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9 75

fuel flow rates,
Have data on % Load &
Engine capacity

IC engine
criteria pollutant
exhaust.
TSP, NOx, CO, TNMHC
flow auto

Compliance Test Report → H₂S Inlet &
Landfill Gas Fired TNMHC Inlet.
Internal Combustion Engine
Oceanside Landfill Gas Recovery Facility
Energy Tactics, Inc.
Oceanside, New York

ROJAC *Environmental Services, Inc.*

Leigh A. Gammie
Principal Engineer

Eszter J. Samodai
Project Scientist

ROJAC Project D92-09

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30 Arbor Street • Hartford, Connecticut 06106 • (203) 232-8959

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1.0 INTRODUCTION

1.1 Summary of Test Program

ROJAC Environmental Services Inc. (ROJAC) was retained by Energy Tactics, Inc. (ET) to conduct an emission measurement test program on one of their landfill gas fired internal combustion engines located at the Oceanside Landfill Gas Recovery Facility in Oceanside, New York. The testing of the engine was conducted in two phases, namely under 75% and 100% of full load conditions.

The test program consisted of measuring total suspended particulates (TSP), oxides of nitrogen (NO_x), carbon monoxide (CO), diluent oxygen (O_2), and total non methane hydrocarbons (TNMHC) being exhausted from the unit. The tests were conducted in triplicate in accordance with EPA Methods 1-5, 7E, 10, 3A, and 18, respectively. In addition, samples of landfill gas (LFG) were collected for hydrogen sulfide (H_2S) content analysis.

1.2 Key Personnel

The ROJAC test team consisted of the Project Manager, Engineer, and Technician. Ms. Eszter Samodai served as the Project Manager and CEM specialist. Mr. John Gammie headed the TSP test team, with Mr. Jim Davis serving as his technical assistant. Mr. Gary Zimmerman was the on-site observer from the New York State Department of Environmental Conservation (NYSDEC).

2.0 SOURCE AND SAMPLING LOCATION DESCRIPTIONS

2.1 Source Description

Energy Tactics, Inc. operates eight (8) Caterpillar Model G-399 HCR TA-SI internal combustion engines at their Oceanside Landfill Gas Recovery Facility located in Oceanside, New York. The engines are modified for a lean burn system, and are fired with LFG produced on site.

Each engine has 16 cylinders with a 3928 cubic inch displacement for a total rated output of 832 horsepower and 590 kilowatts (KW) of generator capacity. The electrical power produced is sold to Long Island Lighting Company (LILCO).

The pretreatment of the LFG consists of moisture removal, followed by compression, cooling, inertial separation, and filtration. The methane (CH_4) content of the LFG is estimated at approximately 50%. No post combustion pollution control system is used. Each engine is exhausted through a muffler and a horizontal duct approximately 15 feet above ground level.

2.2 Sampling Location

Emissions sampling was conducted in the ten inch ID horizontal section of exhaust duct of engine ET-29 (NYSDEC Emission Point 007). Two (2) ports were spaced 90 degrees apart, 186 inches (18.6 duct diameters) downstream from the the two silencers, and 30 inches (3.0 duct diameters) upstream from the end of the ductwork.

In accordance with EPA Method 1, a total of eight (8) sampling points were used for the velocity traverse and TSP tests with four (4) points being accessed from each port. An additional port, placed further downstream was used for the continuous emission monitoring (CEM) tests. Figure 2-1 shows a schematic diagram of the sampling location along with the traverse point locations.

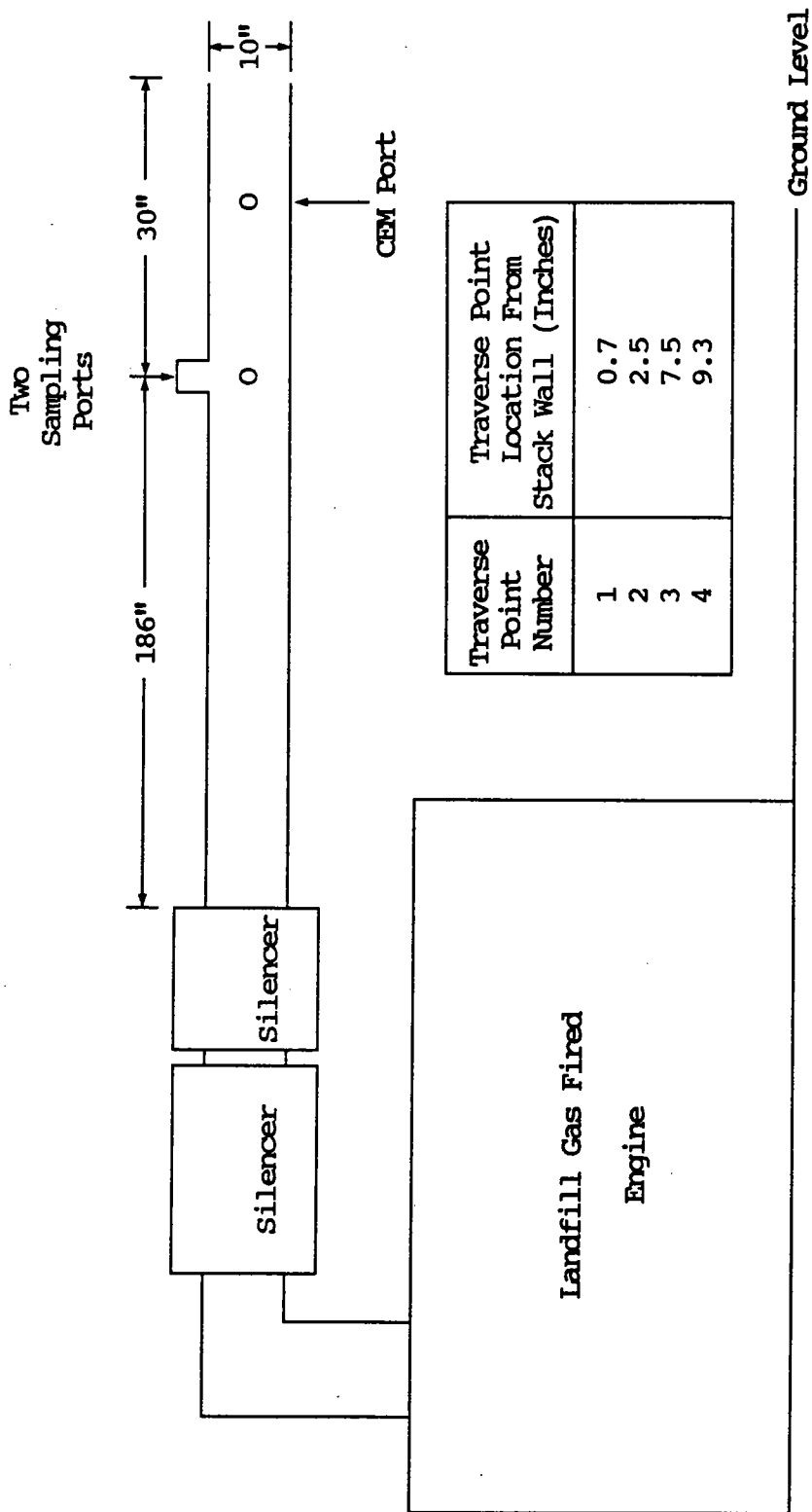


FIGURE 2-1

ET-29 Outlet Sampling Location
 Oceanside Landfill Gas Recovery Facility
 Energy Tactics, Inc.
 Oceanside, New York

3.0 SUMMARY AND DISCUSSION OF RESULTS

3.1 Objectives and Test Matrix

The purpose of the test program was to determine the emissions from LFG fired internal combustion engine number ET-29 (NYSDEC Emission Point 007). Table 3-1 shows the emission measurement test matrix. Testing was conducted under 75% and 100% of full load conditions. All operational data collected during the tests is included in the Appendix. Since all eight (8) Caterpillar engines are identical, only one engine was required to be tested. The specific objectives of the test program were to:

- * measure the emissions of TSP, NO_x, CO, and O₂.
- * collect samples of exhaust gas in Tedlar bags for TNMHC analysis by GC/FID.
- * collect samples of LFG for H₂S analysis.

The emission limitations for each pollutant mentioned above is as follows:

NO _x :	2.80 pounds per hour (lb/hr)
CO:	4.10 lb/hr
TNMHC:	0.04 lb/hr
TSP:	0.50 lb/hr

TABLE 3-1
EMISSION MEASUREMENT TEST MATRIX
OCEANSIDE LANDFILL GAS RECOVERY FACILITY
ENERGY TACTICS, INC. - OCEANSIDE, NEW YORK
OCTOBER 6 & 7, 1992

Sampling Location	No. of Runs	Sample/Type Pollutant	Sampling Method	Sampling Organ.	Sample Run Time (min.)	Analytical Method	Analytical Laboratory
ET-29 OUTLET 100% LOAD	3	TSP	M1 - M5	RES	60	M5 Gravimetric	CIGNA
	3	NOx, CO, O2	M7E, M10 M3A	RES	60	M7E, M10 M3A	RES
	3	TNMHC	M18	RES	60	M18 GC/FID	AAL
	3	LFG	GRAB	ET	GRAB	GC	AAL
ET-29 OUTLET 75% LOAD	3	TSP	M1 - M5	RES	60	M5 Gravimetric	CIGNA
	3	NOx, CO, O2	M7E, M10 M3A	RES	60	M7E, M10 M3A	RES
	3	TNMHC	M18	RES	60	M18 GC/FID	AAL
	3	LFG	GRAB	ET	GRAB	GC	AAL

3.2 Field Test Changes and Problems

The only problem encountered during the test program was a temporary CEM system condenser freeze-up. The condenser allows for the conditioning of the exhaust gas by removing the moisture and supplying dry sample to the analyzers. Because of the high moisture content of the stack gas, water collected in the condenser coils and froze, temporarily blocking the sample flow. The condition was quickly remedied by heating the coils to above freezing whereby the flow of sample gas was resumed. The 15 minutes of CEM sampling time lost due to this problem was added on to the end of the test run. The remainder of the sampling progressed according to schedule with no further testing or operational problems.

3.3 ET-29 - 100% Load

3.3.1 Total Suspended Particulate Summary of Results

Three Method 5 tests were performed on October 6, 1992 while the engine was at 100% of full load. The results are shown on Table 3-2. The average TSP emission rate was 0.03 lb/hr which was below the particulate matter emission rate limit of 0.50 lb/hr.

3.3.2 Oxides of Nitrogen Summary of Results

Triplicate one hour Method 7E tests were conducted in conjunction with the TSP tests. The results (Table 3-2) show an average NO_x (as NO₂) emission rate of 2.4 lb/hr which is below the allowable emission rate of 2.8 lb/hr.

3.3.3 Carbon Monoxide Summary of Results

Triplicate one hour Method 10 tests were conducted simultaneously with the other compliance tests. The average CO emission rate was shown to be 2.4 lb/hr which is below the allowable 4.1 lb/hr limit.

3.3.4 Total Non Methane Hydrocarbons Summary of Results

Triplicate integrated one hour Method 18 bag samples were collected for TNMHC analyses by gas chromatography/flame ionization detection (GC/FID). The results show an average TNMHC emission rate of 1.0 lb/hr which is above the emission limitation of 0.04 lb/hr. All laboratory analysis reports and calculations are contained in the Appendix.

TABLE 3-2
SUMMARY OF COMPLIANCE EMISSION MEASUREMENT RESULTS
OCEANSIDE LANDFILL GAS RECOVERY FACILITY
ENERGY TACTICS, INC. - OCEANSIDE, NEW YORK
OCTOBER 6 & 7, 1992

Method/Component		ET-29 - Emission Pt. 007 - 100% Load - October 6, 1992			
	Units	Run 1	Run 2	Run 3	Avg
Method 5 - TSP	mg	6.3	5.0	3.5	4.9
Method 5 - TSP	lb/hr	0.04	0.03	0.02	0.03
Method 7E - NOx	ppm, dry	191.7	201.0	195.8	196.2
Method 10 - CO	ppm, dry	326.1	325.5	322.6	324.7
Method 18 - TNMHC as CH4	ppm, dry	228.0	228.0	250.0	235.3
Method 7E - NOx as NO2	lb/hr	2.3	2.5	2.4	2.4
Method 10 - CO	lb/hr	2.4	2.4	2.4	2.4
Method 18 - TNMHC as CH4	lb/hr	0.97	0.97	1.06	1.00
Method 3A - O2	%	5.8	5.7	5.8	5.8
Method 3 - CO2	%	12.6	12.8	12.9	12.8
Method 2 - Flow	dscfm	1701	1709	1705	1705
Method 4 - Moisture	%	10.6	13.4	12.9	12.3
Landfill Gas - H2S	ppm	57.0	65.0	62.0	61.3
Method/Component		ET-29 - Emission Pt. 007 - 75% Load - October 7, 1992			
	Units	Run 4	Run 5	Run 6	Avg
Method 5 - TSP	mg	2.5	1.6	2.2	2.1
Method 5 - TSP	lb/hr	0.01	0.01	0.01	0.01
Method 7E - NOx	ppm, dry	147.1	99.9	107.2	118.1
Method 10 - CO	ppm, dry	353.1	338.0	338.8	343.3
Method 18 - TNMHC as CH4	ppm, dry	126.0	60.0	30.0	72.0
Method 7E - NOx as NO2	lb/hr	1.6	1.1	1.1	1.3
Method 10 - CO	lb/hr	2.3	2.2	2.2	2.2
Method 18 - TNMHC as CH4	lb/hr	0.47	0.23	0.11	0.27
Method 3A - O2	%	4.5	4.8	4.7	4.7
Method 3 - CO2	%	13.5	13.7	13.9	13.7
Method 2 - Flow	dscfm	1509	1514	1462	1495
Method 4 - Moisture	%	13.7	13.5	14.0	13.7
Landfill Gas - H2S	ppm	54.0	54.0	45.0	51.0

3.3.5 Fuel Analysis Summary of Results

Triplicate samples of LFG fuel were collected during the compliance tests for H₂S analysis by GC. The results showed an average H₂S content of 61.3 parts per million by volume (ppmv). The H₂S content of the fuel is not subject to any limitations.

3.4 ET-29 - 75% Load

3.4.1 Total Suspended Particulate Summary of Results

Three Method 5 tests were performed on October 7, 1992 while the engine was at 75% of full load. The results are shown on Table 3-2. The average TSP emission rate was 0.01 lb/hr which was below the particulate matter emission rate limit of 0.50 lb/hr.

3.4.2 Oxides of Nitrogen Summary of Results

Triplicate one hour Method 7E tests were conducted in conjunction with the TSP tests. The results (Table 3-2) show an average NO_x (as NO₂) emission rate of 1.3 lb/hr which is below the allowable emission rate of 2.8 lb/hr.

3.4.3 Carbon Monoxide Summary of Results

Triplicate one hour Method 10 tests were conducted simultaneously with the other compliance tests. The average CO emission rate was shown to be 2.2 lb/hr which is below the allowable 4.1 lb/hr limit.

3.4.4 Total Non Methane Hydrocarbons Summary of Results

Triplicate integrated one hour Method 18 bag samples were collected for TNMHC analyses by GC/FID. The results show an average TNMHC emission rate of 0.27 lb/hr which is above the emission limitation of 0.04 lb/hr.

3.4.5 Fuel Analysis Summary of Results

Triplicate samples of LFG fuel were collected during the compliance tests for H₂S analysis by GC. The results showed an average H₂S content of 51.0 ppmv. The H₂S content of the fuel is not subject to any limitations.

4.0 SAMPLING AND ANALYTICAL PROCEDURES

4.1 Particulate Matter Tests

Particulate matter sampling was accomplished using the EPA Method 5 collection train, described in the Code of Federal Regulations, Title 40, Part 60. It is shown schematically in Figure 4-1 and consisted of a nozzle, probe, filter, a flexible umbilical line, Teflon sample line, four impingers, vacuum pump, dry gas meter, and an orifice flowmeter. Complete sampling train calibrations were performed before and after the compliance test program.

A nozzle (1) was attached to a stainless steel probe (2). Pallflex 2500 fiberglass filter paper supported in a 4 inch glass filter holder (3) was used as the collection media. The filter assembly was enclosed in a heated box (4) to maintain temperatures at $248^{\circ}\text{F} \pm 25^{\circ}\text{F}$. An ice bath containing four impingers (5) was attached to the back end of the filter via a Teflon sample line. The first two impingers contained distilled water, the third was dry, and the fourth contained silica gel to remove any remaining moisture. Flexible tubing (6), vacuum gauge (7), needle valve (8), leakless vacuum pump (9), bypass valve (10), dry gas meter (11), calibrated orifice and inclined manometer (12) completed the sampling train. The stack velocity pressure was measured using a pitot tube and inclined manometer (13). The stack temperature was monitored by a thermocouple that was attached to the pitot and connected to a potentiometer (14). A check valve was not used in the ROJAC sampling train.

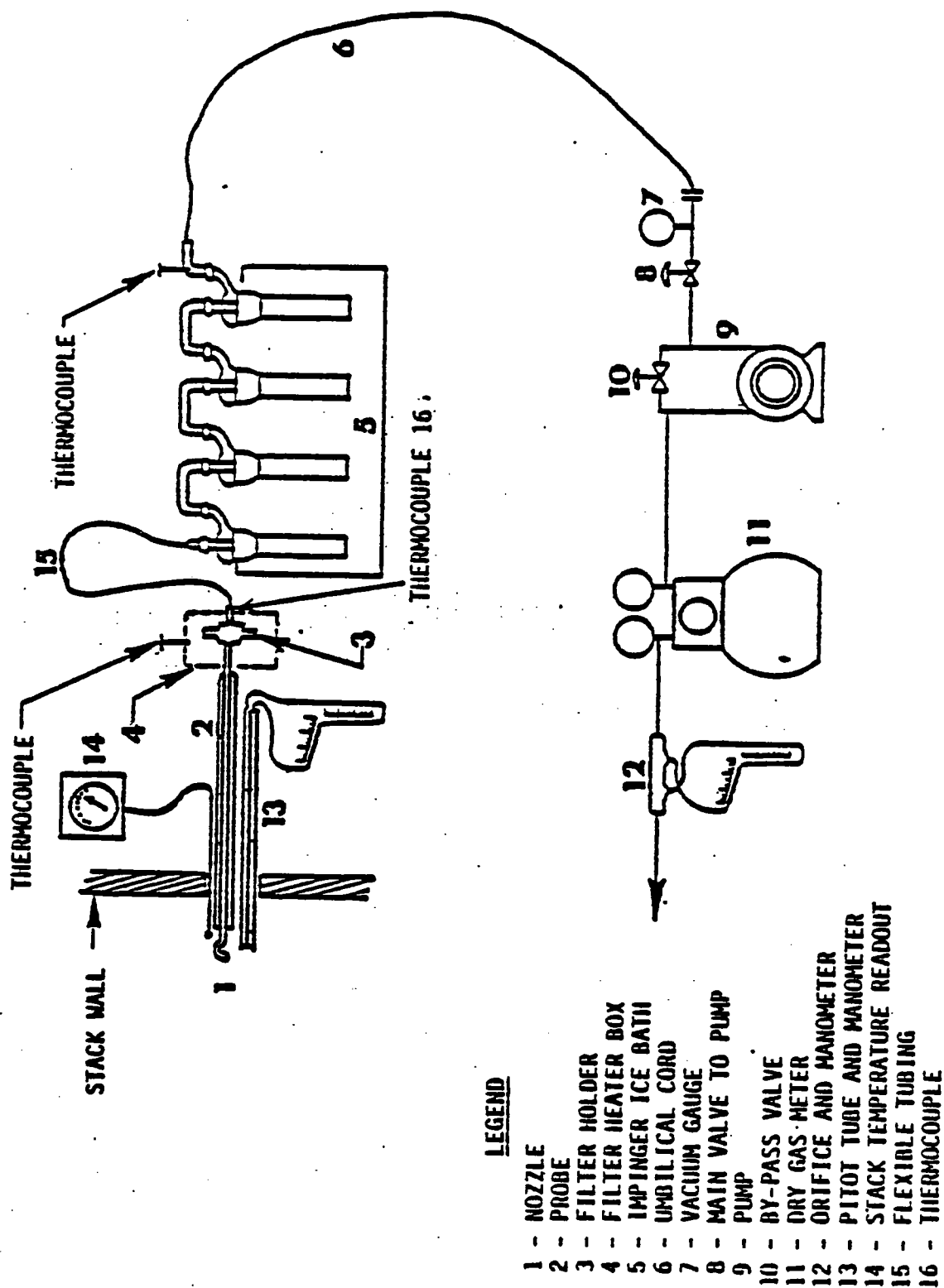


FIGURE 4-1

Modified EPA Method 5 Particulate Sampling Train

A nomograph was used to quickly determine the orifice pressure drop required for any pitot velocity pressure and stack temperature to maintain isokinetic sampling conditions. Sampling flow was adjusted by means of the bypass valve. Before and after each particulate matter test run the sampling train was leak checked.

All recorded test data can be found on the field data sheets contained in the Appendix. At the end of each test, three sample containers were used as follows:

Container 1 - Filter.

Container 2 - Acetone wash of probe and front half of filter. The probe and nozzles were washed and brushed three times.

Container 3 - Silica gel from the fourth impinger.

The samples were transported to the laboratory and the following analyses performed:

Container 1 - Transferred filter and any loose particulate matter from the sample container to a tared glass weighing dish, desiccated and dried to constant weight. Reported results to the nearest 0.1 mg.

Container 2 - Transferred the acetone washings to a tared beaker and evaporated to dryness at ambient temperature and pressure. Desiccated and dried to a constant weight. Reported results to the nearest 0.1 mg.

Container 3 - Weighed silica gel to the nearest 0.5 g. The weight of the moisture entrapped in the silica gel, along with the volume of moisture which condensed in the impingers, was used to calculate the moisture content of the flue gas.

Prior to testing, a preliminary velocity traverse, covering all sampling points, was performed to check for cyclonic flow. The pitot-nulling technique was used to determine whether cyclonic flow was present, as detailed in EPA Methods 1 and 2.

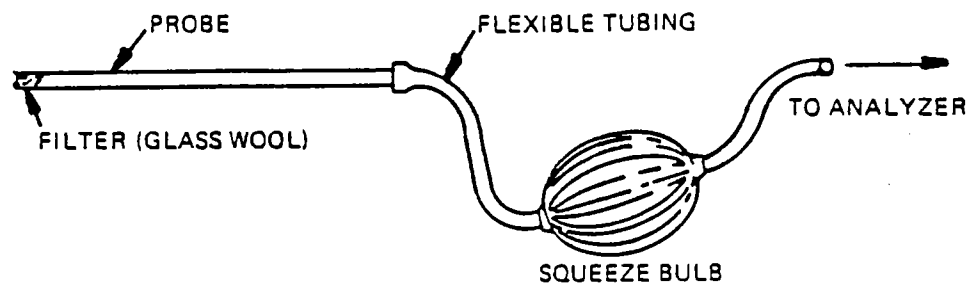
A computer program developed by ROJAC was used to calculate mass emission rates in pounds per hour (lb/hr) based on the measured flowrates in dry standard cubic feet per minute (dscfm). The program also calculated percent moisture, molecular weight of the stack gas at stack conditions, and the percent isokinetics (Appendix).

4.2 Gas Analysis

The composition of the gas stream at the sampling location was analyzed for oxygen and carbon dioxide during each test run in accordance with CFR, Title 40, Part 60, Appendix A, Method 3. To make accurate assessment of the flue gas composition, redundant Orsat analyses were conducted. During each particulate matter test run one multi-point integrated sample of flue gas was taken for Orsat analyses. The integrated gas sampling train used for Method 3 is shown in Figure 4-2.

4.3 Continuous Emission Monitoring

ROJAC conducted exhaust flue gas measurements for O_2 , NO_x , and CO using EPA Reference Methods 3A, 7E, and 10, respectively. Sample gas was drawn through a stainless steel probe, through a filter, a heated Teflon sample line, and a refrigerator type condenser by a Teflon lined diaphragm vacuum pump.



GRAB SAMPLE SETUP FOR MOLECULAR WEIGHT DETERMINATION

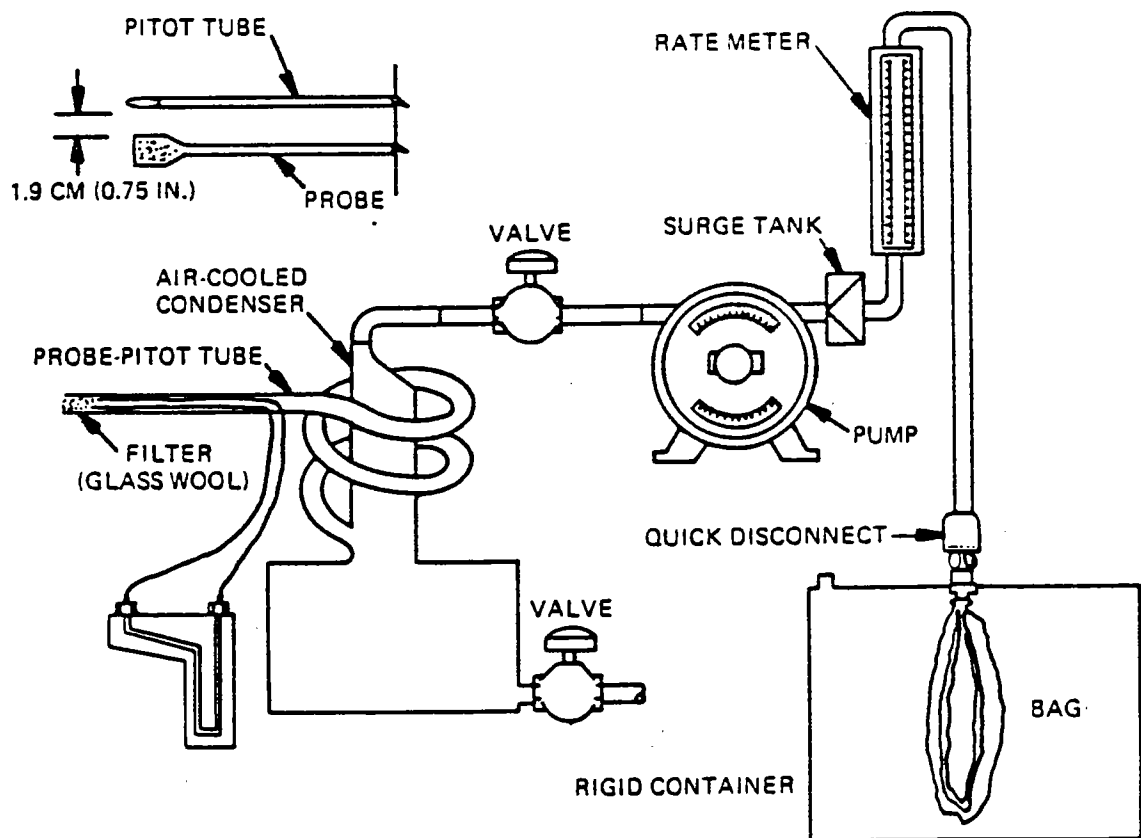


FIGURE 4-2

EPA Method 3 Exhaust Gas Measurement Sampling Train

From the pump the sample was sent into a manifold to which the analyzers were attached. Figure 4-3 shows a schematic diagram of the CEM sampling system.

Analyzer outputs were recorded by a data acquisition system (DAS) at 30 second intervals. Triplicate one hour test runs were conducted.

The O₂ instrument was a Servomex Model 1420 analyzer which measures O₂ concentration by means of the paramagnetic susceptibility of the sample gas using a proven magneto-type measuring cell. Oxygen molecules are attracted more strongly by the magnetic field than are molecules of other gases and their concentrations can thereby be measured.

The NO_x instrument was a Beckman Model 951 NO/NO_x analyzer. This analyzer utilizes the principle of chemiluminescence, whereby NO in the sample gas reacts with ozone at a specific wavelength. The intensity of this light is proportional to the NO concentration.

The CO instrument was an Horiba Model PIR-2000 analyzer. This analyzer measures CO concentration by means of non-dispersive infrared radiation (NDIR). The infrared radiation is produced by the analyzer and is, in turn, absorbed by the continuous flow of sample gas through the analyzer. The percentage of infrared radiation thus absorbed is proportional to the concentration of CO in the gas stream.

Certified EPA Protocol 1 compressed gas mixtures of NO, CO, and O₂, supplied by Scott Specialty Gases and Matheson Gas Products, were used as the calibration standards. The high range CO calibration gas was non-protocol, as allowed by EPA Method 10. High purity zero grade air served as the zero gas and high-level (21.0%) O₂ calibration gas.

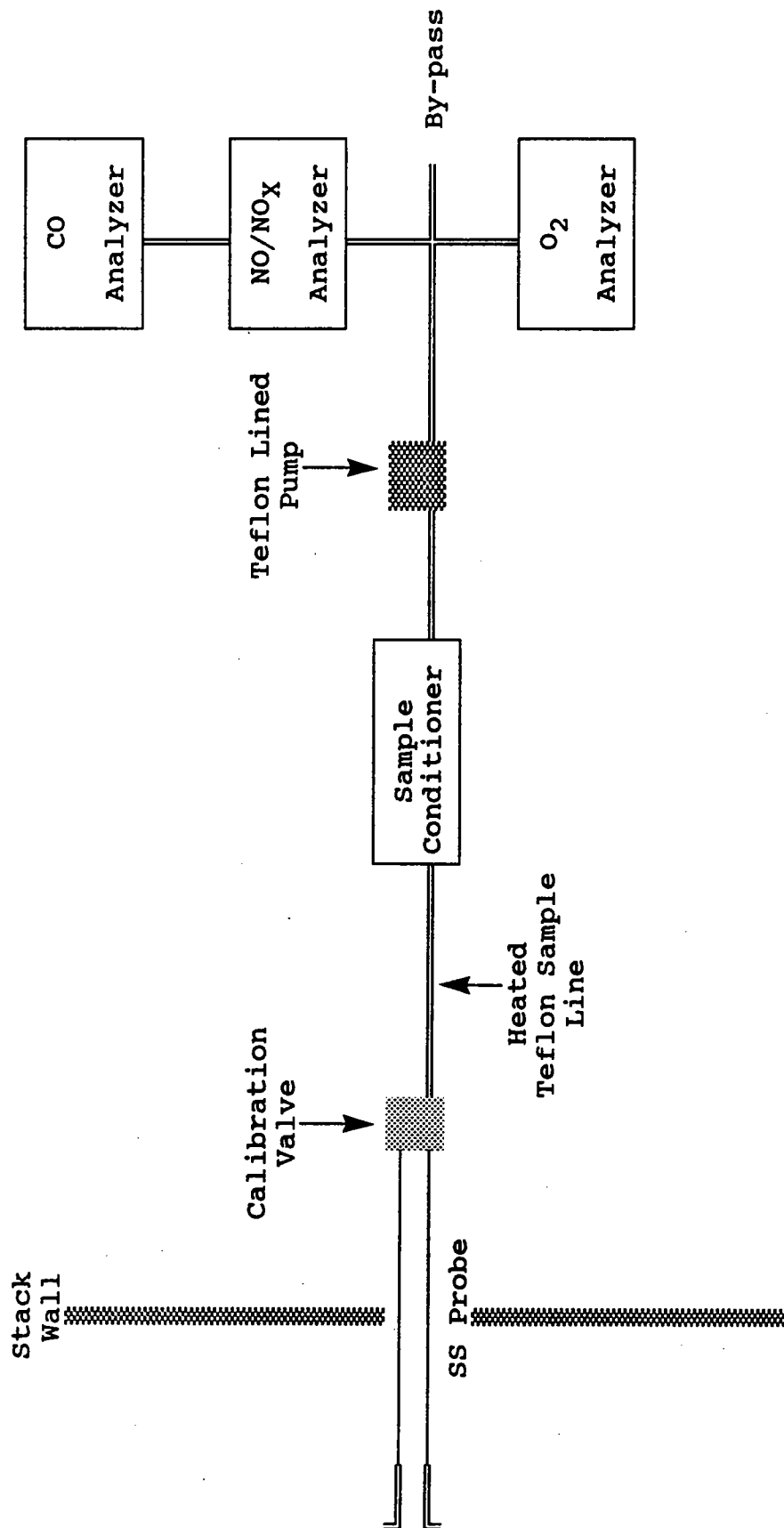


FIGURE 4-3
 EPA Methods 3A, 7E, and 10
 Continuous Emission Monitoring Sampling System

A full range calibration and linearity check was performed on each analyzer at the beginning of each test day. In addition, each analyzer was zeroed and spanned before and after each test run. These multi-point and single-point calibrations were performed with the above-mentioned calibration standards and zero gas. The span and zero gases passed through all components of the sampling train except the sampling probe.

The gas mixtures were chosen in accordance with the appropriate methodologies as outlined in CFR Title 40, Part 60, Appendix A. Copies of the EPA Protocol 1 Certifications are contained in the Appendix.

The zero and span calibrations were performed to document any instrument drift. CEM readings were recorded at 30 second intervals by the DAS during the entire test program. Using Equation 6C-1, the readings were corrected to account for the zero and span values and any instrument drift as follows:

$$C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_m - C_0},$$

where C_{gas} = emissions concentration (ppm or %)

$\bar{C}$ = average emissions reading (ppm or %)

C_0 = average zero reading (ppm or %)

C_m = average span reading (ppm or %)

C_{ma} = span gas concentration (ppm or %).

4.4 Total Non-Methane Hydrocarbons Tests

TNMHC determinations were made in accordance with EPA Reference Method 18. Collected samples were analyzed for all detectable organic compounds, with the exception of methane (CH_4), by GC/FID. Extreme care was taken during both the sampling and analytical portions of this phase of the testing. Strict QA/QC procedures were followed to produce the most accurate and reliable results possible.

Integrated samples were collected in conjunction with the EPA Method 5 tests. A short non-heated Teflon sample line conveyed the exhaust gas to a Tedlar bag. Sampling during each test run was conducted over a minimum 45 minute period. The approximate sample volume was 28 liters (1 cubic foot) per bag.

The bags were filled at a constant rate of approximately 0.6 liters per minute (lpm) by placing them inside a rigid container and evacuating the air within the container. The Teflon sample line passed through the wall of the rigid container and connected to the sample bag, creating a vacuum seal. The resulting vacuum served to inflate the bag with the extracted flue gas sample. In this manner, sample integrity was assured. Each sample line/bag pair was filled, purged, and filled again to condition the sampling train and minimize any wall absorption effects. Figure 4-4 shows a schematic of the "bag-in-the-box" setup.

At the end of the field test program, the bag samples were rushed to the laboratory and analyzed within 24 hours. The analysis method for TNMHC concentration was by GC/FID.

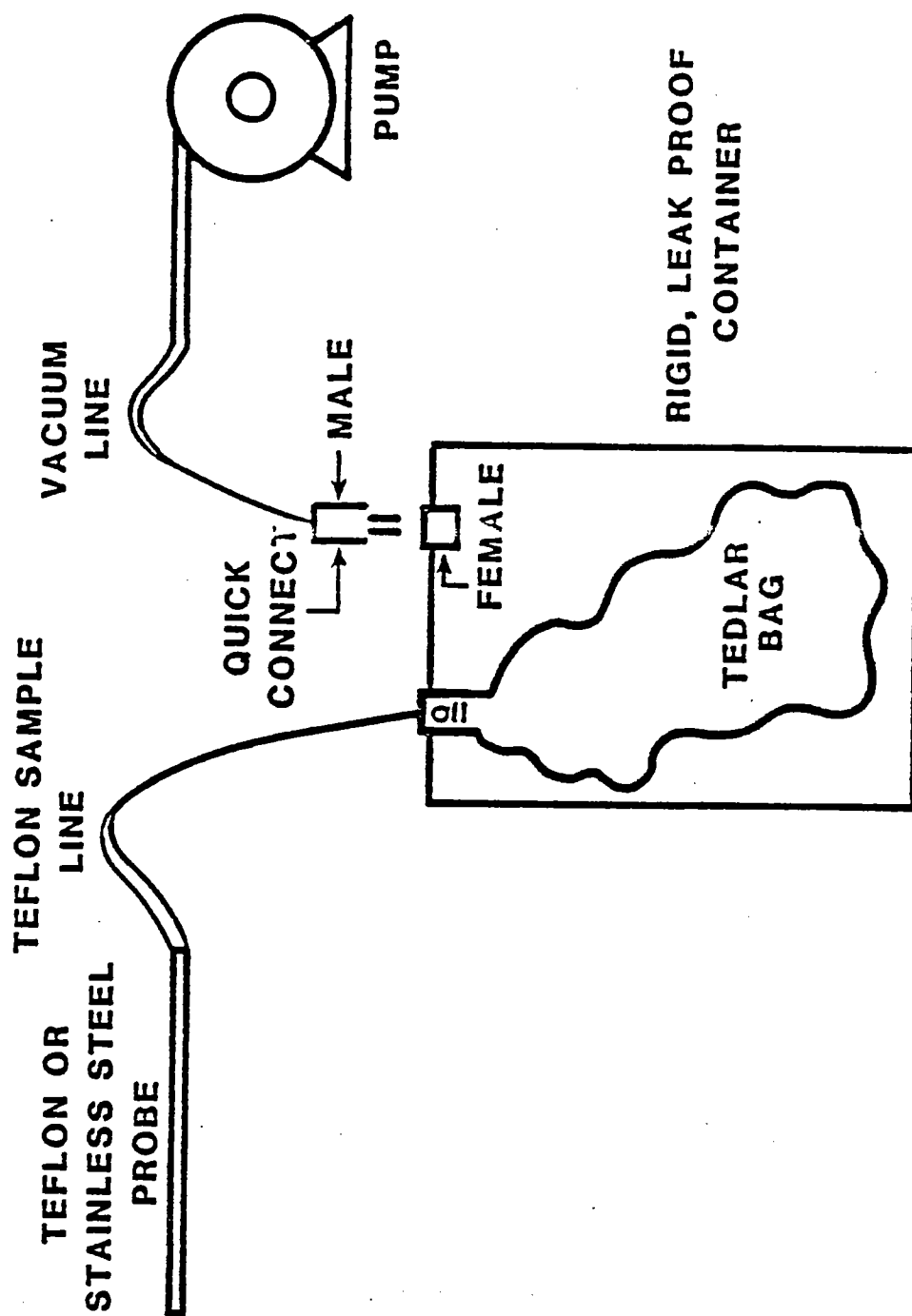


FIGURE 4-4
EPA Method 18 Sampling Train

GC conditions, such as column type, carrier flowrate, temperature, and injected sample volume were carefully determined to maximize peak resolution and separation. Calibration standards were prepared in advance according to the Method 18 protocol. Three standards for high, low, and middle concentration ranges were prepared to encompass the expected stack gas concentration of each compound. Each bag sample was analyzed in duplicate.

The low end of the analytical range of this method of analysis is one (1) ppm. The precision of duplicate analyses is within 5% of their mean value, and the accuracy is within 10% of expected values.

4.5 Fuel Analysis

In addition to the triplicate bag samples collected at the outlet during each phase of testing, samples of LFG were also collected during each test run. These LFG samples were analyzed for H₂S content by GC using a "Hall" detector. The results were reported in ppm by volume. All laboratory analysis reports are contained in the Appendix.

5.0 QA/QC ACTIVITIES

ROJAC maintains specific laboratory facilities dedicated to maintenance and calibration of source sampling equipment used in performing EPA reference method source tests. These facilities include all equipment and standards necessary for equipment calibration using the procedures outlined in the Quality Assurance Handbook for Air Pollution Measurement Systems, Volume III, Stationary Source Specific Methods, (EPA 600/4-77-027b).

The checkout and calibration of the source sampling equipment was performed prior to and at the completion of the project. Referenced calibration procedures were strictly followed and the results properly documented and retained. The following calibrated equipment was used during the test program.

- * Type-S Pitot Tubes
- * Sampling Nozzles
- * Type-K Thermocouples
- * Dry Gas Meters

Calculations for determining flow rates, moisture contents, isokinetics, particulate and gaseous concentrations were made using a computer program developed by the QA/QC Manager at ROJAC. This program utilizes the calculation procedures and equations specified in EPA Methods 2, 4, and 5. The program has been successfully used for numerous test efforts and has been validated by independent performance audits.

Data were input to the software directly from the field data sheets. Sample calculations were performed by the spreadsheet programs, and all information is contained in the Appendix.

Quality control for the various organic and inorganic analytical procedures was established using field blanks, method blanks, trip blanks, surrogate spiking, and internal standards for quantification. Any specific occurrences encountered during sample analysis are provided in the Appendix.

Sample analysis of TNMHC for this particular test program was conducted by Atlantic Analytical Laboratory, Inc. (AAL), located in Whitehouse, New Jersey. AAL was chosen because of their extensive knowledge of the methodology involved, and their strict adherence to recognized QA/QC procedures.

Sample custody procedures for this program were based on EPA recommended procedures. The project manager was responsible for ensuring that proper custody and documentation procedures were followed for the field sampling and field analytical efforts. The project manager was assisted in this effort by key sampling personnel involved in sample recovery.

All sampling data, including information regarding sampling times, locations, and any specific considerations associated with sample acquisition were recorded in black ink on pre-formatted data sheets which can be found in the Appendix.

Following sample collection, all samples were given a unique alphanumeric sample identification code. Sample labels and integrity seals were completed and affixed to the sample container. Samples were stored in a secure area until shipment. The sample volumes were measured and recorded, and the liquid levels on each bottle were marked. All samples were packed and shipped according to Department of Transportation (DOT) guidelines. As the samples were packed for shipment to the appropriate laboratories, chain-of-custody forms were completed for each shipment box, and enclosed therein.

APPENDIX A

Test Results and Calculations

EPA METHODS 2, 3, 4, AND 5

CLIENT: ET/OCEANSIDE
 PROJ. NO.: D92-09
 LOCATION: OUTLET - 100% LOAD

RUN NO.:	M5-1	M5-2	M5-3	AVERAGE
DATE:	10/06/92	10/06/92	10/06/92	
TIME:	1015-1125	1212-1323	1353-1502	
PBAR, (in. Hg)	30.36	30.36	30.36	30.36
STACK AREA, (Sq. Ft.)	0.55	0.55	0.55	0.55
NOZZLE DIA., (in.)	0.188	0.188	0.188	0.188
TOTAL TIME, (minutes)	64	64	64	64
CALIBRATION FACTOR	1.0014	1.0014	1.0014	1.0014
PITOT COEFFICIENT	0.84	0.84	0.84	0.84
SQ. RT. DELTA P, (in. H2O)	1.61	1.66	1.65	1.64
DELTA H, (in. H2O)	1.32	1.28	1.18	1.26
METER TEMP., (Degree F)	82	82	88	84
STATIC PRESS., (in. H2O)	0.96	0.97	1.00	0.98
STACK TEMP., (Degree F)	855	855	854	855
METER VOLUME, (cu.ft.)	40.17	40.01	38.76	39.65
TOTAL H2O VAPOR, (ml)	100.7	130.3	119.3	116.8
CO2 IN STACK GAS, (%)	12.6	12.8	12.9	12.8
O2 IN STACK GAS, (%)	6.4	6.0	6.1	6.2
CO IN STACK GAS, (%)	0.0	0.0	0.0	0.0
N2 IN STACK GAS, (%)	81.0	81.2	81.0	81.1
TOTAL PART. CATCH, (mg)	6.3	5.0	3.5	4.9
HYDROGEN IN FUEL, (%)				0.0
CARBON IN FUEL, (%)				0.0
SULFUR IN FUEL, (%)				0.0
NITROGEN IN FUEL, (%)				0.0
OXYGEN IN FUEL, (%)				0.0
GCV, (BTU/lb)				0.0
METER VOL. STD, (cu.ft.)	39.89	39.73	38.06	39.22
H2O IN STACK GAS, (%)	10.62	13.37	12.86	12.28
STACK GAS MOLECULAR WT	28.97	28.64	28.73	28.78
EXCESS AIR, (%)	42.7	38.9	39.9	40.5
STACK GAS VEL., (FPM)	8472.58	8784.85	8703.87	8653.77
GAS FLOWRATE, (ACFM)	4660	4832	4787	4760
STP FLOWRATE, (DSCFM)	1701	1709	1705	1705
ISOKINETIC, (%)	104.6	103.7	99.6	102.6
PART. CONC., (GR/ACF)	8.8953E-04	6.8699E-04	5.0542E-04	6.9398E-04
PART. CONC., (GR/DSCF)	2.4371E-03	1.9419E-03	1.4191E-03	1.9327E-03
EMISSION RATE, (lb/hr)	0.04	0.03	0.02	0.03
CONC., (GR/DSCF@12%CO2)	2.3210E-03	1.8205E-03	1.3200E-03	1.8205E-03
F-FACTOR, (DSCF/MMBTU)	ERR	ERR	ERR	ERR
EMISSIONS, (lb/MMBTU)	ERR	ERR	ERR	ERR

EPA METHODS 2, 3, 4, AND 5

CLIENT: ET/OCEANSIDE
 PROJ. NO.: D92-09
 LOCATION: OUTLET - 75% LOAD

RUN NO.:	M5-4	M5-5	M5-6	AVERAGE
DATE:	10/07/92	10/07/92	10/07/92	
TIME:	0928-1037	1112-1221	1258-1406	
PBAR, (in. Hg)	30.30	30.30	30.30	30.30
STACK AREA, (Sq. Ft.)	0.55	0.55	0.55	0.55
NOZZLE DIA., (in.)	0.250	0.250	0.250	0.250
TOTAL TIME, (minutes)	64	64	64	64
CALIBRATION FACTOR	1.0014	1.0014	1.0014	1.0014
PITOT COEFFICIENT	0.84	0.84	0.84	0.84
SQ. RT. DELTA P, (in. H2O)	1.49	1.50	1.45	1.48
DELTA H, (in. H2O)	2.92	3.00	2.79	2.90
METER TEMP., (Degree F)	84	91	90	88
STATIC PRESS., (in. H2O)	0.90	0.92	0.90	0.91
STACK TEMP., (Degree F)	884	900	894	893
METER VOLUME, (cu.ft.)	56.68	58.37	56.85	57.30
TOTAL H2O VAPOR, (ml)	189.6	189.1	192.1	190.3
CO2 IN STACK GAS, (%)	13.5	13.7	13.9	13.7
O2 IN STACK GAS, (%)	5.1	4.9	4.9	5.0
CO IN STACK GAS, (%)	0.0	0.0	0.0	0.0
N2 IN STACK GAS, (%)	81.4	81.4	81.2	81.3
TOTAL PART. CATCH, (mg)	2.5	1.6	2.2	2.1
HYDROGEN IN FUEL, (%)				0.0
CARBON IN FUEL, (%)				0.0
SULFUR IN FUEL, (%)				0.0
NITROGEN IN FUEL, (%)				0.0
OXYGEN IN FUEL, (%)				0.0
GCV, (BTU/lb)				0.0
METER VOL. STD, (cu.ft.)	56.18	57.13	55.72	56.35
H2O IN STACK GAS, (%)	13.71	13.48	13.96	13.72
STACK GAS MOLECULAR WT	28.67	28.72	28.69	28.69
EXCESS AIR, (%)	31.1	29.5	29.6	30.1
STACK GAS VEL., (FPM)	7975.19	8076.29	7803.72	7951.73
GAS FLOWRATE, (ACFM)	4386	4442	4292	4373
STP FLOWRATE, (DSCFM)	1509	1514	1462	1495
ISOKINETIC, (%)	93.9	95.2	96.2	95.1
PART. CONC., (GR/ACF)	2.3623E-04	1.4732E-04	2.0744E-04	1.9700E-04
PART. CONC., (GR/DSCF)	6.8658E-04	4.3212E-04	6.0921E-04	5.7597E-04
EMISSION RATE, (lb/hr)	0.01	0.01	0.01	0.01
CONC., (GR/DSCF@12%CO2)	6.1030E-04	3.7850E-04	5.2594E-04	5.0491E-04
F-FACTOR, (DSCF/MMBTU)	ERR	ERR	ERR	ERR
EMISSIONS, (lb/MMBTU)	ERR	ERR	ERR	ERR

EXAMPLE CALCULATIONS

EPA METHODS 2, 3, 4, AND 5

CLIENT: ET/OCEANSIDE
 LOCATION: OUTLET - 100% LOAD
 PROJ. NO: D92-09
 DATE: 10/06/92

EMISSION CALCULATION SYMBOLS

INPUTS

P bar	=	30.36	-Barometric pressure, "Hg
As	=	0.55	-Cross sectional area of duct, square feet
Dn	=	0.188	-Nozzle Diameter, inches
T tot	=	64	-Total sampling time, minutes
Y	=	1.0014	-Dry gas meter calibration factor
Cp	=	0.84	-Pitot tube coefficient, dimensionless
DP avg	=	1.6100	-Average square root of velocity head, sqrt(" H2O)
DH avg	=	1.32	-Average orifice pressure drop, "H2O
Tm avg	=	82	-Average dry gas meter temperature, degrees F
Ps avg	=	0.96	-Average duct static pressure, "H2O
Ts avg	=	855	-Average Stack Temperature, degrees F
Vm tot	=	40.167	-Total meter sample volume, cubic feet
Vi+Vsg	=	100.7	-Total volume of liquid collected
% CO2	=	12.6	-Percent CO2 by volume (dry basis), %
% O2	=	6.4	-Percent O2 by volume (dry basis), %
% CO	=	0.0	-Percent CO by volume (dry basis), %
% N2	=	81.0	-Percent N2 by volume (dry basis), %
Mn	=	6.3	-Total particulate collected, mg

Fuel Input

%H	=		-Percent by weight of hydrogen in fuel
%C	=		-Percent by weight of carbon in fuel
%S	=		-Percent by weight of sulfur in fuel
%N	=		-Percent by weight of nitrogen in fuel
%O	=		-Percent by weight of oxygen in fuel
GCV	=		-Gross calorific value of fuel, BTU/lb
Tstd	=	68	-Standard Temperature, degrees F
Pstd	=	29.92	-Standard Pressure, "Hg
Lp	=		-Final Leak Rate of Sampling Train, cfm

EXAMPLE CALCULATIONS

EPA METHODS 2, 3, 4, AND 5

1. Volume of Sample Measured By Dry Gas Meter, Corrected to Standard Conditions (Vm std)

$$= Vm \text{ total} \times Y \times \frac{(T_{std} + 460)}{Tm \text{ avg} + 460} \times \frac{Pbar + (DH \text{ avg}/13.6)}{Pstd}$$

$$= 40.167 \times 1.001 \times \frac{68 + 460}{82 + 460} \times \frac{30.36 + 1.32/13.6}{29.92}$$

Vm std = 39.89 dscf

2. Moisture Content of Duct Gas (%H2O)

$$= \frac{0.04707 \times (Vi + Vsg)}{Vm \text{ std} + 0.04707 \times (Vi + Vsg)}$$

$$= \frac{0.04707 \times 100.7}{39.8876 + 0.04707 \times 100.7}$$

% H2O = 10.62 % BY VOLUME

parts per - 1000. 10.62% is not a standard unit. P = 1013.25

3. Molecular Weight of Stack Gas (MW)

$$= \{(0.44 \times \%CO_2) + (0.28 \times \%CO) + (0.28 \times \%N_2) + (0.32 \times \%O_2)\} \times \left\{1 - \frac{\%H_2O}{100}\right\} + (0.18) (\%H_2O)$$

$$= \{(0.44 \times 12.6) + (0.28 \times 0) + (0.28 \times 81) + (0.32 \times 6.4)\} \times \left(1 - \frac{10.62}{100}\right) + (0.18 \times 10.62)$$

MW = 28.97 lb/lb-mole

EXAMPLE CALCULATIONS

EPA METHODS 2, 3, 4, AND 5

4. Average Duct Gas Density (Dst)

$$= 0.0458 \times MW \times \left\{ \frac{P_{\text{bar}} + P_{\text{s avg}}/13.6}{T_{\text{s avg}} + 460} \right\}$$

$$= 0.0458 \times MW \times \left\{ \frac{30.36 + 0.96/13.6}{855 + 460} \right\}$$

$$Dst = 0.0307 \text{ lbs / cubic feet}$$

5. Excess Air (EA)

$$= 100 \times \left\{ \frac{\%O_2 - (0.5 \%CO)}{0.264 \times \%N_2 - (\%O_2 - (0.5 \times \%CO))} \right\}$$

$$= 100 \times \left\{ \frac{6.4 - (0.5 \times 0)}{0.264 \times 81 - (6.4 - (0.5 \times 0))} \right\}$$

$$EA = 42.71 \%$$

6. Average Duct Velocity (Vs)

$$= 5129.4 \times C_p \times DP_{\text{avg}} \times \sqrt{\frac{T_{\text{s avg}} + 460}{(P_{\text{bar}} + P_{\text{s avg}}/13.6) \times MW}}$$

$$= 5129.4 \times 0.84 \times 1.61 \times \sqrt{\frac{855 + 460}{(30.36 + 0.96/13.6) \times 28.96}}$$

$$Vs = 8472.6 \text{ ft/min}$$

EXAMPLE CALCULATIONS

EPA METHODS 2, 3, 4, AND 5

7. Duct Volumetric Flow Rate, (Q)

$$= V_s \times A_s$$

$$= 8472.58 \times 0.55$$

$$V_s = 4660 \text{ acfm}$$

8. Duct Volumetric Flow Rate, Corrected to Dry Standard Conditions (Qstd)

$$= Q \times \left(1 - \frac{\% \text{ H}_2\text{O}}{100}\right) \times \left(\frac{T_{\text{std}} + 460}{T_{\text{s avg}} + 460}\right) \times \left(\frac{P_{\text{bar}} + P_{\text{s avg}}/13.6}{P_{\text{std}}}\right)$$

$$= 4659.92 \times \left(1 - \frac{10.62}{100}\right) \times \left(\frac{68 + 460}{T_{\text{s avg}} + 460}\right) \times \left(\frac{30.36 + 0.96/13.6}{29.92}\right)$$

$$Q_{\text{std}} = 1701 \text{ dscfm}$$

9. Isokinetic Factor

$$= \frac{5.67 \times (T_{\text{s avg}} + 460) \times V_{\text{m std}}}{(P_{\text{bar}} + \frac{P_{\text{s avg}}}{13.6}) \times V_s \times T_{\text{tot}} \times \left(1 - \frac{\% \text{H}_2\text{O}}{100}\right) \times \left(\frac{D_n'^2 \times 0.7854}{144}\right)}$$

$$= \frac{5.67 \times (855 + 460) \times 39.88}{(30.36 + \frac{0.96}{13.6}) \times 4659.9 \times 64 \times \left(1 - \frac{10.62}{100}\right) \times \left(\frac{0.035 \times 0.7854}{144}\right)}$$

$$I = 104.6 \%$$

EXAMPLE CALCULATIONS

EPA METHODS 2, 3, 4, AND 5

10. Actual Particulate Concentration, (C)

$$C = \frac{0.01543 \times M_n \times (T_{std} + 460) \times (P_{bar} + P_{s\ avg}/13.6) \times (1 - (\% H_2O / 100))}{V_{m\ std} \times (T_{s\ avg} + 460) \times P_{std}}$$

$$C = \frac{0.01543 \times 6.3 \times (68 + 460) \times (30.36 + 0.96/13.6) \times (1 - (10.62/100))}{39.88 \times (855 + 460) \times 29.92}$$

C = 0.0009 grains/acf

11. Particulate Concentration, Corrected to Dry Standard Conditions, (Cs)

$$C_s = 0.01543 \times \frac{M_n}{V_{m\ std}}$$

$$C_s = 0.01543 \times \frac{6.3}{39.88}$$

Cs = 0.0024 gr/dscf

12. Particulate Emission Rate, (ER)

$$ER = 0.008571 \times C_s \times Q_{std}$$

$$ER = 0.008571 \times 0.002 \times 1700.8$$

ER = 0.036 lbs/hr

EXAMPLE CALCULATIONS

EPA METHODS 2, 3, 4, AND 5

13. F - Factor (F)

$$= \frac{(1 \times 10^6) \times \{(3.64 \times \%H) + (1.53 \times \%C) + (0.57 \times \%S) + (0.14 \times \%N) - (0.46 \times \%O)\}}{GCV}$$

$$= \frac{(1 \times 10^6) \times \{(3.64 \times) + (1.53 \times) + (0.57 \times) + (0.14 \times) - (0.46 \times)\}}{}$$

$$F = \text{ERR dscf/MM BTU}$$

14. Particulate Emission, (E)

$$= 0.0001429 \times Cs \times F \times \left(\frac{20.9}{20.9 - \%O_2} \right)$$

$$= 0.0001429 \times 0.002 \times \text{ERR} \times \left(\frac{20.9}{20.9 - 6.4} \right)$$

$$E = \text{ERR lb/MM BTU}$$

15. Particulate Concentration Corrected to Dry Standard Conditions and 12% CO₂, (Cs @12%CO₂)

$$= Cs \times \frac{12}{\%CO_2}$$

$$= 0.002 \times \frac{12}{12.6}$$

$$Cs @12\%CO_2 = 0.0023 \text{ grains/dscf @ 12\% CO}_2$$

EXAMPLE CALCULATIONS

EPA METHODS 2, 3, 4, AND 5

16. Allowable Leak Rate, (La)

$$= 0.02 \text{ cfm or } 0.04 \times \frac{V_m \text{ tot}}{T \text{ tot}}$$

$$= 0.04 \times \frac{40.16}{64}$$

$$La = 0.02510 \text{ cfm}$$

17. Correction for Excessive Leak Rate, (Vmc total)

if $L_p > La$ use Vmc total in place of Vm total in all subsequent equations.

L_p - Final leak rate of sampling train, cfm

$$= V_m \text{ tot} - (L_p - La) \times T \text{ tot}$$

$$= 40.167 - (0 - 0.0251) \times 64$$

$$V_{mc} \text{ tot} = 41.7736 \text{ cubic feet}$$

PPM CONVERSIONS

CLIENT: ET/OCEANSIDE
LOCATION: OUTLET - 100% LOAD
PROJ. NO: D92-09
DATE: 10/06/92

	RUN NO.	PPM	MW	GM/DSCM	LB/DSCF	OXYGEN	CO2	DSCFM	LB/HR	LIMIT
NOx (as NO2)	M7E-1	191.7	46.00	3.670E-01	2.292E-05	5.8 %	12.6 %	1701	2.34	
	M7E-2	201.0	46.00	3.848E-01	2.403E-05	5.7 %	12.8 %	1709	2.46	
	M7E-3	195.8	46.00	3.748E-01	2.341E-05	5.8 %	12.9 %	1705	2.39	
	AVERAGE	196.2		3.755E-01	2.345E-05	5.8 %	12.8 %	1705	2.40	2.80
CO	M10-1	326.1	28.00	3.800E-01	2.373E-05	5.8 %	12.6 %	1701	2.42	
	M10-2	325.5	28.00	3.793E-01	2.369E-05	5.7 %	12.8 %	1709	2.43	
	M10-3	322.6	28.00	3.759E-01	2.347E-05	5.8 %	12.9 %	1705	2.40	
	AVERAGE	324.7		3.784E-01	2.363E-05	5.8 %	12.8 %	1705	2.42	4.10
TNMHC (as CH4)	M18-1	228.0	16.00	1.518E-01	9.481E-06	5.8 %	12.6 %	1701	0.97	
	M18-2	228.0	16.00	1.518E-01	9.481E-06	5.7 %	12.8 %	1709	0.97	
	M18-3	250.0	16.00	1.665E-01	1.040E-05	5.8 %	12.9 %	1705	1.06	
	AVERAGE	235.3		1.567E-01	9.785E-06	5.8 %	12.8 %	1705	1.00	0.04

PPMCONV

ROJAC Environmental Services, Inc.

PPM CONVERSIONS

CLIENT: ET/OCEANSTIDE
 LOCATION: OUTLET - 75% LOAD
 PROJ. NO: D92-09
 DATE: 10/07/92

	RUN NO.	PPM	MW	GM/DSCM	LB/DSCF	OXYGEN	CO2	DSCFM	LB/HR	LIMIT
NOx (as NO2)	M7E-4	147.1	46.00	2.816E-01	1.759E-05	4.5 %	13.5 %	1509	1.59	
	M7E-5	99.9	46.00	1.912E-01	1.194E-05	4.8 %	13.7 %	1514	1.08	
	M7E-6	107.2	46.00	2.052E-01	1.282E-05	4.7 %	13.9 %	1462	1.12	
	AVERAGE	118.1		2.260E-01	1.411E-05	4.7 %	13.7 %	1495	1.27	2.80
CO	M10-4	353.1	28.00	4.114E-01	2.569E-05	4.5 %	13.5 %	1509	2.33	
	M10-5	338.0	28.00	3.938E-01	2.460E-05	4.8 %	13.7 %	1514	2.23	
	M10-6	338.8	28.00	3.948E-01	2.465E-05	4.7 %	13.9 %	1462	2.16	
	AVERAGE	343.3		4.000E-01	2.498E-05	4.7 %	13.7 %	1495	2.24	4.10
TNMHC (as CH4)	M18-4	126.0	16.00	8.390E-02	5.239E-06	4.5 %	13.5 %	1509	0.47	
	M18-5	60.0	16.00	3.995E-02	2.495E-06	4.8 %	13.7 %	1514	0.23	
	M18-6	30.0	16.00	1.998E-02	1.247E-06	4.7 %	13.9 %	1462	0.11	
	AVERAGE	72.0		4.794E-02	2.994E-06	4.7 %	13.7 %	1495	0.27	0.04

PPMCONV

ROJAC Environmental Services, Inc.

EXAMPLE CALCULATIONS

PPM CONVERSIONS

CLIENT: ET/OCEANSIDE
 LOCATION: OUTLET - 100% LOAD
 PROJ. NO: D92-09
 DATE: 10/06/92

RUN NO.	PPM	MW	GM/DSCM	LB/DSCF	OXYGEN	CO2	DSCFM	LB/HR
OUTLET M10-1	326.1	28.00	3.800E-01	2.373E-05	5.8 %	12.6 %	1701	2.42
$\text{GM/DSCM} = \frac{\text{PPM} \times \text{MW}}{22.414 \text{ L/G-MOLE} \times 10^3 \text{ M}^3/\text{L} \times (293.15\text{K}/273.15\text{K})} \times (1/1\text{E}6 \text{ PPM})$								
			326.1	28.0				
$\text{GM/DSCM} = \frac{326.1 \times 28.0}{24.055\text{E}-3} \times (1/1\text{E}6 \text{ PPM}) = 3.800\text{E}-01 \text{ GM/DSCM}$								
$\text{LB/DSCF} = \frac{\text{PPM} \times \text{MW} \times 2.205\text{E}-3 \text{ LB/G}}{22.414 \text{ L/G-MOLE} \times 3.531\text{E}-2 \text{ CF/L} \times (528.27\text{R}/492.27\text{R})} \times (1/1\text{E}6 \text{ PPM})$								
			326.1	28.0				
$\text{LB/DSCF} = \frac{326.1 \times 28.0 \times 2.205\text{E}-3 \text{ LB/G}}{0.8493} \times (1/1\text{E}6 \text{ PPM}) = 2.373\text{E}-05 \text{ LB/DSCF}$								
$\text{LB/HR} = (\text{LB/DSCF}) \times (\text{DSCFM}) \times 60$								
			1701	60				
$\text{LB/HR} = 2.373\text{E}-05 \times 1701 \times 60 = 2.42 \text{ LB/HR}$								

EXAMPLE CALCULATIONS

PPM CONVERSIONS

CONTINUED

WHERE GM/DSCM = GRAMS PER DRY STANDARD CUBIC METER
LB/DSCF = POUNDS PER DRY STANDARD CUBIC FOOT
PPM = PARTS PER MILLION
MW = MOLECULAR WEIGHT IN GRAMS PER GRAM-MOLE (CO = 28.0)
LB/G = POUNDS PER GRAM
L/G-MOLE = LITERS PER GRAM-MOLE
CF/L = CUBIC FEET PER LITER
OK = DEGREES KELVIN
OR = DEGREES RANKINE
LB/HR = POUNDS PER HOUR

EXCALCNV

EQUATION 6C-1 - POLLUTANT CONCENTRATION

CLIENT: ET/OCEANSIDE
 LOCATION: STACK - NOx - 100% LOAD
 PROJ. NO: D92-09
 DATE: 10/06/92

RUN NUMBER	ANALYZER AVERAGE	ZERO RESPONSE		UPSCALE RESPONSE		AVERAGE ZERO	AVERAGE SPAN	SPAN GAS VALUE	EMISSION CONCENTRATION
		INITIAL	FINAL	INITIAL	FINAL				
M7E-1	190.2	0.9	1.3	240.1	239.5	1.1	239.8	242.0	191.7
M7E-2	202.7	1.3	3.1	239.5	247.6	2.2	243.6	242.0	201.0
M7E-3	198.2	3.1	4.6	247.6	240.5	3.9	244.1	242.0	195.8
AVERAGE	197.0	1.8	3.0	242.4	242.5	2.4	242.5	242.0	196.2

CLIENT: ET/OCEANSIDE
 LOCATION: STACK - NOx - 75% LOAD
 PROJ. NO: D92-09
 DATE: 10/07/92

RUN NUMBER	ANALYZER AVERAGE	ZERO RESPONSE		UPSCALE RESPONSE		AVERAGE ZERO	AVERAGE SPAN	SPAN GAS VALUE	EMISSION CONCENTRATION
		INITIAL	FINAL	INITIAL	FINAL				
M7E-4	149.4	0.4	4.3	242.9	245.6	2.4	244.3	242.0	147.1
M7E-5	103.4	4.3	1.0	245.6	247.7	2.7	246.7	242.0	99.9
M7E-6	110.3	1.0	1.9	247.7	246.6	1.5	247.2	242.0	107.2
AVERAGE	121.0	1.9	2.4	245.4	246.6	2.2	246.0	242.0	118.1

EQUATION 6C-1 - POLLUTANT CONCENTRATION

CLIENT: ET/OCEANSIDE

LOCATION: STACK - 02 - 100% LOAD

PROJ. NO: D92-09

DATE: 10/06/92

RUN NUMBER	ANALYZER AVERAGE	ZERO RESPONSE		UPSCALE RESPONSE		AVERAGE ZERO	AVERAGE SPAN	SPAN GAS VALUE	EMISSION CONCENTRATION
		INITIAL	FINAL	INITIAL	FINAL				
M3A-1	5.9	0.0	0.1	16.2	16.3	0.1	16.3	16.1	5.8
M3A-2	5.8	0.1	0.1	16.3	16.3	0.1	16.3	16.1	5.7
M3A-3	5.9	0.1	0.0	16.3	16.2	0.1	16.3	16.1	5.8
AVERAGE	5.9	0.1	0.1	16.3	16.3	0.1	16.3	16.1	5.8

CLIENT: ET/OCEANSIDE

LOCATION: STACK - 02 - 75% LOAD

PROJ. NO: D92-09

DATE: 10/07/92

RUN NUMBER	ANALYZER AVERAGE	ZERO RESPONSE		UPSCALE RESPONSE		AVERAGE ZERO	AVERAGE SPAN	SPAN GAS VALUE	EMISSION CONCENTRATION
		INITIAL	FINAL	INITIAL	FINAL				
M3A-4	4.5	0.0	0.0	16.1	16.1	0.0	16.1	16.1	4.5
M3A-5	4.7	0.0	-0.1	16.1	16.0	-0.1	16.1	16.1	4.8
M3A-6	4.6	-0.1	-0.1	16.0	15.9	-0.1	16.0	16.1	4.7
AVERAGE	4.6	0.0	-0.1	16.1	16.0	-0.1	16.0	16.1	4.7

EQUATION 6C-1 - POLLUTANT CONCENTRATION

CLIENT: ET/OCEANSIDE
 LOCATION: STACK - CO - 100% LOAD
 PROJ. NO: D92-09
 DATE: 10/06/92

RUN NUMBER	ANALYZER AVERAGE	ZERO RESPONSE INITIAL	ZERO RESPONSE FINAL	UPSCALE RESPONSE INITIAL	UPSCALE RESPONSE FINAL	AVERAGE ZERO	AVERAGE SPAN	SPAN GAS VALUE	EMISSION CONCENTRATION	PERCENT CO2	CO CORRECTED TO EQ10-1
M10-1	378.0	3.6	4.4	495.5	488.8	4.0	492.2	487.0	373.1	12.6	326.1
M10-2	375.5	4.4	1.5	488.8	489.3	3.0	489.1	487.0	373.2	12.8	325.5
M10-3	373.1	1.5	1.1	489.3	490.9	1.3	490.1	487.0	370.4	12.9	322.6
AVERAGE	375.5	3.2	2.3	491.2	489.7	2.8	490.4	487.0	372.3	12.8	324.7

CLIENT: ET/OCEANSIDE
 LOCATION: STACK - CO - 75% LOAD
 PROJ. NO: D92-09
 DATE: 10/07/92

RUN NUMBER	ANALYZER AVERAGE	ZERO RESPONSE INITIAL	ZERO RESPONSE FINAL	UPSCALE RESPONSE INITIAL	UPSCALE RESPONSE FINAL	AVERAGE ZERO	AVERAGE SPAN	SPAN GAS VALUE	EMISSION CONCENTRATION	PERCENT CO2	CO CORRECTED TO EQ10-1
M10-4	414.2	2.2	-0.2	494.4	493.5	1.0	494.0	487.0	408.2	13.5	353.1
M10-5	397.8	-0.2	0.3	493.5	495.8	0.1	494.7	487.0	391.6	13.7	338.0
M10-6	400.7	0.3	1.0	495.8	495.7	0.7	495.8	487.0	393.5	13.9	338.8
AVERAGE	404.2	0.8	0.4	494.6	495.0	0.6	494.8	487.0	397.8	13.7	343.3

EQ6C1C0

ROJAC Environmental Services, Inc.

EXAMPLE CALCULATIONS

EQUATIONS 6C-1 AND 10-1 - EMISSIONS CONCENTRATIONS

CLIENT: ET/OCEANSIDE
 LOCATION: STACK-CO - 100% LOAD
 PROJ. NO: D92-09
 DATE: 10/06/92

RUN NUMBER	ANALYZER AVERAGE	ZERO RESPONSE INITIAL	ZERO RESPONSE FINAL	SPAN RESPONSE INITIAL	SPAN RESPONSE FINAL	AVERAGE ZERO	AVERAGE SPAN	SPAN GAS VALUE	EMISSION CONCENTRATION	PERCENT CO2	CO CORRECTED TO EQ 10-1
M10-1	378.0	3.6	4.4	495.5	488.8	4.0	492.2	487.0	373.1 ppm	12.6	326.1 ppm

$$\text{EQUATION 6C-1: } C_{\text{gas}} = \frac{(C - C_0) \times (C_{\text{ma}})}{(C_{\text{m}} - C_0)} \quad \text{WHERE}$$

$\bar{C}$ = ANALYZER RUN AVERAGE
 C_0 = AVERAGE ZERO RESPONSE
 C_{m} = AVERAGE SPAN RESPONSE
 C_{ma} = UPSCALE SPAN GAS CONCENTRATION
 C_{gas} = EMISSION CONCENTRATION

$$C_{\text{gas}} = (378.0 - 4.0) \times \frac{(487.0)}{(492.2 - 4.0)} = 373.1 \text{ ppm}$$

$$\text{EQUATION 10-1} = \text{ppm} \times (1 - (\%CO_2/100)) = 373.1 \text{ ppm} \times (1 - (12.6 / 100)) = 326.1 \text{ ppm}$$

APPENDIX B

Field Data Sheets

EPA METHOD 2
VELOCITY TRAVERSE AND FLOWRATE DETERMINATION

PLANT Energy Turtics
 DATE 10-6-92
 LOCATION Engine outlet 100' level
 STACK DIMENSIONS 10" AREA ft²
 BAROMETRIC PRESSURE, P_b = 30.36 in. Hg
 STATIC PRESSURE, P_s = ± in. H₂O
 STACK GAS MOLECULAR WEIGHT (W_g), M = 28
 STACK GAS MOISTURE CONTENT, % H₂O = 5
 PITOT NO. C_p = .84
 TESTER

Page Of

SCHEMATIC OF TRAVERSE POINT LOCATION

+ 0 Clockwise

Cyclonic Flow Angle - 0 Clockwise

PORT	POINT	DELTA P Inch H ₂ O	√(DELTA P) Inch H ₂ O	T _s (°F)	Cyclonic Flow Angle	Other	Other
1	1	2.58		840	10		
	2	2.59		864	11		
	3	2.43		855	9		
	4	2.30		850	14		
2	1	2.80		865	6		
	2	2.80		863	4		
	3	2.50		861	11		
	4	2.50		862	9		
AVERAGE				T _s = °F			

* Avg. of absolute values
including zeroes

Absolute Gas Temperature = T_s + 460°R

Absolute Gas Pressure, P_g = P_b + P_s/13.6 =

Gas Velocity, V_s = (85.49) (C_p) √(DELTA P_{avg}) √(T_s + 460) / √(P_g * M_g) = ft/sec

Actual Gas Flowrate, Q_a = (V_s) (60) (A) = ACFM

Standard Gas Flowrate, Q_{std} = (Q_a) * (528°R / T_s) * (P_g / 29.92) * (100 - %H₂O) / 100 = DSCFM

EPA METHOD 2

Page__ Of__

SCHEMATIC OF TRAVERSE POINT LOCATION

• 0 Clockwise

Cyclonic Flow Angle - 0 Clockwise

AVERAGE

ft_s

 $\odot_F$

1

- * Avg. of absolute values including zeroes

Absolute Gas Temperature = $T_s + 460^\circ R$

Absolute Gas Pressure, $P_g = P_b + P_s/13.6 =$ _____

$$\text{Gas Velocity, } V_g = (85.49) (C_p) \sqrt{(\Delta P_{avg}) \frac{T_s + 460}{P_g M_g}} = \text{ft/sec}$$

Actual Gas Flowrate, $Q_g = (V_g) (60) (A) = \underline{\hspace{2cm}} \text{ ACFM}$

$$\text{Standard Gas Flowrate, } Q_{\text{std}} = (Q_g) \cdot \left(\frac{5280 \text{ R}}{T_s} \right) \cdot \left(\frac{P_g}{29.92} \right) \cdot \left(\frac{100 - \% \text{H}_2\text{O}}{100} \right) = \text{_____ DSCFM}$$

EPA METHODS FIELD DATA SHEET

RUN NO. MS-1
 PROJ. NO. 072-09
 DATE 10-6-92
 FIRM NAME Energy Tactics
 PLANT LOC. Ocean Side, NY
 TESTER JSG/JJO

MODULE NO. 2827
 DGM, Y 1.0014
 MOD. H@ 1.79
 PROBE I.D. 401
 PITOT (Cp) .84
 NOZ. DIA. .188
 FILTER I.D. ROBT 146
 TARE WT. _____

PITOT LEAK CHECK
 INITIAL 0.00 C 5"
 FINAL _____
 TRAIN LEAK CHECK
 INITIAL 0.010 C 8" 145
 FINAL 0.008 C 6" 145

STACK COND.
 STATIC PRES. .96
 DUCT DIM. 10"
 DUCT AREA 155
 %H₂O 5
 AMBIENT COND.
 AMB. TEMP 45
 BAR. PRES. 30.36

FULL LOW

TRAV. PT	SAMPLE TIME (min)	CLOCK TIME (hours)	VEL. (ft/s)	ORIFICE H	DGM Tm In °F	DGM Tm In °F	STACK TEMP. T _{st} °F	GAS SAMPLE VOLUME V _m CUBIC FEET	COND. OUTLET °F	HEATER BOX °F	PROBE TEMP. °F	FILTER OUTLET °F	PUMP VAC. In. Hg.	OTHER
1	8 min	1015	2.45	1.34	75	75	816	226.020	465	250	250	N/A	3	
2		31	2.77	1.37	85	77	862	232.4		260	255		3	
3		39	2.55	1.28	89	78	867	236.7		255	254		3	
4		47	2.73	1.38	87	79	866	241.6		271	255		3	
1		1101	2.80	1.41	81	79	858	251.8		266	255		3	
2		09	2.73	1.40	89	79	851	256.9		258	254		3	
3		17	2.40	1.21	91	81	866	262.0		265	255		3	
4		25	2.40	1.22	89	81	853	266.787		262	260		3	
AVERAGE				1.32		82	855	TOTAL 40.167						
			1.61											

REMARKS

ORSAT BAG ANALYSIS

AVERAGE

157 88

PRE IMPINGERS TARE _____
 POST IMPINGERS TARE _____
 TOTAL IMP'S CONTENTS 88

PRE S.G. TARE _____
 POST S.G. TARE 12.7
 TOTAL S.G. CONTENTS 100.7

	1	2	3	AVERAGE
CO ₂	12.6	12.6	12.6	12.6
O ₂	6.4	6.4	6.4	6.4
CO	0	0	0	0
N ₂	81.0	81.0	81.0	81.0

EPA METHODS FIELD DATA SHEET

RUN NO. MS-2
 PROJ. NO. 092-09
 DATE 10-6-92
 FIRM NAME Energy Tactics
 PLANT LOC. Ocean Side, NJ
 TESTER JSK/JN

MODULE NO.	2827
DGM, Y	1.0014
MOD. #H@	1.79
PROBE I.D.	401
PITOT (Dp)	.84
NOZ. DIA.	.188
FILTER I.D.	ROAT 147
TARE WT.	

PITOT LEAK CHECK

INITIAL	<u>0.00 e 5"</u>
FINAL	<u> </u>

TRAIN LEAK CHECK

INITIAL	<u>0.002 e 6" 145</u>
FINAL	<u>0.009 e 6" 145</u>

STACK COND.	
STATIC PRES.	.97
DUCT DIM.	16"
DUCT AREA	.55
%H2O	10
AMBIENT COND.	
AMB. TEMP	60s
BAR. PRES.	30.36

Full Load

[illegible]

PRIE IMPINGERS TARE	
POST IMPINGERS TARE	
TOTAL IMP'S CONTENTS	130

PRIE S.G. TARE	
POST S.G. TARE	100
TOTAL S.G. CONTENTS	130

REMARKS

ORSAT BAG ANALYSIS

152 120

	1	2	3	AVERAGE
CO ₂	12.8	15.8	12.8	12.8
O ₂	6.0	6.0	6.0	6.0
CO	0	0	0	0
N ₂	81.2	81.2	81.2	81.2

EPA METHODS FIELD DATA SHEET

RUN NO. M5-3
 PROJ. NO. 092-09
 DATE 10-6-92
 FIRM NAME Energy Techs
 PLANT LOC. Accon Sdc, NY
 TESTER JSG/LJO

MODULE NO. 2027
 DGM, Y 1.0014
 MOD. @H@ 1.37
 PROBE I.D. 401
 PITOT (Cp) .84
 NOZ. DIA. .188
 FILTER I.D. EQMT 148
 TARE WT. _____

PITOT LEAK CHECK

INITIAL _____
 FINAL 5.00 e 4" Hg

TRAIN LEAK CHECK

INITIAL _____
 FINAL 0.010 e 5" Hg
0.006 e 6" Hg

STACK COND.

STATIC PRES. + 1.0
 DUCT DIM. 10"
 DUCT AREA .53
 %H₂O 15

AMBIENT COND.

AMB. TEMP 60.5
 BAR. PRES. 20.36

FULL LOAD

TRAV. PT	SAMPLE TIME (min)	CLOCK TIME (hours)	VEL. (MP)	ORIFICE H	DGM Tm In °F	DGM Tm In °F	STACK TEMP. T _s °F	GAS SAMPLE VOLUME Vm CUBIC FEET	COND. OUTLET °F	HEATER BOX °F	PROBE TEMP. °F	FILTER OUTLET °F	PUMP VAC. in. Hg.	OTHER
1	8.1414	1353	2.50	1.07	80	80	859	308.350	165	250	249	165	2	
2		09	2.95	1.27	90	90	857	312.9		262	252		2	
3		17	2.45	1.07	83	83	847	317.8		265	254		3	
4		25	2.50	1.09	83	83	850	322.7		261	253		3	
1		38	2.80	1.21	87	87	849	327.0		259	254		3	
2		46	3.00	1.30	85	85	855	332.1		255	252		3	
3		54	2.90	1.26	87	87	857	337.2		253	253		3	
4		1502	2.65	1.15	87	87	856	342.3		255	253		3	
								347.11						
AVERAGE			1.6477	1.18	88	88	854	TOTAL 387.61						

REMARKS

110

ORSAT BAG ANALYSIS

	1	2	3	AVERAGE
CO ₂	13.0	12.7	13.0	12.9
O ₂	6.0	6.2	6.0	6.0
CO	0	0	0	0
N ₂	81.0	81.1	81.0	81.0

PRE IMPINGERS TARE

POST IMPINGERS TARE

TOTAL IMP'S CONTENTS 110

PRE S.G. TARE

POST S.G. TARE 9.3

TOTAL S.G. CONTENTS 119.3

EPA METHODS FIELD DATA SHEET

RUN NO. MS-4
PROJ. NO. 092-09
DATE 10-7-92
FIRM NAME Energy Tactics
PLANT LOC. Alcan, NY
TESTER JSC/TD

75% LOAD

MODULE NO.	2827
DGM. Y	10014
MOD. ^H@	1.79
PROBE I.D.	401
PITOT (Cp)	184
NOZ. DIA.	1250
FILTER I.D.	EQWT 103
TARE WT.	

PITOT LEAK CHECK

INITIAL o e 4.5"

FINAL

TRAIN LEAK CHECK

INITIAL	0.010 e	0.6" Hg
FINAL	0.006 e	7" "

STACK COND.	
STATIC PRES.	.90
DUCT DIM.	10"
DUCT AREA	.53
%H ₂ O	14
AMBIENT COND.	
AMB. TEMP.	50
BAR. PRES.	30.30

[illegible]

PRE IMPINGERS TARE

POST IMPINGERS TARE

TOTAL IMP'S CONTENTS

PRE S.G. TARE

POST S.G. TARE

TOTAL S.G. CONTENTS

REMARKS

271 151

OHSA T BAG ANALYSIS

AVERAGE

	1	2	3	AVERAGE
CO ₂	13.7	13.6	13.6	13.5
O ₂	5.0	5.2	5.0	5.1
CO	0	0	0	0
N ₂	8.6	8.7	8.4	8.6

FIELD DATA SHEET

FIRM NAME Energy Tactics
 PLANT LOCATION Outside NY
 RUN NUMBER M5-5
 SAMPLING LOCATION Outlet
 PROJECT NUMBER 092-09
 DATE 10-7-72
 TESTER JSG/JJD

MODULE NO. 2837
 STACK PRESSURE (in. H₂O) 92
 BAR. PRESSURE 30.30
 PROBE ID NO. 401
 FILTER ID NO. R047175
 FILTER TARE WT. 250
 NOZZLE NO./DIA. (in.) 250
 DUCT AREA (ft²) 1.55

ASSUMED MOISTURE (%) 14
 TEST DURATION 64
 TRAVERSE POINT INTERVAL 0.4min
 PROBE HEATER SETTING 250
 FILTER HEATING SETTING 250
 LEAK CHECK: INITIAL 0.00 @ 0.8"
 FINAL 0.007 @ 0.8"

DRY GAS METER Y 1.004
 PITOT COEFFICIENT .84
 MONOGRAPH C FACTOR .88
 MODULE ΔH_A 1.77
 TEST START TIME 1112
 TEST FINAL TIME 1221
 AMBIENT TEMP. 60's

TRAVERSE POINT	SAMPLE TIME (min)	CLOCK TIME (hours)	VELOCITY HEAD (ΔP) (in. H ₂ O)	ORIFICE ΔH	DGM Tm in of	DGM Tm out of	STACK TEMP. T _s of	GAS SAMPLE VOLUME Vm CUBIC FEET	FILTER OUTLET of	CONDENSOR OUTLET of	HEATER BOX of	PROBE TEMP. F	PUMP VAC. in. Hg
1	8min	1112	2.30	3.03	80	78	882	405.300	N/A	261	254	255	6
2		20	2.40	3.14	95	83	914	412.7			255	252	6
3		36	2.00	2.66	101	84	900	419.8			258	268	5
4		44	2.00	2.66	100	86	901	433.6			262	269	5
1		57	2.40	3.24	93	88	876	441.3			266	276	6
2		1205	2.50	3.34	101	89	901	449.0			262	271	6
3		13	2.20	2.92	103	87	911	456.5			262	272	5
4		21	2.25	2.98	102	88	913	463.666			264	268	5
AVERAGE			$\sum \sqrt{\Delta P}$	3.00	911	900	900	TOTAL					
			1.5010					58.366					

ORSAT BAG ANALYSIS

TRIPPLICATE ANALYSIS

CO₂ O₂ CO N₂

13.8	4.8	0	81.4
13.8	5	0	81.3
13.6	5	0	81.4

H₂O COLLECTED 173 ml.
 S. G. WEIGHT 161 gr.
 TOTAL VOLUME 189.1 ml.
 COLLECTED

10-173 COMMENTS

75% CO₂

FIELD DATA SHEET

FIRM NAME Energy Tactics
 PLANT LOCATION Exxon, NY
 RUN NUMBER MS-6
 SAMPLING LOCATION Outlet

MODULE NO. 2827
 STACK PRESSURE (in. H₂O) .90
 BAR. PRESSURE 30.30
 PROBE ID NO. 401
 FILTER ID NO. RQWT 149
 FILTER TARE WT. 250
 NOZZLE NO./DIA. (in.) 250
 DUCT AREA (ft²) .55

DRY GAS METER Y 1.0014
 PITOT COEFFICIENT 1.87
 MONOGRAPH C FACTOR 1.88
 MODULE ΔH 1.77
 TEST START TIME 1258
 TEST FINAL TIME 1406
 AMBIENT TEMP. 60.3

ASSUMED MOISTURE (X) 17
 TEST DURATION 64
 TRAVERSE POINT INTERVAL 8 min
 PROBE HEATER SETTING 250
 FILTER HEATING SETTING 250
 LEAK CHECK: 0.007 @ 0.75"
 INITIAL 0.001 @ 0.75"
 FINAL 0.001 @ 0.75"

TRAVERSE POINT	SAMPLE TIME (min)	CLOCK TIME (hours)	VELOCITY HEAD (ΔP) (in. H ₂ O)	ORIFICE ΔH	DGM Tm in °F	DGM Tm out °F	STACK TEMP. T ₈ °F	GAS SAMPLE VOLUME Vm CUBIC FEET	FILTER OUTLET °F	CONDENSOR OUTLET °F	HEATER BOX °F	PROBE TEMP. °F	PUMP VAC. in. Hg
1	8 min	1258	2.20	3.86	78	77	883	465.050	N/A	465	253	255	6
2		1306	2.20	3.91	95	81	882	472.2			255	253	6
3		22	1.90	2.48	100	61	907	479.9			251	261	5
4		30	2.00	2.62	101	84	907	486.5			253	266	5
1		42	2.25	3.02	94	86	870	493.4			264	271	6
2		50	2.30	3.07	101	87	880	500.9			261	272	6
3		58	2.00	2.63	100	87	908	508.3			260	260	5
4		1406	2.05	2.69	100	86	909	514.9			259	257	5
								521.900					
AVERAGE			$\sum \sqrt{\Delta P}$	2.79	90	894	TOTAL	56.850					
			1.4527										

ORSAT BAG ANALYSIS

TRIPPLICATE ANALYSIS

CO₂ O₂ CO N₂

13.8	4.8	0	81.4
14	5	0	81.0
14	5	0	81.0

H₂O COLLECTED 177 ml.
 S. G. WEIGHT 151 gr.
 TOTAL VOLUME 1001 ml.
 COLLECTED

177 COMMENTS

75% LOAD

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: Oceanside Landfill/ET - 29 # 007 100% load
DATE: 10/6/92
RUN NO: Linearity + #1 (1015 - 1141)
GAS CONSTITUENT: NO_x
ATTENUATION (SPAN): 0 - 500 ppm

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE		HIGH RANGE
CAL GAS CONCENTRATION:	0.0	97.5	242.0	480.0
ANALYZER CAL RESPONSE:	0.8	99.3	245.2	486.4
ABSOLUTE DIFFERENCE:	0.8	1.8	3.2	6.4
CALIBRATION ERROR (<%):	0.2%	0.4%	0.6%	1.3%

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL	
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)
ZERO:	0.8	0.9	0.0%	1.3	0.1%
UPSCALE:	245.2	240.1	1.0%	239.5	1.1%

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0}$$

$$\begin{aligned} \bar{C} &= \underline{190.2} && \text{(RUN AVERAGE)} \\ C_0 &= \underline{1.1} && \text{(AVERAGE ZERO)} \\ C_{\text{m}} &= \underline{239.8} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{242.0} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{191.7} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: Duanside Landfill / ET-29 #007 75% load
DATE: 10/7/92
RUN NO: Linearity + #4 (0935-1035)
GAS CONSTITUENT: NO_x
ATTENUATION (SPAN): 0-500 ppm

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE		HIGH RANGE
CAL GAS CONCENTRATION:	0.0	97.5	242.0	480.0
ANALYZER CAL RESPONSE:	0.7	98.3	247.0	481.5
ABSOLUTE DIFFERENCE:	0.7	0.8	5.0	1.5
CALIBRATION ERROR (<%) :	0.1%	0.2%	1.0%	0.3%

SYSTEM CAL BIAS & DRIFT:

		PRE CAL		POST CAL	
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)
ZERO:	0.7	0.4	0.1%	4.3	0.7%
UPSCALE:	247.0	242.9	0.8%	245.6	0.3%

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0},$$

$$\begin{aligned} \bar{C} &= \underline{149.4} && \text{(RUN AVERAGE)} \\ C_0 &= \underline{2.4} && \text{(AVERAGE ZERO)} \\ C_{\text{m}} &= \underline{244.3} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{242.0} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{147.1} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: Oceanside Landfill/ET-29 #007 75% load
 DATE: 10/7/92
 RUN NO: #5 (1115-1215)
 GAS CONSTITUENT: NO_x
 ATTENUATION (SPAN): 0-500 ppm

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:			
ANALYZER CAL RESPONSE:			
ABSOLUTE DIFFERENCE:			
CALIBRATION ERROR (<2%):			

SYSTEM CAL BIAS & DRIFT:

		PRE CAL		POST CAL	
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)
ZERO:	<u>0.7</u>	<u>4.3</u>	<u>0.7%</u>	<u>1.0</u>	<u>0.1%</u>
UPSCALE:	<u>247.0</u>	<u>245.6</u>	<u>0.3%</u>	<u>247.7</u>	<u>0.1%</u>

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_m - C_0}$$

$$\begin{aligned} \bar{C} &= \underline{103.4} && \text{(RUN AVERAGE)} \\ C_0 &= \underline{2.7} && \text{(AVERAGE ZERO)} \\ C_m &= \underline{246.7} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{242.0} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{99.9} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: Oceanside Landfill / ET-29 #007 75% load
DATE: 10/7/92
RUN NO: #6 (1250-1350)
GAS CONSTITUENT: NO_x
ATTENUATION (SPAN): 0-500 ppm

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:			
ANALYZER CAL RESPONSE:			
ABSOLUTE DIFFERENCE:			
CALIBRATION ERROR (<2%):			

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL		
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	DRIFT (<3%)
ZERO:	0.7	1.0	0.1%	1.9	0.2%	0.2%
UPSCALE:	247.0	247.7	0.3%	246.6	0.1%	0.2%

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_o) \times \frac{C_{\text{ma}}}{C_m - C_o}$$

$$\begin{aligned} \bar{C} &= \frac{110.3}{\quad} && \text{(RUN AVERAGE)} \\ C_o &= \frac{1.5}{\quad} && \text{(AVERAGE ZERO)} \\ C_m &= \frac{247.2}{\quad} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \frac{242.0}{\quad} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \frac{107.2}{\quad} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: Oceanside Landfill/ET-29 #007 100% load
DATE: 10/6/92
RUN NO: Linearity + #1 (1015-1141)
GAS CONSTITUENT: CO
ATTENUATION (SPAN): 0 - 500 ppm

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE		HIGH RANGE
CAL GAS CONCENTRATION:	0.0	141.0	284.0	487.0
ANALYZER CAL RESPONSE:	0.4	144.6	278.2	490.4
ABSOLUTE DIFFERENCE:	0.4	3.6	5.8	3.4
CALIBRATION ERROR (<2%):	0.1%	0.7%	1.2%	0.7%

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL	
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)
ZERO:	0.4	3.6	0.7%	4.4	0.8%
UPSCALE:	490.4	495.5	1.0%	488.8	0.3%

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_o) \times \frac{C_{\text{ma}}}{C_m - C_o}$$

$$\begin{aligned} \bar{C} &= \underline{378.0} && \text{(RUN AVERAGE)} \\ C_o &= \underline{4.0} && \text{(AVERAGE ZERO)} \\ C_m &= \underline{492.2} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{487.0} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{373.1} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: Oceanside Landfill / ET-29 # 007 100% load
DATE: 10/6/92
RUN NO: #2 (1212 - 1312)
GAS CONSTITUENT: CO
ATTENUATION (SPAN): 0 - 500 ppm

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:			
ANALYZER CAL RESPONSE:			
ABSOLUTE DIFFERENCE:			
CALIBRATION ERROR (<2%):			

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL		
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	DRIFT (<3%)
ZERO:	0.4	4.4	0.8%	1.5	0.2%	0.6%
UPSCALE:	490.4	488.8	0.3%	489.3	0.2%	0.1%

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0}$$

$$\begin{aligned} \bar{C} &= \underline{375.5} && \text{(RUN AVERAGE)} \\ C_0 &= \underline{3.0} && \text{(AVERAGE ZERO)} \\ C_{\text{m}} &= \underline{489.1} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{487.0} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{\frac{372.5}{373.2}} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: *Oceanside Landfill/ET-29 #007* *100% load*
 DATE: *10/6/92*
 RUN NO: *#3*
 GAS CONSTITUENT: *CO (1400 - 1500)*
 ATTENUATION (SPAN): *0 - 500 ppm*

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:			
ANALYZER CAL RESPONSE:			
ABSOLUTE DIFFERENCE:			
CALIBRATION ERROR (<2%):			

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL		
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	DRIFT (<3%)
ZERO:	<i>0.4</i>	<i>1.5</i>	<i>0.2%</i>	<i>1.1</i>	<i>0.1%</i>	<i>0.1%</i>
UPSCALE:	<i>490.4</i>	<i>489.3</i>	<i>0.2%</i>	<i>490.9</i>	<i>0.1%</i>	<i>0.3%</i>

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0}$$

$$\begin{aligned} \bar{C} &= \underline{373.1} && \text{(RUN AVERAGE)} \\ C_0 &= \underline{1.3} && \text{(AVERAGE ZERO)} \\ C_{\text{m}} &= \underline{490.1} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{487.0} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{370.4} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: Oceanside Landfill/ET-29 #007 75% load
DATE: 10/7/92
RUN NO: Linearity + #4 (0935-1035)
GAS CONSTITUENT: CO
ATTENUATION (SPAN): 0-500 ppm

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE		HIGH RANGE
CAL GAS CONCENTRATION:	0.0	141.0	284.0	487.0
ANALYZER CAL RESPONSE:	1.2	147.4	281.1	490.4
ABSOLUTE DIFFERENCE:	1.2	6.4	2.9	3.4
CALIBRATION ERROR (<2%):	0.2%	1.3%	0.6%	0.7%

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL		
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	DRIFT (<3%)
ZERO:	1.2	2.2	0.2%	-0.2	0.3%	0.5%
UPSCALE:	490.4	494.4	0.8%	493.5	0.6%	0.2%

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0},$$

$$\begin{aligned} \bar{C} &= \underline{414.2} && \text{(RUN AVERAGE)} \\ C_0 &= \underline{1.0} && \text{(AVERAGE ZERO)} \\ C_{\text{m}} &= \underline{494.0} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{487.0} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{408.2} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: Oceanside Landfill/ET-29 #007 75% load
DATE: 10/7/92
RUN NO: #5 (1115-1215)
GAS CONSTITUENT: CO
ATTENUATION (SPAN): 0-500 ppm

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:			
ANALYZER CAL RESPONSE:			
ABSOLUTE DIFFERENCE:			
CALIBRATION ERROR (<2%):			

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL		
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	DRIFT (<3%)
ZERO:	1.2	-0.2	0.3%	0.3	0.2%	0.1%
UPSCALE:	490.4	493.5	0.6%	495.8	1.1%	0.5%

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_o) \times \frac{C_{\text{ma}}}{C_m - C_o}$$

$$\begin{aligned} \bar{C} &= \underline{397.8} && \text{(RUN AVERAGE)} \\ C_o &= \underline{0.1} && \text{(AVERAGE ZERO)} \\ C_m &= \underline{494.7} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{487.0} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{391.6} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: *Oceanside Landfill/ET-29 #007 75% load*
 DATE: *10/7/92*
 RUN NO: *#6 (1250-1350)*
 GAS CONSTITUENT: *CO*
 ATTENUATION (SPAN): *0-500 ppm*

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:			
ANALYZER CAL RESPONSE:			
ABSOLUTE DIFFERENCE:			
CALIBRATION ERROR (<2%):			

SYSTEM CAL BIAS & DRIFT:

		PRE CAL		POST CAL	
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)
ZERO:	<i>1.2</i>	<i>0.3</i>	<i>0.2%</i>	<i>1.0</i>	<i>0.0%</i>
UPSCALE:	<i>490.4</i>	<i>495.8</i>	<i>1.1%</i>	<i>495.7</i>	<i>1.1%</i>

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_o) \times \frac{C_{\text{ma}}}{C_m - C_o}$$

$$\begin{aligned} \bar{C} &= \underline{400.7} && \text{(RUN AVERAGE)} \\ C_o &= \underline{0.7} && \text{(AVERAGE ZERO)} \\ C_m &= \underline{495.8} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{487.0} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{393.5} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: Seaside Landfill/ET-29 #007 100% load
DATE: 10/6/92
RUN NO: Linearity + #1 (1015-1141)
GAS CONSTITUENT: O_2
ATTENUATION (SPAN): 0-25%

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:	0.0%	16.1%	20.9%
ANALYZER CAL RESPONSE:	0.0%	16.3%	21.0%
ABSOLUTE DIFFERENCE:	0.0%	0.2%	0.1%
CALIBRATION ERROR (<2%):	0.0%	0.8%	0.4%

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL	
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)
ZERO:	0.0%	0.0%	0.0%	0.1%	0.4%
UPSCALE:	16.3%	16.2%	0.4%	16.3%	0.0%

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_m - C_0}$$

$$\begin{aligned} \bar{C} &= \underline{5.9} && \text{(RUN AVERAGE)} \\ C_0 &= \underline{0.1} && \text{(AVERAGE ZERO)} \\ C_m &= \underline{16.3} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{16.1} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{5.8} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: *Oceanside Landfill/ET-29 #007 100% load*
DATE: *10/6/92*
RUN NO: *#2 (1212 - 1312)*
GAS CONSTITUENT: *O₂*
ATTENUATION (SPAN): *0-25%*

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:			
ANALYZER CAL RESPONSE:			
ABSOLUTE DIFFERENCE:			
CALIBRATION ERROR (<2%):			

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL		
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	DRIFT (<3%)
ZERO:	<i>0.0%</i>	<i>0.1%</i>	<i>0.4%</i>	<i>0.1%</i>	<i>0.4%</i>	<i>0.0%</i>
UPSCALE:	<i>16.3%</i>	<i>16.3%</i>	<i>0.0%</i>	<i>16.3%</i>	<i>0.0%</i>	<i>0.0%</i>

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0}$$

$$\begin{aligned} \bar{C} &= \underline{5.8} && \text{(RUN AVERAGE)} \\ C_0 &= \underline{0.1} && \text{(AVERAGE ZERO)} \\ C_{\text{m}} &= \underline{16.3} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{16.1} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{5.7} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: *Oceanside Landfill / ET-29 #007 100% load*
DATE: *10/6/92*
RUN NO: *#3 (1400-1500)*
GAS CONSTITUENT: *O₂*
ATTENUATION (SPAN): *0-25%*

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:			
ANALYZER CAL RESPONSE:			
ABSOLUTE DIFFERENCE:			
CALIBRATION ERROR (<2%):			

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL	
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)
ZERO:	<i>0.0%</i>	<i>0.1%</i>	<i>0.4%</i>	<i>0.0%</i>	<i>0.0%</i>
UPSCALE:	<i>16.3%</i>	<i>16.3%</i>	<i>0.0%</i>	<i>16.2%</i>	<i>0.4%</i>

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0}$$

$$\begin{aligned} \bar{C} &= \underline{5.9} && \text{(RUN AVERAGE)} \\ C_0 &= \underline{0.1} && \text{(AVERAGE ZERO)} \\ C_{\text{m}} &= \underline{16.3} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{16.1} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{5.8} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: Oceanside Landfill/ET-29 #007 75% load
DATE: 10/7/92
RUN NO: Linearity #4 (0935-1035)
GAS CONSTITUENT: C_2
ATTENUATION (SPAN): 0-25%.

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:	0.0 %	16.1 %	20.9 %
ANALYZER CAL RESPONSE:	0.0 %	16.2 %	20.8 %
ABSOLUTE DIFFERENCE:	0.0 %	0.1 %	0.1 %
CALIBRATION ERROR (<2%):	0.0 %	0.4 %	0.4 %

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL		
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	DRIFT (<3%)
ZERO:	0.0 %	0.0 %	0.0 %	0.0 %	0.0 %	0.0 %
UPSCALE:	16.2 %	16.1 %	0.4 %	16.1 %	0.4 %	0.0 %

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0},$$

$$\begin{aligned} \bar{C} &= 4.5 && \text{(RUN AVERAGE)} \\ C_0 &= 0.0 && \text{(AVERAGE ZERO)} \\ C_{\text{m}} &= 16.1 && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= 16.1 && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= 4.5 && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: *Oceanside Landfill/ET-29 #007 75% load*
 DATE: *10/7/92*
 RUN NO: # *5 (1115-1215)*
 GAS CONSTITUENT: *O₂*
 ATTENUATION (SPAN): *0-25 %*

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:			
ANALYZER CAL RESPONSE:			
ABSOLUTE DIFFERENCE:			
CALIBRATION ERROR (<%) :			

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL		
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	DRIFT (<3%)
ZERO:	<i>0.0%</i>	<i>0.0%</i>	<i>0.0%</i>	<i>-0.1%</i>	<i>0.4%</i>	<i>0.4%</i>
UPSCALE:	<i>16.2%</i>	<i>16.1%</i>	<i>0.4%</i>	<i>16.0%</i>	<i>0.8%</i>	<i>0.4%</i>

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_o) \times \frac{C_{\text{ma}}}{C_m - C_o}$$

$$\begin{aligned} \bar{C} &= \underline{4.7} && \text{(RUN AVERAGE)} \\ C_o &= \underline{-0.1} && \text{(AVERAGE ZERO)} \\ C_m &= \underline{16.1} && \text{(AVERAGE SPAN)} \\ C_{\text{ma}} &= \underline{16.1} && \text{(SPAN GAS CONC)} \\ C_{\text{gas}} &= \underline{4.8} && \text{(POLLUTANT CONC)} \end{aligned}$$

CEM SYSTEM CALIBRATION DATA
EPA Methods 3A, 6C, and 7E

SOURCE IDENTIFICATION: *Oceanside Landfill/ET-29 #007 75% load*
 DATE: *10/7/92*
 RUN NO: *#6 (1250-1350)*
 GAS CONSTITUENT: *O₂*
 ATTENUATION (SPAN): *0-25%*

ANALYZER CALIBRATION DATA AND/OR LINEARITY CHECK:

	ZERO	MIDRANGE	HIGH RANGE
CAL GAS CONCENTRATION:			
ANALYZER CAL RESPONSE:			
ABSOLUTE DIFFERENCE:			
CALIBRATION ERROR (<2%):			

SYSTEM CAL BIAS & DRIFT:

	PRE CAL			POST CAL	
	ANALYZER CAL RESPONSE	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)	SYSTEM CAL RESPONSE	SYSTEM BIAS (<5%)
ZERO:	<i>0.0%</i>	<i>-0.1%</i>	<i>0.4%</i>	<i>-0.1%</i>	<i>0.4%</i>
UPSCALE:	<i>16.2%</i>	<i>16.0%</i>	<i>0.8%</i>	<i>15.9%</i>	<i>1.2%</i>

$$\text{SYSTEM BIAS} = \frac{(\text{SYSTEM CAL RESPONSE} - \text{ANALYZER CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{(\text{POST SYSTEM CAL RESPONSE} - \text{PRE SYSTEM CAL RESPONSE})}{\text{SPAN}} \times 100$$

$$\text{EQ. 6C-1: } C_{\text{gas}} = (\bar{C} - C_0) \times \frac{C_{\text{ma}}}{C_{\text{m}} - C_0},$$

$$\begin{aligned} \bar{C} &= \underline{4.6} && (\text{RUN AVERAGE}) \\ C_0 &= \underline{-0.1} && (\text{AVERAGE ZERO}) \\ C_{\text{m}} &= \underline{16.0} && (\text{AVERAGE SPAN}) \\ C_{\text{ma}} &= \underline{16.1} && (\text{SPAN GAS CONC}) \\ C_{\text{gas}} &= \underline{4.7} && (\text{POLLUTANT CONC}) \end{aligned}$$

Operational Data

10-6-92

#29 BEFORE TEST (100%)

49°F AMBIENT, CLEAR, DRY

590 KW

52% CH₄

.30 AP @ 6" DWYER, -37" VAC, 56°F (7 eng)

10 PSI CH. AIR @ 88°F STARBOARD (ODD)

92°F PORT (EVEN)

ODD STACK 931°F

EVEN STACK 912°F

37° TIMING BTDC

EXHAUST TEMPS 1082°F (CYL #1) → 1127°F (CYL #3)

ENERAC 109 PPM NO

429 PPM CO

TELEDYNE 5.8% O₂

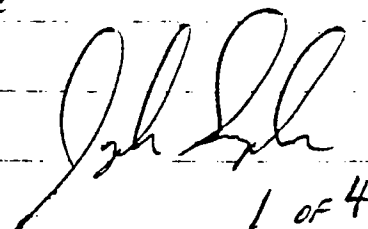
THROTTLE FULL OPEN

PSC FULL OPEN

~~12 1/2" WC~~ 12 1/2" WC G/A ODD, 12" WC G/A EVEN

10 PSI BOOST PRESSURE

8 1/2 PSI MANIFOLD PRESSURE, ± 2" WC BALANCE


1 of 4

ET-29 ENGINE TEST DATA
EMISSION PT. 007 TAKEN BY: J. SNYDER DATE: 10-6-92
BAROMETER: _____ AMBIENT TEMP: _____ RUN#: 1
PRESSURE AT COMPRESSOR INLET: -37", "WC

DATE: 10-6-92

RUN# : 1

PRESSURE AT COMPRESSOR INLET: -37" , "WC

COMMENTS:

SEE OTHER SHEET FOR ENGINE SETTINGS.

2 of 4

10-7-92

#29 BEFORE TEST (75%)

50°F AMBIENT, CLEAR, DRY

448 KW

51% CH₄

.23 AP @ 6" DWYER, -34" WC, 58°F (7 ENG.)

10 PSI CH. AIR @ 88.1°F PORT (EVEN)

ODD STACK 991°F

EVEN STACK 954°F

31° TIMING BTDC

EXHAUST TEMPS 1093° (CYL #11) → 1172°F (CYL #2)

ENERAC 123 PPM NO

492 PPM CO

TELETYPE 4.8% O₂

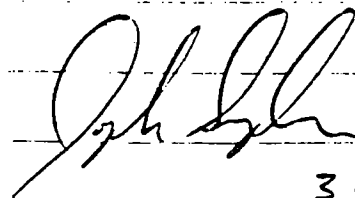
THROTTLE ~ 40% OPEN

PSC ~ 50% OPEN

14" G/A EVEN, 14" G/A ODD

10 1/2 PSI BOOST, 4 PSI MANIFOLD EVEN

10 1/2 PSI BOOST, 4 1/4 PSI MANIFOLD ODD (THROTTLE PLATES NON-LINEAR)



3 of 4

ENGINE TEST DATA
E1-29 EMISSION PT.007 TAKEN BY: J. Snyder DATE: 10-7-92
BAROMETER: _____ AMBIENT TEMP: _____ RUN#: 1
PRESSURE AT COMPRESSOR INLET: -34, "WC

DATE: 10-7-92

RUN# : (

ACCORDING TO: _____

COMMENTS:

[Signature]

4 OF 4

APPENDIX C

DAS Printouts

DATE 10-01-1992

10-01-1992 08:01:58

Mode: 14, A/L

A/D (Analog to Digital) Converter address= 772

Storage Interval: hours= 0 minutes= 0 seconds= 30

Printer will log data.

Alarms are silent

Autostop is off

Autostore on disk C

Oceanside Landfill Page 1
 Energy Tactics
 ET-29 #007 100% load

Point	Label	Units	Offset	Scaling	Dec Pl	High Alarm	Low Alarm	Channel	Ext Mod
1	NOX	ppm	-7	.1	1	0	0	0	0
2	O2	%	-2.75	.025	1	0	0	0	2
3	CO	ppm	33.5	.25	1	0	0	0	4

DATE 10-01-1992

Start # 1 08:01:26

NOX 3.2 ppm 02 21.0 % 00 13.7 ppm

Start # 2 08:02:58

NOX 2.8 ppm 02 21.0 % 00 12.5 ppm

Start # 3 08:03:26

NOX 3.0 ppm 02 21.0 % 00 13.1 ppm

Start # 4 08:03:58

NOX 2.4 ppm 02 21.0 % 00 13.1 ppm

Start # 5 08:04:26

NOX 8.5 ppm 02 21.0 % 00 15.1 ppm

Start # 6 08:04:58

NOX 6.9 ppm 02 20.7 % 00 10.3 ppm

Start # 7 08:05:26

NOX 6.5 ppm 02 20.7 % 00 7.0 ppm

Start # 8 08:05:58

NOX -0.2 ppm 02 20.7 % 00 5.9 ppm

Start # 9 08:06:26

NOX -0.1 ppm 02 20.7 % 00 5.5 ppm

Start # 10 08:06:58

NOX -0.1 ppm 02 20.7 % 00 5.0 ppm

Start # 11 08:07:26

NOX -0.6 ppm 02 20.7 % 00 2.0 ppm

Start # 12 08:07:58

NOX -0.5 ppm 02 20.7 % 00 1.8 ppm

Start # 13 08:08:26

NOX -0.6 ppm 02 20.7 % 00 1.7 ppm

Ambient air
 20.9 % O₂

Scan # 10	08:19:11				
Adm	-1.2 ppm	01	20.7 %	00	1.3 ppm
DATE 10-06-1992					
Scan # 1	08:11:07				
Adm	0.5 ppm	02	20.7 %	00	-1.0 ppm
Scan # 2	08:12:07				
Adm	0.5 ppm	02	20.7 %	00	2.0 ppm
Scan # 3	08:12:37				
Adm	0.3 ppm	01	20.7 %	00	-0.6 ppm
Scan # 4	08:13:07				
Adm	0.5 ppm	02	20.7 %	00	0.4 ppm
Scan # 5	08:13:37				
Adm	0.6 ppm	02	20.7 %	00	-170.2 ppm
Scan # 6	08:14:07				
Adm	0.7 ppm	02	20.7 %	00	-169.8 ppm
Scan # 7	08:14:37				
Adm	0.6 ppm	02	20.7 %	00	-0.4 ppm
Scan # 8	08:15:07				
Adm	0.5 ppm	02	20.7 %	00	-0.3 ppm
Scan # 9	08:15:37				
Adm	0.9 ppm	02	20.7 %	00	1.1 ppm
Scan # 11	08:16:07				
Adm	0.5 ppm	01	20.7 %	00	0.9 ppm
Scan # 11	08:16:37				
Adm	0.5 ppm	02	20.7 %	00	-0.5 ppm
Scan # 12	08:17:07				
Adm	0.8 ppm	02	20.7 %	00	-0.6 ppm
Scan # 13	08:17:37				
Adm	0.7 ppm	02	20.7 %	00	-1.2 ppm
Scan # 14	08:18:07				
Adm	0.5 ppm	02	20.7 %	00	-1.2 ppm
Scan # 15	08:18:37				
Adm	0.5 ppm	02	20.7 %	00	0.0 ppm
Scan # 16	08:19:07				
Adm	0.5 ppm	02	20.7 %	00	-1.5 ppm
Scan # 17	08:19:37				
Adm	0.3 ppm	01	20.7 %	00	-1.5 ppm
Scan # 18	08:20:07				
Adm	0.2 ppm	02	20.7 %	00	-0.2 ppm
Scan # 19	08:20:37				
Adm	0.2 ppm	01	20.7 %	00	-0.5 ppm

Scan # 21	09:21:37				
NOx	1.4 ppm	01	20.7 %	01	-1.0 ppm
Scan # 22	09:22:07				
NOx	1.2 ppm	02	20.7 %	02	-1.3 ppm
Scan # 23	09:22:37				
NOx	1.1 ppm	01	20.7 %	01	0.4 ppm
Scan # 24	09:23:07				
NOx	1.0 ppm	01	20.7 %	00	-2.3 ppm
Scan # 25	09:23:37				
NOx	0.9 ppm	02	20.7 %	00	-0.5 ppm
Scan # 26	09:24:07				
NOx	0.9 ppm	02	20.7 %	00	-1.9 ppm
Scan # 27	09:24:37				
NOx	0.9 ppm	02	20.7 %	00	-2.9 ppm
Scan # 28	09:25:07				
NOx	0.8 ppm	01	20.7 %	00	-0.1 ppm
Scan # 29	09:25:37				
NOx	1.3 ppm	02	20.7 %	00	-0.6 ppm
Scan # 30	09:26:07				
NOx	1.2 ppm	01	20.7 %	00	-0.6 ppm

*Begin analyzer
cals*

DATE 10-01-1991

Scan # 1	09:35:23				
NOx	0.5 ppm	02	20.7 %	00	0.4 ppm
Scan # 2	09:35:53				
NOx	0.3 ppm	01	20.7 %	00	0.2 ppm
Scan # 3	09:36:23				
NOx	0.4 ppm	01	20.7 %	00	-0.3 ppm
Scan # 4	09:36:53				
NOx	0.1 ppm	01	20.7 %	00	0.2 ppm
Scan # 5	09:37:23				
NOx	0.0 ppm	02	20.7 %	00	1.4 ppm
Scan # 6	09:37:53				
NOx	0.8 ppm	00	20.7 %	00	-0.6 ppm
Scan # 7	09:38:23				
NOx	0.9 ppm	01	20.7 %	00	0.1 ppm
Scan # 8	09:38:53				
NOx	0.7 ppm	02	20.7 %	00	0.5 ppm
Scan # 9	09:39:23				
NOx	0.8 ppm	01	20.7 %	00	0.1 ppm
Scan # 10	09:39:53				
NOx	0.6 ppm	01	20.7 %	01	0.5 ppm

zero

Scan # 12	08:40:53				
NO _x	0.8 ppm	02	0.4 %	00	488.5 ppm
Scan # 13	08:41:23				
NO _x	1.0 ppm	02	0.6 %	00	489.1 ppm
Scan # 14	08:41:53				
NO _x	0.7 ppm	02	0.4 %	00	489.4 ppm
Scan # 15	08:42:23				
NO _x	0.8 ppm	02	0.4 %	00	490.7 ppm
Scan # 16	08:42:53				
NO _x	0.8 ppm	02	0.4 %	00	490.5 ppm
Scan # 17	08:43:23				
NO _x	0.3 ppm	02	0.0 %	00	490.7 ppm
Scan # 18	08:43:53				
NO _x	487.0 ppm	02	0.1 %	00	15.5 ppm
Scan # 19	08:44:23				
NO _x	489.8 ppm	02	0.0 %	00	1.6 ppm
Scan # 20	08:44:53				
NO _x	484.1 ppm	02	0.0 %	00	1.0 ppm
Scan # 21	08:45:23				
NO _x	487.1 ppm	02	0.0 %	00	0.5 ppm
Scan # 22	08:45:53				
NO _x	485.6 ppm	02	0.0 %	00	1.1 ppm
Scan # 23	08:46:23				
NO _x	485.5 ppm	02	0.0 %	00	0.2 ppm
Scan # 24	08:46:53				
NO _x	485.1 ppm	02	0.0 %	00	0.8 ppm
Scan # 25	08:47:23				
NO _x	474.9 ppm	02	0.0 %	00	5.4 ppm
Scan # 26	08:47:53				
NO _x	2.6 ppm	02	0.0 %	00	272.7 ppm
Scan # 27	08:48:23				
NO _x	1.5 ppm	02	0.0 %	00	273.4 ppm
Scan # 28	08:48:53				
NO _x	0.6 ppm	02	0.0 %	00	274.6 ppm
Scan # 29	08:49:23				
NO _x	0.2 ppm	02	0.0 %	00	274.0 ppm
Scan # 30	08:49:53				
NO _x	0.1 ppm	02	0.0 %	00	278.3 ppm
Scan # 31	08:50:23				
NO _x	0.0 ppm	02	0.0 %	00	278.9 ppm
Scan # 32	08:50:53				
NO _x	0.0 ppm	02	0.0 %	00	278.1 ppm
Scan # 33	08:51:23				

4

487.0 ppm CO
O₂ zero

480.0 ppm NO

284.0 ppm CO

Scan # 34	08:51:51				
NO ₂	-0.6 ppm	01	-0.0 %	00	276.5 ppm
Scan # 35	08:52:27				
NO ₂	55.0 ppm	01	0.0 %	01	3.2 ppm
Scan # 36	08:52:53				
NO ₂	55.0 ppm	01	0.0 %	01	0.4 ppm
Scan # 37	08:53:20				
NO ₂	55.6 ppm	02	0.0 %	02	0.3 ppm
Scan # 38	08:53:57				
NO ₂	55.1 ppm	02	0.0 %	02	-0.3 ppm
Scan # 39	08:54:23				
NO ₂	54.4 ppm	02	0.0 %	02	-0.3 ppm
Scan # 40	08:54:50				
NO ₂	57.0 ppm	02	0.0 %	02	0.0 ppm
Scan # 41	08:55:23				
NO ₂	0.3 ppm	02	0.0 %	02	144.8 ppm
Scan # 42	08:55:53				
NO ₂	0.3 ppm	02	0.0 %	02	144.8 ppm
Scan # 43	08:56:23				
NO ₂	0.1 ppm	02	0.0 %	02	144.6 ppm
Scan # 44	08:56:53				
NO ₂	-0.3 ppm	02	0.0 %	02	144.3 ppm
Scan # 45	08:57:23				
NO ₂	0.6 ppm	01	0.0 %	01	144.0 ppm
Scan # 46	08:57:53				
NO ₂	-0.2 ppm	02	16.1 %	02	1.2 ppm
Scan # 47	08:58:23				
NO ₂	0.1 ppm	01	16.2 %	02	-0.1 ppm
Scan # 48	08:58:53				
NO ₂	0.0 ppm	02	16.3 %	02	0.4 ppm
Scan # 49	08:59:20				
NO ₂	0.3 ppm	02	16.3 %	02	-0.5 ppm
Scan # 50	08:59:50				
NO ₂	0.0 ppm	02	16.3 %	02	0.0 ppm
Scan # 51	09:00:20				
NO ₂	0.1 ppm	02	16.3 %	02	-0.6 ppm
Scan # 52	09:00:50				
NO ₂	0.5 ppm	01	16.2 %	02	-0.6 ppm
Scan # 53	09:01:20				
NO ₂	110.0 ppm	01	0.2 %	02	1.5 ppm
Scan # 54	09:01:50				
NO ₂	276.5 ppm	01	0.0 %	02	-0.3 ppm
Scan # 55	09:02:20				

97.5 ppm NO

141.0 ppm CO

16.1% O₂

6

242.0 ppm NO

Scan # 50	09:02:55				
NO _x	244.7 ppm	02	1.1 %	00	0.1 ppm
Scan # 51	09:03:27				
NO _x	245.5 ppm	02	0.0 %	00	0.0 ppm
Scan # 52	09:03:53				
NO _x	245.4 ppm	01	0.0 %	01	-0.1 ppm
Scan # 55	09:04:23				
NO _x	245.3 ppm	02	0.0 %	00	-0.4 ppm
Scan # 60	09:04:57				
NO _x	244.5 ppm	02	0.0 %	00	-0.1 ppm
Scan # 61	09:05:23				
NO _x	237.9 ppm	02	1.3 %	00	1.3 ppm
Scan # 62	09:05:53				
NO _x	1.7 ppm	02	21.1 %	00	6.0 ppm
Scan # 63	09:06:23				
NO _x	1.3 ppm	02	21.2 %	00	7.4 ppm
Scan # 64	09:06:53				
NO _x	0.9 ppm	02	21.2 %	00	7.9 ppm
Scan # 65	09:07:23				
NO _x	1.1 ppm	02	21.1 %	00	7.9 ppm
Scan # 66	09:07:53				
NO _x	2.3 ppm	02	20.6 %	00	7.4 ppm
Scan # 67	09:08:23				
NO _x	-1.3 ppm	02	20.5 %	00	7.2 ppm
Scan # 68	09:08:53				
NO _x	0.1 ppm	02	20.4 %	00	7.9 ppm
Scan # 69	09:09:23				
NO _x	-0.3 ppm	02	20.0 %	00	7.0 ppm
Scan # 70	09:09:53				
NO _x	-0.2 ppm	02	19.1 %	00	6.9 ppm
Scan # 71	09:10:27				
NO _x	-0.3 ppm	02	20.7 %	00	7.8 ppm
Scan # 72	09:10:53				
NO _x	0.1 ppm	02	20.6 %	00	8.4 ppm
Scan # 73	09:11:23				
NO _x	2.2 ppm	02	20.9 %	00	8.7 ppm
Scan # 74	09:11:53				
NO _x	-0.2 ppm	02	20.6 %	00	7.7 ppm
Scan # 75	09:12:27				
NO _x	-0.1 ppm	02	20.6 %	00	7.8 ppm
Scan # 76	09:12:53				
NO _x	0.4 ppm	02	20.6 %	00	8.4 ppm
Scan # 77	09:13:27				

Scan # 78	09:13:53				
NO _x	0.6 ppm	02	20.6 %	00	6.6 ppm
Scan # 79	09:14:23				
NO _x	0.7 ppm	02	20.6 %	00	7.4 ppm
Scan # 80	09:14:53				
NO _x	0.7 ppm	02	20.6 %	00	7.7 ppm
Scan # 81	09:15:23				
NO _x	0.9 ppm	02	20.6 %	00	8.1 ppm
Scan # 82	09:15:53				
NO _x	0.7 ppm	02	20.6 %	00	8.3 ppm
Scan # 83	09:16:23				
NO _x	0.8 ppm	02	20.6 %	00	8.6 ppm
Scan # 84	09:16:53				
NO _x	0.7 ppm	02	20.5 %	00	7.9 ppm
Scan # 85	09:17:23				
NO _x	1.1 ppm	02	20.5 %	00	8.4 ppm
Scan # 86	09:17:53				
NO _x	1.1 ppm	02	20.5 %	00	8.7 ppm
Scan # 87	09:18:23				
NO _x	1.3 ppm	02	20.5 %	00	7.7 ppm
Scan # 88	09:18:53				
NO _x	1.1 ppm	02	20.5 %	00	8.9 ppm
Scan # 89	09:19:23				
NO _x	1.4 ppm	02	20.6 %	00	8.8 ppm
Scan # 90	09:19:53				
NO _x	0.7 ppm	02	20.6 %	00	8.4 ppm
Scan # 91	09:20:23				
NO _x	1.4 ppm	02	20.7 %	00	9.2 ppm
Scan # 92	09:20:53				
NO _x	1.3 ppm	02	20.7 %	00	8.3 ppm
Scan # 93	09:21:23				
NO _x	1.1 ppm	02	20.7 %	00	8.1 ppm
Scan # 94	09:21:53				
NO _x	0.8 ppm	02	20.7 %	00	7.7 ppm
Scan # 95	09:22:23				
NO _x	0.9 ppm	02	20.6 %	00	7.3 ppm
Scan # 96	09:22:53				
NO _x	0.9 ppm	02	20.6 %	00	8.0 ppm
Scan # 97	09:23:23				
NO _x	0.6 ppm	02	20.6 %	00	7.9 ppm
Scan # 98	09:23:53				
NO _x	0.5 ppm	02	20.6 %	00	7.9 ppm
Scan # 99	09:24:23				

Standby for
leak check

Score # 100	09:24:57				
Ad	0.3 ppm	00	20.6 %	00	8.2 ppm
Score # 101	09:25:23				
Ad	0.6 ppm	01	20.6 %	00	8.1 ppm
Score # 102	09:25:53				
Ad	1.0 ppm	01	20.6 %	01	7.6 ppm
Score # 103	09:26:23				
Ad	1.1 ppm	01	20.6 %	00	7.3 ppm
Score # 104	09:26:53				
Ad	1.2 ppm	02	20.6 %	00	7.9 ppm
Score # 105	09:27:23				
Ad	1.5 ppm	02	20.6 %	00	7.3 ppm
Score # 106	09:27:53				
Ad	1.3 ppm	02	20.6 %	00	8.7 ppm
Score # 107	09:28:23				
Ad	1.3 ppm	02	20.6 %	00	7.7 ppm
Score # 108	09:28:53				
Ad	1.1 ppm	02	20.6 %	00	7.4 ppm
Score # 109	09:29:23				
Ad	1.3 ppm	02	20.6 %	00	8.4 ppm
Score # 110	09:29:53				
Ad	1.3 ppm	02	20.6 %	00	8.1 ppm
Score # 111	09:30:23				
Ad	1.1 ppm	02	20.6 %	00	8.3 ppm
Score # 112	09:30:53				
Ad	1.3 ppm	01	20.6 %	00	7.6 ppm
Score # 113	09:31:23				
Ad	1.6 ppm	01	20.6 %	00	7.8 ppm
Score # 114	09:31:53				
Ad	1.1 ppm	02	20.6 %	00	7.8 ppm
Score # 115	09:32:23				
Ad	1.4 ppm	02	20.5 %	00	7.6 ppm
Score # 116	09:32:53				
Ad	1.1 ppm	01	20.5 %	00	8.6 ppm
Score # 117	09:33:23				
Ad	0.9 ppm	01	20.5 %	00	8.2 ppm
Score # 118	09:33:53				
Ad	0.8 ppm	01	20.5 %	00	8.0 ppm
Score # 119	09:34:23				
Ad	0.6 ppm	01	20.5 %	01	8.1 ppm
Score # 120	09:34:53				
Ad	0.4 ppm	01	20.5 %	00	8.1 ppm

Scan # 113	09:36:11	0.0 ppm	01	20.5 %	00	8.4 ppm
Scan # 113	09:36:27	0.4 ppm	02	20.5 %	00	7.6 ppm
Scan # 114	09:36:57	0.9 ppm	02	20.5 %	00	8.1 ppm
Scan # 115	09:37:23	0.7 ppm	02	20.5 %	00	7.5 ppm
Scan # 116	09:37:50	0.6 ppm	02	20.5 %	00	7.9 ppm
Scan # 117	09:38:20	0.2 ppm	02	20.5 %	00	7.6 ppm
Scan # 118	09:38:55	0.9 ppm	02	20.4 %	00	8.0 ppm
Scan # 119	09:39:23	0.7 ppm	02	20.4 %	00	8.5 ppm
Scan # 120	09:39:50	0.7 ppm	02	20.4 %	00	7.4 ppm
Scan # 121	09:40:23	0.4 ppm	02	20.4 %	00	8.3 ppm
Scan # 122	09:40:53	0.5 ppm	02	20.4 %	00	7.9 ppm
Scan # 123	09:41:20	0.5 ppm	02	20.4 %	00	8.1 ppm
Scan # 124	09:41:57	0.5 ppm	02	20.4 %	00	7.9 ppm
Scan # 125	09:42:23	0.6 ppm	02	20.4 %	00	8.0 ppm
Scan # 126	09:42:50	0.2 ppm	02	20.4 %	00	8.0 ppm
Scan # 127	09:43:20	0.4 ppm	02	20.4 %	00	8.3 ppm
Scan # 128	09:43:53	0.2 ppm	02	20.4 %	00	7.7 ppm
Scan # 129	09:44:23	0.1 ppm	02	20.4 %	00	7.9 ppm
Scan # 130	09:44:53	0.2 ppm	02	20.4 %	00	7.2 ppm
Scan # 141	09:45:01	0.4 ppm	02	20.3 %	00	8.3 ppm
Scan # 142	09:45:50	0.7 ppm	02	20.3 %	00	8.4 ppm
Scan # 143	09:46:17					

Leak check
Good

144	Scan # 144	09:45:53	02	20.3 %	00	8.3 ppm
	ADx	0.5 ppm				
145	Scan # 145	09:47:23	02	20.3 %	00	8.1 ppm
	ADx	0.3 ppm				
146	Scan # 146	09:47:53	02	20.3 %	00	9.8 ppm
	ADx	-1.0 ppm				
147	Scan # 147	09:48:23	02	21.1 %	00	9.0 ppm
	ADx	-1.1 ppm				
148	Scan # 148	09:48:53	02	21.2 %	00	10.1 ppm
	ADx	-0.5 ppm				
149	Scan # 149	09:49:23	02	21.1 %	00	10.5 ppm
	ADx	-0.9 ppm				
150	Scan # 150	09:49:53	02	21.1 %	00	9.8 ppm
	ADx	-0.9 ppm				
151	Scan # 151	09:50:23	02	21.1 %	00	10.1 ppm
	ADx	0.9 ppm				
152	Scan # 152	09:50:53	02	20.9 %	00	9.3 ppm
	ADx	-0.3 ppm				
153	Scan # 153	09:51:23	02	20.7 %	00	8.3 ppm
	ADx	-2.6 ppm				
154	Scan # 154	09:51:53	02	20.7 %	00	7.7 ppm
	ADx	-2.9 ppm				
155	Scan # 155	09:52:23	02	20.7 %	00	8.4 ppm
	ADx	-2.6 ppm				
156	Scan # 156	09:52:53	02	20.7 %	00	8.0 ppm
	ADx	-1.0 ppm				
157	Scan # 157	09:53:23	02	20.7 %	00	7.1 ppm
	ADx	-0.9 ppm				
158	Scan # 158	09:53:53	02	20.7 %	00	8.1 ppm
	ADx	-3.0 ppm				
159	Scan # 159	09:54:23	02	20.7 %	00	6.2 ppm
	ADx	-0.9 ppm				
160	Scan # 160	09:54:53	02	20.7 %	00	4.0 ppm
	ADx	-0.4 ppm				
161	Scan # 161	09:55:23	02	20.7 %	00	2.3 ppm
	ADx	0.1 ppm				
162	Scan # 162	09:55:53	02	20.7 %	00	3.1 ppm
	ADx	0.5 ppm				
163	Scan # 163	09:56:23	02	20.7 %	00	3.9 ppm
	ADx	0.3 ppm				
164	Scan # 164	09:56:53	02	20.7 %	00	3.2 ppm
	ADx	0.5 ppm				
165	Scan # 165	09:57:23	02	20.7 %	00	3.2 ppm
	ADx	0.5 ppm				

Begin system cals

14

Scan # 167	09:59:20	20.7 %	CO	3.9 ppm
NOx	1.1 ppm	20.7 %	CO	3.9 ppm
Scan # 168	09:59:50			
NOx	-0.5 ppm	7.4 %	CO	392.5 ppm
Scan # 169	09:59:20			
NOx	0.3 ppm	0.4 %	CO	497.2 ppm
Scan # 170	09:59:50			
NOx	0.3 ppm	0.1 %	CO	500.5 ppm
Scan # 171	10:00:20			
NOx	-0.6 ppm	0.1 %	CO	501.7 ppm
Scan # 172	10:00:50			
NOx	0.2 ppm	0.1 %	CO	499.5 ppm
Scan # 173	10:01:20			
NOx	0.3 ppm	0.0 %	CO	495.6 ppm
Scan # 174	10:01:50			
NOx	0.6 ppm	0.0 %	CO	495.6 ppm
Scan # 175	10:02:20			
NOx	0.3 ppm	0.0 %	CO	494.8 ppm
Scan # 176	10:02:50			
NOx	0.3 ppm	0.0 %	CO	495.6 ppm
Scan # 177	10:03:20			
NOx	0.5 ppm	0.0 %	CO	495.6 ppm
Scan # 178	10:03:50			
NOx	0.8 ppm	4.4 %	CO	321.9 ppm
Scan # 179	10:04:20			
NOx	0.8 ppm	20.2 %	CO	15.9 ppm
Scan # 180	10:04:50			
NOx	202.2 ppm	1.8 %	CO	5.7 ppm
Scan # 181	10:05:20			
NOx	201.1 ppm	0.1 %	CO	4.5 ppm
Scan # 182	10:05:50			
NOx	234.8 ppm	0.0 %	CO	4.3 ppm
Scan # 183	10:06:20			
NOx	234.9 ppm	0.0 %	CO	4.9 ppm
Scan # 184	10:06:50			
NOx	235.7 ppm	0.0 %	CO	4.8 ppm
Scan # 185	10:07:20			
NOx	235.7 ppm	0.0 %	CO	4.7 ppm
Scan # 186	10:07:50			
NOx	235.2 ppm	0.0 %	CO	4.0 ppm
Scan # 187	10:08:20			
NOx	241.1 ppm	0.0 %	CO	4.7 ppm

487.0 ppm CO
O2 zero

242.0 ppm NO

I

12

Scan #	187	10:09:27	02	0.0 %	00	3.9 ppm
NOx	239.6 ppm		02	0.0 %	00	3.9 ppm
Scan #	190	10:09:50	02	0.0 %	00	5.1 ppm
NOx	239.4 ppm		02	0.0 %	00	5.1 ppm
Scan #	191	10:10:27	02	15.3 %	00	5.5 ppm
NOx	18.5 ppm		02	15.3 %	00	5.5 ppm
Scan #	192	10:10:53	02	16.2 %	00	5.1 ppm
NOx	2.1 ppm		02	16.2 %	00	5.1 ppm
Scan #	193	10:11:23	02	16.2 %	00	5.2 ppm
NOx	1.6 ppm		02	16.2 %	00	5.2 ppm
Scan #	194	10:11:53	02	16.2 %	00	4.3 ppm
NOx	1.5 ppm		02	16.2 %	00	4.3 ppm
Scan #	195	10:12:23	02	16.2 %	00	4.1 ppm
NOx	1.7 ppm		02	16.2 %	00	4.1 ppm
Scan #	196	10:12:53	02	16.2 %	00	3.8 ppm
NOx	1.3 ppm		02	16.2 %	00	3.8 ppm
Scan #	197	10:13:23	02	16.2 %	00	4.9 ppm
NOx	1.4 ppm		02	16.2 %	00	4.9 ppm
Scan #	198	10:13:53	02	16.2 %	00	18.1 ppm
NOx	18.1 ppm		02	16.2 %	00	18.1 ppm
Scan #	199	10:14:23	02	6.8 %	00	368.4 ppm
NOx	168.2 ppm		02	6.8 %	00	368.4 ppm
Scan #	200	10:14:53	02	5.9 %	00	378.4 ppm
NOx	156.6 ppm		02	5.9 %	00	378.4 ppm
Scan #	201	10:15:23	02	5.8 %	00	381.9 ppm
NOx	153.1 ppm		02	5.8 %	00	381.9 ppm
Scan #	202	10:15:53	02	5.8 %	00	383.2 ppm
NOx	153.6 ppm		02	5.8 %	00	383.2 ppm
Scan #	203	10:16:23	02	5.8 %	00	379.9 ppm
NOx	154.4 ppm		02	5.8 %	00	379.9 ppm
Scan #	204	10:16:53	02	5.8 %	00	379.1 ppm
NOx	159.1 ppm		02	5.8 %	00	379.1 ppm
Scan #	205	10:17:23	02	5.8 %	00	379.5 ppm
NOx	159.1 ppm		02	5.8 %	00	379.5 ppm
Scan #	206	10:17:53	02	5.9 %	00	376.7 ppm
NOx	157.1 ppm		02	5.9 %	00	376.7 ppm
Scan #	207	10:18:23	02	5.9 %	00	377.0 ppm
NOx	156.1 ppm		02	5.9 %	00	377.0 ppm
Scan #	208	10:18:53	02	5.9 %	00	378.3 ppm
NOx	156.1 ppm		02	5.9 %	00	378.3 ppm
Scan #	209	10:19:23	02	5.9 %	00	377.5 ppm
NOx	156.4 ppm		02	5.9 %	00	377.5 ppm

16.1% 02

Begin Run 1

	Scan #	211	10:21:23				
	NOx	181.9 ppm	02	6.9 %	00	375.9 ppm	
	Scan #	212	10:21:50				
	NOx	180.3 ppm	02	6.9 %	00	377.4 ppm	
	Scan #	213	10:21:23				
	NOx	181.5 ppm	02	6.0 %	00	375.4 ppm	
	Scan #	214	10:21:53				
	NOx	179.2 ppm	02	6.2 %	00	371.9 ppm	
	Scan #	215	10:22:00				
	NOx	184.6 ppm	02	6.2 %	00	370.2 ppm	
	Scan #	216	10:22:53				
	NOx	174.1 ppm	01	6.2 %	00	369.2 ppm	
	Scan #	217	10:23:23				
	NOx	186.3 ppm	02	6.3 %	00	367.8 ppm	
	Scan #	218	10:23:53				
	NOx	166.5 ppm	02	6.3 %	00	367.3 ppm	
	Scan #	219	10:24:03				
	NOx	166.6 ppm	02	6.2 %	00	370.6 ppm	
	Scan #	220	10:24:53				
	NOx	175.9 ppm	02	6.3 %	00	369.2 ppm	
	Scan #	221	10:25:23				
	NOx	182.7 ppm	02	6.3 %	00	368.1 ppm	
	Scan #	222	10:25:53				
	NOx	165.9 ppm	01	6.4 %	00	364.6 ppm	
	Scan #	223	10:26:23				
	NOx	176.6 ppm	02	6.4 %	00	365.1 ppm	
	Scan #	224	10:26:53				
	NOx	172.6 ppm	02	6.4 %	00	366.4 ppm	
	Scan #	225	10:27:23				
	NOx	184.6 ppm	02	6.3 %	00	367.0 ppm	
	Scan #	226	10:27:53				
	NOx	171.4 ppm	02	6.4 %	00	366.1 ppm	
	Scan #	227	10:28:03				
	NOx	183.5 ppm	02	6.4 %	00	366.8 ppm	
	Scan #	228	10:28:53				
	NOx	171.4 ppm	02	6.4 %	00	364.8 ppm	
	Scan #	229	10:29:03				
	NOx	179.4 ppm	02	6.4 %	00	363.7 ppm	
	Scan #	230	10:29:53				
	NOx	181.6 ppm	01	6.4 %	00	364.6 ppm	
	Scan #	231	10:30:23				
	NOx	179.7 ppm	01	6.4 %	00	365.5 ppm	

Scan #	133	10:31:13	NOx	181.8 ppm	02	6.4 %	00	364.1 ppm
Scan #	234	10:31:58	NOx	171.8 ppm	01	6.4 %	00	364.8 ppm
Scan #	235	10:32:27	NOx	161.9 ppm	01	6.4 %	00	364.5 ppm
Scan #	236	10:32:53	NOx	165.5 ppm	01	6.4 %	00	364.7 ppm
Scan #	237	10:33:23	NOx	151.3 ppm	01	6.4 %	00	365.6 ppm
Scan #	238	10:33:51	NOx	175.1 ppm	02	6.5 %	00	362.1 ppm
Scan #	239	10:34:27	NOx	177.9 ppm	02	6.5 %	00	361.9 ppm
Scan #	240	10:34:53	NOx	174.2 ppm	01	6.5 %	00	364.6 ppm
Scan #	241	10:35:23	NOx	167.9 ppm	02	6.2 %	00	376.2 ppm
Scan #	242	10:35:53	NOx	182.4 ppm	01	5.8 %	00	377.2 ppm
Scan #	243	10:36:23	NOx	182.4 ppm	02	5.8 %	00	376.5 ppm
Scan #	244	10:36:51	NOx	178.7 ppm	01	5.9 %	00	377.5 ppm
Scan #	245	10:37:27	NOx	187.3 ppm	01	5.8 %	00	380.1 ppm
Scan #	246	10:37:53	NOx	185.2 ppm	02	5.8 %	00	380.6 ppm
Scan #	247	10:38:27	NOx	186.5 ppm	02	5.8 %	00	377.3 ppm
Scan #	248	10:38:53	NOx	189.5 ppm	02	5.8 %	00	379.5 ppm
Scan #	249	10:39:23	NOx	194.6 ppm	01	5.8 %	00	383.0 ppm
Scan #	250	10:39:53	NOx	190.4 ppm	02	5.8 %	00	377.8 ppm
Scan #	251	10:40:23	NOx	185.2 ppm	02	5.8 %	00	377.1 ppm
Scan #	252	10:40:53	NOx	191.7 ppm	01	5.8 %	00	378.2 ppm
Scan #	253	10:41:23	NOx	190.4 ppm	01	5.8 %	00	381.7 ppm

Scan # 251	10:42:27				
NOx	190.6 ppm	02	5.8 %	00	379.1 ppm
Scan # 256	10:42:53				
NOx	192.0 ppm	02	5.8 %	01	380.8 ppm
Scan # 257	10:43:23				
NOx	201.9 ppm	02	5.8 %	00	380.5 ppm
Scan # 259	10:43:53				
NOx	197.9 ppm	02	5.8 %	00	381.1 ppm
Scan # 259	10:44:23				
NOx	192.9 ppm	02	5.8 %	00	381.4 ppm
Scan # 260	10:44:53				
NOx	192.4 ppm	02	5.8 %	00	378.0 ppm
Scan # 261	10:45:23				
NOx	200.1 ppm	02	5.8 %	00	381.8 ppm
Scan # 262	10:45:53				
NOx	198.0 ppm	02	5.8 %	00	378.7 ppm
Scan # 263	10:46:23				
NOx	198.3 ppm	02	5.8 %	00	379.4 ppm
Scan # 264	10:46:53				
NOx	192.5 ppm	02	5.8 %	00	378.5 ppm
Scan # 265	10:47:23				
NOx	201.4 ppm	02	5.8 %	00	379.7 ppm
Scan # 266	10:47:53				
NOx	202.6 ppm	02	5.8 %	01	383.0 ppm
Scan # 267	10:48:23				
NOx	202.1 ppm	02	5.8 %	00	382.0 ppm
Scan # 268	10:48:53				
NOx	200.9 ppm	02	5.8 %	00	374.1 ppm
Scan # 269	10:49:23				
NOx	198.1 ppm	02	5.8 %	00	377.2 ppm
Scan # 270	10:49:53				
NOx	202.7 ppm	02	5.8 %	00	379.2 ppm
Scan # 271	10:50:23				
NOx	200.7 ppm	02	5.8 %	00	379.7 ppm
Scan # 272	10:50:53				
NOx	199.9 ppm	02	5.8 %	01	378.9 ppm
Scan # 273	10:51:23				
NOx	195.2 ppm	02	5.8 %	00	380.8 ppm
Scan # 274	10:51:53				
NOx	197.1 ppm	02	5.8 %	01	381.3 ppm
Scan # 275	10:52:23				
NOx	196.7 ppm	02	5.8 %	01	380.4 ppm

16

Scan #	177	10:53:21	NOx	205.9 ppm	01	5.8 %	00	381.8 ppm
Scan #	178	10:53:57	NOx	199.2 ppm	01	5.7 %	00	382.6 ppm
Scan #	179	10:54:27	NOx	195.9 ppm	02	5.8 %	00	383.5 ppm
Scan #	180	10:54:50	NOx	191.2 ppm	02	5.8 %	00	382.1 ppm
Scan #	181	10:55:13	NOx	201.1 ppm	01	5.8 %	00	382.6 ppm
Scan #	182	10:55:33	NOx	198.2 ppm	02	5.8 %	00	382.6 ppm
Scan #	183	10:55:53	NOx	193.5 ppm	02	5.8 %	00	382.9 ppm
Scan #	184	10:56:17	NOx	162.8 ppm	02	5.7 %	00	382.7 ppm
Scan #	185	10:57:23	NOx	210.0 ppm	02	5.8 %	00	385.7 ppm
Scan #	186	10:57:50	NOx	209.6 ppm	02	5.7 %	00	386.0 ppm
Scan #	187	10:58:27	NOx	188.9 ppm	02	5.8 %	00	385.1 ppm
Scan #	188	10:58:57	NOx	210.7 ppm	02	5.7 %	00	385.5 ppm
Scan #	189	10:59:00	NOx	211.2 ppm	01	5.8 %	00	384.1 ppm
Scan #	190	10:59:57	NOx	196.5 ppm	02	5.7 %	00	384.1 ppm
Scan #	191	11:00:23	NOx	182.2 ppm	01	6.7 %	00	365.2 ppm
Scan #	192	11:00:53	NOx	210.5 ppm	02	5.8 %	00	380.2 ppm
Scan #	193	11:01:21	NOx	201.4 ppm	02	5.8 %	00	382.3 ppm
Scan #	194	11:01:50	NOx	17.3 ppm	01	5.8 %	00	381.0 ppm
Scan #	195	11:02:27	NOx	2.1 ppm	02	5.8 %	00	382.2 ppm
Scan #	196	11:02:50	NOx	1.1 ppm	01	5.8 %	00	383.9 ppm
Scan #	197	11:03:27	NOx	40.5 ppm	01	15.2 %	00	383.2 ppm

Condenser freeze-up
no sample flow -
standby



Scan # 299	11:04:23	18.4 %	35.2 ppm
NO ₂	3.3 ppm	02	35.2 ppm
Scan # 300	11:04:53	18.5 %	35.0 ppm
NO ₂	3.2 ppm	02	35.0 ppm
Scan # 301	11:05:23	18.4 %	35.0 ppm
NO ₂	3.4 ppm	02	35.0 ppm
Scan # 302	11:05:53	18.4 %	35.8 ppm
NO ₂	3.8 ppm	02	35.8 ppm
Scan # 303	11:06:23	18.4 %	35.5 ppm
NO ₂	3.5 ppm	02	35.5 ppm
Scan # 304	11:06:53	18.3 %	35.7 ppm
NO ₂	3.7 ppm	02	35.7 ppm
Scan # 305	11:07:23	18.3 %	35.6 ppm
NO ₂	3.5 ppm	02	35.6 ppm
Scan # 306	11:07:53	18.2 %	35.6 ppm
NO ₂	3.4 ppm	02	35.6 ppm
Scan # 307	11:08:23	18.2 %	37.9 ppm
NO ₂	3.3 ppm	02	37.9 ppm
Scan # 308	11:08:53	18.3 %	35.5 ppm
NO ₂	3.1 ppm	02	35.5 ppm
Scan # 309	11:09:23	15.0 %	62.9 ppm
NO ₂	35.4 ppm	02	62.9 ppm
Scan # 310	11:09:53	20.5 %	7.9 ppm
NO ₂	15.1 ppm	02	7.9 ppm
Scan # 311	11:10:23	20.7 %	7.1 ppm
NO ₂	2.5 ppm	02	7.1 ppm
Scan # 312	11:10:53	20.7 %	5.9 ppm
NO ₂	2.6 ppm	02	5.9 ppm
Scan # 313	11:11:23	20.7 %	7.3 ppm
NO ₂	2.7 ppm	02	7.3 ppm
Scan # 314	11:11:53	20.7 %	6.5 ppm
NO ₂	2.4 ppm	02	6.5 ppm
Scan # 315	11:12:23	20.7 %	5.5 ppm
NO ₂	2.6 ppm	02	5.5 ppm
Scan # 316	11:12:53	20.7 %	7.6 ppm
NO ₂	2.4 ppm	02	7.6 ppm
Scan # 317	11:13:23	20.7 %	6.2 ppm
NO ₂	2.4 ppm	02	6.2 ppm
Scan # 318	11:13:53	20.7 %	7.2 ppm
NO ₂	2.3 ppm	02	7.2 ppm
Scan # 319	11:14:23	20.7 %	5.6 ppm
NO ₂	2.5 ppm	02	5.6 ppm

Standby

17

V

Standby

	Scan # 321	11:16:57	02	20.7 %	00	7.4 ppm
	NOx	2.5 ppm	02	20.7 %	00	7.4 ppm
	Scan # 322	11:16:57	02	20.7 %	00	7.5 ppm
	NOx	2.1 ppm	02	20.7 %	00	7.5 ppm
	Scan # 323	11:16:58	02	20.7 %	00	6.8 ppm
	NOx	1.9 ppm	02	20.7 %	00	6.8 ppm
	Scan # 324	11:16:58	02	20.7 %	00	6.3 ppm
	NOx	1.9 ppm	02	20.7 %	00	6.3 ppm
	Scan # 325	11:17:00	02	20.6 %	00	6.0 ppm
	NOx	1.8 ppm	02	20.6 %	00	6.0 ppm
	Scan # 326	11:17:53	02	20.6 %	00	6.2 ppm
	NOx	1.8 ppm	02	20.6 %	00	6.2 ppm
	Scan # 327	11:18:23	02	20.6 %	00	6.4 ppm
	NOx	1.5 ppm	02	20.6 %	00	6.4 ppm
	Scan # 328	11:18:53	02	20.6 %	00	7.1 ppm
	NOx	1.9 ppm	02	20.6 %	00	7.1 ppm
	Scan # 329	11:19:23	02	20.6 %	00	6.6 ppm
	NOx	1.7 ppm	02	20.6 %	00	6.6 ppm
	Scan # 330	11:19:53	02	20.6 %	00	7.2 ppm
	NOx	1.5 ppm	02	20.6 %	00	7.2 ppm
	Scan # 331	11:20:23	02	20.6 %	00	6.1 ppm
	NOx	1.4 ppm	02	20.6 %	00	6.1 ppm
	Scan # 332	11:20:53	02	20.6 %	00	6.2 ppm
	NOx	1.4 ppm	02	20.6 %	00	6.2 ppm
	Scan # 333	11:21:23	02	21.1 %	00	7.0 ppm
	NOx	6.0 ppm	02	21.1 %	00	7.0 ppm
	Scan # 334	11:21:53	02	11.2 %	00	329.1 ppm
	NOx	230.1 ppm	02	11.2 %	00	329.1 ppm
	Scan # 335	11:22:23	02	5.9 %	00	391.4 ppm
	NOx	237.7 ppm	02	5.9 %	00	391.4 ppm
	Scan # 336	11:22:53	02	5.8 %	00	390.6 ppm
	NOx	244.9 ppm	02	5.8 %	00	390.6 ppm
	Scan # 337	11:23:23	02	5.7 %	00	392.7 ppm
	NOx	248.5 ppm	02	5.7 %	00	392.7 ppm
	Scan # 338	11:23:53	02	5.7 %	00	392.7 ppm
	NOx	250.1 ppm	02	5.7 %	00	392.7 ppm
	Scan # 339	11:24:23	02	5.7 %	00	394.6 ppm
	NOx	277.6 ppm	02	5.7 %	00	394.6 ppm
	Scan # 340	11:24:53	02	5.7 %	00	393.4 ppm
	NOx	272.0 ppm	02	5.7 %	00	393.4 ppm
	Scan # 341	11:25:13	02	5.8 %	00	394.7 ppm
	NOx	269.2 ppm	02	5.8 %	00	394.7 ppm



Scan #	341	11:25:10	195.8 ppm	5.8 %	381.4 ppm
Scan #	344	11:25:50	194.8 ppm	5.8 %	381.0 ppm
Scan #	345	11:27:20	194.8 ppm	5.8 %	381.5 ppm
Scan #	346	11:27:57	191.4 ppm	5.8 %	376.5 ppm
Scan #	347	11:28:23	192.2 ppm	5.8 %	379.1 ppm
Scan #	348	11:28:57	193.9 ppm	5.8 %	381.3 ppm
Scan #	349	11:29:23	194.5 ppm	5.8 %	381.8 ppm
Scan #	350	11:29:57	202.7 ppm	5.8 %	384.7 ppm
Scan #	351	11:30:23	200.9 ppm	5.8 %	382.8 ppm
Scan #	352	11:30:53	196.8 ppm	5.8 %	380.0 ppm
Scan #	353	11:31:23	197.8 ppm	5.8 %	381.8 ppm
Scan #	354	11:31:53	196.3 ppm	5.8 %	384.0 ppm
Scan #	355	11:32:23	191.8 ppm	5.8 %	381.9 ppm
Scan #	356	11:32:57	193.4 ppm	5.8 %	384.7 ppm
Scan #	357	11:33:27	194.5 ppm	5.8 %	383.5 ppm
Scan #	358	11:33:53	193.4 ppm	5.8 %	384.5 ppm
Scan #	359	11:34:23	193.9 ppm	5.8 %	383.5 ppm
Scan #	360	11:34:57	192.2 ppm	5.8 %	383.0 ppm
Scan #	361	11:35:27	191.4 ppm	5.8 %	382.4 ppm
Scan #	362	11:35:57	191.4 ppm	5.8 %	384.7 ppm
Scan #	363	11:36:27	190.2 ppm	5.8 %	380.0 ppm

resume
add 15 min. to
sample run. 19

Scan #	367	11:37:07	02	5.8 %	00	382.0 ppm
NOx	191.2 ppm		02	5.8 %	00	382.0 ppm
Scan #	368	11:37:53	02	5.8 %	00	383.6 ppm
NOx	191.2 ppm		02	5.8 %	00	383.6 ppm
Scan #	369	11:38:20	02	5.8 %	00	384.3 ppm
NOx	191.2 ppm		02	5.8 %	00	384.3 ppm
Scan #	370	11:39:03	02	5.8 %	00	385.3 ppm
NOx	191.2 ppm		02	5.8 %	00	385.3 ppm
Scan #	371	11:39:53	02	5.8 %	00	386.4 ppm
NOx	191.2 ppm		02	5.8 %	00	386.4 ppm
Scan #	372	11:40:23	02	5.8 %	00	387.4 ppm
NOx	191.2 ppm		02	5.8 %	00	387.4 ppm
Scan #	373	11:40:53	02	5.7 %	00	388.9 ppm
NOx	201.9 ppm		02	5.7 %	00	388.9 ppm
Scan #	374	11:41:27	02	5.8 %	00	389.1 ppm
NOx	201.4 ppm		02	5.8 %	00	389.1 ppm
Scan #	375	11:42:23	02	5.8 %	00	389.2 ppm
NOx	201.6 ppm		02	5.8 %	00	389.2 ppm
Scan #	376	11:42:51	02	5.7 %	00	389.5 ppm
NOx	201.4 ppm		02	5.7 %	00	389.5 ppm
Scan #	377	11:43:23	02	5.7 %	00	389.8 ppm
NOx	201.4 ppm		02	5.7 %	00	389.8 ppm
Scan #	378	11:43:53	02	5.6 %	00	389.5 ppm
NOx	201.9 ppm		02	5.6 %	00	389.5 ppm
Scan #	379	11:44:23	02	5.7 %	00	389.5 ppm
NOx	192.1 ppm		02	5.7 %	00	389.5 ppm
Scan #	380	11:44:53	02	10.4 %	00	390.4 ppm
NOx	27.0 ppm		02	10.4 %	00	390.4 ppm
Scan #	381	11:45:23	02	19.8 %	00	389.0 ppm
NOx	11.4 ppm		02	19.8 %	00	389.0 ppm
Scan #	382	11:45:53	02	20.3 %	00	389.0 ppm
NOx	9.2 ppm		02	20.3 %	00	389.0 ppm
Scan #	383	11:46:23	02	21.0 %	00	13.4 ppm
NOx	6.2 ppm		02	21.0 %	00	13.4 ppm
Scan #	384	11:46:53	02	21.1 %	00	13.5 ppm
NOx	7.1 ppm		02	21.1 %	00	13.5 ppm
Scan #	385	11:47:23	02	21.1 %	00	13.6 ppm
NOx	7.4 ppm		02	21.1 %	00	13.6 ppm

End Run 1

Leak check
good

2

Begin system
cals

16.1% O₂

Zero

Scan # 387	11:48:10Z	0.9 ppm	02	21.0 %	02	24.8 ppm
Scan # 388	11:48:15Z	1.1 ppm	02	20.9 %	02	25.7 ppm
Scan # 389	11:48:20Z	3.5 ppm	01	20.8 %	02	26.5 ppm
Scan # 390	11:48:25Z	20.9 ppm	02	19.0 %	02	17.6 ppm
Scan # 391	11:50:10Z	10.1 ppm	02	16.4 %	02	13.8 ppm
Scan # 392	11:50:15Z	5.3 ppm	02	16.3 %	02	12.7 ppm
Scan # 393	11:51:20Z	3.7 ppm	02	16.3 %	02	12.0 ppm
Scan # 394	11:51:50Z	3.2 ppm	02	16.3 %	02	12.3 ppm
Scan # 395	11:52:20Z	2.5 ppm	02	16.3 %	02	11.2 ppm
Scan # 396	11:52:50Z	1.5 ppm	02	16.3 %	02	12.2 ppm
Scan # 397	11:53:20Z	2.4 ppm	02	17.6 %	02	11.8 ppm
Scan # 398	11:53:50Z	1.8 ppm	02	20.6 %	02	11.8 ppm
Scan # 399	11:54:20Z	1.3 ppm	02	20.7 %	02	4.0 ppm
Scan # 400	11:54:50Z	1.2 ppm	02	20.7 %	02	4.0 ppm
Scan # 401	11:55:20Z	2.4 ppm	02	20.7 %	02	4.9 ppm
Scan # 402	11:55:50Z	1.1 ppm	02	20.7 %	02	4.1 ppm
Scan # 403	11:56:20Z	1.1 ppm	02	20.7 %	02	4.4 ppm
Scan # 404	11:56:50Z	1.6 ppm	02	20.7 %	02	4.3 ppm
Scan # 405	11:57:20Z	1.1 ppm	02	20.7 %	02	4.5 ppm
Scan # 406	11:57:50Z	1.1 ppm	02	20.7 %	02	4.8 ppm
Scan # 407	11:58:20Z	1.2 ppm	02	16.4 %	02	404.4 ppm
Scan # 408	11:58:50Z					

Scan # 400	11:59:27	NOx	0.7 ppm	00	0.1 %	00	489.0 ppm
Scan # 410	12:00:50	NOx	0.9 ppm	00	0.1 %	00	489.4 ppm
Scan # 411	12:00:27	NOx	0.9 ppm	00	0.1 %	00	489.9 ppm
Scan # 412	12:00:53	NOx	0.9 ppm	00	0.1 %	00	489.5 ppm
Scan # 413	12:01:20	NOx	1.3 ppm	00	0.1 %	00	487.6 ppm
Scan # 414	12:01:52	NOx	207.7 ppm	00	1.2 %	00	13.6 ppm
Scan # 415	12:02:23	NOx	221.2 ppm	00	0.1 %	00	6.0 ppm
Scan # 416	12:02:53	NOx	223.4 ppm	00	0.1 %	00	6.4 ppm
Scan # 417	12:03:23	NOx	222.9 ppm	00	0.1 %	00	5.9 ppm
Scan # 418	12:03:53	NOx	240.3 ppm	00	0.1 %	00	6.6 ppm
Scan # 419	12:04:23	NOx	239.8 ppm	00	0.1 %	00	6.4 ppm
Scan # 420	12:04:53	NOx	239.3 ppm	00	0.0 %	00	6.7 ppm
Scan # 421	12:05:23	NOx	238.6 ppm	00	0.0 %	00	6.3 ppm
Scan # 422	12:05:53	NOx	239.5 ppm	00	0.0 %	00	6.5 ppm
Scan # 423	12:06:23	NOx	60.2 ppm	00	11.9 %	00	7.4 ppm
Scan # 424	12:06:53	NOx	2.9 ppm	00	21.0 %	00	7.3 ppm
Scan # 425	12:07:23	NOx	2.0 ppm	00	21.2 %	00	7.7 ppm
Scan # 426	12:07:53	NOx	2.2 ppm	00	21.2 %	00	7.3 ppm
Scan # 427	12:08:23	NOx	1.9 ppm	00	21.2 %	00	6.5 ppm
Scan # 428	12:08:53	NOx	165.7 ppm	00	16.0 %	00	203.7 ppm
Scan # 429	12:09:23	NOx	193.2 ppm	00	6.1 %	00	376.1 ppm

487.0 ppm CO
O₂ zero

22

242.0 ppm NO

Scan # 431	12:10:27				
NOx	207.9 ppm	01	5.8 %	00	376.9 ppm
Scan # 432	12:10:57				
NOx	209.3 ppm	02	5.8 %	00	376.2 ppm
Scan # 433	12:11:27				
NOx	201.4 ppm	01	5.8 %	01	377.4 ppm
Scan # 434	12:11:57				
NOx	207.8 ppm	02	5.8 %	00	376.6 ppm
Scan # 435	12:12:27				
NOx	207.6 ppm	02	5.8 %	00	375.4 ppm
Scan # 436	12:12:57				
NOx	214.0 ppm	02	5.8 %	00	378.0 ppm
Scan # 437	12:13:27				
NOx	206.3 ppm	02	5.8 %	00	377.8 ppm
Scan # 438	12:13:57				
NOx	207.8 ppm	01	5.8 %	00	375.6 ppm
Scan # 439	12:14:27				
NOx	208.5 ppm	02	5.9 %	00	376.3 ppm
Scan # 440	12:14:57				
NOx	200.1 ppm	02	5.8 %	00	372.3 ppm
Scan # 441	12:15:27				
NOx	201.7 ppm	02	5.8 %	00	377.6 ppm
Scan # 442	12:15:57				
NOx	199.6 ppm	02	5.9 %	00	375.3 ppm
Scan # 443	12:16:27				
NOx	198.2 ppm	02	5.8 %	00	373.9 ppm
Scan # 444	12:16:57				
NOx	198.7 ppm	01	5.8 %	00	375.1 ppm
Scan # 445	12:17:27				
NOx	200.9 ppm	02	5.8 %	00	377.8 ppm
Scan # 446	12:17:57				
NOx	200.4 ppm	02	5.8 %	00	374.9 ppm
Scan # 447	12:18:27				
NOx	201.4 ppm	02	5.8 %	00	370.5 ppm
Scan # 448	12:18:57				
NOx	204.8 ppm	02	5.8 %	00	376.0 ppm
Scan # 449	12:19:27				
NOx	205.1 ppm	02	5.8 %	00	378.1 ppm
Scan # 450	12:19:57				
NOx	201.4 ppm	01	5.8 %	00	375.6 ppm
Scan # 451	12:20:27				
NOx	198.3 ppm	02	5.8 %	00	374.9 ppm

Begin Run 2

Scan # 453	12:21:23				
NOx	195.9 ppm	02	5.8 %	00	373.7 ppm
Scan # 454	12:21:53				
NOx	202.4 ppm	02	5.8 %	01	374.3 ppm
Scan # 455	12:22:23				
NOx	203.4 ppm	02	5.8 %	00	375.5 ppm
Scan # 456	12:22:53				
NOx	204.4 ppm	02	5.9 %	00	375.2 ppm
Scan # 457	12:23:23				
NOx	195.1 ppm	02	5.8 %	01	373.9 ppm
Scan # 458	12:23:53				
NOx	197.4 ppm	02	5.9 %	00	373.4 ppm
Scan # 459	12:24:23				
NOx	200.9 ppm	02	5.8 %	00	377.4 ppm
Scan # 460	12:24:53				
NOx	199.2 ppm	02	5.8 %	00	374.2 ppm
Scan # 461	12:25:23				
NOx	211.2 ppm	02	5.8 %	00	375.9 ppm
Scan # 462	12:25:53				
NOx	206.1 ppm	02	5.8 %	00	377.1 ppm
Scan # 463	12:26:23				
NOx	200.0 ppm	02	5.9 %	00	377.2 ppm
Scan # 464	12:26:53				
NOx	206.7 ppm	02	5.8 %	00	378.9 ppm
Scan # 465	12:27:23				
NOx	206.9 ppm	02	5.8 %	00	376.7 ppm
Scan # 466	12:27:53				
NOx	206.3 ppm	02	5.8 %	00	376.5 ppm
Scan # 467	12:28:23				
NOx	203.1 ppm	02	5.8 %	00	377.1 ppm
Scan # 468	12:28:53				
NOx	214.7 ppm	02	5.8 %	00	379.0 ppm
Scan # 469	12:29:23				
NOx	201.9 ppm	02	5.8 %	00	377.3 ppm
Scan # 470	12:29:53				
NOx	202.9 ppm	02	5.8 %	00	374.8 ppm
Scan # 471	12:30:23				
NOx	203.1 ppm	02	5.9 %	00	377.8 ppm
Scan # 472	12:30:53				
NOx	200.5 ppm	02	5.8 %	00	373.5 ppm
Scan # 473	12:31:23				
NOx	195.5 ppm	02	5.8 %	00	375.6 ppm

Scan # 470	12:32:27	NOx	199.4 ppm	02	5.8 %	CO	377.3 ppm
Scan # 471	12:32:53	NOx	203.9 ppm	02	5.8 %	CO	378.0 ppm
Scan # 472	12:33:23	NOx	205.7 ppm	02	5.8 %	CO	378.4 ppm
Scan # 473	12:33:53	NOx	200.4 ppm	02	5.8 %	CO	376.2 ppm
Scan # 474	12:34:23	NOx	197.7 ppm	02	5.8 %	CO	373.9 ppm
Scan # 475	12:34:53	NOx	198.6 ppm	02	5.8 %	CO	376.7 ppm
Scan # 476	12:35:23	NOx	195.5 ppm	02	5.8 %	CO	374.8 ppm
Scan # 477	12:35:53	NOx	202.5 ppm	02	5.8 %	CO	375.9 ppm
Scan # 478	12:36:23	NOx	203.7 ppm	02	5.8 %	CO	376.9 ppm
Scan # 479	12:36:53	NOx	201.8 ppm	02	5.8 %	CO	373.4 ppm
Scan # 480	12:37:23	NOx	199.1 ppm	02	5.8 %	CO	375.8 ppm
Scan # 481	12:37:53	NOx	207.4 ppm	02	5.8 %	CO	378.5 ppm
Scan # 482	12:38:23	NOx	206.1 ppm	02	5.8 %	CO	377.5 ppm
Scan # 483	12:38:53	NOx	211.5 ppm	02	5.8 %	CO	376.3 ppm
Scan # 484	12:39:23	NOx	203.1 ppm	02	5.8 %	CO	377.6 ppm
Scan # 485	12:39:53	NOx	205.3 ppm	02	5.8 %	CO	376.5 ppm
Scan # 486	12:40:23	NOx	208.3 ppm	02	5.8 %	CO	377.1 ppm
Scan # 487	12:40:53	NOx	214.5 ppm	02	5.8 %	CO	377.3 ppm
Scan # 488	12:41:23	NOx	211.4 ppm	02	5.8 %	CO	379.3 ppm
Scan # 489	12:41:53	NOx	205.7 ppm	02	5.8 %	CO	375.7 ppm
Scan # 490	12:42:23	NOx	201.3 ppm	02	5.8 %	CO	376.5 ppm
Scan # 491	12:42:53	NOx					

Scan # 499	12:43:23				
NO _x	210.1 ppm	02	5.8 %	00	375.8 ppm
Scan # 498	12:43:53				
NO _x	209.3 ppm	01	5.8 %	00	376.7 ppm
Scan # 499	12:44:23				
NO _x	209.5 ppm	02	5.8 %	00	375.3 ppm
Scan # 500	12:44:53				
NO _x	211.9 ppm	02	5.8 %	00	375.1 ppm
Scan # 501	12:45:23				
NO _x	209.4 ppm	02	5.8 %	00	376.6 ppm
Scan # 502	12:45:53				
NO _x	215.9 ppm	02	5.8 %	00	375.2 ppm
Scan # 503	12:46:23				
NO _x	209.3 ppm	02	5.8 %	00	376.5 ppm
Scan # 504	12:46:53				
NO _x	216.0 ppm	02	5.8 %	00	380.8 ppm
Scan # 505	12:47:23				
NO _x	211.4 ppm	02	5.8 %	00	380.6 ppm
Scan # 506	12:47:53				
NO _x	215.3 ppm	01	5.8 %	00	378.3 ppm
Scan # 507	12:48:23				
NO _x	205.4 ppm	02	5.8 %	00	375.1 ppm
Scan # 508	12:48:53				
NO _x	209.9 ppm	02	5.8 %	00	377.6 ppm
Scan # 509	12:49:23				
NO _x	201.6 ppm	02	5.8 %	00	376.1 ppm
Scan # 510	12:49:53				
NO _x	206.0 ppm	02	5.8 %	00	377.5 ppm
Scan # 511	12:50:23				
NO _x	205.6 ppm	02	5.8 %	00	375.8 ppm
Scan # 512	12:50:53				
NO _x	201.0 ppm	02	5.8 %	00	374.5 ppm
Scan # 513	12:51:23				
NO _x	201.3 ppm	02	5.8 %	00	376.4 ppm
Scan # 514	12:51:53				
NO _x	206.8 ppm	02	5.8 %	00	374.5 ppm
Scan # 515	12:52:23				
NO _x	207.5 ppm	02	5.8 %	00	372.8 ppm
Scan # 516	12:52:53				
NO _x	207.8 ppm	02	5.8 %	00	374.8 ppm
Scan # 517	12:53:23				
NO _x	214.3 ppm	01	5.8 %	01	377.8 ppm

Scan #	519	12:54:23				
NO _x	210.9 ppm	02	5.8 %	00	373.8 ppm	
Scan #	520	12:54:57				
NO _x	212.2 ppm	02	5.8 %	00	372.9 ppm	
Scan #	521	12:55:23				
NO _x	208.1 ppm	01	5.8 %	00	378.8 ppm	
Scan #	522	12:55:53				
NO _x	209.4 ppm	02	5.8 %	00	376.2 ppm	
Scan #	523	12:56:23				
NO _x	209.3 ppm	02	5.8 %	00	376.3 ppm	
Scan #	524	12:56:50				
NO _x	211.2 ppm	02	5.8 %	00	373.7 ppm	
Scan #	525	12:57:23				
NO _x	209.8 ppm	02	5.8 %	00	375.7 ppm	
Scan #	526	12:57:53				
NO _x	209.4 ppm	02	5.8 %	00	373.4 ppm	
Scan #	527	12:58:23				
NO _x	198.8 ppm	02	5.9 %	00	374.9 ppm	
Scan #	528	12:58:53				
NO _x	191.4 ppm	02	5.8 %	00	371.7 ppm	
Scan #	529	12:59:23				
NO _x	201.6 ppm	02	5.8 %	00	374.7 ppm	
Scan #	530	12:59:57				
NO _x	198.5 ppm	02	5.8 %	00	374.5 ppm	
Scan #	531	13:00:27				
NO _x	203.4 ppm	02	5.8 %	00	375.9 ppm	
Scan #	532	13:01:53				
NO _x	210.2 ppm	02	5.8 %	00	376.5 ppm	
Scan #	533	13:02:23				
NO _x	213.5 ppm	02	5.8 %	00	374.1 ppm	
Scan #	534	13:02:57				
NO _x	192.8 ppm	01	5.8 %	00	371.0 ppm	
Scan #	535	13:03:27				
NO _x	199.4 ppm	02	5.8 %	00	375.7 ppm	
Scan #	536	13:03:53				
NO _x	199.8 ppm	01	5.8 %	00	375.9 ppm	
Scan #	537	13:04:27				
NO _x	189.2 ppm	02	5.9 %	00	372.6 ppm	
Scan #	538	13:04:57				
NO _x	196.7 ppm	01	5.9 %	00	372.0 ppm	
Scan #	539	13:05:27				
NO _x	197.4 ppm	01	5.9 %	00	372.3 ppm	

Scan # 541	13:06:23				
NOx	191.9 ppm	02	5.9 %	00	371.2 ppm
Scan # 542	13:06:53				
NOx	192.3 ppm	02	5.9 %	00	372.0 ppm
Scan # 543	13:06:27				
NOx	193.4 ppm	02	5.9 %	00	371.7 ppm
Scan # 544	13:06:53				
NOx	196.4 ppm	02	5.9 %	00	375.2 ppm
Scan # 545	13:07:23				
NOx	192.4 ppm	02	5.9 %	00	371.4 ppm
Scan # 546	13:07:53				
NOx	197.7 ppm	02	5.9 %	00	373.6 ppm
Scan # 547	13:08:23				
NOx	194.4 ppm	02	5.9 %	00	372.5 ppm
Scan # 548	13:08:53				
NOx	204.7 ppm	02	5.9 %	00	373.9 ppm
Scan # 549	13:09:23				
NOx	191.2 ppm	02	5.9 %	00	371.0 ppm
Scan # 550	13:09:53				
NOx	198.0 ppm	02	5.9 %	00	372.8 ppm
Scan # 551	13:10:23				
NOx	190.9 ppm	02	5.9 %	00	372.3 ppm
Scan # 552	13:10:53				
NOx	193.7 ppm	02	5.9 %	00	370.8 ppm
Scan # 553	13:11:23				
NOx	191.1 ppm	02	5.9 %	00	372.5 ppm
Scan # 554	13:11:53				
NOx	192.3 ppm	02	5.9 %	00	373.6 ppm
Scan # 555	13:12:23				
NOx	187.8 ppm	02	5.9 %	00	372.0 ppm
Scan # 556	13:12:53				
NOx	195.3 ppm	02	5.9 %	00	371.7 ppm
Scan # 557	13:13:23				
NOx	193.2 ppm	02	5.9 %	00	372.1 ppm
Scan # 558	13:13:53				
NOx	182.9 ppm	02	5.9 %	00	373.5 ppm
Scan # 559	13:14:23				
NOx	193.2 ppm	02	5.9 %	00	370.0 ppm
Scan # 560	13:14:53				
NOx	197.0 ppm	02	5.9 %	00	371.0 ppm
Scan # 561	13:15:23				
NOx	187.1 ppm	02	5.9 %	00	369.8 ppm

End Run 2

Scan # 567	13:16:23				
NO _x	195.5 ppm	01	5.9 %	00	374.4 ppm
Scan # 568	13:16:53				
NO _x	200.4 ppm	01	5.8 %	00	375.5 ppm
Scan # 569	13:17:27				
NO _x	215.2 ppm	02	5.9 %	00	375.4 ppm
Scan # 570	13:17:53				
NO _x	214.5 ppm	02	5.8 %	00	377.8 ppm
Scan # 571	13:18:23				
NO _x	205.3 ppm	01	5.9 %	00	374.7 ppm
Scan # 572	13:18:53				
NO _x	210.5 ppm	02	5.8 %	00	375.3 ppm
Scan # 573	13:19:23				
NO _x	209.3 ppm	02	5.9 %	00	373.3 ppm
Scan # 574	13:19:53				
NO _x	210.4 ppm	01	5.8 %	00	374.8 ppm
Scan # 575	13:20:23				
NO _x	203.8 ppm	02	5.9 %	00	375.1 ppm
Scan # 576	13:20:53				
NO _x	205.2 ppm	02	5.8 %	00	377.8 ppm
Scan # 577	13:21:23				
NO _x	215.5 ppm	02	5.8 %	00	377.8 ppm
Scan # 578	13:21:53				
NO _x	214.1 ppm	02	5.8 %	00	375.0 ppm
Scan # 579	13:22:23				
NO _x	213.2 ppm	02	5.8 %	00	377.5 ppm
Scan # 580	13:22:53				
NO _x	219.9 ppm	01	5.8 %	00	375.3 ppm
Scan # 581	13:23:23				
NO _x	215.1 ppm	01	5.8 %	00	376.4 ppm
Scan # 582	13:23:53				
NO _x	220.2 ppm	02	5.8 %	00	376.9 ppm
Scan # 583	13:24:23				
NO _x	184.6 ppm	01	6.8 %	00	323.9 ppm
Scan # 584	13:24:53				
NO _x	19.3 ppm	02	20.3 %	00	9.6 ppm
Scan # 585	13:25:23				
NO _x	13.4 ppm	02	21.1 %	00	2.3 ppm
Scan # 586	13:25:53				
NO _x	13.6 ppm	01	21.1 %	00	1.9 ppm
Scan # 587	13:26:23				
NO _x	13.8 ppm	02	21.1 %	00	4.8 ppm

Begin system
calls

Station # 585	13:17:27				
NO ₂	8.9 ppm	02	21.1 %	00	4.1 ppm
Station # 586	13:27:57				
NO ₂	6.7 ppm	02	21.1 %	00	3.7 ppm
Station # 587	13:28:20				
NO ₂	26.8 ppm	02	21.2 %	00	4.7 ppm
Station # 588	13:28:53				
NO ₂	9.1 ppm	02	20.7 %	01	0.8 ppm
Station # 589	13:29:23				
NO ₂	6.7 ppm	02	20.7 %	00	0.3 ppm
Station # 590	13:29:53				
NO ₂	5.8 ppm	02	20.7 %	00	-0.3 ppm
Station # 591	13:30:23				
NO ₂	5.0 ppm	02	20.7 %	00	1.3 ppm
Station # 592	13:30:53				
NO ₂	4.3 ppm	02	20.7 %	00	1.8 ppm
Station # 593	13:31:22				
NO ₂	3.9 ppm	02	20.7 %	00	0.8 ppm
Station # 594	13:31:53				
NO ₂	3.8 ppm	01	20.7 %	00	1.7 ppm
Station # 595	13:32:23				
NO ₂	3.4 ppm	02	20.7 %	00	1.4 ppm
Station # 596	13:32:51				
NO ₂	2.8 ppm	02	20.7 %	00	1.4 ppm
Station # 597	13:33:23				
NO ₂	3.2 ppm	02	20.7 %	00	1.4 ppm
Station # 598	13:33:53				
NO ₂	3.0 ppm	01	20.7 %	01	1.6 ppm
Station # 599	13:34:23				
NO ₂	3.8 ppm	02	20.7 %	00	1.3 ppm
Station # 600	13:34:53				
NO ₂	3.8 ppm	00	20.8 %	00	3.7 ppm
Station # 601	13:35:23				
NO ₂	3.5 ppm	01	16.5 %	00	2.7 ppm
Station # 602	13:35:53				
NO ₂	3.4 ppm	02	16.7 %	00	2.5 ppm
Station # 603	13:36:23				
NO ₂	3.0 ppm	02	16.3 %	00	2.9 ppm
Station # 604	13:36:53				
NO ₂	3.8 ppm	01	16.3 %	01	2.6 ppm
Station # 605	13:37:23				
NO ₂	2.8 ppm	02	16.3 %	00	2.7 ppm

check check
good

30

✓

zero

16.1 % O₂

Scan # 607	13:38:27				
NO _x	2.2 ppm	02	10.3 %	00	302.4 ppm
Scan # 608	13:38:53				
NO _x	2.2 ppm	02	0.3 %	00	487.4 ppm
Scan # 609	13:39:20				
NO _x	2.4 ppm	02	0.1 %	00	489.6 ppm
Scan # 610	13:39:52				
NO _x	2.2 ppm	02	0.1 %	00	488.9 ppm
Scan # 611	13:40:22				
NO _x	2.2 ppm	02	0.1 %	00	489.1 ppm
Scan # 612	13:41:02				
NO _x	2.3 ppm	02	0.1 %	00	489.4 ppm
Scan # 613	13:41:23				
NO _x	2.2 ppm	02	0.1 %	00	490.1 ppm
Scan # 614	13:41:52				
NO _x	60.5 ppm	02	6.9 %	00	163.8 ppm
Scan # 615	13:42:22				
NO _x	242.9 ppm	02	0.3 %	00	4.2 ppm
Scan # 616	13:42:52				
NO _x	247.9 ppm	02	0.1 %	00	2.9 ppm
Scan # 617	13:43:22				
NO _x	247.6 ppm	02	0.1 %	00	2.4 ppm
Scan # 618	13:43:52				
NO _x	249.8 ppm	02	0.1 %	00	1.9 ppm
Scan # 619	13:44:22				
NO _x	247.0 ppm	02	0.1 %	00	1.0 ppm
Scan # 620	13:44:52				
NO _x	249.8 ppm	02	0.1 %	00	2.1 ppm
Scan # 621	13:45:22				
NO _x	43.0 ppm	02	15.2 %	00	3.1 ppm
Scan # 622	13:45:52				
NO _x	4.2 ppm	02	21.1 %	00	1.9 ppm
Scan # 623	13:46:22				
NO _x	3.7 ppm	02	21.2 %	00	1.6 ppm
Scan # 624	13:46:52				
NO _x	3.2 ppm	02	21.2 %	00	2.3 ppm
Scan # 625	13:47:22				
NO _x	3.2 ppm	02	21.2 %	00	2.3 ppm
Scan # 626	13:47:52				
NO _x	3.3 ppm	02	21.2 %	00	1.6 ppm
Scan # 627	13:48:22				
NO _x	1.9 ppm	02	21.2 %	00	1.4 ppm
Scan # 628	13:48:52				

487.0 ppm CO
O₂ zero

242.0 ppm NO

Scan # 639	17:49:02				
NO _x	3.0 ppm	02	21.2 %	00	1.2 ppm
Scan # 640	17:49:52				
NO _x	2.9 ppm	02	21.2 %	00	1.5 ppm
Scan # 641	17:50:02				
NO _x	3.2 ppm	02	21.2 %	00	1.7 ppm
Scan # 642	17:50:52				
NO _x	2.9 ppm	02	21.2 %	00	1.4 ppm
Scan # 643	17:51:02				
NO _x	3.0 ppm	02	21.2 %	00	1.6 ppm
Scan # 644	17:51:51				
NO _x	3.3 ppm	02	21.2 %	00	1.4 ppm
Scan # 645	17:52:02				
NO _x	2.6 ppm	02	21.2 %	00	1.2 ppm
Scan # 646	17:52:52				
NO _x	2.9 ppm	02	21.2 %	00	1.9 ppm
Scan # 647	17:53:22				
NO _x	2.6 ppm	02	21.2 %	00	0.5 ppm
Scan # 648	17:53:52				
NO _x	2.4 ppm	02	21.2 %	00	1.6 ppm
Scan # 649	17:54:22				
NO _x	2.5 ppm	02	21.2 %	00	1.8 ppm
Scan # 650	17:54:51				
NO _x	2.5 ppm	02	21.2 %	00	1.0 ppm
Scan # 651	17:55:01				
NO _x	2.4 ppm	02	21.2 %	00	1.1 ppm
Scan # 652	17:55:51				
NO _x	2.1 ppm	02	21.2 %	00	1.0 ppm
Scan # 653	17:56:22				
NO _x	2.5 ppm	02	21.3 %	00	1.1 ppm
Scan # 654	17:56:52				
NO _x	2.1 ppm	02	21.3 %	00	1.6 ppm
Scan # 655	17:57:22				
NO _x	1.9 ppm	02	21.2 %	00	1.1 ppm
Scan # 656	17:57:52				
NO _x	35.3 ppm	02	21.0 %	00	22.2 ppm
Scan # 657	17:58:02				
NO _x	211.4 ppm	02	6.4 %	00	374.2 ppm
Scan # 658	17:58:51				
NO _x	210.4 ppm	02	5.9 %	00	361.2 ppm
Scan # 659	17:59:01				
NO _x	204.2 ppm	02	5.9 %	01	377.5 ppm

Scan # 651	14:00:21				
NO ₂	205.9 ppm	02	5.9 %	00	375.3 ppm
Scan # 652	14:00:52				
NO ₂	215.2 ppm	02	5.9 %	00	376.6 ppm
Scan # 653	14:01:22				
NO ₂	215.9 ppm	01	5.9 %	00	377.8 ppm
Scan # 654	14:01:52				
NO ₂	221.5 ppm	02	5.9 %	00	380.1 ppm
Scan # 655	14:02:22				
NO ₂	224.2 ppm	02	5.8 %	00	379.1 ppm
Scan # 656	14:02:52				
NO ₂	223.2 ppm	01	5.8 %	00	379.9 ppm
Scan # 657	14:03:22				
NO ₂	220.9 ppm	02	5.8 %	00	380.0 ppm
Scan # 658	14:03:52				
NO ₂	219.2 ppm	02	5.8 %	00	380.3 ppm
Scan # 659	14:04:22				
NO ₂	218.4 ppm	02	5.8 %	00	380.7 ppm
Scan # 660	14:04:52				
NO ₂	225.4 ppm	02	5.8 %	00	380.5 ppm
Scan # 661	14:05:22				
NO ₂	224.4 ppm	02	5.8 %	00	379.7 ppm
Scan # 662	14:05:52				
NO ₂	208.1 ppm	02	5.8 %	00	375.4 ppm
Scan # 663	14:06:22				
NO ₂	185.2 ppm	02	6.0 %	00	370.5 ppm
Scan # 664	14:06:52				
NO ₂	185.0 ppm	02	5.9 %	00	371.3 ppm
Scan # 665	14:07:22				
NO ₂	180.5 ppm	01	6.0 %	00	371.0 ppm
Scan # 666	14:07:52				
NO ₂	161.9 ppm	02	5.9 %	00	372.1 ppm
Scan # 667	14:08:22				
NO ₂	178.4 ppm	02	5.9 %	00	370.1 ppm
Scan # 668	14:08:52				
NO ₂	196.5 ppm	02	5.9 %	00	374.7 ppm
Scan # 669	14:09:22				
NO ₂	183.2 ppm	02	5.9 %	00	372.6 ppm
Scan # 670	14:09:52				
NO ₂	201.8 ppm	02	5.9 %	00	373.2 ppm
Scan # 671	14:10:22				
NO ₂	187.8 ppm	02	5.9 %	00	374.7 ppm

Begin
Run 3

Scan # 670	14:11:11				
NO ₂	187.0 ppm	01	5.9 %	01	370.1 ppm
Scan # 671	14:11:51				
NO ₂	203.1 ppm	01	5.9 %	00	370.9 ppm
Scan # 672	14:12:17				
NO ₂	178.0 ppm	00	5.0 %	00	368.4 ppm
Scan # 673	14:12:52				
NO ₂	191.2 ppm	00	5.9 %	00	373.4 ppm
Scan # 677	14:13:10				
NO ₂	187.9 ppm	00	5.9 %	00	374.3 ppm
Scan # 678	14:13:33				
NO ₂	201.7 ppm	01	5.8 %	00	374.3 ppm
Scan # 679	14:14:01				
NO ₂	187.6 ppm	01	5.9 %	00	371.3 ppm
Scan # 680	14:14:52				
NO ₂	207.5 ppm	00	5.8 %	01	376.1 ppm
Scan # 681	14:15:22				
NO ₂	191.2 ppm	00	5.9 %	00	375.2 ppm
Scan # 681	14:15:52				
NO ₂	211.0 ppm	00	5.8 %	00	378.2 ppm
Scan # 683	14:16:22				
NO ₂	209.5 ppm	00	5.8 %	00	374.3 ppm
Scan # 684	14:16:51				
NO ₂	224.3 ppm	01	5.8 %	00	378.0 ppm
Scan # 685	14:17:22				
NO ₂	221.4 ppm	00	5.8 %	00	381.2 ppm
Scan # 686	14:17:51				
NO ₂	217.7 ppm	01	5.7 %	00	380.7 ppm
Scan # 687	14:18:23				
NO ₂	211.2 ppm	00	5.8 %	00	376.2 ppm
Scan # 688	14:18:52				
NO ₂	221.4 ppm	00	5.8 %	00	379.7 ppm
Scan # 689	14:19:11				
NO ₂	211.4 ppm	01	5.8 %	00	378.9 ppm
Scan # 690	14:19:51				
NO ₂	231.1 ppm	01	5.8 %	00	382.5 ppm
Scan # 691	14:20:22				
NO ₂	211.3 ppm	00	5.8 %	00	378.6 ppm
Scan # 692	14:21:51				
NO ₂	211.0 ppm	01	5.7 %	01	378.3 ppm
Scan # 693	14:22:11				
NO ₂	211.1 ppm	00	5.8 %	01	378.0 ppm

Star # 690	14:20:12	218.4 ppm	02	5.8 %	00	375.4 ppm
Star # 690	14:20:52	218.8 ppm	01	5.8 %	00	375.3 ppm
Star # 697	14:20:12	218.4 ppm	02	5.8 %	01	374.3 ppm
Star # 698	14:20:52	222.9 ppm	01	5.8 %	00	375.4 ppm
Star # 699	14:24:21	215.1 ppm	02	5.8 %	00	375.3 ppm
Star # 700	14:24:51	221.3 ppm	02	5.8 %	00	377.4 ppm
Star # 701	14:25:22	209.1 ppm	02	5.8 %	00	374.9 ppm
Star # 702	14:25:52	224.7 ppm	01	5.8 %	00	377.5 ppm
Star # 703	14:26:22	219.1 ppm	02	5.8 %	01	373.2 ppm
Star # 704	14:26:52	201.7 ppm	01	5.7 %	00	376.0 ppm
Star # 705	14:27:22	121.6 ppm	01	5.8 %	00	376.2 ppm
Star # 706	14:27:52	230.1 ppm	02	5.7 %	00	378.3 ppm
Star # 707	14:28:22	203.0 ppm	01	5.8 %	00	375.8 ppm
Star # 708	14:28:51	181.8 ppm	01	5.7 %	00	377.3 ppm
Star # 709	14:29:22	215.7 ppm	02	5.8 %	00	379.3 ppm
Star # 710	14:29:51	129.2 ppm	02	5.8 %	00	374.7 ppm
Star # 711	14:30:22	210.6 ppm	02	5.8 %	00	372.9 ppm
Star # 712	14:30:52	220.4 ppm	02	5.7 %	00	376.2 ppm
Star # 713	14:31:22	211.2 ppm	02	5.8 %	00	373.2 ppm
Star # 714	14:31:51	211.8 ppm	01	5.8 %	01	375.4 ppm
Star # 715	14:32:21	201.1 ppm	01	5.8 %	01	371.1 ppm

Scan # 717	14:33:21				
Alt	213.1 ppm	02	5.8 %	00	371.7 ppm
Scan # 718	14:33:51				
Alt	213.7 ppm	02	5.7 %	00	377.1 ppm
Scan # 719	14:34:21				
Alt	210.1 ppm	01	5.8 %	00	372.8 ppm
Scan # 720	14:34:51				
Alt	222.3 ppm	02	5.8 %	00	374.2 ppm
Scan # 721	14:35:21				
Alt	196.4 ppm	01	5.9 %	00	374.6 ppm
Scan # 722	14:35:52				
Alt	192.5 ppm	02	5.9 %	00	375.5 ppm
Scan # 723	14:36:21				
Alt	182.6 ppm	02	6.0 %	00	377.9 ppm
Scan # 724	14:36:52				
Alt	215.4 ppm	02	5.9 %	00	378.2 ppm
Scan # 725	14:37:22				
Alt	193.7 ppm	02	5.9 %	00	372.5 ppm
Scan # 726	14:37:52				
Alt	193.1 ppm	01	5.9 %	00	373.1 ppm
Scan # 727	14:38:22				
Alt	185.1 ppm	02	5.9 %	00	370.2 ppm
Scan # 728	14:38:51				
Alt	197.5 ppm	02	5.9 %	00	368.5 ppm
Scan # 729	14:39:21				
Alt	187.6 ppm	02	5.9 %	00	368.4 ppm
Scan # 730	14:39:51				
Alt	201.1 ppm	01	5.9 %	00	370.2 ppm
Scan # 731	14:40:21				
Alt	197.2 ppm	01	5.9 %	00	371.7 ppm
Scan # 732	14:40:51				
Alt	193.8 ppm	02	5.9 %	00	370.8 ppm
Scan # 733	14:41:21				
Alt	190.8 ppm	02	5.9 %	00	369.0 ppm
Scan # 734	14:41:51				
Alt	188.8 ppm	02	5.9 %	00	372.4 ppm
Scan # 735	14:42:21				
Alt	175.7 ppm	01	6.0 %	00	369.8 ppm
Scan # 736	14:42:51				
Alt	177.0 ppm	01	6.0 %	00	371.3 ppm
Scan # 737	14:43:21				
Alt	171.5 ppm	02	6.0 %	00	370.1 ppm

Scan # 739	14:44:12			
NDx	171.7 ppm	02	6.0 %	367.5 ppm
Scan # 740	14:44:51			
NDx	180.4 ppm	01	5.9 %	370.9 ppm
Scan # 741	14:45:11			
NDx	176.5 ppm	02	6.0 %	365.5 ppm
Scan # 742	14:45:52			
NDx	180.6 ppm	01	5.9 %	365.7 ppm
Scan # 743	14:46:12			
NDx	171.1 ppm	01	6.0 %	367.6 ppm
Scan # 744	14:46:51			
NDx	180.6 ppm	02	6.0 %	365.1 ppm
Scan # 745	14:47:22			
NDx	174.4 ppm	02	6.0 %	367.8 ppm
Scan # 746	14:47:51			
NDx	180.4 ppm	01	6.0 %	366.4 ppm
Scan # 747	14:48:22			
NDx	177.4 ppm	02	6.0 %	369.1 ppm
Scan # 748	14:48:52			
NDx	177.9 ppm	02	6.0 %	368.5 ppm
Scan # 749	14:49:22			
NDx	173.4 ppm	02	6.0 %	369.3 ppm
Scan # 750	14:49:52			
NDx	182.5 ppm	02	5.7 %	368.0 ppm
Scan # 751	14:50:22			
NDx	185.2 ppm	01	6.0 %	365.5 ppm
Scan # 752	14:50:52			
NDx	181.8 ppm	02	6.0 %	370.0 ppm
Scan # 753	14:51:22			
NDx	173.1 ppm	02	6.0 %	367.4 ppm
Scan # 754	14:51:52			
NDx	174.3 ppm	02	6.0 %	365.0 ppm
Scan # 755	14:52:22			
NDx	167.1 ppm	02	6.0 %	365.5 ppm
Scan # 756	14:52:52			
NDx	174.2 ppm	02	6.0 %	367.2 ppm
Scan # 757	14:53:21			
NDx	163.1 ppm	02	6.0 %	369.8 ppm
Scan # 758	14:53:51			
NDx	167.1 ppm	01	6.0 %	365.5 ppm
Scan # 759	14:54:21			
NDx	163.7 ppm	01	6.0 %	364.5 ppm

Star # 761	14:55:00				
NO	164.8 ppm	02	6.0 %	01	365.3 ppm
Star # 762	14:55:50				
NO	170.4 ppm	02	6.0 %	00	365.0 ppm
Star # 763	14:56:21				
NO	169.6 ppm	02	6.0 %	01	368.8 ppm
Star # 764	14:56:50				
NO	172.9 ppm	02	6.0 %	01	367.6 ppm
Star # 765	14:57:22				
NO	166.3 ppm	02	6.1 %	00	366.9 ppm
Star # 766	14:57:51				
NO	171.6 ppm	01	6.0 %	00	368.1 ppm
Star # 767	14:58:22				
NO	169.5 ppm	02	6.0 %	00	368.6 ppm
Star # 768	14:58:52				
NO	169.5 ppm	02	6.0 %	00	367.3 ppm
Star # 769	14:59:22				
NO	166.3 ppm	02	6.0 %	00	364.7 ppm
Star # 770	14:59:52				
NO	169.5 ppm	01	6.0 %	00	368.7 ppm
Star # 771	15:00:22				
NO	168.1 ppm	02	6.0 %	00	368.6 ppm
Star # 772	15:00:51				
NO	170.4 ppm	00	6.0 %	00	367.0 ppm
Star # 773	15:01:22				
NO	160.1 ppm	02	6.0 %	00	365.8 ppm
Star # 774	15:01:50				
NO	170.9 ppm	02	6.0 %	00	368.5 ppm
Star # 775	15:02:20				
NO	170.1 ppm	02	6.0 %	02	370.3 ppm
Star # 776	15:02:50				
NO	178.6 ppm	02	6.0 %	00	369.5 ppm
Star # 777	15:03:20				
NO	166.8 ppm	02	6.0 %	00	367.3 ppm
Star # 778	15:03:50				
NO	170.8 ppm	02	6.0 %	00	366.2 ppm
Star # 779	15:04:20				
NO	21.4 ppm	02	19.0 %	00	29.4 ppm
Star # 780	15:04:50				
NO	11.7 ppm	01	20.0 %	00	1.1 ppm
Star # 781	15:05:20				
NO	11.7 ppm	02	21.0 %	00	0.7 ppm

End Run 3

Leak check
good

Begin system
calc

Scan # 730	15:05:11				
NO ₂	5.5 ppm	00	20.5 %	00	1.2 ppm
Scan # 734	15:05:51				
NO ₂	6.7 ppm	01	20.5 %	00	1.3 ppm
Scan # 735	15:07:20				
NO ₂	7.2 ppm	01	20.5 %	00	1.0 ppm
Scan # 736	15:07:51				
NO ₂	6.1 ppm	00	20.5 %	00	0.7 ppm
Scan # 737	15:08:21				
NO ₂	5.8 ppm	01	20.5 %	00	1.1 ppm
Scan # 739	15:08:52				
NO ₂	5.6 ppm	02	20.5 %	00	0.4 ppm
Scan # 789	15:09:22				
NO ₂	4.6 ppm	00	20.5 %	00	1.3 ppm
Scan # 790	15:09:52				
NO ₂	4.8 ppm	02	20.6 %	00	1.4 ppm
Scan # 791	15:10:22				
NO ₂	4.7 ppm	02	20.6 %	00	0.5 ppm
Scan # 792	15:10:52				
NO ₂	4.2 ppm	02	20.6 %	00	1.3 ppm
Scan # 793	15:11:22				
NO ₂	4.3 ppm	00	20.5 %	00	1.7 ppm
Scan # 794	15:11:52				
NO ₂	4.8 ppm	02	20.2 %	00	0.9 ppm
Scan # 795	15:12:22				
NO ₂	3.9 ppm	00	16.2 %	00	0.6 ppm
Scan # 796	15:12:52				
NO ₂	3.7 ppm	00	16.2 %	00	0.8 ppm
Scan # 797	15:13:22				
NO ₂	3.7 ppm	02	16.2 %	00	1.7 ppm
Scan # 798	15:13:52				
NO ₂	3.5 ppm	02	16.2 %	00	2.0 ppm
Scan # 799	15:14:22				
NO ₂	4.0 ppm	02	16.2 %	00	1.5 ppm
Scan # 800	15:14:52				
NO ₂	3.7 ppm	00	16.0 %	00	316.9 ppm
Scan # 801	15:15:22				
NO ₂	3.5 ppm	02	0.2 %	00	488.7 ppm
Scan # 802	15:15:52				
NO ₂	2.5 ppm	00	0.1 %	00	491.3 ppm
Scan # 803	15:16:22				
NO ₂	3.0 ppm	00	0.1 %	00	490.8 ppm

zero

16.1 °C O₂

487.0 ppm CO

Scan # 805	15:17:22				
NOx	2.4 ppm	02	0.0 %	00	450.9 ppm
Scan # 806	15:17:52				
NOx	3.0 ppm	02	0.1 %	00	450.8 ppm
Scan # 807	15:18:22				
NOx	2.1.2 ppm	02	2.1 %	00	31.5 ppm
Scan # 808	15:18:52				
NOx	235.9 ppm	01	0.1 %	00	3.4 ppm
Scan # 809	15:19:22				
NOx	241.5 ppm	00	0.0 %	00	1.7 ppm
Scan # 810	15:19:52				
NOx	240.1 ppm	02	0.0 %	00	0.5 ppm
Scan # 811	15:20:22				
NOx	240.1 ppm	02	0.0 %	00	1.1 ppm
Scan # 812	15:20:52				
NOx	240.5 ppm	02	0.0 %	00	2.2 ppm
Scan # 813	15:21:22				
NOx	240.5 ppm	02	0.0 %	00	2.2 ppm
Scan # 814	15:21:52				
NOx	241.2 ppm	02	0.0 %	00	1.4 ppm
Scan # 815	15:22:22				
NOx	235.9 ppm	02	0.1 %	00	1.9 ppm
Scan # 816	15:22:52				
NOx	212.9 ppm	01	0.1 %	00	2.1 ppm
Scan # 817	15:23:22				
NOx	3.9 ppm	01	0.1 %	00	1.8 ppm
Scan # 818	15:23:52				
NOx	2.8 ppm	02	0.1 %	00	2.8 ppm

242.0 ppm NO
O₂ zero

End ET-29
#007 100% load

Oceanside Landfill
ET-29 #007
75% load

1400 LBS/HR CO₂ RELEASE RATE 10-07-1991 09:23:31

Model 140 A-1
A/D (Analog to Digital) Converter address= 7.2
Storage Interval: hours= 0 minutes= 0 seconds= 30
Printer will log data.
Alarms are silent
Autostop is off
Autostore on disk 0

POINT	LABEL	UNITS	OFFSET	SAMPLING	SEC PL	HIGH ALARM	LOW ALARM	CHANNEL	EXT MOD
1	N2	ppm	8.25	.2	1	0	0	0	0
2	O2	%	-2.75	.025	1	0	0	0	2
3	CO	ppm	40.75	.25	1	0	0	0	4

DATE 10-07-1991

Scan # 1 09:23:51

N2 -0.3 ppm 02 20.8 % 00 0.0 ppm

Scan # 2 09:24:21

N2 -0.1 ppm 02 20.8 % 00 1.6 ppm

Scan # 3 09:24:51

N2 0.6 ppm 02 20.8 % 00 0.8 ppm

Scan # 4 09:25:21

N2 0.4 ppm 02 20.8 % 00 2.8 ppm

Scan # 5 09:25:51

N2 0.0 ppm 02 20.8 % 00 2.4 ppm

Scan # 6 09:26:21

N2 1.1 ppm 02 20.8 % 00 3.4 ppm

Scan # 7 09:26:51

N2 1.1 ppm 02 20.8 % 00 2.4 ppm

Scan # 8 09:27:21

N2 1.5 ppm 02 20.8 % 00 2.7 ppm

Scan # 9 09:27:51

N2 1.0 ppm 02 20.8 % 00 2.1 ppm

Scan # 10 09:28:21

N2 1.0 ppm 02 20.8 % 00 1.7 ppm

Scan # 11 09:28:51

N2 1.1 ppm 02 20.8 % 00 1.2 ppm

Scan # 12 09:29:21

N2 1.1 ppm 02 20.8 % 00 1.6 ppm

Scan # 13 09:29:51

N2 1.5 ppm 02 20.8 % 00 0.5 ppm

Begin analyzer
cals

Ambient air
20.9 % O₂

zero

Scan # 15	08:31:51				
NO _x	0.6 ppm	02	20.6 %	02	1.0 ppm
Scan # 16	08:32:21				
NO _x	0.6 ppm	02	20.7 %	01	0.9 ppm
Scan # 17	08:33:51				
NO _x	0.9 ppm	02	20.1 %	02	1.0 ppm
Scan # 18	08:32:21				
NO _x	0.5 ppm	01	16.4 %	00	0.6 ppm
Scan # 19	08:32:51				
NO _x	0.5 ppm	02	16.2 %	00	0.7 ppm
Scan # 20	08:33:21				
NO _x	0.8 ppm	01	16.1 %	00	0.7 ppm
Scan # 21	08:33:51				
NO _x	0.9 ppm	02	16.2 %	00	0.8 ppm
Scan # 22	08:34:21				
NO _x	0.7 ppm	02	16.2 %	00	0.8 ppm
Scan # 23	08:34:51				
NO _x	0.6 ppm	02	16.2 %	00	-0.5 ppm
Scan # 24	08:35:21				
NO _x	0.2 ppm	02	16.2 %	00	-0.2 ppm
Scan # 25	08:35:51				
NO _x	0.0 ppm	02	0.4 %	00	486.0 ppm
Scan # 26	08:36:21				
NO _x	0.1 ppm	02	0.1 %	00	489.8 ppm
Scan # 27	08:36:51				
NO _x	0.1 ppm	02	0.0 %	00	491.4 ppm
Scan # 28	08:37:21				
NO _x	0.2 ppm	02	-0.0 %	00	490.4 ppm
Scan # 29	08:37:51				
NO _x	0.1 ppm	02	-0.0 %	00	490.7 ppm
Scan # 30	08:38:21				
NO _x	0.5 ppm	02	-0.0 %	00	491.0 ppm
Scan # 31	08:38:51				
NO _x	0.2 ppm	02	-0.0 %	00	490.6 ppm
Scan # 32	08:39:21				
NO _x	0.2 ppm	02	-0.0 %	00	490.6 ppm
Scan # 33	08:39:51				
NO _x	509.1 ppm	02	0.0 %	01	4.2 ppm
Scan # 34	08:40:21				
NO _x	509.2 ppm	02	0.0 %	00	0.0 ppm
Scan # 35	08:40:51				
NO _x	473.6 ppm	02	-0.0 %	00	0.0 ppm

16.1% O₂487.0 ppm CO
O₂ zero

Scan # 37	08:42:51				
NOx	481.5 ppm	02	-0.0 %	00	0.5 ppm
Scan # 38	08:43:01				
NOx	482.1 ppm	02	-0.0 %	01	-0.1 ppm
Scan # 39	08:43:51				
NOx	481.2 ppm	02	-0.0 %	00	-1.1 ppm
Scan # 40	08:43:21				
NOx	481.5 ppm	02	-0.0 %	10	0.5 ppm
Scan # 41	08:43:51				
NOx	211.1 ppm	02	-0.0 %	00	-0.1 ppm
Scan # 42	08:44:01				
NOx	36.5 ppm	02	0.0 %	09	244.5 ppm
Scan # 43	08:44:51				
NOx	-1.5 ppm	01	-0.0 %	00	247.5 ppm
Scan # 44	08:45:21				
NOx	-1.4 ppm	02	-0.0 %	00	245.3 ppm
Scan # 45	08:45:51				
NOx	-1.4 ppm	02	-0.0 %	00	244.3 ppm
Scan # 46	08:46:21				
NOx	-1.7 ppm	02	-0.0 %	00	244.9 ppm
Scan # 47	08:46:51				
NOx	-1.2 ppm	02	-0.0 %	00	244.5 ppm
Scan # 48	08:47:21				
NOx	-1.6 ppm	02	-0.0 %	00	244.5 ppm
Scan # 49	08:47:51				
NOx	-0.9 ppm	02	-0.0 %	00	243.3 ppm
Scan # 50	08:48:21				
NOx	-1.2 ppm	02	-0.0 %	00	243.6 ppm
Scan # 51	08:48:52				
NOx	-1.0 ppm	02	-0.0 %	00	243.8 ppm
Scan # 52	08:49:21				
NOx	-0.9 ppm	02	-0.0 %	00	242.7 ppm
Scan # 53	08:49:51				
NOx	-1.2 ppm	02	-0.0 %	00	243.5 ppm
Scan # 54	08:50:21				
NOx	-1.1 ppm	02	0.0 %	00	243.1 ppm
Scan # 55	08:50:51				
NOx	-0.8 ppm	02	0.0 %	00	243.3 ppm
Scan # 56	08:51:21				
NOx	-0.9 ppm	02	0.0 %	00	242.5 ppm
Scan # 57	08:51:51				
NOx	-0.8 ppm	02	0.0 %	00	243.1 ppm

480.0 ppm NO

071

071

071

071

071

Scan # 59	08:52:51				
NO _x	-1.2 ppm	02	0.0 %	00	263.1 ppm
Scan # 60	08:53:22				
NO _x	-0.9 ppm	02	0.0 %	00	262.3 ppm
Scan # 61	08:53:51				
NO _x	-0.9 ppm	02	0.1 %	01	264.1 ppm
Scan # 62	08:54:21				
NO _x	-0.9 ppm	02	0.1 %	00	262.5 ppm
Scan # 63	08:54:51				
NO _x	-1.1 ppm	02	0.1 %	00	263.4 ppm
Scan # 64	08:55:21				
NO _x	-0.9 ppm	02	0.1 %	00	263.1 ppm
Scan # 65	08:55:51				
NO _x	-0.8 ppm	02	0.1 %	00	262.1 ppm
Scan # 66	08:56:22				
NO _x	-0.9 ppm	02	0.1 %	00	263.7 ppm
Scan # 67	08:56:51				
NO _x	-0.7 ppm	02	0.1 %	00	262.9 ppm
Scan # 68	08:57:21				
NO _x	5.5 ppm	02	0.1 %	00	274.6 ppm
Scan # 69	08:57:51				
NO _x	-0.7 ppm	02	-0.0 %	00	274.2 ppm
Scan # 70	08:58:21				
NO _x	-1.3 ppm	02	-0.0 %	00	273.8 ppm
Scan # 71	08:58:52				
NO _x	-1.0 ppm	02	-0.0 %	00	274.1 ppm
Scan # 72	08:59:21				
NO _x	-0.9 ppm	02	-0.0 %	00	273.5 ppm
Scan # 73	08:59:51				
NO _x	-1.1 ppm	02	-0.0 %	00	281.7 ppm
Scan # 74	09:00:21				
NO _x	-1.1 ppm	02	-0.0 %	00	280.9 ppm
Scan # 75	09:00:51				
NO _x	-0.9 ppm	02	-0.0 %	00	281.1 ppm
Scan # 76	09:01:22				
NO _x	-1.3 ppm	02	-0.0 %	00	280.3 ppm
Scan # 77	09:01:51				
NO _x	-1.2 ppm	02	-0.0 %	01	280.5 ppm
Scan # 78	09:02:21				
NO _x	-1.3 ppm	02	-0.1 %	00	281.5 ppm
Scan # 79	09:02:51				
NO _x	63.7 ppm	02	0.0 %	00	31.3 ppm

284.0 ppm CO

45

97.5 ppm NO

141.0 ppm CO

242.0 ppm NO

Leak check

Scan # 81	09:03:51				
NOx	97.5 ppm	02	-0.0 %	00	3.4 ppm
Scan # 82	09:04:21				
NOx	98.3 ppm	02	-0.0 %	00	4.7 ppm
Scan # 83	09:04:51				
NOx	98.1 ppm	02	-0.0 %	00	2.7 ppm
Scan # 84	09:05:21				
NOx	98.4 ppm	02	-0.0 %	00	4.4 ppm
Scan # 85	09:05:51				
NOx	98.2 ppm	02	-0.0 %	00	4.2 ppm
Scan # 86	09:06:22				
NOx	98.0 ppm	02	-0.0 %	00	8.5 ppm
Scan # 87	09:06:52				
NOx	-0.9 ppm	02	-0.0 %	00	146.6 ppm
Scan # 88	09:07:21				
NOx	-0.7 ppm	02	-0.0 %	00	147.9 ppm
Scan # 89	09:07:51				
NOx	-0.9 ppm	02	-0.0 %	00	147.0 ppm
Scan # 90	09:08:22				
NOx	-0.9 ppm	02	-0.0 %	00	147.1 ppm
Scan # 91	09:08:52				
NOx	-0.6 ppm	02	-0.0 %	00	147.5 ppm
Scan # 92	09:09:21				
NOx	-0.9 ppm	02	-0.1 %	00	147.7 ppm
Scan # 93	09:09:51				
NOx	238.1 ppm	02	-0.0 %	00	10.3 ppm
Scan # 94	09:10:21				
NOx	241.7 ppm	02	-0.0 %	00	5.2 ppm
Scan # 95	09:10:51				
NOx	243.9 ppm	02	-0.0 %	00	5.0 ppm
Scan # 96	09:11:22				
NOx	248.8 ppm	02	-0.0 %	00	3.3 ppm
Scan # 97	09:11:52				
NOx	247.4 ppm	02	-0.0 %	00	4.0 ppm
Scan # 98	09:12:21				
NOx	248.9 ppm	02	-0.0 %	00	4.0 ppm
Scan # 99	09:12:51				
NOx	240.3 ppm	02	-0.0 %	00	3.8 ppm
Scan # 100	09:13:21				
NOx	240.2 ppm	02	-0.0 %	00	3.6 ppm
Scan # 101	09:13:52				
NOx	239.8 ppm	02	-0.0 %	00	4.0 ppm

Design
545 terms

zero

16.1% O₂

Scan # 104	09:14:51	02	20.8 %	02	13.4 ppm
NO _x	3.3 ppm				
Scan # 105	09:15:21	02	20.6 %	00	14.6 ppm
NO _x	-0.7 ppm				
Scan # 106	09:15:52	02	20.7 %	00	11.5 ppm
NO _x	0.3 ppm				
Scan # 107	09:16:22	02	20.4 %	00	12.7 ppm
NO _x	-0.5 ppm				
Scan # 107	09:16:52	02	20.5 %	00	2.3 ppm
NO _x	0.5 ppm				
Scan # 108	09:17:21	02	20.5 %	00	2.0 ppm
NO _x	0.3 ppm				
Scan # 108	09:17:51	02	20.5 %	00	2.7 ppm
NO _x	0.3 ppm				
Scan # 110	09:18:22	02	20.5 %	00	1.8 ppm
NO _x	0.5 ppm				
Scan # 111	09:18:52	02	20.4 %	00	3.1 ppm
NO _x	0.2 ppm				
Scan # 112	09:19:22	02	20.1 %	02	4.9 ppm
NO _x	0.3 ppm				
Scan # 113	09:19:51	02	16.2 %	00	2.7 ppm
NO _x	0.2 ppm				
Scan # 114	09:20:21	02	16.1 %	00	3.4 ppm
NO _x	0.1 ppm				
Scan # 115	09:20:52	02	16.1 %	00	3.2 ppm
NO _x	0.2 ppm				
Scan # 116	09:21:22	02	16.1 %	00	3.1 ppm
NO _x	0.4 ppm				
Scan # 117	09:21:52	02	16.1 %	00	3.5 ppm
NO _x	0.3 ppm				
Scan # 118	09:22:21	02	16.1 %	00	3.6 ppm
NO _x	0.3 ppm				
Scan # 119	09:22:51	02	6.2 %	00	4.7 ppm
NO _x	207.0 ppm				
Scan # 120	09:23:21	02	0.0 %	00	3.2 ppm
NO _x	245.7 ppm				
Scan # 121	09:23:52	02	0.0 %	00	3.6 ppm
NO _x	245.4 ppm				
Scan # 122	09:24:21	02	0.0 %	00	3.2 ppm
NO _x	244.9 ppm				
Scan # 123	09:24:51	02	0.0 %	00	3.4 ppm
NO _x	244.5 ppm				
Scan # 124	09:25:21				
NO _x	244.4 ppm				

242.0 ppm
NO

Scan # 121	09:25:52				
NOx	243.1 ppm	02	-0.0 %	00	3.4 ppm
Scan # 122	09:26:21				
NOx	242.6 ppm	02	-0.0 %	00	3.6 ppm
Scan # 127	09:26:52				
NOx	242.7 ppm	01	-0.0 %	00	2.6 ppm
Scan # 128	09:27:22				
NOx	230.9 ppm	02	-0.0 %	00	4.1 ppm
Scan # 129	09:27:51				
NOx	115.7 ppm	02	0.7 %	00	141.6 ppm
Scan # 130	09:28:01				
NOx	3.1 ppm	02	0.1 %	00	491.5 ppm
Scan # 131	09:28:52				
NOx	3.0 ppm	02	-0.0 %	00	494.7 ppm
Scan # 132	09:29:22				
NOx	3.1 ppm	02	-0.0 %	00	493.4 ppm
Scan # 133	09:29:52				
NOx	3.2 ppm	02	-0.0 %	00	498.9 ppm
Scan # 134	09:30:21				
NOx	3.2 ppm	02	-0.0 %	00	493.6 ppm
Scan # 135	09:30:52				
NOx	3.4 ppm	02	-0.0 %	00	494.8 ppm
Scan # 136	09:31:22				
NOx	3.1 ppm	02	-0.0 %	00	494.7 ppm
Scan # 137	09:31:51				
NOx	5.2 ppm	02	19.3 %	00	24.6 ppm
Scan # 138	09:32:22				
NOx	147.1 ppm	02	5.3 %	00	410.9 ppm
Scan # 139	09:32:51				
NOx	155.6 ppm	01	4.4 %	00	419.7 ppm
Scan # 140	09:33:22				
NOx	154.1 ppm	02	4.5 %	00	417.0 ppm
Scan # 141	09:33:52				
NOx	149.4 ppm	02	4.4 %	00	420.9 ppm
Scan # 142	09:34:22				
NOx	153.9 ppm	02	4.4 %	00	418.5 ppm
Scan # 143	09:34:52				
NOx	155.4 ppm	01	4.4 %	00	415.2 ppm
Scan # 144	09:35:21				
NOx	154.7 ppm	02	4.4 %	00	420.3 ppm
Scan # 145	09:35:51				
NOx	156.3 ppm	02	4.4 %	00	415.1 ppm
Scan # 146	09:36:21				
NOx	155.5 ppm	02	4.4 %	00	415.1 ppm

487.0 ppm CO
O2 zero

Begin Run 4

Scan # 147	09:36:10				
NO ₂	150.2 ppm	02	4.4 %	00	410.5 ppm
Scan # 148	09:37:02				
NO ₂	154.1 ppm	01	4.4 %	00	418.3 ppm
Scan # 149	09:37:51				
NO ₂	154.9 ppm	01	4.4 %	00	411.5 ppm
Scan # 150	09:38:22				
NO ₂	157.5 ppm	02	4.4 %	00	416.8 ppm
Scan # 151	09:39:02				
NO ₂	157.0 ppm	01	4.4 %	00	417.9 ppm
Scan # 151	09:39:01				
NO ₂	156.3 ppm	02	4.4 %	00	418.1 ppm
Scan # 153	09:39:51				
NO ₂	158.1 ppm	02	4.4 %	00	416.5 ppm
Scan # 154	09:40:22				
NO ₂	152.4 ppm	02	4.5 %	00	414.6 ppm
Scan # 155	09:40:51				
NO ₂	155.1 ppm	02	4.4 %	00	418.0 ppm
Scan # 156	09:41:22				
NO ₂	151.8 ppm	02	4.5 %	00	415.3 ppm
Scan # 157	09:41:52				
NO ₂	155.1 ppm	02	4.4 %	00	420.4 ppm
Scan # 158	09:42:22				
NO ₂	151.4 ppm	02	4.4 %	00	416.5 ppm
Scan # 159	09:42:52				
NO ₂	154.1 ppm	02	4.4 %	00	420.0 ppm
Scan # 160	09:43:01				
NO ₂	148.5 ppm	01	4.4 %	00	416.5 ppm
Scan # 161	09:43:52				
NO ₂	157.8 ppm	02	4.4 %	00	420.7 ppm
Scan # 162	09:44:22				
NO ₂	150.8 ppm	02	4.4 %	00	416.0 ppm
Scan # 163	09:44:52				
NO ₂	150.5 ppm	02	4.4 %	00	416.8 ppm
Scan # 164	09:45:22				
NO ₂	150.9 ppm	02	4.4 %	00	416.6 ppm
Scan # 165	09:45:52				
NO ₂	150.9 ppm	02	4.4 %	00	421.3 ppm
Scan # 166	09:46:22				
NO ₂	150.5 ppm	01	4.4 %	00	416.6 ppm
Scan # 167	09:46:51				
NO ₂	150.4 ppm	01	4.4 %	00	421.1 ppm
Scan # 168	09:47:01				

I	Scan # 169	09:44:51			
	NO _x	155.4 ppm	02	4.4 %	418.7 ppm
	Scan # 170	09:45:22			
	NO _x	156.8 ppm	02	4.4 %	418.8 ppm
	Scan # 171	09:45:52			
	NO _x	160.4 ppm	02	4.4 %	420.5 ppm
II	Scan # 172	09:46:21			
	NO _x	158.4 ppm	02	4.4 %	418.2 ppm
	Scan # 173	09:46:51			
	NO _x	160.3 ppm	02	4.4 %	420.7 ppm
	Scan # 174	09:47:22			
	NO _x	154.5 ppm	02	4.4 %	419.2 ppm
III	Scan # 175	09:50:52			
	NO _x	163.2 ppm	02	4.3 %	419.5 ppm
	Scan # 176	09:51:22			
	NO _x	149.9 ppm	02	4.4 %	416.8 ppm
	Scan # 177	09:51:52			
	NO _x	158.8 ppm	02	4.4 %	420.0 ppm
	Scan # 178	09:52:21			
	NO _x	148.9 ppm	02	4.4 %	415.5 ppm
	Scan # 179	09:52:52			
	NO _x	153.4 ppm	02	4.4 %	420.0 ppm
	Scan # 180	09:53:22			
	NO _x	149.7 ppm	02	4.4 %	420.0 ppm
IV	Scan # 181	09:53:52			
	NO _x	162.5 ppm	02	4.4 %	422.2 ppm
	Scan # 182	09:54:22			
	NO _x	150.2 ppm	02	4.4 %	420.3 ppm
	Scan # 183	09:54:52			
	NO _x	163.4 ppm	02	4.3 %	423.1 ppm
V	Scan # 184	09:55:21			
	NO _x	155.3 ppm	02	4.4 %	415.5 ppm
	Scan # 185	09:55:52			
	NO _x	163.8 ppm	02	4.3 %	418.2 ppm
	Scan # 186	09:56:22			
	NO _x	156.5 ppm	02	4.4 %	419.1 ppm
	Scan # 187	09:56:52			
	NO _x	164.3 ppm	02	4.3 %	422.8 ppm
	Scan # 188	09:57:22			
	NO _x	174.5 ppm	02	4.4 %	417.5 ppm
	Scan # 189	09:57:52			
	NO _x	164.7 ppm	02	4.3 %	420.7 ppm
	Scan # 190	09:58:22			
	NO _x				

L	Scan # 191	09:58:01			
	NO _x	164.4 ppm	02	4.3 %	00 421.2 ppm
	Scan # 192	09:59:22			
	NO _x	165.5 ppm	02	4.4 %	00 419.0 ppm
	Scan # 193	09:59:52			
	NO _x	165.4 ppm	02	4.3 %	00 421.7 ppm
m	Scan # 194	10:00:22			
	NO _x	165.4 ppm	02	4.4 %	00 419.5 ppm
	Scan # 195	10:00:52			
	NO _x	165.3 ppm	02	4.4 %	00 414.8 ppm
	Scan # 196	10:01:22			
	NO _x	142.3 ppm	02	4.5 %	00 406.4 ppm
n	Scan # 197	10:01:52			
	NO _x	144.4 ppm	02	4.5 %	00 412.4 ppm
	Scan # 198	10:02:22			
	NO _x	139.2 ppm	02	4.5 %	00 412.7 ppm
	Scan # 199	10:02:52			
	NO _x	143.7 ppm	02	4.5 %	00 405.8 ppm
	Scan # 200	10:03:22			
	NO _x	144.9 ppm	02	4.5 %	00 409.0 ppm
	Scan # 201	10:03:52			
	NO _x	146.0 ppm	02	4.5 %	00 411.6 ppm
	Scan # 202	10:04:22			
	NO _x	136.9 ppm	02	4.5 %	00 405.8 ppm
o	Scan # 203	10:04:52			
	NO _x	147.9 ppm	02	4.5 %	00 412.0 ppm
	Scan # 204	10:05:22			
	NO _x	136.9 ppm	02	4.5 %	00 406.3 ppm
	Scan # 205	10:05:52			
	NO _x	141.8 ppm	02	4.5 %	00 411.4 ppm
p	Scan # 206	10:06:22			
	NO _x	138.2 ppm	02	4.6 %	00 404.1 ppm
	Scan # 207	10:06:52			
	NO _x	143.7 ppm	02	4.5 %	00 412.3 ppm
	Scan # 208	10:07:22			
	NO _x	140.3 ppm	02	4.5 %	00 408.8 ppm
	Scan # 209	10:07:52			
	NO _x	146.0 ppm	02	4.5 %	00 413.5 ppm
	Scan # 210	10:08:22			
	NO _x	141.8 ppm	02	4.5 %	00 416.3 ppm
	Scan # 211	10:08:52			
	NO _x	144.7 ppm	02	4.5 %	00 413.1 ppm
	Scan # 212	10:09:22			

Star # 210	10:09:52				
Alt	147.4 ppm	02	4.5 %	01	413.4 ppm
Star # 214	10:10:22				
Alt	155.6 ppm	03	4.5 %	00	413.7 ppm
Star # 215	10:10:51				
Alt	150.4 ppm	02	4.5 %	01	417.4 ppm
Star # 216	10:11:02				
Alt	159.6 ppm	02	4.5 %	00	408.1 ppm
Star # 217	10:11:52				
Alt	145.4 ppm	02	4.5 %	00	417.5 ppm
Star # 218	10:12:22				
Alt	141.4 ppm	02	4.5 %	01	411.3 ppm
Star # 219	10:12:52				
Alt	148.8 ppm	02	4.5 %	00	413.8 ppm
Star # 220	10:13:22				
Alt	141.4 ppm	02	4.5 %	00	408.7 ppm
Star # 221	10:13:52				
Alt	144.5 ppm	02	4.5 %	00	410.1 ppm
Star # 222	10:14:22				
Alt	139.4 ppm	02	4.5 %	00	411.1 ppm
Star # 223	10:14:52				
Alt	152.3 ppm	02	4.5 %	00	413.5 ppm
Star # 224	10:15:22				
Alt	141.3 ppm	03	4.5 %	00	417.4 ppm
Star # 225	10:16:01				
Alt	150.6 ppm	02	4.5 %	00	413.3 ppm
Star # 226	10:16:31				
Alt	141.3 ppm	02	4.5 %	00	408.8 ppm
Star # 227	10:16:51				
Alt	145.2 ppm	02	4.5 %	00	410.7 ppm
Star # 228	10:17:22				
Alt	135.8 ppm	02	4.5 %	00	405.3 ppm
Star # 229	10:17:52				
Alt	147.4 ppm	02	4.5 %	00	415.0 ppm
Star # 230	10:18:22				
Alt	142.7 ppm	02	4.5 %	00	410.7 ppm
Star # 231	10:18:52				
Alt	143.5 ppm	01	4.5 %	00	415.5 ppm
Star # 232	10:19:22				
Alt	141.4 ppm	01	4.5 %	00	411.1 ppm
Star # 233	10:19:51				
Alt	145.6 ppm	02	4.5 %	00	414.6 ppm
Star # 234	10:20:22				

Scan # 235	10:20:51				
NOx	141.4 ppm	01	4.5 %	00	414.9 ppm
Scan # 236	10:21:22				
NOx	141.1 ppm	02	4.5 %	00	413.1 ppm
Scan # 237	10:21:52				
NOx	141.2 ppm	02	4.5 %	00	410.1 ppm
Scan # 238	10:22:22				
NOx	139.8 ppm	01	4.5 %	00	407.4 ppm
Scan # 239	10:22:52				
NOx	140.1 ppm	02	4.5 %	00	410.2 ppm
Scan # 240	10:23:22				
NOx	141.5 ppm	02	4.5 %	00	407.4 ppm
Scan # 241	10:23:52				
NOx	149.6 ppm	02	4.5 %	00	410.7 ppm
Scan # 242	10:24:22				
NOx	144.1 ppm	02	4.5 %	00	405.6 ppm
Scan # 243	10:24:52				
NOx	149.9 ppm	02	4.5 %	00	411.7 ppm
Scan # 244	10:25:21				
NOx	145.6 ppm	02	4.5 %	00	407.2 ppm
Scan # 245	10:25:52				
NOx	144.9 ppm	02	4.5 %	00	410.8 ppm
Scan # 246	10:26:22				
NOx	144.6 ppm	02	4.5 %	00	406.4 ppm
Scan # 247	10:26:52				
NOx	150.2 ppm	02	4.5 %	00	413.5 ppm
Scan # 248	10:27:12				
NOx	139.9 ppm	02	4.5 %	00	412.8 ppm
Scan # 249	10:27:52				
NOx	145.5 ppm	02	4.5 %	00	412.8 ppm
Scan # 250	10:28:22				
NOx	140.2 ppm	02	4.5 %	00	409.0 ppm
Scan # 251	10:28:52				
NOx	151.1 ppm	02	4.5 %	00	414.2 ppm
Scan # 252	10:29:22				
NOx	145.2 ppm	02	4.5 %	00	406.9 ppm
Scan # 253	10:29:52				
NOx	148.9 ppm	02	4.5 %	00	411.6 ppm
Scan # 254	10:30:22				
NOx	140.7 ppm	02	4.5 %	00	405.1 ppm
Scan # 255	10:31:52				
NOx	141.7 ppm	02	4.5 %	00	411.6 ppm
Scan # 256	10:32:22				

Scan # 250	10:31:51				
NOx	153.2 ppm	02	4.5 %	00	402.4 ppm
Scan # 251	10:32:22				
NOx	141.2 ppm	02	4.5 %	00	410.9 ppm
Scan # 252	10:32:52				
NOx	153.2 ppm	02	4.5 %	02	413.3 ppm
Scan # 253	10:33:21				
NOx	142.2 ppm	02	4.5 %	00	406.5 ppm
Scan # 254	10:33:52				
NOx	141.2 ppm	02	4.5 %	00	411.3 ppm
Scan # 255	10:34:21				
NOx	145.1 ppm	02	4.5 %	00	408.2 ppm
Scan # 256	10:34:51				
NOx	111.7 ppm	02	4.5 %	00	408.5 ppm
Scan # 257	10:35:22				
NOx	103.7 ppm	02	4.6 %	00	409.0 ppm
Scan # 258	10:35:52				
NOx	193.8 ppm	02	4.5 %	00	416.6 ppm
Scan # 259	10:36:22				
NOx	140.7 ppm	02	4.8 %	00	393.1 ppm
Scan # 260	10:36:52				
NOx	124.0 ppm	02	5.5 %	00	457.6 ppm
Scan # 261	10:37:22				
NOx	125.3 ppm	02	5.2 %	00	405.8 ppm
Scan # 262	10:37:51				
NOx	162.9 ppm	02	4.9 %	00	399.0 ppm
Scan # 263	10:38:22				
NOx	192.6 ppm	02	4.5 %	00	410.5 ppm
Scan # 264	10:38:52				
NOx	180.4 ppm	02	4.8 %	00	390.5 ppm
Scan # 265	10:39:22				
NOx	159.7 ppm	02	4.9 %	00	387.1 ppm
Scan # 266	10:39:52				
NOx	154.5 ppm	02	5.7 %	00	453.4 ppm
Scan # 267	10:40:22				
NOx	162.7 ppm	02	4.9 %	00	385.1 ppm
Scan # 268	10:40:52				
NOx	173.2 ppm	02	4.9 %	00	388.0 ppm
Scan # 269	10:41:21				
NOx	205.7 ppm	02	4.7 %	00	392.2 ppm
Scan # 270	10:41:52				
NOx	222.1 ppm	02	4.6 %	00	397.5 ppm
Scan # 271	10:42:22				
NOx	154.5 ppm	02	5.7 %	00	453.4 ppm

End Run 4

E	Scan # 257	10:42:52			
	NOx	277.6 ppm	02	4.6 %	00
	Scan # 258	10:43:22			
	NOx	281.6 ppm	02	4.6 %	00
	Scan # 259	10:43:52			
	NOx	187.8 ppm	02	4.6 %	00
C1	Scan # 260	10:44:22			
	NOx	138.4 ppm	02	4.6 %	00
	Scan # 261	10:44:52			
	NOx	117.4 ppm	02	4.6 %	00
	Scan # 262	10:45:22			
	NOx	112.6 ppm	02	4.6 %	00
C2	Scan # 263	10:45:52			
	NOx	113.4 ppm	02	4.4 %	00
	Scan # 264	10:46:22			
	NOx	120.6 ppm	02	4.4 %	00
	Scan # 267	10:46:52			
	NOx	58.4 ppm	02	12.8 %	00
	Scan # 268	10:47:22			
	NOx	20.6 ppm	02	17.5 %	00
	Scan # 269	10:47:52			
	NOx	14.2 ppm	02	19.0 %	00
	Scan # 280	10:48:22			
	NOx	4.6 ppm	02	19.6 %	00
L	Scan # 281	10:48:52			
	NOx	28.6 ppm	02	20.6 %	00
	Scan # 282	10:49:22			
	NOx	10.8 ppm	02	20.3 %	00
	Scan # 283	10:49:52			
	NOx	8.1 ppm	02	20.4 %	00
C3	Scan # 284	10:50:22			
	NOx	7.5 ppm	02	20.4 %	00
	Scan # 295	10:50:52			
	NOx	6.3 ppm	02	20.4 %	00
	Scan # 296	10:51:22			
	NOx	6.0 ppm	02	20.4 %	00
	Scan # 297	10:51:52			
	NOx	5.7 ppm	02	20.4 %	00
	Scan # 298	10:52:22			
	NOx	5.0 ppm	02	20.4 %	00
	Scan # 299	10:52:52			
	NOx	5.1 ppm	02	20.4 %	00
	Scan # 300	10:53:22			
	NOx	5.1 ppm	02	20.4 %	00

Test. Check
Good
↓

Begin system
cals

Scan # 301	10:53:51				
NOx	4.3 ppm	02	20.5 %	00	0.3 ppm
Scan # 302	10:54:22				
NOx	4.2 ppm	02	20.5 %	00	-0.5 ppm
Scan # 303	10:54:52				
NOx	4.1 ppm	02	20.5 %	00	-0.1 ppm
Scan # 304	10:55:22				
NOx	4.0 ppm	01	20.4 %	00	-0.1 ppm
Scan # 305	10:55:52				
NOx	4.0 ppm	02	19.7 %	00	1.2 ppm
Scan # 306	10:56:22				
NOx	3.8 ppm	01	16.2 %	00	-0.1 ppm
Scan # 307	10:56:52				
NOx	3.3 ppm	02	16.1 %	00	0.1 ppm
Scan # 308	10:57:21				
NOx	3.4 ppm	02	16.1 %	00	-0.3 ppm
Scan # 309	10:57:52				
NOx	2.8 ppm	02	16.1 %	00	-0.5 ppm
Scan # 310	10:58:22				
NOx	3.2 ppm	02	16.1 %	00	-0.7 ppm
Scan # 311	10:58:52				
NOx	2.8 ppm	02	16.1 %	00	-0.8 ppm
Scan # 312	10:59:22				
NOx	2.4 ppm	01	16.0 %	00	0.3 ppm
Scan # 313	10:59:52				
NOx	2.7 ppm	00	15.9 %	00	114.5 ppm
Scan # 314	11:00:22				
NOx	1.5 ppm	00	0.4 %	00	487.9 ppm
Scan # 315	11:00:52				
NOx	2.4 ppm	00	0.0 %	00	490.6 ppm
Scan # 316	11:01:22				
NOx	1.8 ppm	00	0.0 %	00	492.8 ppm
Scan # 317	11:01:52				
NOx	2.0 ppm	01	-0.0 %	00	493.5 ppm
Scan # 318	11:02:22				
NOx	2.0 ppm	00	-0.0 %	00	494.2 ppm
Scan # 319	11:02:52				
NOx	2.5 ppm	01	-0.0 %	00	491.8 ppm
Scan # 320	11:03:22				
NOx	205.2 ppm	01	1.4 %	01	19.4 ppm
Scan # 321	11:03:52				
NOx	244.8 ppm	01	-0.0 %	01	0.4 ppm
Scan # 322	11:04:22				

zero

55

16.1 % O₂

487.0 ppm CO
O₂ zero

242.0 ppm
NO

Scan # 321	245.6 ppm	01	-0.0 %	00	-0.0 ppm
Scan # 324	245.6 ppm	02	-0.0 %	00	-0.0 ppm
Scan # 326	245.6 ppm	03	-0.0 %	00	-0.0 ppm
Scan # 328	245.6 ppm	02	-0.0 %	00	1.1 ppm
Scan # 327	235.6 ppm	01	12.7 %	01	3.7 ppm
Scan # 329	3.6 ppm	00	20.9 %	00	6.3 ppm
Scan # 329	2.8 ppm	01	20.9 %	00	3.6 ppm
Scan # 330	2.8 ppm	02	20.9 %	00	4.5 ppm
Scan # 331	2.3 ppm	02	20.9 %	00	3.9 ppm
Scan # 332	2.7 ppm	02	20.9 %	00	4.9 ppm
Scan # 333	2.5 ppm	02	20.9 %	00	4.0 ppm
Scan # 334	2.9 ppm	02	21.0 %	00	4.5 ppm
Scan # 335	2.6 ppm	02	21.0 %	00	4.4 ppm
Scan # 336	2.4 ppm	01	21.0 %	00	4.0 ppm
Scan # 337	2.4 ppm	02	21.0 %	00	4.7 ppm
Scan # 338	2.7 ppm	02	21.0 %	00	4.2 ppm
Scan # 339	2.8 ppm	02	21.0 %	00	4.5 ppm
Scan # 340	97.4 ppm	02	9.4 %	00	346.3 ppm
Scan # 341	111.2 ppm	02	4.9 %	00	397.7 ppm
Scan # 342	111.2 ppm	01	4.9 %	00	394.3 ppm
Scan # 343	97.4 ppm	02	4.8 %	01	398.6 ppm
Scan # 344	111.2 ppm				

Begin Run 5

1	Scan # 345	11:15:15				
	ADP	100.1 ppm	02	4.7 %	00	391.9 ppm
	Scan # 346	11:16:22				
	ADP	98.6 ppm	02	4.6 %	00	391.3 ppm
	Scan # 347	11:16:52				
	ADP	103.1 ppm	02	4.6 %	00	391.7 ppm
2	Scan # 348	11:17:22				
	ADP	99.3 ppm	02	4.7 %	00	391.3 ppm
	Scan # 349	11:17:51				
	ADP	98.3 ppm	02	4.7 %	00	391.7 ppm
	Scan # 350	11:18:22				
	ADP	99.0 ppm	02	4.7 %	00	391.1 ppm
3	Scan # 351	11:18:51				
	ADP	97.2 ppm	02	4.7 %	00	391.2 ppm
	Scan # 352	11:19:22				
	ADP	101.8 ppm	02	4.7 %	00	391.5 ppm
	Scan # 353	11:19:52				
	ADP	98.1 ppm	02	4.6 %	00	391.0 ppm
	Scan # 354	11:20:22				
	ADP	97.5 ppm	02	4.8 %	00	397.9 ppm
	Scan # 355	11:20:52				
	ADP	97.0 ppm	02	4.7 %	00	395.9 ppm
	Scan # 356	11:21:22				
	ADP	107.1 ppm	02	4.7 %	00	399.8 ppm
4	Scan # 357	11:21:51				
	ADP	97.0 ppm	02	4.8 %	00	401.0 ppm
	Scan # 358	11:22:21				
	ADP	99.3 ppm	02	4.6 %	10	395.9 ppm
	Scan # 359	11:22:51				
	ADP	98.7 ppm	02	4.7 %	00	397.4 ppm
5	Scan # 360	11:23:22				
	ADP	102.5 ppm	02	4.7 %	00	391.8 ppm
	Scan # 361	11:23:52				
	ADP	101.6 ppm	02	4.7 %	00	397.9 ppm
	Scan # 362	11:24:22				
	ADP	104.8 ppm	02	4.7 %	00	399.0 ppm
	Scan # 363	11:24:52				
	ADP	101.6 ppm	02	4.7 %	00	395.7 ppm
	Scan # 364	11:25:22				
	ADP	99.2 ppm	02	4.7 %	00	391.2 ppm
	Scan # 365	11:25:51				
	ADP	100.6 ppm	02	4.7 %	00	395.7 ppm
	Scan # 366	11:26:22				

Scan # 364	101.5 ppm	11:27:52	01	4.7 %	00	391.7 ppm
Scan # 365	99.3 ppm	11:27:52	01	4.7 %	00	391.5 ppm
Scan # 365	101.4 ppm	11:27:52	02	4.7 %	00	391.4 ppm
Scan # 370	101.2 ppm	11:28:22	02	4.7 %	00	391.7 ppm
Scan # 371	101.5 ppm	11:28:52	01	4.7 %	00	391.5 ppm
Scan # 372	103.0 ppm	11:29:22	01	4.7 %	00	391.4 ppm
Scan # 373	99.3 ppm	11:29:52	01	4.8 %	00	391.5 ppm
Scan # 374	102.2 ppm	11:30:22	02	4.8 %	00	391.0 ppm
Scan # 375	104.6 ppm	11:30:52	02	4.8 %	00	392.0 ppm
Scan # 376	101.5 ppm	11:31:22	02	4.7 %	00	400.7 ppm
Scan # 377	105.8 ppm	11:31:52	02	4.7 %	00	391.3 ppm
Scan # 378	99.3 ppm	11:32:22	01	4.7 %	00	391.5 ppm
Scan # 379	103.4 ppm	11:32:52	02	4.7 %	00	391.8 ppm
Scan # 380	101.7 ppm	11:33:22	01	4.8 %	00	391.9 ppm
Scan # 381	100.7 ppm	11:33:52	02	4.8 %	00	391.9 ppm
Scan # 382	105.5 ppm	11:34:22	01	4.7 %	00	393.1 ppm
Scan # 383	99.7 ppm	11:34:52	01	4.7 %	00	399.5 ppm
Scan # 384	102.4 ppm	11:35:22	02	4.7 %	00	391.2 ppm
Scan # 385	100.0 ppm	11:35:52	02	4.8 %	00	392.6 ppm
Scan # 386	99.2 ppm	11:36:22	01	4.8 %	00	391.1 ppm
Scan # 387	101.5 ppm	11:36:52	01	4.8 %	00	391.4 ppm
Scan # 388	101.7 ppm	11:37:22	01	4.8 %	00	391.4 ppm

1-	Spot # 387	11:38:01				
	AL	104.5 ppm	C1	4.7 %	00	393.7 ppm
	Spot # 388	11:38:02				
	AL	104.6 ppm	C2	4.7 %	00	394.3 ppm
	Spot # 389	11:38:03				
	AL	104.8 ppm	C1	4.7 %	00	394.7 ppm
2-	Spot # 390	11:38:11				
	AL	105.2 ppm	C2	4.7 %	00	395.9 ppm
	Spot # 391	11:38:02				
	AL	105.0 ppm	C2	4.7 %	00	397.0 ppm
	Spot # 394	11:40:01				
	AL	106.1 ppm	C1	4.7 %	00	400.4 ppm
3-	Spot # 395	11:40:52				
	AL	105.8 ppm	C2	4.7 %	00	402.9 ppm
	Spot # 396	11:41:02				
	AL	107.6 ppm	C1	4.7 %	00	396.8 ppm
	Spot # 397	11:41:52				
	AL	105.6 ppm	C2	4.7 %	00	395.8 ppm
	Spot # 398	11:42:02				
	AL	101.6 ppm	C2	4.7 %	00	397.9 ppm
	Spot # 399	11:42:52				
	AL	103.3 ppm	C2	4.7 %	00	397.7 ppm
	Spot # 400	11:43:01				
	AL	107.3 ppm	C2	4.7 %	00	401.6 ppm
4-	Spot # 401	11:43:51				
	AL	105.8 ppm	C2	4.7 %	00	395.3 ppm
	Spot # 402	11:44:01				
	AL	107.6 ppm	C2	4.7 %	00	395.6 ppm
	Spot # 403	11:44:51				
	AL	101.3 ppm	C2	4.7 %	00	396.4 ppm
5-	Spot # 404	11:45:01				
	AL	102.1 ppm	C2	4.7 %	00	393.6 ppm
	Spot # 405	11:45:52				
	AL	105.6 ppm	C2	4.7 %	00	393.0 ppm
	Spot # 406	11:46:02				
	AL	102.8 ppm	C2	4.7 %	00	394.7 ppm
	Spot # 407	11:46:52				
	AL	106.8 ppm	C2	4.7 %	00	400.5 ppm
	Spot # 408	11:47:02				
	AL	107.1 ppm	C1	4.7 %	00	397.5 ppm
	Spot # 409	11:47:52				
	AL	101.4 ppm	C1	4.7 %	00	398.3 ppm
	Spot # 410	11:48:01				

Scan # 411	106.7 ppm	11:49:52	02	4.7 %	00	401.7 ppm
Scan # 412	106.8 ppm	11:49:52	01	4.7 %	01	400.1 ppm
Scan # 413	104.2 ppm	11:49:52	02	4.7 %	01	400.1 ppm
Scan # 414	99.7 ppm	11:50:22	01	4.7 %	00	397.2 ppm
Scan # 415	102.0 ppm	11:50:52	01	4.7 %	01	398.1 ppm
Scan # 416	103.2 ppm	11:51:22	02	4.7 %	00	398.2 ppm
Scan # 417	103.0 ppm	11:51:52	02	4.7 %	01	401.0 ppm
Scan # 418	104.5 ppm	11:52:22	01	4.7 %	00	397.2 ppm
Scan # 419	104.5 ppm	11:52:52	02	4.7 %	00	395.9 ppm
Scan # 420	102.7 ppm	11:53:22	02	4.7 %	00	395.0 ppm
Scan # 421	102.5 ppm	11:53:52	02	4.7 %	00	397.6 ppm
Scan # 422	102.7 ppm	11:54:22	01	4.7 %	01	395.2 ppm
Scan # 423	103.0 ppm	11:54:52	02	4.7 %	01	400.1 ppm
Scan # 424	99.2 ppm	11:55:22	01	4.7 %	00	392.5 ppm
Scan # 425	103.5 ppm	11:55:52	02	4.7 %	00	396.0 ppm
Scan # 426	104.0 ppm	11:56:22	02	4.7 %	00	394.8 ppm
Scan # 427	101.3 ppm	11:56:52	02	4.7 %	00	395.8 ppm
Scan # 428	106.3 ppm	11:57:22	02	4.7 %	00	396.9 ppm
Scan # 429	99.6 ppm	11:57:52	01	4.7 %	01	398.6 ppm
Scan # 430	101.7 ppm	11:58:22	02	4.6 %	00	399.2 ppm
Scan # 431	101.0 ppm	11:58:52	01	4.7 %	02	401.2 ppm
Scan # 432						

Star # 411	12:00:00	101.7 ppr	01	4.7 %	00	402.0 ppr
Star # 414	12:00:22	104.7 ppr	02	4.6 %	00	397.5 ppr
Star # 431	12:01:51	102.6 ppr	01	4.7 %	00	395.4 ppr
Star # 431	12:01:22	104.6 ppr	02	4.6 %	00	395.0 ppr
Star # 437	12:01:50	101.1 ppr	01	4.7 %	01	400.4 ppr
Star # 438	12:01:22	102.3 ppr	01	4.6 %	00	394.5 ppr
Star # 439	12:02:51	104.7 ppr	02	4.6 %	00	395.3 ppr
Star # 441	12:03:22	101.7 ppr	02	4.7 %	00	400.5 ppr
Star # 441	12:03:51	101.3 ppr	02	4.7 %	00	402.8 ppr
Star # 442	12:04:21	101.7 ppr	02	4.7 %	00	397.9 ppr
Star # 443	12:04:52	103.6 ppr	02	4.7 %	00	401.6 ppr
Star # 444	12:05:22	101.7 ppr	01	4.6 %	00	401.6 ppr
Star # 445	12:05:51	104.3 ppr	02	4.7 %	00	403.7 ppr
Star # 446	12:06:21	101.6 ppr	01	4.6 %	00	400.3 ppr
Star # 447	12:06:52	103.9 ppr	01	4.6 %	00	398.8 ppr
Star # 448	12:07:21	103.6 ppr	02	4.6 %	00	400.7 ppr
Star # 449	12:07:52	105.1 ppr	02	4.6 %	00	400.1 ppr
Star # 450	12:08:22	107.0 ppr	01	4.6 %	00	404.3 ppr
Star # 451	12:08:51	107.0 ppr	01	4.6 %	00	395.6 ppr
Star # 452	12:09:22	107.0 ppr	01	4.6 %	00	397.5 ppr
Star # 453	12:09:52	107.0 ppr	02	4.6 %	00	397.9 ppr
Star # 454	12:10:21					

1-	Scan # 400	12:10:52	NOx	103.8 ppm	01	4.6 %	00	403.0 ppm
	Scan # 401	12:11:02	NOx	103.8 ppm	01	4.6 %	00	400.3 ppm
	Scan # 402	12:11:51	NOx	102.6 ppm	00	4.6 %	01	396.2 ppm
	Scan # 403	12:12:22	NOx	102.7 ppm	00	4.6 %	00	397.3 ppm
	Scan # 404	12:12:52	NOx	102.0 ppm	01	4.6 %	00	391.2 ppm
	Scan # 405	12:13:21	NOx	101.5 ppm	00	4.6 %	00	401.5 ppm
	Scan # 406	12:13:52	NOx	104.5 ppm	02	4.6 %	00	398.8 ppm
	Scan # 407	12:14:22	NOx	105.0 ppm	02	4.6 %	00	400.0 ppm
	Scan # 408	12:14:52	NOx	104.6 ppm	02	4.6 %	00	399.6 ppm
	Scan # 409	12:15:22	NOx	104.3 ppm	01	4.6 %	00	396.6 ppm
	Scan # 410	12:15:52	NOx	104.4 ppm	02	4.6 %	00	399.6 ppm
	Scan # 411	12:16:22	NOx	98.3 ppm	01	4.7 %	00	394.0 ppm
	Scan # 412	12:16:52	NOx	107.3 ppm	02	4.6 %	00	400.3 ppm
	Scan # 413	12:17:21	NOx	106.3 ppm	02	4.6 %	00	399.9 ppm
	Scan # 414	12:17:51	NOx	103.3 ppm	02	4.6 %	00	402.5 ppm
	Scan # 415	12:18:21	NOx	107.0 ppm	02	4.6 %	00	400.5 ppm
	Scan # 416	12:18:51	NOx	101.2 ppm	02	4.6 %	00	391.2 ppm
	Scan # 417	12:19:21	NOx	31.0 ppm	00	12.7 %	00	121.7 ppm
	Scan # 418	12:19:51	NOx	13.5 ppm	02	19.8 %	00	13.2 ppm
	Scan # 419	12:20:22	NOx	1.4 ppm	00	19.5 %	00	11.5 ppm
	Scan # 420	12:20:51	NOx	0.3 ppm	01	19.2 %	00	41.5 ppm
	Scan # 421	12:21:21						

End Run 5

Leak check
good
↓

Begin system
cals

Scan # 470	NO ₂	3.0 ppm	01	20.1 %	00	-0.7 ppm
Scan # 471	NO ₂	3.0 ppm	01	20.3 %	00	0.0 ppm
Scan # 472	NO ₂	3.0 ppm	01	20.3 %	00	0.5 ppm
Scan # 473	NO ₂	3.0 ppm	01	20.3 %	00	0.5 ppm
Scan # 474	NO ₂	3.0 ppm	01	20.3 %	00	0.5 ppm
Scan # 475	NO ₂	3.0 ppm	01	20.3 %	00	0.4 ppm
Scan # 476	NO ₂	2.5 ppm	01	20.7 %	00	0.0 ppm
Scan # 477	NO ₂	2.1 ppm	02	20.3 %	00	0.3 ppm
Scan # 478	NO ₂	1.5 ppm	02	20.3 %	00	0.3 ppm
Scan # 479	NO ₂	1.3 ppm	02	20.4 %	00	0.5 ppm
Scan # 480	NO ₂	1.1 ppm	02	20.3 %	00	0.3 ppm
Scan # 481	NO ₂	0.5 ppm	02	20.4 %	00	-0.1 ppm
Scan # 482	NO ₂	1.1 ppm	02	20.4 %	00	0.7 ppm
Scan # 483	NO ₂	1.4 ppm	02	20.3 %	00	0.5 ppm
Scan # 484	NO ₂	1.7 ppm	02	19.1 %	00	1.2 ppm
Scan # 485	NO ₂	1.0 ppm	02	18.1 %	00	0.3 ppm
Scan # 486	NO ₂	0.5 ppm	02	18.0 %	00	0.1 ppm
Scan # 487	NO ₂	1.8 ppm	02	18.0 %	00	0.5 ppm
Scan # 488	NO ₂	1.3 ppm	02	18.0 %	00	0.5 ppm
Scan # 489	NO ₂	1.5 ppm	02	18.0 %	00	0.5 ppm
Scan # 490	NO ₂	1.5 ppm	02	18.0 %	00	0.5 ppm
Scan # 491	NO ₂	1.5 ppm	02	7.4 %	00	399.1 ppm
Scan # 492	NO ₂					

ZRND

16.1 % O₂

64

487.0 ppm CO
O2 zero

242.0 ppm NO

1-	Scan # 500	12:32:51			
	NO	0.7 ppm	02	-0.2 %	00
					490.0 ppm
	Scan # 501	12:33:01			
	NO	0.9 ppm	02	-0.1 %	00
					490.8 ppm
	Scan # 502	12:33:51			
	NO	1.2 ppm	00	-0.1 %	00
					490.5 ppm
2-	Scan # 503	12:34:01			
	NO	0.9 ppm	02	-0.1 %	00
					490.7 ppm
	Scan # 504	12:34:51			
	NO	0.9 ppm	02	-0.1 %	00
					490.1 ppm
	Scan # 505	12:35:01			
	NO	1.4 ppm	00	-0.1 %	00
					490.6 ppm
3-	Scan # 506	12:35:51			
	NO	189.7 ppm	02	2.6 %	00
					69.3 ppm
	Scan # 507	12:36:01			
	NO	246.1 ppm	02	-0.1 %	00
					2.0 ppm
	Scan # 508	12:36:51			
	NO	246.9 ppm	02	-0.1 %	00
					0.0 ppm
	Scan # 509	12:37:01			
	NO	247.4 ppm	02	-0.1 %	00
					0.5 ppm
	Scan # 509	12:37:51			
	NO	247.6 ppm	02	-0.1 %	00
					0.3 ppm
	Scan # 510	12:38:01			
	NO	247.9 ppm	02	-0.1 %	00
					0.5 ppm
4-	Scan # 511	12:38:51			
	NO	247.9 ppm	02	-0.1 %	00
					0.2 ppm
	Scan # 512	12:39:01			
	NO	259.4 ppm	02	-0.1 %	00
					1.2 ppm
	Scan # 513	12:39:51			
	NO	40.0 ppm	02	13.3 %	00
					2.7 ppm
5-	Scan # 514	12:40:01			
	NO	5.6 ppm	02	20.4 %	00
					3.5 ppm
	Scan # 515	12:40:51			
	NO	4.3 ppm	02	20.6 %	00
					3.9 ppm
	Scan # 516	12:41:01			
	NO	4.9 ppm	02	20.6 %	00
					3.6 ppm
	Scan # 517	12:41:51			
	NO	4.8 ppm	02	20.7 %	00
					3.9 ppm
	Scan # 518	12:42:01			
	NO	4.1 ppm	00	20.7 %	00
					3.9 ppm
	Scan # 519	12:42:51			
	NO	3.2 ppm	00	20.8 %	00
					3.9 ppm
	Scan # 520	12:43:01			
	NO	3.1 ppm	00	20.8 %	00
					3.9 ppm

65

Scan # 520	12:44:01				
NOx	2.0 ppm	02	20.9 %	00	3.8 ppm
Scan # 521	12:44:01				
NOx	2.0 ppm	02	20.9 %	00	3.8 ppm
Scan # 522	12:44:01				
NOx	2.0 ppm	02	20.9 %	00	2.8 ppm
Scan # 523	12:45:01				
NOx	2.9 ppm	02	20.9 %	00	3.8 ppm
Scan # 524	12:45:01				
NOx	2.9 ppm	02	20.9 %	00	3.8 ppm
Scan # 525	12:45:01				
NOx	2.9 ppm	02	20.9 %	00	3.8 ppm
Scan # 526	12:45:01				
NOx	2.9 ppm	02	20.9 %	00	3.8 ppm
Scan # 527	12:45:01				
NOx	2.9 ppm	02	20.9 %	00	3.3 ppm
Scan # 528	12:47:01				
NOx	2.9 ppm	02	20.9 %	02	3.3 ppm
Scan # 529	12:47:01				
NOx	2.9 ppm	02	20.9 %	02	3.6 ppm
Scan # 530	12:48:01				
NOx	2.2 ppm	02	20.9 %	00	3.5 ppm
Scan # 531	12:48:01				
NOx	85.3 ppm	02	10.3 %	00	335.6 ppm
Scan # 532	12:49:01				
NOx	107.6 ppm	02	4.6 %	00	400.4 ppm
Scan # 533	12:49:01				
NOx	109.5 ppm	02	4.7 %	00	405.0 ppm
Scan # 534	12:50:01				
NOx	108.6 ppm	02	4.6 %	00	400.4 ppm
Scan # 535	12:50:01				
NOx	109.6 ppm	02	4.6 %	00	402.5 ppm
Scan # 536	12:51:01				
NOx	112.2 ppm	02	4.6 %	00	400.8 ppm
Scan # 537	12:51:01				
NOx	113.1 ppm	02	4.6 %	00	403.9 ppm
Scan # 538	12:52:01				
NOx	112.9 ppm	02	4.6 %	00	400.9 ppm
Scan # 539	12:52:01				
NOx	111.6 ppm	02	4.6 %	00	401.4 ppm
Scan # 540	12:53:01				
NOx	110.8 ppm	02	4.6 %	00	401.1 ppm
Scan # 541	12:53:01				
NOx	111.1 ppm	02	4.6 %	00	401.2 ppm
Scan # 542	12:54:01				

Begin Run 6

Spot # 540	107.6 ppt	12:55:21	02	4.6 %	00	404.6 ppt
Spot # 541	107.6 ppt	12:55:21	01	4.6 %	00	402.7 ppt
Spot # 542	107.6 ppt	12:55:51	02	4.6 %	01	399.6 ppt
Spot # 543	107.6 ppt	12:56:21	02	4.6 %	00	401.8 ppt
Spot # 544	107.6 ppt	12:56:51	02	4.6 %	00	404.4 ppt
Spot # 545	107.6 ppt	12:57:21	02	4.6 %	00	402.8 ppt
Spot # 546	107.6 ppt	12:57:51	01	4.6 %	00	399.0 ppt
Spot # 547	107.6 ppt	12:58:21	02	4.6 %	00	401.5 ppt
Spot # 548	107.6 ppt	12:58:51	02	4.6 %	00	400.5 ppt
Spot # 549	107.6 ppt	12:59:21	02	4.6 %	00	400.5 ppt
Spot # 550	107.6 ppt	12:59:51	02	4.6 %	00	396.7 ppt
Spot # 551	107.6 ppt	13:00:21	02	4.6 %	00	399.7 ppt
Spot # 552	107.6 ppt	13:00:51	02	4.6 %	00	400.9 ppt
Spot # 553	107.6 ppt	13:01:21	01	4.6 %	00	397.8 ppt
Spot # 554	107.6 ppt	13:01:51	01	4.6 %	00	399.3 ppt
Spot # 555	107.6 ppt	13:02:21	02	4.6 %	00	404.0 ppt
Spot # 556	107.6 ppt	13:02:51	02	4.6 %	00	399.3 ppt
Spot # 557	107.6 ppt	13:03:21	02	4.6 %	00	399.2 ppt
Spot # 558	107.6 ppt	13:03:51	02	4.6 %	00	402.0 ppt
Spot # 559	107.6 ppt	13:04:21	01	4.6 %	00	399.8 ppt
Spot # 560	107.6 ppt	13:04:51	01	4.6 %	00	399.4 ppt
Spot # 561	107.6 ppt	13:05:21	01	4.6 %	00	399.4 ppt

I-	Star # 565	108.1 ppm	02	4.6 %	00	399.2 ppm
	Star # 566	107.6 ppm	02	4.6 %	00	400.6 ppm
	Star # 567	107.6 ppm	02	4.6 %	00	399.8 ppm
	Star # 568	108.1 ppm	02	4.6 %	00	400.0 ppm
	Star # 569	108.3 ppm	02	4.6 %	00	401.9 ppm
	Star # 570	108.1 ppm	02	4.6 %	00	401.1 ppm
	Star # 571	108.6 ppm	02	4.6 %	00	401.6 ppm
	Star # 572	108.2 ppm	02	4.7 %	00	400.6 ppm
	Star # 573	107.2 ppm	02	4.6 %	00	401.7 ppm
	Star # 574	110.3 ppm	02	4.7 %	00	398.8 ppm
	Star # 575	109.1 ppm	02	4.6 %	00	404.6 ppm
	Star # 576	113.5 ppm	02	4.6 %	00	402.1 ppm
	Star # 577	110.8 ppm	02	4.6 %	00	400.2 ppm
	Star # 578	111.1 ppm	02	4.6 %	00	402.5 ppm
	Star # 579	111.0 ppm	02	4.6 %	00	398.6 ppm
	Star # 580	114.8 ppm	02	4.6 %	00	405.3 ppm
	Star # 581	114.1 ppm	02	4.6 %	00	404.5 ppm
	Star # 582	114.2 ppm	02	4.6 %	00	399.0 ppm
	Star # 583	114.0 ppm	02	4.6 %	00	402.3 ppm
	Star # 584	115.5 ppm	02	4.6 %	00	404.0 ppm
	Star # 585	115.5 ppm	02	4.6 %	00	401.7 ppm
	Star # 586	115.5 ppm	02	4.6 %	00	401.7 ppm

Scan # 587	112.3 ppm	01	4.6 %	00	399.2 ppm
Scan # 588	112.6 ppm	01	4.6 %	00	400.7 ppm
Scan # 589	112.9 ppm	01	4.6 %	00	402.5 ppm
Scan # 590	109.7 ppm	02	4.6 %	01	400.1 ppm
Scan # 591	109.3 ppm	01	4.6 %	00	399.7 ppm
Scan # 592	109.7 ppm	01	4.6 %	03	398.6 ppm
Scan # 593	110.8 ppm	01	4.6 %	00	401.6 ppm
Scan # 594	111.0 ppm	02	4.6 %	00	404.6 ppm
Scan # 595	109.7 ppm	02	4.6 %	00	399.4 ppm
Scan # 596	113.3 ppm	02	4.6 %	00	398.6 ppm
Scan # 597	111.6 ppm	01	4.6 %	00	402.9 ppm
Scan # 598	113.3 ppm	02	4.6 %	00	402.1 ppm
Scan # 599	112.7 ppm	02	4.6 %	00	402.2 ppm
Scan # 600	113.3 ppm	01	4.6 %	00	397.1 ppm
Scan # 601	113.6 ppm	02	4.6 %	00	399.7 ppm
Scan # 602	110.8 ppm	02	4.6 %	00	400.8 ppm
Scan # 603	113.1 ppm	02	4.6 %	00	403.7 ppm
Scan # 604	114.3 ppm	02	4.6 %	00	401.8 ppm
Scan # 605	112.6 ppm	02	4.6 %	01	402.2 ppm
Scan # 606	115.1 ppm	01	4.6 %	00	406.0 ppm
Scan # 607	110.8 ppm	01	4.6 %	00	399.6 ppm
Scan # 608					

L	Scan # 608	13:17:51			
	Alt	110.0 ppm	01	4.6 %	00 199.4 ppm
	Scan # 609	13:28:21			
	Alt	111.1 ppm	01	4.6 %	01 391.8 ppm
	Scan # 611	13:28:51			
	Alt	110.6 ppm	02	4.6 %	00 399.2 ppm
M	Scan # 612	13:29:21			
	Alt	115.0 ppm	01	4.6 %	00 400.9 ppm
	Scan # 613	13:29:51			
	Alt	113.8 ppm	01	4.6 %	00 400.2 ppm
	Scan # 614	13:30:21			
	Alt	114.8 ppm	02	4.6 %	01 400.4 ppm
N	Scan # 615	13:30:51			
	Alt	115.5 ppm	01	4.6 %	00 397.0 ppm
	Scan # 616	13:31:21			
	Alt	109.0 ppm	02	4.6 %	00 403.3 ppm
	Scan # 617	13:31:51			
	Alt	110.0 ppm	02	4.6 %	00 397.7 ppm
	Scan # 618	13:32:21			
	Alt	110.3 ppm	02	4.6 %	00 397.7 ppm
	Scan # 619	13:32:51			
	Alt	107.7 ppm	02	4.6 %	00 396.8 ppm
	Scan # 620	13:33:21			
	Alt	110.3 ppm	01	4.6 %	00 400.6 ppm
L	Scan # 621	13:33:51			
	Alt	105.3 ppm	02	4.7 %	00 398.0 ppm
	Scan # 622	13:34:21			
	Alt	112.8 ppm	01	4.6 %	00 401.4 ppm
	Scan # 623	13:34:51			
	Alt	111.1 ppm	02	4.6 %	00 401.6 ppm
M	Scan # 624	13:35:21			
	Alt	116.8 ppm	02	4.6 %	00 405.2 ppm
	Scan # 625	13:35:51			
	Alt	111.2 ppm	02	4.6 %	00 397.7 ppm
	Scan # 626	13:36:21			
	Alt	109.3 ppm	02	4.6 %	00 400.2 ppm
	Scan # 627	13:36:51			
	Alt	112.8 ppm	01	4.6 %	00 397.2 ppm
	Scan # 628	13:37:21			
	Alt	117.1 ppm	01	4.6 %	00 399.4 ppm
	Scan # 629	13:37:51			
	Alt	117.3 ppm	01	4.6 %	00 397.9 ppm
	Scan # 630	13:38:21			
	Alt				

L	Scan # 631	113.1 ppm	13:39:51	01	4.6 %	00	399.6 ppm
	NOL						
	Scan # 632	110.5 ppm	13:39:52	02	4.6 %	00	400.1 ppm
	NOL						
	Scan # 633	117.1 ppm	13:39:53	00	4.6 %	00	399.4 ppm
	NOL						
M	Scan # 634	112.1 ppm	13:40:01	02	4.6 %	00	399.2 ppm
	NOL						
	Scan # 635	109.5 ppm	13:40:51	01	4.6 %	00	397.7 ppm
	NOL						
	Scan # 636	109.2 ppm	13:41:21	02	4.6 %	00	401.0 ppm
	NOL						
N	Scan # 637	110.0 ppm	13:41:51	02	4.6 %	00	397.8 ppm
	NOL						
	Scan # 638	107.0 ppm	13:42:21	02	4.6 %	00	397.8 ppm
	NOL						
	Scan # 639	107.9 ppm	13:42:51	02	4.6 %	00	401.6 ppm
	NOL						
	Scan # 640	113.7 ppm	13:43:21	02	4.6 %	00	400.6 ppm
	NOL						
	Scan # 641	111.7 ppm	13:43:51	02	4.6 %	00	404.5 ppm
	NOL						
	Scan # 642	112.3 ppm	13:44:21	01	4.6 %	00	401.6 ppm
	NOL						
O	Scan # 643	109.2 ppm	13:44:51	02	4.6 %	00	401.0 ppm
	NOL						
	Scan # 644	107.5 ppm	13:45:21	01	4.6 %	00	399.7 ppm
	NOL						
	Scan # 645	112.3 ppm	13:45:51	02	4.6 %	00	403.3 ppm
	NOL						
P	Scan # 646	109.8 ppm	13:46:21	02	4.6 %	00	401.7 ppm
	NOL						
	Scan # 647	110.3 ppm	13:46:51	02	4.6 %	00	399.1 ppm
	NOL						
	Scan # 648	111.0 ppm	13:47:21	00	4.6 %	00	399.5 ppm
	NOL						
	Scan # 649	111.1 ppm	13:47:51	02	4.6 %	00	404.4 ppm
	NOL						
	Scan # 650	109.0 ppm	13:48:21	01	4.6 %	00	401.1 ppm
	NOL						
	Scan # 651	111.0 ppm	13:48:51	00	4.6 %	00	399.8 ppm
	NOL						
	Scan # 652	111.0 ppm	13:49:21	00	4.6 %	00	399.8 ppm
	NOL						

L

Scan # 654	111.5 ppm	02	4.6 %	00	397.4 ppm
NO ₂					
Scan # 655	111.5 ppm	02	4.6 %	00	400.3 ppm
NO ₂					

End Run 6

T

Scan # 656	112.2 ppm	02	4.6 %	00	397.1 ppm
NO ₂					
Scan # 657	108.8 ppm	02	4.6 %	00	396.5 ppm
NO ₂					

Q

Scan # 658	23.9 ppm	02	16.5 %	00	57.6 ppm
NO ₂					
Scan # 659	11.2 ppm	01	20.4 %	00	5.2 ppm
NO ₂					

Leak check
good



Q

Scan # 660	10.3 ppm	02	20.7 %	00	4.2 ppm
NO ₂					
Scan # 661	9.4 ppm	02	20.7 %	00	6.2 ppm
NO ₂					

Q

Scan # 662	1.7 ppm	02	20.6 %	00	9.1 ppm
NO ₂					
Scan # 663	0.7 ppm	02	20.5 %	00	12.6 ppm
NO ₂					

Scan # 664	0.6 ppm	02	20.5 %	00	11.8 ppm
NO ₂					
Scan # 665	31.8 ppm	02	20.1 %	00	12.2 ppm
NO ₂					

Scan # 666	10.3 ppm	02	20.3 %	00	3.0 ppm
NO ₂					
Scan # 667	0.3 ppm	02	20.2 %	00	1.1 ppm
NO ₂					

Scan # 668	6.0 ppm	02	20.3 %	00	0.8 ppm
NO ₂					
Scan # 669	3.7 ppm	02	20.3 %	00	0.8 ppm
NO ₂					

Scan # 670	3.2 ppm	02	20.3 %	00	1.6 ppm
NO ₂					
Scan # 671	3.0 ppm	02	20.3 %	00	0.8 ppm
NO ₂					

Scan # 672	2.8 ppm	02	20.3 %	00	1.4 ppm
NO ₂					
Scan # 673	2.5 ppm	02	20.3 %	00	0.8 ppm
NO ₂					

Scan # 674	2.3 ppm	01	20.3 %	00	1.4 ppm
NO ₂					
Scan # 675	1.5 ppm	02			
NO ₂					

1	Scan # 670	14:01:01	2.0 ppm	02	20.3 %	00	0.7 ppm
	NOx						
	Scan # 671	14:01:21	1.7 ppm	01	20.3 %	00	1.4 ppm
	NOx						
	Scan # 677	14:01:51	1.8 ppm	02	20.3 %	00	0.9 ppm
	NOx						
	Scan # 678	14:02:21	2.0 ppm	02	20.3 %	00	1.3 ppm
	NOx						
	Scan # 679	14:02:51	2.2 ppm	02	19.2 %	00	2.2 ppm
	NOx						
	Scan # 680	14:03:21	1.8 ppm	02	16.0 %	00	1.3 ppm
	NOx						
	Scan # 681	14:03:51	1.8 ppm	02	15.9 %	00	1.0 ppm
	NOx						
	Scan # 682	14:04:21	1.9 ppm	02	15.9 %	00	1.1 ppm
	NOx						
	Scan # 683	14:04:51	1.5 ppm	02	15.9 %	00	1.2 ppm
	NOx						
	Scan # 684	14:05:21	1.6 ppm	02	15.9 %	00	1.9 ppm
	NOx						
	Scan # 685	14:05:51	1.3 ppm	02	15.9 %	00	1.2 ppm
	NOx						
	Scan # 686	14:06:21	2.2 ppm	02	16.0 %	00	1.8 ppm
	NOx						
	Scan # 687	14:06:51	1.5 ppm	02	1.6 %	00	471.5 ppm
	NOx						
	Scan # 688	14:07:21	1.3 ppm	02	-0.0 %	00	494.8 ppm
	NOx						
	Scan # 689	14:07:51	1.1 ppm	02	-0.1 %	00	495.2 ppm
	NOx						
	Scan # 690	14:08:21	1.0 ppm	02	-0.1 %	00	495.4 ppm
	NOx						
	Scan # 691	14:08:51	0.9 ppm	02	-0.1 %	00	495.6 ppm
	NOx						
	Scan # 692	14:09:21	1.1 ppm	02	-0.2 %	00	496.3 ppm
	NOx						
	Scan # 693	14:09:51	1.3 ppm	02	-0.1 %	00	496.5 ppm
	NOx						
	Scan # 694	14:10:21	206.1 ppm	01	2.0 %	00	49.7 ppm
	NOx						
	Scan # 695	14:10:51	243.9 ppm	01	-0.1 %	00	1.9 ppm
	NOx						
	Scan # 696	14:11:21					
	NOx						

zero

72

16.1 % O₂

487.0 ppm CO

Star #	697	14:12:21	01	-0.1 %	00	1.6 ppm
NO	245.8 ppm		01	-0.1 %	00	2.0 ppm
Star #	699	14:12:51				
NO	245.8 ppm		01	-0.1 %	00	1.7 ppm
Star #	700	14:13:21				
NO	242.4 ppm		01	-0.1 %	00	2.7 ppm
Star #	701	14:13:51				
NO	105.3 ppm		02	7.1 %	00	3.2 ppm
Star #	702	14:14:21				
NO	3.5 ppm		02	2.4 %	00	3.0 ppm
Star #	703	14:14:51				
NO	1.6 ppm		00	20.8 %	00	4.5 ppm
Star #	704	14:15:21				
NO	1.9 ppm		03	20.8 %	00	3.2 ppm
Star #	705	14:15:51				
NO	1.5 ppm		01	20.8 %	00	4.9 ppm
Star #	706	14:16:21				
NO	0.1 ppm		00	20.8 %	00	4.2 ppm
Star #	707	14:16:51				
NO	-0.1 ppm		00	20.8 %	00	4.5 ppm
Star #	708	14:17:21				
NO	-0.1 ppm		00	20.8 %	00	3.5 ppm
Star #	709	14:17:51				
NO	-0.5 ppm		01	20.8 %	00	3.7 ppm

242.0 ppm
NO

73
of
73

End ET
10/7/92

APPENDIX D
Equipment Calibrations
and
EPA Protocol 1 Certification Sheets

METHOD 5 MODULE CALIBRATION

DATE 10/19/92 ORIFICE/MODULE NO. 2827 NAME TEC
 BAROMETRIC PRESSURE P_b 30.20 In Hg STANDARD METER 570415

Post test

MODULE ORIFICE SETTING ΔH (In. H ₂ O)	STANDARD METER			MODULE METER				γ	ΔH_a (In. H ₂ O)	Module Flowrate Q (SCFH)	OF
	Volume V_s (ft ³)	Factor Y_s	Temperature t_s (°F)	Pressure ΔP_s (In. H ₂ O)	Volume V_m (ft ³)	Temperature t_m (°F)	Time θ (min)				
0.5	5.002	1.0001	55	-0.11	5.170	77	64	13.73	1.97	.3919	
1.0	5.000	1.0001	55	-0.12	5.130	77	66	9.42	1.85	.5686	
1.5	10.002	1.0001	57	-0.12	10.246	81	68	15.83	1.96	.6778	
2.0	10.000	1.0001	57	-0.16	10.260	84	71	13.60	1.92	.7955	
3.0	10.004	1.0001	58	-0.16	10.271	86	72	10.80	1.84	1.0061	
								AVERAGE: 9961	1.90		

CHECK:

FOR CHECK, USE THE AVERAGE ΔH_a FOR ΔH

$$\gamma = \frac{V_s (P_b + P_s) (T_m + 460) Y_s}{13.6 V_m (P_b + \Delta H) (t_m + 460)}$$

$$\Delta H_a = \left[\frac{(0.0317) \Delta H}{P_b (t_m + 460)} \right] \left[\frac{(t_s + 460) \theta}{V_s Y_s} \right]^2$$

$$Q = \gamma (17.64) V_m \left[\frac{P_b + \Delta H}{13.6} \right] \left[\frac{(t_m + 460) \theta}{(t_s + 460) \theta} \right]$$

$$OF = \text{orifice factor} = \left[\frac{(t_m + 460) \Delta H}{P_b} \right]^{1/2}$$

ACCEPTANCE CRITERIA:

Each γ must be 1.00 ± 0.01
 Average ΔH_a must be 1.04 ± 0.25
 Each ΔH_a must be within 0.15 of the average ΔH_a

$$\text{Correlation Line Equation}$$

$$Q = a (OF) + b$$

$$Q = \text{ } OF + \text{ }$$

TC Readout Calibrated with Constant Voltage Source
 t_m 57 of two 57 of Reference Thermometer 57 of
 Module Leak Check 0.00 10" Hg
 Heater Box Love Control OK Probe Heater Low Control ✓
 Module Cleaned ✓ Pitot tube manometer leak check ✓

Calibrated and checked by Steve Long Date 10/19/92
 Reviewed by Steve Long Date 10/19/92

METHOD 5 MODULE CALIBRATION

DATE 9/25/92 ORIFICE/MODULE NO. 2827 NAME TEC Pre-test
 BAROMETRIC PRESSURE P_b 30.45 In Hg STANDARD METER 570415

MODULE ORIFICE SETTING ΔH (In. H ₂ O)	STANDARD METER			MODULE METER				ΔH_a (In. H ₂ O)	Module Flowrate Q (SCFH)	OF
	Volume V_m (ft ³)	Factor Y_b	Temperature t_m (°F)	Pressure ΔP_s (In. H ₂ O)	Volume V_m (ft ³)	Temperatures t_m (°F)	Time θ (min)			
0.5	5.000	1.0001	63	-0.11	5.150	69	78	1.77	4.154	
1.0	5.009	1.0001	63	-0.12	5.163	71	79	1.65	6.102	
1.5	10.003	1.0001	63	-0.14	10.323	72	84	1.82	7.148	
2.0	10.004	1.0001	63	-0.15	10.326	73	85	1.88	8.150	
3.0	10.005	1.0001	63	-0.16	10.367	74	87	1.83	10.135	
								AVERAGE 1.0014	1.77	

CHECK:

FOR CHECK, USE THE AVERAGE ΔH_a FOR ΔH

$$Y = V_s (P_b + \frac{P_s}{13.6}) (T_m + 460) Y_b$$

$$\frac{V_m (P_b + \frac{\Delta H}{13.6}) (T_m + 460)}{13.6}$$

$$\Delta H_a = \left[\frac{(0.0317) \Delta H}{P_b (t_m + 460)} \right] \left[\frac{(t_s + 460) \theta}{V_s Y_b} \right]^2$$

$$Q = Y (17.64) V_m \left[\frac{P_b + \frac{\Delta H}{13.6}}{(t_m + 460) \theta} \right]$$

$$\text{OF} = \text{orifice factor} = \left[\frac{(t_m + 460) \Delta H}{P_b} \right]^{1/2}$$

ACCEPTANCE CRITERIA:

Each Y must be 1.00 ± 0.01
 Average ΔH_a must be 1.04 ± 0.25
 Each ΔH_a must be within 0.15 of the average ΔH_a

Correlation Line Equation
 $Q = m (\text{OF}) + b$

$Q =$ _____ OF + _____

TC readout Calibrated with Constant Voltage Source
 tml 6.3 of two 6.3 of Reference Thermometer 6.3 of
 Module Leak Check 0.00 12 HG
 Heater Box Love Control OK ☒ Pilot tube manometer leak check ☒
 Module Cleaned ☒

Calibrated and Checked by TC Date 9/25/92
 Reviewed by TEC Date 9/25/92

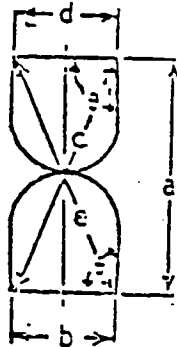
S-TYPE PITOT GEOMETRIC CALIBRATION PART 2 - PITOT ALIGNMENT

Probe Identification 401
Technical Specialist TEC
Date 11/27/91

Pitot Identification 401

A.

Transverse
Tube Axis



a 1.237
b .337
c 1.324
d .390
e 1.325
e' .89
e' .89

$$\frac{a^2 + b^2 - c^2}{2ad} = \cos \theta$$

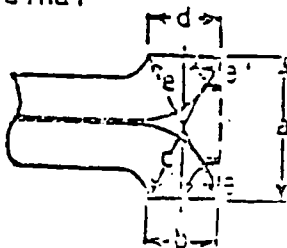
$$\frac{a^2 + d^2 - e^2}{2ed} = \cos \theta'$$

$$(80^\circ < \theta < 100^\circ)$$

$$(80^\circ < \theta' < 100^\circ)$$

B.

Longitudinal
Tube Axis



a 1.237
b .469
c 1.324
d .566
e 1.325
e' .89
e' .89

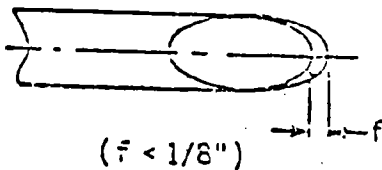
$$\frac{a^2 + b^2 - c^2}{2ad} = \cos \theta$$

$$\frac{a^2 + d^2 - e^2}{2ed} = \cos \theta'$$

$$(35^\circ < \theta < 95^\circ)$$

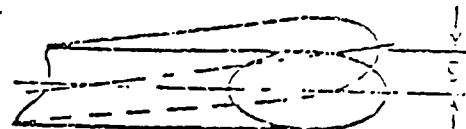
$$(35^\circ < \theta' < 95^\circ)$$

C.



(f < 1/8")

D.



(g < 1/32")

NOTE: values in parentheses are EPA Method 2 specifications.

PROBE THERMOCOUPLE CALIBRATION

Expected Stack Temperature (T_s) _____ or _____

Mercury Thermometer (T_{ref}) _____ or _____

Thermocouple Readout _____ or _____

Probe Identification _____

Technician _____

Date _____

Tolerances

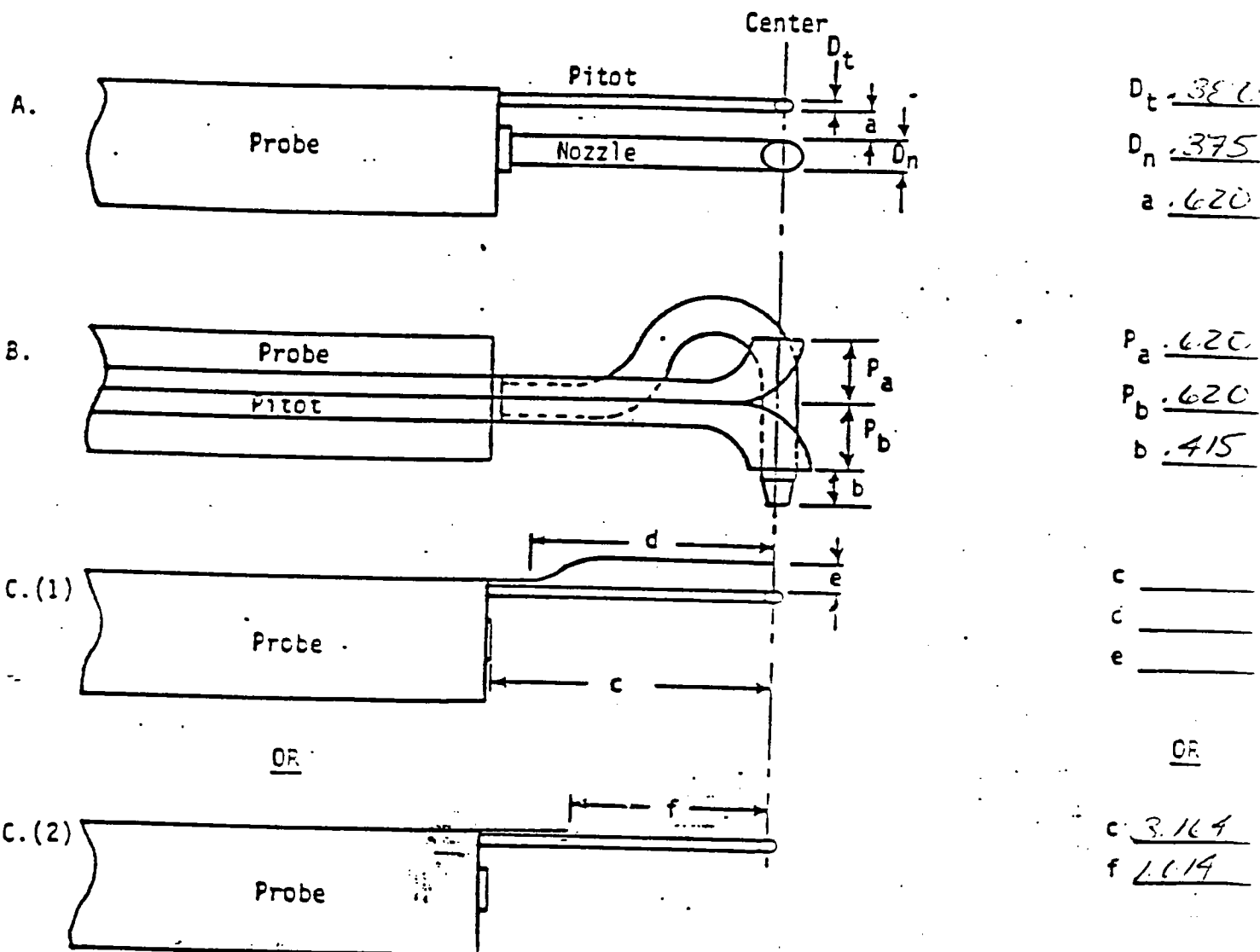
$$(T_s \pm 10\%)$$

$$(T_{ref} \pm 1.5\%)$$

S-TYPE PITOT GEOMETRIC CALIBRATION PART 1 - PROBE CONFIGURATION

Probe Identification 401
Technical Specialist TEC
Date 11/27/91

Pitot Identification 401



Specifications (EPA Method 2)

$D_t = 3/16"$ to $3/8"$
 $D_n = 1/2"$
 $a \geq 3/4"$
 $b \geq 0$

$c \geq 3"$
 $d \geq 3"$
 $e \geq 3/4"$
 $f \geq 2"$

$P_a = P_b$

$1.05 D_t \leq P \leq 1.50 D_t$

If these specifications are met, proceed with Part 2 Pitot alignment

NBS TRACEABLE GAS MIXTURES

The mixture(s) described below are manufactured and certified traceable to the National Bureau of Standards, Standards Reference Materials (NBS, SRM) via the Traceability Protocol for establishing true concentrations of gases used for calibration and audits of continuous Source Emission Monitors (Protocol No. 1) or Air Pollution Analyzers (Protocol No. 2)

ANALYSIS REPORT

Per Protocol Number 1

Control Number 88-18539

Cylinder Number SX-19977

Preparation Date: 07/08/92

Minor Component Oxygen

Mean Concentration 16.1%

REPLICATE ANALYSIS DATA	DATE	ANALYSIS	MEAN
	<u>07/08/92</u>	<u>16.1%</u>	
	<u></u>	<u>16.1%</u>	
	<u></u>	<u>16.2%</u>	<u>16.1%</u>
REPLICATE ANALYSIS DATA	<u></u>	<u></u>	<u></u>
	<u></u>	<u></u>	<u></u>
	<u></u>	<u></u>	<u></u>

Balance Gas Nitrogen

NBS SRM Numbers Used 2659A

Analytical Principle Used Beckman Paramagnetic

Expiration Date 01/08/94

Matheson
Gas Products

World Leader in Specialty Gases & Equipment

P.O. Box 85, East Rutherford, N.J. 07073

Dale Dickey Analyst

NOTEBOOK REFERENCE

NBS TRACEABLE GAS MIXTURES

The mixture(s) described below are manufactured and certified traceable to the National Bureau of Standards, Standards Reference Materials (NBS, SRM) via the Traceability Protocol for establishing true concentrations of gases used for calibration and audits of continuous Source Emission Monitors (Protocol No. 1) or Air Pollution Analyzers (Protocol No. 2)

ANALYSIS REPORT

Per Protocol Number 1

Control Number 88-16516

Cylinder Number SX-16386

Preparation Date: 2/13/92

Minor Component Nitric Oxide

Mean Concentration 97.5PPM

REPLICATE ANALYSIS DATA	DATE	ANALYSIS	MEAN
	<u>2/13/92</u>	<u>97.4PPM</u>	
		<u>97.5PPM</u>	
		<u>97.5PPM</u>	<u>97.5PPM</u>
REPLICATE ANALYSIS DATA	<u>3/16/92</u>	<u>97.5PPM</u>	
		<u>97.4PPM</u>	
		<u>97.4PPM</u>	<u>97.5PPM</u>

Balance Gas Nitrogen

NBS SRM Numbers Used 1684B

Analytical Principle Used Beckman Chemiluminescent

Expiration Date 9/16/93

Katheson
Gas Products

World Leader in Specialty Gases & Equipment

P.O. Box 85, East Rutherford, N.J. 07073

Dale Diller Analyst

NOTEBOOK REFERENCE

NBS TRACEABLE GAS MIXTURES

The mixture(s) described below are manufactured and certified traceable to the National Bureau of Standards, Standards Reference Materials (NBS, SRM) via the Traceability Protocol for establishing true concentrations of gases used for calibration and audits of continuous Source Emission Monitors (Protocol No. 1) or Air Pollution Analyzers (Protocol No. 2)

ANALYSIS REPORT

Per Protocol Number 1

Control Number 88-16446

Cylinder Number SX-24321

Preparation Date: 03/04/92

Minor Component Nitric Oxide

Mean Concentration 242PPM

REPLICATE ANALYSIS DATA	DATE	ANALYSIS	MEAN
	<u>03/04/92</u>	<u>245PPM</u>	
		<u>243PPM</u>	
		<u>241PPM</u>	<u>242PPM</u>
REPLICATE ANALYSIS DATA	<u>03/11/92</u>	<u>240PPM</u>	
		<u>243PPM</u>	
		<u>241PPM</u>	<u>242PPM</u>

Balance Gas Nitrogen

NBS SRM Numbers Used 1685

Analytical Principle Used Beckman Chemiluminescent

Expiration Date 09/11/93

Matheson
Gas Products

World Leader in Specialty Gases & Equipment

P.O. Box 85, East Rutherford, N.J. 07073

Dale Duccio Analyst

NOTEBOOK REFERENCE

NBS TRACEABLE GAS MIXTURES

The mixture(s) described below are manufactured and certified traceable to the National Bureau of Standards, Standards Reference Materials (NBS, SRM) via the Traceability Protocol for establishing true concentrations of gases used for calibration and audits of continuous Source Emission Monitors (Protocol No. 1) or Air Pollution Analyzers (Protocol No. 2)

ANALYSIS REPORT

Per Protocol Number 1

Control Number 88-16443

Cylinder Number SX-24308

Preparation Date: 03/04/92

Minor Component Nitric Oxide

Mean Concentration 480PPM

REPLICATE ANALYSIS DATA	DATE	ANALYSIS	MEAN
	<u>03/04/92</u>	<u>481PPM</u>	
	<u> </u>	<u>478PPM</u>	
	<u> </u>	<u>475PPM</u>	<u>480PPM</u>
REPLICATE ANALYSIS DATA	<u>03/11/92</u>	<u>487PPM</u>	
	<u> </u>	<u>480PPM</u>	
	<u> </u>	<u>478PPM</u>	<u>480PPM</u>

Balance Gas Nitrogen

NBS SRM Numbers Used 1686B

Analytical Principle Used Beckman Chemiluminescent

Expiration Date 09/11/93

Matheson
Gas Products
World Leader in Specialty Gases & Equipment

P.O. Box 85, East Rutherford, N.J. 07073

Paul D. Dineen Analyst
NOTEBOOK REFERENCE

NBS TRACEABLE GAS MIXTURES

The mixture(s) described below are manufactured and certified traceable to the National Bureau of Standards, Standards Reference Materials (NBS, SRM) via the Traceability Protocol for establishing true concentrations of gases used for calibration and audits of continuous Source Emission Monitors (Protocol No. 1) or Air Pollution Analyzers (Protocol No. 2)

ANALYSIS REPORT

Per Protocol Number 1

Control Number 88-14469

Cylinder Number SX22708

Preparation Date: 10-25-91

Minor Component Carbon Monoxide

Mean Concentration 141PPM

REPLICATE ANALYSIS DATA

DATE

ANALYSIS

MEAN

10-25-91

141PPM

142PPM

142PPM

141PPM

REPLICATE ANALYSIS DATA

11-01-91

141PPM

141PPM

140PPM

141PPM

Balance Gas Nitrogen

NBS SRM Numbers Used 2636A

Analytical Principle Used Beckman NDIR

Expiration Date 5/1/93

Matheson
Gas Products
World Leader in Specialty Gases & Equipment

P.O. Box 85, East Rutherford, N.J. 07073

Dale G. Lutz Analyst

NOTEBOOK REFERENCE

NBS TRACEABLE GAS MIXTURES

The mixture(s) described below are manufactured and certified traceable to the National Bureau of Standards, Standards Reference Materials (NBS, SRM) via the Traceability Protocol for establishing true concentrations of gases used for calibration and audits of continuous Source Emission Monitors (Protocol No. 1) or Air Pollution Analyzers (Protocol No. 2)

ANALYSIS REPORT

Per Protocol Number 1

Control Number 88-15792

Cylinder Number SX-24302

Preparation Date: 1/28/92

Minor Component Carbon Monoxide

Mean Concentration 284PPM

REPLICATE ANALYSIS DATA	DATE	ANALYSIS	MEAN
	<u>01/28/92</u>	<u>284PPM</u>	
		<u>284PPM</u>	
		<u>285PPM</u>	<u>284PPM</u>
REPLICATE ANALYSIS DATA	<u>02/04/92</u>	<u>285PPM</u>	
		<u>284PPM</u>	
		<u>284PPM</u>	<u>284PPM</u>

Balance Gas Nitrogen

NBS SRM Numbers Used 2636A

Analytical Principle Used Beckman NDIR

Expiration Date 08/04/93

Katheson
Gas Products

World Leader in Specialty Gases & Equipment

P.O. Box 85, East Rutherford, N.J. 07073

Dale Dickey Analyst
NOTEBOOK REFERENCE



World Leader in Specialty Gases & Equipment

POST OFFICE BOX 85

EAST RUTHERFORD, NEW JERSEY 07073

TELEPHONE: (201) 933-2400

ABCO WELDING & INDUSTRIAL SUPPLY
130 CROSS ROAD
WATERFORD, CONNECTITUCT 06385

Date SEPTEMBER 11, 1992

Our Invoice # 101-89273

Your P.O. # 08-126-BAL

Ref. No. 952/953/954/955

Gentlemen:

Below are the results you requested as reported by our laboratory. Results are in molecular percent, unless otherwise indicated.

LABORATORY REPORT ON GAS CERTIFICATION

Cyl. # SX-11334

Mixture Req.

Certification

CARBON MONOXIDE C.P. 487PPM + 4.8PPM

NITROGEN PREP. BALANCE

Cyl. # SX-19848

Mixture Req.

Certification

CARBON MONOXIDE C.P. 1195PPM + 11

NITROGEN PREP. BALANCE

CYL.# SX-213611

CARBON MONOXIDE C.P. 2199PPM + 22PPM

NITROGEN PREP. BALANCE

CYL.# SX-21373

CARBON MONOXIDE C.P. 4887PPM + 48PPM

NITROGEN PREP. BALANCE

Analyst

JEFF MARSHALL

JM:p

APPENDIX E
Laboratory Analysis Reports
and
Analytical Data Sheets

LABORATORY ANALYSIS REPORT

Environmental Health Laboratory
a division of CIGNA Loss Control Services, Inc.

94 Murphy Road
Hartford, CT 06114
(800) 243-4903
In CT (203) 522-3814

Laboratories In Macon, GA and Hartford, CT



To: John Gammie
ROJAC Environmental Services, Inc.
30 Arbor Street
Hartford, CT 06106

Report No.: 92J1042
P.O. No.: 092-09
Date Received: 10/08/92
Date Reported: 10/16/92

Analysis: Total Particulates
Analytical Method: EPA Method #5

Sample Number	Total Particulates on Filter (g)	Total Particulates in Wash (g)	
M5-1 Filter	0.0026	---	
M5-2 Filter	-0.0002 (av)	---	
M5-3 Filter	0.0013	---	
M5-4 Filter	-0.0009 (av)	---	
M5-5 Filter	0.0008	---	
M5-6 Filter	0.0011	---	
			<u>Total mg</u>
M5-1 AR	---	0.0037	6.3
M5-2 AR	---	0.0050	5.0
M5-3 AR	---	0.0022	3.5
M5-4 AR	---	0.0025	2.5
M5-5 AR	---	0.0008	1.6
M5-6 AR	---	0.0011	2.2
Acetone Blank	---	0.0008	

Analytical results for the acetone rinses have been corrected for the acetone blank reading.

Analyst: Bill Rowe  Date 10/16/92

< = Less than.

92-J1042

ROJAC

Environmental Services, Inc.

SUBMITTAL FOR LABORATORY ANALYSISRECEIVED
HARTFORD, CT

OCT 08 1992

STANDARD SPECTRA
JEMTO: GIGNAFROM: JOHN GAMMIEDATE: 10-8-92PROJECT NO.: 092-09

<u>SAMPLE TYPE</u>	<u>SAMPLE ID</u>	<u>ANALYSIS</u>
✓ Filter	MS-1	MS
✓ "	MS-2	Gravimetric
✓ "	MS-3	↓
✓ "	MS-4	
✓ "	MS-5	
✓ "	MS-6	
✓ Acetone Rinse	MS-1 AR	
✓	MS-2 AR	
✓	MS-3 AR	
✓	MS-4 AR	
✓	MS-5 AR	
✓	MS-6 AR	
✓ Acetone Blank	Blank	

ANALYTICAL DATA

PLANT Oceanside Landfill
 DATE 10/6/92
 SAMPLING LOCATION Engine 007 - outlet
 SAMPLE TYPE MS
 RUN NUMBER MS-1
 SAMPLE BOX NUMBER _____
 CLEAN-UP MAN JSG

COMMENTS: 100% load

FRONT HALF

LABORATORY RESULTS

ACETONE WASH OF NOZZLE, PROBE, CYCLONE (BYPASS),
 FLASK, FRONT HALF OF FILTER HOLDER

CONTAINER Filter 2.6 mg

FILTER NUMBER RQAT146 0.6121 T.W.

CONTAINER AR 3.7 mg

FRONT HALF SUBTOTAL 6.3 mg

BACK HALF

IMPINGER CONTENTS AND WATER WASH OF
 IMPINGERS, CONNECTORS, AND BACK
 HALF OF FILTER HOLDER

CONTAINER _____ mg

ETHER-CHLOROFORM
 EXTRACTION _____ mg

ACETONE WASH OF IMPINGERS, CONNECTORS,
 AND BACK HALF OF FILTER HOLDER

CONTAINER _____ mg

BACK HALF SUBTOTAL _____ mg

TOTAL WEIGHT _____ mg

MOISTURE

IMPINGERS

FINAL VOLUME _____ ml
 INITIAL VOLUME _____ ml
 NET VOLUME _____ ml

SILICA GEL

FINAL WEIGHT _____ g
 INITIAL WEIGHT _____ g
 NET WEIGHT _____ g

TOTAL MOISTURE _____ %

EPA (Dev) 231

ANALYTICAL DATA

PLANT Oceanside Landfill
 DATE 10/6/92
 SAMPLING LOCATION Engine 007 - outlet
 SAMPLE TYPE MS
 RUN NUMBER MS-2
 SAMPLE BOX NUMBER _____
 CLEAN-UP MAN JSG

COMMENTS: 100% load

FRONT HALF

LABORATORY RESULTS

ACETONE WASH OF NOZZLE, PROBE, CYCLONE (BYPASS),
 FLASK, FRONT HALF OF FILTER HOLDER

CONTAINER Filter 0.0 mg

FILTER NUMBER RQAT147 0.6022 T.W.

CONTAINER BR 5.0 mg

FRONT HALF SUBTOTAL 5.0 mg

BACK HALF

IMPINGERS CONTENTS AND WATER WASH OF
 IMPINGERS, CONNECTORS AND BACK
 HALF OF FILTER HOLDER

CONTAINER _____ mg

ETHER-CHLOROFORM
 EXTRACTION _____ mg

ACETONE WASH OF IMPINGERS, CONNECTORS,
 AND BACK HALF OF FILTER HOLDER

CONTAINER _____ mg

BACK HALF SUBTOTAL _____ mg

TOTAL WEIGHT _____ mg

MOISTURE

IMPINGERS

FINAL VOLUME _____ ml

INITIAL VOLUME _____ ml

NET VOLUME _____ ml

SILICA GEL

FINAL WEIGHT _____ g _____ g _____ g

INITIAL WEIGHT _____ g _____ g _____ g

NET WEIGHT _____ g _____ g _____ g

TOTAL MOISTURE _____ %

EPA (Rev) 231

4.72

ANALYTICAL DATA

PLANT Oceanside Landfill
 DATE 10/6/92
 SAMPLING LOCATION Engine 007 - outlet
 SAMPLE TYPE MS
 RUN NUMBER MS-3
 SAMPLE BOX NUMBER _____
 CLEAN-UP MAN JSG

COMMENTS: 100% load

FRONT HALF

LABORATORY RESULTS

ACETONE WASH OF NOZZLE, PROBE, CYCLONE (BYPASS),
 FLASK, FRONT HALF OF FILTER HOLDER

CONTAINER Filter 1.3 g

FILTER NUMBER RQAT148 T.W.
0.6011

CONTAINER AR 2.2 g

FRONT HALF SUBTOTAL 3.5 g

BACK HALF

IMPINGER CONTENTS AND WATER WASH OF
 IMPINGERS, CONNECTORS, AND BACK
 HALF OF FILTER HOLDER

CONTAINER _____ g

TYPE-CHLOROFORM
 EXTRACTION _____ g

ACETONE WASH OF IMPINGERS, CONNECTORS,
 AND BACK HALF OF FILTER HOLDER

CONTAINER _____ g

BACK HALF SUBTOTAL _____ g

TOTAL WEIGHT _____ g

MOISTURE

IMPINGERS

FINAL VOLUME _____ ml

INITIAL VOLUME _____ ml

NET VOLUME _____ ml

SILICA GEL

FINAL WEIGHT _____ g _____ g _____ g

INITIAL WEIGHT _____ g _____ g _____ g

NET WEIGHT _____ g _____ g _____ g

TOTAL MOISTURE _____ %

EPA (D-1) 231

4.72

ANALYTICAL DATA

PLANT Oceanside Landfill
 DATE 10/7/92
 SAMPLING LOCATION Engine 007 - outlet
 SAMPLE TYPE MS
 RUN NUMBER MS-4
 SAMPLE BOX NUMBER _____
 CLEAN-UP MAN JSG

COMMENTS: 75% loadFRONT HALF

LABORATORY RESULTS

ACETONE WASH OF NOZZLE, PROBE, CYCLONE (BYPASS),
 FLASK, FRONT HALF OF FILTER HOLDER

CONTAINER Filter0.0 mg

FILTER NUMBER RQAT149 0.5990 T.W.

CONTAINER AR2.5 mgFRONT HALF SUBTOTAL 2.5 mgBACK HALF

IMPINGERS CONTENTS AND WATER WASH OF
 IMPINGERS, CONNECTORS, AND BACK
 HALF OF FILTER HOLDER

CONTAINER _____

ETHER-CHLOROFORM
EXTRACTION

ACETONE WASH OF IMPINGERS, CONNECTORS,
 AND BACK HALF OF FILTER HOLDER

CONTAINER _____

BACK HALF SUBTOTAL _____ mg

TOTAL WEIGHT _____ mg

MOISTURE

IMPINGERS

FINAL VOLUME _____ ml
 INITIAL VOLUME _____ ml
 NET VOLUME _____ ml

SILICA GEL

FINAL WEIGHT _____ g
 INITIAL WEIGHT _____ g
 NET WEIGHT _____ g

TOTAL MOISTURE _____ %

ANALYTICAL DATA

PLANT Oceanside Landfill
 DATE 10/7/92
 SAMPLING LOCATION Engine 007-outlet
 SAMPLE TYPE MS
 RUN NUMBER MS-5
 SAMPLE BOX NUMBER _____
 CLEAN-UP MAN JSG

COMMENTS: 75% load

FRONT HALF

LABORATORY RESULTS

ACETONE WASH OF NOZZLE, PROBE, CYCLONE (BYPASS),
 FLASK, FRONT HALF OF FILTER HOLDER

CONTAINER Filter 0.8 mg

FILTER NUMBER RQAT150 T.W. 0.6033

CONTAINER AR 0.8 mg

FRONT HALF SUBTOTAL 1.6 mg

BACK HALF

IMPINGERS CONTENTS AND WATER WASH OF
 IMPINGERS, CONNECTORS, AND BACK
 HALF OF FILTER HOLDER

CONTAINER _____ mg
 ETHER-CHLOROFORM
 EXTRACTION _____ mg

ACETONE WASH OF IMPINGERS, CONNECTORS,
 AND BACK HALF OF FILTER HOLDER

CONTAINER _____ mg

BACK HALF SUBTOTAL _____ mg

TOTAL WEIGHT _____ mg

MOISTURE

IMPINGERS

FINAL VOLUME _____ ml

INITIAL VOLUME _____ ml

NET VOLUME _____ ml

SILICA GEL

FINAL WEIGHT _____ g _____ g _____ g

INITIAL WEIGHT _____ g _____ g _____ g

NET WEIGHT _____ g _____ g _____ g

TOTAL MOISTURE _____ %

ANALYTICAL DATA

PLANT Oceanside Landfill
 DATE 10/7/92
 SAMPLING LOCATION Engine 007-outlet
 SAMPLE TYPE MS
 RUN NUMBER MS-6
 SAMPLE BOX NUMBER _____
 CLEAN-UP MAN JSG

COMMENTS: 75% load

FRONT HALF

LABORATORY RESULTS

ACETONE WASH OF NOZZLE, PROBE, CYCLONE (BYPASS),
 FLASK, FRONT HALF OF FILTER HOLDER

CONTAINER Filter 1.1 mg

FILTER NUMBER RQAT151 T.W.
0.5996

CONTAINER AK 1.1 mg

FRONT HALF SUBTOTAL 2.2 mg

BACK HALF

IMPINGER CONTENTS AND WATER WASH OF
 IMPINGERS, CONNECTORS, AND BACK
 HALF OF FILTER HOLDER

CONTAINER _____ mg
 ETHER-CHLOROFORM
 EXTRACTION _____ mg

ACETONE WASH OF IMPINGERS, CONNECTORS,
 AND BACK HALF OF FILTER HOLDER

CONTAINER _____ mg

BACK HALF SUBTOTAL _____ mg

TOTAL WEIGHT _____ mg

MOISTURE

IMPINGERS

FINAL VOLUME _____ ml
 INITIAL VOLUME _____ ml
 NET VOLUME _____ ml

SILICA GEL

FINAL WEIGHT _____ g
 INITIAL WEIGHT _____ g
 NET WEIGHT _____ g

EPA (Du) 231
 4.72

TOTAL MOISTURE _____ %

**A T L A N T I C
A N A L Y T I C A L
L A B O R A T O R Y**

Ms. Eszter J. Samodai
ROJAC Environmental Services, Inc.
30 Arbor Street
Hartford, CT 06106

Report No. AAL-7749
Date Requested 10-08-92
Date Reported 10-14-92
P.O. No. 27195

Material Submitted: Twelve Gas Samples in Tedlar Bags

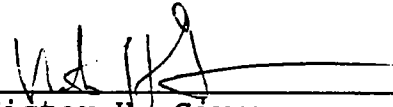
Information Requested: Gas Chromatography Analysis

Notebook: VG072,p82;SS083,p54

Subject samples, received from Energy Tactics, Yaphank, NY on 10/08/92, have been analyzed by gas chromatography for the specified constituents.

Results are reported on the following pages.

d1014



Victor H. Given

FAX: 203-232-5378

Page 2 of 5

Hydrogen Sulfide by Gas Chromatography

GC Method

Varian 3700 equipped with a Tracor 1000 Hall detector.

Column: 4m x 2mm glass, 1.5% XE60, 1% H₃PO₄ on
Carbopack maintained at 20 degrees C.

Injection port: On column @ 100 degrees C.

Detector: "Hall", sulfur mode, reactor 880 degrees C,
Methanol flow rate 0.3 ml/min.

Calibration: Three point calibration curve prepared from
dynamic dilutions of 107 ppm hydrogen sulfide Scott
Specialty Gas Co. calibration standard.

Hydrogen Sulfide by Gas Chromatography

Concentration, ppm by volume

<u>Sample Identity</u>	<u>Results</u>
LFG-1	57
LFG-2	65
LFG-3	62
LFG-4	54
LFG-5	54
LFG-6	45

Page 4 of 5

Total Non Methane Hydrocarbons by Gas Chromatography

GC Method

Varian 6000 FID

Column: 60 m x .32 mm SPB-5 column.
Temperature programmed 10 degrees C to 240 degrees C
@ 15 degrees C/min., head pressure 30 psig.

Injection: Split mode, 10:1 ratio
Temperature 200 degrees C

Detector: Flame ionization, range 10-¹²
nitrogen makeup 20/min

All peaks eluting after methane were integrated and the total area referenced to hexane calibration data.

Samples and standards were run in duplicate per EPA 18 method requirements.

Total Non Methane Hydrocarbons by Gas Chromatography

<u>Sample Identity</u>	<u>Results</u>	
	<u>Conc. ppm by Vol. as Hexane</u>	<u>Conc. ppm by vol. as Methane</u>
M18-1-0	38	228
M18-2-0	38	228
M18-3-0	42	250
M18-4-0	21	126
M18-5-0	10	60
M18-6-0	5	30

✓ 10-9-1 *Rujac - 25ul 107 STD* 38
CHANNEL A INJECT 10/09/92 08:55:45 STORED TO BIN # 52

2.31 11.0

2.91

DATA SAVED TO BIN # 52

10/09/92 08:55:45 CH= "A" PS= 1.
FILE 1. METHOD 0. RUN 146 INDEX 146 BIN 52
PEAK# AREA% RT AREA BC
1 0.391 2.31 10294 01
2 99.609 2.91 2625162 01
TOTAL 100. 2635456

WARNING - MEMORY AT 9. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-2 *25ul 107 ppm STD*
CHANNEL A INJECT 10/09/92 09:01:38 STORED TO BIN # 53

2.25 11.0
2.33 2.63

2.91

DATA SAVED TO BIN # 53

10/09/92 09:01:38 CH= "A" PS= 1.
FILE 1. METHOD 0. RUN 147 INDEX 147 BIN 53
PEAK# AREA% RT AREA BC
1 0.036 2.25 1064 02
2 0.39 2.33 11436 02
3 0.032 2.58 936 02
4 0.003 2.63 90 03
5 99.539 2.91 2918316 01
TOTAL 100. 2931842

WARNING - MEMORY AT 7. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-3

25ul

53.5 ppm H_2S

✓ 1-9-3 25ul 53.5 ppm H₂S

380

CHANNEL A INJECT 10/09/92 09:09:07 STORED TO BIN # 54

2.24 11.0

3.54

2.91

DATA SAVED TO BIN # 54

10/09/92 09:09:07 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 148 INDEX 148 BIN 54

PEAK#	AREA%	RT	AREA BC
1	0.672	2.24	8835 01
2	99.326	2.91	1305160 08
3	0.001	3.54	19 05

TOTAL 100. 1314014

WARNING - MEMORY AT 5. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-5 2.3 ul 53.5 ppm
CHANNEL A INJECT 10/09/92 09:22:37 STORED TO BIN # 56



38

DATA SAVED TO BIN # 56

10/09/92 09:22:37 CH= "A" PS= 1.

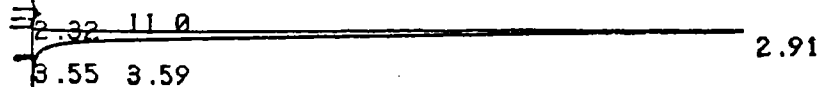
FILE 1. METHOD 0. RUN 150 INDEX 150 BIN 56

PEAK#	AREA%	RT	AREA BC
1	0.95	2.24	9900 02
2	99.042	2.9	1031936 08
3	0.008	3.79	81 05

TOTAL 100. 1041917

WARNING - MEMORY AT 3. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-6 53.5 ppm 5.1 ul
CHANNEL A INJECT 10/09/92 09:34:50 STORED TO BIN # 57



DATA SAVED TO BIN # 57

10/09/92 09:34:50 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 151 INDEX 151 BIN 57

PEAK#	AREA%	RT	AREA BC
1	0.575	2.32	7717 01
2	99.422	2.91	1333517 08
3	0.002	3.55	32 05
4	0.	3.59	6 05

TOTAL 100. 1341272

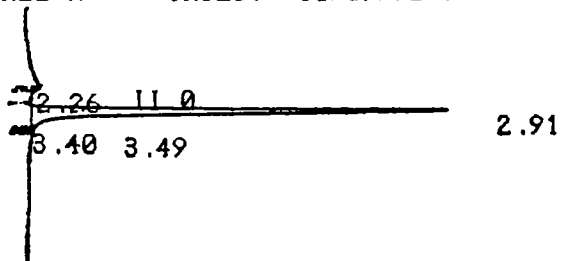
WARNING - MEMORY AT 0. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10-9-7 53.5 ppm H₂S

WARNING - MEMORY AT 2. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-8 2 c.f. run 1/2 S STD

CHANNEL A INJECT 10/09/92 09:46:05 STORED TO BIN # 59



DATA SAVED TO BIN # 59

10/09/92 09:46:05 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 153 INDEX 153 BIN 59

PEAK#	AREA%	RT	AREA BC
1	0.279	2.26	2083 01
2	99.71	2.91	743322 08
3	0.004	3.4	29 05
4	0.007	3.49	50 05

TOTAL 100. 745484

WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-10 26 g ppm STE 125
CHANNEL A INJECT 10/09/92 10:03:42 STORED TO BIN # 61

~~2.23 1624~~
~~2.29 2099~~
2.90
3.47
3.64

DATA SAVED TO BIN # 61

10/09/92 10:03:42 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 155 INDEX 155 BIN 61

PEAK#	AREA%	RT	AREA BC
1	0.222	2.23	1624 02
2	0.287	2.29	2099 02
3	0.449	2.32	3278 03
4	99.026	2.9	723517 08
5	0.001	3.39	9 05
6	0.001	3.47	10 05
7	0.013	3.64	95 05

TOTAL 100. 730632

WARNING - MEMORY AT 0. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-11 25ml ul LFG-6
CHANNEL A INJECT 10/09/92 10:09:19 STORED TO BIN # 62

~~2.26 2793~~
~~2.3 2685~~
2.89
3.47

DATA SAVED TO BIN # 62

10/09/92 10:09:19 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 156 INDEX 156 BIN 62

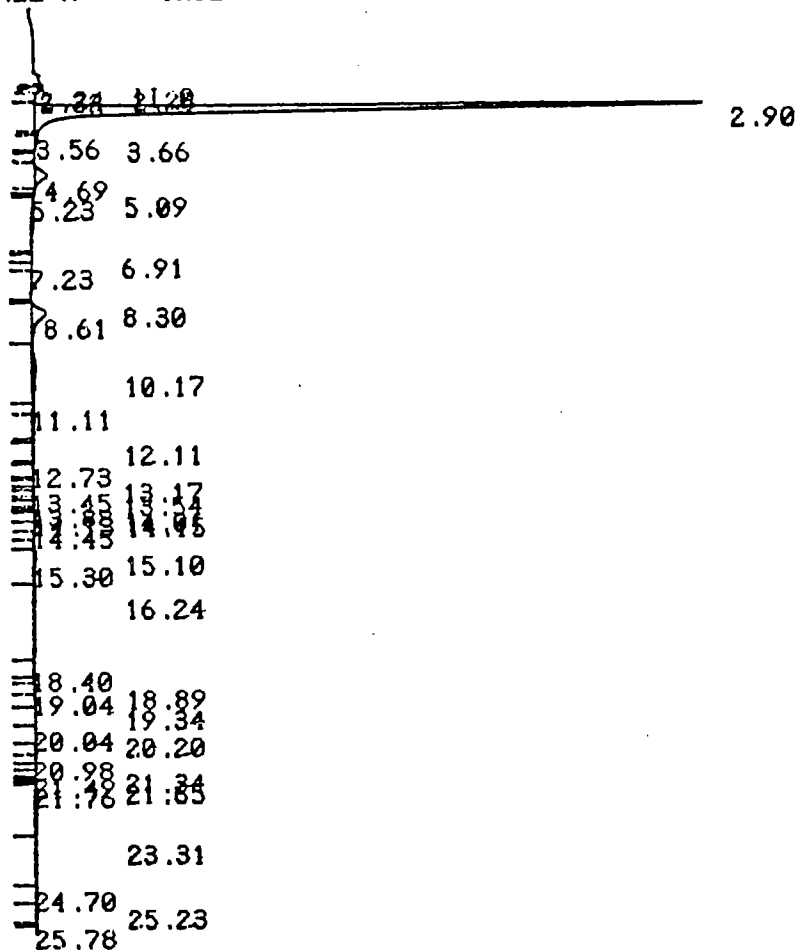
PEAK#	AREA%	RT	AREA BC
1	0.239	2.26	2793 02
2	0.23	2.3	2685 03
3	99.527	2.89	1161604 08
4	0.003	3.47	37 05

TOTAL 100. 1167119

WARNING - MEMORY AT 0. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-12 25ml LFG-5
CHANNEL A INJECT 10/09/92 10:12:12 STORED TO BIN # 63

10-9-12 25ml LFG-5
 CHANNEL A INJECT 10/09/92 10:13:12 STORED TO BIN # 63



DATA SAVED TO BIN # 63

10/09/92 10:13:12 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 157 INDEX 157 BIN 63

PEAK#	AREA%	RT	AREA BC
1	0.111	2.24	1679 02
2	0.095	2.28	1434 02
3	0.279	2.32	4222 03
4	82.629	2.9	1249023 08
5	0.027	3.56	406 07
6	3.4	4.69	51394 02
7	0.102	5.09	1544 02
8	0.007	5.23	102 03
9	0.008	6.91	119 01
10	0.008	7.23	121 01
11	0.026	8.3	393 02
12	5.08	8.61	76792 08
13	1.976	10.17	29873 06
14	0.061	11.11	923 07
15	0.02	12.11	308 01
16	0.009	12.73	142 01
17	0.012	13.17	179 01
18	0.042	13.45	633 02
19	0.014	13.54	209 03

24.70
25.23
25.78

DATA SAVED TO BIN # 63

10/09/92 10:13:12

CH= "A" PS= 1.

FILE 1.

METHOD 0.

RUN 157

INDEX 157

BIN 63

391

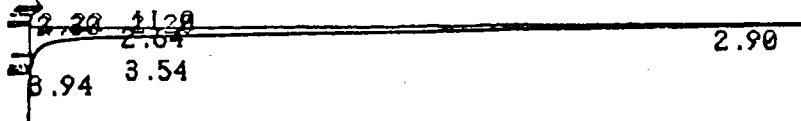
PEAK#	AREA%	RT	AREA BC
1	0.111	2.24	1679 02
2	0.095	2.28	1434 02
3	0.279	2.32	4222 03
4	82.629	2.9	1249023 03
5	0.027	3.56	406 07
6	3.4	4.69	51394 02
7	0.102	5.09	1544 02
8	0.007	5.23	102 03
9	0.008	6.91	119 01
10	0.008	7.23	121 01
11	0.026	8.3	393 02
12	5.08	8.61	76792 08
13	1.976	10.17	29873 06
14	0.061	11.11	923 07
15	0.02	12.11	308 01
16	0.009	12.73	142 01
17	0.012	13.17	179 01
18	0.042	13.45	633 02
19	0.014	13.54	209 03
20	0.073	13.88	1108 02
21	0.03	14.01	450 02
22	0.067	14.13	1008 02
23	0.289	14.15	4367 02
24	0.123	14.45	1856 03
25	0.066	15.1	994 02
26	0.871	15.3	13162 02
27	1.494	16.24	22582 02
28	0.204	18.4	3005 02
29	0.143	18.89	2159 02
30	0.264	19.04	3991 02
31	0.327	19.34	4950 02
32	0.291	20.04	4396 02
33	0.154	20.2	2327 03
34	0.072	20.98	1090 02
35	0.078	21.34	1183 02
36	0.098	21.49	1485 03
37	0.018	21.65	279 01
38	0.012	21.76	177 01
39	0.68	23.31	10285 02
40	0.378	24.7	5710 02
41	0.336	25.23	5085 02
42	0.025	25.78	377 03

TOTAL 100. 1511602

WARNING - MEMORY AT 0. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-13 25ml LFG-5
CHANNEL A INJECT 10/09/92 10:40:25 STORED TO BIN # 64

✓ 10-9-13 25ml LFG-5
CHANNEL A INJECT 10/09/92 10:40:25 STORED TO BIN # 64



DATA SAVED TO BIN # 64

392

10/09/92 10:40:25 CH= "A" PS= 1.

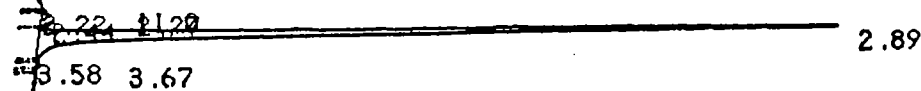
FILE 1. METHOD 0. RUN 158 INDEX 158 BIN 64

PEAK#	AREA%	RT	AREA BC
1	0.141	2.22	2018 02
2	0.121	2.28	1733 02
3	0.219	2.3	3135 03
4	0.014	2.64	203 02
5	99.464	2.9	1423818 08
6	0.004	3.54	61 05
7	0.036	3.94	521 05

TOTAL 100. 1431489

WARNING - MEMORY AT 0. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-14 25ml LFG-5
CHANNEL A INJECT 10/09/92 10:46:31 STORED TO BIN # 65



DATA SAVED TO BIN # 65

10/09/92 10:46:31 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 159 INDEX 159 BIN 65

PEAK#	AREA%	RT	AREA BC
1	0.084	2.22	1263 02
2	0.03	2.27	446 02
3	2.466	2.44	37081 02
4	97.329	2.89	1463792 08
5	0.023	3.58	342 06
6	0.069	3.67	1035 07

TOTAL 100. 1503959

WARNING - MEMORY AT 0. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

WARNING - MEMORY AT 0. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-15 25m LFG-4
CHANNEL A INJECT 10/09/92 10:53:45 STORED TO BIN # 66

2.27 11.0 2.89
3.38 3.68
3.77 4.49
5.22 5.61

393

DATA SAVED TO BIN # 66

10/09/92 10:53:45 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 160 INDEX 160 BIN 66

PEAK#	AREA%	RT	AREA BC
1	0.295	2.27	4297 01
2	99.089	2.89	1442960 08
3	0.002	3.38	24 05
4	0.002	3.68	24 05
5	0.022	3.77	318 05
6	0.284	4.49	4131 08
7	0.235	5.22	3417 06
8	0.073	5.61	1061 07

TOTAL 100. 1456232

WARNING - MEMORY AT 2. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-16 25m LFG-4
CHANNEL A INJECT 10/09/92 11:00:14 STORED TO BIN # 67

2.22 2120 2.88
3.52 3.58

DATA SAVED TO BIN # 67

10/09/92 11:00:14 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 161 INDEX 161 BIN 67

PEAK#	AREA%	RT	AREA BC
1	0.17	2.22	2498 02
2	0.212	2.28	3112 03
3	99.562	2.88	1459060 08
4	0.004	3.49	52 05
5	0.004	3.53	61 05
6	0.005	3.58	72 05
7	0.002	3.74	27 05
8	0.041	3.79	596 05

TOTAL 100. 1465478

1- WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-17 25ul LFG 3

CHANNEL A INJECT 10/09/92 11:05:59 STORED TO BIN # 68

~~2.26 2.32~~
3.59 3.59 2.89

394

DATA SAVED TO BIN # 68

10/09/92 11:05:59 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 162 INDEX 162 BIN 68

PEAK#	AREA%	RT	AREA BC
1	0.231	2.26	3795 02
2	0.157	2.32	2592 03
3	99.595	2.89	1639606 08
4	0.008	3.5	127 05
5	0.01	3.59	158 07

TOTAL 100. 1646278

WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-18 25ul LFG-3

CHANNEL A INJECT 10/09/92 11:11:13 STORED TO BIN # 69

~~2.22 2.27~~
3.95 3.99 2.88

DATA SAVED TO BIN # 69

10/09/92 11:11:13 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 163 INDEX 163 BIN 69

PEAK#	AREA%	RT	AREA BC
1	0.163	2.22	2766 02
2	0.122	2.27	2072 03
3	99.668	2.88	1687542 08
4	0.023	3.77	386 05
5	0.018	3.95	311 05
6	0.005	3.99	78 05

TOTAL 100. 1693155

WARNING - MEMORY AT 4. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-9-19 25ul LFG-2

CHANNEL A INJECT 10/09/92 11:16:38 STORED TO BIN # 70

WARNING - MEMORY AT 4. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10-9-79 25ul LFG-2
CHANNEL A INJECT 10/09/92 11:16:38 STORED TO BIN # 70



DATA SAVED TO BIN # 70

395

10/09/92 11:16:38 CH= "A" PS= 1.

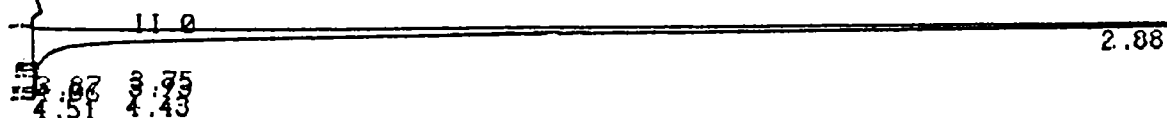
FILE 1. METHOD 0. RUN 164 INDEX 164 BIN 70

PEAK#	AREA%	RT	AREA BC
1	0.092	2.25	1642 01
2	99.868	2.88	1784537 08
3	0.003	3.67	54 05
4	0.001	3.73	11 05
5	0.036	3.8	651 05

TOTAL 100. 1786895

WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10-19-20 25ul 1025H
CHANNEL A INJECT 10/09/92 11:26:25 STORED TO BIN # 72



DATA SAVED TO BIN # 72

10/09/92 11:26:25 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 166 INDEX 166 BIN 72

PEAK#	AREA%	RT	AREA BC
1	99.922	2.88	2968383 08
2	0.008	3.75	234 05
3	0.02	3.87	603 06
4	0.004	3.93	127 06
5	0.019	4.06	573 06
6	0.026	4.43	787 07

TOTAL 100. 2970707

396

✓ 10-9-21 2nd LFG-2
CHANNEL A INJECT 10/09/92 11:32:15 STORED TO BIN # 73

11.0
2.69 2.89
3.52 3.57
3.96 4.06

DATA SAVED TO BIN # 73

10/09/92 11:32:15 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 167 INDEX 167 BIN 73

PEAK#	AREA%	RT	AREA BC
1	0.01	2.69	165 02
2	99.896	2.89	1704743 08
3	0.005	3.52	88 06
4	0.006	3.57	94 07
5	0.011	3.79	188 06
6	0.071	3.96	1210 06
7	0.002	4.06	29 07

TOTAL 100. 1706517

✓ 10-9-23 2nd LFG-1
CHANNEL A INJECT 10/09/92 11:42:17 STORED TO BIN # 75

11.0
3.44 2.89

DATA SAVED TO BIN # 75

10/09/92 11:42:17 CH= "A" PS= 1.

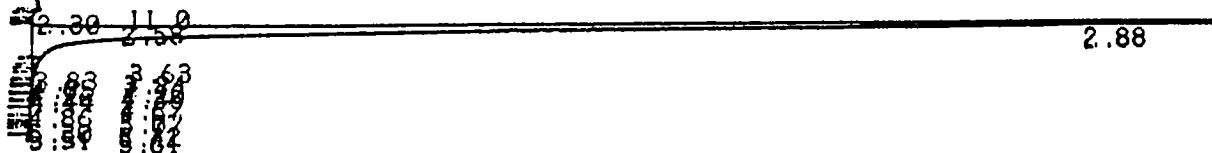
FILE 1. METHOD 0. RUN 169 INDEX 169 BIN 75

PEAK#	AREA%	RT	AREA BC
1	99.996	2.89	1572555 08
2	0.004	3.44	61 05

TOTAL 100. 1572616

WARNING - MEMORY AT 9. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10-9-25 25ul 107 ppm STD
CHANNEL A INJECT 10/09/92 11:55:46 STORED TO BIN # 78



DATA SAVED TO BIN # 78

10/09/92 11:55:46 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 172 INDEX 172 BIN 78

PEAK#	AREA%	RT	AREA BC
1	0.056	2.3	1639 01
2	0.007	2.58	211 01
3	99.55	2.88	2896981 08
4	0.001	3.63	29 05
5	0.013	3.83	366 06
6	0.008	3.94	237 06
7	0.028	4.05	803 06
8	0.01	4.2	303 06
9	0.026	4.26	770 07
10	0.019	4.44	550 01
11	0.022	4.67	629 01
12	0.046	4.86	1333 02
13	0.067	5.07	1955 02
14	0.077	5.3	2228 02
15	0.03	5.42	880 02
16	0.031	5.51	904 02
17	0.009	5.61	269 03

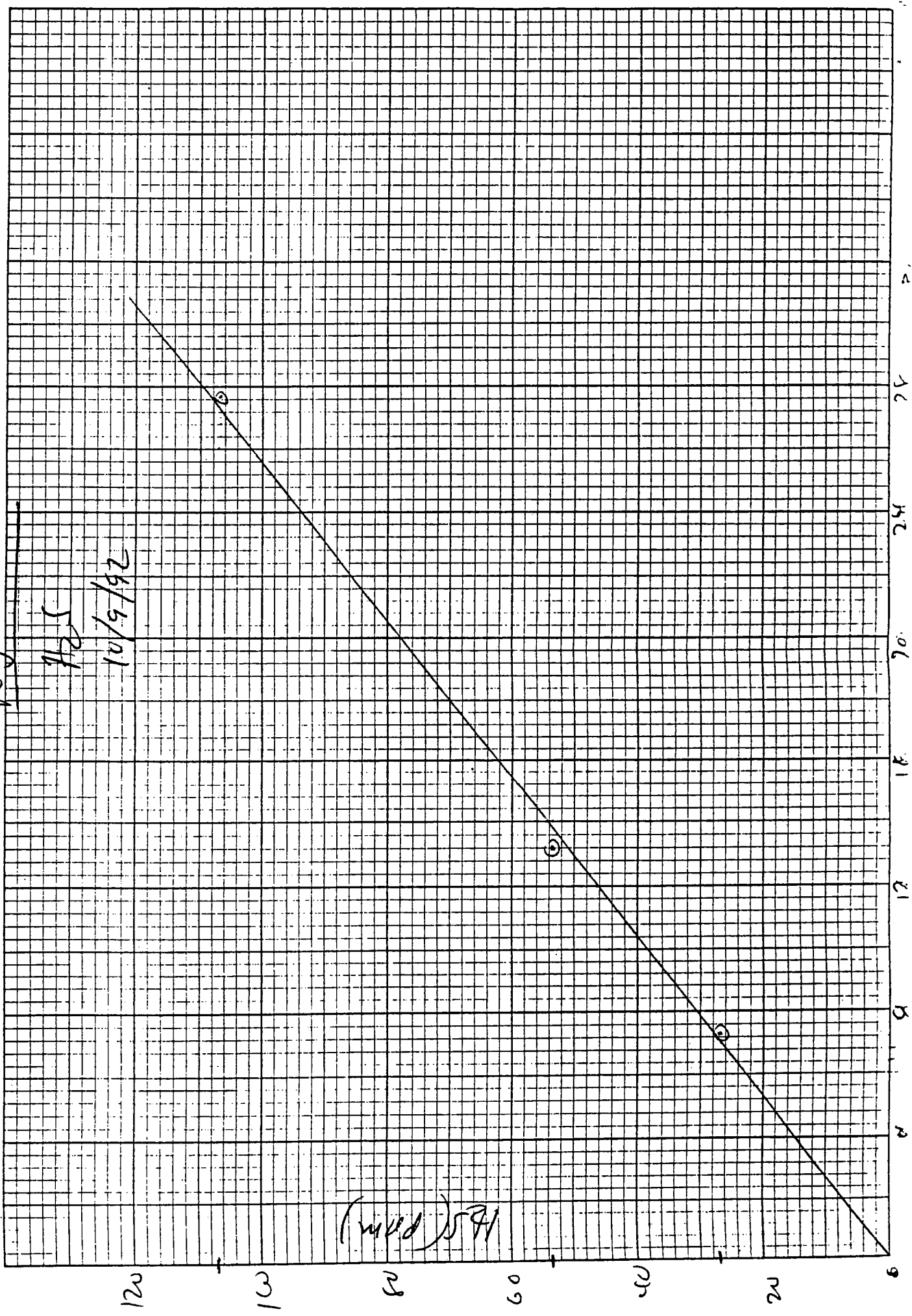
TOTAL 100. 2910087

Rope 7749

725

10/9/92

(mld) 571

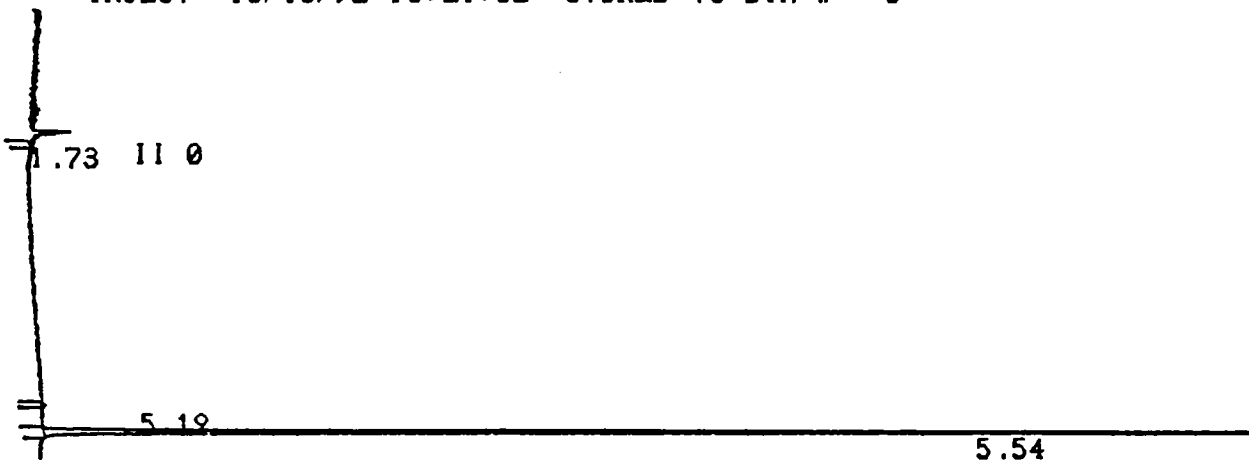


Rejac Bag 4

2

✓ 10-10-4 6.8 ppm hexane std 0.5cc 8x FID

CHANNEL A INJECT 10/10/92 10:21:32 STORED TO BIN # 5



DATA SAVED TO BIN # 5

10/10/92 10:21:32 CH= "A" PS= 1.

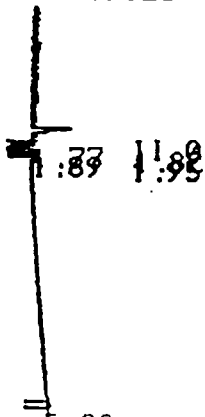
FILE 1. METHOD 0. RUN 672 INDEX 472 BIN 5

PEAK#	AREA%	RT	AREA BC
1	0.185	1.73	55 01
2	0.299	5.19	89 01
3	99.515	5.54	29574 01

TOTAL 100. 29718

✓ 10-10-5 6.8 ppm hexane std 0.5cc 8x FID

CHANNEL A INJECT 10/10/92 10:29:55 STORED TO BIN # 6



10/10/92 10:29:55

CH= "A" PS= 1.

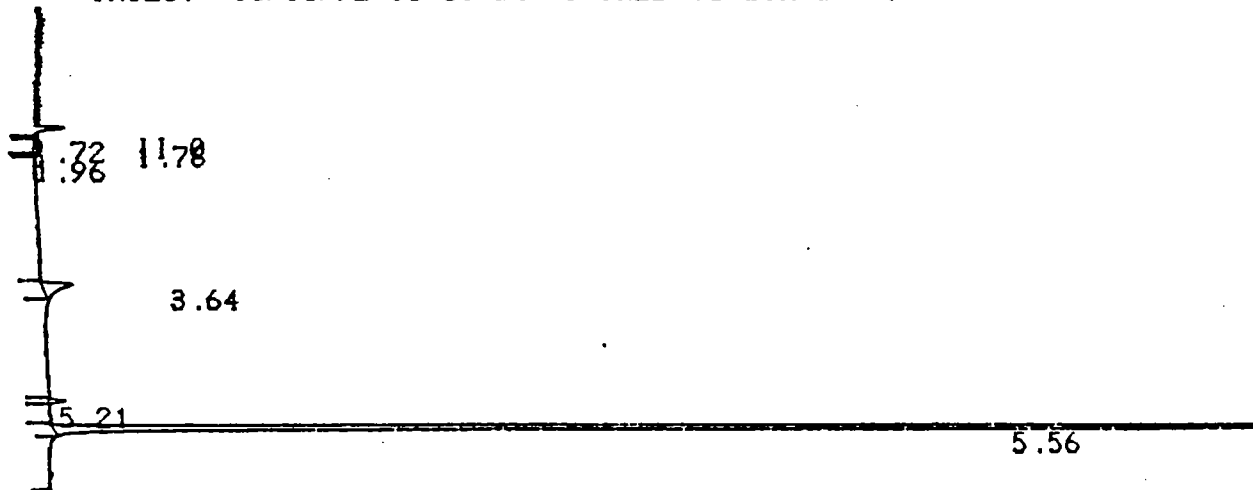
FILE 1. METHOD 0. RUN 673 INDEX 473 BIN 6

PEAK# AREA% RT AREA BC

1	0.179	1.77	56 01
2	0.202	1.82	63 01
3	0.186	1.89	58 01
4	0.115	1.95	36 01
5	0.253	5.2	79 01
6	99.065	5.54	30930 01

TOTAL 100. 31222

10-10-6 33.5 ppm hexane std 0.5cc 8x FID
CHANNEL A INJECT 10/10/92 10:38:24 STORED TO BIN # 7



DATA SAVED TO BIN # 7

10/10/92 10:38:24

CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 674 INDEX 474 BIN 7

PEAK# AREA% RT AREA BC

1	0.035	1.72	52 01
2	0.263	1.78	389 02
3	0.053	1.96	78 03
4	1.297	3.64	1919 01
5	0.23	5.21	340 01
6	98.123	5.56	145225 01

, m236

TOTAL 100. 148003

10-10-7 33.5 ppm hexane std 0.5cc 8x FID



DATA SAVED TO BIN # 7

10/10/92 10:38:24 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 674 INDEX 474 BIN 7

PEAK#	AREA%	RT	AREA BC
1	0.035	1.72	52 01
2	0.263	1.78	389 02
3	0.053	1.96	78 03
4	1.297	3.64	1919 01
5	0.23	5.21	340 01
6	98.123	5.56	145225 01

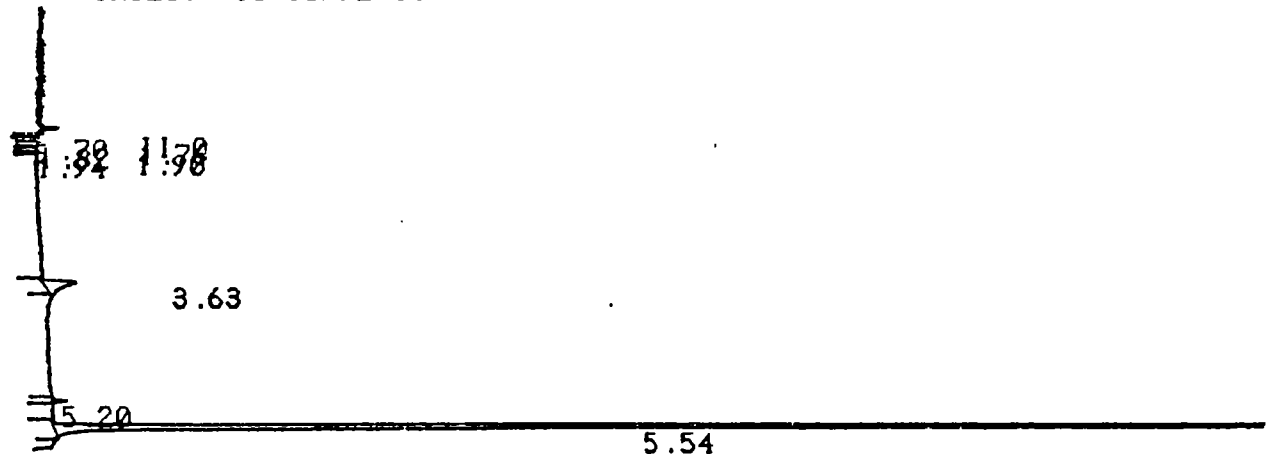
100736

TOTAL 100. 148003

✓ 20-10-7 33.5 ppm hexane std 0.5 cc 8x FID

CHANNEL A INJECT 10/10/92 10:47:36 STORED TO BIN # 8

2



DATA SAVED TO BIN # 8

10/10/92 10:47:36 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 675 INDEX 475 BIN 8

PEAK#	AREA%	RT	AREA BC
1	0.059	1.7	89 01
2	0.042	1.76	64 01
3	0.057	1.82	86 01
4	0.027	1.9	41 02
5	0.038	1.94	57 03
6	1.253	3.63	1894 01
7	0.212	5.2	320 01
8	98.313	5.54	148661 01

TOTAL 100. 151212

1	0.010	1.77	07 01
2	0.025	1.76	108 02
3	0.166	1.82	710 02
4	0.024	1.88	103 03
5	0.01	1.93	43 01
6	0.242	5.21	1032 01
7	99.31	5.55	423528 01
8	0.038	6.15	162 01
9	0.063	6.54	267 01

cur 232

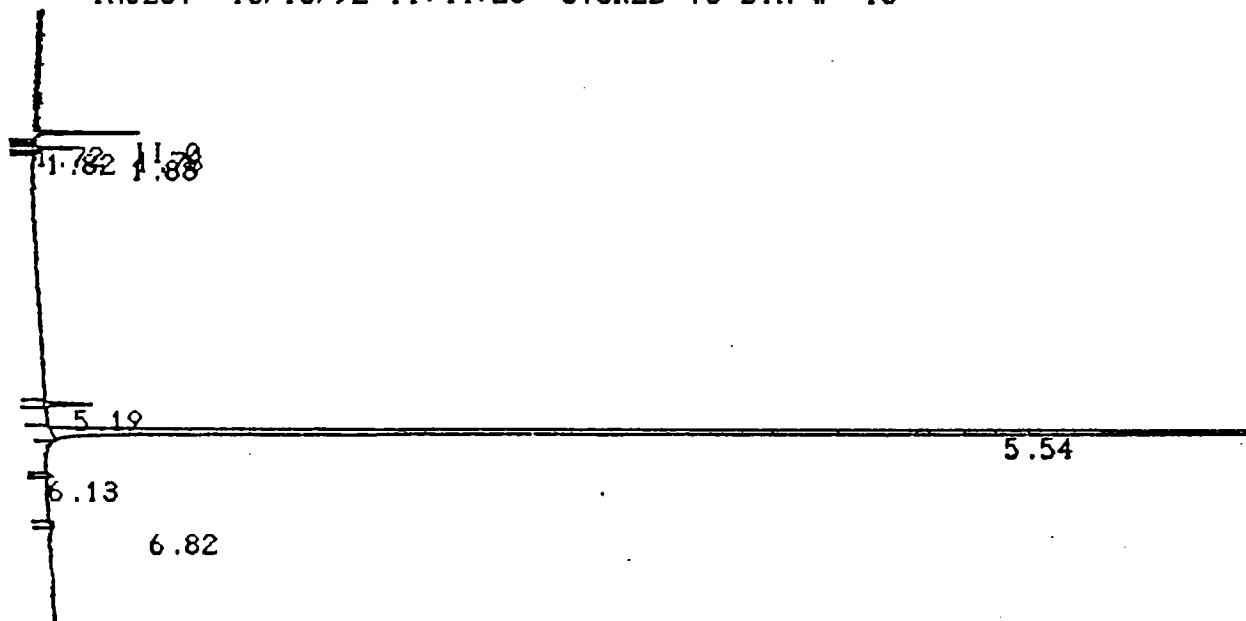
10	0.058	7.73	247 01
11	0.047	8.77	200 01

TOTAL 100. 426469

WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-10-92 0.5 cc 97 gm Sd

CHANNEL A INJECT 10/10/92 11:44:28 STORED TO BIN # 13



DATA SAVED TO BIN # 13

10/10/92 11:44:28 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 680 INDEX 480 BIN 13

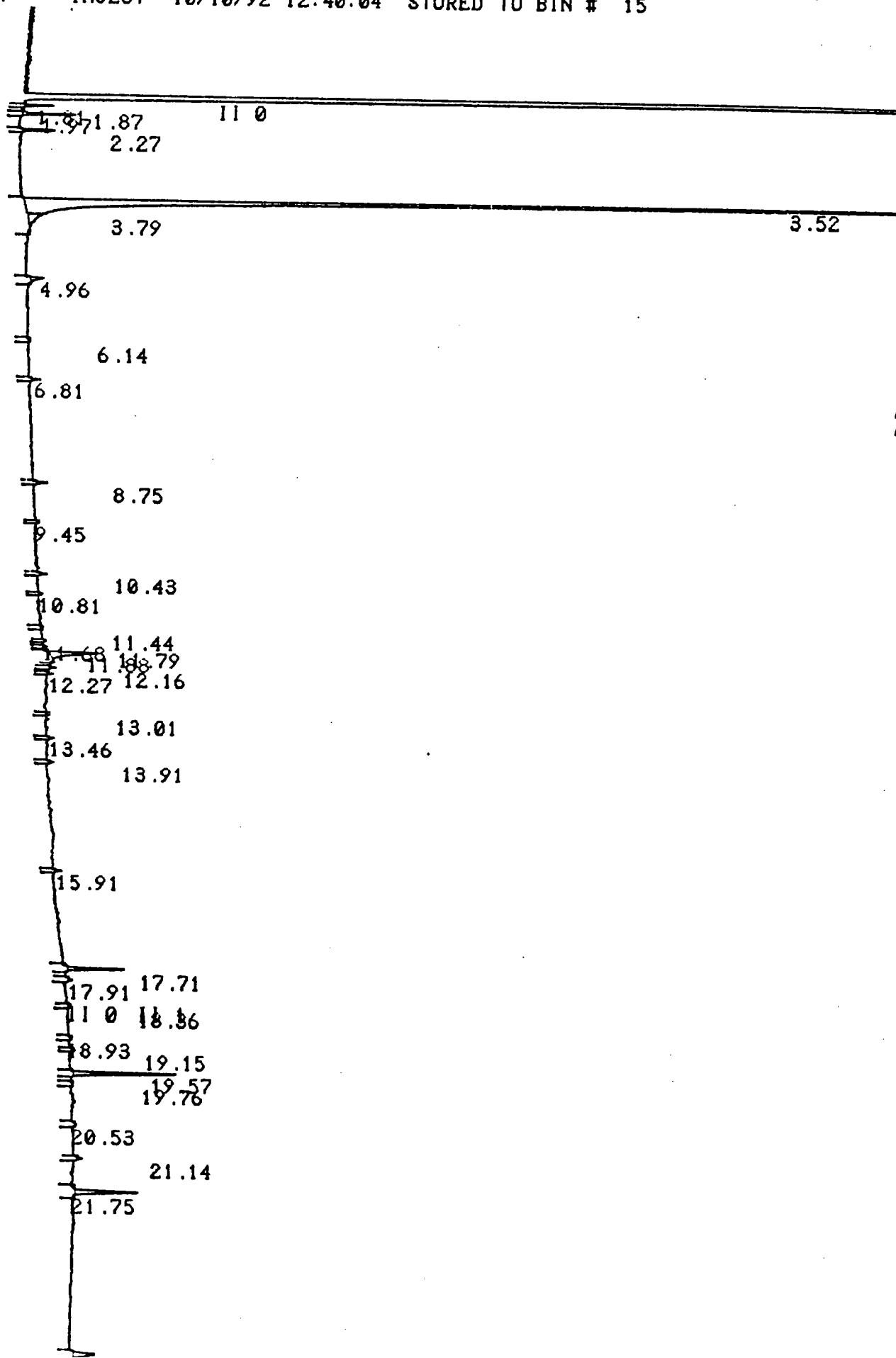
PEAK#	AREA%	RT	AREA BC
1	0.023	1.72	96 02
2	0.027	1.78	112 02
3	0.167	1.82	685 08
4	0.014	1.88	59 05
5	0.245	5.19	1002 01
6	99.462	5.54	406960 01
7	0.037	6.13	150 01
8	0.024	6.82	98 01

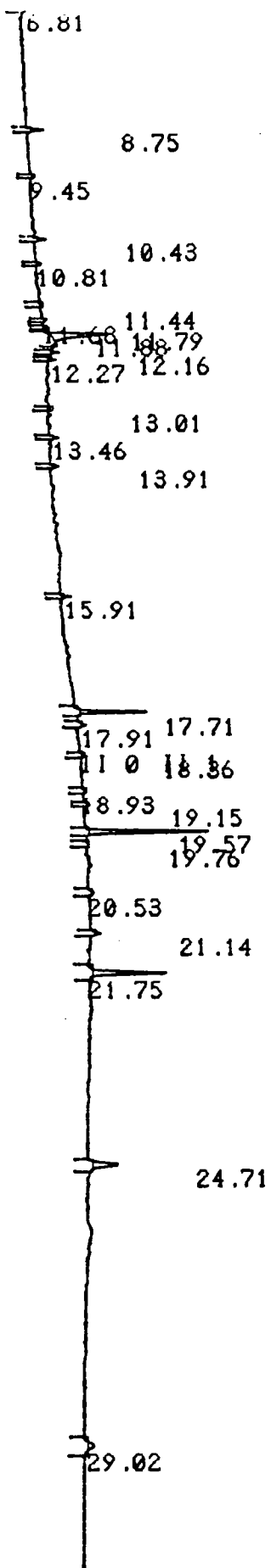
TOTAL 100. 409162

1- WARNING - MEMORY AT 2. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓ 10-10-12 0.5 cc Bag 4 Rojac

CHANNEL A INJECT 10/10/92 12:40:04 STORED TO BIN # 15





DATA SAVED TO BIN # 15

10/10/92 12:40:04

CH= "A" PS= 1.

FILE 1

METHOD 0

RUN 682

INDEX 482

BIN 15

PEAK#	AREA%	RI	AREA	BC
1	0.86	1.81	792	02
2	0.136	1.87	125	02
3	1.606	1.97	1479	03
4	0.992	2.27	913	01
5	74.672	3.52	68747	08
6	0.001	3.79	1	05
7	0.984	4.96	906	01
8	0.058	6.14	53	01

9	0.381	6.81	351	01
10	0.441	8.75	406	01
11	0.084	9.45	77	01
12	0.32	10.43	295	01
13	0.108	10.81	99	01
14	0.072	11.44	66	01
15	0.085	11.68	78	01
16	0.164	11.79	151	01
17	3.426	11.88	3154	01
18	0.24	12.16	221	01
19	0.214	12.27	197	01
20	0.047	13.01	43	01
21	0.211	13.46	194	01
22	0.188	13.91	173	01
23	0.305	15.91	281	01
24	2.14	17.71	1970	01
25	0.301	17.91	277	01
26	0.074	18.36	68	01
27	0.131	18.93	121	01
28	0.173	19.15	159	01
29	4.305	19.57	3963	01
30	0.127	19.76	117	01
31	0.218	20.53	201	01
32	0.322	21.14	296	01
33	3.692	21.75	3399	01
34	1.942	24.71	1788	01
35	0.982	29.02	904	01

TOTAL 100. 92065

FI= 1. FE= 1. MN= 0.
 PRESS 'ENTER' TO SKIP ENTRY
 ENABLE BASELINE DRAWING? [Y/N] (Y)
 STORAGE MENU? [Y,N] (N)

FUNCTION NUMBER [0-10] (0)

FILE NAME () ="
 TIME FUNCTION VALUE
 TT= 31 TF=" ER TV= 1
 TT=

METHOD NUMBER [0.1.2.5] (0) MN=

END OF DIALOG

✓ 10-10-13 05cc Bag 41 R-Jac
 CHANNEL A INJECT 10/10/92 13:20:06 STORED TO BIN # 16

1.84 1.95 2.25

2

3.51

4.96

6.80

8.74

10.30 10.09
10.41
10.80

11.78 11.67 11.87
12.15 12.26

13.45
13.90

14.79

15.90

17.70 17.89
11 1 11 0

18.92 19.13
19.56

20.52

21.12
21.74

24.68

28.97

2

ER 0
DATA SAVED TO BIN # 16

10/10/92 13:20:06

CH= "A" PS= 1.

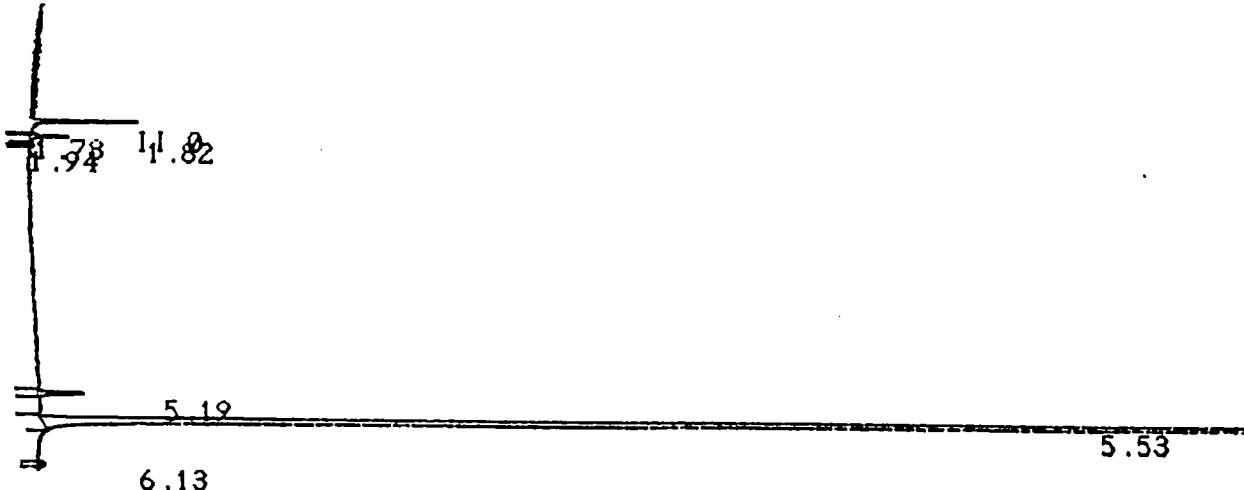
FILE 1. METHOD 0. RUN 683 INDEX 483 BIN 16

PEAK#	AREA%	RT	AREA BC
1	0.047	1.72	41 01
2	0.936	1.79	811 02
3	0.084	1.84	73 03
4	1.697	1.95	1470 01
5	1.103	2.25	955 01
6	73.84	3.51	63958 01
7	0.844	4.96	731 01
8	0.372	6.8	322 01
9	0.455	8.74	394 01
10	0.074	10.09	64 01
11	0.125	10.3	108 01
12	0.305	10.41	264 01
13	0.095	10.8	82 01
14	0.109	11.67	94 01
15	0.201	11.78	174 02
16	2.921	11.87	2530 03
17	0.233	12.15	202 01
18	0.19	12.26	165 01
19	0.196	13.45	170 01
20	0.201	13.9	174 01
21	0.152	14.79	132 01
22	0.272	15.9	236 01
23	1.897	17.7	1643 01
24	0.336	17.89	291 01
25	0.11	18.92	95 01
26	0.241	19.13	209 01
27	4.358	19.56	3775 01
28	0.143	19.76	124 01
29	0.163	20.52	141 01
30	0.487	21.12	422 01
31	4.202	21.74	3640 01
32	2.344	24.68	2030 01
33	1.266	28.97	1097 01

TOTAL 100. 86617

pg - 10-14 0.5 cc 98.4 ppm Sd

CHANNEL A INJECT 10/10/92 13:57:52 STORED TO BIN # 17



DATA SAVED TO BIN # 17

10/10/92 13:57:52 CH= "A" PS= 1.

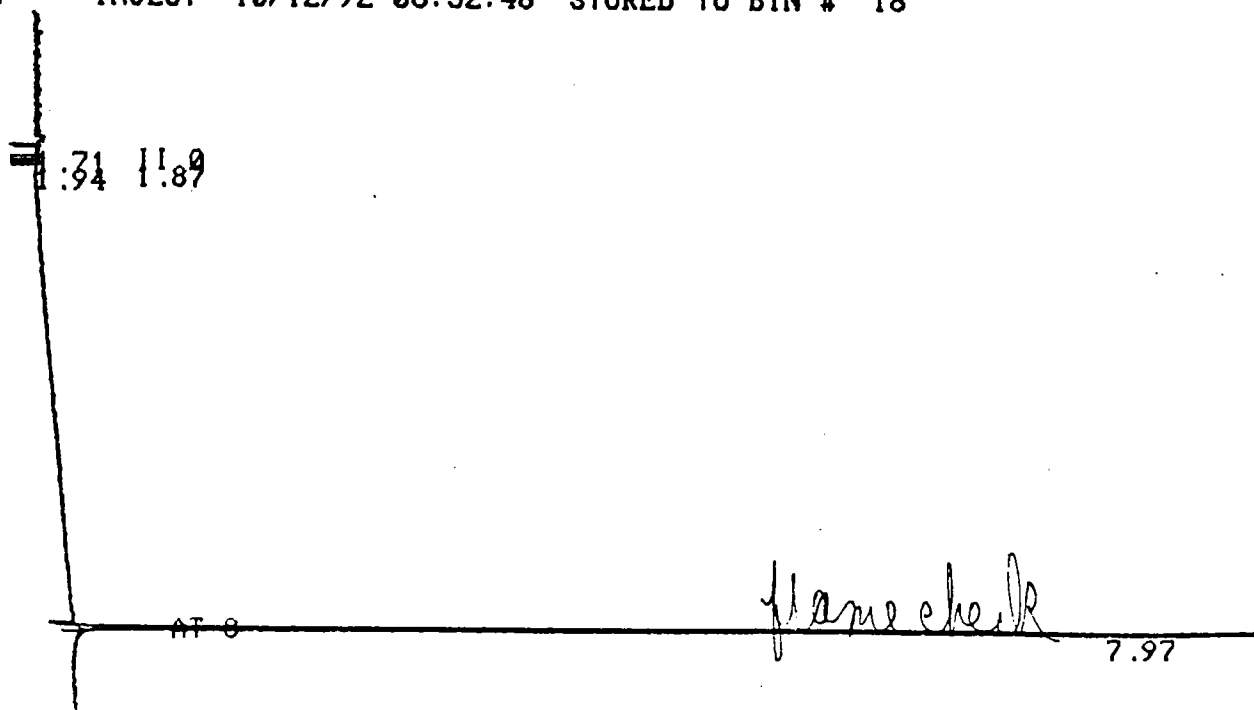
FILE 1. METHOD 0. RUN 684 INDEX 484 BIN 17

PEAK#	AREA%	RT	AREA BC
1	0.012	1.78	49 02
2	0.144	1.82	597 03
3	0.01	1.94	40 01
4	0.229	5.19	952 01
5	99.574	5.53	413773 01
6	0.032	6.13	133 01

TOTAL 100. 415544

N₂ Blank 0.5cc 8x FID

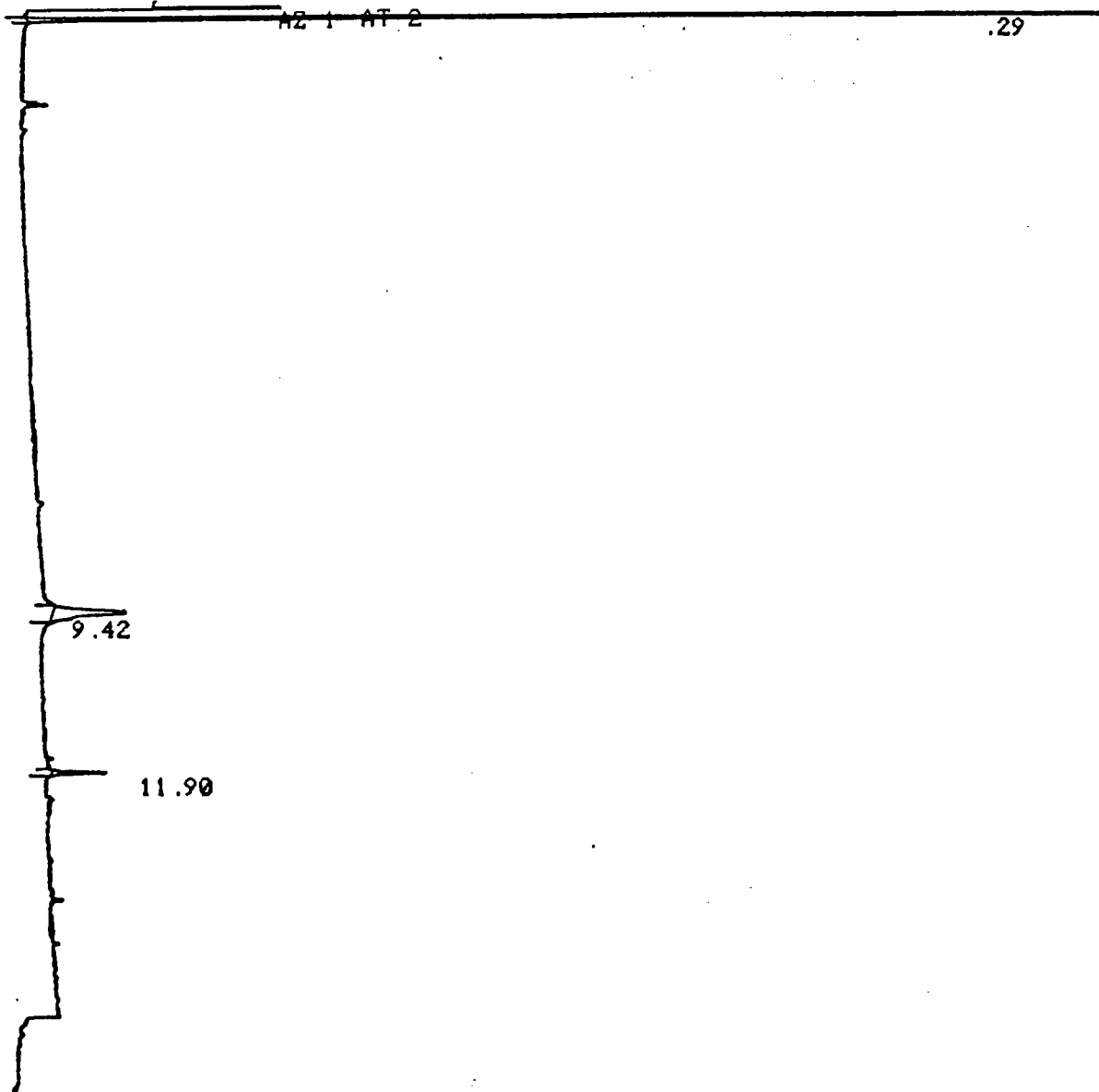
CHANNEL A INJECT 10/12/92 08:32:48 STORED TO BIN # 18



PW = 3. PI = 30. RM = 0.40.
IX = 447. OD = 1. PH = 0.
TB = 0. LC = 0. LS = 0.
SI = 0.

X *N2 Blank*

CHANNEL A INJECT 10/09/92 07:54:22 STORED TO BIN # 110



209

DATA SAVED TO BIN # 110

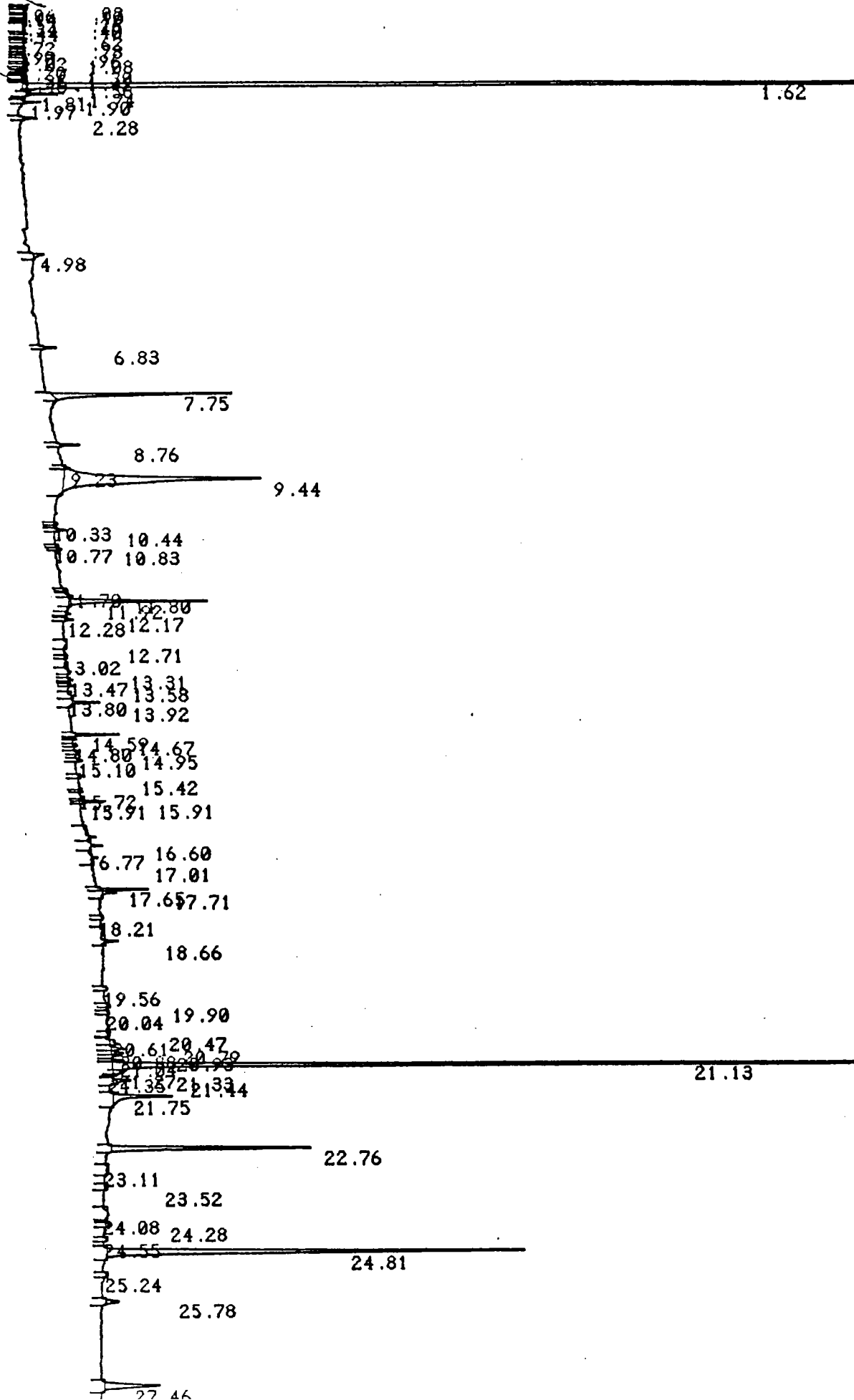
10/09/92 07:54:22				CH= "A"	PS= 1.
FILE 1.	METHOD 0.	RUN 647	INDEX 447	BIN 110	
PEAK#	AREA%	RT	AREA BC		
1	85.629	0.29	12543 01		
2	11.408	9.42	1671 01		
3	2.963	11.9	434 01		
TOTAL	100.		14648		

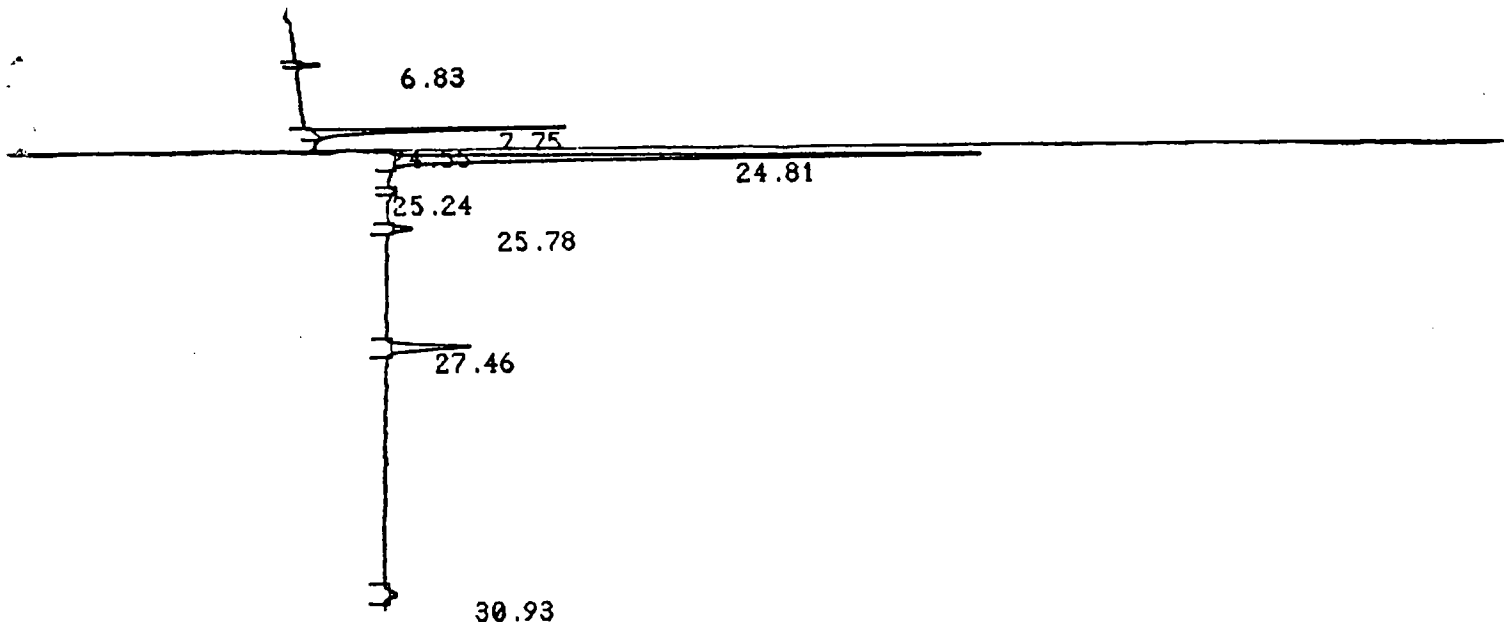
WARNING - MEMORY AT 6. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10-9-2 AAL-7749 Bag 1 repeat

0.5cc 8x FID

CHANNEL A INJECT 10/09/92 09:48:08 STORED TO BIN # 113





DATA SAVED TO BIN # 113

10/09/92 09:48:08 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 650 INDEX 450 BIN 113

PEAK#	AREA%	RT	AREA BC
1	0.012	0.02	79 02
2	0.009	0.06	60 03
3	0.012	0.1	80 02
4	0.012	0.14	77 03
5	0.011	0.26	73 01
6	0.009	0.34	56 01
7	0.005	0.4	36 01
8	0.035	0.44	227 01
9	0.013	0.62	83 01
10	0.009	0.72	57 01
11	0.01	0.78	65 01
12	0.004	0.9	24 01
13	0.006	0.96	38 01
14	0.005	1.02	34 01
15	0.007	1.08	45 01
16	0.005	1.2	35 01
17	0.007	1.3	44 01
18	0.006	1.36	40 01
19	0.006	1.42	42 01
20	0.016	1.46	107 01
21	0.016	1.56	104 02
22	70.885	1.62	465793 08 chg
23	0.007	1.74	43 05
24	0.145	1.81	955 05
25	0.01	1.9	67 02
26	0.091	1.97	600 03
27	0.073	2.28	478 01
28	0.12	4.98	787 01
29	0.071	6.83	466 01
30	1.191	7.75	7823 01

delete 467199

31	0.104	8.76	686 01
32	0.057	9.23	374 02
33	4.074	9.44	26768 03
34	0.016	10.33	108 01
35	0.059	10.44	387 01
36	0.014	10.77	94 02
37	0.026	10.83	173 03
38	0.014	11.7	94 01
39	0.064	11.8	418 02
40	1.098	11.92	7214 03
41	0.031	12.17	204 01
42	0.046	12.28	302 01
43	0.032	12.71	207 01
44	0.005	13.02	34 01
45	0.041	13.31	268 01
46	0.027	13.47	177 01
47	0.016	13.58	106 01
48	0.051	13.8	338 02
49	0.189	13.92	1243 03
50	0.194	14.59	1274 01
51	0.014	14.67	91 01
52	0.018	14.8	121 01
53	0.021	14.95	137 01
54	0.033	15.1	215 01
55	0.012	15.42	77 01
56	0.012	15.72	82 01
57	0.068	15.91	446 02
58	0.051	15.91	336 03
59	0.093	16.6	609 02
60	0.124	16.77	818 02
61	0.061	17.01	398 03
62	0.286	17.65	1879 02
63	0.155	17.71	1021 03
64	0.015	18.21	99 01
65	0.087	18.66	574 01
66	0.033	19.56	215 01
67	0.025	19.9	162 01
68	0.024	20.04	155 01
69	0.021	20.47	138 01
70	0.167	20.61	1099 02
71	0.166	20.79	1093 02
72	0.161	20.88	1057 02
73	0.05	20.93	329 02
74	0.105	21.04	689 02
75	11.25	21.13	73928 08
76	0.056	21.27	365 06
77	0.007	21.33	47 07
78	0.187	21.44	1232 01
79	0.6	21.75	3943 01
80	1.616	22.76	10621 01
81	0.06	23.11	394 01
82	0.023	23.52	150 01
83	0.088	24.08	581 01
84	0.041	24.28	268 01
85	0.029	24.55	188 01
86	4.193	24.81	27554 01
87	0.031	25.24	206 01
88	0.182	25.78	1198 01
89	0.725	27.46	4767 01
90	0.144	30.93	945 01

TOTAL

100.

657114 2 189915

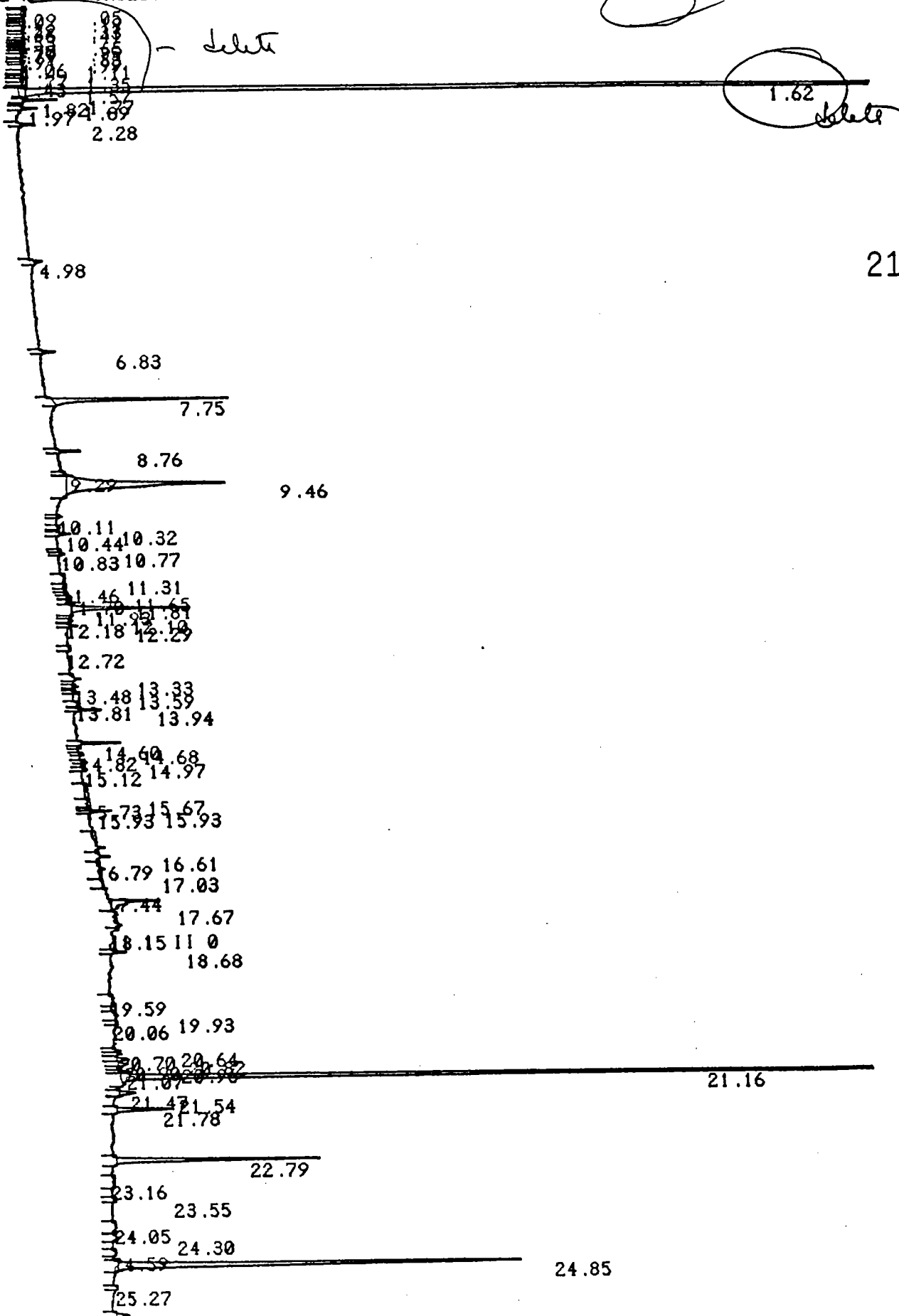
217

PRESS 'INJECT' TO BEGIN.

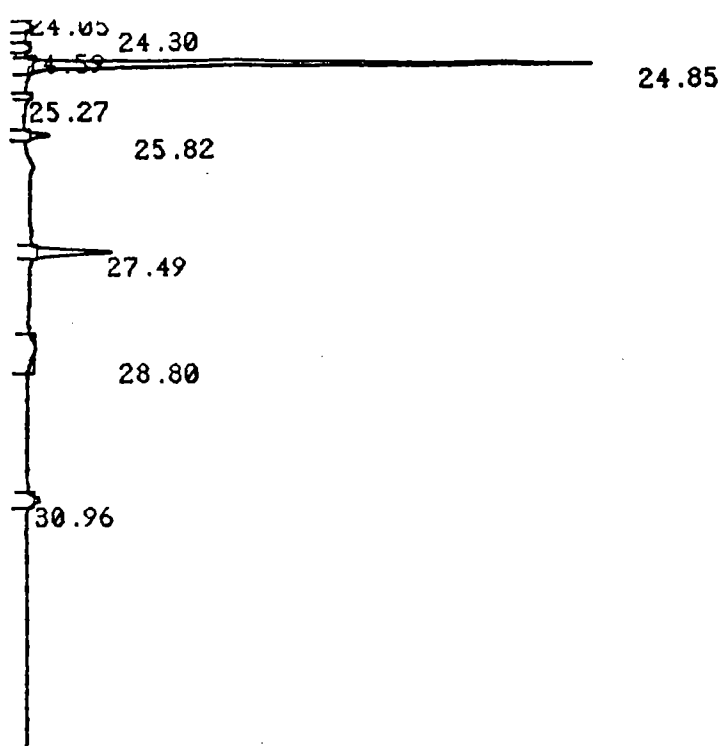
10-9-1

replot lag 1 1st run

CHANNEL A INJECT 10/09/92 09:03:18 REPLAYED FROM BIN # 112



218



219

10/09/92 09:03:18 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 651 INDEX 451 BIN 112

PEAK#	AREA%	RT	AREA BC
-------	-------	----	---------

1	0.009	0.05	61 01
2	0.024	0.09	153 01
3	0.005	0.19	30 01
4	0.012	0.29	80 02
5	0.011	0.33	74 02
6	0.011	0.36	73 02
7	0.013	0.41	87 03
8	0.004	0.53	23 01
9	0.009	0.65	60 01
10	0.009	0.7	59 02
11	0.008	0.75	51 03
12	0.008	0.79	54 01
13	0.013	0.85	83 01
14	0.019	0.91	121 02
15	0.02	0.99	127 03
16	0.013	1.06	84 02
17	0.006	1.11	36 03
18	0.01	1.27	68 01
19	0.006	1.35	37 01
20	0.013	1.43	82 01
21	0.005	1.57	34 02
22	71.448	1.62	464685 08
23	0.012	1.77	76 06
24	0.155	1.82	1005 06
25	0.008	1.89	53 07
26	0.086	1.97	560 01
27	0.066	2.28	429 01
28	0.099	4.98	646 01
29	0.064	6.83	418 01
30	1.19	7.75	7739 01
31	0.107	8.76	699 01
32	0.052	9.29	337 02
33	3.301	9.46	21470 03

Delete 466162

cty

28	0.064	6.83	418 01
29	1.19	7.75	7739 01
30	0.107	8.76	699 01
31	0.052	9.29	337 02
32	3.301	9.46	21470 03
33	0.021	10.11	139 01
34	0.021	10.32	134 01
35	0.073	10.44	472 01
36	0.017	10.77	111 02
37	0.031	10.83	201 03
38	0.052	11.31	335 02
39	0.011	11.46	72 03
40	0.009	11.65	59 02
41	0.024	11.7	158 03
42	0.065	11.81	423 02
43	0.967	11.93	6287 02
44	0.026	12.1	170 02
45	0.034	12.18	220 03
46	0.054	12.29	353 01
47	0.026	12.72	166 01
48	0.063	13.33	411 01
49	0.028	13.48	179 01
50	0.017	13.59	110 01
51	0.019	13.81	126 01
52	0.124	13.94	806 01
53	0.201	14.6	1310 02
54	0.016	14.68	105 03
55	0.016	14.82	105 01
56	0.024	14.97	153 01
57	0.032	15.12	211 01
58	0.052	15.67	335 02
59			

220

60	0.025	15.73	165 03
61	0.061	15.93	395 02
62	0.048	15.93	310 03
63	0.108	16.61	703 02
64	0.115	16.79	749 02
65	0.118	17.03	766 02
66	0.08	17.44	523 02
67	0.686	17.67	4463 02
68	0.14	18.15	913 03
69	0.084	18.68	547 01
70	0.06	19.59	392 01
71	0.064	19.93	417 02
72	0.019	20.06	125 03
73	0.071	20.64	461 02
74	0.07	20.7	458 02
75	0.142	20.82	925 02
76	0.139	20.9	905 02
77	0.025	20.96	160 02
78	0.112	21.07	727 02
79	11.08	21.16	72063 03
80	0.177	21.47	1152 02
81	0.005	21.54	34 03
82	0.43	21.78	2795 01
83	1.657	22.79	10778 01
84	0.042	23.16	271 01
85	0.021	23.55	139 01
86	0.073	24.05	472 01
87	0.056	24.3	362 01
88	0.037	24.59	242 01
89	4.18	24.85	27188 01
90	0.029	25.27	187 01
91	0.178	25.82	1156 01
92	0.721	27.49	4689 01
93	0.169	28.8	1096 01
94	0.14	30.96	908 01

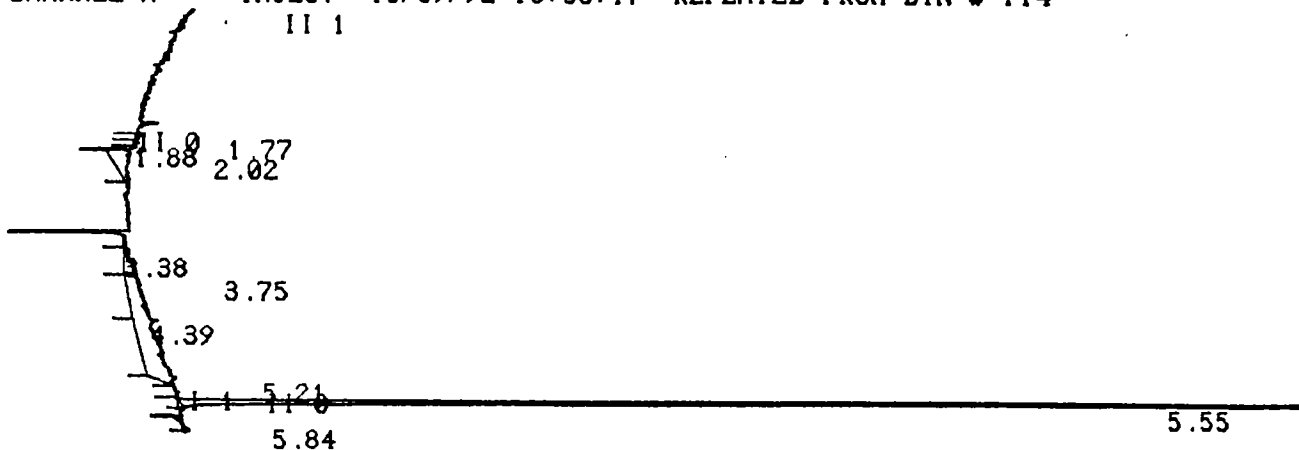
TOTAL

100.

650381 = 184219

10-9-3 replot 11.2 ppm std

CHANNEL A INJECT 10/09/92 10:56:17 REPLAYED FROM BIN # 114



10/09/92 10:56:17 CH= "A" PS= 1.

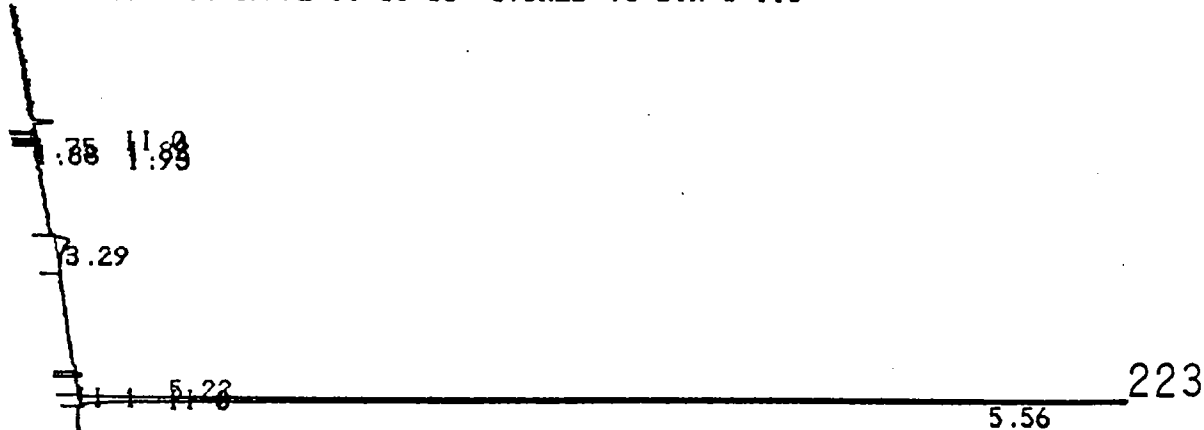
FILE 1. METHOD 0. RUN 653 INDEX 453 BIN 114

PEAK#	AREA%	RT	AREA BC
1	0.246	1.77	200 02
2	0.116	1.88	94 03
3	4.196	2.02	3408 01
4	2.012	3.38	1634 02
5	7.595	3.75	6169 02
6	13.531	4.39	10991 02
7	1.517	5.21	1232 03
8	69.68	5.55	56600 01
9	1.109	5.84	901 01

TOTAL 100. 81229

10-9-4 11.2 ppm std repeat 0.5cc 8xFID

CHANNEL A INJECT 10/09/92 11:08:35 STORED TO BIN # 115



DATA SAVED TO BIN # 115

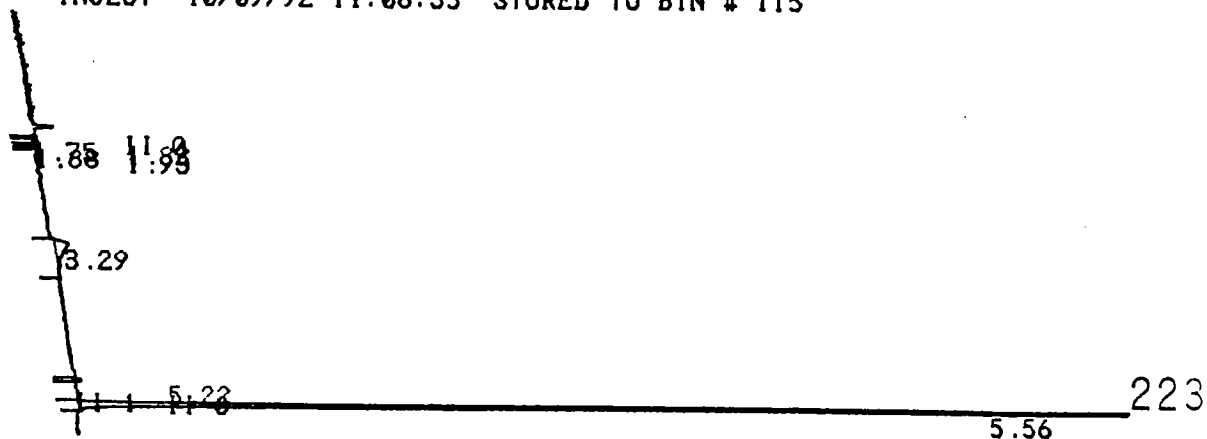
10/09/92 11:08:35 CH= "A" PS= 1.

9 1.109 5.84 901 01

TOTAL 100. 81229

10-9-4 11.2 ppm std repeat 0.5cc 8xFID

CHANNEL A INJECT 10/09/92 11:08:35 STORED TO BIN # 115



DATA SAVED TO BIN # 115

10/09/92 11:08:35 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 654 INDEX 454 BIN 115

PEAK#	AREA%	RT	AREA BC
1	0.213	1.75	131 02
2	0.208	1.82	128 02
3	0.114	1.88	70 03
4	0.081	1.93	50 01
5	2.855	3.29	1755 01
6	0.239	5.22	147 01
7	96.289	5.56	59188 01

TOTAL 100. 61469

WARNING - MEMORY AT 2. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

FI= 1. FE= 1. MN= 0.
PRESS 'ENTER' TO SKIP ENTRY
ENABLE BASELINE DRAWING? [Y/N] (Y) Y
STORAGE MENU? [Y,N] (N)

FUNCTION NUMBER [0-10] (0)

FILE NAME () =

TIME FUNCTION VALUE
TT= -5.35 TF= " II TV= 1
TT= -5.39 TF= " II TV= 0
TT=

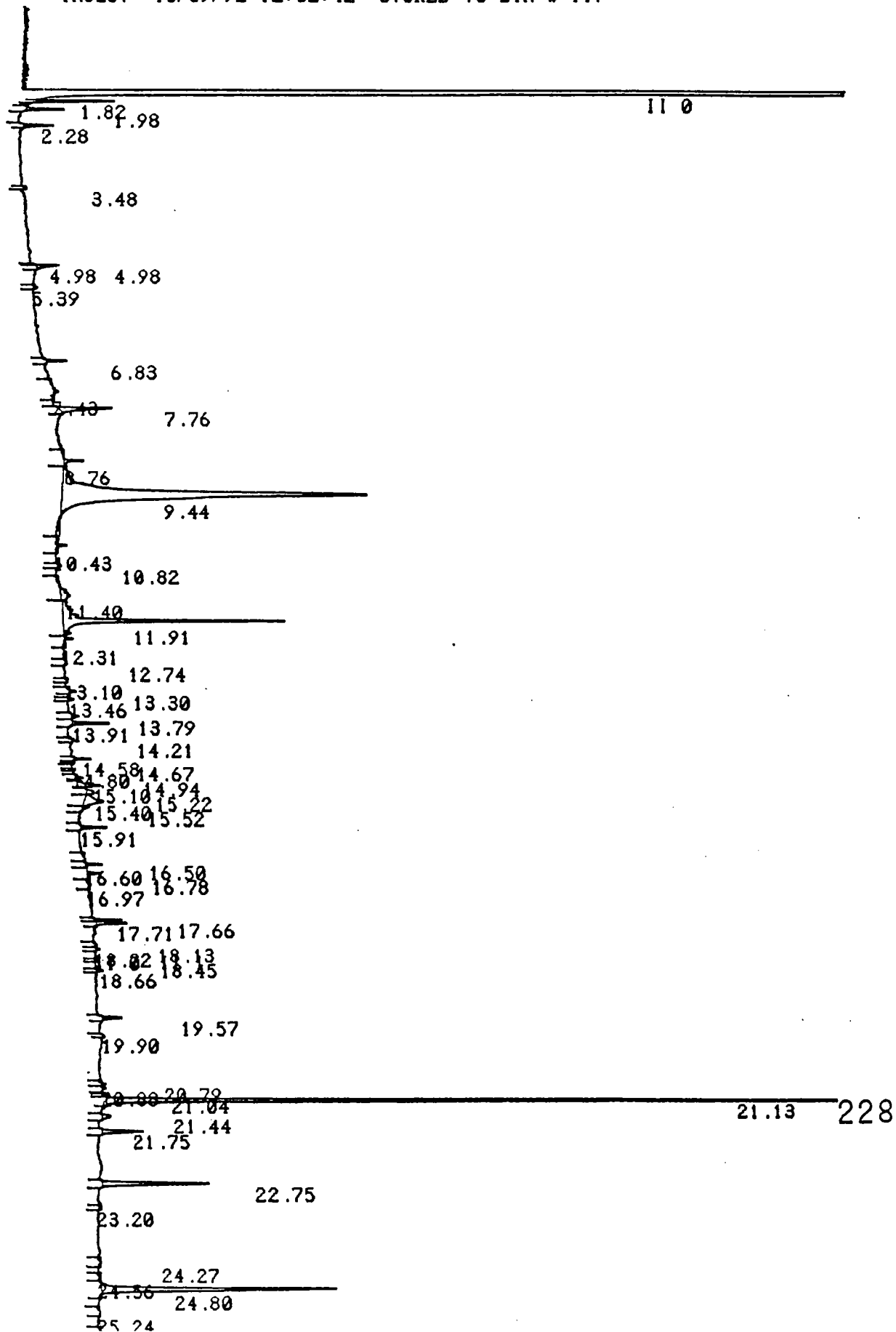
METHOD NUMBER [0,1,2,5] (0) MN=

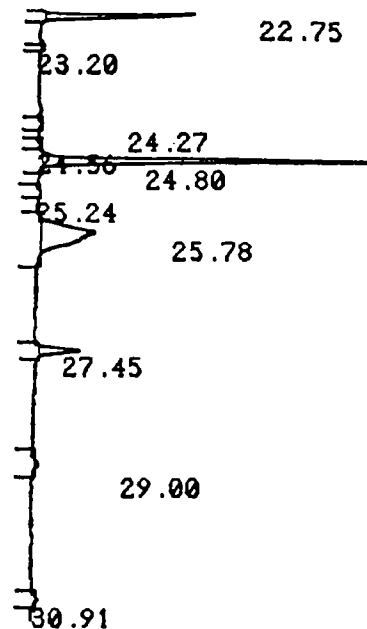
END OF DIALOG

MN= 0. REM FE= 1. CH= "A" PS= 1.

^X10-9-6. AAL-7749 Bag 2 repeat 0.5cc 8x FID

CHANNEL A INJECT 10/09/92 12:02:42 STORED TO BIN # 117





DATA SAVED TO BIN # 117

10/09/92 12:02:42

CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 656 INDEX 456 BIN 117

PEAK#	AREA%	RT	AREA BC
1	1.149	1.82	2095 01
2	0.75	1.98	1368 01
3	0.608	2.28	1108 01
4	0.09	3.48	164 01
5	0.208	4.98	380 02
6	0.382	4.98	697 03
7	0.065	5.39	119 01
8	0.383	6.83	699 01
9	0.427	7.43	778 01
10	1.451	7.76	2645 01
11	0.829	8.76	1512 02
12	28.924	9.44	52740 02
13	0.194	10.43	353 03
14	0.085	10.82	155 01
15	1.292	11.4	2356 02
16	9.159	11.91	16701 02
17	0.228	12.31	416 03
18	0.129	12.74	236 01
19	0.049	13.1	90 01
20	0.253	13.3	462 01
21	0.106	13.46	193 01
22	0.297	13.79	542 02
23	0.856	13.91	1560 03
24	0.119	14.21	217 01
25	0.31	14.58	566 01
26	0.038	14.67	70 01
27	0.03	14.8	55 01
28	0.098	14.94	178 01
29	0.449	15.1	819 01
30	0.498	15.22	908 02
31	1.556	15.4	2838 02
32	0.215	15.52	392 03
33	0.57	15.91	1040 01
34	0.105	16.5	191 02
35	0.438	16.6	799 02
36	0.512	16.78	934 02
37	0.114	16.97	207 03
38	0.569	17.66	1038 02

3	0.008	2.28	1108 01
4	0.09	3.48	164 01
5	0.208	4.98	380 02
6	0.382	4.98	697 03
7	0.065	5.39	119 01
8	0.383	6.83	699 01
9	0.427	7.43	778 01
10	1.451	7.76	2645 01
11	0.829	8.76	1512 02
12	28.924	9.44	52740 02
13	0.194	10.43	353 03
14	0.085	10.82	155 01
15	1.292	11.4	2356 02
16	9.159	11.91	16701 02
17	0.228	12.31	416 03
18	0.129	12.74	236 01
19	0.049	13.1	90 01
20	0.253	13.3	462 01
21	0.106	13.46	193 01
22	0.297	13.79	542 02
23	0.856	13.91	1560 03
24	0.119	14.21	217 01
25	0.31	14.58	566 01
26	0.038	14.67	70 01
27	0.03	14.8	55 01
28	0.098	14.94	178 01
29	0.449	15.1	819 01
30	0.498	15.22	908 02
31	1.556	15.4	2838 02
32	0.215	15.52	392 03
33	0.57	15.91	1040 01
34	0.105	16.5	191 02
35	0.438	16.6	799 02
36	0.512	16.78	934 02
37	0.114	16.97	207 03
38	0.569	17.66	1038 02
39	0.666	17.71	1214 03
40	0.072	18.13	132 02

229

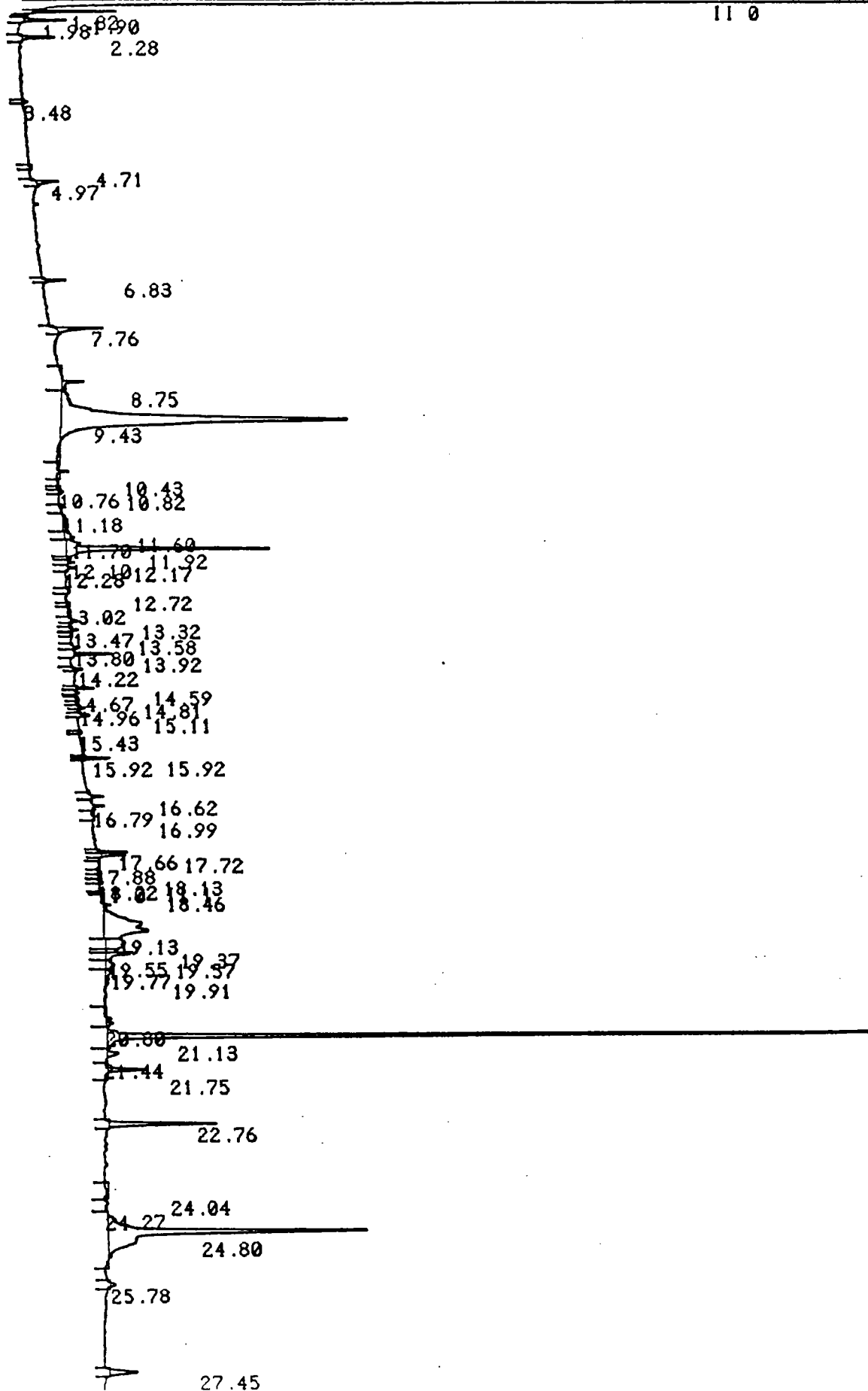
41	0.115	18.22	209 03
42	0.056	18.45	103 01
43	0.155	18.66	282 01
44	0.509	19.57	929 01
45	0.078	19.9	143 01
46	0.164	20.79	299 02
47	0.191	20.88	348 03
48	0.186	21.04	340 02
49	21.953	21.13	40030 03
50	0.454	21.44	827 01
51	1.2	21.75	2188 01
52	3.161	22.75	5764 01
53	0.063	23.2	114 01
54	0.116	24.27	212 01
55	0.082	24.56	149 02
56	8.823	24.8	16088 03
57	0.102	25.24	186 01
58	6.279	25.78	11449 01
59	1.474	27.45	2687 01
60	0.301	29.	549 01
61	0.263	30.91.	479 01

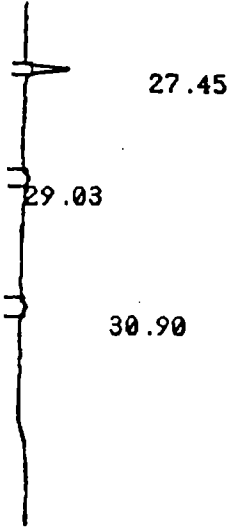
TOTAL 100. 182342

10-9-7 HAL-7749 Bag 2 repeat 0.5cc 8x F117

CHANNEL A

INJECT 10/09/92 12:44:18 STORED TO BIN # 118





DATA SAVED TO BIN # 118

10/09/92 12:44:18

CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 657 INDEX 457 BIN 118

PEAK#	AREA%	RT	AREA BC
1	1.08	1.82	2161 01
2	0.037	1.9	75 02
3	0.732	1.98	1465 03
4	0.669	2.28	1338 01
5	0.07	3.48	141 01
6	0.03	4.71	61 01
7	0.585	4.97	1171 01

8	0.347	6.83	694 01
9	1.246	7.76	2492 01
10	1.173	8.75	2346 02
11	23.472	9.43	46955 02
12	0.235	10.43	471 03
13	0.039	10.76	79 02
14	0.091	10.82	183 03
15	0.084	11.18	168 02
16	0.747	11.6	1494 02
17	0.642	11.7	1285 02
18	6.526	11.92	13055 02
19	0.163	12.1	327 02
20	0.203	12.17	407 02
21	0.196	12.28	392 03
22	0.122	12.72	244 01
23	0.018	13.02	36 01
24	0.196	13.32	393 01
25	0.129	13.47	259 01
26	0.019	13.58	39 01
27	0.225	13.8	450 02
28	0.784	13.92	1568 03
29	0.16	14.22	321 01
30	0.257	14.59	514 01
31	0.054	14.67	108 01
32	0.041	14.81	82 01
33	0.076	14.96	153 01
34	0.188	15.11	377 01
35	0.042	15.43	85 01
36	0.237	15.92	475 02
37	0.202	15.92	405 03
38	0.263	16.62	527 01
39	0.336	16.79	672 02

8	0.347	6.83	694 01
9	1.246	7.76	2492 01
10	1.173	8.75	2346 02
11	23.472	9.43	46955 02
12	0.235	10.43	471 03
13	0.039	10.76	79 02
14	0.091	10.82	183 03
15	0.084	11.18	168 02
16	0.747	11.6	1494 02
17	0.642	11.7	1285 02
18	6.526	11.92	13055 02
19	0.163	12.1	327 02
20	0.203	12.17	407 02
21	0.196	12.28	392 03
22	0.122	12.72	244 01
23	0.018	13.02	36 01
24	0.196	13.32	393 01
25	0.129	13.47	259 01
26	0.019	13.58	39 01
27	0.225	13.8	450 02
28	0.784	13.92	1568 03
29	0.16	14.22	321 01
30	0.257	14.59	514 01
31	0.054	14.67	108 01
32	0.041	14.81	82 01
33	0.076	14.96	153 01
34	0.188	15.11	377 01
35	0.042	15.43	85 01
36	0.237	15.92	475 02
37	0.202	15.92	405 03
38	0.263	16.62	527 01
39	0.336	16.79	672 02
40	0.083	16.99	167 03
41	0.518	17.66	1037 02
42	0.5	17.72	1000 03
43	0.06	17.88	120 01
44	0.034	18.13	69 01
45	0.081	18.22	163 01
46	0.036	18.46	72 01
47	7.912	19.13	15828 02
48	1.917	19.37	3835 02
49	0.577	19.55	1154 02
50	0.855	19.57	1711 02
51	0.82	19.77	1641 02
52	1.53	19.91	3060 02
53	0.874	20.8	1748 02
54	20.886	21.13	41783 02
55	0.773	21.44	1547 02
56	1.178	21.75	2357 03
57	2.804	22.76	5610 01
58	0.16	24.04	320 02
59	0.219	24.27	439 02
60	14.484	24.8	28975 03
61	0.301	25.78	603 01
62	1.16	27.45	2321 01
63	0.259	29.03	518 01
64	0.252	30.9	505 01

TOTAL 100. 200051

WARNING - MEMORY AT 6. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

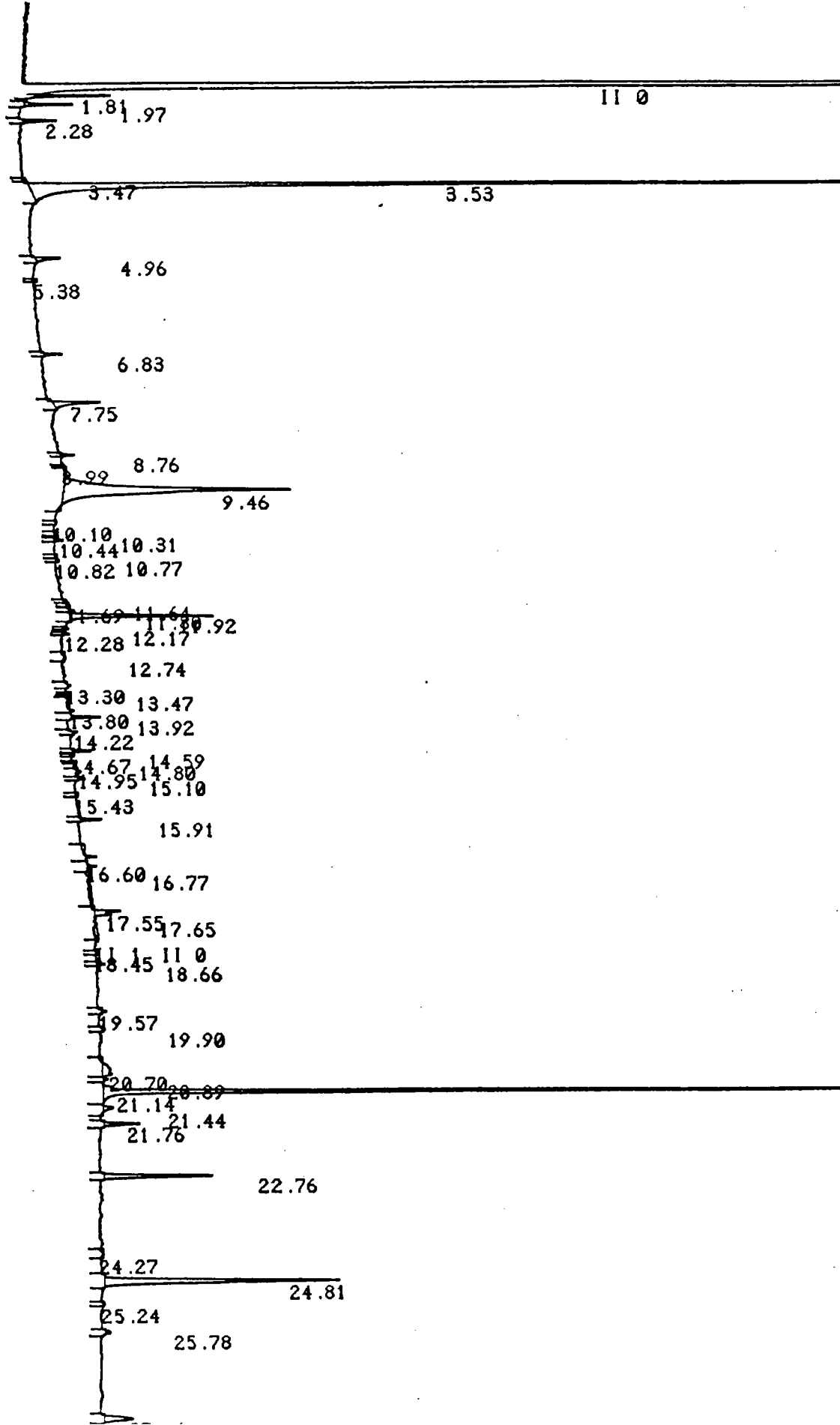
20	0.030	12.71	111 03
21	0.082	12.27	250 05

WARNING - MEMORY AT 5. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

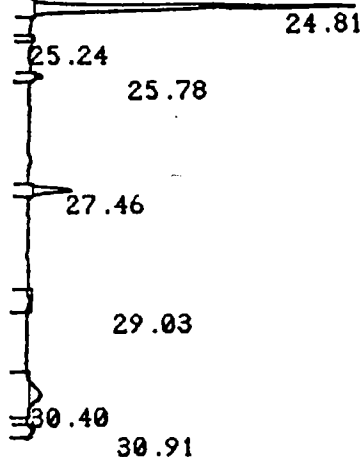
X 10-9-9 AAL-7749 Bag 3 repeat 0.5cc 8x FID

CHANNEL A

INJECT 10/09/92 14:15:38 STORED TO BIN # 120



23



DATA SAVED TO BIN # 120

236

10/09/92 14:15:38 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 659 INDEX 459 BIN 120

PEAK#	AREA%	RT	AREA BC
1	1.001	1.81	2042 01
2	0.809	1.97	1650 01
3	0.664	2.28	1354 01
4	0.043	3.47	88 02
5	31.57	3.53	64394 03
6	0.625	4.96	1275 01
7	0.039	5.38	79 01
8	0.306	6.83	624 01
9	1.296	7.75	2643 01
10	0.199	8.76	405 01
11	0.039	8.99	79 01
12	15.405	9.46	31422 01
13	0.04	10.1	81 01
14	0.036	10.31	73 01
15	0.152	10.44	310 01
16	0.036	10.77	73 02
17	0.076	10.82	154 03
18	0.034	11.64	70 02
19	0.045	11.69	91 03
20	0.191	11.8	389 02
21	3.624	11.92	7392 03
22	0.06	12.17	122 01
23	0.092	12.28	187 01
24	0.109	12.74	223 01
25	0.134	13.3	273 01
26	0.052	13.47	107 01
27	0.299	13.8	609 02
28	0.639	13.92	1304 03
29	0.181	14.22	370 01
30	0.262	14.59	535 01
31	0.04	14.67	82 01
32	0.022	14.8	44 01
33	0.222	14.95	453 02
34	0.172	15.1	351 03
35	0.039	15.43	80 01
36	0.362	15.91	739 01
37	0.395	16.6	806 02
38	0.391	16.77	797 02
39	0.338	17.55	690 02
40	1.131	17.65	2306 03
41	0.034	18.45	70 01

13	0.04	10.1	81 01
14	0.036	10.31	73 01
15	0.152	10.44	310 01
16	0.036	10.77	73 02
17	0.076	10.82	154 03
18	0.034	11.64	70 02
19	0.045	11.69	91 03
20	0.191	11.8	389 02
21	3.624	11.92	7392 03
22	0.06	12.17	122 01
23	0.092	12.28	187 01
24	0.109	12.74	223 01
25	0.134	13.3	273 01
26	0.052	13.47	107 01
27	0.299	13.8	609 02
28	0.639	13.92	1304 03
29	0.181	14.22	370 01
30	0.262	14.59	535 01
31	0.04	14.67	82 01
32	0.022	14.8	44 01
33	0.222	14.95	453 02
34	0.172	15.1	351 03
35	0.039	15.43	80 01
36	0.362	15.91	739 01
37	0.395	16.6	806 02
38	0.391	16.77	797 02
39	0.338	17.55	690 02
40	1.131	17.65	2306 03
41	0.034	18.45	70 01
42	0.14	18.66	285 01
43	0.156	19.57	318 01
44	0.106	19.9	217 01
45	1.273	20.7	2596 02
46	0.281	20.89	574 02
47	21.278	21.14	43400 02
48	0.537	21.44	1095 03
49	0.888	21.76	1811 01
50	2.838	22.76	5789 01
51	0.105	24.27	215 01
52	7.89	24.81	16094 01
53	0.066	25.24	134 01
54	0.252	25.78	514 01
55	1.252	27.46	2553 01
56	0.138	29.03	282 01
57	1.39	30.4	2836 01
58	0.207	30.91	422 01

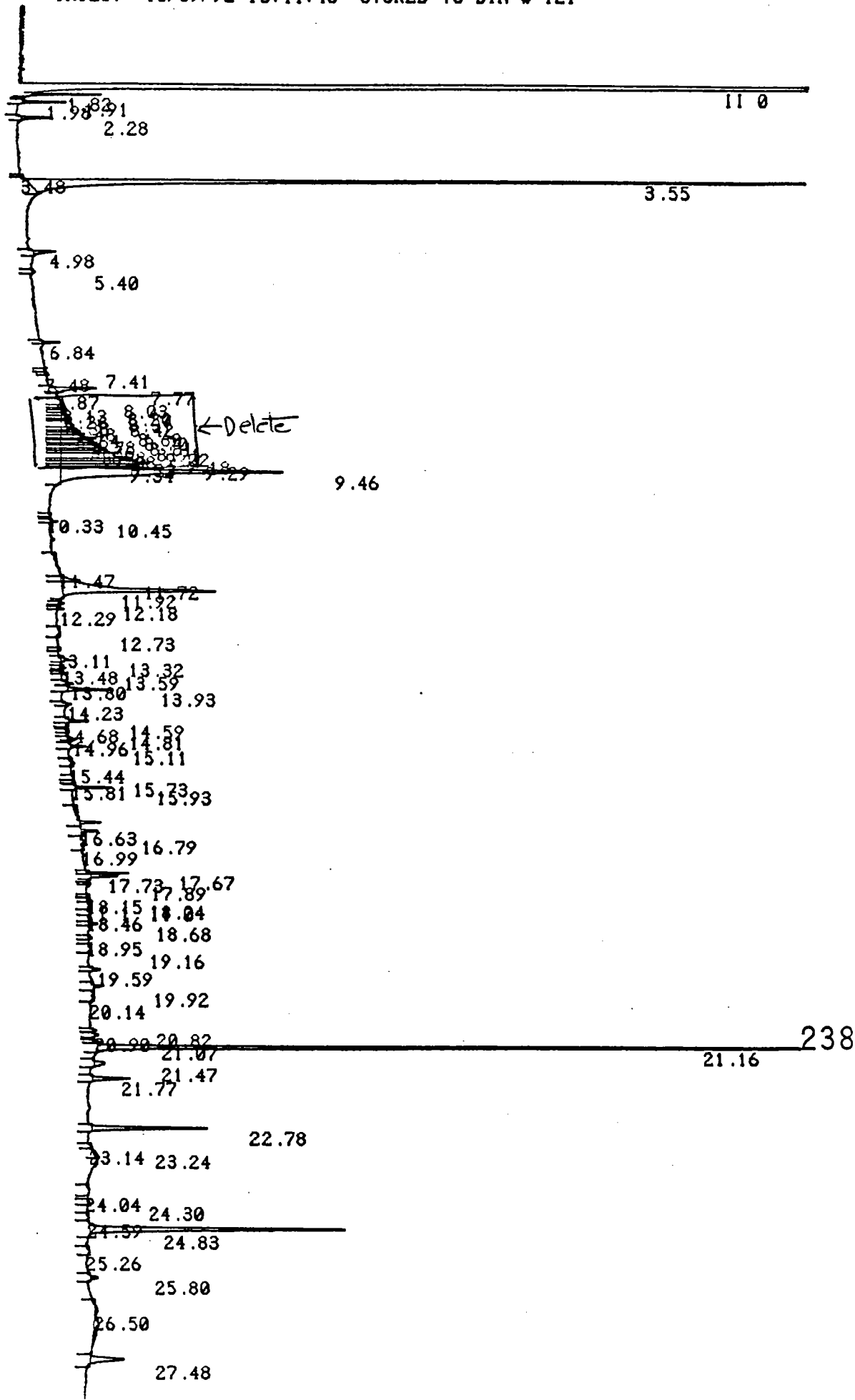
TOTAL 100. 203971

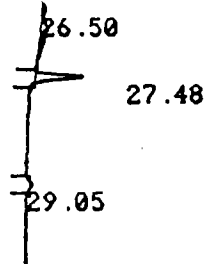
WARNING - MEMORY AT 6. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

X
10-9-10 AAL-7749 Bag 3 repeat 0.5cc 8x FID

CHANNEL A

INJECT 10/09/92 15:11:43 STORED TO BIN # 121





DATA SAVED TO BIN # 121

10/09/92 15:11:43

CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 660 INDEX 460 BIN 121

PEAK#	AREA%	RT	AREA BC
1	0.76	1.82	1998 01
2	0.02	1.91	52 02
3	0.554	1.98	1456 03
4	0.51	2.28	1339 01
5	0.045	3.48	119 02
6	23.293	3.55	61198 03
7	0.492	4.98	1292 01
8	0.057	5.4	151 01
9	0.2	6.84	525 01
10	0.028	7.41	74 02
11	0.04	7.48	106 03
12	0.896	7.77	2354 02
13	0.011	7.87	28 03
14	0.257	8.03	674 02
15	0.172	8.13	452 02
16	0.147	8.2	386 02
17	0.182	8.26	479 02
18	0.201	8.31	527 02
19	0.26	8.38	683 02
20	0.187	8.42	490 02
21	0.721	8.48	1893 02
22	0.44	8.6	1157 02
23	0.342	8.64	899 02
24	0.535	8.7	1405 02
25	0.9	8.78	2364 02
26	0.443	8.81	1163 02
27	0.837	8.86	2198 02
28	0.721	8.91	1893 02
29	1.096	8.98	2880 02
30	0.849	9.02	2231 02
31	1.161	9.08	3051 02
32	2.672	9.18	7021 02
33	1.578	9.23	4147 02
34	2.077	9.29	5457 02
35	1.658	9.34	4357 02
36	9.93	9.46	26089 03
37	0.03	10.33	79 01
38	0.103	10.45	271 01
39	0.609	11.47	1600 02
40	0.742	11.72	1950 02
41	6.163	11.92	16193 03
42	0.065	12.18	170 01

Delete
45834

43	0.078	12.29	205 01
44	0.086	12.73	226 01
45	0.022	13.11	58 01
46	0.185	13.32	485 01
47	0.067	13.48	176 01
48	0.022	13.59	57 01

31	1.161	9.08	2231 02
32	2.672	9.18	3051 02
33	1.578	9.23	7021 02
34	2.077	9.29	4147 02
35	1.658	9.34	5457 02
36	9.93	9.46	4357 02
37	0.03	10.33	26089 03
38	0.103	10.45	79 01
39	0.609	11.47	271 01
40	0.742	11.72	1600 02
41	6.163	11.92	1950 02
42	0.065	12.18	16193 03
			170 01

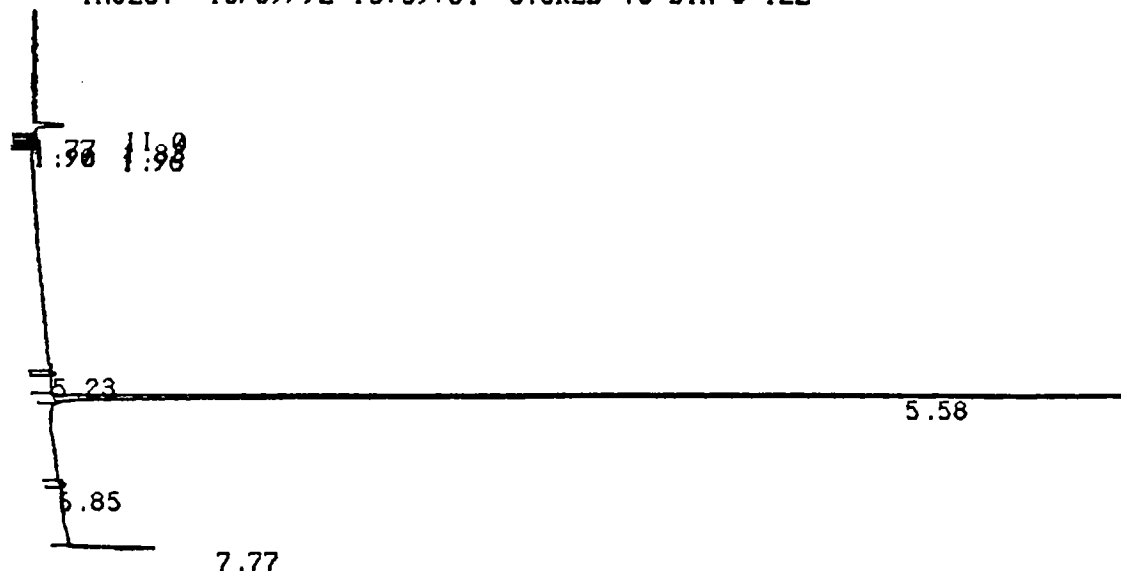
43	0.078	12.29	205 01
44	0.086	12.73	226 01
45	0.022	13.11	58 01
46	0.185	13.32	485 01
47	0.067	13.48	176 01
48	0.022	13.59	57 01
49	0.156	13.8	409 01
50	0.799	13.93	2098 01
51	0.124	14.23	327 01
52	0.321	14.59	844 02
53	0.038	14.68	100 03
54	0.034	14.81	89 01
55	0.108	14.96	283 01
56	0.275	15.11	723 01
57	0.057	15.44	149 01
58	0.041	15.73	108 02
59	0.044	15.81	116 03
60	0.515	15.93	1353 01
61	0.524	16.63	1378 02
62	0.434	16.79	1139 02
63	0.185	16.99	487 03
64	0.574	17.67	1509 02
65	0.437	17.73	1147 03
66	0.024	17.89	62 01
67	0.041	18.15	108 01
68	0.071	18.24	187 01
69	0.063	18.46	165 01
70	0.107	18.68	282 01
71	0.046	18.95	122 01
72	0.059	19.16	156 01
73	0.183	19.59	480 01
74	0.201	19.92	527 02
75	0.134	20.14	352 03
76	0.081	20.82	213 01
77	0.111	20.9	291 01
78	0.174	21.07	458 02
79	16.757	21.16	44024 03
80	0.398	21.47	1046 01
81	0.792	21.77	2082 01
82	2.397	22.78	6298 01
83	0.058	23.14	152 02
84	0.118	23.24	310 03
85	0.11	24.04	289 01
86	0.082	24.3	215 01
87	0.056	24.59	146 02
88	6.763	24.83	17767 03
89	0.073	25.26	192 01
90	0.273	25.8	718 01
91	2.278	26.5	5986 02
92	1.247	27.48	3277 03
93	0.192	29.05	505 01

TOTAL 100.

262727 - 91051 - 2(CP93)

X
10-9-11 11.2 ppm heptane std 0.5cc 8x FID

CHANNEL A INJECT 10/09/92 15:59:34 STORED TO BIN # 122



DATA SAVED TO BIN # 122

10/09/92 15:59:34 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 661 INDEX 461 BIN 122

PEAK#	AREA%	RT	AREA BC
1	0.109	1.77	59 01
2	0.152	1.83	82 01
3	0.145	1.9	78 01
4	0.143	1.96	77 01
5	0.221	5.23	119 01
6	98.684	5.58	53243 01
7	0.2	6.85	108 01
8	0.347	7.77	187 01

TOTAL 100. 53953

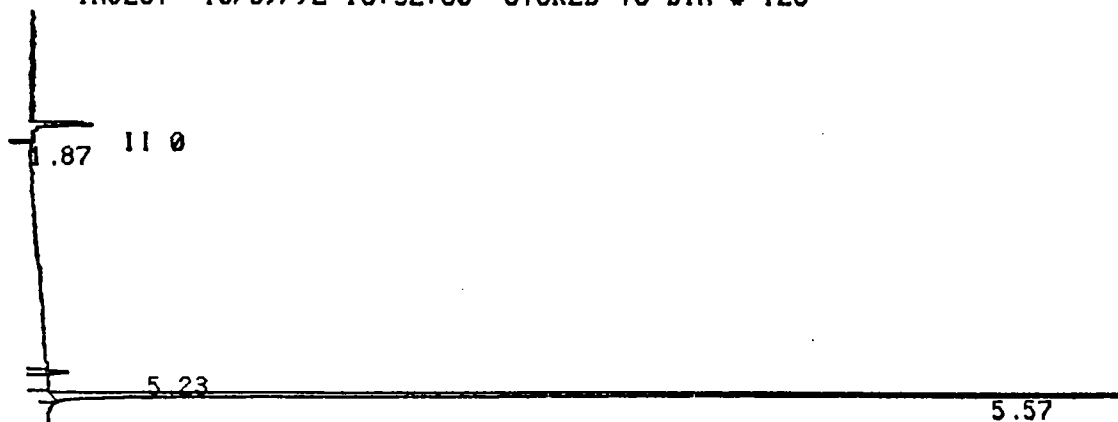
***** METHOD AT 0.5 MIN. UNEXPECTED SUBSTRATE MAY BE DETECTED *****

10	0.113	6.84	185 02
11	0.069	6.84	114 03
12	8.184	7.17	13442 01

TOTAL 100. 164255

24.

10-9-15 43.05 ppm std 0.5cc 8x FID
 CHANNEL A INJECT 10/09/92 16:52:30 STORED TO BIN # 126



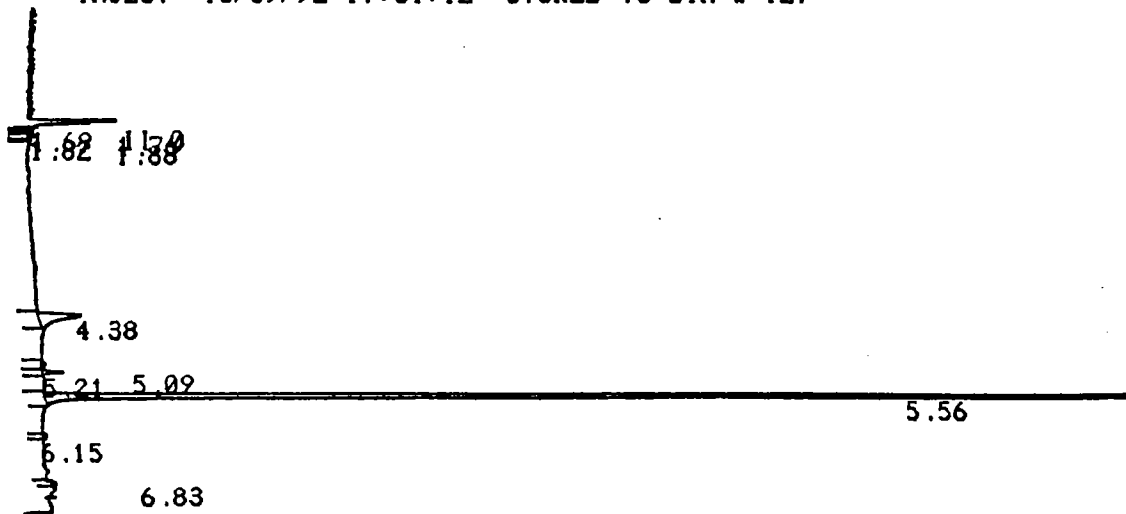
DATA SAVED TO BIN # 126

10/09/92 16:52:30 CH= "A" PS= 1.
 FILE 1. METHOD 0. RUN 665 INDEX 465 BIN 126

PEAK#	AREA%	RT	AREA BC
1	0.021	1.87	46 01
2	0.234	5.23	503 01
3	99.744	5.57	214249 01

x TOTAL 100. 214798
 10-9-16 43.05 ppm heptane std 0.5cc 8x FID

CHANNEL A INJECT 10/09/92 17:01:12 STORED TO BIN # 127



DATA SAVED TO BIN # 127

10/09/92 17:01:12 CH= "A" PS= 1.
 FILE 1. METHOD 0. RUN 666 INDEX 466 BIN 127

DATA SAVED TO BIN # 126

10/09/92 16:52:30

CH= "A" PS= 1.

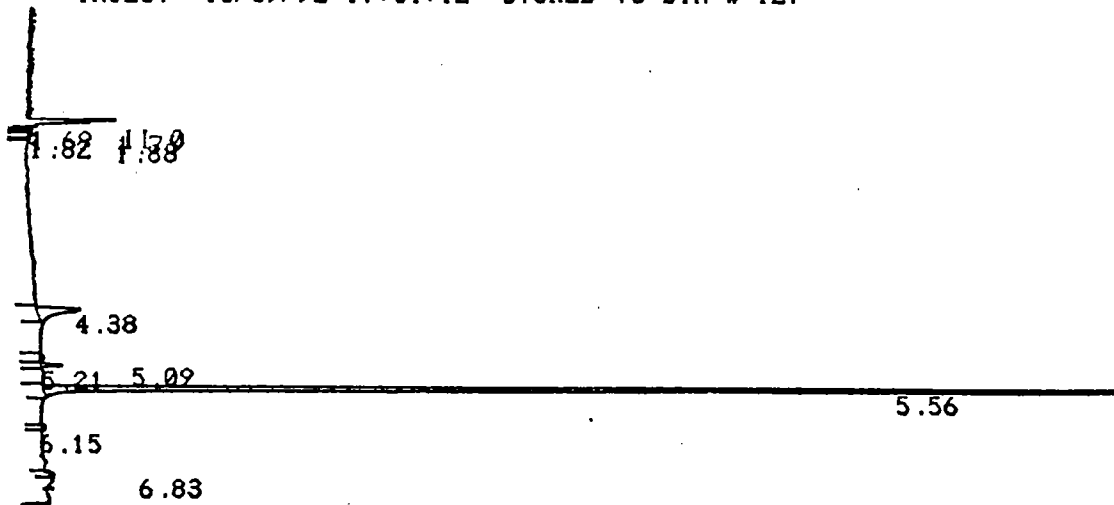
FILE 1. METHOD 0. RUN 665 INDEX 465 BIN 126

PEAK#	AREA%	RT	AREA BC
1	0.021	1.87	46 01
2	0.234	5.23	503 01
3	99.744	5.57	214249 01

X TOTAL 100. 214798

10-9-16 43.05 ppm heptane std 0.5cc 8x FID

CHANNEL A INJECT 10/09/92 17:01:12 STORED TO BIN # 127



DATA SAVED TO BIN # 127

10/09/92 17:01:12

CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 666 INDEX 466 BIN 127

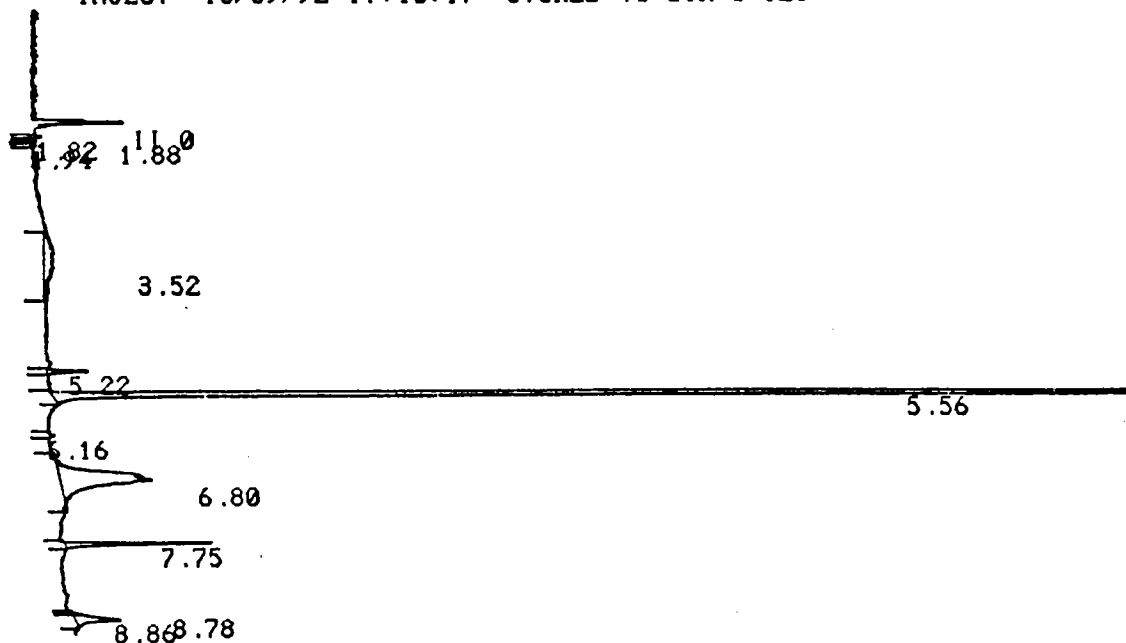
PEAK#	AREA%	RT	AREA BC
1	0.036	1.69	75 01
2	0.035	1.76	73 01
3	0.071	1.82	150 02
4	0.022	1.88	46 03
5	1.387	4.38	2928 01
6	0.084	5.09	177 02
7	0.231	5.21	487 03

8	98.037	5.56	206968 01
9	0.028	6.15	59 01
10	0.071	6.83	150 01

TOTAL 100. 211113

244

X A FAULT 33: AT 2680
 10-9-17 82.1 ppm hexane std 0.5cc 8x FID
 CHANNEL A INJECT 10/09/92 17:15:17 STORED TO BIN # 128



DATA SAVED TO BIN # 128

10/09/92 17:15:17 CH= "A" PS= 1.
 FILE 1. METHOD 0. RUN 667 INDEX 467 BIN 128

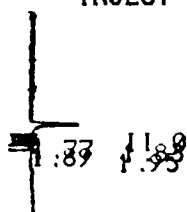
PEAK#	AREA%	RT	AREA BC
1	0.036	1.82	157 01
2	0.018	1.88	78 01
3	0.015	1.94	63 01
4	0.642	3.52	2781 01
5	0.227	5.22	984 01
6	93.543	5.56	405118 01
7	0.035	6.16	151 01
8	3.857	6.8	16706 01
9	0.872	7.75	3775 01
10	0.062	8.78	270 02
11	0.693	8.86	3001 03
TOTAL	100.		433084

245

WARNING - MEMORY AT 3. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

X 10-9-18 82.1 ppm hexane std 0.5cc 8x FID

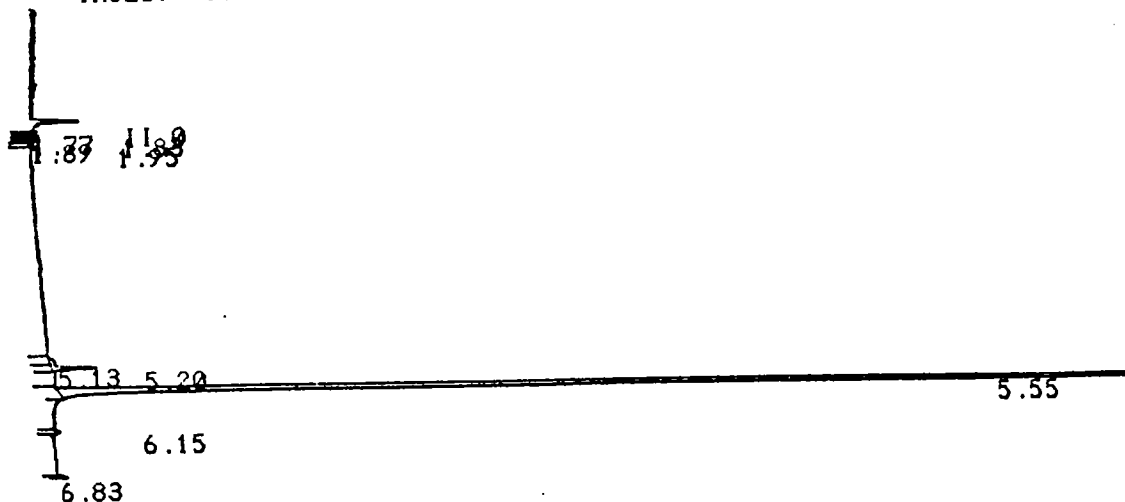
CHANNEL A INJECT 10/09/92 17:29:17 STORED TO BIN # 1



WARNING - MEMORY AT 3. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10-9-18 82.1 ppm heptane std 0.5cc 8x FID

CHANNEL A INJECT 10/09/92 17:29:17 STORED TO BIN # 1



DATA SAVED TO BIN # 1

10/09/92 17:29:17 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 668 INDEX 468 BIN 1

PEAK#	AREA%	RT	AREA BC
1	0.015	1.77	60 01
2	0.022	1.83	89 01
3	0.012	1.89	48 01
4	0.014	1.95	58 01
5	0.066	5.13	271 02
6	0.266	5.2	1100 03
7	99.574	5.55	411337 01
8	0.033	6.15	135 01

TOTAL 100. 413098

WARNING - MEMORY AT 3. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

✓
10-10-3 N₂ Blank

0.5cc 8 x FID

CHANNEL A

INJECT 10/10/92 09:46:31 STORED TO BIN # 5

11.38 11.70

9.88

10.43 10.54

10.75 10.95

11.00 11.21

11.38 11.67

11.80 11.98

12.14 12.23

12.40 12.49

12.73

17.63

11 1 11 0

20.03

20.65 20.59

21.69

10-12-1

N2 Blank

0.5cc 8x

CHANNEL A

INJECT 10/12/92 10:33:22 STORED TO BIN # 21

1.35 1.80

10.77

11.69 11.91

13.92

17.71

11 1 11 0

19.58

21.75

ER 0

DATA SAVED TO BIN # 21

10/12/92 10:33:22

CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 688 INDEX 488 BIN 21

PEAK#	AREA%	RT	AREA BC
1	3.725	1.75	98 01
2	2.623	1.81	69 01
3	2.014	1.95	53 01
4	2.052	10.77	54 01
5	13.303	11.69	350 01
6	6.005	11.91	158 01
7	4.181	13.92	110 01
8	13.417	17.71	353 01
9	21.931	19.58	577 01
10	20.487	21.75	539 01
11	10.262	24.71	270 01

TOTAL 100. 2631

WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

CHANNEL A INJECT 10/12/92 11:17:06 STORED TO BIN # 22

1:33 1:35

5.56

DATA SAVED TO BIN # 22

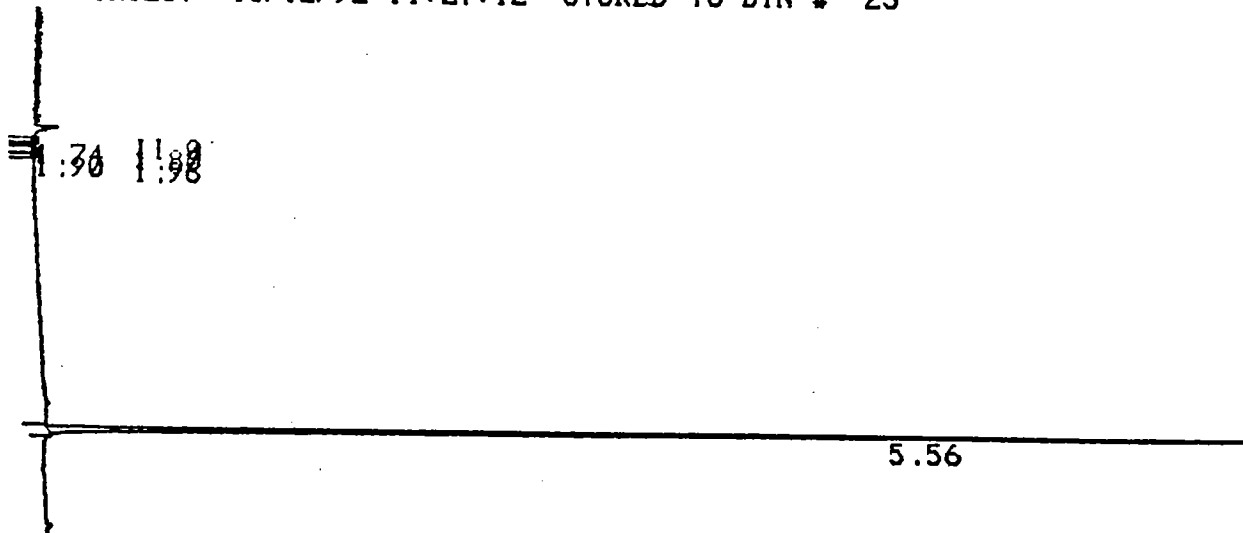
10/12/92 11:17:06

CH= "A" PS= 1.

PEAK#	AREA%	RT	AREA BC
1	0.17	1.77	51 01
2	0.22	1.83	66 01
3	0.19	1.89	57 02
4	0.383	1.95	115 03
5	99.039	5.56	29771 01
TOTAL	100.		30060

x
10-12-3 6.8 ppm hexane std 0.5cc 8x FID

CHANNEL A INJECT 10/12/92 11:27:12 STORED TO BIN # 23



DATA SAVED TO BIN # 23

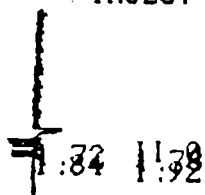
10/12/92 11:27:12 CH= "A" PS= 1.

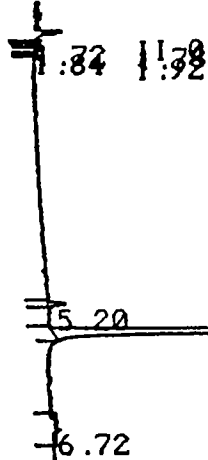
FILE 1. METHOD 0. RUN 690 INDEX 490 BIN 23

PEAK#	AREA%	RT	AREA BC
1	0.36	1.74	110 02
2	0.318	1.8	97 03
3	0.41	1.9	125 01
4	0.249	1.96	76 01
5	98.663	5.56	30113 01
TOTAL	100.		30521

x
10-12-4 33.5 ppm hexane std 0.5cc 8x FID

CHANNEL A INJECT 10/12/92 11:37:07 STORED TO BIN # 24





27

DATA SAVED TO BIN # 24

10/12/92 11:37:07

CH= "A" PS= 1.

FILE 1.

METHOD 0.

RUN 691

INDEX 491

BIN 24

PEAK#	AREA%	RT	AREA BC
1	0.063	1.72	99 01
2	0.046	1.78	73 01
3	0.027	1.84	42 01
4	0.031	1.92	49 01
5	0.237	5.2	373 01
6	99.206	5.54	156061 01
7	0.39	6.72	613 01

TOTAL

100.

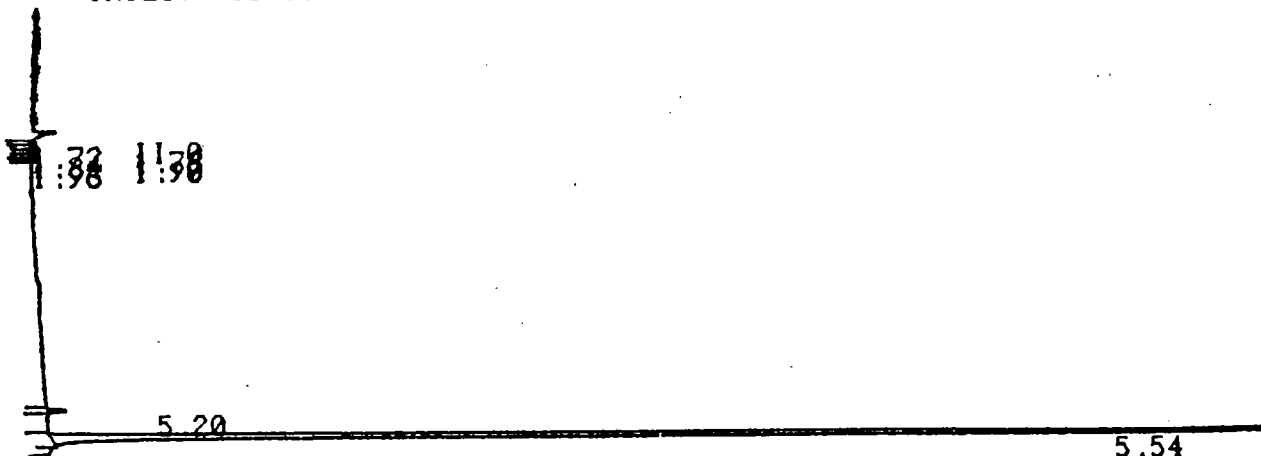
157310

WARNING - MEMORY AT 7. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10-12-5 33.5 ppm before std 0.5cc 8x

CHANNEL A

INJECT 10/12/92 11:47:45 STORED TO BIN # 25



DATA SAVED TO BIN # 25

10/12/92 11:47:45

CH= "A" PS= 1.

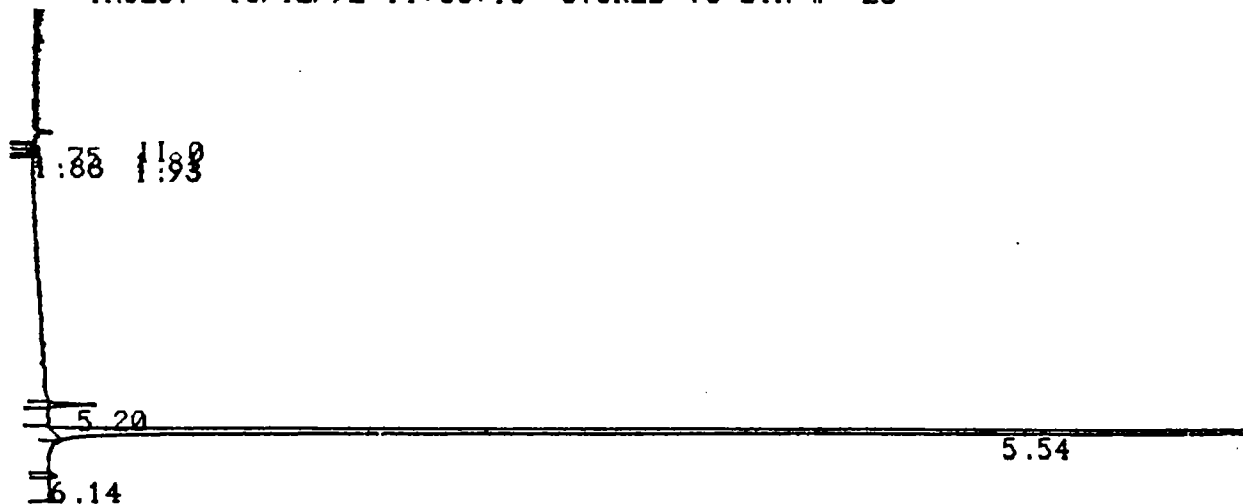
2	0.04	1.78	65 01
3	0.042	1.84	69 01
4	0.051	1.9	83 01
5	0.021	1.96	34 01
6	0.231	5.2	376 01
7	99.567	5.54	162282 01

TOTAL 100. 162987

WARNING - MEMORY AT 4. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10-12-6 98.4 ppm hexane std 0.5cc 8x FID

CHANNEL A INJECT 10/12/92 11:56:16 STORED TO BIN # 26



DATA SAVED TO BIN # 26

10/12/92 11:56:16 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 693 INDEX 493 BIN 26

PEAK#	AREA%	RT	AREA BC
1	0.01	1.75	43 01
2	0.017	1.81	74 01
3	0.013	1.86	58 01
4	0.014	1.93	62 01
5	0.21	5.2	921 01
6	99.696	5.54	437222 01
7	0.04	6.14	174 01

TOTAL 100. 438554

WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10-12-7 98.4 ppm hexane std 0.5cc 8x FID

CHANNEL A INJECT 10/12/92 12:05:19 STORED TO BIN # 27

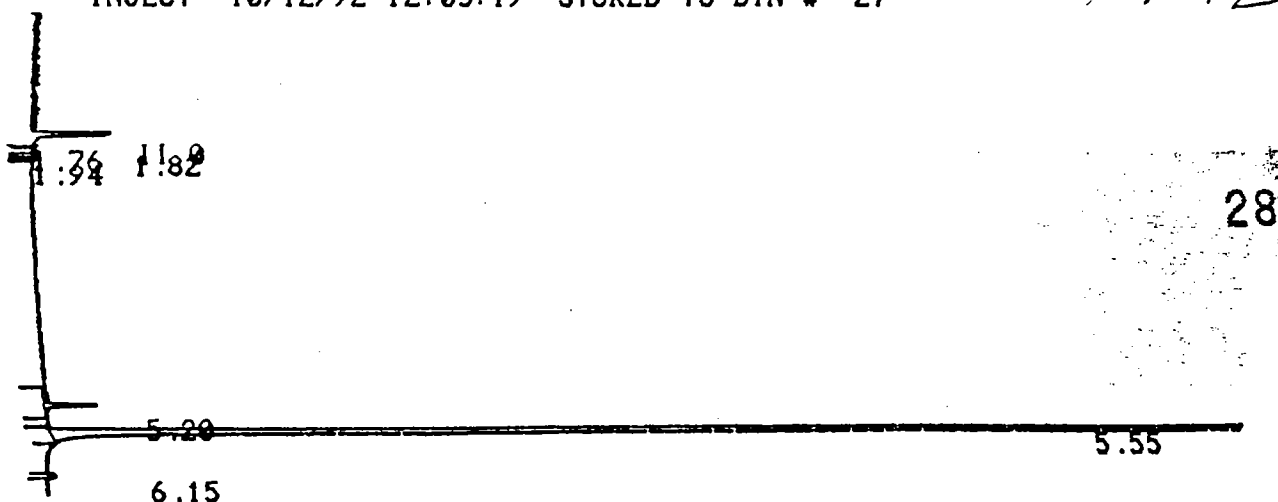
FILE 1. METHOD 0. RUN 693 INDEX 493 BIN 26

PEAK#	AREA%	RT	AREA BC
1	0.01	1.75	43 01
2	0.017	1.81	74 01
3	0.013	1.86	58 01
4	0.014	1.93	62 01
5	0.21	5.2	921 01
6	99.696	5.54	437222 01
7	0.04	6.14	174 01

TOTAL 100. 438554

WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10-12-7 98.4 ppm hexane std 0.5cc 8x FID
CHANNEL A INJECT 10/12/92 12:05:19 STORED TO BIN # 27



DATA SAVED TO BIN # 27

10/12/92 12:05:19 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 694 INDEX 494 BIN 27

PEAK#	AREA%	RT	AREA BC
1	0.018	1.76	82 01
2	0.016	1.82	70 01
3	0.018	1.94	82 01
4	0.277	5.2	1228 01
5	99.633	5.55	442200 01
6	0.037	6.15	166 01

TOTAL 100. 443828

10-12-8 AAL-7749 Bag 5 0.5cc 8x FID
CHANNEL A INJECT 10/12/92 12:14:50 STORED TO BIN # 28

9	0.408	8.76	345 01
10	0.082	10.11	69 01
11	0.273	10.44	231 01
12	0.089	10.82	75 01
13	0.151	11.8	128 01
14	1.149	11.92	972 01
15	0.171	12.17	145 01
16	0.199	12.28	168 01
17	0.203	13.46	172 01
18	0.222	13.92	188 01

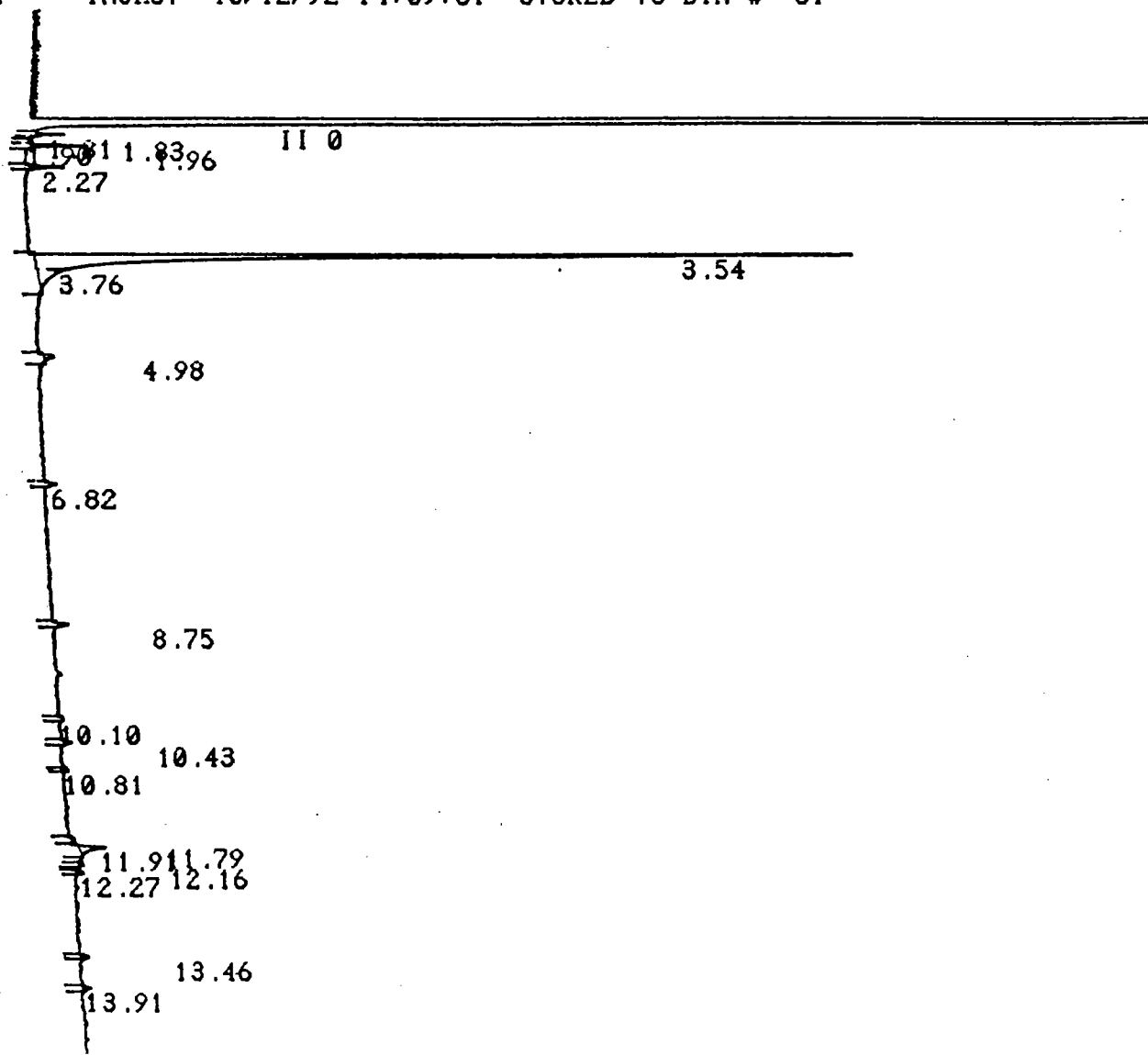
2

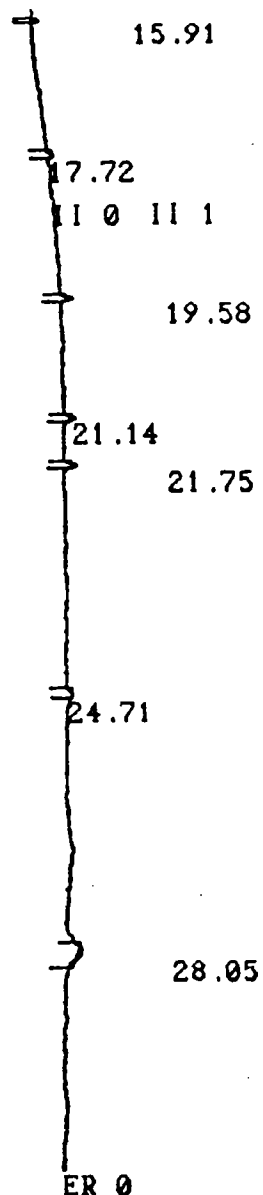
19	0.139	15.91	118 01
20	0.174	17.72	147 01
21	0.311	19.58	263 01
22	0.399	21.15	338 01
23	0.255	21.76	216 01
24	53.184	28.37	45010 01

TOTAL 100. 84630

WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

X 10-12-11 AAL-7749 Bag 5 0.5cc 8x FID
 CHANNEL A INJECT 10/12/92 14:09:31 STORED TO BIN # 31





ER 0

DATA SAVED TO BIN # 31

10/12/92 14:09:31

CH= "A" PS= 1.

FILE 1.

METHOD 0.

RUN 698

INDEX 498

BIN 31

PEAK#	AREA%	RT	AREA BC
1	1.421	1.81	635 02
2	0.183	1.83	82 03
3	0.213	1.9	95 02
4	2.678	1.96	1197 03
5	1.729	2.27	773 01
6	78.935	3.54	35284 08
7	0.004	3.76	2 05
8	1.622	4.98	725 01
9	0.626	6.82	280 01
10	0.841	8.75	376 01
11	0.266	10.1	119 01
12	0.586	10.43	262 01
13	0.181	10.81	81 01
14	0.262	11.79	117 02
15	3.494	11.91	1562 03
16	0.367	12.16	164 01
17	0.347	12.27	155 01

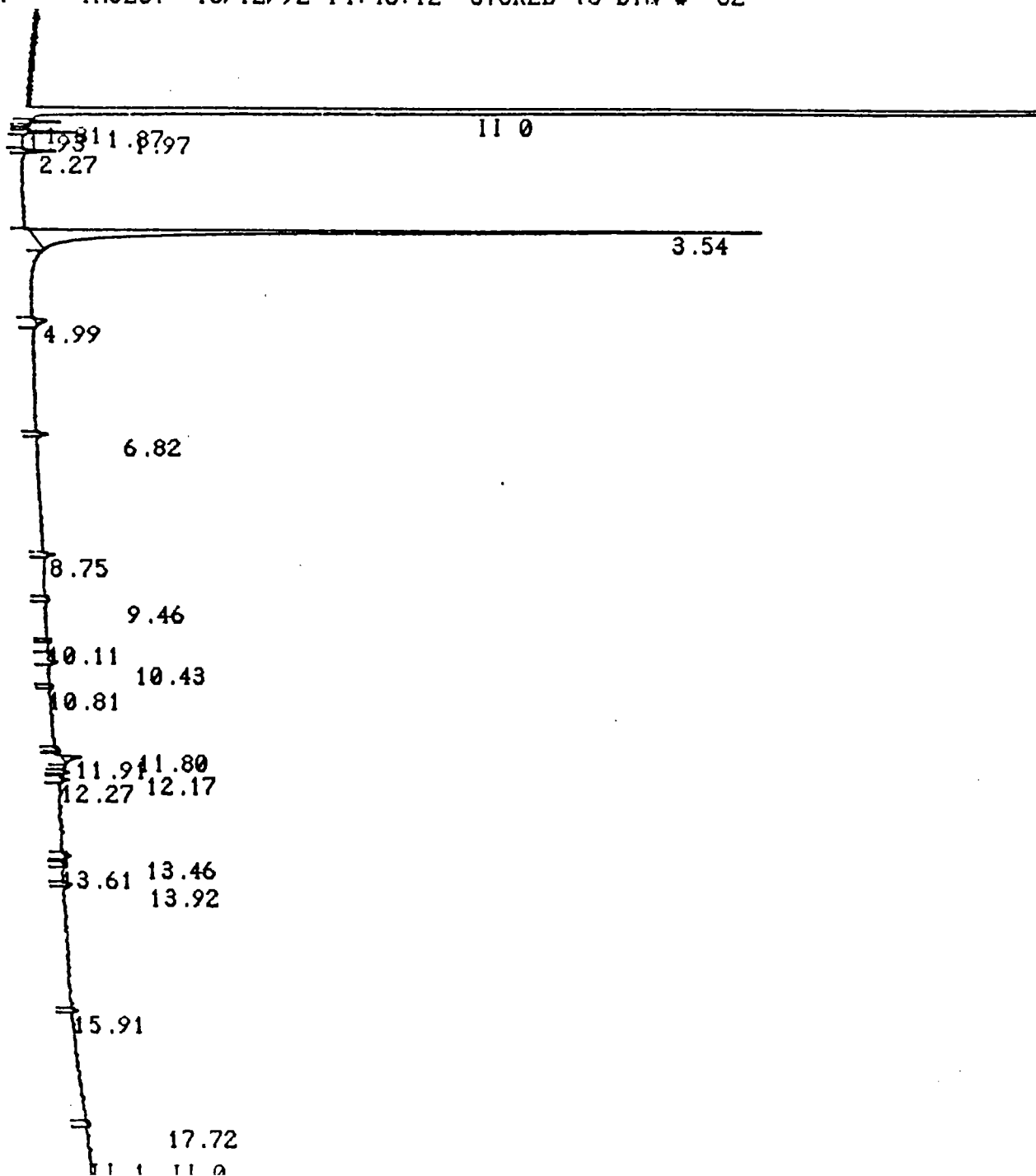
17	0.342	15.91	153 01
20	0.342	15.91	153 01
21	0.356	17.72	159 01
22	0.696	19.58	311 01
23	0.647	21.14	289 01
24	0.694	21.75	310 01
25	0.4	24.71	179 01
26	2.208	28.05	987 01

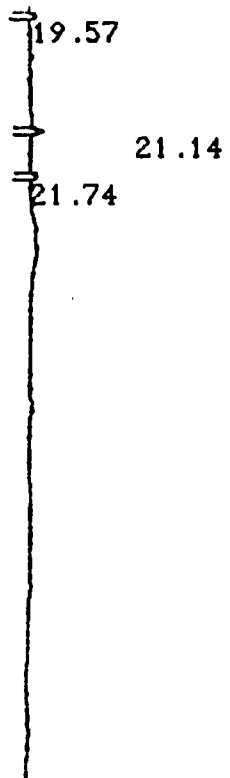
TOTAL 100. 44700

WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10-12-12 AAL-7749 bag 5 repeat 0.5cc 8x

CHANNEL A INJECT 10/12/92 14:46:12 STORED TO BIN # 32





DATA SAVED TO BIN # 32

10/12/92 14:46:12

CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 699 INDEX 499 BIN 32

PEAK#	AREA%	RT	AREA BC
1	1.727	1.81	710 02
2	0.263	1.87	108 03
3	0.263	1.93	108 02
4	2.731	1.97	1123 03
5	1.877	2.27	772 01
6	80.022	3.54	32905 01
7	1.89	4.99	777 01
8	0.679	6.82	279 01
9	0.786	8.75	323 01
10	0.263	9.46	108 01
11	0.195	10.11	80 01
12	0.824	10.43	339 01
13	0.236	10.81	97 01
14	0.27	11.8	111 01
15	3.329	11.91	1369 01
16	0.489	12.17	201 01
17	0.615	12.27	253 01
18	0.547	13.46	225 01
19	0.212	13.61	87 01
20	0.479	13.92	197 01
21	0.384	15.91	158 01
22	0.304	17.72	125 01
23	0.455	19.57	187 01
24	0.72	21.14	296 01
25	0.443	21.74	182 01

TOTAL 100.

41120

CHANNEL A

INJECT 10/12/92 15:25:11 STORED TO BIN # 33

11 0
1.81 1.91
1.97 2.27

3.58

4.99

6.81

8.75

9.45

10.11
10.43

10.82

11.26

11.91
12.16 12.27

13.26 13.47

13.63
13.96 13.91

15.90 15.80

16.60

17.70

11 0 11 1

19.57

21.13

21.73

24.68

DATA SAVED TO BIN # 33

10/12/92 15:25:11 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 700 INDEX 500 BIN 33

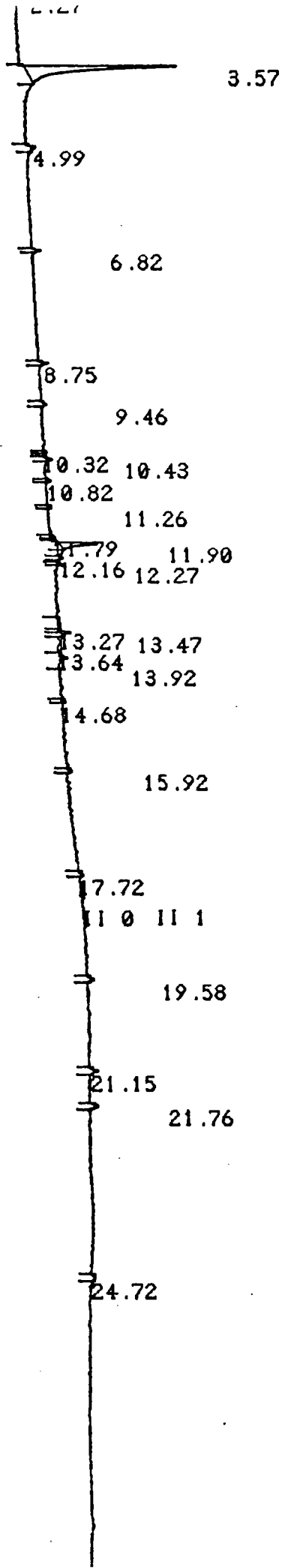
PEAK#	AREA%	RT	AREA BC
1	3.753	1.81	774 08
2	0.475	1.91	98 06
3	4.941	1.97	1019 03
4	3.03	2.27	625 01
5	49.903	3.58	10292 01
6	2.638	4.99	544 01
7	1.11	6.81	229 01
8	1.392	8.75	287 01
9	0.655	9.45	135 01
10	0.31	10.11	64 01
11	1.522	10.43	314 01
12	0.635	10.82	131 01
13	0.272	11.26	56 01
14	10.745	11.91	2216 01
15	0.645	12.16	133 01
16	0.756	12.27	156 01
17	0.432	13.26	89 01
18	2.74	13.47	565 01
19	1.906	13.63	393 02
20	1.489	13.91	307 02
21	0.247	13.96	51 03
22	2.856	15.8	589 02
23	1.062	15.9	219 03
24	0.344	16.6	71 01
25	0.655	17.7	135 01
26	1.484	19.57	306 01
27	1.299	21.13	268 01
28	1.823	21.73	376 01
29	0.882	24.68	182 01

TOTAL 100. 20624

WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

CHANNEL A INJECT 10/12/92 16:01:41 STORED TO BIN # 34

10-12-14 AAL-7749 Bag 6 0.5 cc 8x FID



10/12/92 16:01:41

CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 701 INDEX 501 BIN 34

PEAK# AREA% RT AREA BC

1	0.404	1.78	89 02
2	2.849	1.81	628 03
3	0.254	1.9	56 02
4	5.018	1.97	1106 03
5	3.122	2.27	688 01
6	53.469	3.57	11784 01
7	2.287	4.99	504 01
8	1.121	6.82	247 01
9	1.307	8.75	288 01
10	0.685	9.46	151 01
11	0.322	10.32	71 01
12	1.143	10.43	252 01
13	0.49	10.82	108 01
14	0.363	11.26	80 01
15	0.476	11.79	105 01
16	11.797	11.9	2600 01
17	0.672	12.16	148 01
18	0.631	12.27	139 01
19	0.998	13.27	220 02
20	3.076	13.47	678 03
21	1.357	13.64	299 02
22	1.629	13.92	359 03
23	0.118	14.68	26 01
24	0.758	15.92	167 01
25	0.662	17.72	146 01
26	1.307	19.58	288 01
27	1.525	21.15	336 01
28	1.243	21.76	274 01
29	0.917	24.72	202 01

TOTAL 100.

22039

X WARNING - MEMORY AT 1. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

0-12-15
CHANNEL A98.4 ppm hexane std
INJECT

10/12/92 16:42:01 STORED TO BIN # 35

1.89 1.93

6.13

DATA SAVED TO BIN # 35

10/12/92 16:42:01 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 702 INDEX 502 BIN 35

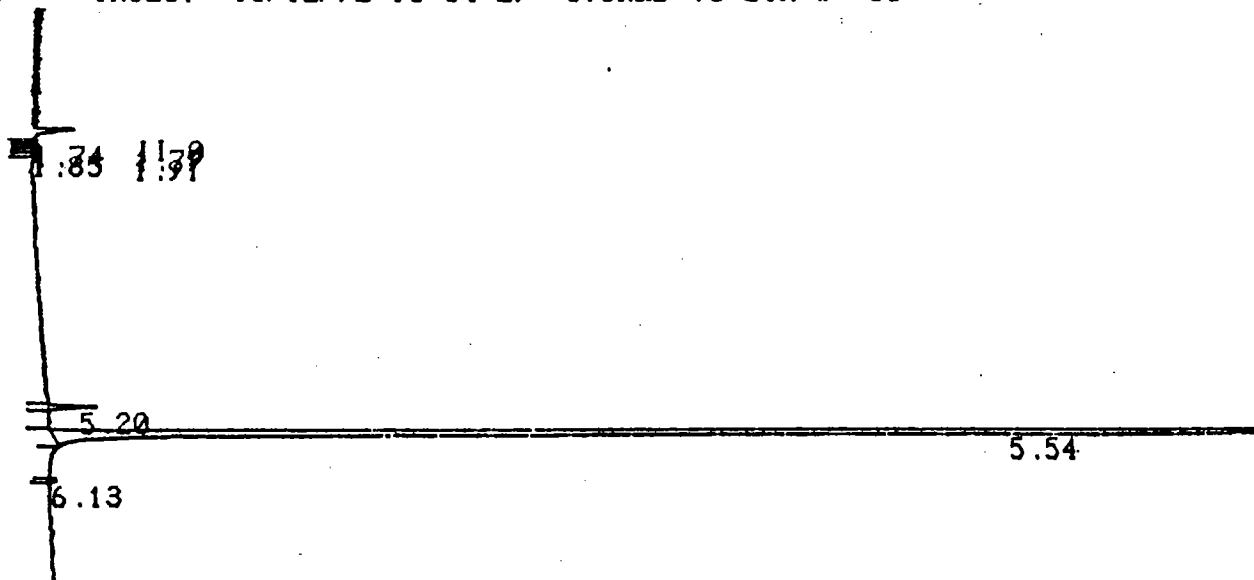
PEAK#	AREA%	RT	AREA BC
1	0.027	1.71	113 01
2	0.015	1.77	63 01
3	0.012	1.89	49 01
4	0.016	1.95	67 01
5	0.235	5.19	976 01
6	99.67	5.53	413690 01
7	0.024	6.13	100 01

TOTAL 100. 415058

WARNING - MEMORY AT 0. K - UNPROTECTED CHROMATOGRAMS WILL BE REPLACED

10^x-12-16 98.4 ppm std 0.5cc 8x

CHANNEL A INJECT 10/12/92 16:54:29 STORED TO BIN # 36



DATA SAVED TO BIN # 36

10/12/92 16:54:29 CH= "A" PS= 1.

FILE 1. METHOD 0. RUN 703 INDEX 503 BIN 36

PEAK# AREA% RT AREA BC

2	0.013	1.77	03 01
3	0.014	1.85	60 01
4	0.017	1.91	75 01
5	0.235	5.2	1022 01
6	99.683	5.54	434257 01
7	0.028	6.13	120 01
TOTAL	100.		435640

APPENDIX F

List of Participants

LIST OF PARTICIPANTS

ROJAC ENVIRONMENTAL SERVICES, INC.
30 Arbor Street
Hartford, CT 06106
Ms. Eszter Samodai - Project Manager
Mr. John Gammie - Project Engineer
Mr. James Davis - Project Technician
tel: (203) 232-8959

ENERGY TACTICS, INC.
124 Sills Road (Rte. 101)
P.O. Box 7
Yaphank, NY 11980
Mr. Richard Voldstad - Vice President, Engineering
Mr. Joseph Snyder - Project Engineer
tel: (516) 924-5300

NEW YORK STATE DEPARTMENT OF ENVIRONMENTAL CONSERVATION
SUNY, Bldg. 40
Stony Brook, NY 11794
Mr. Gary E. Zimmerman - Principal Engineering Technician
Mr. Humberto Roman - Environmental Engineer I
tel: (516) 751-7900

CIGNA ENVIRONMENTAL HEALTH LABORATORY
94 Murphy Road
Hartford, CT 06114
Mr. James Kenny - Laboratory Manager
tel: (203) 522-3814

ATLANTIC ANALYTICAL LABORATORY, INC.
P.O. Box 220
Salem Industrial Park, Bldg. #4
Whitehouse, NJ 08888
Mr. Victor Given - Laboratory Analyst
tel: (908) 534-5600

