

Tony Knowles
Mayor

STAPPA / ALARCO
ANCHORAGE WATER & SEWER UTILITIES

2.5
3000 Arctic Boulevard
Anchorage, Alaska 99503
(907) 277-7622



Owned by the Municipality
of Anchorage

October 14, 1982

Alaska Department of Environmental Conservation
Air Quality Control
437 "E" Street, 2nd Floor
Anchorage, Alaska 99501

Attention: Mr. Carl Harmon

Subject: Pt. Woronzof Wastewater Treatment Facility Incinerator Stack
Emissions Report - A.A.P.C.A.
0580, AQC-517 Permits

RECEIVED

OCT 27 1982

ENVIRONMENTAL CONSERVATION
REGION II

On the 20, 21, 22 of September, 1982, Chemical and Geological Laboratories of Alaska, Inc. performed particulate loading and sulfur dioxide tests on the Pt. Woronzof Wastewater Treatment Facility incinerator stack emissions. Results of their analyses are attached. Listed below is other information required by the Pt. Woronzof Air Quality Permits:

1. Highest six month average opacity reading from transmissometer:

July 1982 - 22.5% for 1.6 minutes

2. Days operated:

1982	<u>April</u>	<u>May</u>	<u>June</u>	<u>July</u>	<u>August</u>	<u>September</u>
	28.1	23.6	24.4	27.9	27.1	25.1

3. Fuel Consumed (hundred cubic feet):

1982	<u>April</u>	<u>May</u>	<u>June</u>	<u>July</u>	<u>August</u>	<u>September</u>
	14,992	13,363	12,105	12,787	12,871	11,842
	1.5	1.3	1.2	1.3	1.3	1.2

The next incinerator stack emission report will be submitted in April 1983. If you have any questions concerning this report, I can be reached at telephone number 338-3870.

R. E. Hutson
Manager
Treatment Division
AWWU

REH, JKW, /vw

Anchorage



The Treatment Section is charged with the responsibility for effective treatment of wastewater from residential, commercial, and industrial users of all area-wide sewerage systems within the municipal boundaries, prior to discharge to the waters of Cook Inlet. In carrying out this responsibility the Section operates treatment facilities serving the Anchorage, Eagle River and Girdwood communities, as well as over 20 sewage pumping and metering stations in the Anchorage area. The Section has also operated a solid waste incineration facility at the Point Woronzof treatment plant site since late 1971, first through a contractual agreement with the State of Alaska, Division of Aviation, for disposal of international air traffic garbage, and now for the disposal of classified documents and other materials from various governmental agencies and private organizations. This service will be discontinued in mid-1979.

The Point Woronzof treatment plant, located on a 46 acre tract on the northwestern corner of the Greater Anchorage area, operates 24 hours a day, 7 days a week, to provide primary treatment for the sewage from the community. The facility, which began operation in July 1972, has an optimum treatment capacity of 34 million gallons per day (MGD), and a hydraulic capacity of 75 MGD. It is designed to be readily expanded through duplication of certain units, and by further additions can provide for higher degrees of treatment, as may be required by regulatory authorities.

Raw wastewater enters the plant headworks through a 96 inch diameter tunnel, goes through a screening process, then is diverted to clarifiers where settleable and floatable solids are both separated from the water and pumped to other units for thickening, drying, incineration, and final disposal of the ash to the sanitary landfill. The water, or effluent, is chlorinated for reduction of harmful bacteria, routed through a long section of 84 inch diameter outfall pipe which also serves as a chlorine contact chamber, to a control structure, and then discharged a short distance out in the inlet, at a location where water currents provide some mixing and dispersion. The outfall pipe is designed to be extended if necessary.

As a means of assuring control of effluent quality and of the operational processes, the treatment plant laboratory carries out a great many examinations on samples of sewage and its components. The results of these tests document treatment efficiencies and the characteristics of the materials tested, and are necessary to the effective management of the facility. In addition, data resulting from the test procedures forms the basis for regular, required, monitoring reports to the Environmental Protection Agency and the Alaska Department of Environmental Conservation. The laboratory also provides analytical services from time to time to other agencies, such as U.S. Public Health, U.S.G.S., B.L.M., and the Corps. of Engineers, and to municipal government departments, including Solid Waste, Utility Engineering, and the School District.

The Point Woronzof treatment plant is presently treating a wastewater flow averaging nearly 24 million gallons per day (MGD). From that volume about 250 to 300 tons of wet sludge containing 10 to 12 tons of dry solids are removed each day for conditioning, incineration, and disposal. From $1\frac{1}{2}$ to 2 tons of ash are produced each day from the incineration process, and that residue together with about $1\frac{1}{2}$ tons of grit separated daily from the raw wastewater is hauled to a landfill site for final disposal. Eleven to twelve hundred pounds of chlorine are required for disinfection of the plant effluent as it is being discharged to Cook Inlet each day.

The Eagle River facility, in service since 1971, is a small aerated lagoon treatment works, and is severely overloaded as a result of the rapid growth of that community. Construction of a larger plant, which will provide a higher degree of treatment, is scheduled to begin in late 1979 and be completed by the end of 1980. The plant will utilize biological treatment units, which include large air-driven rotating reactors, with primary and secondary solids separation, and aerobic digestion of the solids. Land disposal of the digested sludge will be practised at this facility. The disinfected effluent is discharged to Eagle River, a freshwater stream nearby.

The Girdwood-Alyeska ski resort and residential area placed an all-new sewer system and treatment plant in operation in the fall of 1978, to meet the growth requirements of this popular area. The sophisticated tertiary treatment process includes activated bio-filters, mixed-media filtration, and discharge of a very high quality effluent to an on-site leaching pond, where the water will percolate into the ground rather than be released directly to a receiving stream. The aerobically digested sludge produced in the Girdwood plant will be dewatered and trucked to Anchorage for final disposal.

MUNICIPALITY OF ANCHORAGE
Sewer Utility - Treatment Section

5-17-79

Pt. Woronzof Wastewater Treatment Plant

DESIGN DATA

TRIBUTARY POPULATION

Initial Design	221,000
Ultimate Design	442,000

SEWAGE QUANTITY, MGD

Average Flow	
Initial Design	34
Ultimate Design	75
Minimum Flow	
Initial Design	17
Ultimate Design	34
Maximum Flow	
Initial Design	75
Ultimate Design	150

DESIGN LOADINGS

Biochemical Oxygen Demand (1,000 lbs. per day)	
Initial Design	40.7
Ultimate Design	81.4
Suspended Solids (1,000 lbs. per day)	
Initial Design	21.5
Ultimate Design	43.0

INFLUENT SEWER

Diameter (inches)	96
-------------------	----

COMMINUTER UNITS

Number	3
Channel Width (feet)	5
Channel Depth (feet)	11
Maximum Water Depth (feet)	7.33
Clear Opening (inches)	0.75

SEDIMENTATION TANKS

Number	
Initial Design	3
Ultimate Design	6
Diameter (feet)	120
Side Water Depth (feet)	10
Detention Time at Design Flow (hrs.)	1.80
Maximum Hydraulic Capacity per Tank (mgd)	37.5
Overflow Rate at Design Flow (gal. per day, per sq. ft.)	1,000

SLUDGE THICKENERS

Number	
Initial Design	1
Ultimate Design	2
Diameter (feet)	40
Solids Loading (lbs. per day, per sq. ft.)	20

CHLORINATORS

Number	2
Maximum Feed Rate (lbs. per day)	16,000
Minimum Feed Rate (lbs. per day)	500

FLOW METER

Minimum Flow (gpm)	3,400
Maximum Flow (gpm)	35,000

RAW SLUDGE PUMPS

Number	
Initial Design	3
Ultimate Design	6
Capacity per Unit (gpm)	200

THICKENED SLUDGE PUMPS

Number	
Initial Design	2
Ultimate Design	3
Capacity per Unit	
Minimum (gpm)	12
Maximum (gpm)	37

VACUUM FILTERS

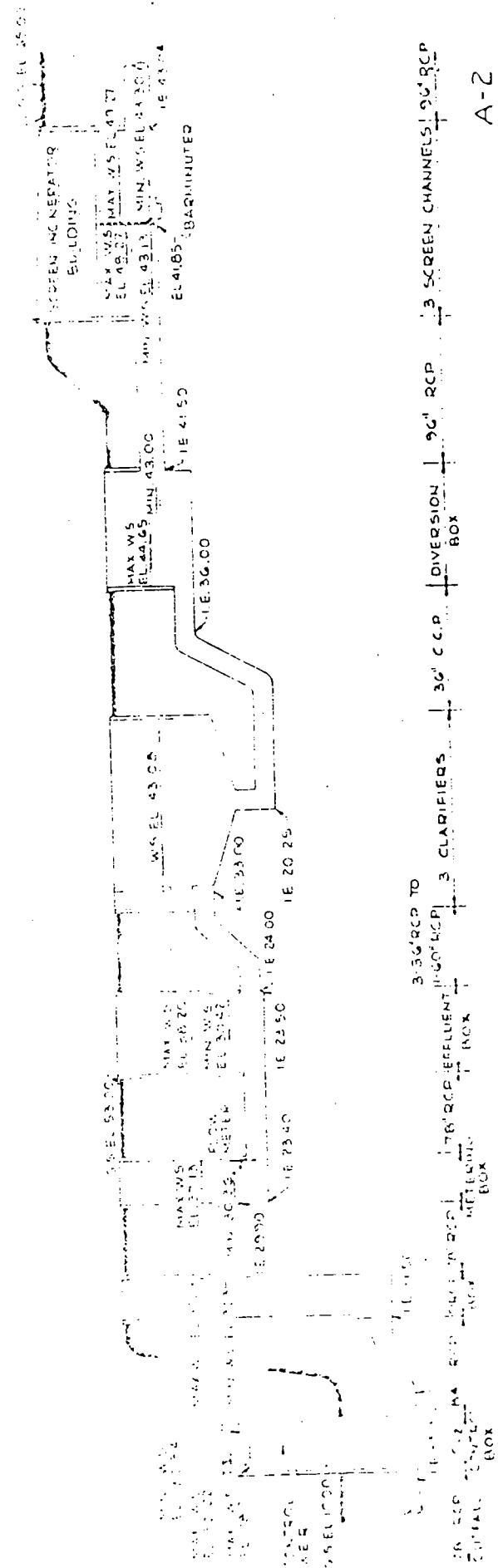
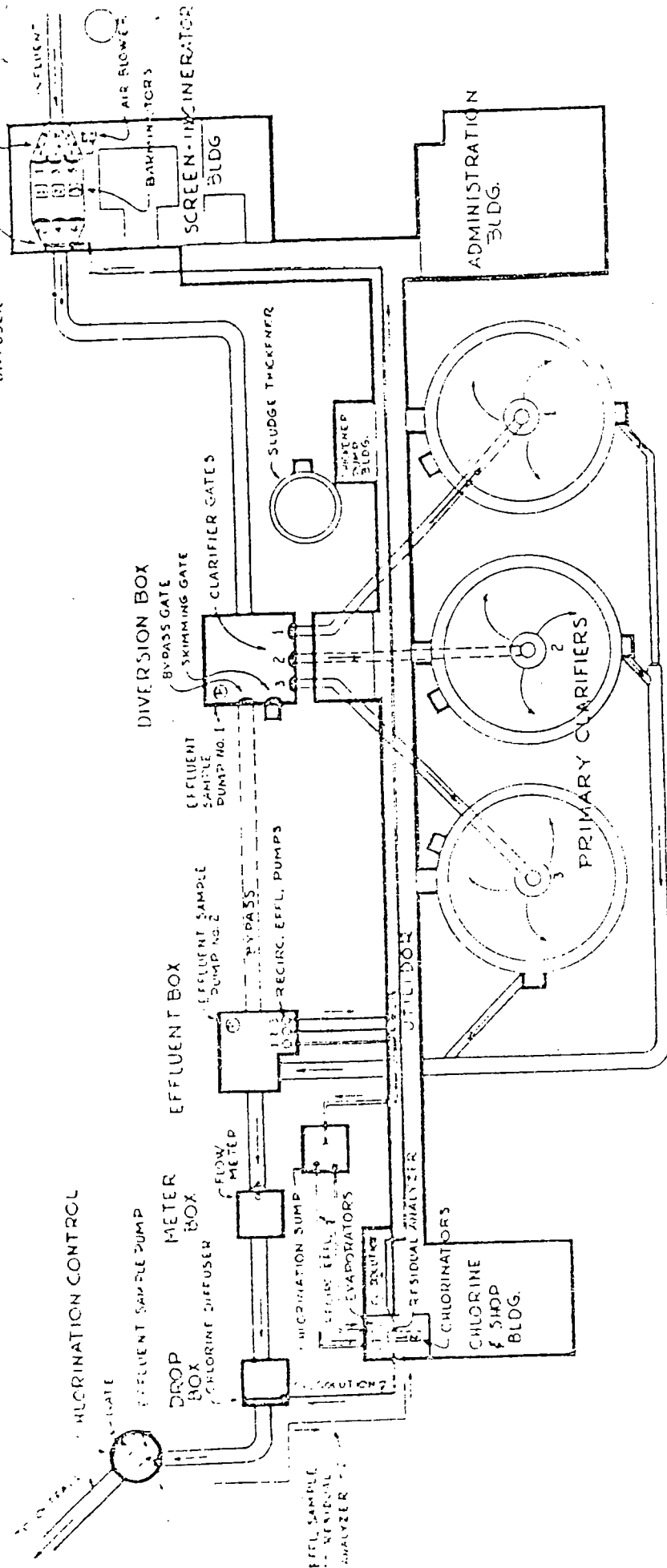
Number	
Initial Design	1
Ultimate Design	2
Solids Loading Rate (lbs. per hr, per sq. ft.)	8
Sludge Cake Moisture	% 70-75

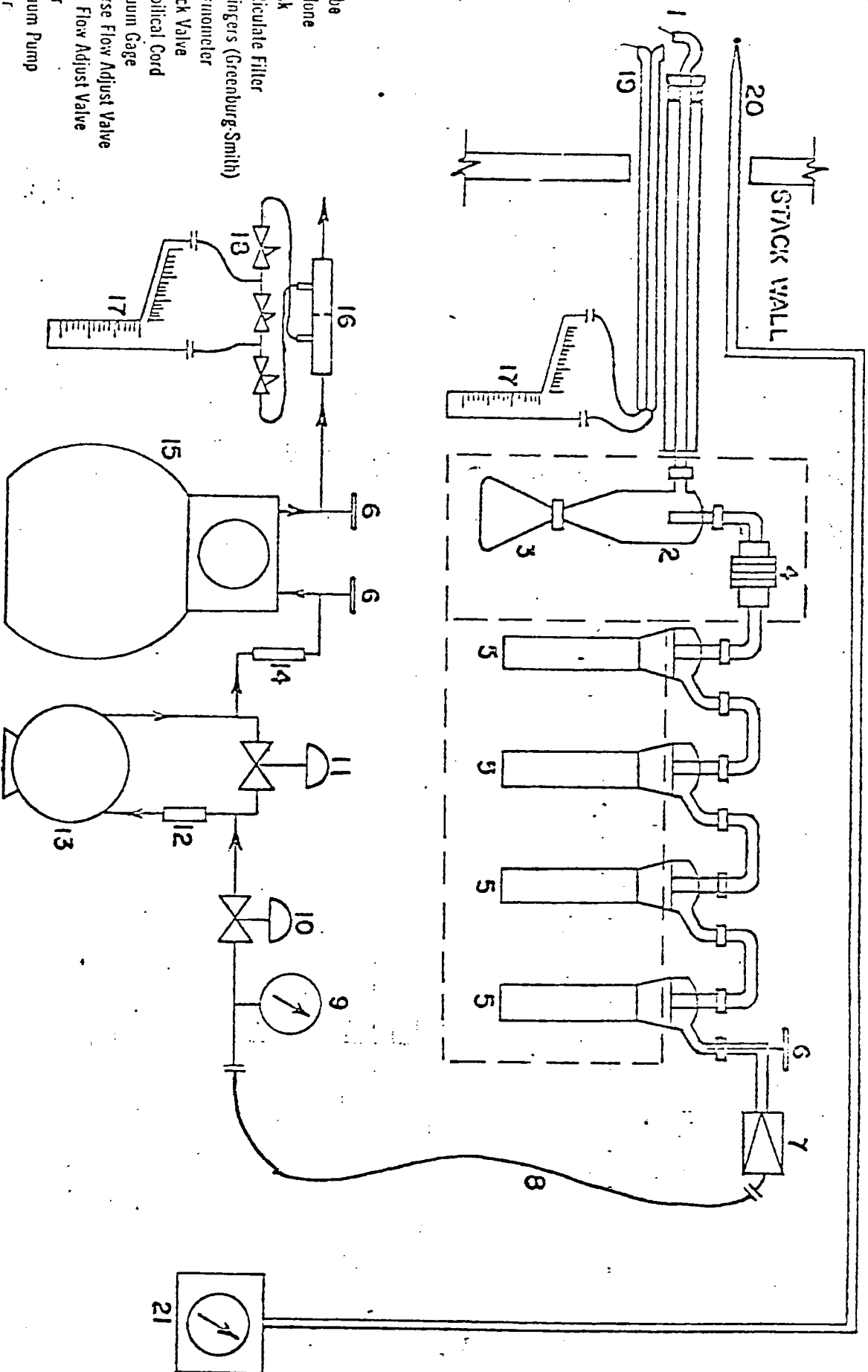
INCINERATORS

Number	
Initial Design	1
Ultimate Design	2
Capacity (tons dry solids per hr.)	0.5
Fuel Value (Btu per lb. combustible)	10,000

5-17-79

Pt. Morozof Wastewater Treatment Plant





- 1) Probe
- 2) Cyclone
- 3) Flask
- 4) Particulate Filter
- 5) Thermomater (Greenburg Smith)
- 7) Check Valve
- 8) Umbilical Cord
- 9) Vacuum Gage
- 10) Coarse Flow Adjust Valve
- 11) Fine Flow Adjust Valve
- 12) Oiler
- 13) Vacuum Pump
- 14) Filler
- 15) Dry Gas Heater
- 16) Orifice Tube
- 17) Inclined Manometer
- 18) Solenoid Valves
- 19) Pilot
- 20) Thermocouple
- 21) Pyrometer

FIGURE TWO

PROPERTY OF
RESEARCH APPLIANCE CO. ALLISON PARK, PA.

TOLERANCES
DEC. $\pm$
FRAC. $\pm$

TITLE
SYSTEMS AND FLOW SYSTEM

SCALE

NO. REQ'D

DWG. NO.
174-23

MATL

DATE
6-23-67

FINISH

DRAWN BY
R.G.

APPR.
E.A.

DATE
6-23-67

JIG NO.

PAINT NO.

Stack Gas Composition = MD

Run #1

	<u>%</u>	<u>Mol Wt</u>	<u>Wt/mole</u>
O ₂	17.85	32.0	5.71
N ₂	77.81	28.0	21.79
CO	0.18	28.0	0.05
CO ₂	4.16	44.0	<u>1.83</u>
			29.38

Run #2

O ₂	16.80		5.38
N ₂	78.79		22.06
CO	0.11		0.03
CO ₂	4.30		<u>1.89</u>
			29.36

Run #3

	17.85		
O ₂	17.56		5.62
N ₂	78.08		21.86
CO	0.14		0.04
CO ₂	4.22		<u>1.86</u>
			29.38

Calculation

#584

Volume of water collected = V_{WSTD}

$$V_{WSTD} = (0.0474)(23.727) = 1.12 \text{ ft}^3$$

Volume of gas metered @ STP = V_{WSTD}

$$V_{WSTD} = 80.81 \left(\frac{0.957}{554} \right) \left(\frac{29.92}{29.92} \right) = 77.34$$

Moisture content = M_c

$$M_c = \frac{1.12}{77.34 + 1.12} = 0.014$$

Molecular wt of stack gas = M_s

$$29.38 \left(\frac{.986}{.986} \right) + 18 \left(\frac{0.014}{.986} \right) = 29.22$$

Area of stack = A

$$\frac{\left(\frac{20}{2} \right)^2 \pi}{144} = 2.18$$

Volume of stack gas = V_s

$$V_s = (85.48)(0.80)(0.76) \sqrt{\frac{593}{(29.92)(29.22) \cdot 0.76}} = 42.825 \text{ ft}^3/\text{sec}$$

Volume flow rate = Q

$$(42.825)(2.18)(3600) = 3.3609 \times 10^5 \text{ ft}^3/\text{hr}$$

Volumetric flow rate @ STP = Q_{sw}

$$(3.3609) \left(\frac{530}{593} \right) \left(\frac{29.92}{29.92} \right) = 3.0046 \times 10^5$$

Volumetric flow rate (dry basis) @ STP = Q_{sd}

$$\left(\frac{77.34}{77.34 + 1.12} \right) (3.0046 \times 10^5) = 2.9617 \times 10^5$$

Sample Area = A_N

$$A_N = \left(\frac{\left(\frac{1.250}{1.2} \right)^2 \pi}{144} \right) = 0.0034 \text{ ft}^2$$

Concentration of particulates/scf = C_s

$$C_s = \frac{0.0329 (15.43)}{77.34} = 0.0066$$

Concentration of particulates, gr/scf @ standard gas cond = C_{an}

$$C_{an} = \frac{0.0329 (15.43)}{77.34 + 1.12} = 0.0065$$

Particulate, lb/hr = C_{ax}

$$\frac{(0.0065) (3.0046 \times 10^5)}{7000} = 0.279$$

$$S @ 12\% CO_2 = (0.0066) \left(\frac{12.00}{4.16} \right) = 0.0190$$

Refractive Index = I

$$C_{ax} @ 12\% (0.0065) \left(\frac{12.00}{4.16} \right) = 0.0190$$

$$I = \frac{77.34 + 1.12}{102.525} \left(\frac{1.00}{29.92} \right) \left(\frac{2.9617}{593} \right) \left(\frac{78.34}{78.10} \right) \times 100 = 100.37\%$$

Plant	Spring Machine & Ref.	Sample Box Number	Ambient Temp	55°F						
Location	St. Wilson Ref	Meter Box No.	Barometric Pressure	29.90						
Run No.	1	Meter $\frac{1}{2}$ Hg	Assumed moisture	1.8						
Date	9/20/82	C Factor	Nozzle Diameter, in.	2.494						
Traverse Point	Sampling Time, min	Static Pressure (P _s) in. Hg	Gas Sample of Dry Gas	Temperature Meter	Sample Box Temp, F					
	5 min/pool									
	1440-1520									
1	5 min	1.85	105	0.555 (0.74)	2.0	694.02	Inlet 78 (Tm in) F	90	80	
2	5 min	1.89	128	0.63 (0.77)	2.40	697.00	102	82	460	
3	5 min	1.30	135	0.66 (0.82)	2.50	702.20	110	83	54	
4	5 min	1.30	140	0.70 (0.84)	2.55	706.52	112	84	58	
5	5 min	1.32	141	0.69 (0.83)	2.50	710.95	114	86	62	
	5 min	1.33	131	0.72 (0.85)	2.55	715.25	113	86	65	
7	5 min	1.34	121	0.70 (0.84)	2.55	719.70	112	86	66	
8	5 min	1.34	109	0.64 (0.81)	2.40	724.10	112	86	67	
9	5 min	1.84	105	0.56 (0.71)	1.80	728.45	112	86	65	
10	5 min	1.83	108	0.12 (0.35)	0.45	732.20	114	86	64	
		0.847	722.3			734.65	110	86	62	

[illegible]

LIQUID WATER AND PARTICULATE COLLECTED

Plant St. Wronoff - Sewage Treatment Plant
 Date 9/20/82
 Run No. 1

VOLUME OF LIQUID WATER COLLECTED

	<u>Final</u>		<u>Initial</u>		<u>Gain</u>	
Impinger No. 1	<u>232</u>	ml	<u>250</u>	ml	<u>-8.0</u>	ml
Impinger No. 2	<u>158</u>	ml	<u>150</u>	ml	<u>8.0</u>	ml
Impinger No. 3	<u>1</u>	ml	<u>0</u>	ml	<u>1.0</u>	ml
Impinger No. 4 (**) Silica Gel	<u>208.261</u>	gm	<u>185.534</u>	gm	<u>22.727</u>	ml
Cyclone		ml	<u>0</u>	ml		ml

(**) 1 gram = 1 milliliter

Total volume collected 23.727 ml

WEIGHT OF PARTICULATE COLLECTED

	<u>Final</u>		<u>Tare</u>		<u>Gain</u>	
Filter No. <u>2</u>	<u>0.012</u>	gm	<u>0.0215</u>	gm	<u>0.010</u>	gm
Cyclone	<u>0.012</u>	gm	<u>X X X X X X</u>		<u>0.000</u>	gm
Probe	<u>0.004</u>	gm	<u>X X X X X X</u>		<u>0.000</u>	gm

(1 gram = 1000 milligrams)

Total weight collected 0.010 gm

Calculation

Run #
2
#584

Volume of water collected = V_{WSTD}

$$V_{WSTD} = (0.0474)(22.671) = 1.07 \text{ ft}^3$$

Volume of gas metered @ STP = V_{WSTD}

$$V_{WSTD} = 78.805 \left(\frac{530}{538} \right) \left(\frac{29.84}{29.92} \right) = 75.97$$

Moisture content = M_c

$$M_c = \frac{1.07}{75.97 + 1.07} = 0.014$$

Molecular wt of stack gas = M_s

$$29.36 (1 - 0.014) + 18 (0.014) = 29.20$$

Area of stack = A

$$\frac{\left(\frac{20}{2} \right)^2 \pi}{144} = 2.18$$

Volume of stack gas = V_s

$$V_s = (85.48)(0.80)(0.75) \sqrt{\frac{597}{(29.84)(29.20)}} = 42.466 \text{ ft}^3/\text{sec}$$

Volume flow Rate = Q

$$(42.466)(2.18)(3600) = 3.3328 \times 10^5 \text{ ft}^3/\text{hr}$$

LIQUID WATER AND PARTICULATE COLLECTED

Plant _____
 Date _____
 Run No. 2

VOLUME OF LIQUID WATER COLLECTED

	<u>Final</u>		<u>Initial</u>		<u>Gain</u>	
Impinger No. 1	<u>234</u>	ml	<u>250</u>	ml	<u>-10.0</u>	m
Impinger No. 2	<u>160</u>	ml	<u>150</u>	ml	<u>+10.0</u>	m
Impinger No. 3	<u>0</u>	ml	<u>0</u>	ml	<u>0.0</u>	m
Impinger No. 4 (**) Silica Gel	<u>227.0</u>	gm	<u>224.8</u>	gm	<u>+2.2</u>	m
Cyclone	<u>0</u>	ml	<u>0</u>	ml	<u>0.0</u>	m

Total volume collected

22.0 m

(**) 1 gram = 1 milliliter

WEIGHT OF PARTICULATE COLLECTED

	<u>Final</u>		<u>Tare</u>		<u>Gain</u>	
Filter No. <u>23</u>	<u>0.2365</u>	gm	<u>0.2179</u>	gm	<u>0.0186</u>	g
Cyclone	<u>0.0041</u>	gm	<u>X X X X X X</u>		<u>0.0041</u>	g
Probe	<u>0.0000</u>	gm	<u>X X X X X X</u>		<u>0.0000</u>	g

Total weight collected

0.0227 g

(1 gram = 1000 milligrams)

Volumetric flow rate @ STP = Q_{sw}

$$(3.3328 \times 10^5) \left(\frac{530}{597} \right) \left(\frac{29.84}{29.92} \right) = 2.9506 \times 10^5$$

Volumetric flow rate (dry basis) @ STP = Q_{sd}

$$\left(\frac{75.97}{75.97 + 1.07} \right) (2.9506 \times 10^5) = 2.9096 \times 10^5$$

Sample Area = A_N

$$A_N = \left(\frac{\left(\frac{1.250}{1.2} \right)^2}{144} \right) \pi = 0.00034 \text{ ft}^2$$

Concentration of particulates/scf = C_s

$$C_s = \frac{0.0255 (15.43)}{75.97} = 0.0052$$

Concentration of particulates, gr/scf @ standard gas cond = C_{sc}

$$C_{sc} = \frac{0.0255 (15.43)}{75.97 + 1.07} = 0.0051$$

Particulate, lb/hr = C_{ax}

$$\frac{(0.0051) (2.9506 \times 10^5)}{7060} = 0.214$$

$$S @ 12\% CO_2 = (0.0052) \left(\frac{12.00}{4.30} \right) = 0.0145$$

Dishenetic = I

$$I = \frac{77.04}{75.97 + 1.07} \times 100 = 100.4\%$$

$$C_{ax} @ 12\% (0.0051) \left(\frac{12.00}{4.30} \right) = 0.0145$$

$$\frac{77.04}{76.30} \times 100 = 100.4\%$$

Location		Sample Box Number		Ambient Temp		Pressure	
Western		Meter Box No.		Barometric		89.82	
Run No.		Meter H _g		Assured moisture		2.4	
Date		C Factor		Nozzle Diameter, in.		.2498	
Reverse		Velocity		Diff. across		Gas Sample	
Point		Head (P _s)		or. Meter		Vol (Vn) ft ³	
Sampling Time, min		Pressure (P _g) in. Hg		Inlet		Gas Sample of Dry Gas	
7/457		109		62		Temperature	
1		0.15		1.10		Inlet (Tm in) F	
2		0.25		1.55		Outlet (Tm out)	
3		0.32		2.10		Sample Box	
4		0.34		2.30		Temp, F	
5		0.34		2.30		853.90	
6		0.39		2.45		857.00	
7		0.35		2.60		860.90	
8		0.33		2.50		865.10	
9		0.33		2.30		869.30	
10		0.20		2.10		873.60	
11		0.20		2.10		877.90	
12		0.20		2.10		882.20	
13		0.20		2.10		886.45	
14		0.20		2.10		890.67	
15		0.20		2.10		894.90	
16		0.20		2.10		899.10	
17		0.20		2.10		903.30	
18		0.20		2.10		907.50	
19		0.20		2.10		911.70	
20		0.20		2.10		915.90	
21		0.20		2.10		920.10	
22		0.20		2.10		924.30	
23		0.20		2.10		928.50	
24		0.20		2.10		932.70	
25		0.20		2.10		936.90	
26		0.20		2.10		941.10	
27		0.20		2.10		945.30	
28		0.20		2.10		949.50	
29		0.20		2.10		953.70	
30		0.20		2.10		957.90	
31		0.20		2.10		962.10	
32		0.20		2.10		966.30	
33		0.20		2.10		970.50	
34		0.20		2.10		974.70	
35		0.20		2.10		978.90	
36		0.20		2.10		983.10	
37		0.20		2.10		987.30	
38		0.20		2.10		991.50	
39		0.20		2.10		995.70	
40		0.20		2.10		1000.00	
41		0.20		2.10		1004.20	
42		0.20		2.10		1008.40	
43		0.20		2.10		1012.60	
44		0.20		2.10		1016.80	
45		0.20		2.10		1021.00	
46		0.20		2.10		1025.20	
47		0.20		2.10		1029.40	
48		0.20		2.10		1033.60	
49		0.20		2.10		1037.80	
50		0.20		2.10		1042.00	
51		0.20		2.10		1046.20	
52		0.20		2.10		1050.40	
53		0.20		2.10		1054.60	
54		0.20		2.10		1058.80	
55		0.20		2.10		1063.00	
56		0.20		2.10		1067.20	
57		0.20		2.10		1071.40	
58		0.20		2.10		1075.60	
59		0.20		2.10		1079.80	
60		0.20		2.10		1084.00	
61		0.20		2.10		1088.20	
62		0.20		2.10		1092.40	
63		0.20		2.10		1096.60	
64		0.20		2.10		1100.80	
65		0.20		2.10		1105.00	
66		0.20		2.10		1109.20	
67		0.20		2.10		1113.40	
68		0.20		2.10		1117.60	
69		0.20		2.10		1121.80	
70		0.20		2.10		1126.00	
71		0.20		2.10		1130.20	
72		0.20		2.10		1134.40	
73		0.20		2.10		1138.60	
74		0.20		2.10		1142.80	
75		0.20		2.10		1147.00	
76		0.20		2.10		1151.20	
77		0.20		2.10		1155.40	
78		0.20		2.10		1159.60	
79		0.20		2.10		1163.80	
80		0.20		2.10		1168.00	
81		0.20		2.10		1172.20	
82		0.20		2.10		1176.40	
83		0.20		2.10		1180.60	
84		0.20		2.10		1184.80	
85		0.20		2.10		1189.00	
86		0.20		2.10		1193.20	
87		0.20		2.10		1197.40	
88		0.20		2.10		1201.60	
89		0.20		2.10		1205.80	
90		0.20		2.10		1210.00	
91		0.20		2.10		1214.20	
92		0.20		2.10		1218.40	
93		0.20		2.10		1222.60	
94		0.20		2.10		1226.80	
95		0.20		2.10		1231.00	
96		0.20		2.10		1235.20	
97		0.20		2.10		1239.40	
98		0.20		2.10		1243.60	
99		0.20		2.10		1247.80	
100		0.20		2.10		1252.00	

Count	Instrument	Sample Box Number	Ambient Temp						
	Alfa Instruments		Barometric Pressure	29.82					
	9-21-82		Assumed moisture	2.4					
			Nozzle Diameter, in.	.2491					
Reverse Count	Sampling Time, min	Static Pressure (P _g) In. Hg	Stack Temp (T _s) F	Velocity Head (P _s P _g)	Diff. across or. Meter (ft) In H ₂ O	Gas Sample Vol (Vn) ft ³	Gas Sample of Dry Gas Inlet (Tm in) F	Temperature Meter Outlet (Tm out)	Sample Box Temp, F
11	5 min	0.12	121	0.38 (0.63)	1.45	890.67	80	78	64
12	5 min	0.18	142	0.44 (0.66)	1.60	894.00	90	78	55
13	5 min	0.26	175	0.52 (0.74) 0.40	1.90	897.30	95	78	62
14	5 min	0.30	210	0.55 (0.74)	2.00	901.00	100	78	66
15	5 min	0.32	201	0.58 (0.76)	2.10	904.85	102	79	69
16	5 min	0.40	150	0.65 (0.81)	2.35	908.75	104	80	66
17	5 min	0.42	126	0.70 (0.84)	2.50	913.00	106	80	64
18	5 min	0.45	119	0.70 (0.84)	2.58	917.30	108	80	64
19	5 min	0.42	118	0.60 (0.71)	2.20	921.60	110	82	64
20	5 min	0.17	107	0.42 (0.63)	1.55	925.70	108	83	62
21	5 min		2735	14.98 (0.71)		928.85	108	84	62

Calculation

Run #1
3
584

Volume of water collected = V_{WSTD}

$$V_{WSTD} = (0.0474)(24.300) = 1.15 \text{ ft}^3$$

Volume of gas metered @ STP = V_{WSTD}

$$V_{WSTD} = 77.745 \left(\frac{530}{553} \right) \left(\frac{29.99}{29.92} \right) = 74.63$$

Moisture content = M_c

$$M_c = \frac{1.15}{74.63 + 1.15} = 0.015$$

Molecular wt of stack gas = M_s

$$29.38 (1 - 0.015) + 18 (0.015) = 29.21$$

Area area of stack = A

$$\frac{\left(\frac{1}{2} \right)^2 \pi}{144} = 2.18$$

Volume of stack gas = V_s

$$V_s = (85.48)(0.80)(0.75) \sqrt{\frac{582}{(29.99)(29.21) \cdot 0.664}} = 41.742 \text{ ft}^3/\text{sec}$$

Volometric flow Rate = Q

$$(41.742)(2.18)(3600) = 3.2764 \times 10^5 \text{ ft}^3/\text{hr}$$

Volumetric flow rate @ STP = Q_{sw}

$$(3.2764 \times 10^5) \left(\frac{580}{582} \right) \left(\frac{29.99}{29.92} \right) = 2.9908 \times 10^5$$

Volumetric flow rate (dry basis) @ STP = Q_{sd}

$$\left(\frac{74.63}{74.63 + 1.15} \right) (2.9908 \times 10^5) = 2.9454 \times 10^5$$

Sample Area = A_N

$$A_N = \left(\frac{(\frac{1}{2})^2 \pi}{144} \right) = 0.0034 \text{ ft}^2$$

Concentration of particulates/scf = C_s

$$C_s = \frac{0.0326 (15.43)}{74.63} = 0.0067$$

Concentration of particulates, gr/scf @ standard gas cond = C_{sc}

$$C_{sc} = \frac{0.0326 (15.43)}{\frac{74.63 + 1.15}{75.78}} = 0.0066$$

Particulate, lb/hr = C_{ax}

$$\frac{(0.0066) (2.9908 \times 10^5)}{7000} = 0.282$$

$$S @ 12\% \text{ CO}_2 = (0.0067) \left(\frac{12}{4.22} \right)^{2.84} = 0.0190$$

Deskinetic = I

$$C_{ax} @ 12\% (0.0066) \left(\frac{12}{4.22} \right)^{2.84} = 0.0181$$

$$I = \frac{\frac{74.63 + 1.15}{75.78} (41.749) (6000) \frac{1.002}{29.92} \frac{1.911}{582} (0.0034)}{\frac{75.78}{77.24} \times 1000} = 97.5$$

Plant		Sample Box Number		Ambient Temp	47	2			
Location	Worship	Meter Box No.		Barometric Pressure		29.97			
Run No.	3	Meter Δ H _g	1.79	Assumed moisture %					
Date	9-27-82	C Factor	1.00	Nozzle Diameter, in.		1.2498			
Traverse Point	Sampling Time, min	Static Pressure (P _s) in. Hg	Stack Temp (T _s) F	Velocity Head (Δ P _s)	Pressure Diff. across or. Meter (H) in H ₂ O	Gas Sample Vol (V _m) ft ³	Gas Sample of Dry Gas Inlet (T _m in) F	Temperature Meter Outlet (T _m out)	Sample Box Temp, F
	12 25			<u>0.62</u> <u>0.39</u>		930.775	64	64	56
11	5 min	0.10	149	<u>0.67</u> <u>0.39</u>	1.45	930.775	64	64	56
12	5 min	0.15	171	<u>0.67</u> <u>0.39</u>	1.60	934.00	75	65	44
13	5 min	0.20	176	<u>0.71</u> <u>0.50</u>	1.80	937.90	88	68	49
14	5 min	0.24	185	<u>0.74</u> <u>0.55</u>	1.95	941.30	94	70	53
15	5 min	0.27	188	<u>0.77</u> <u>0.59</u>	2.20	944.90	98	71	55
	5 min	0.35	94	<u>0.81</u> <u>0.65</u>	2.40	948.70	102	78	56
17	5 min	0.42	89	<u>0.84</u> <u>0.70</u>	2.50	953.00	108	80	58
1	5 min	0.43	85	<u>0.87</u> <u>0.73</u>	2.40	957.40	110	84	58
1	5 min	0.40	80	<u>0.81</u> <u>0.67</u>	2.20	961.55	114	86	58
	5 min	0.25	78	<u>0.81</u> <u>0.50</u>	1.40	965.70	114	88	58
			(122)	<u>0.81</u> <u>0.50</u>		969.30	110	<u>88</u> <u>84</u>	<u>58</u> <u>53</u>

Point	Location	Sample Box Number	Ambient Temp	Barometric Pressure	Assumed moisture	Nozzle Diameter, in.	Temperature of Dry Gas	Inlet/Outlet (Tm in) F	Outlet (Tm out)	Sample Box Temp, F
Altitude	9-2-2									
Station No.	3	Meter Box No.								
Reverse										
Point										
Sampling Time, min		Stack Temp (Tg) F								
Static Pressure (Pg) in. Hg		Velocity Head (V Pg)								
1	5 min	87	0.45 (0.67)	1.65	969.30	106	88	60		
2	5 min	92	0.55 (0.74)	2.06	973.00	102	88	58		
3	5 min	97	0.10 (0.57)	2.20	976.75	110	90	53		
4	5 min	98	0.65 (0.65)	2.30	980.80	112	80	56		
5	5 min	98	0.65 (0.65)	2.30	985.60	114	91	56		
6	5 min	133	0.70 (0.64)	2.50	989.20	114	92	56		
7	5 min	135	0.68 (0.62)	2.45	993.50	116	93	56		
8	5 min	140	0.65 (0.61)	2.36	997.80	116	94	56		
9	5 min	130	0.50 (0.71)	1.80	1002.0	116	94	56		
10	5 min	130	0.25 (0.50)	0.90	1005.80	112	92	57		
Stop 1420					77.1442	104	91	57		

LIQUID WATER AND PARTICULATE COLLECTED

Plant Point Winona
 Date 4-22-82
 Run No. 3

VOLUME OF LIQUID WATER COLLECTED

	<u>Final</u>		<u>Initial</u>		<u>Gain</u>	
Impinger No. 1	<u>255</u>	ml	<u>250</u>	ml	<u>5.0</u>	ml
Impinger No. 2	<u>153</u>	ml	<u>150</u>	ml	<u>3.0</u>	ml
Impinger No. 3	<u>0</u>	ml	<u>0</u>	ml	<u>0</u>	ml
Impinger No. 4 (**) Silica Gel	<u>223.542</u>	gm	<u>221.092</u>	gm	<u>2.450</u>	ml
Cyclone	<u>0</u>	ml	<u>0</u>	ml	<u>0</u>	ml

(**) 1 gram = 1 milliliter

Total volume collected 24.300 ml

WEIGHT OF PARTICULATE COLLECTED

	<u>Final</u>		<u>Tare</u>		<u>Gain</u>	
Filter No. <u>24</u>	<u>0.2455</u>	gm	<u>0.2209</u>	gm	<u>0.0246</u>	g
Cyclone	<u>0.0058</u>	gm	<u>X X X X X X</u>		<u>0.0058</u>	g
Probe	<u>0.0002</u>	gm	<u>X X X X X X</u>		<u>0.0002</u>	g

(1 gram = 1000 milligrams)

Total weight collected 0.0306 g