

MICROMETALLICS CORPORATION  
1695 MONTEREY HIGHWAY  
SAN JOSE, CA 95112  
ATTENTION: MR. JIM QUINTAL

Reference: TMA/Norcal C.N. 5328-2,3

March 22-24, 1988

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**TMA**  
**Thermo Analytical Inc.**

**TMA/Norcal**

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April 27, 1988

Micrometallics Corporation  
1695 Monterey Highway  
San Jose, CA 95112

Attention: Mr. Jim Quintal

Subject: Sampling and analysis of three units (Ball Mill, Shredder, Incinerator) for particulate, beryllium, silver, gold, lead, copper and chrome. The incinerator unit was also tested for nonmethane organic hydrocarbons.

Sampling Date: March 22-24, 1988.

Sampling Location: Micrometallics Corporation, 1695 Monterey Highway, San Jose, CA 95112.

Sampling Personnel: Guy Worthington and Juan Rios of TMA/Norcal.

Sampling Procedures: Sampling methods are described in the California Air Resources Board's Stationary Source Test Methods, Volume I & III.

|            |                                   |
|------------|-----------------------------------|
| Method 1   | Sample and Velocity Traverse      |
| Method 2   | Velocity and Volumetric Flow Rate |
| Method 4   | Moisture Content                  |
| Method 5   | Particulate Matter Emissions      |
| Method 12  | Inorganic Lead Emissions          |
| Method 104 | Beryllium                         |
| Method 425 | Total Chromium                    |
| Method 100 | Continuous Sampling               |

Monitoring Equipment: The following continuous monitoring equipment was used:

Carbon Dioxide and Carbon Monoxide (Infrared Industries Model 7752/7020; CO/CO<sub>2</sub> NDIR)

Oxygen (TAI Series 326A)

Ratfish 55S Hydrocarbon Analyzer

Comments: The incinerator unit had no meter that would monitor the gas flow rate. However, since the material burned contained almost no carbon, it was assumed that the CO<sub>2</sub> content was due to the burning gas. This method of 2-

Micrometallics Corporation

April 27, 1988

correction was used after consulting with Tim Underwood of the Bay Area Air Management District. Therefore, the 12% CO<sub>2</sub> correction factor was calculated based on the following formula:

$$\text{Correction factor} = \frac{(12/100) (Q_o - 10.24Q_g)}{(Q_o)(\text{CO}_2\%/100) - 1.11Q_g}$$

Q<sub>o</sub> - Dry Stack Flow Rate, SDCFM

Q<sub>g</sub> - Natural Gas Flow Rate, SCFM

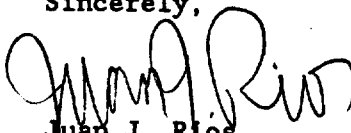
CO<sub>2</sub> - % CO<sub>2</sub> in Stack

$$\text{New correction factor} = \frac{(12/100)(Q_o)}{(Q_o)(\text{CO}_2\%/100)}$$

The gold analyses has been delayed by the laboratory but the results will be sent under an addendum to the report.

If you have any questions, please do not hesitate to call.

Sincerely,

  
Juan J. Rios  
Technical Director  
Air Source Testing

JJR/aer

TABLE I

CLIENT: MICROMETALLICS  
 UNIT: BALL MILL  
 DATE TESTED: MARCH 22, 1988

| TEST                           | 1                    | 2                    | 3                    |
|--------------------------------|----------------------|----------------------|----------------------|
| Time of Test                   | 1127-1230            | 1247-1408            | 1524-1627            |
| Stack Temperature, °F          | 87                   | 90                   | 91                   |
| Volume Flow, SDCFM             | 8852                 | 9417                 | 9250                 |
| Sampled Volume, SDCF           | 43.7                 | 43.0                 | 42.8                 |
| Oxygen, Vol % (dry)            | 21.0                 | 21.0                 | 21.0                 |
| Carbon Dioxide, Vol % (dry)    | 0.0                  | 0.0                  | 0.0                  |
| Particulate Wt., grams         | 0.0008               | 0.0034               | 0.0093               |
| Particulate Conc., grains/SDCF | 0.0003               | 0.0012               | 0.0034               |
| Particulate Emissions, lbs/hr  | 0.02                 | 0.1                  | 0.3                  |
| Isokinetic Sampling, %         | 109                  | 101                  | 102                  |
| Beryllium Wt., grams           | ND                   | ND                   | ND                   |
| Beryllium Conc., grains/SDCF   | ND                   | ND                   | ND                   |
| Beryllium Emissions, lb/hr     | ND                   | ND                   | ND                   |
| Chromium Wt., grams            | $5.1 \times 10^{-6}$ | $5.1 \times 10^{-6}$ | $7.2 \times 10^{-6}$ |
| Chromium Conc., grains/SDCF    | $1.8 \times 10^{-6}$ | $1.8 \times 10^{-6}$ | $2.6 \times 10^{-6}$ |
| Chromium Emissions, lbs/hr     | $1.4 \times 10^{-4}$ | $1.5 \times 10^{-4}$ | $2.0 \times 10^{-4}$ |
| Copper Wt., grams              | $4.8 \times 10^{-5}$ | $2.1 \times 10^{-4}$ | $2.5 \times 10^{-4}$ |
| Copper Conc., grains/SDCF      | $1.7 \times 10^{-5}$ | $0.8 \times 10^{-4}$ | $0.9 \times 10^{-4}$ |
| Copper Emissions, lbs/hr       | $1.3 \times 10^{-3}$ | $6.5 \times 10^{-3}$ | $7.1 \times 10^{-3}$ |
| Lead Wt., grams                | $3.9 \times 10^{-5}$ | $1.2 \times 10^{-4}$ | $1.9 \times 10^{-4}$ |
| Lead Conc., grains/SDCF        | $1.4 \times 10^{-5}$ | $0.4 \times 10^{-4}$ | $0.7 \times 10^{-4}$ |
| Lead Emissions, lbs/hr         | $1.1 \times 10^{-3}$ | $3.2 \times 10^{-3}$ | $5.6 \times 10^{-3}$ |
| Nickel Wt., grams              | $3.4 \times 10^{-6}$ | $6.3 \times 10^{-6}$ | $1.6 \times 10^{-6}$ |
| Nickel Conc., grains/SDCF      | $1.2 \times 10^{-6}$ | $2.3 \times 10^{-6}$ | $0.6 \times 10^{-6}$ |
| Nickel Emissions, lbs/hr       | $9.1 \times 10^{-5}$ | $1.9 \times 10^{-4}$ | $4.8 \times 10^{-5}$ |
| Silver Wt., grams              | $1.0 \times 10^{-6}$ | $1.0 \times 10^{-6}$ | $5.8 \times 10^{-6}$ |
| Silver Conc., grains/SDCF      | $0.4 \times 10^{-6}$ | $0.4 \times 10^{-6}$ | $2.1 \times 10^{-6}$ |
| Silver Emissions, lbs/hr       | $3.0 \times 10^{-5}$ | $3.2 \times 10^{-5}$ | $1.7 \times 10^{-4}$ |

All weights are filter plus impinger catches except for particulate which is filter and probe wash.

TABLE II

CLIENT: MICROMETALLICS  
 UNIT: SHREDDER  
 DATE TESTED: MARCH 23, 1988

| TEST                           | 1                    | 2                    | 3                    |
|--------------------------------|----------------------|----------------------|----------------------|
| Time of Test                   | 1147-1252            | 1445-1550            | 1605-1710            |
| Stack Temperature, °F          | 91                   | 96                   | 94                   |
| Volume Flow, SDCFM             | 6367                 | 8083                 | 6952                 |
| Sampled Volume, SDCF           | 42.4                 | 53.7                 | 46.2                 |
| Oxygen, Vol % (dry)            | 21.0                 | 21.0                 | 21.0                 |
| Carbon Dioxide, Vol % (dry)    | 0.0                  | 0.0                  | 0.0                  |
| Particulate Wt., grams         | 0.0004               | 0.0007               | 0.0009               |
| Particulate Conc., grains/SDCF | 0.0001               | 0.0002               | 0.0003               |
| Particulate Emissions, lbs/hr  | 0.01                 | 0.01                 | 0.02                 |
| Isokinetic Sampling, %         | 101                  | 101                  | 101                  |
| Beryllium Wt., grams           | ND                   | ND                   | ND                   |
| Beryllium Conc., grains/SDCF   | ND                   | ND                   | ND                   |
| Beryllium Emissions, lb/hr     | ND                   | ND                   | ND                   |
| Chromium Wt, grams             | $8.9 \times 10^{-5}$ | $7.9 \times 10^{-6}$ | $4.0 \times 10^{-6}$ |
| Chromium Conc., grains/SDCF    | $3.2 \times 10^{-5}$ | $2.3 \times 10^{-6}$ | $1.3 \times 10^{-6}$ |
| Chromium Emissions, lbs/hr     | $1.7 \times 10^{-3}$ | $1.6 \times 10^{-4}$ | $7.7 \times 10^{-5}$ |
| Copper Wt., grams              | $2.0 \times 10^{-4}$ | $4.0 \times 10^{-5}$ | $3.1 \times 10^{-5}$ |
| Copper Conc., grains/SDCF      | $0.7 \times 10^{-4}$ | $0.2 \times 10^{-5}$ | $1.0 \times 10^{-5}$ |
| Copper Emissions, lbs/hr       | $3.8 \times 10^{-3}$ | $1.4 \times 10^{-4}$ | $6.0 \times 10^{-4}$ |
| Lead Wt., grams                | $7.2 \times 10^{-5}$ | $7.1 \times 10^{-5}$ | $3.7 \times 10^{-5}$ |
| Lead Conc., grains/SDCF        | $2.6 \times 10^{-5}$ | $2.0 \times 10^{-5}$ | $1.2 \times 10^{-5}$ |
| Lead Emissions, lbs/hr         | $1.4 \times 10^{-3}$ | $1.4 \times 10^{-3}$ | $7.2 \times 10^{-4}$ |
| Nickel Wt., grams              | $1.7 \times 10^{-4}$ | $1.2 \times 10^{-6}$ | ND                   |
| Nickel Conc., grains/SDCF      | $0.6 \times 10^{-4}$ | $0.3 \times 10^{-6}$ | ND                   |
| Nickel Emissions, lbs/hr       | $3.3 \times 10^{-3}$ | $2.1 \times 10^{-5}$ | ND                   |
| Silver Wt., grams              | $0.6 \times 10^{-6}$ | $1.3 \times 10^{-6}$ | $0.8 \times 10^{-6}$ |
| Silver Conc., grains/SDCF      | $0.2 \times 10^{-6}$ | $0.4 \times 10^{-6}$ | $0.3 \times 10^{-6}$ |
| Silver Emissions, lbs/hr       | $1.1 \times 10^{-5}$ | $2.8 \times 10^{-5}$ | $1.8 \times 10^{-5}$ |

All weights are filter plus impinger catches except for particulate which is filter and probe wash.

TABLE III

CLIENT: MICROMETALLICS  
 UNIT: INCINERATOR  
 DATE TESTED: MARCH 24, 1988

| TEST                                              | 1                    | 2                    | 3                    | 4                    |
|---------------------------------------------------|----------------------|----------------------|----------------------|----------------------|
|                                                   | PC BOARDS            |                      | SLUDGE               |                      |
| Time of Test                                      | 1150-1304            | 1342-1449            | 1530-1640            | 1705-1809            |
| Stack Temperature, °F                             | 657                  | 629                  | 597                  | 586                  |
| Volume Flow, SDCFM                                | 4337                 | 4296                 | 4320                 | 4402                 |
| Sampled Volume, SDCF                              | 30.2                 | 29.5                 | 33.2                 | 34.1                 |
| Water Vapor, vol %                                | 3.8                  | 4.0                  | 3.8                  | 3.5                  |
| Oxygen, Vol % (dry)                               | 17.3                 | 17.8                 | 18.1                 | 18.4                 |
| Carbon Dioxide, Vol % (dry)                       | 1.8                  | 1.5                  | 1.5                  | 1.4                  |
| Particulate Wt., grams                            | 0.0718               | 0.0621               | 0.0075               | 0.0090               |
| Particulate Conc., grains/SDCF                    | 0.0367               | 0.0325               | 0.0035               | 0.0041               |
| Particulate Emissions, lbs/hr                     | 1.36                 | 1.20                 | 0.13                 | 0.15                 |
| Isokinetic Sampling, %                            | 93                   | 91                   | 102                  | 103                  |
| Grains/SDCF, Corrected*                           | 0.2447               | 0.2600               | 0.0280               | 0.0351               |
| Auxillary Fuel Usage, SCFM                        | ---                  | ---                  | ---                  | ---                  |
| Material Burned, lbs                              | 34                   | 27                   | 105                  | 117                  |
| Carbon Monoxide Conc., ppm                        | 279                  | 180                  | ND                   | ND                   |
| Carbon Monoxide, lbs/hr as CO                     | 5.25                 | 3.36                 | ND                   | ND                   |
| Nonmethane Hydrocarbons, ppm as C <sub>1</sub>    | 6                    | 5                    | 2                    | 2                    |
| Nonmethane Hydrocarbons, lbs/hr as C <sub>1</sub> | $4.8 \times 10^{-2}$ | $4.0 \times 10^{-2}$ | $1.6 \times 10^{-2}$ | $1.6 \times 10^{-2}$ |
| Chromium Wt., grams                               | $3.1 \times 10^{-4}$ | $3.1 \times 10^{-4}$ | $2.5 \times 10^{-4}$ | $3.4 \times 10^{-4}$ |
| Chromium Conc., grains/SDCF                       | $1.6 \times 10^{-4}$ | $1.6 \times 10^{-4}$ | $1.2 \times 10^{-4}$ | $1.5 \times 10^{-4}$ |
| Chromium Emissions, lbs/hr                        | $5.9 \times 10^{-3}$ | $5.9 \times 10^{-3}$ | $4.4 \times 10^{-3}$ | $5.7 \times 10^{-3}$ |
| Copper Wt., grams                                 | $8.0 \times 10^{-3}$ | $8.7 \times 10^{-3}$ | $6.0 \times 10^{-4}$ | $7.8 \times 10^{-4}$ |
| Copper Conc., grains/SDCF                         | $4.1 \times 10^{-3}$ | $4.6 \times 10^{-3}$ | $2.8 \times 10^{-4}$ | $3.5 \times 10^{-4}$ |
| Copper Emissions, lbs/hr                          | 0.15                 | 0.17                 | $1.0 \times 10^{-2}$ | $1.3 \times 10^{-2}$ |
| Lead Wt., grams                                   | $9.9 \times 10^{-3}$ | $1.0 \times 10^{-2}$ | $1.3 \times 10^{-3}$ | $1.7 \times 10^{-3}$ |
| Lead Conc., grains/SDCF                           | $5.1 \times 10^{-3}$ | $5.2 \times 10^{-3}$ | $0.6 \times 10^{-3}$ | $0.8 \times 10^{-3}$ |
| Lead Emissions, lbs/hr                            | 0.19                 | 0.19                 | $2.2 \times 10^{-2}$ | $3.0 \times 10^{-2}$ |
| Nickel Wt., grams                                 | $1.3 \times 10^{-4}$ | $1.2 \times 10^{-4}$ | $8.2 \times 10^{-5}$ | $1.3 \times 10^{-4}$ |
| Nickel Conc., grains/SDCF                         | $0.7 \times 10^{-4}$ | $0.6 \times 10^{-4}$ | $3.8 \times 10^{-5}$ | $5.9 \times 10^{-5}$ |
| Nickel Emissions, lbs/hr                          | $2.6 \times 10^{-3}$ | $2.2 \times 10^{-3}$ | $1.4 \times 10^{-3}$ | $2.2 \times 10^{-3}$ |
| Silver Wt., grams                                 | $1.7 \times 10^{-5}$ | $1.7 \times 10^{-5}$ | $2.0 \times 10^{-5}$ | $1.0 \times 10^{-5}$ |
| Silver Conc., grains/SDCF                         | $0.9 \times 10^{-5}$ | $0.9 \times 10^{-5}$ | $0.9 \times 10^{-5}$ | $0.5 \times 10^{-5}$ |
| Silver Emissions, lbs/hr                          | $3.3 \times 10^{-4}$ | $3.3 \times 10^{-4}$ | $3.3 \times 10^{-4}$ | $1.9 \times 10^{-4}$ |

Footnotes on the next page.

## Table III (cont'd)

## Footnotes:

All weights are filter plus impinger catches except for particulate which is filter and probe wash.

\*Particulate concentration corrected to 12% CO<sub>2</sub>. Since there was no meter to measure Auxiliary Flow Rate, the correction was made by assuming that all CO<sub>2</sub> was a result of the auxiliary fuel.

Tests 1 & 2 Burned Printed Circuit Boards.

Tests 3 & 4 Burned Sludge.

APPENDIX I  
FLOW AND PARTICULATE CALCULATIONS

# THERMO ANALYTICAL

Client : INCINERATER

Date Tested : 3/24/88

Test No. : 1

Time : 1150

## GAS FLOW DATA

Sample Points 123456789

Barometric Pressure 30.2

Sample Nozzle Area .000759 ft<sup>2</sup>

Duct Pressure 30.2 "Hg

Condensate 25 ml.

Avg. Gas Meter Pressure 0 in.Hg

Vol. of Gas Samples 30.95 CF

Avg Gas Meter Temp 88 F

Avg Duct Temp 657 F

Wgt. Collected .0718 Gms.

Duration of Test 63 Min.

Avg. Velocity at Sampling Pts 24.6 ft/sec.

## Calculations

Condensed Water Vapor:

$$vw = 0.00267 * 25 * (460 + 70) / 29.92 = 1.18 \text{ SCF}$$

Corrected Meter Volume:

$$Vo = 30.95 * 30.2 / 29.92 * 530 / 548 = 30.21 \text{ SDCF}$$

Percent Water Vapor:

$$\% \text{ H}_2\text{O} = 1.18 / 31.4 * 100 = 3.8 \%$$

Particulate Concentration (Grain Loading):

$$Go = ( .0718 \text{ Gms.} * 15.43 ) / 30.21 \text{ SDCF} = .0367 \text{ Grs/SDCF}$$

Particulate Emission Rate:

$$( .0367 \text{ Grs/SDCF} * 4337 \text{ SDCFM} * 60 ) / 7000 = 1.36 \text{ Lbs/Hr.}$$

Percentage of Isokinetic Sampling Attained: %I = 93 %

# THERMO ANALYTICAL

Client : INCINERATER

Date Tested : 3/24/88

Test No. : 1

Time : 1150

## Gas Flow Rate Data

| Point | h   | T.  | Vel. Ft/Sec |
|-------|-----|-----|-------------|
| 1     | .09 | 605 | 23.9        |
| 2     | .07 | 643 | 21.4        |
| 3     | .08 | 650 | 23          |
| 4     | .1  | 660 | 25.8        |
| 5     | .1  | 669 | 25.9        |
| 6     | .1  | 668 | 25.9        |
| 7     | .08 | 670 | 23.2        |
| 8     | .1  | 676 | 26          |
| 9     | .1  | 677 | 26          |

$$V_s = C_p [h * (T + 460)]^{.5} [1/M.W. * P_s]^{.5} * 85.49$$

Conc. of CO2 = 1.8 %

Conc. of O2 = 17.3 %

Conc. of H2O = 3.8 %

Avg. Gas Velocity;  $V_s$ , Avg. 24.6 Ft/Sec

Pitot Tube Correction Factor,  $C_p$  .84

Duct Gas Molecular Weight, M.W. 28.68

Duct Pressure,  $P_s$ . 30.2 ''Hg

Barometric Pressure 30.2 ''Hg

Duct Size Rectangle 36 '' X 25.5 '' Static Pressure -.03 ''H2O

Duct Area 6.38 Sq. Ft

Avg. Gas Temp. 657

Gas Flow Rate 24.6 Ft/Sec \* 6.38 Sq. Ft \* 60 = 9416 CFM

$$9416 \text{ CFM} * 530 / 1117 * 30.2 / 29.92 * (1.00 - 3.8 / 100\% \text{H}_2\text{O}) = 4337 \text{ SDCFM}$$

M.W. Factor = .0339

Standard Cond. Temp. 70

# THERMO ANALYTICAL

Client : INCINERATER

Date Tested : 3/24/88

Test No. : 2

Time : 1342

## Gas Flow Rate Data

| Point | h   | T.  | Vel. Ft/Sec |
|-------|-----|-----|-------------|
| 1     | .09 | 614 | 24          |
| 2     | .07 | 619 | 21.2        |
| 3     | .08 | 616 | 22.7        |
| 4     | .07 | 627 | 21.3        |
| 5     | .09 | 627 | 24.2        |
| 6     | .09 | 640 | 24.3        |
| 7     | .1  | 632 | 25.5        |
| 8     | .1  | 643 | 25.6        |
| 9     | .1  | 643 | 25.6        |

$$V_s = C_p [h * (T + 460)]^{.5} [1/M.W. * P_s]^{.5} * 85.49$$

Conc. of CO2 = 1.5 %

Conc. of O2 = 17.8 %

Conc. of H2O = 4 %

Avg. Gas Velocity;  $V_s$ , Avg. 23.8 Ft/Sec

Pitot Tube Correction Factor,  $C_p$  .84

Duct Gas Molecular Weight, M.W. 28.63

Duct Pressure,  $P_s$  30.2 ''Hg

Barometric Pressure 30.2 ''Hg

Duct Size Rectangle 36 '' X 25.5 '' Static Pressure -.03 ''H2O

Duct Area 6.38 Sq. Ft

Avg. Gas Temp. 629

Gas Flow Rate 23.8 Ft/Sec \* 6.38 Sq. Ft \* 60 = 9110 CFM

9110 CFM \* 530 / 1089 \* 30.2 / 29.92 \* (1.00 - 4 / 100% H2O) = 4296 SDCFM

M.W. Factor = .034

Standard Cond. Temp. 70

# THERMO ANALYTICAL

Client : INCINERATER

Date Tested : 3/24/88

Test No. : 2

Time : 1342

## GAS FLOW DATA

Sample Points 123456789

Barometric Pressure 30.2

Sample Nozzle Area .000759 ft<sup>2</sup>

Duct Pressure 30.2 ''Hg

Condensate 26 ml.

Avg. Gas Meter Pressure 0 in.Hg

Vol. of Gas Samples 30.24 CF

Avg Gas Meter Temp 88 F

Avg Duct Temp 629 F

Wgt. Collected .0621 Gms.

Duration of Test 63 Min.

Avg. Velocity at Sampling Pts 23.8 ft/sec.

## Calculations

Condensed Water Vapor:

$$vw = 0.00267 * 26 * (460 + 70) / 29.92 = 1.23 \text{ SCF}$$

Corrected Meter Volume:

$$Vo = 30.24 * 30.2 / 29.92 * 530 / 548 = 29.52 \text{ SDCF}$$

Percent Water Vapor:

$$\% \text{ H}_2\text{O} = 1.23 / 30.75 * 100 = 4 \%$$

Particulate Concentration (Grain Loading):

$$Go = (.0621 \text{ Gms.} * 15.43) / 29.52 \text{ SDCF} = .0325 \text{ Grs/SDCF}$$

Particulate Emission Rate:

$$(.0325 \text{ Grs/SDCF} * 4296 \text{ SDCFM} * 60) / 7000 = 1.2 \text{ Lbs/Hr.}$$

# THERMO ANALYTICAL

Client : INCINERATER

Date Tested : 3/24/88

Test No. : 3

Time : 1530

## GAS FLOW DATA

Sample Points 123456789

Barometric Pressure 30.2

Sample Nozzle Area .000759 ft<sup>2</sup>

Duct Pressure 30.2 ''Hg

Condensate 29 ml.

Avg. Gas Meter Pressure 0 in.Hg

Vol. of Gas Samples 33.83 CF

Avg Gas Meter Temp 86 F

Avg Duct Temp 597 F

Wgt. Collected .0075 Gms.

Duration of Test 63 Min.

Avg. Velocity at Sampling Pts 23.2 ft/sec.

## Calculations

Condensed Water Vapor:

$$vw = 0.00267 * 28 * (460 + 70) / 29.92 = 1.32 \text{ SCF}$$

Corrected Meter Volume:

$$Vo = 33.83 * 30.2 / 29.92 * 530 / 546 = 33.15 \text{ SDCF}$$

Percent Water Vapor:

$$\% \text{ H}_2\text{O} = 1.32 / 34.47 * 100 = 3.8 \%$$

Particulate Concentration (Grain Loading):

$$Go = (.0075 \text{ Gms.} * 15.43) / 33.15 \text{ SDCF} = .0035 \text{ Grs/SDCF}$$

Particulate Emission Rate:

$$(.0035 \text{ Grs/SDCF} * 4320 \text{ SDCFM} * 60) / 7000 = .13 \text{ Lbs/Hr.}$$

# THERMO ANALYTICAL

Client : INCINERATER

Date Tested : 3/24/88

Test No. : 3

Time : 1530

## Gas Flow Rate Data

| Point | h   | T.  | Vel. Ft/Sec |
|-------|-----|-----|-------------|
| 1     | .1  | 567 | 24.7        |
| 2     | .1  | 594 | 25.1        |
| 3     | .1  | 594 | 25.1        |
| 4     | .07 | 586 | 20.9        |
| 5     | .09 | 608 | 23.9        |
| 6     | .09 | 611 | 24          |
| 7     | .08 | 598 | 22.5        |
| 8     | .07 | 614 | 21.2        |
| 9     | .07 | 605 | 21.1        |

$$V_s = C_p [h * (T + 460)]^{.5} [1/M.W. * P_s]^{.5} * 85.49$$

Conc. of CO2 = 1.5 %

Conc. of O2 = 18.1 %

Conc. of H2O = 3.8 %

Avg. Gas Velocity;  $V_s$ , Avg. 23.2 Ft/Sec

Pitot Tube Correction Factor,  $C_p$  .84

Duct Gas Molecular Weight, M.W. 28.66

Duct Pressure,  $P_s$ . 30.2 ''Hg

Barometric Pressure 30.2 ''Hg

Duct Size Rectangle 36 '' X 25.5 '' Static Pressure -.03 ''H2O

Duct Area 6.38 Sq. Ft

Avg. Gas Temp. 597

Gas Flow Rate 23.2 Ft/Sec \* 6.38 Sq. Ft \* 60 = 8880 CFM

$8880 \text{ CFM} * 530 / 1057 * 30.2 / 29.92 * (1.00 - 3.8 / 100\% \text{H}_2\text{O}) = 4320 \text{ SDCFM}$

M.W. Factor = .0339

Standard Cond. Temp. 70

# THERMO ANALYTICAL

Client : INCINERATER

Date Tested : 3/24/88

Test No. : 4

Time : 1705

## Gas Flow Rate Data

| Point | h   | T.  | Vel. Ft/Sec |
|-------|-----|-----|-------------|
| 1     | .1  | 522 | 24.2        |
| 2     | .07 | 577 | 20.8        |
| 3     | .07 | 592 | 20.9        |
| 4     | .07 | 583 | 20.8        |
| 5     | .09 | 600 | 23.8        |
| 6     | .09 | 607 | 23.9        |
| 7     | .1  | 595 | 25.1        |
| 8     | .1  | 596 | 25.1        |
| 9     | .1  | 604 | 25.2        |

$$V_s = C_p [h * (T + 460)]^{.5} [1/M.W. * P_s]^{.5} * 85.49$$

Conc. of CO2 = 1.4 %

Conc. of O2 = 18.4 %

Conc. of H2O = 3.5 %

Avg. Gas Velocity;  $V_s$ , Avg. 23.3 Ft/Sec

Pitot Tube Correction Factor,  $C_p$  .84

Duct Gas Molecular Weight, M.W. 28.7

Duct Pressure,  $P_s$ . 30.2 ''Hg

Barometric Pressure 30.2 ''Hg

Duct Size Rectangle 36 '' X 25.5 '' Static Pressure -.03 ''H2O

Duct Area 6.38 Sq. Ft

Avg. Gas Temp. 586

Gas Flow Rate 23.3 Ft/Sec \* 6.38 Sq. Ft \* 60 = 8919 CFM

$8919 \text{ CFM} * 530 / 1046 * 30.2 / 29.92 * (1.00 - 3.5 / 100\% \text{H}_2\text{O}) = 4402 \text{ SDCFM}$

M.W. Factor = .0339

Standard Cond. Temp. 70

# THERMO ANALYTICAL

Client : INCINERATER

Date Tested : 3/24/88

Test No. : 4

Time : 1705

## GAS FLOW DATA

Sample Points 123456789

Barometric Pressure 30.2

Sample Nozzle Area .000759 ft<sup>2</sup>

Duct Pressure 30.2 ''Hg

Condensate 26 ml.

Avg. Gas Meter Pressure 0 in.Hg

Vol. of Gas Samples 34.52 CF

Avg Gas Meter Temp 81 F

Avg Duct Temp 586 F

Wgt. Collected .009 Gms.

Duration of Test 63 Min.

Avg. Velocity at Sampling Pts 23.3 ft/sec.

## Calculations

Condensed Water Vapor:

$$vw = 0.00267 * 26 * (460 + 70) / 29.92 = 1.23 \text{ SCF}$$

Corrected Meter Volume:

$$Vo = 34.52 * 30.2 / 29.92 * 530 / 541 = 34.13 \text{ SDCF}$$

Percent Water Vapor:

$$\% \text{ H}_2\text{O} = 1.23 / 35.36 * 100 = 3.5 \%$$

Particulate Concentration (Grain Loading):

$$Go = (.009 \text{ Gms.} * 15.43) / 34.13 \text{ SDCF} = .0041 \text{ Grs/SDCF}$$

Particulate Emission Rate:

$$(.0041 \text{ Grs/SDCF} * 4402 \text{ SDCFM} * 60) / 7000 = .15 \text{ Lbs/Hr.}$$

# THERMO ANALYTICAL

Client :SHREDDER

Date Tested :3/23/88

Test No.A,B,C

## -- TABULATED RESULTS --

| Test                         | A     | B     | C     |
|------------------------------|-------|-------|-------|
| Velocity,Ft/Sec (avg)        | 56.2  | 72    | 61.7  |
| Duct temp; °F                | 91    | 96    | 94    |
| Volume Flow, CFM             | 6575  | 8424  | 7218  |
| Volume Flow, SDCFM           | 6367  | 8083  | 6952  |
| Water Vapor, vol. %          | 0     | 0     | 0     |
| Oxygen, vol % (dry)          | 21    | 21    | 21    |
| Carbon Dioxide, vol. % (dry) | 0     | 0     | 0     |
| Time of Sampling             | 1147  | 11445 | 11605 |
| Duration of test; minutes    | 63    | 63    | 63    |
| Sampled Volume;SDCF          | 42.38 | 53.74 | 46.2  |
| Wt. of Sample; Grams         | .0004 | .0007 | .0009 |
| Part. Conc.; grains/SDCF     | .0001 | .0002 | .0003 |
| Particulate Emissions; Lb/hr | .01   | .01   | .02   |

# THERMO ANALYTICAL

Client : SHREDDER

Date Tested : 3/23/88

Test No. : 1

Time : 1147

## Gas Flow Rate Data

| Point | h   | T. | Vel. Ft/Sec |
|-------|-----|----|-------------|
| 1     | .83 | 91 | 52          |
| 2     | .89 | 91 | 53.8        |
| 3     | .89 | 91 | 53.8        |
| 4     | 1.1 | 91 | 59.9        |
| 5     | 1.2 | 91 | 62.5        |
| 6     | 1   | 91 | 57.1        |
| 7     | .93 | 91 | 55          |
| 8     | .97 | 91 | 56.2        |
| 9     | .95 | 91 | 55.6        |

$$V_s = C_p [h * (T + 460)]^{.5} [1/M.W. * P_s]^{.5} * 85.49$$

Conc. of CO2 = 0 %

Conc. of O2 = 21 %

Conc. of H2O = 0 %

Avg. Gas Velocity;  $V_s$ , Avg. 56.2 Ft/Sec

Pitot Tube Correction Factor,  $C_p$  .84

Duct Gas Molecular Weight, M.W. 28.96

Duct Pressure,  $P_s$ . 30.12 ''Hg      Barometric Pressure 30.1 ''Hg

Duct Size Rectangle 16.5 '' X 17 ''      Static Pressure .22 ''H2O

Duct Area 1.95 Sq. Ft      Avg. Gas Temp. 91

Gas Flow Rate 56.2 Ft/Sec \* 1.95 Sq. Ft \* 60 = 6575 CFM

$$6575 \text{ CFM} * 530 / 551 * 30.12 / 29.92 * (1.00 - 0 / 100\% \text{H}_2\text{O}) = 6347 \text{ SCFM}$$

M.W. Factor = .0338

Standard Cond. Temp. 70

# THERMO ANALYTICAL

Client : SHREDDER

Date Tested : 3/23/88

Test No. : 1

Time : 1147

## GAS FLOW DATA

Sample Points 123456789

Barometric Pressure 30.1

Sample Nozzle Area .000203 ft<sup>2</sup>

Duct Pressure 30.12 ''Hg

Condensate 0 ml.

Avg. Gas Meter Pressure .05 in.Hg

Vol. of Gas Samples 42.58 CF

Avg Gas Meter Temp 77 F

Avg Duct Temp 91 F

Wgt. Collected .0004 Gms.

Duration of Test 63 Min.

Avg. Velocity at Sampling Pts 56.2 ft/sec.

## Calculations

Condensed Water Vapor:

$$vw = 0.00267 * 0 * (460 + 70) / 29.92 = 0 \text{ SCF}$$

Corrected Meter Volume:

$$Vo = 42.58 * 30.17 / 29.92 * 530 / 537 = 42.38 \text{ SCF}$$

Percent Water Vapor:

$$\% \text{ H}_2\text{O} = 0 / 42.38 * 100 = 0 \%$$

Particulate Concentration (Grain Loading):

$$Go = ( .0004 \text{ Gms.} * 15.43 ) / 42.38 \text{ SCF} = .0001 \text{ Grs/SCF}$$

Particulate Emission Rate:

$$( .0001 \text{ Grs/SCF} * 6367 \text{ SDCFM} * 60 ) / 7000 = .01 \text{ Lbs/Hr.}$$

Percentage of Isokinetic Sampling Attained: %I = 101 %

# THERMO ANALYTICAL

Client : SHREDDER

Date Tested : 3/23/88

Test No. : 2

Time : 1445

## GAS FLOW DATA

Sample Points 123456789

Barometric Pressure 30.1

Sample Nozzle Area .000203 ft<sup>2</sup>

Duct Pressure 30.12 ''Hg

Condensate 0 ml.

Avg. Gas Meter Pressure .05 in.Hg

Vol. of Gas Samples 54.9 CF

Avg Gas Meter Temp 86 F

Avg Duct Temp 96 F

Wgt. Collected .0007 Gms.

Duration of Test 63 Min.

Avg. Velocity at Sampling Pts 72 ft/sec.

## Calculations

Condensed Water Vapor:

$$vw = 0.00267 * 0 * (460 + 70) / 29.92 = 0 \text{ SCF}$$

Corrected Meter Volume:

$$Vo = 54.9 * 30.17 / 29.92 * 530 / 546 = 53.74 \text{ SCF}$$

Percent Water Vapor:

$$\% \text{ H}_2\text{O} = 0 / 53.74 * 100 = 0 \%$$

Particulate Concentration (Grain Loading):

$$Go = (.0007 \text{ Gms.} * 15.43) / 53.74 \text{ SCF} = .0002 \text{ Grs/SCF}$$

Particulate Emission Rate:

$$(.0002 \text{ Grs/SCF} * 8083 \text{ SDCFM} * 60) / 7000 = .01 \text{ Lbs/Hr.}$$

Percentage of Isokinetic Sampling Attained: %I = 101 %

# THERMO ANALYTICAL

Client : SHREDDER

Date Tested : 3/23/88

Test No. : 2

Time : 1445

## Gas Flow Rate Data

| Point | h    | T. | Vel.Ft/Sec |
|-------|------|----|------------|
| 1     | 2.05 | 96 | 82.1       |
| 2     | 1.75 | 96 | 75.8       |
| 3     | 1.5  | 96 | 70.2       |
| 4     | 1.4  | 96 | 67.8       |
| 5     | 2.1  | 96 | 83.1       |
| 6     | 1.7  | 96 | 74.8       |
| 7     | 1.5  | 96 | 70.2       |
| 8     | 1.25 | 96 | 64.1       |
| 9     | 1.1  | 96 | 60.1       |

$$V_s = C_p [h * (T + 460)]^{.5} [1/M.W. * P_s]^{.5} * 85.49$$

Conc. of CO2 = 0 %

Conc. of O2 = 21 %

Conc. of H2O = 0 %

Avg. Gas Velocity; Vs, Avg. 72 Ft/Sec

Pitot Tube Correction Factor, Cp .84

Duct Gas Molecular Weight, M.W. 28.96

Duct Pressure, Ps. 30.12 ''Hg      Barometric Pressure 30.1 ''Hg

Duct Size Rectangle 16.5 '' X 17 ''      Static Pressure .26 ''H2O

Duct Area 1.95 Sq. Ft      Avg. Gas Temp. 96

Gas Flow Rate 72 Ft/Sec \* 1.95 Sq. Ft \* 60 = 8424 CFM

$$8424 \text{ CFM} * 530 / 556 * 30.12 / 29.92 * (1.00 - 0 / 100\% \text{H}_2\text{O}) = 8093 \text{ SCFM}$$

M.W. Factor = .0338

Standard Cond. Temp. 70

# THERMO ANALYTICAL

Client : SHREDDER

Date Tested : 3/23/88

Test No. : 3

Time : 1605

## GAS FLOW DATA

Sample Points 123456789

Barometric Pressure 30.1

Sample Nozzle Area .000203 ft<sup>2</sup>

Duct Pressure 30.12 ''Hg

Condensate 0 ml.

Avg. Gas Meter Pressure .05 in.Hg Vol. of Gas Samples 48.58 CF

Avg Gas Meter Temp 102 F

Avg Duct Temp 94 F

Wgt. Collected .0009 Gms.

Duration of Test 63 Min.

Avg. Velocity at Sampling Pts 61.7 ft/sec.

## Calculations

Condensed Water Vapor:

$$vw = 0.00267 * 0 * (460 + 70) / 29.92 = 0 \text{ SCF}$$

Corrected Meter Volume:

$$Vo = 48.58 * 30.17 / 29.92 * 530 / 562 = 46.2 \text{ SCF}$$

Percent Water Vapor:

$$\% \text{ H}_2\text{O} = 0 / 46.2 * 100 = 0 \%$$

Particulate Concentration (Grain Loading):

$$Go = ( .0009 \text{ Gms.} * 15.43 ) / 46.2 \text{ SCF} = .0003 \text{ Grs/SCF}$$

Particulate Emission Rate:

$$( .0003 \text{ Grs/SCF} * 6952 \text{ SDCFM} * 60 ) / 7000 = .02 \text{ Lbs/Hr.}$$

Percentage of Isokinetic Sampling Attained: %I = 101 %

# THERMO ANALYTICAL

Client : SHREDDER

Date Tested : 3/23/88

Test No. : 3

Time : 1605

## Gas Flow Rate Data

| Point | h    | T. | Vel. Ft/Sec |
|-------|------|----|-------------|
| 1     | 1.3  | 94 | 65.3        |
| 2     | 1.1  | 94 | 60          |
| 3     | 1.15 | 94 | 61.4        |
| 4     | 1.1  | 94 | 60          |
| 5     | 1.5  | 94 | 70.1        |
| 6     | 1.2  | 94 | 62.7        |
| 7     | 1.05 | 94 | 58.6        |
| 8     | 1.05 | 94 | 58.6        |
| 9     | 1.05 | 94 | 58.6        |

$$V_s = C_p [h * (T + 460)]^{.5} [1/M.W. * P_s]^{.5} * 85.49$$

Conc. of CO2 = 0 %

Conc. of O2 = 21 %

Conc. of H2O = 0 %

Avg. Gas Velocity;  $V_s$ , Avg. 61.7 Ft/Sec

Pitot Tube Correction Factor,  $C_p$  .84

Duct Gas Molecular Weight, M.W. 28.96

Duct Pressure,  $P_s$  30.12 ''Hg

Barometric Pressure 30.1 ''Hg

Duct Size Rectangle 16.5 '' X 17 '' Static Pressure .24 ''H2O

Duct Area 1.95 Sq. Ft

Avg. Gas Temp. 94

Gas Flow Rate 61.7 Ft/Sec \* 1.95 Sq. Ft \* 60 = 7218 CFM

$$7218 \text{ CFM} * 530 / 554 * 30.12 / 29.92 * (1.00 - 0 / 100\% \text{H}_2\text{O}) = 6952 \text{ SCFM}$$

M.W. Factor = .0338

Standard Cond. Temp. 70

# THERMO ANALYTICAL

Client : BALL MILL

Date Tested : 3/22/88

Test No. : 1

Time : 1127

## Gas Flow Rate Data

| Point | h   | T. | Vel. Ft/Sec |
|-------|-----|----|-------------|
| 1     | .68 | 87 | 46.9        |
| 2     | .68 | 87 | 46.9        |
| 3     | 1   | 87 | 56.9        |
| 4     | 1   | 87 | 56.9        |
| 5     | .8  | 87 | 50.9        |
| 6     | .6  | 87 | 44.1        |
| 7     | .8  | 87 | 50.9        |
| 8     | 1   | 87 | 56.9        |
| 9     | 1.5 | 87 | 69.7        |

$$V_s = C_p [h * (T + 460)]^{.5} [1/M.W. * P_s]^{.5} * 85.49$$

Conc. of CO2 = 0 %

Conc. of O2 = 21 %

Conc. of H2O = 0 %

Avg. Gas Velocity;  $V_s$ , Avg. 53.3 Ft/Sec

Pitot Tube Correction Factor,  $C_p$  .84

Duct Gas Molecular Weight, M.W. 28.96

Duct Pressure,  $P_s$  30.1 ''Hg

Barometric Pressure 30.1 ''Hg

Duct Size Rectangle 21.5 '' X 19 '' Static Pressure 0 ''H2O

Duct Area 2.84 Sq. Ft

Avg. Gas Temp. 87

Gas Flow Rate 53.3 Ft/Sec \* 2.84 Sq. Ft \* 60 = 9082 CFM

$$9082 \text{ CFM} * 530 / 547 * 30.1 / 29.92 * (1.00 - 0 / 100\% \text{H}_2\text{O}) = 8952 \text{ SCFM}$$

M.W. Factor = .0338

Standard Cond. Temp. 70

# THERMO ANALYTICAL

Client : BALL MILL

Date Tested : 3/22/88

Test No. : 1

Time : 1127

## GAS FLOW DATA

Sample Points 123456789

Barometric Pressure 30.1

Sample Nozzle Area .000203 ft<sup>2</sup>

Duct Pressure 30.1 ''Hg

Condensate 0 ml.

Avg. Gas Meter Pressure .05 in.Hg

Vol. of Gas Samples 45.46 CF

Avg Gas Meter Temp 96 F

Avg Duct Temp 87 F

Wgt. Collected .0008 Gms.

Duration of Test 63 Min.

Avg. Velocity at Sampling Pts 53.3 ft/sec.

## Calculations

Condensed Water Vapor:

$$vw = 0.00267 * 0 * (460 + 70) / 29.92 = 0 \text{ SCF}$$

Corrected Meter Volume:

$$Vo = 45.46 * 30.15 / 29.92 * 530 / 556 = 43.67 \text{ SCF}$$

Percent Water Vapor:

$$\% \text{ H}_2\text{O} = 0 / 43.67 * 100 = 0 \%$$

Particulate Concentration (Grain Loading):

$$Go = ( .0008 \text{ Gms.} * 15.43 ) / 43.67 \text{ SCF} = .0003 \text{ Grs/SCF}$$

Particulate Emission Rate:

$$( .0003 \text{ Grs/SCF} * 8852 \text{ SDCFM} * 60 ) / 7000 = .02 \text{ Lbs/Hr.}$$

# THERMO ANALYTICAL

Client : BALL MILL

Date Tested : 3/33/88

Test No. : 2

Time : 1247

## Gas Flow Rate Data

| Point | h    | T. | Vel. Ft/Sec |
|-------|------|----|-------------|
| 1     | 1.1  | 87 | 59.7        |
| 2     | 1.1  | 87 | 59.7        |
| 3     | 1.33 | 87 | 65.6        |
| 4     | 1    | 87 | 56.9        |
| 5     | .88  | 87 | 53.4        |
| 6     | 1    | 87 | 56.9        |
| 7     | 1.05 | 87 | 58.3        |
| 8     | .83  | 87 | 51.8        |
| 9     | .7   | 87 | 47.6        |

$$V_s = C_p [h * (T + 460)]^{.5} [1/M.W. * P_s]^{.5} * 85.49$$

Conc. of CO2 = 0 %

Conc. of O2 = 21 %

Conc. of H2O = 0 %

Avg. Gas Velocity;  $V_s$ , Avg. 56.7 Ft/Sec

Pitot Tube Correction Factor,  $C_p$  .84

Duct Gas Molecular Weight, M.W. 28.96

Duct Pressure,  $P_s$  30.1 "Hg

Barometric Pressure 30.1 "Hg

Duct Size Rectangle 21.5 "X 19 " Static Pressure 0 "H2O

Duct Area 2.84 Sq. Ft

Avg. Gas Temp. 87

Gas Flow Rate 56.7 Ft/Sec \* 2.84 Sq. Ft \* 60 = 9661 CFM

$$9661 \text{ CFM} * 530 / 547 * 30.1 / 29.92 * (1.00 - 0 / 100\% \text{H}_2\text{O}) = 9417 \text{ SCFM}$$

M.W. Factor = .0338

Standard Cond. Temp. 70

# THERMO ANALYTICAL

Client : BALL MILL

Date Tested : 3/33/88

Test No. : 2

Time : 1247

## GAS FLOW DATA

Sample Points 123456789

Barometric Pressure 30.1

Sample Nozzle Area .000203 ft<sup>2</sup>

Duct Pressure 30.1 "Hg

Condensate 0 ml.

Avg. Gas Meter Pressure .05 in.Hg

Vol. of Gas Samples 44.92 CF

Avg Gas Meter Temp 97 F

Avg Duct Temp 87 F

Wgt. Collected .0034 Gms.

Duration of Test 63 Min.

Avg. Velocity at Sampling Pts 56.7 ft/sec.

## Calculations

Condensed Water Vapor:

$$vw = 0.00267 * 0 * (460 + 70) / 29.92 = 0 \text{ SCF}$$

Corrected Meter Volume:

$$Vo = 44.82 * 30.15 / 29.92 * 530 / 557 = 42.98 \text{ SCF}$$

Percent Water Vapor:

$$\% \text{ H}_2\text{O} = 0 / 42.98 * 100 = 0 \%$$

Particulate Concentration (Grain Loading):

$$Go = ( .0034 \text{ Gms.} * 15.43 ) / 42.98 \text{ SCF} = .0012 \text{ Grs/SCF}$$

Particulate Emission Rate:

$$( .0012 \text{ Grs/SCF} * 9417 \text{ SDCFM} * 60 ) / 7000 = .1 \text{ Lbs/Hr.}$$

# THERMO ANALYTICAL

Client : BALL MILL

Date Tested : 3/22/88

Test No. : 3

Time : 1524

## Gas Flow Rate Data

| Point | h   | T. | Vel. Ft/Sec |
|-------|-----|----|-------------|
| 1     | 1.1 | 91 | 59.9        |
| 2     | .9  | 91 | 54.2        |
| 3     | .75 | 91 | 49.4        |
| 4     | .75 | 91 | 49.4        |
| 5     | .82 | 91 | 51.7        |
| 6     | .7  | 91 | 47.8        |
| 7     | 1   | 91 | 57.1        |
| 8     | 1.3 | 91 | 65.1        |
| 9     | 1.5 | 91 | 69.9        |

$$V_s = C_p [h * (T + 460)]^{.5} [1/M.W. * P_s]^{.5} * 85.49$$

Conc. of CO2 = 0 %

Conc. of O2 = 21 %

Conc. of H2O = 0 %

Avg. Gas Velocity;  $V_s$ , Avg. 56.1 Ft/Sec

Pitot Tube Correction Factor,  $C_p$  .84

Duct Gas Molecular Weight, M.W. 28.96

Duct Pressure,  $P_s$ . 30.1 ''Hg

Barometric Pressure 30.1 ''Hg

Duct Size Rectangle 21.5 '' X 19 '' Static Pressure 0 ''H2O

Duct Area 2.84 Sq. Ft

Avg. Gas Temp. 91

Gas Flow Rate 56.1 Ft/Sec \* 2.84 Sq. Ft \* 60 = 9559 CFM

$$9559 \text{ CFM} * 530 / 551 * 30.1 / 29.92 * (1.00 - 0 / 100\% \text{H}_2\text{O}) = 9250 \text{ SCFM}$$

M.W. Factor = .0338

Standard Cond. Temp. 70

# THERMO ANALYTICAL

Client : BALL MILL

Date Tested : 3/22/88

Test No. : 3

Time : 1524

## GAS FLOW DATA

Sample Points 123456789

Barometric Pressure 30.1

Sample Nozzle Area .000203 ft<sup>2</sup>

Duct Pressure 30.1 ''Hg

Condensate 0 ml.

Avg. Gas Meter Pressure .05 in.Hg

Vol. of Gas Samples 44.05 CF

Avg Gas Meter Temp 90 F

Avg Duct Temp 91 F

Wgt. Collected .0093 Gms.

Duration of Test 63 Min.

Avg. Velocity at Sampling Pts 56.1 ft/sec.

## Calculations

Condensed Water Vapor:

$$vw = 0.00267 * 0 * (460 + 70) / 29.92 = 0 \text{ SCF}$$

Corrected Meter Volume:

$$Vo = 44.05 * 30.15 / 29.92 * 530 / 550 = 42.77 \text{ SCF}$$

Percent Water Vapor:

$$\% \text{ H}_2\text{O} = 0 / 42.77 * 100 = 0 \%$$

Particulate Concentration (Grain Loading):

$$Go = ( .0093 \text{ Gms.} * 15.43 ) / 42.77 \text{ SCF} = .0034 \text{ Grs/SCF}$$

Particulate Emission Rate:

$$( .0034 \text{ Grs/SCF} * 9250 \text{ SDCFM} * 60 ) / 7000 = .27 \text{ Lbs/Hr.}$$

APPENDIX II  
FIELD DATA SHEETS





THERMO-ANALYTICAL NORCAL CO.  
 AIR POLLUTION ANALYSIS

DATE: 7-22-88  
 PLANT: MICROMET  
 SAMPLE TYPE: Particulates  
 DUCT LOCATION: BALL MILL  
 DUCT DIAM: 21 1/2 x 19  
 FITTING SIZE:  
 WALL THICKNESS:  
 DUCT STATIC PRESS:

Source Test Field Data Sheet  
 FILTER # 4  
 Test Number 3

THIMBLE NO.  
 NOZZLE DIAM  
 NOZZLE TYPE  
 GAS COLLECTOR  
 METER NO.  
 BAROMETRIC PRESS.  
 DRAFT GAGE  
 TRAVERSE PITOT TUBE  
 MONITORING PITOT TUBE  
 CONDENSATE

-1nd

| PITOT TRAVERSE |               |          |              | PITOT MONITOR |           |              | SAMPLING |      |       |                |               |                  |         | REMARKS     |           |                     |
|----------------|---------------|----------|--------------|---------------|-----------|--------------|----------|------|-------|----------------|---------------|------------------|---------|-------------|-----------|---------------------|
| Point          | In from Cent. | Time:    |              | Val FPS       | No. 11120 | Duct Temp °F | Val FPS  | Time | Point | Water Rate CFM | Water Temp °F | Water Press 111g | Vol Ft³ | Orif. Sett. | Pump Vac. |                     |
|                |               | Δh 11120 | Duct Temp °F |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               | 1.0       | 91           | 61.0     | 1524 | 1     | .75            | 90            | 0.05             | 907.53  | 1.540       | 5         | Pre test Leak chkl  |
|                |               |          |              |               | 0.9       | 91           | 59.2     | 1531 | 2     | .68            | 90            |                  | 912.7   | 1.31        | 4         | at 6" Hg            |
|                |               |          |              |               | 0.8       | 91           | 50.4     | 1538 | 3     | .62            | 90            |                  | 917.8   | 1.09        | 3         | 20.005 CFM          |
|                |               |          |              |               | 0.75      | 91           | 50.4     | 1545 | 1     | .62            | 90            |                  | 921.9   | 1.09        | 3         |                     |
|                |               |          |              |               | 0.82      | 91           | 52.7     | 1552 | 2     | .65            | 90            |                  | 925.8   | 1.19        | 6         | 19.9 m/s            |
|                |               |          |              |               | 0.7       | 91           | 48.7     | 1559 | 3     | .59            | 90            |                  | 930.4   | 1.01        | 4         |                     |
|                |               |          |              |               | 1.0       | 91           | 56.2     | 1606 | 1     | .71            | 90            |                  | 934.6   | 1.45        | 8         |                     |
|                |               |          |              |               | 1.3       | 91           | 60.3     | 1613 | 2     | .81            | 90            |                  | 939.6   | 1.89        | 5         |                     |
|                |               |          |              |               | 1.5       | 91           | 71.3     | 1620 | 3     | .87            | 90            |                  | 945.1   | 2.18        | 5         | Post test Leak chkl |
|                |               |          |              |               |           |              |          | 1627 |       |                |               |                  | 951.58  |             |           | at 10" Hg           |
|                |               |          |              |               |           |              |          |      |       |                |               |                  | 944.05  |             |           | 20.02 CFM           |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              |          |      |       |                |               |                  |         |             |           |                     |
|                |               |          |              |               |           |              | </       |      |       |                |               |                  |         |             |           |                     |

Gas sampling time: 63 mins.  
 Start:

Team members: JFW LJR

3350  
 50%  
 16.6%  
 0.15  
 2.74  
 16 1/2

DATE: 3-23-88  
 PLANT: MICROMET.  
 SAMPLE TYPE: Partic + metals  
 DUCT LOCATION: SHREDDER  
 DUCT DIAM: 24" x 16 1/2 x 17  
 FITTING SIZE:  
 WALL THICKNESS:  
 DUCT STATIC PRESS: + 0.22  
 THERMO-ANALYTICAL HORCAL CO.  
 AIR POLLUTION ANALYSIS  
 Source Test Field Data Sheet  
 FILTER # 5  
 Test Number  
 THIMBLE NO. 100203  
 NOZZLE TYPE 2140  
 GAS COLLECTOR 20.00  
 METER NO. Red Max  
 BAROMETRIC PRESS. 241.571  
 DRAFT GAGE 0.84  
 TRAVERSE PITOT TUBE  
 MONITORING PITOT TUBE  
 CONDENSATE  
 IMPIINGER VOLUME: 210ml

| PITOT TRAVERSE |               |           |         | PITOT MONITOR |         |          | SAMPLING     |         |      |       |                |               |                 | REMARKS |                     |                   |
|----------------|---------------|-----------|---------|---------------|---------|----------|--------------|---------|------|-------|----------------|---------------|-----------------|---------|---------------------|-------------------|
| Point          | In from Cent. | Time: 136 |         | Duct Temp °F  | Vel FPS | Ah "1120 | Duct Temp °F | Vel FPS | Time | Point | Water Rate CFM | Water Temp °F | Water Press "Hg |         | Vol Ft <sup>3</sup> | Orif. Sett.       |
|                |               | Ah "1120  | Vel FPS |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               | 0.7       | 91      |               |         | 0.83     | 91           | 53.0    | 1    | 1.62  | 70             | .05           | 954.85          | 1.14    | 7                   | Pre test leak chk |
|                |               | 0.75      |         |               |         | 0.89     | 91           | 54.9    | 2    | 1.63  | 76             | .05           | 959.18          | 1.24    | 8                   | 20.02 CFM         |
|                |               | 0.75      |         |               |         | 0.89     | 91           | 54.9    | 3    | 1.65  | 76             | .05           | 963.69          | 1.24    | 8                   |                   |
|                |               | 0.92      |         |               |         | 1.10     | 91           | 61.0    | 1    | 1.72  | 77             | .05           | 968.2           | 1.54    | 10                  |                   |
|                |               | 1.0       |         |               |         | 1.20     | 91           | 63.7    | 2    | 1.78  | 77             | .05           | 973.2           | 1.68    | 11                  | Pre test leak chk |
|                |               | 0.84      |         |               |         | 1.0      | 91           | 58.2    | 3    | 1.69  | 78             | .05           | 978.5           | 1.90    | 9                   |                   |
|                |               | 0.78      | ✓       |               |         | 0.93     | 91           | 56.1    | 1    | 1.67  | 79             | .05           | 983.3           | 1.31    | 9                   |                   |
|                |               | 0.82      | ✓       |               |         | 0.97     | 91           | 57.3    | 2    | 1.68  | 79             | .05           | 988.0           | 1.36    | 9                   |                   |
|                |               | 0.80      |         |               |         | 0.95     | 91           | 56.7    | 2    | 1.67  | 79             | .05           | 992.7           | 1.33    | 9                   |                   |
|                |               |           |         |               |         |          |              | 51.0    | 2    | 1.67  | 79             | .05           | 997.4           | 1.33    | 9                   | Pre test leak chk |
|                |               |           |         |               |         |          |              |         |      |       |                |               | 42.575          |         |                     | at 12.5 Hg        |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     | 20.02 CFM         |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      |       |                |               |                 |         |                     |                   |
|                |               |           |         |               |         |          |              |         |      | </    |                |               |                 |         |                     |                   |

Team members: GWT + JR

Gas sampling time: 63 mins.

Team members: BW + JR

THE B40-ANALYTICAL NORCAL CO.

PLANT: Micromet.

## AIR POLLUTION ANALYSIS

**SAMPLE TYPE:**

**DUCT LOCATION:**

# Source Test Field Data Sheet

**DUCT DIAM:**

**FITTING SIZE:**

## WALL THICKNESS:

DUCT STATIC PRESS: + 0.24.

**TIME NO.**

**NOZZLE DIAM**

**NOZZLE TYPE**

# CAS COLLECTOR

METER NO.

**BAROMETRIC PRESS.**

**DRAFT CAGE**

## TRAVERSE PITOT TUBE

## MONITORING

## CONDENSATE

[illegible]

**Gas sampling time:**

## Team members:

6211R

0.194 lbs  
OUT 110 lbs #1 paint all way in

DATE: 3-24-88

THERMO-ANALYTICAL NORCAL CO.

PLANT: Micro Metallics Inc. AIR POLLUTION ANALYSIS

SAMPLE TYPE: Particulate, Metals

DUCT LOCATION: Outlet Incinerator

DUCT DIAH: 36 x 25.5"

FITTING SIZE: 10"

WALL THICKNESS:

DUCT STATIC PRESS: -0.3

THIMBLE NO. 2373  
NOZZLE DIAM 2.0  
NOZZLE TYPE AREA 0.000758  
GAS COLLECTOR  
METER NO. 30.2  
BAROMETRIC PRESS. Standard  
DRAFT GAGE Standard  
TRAVERSE PITOT TUBE 84  
MONITORING-PITOT TUBE 84  
CONDENSATE 12372

Source Test Field Data Sheet

Filter #8  
Test Number

V01-223m

| PITOT TRAVERSE |               |       |   |         | PITOT MONITOR     |              |         | SAMPLING |       |                |               |                               |                     |             | REMARKS   |               |
|----------------|---------------|-------|---|---------|-------------------|--------------|---------|----------|-------|----------------|---------------|-------------------------------|---------------------|-------------|-----------|---------------|
| Point          | In from Cent. | Time: |   | Vel FPS | NH <sub>3</sub> % | Duct Temp °F | Vel FPS | Time     | Point | Meter Rate CFM | Water Temp °F | Meter Press "H <sub>2</sub> O | Vol Ft <sup>3</sup> | Orif. Sett. | Pump Vac. |               |
|                |               | h     | m |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 1-1            |               | 09    |   | →       | 0.08              | 605          | 24.55   | 0        | 1     | 1.48           | 78            | 0                             | 104.585             | .73         | 10"       | 0.10 leak     |
| 2-2            |               |       |   | →       | 0.07              | 643          | 24.6    | 7        | 2     | 1.44           | 82            |                               | 106.12              | .57         | 10"       | stop          |
| 3-3            |               |       |   | →       | 0.08              | 650          | 23.15   | 14       | 3     | 1.47           | 86            |                               | 111.07              | .65         | 11"       |               |
| 4-4            |               |       |   | →       |                   |              |         | 21       |       |                |               |                               | 114.265             |             |           | stop          |
| 5-5            |               |       |   | →       | 0.10              | 660          | 25.88   | 0        | 1     | 1.53           | 84            |                               | 114.265             | .81         | 12"       | START         |
| 6-6            |               |       |   | →       | 0.10              | 669          | 25.88   | 7        | 2     | 1.53           | 89            |                               | 117.87              | .81         | 11"       |               |
| 7-7            |               |       |   | →       | 0.10              | 668          | 25.88   | 14       | 3     | 1.53           | 90            |                               | 121.60              | .81         | 11"       |               |
| 8-8            |               |       |   | →       |                   |              |         | 21       |       |                |               |                               | 125.04              |             |           | stop          |
| 9-9            |               |       |   | →       | 0.08              | 670          | 23.15   | 0        | 1     | 1.47           | 86            |                               | 125.04              | .65         | 12"       | START         |
| 10-10          |               |       |   | →       | 0.10              | 676          | 25.88   | 7        | 2     | 1.53           | 87            |                               | 128.26              | .81         | 12"       |               |
| 11-11          |               |       |   | →       | 0.10              | 677          | 25.88   | 14       | 3     | 1.53           | 87            |                               | 131.86              | .81         | 13"       |               |
| 12-12          |               |       |   | →       |                   |              |         | 21       |       |                |               |                               | 135.46              |             |           | stop 11:44 PM |
| 13-13          |               |       |   |         |                   |              |         |          |       |                |               |                               | 151.12              |             |           |               |
| 14-14          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 15-15          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 16-16          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 17-17          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 18-18          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 19-19          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 20-20          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 21-21          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 22-22          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 23-23          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 24-24          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 25-25          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 26-26          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 27-27          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 28-28          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 29-29          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |
| 30-30          |               |       |   |         |                   |              |         |          |       |                |               |                               |                     |             |           |               |

Gas sampling time:

Team members: CTR

**DUCT STATIC PRESS: -0.3**

2-284 mL

$$\begin{array}{r} 187 \\ 24 \overline{) 5472} \\ \underline{48} \phantom{00} \\ 67 \phantom{00} \\ \underline{48} \phantom{00} \\ 197 \phantom{00} \\ \underline{192} \phantom{00} \\ 52 \phantom{00} \\ \underline{48} \phantom{00} \\ 40 \phantom{00} \\ \underline{40} \phantom{00} \\ 0 \phantom{00} \end{array}$$

Gas sampling time: \_\_\_\_\_

Team members: CAFJR

**Gas sampling time:**

DATE: 3-24  
PLANT: MICROMETALS

SAMPLE TYPE: Part & met  
DUCT LOCATION: incinerator

DUCT DIAM: 36 x 26.5  
FITTING SIZE:  
WALL THICKNESS:  
DUCT STATIC PRESS: -0.3

THERMO-ANALYTICAL NORCAL CO.  
AIR POLLUTION ANALYSIS

Source Test Field Data Sheet

Filter #10

Test Number

3

Total  
Volume = 226

THIMBLE NO.  
NOZZLE DIAM  
NOZZLE TYPE: AFS  
GAS COLLECTOR  
METER NO.  
BAROMETRIC PRESS.  
DRAFT GAGE  
TRAVERSE PITOT TUBE  
MONITORING PITOT TUBE  
CONDENSATE

373  
0.009758  
30.2  
184  
26.1

| PITOT TRAVERSE |               |                                    |              |         | PITOT MONITOR |                                    |              | SAMPLING |      |       |                |               |                               |                     | REMARKS     |           |                  |
|----------------|---------------|------------------------------------|--------------|---------|---------------|------------------------------------|--------------|----------|------|-------|----------------|---------------|-------------------------------|---------------------|-------------|-----------|------------------|
| Point          | In from Cent. | Time:                              |              |         | Vel FPS       | h <sub>2</sub> O "H <sub>2</sub> O | Duct Temp °F | Vel FPS  | Time | Point | Meter Rate CFM | Meter Temp °F | Meter Press "H <sub>2</sub> O | Vol Ft <sup>3</sup> | Orif. Sett. | Pump Vac. |                  |
|                |               | h <sub>2</sub> O "H <sub>2</sub> O | Duct Temp °F | Vel FPS |               |                                    |              |          |      |       |                |               |                               |                     |             |           |                  |
| East           |               |                                    |              |         |               |                                    |              |          | 0    | 1     | 15.4           | 57.8          | 0                             | 116.20              | 1.0         | 11"       | 102 @ 11" Stand. |
|                |               |                                    |              |         |               |                                    |              |          | 17   | 2     | 5.8            | 86            |                               | 170.20              | .99         | 11"       |                  |
|                |               |                                    |              |         |               |                                    |              |          | 14   | 3     | 5.8            | 87            |                               | 174.35              | .99         | 11"       |                  |
|                |               |                                    |              |         |               |                                    |              |          | 21   |       |                |               |                               | 173.40              |             |           |                  |
| Center         |               |                                    |              |         |               |                                    |              |          | 0    | 1     | 4.9            | 87            |                               | 128.50              | .70         | 12"       |                  |
|                |               |                                    |              |         |               |                                    |              |          | 17   | 2     | 5.5            | 85            |                               | 181.87              | .87         | 11"       |                  |
|                |               |                                    |              |         |               |                                    |              |          | 14   | 3     | 5.2            | 85.5          |                               | 185.68              | .87         | 11"       |                  |
|                |               |                                    |              |         |               |                                    |              |          | 21   |       |                |               |                               | 189.59              |             |           |                  |
| West           |               |                                    |              |         |               |                                    |              |          | 0    | 1     | 5.3            | 86            |                               | 189.59              | .79         | 12"       |                  |
|                |               |                                    |              |         |               |                                    |              |          | 17   | 2     | 4.8            | 85            |                               | 193.19              | .68         | 10"       |                  |
|                |               |                                    |              |         |               |                                    |              |          | 14   | 3     | 4.8            | 86            |                               | 146.61              | .68         | 10"       |                  |
|                |               |                                    |              |         |               |                                    |              |          | 21   |       |                |               |                               | 200.03              |             |           | PM 4:40 end      |
|                |               |                                    |              |         |               |                                    |              |          |      |       |                |               |                               | 155.53              |             |           | 102 @ end        |

Gas sampling time:

Team members: JTR

DUCT DIAM:  
FITTING SIZE:  
WALL THICKNESS:  
DUCT STATIC PRESS: 0.7

# Source Test Field Data Sheet

| <b>Filler</b> | <b>#</b> | <b>Total</b> | <b>Test Number</b> | <b>Run #</b> |
|---------------|----------|--------------|--------------------|--------------|
|               | 11       |              |                    | 7            |
|               |          |              |                    | 8            |
|               |          |              |                    | 9            |
|               |          |              |                    | 10           |
|               |          |              |                    | 11           |
|               |          |              |                    | 12           |
|               |          |              |                    | 13           |
|               |          |              |                    | 14           |
|               |          |              |                    | 15           |
|               |          |              |                    | 16           |
|               |          |              |                    | 17           |
|               |          |              |                    | 18           |
|               |          |              |                    | 19           |
|               |          |              |                    | 20           |
|               |          |              |                    | 21           |
|               |          |              |                    | 22           |
|               |          |              |                    | 23           |
|               |          |              |                    | 24           |
|               |          |              |                    | 25           |
|               |          |              |                    | 26           |
|               |          |              |                    | 27           |
|               |          |              |                    | 28           |
|               |          |              |                    | 29           |
|               |          |              |                    | 30           |
|               |          |              |                    | 31           |
|               |          |              |                    | 32           |
|               |          |              |                    | 33           |
|               |          |              |                    | 34           |
|               |          |              |                    | 35           |
|               |          |              |                    | 36           |
|               |          |              |                    | 37           |
|               |          |              |                    | 38           |
|               |          |              |                    | 39           |
|               |          |              |                    | 40           |
|               |          |              |                    | 41           |
|               |          |              |                    | 42           |
|               |          |              |                    | 43           |
|               |          |              |                    | 44           |
|               |          |              |                    | 45           |
|               |          |              |                    | 46           |
|               |          |              |                    | 47           |
|               |          |              |                    | 48           |
|               |          |              |                    | 49           |
|               |          |              |                    | 50           |
|               |          |              |                    | 51           |
|               |          |              |                    | 52           |
|               |          |              |                    | 53           |
|               |          |              |                    | 54           |
|               |          |              |                    | 55           |
|               |          |              |                    | 56           |
|               |          |              |                    | 57           |
|               |          |              |                    | 58           |
|               |          |              |                    | 59           |
|               |          |              |                    | 60           |
|               |          |              |                    | 61           |
|               |          |              |                    | 62           |
|               |          |              |                    | 63           |
|               |          |              |                    | 64           |
|               |          |              |                    | 65           |
|               |          |              |                    | 66           |
|               |          |              |                    | 67           |
|               |          |              |                    | 68           |
|               |          |              |                    | 69           |
|               |          |              |                    | 70           |
|               |          |              |                    | 71           |
|               |          |              |                    | 72           |
|               |          |              |                    | 73           |
|               |          |              |                    | 74           |
|               |          |              |                    | 75           |
|               |          |              |                    | 76           |
|               |          |              |                    | 77           |
|               |          |              |                    | 78           |
|               |          |              |                    | 79           |
|               |          |              |                    | 80           |
|               |          |              |                    | 81           |
|               |          |              |                    | 82           |
|               |          |              |                    | 83           |
|               |          |              |                    | 84           |
|               |          |              |                    | 85           |
|               |          |              |                    | 86           |
|               |          |              |                    | 87           |
|               |          |              |                    | 88           |
|               |          |              |                    | 89           |
|               |          |              |                    | 90           |
|               |          |              |                    | 91           |
|               |          |              |                    | 92           |
|               |          |              |                    | 93           |
|               |          |              |                    | 94           |
|               |          |              |                    | 95           |
|               |          |              |                    | 96           |
|               |          |              |                    | 97           |
|               |          |              |                    | 98           |
|               |          |              |                    | 99           |
|               |          |              |                    | 100          |

THIMBLE NO.  
 NOZZLE DIAM  
 NOZZLE TYPE  
 GAS COLLECTOR  
 METER NO.  
 BAROMETRIC PRESSURE  
 DRAFT GAGE  
 TRAVERSE PITOT  
 MONITORING-PITOT  
 CONDENSATE

File # 11

| PITOT TRAVERSE |               |                      |              | PITOT MONITOR        |              |         | SAMPLING |       |                |               |                 |                     |             | REMARKS |                                 |
|----------------|---------------|----------------------|--------------|----------------------|--------------|---------|----------|-------|----------------|---------------|-----------------|---------------------|-------------|---------|---------------------------------|
| Point          | In from Cent. | Time:                |              | A <sub>h</sub> "1120 | Duct Temp °F | Vel FPS | Time     | Point | Meter Rate CFM | Meter Temp °F | Meter Press "Hg | Vol Ft <sup>3</sup> | Orif. Sett. |         | Pump Vac.                       |
|                |               | A <sub>h</sub> "1120 | Duct Temp °F |                      |              |         |          |       |                |               |                 |                     |             | Vel FPS |                                 |
|                | West          |                      |              | .10                  | 522          | 24.6    | 0        | 1     | .59            | 77            | 0               | 20.20               | 1.0         | 12      | .016 back ✓<br>@ 5:05 PM 5/6/49 |
|                |               |                      |              | .11                  | 599          | 21.1    | 7        | 2     | .49            | 82            |                 | 20.43               | 1.70        | 12      | 5:12                            |
|                |               |                      |              | .08                  | 592          | 22.8    | 14       | 3     | .52            | 80            |                 | 207.9               | .78         | 12      | 5:19                            |
|                |               |                      |              |                      |              |         | 21       |       |                |               |                 | 211.43              |             |         | 5:26                            |
|                | East          |                      |              | .07                  | 583          | 21.2    | 0        | 1     | .49            | 81            |                 | 214.93              | .69         | 12      |                                 |
|                |               |                      |              | .09                  | 600          | 24.2    | 7        | 2     | .55            | 81            |                 | 214.88              | .87         | 12      |                                 |
|                |               |                      |              | .09                  | 607          | 24.2    | 14       | 3     | .25            | 83            |                 | 287.2               | .87         | 12      |                                 |
|                |               |                      |              |                      |              |         | 21       |       |                |               |                 | 232.60              |             |         |                                 |
|                | East          |                      |              | .10                  | 595          | 25.5    | 0        | 1     | .57            | 78            |                 | 232.60              | .97         | 12      |                                 |
|                |               |                      |              | .10                  | 596          | 25.5    | 7        | 2     | .57            | 79            |                 | 236.70              | .91         | 12      |                                 |
|                |               |                      |              | .10                  | 604          | 25.6    | 14       | 3     | .57            | 80            |                 | 230.70              | .87         | 12      | .016 back ✓                     |
|                |               |                      |              |                      |              |         | 21       |       |                |               |                 | 234.72              |             |         | end                             |
|                |               |                      |              |                      |              |         |          |       |                |               |                 | (24.51)             |             |         |                                 |

**Gas sampling time:**

## Team members:

APPENDIX III  
LABORATORY RESULTS

TMA/Richmond Sample Data Sheet  
List for Program Manager

MICRO METALLICS CORP.  
1695 MONTEREY HIGHWAY  
SAN JOSE, CA 95112

Date Recvd 3/28/1988  
Lossed-In 3/28/1988  
Due date 4/18/1988  
QA/QC Level 1  
P.O. No.

Cust, set 5328 3

Nuc Sci grp 0  
Manager .....MP

Value.....\$781.20

Lab address: MTL

Set Comment:

Sample Receipt Info: Shipped by: gr

Condition: OK Not OK

Containers: OK Not OK

Temperature: Ice/Cool/Ambient

Split/Preservation: OK Needed: Completed by: ry

| Smr Customer ID        | Type | Comment | Volume/aliquot | Ref. time |
|------------------------|------|---------|----------------|-----------|
| 1 #1 BALL MILL TEST 1  | FILT | .....   | .....          | .....     |
| 2 #2 BALL MILL TEST 2  | FILT | .....   | .....          | .....     |
| 3 #4 BALL MILL TEST 3  | FILT | .....   | .....          | .....     |
| 4 #5 SHREDDER TEST 1   | FILT | .....   | .....          | .....     |
| 5 #6 SHREDDER TEST 2   | FILT | .....   | .....          | .....     |
| 6 #7 SHREDDER TEST 3   | FILT | .....   | .....          | .....     |
| 7 #8 INCINERATOR TEST1 | FILT | .....   | .....          | .....     |
| 8 #9 INCINERATOR TEST2 | FILT | .....   | .....          | .....     |

| Analysis-Date-Ref BY ICP | Unit    | 1    | 2    | 3    | 4    | 5    | 6    | 7    | 8       |
|--------------------------|---------|------|------|------|------|------|------|------|---------|
| BERYLLIUM                | BE ug/F | <0.1 | <0.1 | 0.19 | <0.1 | <0.1 | <0.1 | #no# | #no#    |
| Run 614 batch 1011       |         |      |      |      |      |      |      | #no# | #no#    |
| CHROMIUM                 | CR ug/F | 1.2  | 1.2  | 1.8  | 0.93 | <0.5 | <0.5 | 1.2  | 1.4     |
| Run 618 & 614 batch 1011 |         |      |      |      |      |      |      |      |         |
| COPPER                   | CU ug/F | 40   | 200  | 240  | 23   | 16   | 23   | 7700 | 8600    |
| Run 614 & 617 batch 1011 |         |      |      |      |      |      |      |      |         |
| LEAD flame               | PB ug/F | 39   | 120  | 160  | 15   | 18   | 8.8  | 4800 | 10,000. |
| Run 1866 P.B # 1011      |         |      |      |      |      |      |      |      |         |
| NICKEL                   | NI ug/F | 3.4  | 6.3  | 16   | 1.9  | 1.2  | <0.8 | 11   | 7.8     |
| Run 614 batch 1011       |         |      |      |      |      |      |      |      |         |
| SILVER                   | AG ug/F | 0.97 | 2.3  | 5.8  | 0.57 | 1.3  | 0.83 | 24   | 17      |
| Run 614 batch 1011       |         |      |      |      |      |      |      |      |         |

✓ npl 4/19/88

| Smp Customer ID         | Type | Comment  | Volume/aliquot | Ref. time |
|-------------------------|------|----------|----------------|-----------|
| 9 10 INCINERATOR TEST3  | FILT | .....    | .....          | .....     |
| 10 11 INCINERATOR TEST4 | FILT | .....    | .....          | .....     |
| 11 12 BLANK             | FILT | .....    | .....          | .....     |
| Analysis-Date-Ref       | Unit | 9        | 10             | 11        |
| BERYLLIUM               | BE   | #no#     | #no#           | #no#      |
|                         |      | #no#     | #no#           | <0.1      |
| CHROMIUM                | CR   | Total    | 0.50           |           |
| Run # 618 P.B.# 1011    |      | ug/F     | 4.6            | 0.59 <0.5 |
| COPPER                  | CU   | Total    |                |           |
| Run # 618 P.B.# 1011    |      | ug/F     | 580.           | 720 4.8   |
| LEAD                    | PB   | Total ug |                |           |
| Run # 1866 P.B.# 1011   |      | F        | 1300           | 1700 <2   |
| NICKEL                  | NI   | Total    |                |           |
| Run # 618 P.B.# 1011    |      | ug/F     | 2.8            | 2.7 <0.8  |
| SILVER                  | AG   | Total    |                |           |
| Run # 618 P.B.# 1011    |      | ug/F     | 20             | 9.7 ≤0.4  |

LAST PAGE

TMA/NORCAL SAMPLE CONTROL CENTER  
REQUEST FOR LOG-IN INFORMATIONPROGRAM MANAGER Michelle PappeTODAY'S DATE 28 Mar 88

THE FOLLOWING SAMPLES HAVE ARRIVED IN SAMPLE CONTROL WITHOUT ADEQUATE LOG-IN INFORMATION:

DATE RECEIVED 28 Mar 88

DATE DUE \_\_\_\_\_

CUSTOMER micrometals

TELEPHONE \_\_\_\_\_

ADDRESS 1695 Monterey Hwy

P.O. # \_\_\_\_\_

San Jose, CA 95112CONTACT Jim Quintal

TMA/NORCAL ID \_\_\_\_\_

| SAMPLE ID          | CONTAINER | SAMPLE      | TEST CODES*           |
|--------------------|-----------|-------------|-----------------------|
| 1 Ball Mill Test 1 | Glass     | Glass Fiber | AG, BE, CR, CU, PB, N |
| 2 Test 2           | Dish      | Filter      |                       |
| 4 Test 3           |           |             |                       |
| 5 shredder Test 1  |           |             |                       |
| 6 Test 2           |           |             |                       |
| 7 Test 3           |           |             |                       |
| 8 Tincup Test 1    |           |             | AG, CR, CU, PB, N     |
| 9 Test 2           |           |             |                       |
| 10 Test 3          |           |             |                       |
| 11 Test 4          |           |             |                       |
| 12 Blank           |           |             | AG, BE, CR, CU, PB, N |

SPECIAL INSTRUCTIONS

Return Glass Filter Containers

\*Use the space above for the proper TMA/Norcal Test Codes and any special instructions. Test codes are listed in the Environmental Sciences Price File. The samples are being held in SAMPLE CONTROL pending receipt of this completed form.

TMA/Richmond

MTL Sample Data

12 Sheet

MICRO METALLICS CORP.  
1695 MONTEREY HIGHWAY  
SAN JOSE, CA 95112

Date Recvd 3/25/1988  
Lossed-In 3/25/1988  
Due date 4/15/1988  
QA/QC Level 1  
P.O. No.

Cust, set 5328 2

Nuc Sci grp 0  
Manager .....MP

Value.....\$781.20

Lab areas: MTL  
SMP Customer ID

Set Comment:

Type Comment Volume/aliquot Ref. time

| Type | Comment | Volume/aliquot | Ref. time |
|------|---------|----------------|-----------|
| IMP  | 195 ML  | .....          | .....     |
| IMP  | 198     | .....          | .....     |
| IMP  | 199     | .....          | .....     |
| IMP  | 210     | .....          | .....     |
| IMP  | 198     | .....          | .....     |
| IMP  | 199     | .....          | .....     |
| IMP  | 223     | .....          | .....     |
| IMP  | 284     | .....          | .....     |

Analysis-Date-Ref

Unit

1

2

3

4

5

6

7

8

BERYLLIUM

BE

mg/L

|        |        |        |        |        |        |      |      |
|--------|--------|--------|--------|--------|--------|------|------|
| <0.005 | <0.005 | <0.005 | <0.005 | <0.005 | <0.005 | #no# | #no# |
|--------|--------|--------|--------|--------|--------|------|------|

Run 614 batch 1011

CHROMIUM

CR

mg/L

|      |      |      |      |      |      |     |     |
|------|------|------|------|------|------|-----|-----|
| 0.02 | 0.02 | 0.02 | 0.42 | 0.04 | 0.02 | 1.4 | 1.1 |
|------|------|------|------|------|------|-----|-----|

Run 614 batch 1011

COPPER

CU

mg/L

|      |      |      |      |      |      |     |      |
|------|------|------|------|------|------|-----|------|
| 0.04 | 0.04 | 0.06 | 0.82 | 0.12 | 0.04 | 1.5 | 0.47 |
|------|------|------|------|------|------|-----|------|

Run 614 batch 1011

LEAD

PB

mg/L

|       |       |      |      |      |      |      |      |
|-------|-------|------|------|------|------|------|------|
| <0.07 | <0.07 | 0.14 | 0.27 | 0.27 | 0.14 | 0.60 | 0.28 |
|-------|-------|------|------|------|------|------|------|

Run 1832 batch 1010

NICKEL

NI

mg/L

|       |       |       |      |       |       |      |      |
|-------|-------|-------|------|-------|-------|------|------|
| <0.04 | <0.04 | <0.04 | 0.81 | <0.04 | <0.04 | 0.52 | 0.38 |
|-------|-------|-------|------|-------|-------|------|------|

Run 614 batch 1011

SILVER

AG

mg/L

|       |       |       |       |       |       |       |       |
|-------|-------|-------|-------|-------|-------|-------|-------|
| <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 |
|-------|-------|-------|-------|-------|-------|-------|-------|

Run 614 batch 1011

✓ rpl 4/19/88

| LABORATORY ID         |      | 5328    | 2 List for Metals Lab |           | PAGE 2 |
|-----------------------|------|---------|-----------------------|-----------|--------|
| Smp Customer ID       | Type | Comment | Volume/aliquot        | Ref. time |        |
| 9 INCINERATOR TEST 3  | IMP  | 226     | .....                 | .....     |        |
| 10 INCINERATOR TEST 4 | IMP  | 224     | .....                 | .....     |        |
| 11 BLANK              | IMP  | .....   | .....                 | .....     |        |

| Analysis-Date-Ref | Unit    | 9     | 10    | 11     |
|-------------------|---------|-------|-------|--------|
| BERYLLIUM         | BE mg/L | #no#  | #no#  | #no#   |
|                   |         | #no#  | #no#  | <0.005 |
| CHROMIUM          | CR mg/L | 1.1   | 1.5   | <0.01  |
| COPPER            | CU mg/L | 0.09  | 0.25  | <0.02  |
| LEAD              | PB mg/L | 0.15  | 0.22  | <0.07  |
| NICKEL            | NI mg/L | 0.35  | 0.55  | <0.04  |
| SILVER            | AG mg/L | ≤0.01 | <0.01 | <0.01  |

LAST PAGE FOR Metals Lab

APPENDIX IV  
PRINTOUT FOR INCINERATOR TEST

SUMMARY OF SETUP PARAMETERS PROGRAM 3- CHART : MICROMET

DATE : 3/24/88 TIME : 11:02:39 CHART SPEED : 1 CM/MIN

CONSTANTS

1 0.0000E+00 2 0.0000E+00 3 0.0000E+00 4 0.0000E+00 5 0.0000E+00 6 0.0000E+00

OPTIONS AVAILABLE ARE

1 PRINT TIME OF DAY

7 DISABLE AUTORANGING

| CHAN | TITLE | UNITS | SCALE FACTOR          | ZERO           | ANALOG SENSITIVITY | ANALOG ZERO    |
|------|-------|-------|-----------------------|----------------|--------------------|----------------|
| 1    | -     | -     | -                     | -              | -                  | -              |
| 2    | O2    | PCT   | 4.0000E-05 VOLTS/ PCT | 0.0000E+00 PCT | 2.5000E+00 PCT /CM | 0.0000E+00 PCT |
| 3    | THC   | PPM   | 1.0000E-02 VOLTS/ PPM | 0.0000E+00 PPM | 1.0000E+02 PPM /CM | 0.0000E+00 PPM |
| 4    | CO    | PPM   | 1.0000E-06 VOLTS/ PPM | 0.0000E+00 PPM | 1.0000E+03 PPM /CM | 0.0000E+00 PPM |
| 5    | CO2   | PCT   | 5.0000E-04 VOLTS/ PCT | 0.0000E+00 PCT | 2.0000E+00 PCT /CM | 0.0000E+00 PCT |
| 6    | -     | -     | -                     | -              | -                  | -              |
| 7    | -     | -     | -                     | -              | -                  | -              |
| 8    | -     | -     | -                     | -              | -                  | -              |
| 9    | -     | -     | -                     | -              | -                  | -              |
| 10   | -     | -     | -                     | -              | -                  | -              |
| 11   | -     | -     | -                     | -              | -                  | -              |
| 12   | -     | -     | -                     | -              | -                  | -              |

↑ 4 INDICATES AUTOMATIC RANGE CHANGE IN FOLLOWING DIGITAL CHANNEL

TO START CHART JUST PRESS RUN

TO STOP CHART JUST PRESS STOP

TO END CHART PRESS SFT THEN END

TO CHANGE PARAMETERS ENTER A NUMBER THEN PRESS ENTR SEE MANUAL

1 CHART SPEED

4 PEN DROP

7 ANALOG ZERO

2 SET CHANNEL

5 DIGITAL ZERO

8 ANALOG SENSITIVITY

3 PEN LIFT

6 CHANNEL SCALE

9 SET CONSTANT

PRESS RUN TO START CHART OR PRESS END TO RETURN TO START

INCINERATOR #2 ONLY  
#1 ~~DOWN~~ DOWN.  
normally operate both  
simultaneously.

NAT GAS FLOW RATE  
300 CFH per burner. 3 BURNERS  
= 900 CFH

LL9788

LL438

THC

17-469

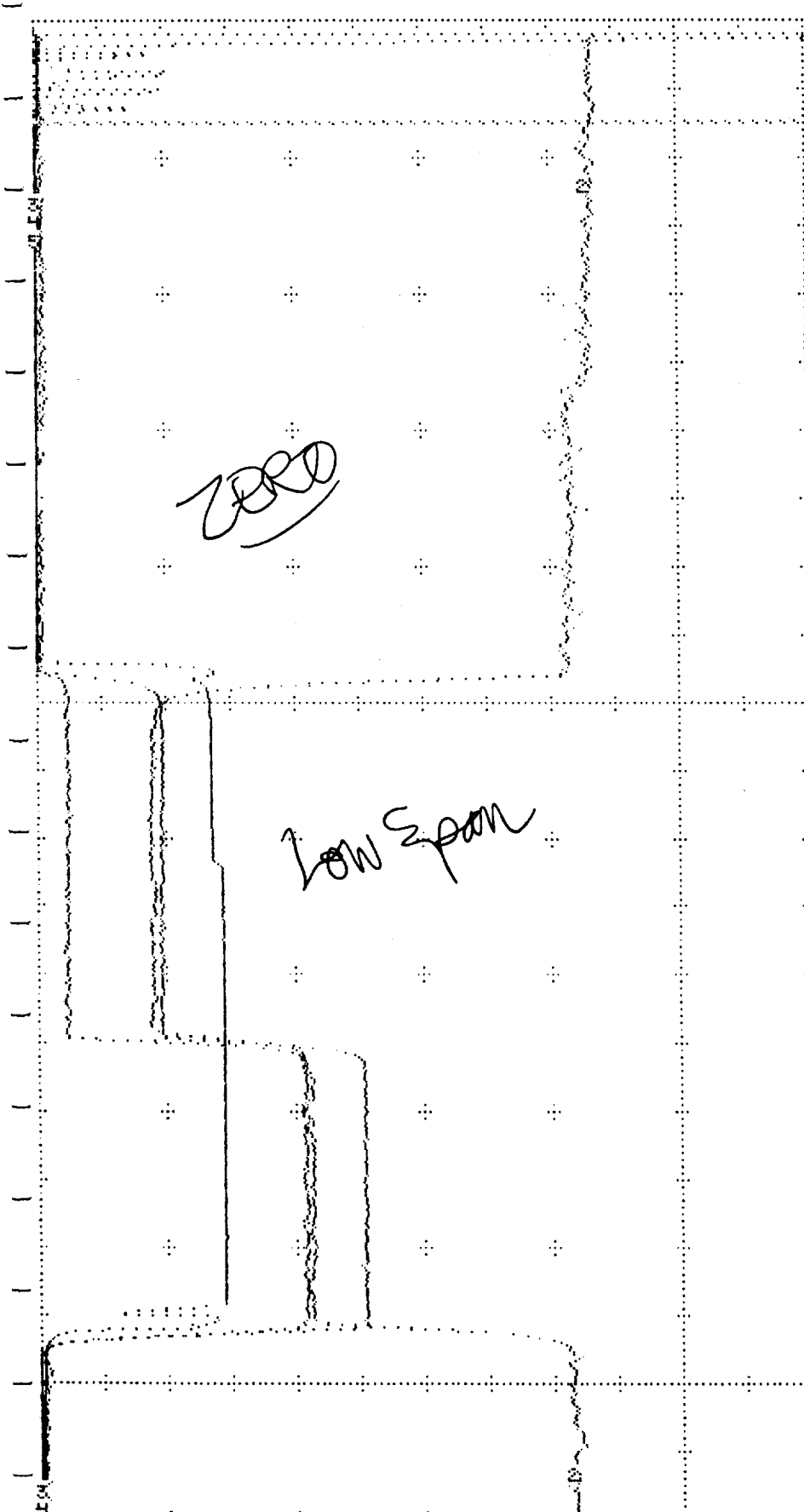
O2-10.22, CO2-3.93,  
O2 4.22 CO2 9.69

PO 96.5 (2907HC)

CO-419

CO 455

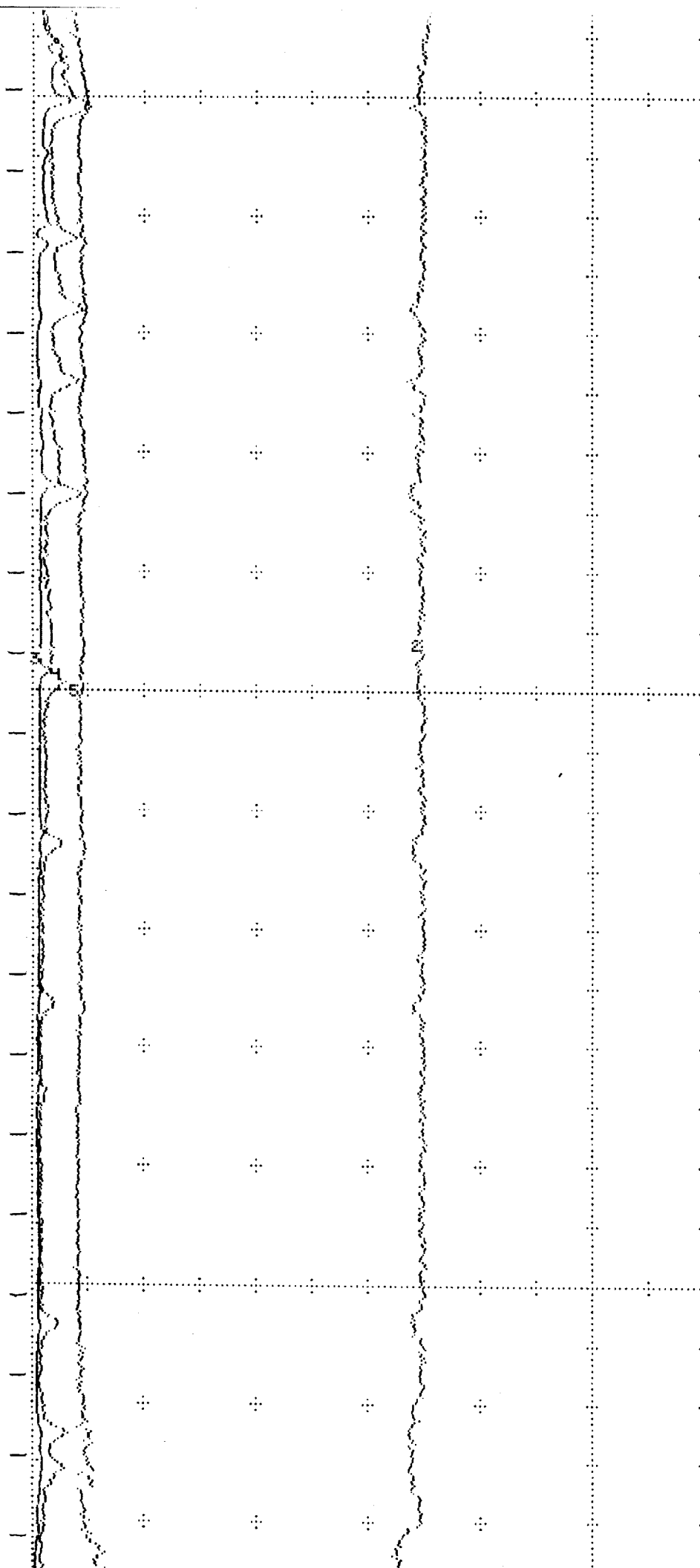
0 2 4 6 8 10 12



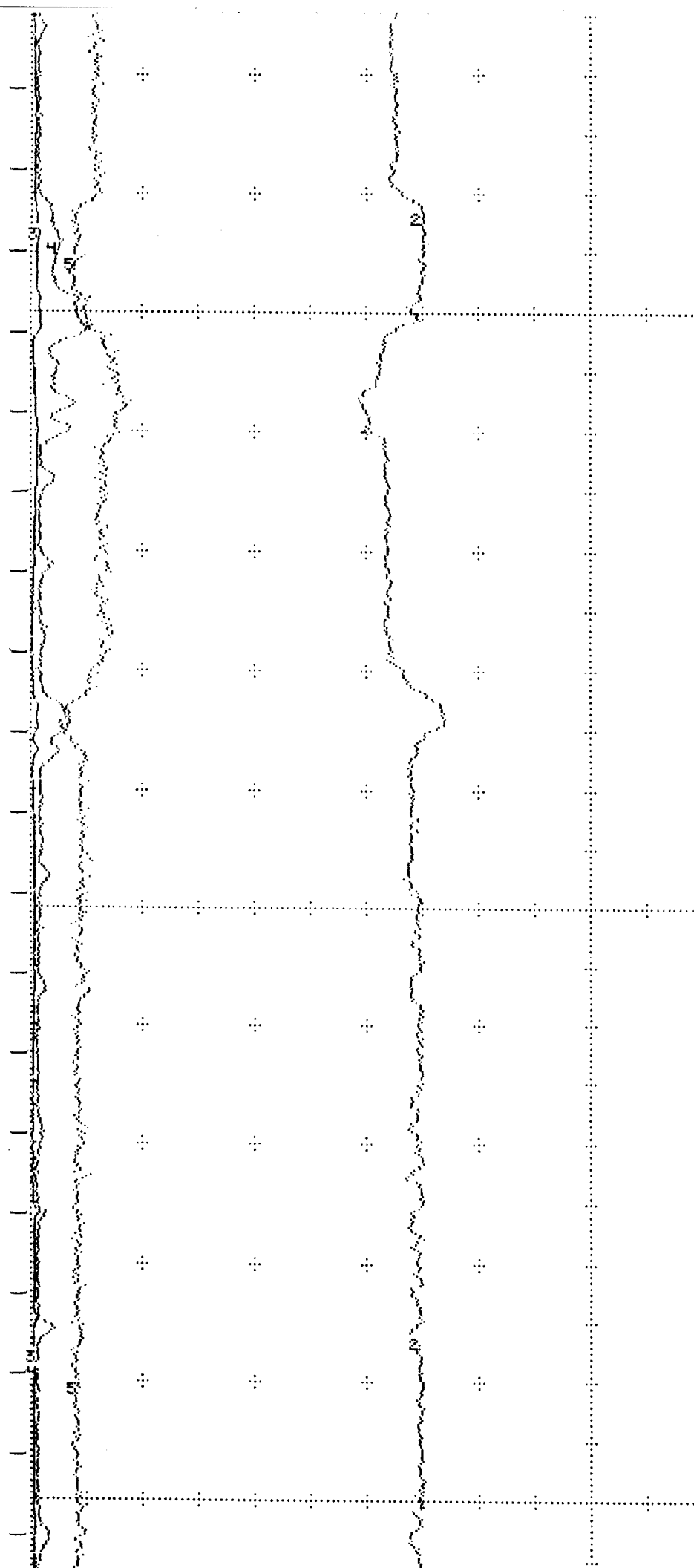
| TIME<br>H M S | 2<br>O2<br>PCT | 3<br>THC<br>PPH | 4<br>CO<br>PPH | 5<br>CO2<br>PCT |
|---------------|----------------|-----------------|----------------|-----------------|
| 11:04:44      | 21.740         | 5.3170          | 51.860         | 4.1480          |
| 11:05:44      | 21.450         | 3.4180          | 98.050         | -11.930         |
| 11:06:44      | 21.460         | 1.8200          | 103.70         | -13.040         |
| 11:07:44      | 21.630         | 3.0310          | 110.20         | -.54240         |
| 11:08:44      | 21.310         | 2.7340          | 165.10         | -.24020         |
| 11:09:44      | 20.660         | 2.7880          | 43.510         | -.25810         |
| 11:10:44      | 20.720         | .38840          | -125.10        | -.42680         |
| 11:11:44      | 20.800         | 1.9760          | 116.50         | -.19370         |
| 11:12:44      | 20.670         | 1.7390          | 90.010         | -.25090         |
| 11:13:44      | 4.9690         | 268.90          | 491.70         | 3.8900          |
| 11:14:44      | 4.4480         | 271.20          | 498.00         | 3.9100          |
| 11:15:44      | 4.4700         | 272.50          | 458.30         | 3.8990          |
| 11:16:44      | 4.5520         | 289.30          | 466.10         | 3.9210          |
| 11:17:44      | 4.5070         | 290.60          | 456.90         | 3.9460          |
| 11:18:44      | 9.0230         | 290.20          | 2651.0         | 7.0730          |
| 11:19:44      | 10.310         | 290.00          | 4109.0         | 10.210          |
| 11:20:44      | 10.720         | 290.70          | 4135.0         | 10.150          |
| 11:21:44      | 10.810         | 291.10          | 4139.0         | 10.160          |
| 11:22:44      | 10.670         | 260.90          | 4173.0         | 10.220          |
| 11:23:44      | 20.630         | 6.1340          | 64.670         | -.33970         |
| 11:24:44      | 20.880         | 4.6990          | 76.590         | -.24490         |

INCINERATOR #2 ONLY.  
TEST 1 1744# IN  
P.C BOARD

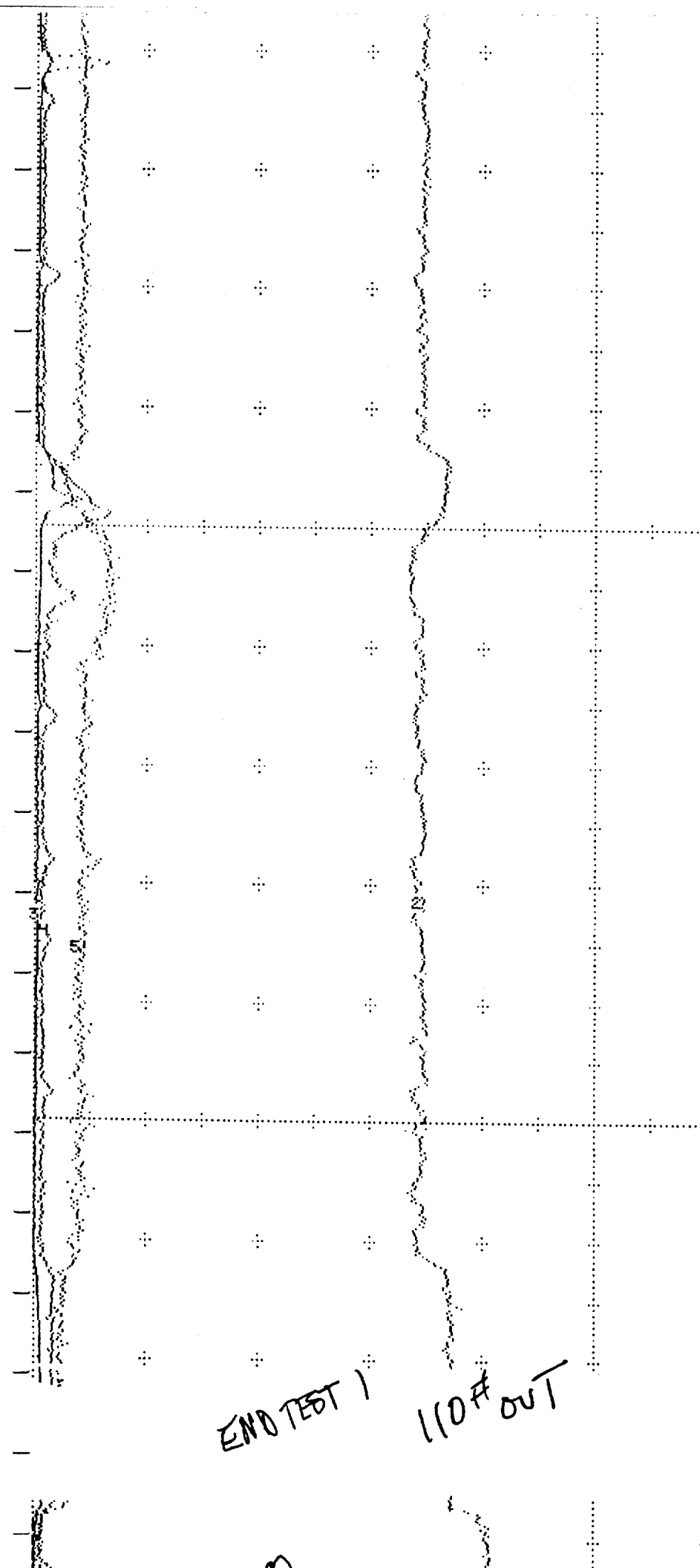
|          |        |        |         |         |
|----------|--------|--------|---------|---------|
| 11:26:44 | 20.370 | 3.7500 | 100.70  | -.33320 |
| 11:27:44 | 20.250 | 4.6410 | 150.80  | -.33910 |
| 11:28:44 | 20.600 | 4.6520 | 93.280  | -.25510 |
| 11:29:44 | 20.640 | 3.4010 | 123.30  | -.26250 |
| 11:30:44 | 20.810 | 4.0020 | 83.750  | -.17820 |
| 11:31:44 | 20.750 | 4.7800 | 118.30  | -.23480 |
| 11:32:44 | 20.820 | 5.3420 | 116.20  | -.17220 |
| 11:33:44 | 20.660 | 4.9020 | 67.650  | -.24200 |
| 11:34:44 | 20.870 | 4.7550 | 81.660  | -.26640 |
| 11:35:44 | 20.680 | 4.0760 | 76.000  | -.24490 |
| 11:36:44 | 20.720 | 3.7580 | 44.700  | -.25510 |
| 11:37:44 | 20.790 | 3.5450 | -48.870 | -.19790 |
| 11:38:44 | 20.780 | 4.8870 | 84.640  | -.19250 |
| 11:39:44 | 20.830 | 4.5190 | 45.600  | -.32900 |
| 11:40:44 | 20.920 | 4.6820 | 76.000  | -.21750 |
| 11:41:44 | 20.790 | 3.9380 | 106.10  | -.37370 |
| 11:42:44 | 20.730 | 4.7450 | 96.860  | -.23000 |
| 11:43:44 | 20.840 | 4.4660 | 36.650  | -.23780 |
| 11:44:44 | 20.730 | 3.8800 | 505.40  | 3.7790  |
| 11:45:44 | 20.990 | 5.0890 | 476.80  | 3.8220  |
| 11:46:44 | 20.720 | 4.1090 | 419.60  | 3.8960  |
| 11:47:44 | 18.260 | 12.400 | 77.490  | 1.1680  |
| 11:48:44 | 18.900 | 14.890 | 136.50  | .87920  |
| 11:49:44 | 17.930 | 6.5190 | 118.60  | 1.2980  |
| 11:50:44 | 17.520 | 55.220 | 712.00  | 1.6970  |
| 11:51:44 | 18.610 | 23.740 | 191.30  | .78800  |



|          |        |               |        |        |
|----------|--------|---------------|--------|--------|
| 11:52:44 | 17.660 | 33.590        | 356.70 | 1.5580 |
| 11:53:44 | 17.230 | 53.380        | 758.20 | 1.9580 |
| 11:54:44 | 17.450 | 23.690        | 343.30 | 1.6530 |
| 11:55:44 | 17.430 | <u>24.750</u> | 433.30 | 1.7220 |
|          |        | CHA           |        |        |
| 11:56:44 | 17.460 | 11.040        | 456.30 | 1.7830 |
| 11:57:44 | 17.430 | 10.320        | 326.90 | 1.7990 |
| 11:58:44 | 17.450 | <u>13.720</u> | 492.00 | 1.8490 |
|          |        | THC           |        |        |
| 11:59:44 | 17.280 | 18.600        | 478.60 | 1.8390 |
| 12:00:44 | 17.090 | 15.490        | 330.50 | 1.8730 |
| 12:01:44 | 17.340 | 13.930        | 265.20 | 1.6600 |
| 12:02:44 | 17.330 | 16.560        | 344.50 | 1.7530 |
| 12:03:44 | 17.180 | 13.930        | 447.30 | 1.8120 |
| 12:04:44 | 17.350 | 13.890        | 246.70 | 1.5800 |
| 12:05:44 | 17.360 | 13.810        | 253.00 | 1.7510 |
| 12:06:44 | 17.510 | 13.710        | 227.40 | 1.7450 |
| 12:07:44 | 17.460 | 11.710        | 207.70 | 1.6570 |
| 12:08:44 | 17.530 | 12.900        | 164.50 | 1.7240 |
| 12:09:44 | 17.540 | 11.420        | 159.70 | 1.7310 |
| 12:10:44 | 17.490 | 10.730        | 163.30 | 1.7760 |
| 12:11:44 | 17.410 | 11.730        | 177.30 | 1.6880 |
| 12:12:44 | 17.480 | 12.940        | 194.00 | 1.6650 |
| 12:13:44 | 17.520 | 12.490        | 156.10 | 1.7390 |
| 12:14:44 | 17.480 | 11.310        | 178.50 | 1.6530 |
| 12:15:44 | 17.020 | 10.080        | 199.30 | 1.9040 |
| 12:16:44 | 16.920 | 17.640        | 410.40 | 1.9890 |
| 12:17:44 | 17.400 | 10.290        | 219.30 | 2.0540 |
|          |        | CHA           |        |        |



| Time     | Lat    | Long   | Alt    | Speed  |
|----------|--------|--------|--------|--------|
| 12:19:44 | 16.250 | 7.2880 | 102.20 | 2.4040 |
| 12:20:44 | 16.300 | 8.3110 | 153.40 | 2.2140 |
| 12:21:44 | 16.570 | 6.3770 | 161.50 | 2.5700 |
| 12:22:44 | 17.550 | 12.270 | 464.90 | 1.5780 |
| 12:23:44 | 17.190 | 16.650 | 849.10 | 2.0330 |
| 12:24:44 | 15.610 | 8.2470 | 478.90 | 3.0190 |
| 12:25:44 | 14.920 | 13.280 | 681.60 | 3.6600 |
| 12:26:44 | 15.960 | 10.360 | 234.20 | 2.6460 |
| 12:27:44 | 15.990 | 6.7010 | 196.40 | 2.6830 |
| 12:28:44 | 15.980 | 3.7330 | 175.50 | 2.5880 |
| 12:29:44 | 16.660 | 2.8150 | 133.50 | 2.1720 |
| 12:30:44 | 17.840 | 12.800 | 614.50 | 1.1820 |
| 12:31:44 | 17.140 | 5.0760 | 188.90 | 1.8720 |
| 12:32:44 | 17.040 | 7.5800 | 199.60 | 1.9130 |
| 12:33:44 | 17.320 | 6.4490 | 109.90 | 1.6290 |
| 12:34:44 | 17.410 | 7.0160 | 139.70 | 1.8470 |
| 12:35:44 | 17.290 | 5.0000 | 115.00 | 1.8100 |
| 12:36:44 | 17.500 | 4.6600 | 139.40 | 1.7590 |
| 12:37:44 | 17.300 | 4.8680 | 173.70 | 1.9530 |
| 12:38:44 | 17.530 | 4.8840 | 115.00 | 1.7400 |
| 12:39:44 | 17.300 | 7.2680 | 156.10 | 1.7100 |
| 12:40:44 | 17.430 | 11.260 | 235.40 | 1.7050 |
| 12:41:44 | 17.540 | 5.3610 | 114.70 | 1.7090 |
| 12:42:44 | 17.390 | 5.1910 | 111.10 | 1.7030 |
| 12:43:44 | 17.360 | 5.6260 | 179.10 | 1.6850 |



|                                                    |        |                          |        |          |
|----------------------------------------------------|--------|--------------------------|--------|----------|
| 12:45:44                                           | 17.360 | 6.6890                   | 123.60 | 1.5190   |
| 12:46:44                                           | 17.310 | 5.9670                   | 205.90 | 1.7440   |
| 12:47:44                                           | 17.440 | 5.4140                   | 137.40 | 1.6780   |
| 12:48:44                                           | 17.090 | 5.3420                   | 116.80 | 1.8040   |
| 12:49:44                                           | 17.250 | 4.9160                   | 202.30 | 1.9850   |
| 12:50:44                                           | 17.160 | 3.2960                   | 118.30 | 1.9280   |
| 12:51:44                                           | 17.020 | 4.7050                   | 122.40 | 1.6450   |
| 12:52:44                                           | 18.380 | 28.090                   | 369.20 | 1.1620   |
| 12:53:44                                           | 17.390 | 11.360                   | 779.60 | 1.8990   |
| 12:54:44                                           | 16.780 | 9.4470                   | 460.40 | 2.7310   |
| 12:55:44                                           | 16.990 | 5.7710                   | 254.50 | 2.3130   |
| 12:56:44                                           | 17.090 | 9.9420                   | 195.20 | 1.7620   |
| 12:57:44                                           | 17.280 | 4.7430                   | 129.60 | 1.8590   |
| 12:58:44                                           | 17.360 | 3.5400                   | 139.10 | 1.6990   |
| 12:59:44                                           | 17.000 | <del>3.5860</del><br>644 | 138.20 | 1.5770   |
| 13:00:44                                           | 17.270 | <del>5.7450</del>        | 283.40 | 1.8190   |
| 13:01:44                                           | 17.360 | 4.7680                   | 140.00 | 1.8220   |
| 13:02:44                                           | 17.390 | 3.5200                   | 144.80 | 1.7970   |
| 13:03:44                                           | 17.440 | 2.4650                   | 179.70 | 1.5640   |
| 13:04:44                                           | 16.980 | 1.3950                   | 150.50 | 1.8470   |
| 13:05:44                                           | 17.100 | 1.0800                   | 73.610 | 1.2830   |
| 13:06:44                                           | 18.650 | 8.5840                   | 358.80 | .99300   |
| 13:07:44                                           | 18.760 | 12.170                   | 332.90 | .85770   |
| <div>17.3      THG-13<br/>CH4-7/279      1.8</div> |        |                          |        |          |
| 13:08:44                                           | 20.250 | 4.2710                   | 120.40 | -1.18710 |

2000

LOW SPAN

HIGH SPAN

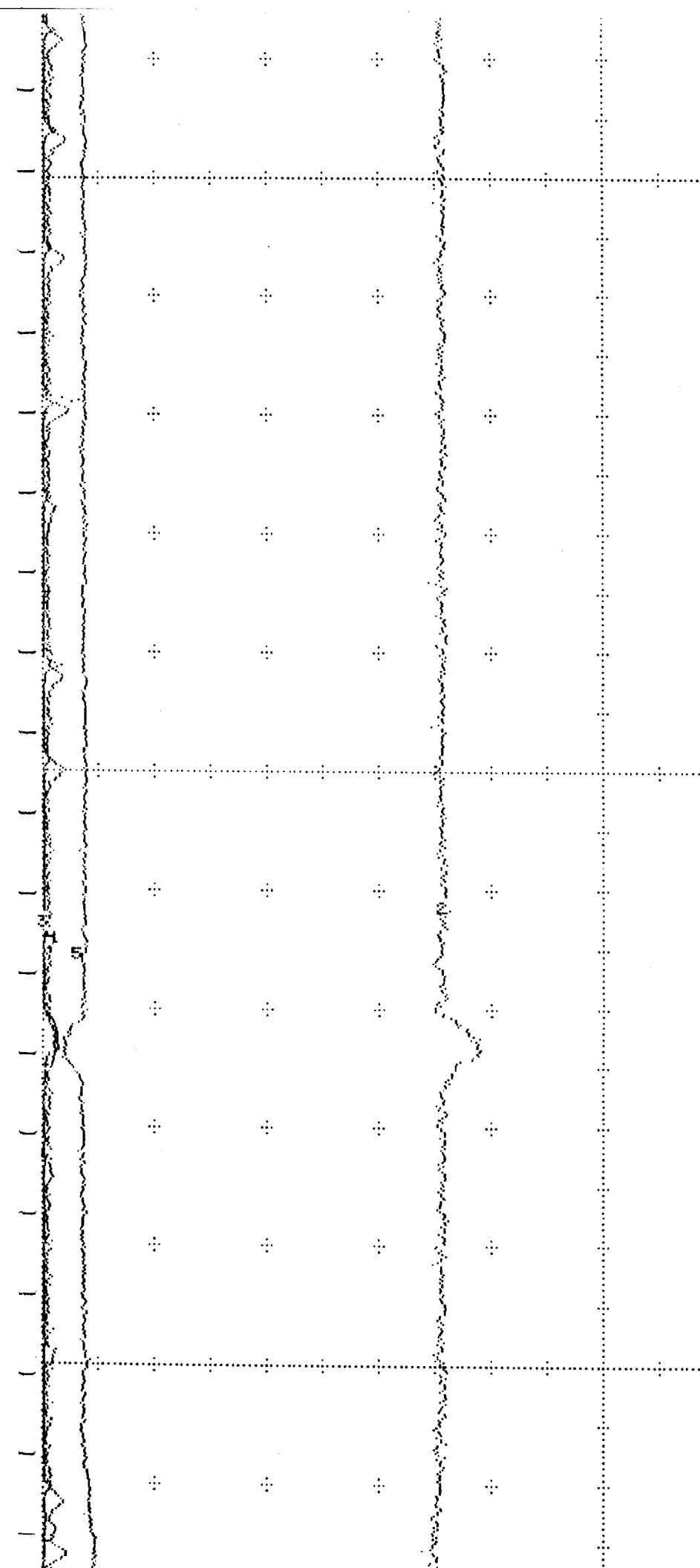
|          |        |         |                              |         |
|----------|--------|---------|------------------------------|---------|
| 13:09:44 | 20.210 | 3.1200  | 130.80                       | .18470  |
| 13:10:44 | 20.340 | 2.4110  | 108.10                       | -0.0631 |
| 13:11:44 | 20.350 | .55490  | 121.90                       | -.72960 |
| 13:12:44 | 20.330 | 2.6850  | 130.20                       | -.40350 |
| 13:13:44 | 20.180 | .31150  | 113.50                       | -.52930 |
| 13:14:44 | 8.1660 | 285.60  | 546.90                       | 3.6230  |
| 13:15:44 | 4.3810 | 294.80  | 535.50                       | 3.8080  |
| 13:16:44 | 4.3730 | 296.90  | 537.90                       | 3.8870  |
| 13:17:44 | 10.140 | 297.50  | 4184.0                       | 10.110  |
| 13:18:44 | 10.050 | 296.20  | 4194.0                       | 9.9830  |
| 13:19:44 | 10.110 | 293.60  | 104.60                       | 0.0828  |
| 13:20:44 | 10.320 | 292.10  | 97.460                       | -0.0721 |
| 13:21:44 | 10.230 | 292.30  | 80.470                       | -.28370 |
| 13:22:44 | 10.350 | 292.90  | 71.230                       | 0.0232  |
| 13:23:44 | 10.430 | 291.10  | 46.190                       | -.18890 |
| 13:24:44 | 10.080 | 25.150  | 534.60                       | .25810  |
| 13:25:44 | 10.140 | .10330  | 118.30                       | .73730  |
| 13:26:44 | 10.250 | -.57160 | 113.50                       | -.94180 |
| 13:27:44 | 10.340 | -.51580 | -244.30                      | -.58110 |
| 13:28:44 | 10.380 | -.43900 | <u>zero</u><br>-89.110       | -1.2790 |
| 13:29:44 | 10.370 | -.13780 | -88.220                      | -.56980 |
| 13:30:44 | 10.100 | 5.7210  | 123.00                       | 0.0333  |
| 13:31:44 | 20.580 | 5.2450  | <u>Span</u><br>443.70        | 3.7000  |
| 13:32:44 | 20.450 | 2.8070  | 481.30                       | 3.7960  |
| 13:33:44 | 20.300 | 1.7030  | 460.40                       | 3.9490  |
| 13:34:44 | 20.520 | 6.9310  | <u>231.20</u><br><u>zero</u> | .30220  |

START TEST 2  
PC BOARD 98#  
IN

|          |        |        |         |         |
|----------|--------|--------|---------|---------|
| 13:36:44 | 20.540 | 3.5180 | -33.670 | -.21280 |
| 13:37:44 | 20.380 | 4.6760 | 47.680  | -.20740 |
| 13:38:44 | 20.570 | 3.9680 | 124.20  | -.23780 |
| 13:39:44 | 20.320 | 3.5540 | 99.540  | -.33500 |
| 13:40:44 | 20.300 | 2.8580 | 46.490  | -.33260 |
| 13:41:44 | 20.370 | 1.7710 | 112.00  | -.31170 |
| 13:42:44 | 18.720 | 7.9110 | 120.70  | .79040  |

THC

|          |        |        |        |        |
|----------|--------|--------|--------|--------|
| 13:43:44 | 17.890 | 71.160 | 965.60 | 1.6890 |
| 13:44:44 | 17.910 | 13.280 | 475.60 | 1.5870 |
| 13:45:44 | 17.700 | 15.640 | 271.20 | 1.4370 |
| 13:46:44 | 17.820 | 11.430 | 297.10 | 1.6300 |
| 13:47:44 | 17.850 | 7.7490 | 199.30 | 1.5670 |
| 13:48:44 | 17.760 | 8.2620 | 238.40 | 1.6150 |
| 13:49:44 | 18.000 | 5.4570 | 148.40 | 1.5800 |
| 13:50:44 | 17.770 | 6.0150 | 227.40 | 1.6980 |
| 13:51:44 | 17.580 | 7.7020 | 405.60 | 1.9880 |
| 13:52:44 | 17.840 | 5.4410 | 207.40 | 1.6890 |
| 13:53:44 | 17.630 | 4.9380 | 180.60 | 1.7250 |
| 13:54:44 | 17.820 | 4.8410 | 302.50 | 1.5920 |
| 13:55:44 | 18.670 | 28.840 | 220.20 | .98830 |
| 13:56:44 | 19.520 | 26.370 | 204.70 | .75280 |
| 13:57:44 | 17.940 | 5.8210 | 100.40 | 1.4680 |
| 13:58:44 | 17.920 | 5.8380 | 192.80 | 1.5540 |
| 13:59:44 | 18.180 | 8.6150 | 129.60 | 1.5920 |



|          |        |        |        |        |
|----------|--------|--------|--------|--------|
| 14:01:44 | 17.560 | 4.6830 | 81.960 | 1.4620 |
| 14:02:44 | 17.850 | 4.2930 | 118.60 | 1.5320 |
| 14:03:44 | 17.770 | 3.2350 | 122.10 | 1.5520 |
| 14:04:44 | 17.770 | 3.6480 | 101.30 | 1.4700 |
| 14:05:44 | 17.900 | 2.6850 | 141.80 | 1.3970 |
| 14:06:44 | 17.830 | 3.1250 | 96.860 | 1.5090 |
| 14:07:44 | 17.760 | 5.0510 | 427.60 | 1.5770 |
| 14:08:44 | 17.780 | 3.9010 | 118.30 | 1.4980 |
| 14:09:44 | 18.000 | 3.0890 | 113.50 | 1.5240 |
| 14:10:44 | 17.920 | 4.7580 | 128.10 | 1.4830 |
| 14:11:44 | 17.890 | 3.0540 | 133.50 | 1.4590 |
| 14:12:44 | 17.850 | 3.5460 | 113.80 | 1.5410 |
| 14:13:44 | 17.560 | 4.6150 | 415.70 | 1.5950 |
| 14:14:44 | 17.840 | 4.0290 | 66.460 | 1.5890 |
| 14:15:44 | 17.990 | 2.6240 | 118.30 | 1.5410 |
| 14:16:44 | 17.790 | 1.7390 | 133.20 | 1.5740 |
| 14:17:44 | 17.500 | 2.6750 | 111.70 | 1.3810 |
| 14:18:44 | 18.440 | 5.4520 | 178.80 | 1.0970 |
| 14:19:44 | 17.780 | 3.6620 | 94.180 | 1.5060 |
| 14:20:44 | 17.780 | 3.2960 | 87.030 | 1.5320 |
| 14:21:44 | 17.590 | 4.7950 | 98.050 | 1.5130 |
| 14:22:44 | 17.940 | 3.6880 | 63.480 | 1.5640 |
| 14:23:44 | 17.910 | 3.5170 | 178.50 | 1.5760 |
| 14:24:44 | 17.740 | 3.2350 | 102.20 | 1.5010 |
| 14:25:44 | 17.750 | 4.4380 | 130.50 | 1.6850 |
| 14:26:44 | 17.420 | 5.1020 | 137.10 | 1.9010 |

|          |        |                                  |        |        |
|----------|--------|----------------------------------|--------|--------|
| 14:27:44 | 17.270 | 3.1080                           | 249.70 | 2.0730 |
| 14:28:44 | 17.770 | 1.0070                           | 163.90 | 1.6980 |
| 14:29:44 | 17.860 | 3.2160                           | 92.090 | 1.6230 |
| 14:30:44 | 17.770 | .56460                           | 141.20 | 1.5630 |
| 14:31:44 | 17.900 | 2.4250                           | 59.600 | 1.5680 |
| 14:32:44 | 17.990 | .35720                           | 49.770 | 1.5050 |
| 14:33:44 | 17.910 | <del>2.4270</del> <sup>ptc</sup> | 212.50 | 1.5830 |
| 14:34:44 | 17.940 | 2.2580                           | 93.280 | 1.4880 |
| 14:35:44 | 17.740 | 2.2940                           | 72.120 | 1.4940 |
| 14:36:44 | 17.560 | 3.1120                           | 151.10 | 1.4580 |
| 14:37:44 | 17.520 | 3.1010                           | 81.960 | 1.5420 |
| 14:38:44 | 17.380 | 2.8880                           | 160.30 | 1.3220 |
| 14:39:44 | 17.670 | 2.0450                           | 133.20 | 1.4550 |
| 14:40:44 | 17.720 | 2.9030                           | 73.610 | 1.3750 |
| 14:41:44 | 17.780 | 2.8110                           | 132.00 | 1.4620 |
| 14:42:44 | 17.880 | 2.8990                           | 384.40 | 1.5840 |
| 14:43:44 | 17.840 | 2.8960                           | 245.20 | 1.5840 |
| 14:44:44 | 17.690 | 3.0120                           | 176.40 | 1.5510 |
| 14:45:44 | 18.040 | 1.8270                           | 217.50 | 1.5990 |
| 14:46:44 | 17.680 | 1.9070                           | 637.90 | 1.5890 |
| 14:48:44 | 17.860 | 2.8660                           | 60.200 | 1.4790 |

END TEST 2 DC Board.

71 ~~17.8~~ # 17.8 THG-9  
OUT, CH4-2 180 1.5

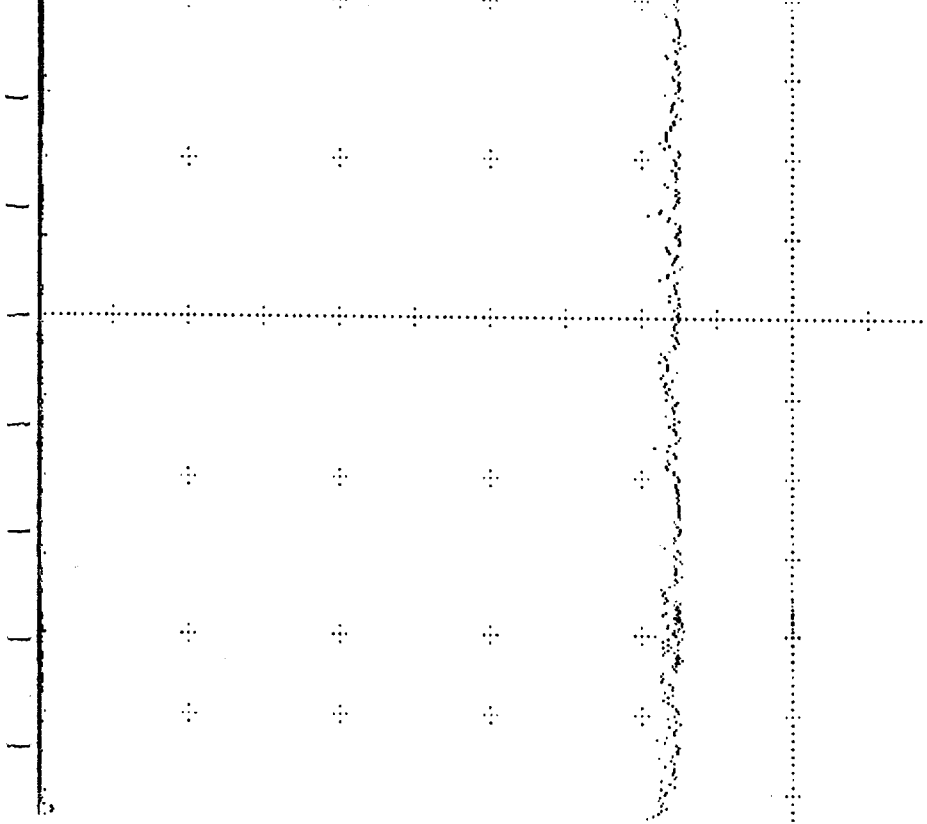
ZERO

|          |        |         |         |         |
|----------|--------|---------|---------|---------|
| 14:49:44 | 19.380 | 19.540  | 162.40  | .74570  |
| 14:50:44 | 20.910 | 1.9900  | 35.460  | -.14900 |
| 14:51:44 | 20.640 | -0.0211 | -37.550 | -.46190 |
| 14:52:44 | 20.830 | -.18750 | -109.90 | -.36360 |

Low  
span

High  
span

|          |        |        |         |         |
|----------|--------|--------|---------|---------|
| 14:53:44 | 12.220 | 258.60 | -23.240 | .15550  |
| 14:54:44 | 4.5450 | 283.30 | 407.70  | 3.6030  |
| 14:55:44 | 4.4700 | 283.80 | 429.40  | 3.5820  |
| 14:56:44 | 4.4030 | 284.60 | 427.30  | 3.5650  |
| 14:57:44 | 4.4330 | 286.40 | 421.40  | 3.5700  |
| 14:58:44 | 9.9320 | 285.20 | 3916.0  | 9.3090  |
| 14:59:44 | 10.370 | 286.20 | 3982.0  | 9.3440  |
| 15:00:44 | 10.270 | 286.20 | 4004.0  | 9.9280  |
| 15:01:44 | 18.400 | 11.430 | 491.40  | 1.0960  |
| 15:02:44 | 20.930 | 5.0490 | -51.260 | -.15140 |
| 15:03:44 | 20.660 | 4.0600 | -78.380 | -.18240 |
| 15:04:44 | 21.000 | 4.7540 | -82.560 | -.26280 |
| 15:05:44 | 20.780 | 4.9260 | 26.220  | -.24730 |
| 15:06:44 | 20.990 | 4.5780 | -76.890 | -.20680 |
| 15:07:44 | 20.980 | 3.6260 | -80.770 | -.30690 |
| 15:08:44 | 20.860 | 6.7950 | 10.130  | -.21810 |
| 15:09:44 | 21.040 | 10.090 | -46.190 | -.24970 |
| 15:10:44 | 21.160 | 10.440 | -58.110 | -.36000 |
| 15:11:44 | 21.030 | 5.0170 | -48.870 | -.32960 |
| 15:12:44 | 20.860 | 4.8410 | -70.030 | -.19550 |
| 15:13:44 | 21.160 | 4.7670 | -110.20 | -.22940 |
| 15:14:44 | 20.770 | 3.4080 | -115.00 | -.25390 |
| 15:15:44 | 20.910 | 3.4530 | -104.60 | -.40530 |
| 15:16:44 | 20.980 | 3.5590 | -119.80 | -.34450 |
| 15:17:44 | 20.930 | 3.1720 | -109.90 | -.22770 |
| 15:18:44 | 20.550 | 3.8680 | 47.380  | -.24490 |

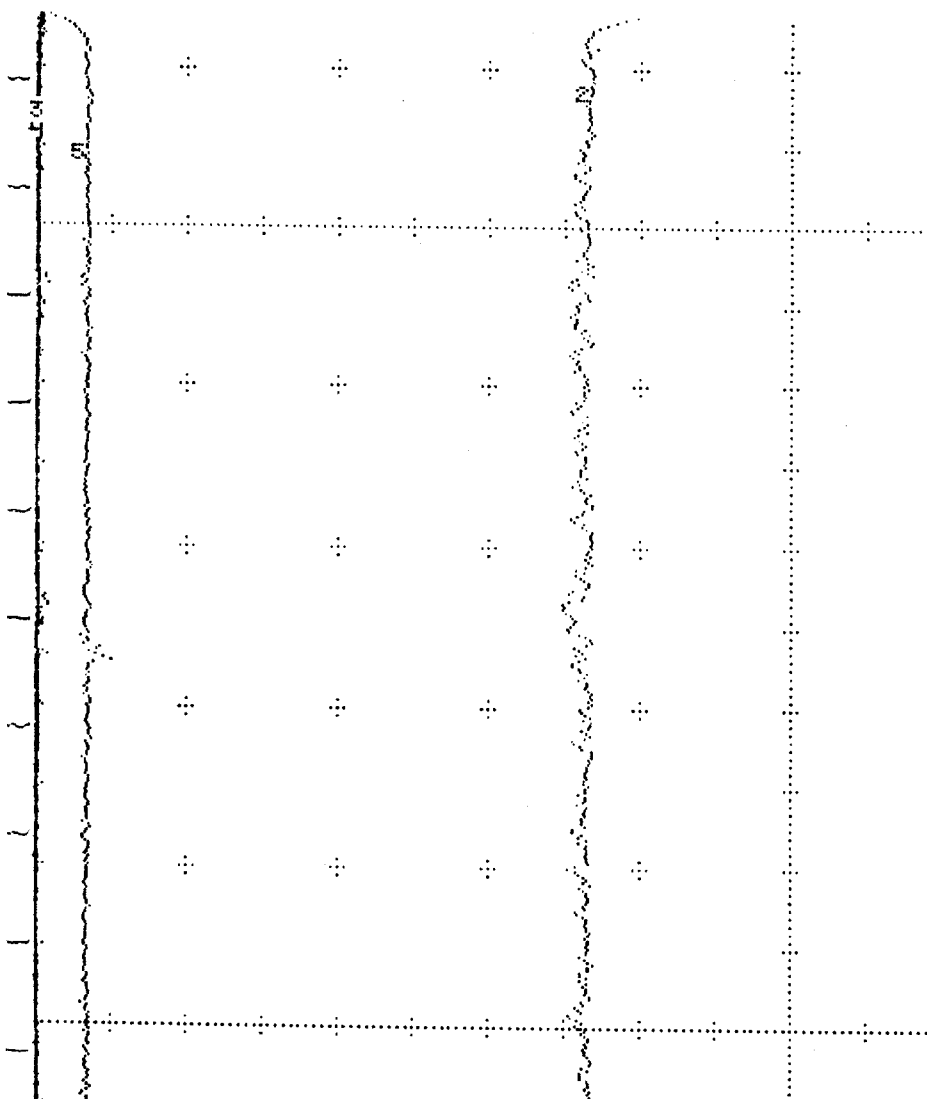


|          |        |        |         |         |
|----------|--------|--------|---------|---------|
| 15:18:44 | 21.210 | 4.5300 | -77.190 | -.23480 |
| 15:20:44 | 21.110 | 5.2210 | -67.650 | -.20320 |
| 15:21:44 | 21.100 | 2.9140 | -101.30 | -.18470 |
| 15:22:44 | 21.250 | 4.8970 | -45.600 | -.23360 |
| 15:23:44 | 21.290 | 4.0600 | -66.160 | -.31590 |
| 15:24:44 | 20.840 | 4.1590 | -61.690 | -.33730 |
| 15:25:44 | 21.230 | 2.9900 | -159.10 | -.36950 |
| 15:26:44 | 21.160 | 3.7020 | -91.500 | -.23420 |
| 15:28:44 | 20.450 | 4.8550 | -48.530 | -.31880 |
| 15:29:44 | 21.060 | 2.8280 | -103.10 | -.18350 |
| 15:30:44 | 20.780 | 3.4550 | -118.30 | -.21750 |

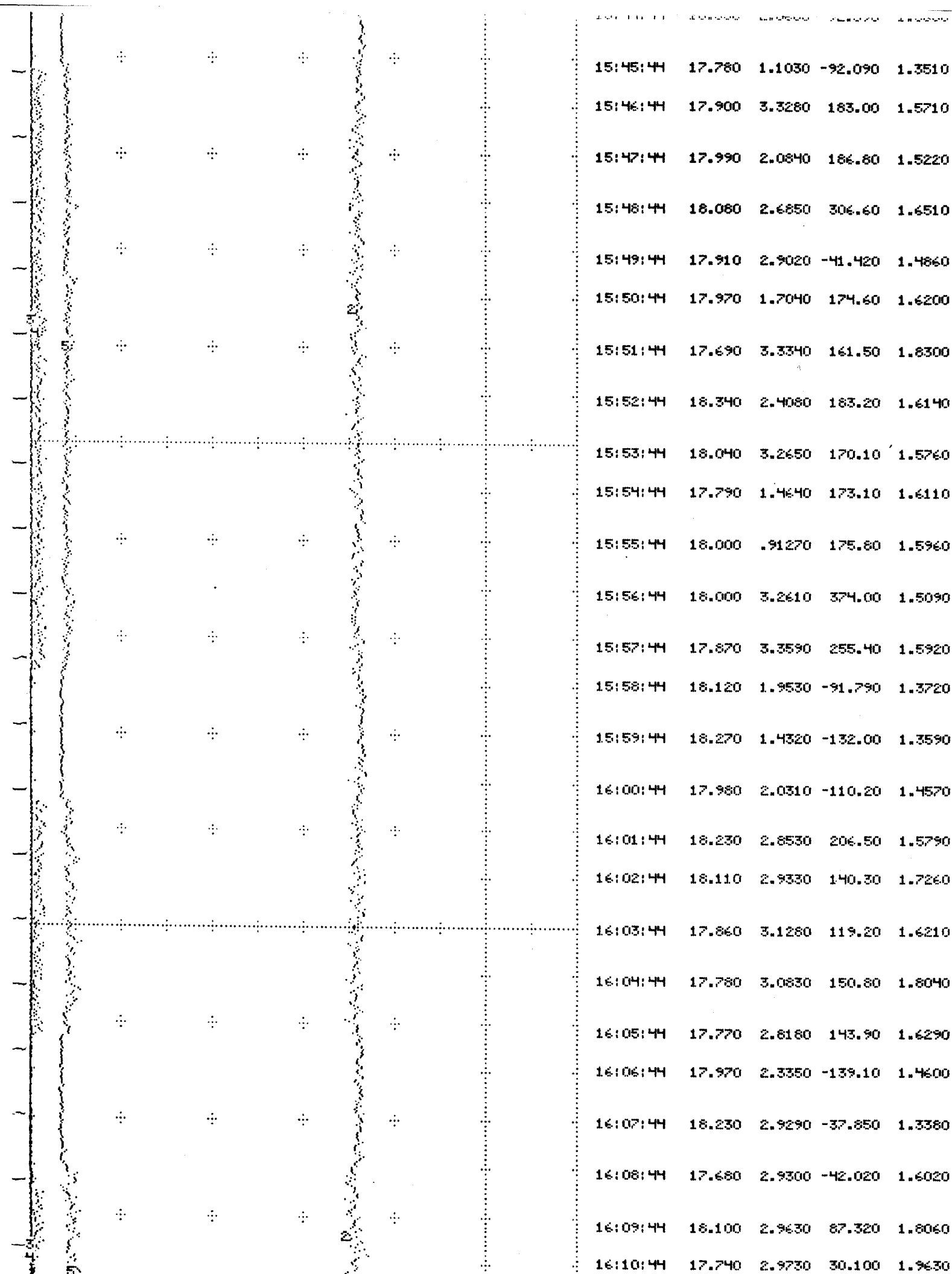
START TEST

1

SLUDGE  
IN AT 157#



|          |        |        |         |        |
|----------|--------|--------|---------|--------|
| 15:31:44 | 18.440 | 2.6690 | 40.230  | 1.3870 |
| 15:32:44 | 17.970 | 1.7610 | -105.50 | 1.3560 |
| 15:33:44 | 18.270 | 3.1640 | -101.00 | 1.3870 |
| 15:34:44 | 17.950 | 2.0970 | 29.800  | 1.3090 |
| 15:35:44 | 18.150 | 1.7980 | -81.360 | 1.3550 |
| 15:36:44 | 18.220 | 1.4280 | -61.690 | 1.3130 |
| 15:37:44 | 18.430 | 1.9530 | -47.980 | 1.3510 |
| 15:38:44 | 17.640 | 2.8910 | 70.930  | 1.2890 |
| 15:39:44 | 18.050 | 2.8340 | -89.710 | 1.3940 |
| 15:40:44 | 18.190 | 1.7090 | -63.780 | 1.3910 |
| 15:41:44 | 17.640 | 2.6850 | -87.320 | 1.4370 |
| 15:42:44 | 18.320 | 1.2120 | -172.50 | 1.2940 |
| 15:43:44 | 18.120 | 2.9450 | -63.480 | 1.3440 |



|          |        |                                 |         |        |
|----------|--------|---------------------------------|---------|--------|
| 16:11:44 | 18.210 | <del>3.4980</del>               | -28.010 | 1.5870 |
| 16:12:44 | 17.910 | <del>3.0540</del>               | 112.30  | 1.7210 |
| 16:13:44 | 17.890 | <u>CH<sub>4</sub></u><br>1.9850 | 19.070  | 1.7730 |
| 16:14:44 | 18.060 | 0.0212                          | -114.10 | 1.4890 |
| 16:15:44 | 18.350 | -0.0201                         | -67.950 | .98350 |
| 16:16:44 | 18.110 | -0.0220                         | -60.500 | 1.3760 |
| 16:17:44 | 18.030 | 3.1380                          | -148.40 | 1.4480 |
| 16:18:44 | 17.950 | 1.1680                          | -131.70 | 1.3790 |
| 16:19:44 | 18.210 | .93920                          | -102.80 | 1.3940 |
| 16:20:44 | 18.060 | 1.4560                          | -161.80 | 1.4380 |
| 16:21:44 | 18.190 | 1.1160                          | -191.60 | 1.3930 |
| 16:22:44 | 18.050 | 1.7630                          | -129.30 | 1.4080 |
| 16:23:44 | 17.970 | 3.4010                          | -68.250 | 1.4470 |
| 16:24:44 | 18.160 | 1.1820                          | -124.20 | 1.4770 |
| 16:25:44 | 17.940 | 3.0160                          | -128.10 | 1.4790 |
| 16:26:44 | 18.220 | 3.3850                          | -94.770 | 1.4440 |
| 16:27:44 | 17.990 | 1.2200                          | -100.10 | 1.4440 |
| 16:28:44 | 18.040 | .97630                          | -92.090 | 1.4830 |
| 16:29:44 | 18.160 | 2.8700                          | -104.90 | 1.5030 |
| 16:30:44 | 17.850 | .78520                          | -87.620 | 1.3640 |
| 16:31:44 | 17.990 | 1.9830                          | -46.790 | 1.4690 |
| 16:32:44 | 18.120 | 3.3200                          | -59.600 | 1.5090 |
| 16:33:44 | 18.320 | 3.4020                          | -79.280 | 1.4720 |
| 16:34:44 | 18.160 | 3.1350                          | -96.260 | 1.4710 |
| 16:35:44 | 18.320 | .67930                          | -135.30 | 1.4240 |
| 16:36:44 | 17.890 | 2.8800                          | 69.140  | 1.8560 |

END TEST 1 Sludge  
WEIGHT OUT = 52#

2010

low span

high span

|                     |                   |                   |                   |                   |
|---------------------|-------------------|-------------------|-------------------|-------------------|
| 16:37:44            | 18.160            | 2.8640            | -53.050           | 1.6270            |
| 16:38:44            | 17.770            | 2.8080            | -67.950           | 1.7290            |
| 16:39:44            | 18.240            | 3.1430            | -53.350           | 1.5830            |
| 16:40:44            | 18.090            | 1.8300            | -57.520           | 1.7320            |
|                     | 18.1              | 1.83              | 0                 | 1.5               |
| 16:41:44            | 21.330            | -.30740           | -69.440           | .61030            |
| 16:42:44            | 21.380            | -.86720           | -156.40           | 1.3310            |
| 16:43:44            | 21.220            | -.78660           | -180.60           | 1.0300            |
| 16:44:44            | 21.210            | -.24790           | -31.890           | .70510            |
| 16:45:44            | 21.460            | -.32970           | -57.220           | .65030            |
| 16:46:44            | 20.190            | .21900            | -94.770           | .44400            |
| <del>16:47:44</del> | <del>19.260</del> | <del>263.30</del> | <del>216.60</del> | <del>1.9520</del> |
| 16:48:44            | 4.4780            | 281.70            | 390.40            | 3.9130            |
| 16:49:44            | 4.3430            | 282.40            | 599.30            | 3.7640            |
| 16:50:44            | 4.4250            | 283.30            | 442.00            | 3.8990            |
| <del>16:51:44</del> | <del>4.2470</del> | <del>283.80</del> | <del>494.10</del> | <del>3.9090</del> |
| 16:52:44            | 10.310            | <del>283.30</del> | 3913.0            | 9.8960            |
| 16:53:44            | 10.360            | 285.90            | 3999.0            | 9.9700            |
| 16:54:44            | 10.300            | 286.50            | -54.840           | .14840            |
| 16:55:44            | 10.330            | 286.50            | -122.70           | -.17640           |
| 16:56:44            | 10.400            | 287.10            | EEEE              | 19.620            |
| 16:57:44            | 10.260            | 287.00            | 449.10            | 3.6380            |
| 16:58:44            | 10.250            | 287.40            | 460.40            | 3.8720            |
| 16:59:44            | 10.400            | 287.90            | 4704.0            | 10.040            |
| 17:00:44            | 10.450            | 287.60            | 4689.0            | 10.050            |
| 17:01:44            | 10.570            | 288.10            | EEEE              | 20.160            |
|                     |                   |                   | ZERO              |                   |
| 17:02:44            | 19.380            | 7.4540            | -91.500           | -.16920           |
| 17:03:44            | 21.450            | 4.9110            | -61.890           | -1.7740           |

17:04:44 21.390 2.5210 431.50 3.8640

START SLUDGE TEST 2 WT=170

PRIMARY + SECONDARY TEMP ~ 700°F, 400°C.  
- 860°F

17:05:44 19.840 8.1730 54.540 .70570

17:06:44 18.370 1.9830 95.970 1.2930

17:07:44 18.440 3.1100 -47.980 1.3650

17:08:44 18.320 3.1130 -105.20 1.2890

17:09:44 18.520 .94600 -51.260 1.3650

17:10:44 18.500 1.9660 -121.60 1.3780

17:11:44 18.410 2.7770 -73.020 1.4390

17:12:44 18.390 1.4770 -90.300 1.3300

17:13:44 18.350 3.3440 -62.880 1.4480

17:14:44 18.420 .85450 -112.30 1.3540

17:15:44 18.190 1.6630 -61.990 1.4010

17:16:44 18.280 3.1000 -89.110 1.3750

17:17:44 18.270 .78570 -73.610 1.4440

17:18:44 18.240 1.9220 -64.970 1.4650

17:19:44 18.410 .17710 -244.30 1.3370

17:20:44 18.440 .64110 -98.350 1.4190

17:21:44 18.300 .57780 -89.710 1.3900

17:22:44 18.330 2.0960 -93.280 1.3320

17:23:44 17.910 2.9290 -87.620 1.4560

17:24:44 18.470 2.4410 -91.790 1.3590

17:25:44 18.430 0.0408 -73.910 1.3810

17:26:44 18.430 -.32380 -147.80 .90420

17:27:44 18.600 -.30220 -154.60 1.0610

17:28:44 18.520 -.48790 -122.10 1.4800

OK4

|          |        |               |         |        |
|----------|--------|---------------|---------|--------|
| 17:29:44 | 18.380 | -.30100       | -118.90 | 1.2790 |
| 17:30:44 | 18.470 | <u>0.0746</u> | -146.60 | 1.4660 |
| 17:31:44 | 18.410 | 2.4410        | -108.70 | 1.4120 |
| 17:32:44 | 18.320 | .49980        | -110.20 | 1.4360 |
| 17:33:44 | 18.420 | 2.5590        | -76.590 | 1.4940 |
| 17:34:44 | 18.500 | .36430        | -79.870 | 1.4340 |
| 17:35:44 | 17.990 | 3.0510        | -80.170 | 1.4630 |
| 17:36:44 | 18.580 | 0.0078        | -175.50 | 1.0630 |
| 17:37:44 | 18.770 | .12540        | -148.40 | 1.4920 |
| 17:38:44 | 18.290 | 1.6970        | -98.950 | 1.4990 |
| 17:39:44 | 18.120 | 2.9300        | -91.200 | 1.4950 |
| 17:40:44 | 18.700 | -0.0389       | -220.80 | 1.4480 |
| 17:41:44 | 18.860 | 2.3370        | -90.600 | 1.5380 |
| 17:42:44 | 18.380 | .15270        | -100.70 | 1.4450 |
| 17:43:44 | 18.490 | .71780        | -135.60 | 1.4150 |
| 17:44:44 | 18.490 | .10960        | -163.30 | 1.0580 |
| 17:45:44 | 18.350 | 2.0360        | -132.90 | 1.4910 |
| 17:46:44 | 18.500 | 0.0259        | -182.10 | 1.4320 |
| 17:47:44 | 18.490 | 2.4410        | -180.90 | 1.3530 |
| 17:48:44 | 18.510 | 1.6550        | -333.50 | 1.4420 |
| 17:49:44 | 18.610 | 2.3430        | -111.40 | 1.4680 |
| 17:50:44 | 18.290 | 1.1180        | -184.70 | 1.4620 |
| 17:51:44 | 18.420 | .52090        | -193.70 | 1.4280 |
| 17:52:44 | 18.370 | 2.1930        | -97.160 | 1.4500 |
| 17:53:44 | 18.190 | .66950        | -125.10 | 1.3810 |
| 17:54:44 | 18.230 | 2.7180        | -106.90 | 1.4650 |

|          |                   |                   |                   |                   |
|----------|-------------------|-------------------|-------------------|-------------------|
| 17:56:44 | 18.370            | .60480            | -186.80           | 1.3790            |
| 17:57:44 | 18.400            | 2.4410            | -109.30           | 1.4190            |
| 17:58:44 | 18.270            | 2.5630            | -136.80           | 1.4250            |
| 17:59:44 | 18.380            | 1.2320            | -109.30           | 1.4060            |
| 18:00:44 | 18.540            | 2.6450            | -171.00           | 1.4040            |
| 18:01:44 | 18.600            | .17290            | -165.70           | 1.4500            |
| 18:02:44 | 18.530            | 2.4410            | -212.50           | 1.4530            |
| 18:03:44 | 18.670            | .36170            | -304.30           | 1.1490            |
| 18:04:44 | 18.240            | 2.4410            | -143.30           | 1.4540            |
| 18:05:44 | 18.700            | .34030            | -227.40           | 1.3570            |
| 18:06:44 | 18.440            | 1.8710            | -180.00           | 1.4130            |
| 18:07:44 | 18.630            | 0.0931            | -270.00           | 1.3140            |
| 18:08:44 | 18.500            | .81970            | -139.10           | 1.4480            |
| 18:09:44 | 18.590            | .45450            | -205.90           | 1.4760            |
| 18:10:44 | 18.590            | 2.8760            | -180.90           | 1.4120            |
| 18:11:44 | 18.460            | 1.8920            | -151.10           | 1.4660            |
|          | 18.4              | 2.96              | 0                 | 1.4               |
| 18:12:44 | 21.630            | 285.00            | -267.00           | -0.36180          |
| 18:13:44 | 21.690            | 286.50            | -167.20           | -.29260           |
| 18:14:44 | 21.540            | 288.20            | -205.90           | -.25270           |
| 18:15:44 | 21.480            | 288.60            | -202.60           | -.28550           |
| 18:16:44 | <del>4.5820</del> | <del>3.6970</del> | <del>369.80</del> | <del>3.7200</del> |
|          | 2.0               |                   |                   |                   |
| 18:17:44 | 4.6490            | -.72380           | 363.00            | 3.9490            |
| 18:18:44 | 4.1420            | -.22140           | 391.60            | 3.7460            |
| 18:19:44 | 4.3360            | .24600            | 334.40            | 3.8190            |
| 18:20:44 | 10.340            | 3.2350            | 4511.0            | 10.140            |

END SLUDGE TEST 2

END WT = 53

2018

LOW SPAN

STOP

18:22:44 10.500 2.7440 4585.0 10.190

APPENDIX V

GAS CALIBRATION SHEETS FOR INSTRUMENT VAN  
USED IN INCINERATOR TEST



**RARE & SPECIALTY GASES DEPT**

## ANALYTICAL REPORT

**To:** Atlas Welding Supply  
1224 6th Street  
Berkeley Ca. 94710

**Date Reported:** 5/11/87

Reference: 556722  
Test# SCO587048  
P.O. #1252

**Material Submitted:** Oxygen, Carbon Monoxide, Carbon Dioxide, Nitrogen

**Information Requested:** Ratio Analysis

**Method of Analysis:** Oxygen Analyzer/ Gas Chromatograph

**Result of Investigation:** Cyl; - LL-9788

| <u>Component</u> | <u>Specification</u> | <u>Concentration</u> |
|------------------|----------------------|----------------------|
| Oxygen           | 9/11%                | 10.2%                |
| Carbon Monoxide  | 400/500 ppm          | 414 ppm              |
| Carbon Dioxide   | 3/5%                 | 3.93%                |
| Nitrogen         | Balance              | Balance              |

By \_\_\_\_\_  
PRINCIPAL GAS ANALYST

This report states accurately the results of the investigation made upon the materials submitted to the Analytical Laboratory. The Laboratory has endeavored to use its resources to determine, and to present, the information requested objectively. HOWEVER, such investigation is undertaken, and this report is rendered, on the condition that, under no circumstances (including negligence) shall The ROC Group, Inc. have any liability in excess of its established charge for such investigation. There is NO WARRANTY OF FITNESS FOR ANY PURPOSE, and any use of this report or the information contained herein shall be at the sole risk of the user.



Industrial Gases

RARE & SPECIALTY GASES DEPT.

## ANALYTICAL REPORT

To: Atlas Welding Supply  
1224 6th Street  
Berkely, CA. 94710

Date Reported: 9/21/87

Reference: PO#3884  
SO#558865-00  
Test# SC0987082

Material Submitted: Carbon Monoxide, Carbon Dioxide, Oxygen, Nitrogen  
Gas Mixture

Information Requested: Ratio Analysis

Method of Analysis: Gas Chromatograph, Oxygen Analyzer

Result of Investigation: Cyl# LL438

| Component       | Specification | Concentration |
|-----------------|---------------|---------------|
| Carbon Monoxide | 4000-5000 ppm | 4555 ppm      |
| Carbon Dioxide  | 9-11%         | 9.69%         |
| Oxygen          | 3-5%          | 4.22%         |
| Nitrogen        | Balance       | Balance       |

By

PRINCIPAL GAS ANALYST

This report states accurately the results of the investigation made upon the materials submitted to the Analytical Laboratory. The Laboratory has endeavored to use its resources to determine, and to present the information requested objectively. HOWEVER such investigation is undertaken and this report is rendered on the condition that under no circumstances, including negligence, shall The BOC Group Inc. have any liability in excess of its established charge for such investigation. THERE IS NO WARRANTY OF FITNESS FOR ANY PURPOSE and any use of this report or the information contained herein shall be at the sole risk of the user.



HAIR & SKIN: 7-11, 12-13, 14-15, 16-17, 18-19, 20-21, 22-23, 24-25, 26-27, 28-29, 30-31, 32-33, 34-35, 36-37, 38-39, 40-41, 42-43, 44-45, 46-47, 48-49, 50-51, 52-53, 54-55, 56-57, 58-59, 60-61, 62-63, 64-65, 66-67, 68-69, 70-71, 72-73, 74-75, 76-77, 78-79, 80-81, 82-83, 84-85, 86-87, 88-89, 90-91, 92-93, 94-95, 96-97, 98-99, 100-101, 102-103, 104-105, 106-107, 108-109, 110-111, 112-113, 114-115, 116-117, 118-119, 120-121, 122-123, 124-125, 126-127, 128-129, 130-131, 132-133, 134-135, 136-137, 138-139, 140-141, 142-143, 144-145, 146-147, 148-149, 150-151, 152-153, 154-155, 156-157, 158-159, 160-161, 162-163, 164-165, 166-167, 168-169, 170-171, 172-173, 174-175, 176-177, 178-179, 180-181, 182-183, 184-185, 186-187, 188-189, 190-191, 192-193, 194-195, 196-197, 198-199, 200-201, 202-203, 204-205, 206-207, 208-209, 210-211, 212-213, 214-215, 216-217, 218-219, 220-221, 222-223, 224-225, 226-227, 228-229, 230-231, 232-233, 234-235, 236-237, 238-239, 240-241, 242-243, 244-245, 246-247, 248-249, 250-251, 252-253, 254-255, 256-257, 258-259, 260-261, 262-263, 264-265, 266-267, 268-269, 270-271, 272-273, 274-275, 276-277, 278-279, 280-281, 282-283, 284-285, 286-287, 288-289, 290-291, 292-293, 294-295, 296-297, 298-299, 300-301, 302-303, 304-305, 306-307, 308-309, 310-311, 312-313, 314-315, 316-317, 318-319, 320-321, 322-323, 324-325, 326-327, 328-329, 330-331, 332-333, 334-335, 336-337, 338-339, 340-341, 342-343, 344-345, 346-347, 348-349, 350-351, 352-353, 354-355, 356-357, 358-359, 360-361, 362-363, 364-365, 366-367, 368-369, 370-371, 372-373, 374-375, 376-377, 378-379, 380-381, 382-383, 384-385, 386-387, 388-389, 390-391, 392-393, 394-395, 396-397, 398-399, 400-401, 402-403, 404-405, 406-407, 408-409, 410-411, 412-413, 414-415, 416-417, 418-419, 420-421, 422-423, 424-425, 426-427, 428-429, 430-431, 432-433, 434-435, 436-437, 438-439, 440-441, 442-443, 444-445, 446-447, 448-449, 450-451, 452-453, 454-455, 456-457, 458-459, 460-461, 462-463, 464-465, 466-467, 468-469, 470-471, 472-473, 474-475, 476-477, 478-479, 480-481, 482-483, 484-485, 486-487, 488-489, 490-491, 492-493, 494-495, 496-497, 498-499, 500-501, 502-503, 504-505, 506-507, 508-509, 510-511, 512-513, 514-515, 516-517, 518-519, 520-521, 522-523, 524-525, 526-527, 528-529, 530-531, 532-533, 534-535, 536-537, 538-539, 540-541, 542-543, 544-545, 546-547, 548-549, 550-551, 552-553, 554-555, 556-557, 558-559, 560-561, 562-563, 564-565, 566-567, 568-569, 570-571, 572-573, 574-575, 576-577, 578-579, 580-581, 582-583, 584-585, 586-587, 588-589, 590-591, 592-593, 594-595, 596-597, 598-599, 600-601, 602-603, 604-605, 606-607, 608-609, 610-611, 612-613, 614-615, 616-617, 618-619, 620-621, 622-623, 624-625, 626-627, 628-629, 630-631, 632-633, 634-635, 636-637, 638-639, 640-641, 642-643, 644-645, 646-647, 648-649, 650-651, 652-653, 654-655, 656-657, 658-659, 660-661, 662-663, 664-665, 666-667, 668-669, 670-671, 672-673, 674-675, 676-677, 678-679, 680-681, 682-683, 684-685, 686-687, 688-689, 690-691, 692-693, 694-695, 696-697, 698-699, 700-701, 702-703, 704-705, 706-707, 708-709, 710-711, 712-713, 714-715, 716-717, 718-719, 720-721, 722-723, 724-725, 726-727, 728-729, 730-731, 732-733, 734-735, 736-737, 738-739, 740-741, 742-743, 744-745, 746-747, 748-749, 750-751, 752-753, 754-755, 756-757, 758-759, 760-761, 762-763, 764-765, 766-767, 768-769, 770-771, 772-773, 774-775, 776-777, 778-779, 780-781, 782-783, 784-785, 786-787, 788-789, 790-791, 792-793, 794-795, 796-797, 798-799, 800-801, 802-803, 804-805, 806-807, 808-809, 810-811, 812-813, 814-815, 816-817, 818-819, 820-821, 822-823, 824-825, 826-827, 828-829, 830-831, 832-833, 834-835, 836-837, 838-839, 840-841, 842-843, 844-845, 846-847, 848-849, 850-851, 852-853, 854-855, 856-857, 858-859, 860-861, 862-863, 864-865, 866-867, 868-869, 870-871, 872-873, 874-875, 876-877, 878-879, 880-881, 882-883, 884-885, 886-887, 888-889, 890-891, 892-893, 894-895, 896-897, 898-899, 900-901, 902-903, 904-905, 906-907, 908-909, 910-911, 912-913, 914-915, 916-917, 918-919, 920-921, 922-923, 924-925, 926-927, 928-929, 930-931, 932-933, 934-935, 936-937,

## ANALYTICAL REPORT

**To:** Atlas Welding Supply  
1224 6th Street  
Berkeley, CA. 94710

**Date Reported:** 9/21/87

Reference: PO#3884  
SO#558865-00  
Test#SC0987084

**Material Submitted:** Propane, Carbon Dioxide, Nitrogen Gas Mixture

**Information Requested:** Ratio Analysis

**Method of Analysis:** Gas Chromatography

**Result of Investigation:** Cyl = 17-1469

| Component      | Specification | Concentration |
|----------------|---------------|---------------|
| Propane        | 80-100 ppm    | 96.3 ppm      |
| Carbon Dioxide | 2000 ppm      | 2006 ppm      |
| Nitrogen       | Balance       | Balance       |

By \_\_\_\_\_

[illegible]

1. *Chlorophyll a* and *Chlorophyll b* were determined by the method of Arar and Collins (1971) using a Shimadzu 1601 UV-Visible Spectrophotometer. The concentration of chlorophyll was expressed in mg/L.