1.730	163	82
2-7	1.800	0.884	1.800	164	82
2-8	1.100	1.046	1.100	163	82
2-9	1.200	1.095	1.200	154	82
2-10	1.200	1.095	1.200	159	82
2-11	1.300	1.140	1.300	155	83
2-12	1.300	1.140	1.300	155	83
AVERAGES	-----	1.049	1.117	157	80
	RUN 2				

NOZZLE AREA(SQ.FT.):	0.0002226		
Avg. VELOCITY HEAD:	1.10 "H2O	VOL. FLOW ACFM:	86105
Avg. STACK TEMP.:	157 F	VOL. FLOW SCFMD:	55686
Avg. METER TEMP.:	80 F		
Avg. ORIFICE DIFFERENTIAL:	1.12 "H2O	PARTICULATE DATA:	
METER STANDARD CUBIC FEET:	31,750		
% H2O VAPOR:	27.1	POUNDS PER HOUR:	30,786
GAS MOL. WT. DRY:	30.00	POUNDS PER SCF:	0.0000092
GAS MOL. WT. WET:	26.75	GRAINS/SCF:	0.064
% EXCESS AIR:	89.33	GRAINS/SCF @ 8% O2:	0.076
Avg. STACK VEL. (FPS):	65.78	GRAINS/SCF @ 50% EA:	0.082
METER INPUT:	192.75	POUNDS PER MMBTU:	0.159
PERCENT DECKINETIC:	86.19	LEB/MMBTU/F"FACTOR:	0.000

SAMPLE CALCULATIONS - RUN 2

NOZZLE AREA (FT.2)	$(Dn/12)^2 \times 3.1415/4$	0.000228
Avg. Velocity Head:	$(AVG. SG. RT.)/12$	65.73
METER STNO. FT3:	$(Mf-Mi) \times SCF \times (AVG. DRF. DIFF. /$ $13.6) / 29.52 \times (528 / (Tm+460))$	31.750
PERCENT H2O:	$((IMF+SG) \times (((IMF+SG) \times .0474) +$ $SCF) \times 100$	
Mw DRY:	$((CO2 \times .32) + CO2 \times .44) + (100 - (CO2 + CO2) \times .26)$	30.00
Mw WET:	$Mw DRY \times (1 - \%H2O/100) + \%H2O \times .18$	26.75
% EXCESS AIR:	$\%O2 / (((100 - (\%CO2 + \%O2)) \times .264) - \%O2) \times$ 100	69.83
STACK VEL. (FPS):	$85.49 \times .64 \times (AVG. SG. RT. VEL. HC.) \times ((Ts$ $+460) / (Ps \times MwWET)) + .5$	65.73
% ISOkinetic:	$((Ts+460) \times SCF \times 2952) / (528 \times FPS \times TIME \times$ $Am \times Ps \times 60 \times As$	55.35
VOL. FLOW (ACFM):	$ACFM \times 528 / (Ts+460) \times (1 - \%H2O/100) \times$ $(Ps/29.92)$	66105
STND. FLOW(SCFMD):	$ACFM \times 528 / (Ts+460) \times (1 - \%H2O/100) \times$ $(Ps/29.92)$	55686
PARTICULATE LB/HR:	$PROBE+FILTER \text{ md.} / 453600 \times (SCFMD /$ $SCF) \times 60$	30.786
PARTICULATE LB/SCF:	$PROBE+FILTER \text{ md.} / 453600 / SCF$	0.0000092
GRAINS/SCF:	$LB/SCF \times 7000$	0.0645
GR/SCF @ 8% O2:	$(12.9 / (20.9 - \%O2)) \times GR/SCF$	0.0763
GR/SCF @ 50% E.A.:	$GR/SCF \times ((100 + \%E.A.) / 150)$	0.0817
LB/MMETU:	$(LB/HR) / (LB/MMETU)$	0.183
LB/MMETU "F" FACTOR:	$LB/SCF \times "F" \text{ FACTOR} \times (20.9 /$ $(20.9 - \%O2))$	0.000

AIR CONSULTING and ENGINEERING
COMPLETE EMISSION DATA

PLANT: SUGAR CANE GROWERS COOPERATIVE OF FLORIDA
SOURCE: NUMBER 3 BOILER SCRUBBER OUTLET
DATE: 11-21-81

RUN NO.:	5	IMPIINGER ml	235	AVG P.D.
BEGIN TIME:	1241	SILICA GEL gms.	5.0	
END TIME:	1348	PERCENT O2	9.7	
TOTAL RUN TIME:	60.00 min.	PERCENT CO2	10.0	
BAROMETRIC PRESSURE:	30.30 "Hg	"F" FACTOR	N/A	
STACK PRESSURE:	30.30 "Hg.			
NOZZLE DIAMETER:	.202 inches	PARTICULATE		
METER CORR. FACTOR:	1.004			
FINAL METER:	868.727 cubic ft.	FILTER mg.	88.4	
INITIAL METER:	837.620 cubic ft.	WASH mg.	63.8	
STACK AREA:	22.340 sq. ft.			

PORT-POINT	VELOCITY HEAD	SQUARE RT. VEL. HEAD	ORIF. DIFF.	STACK TEMP.	METER TEMP.
1-1	1.300	1.140	1.300	151	61
1-2	1.300	1.140	1.300	161	61
1-3	1.300	1.140	1.300	151	61
1-4	1.300	1.140	1.300	160	61
1-5	1.200	1.095	1.200	154	61
1-6	.740	0.660	.740	164	61
1-7	.670	0.613	.670	163	62
1-8	1.000	1.000	1.000	159	62
1-9	1.200	1.095	1.200	155	62
1-10	1.200	1.095	1.200	154	64
1-11	1.300	1.140	1.300	153	64
1-12	1.300	1.140	1.300	151	64
2-1	1.450	1.204	1.450	164	65
2-2	1.200	1.153	1.400	155	65
2-3	1.200	1.095	1.200	155	65
2-4	1.100	1.049	1.100	151	66
2-5	1.000	1.000	1.000	153	66
2-6	.880	0.911	.880	155	66
2-7	.660	0.748	.660	160	66
2-8	.640	0.800	.640	158	66
2-9	.820	0.906	.820	147	66
2-10	.800	0.894	.800	153	67
2-11	.860	0.922	.860	153	67
2-12	.860	0.922	.860	155	67
AVERAGES	-----	1.018	1.058	157	64
RUN 3					

NOZZLE AREA (SQ. FT.):	0.0002226	VOL. FLOW ACFM:	85826
AVE. VELOCITY HEAD :	1.04 "H2O	VOL. FLOW SCFM:	84050
Avg. STACK TEMP. :	157 F		
Avg. METER TEMP. :	64 F		
AVE. ORIFICE DIFFERENTIAL:	1.08 "H2O	PARTICULATE DATA :	
METER STANDARD CUBIC FEET:	30.776		
% H2O VAPOR:	27.1	POUNDS PER HOUR:	35,357
GAS MOL. WT. DRY:	29.59	POUNDS PER SCF :	0.0000109
GAS MOL. wt. WET:	26.74	GRAINS/SCF:	0.076
% EXCESS AIR:	86.26	GRAINS/SCF @ 5% O2	0.088
Avg. STACK VEL. (FPPS):	63.51	GRAINS/SCF @ 50% EA	0.094
MMBTU INPUT:	803.43	POUNDS PER MMBTU:	0.174
PERCENT ISOCALORIC:	66.16	LB/MMBTU "F" FACTOR	0.000

Avg = 154

Avg = 56.064

SAMPLE CALCULATIONS - RUN 3

NOZZLE AREA (FT.2)	$(Dn/12)^2 \times \pi \times 1416/4$	0.000223
Avg. Velocity Head:	$(AVG_SO, RT.)^2/2$	63.81
METER STNO. FT3:	$(Mf-Mi) \times SCF \times (AVG_GRF \times DIFF. / 13.6) / 25.92 \times (528 / (Tm+460))$	30.776
PERCENT H2O:	$((IMP+SG) \times ((IMP+SG) \times .0474) + SCF) \times 100$	
Mw DRY:	$((.024 \times .32) + .002 \times .44) + (100 - (.02 + .002) \times .28)$	29.99
Mw WET:	$(Mw_DRY \times (1 - \%H2O/100)) + \%H2O \times .19$	26.74
% EXCESS AIR:	$\frac{.002 / (((100 - (.002 + .002)) \times .264) - .002) \times 100}{.002}$	85.26
STACK VEL. (FPS):	$65.49 \times .84 \times (AVG_SO, RT. VEL. HD.) \times ((Tm + 460) / (Ps \times MwWET))^{1/5}$	63.81
% ISOKINETIC:	$((Tm + 460) \times SCF \times 2592) / (528 \times FPS \times TIME \times A_m \times Ps \times 60 \times (1 - \%O2/100))$	95.26
VOL. FLOW (ACFM):	$ACFM \times 528 / (Tm + 460) \times (1 - \%H2O/100) \times (Ps / 25.92)$	65526
STND. FLOW(SCFM):	$ACFM \times 528 / (Tm + 460) \times (1 - \%H2O/100) \times (Ps / 25.92)$	54050
PARTICULATE LB/HRT:	$PROBE+FILTER \text{ mg.} / 453600 \times (SCFM) / SCF \times 60$	08.357
PARTICULATE LB/SCF:	$(PROBE+FILTER \text{ mg.} / 453600) / SCF$	0.0000109
GRAINS/SCF:	$LB/SCF \times 7000$	0.0763
GR/SCF @ 6% O2:	$(12.9 / (20.9 - \%O2)) \times GR/SCF$	0.0683
GR/SCF @ 50% E.A.:	$GR/SCF \times ((100 + \%E.A.) / 150)$	0.0643
LB/MMBTU:	$(LB/HRT) / (LB/MMBTU)$	0.174
LB/MMBTU "F" FACTOR:	$LB/SCF \times "F" \text{ FACTOR} \times (20.9 / 20.9 - \%O2)$	0.000

APPENDIX B
FIELD DATA SHEETS

STACK SAMPLING FIELD DATA SHEET



PLANT Sugar Cane Growers Corp. of Fla.

SOURCE Boiler #3

PLANT LOCATION Belle Glade, Fla.

TYPE OF SAMPLING TRAIN EPA-5

TYPE OF SAMPLES P.M.

TIME START 11-21-91

TIME END 0932

SAMPLE TIME 2.5 / 24 (min/pt) = 60 Total min

ASSUMED MOISTURE 28 % FDA 72

NOMOGRAPH C₁ 110 PITOT CORR. 84P_b 30.30 "Hg P_a 30.30 "Hg

WEATHER PH4 CLOUDY TEMP 80 °F

METER BOX NO. 1 H 2.15 Y 1.004

NOZZLE CAL. 1.202 1.202 = .202

STACK DIMENSIONS 64" x 202 = .202

STACK AREA 22.34 ft² EFFECTIVE 11.2

STACK HEIGHT 112 ft

STACK DIAMETER: UPSTRM. DNSTRM.

PORT SIZE In. NIPPLE LENGTH In.

U CORD LENGTH 200

REMARKS:

MAT'L PROCESSING RATE 804610 ft³
 GAS METER READINGS: FINAL 469470 ft³
 INITIAL 3512 ft³
 NET 35140 ft³

FILTER NO. 3512 IMP. VOL. GAIN 248 ml.
 SIL GEL NO. 20 WT. GAIN 9.6 ml.
 TOTAL CONDENSATE 2816 ml.

	1	2	3	4	Avg.
% CO ₂	10	10			10
% O ₂	10.5	10			10.25
% CO					
% N ₂					

F₀ = F₀ RANGE =

ORSAT ANALYZER

LEAK CHECKS
 PRE 0.00 cfm 15 "Hg POST 0.005 cfm 15 "Hg

METER BOX/PUMP GAS SAMPLE SYST.
 ORSAT BAG

PITOT TUBE NO. 1 PRE-TEST OK
 POST-TEST(+) 0.00 / 15 H₂O/SEC
 POST-TEST(-) 0.00 / 15 H₂O/SEC

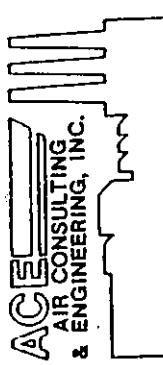
PYROMETER NO. 2
 BOX OPERATOR S. N. PROBE HOLDER S. N. C. S. N.

2106 N.W. 67th PLACE Suite 9810
GAINESVILLE, FLORIDA 32606

PORT AND TRaverse POINT NUMBER	DISTANCE FROM INSIDE STACK / COMMENTS	CLOCK TIME	GAS METER READING (FT.3)	STACK GAS VELOCITY HEAD CALC.	METER ORIFICE PRESS DIFF ("H ₂ O) ACTUAL	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP F	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN (Hg)
1-1		08:21	771.15	1.40	1.54	156	240	50	76 8.0
2		08:24	772.50	1.40	1.54	156	240	50	76 8.0
3		08:26	774.01	1.46	1.54	156	241	49	76 8.0
4		08:29	775.66	1.40	1.54	154	238	51	76 9.0
5		08:31	777.46	1.35	1.49	158	235	51	76 9.0
6		08:34	778.50	0.85	0.94	132	229	51	76 7.0

PORT AND TRAVERSE POINT NUMBER	DISTANCE FROM INSIDE STACK WALL /COMMENTS	CLOCK TIME	GAS METER READING (11.3)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O)	STACK GAS TEMP. (°F)	SAMPLE BOX TEMP. (°F)	LASER IMPINGER TEMP. (°F)	DRY GAS METER TEMP. (°F)	VACUUM ON SAMPLE TRAIN (-Hg)
1-1		08:36	779.77	.87	.96	163	243	50	76	7.0
8		08:39	781.31	1.20	1.32	140	235	50	76	4.0
9		08:41	783.20	1.35	1.49	125	233	56	76	10.0
10		08:44	784.23	1.40	1.54	127	233	56	78	11.0
11		08:46	785.81	1.55	1.71	125	237	56	78	12.0
12		08:49	787.51	1.55	1.71	127	237	56	78	12.0
West										
2-1		08:54	789.31	1.50	1.84	155	239	58	78	14.5
2		08:57	790.91	1.50	1.65	154	237	59	78	13.5
3		08:59	790.44	1.35	1.49	159	237	59	78	13.0
4		08:02	793.91	1.35	1.43	155	234	59	79	12.5
5		09:04	795.42	1.26	1.32	157	230	61	79	12.5
6		09:04	796.81	1.00	1.10	147	230	61	79	11.0
7		09:10	797.00	.79	.87	161	234	60	79	10.0
8		09:12	799.12	.85	.94	146	234	60	79	10.0
9		09:15	800.46	.95	1.05	155	233	60	79	11.0
10		09:17	801.92	1.10	1.21	160	233	60	79	12.0
11		09:20	802.20	1.10	1.21	149	233	60	79	12.5
12		09:22	804.61	1.10	1.21	149	234	60	79	12.5

STACK SAMPLING FIELD DATA SHEET



PLANT Sugar Cane Growers Coop. of Florida

SOURCE Boiler #3

PLANT LOCATION Belle Glade, Florida

EPA - 5

TYPE OF SAMPLING TRAIN P.M.

DATE 11-21-91

RUN NO. 2

TIME START 10:26

TIME END 11:29

SAMPLE TIME 2.5 / .24 (min:pt) = .60 Total min

ASSUMED MOISTURE 38 % FDA .72

ANOMOGRAPH C₁ 1.02 PITOT CORR. .84

P_b 30.130 "Hg P_a 30.30 "Hg

WEATHER Partly cloudy TEMP 80 °F

METER BOX NO. 1 H 2.15 Y 1.004

NOZZLE CAL. .202 .202 .202 = .202

STACK DIMENSIONS 64"

STACK AREA 82.34 ft² EFFECTIVE 11.2

STACK HEIGHT 112 ft

STACK DIAMETER: UPSTRM. DNSTRM. DNSTRM.

PORT SIZE 1 in. NIPPLE LENGTH 1 in.

U CORD LENGTH 200'

REMARKS:

2106 N.W. 67th PLACE - SUITE 9 & 10
GAINESVILLE, FLORIDA 32606

MAT'L PROCESSING RATE 836.640 ft³
GAS METER READINGS: FINAL 854.810 ft³
INITIAL 31.850 ft³
NET 812.180 ft³

FILTER NO. 3513 IMP. VOL. GAIN 241.0 ml.
SIL GEL NO. 18 WT. GAIN .4 ml.
TOTAL CONDENSATE .418.4 ml.

ORSAT

	1	2	3	4	Avg.
% CO ₂	10.0	10.0			10.0
% O ₂	10.0	10.0			10.0
% CO					
% N ₂					

F₀ = F₀ RANGE =

ORSAT ANALYZER

LEAK CHECKS

PRE 0.00 cfm / 15 "Hg POST 0.00 cfm / 15 "Hg
METER BOX/PUMP GAS SAMPLE SYST.

ORSAT BAG PRE-TEST OK

PITOT TUBE NO. 0.00 / 15 H₂O / sec
POST-TEST (+) 0.00 / 15 H₂O / sec
PYROMETER NO. 2

BOX OPERATOR Garrison PROBE HOLDER McClelland

PORT AND TRaverse POINT NUMBER	DISTANCE FROM INSIDE STACK / COMMENTS	CLOCK TIME	GAS METER READING (FT. ³)	STACK VELOCITY HEAD CALC.	STACK GAS TEMP CALC. ACTUAL	METER ORIFICE PRESS. DIFF. ("H ₂ O)	SAMPLE BOX TEMP (°F)	LAST IMPINGING TEMP. F	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN (Hg)
1-1		10:28	806.75	1.60	1.60	-154	250	55	78.88	8.0
2		10:31	808.15	1.62	1.62	-154	252	52	78.88	8.5
3		10:33	809.44	1.35	1.35	-152	252	52	78	8.0
4		10:36	810.88	1.20	1.20	-154	260	52	78	7.5
5		10:38	812.26	1.10	1.10	-153	257	52	78	7.5
6		10:41	813.45	.90	.90	-153	258	51	78	7.0

PORT AND DISTANCE FROM TRAVERSE INSIDE STACK POINT NUMBER WESST	CLOCK TIME	GAS METER READING (ft.3)	STACK VELOCITY HEAD	METER ORIFICE PRESS. DIFF. ("H ₂ O)		STACK GAS TEMP. (°F)	SAMPLE BOX TEMP. (°F)	LASTER IMPINGER TEMP. (°F)	DRY GAS METER TEMP. (°F)	VACUUM ON SAMPLE TRAIN (in Hg)
				CALC.	ACTUAL					
1-1	1044	814.32	.60	.60	.60	156	258	157	148	6.0
8	1046	815.42	.73	.73	.73	160	262	157	148	6.5
9	1047	816.73	.87	.87	.87	160	260	157	148	7.0
10	1051	817.90	.91	.91	.91	154	261	157	149	7.0
11	1054	819.10	.93	.93	.93	154	261	157	149	7.5
12	1056	820.36	.93	.93	.93	154	261	157	149	7.5
North										
2-1	1101	821.71	1.40	1.40	1.40	154	262	157	81	10.0
2	1104	823.93	1.35	1.35	1.35	157	263	156	81	10.0
3	1106	824.13	1.35	1.35	1.35	161	261	156	81	10.0
4	1109	826.10	1.80	1.80	1.80	163	258	156	81	9.5
5	1111	827.51	1.15	1.15	1.15	163	256	157	81	9.5
6	1114	828.51	.83	.83	.83	163	259	157	81	7.0
7	1116	829.65	.80	.80	.80	164	259	157	81	8.5
8	1119	830.99	1.10	1.10	1.10	163	263	157	81	8.9
9	1121	832.32	1.20	1.20	1.20	157	263	157	82	10.0
10	1124	833.55	1.20	1.20	1.20	153	264	157	82	11.0
11	1126	835.16	1.30	1.30	1.30	155	257	157	83	11.0
12	1129	836.66	1.30	1.30	1.30	155	256	157	83	12.0

STACK SAMPLING FIELD DATA SHEET



PLANT Sugar Cane Growers Coop. of Florida

SOURCE Boiler #3

PLANT LOCATION Belle Glade, Florida

TYPE OF SAMPLING TRAIN EPA-S

TYPE OF SAMPLES P.M.

DATE 11-21-91

RUN NO. 3

TIME START 1241

TIME END 1346

SAMPLE TIME 0.15, 24 (min:pt)= 60 Total min

ASSUMED MOISTURE 2.8 % FDA .72

PIOT CORR. .84

NOMOGRAPH C₁ 1.0Hg P₀ 30.20

TEMP 80 °F

WEATHER PTLY CLDY

METER BOX NO. 1

NOZZLE CAL. 302

NOZZLE AREA 202

STACK DIMENSIONS 64"

STACK AREA 82.34 ft² EFFECTIVE

STACK HEIGHT 12 ft

STACK DIAMETER: UPSTRM. DNSTRM.

PORT SIZE In. NIPPLE LENGTH In.

U CORD LENGTH 200'

REMARKS:

PORT AND DISTANCE FROM INSIDE STACK

POINT / COMMENTS

CLOCK TIME

GAS METER READING (FT.3)

STACK VELOCITY HEAD

CALC. ACTUAL

STACK GAS TEMP (°F)

METER ORIFICE PRESS DIFF ("H₂O)

CALC. ACTUAL

SAMPLE BOX TEMP (°F)

LAST IMPINGER TEMP F

DRY GAS METER TEMP (°F)

VACUUM ON SAMPLE TRAIN ("Hg)

2106 N.W. 67th PLACE - Suites 9 & 10
GAINESVILLE, FLORIDA 32606

MAT'L PROCESSING RATE

GAS METER READINGS: FINAL 868.724 ft³INITIAL 837.620 ft³NET 31.104 ft³IMP. VOL. GAIN 235 ft³

WT. GAIN 60 mi.

TOTAL CONDENSATE 241 mi.

ORSAT

	1	2	3	4	Avg.
% CO ₂	10.0	10.0			10.0
% O ₂	9.5	10.0			9.75
% CO					
% N ₂					

F₀ = F₀ RANGE =

ORSAT ANALYZER

LEAK CHECKS

PRE 0.01 cm³ Hg POST 0.01 cm³ Hg

METER BOX/PUMP GAS SAMPLE SYST.

ORSAT BAG

PITOT TUBE NO. 1 PRE-TEST OK

POST-TEST (+) 0.00 1/15 H₂O / SECPOST-TEST (-) 0.00 1/15 H₂O / SEC

PYROMETER NO. 2

BOX OPERATOR GANTHER PROBE HOLDER McFarland

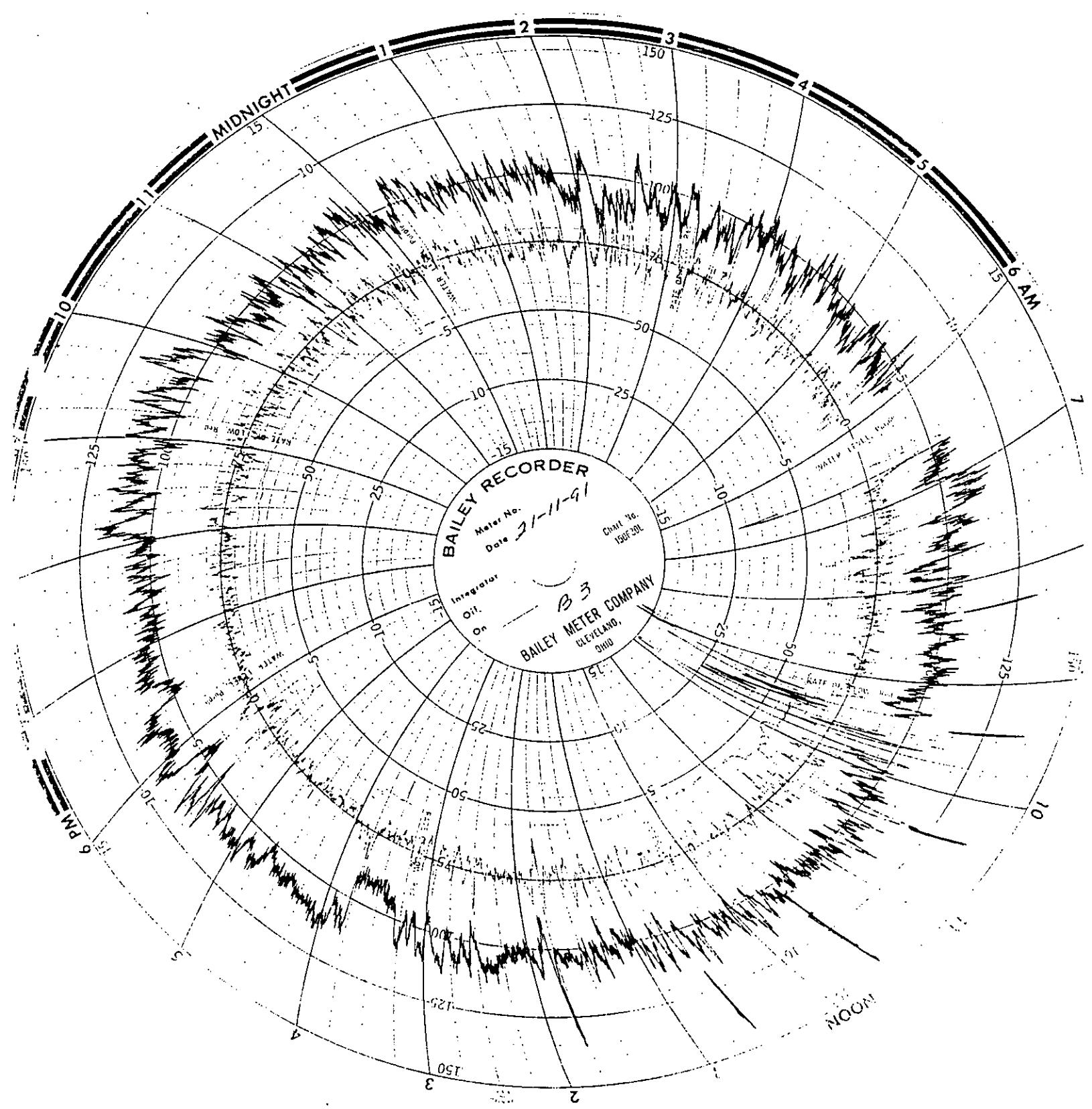
PORT AND TRAVERSE NUMBER	DISTANCE FROM INSIDE STACK	CLOCK TIME	GAS METER READING (FT.3)	STACK VELOCITY HEAD	STACK GAS TEMP (°F)	METER ORIFICE PRESS DIFF ("H ₂ O)	SAMPLE BOX TEMP (°F)	LAST IMPINGER TEMP F	DRY GAS METER TEMP (°F)	VACUUM ON SAMPLE TRAIN ("Hg")
1-1	1243	839.31	1.30	1.30	16	254	59	81	81	8.0
2	1244	840.55	1.30	1.30	16	254	59	81	81	8.0
3	1245	842.12	1.30	1.30	16	255	59	81	81	8.0
4	1251	843.61	1.30	1.30	16	256	60	81	81	8.0
5	1253	844.92	1.20	1.20	16	253	60	81	81	8.0
6	1256	845.93	1.44	1.44	16	253	61	81	81	8.0

PORT AND TRAVERSE POINT NUMBER No. 1	DISTANCE FROM INSIDE STACK WALL /COMMENTS	CLOCK TIME	GAS METER READING (1.3)	STACK VELOCITY HEAD	STACK GAS TEMP (°F)		SAMPLE BOX TEMP. (°F)	LAST IMPINGER TEMP. (°F)	DRY GAS METER TEMP. (°F)	VACUUM ON SAMPLE TRAIN (mm Hg)
					CALC.	ACTUAL				
1-7		13:59	847.21	.64	67	63	262	82	82	5.5
8		13:01	848.23	1.00	1.00	1.00	255	83	83	0.0
9		13:04	849.46	.80	1.20	1.20	259	83	83	0.0
10		13:06	851.11	1.20	1.20	1.20	258	84	84	0.0
11		13:11	852.61	1.30	1.30	1.30	258	84	84	0.0
12		13:14	854.12	1.30	1.30	1.30	268	84	84	0.0
west										
2-1		13:18	855.42	1.45	1.45	1.45	266	85	85	11.0
2		13:21	856.91	1.40	1.40	1.40	271	84	85	11.0
3		13:23	858.32	1.20	1.20	1.20	267	83	85	11.0
4		13:26	859.81	1.10	1.10	1.10	268	84	86	11.0
5		13:29	861.32	1.00	1.00	1.00	265	84	86	10.0
6		13:31	862.81	.83	.83	.83	271	85	86	9.0
7		13:33	863.10	.56	.56	.56	275	85	86	8.0
8		13:36	864.11	.64	.64	.64	275	85	86	7.0
9		13:38	865.21	.88	.88	.88	274	85	86	6.0
10		13:41	866.30	.80	.80	.80	270	84	85	5.0
11		13:43	867.44	.85	.85	.85	273	84	85	4.0
12		13:46	868.72	.85	.85	.85	273	84	85	3.0

APPENDIX C

LABORATORY ANALYSIS

APPENDIX D
PRODUCTION RATE CERTIFICATION



ATB CONSULTING & ENGINEERING, INC.
Complete Emission Data

PLANT: SUGAR CANE GROWERS COOPERATIVE DATE: 11-21-91
LOCATION: BELLE GLADE, FLORIDA RUN NUMBER 1
SOURCE: NUMBER 3 BOILER, SCRUBBER OUTLET TIME: 0816-927

TIME INTERVAL----- 71 MINUTES

OIL:

FINAL OIL-----	1265
BEGIN OIL-----	1175
FACTOR-----	1

STEAM:

FINAL STEAM-----	715271
BEGIN STEAM-----	715192
FACTOR-----	1500
TEMPERATURE-----	560 DEGREES F
PRESSURE-----	426 PSIG
	440 PSIA

FEEDWATER:

TEMPERATURE-----	260 DEGREES F
PRESSURE-----	600 PSIG
	616 PSIA

HEAT INPUT:

STEAM-----	1279.4 BTU/LB
FEEDWATER-----	226.6 BTU/LB
NET STEAM-----	1050.8 BTU/LB
STEAM RATE-----	100141 LB/HR
BOILER EFFICIENCY-----	35.0 %
TOTAL FUEL HEAT INPUT-----	151,52 MMBTUH
STEAM CALIBRATION FACTOR-----	1.00

OIL-----	76.06 GPH
OIL-----	160000 BTU/GAL

TOTAL HEAT INPUT (OIL)-----	11,41 MMBTUH
TOTAL HEAT INPUT (NON-OIL)-----	175,92 MMBTUH

ALLOWABLES:

ALLOWABLE EMISSION (OIL)-----	.10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)-----	.25 LB/MMBTU

TOTAL ALLOWABLE EMISSION-----	45.12 LB/HR
TOTAL ACTUAL EMISSION-----	40.43 LB/HR

TOTAL ALLOWABLE EMISSION-----	0.241 LB/MMBTU
TOTAL ACTUAL EMISSION-----	0.211 LB/MMBTU

BOILER OPERATION PARAMETERS

PLANT Sugar Cane Growers Corp. of Fla. BOILER NUMBER 3

DATE 11-21-91 RUN NUMBER 1 OIL METER FACTOR 1

STEAM INTEGRATOR FACTOR 1500 SCRUBBER(S) PRESS.DROP 100

OPERATOR SIGNATURE E. H. Gray SCRUBBER(S) CHARGE _____
SCRUBBER(S) H2O LEVEL _____
PH (if applicable) _____

INITIAL INTEGRATOR 715192 FINAL INTEGRATOR 715271

AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

PLANT: SUGAR CANE GROWERS COOPERATIVE DATE: 11-21-81
 LOCATION: BELLE GLADE, FLORIDA RUN NUMBER 2
 SOURCE: NUMBER 3 BOILER, SCRUBBER OUTLET TIME: 1028-1134

TIME INTERVAL-----	71 MINUTES
OIL:	
FINAL OIL-----	1890
BEGIN OIL-----	1365
FACTOR-----	1
STEAM:	
FINAL STEAM-----	715397
BEGIN STEAM-----	715317
FACTOR-----	1500
TEMPERATURE-----	560 DEGREES F
PRESSURE-----	425 PSIG
	440 PSIA
FEEDWATER:	
TEMPERATURE-----	260 DEGREES F
PRESSURE-----	600 PSIG
	615 PSIA
HEAT INPUT:	
STEAM-----	1279.4 BTU/LB
FEEDWATER-----	228.6 BTU/LB
NET STEAM-----	1050.8 BTU/LB
STEAM RATE-----	101408 LB/HR
BOILER EFFICIENCY-----	55.0 %
TOTAL FUEL HEAT INPUT-----	153.75 MMBTUH
STEAM CALIBRATION FACTOR-----	1.00
OIL:	
TOTAL HEAT INPUT (OIL)-----	190.14 GPH
TOTAL HEAT INPUT (NON-OIL)-----	1860000 BTU/GAL
TOTAL HEAT INPUT (OIL+NON-OIL)-----	
26.52 MMBTUH	
165.22 MMBTUH	
ALLOWABLES:	
ALLOWABLE EMISSION (OIL)-----	.10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)-----	.25 LB/MMBTU
TOTAL ALLOWABLE EMISSION-----	
44.16 LB/HR	
TOTAL ACTUAL EMISSION-----	
30.79 LB/HR	
TOTAL ALLOWABLE EMISSION-----	
0.228 LB/MMBTU	
TOTAL ACTUAL EMISSION-----	
0.156 LB/MMBTU	

BOILER OPERATION PARAMETERS

PLANT Sugar Cane Growers Coop. of Fla.

DATE 11-21-91 RUN NUMBER 2

STEAM INTEGRATOR FACTOR 1500

OPERATOR SIGNATURE Maurice Bent

INITIAL INTEGRATOR 715317

BOILER NUMBER 3

OIL METER FACTOR 1

SCRUBBER(S) PRESS. DROP ____, ____

SCRUBBER(S) GPM _____, _____

SCRUBBER(S) H₂O LEVEL _____,
Pb (if applicable) _____

1911 applicable, _____, _____

FINAL INTEGRATOR 715397

FINAL INTEGRATOR 715397

FINAL INTEGRATOR 715397

AIR CONSULTING & ENGINEERING, INC.
Complete Emission Data

PLANT: SUGAR CANE GROWERS COOPERATIVE DATE: 11-21-81
LOCATION: BELLE GLADE, FLORIDA RUN NUMBER 3
SOURCE: NUMBER 3 BOILER, SCRUBBER OUTLET TIME: 1240-1351

TIME INTERVAL-----	71 MINUTES
OIL:	
FINAL OIL-----	1990
BEGIN OIL-----	1750
FACTOR-----	1
STEAM:	
FINAL STEAM-----	715558
BEGIN STEAM-----	715474
FACTOR-----	1500
TEMPERATURE-----	560 DEGREES F
PRESSURE-----	425 PSIG
	440 PSIA
FEEDWATER:	
TEMPERATURE-----	260 DEGREES F
PRESSURE-----	600 PSIG
	615 PSIA
HEAT INPUT:	
STEAM-----	1279.4 BTU/LB
FEEDWATER-----	226.6 BTU/LB
NET STEAM-----	1050.8 BTU/LB
STEAM RATE-----	106475 LB/HR
BOILER EFFICIENCY-----	65.0 %
TOTAL FUEL HEAT INPUT-----	203,45 MMBTU AVH
STEAM CALIBRATION FACTOR-----	1.00
 OIL-----	 169.01 GPH 145.07
OIL-----	150000 BTU/GAL
 TOTAL HEAT INPUT (OIL)-----	 25,35 MMBTU 21.76
TOTAL HEAT INPUT (NON-OIL)-----	178,08 MMBTU <u>174.74</u>
 ALLOWABLES:	 <u>196.50</u>
ALLOWABLE EMISSION (OIL)-----	.10 LB/MMBTU
ALLOWABLE EMISSION (NON-OIL)-----	.25 LB/MMBTU
 TOTAL ALLOWABLE EMISSION-----	 47.05 LB/HR
TOTAL ACTUAL EMISSION-----	35.36 LB/HR
 TOTAL ALLOWABLE EMISSION-----	 0.291 LB/MMBTU
TOTAL ACTUAL EMISSION-----	0.174 LB/MMBTU

APPENDIX E

QUALITY ASSURANCE

AND

CHAIN OF CUSTODY

STANDARD METER CALIBRATION
Meter Number 1040616

Air Consulting and Engineering, Inc. (ACE) uses a dry gas meter for the calibration standard. This meter has been calibrated against a wet test meter in triplicate. This data was used to generate a standard meter calibration curve (see next page). Field meter calibrations are corrected to this curve using the following formula:

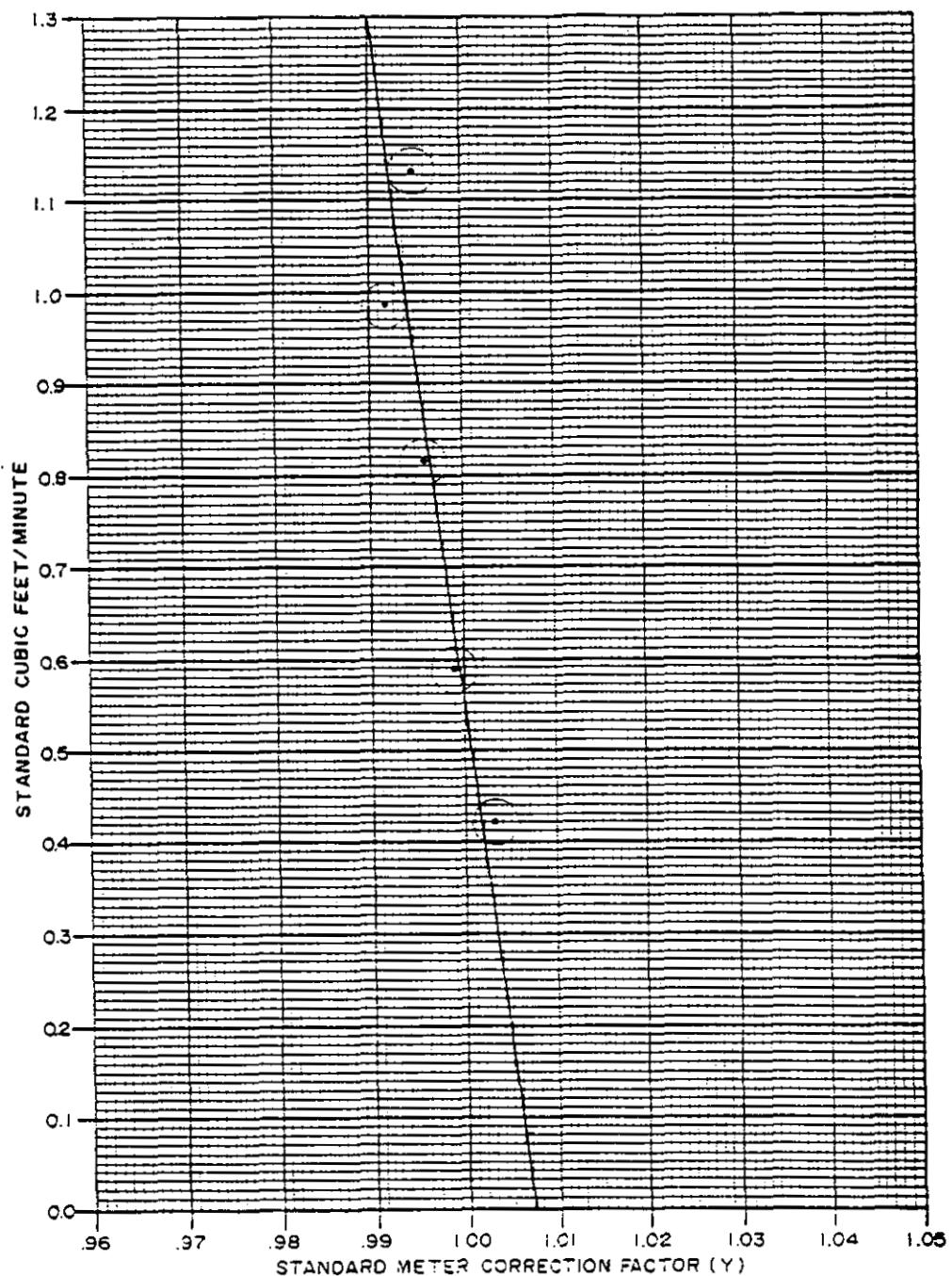
$$Y_a \times Y_s = Y$$

Y_a = actual ratio of field meter to standard meter

Y_s = ratio of standard meter to wet test meter at a given flow rate (from Calibration Curve)

Y = corrected ratio of field meter

The dry standard meter was calibrated on June 11, 1991, and is checked and/or recalibrated at least annually.



STANDARD METER CALIBRATION
CURVE

JUNE 11, 1991

AIR CONSULTING
and
ENGINEERING

AIR CONSULTING & ENGINEERING

water (a: 13.49)

LEAK CHECK 2.0 nD CFM at 15 in. Hg

STD GAS METER TEMPERATURE 71° °F / ASTM GLASS THERMOMETER TEMPERATURE 74° °F

WET ΔH	STD ΔH	GAS VOLUME, WET TEST METER			GAS VOLUME, STD GAS METER			TEMP WET TEST METER (°F)	TEMP OF STD METER (°F)	TIME (Minutes)
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³			
-1.3	-1.60	11.553	5.511	0.003	5.500	5.197	1.1	79	75	13
-1.3	-1.60	11.553	7.030	2.479	5.500	5.197	7.5	100	95	13
-1.3	-1.60	11.553	13.729	5.177	16.150	5.171	1.3	119	100	13
-1.3	-1.60	11.553	8.143	5.290	16.301	22.127	5.323	127	113	9
-1.4	-1.6	6.143	13.730	5.287	22.127	27.442	5.315	75	76	9
-1.4	-1.6	3.430	3.703	5.273	32.753	5.311	75	77	76	7
-1.4	-1.6	9.252	14.995	5.743	33.311	39.123	5.812	76	78	7
-1.4	-1.6	4.995	10.713	5.718	39.123	44.909	5.786	76	78	7
-1.4	-1.6	6.713	6.475	5.732	50.707	5.798	76	78	76	7
-1.5	-2.1	6.741	12.917	5.976	51.214	6.018	7.6	78	76	6
-1.5	-2.1	3.917	8.898	5.981	57.292	63.375	6.083	76	78	6
-1.5	-2.1	8.898	14.313	5.975	63.375	61.452	6.077	76	78	6
-1.6	-2.7	5.378	10.988	5.710	67.866	75.663	5.797	76	78	5
-1.6	-2.7	0.988	6.708	5.720	81.474	5.811	7.6	78	78	5
-1.7	-3.7	6.103	12.386	5.678	81.474	5.773	7.6	78	78	5

CALIBRATED BY: G. F. Haber

CALIBRATED BY S. T. Glabek

	Run 2	Run 3	Average
1.001	0.419	0.419	0.420
1.003	0.419	0.419	0.420
0.999	0.999	0.999	0.999
0.584	0.582	0.582	0.583
0.996	0.996	0.996	0.996
0.810	0.812	0.812	0.812
0.992	0.992	0.992	0.992
0.989	0.988	0.988	0.988
0.995	0.994	0.994	0.994
1.134	1.126	1.126	1.126
1.131	1.131	1.131	1.131

AIR CONSULTING & ENGINEERING

ANNUAL METER CALIBRATION

DATE 6-14-91LEAK CHECK 0.000 CFM at 14 in. Hg.METER BOX NUMBER #1BAROMETRIC PRESSURE 30.10 in. Hg.DRY GAS METER TEMPERATURE 87 °F/ASTM GLASS THERMOMETER TEMPERATURE 88 °F

ΔHs	GAS VOLUME, STANDARD METER			GAS VOLUME, DRY GAS METER			TEMP STD METER	TEMP OF DRY METER	TIME (Minutes)	TIME TIMER
	AVERAGE ΔHd	INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL				
-0.6	.5	977.651	993.301	5.650	894.756	890.239	5.483	87	88	15 15
-1.2	1.0	971.708	977.548	5.840	878.739	884.547	5.808	86	87	11 11
-1.6	1.5	985.835	993.630	7.795	892.764	900.523	7.759	88	89	12 12
-2.3	2.0	993.630	1000.397	6.767	900.523	907.262	6.739	88	89	9 9
-3.3	3.0	1000.397	1006.790	6.393	907.262	913.626	6.364	89	90	7 7
-4.7	4.0	1007.008	1012.339	5.331	913.950	919.144	5.194	89	91	5 5

DELTA H	Y _a	SCFM	Y _s	Y
2.026	1.031	0.366	1.000	1.031
2.036	1.005	0.516	0.998	1.003
2.048	1.003	0.630	0.996	0.999
2.038	1.001	0.729	0.994	0.995
2.076	0.999	0.884	0.991	0.990
2.027	1.020	1.032	0.988	1.008
MEAN:	2.042	1.010	0.995	1.004

Greg R. Brown
CALIBRATED BY:

AIR CONSULTING & ENGINEERING, inc.

POST TEST CALIBRATION

DATE 11-28-91 METER BOX NUMBER 1 LEAK CHECK 0.000 CFM at 20 in. Hg.
 CLIENT SUGAR CANE CONSULTING CO-OP SOURCE 411 THERMOCOUPLE NUMBER A7K2 PYROMETER NUMBER 88
 FLIGHT SERVICE PB 30.12 in. Hg. ACE BAROMETER PB 30.30 in. Hg.
 ASTM GLASS THERMOMETER 150 °F / THERMOCOUPLE 150 °F ASTM GLASS THERMOMETER 75 °F / METER TEMP 76 °F

ΔHS	AVERAGE ΔHD	GAS VOLUME, STANDARD METER			GAS VOLUME, DRY GAS METER			TEMP. STANDARD METER	TEMP. OF DRY METER	TIME (Minutes)	MAX. VACUUM in. Hg.
		INITIAL	FINAL	ACTUAL ft ³	INITIAL	FINAL	ACTUAL ft ³				
1.82	1.2	396.050	410.553	414.503	589.332	604.342	615.010	75.5	79	27	23
1.1	1.8	411.942	415.738	415.97	605.777	642.638	320.61	77	79	56	15
1.2	2.0	448.113	434.770	36.657	643.230	681.586	38.356	79	91	52	18.5

CALIBRATED BY: S & D

RUN NUMBER	SCFM	STANDARD M. C. F.	DELTA Ha	M. C. F.
1	0.53	1.005	2.338	0.971
2	0.63	1.005	2.464	0.979
3	0.69	1.005	2.230	0.979
AVERAGES	0.62	1.005	2.344	0.976



Air Consulting and Engineering

AIR CONSULTING & ENGINEERING, INC.

PYROMETER CALIBRATION

DATE 10-1-90PYROMETER NUMBER Atkins # 2

SOURCE (SPECIFY)	GLASS THERMOMETER WITH NBS MERCURY (°F)	PYROMETER (°F)	DEGREE DIFFERENCE	PERCENT DIFFERENCE
ICE BATH	<u>42</u>	<u>41</u>	<u>1</u>	<u>0.2</u>
AMBIENT	<u>88</u>	<u>88</u>	<u>0</u>	<u>0.0</u>
HOT OVEN	<u>321.5</u>	<u>344.1</u>	<u>1</u>	<u>0.2</u>

FDER - MAXIMUM 5° DIFFERENCE

$$EPA \left[\frac{(REF. TEMP. °F + 460°) - (PYROMETER TEMP. °F + 460°)}{REF. TEMP. °F + 460°} \right] 100 \leq 1.5\%$$

CALIBRATED BY: J. L. Carter

AIR CONSULTING & ENGINEERING, INC.

PITOT TUBE CALIBRATION

DATE CALIBRATED 10-21-91

PITOT TUBE 88

IS PITOT TUBE ASSEMBLY LEVEL YES

ARE PITOT TUBE OPENINGS DAMAGED NO

$$\alpha_1 = \underline{2}^{\circ}(\leq 10^{\circ}), \alpha_2 = \underline{0}^{\circ}(\leq 10^{\circ}), \beta_1 = \underline{0}^{\circ}(\leq 5^{\circ}), \beta_2 = \underline{1}^{\circ}(\leq 5^{\circ})$$

$$\gamma = \underline{2}^{\circ}, \theta = \underline{1}^{\circ}, A = \underline{1.025} \text{ in.} = (P_a + P_b)$$

$$z = A \sin \gamma = \underline{0.036} \text{ in.} < 0.32 / < 1/8 \text{ in.}$$

$$w = A \sin \theta = \underline{0.018} \text{ in.} < 0.08 / < 1/32 \text{ in.}$$

$$P_a \underline{0.512} \text{ in.}, P_b \underline{0.512} \text{ in.}, D_1 \underline{375}$$

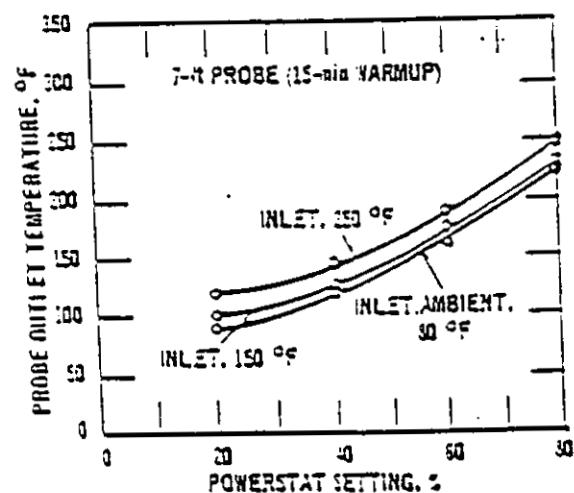
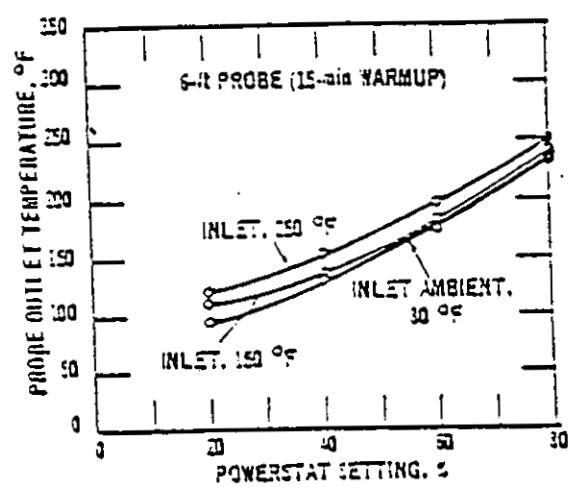
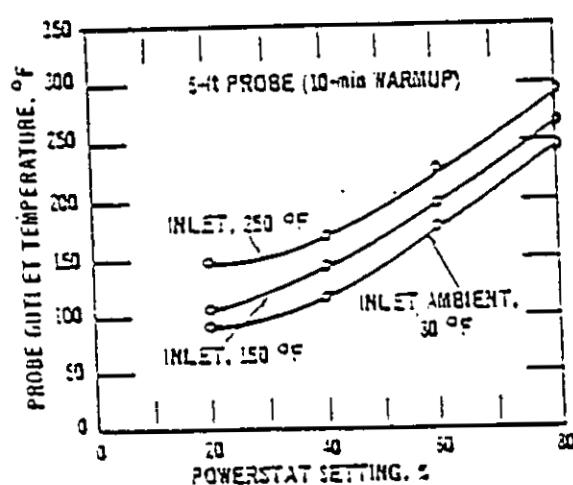
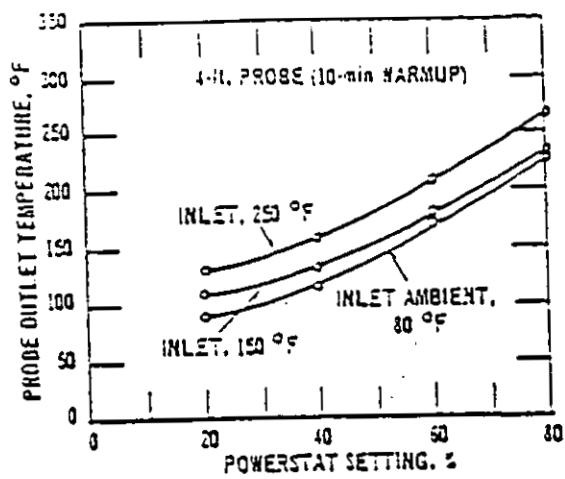
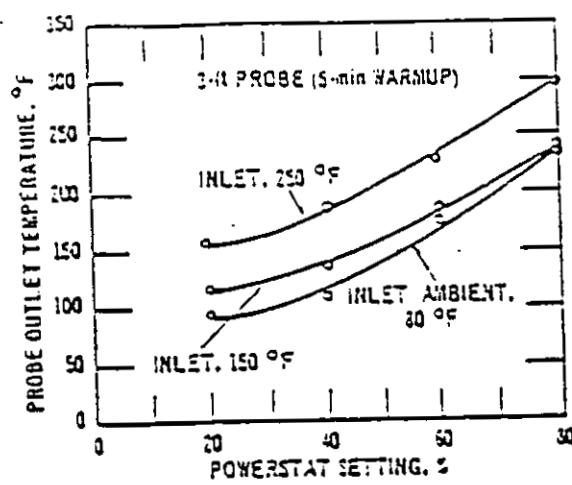
WAS CALIBRATION REQUIRED NO

THERMOCOUPLE CALIBRATION

SOURCE (SPECIFY)	ASTM GLASS THERMOMETER WITH MERCURY (°F)	PYROMETER (°F)	DEGREE DIFFERENCE	PERCENT DIFFERENCE
ICE BATH	<u>44</u>	<u>45</u>	<u>1</u>	<u>0.19</u>
AMBIENT	<u>77</u>	<u>78</u>	<u>1</u>	<u>0.19</u>
HOT OVEN	<u>345</u>	<u>346</u>	<u>1</u>	<u>0.19</u>

FOER - MAXIMUM 0° DIFFERENCE
CALIBRATED BY: _____

$$\text{EPA} \left[\frac{(\text{REF. TEMP. } ^\circ\text{F} + 460^\circ) - (\text{PYROMETER TEMP. } ^\circ\text{F} + 460^\circ)}{\text{REF. TEMP. } ^\circ\text{F} + 460^\circ} \right] 100 \leq 1.5\%$$



NOTE: Flow rate held constant at 0.75; 50% change in flow rate has little effect on probe temperature.

Probe temperatures.

AIR CONSULTING AND ENGINEERING, Inc.

SAMPLE RECOVERY AND CHAIN OF CUSTODY

PLANT NAME Sugar Grower's WOP TEST DATE 11-21-91
SOURCE NAME Boiler #3 SAMPLE RECOVERED BY Gerard
TYPE OF SAMPLE Pm PARTICULATE ANALYSES BY Christy

SAMPLE RECOVERY

SILICA GEI

RUN NO.	CONTAINER NO.	FINAL WT. (g)	INIT. WT. (g)	NET WT. (g)	COLOR
1	20	209.2	200.0	9.2	Pink
2	18	207.2	200.0	7.2	Pink
3	47	206.0	200.0	.60	Pink
			200.0		
			200.0		
			200.0		
			200.0		
			200.0		

APPENDIX F
PROJECT PARTICIPANTS

PROJECT PARTICIPANTS
AIR CONSULTING AND ENGINEERING, INC.

Stephen L. Neck, P.E.
Project Manager

Gerard Gauthreaux
Field Testing

Early McFarland
Field Testing

Christy Neck
Laboratory Analysis

Dagmar Neck
Report Preparation

Candace V. Taylor
Document Production

SUGAR CANE GROWERS

Jose Alvarez
Test Coordinator

Blas Marin
Test Coordinator

FDER

Ken Tucker
Test Observer

Sterling Jordan
Test Observer

PALM BEACH COUNTY

Jeffrey K. Koerner
Test Observer

David Brown
Test Observer