



HERMAN STRAUSS, INC.

Scrap Iron · Steel · Metals

THIRTY-FIFTH AND McCOLLOCH STS. · WHEELING, WEST VIRGINIA 26003 · (304) 232-8770

EMISSION TEST REPORT
DRY AUTO SHREDDER
WET SCRUBBER
DIESELS No. 1 and 2

December 8, 1987

←←← Cross/Tessitore & Associates, P.A.
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R-5006

1.0 INTRODUCTION

Compliance Testing was conducted at the Yorke Doliner facility in Rockledge, Florida on October 26, 1987. The testing consisted of particulate (Method 5), and visual emissions (Method 9), on the wet scrubber system of the dry automotive metal shredder (Z box). Visual emission (EPA Method 9), were also run concurrently on the diesel engines powering this source.

The above tests were conducted according to FDER and U.S. EPA approved methods, in accordance with permit number A005-111877, Auto Shredder, and A005-123074, Diesels 1 and 2.

The results of the testing, including calculations, testing procedures, and laboratory procedures, are presented in the following sections of this report.

2.0 PROCESS DESCRIPTION

The junk car (without gas tank), or loose scrap such as appliances (no pressure or gas bottles) is placed on the feeding device which then tips it down under the two rollers.

The rollers (operator controlled) feed the car/scrap into the shredder where the rotor (spinning at approximately 600 rpm with 16 hammers at 280 lbs.) cuts it up and discharges the fist-sized pieces down to the discharge oscillator.

The smoke and dust from the shredder are carried up the pipe at the discharge of the shredder to the cyclone and then to the scrubber. The solids are discharged from the bottom of the cyclone, through an airlock, the the trash conveyor where it will be carried to a landfill.

The shredded scrap and trash are carried up the conveyor to the Z-box where they are exposed to a strong suction. This suction carries away almost all of the light weight trash (upholstery, etc.). The solids are discharged through the air lock onto the conveyor.

Most (75% approximately) of the air used in the Z-box is recirculated back through the bottom of the box. The other 25% is vented to the atmosphere.

The water used in the scrubber is recirculated from the in-ground tank which will be cleaned at some regular interval (30 to 60 days).

The now clean shredded scrap is fed from the Z-box to the drum magnet by the oscillator where the main product, shredded steel scrap, is carried over to the stocking conveyor. This conveyor then will discharge either onto a stockpile or directly into a railcar.

The non-magnetic fraction that is not picked up by the drum magnet falls onto the conveyor. This mixture has approximately 50% non-ferrous metals (zinc, aluminum, copper, etc.), and 50% heavy trash (rubber, wood, glass, etc.). It is cleaned by means of the trommel screen which drops out most of the minus 1/2" material (principally glass, rubber, and dirt), which will be transported to a landfill.

The non-ferrous material is discharged from the trommel to the rubber separator where much of the rubber and wood is separated. This rubber, etc., will be transported to a landfill and the non 70%+ non-ferrous metals are sold as-is.

The complete process takes junk cars and other types of light scrap and, through shredding and separation, yields about 80% as scrap steel/iron, 17% trash (carried to a landfill) and 3% non-ferrous metals.

3.0 SUMMARY OF TEST RESULTS

The particulate test results for the wet scrubber are presented in Table 3-1, and the opacity observation for the wet scrubber, and Diesels 1 and 2 results are presented in Table 3-2.

4.0 DISCUSSION OF TEST RESULTS

The test results from Tables 3-1 and 3-2 for the wet scrubber and Diesels 1 and 2 are compared with the permit limitations as shown in Table 3-1. It can be concluded that:

1. The wet scrubber and Diesels 1 and 2, have met opacity permit limitations
2. The wet scrubber has met particulate emissions permit limitations.

FIGURE 2-1

YORKE DOLINER
PROCESS FLOW DIAGRAM
NEW Z BOX SYSTEM

Particulate Matter
6 lb/hr (from stack tests)

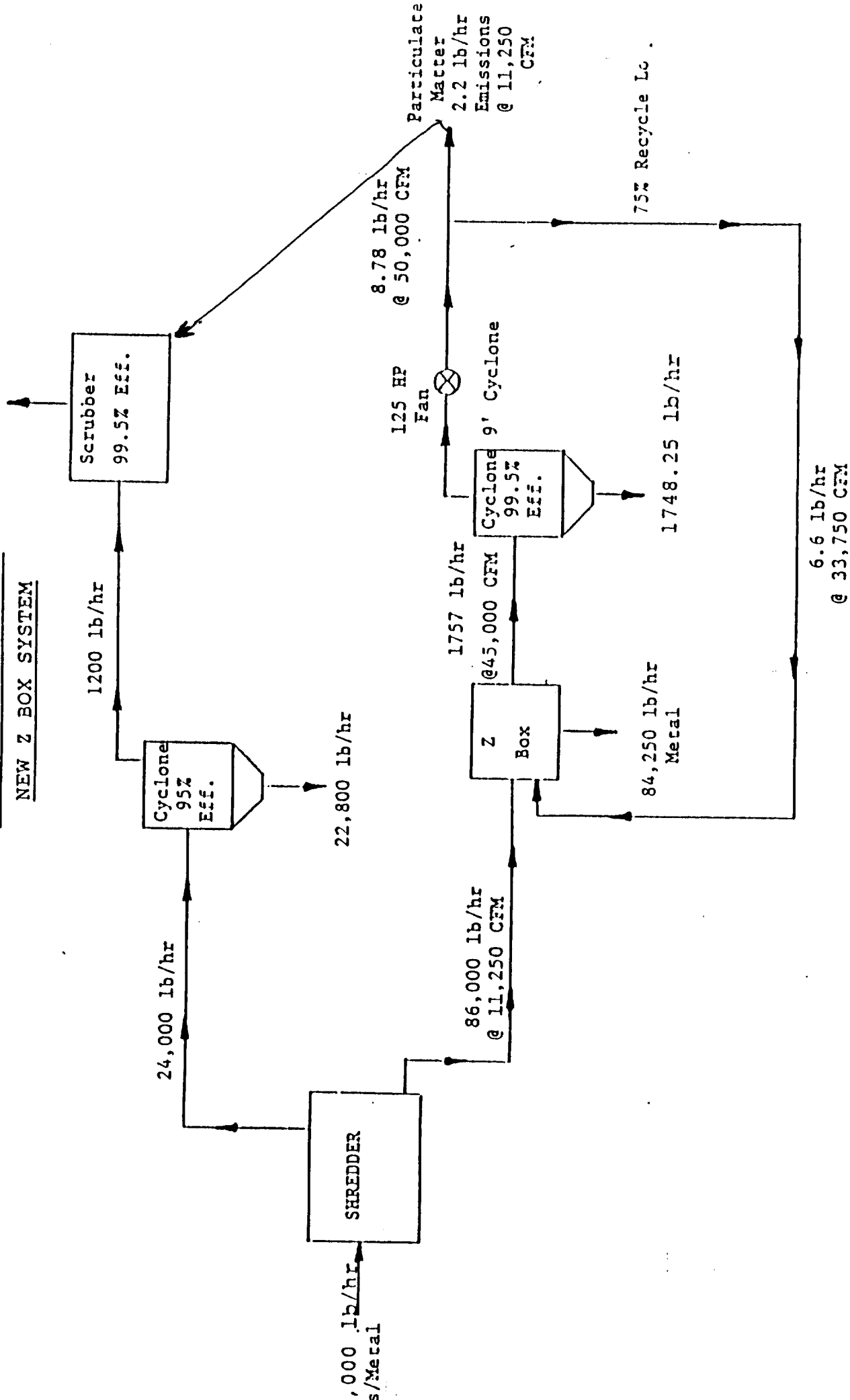


TABLE 3-1

WET SCRUBBER TEST RESULTS FOR PARTICULATES

STACK NO. (VENT)	RUN NO.	PROCESS WEIGHT (TPH)	EMISSIONS		ISOKINETICS (%)
			LBS./HR.	LBS./TON	
Wet Scrubber	1	60.5	3.00	0.0165	99
Wet Scrubber	2	63.8	4.25	0.0157	102
Wet Scrubber	3	51.7	3.92	0.0193	108

Strauss
~ 45TPH

13.5/hr
TPH
16.5/hr

32 lbs/hr

TABLE 3-2
VISIBLE EMISSION ON WET SCRUBBER
AND
DIESELS 1 AND 2

STACK NO. (VENT)	TIME OF OBSERVATION	AVERAGE OPACITY (%)
Wet Scrubber	10:07-11:07 a.m.	2.29
Diesel No. 1	10:07-11:07 a.m.	11.45
Diesel No. 2	10:07-11:07 a.m.	10.00

TABLE 4-1
WET SCRUBBER AND DIESELS 1 AND 2
COMPLIANCE EMISSIONS

SOURCE	TYPE EMISSION		TEST DATE	PERMIT LIMITATION	
	% AVERAGE OPACITY	AVERAGE PARTICULATE		% AVERAGE OPACITY	AVERAGE PARTICULATE
Wet Scrubber	2.29	3.72 lb/hr	10/26/87	5% _≤	32.87 lb/hr
Diesel #1	11.45	N/A	10/26/87	<20	N/A
Diesel #2	10	N/A	10/26/87	<20	N/A

SUMMARY OF TEST DATA.Plant: Yorke DolinerUnit Tested: Auto ShredderTest Date: 26 October 1987Run Number (s) 1 - 3

	# 1	# 2	# 3
Date	<u>26 Oct</u>	<u>26 Oct</u>	<u>26 Oct</u>
Start Time	<u>0830</u>	<u>1004</u>	<u>1148</u>
End Time	<u>0932</u>	<u>1114</u>	<u>1255</u>
Stack Diameter, inches	<u>48</u>	<u>48</u>	<u>48</u>
Nozzle Diameter, inches	<u>0.248</u>	<u>0.184</u>	<u>0.184</u>
Test Time, minutes	<u>60</u>	<u>60</u>	<u>60</u>
Number of Test Points, per run	<u>24</u>	<u>24</u>	<u>24</u>
Stack Gas Temperature, deg. F	<u>96</u>	<u>103</u>	<u>111</u>
Stack Gas Moisture Content, %	<u>3</u>	<u>4</u>	<u>4</u>
Stack Gas Molecular Weight	<u>28.67</u>	<u>28.56</u>	<u>28.56</u>
Stack Gas Volume Sampled, CF	<u>51.23</u>	<u>30.93</u>	<u>33.23</u>
Volume Sampled, SCF @ 68 deg. F	<u>50.13</u>	<u>29.76</u>	<u>31.56</u>
Stack Gas Velocity, FPS	<u>45.09</u>	<u>47.21</u>	<u>48.13</u>
Stack Gas Flowrate, ACFM	<u>33,980</u>	<u>35,577</u>	<u>36,271</u>
Stack Gas Flowrate, SCFM @ 68 deg.F	<u>31,299</u>	<u>32,029</u>	<u>32,196</u>
Particulate Collected, grams	<u>0.0364</u>	<u>0.0299</u>	<u>0.0290</u>
Part. Concentration, grains/scf	<u>0.0112</u>	<u>0.0155</u>	<u>0.0142</u>
Pollutant Mass Rate, lb/hr	<u>3.00</u>	<u>4.25</u>	<u>3.92</u>
Percent Isokinetic of Test	<u>99</u>	<u>102</u>	<u>108</u>
	<u> </u>	<u> </u>	<u> </u>
	<u> </u>	<u> </u>	<u> </u>

Field Data and Samples under control of:

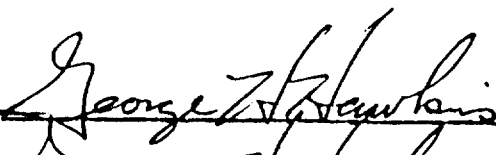


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5.0 PARTICULATE TESTING SUMMARY

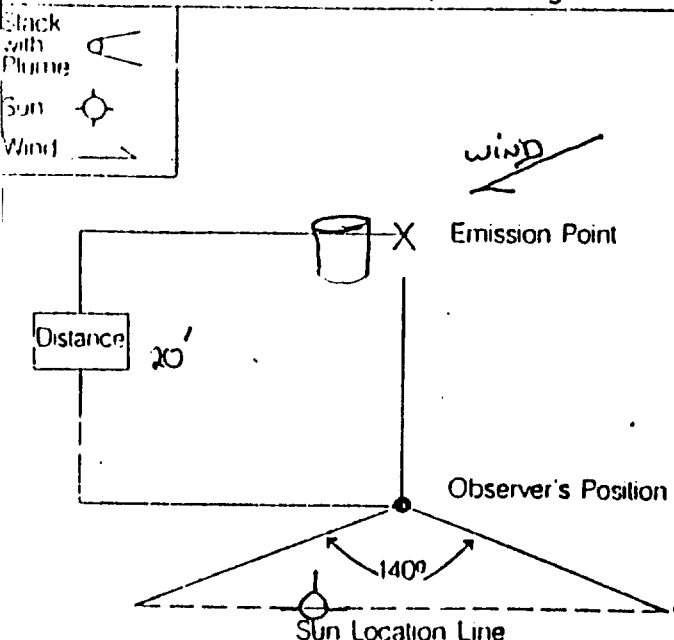
6.0 OPACITY MEASUREMENT FIELD REPORTS

Visible Emissions Observation Form

CEMP/FORM E
STATUS

15 10 10

Source/Process Information				Opacity Readings									
Source Name				OBSERVATION DATE				START TIME				STOP TIME	
YORKE DOLIVER AND COMPANY				10-26-87				10:07AM				11:07AM	
PERMIT NO.				SEC				MIN				SEC	
A005-111877				0 15 30 45				0 15 30 45				0 15 30 45	
ADDRESS				MIN				MIN				MIN	
NOVA INDUSTRIAL PARK, U.S. HIGHWAY 1, ROCKLEDGE, FLA				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
CONTACT				MIN				MIN				MIN	
Dan Smith				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
TELEPHONE				MIN				MIN				MIN	
1-305-636-2781				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
PROCESS OR PRODUCTION RATE				MIN				MIN				MIN	
58 CARS x 2200 lb/hr 23.8 Ton/hour				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
CENTRAL EQUIPMENT				MIN				MIN				MIN	
WET SCRUBBER				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
OPERATING MODE				MIN				MIN				MIN	
ON				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
FUEL TYPE				MIN				MIN				MIN	
N/A				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
EMISSIONS POINT				MIN				MIN				MIN	
Cylindrical Vent Stack				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
HEIGHT ABOVE GROUND LEVEL				MIN				MIN				MIN	
45 ft				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
HEIGHT RELATIVE TO OBSERVER				MIN				MIN				MIN	
36 ft				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Emissions Description				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Color				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
White				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Intermittent Slight Gray Smoke				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Plume Type				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Same				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Slight Grey-White				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Water Condensate Present				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Yes ☐ No ☒				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
If Yes Is Plume				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Attached ☐ Detached ☐				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Meteorological Information				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Sky Condition				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Overcast				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Cloud Color				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Grey-White Cloud				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Cloud Cover				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Partly Cloudy				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Wind Speed				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
5-10 Variable				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Wind Direction				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
NE				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	
Observation Data, Site Diagram				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45				1 5 10 15 20 25 30 35 40 45	



Comments: Permit 5% ≤ ; Production Permit Avg 2.3%

Water Flow Meter — 200 GPM

Water Pressure Gauge — 70 PSI

CARS PROCESSED — 58

Weight / CAR — 2200

STATE OF FLORIDA
DEPARTMENT OF ENVIRONMENTAL REGULATION

THIS IS TO CERTIFY THAT

GREGORY GONZALES HAS COMPLETED THE
STATE OF FLORIDA VISIBLE EMISSIONS EVALUATION TRAINING
EPA REFERENCE METHOD 9.
THIS CERTIFICATE EXPIRES Mar 10, 1988

Visible Emissions Observation Form

COMPLIANCE STATUS

YES NO N/A

Source/Process Information				Opacity Readings										
Source Name YORKE DOLIVER AND COMPANY				OBSERVATION 10-26-87				START TIME 10:07 AM				STOP TIME 11:07 AM		
FUEL TYPE Diesel No. 1		PERMIT NO. A005-123074		SEC	0	15	30	45	MIN	SEC	0	15	30	45
ADDRESS NOVA INDUSTRIAL PARK, U.S. Highway 1 Rockledge FLA.				1	10	10	10	10	11	10	15	15	5	
CONTACT DAN SMITH				2	5	5	5	5	12	5	5	15	5	
PHONE NO. 1-305-636-2781				3	5	5	5	5	13	5	0	10	0	
FUEL TYPE RATE				4	5	5	5	10	14	0	15	5	10	
FUELS TYPE RATE				5	5	5	10	10	15	5	0	10	10	
OPERATING MODE ON				6	10	5	5	5	16	0	10	15	5	
Emissions Description Exhaust Stack				7	0	5	5	5	17	5	5	5	0	
HEIGHT ABOVE GROUND LEVEL 35 FT				8	10	10	10	5	18	5	10	5	5	
HEIGHT RELATIVE TO OBSERVER 15 FT				9	15	5	5	10	19	5	5	5	5	
Emissions Description Intermittent Grey Smoke				10	10	10	5	0	20	5	5	5	5	
PLUME TYPE Greyish black intermittent				11	5	5	10	15	21	0	0	5	10	
IF YES IS PLUME N/A				12	15	15	0	10	22	5	15	0	5	
ATTACHED ☐ DETACHED ☐				13	15	15	10	10	23	5	5	5	15	
METEOROLOGICAL INFORMATION				14	15	5	0	5	24	5	5	0	0	
OVERCAST				15	0	10	10	5	25	0	5	15	5	
Grey white cloud				16	10	10	5	5	26	10	5	0	5	
Scattered				17	5	0	5	0	27	10	15	10	5	
Partly cloudy				18	10	0	5	10	28	5	5	5	5	
5-10 Variable				19	5	5	5	10	29	5	5	5	5	
Wind				20	0	5	5	5	30	0	10	5	10	
Wind direction				21	5	0	5	5	31	5	10	10	15	
Wind speed				22	5	0	5	0	32	5	0	5	5	
Wind direction				23	5	5	10	0	33	10	5	5	0	
Wind speed				24	0	5	5	5	34	5	5	5	5	
Wind direction				25	0	0	5	5	35	0	5	5	5	
Wind speed				26	5	5	5	5	36	5	5	5	5	
Wind direction				27	5	15	10	10	37	5	5	5	5	
Wind speed				28	5	5	5	5	38	5	10	10	15	
Wind direction				29	5	5	5	5	39	5	5	5	5	
Wind speed				30	5	5	5	5	40	5	5	5	5	

Comments:

Type Fuel - NO. 2

Heat Input - 4.29 mm BTU / hour

6 min high avg opacity 11.45%

Permit limitation 20% ≤

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EPA REFERENCE METHOD 9.
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Visible Emissions Observation Form

COMPLIANCE
STATUS
YES NO N/A

Source/Process Information				Opacity Readings										
YORKE DOLIVER AND COMPANY				OBSERVATION 10-26-87				START TIME 10:07AM				STOP TIME 11:07AM		
FUEL TYPE		PERMIT NO		SEC	0	15	30	45	MIN	SEC	0	15	30	45
Diesel NO. 2		A005-123074		1	10	10	10	10	11	10	10	10	10	5
NOVA INDUSTRIAL PARK, U.S. HIGHWAY 1, ROCKLEDGE, FLA.				2	5	5	5	5	12	0	5	10	5	
CONTACT: DAN SMITH		PHONE NO: 1-305-636-2781		3	5	5	5	5	13	5	0	15	5	
FUEL TYPE: RATE		MATERIAL TYPE: RATE		4	5	5	5	10	14	0	15	5	5	
PERMITTED RATE		OPERATING MODE		5	5	5	10	10	15	5	0	10	10	
EXHAUST STACK				6	10	5	5	5	16	0	5	15	5	
HEIGHT ABOVE GROUND LEVEL: 35 FT		HEIGHT RELATIVE TO OBSERVER: 15 FT		7	0	5	5	5	17	5	5	5	0	
Emissions Description				8	10	10	10	5	18	5	5	10	5	
INTERMITTENT GREYISH-BLACK				9	15	5	5	10	19	5	5	5	5	
GREYISH BLACK INTERMITTENT				10	10	10	10	0	20	5	5	5	5	
IF YES IS PLUME				11	0	5	10	15	21	0	0	5	5	
ATTACHED ☐ DETACHED ☐				12	15	15	0	15	22	5	15	0	5	
METEOROLOGICAL INFORMATION				13	10	10	10	10	23	5	5	5	15	
OVERCAST				14	10	10	0	5	24	5	5	0	0	
GREY-WHITE CLOUD				15	0	5	10	5	25	0	10	5	5	
PARTLY CLOUDY				16	5	5	5	5	26	5	10	10	10	
5-10 VARIABLE				17	5	0	5	0	27	5	5	5	5	
NE				18	5	5	5	5	28	5	5	5	5	
NE				19	5	0	5	5	29	5	5	5	5	
NE				20	5	5	5	5	30	5	5	5	5	
NE				21	0	5	0	0	31	0	10	10	5	
NE				22	5	0	5	10	32	5	10	10	10	
NE				23	0	5	5	0	33	5	0	0	10	
NE				24	5	0	0	0	34	15	5	5	0	
NE				25	0	5	10	5	35	5	5	5	5	
NE				26	0	0	5	5	36	0	0	0	5	
NE				27	5	5	5	5	37	0	5	5	5	
NE				28	5	15	10	10	38	5	5	5	5	
NE				29	5	0	5	5	39	5	5	5	5	
NE				30	0	5	5	5	40	15	5	5	5	

Comments:

Type Fuel - NO. 2

Heat Input - 4.29 mmBTU / hour

2 min high run avg opacity 10 %

Permit Limitation 20 %

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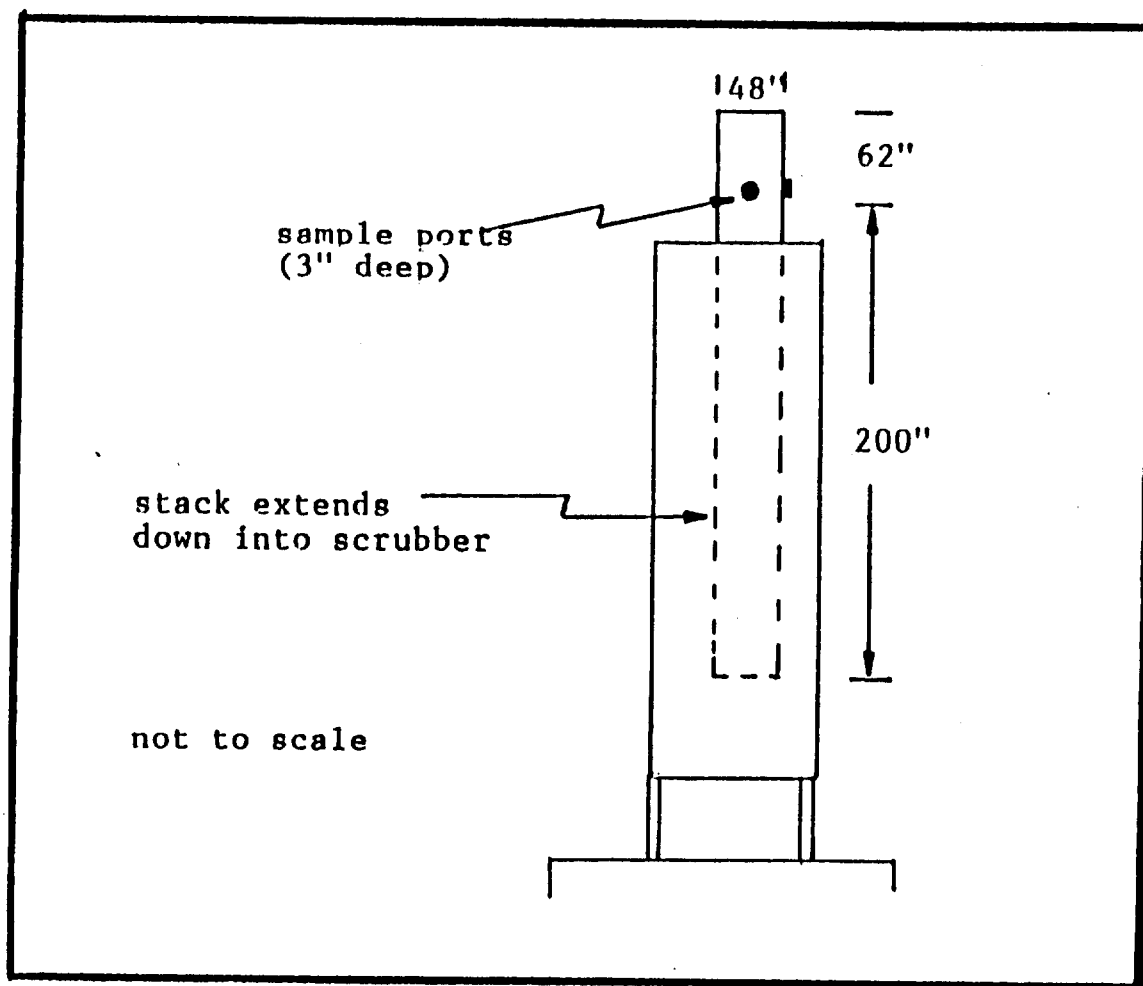
7.0 STACK CONFIGURATION

YORKE DOLINER
ROCKLEDGE, FLORIDA

AUTO SHREDDER

The auto shredder has tested at two sample ports which are located at 90° to each other. The ports are located 4.2 stack diameters down stream and 1.3 stack diameters up stream from any obstruction or opening. Each sample port was tested at 12 test points for 2.5 minutes per test point for a total of 24 test points and 60 minutes per test run. The location of the test points in relation to the stack wall is listed below.

point distance		point distance	
1	1.0"	7	30.9"
2	3.2"	8	36.0"
3	5.7"	9	39.5"
4	8.5"	10	42.3"
5	12.0"	11	44.8"
5	17.1"	12	47.0"



8.0 PARTICULATE TESTING PROCEDURE

FIELD AND ANALYTICAL PROCEDURES

SAMPLING

The sampling equipment consisted of the following:

1. Pitobe Assembly

- a. Nozzle - Stainless steel with a sharp, tapered leading edge.
- b. Probe - Stainless steel sheath with a 5/8-inch OD stainless steel insert wrapped with nichrome wire. Rheostat controlled and capable of maintaining a minimum temperature of 250°F.
- c. Pitot - Type "S" constructed and attached to probe according to specifications outlined in Part 60 of Chapter 1 of Title 40 of the Code of Federal Regulations, Appendix A, Method 2 as amended August 18, 1977.
- d. Orsat Probe - Stainless steel 1/4-inch tubing attached to pitot tube in an interference-free arrangement.
- e. Thermocouple - Type "K" attached to the pitot tube such that the tip has no contact with metal and does not interfere with the pitot tube face openings.

2. Filter Holder - Pyrex glass with fritted glass filter support.

3. Filter Heating Assembly - Controlled heating element in aluminum module attached to end of probe; capable of maintaining 250°F±°F.

4. Impingers - Four impingers connected in series with glass ball joint fittings and placed in an ice bath. The first, third, and fourth impingers are the modified Greenburg-Smith design. The second impinger is the Greenburg-Smith design with a standard tip. Final gas exit temperature is measured to within ±5° with a dial thermometer immersed in the gas stream.

5. Control Box - Module containing vacuum gauge, leak-free pump, thermometers capable of measuring temperature to within ±5°, dry gas meter with a minimum of 2 percent accuracy, valves, and related equipment as required to maintain an isokinetic sampling rate and to determine sample volume.

6. Nemograph - To determine isokinetic sampling rate.

A schematic of the sampling train is enclosed. (p.19)

Prior to leaving the laboratory, glass fiber filters had been numbered for identification, heated for 2 hours at 105°C, desiccated for 2 hours, and preweighed to the nearest 0.1 mg. Silica gel (indicating type, 6-16 Mesh) had also been preweighed to approximately 200 grams after drying for 2 hours.

Upon arrival at the sampling site, the control box was leak-checked from pump to orifice at 5 to 7 inches of water.

The sample train was prepared in the following manner: 125 ml of distilled water was added to each of the first two impingers. The third impinger was left empty to act as a moisture trap, and the preweighed silica gel was added to the fourth impinger. After assembling the train with the pitotube as shown in the schematic, the system was leak-checked by plugging the inlet to the probe nozzle and pulling a 15-inch Hg vacuum. A leakage rate not in excess of 0.02 cfm was considered acceptable. The pitot tube system was also leak-checked at 5 to 7 inches of water, and any leaks found were corrected.

The inside dimensions of each stack were measured and recorded. The number of sampling points and the location of these points on a traverse were determined by the guidelines set forth in the Federal Register, Vol. 36, No. 247, Sec. 60.85, Method 1. These points were then marked on the probe for easy visibility.

A preliminary traverse was conducted to determine the range of velocity head and the pressure of the stack. A wet bulb and a dry bulb temperature were taken to determine stack temperature and moisture. From this data, the correct nozzle size and the nemograph correction factor were determined. The correct nozzle tip was measured to within 0.001 in. and recorded on the data sheet.

The probe was attached and the heater was adjusted to provide a gas temperature of approximately 250°F. The filter heating system was turned on, and crushed ice was placed around the impingers. After a suitable warmup period, the nozzle was placed on the first traverse point with the tip point directly into the gas stream. The pump was started immediately, the flow was adjusted to isokinetic conditions. After the required time interval had elapsed, the probe was repositioned to the next traverse point, and isokinetic sampling was reestablished. This was done for each point on the traverse until the run was completed. Reading of stack conditions were taken at least every six minutes or when significant changes in stack conditions necessitated additional adjustments in flow rate. At the conclusion of each run, the pump was turned off and the final readings were recorded.

A final leak check of the system was performed as previously described at the highest vacuum encountered during testing and a leak check of the pitot system was repeated.

PARTICULATE SAMPLE RECOVERY

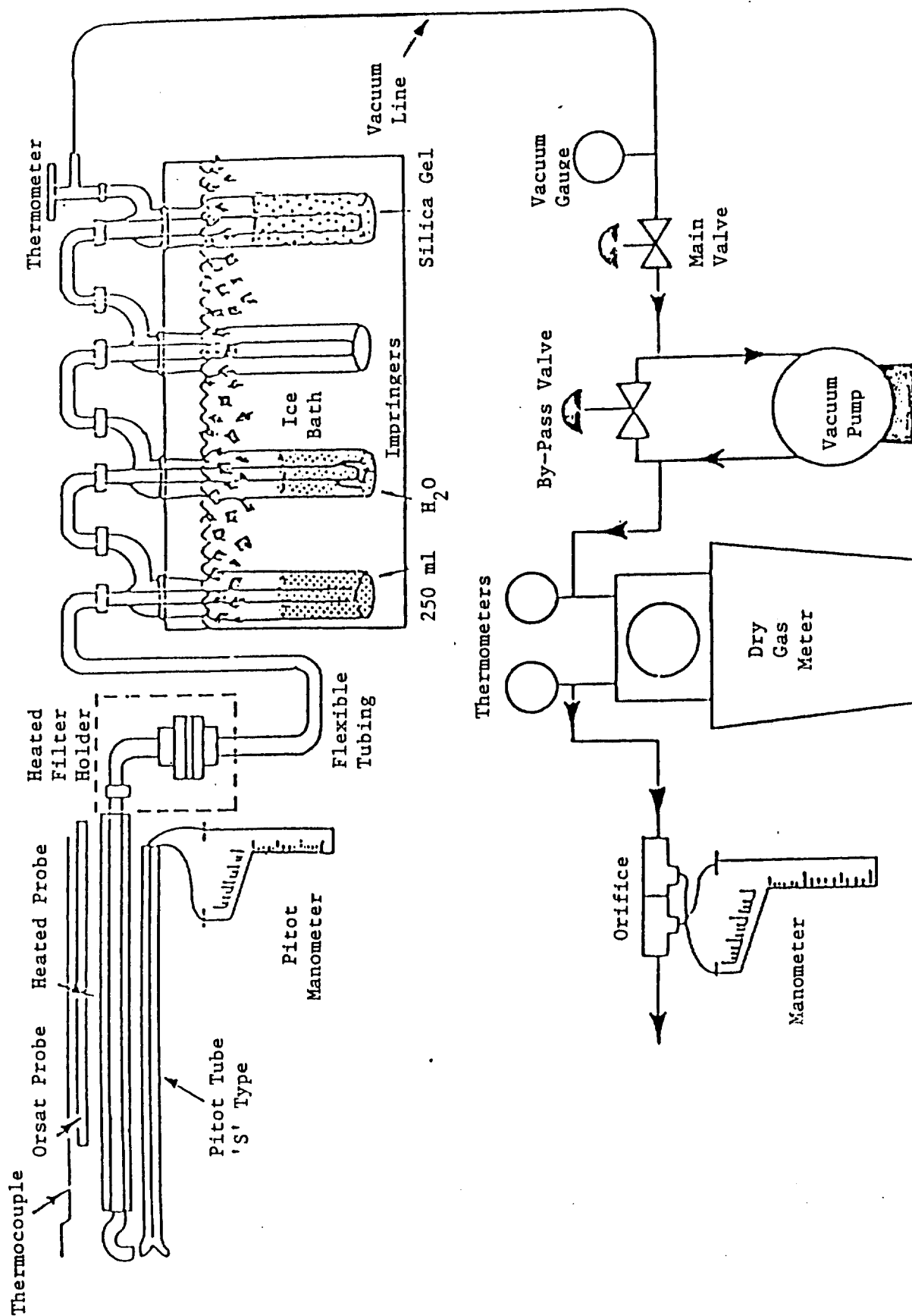
Care was exercised in moving the collection train to the sample recovery area to minimize the loss of collected sample or the gain of extraneous particulate matter. The volume of water in the first three impingers was measured and recorded on the field data sheet. The probe, nozzle, and all sample-exposed surfaces were washed with reagent grade acetone and put into a clean sample bottle marked "prefilter." A brush was used to loosen any adhering particulate matter, and subsequent washings were put into the "prefilter" container. The filter was carefully removed from the fritted glass support and placed in its original container.* The silica gel was removed from the fourth impinger and transferred to its original container. A sample of the acetone used in washing the probe was saved for a blank laboratory analysis.

PARTICULATE ANALYTICAL PROCEDURES

The filter and any loose particulate matter were transferred from the sample bottle to a clean, tared glass weighing dish. The filter was placed in an oven at 105°C for 2 hours, desiccated for 2 hours, and then weighed. The original weight of the filter was deducted, and the weight gain was recorded to the nearest 0.1 mg.

The "prefilter" and blank solutions were transferred to clean, tared beakers, evaporated to dryness, and desiccated to a constant weight. The blank correction was made, and the weight gain was recorded to the nearest 0.1 mg. The silica gel was weighed, and the weight gain was recorded to the nearest 0.1 gram.

* When practical, samples are changed out upon return to laboratory.



METHOD 5 SAMPLING TRAIN

9.0 PARTICULATE TESTING FIELD DATA SHEETS

FIELD DATA SHEET

PLANT Yonkers District UNIT TESTED Bata building DATE 26 Oct 87 RUN NUMBER 1

OPERATOR Hankins, Patterman AMBIENT Temperature 70's Barometric Pressure 29.92

Stack Diameter 48" Probe Length 6' Probe Heater Setting 0 Nozzle Number A 1/4

Assumed Moisture 6% Number of Points 24 Heater Box Setting 250 Nozzle diameter .248

START TIME 0830 Filter Number 1 Pitot Corr. Factor 0.84 Meter Box Number A-1

END TIME 0932 "C" factor/nomograph 1.00 Meter Box DH # 1.80

***** LEAK CHECKS *****	PITOT TUBE (inlet & outlet)	VACUUM LINE
	a) ✓	a) OK at 16"
	b) ✓	b) OK at 9"

TRAVERSE POINT	SAMPLING TIME (θ), min.	STATIC PRESSURE in. of H ₂ O	STACK TEMPERATURE (T _s), F	Velocity Head (Dps) ($\sqrt{Dps}$) ²	Pressure Differential Meter (DH) in. of H ₂ O	GAS VOLUME SAMPLED (V _m) ft ³	GAS METER TEMPERATURE Inlet θ Outlet θ	SAMPLE BOX TEMPERATURE	TEMPERATURE OF LAST IMPINGER	PUMP VACUUM in. of Hg
1-1	0		.93	.64 .80	2.40	383.645	.74 .74	238	<60	<4
2	2.5			.64 .80	2.40	386.0				
3	5		.93	.66 .81	2.60	388.0	.75 .74	232	<60	<4
4	7.5	.14		.72 .85	2.80	390.0				
5	10		.94	.72 .85	2.80	393.06	.75 .74	242	56	<4
6	12.5			.70 .84	2.70	394.8				
7	15		.93	.64 .80	2.40	397.0	.74 .74	240	54	<4
8	17.5			.64 .80	2.38	398.98				
9	20		.94	.62 .79	2.30	401.0	.74 .73	240	52	<4
10	22.5			.60 .77	2.20	402.91				
11	25		.96	.58 .76	2.15	404.88	.74 .73	238	50	<5
12	27.5			.54 .73	2.00	406.99				
1	30		.97	.66 .81	2.50	409.035	.75 .73	240	48	<6
2	32.5			.66 .81	2.50	411.15				
3	35		.95	.68 .82	2.55	413.59	.75 .73	242	48	<6
4	37.5			.68 .82	2.55	415.0				

1

RUN

[illegible]

PLANT Yorke Polymer UNIT TESTED Rato Shredder DATE 26 Oct 87 RUN NUMBER 2
 OPERATOR Hawkins, P. Henson AMBIENT Temperature 70's Barometric Pressure 29.92
 Stack Diameter 48" Probe Length 6' Probe Heater Setting -0- Nozzle Number 1316
 Assumed Moisture 2.5% Number of Points 24 Heater Box Setting 250 Nozzle diameter .185 > 0.18
 START TIME 1004 Filter Number 2 Pitot Corr. Factor 0.84 Meter Box Number 111
 END TIME 1114 "C" factor/nomograph 0.98 Meter Box DH # 1.80
 ***** LEAK CHECKS ***** PITOT TUBE (inlet & outlet) a) ✓ VACUUM LINE c) OK at 12"
b) ✓ b) OK at 10"

TRAVERSE POINT	SAMPLING TIME (θ), min.	STATIC PRESSURE in. of H ₂ O	STACK TEMPERATURE (T _s), °F	Velocity Head (Dps) ($\sqrt{Dps}$)	Pressure Differential Across Orifice Meter (DH) in. of H ₂ O desired (DH)	GAS VOLUME SAMPLED ₃ (V _m) ft ³	GAS METER TEMPERATURE Inlet Outlet	SAMPLE BOX TEMPERATURE	TEMPERATURE OF LAST IMPINGER	PUMP VACUUM in. of Hg
1-1	0		.103	.62	.79	436.080	.77	77	52	24
2	2.5			.64	.80	437.0				
3	5		.101	.66	.81	439.03	.77	77	50	24
4	7.5			.66	.81	440. -				
5	10		.100	.68	.82	441.55	.78	77	50	24
6	12.5			.68	.82	442.805				
7	15		.102	.70	.84	444.08	.79	78	50	25
8	17.5			.68	.82	445.37				
9	20		.102	.68	.82	446.65	.81	79	48	25
10	22.5			.64	.80	447.9 -				
11	25		.101	.64	.80	449.04	.83	79	46	24
12	27.5			.60	.77	450.02				
2-1	30		.105	.64	.80	451.545	.83	80	44	26
2	32.5			.66	.81	452.70				
3	35		.105	.68	.82	454.0	.83	81	44	26
4	37.5			.68	.82	455.415				

DATE 26 Oct 1987 RUN # 2

DATE 26 Oct 1987 RUN # 2

DATE 26 Oct 1987 RUN # 2

TRAVERSE POINT	SAMPLING TIME (s)	STATIC PRESSURE	STACK TEMPERATURE (Ts), °F	VELOCITY HEAD (Dps) (NDps)	ACTUAL DESIRED (Dh) (Dh)	PRESSURE ACROSS ORIFICE AFTER METER	GAS VOLUME SAMPLED (Vm) ft ³	GAS METER TEMPERATURE °F INLET OUTLET	SAMPLE BOX TEMPERATURE	TEMPERATURE OF LAST IMPINGER	PUMP VACUUM IN. of Hg
5	40		104	.70 .84	.85		456.64	.84 82	246	46	44
6	42.5			.70 .84	.85		457.98				
7	45		104	.68 .82	.82		459.4	.86 83	246	46	44
8	47.5			.68 .82	.82		460.6				
9	50		103	.66 .81	.80		461.3	.88 84	246	48	45
10	53.5			.66 .81	.80		463.3				
11	55		104	.64 .80	.76		464.6	.89 84	248	46	45
12	57.5			.64 .80	.76		465.7				
	60		103	— —	—		467.010	.90 84	—	—	—
			103	0.81	0.39		30.930	82			

PLANT Yorba Linda UNIT TESTED Auto Shredder DATE 26 Feb 87 RUN NUMBER 3
 OPERATOR Hawkins AMBIENT Temperature 80's Barometric Pressure 29.92
 Stack Diameter 48" Probe Length 6' Probe Heater Setting 0-1 Nozzle Number 14316
 Assumed Moisture 62 Number of Points 24 Heater Box Setting 250 Nozzle diameter 0.184
 START TIME 1148 Filter Number 3 Pitot Corr. Factor .84 Meter Box Number 14-1
 END TIME 1255 "C" factor/nomograph 100 Meter Box DH # 1.88

***** LEAK CHECKS ***** PITOT TUBE (inlet & outlet) c) ✓ VACUUM LINE a) OK at 16"
b) ✓ b) OK at 10"

TRAVERSE POINT	SAMPLING TIME (θ), min.	STATIC PRESSURE In. of H ₂ O	STACK TEMPERATURE (T _s), F	Velocity Head (Dp _s) ($\sqrt{Dp_s}$)	Pressure Differential Across Orifice (DH) actual (DH) desired In. of H ₂ O	GAS VOLUME SAMPLED ₃ (V _m) ft ³	GAS METER TEMPERATURE Inlet Outlet	SAMPLE BOX TEMPERATURE	TEMPERATURE OF LAST IMPINGER	PUMP VACUUM In. of Hg
1-1	0		.118	.66 .81	.80	466.405	.89 .89	258	<60	<4
2	3.5			.66 .81	.80	469.1				
3	5		.119	.70 .84	.84	470.9	.89 .89	253	<60	<4
4	7.5	.16		.76 .87	.92	472.33				
5	10		.116	.76 .87	.92	473.71	.90 .89	258	48	<4
6	12.5			.74 .86	.88	475.0				
7	15		.117	.74 .86	.88	476.1	.89 .89	258	48	<4
8	17.5			.66 .81	.80	477.8				
9	20		.114	.66 .81	.80	479.09	.90 .89	260	46	<5
10	22.5			.64 .80	.76	480.37				
11	25		.111	.64 .80	.76	481.64	.90 .88	258	48	<5
12	27.5			.60 .77	.72	482.92				
1	30		.110	.64 .80	.76	484.145	.90 .88	256	<50	<4
2	32.5			.64 .80	.76	485.24				
3	35		.110	.66 .81	.80	487.0	.90 .88	252	<50	<4
4	37.5			.66 .81	.80	488.0				

[illegible]

10.0 PARTICULATE TESTING LABORATORY WORK SHEET

LABORATORY WORKSHEET

Plant Yorke Delineer
Source Auto shredder

RUN# 1
Date 26 Oct 87

A. Weight of Water Collected

Impinger NO. all Dessicant NO. 1
Final Wt. 760.0 gms
Initial wt. 744.5 gms
difference 12 ml 15.5 gms

Total volume collected = (gms water)+(gms dessicant) = 27.5 gms

B. Weight of particulate collected in probe wash

Container NO. 1 into dish NO. 523 Blank dish NO.
Date/Time of wt. 28 Oct 87 gross wt 22.2473 gms Apr 87 lat gms
tare wt 22.2276 gms gms
less acetone blank wt .0002 gms + 0.0002 blank wt
Weight of particulate in wash 0.0195 gms

C. Weight of particulate collected on filter

FILTER NO. 1 BLANK
Date/time of wt. 28 Oct 87 gross wt. 0.4252 0.4091 gms
less tare wt. 0.4084 0.4092 gms
+ less blank wt. 0.0001 (-) 0.0001 blank
Total weight collected wt. 0.0169

Total particulate collected on all filters 0.0169 gms

Plus weight of particulate in probe wash 0.0195 gms

Total wt. 0.0364 gms

Signature of Analyst George Hawkins

LABORATORY WORKSHEET

Plant Yorker Bohner
Source auto shredder

RUN# 2
Date 26 Oct '87

A. Weight of Water Collected

Impinger NO. all Dessicant NO. 2
Final Wt. 708.3 gms
Initial wt. 701.1 gms
difference 7.2 gms

Total volume collected = (gms water) + (gms dessicant) = 27.2 gms

B. Weight of particulate collected in probe wash

Container NO. 522 into dish NO. 522 Blank dish NO.
Date/Time of wt 280 0630 gross wt 22.9929 gms
tare wt 22.9766 gms see #1 gms
less acetone blank wt .0002 gms blank wt

Weight of particulate in wash 0.0161 gms

C. Weight of particulate collected on filter

FILTER NO. 2 BLANK
Date/time of wt. 280 0630 gross wt. .4223 gms
less tare wt. .4086 gms see #1 gms
+ less blank wt. 0.0001 blank
Total weight collected wt. 0.0138

Total particulate collected on all filters 0.0138 gms

Plus weight of particulate in probe wash 0.0161 gms

Total wt. 0.0299 gms

Signature of Analyst George H. Perkins

LABORATORY WORKSHEET

Plant Yorke Doliner
Source auto shredder

RUN# 3
Date 26 Oct 87

A. Weight of Water Collected

Impinger NO. all Dessicant NO. 3
Final Wt. 744.3 gms
Initial wt. 736.4 gms
difference 18 7.9 gms

Total volume collected = (gms water)+(gms dessicant)=25.9 gms

B. Weight of particulate collected in probe wash

Container NO. 3 into dish NO. 87 Blank dish NO. -
Date/Time of wt 2800630 gross wt 28.4924 gms gms
tare wt 22.4771 gms see #1 gms
less acetone blank wt .0002 gms blank wt

Weight of particulate in wash 0.0151 gms

C. Weight of particulate collected on filter

FILTER NO. 3 BLANK
Date/time of wt. 2800630 gross wt. 0.4400 gms
less tare wt. 0.4262 see #1 gms
+ less blank wt. 0.0001 blank
Total weight collected wt. 0.0139

Total particulate collected on all filters 0.0139 gms

Plus weight of particulate in probe wash 0.0151 gms

Total wt. 0.0290 gms

Signature of Analyst George A. Shankin

11.0 PARTICULATE EMISSION CALCULATIONS

TERMS USED FOR CALCULATIONS:

- DP - AVERAGE PRESSURE ON PITOT TUBE
- TS - AVERAGE TEMPERATURE OF STACK, DEGREES ABSOLUTE
- TM - AVERAGE TEMPERATURE OF DRY GAS METER, DEGREES ABSOLUTE
- VM - VOLUME OF DRY GAS METER, ACTUAL CUBIC FEET
- θ - TOTAL TIME OF THE TEST RUN, MINUTES
- AN - AREA OF THE NOZZLE TIP, SQUARE FEET
- PB - BAROMETRIC PRESSURE
- DH - AVERAGE PRESSURE ON THE LIMITING ORIFICE
- VWC - VOLUME OF WATER COLLECTED FROM IMPINGERS AND SILICA GEL, GRAMS
- VMSTD - VOLUME OF THE DRY METER IN STANDARD CUBIC FEET
- BWO - PERCENT OF MOISTURE IN FLUE GAS
- MD - MOLECULAR WEIGHT OF DRY FLUE GAS
- MS - MOLECULAR WEIGHT OF FLUE GAS
- VS - VELOCITY OF FLUE GAS
- QS - VOLUMETRIC FLOW OF FLUE GAS, CUBIC FEET PER MINUTE
- QS STD- VOLUMETRIC FLOW OF FLUE GAS, STANDARD CUBIC FEET DRY
- %I - PERCENT OF THEORETICAL IDEAL SAMPLING RATE
- WT COLLECTED - TOTAL WEIGHT OF PARTICULATE COLLECTED BY
SAMPLING TRAIN, IN GRAMS
- DIAMETER AVERAGE - AVERAGE DIAMETER OF NOZZLE TIP, INCHES

Derivation of Constants on Calculation Sheet

Equation

A. Volume of water vapor collected

$$\text{Volume} = \frac{(\text{volume collected, grams})(p_w)(R)(T_{std})}{(P_{std})(M_w)}$$

$$\begin{aligned} \text{Volume} &= (\text{grams}) (0.02201, p_w)(21.85, R)(528, T_{std}) / (29.92, P_{std})(18, M_w) \\ \text{Volume} &= (\text{grams}) (0.0471) \end{aligned}$$

B. Converting to standard volume

$$V_{m\ std} = (V_m) \frac{T_{std}}{T_m} \frac{P_m^*}{P_{std}} \quad * P_m = (P_b + D_h / 13.6)$$

$$V_{m\ std} = (V_m) \frac{P_m}{T_m} \frac{528^\circ A}{29.92 \text{ "Hg}} = (V_m) \frac{P_m}{T_m} (17.65)$$

F. Stack gas velocity

$$\text{Pitot tube constant } (K_p) = 85.49 \text{ ft/s} \left[\frac{(1 \text{ lb/lb-mole})(\text{in. Hg})}{(^{\circ}R)(\text{in. H}_2\text{O})} \right]^{1/2}$$

G. same as B above

H. Isokinetic sampling rate

$$\%I = \frac{100 T_s V_{mstd} P_{std}}{60 \theta V_s P_s A_n T_{std} (1-B_{wo})}$$

$$\%I = \frac{T_s V_{mstd}}{\theta V_s P_s A_n (1-B_{wo})} \frac{(100)(29.92, \text{ "Hg})}{(60)(528^\circ A)} = 0.0945 \left[\text{etc.} \right]$$

J. Factor (0.00857) converts grains to pounds and flow per minute to flow per hour.

$$0.00857 = \frac{1}{(7000 \text{ grains/lb})} (60 \text{ min/hour})$$

*Area of nozzle

$$A_n = \frac{(3.14) \left[\frac{(\text{diameter, inches})}{2} \right]^2}{144 \text{ inches/sq. ft.}} = (0.0055)$$

Terms

R = ideal gas constant, 21.85 (in.Hg)(ft³) / (lb-mole)

Tstd = standard absolute temperature, 528°K

Pstd = standard absolute pressure, 29.92 in.Hg

Mw = molecular weight of water, 18.0 lb/lb-mole

pW = density of water, 0.002201 lb/ml

CALCULATIONS: PLANT Yorke Bolener RUN# 1
 SOURCE auto shredder DATE 26 Oct 87

A) Volume of water vapor collected

$$V_{wc} = (0.0471) (27.5 \text{ gm}) = 1.30$$

B) Volume of air metered to 68 deg.F, 29.92"Hg, dry

$$V_{mstd} = (17.64) (Y) (V_m) (P_m) / (T_m)$$

$$V_{mstd} = (17.64) (.986) (51.225) \frac{(30.10)}{(535)} = 50.13 \text{ cuft}$$

C) Moisture Content of Flue Gas

$$B_{wo} = \frac{V_{wc}}{V_{wc} + V_{mstd}} = \frac{1.30}{(50.13 + 1.30)} (100) = 3 \% H_2O$$

D) Dry Gas Molecular Weight

$$M_d = 0.44 (\% CO_2) + 0.32 (\% O_2) + 0.28 (\% N + \% CO)$$

$$M_d = 0.44 () + 0.32 () + 0.28 () = \text{assume } 29$$

E) Stack Gas Molecular Weight

$$M_s = M_d (1 - B_{wo}) + (18) (B_{wo}) = (29) (.97) + (18) (.03)$$

F) Stack Gas Velocity

$$M_s = 28.67$$

$$V_s = K_p C_p \sqrt{\frac{D_p}{P_s}} \sqrt{\frac{(T_s \text{ avg})}{M_s}} = (85.49) (.84) (0.78) \sqrt{\frac{(556)}{(29.93) (28.67)}} = 45.09 \text{ ft/sec}$$

G) Stack Gas Flowrate

$$Q_s = (60 \text{ sec/min}) (A_s) (V_s) = (60) (12.56) (45.09) = 33980 \text{ cuftmin}$$

$$Q_{s \text{ std}} = \frac{Q_s (T_{std}) (P_s) (1 - B_{wo})}{(T_s) (P_{std})} = \frac{(17.64) (33980) (29.93) (.97)}{(556)} = 31299 \text{ DSCFM}$$

H) Isokinetic Sampling Rate

$$\% I = 0.0945 \frac{T_s (V_{mstd})}{P_s V_s A_n \theta (1 - B_{wo})}$$

$$\% I = \frac{(0.0945) (556) (50.13)}{(29.93) (45.09) (0.00034) (60) (.97)} = \frac{2634}{26.70} = 99 \%$$

I) Concentration = (15.43 grains/gram) (Wt collected) / (V_m std)

$$= (15.43) (0.0364) / (50.13) = 0.0112 \text{ grains/dscf}$$

J) Emission Rate = (0.00857) (grains/dscf) (Q_{std})

$$= (0.00857) (0.0112) (31,299) = 3.00 \text{ lbs/hr}$$

VALUES FROM TEST FORM

$\overline{D_p}$ = 0.78	"H ₂ O
T _s = 556	deg R
T _m = 535	deg R
V _m = 51.225	cuft
Y = 0.986	--
θ = 60	min
A _n = 0.00034	cuft
P _b = 29.92	"Hg
D _h = 0.18	"Hg
C _p = 0.84	--
P _s = 29.93	"Hg
A _s = 12.56	cuft
M _d = 29	lb/cuft
V _{wc} = 27.5	gm
W _t (PM) = 0.0364	gm
P _m = 30.10	"Hg

CALCULATIONS: PLANT

Yorke Doliner

RUN# 2

SOURCE

auto shredder

DATE 26 Oct '87

A) Volume of water vapor collected

$$V_{wc} = (0.0471) (27.2 \text{ gm}) = 1.28$$

B) Volume of air metered to 68 deg.F, 29.92"Hg, dry

$$V_{mstd} = (17.64) (Y) (V_m) (P_m) / (T_m)$$

$$V_{mstd} = (17.64) (.986) (30.930) \frac{(29.98)}{(542)} = 29.76 \text{ cuft}$$

C) Moisture Content of Flue Gas

$$B_{wo} = \frac{V_{wc}}{V_{wc} + V_{mstd}} = \frac{1.28}{1.28 + 29.76} (100) = 4 \% H_2O$$

D) Dry Gas Molecular Weight

$$M_d = 0.44 (\% CO_2) + 0.32 (\% O_2) + 0.28 (\% N + \% CO)$$

$$M_d = 0.44 () + 0.32 () + 0.28 () = \text{assume } 29$$

E) Stack Gas Molecular Weight

$$M_s = M_d (1 - B_{wo}) + (18) (B_{wo}) = (29) (.96) + (18) (.04)$$

F) Stack Gas Velocity

$$M_s = 28.56$$

$$V_s = K_p C_p \sqrt{\frac{D_p}{P_s}} \sqrt{\frac{(T_s \text{ avg})}{M_s}} = (85.49) (0.84) (0.81) \sqrt{\frac{(563)}{(29.93) (28.56)}} = 47.21 \text{ ft/sec}$$

G) Stack Gas Flowrate

$$Q_s = (60 \text{ sec/min}) (A_s) (V_s) = (60) (12.56) (47.21) = 35,577 \text{ cuft/min}$$

$$Q_{s \text{ std}} = \frac{Q_s (T_{std}) (P_s) (1 - B_{wo})}{(T_s) (P_{std})} = \frac{(17.64) (35,577) (29.93) (.96)}{(563)} = 32,029 \text{ DSCFM}$$

H) Isokinetic Sampling Rate

$$\% I = 0.0945 \frac{T_s (V_{mstd})}{P_s V_s A_n \theta (1 - B_{wo})}$$

$$\% I = \frac{(0.0945) (563) (29.76)}{(29.93) (47.21) (0.00019) (60) (.96)} = \frac{15.83}{15.46} = 102 \%$$

I) Concentration = (15.43 grains/gram) (Wt collected) / (V_m std)

$$= (15.43) (0.0299) / (29.76) = 0.0155 \text{ grains/dscf}$$

J) Emission Rate = (0.00857) (grains/dscf) (Q_{std})

$$= (0.00857) (0.0155) (32,029) = 4.25 \text{ lbs/hr}$$

VALUES FROM TEST FORM

$\overline{DP} = 0.81$	"H ₂ O
$T_s = 563$	deg R
$T_{mr} = 542$	deg R
$V_{mr} = 30.930$	cuft
$Y = 0.986$	--
$\theta = 60$	min
$A_n = .00019$	cuft
$P_b = 29.92$	"Hg
$D_h = 0.06$	"Hg
$C_p = 0.84$	--
$P_s = 29.93$	"Hg
$A_s = 12.56$	cuft
$M_d = 29$	lb/cuft
$V_{wc} = 27.2$	gm
$W_t (PM) = .0299$	gm
$P_m = 29.98$	"Hg

CALCULATIONS: PLANT Yorke Polimer RUN# 3
 SOURCE auto shredder DATE 26 Oct 87

A) Volume of water vapor collected

$$V_{wc} = (0.0471) (25.9 \text{ gm}) = 1.22$$

B) Volume of air metered to 68 deg.F, 29.92"Hg, dry

$$V_{mstd} = (17.64) (Y) (V_m) (P_m) / (T_m)$$

$$V_{mstd} = (17.64) (.986) (33.230) \left(\frac{29.98}{549} \right) = 31.56 \text{ cuft}$$

C) Moisture Content of Flue Gas

$$B_{wo} = \frac{V_{wc}}{V_{wc} + V_{mstd}} = \frac{1.22}{1.22 + 31.56} (100) = 4 \% H_2O$$

D) Dry Gas Molecular Weight

$$M_d = 0.44 (\% CO_2) + 0.32 (\% O_2) + 0.28 (\% N + \% CO)$$

$$M_d = 0.44 () + 0.32 () + 0.28 () = \text{assume } 29$$

E) Stack Gas Molecular Weight

$$M_s = M_d (1 - B_{wo}) + (18) (B_{wo}) = (29) (.96) + (18) (.04)$$

F) Stack Gas Velocity

$$M_s = 28.56$$

$$V_s = K_p C_p \sqrt{\frac{D_p}{P_s M_s}} \sqrt{\frac{(T_s \text{ avg})}{P_s M_s}} = (85.49) (.84) (0.82) \sqrt{\frac{(571)}{(29.93) (28.56)}} = 48.13 \text{ ft/sec}$$

G) Stack Gas Flowrate

$$Q_s = (60 \text{ sec/min}) (A_s) (V_s) = (60) (12.56) (48.13) = 36,271 \text{ cuft/min}$$

$$Q_{s \text{ std}} = \frac{Q_s (T_{std}) (P_s) (1 - B_{wo})}{(T_s) (P_{std})} = \frac{(17.64) (36,271) (29.93) (.96)}{(571)} = 32,196 \text{ DSCFM}$$

H) Isokinetic Sampling Rate $\% I = 0.0945 \frac{T_s (V_{mstd})}{P_s V_s A_n \theta (1 - B_{wo})}$

$$\% I = \frac{(0.0945) (571) (31.56)}{(29.93) (48.13) (0.00019) (60) (.96)} = \frac{1703}{15.77} = 108 \%$$

I) Concentration = (15.43 grains/gram) (Wt collected) / (V_m std)

$$= (15.43) (.0290) / (31.56) = 0.0142 \text{ grains/dscf}$$

J) Emission Rate = (0.00857) (grains/dscf) (Q_{std})

$$= (0.00857) (0.0142) (32,196) = 3.92 \text{ lbs/hr}$$

VALUES FROM TEST FORM

$\bar{D}_p = 0.82$	"H ₂ O
$T_s = 571$	deg R
$T_m = 549$	deg R
$V_m = 33.230$	cuft
$Y = 0.986$	—
$\theta = 60$	min
$A_n = 0.00019$	cuft
$P_b = 29.92$	"Hg
$D_h = .06$	"Hg
$C_p = 0.84$	—
$P_s = 29.93$	"Hg
$A_s = 12.56$	cuft
$M_d = 29$	lb/cuft
$V_{wc} = 25.9$	gm
$W_t (PM) = .0290$	gm
$P_m = 29.98$	"Hg

12.0 EQUIPMENT CALIBRATION DATA

CALIBRATION OF EQUIPMENT

Calibration of the stack sampling equipment was performed as directed by Chapter 17-2.700 (6)(a) 5.f. of the Florida Administrative Code and the Federal EPA handbook on Quality Assurance. While in the field the following quality assurance is performed.

- A. Nozzles. Prior to starting the test, the nozzle selected for the test is calibrated by micrometer. This is normally found listed on the first run field data sheet in the blank after nozzle diameter. The general appearance of the pitot and probe is noted before and after the test.
- B. Dry Gas Meter. Before beginning each series of tests, the back half of the sample train (in the control box) is checked for leaks.
- C. Sampling Train. Before the test and after the train has been assembled, a leak check is performed from the nozzle back. A vacuum of 15" or greater is used. During the test the vacuum on the sampling train is recorded to allow a final (after the test run) leak check equal to or greater than the highest vacuum during the run.

Other calibration as required by the above listed code, was performed in the lab in a manner prescribed by the State Code.

Calibration Schedule
(Reference: 17-2.700(6)(a)5.f.)

10/83

DER 17 - 2.700

Item	Minimum Calibration	Reference Instrument Frequency	Tolerance
Thermometers Liquid in glass	Annually	ASIM Hg in glass ref. thermometer or equivalent or thermometric points.	±2%
Bimetallic	Quarterly	Calib. liq. in glass thermometer	5°F
Thermocouple	Annually	ASIM Hg in glass ref. thermometer, NBS calibrated reference thermocouple and potentiometer.	5°F
Barometer	Monthly	Hg barometer, or NOAA station	±1% scale
Pitot Tube	1. When required 2. When damaged	By construction or measurements or wind tunnel D greater than 16" and standard pitot tube	See EPA Method 2 Figs. 2-2 & 2-3
Probe Nozzles	1. Before each test or 2. When nicked, dented, corroded	Micrometer	±0.001" mean of at least 3 readings. Maximum deviation between readings 0.004"
Dry Gas Meter and Orifice Meter	1. Full Scale: When received; When 5% change observed; annually 2. One Point: semiannually 3. Check after each test series	Spirometer of calibrated wet test or dry gas test meter Comparison check	2% 5%

POSTTEST DRY GAS METER CALIBRATION DATA FORM (English units)

Test numbers _____ Date 10 Mar 82 Meter box number A-1 Plant _____
 Barometric pressure, $P_b =$ 29.98 in. Hg Dry gas meter number 14-1 Pretest Y 1.80

Orifice manometer setting, (ΔH), in. H_2O	Gas volume		Temperature					Time (Θ), min	Vacuum setting, in. Hg	Y_i	Y_i	
	Wet test meter (V_w), ft^3	Dry gas meter (V_d), ft^3	Wet test meter (t_w), $^{\circ}F$	Dry gas meter		Average (t_d), $^{\circ}F$	$V_w P_b (t_d + 460)$				$V_d P_b + \frac{\Delta H}{13.6} t_w + 460$	
				Inlet (t_{d_i}), $^{\circ}F$	Outlet (t_{d_o}), $^{\circ}F$							
1 1.5	10	10.312	74	84	84	544	14.86	7	.982			
2 1.5	10	10.324	74	84.5	84	544.25	14.84	7	.981			
3 1.5	10	10.230	74	84.5	84	544.25	14.91	7	.990			
$V_{vac} = 7"$										$Y = 0.984$		

$V_{acc} = 7"$

^a If there is only one thermometer on the dry gas meter, record the temperature under t_d .

V_w = Gas volume passing through the wet test meter, ft^3 .

V_d = Gas volume passing through the dry gas meter, ft^3 .

t_w = Temperature of the gas in the wet test meter, $^{\circ}F$.

t_{d_i} = Temperature of the inlet gas of the dry gas meter, $^{\circ}F$.

t_{d_o} = Temperature of the outlet gas of the dry gas meter, $^{\circ}F$.

t_d = Average temperature of the gas in the dry gas meter, obtained by the average of t_{d_i} and t_{d_o} , $^{\circ}F$.
 ΔH = Pressure differential across orifice, in H_2O .

Y_i = Ratio of accuracy of wet test meter to dry gas meter for each run.

Y = Average ratio of accuracy of wet test meter to dry gas meter for all three runs;
 tolerance = pretest $Y \pm 0.05Y$

P_b = Barometric pressure, in. Hg.

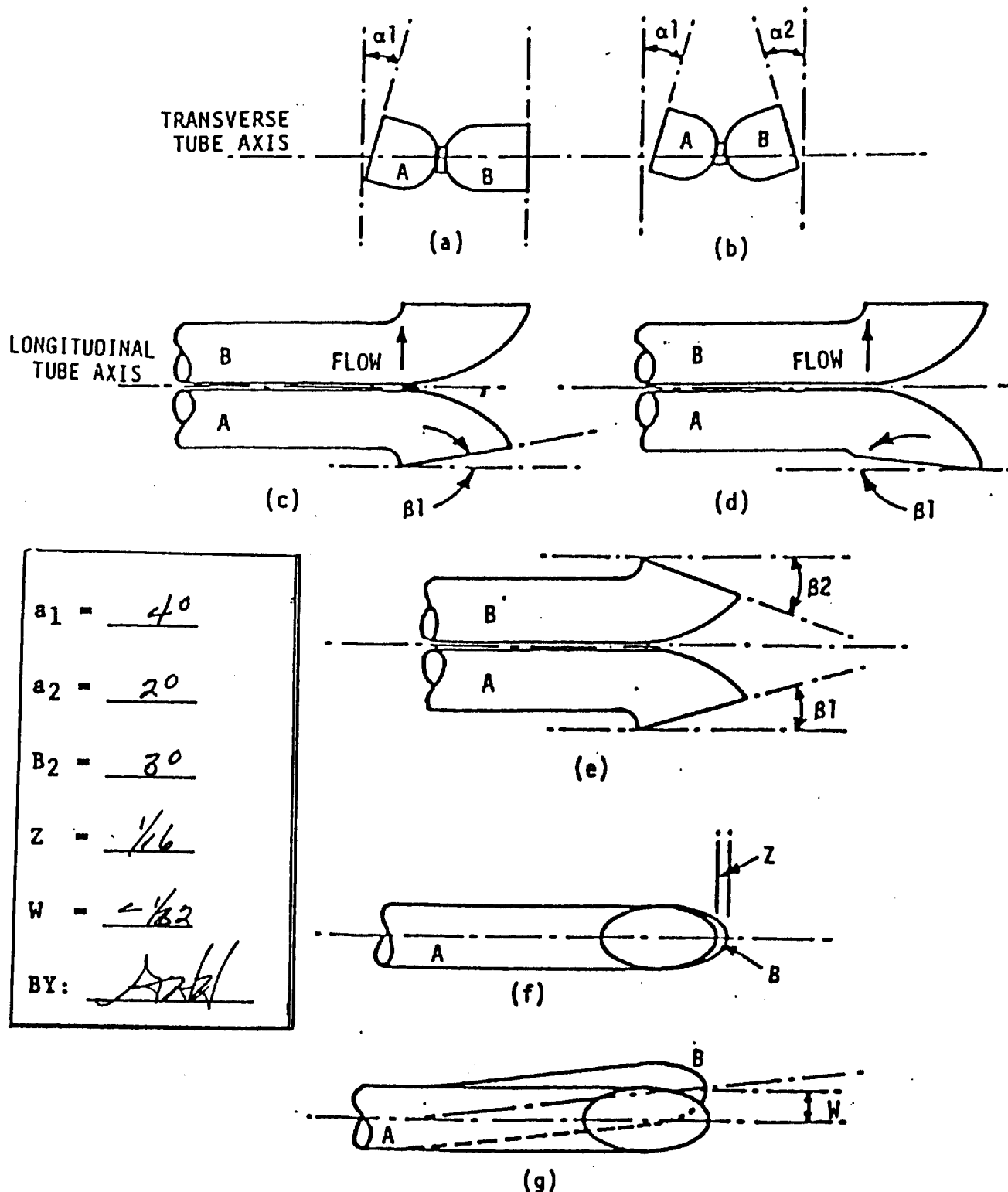
θ = Time of calibration run, min.

$$\frac{(10)(29.98)(544)}{(X)(30.17)(534)} = \frac{163091.2}{16110.8}$$

PITOT TUBE ALIGNMENT CHECK

PITOT TUBE # 146'

DATE: 2 Nov 87



$\alpha_1 = 4^\circ$

$\alpha_2 = 2^\circ$

$\beta_2 = 3^\circ$

$Z = 1/16$

$W = 1/32$

BY: AKL

Figure 1.4. Types of face-opening misalignment that can result from field use or improper construction of Type S pitot tubes. These will not affect C_p so long as α_1 and $\alpha_2 < 10^\circ$, $\beta_2 < 5^\circ$, $z < 0.32$ cm (1/8 in.) and $w < 0.08$ cm (1/32 in.).

CALIBRATION DATE: 2 Nov '87

AMBIENT TEMPERATURE: 74°F

CALIBRATOR: GHH

REFERENCE TEMPERATURE SENSOR: BESD Hg in Glass

a. Every (50°F).
b. Type of calibration system used.
c. calculation of % difference. **MUST BE LTEQ TO 1.5 %**

$$\left(\frac{(\text{ref temp deg F} + 460) - (\text{test thermon temp. deg. F} + 460)}{\text{ref temp. deg. F} + 460} \right) 100$$

POST TEST METER ORFICE CHECK

Meter Box NO. H-1

Delta Ha of box 1.80

Date of Check 2 Nov 87

Time required to draw 10 ft³ at Delta Ha of control box 13 min 46 sec

10 cuft ÷ by 13.77 total minutes = 0.73 DHa₂

$0.75 = \frac{1.03}{DHa_2} \times (100) = 103\%$ of present calibration for
meter box.

Procedure.

Set the flow of meter box at DHa of meter box as determined by last calibration. Record the amount of time required to draw 10.00 cuft. If the percent of the resulting ratio to the calibration of the meter box is NOT five percent or less, the meter box must be recalibrated.

NOZZLE CALIBRATION DATA

Nozzle ID Number	D ₁	D ₂	D ₃	D _{avg.}
H 1/4	see run #1			
H 3/16	see run #2			

- D_{1,2,3} = three different nozzle diameters, each diameter must be within 0.001 in.
- Maximum difference between any two diameters ≤ 0.004 in.
- D_{avg.} = average of D_{1,2,3}.

METER BOX CALIBRATION DATA AND CALCULATION FORM

(English units)

Date 5 Sept 1985

Meter box number H-1

Barometric pressure, $P_b = 29.98$ in. Hg Calibrated by Hawkins

Orifice manometer setting (ΔH), in. H ₂ O	Gas volume		Temperature				Time (θ), min	Y _i	$\Delta H@_{i0}$ in. H ₂ O
	Wet test meter (V _w), ft ³	Dry gas meter (V _d), ft ³	Wet test meter (t _w), °F	Dry gas meter					
				Inlet (t _{d_i}), °F	Outlet (t _{d_o}), °F	Avg ^a (t _d), °F			
0.5	5	5.215	74	88.5	87	87.75	2.38	.982	1.69
1.0	5	5.205	74	88.5	87	87.75	8.75	.982	1.69
1.5	10	10.308	75	89	87.5	88.25	4.90	.991	1.84
2.0	10	10.268	75	89	87.5	88.25	2.97	.994	1.86
3.0	10	10.355	75.5	90	88	89.0	0.70	.983	1.90
4.0	10								
Avg								.986	1.80

ΔH , in. H_2O	$\frac{\Delta H}{13.6}$	$Y_i = \frac{V_w P_b (t_d + 460)}{V_d (P_b + \frac{\Delta H}{13.6}) (t + 460)}$	$\Delta H @_i = \frac{0.0317 \Delta H}{P_b (t_d + 460)} \left[\frac{(t_w + 460) \theta}{V_w} \right]^2$
0.5	0.0368	82107.7 ± 83591.1	27708.5 ± 16421.5
1.0	0.0737	82107.7 ± 83611.6	27735.2 ± 16421.5
1.5	0.110	164365.3 ± 165939.7	30215.5 ± 16436.5
2.0	0.147	164515.3 ± 165499.1	30526.5 ± 16451.5
3.0	0.221	164590.2 ± 167467.6	31222.5 ± 16459.0
4.0	0.294		

^a If there is only one thermometer on the dry gas meter, record the temperature under t_d .

APPENDIX
PROCESS DATA SHEETS

Yorke Doliner & Company

TELEPHONE - 305-638-2781
TELEX - YD & C BONA 584373

POST OFFICE BOX 1859
COCOA, FLORIDA 32923-1859

October 26, 1987

INPUT PROCESS WEIGHT

Test 1

8:30 - 9:30 a.m. 55 Cars X 2200# = 121,000

Test 2

10:00 - 11:10 a.m. 58 Cars X 2200# = 127,600

Test 3

11:42 - 12:52 p.m. 47 Cars X 2200# = 103,400


Daniel W. Smith, Maintenance Supervisor

Yorke Doliner & Company

TELEPHONE - 305-636-2781
TELEX - YD & C BONA 564373

POST OFFICE BOX 1659
COCOA, FLORIDA 32923-1659

November 25, 1987

To Whom It May Concern:

On October 20th, the following readings were taken on the Scrubber System:

Measurement Readings:

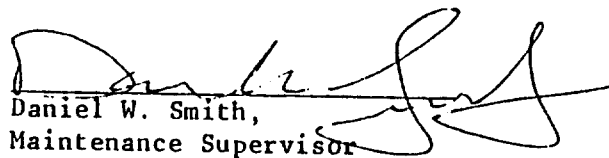
-Scrubber-

Input (4) 1 1/2"

Output - (-) 1/4"

Differential= 1 3/4"

Water PSI = 70 PSI
Water Flow = 200 GPM-


Daniel W. Smith,
Maintenance Supervisor



WEST VIRGINIA
AIR POLLUTION CONTROL COMMISSION
NORTHERN PANHANDLE REGIONAL OFFICE
1911 Warwood Avenue
WHEELING, WEST VIRGINIA 26003
Telephone: 304-277-2662

MEMORANDUM FOR RECORD

TO: Dale Farley
Chief, Engineering

DATE: September 3, 1982

FROM: John Reggi
Regional Engineer

SUBJECT: HERMAN STRAUSS COMPANY
Aluminum Reclaiming Furnace

FILE: Herman Strauss Co.

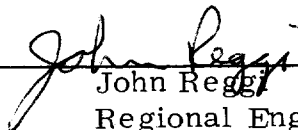
As per our phone conversation on August 24, 1982, I have completed an inspection of the Aluminum Reclaiming Furnace installed (without permit) by Herman Strauss Company. The unit began operation during the first week of August, 1982. Enclosed please find operating and construction data supplied by the manufacturer.

During my observation the furnace was operating with temperatures in the primary and secondary chambers as described in the data (i.e. 1500° F and 1700° F respectively). The unit is natural gas fired. No stack emissions were observed during charging, tapping, or in the melting phase of operation. Also no fugitive emissions were observed during charging or topping.

Mr. Ken Burns representing the company indicated that most aluminum scrap was obtained from the Ormet plant located in Ohio north of New Martinsville, W. Va. He indicated the operation would be essentially as described in the enclosed letter from Eurich-Falcone Incinerator Co. to Mr. Nim of the Allegheny Health Department.

In my estimation there will be no visible emissions from this operation. Stack emissions although not measured will probably not be a problem because of the natural gas fuel and clean scrap charged. I have made no evaluation of any emissions that might occur from the melting aluminum scrap (approximately 97% pure aluminum).

JR/gag
cc: C. G. Beard, II


John Reggi
Regional Engineer

EURICH-FALCONE INCINERATOR CO.

"FORMERLY O'HARA INCINERATOR CO."

51 WILL STREET • McKEESPORT, PA 15132

PHONE (412) 751-6700

Allegheny County Health Department
Bureau of Air Pollution Control
39th & Penn Avenue
Pittsburgh, PA 15224

ATTN: Mr. Karl Nim

Dear Mr. Nim:

Re: Permit information on Aluminum Furnace

The following is the information you requested on the aluminum furnace to be installed at our location:

- A. Secondary combustion air blower is rated at 880 CFM @ 1½" S.P./½ H.P. 1750 RPM.
- B. Two secondary gas burners are rated at 800.000 BTU/HR capacity each.
- C. There are five air port openings into the base of the secondary holding chamber, for combustion air and mixing (turbulence).
- D. We have four primary gas burners for melting the aluminum, each burner is rated at 1,200.000 BTU/HR (max. rating). One burner is used also for keeping the aluminum in a liquid form in the holding pot area.
- E. Both the primary chamber and the secondary chamber is equipped with temperature modulation controls to maintain proper temperatures for smoke destruction and melting aluminum. 1500°F primary and 1700°F secondary chamber.
- F. The volume of the primary chamber, less the hearth area, is 359.92 cu/ft.
- G. Total volume of the secondary chamber is 56.27 cu/ft plus additional smoke combustion in the refractory stack. Stack is 16½" diameter @ 8'-0" high with a volume of 20.53 cu/ft.
- H. Upper stack is equipped with a test port for reading temperature, velocity, and particulate matter.
- I. We estimate the holding time @ 1700°F to be at least ½ sec residence time.
- J. The melting chamber is of starved air design, with combustion air supplied through the burners only.
- K. We will not be doing any fluxing of the aluminum bath.

Very truly yours,

EURICH-FALCONE INCINERATOR CO.

"FORMERLY O'HARA INCINERATOR CO."

51 WILL STREET • McKEESPORT, PA 15132

PHONE (412) 751-6700

Aug. 25, 1982

City County Building
1500 Chapline Street
Wheeling, W. Va. 26003
ATTN: Mr. Tim Carroll

Dear Tim:

We installed a aluminum reclaiming furnace at the Herman Strauss Company in Wheeling, W. Va.

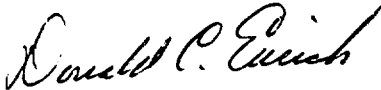
This equipment was installed at our Pittsburgh plant, and was approved by the local Air Pollution Control Dept.

Attached is the information you requested on the furnace along with drawing.

Please inspect the installation so the new owner can obtain the necessary permits to operate the equipment.

If there are any questions, please feel free to call my office at any time.

Very truly yours,
EURICH-FALCONE INCINERATOR CO.



Donald C. Eurich
President

DCE/re
Encl.

Allegheny County Health Department

COUNTY COMMISSIONERS

TOM FOERSTER
chairman

CYRIL H. WECHT, M.D., J.D.

WILLIAM R. HUNT, M.D.

N. MARK RICHARDS, M.D.
director



Bureau of Air Pollution Control
301 Thirty-ninth Street
Pittsburgh, Pennsylvania 15201

November 24, 1980

BOARD OF HEALTH

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JAMES HAWES

LEWIS H. KULLER, M.D., Dr. PH

CHARLES L. WINEK, Ph. D.

Eurich-Falcone Incinerator Company
51 Will Street
McKeesport, Pennsylvania 15132
Attention: Mr. Donald C. Eurich

PERMIT NO.: 80-I-0074-P
EQUIPMENT: Aluminum Melting Process
LOCATION: McKeesport
FIRST OPERATING PERMIT FEE: \$50.00

NOTICE OF INSTALLATION PERMIT APPROVAL

The subject installation has been approved for construction. The installation shall be made in conformity with the plans and specifications which are a part of your application, and must be inspected and approved by the Bureau before it can be placed into operation.

Upon completion of the installation, please submit an application for an Operating Permit with the fee listed above, and an inspection will then be scheduled. When it is determined by the Bureau that the installation complies with the Regulations and the approved permit application, the facility may be placed into operation.

The installation will require emission testing prior to the issuance of the Operating Permit. The approved test procedure, as outlined in Article XVIII, shall apply. The Bureau must be notified at least ten (10) days prior to the date of any tests.

If emission testing demonstrates compliance with Article XVIII, the Operating Permit will be issued.

This Installation Permit shall be posted at the site during the construction period.

Permit Issued by:

BUREAU OF AIR POLLUTION CONTROL

J. D. Graham
Engineering and Plan Review Section

JDG/cg

Attachment

PERMIT - PROCESS

COMPLETION DATE

November 1980

DATE INSTALLED

INSTALLATION ☒

OPERATING ☐

Receipt No. 11/5/80

Issued 11/24/80

Expires

Fee \$60.00

Basis

BUSINESS

NAME ADDRESS BUSINESS
Eurich-Falcone Incinerator Co. 51 Will Street McKeesport, PA 15132

OWNER ADDRESS PHONE
Eurich-Falcone Incinerator Co. 51 Will Street McKeesport, PA 15132 751-6700

INSTALLER OR CONTRACTOR ADDRESS PHONE
Eurich-Falcone Incinerator Co. 51 Will Street McKeesport, PA 15132 751-6700

AUTHORIZED REPRESENTATIVE TITLE SIGNATURE PHONE
Donald C. Eurich President 751-6700

PROCESS YOUR IDENTIFICATION PRODUCTION RATE ☐ 1000 LB/HR Gross* FEE
Aluminum Melting CHARGING RATE ☐ TONS/HR. \$ 60.00

OPERATING TIME 16 HOURS/DAY 5 - 6 DAYS/WK. 52 WEEKS/YR. CONTINUOUS ☐ BATCH ☒ BATCH TIME 1 HR.

RAW MATERIALS TOTAL
Aluminum Scrap

MATERIALS PRODUCED TOTAL
Aluminum Ingots & Sows

FUEL	AMT./HR.	BTU	% ASH	% SULFUR	FUEL	AMT./HR.	BTU	% ASH	% SULFUR
Nat. Gas	4,800,000		-----	-----					
FUEL	AMT./HR.	BTU	% ASH	% SULFUR	FUEL	AMT./HR.	BTU	% ASH	% SULFUR

GAS CLEANER	GAS FLOW	INLET TEMP.	DUST LOADING	EFFICIENCY	PRESSURE DROP
None	SCFM	° F	GR./SCF.	%	" W.G.

GAS CLEANER	GAS FLOW	INLET TEMP.	DUST LOADING	EFFICIENCY	PRESSURE DROP
None	SCFM	° F	GR./SCF.	%	" W.G.

EMISSION ANALYSIS	PARTICULATE	SO ₂	CO	NOX	HC	OTHER
POTENTIAL						

FINAL	Less than .125 LBS/100 LBS waste (scrap)	GR./SCF.

STACK HEIGHT	STACK AREA	EXHAUST FLOW	TEMPERATURE	DUST LOADING
32 FT.	16" Dia. SQ. FT.	ACFM	500 ° F	GR./SCF.

EMISSION BASIS	MFG. DATA	EMISSION FACTORS	STACK TEST	COMPANY ESTIMATE	SUBMIT SUPPORTING DATA FOR METHOD USED.
	☒	☐	☐	☐	

NEAREST BUILDING:	HEIGHT	DISTANCE	COST OF EQUIPMENT	COST OF GAS CLEANING SYSTEM \$
	28 FT.	20 FT.	\$	

DRAWING NO'S. AND TITLES

REMARKS

Conversion of solid waste incinerator, to reclaim aluminum from scrap yards, to melt and

form ingots and sows.

* Gross weight is aluminum and steel mixed, approximately 50/50%

REVIEWED BY	TITLE	DATE	REVIEWED BY	TITLE	DATE

REVIEWED BY	TITLE	DATE	PERMIT APPROVED BY	TITLE	DATE

A Secondary combustion chamber @ 1500 - 1700 ° F and

0.5 sec residence time See letter Eurich to Nema 11/21/80