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# **REPORT OF AIR POLLUTION SOURCE TESTING FOR CALIFORNIA AB2588 AT THE KERN RIVER COGENERATION COMPANY BAKERSFIELD, CALIFORNIA**

**Submitted to:**

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**Submitted on:**

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**REPORT OF AIR POLLUTION SOURCE TESTING  
FOR CALIFORNIA AB2588 AT THE  
KERN RIVER COGENERATION COMPANY  
BAKERSFIELD, CALIFORNIA**

**INTRODUCTION**

Kern River Cogeneration Company (KRCC) retained Engineering-Science (ES) to conduct air pollution source tests on a 75 MW cogeneration unit operated at Bakersfield, California. The purpose of the testing program was to determine emissions as stipulated by California Assembly Bill 2588.

AB2588 requires that KRCC conduct a monitoring program on one of the gas turbines while the unit is fired on fuel oil. Included in the source testing program were the determination of emission rates of formaldehyde, benzene, polynuclear aromatic hydrocarbons (PAH), dioxins (PCDD), furans (PCDF), hydrogen chloride, and trace elements, hexavalent chromium, beryllium, cadmium, nickel, arsenic, copper, lead, manganese, mercury, selenium, and zinc). Radionuclides were determined on a fuel sample collected by Engineering-Science during the testing program. The testing program was conducted in accordance with California Air Resources Board (CARB) and EPA test procedures.

The testing commenced January 25 and concluded in the early morning hours of January 26, 1990. Mr. Mervyn Soares, Environmental Engineer for KRCC coordinated the testing program. The ES testing team was comprised of Messrs. Dennis Bautista, Dennis Becvar (team leader), Jonathan Dailey, Humbert Deriada, Mike Edwards, Senen Karikitan, Tony King, Rollie Rosario and Dwight Wieman. Kern County Air Pollution Control District test observers were Messrs. Steven Arita, Greg Lafore and Ted Strauss.

**SOURCE INFORMATION**

KRCC operates a cogeneration facility comprised of four natural gas fired turbines with the capabilities of using fuel oil as a backup fuel. The units are comprised of General Electric, Frame 7, gas turbines rated at 75 MW (nominal) electrical power. The turbines are also equipped with heat recovery steam generators (HRSG) that produce steam for use in enhanced oil recovery. The

turbines are equipped with water injection for NO<sub>x</sub> control. The testing program was conducted at the Heat Recovery Steam Generator (HRSG) on Unit #2. The primary fuel for the Omar Hill Unit #2 turbine is natural gas, however, it was operated on distillate oil for the AB 2588 testing.

## **SOURCE TEST PROCEDURES**

### **Testing Methods**

This section provides information on the sampling procedures and analytical methods used for each pollutant determination.

### **Location and Number of Traverse Points**

The sampling ports were located one half diameter from the nearest downstream disturbance and two diameters from the nearest upstream disturbance. In accordance with CARB Method 1, a sample traverse of 24 traverse points, 12 points per port for two ports was conducted.

The absence of cyclonic flow was determined using an S type pitot tube connected to an inclined oil manometer. The pitot tube was rotated so the planes of the face openings were perpendicular to the stack cross-sectional plane. This is referred to as the 0° reference position. A zero reading obtained in this position indicates no cyclonic flow. If the manometer did not read zero, the pitot tube was rotated until a zero reading was obtained. The angle of rotation was measured to the nearest degree. All traverse points were examined in this fashion. The average of all the rotation angles was less than 20°. The source testing location was deemed acceptable.

### **Preliminary Velocity and Temperature Traverse**

A preliminary velocity and temperature traverse was conducted in accordance with CARB Method 1 to calculate the diameter of the isokinetic source sampling nozzle and sampling rate required for the tests. An S type pitot tube and a K type thermocouple were positioned at each traverse point and the appropriate data recorded on a data sheet. The pitot tube was connected to an inclined oil manometer and the thermocouple was connected to an appropriate digital temperature readout device. All pitot tube and thermocouple sets were calibrated prior to use in the field.



## Trace Elements

Trace elements that were analyzed concluded samples for trace elements Zn, Cu, Be, Cd, Mn Pb, Se, and Hg. Each sample was collected isokinetically using an EPA proposed combined trace elements sampling train. The train was configured similar to the sampling train used for determining particulates (Method 5) except the first and second impingers contained nitric acid (HNO<sub>3</sub>) in a hydrogen peroxide (H<sub>2</sub>O<sub>2</sub>) solution. The third impinger was an empty modified Greenberg-Smith. The fourth impinger contained an acidified potassium permanganate (KMnO<sub>4</sub>) solution. The fifth impinger contained approximately 400 grams of indicating silica gel. A glass fiber filter was located between the fourth and fifth impingers. Sampling train components were recovered in separate HNO<sub>3</sub> and KMnO<sub>4</sub> fractions. After the testing, the samples were analyzed by Inductively Coupled Argon Plasma Mass Spectrometry (ICAP-MS).

Hexavalent Chromium sampling was conducted in accordance with CARB Method 425. The sampling technique is the same as that for Carb Method 5 for particulates except the impinger solution was sodium bicarbonate. The samples were analyzed for hexavalent chromium by colorimetric technique.

A separate sampling train was operated for Arsenic in according with CARB Method 423 for Arsenic. The method 423 sampling train was run concurrently with the trace metals train.

## Formaldehyde

Formaldehyde samples were collected in accordance with CARB Method 430. Three 4 hour test runs were conducted.

The sample train consisted of a Teflon lined probe connected to four impingers in series. The first and second impingers each contained 100ml each of @ 1% sodium bisulfite, the third impinger was empty, and the fourth contained about 400 grams of indicating silica gel.

After the testing the samples was sent to Thermo Analytical, Analytical Research Labs Inc. (TMA/ARLI) Monrovia, California.

## **Benzene Sampling**

Benzene samples were collected in accordance with CARB Method 410A. Three integrated samples were collected over one hour periods. The analysis were performed using a gas chromatograph (GC) equipped with a photo-ionization detector (PID).

## **Dioxins, Dibenzofurans, and Polynuclear Aromatic Hydrocarbons**

Dioxins (PCDD), Dibenzofurans (PCDF), and Polynuclear Aromatic Hydrocarbons (PAH) were collected in accordance with CARB Methods 428 and 429. The train design is based on a validated emission collection system with the addition of an adsorbent cartridge of XAD-2 resin to collect vaporous emissions for semi-volatile organics. The trains were operated for a period of 4 hours during each of three runs. The samples were collected using isokinetic sampling techniques described in CARB Method 5. The train recovery was modified from Method 5 procedures to include a sample wash with 1:1 methanol and methylene chloride.

The sampling probe liner was Teflon. Organics were collected by the adsorbent trap containing a precleaned XAD-2 Resin. This trap was made of glass and located in the sample line downstream of a heated filter holder and upstream of the first impinger. The module housing the trap was jacketed, and cold water was circulated to maintain an outlet temperature below 68°F. The trap was wrapped with aluminum foil to eliminate possible effects from ultraviolet light. A glass Hempal-type condenser was located between the filter and the XAD-2 cartridge to ensure that cool stack gas was entering the adsorbent trap.

All solvents used for preparing the sampling train for testing and field sample recovery were stored in glass bottles and were spectrographic grade. The train components that came in contact with the sample were handled with clean, bare hands. All components were free of potential interfering materials, especially silicone grease.

The probe was rinsed with three portions of 1:1 methanol and methylene chloride and brushed during each rinse. The connecting tube between the filter and the adsorbent cartridge were also rinsed with 1:1 methanol and methylene chloride. All probe, filter, connecting tubing, and impinger washings were collected in precleaned glass containers. The sample train were separated into front and back halves. Field and sample blanks were collected during the testing program. Composite samples

of the front and back halves were sealed and shipped to Cal-Analytical Labs Enseco, Sacramento, California for analysis.

The samples submitted to the laboratory included a sample train blank which was collected on site. A sampling train was prepared as if it were to be used on the stack; however, the train was washed with the appropriate solvents and collected in the respective containers, and designated as the blank.

### Hydrogen Chloride

Hydrogen Chloride sampling was conducted in accordance with CARB Method 421. It was similar to CARB 5 for particulate with two exceptions. First, the probe was lined with quartz glass to limit reactions between the gas and the probe. Second, to chemically collect the HCL, sodium carbonate and sodium bicarbonate solutions were used in the impingers. The impinger solution was analyzed for chloride ions using ion chromatography.

### Radionuclides

Radionuclides were analyzed by TMA/NORCAL, Emery, CA, Nuclear Science Laboratory for alpha, beta and gamma emitters from a fuel sample collected by Engineering-Science.

## **QUALITY CONTROL**

The following section describe the various quality assurance and quality control (QA/QC) procedures utilized by ES during this program.

### Sample Custody

A specific Chain-of-Custody procedure was used for this project. The elements of this plan include:

- Train component identification
- Sample identification
- Sample labels
- Documentation
- Chain of custody forms

The sequence of activities concerned with sample custody together with identification and tracing procedures are described below:

1. Sample train preparation by laboratory included filter holders, impingers, and other sampling equipment identified by tags and codes.
2. Sample train issued to test team and master log filled out. Sample I.D. number stickers issued according to test identification code.
3. Train returned to recovery area when a valid sample was obtained. Sample train accompanied by all field data sheets.
4. Recovery team recovered samples using appropriate containers, affixed sample I.D. labels to sample containers, to master log, to field data sheet, and to train recovery sheet.
5. Samples transferred or shipped to appropriate laboratory with Chain-of-Custody form.
6. Samples examined at each transfer point for integrity (broken containers, loss in liquid, seal and identity).

Upon completing the required analysis, the analyzing laboratory returned the Chain-of Custody form along with results to ES. All samples were accounted for by the ES Laboratory Supervisor and Project Manager. Each laboratory identified the samples in its own laboratory notebooks by the ES I.D. number as well as any internal identification. Notebooks are retained by each laboratory according to usual laboratory practices.

## **RESULTS**

The test results are presented in Tables 1-7. Supporting data are included in the appendices.

**Table 1**  
**Summary of Average Flow Data**  
**Unit #2 Stack**  
**January 25-26, 1990**  
**Kern River Cogeneration Company**  
**Bakersfield, California**

Parameter	Average
Stack Diameter (inches)	167.5
Stack Area (ft <sup>2</sup> )	153.02
Temperature (°F)	298
Moisture (%)	7.3
Oxygen (%)	14.4
Carbon Dioxide (%)	4.65
Molecular Wt. (dry)	29.32
Molecular Wt. (wet)	28.51
Velocity (fps)	73.05
Volumetric flow	
DSCFM (F factor)	393,650

**Table 2**  
**Summary of Radionuclides**  
**Fuel Sample**  
**January 25-26, 1990**  
**Kern River Cogeneration Company**  
**Bakersfield, California**

Parameter	Results Pico Curie/liter
Gross Alpha	$0 \pm 3$
Gross Beta	$87 \pm 4$
Gamma Scan:	
<sup>40</sup> K Potassium	<131
<sup>137</sup> Cs Cesium	<8
<sup>226</sup> Ra Radium	<19
<sup>228</sup> Th Thorium	<19
<sup>232</sup> Th Thorium	<40

**Table 3**  
**Summary of Trace Elements Emissions**  
**Unit #2 Stack**  
**January 25-26, 1990**  
**Kern River Cogeneration Company**  
**Bakersfield, California**

Parameter	Run #1		Run #2		Run #3		Average Emission Rate	
	lb/hr	lb/hr	lb/hr	lb/hr	lb/hr	lb/hr	lb/MMBTU	lb/MMBTU
Arsenic ✓	$1.5 \times 10^{-3}$	$4.5 \times 10^{-4}$	$1.6 \times 10^{-3}$	$1.2 \times 10^{-3}$	$1.5 \times 10^{-6}$			
Beryllium ✓	$<4.1 \times 10^{-5}$	$7.8 \times 10^{-4}$	$<5.1 \times 10^{-5}$	$<2.9 \times 10^{-4}$	$<3.7 \times 10^{-7}$			
Cadmium ✓	$<1.6 \times 10^{-3}$	$<2.0 \times 10^{-3}$	$<2.0 \times 10^{-3}$	$<1.9 \times 10^{-3}$	$<2.4 \times 10^{-6}$			
Chromium VI ✓	$3.4 \times 10^{-5}$	$6.7 \times 10^{-5}$	$1.0 \times 10^{-4}$	$6.8 \times 10^{-5}$	$8.6 \times 10^{-8}$			
Chromium (Total) ✓	$3.4 \times 10^{-3}$	$<2.0 \times 10^{-3}$	$2.6 \times 10^{-3}$	$2.7 \times 10^{-3}$	$<3.4 \times 10^{-6}$			
Copper ✓	$5.8 \times 10^{-3}$	$8.5 \times 10^{-3}$	$2.9 \times 10^{-3}$	$5.7 \times 10^{-3}$	$7.3 \times 10^{-6}$			
Mercury ✓	$9.4 \times 10^{-6}$	$2.9 \times 10^{-5}$	$7.7 \times 10^{-6}$	$1.5 \times 10^{-6}$	$2.0 \times 10^{-9}$			
Manganese ✓	$8.2 \times 10^{-2}$	$4.2 \times 10^{-2}$	$5.1 \times 10^{-2}$	$5.8 \times 10^{-2}$	$7.4 \times 10^{-5}$			
Nickel ✓	$1.6 \times 10^{-2}$	$8.2 \times 10^{-1}$	$6.4 \times 10^{-3}$	$2.8 \times 10^{-1}$	$3.5 \times 10^{-4}$			
Lead ✓	$4.0 \times 10^{-3}$	$4.1 \times 10^{-3}$	$2.3 \times 10^{-3}$	$3.5 \times 10^{-3}$	$4.4 \times 10^{-3}$			
Selenium ✓	$<4.1 \times 10^{-5}$	$<5.2 \times 10^{-5}$	$<5.1 \times 10^{-5}$	$<4.8 \times 10^{-4}$	$6.1 \times 10^{-8}$			
Zinc ✓	$7.7 \times 10^{-2}$	$8.8 \times 10^{-1}$	$3.2 \times 10^{-2}$	$3.3 \times 10^{-1}$	$4.2 \times 10^{-4}$			

**Table 4**  
**Summary of Furans and Dioxins Emission**  
**Unit #2 Stack**  
**January 25-26, 1990**  
**Kern River Cogeneration Company**  
**Bakersfield, California**

	Run #1		Run #2		Run #3		Average Emissions Rates	
	ug/ sample	lb/hr	ug/ sample	lb/hr	ug/ sample	lb/hr	lb/hr	lb/MMBTU
<b>Furans</b>								
TCDFs (total)	26	$7.8 \times 10^{-9}$	45	$1.5 \times 10^{-8}$	1600	$5.5 \times 10^{-7}$	$1.9 \times 10^{-7}$	$2.4 \times 10^{-10}$
PeCDFs (total)	19	$5.7 \times 10^{-9}$	120	$4.0 \times 10^{-8}$	2200	$7.6 \times 10^{-7}$	$2.7 \times 10^{-7}$	$3.4 \times 10^{-10}$
HxCDFs (total)	14	$4.2 \times 10^{-9}$	94	$3.2 \times 10^{-8}$	1100	$3.8 \times 10^{-7}$	$1.4 \times 10^{-7}$	$1.8 \times 10^{-10}$
HpCDFs (total)	76	$2.3 \times 10^{-8}$	110	$3.7 \times 10^{-8}$	660	$2.3 \times 10^{-7}$	$1.0 \times 10^{-7}$	$1.2 \times 10^{-10}$
OCDF	<18	$<5.4 \times 10^{-8}$	66	$2.2 \times 10^{-8}$	196	$6.7 \times 10^{-8}$	$3.1 \times 10^{-8}$	$4.0 \times 10^{-11}$
<b>Dioxins</b>								
TCDDs (total)	<15	$<4.5 \times 10^{-9}$	<19	$<6.4 \times 10^{-9}$	160	$5.5 \times 10^{-8}$	$<2.2 \times 10^{-8}$	$2.8 \times 10^{-11}$
PeCDDs (total)	<9.2	$<2.8 \times 10^{-9}$	<14	$<4.7 \times 10^{-9}$	340	$1.2 \times 10^{-7}$	$<4.2 \times 10^{-8}$	$5.4 \times 10^{-11}$
HxCDDs (total)	43	$1.3 \times 10^{-8}$	43	$1.4 \times 10^{-8}$	370	$1.3 \times 10^{-7}$	$5.2 \times 10^{-8}$	$6.6 \times 10^{-11}$
HpCDDs (total)	110	$3.3 \times 10^{-8}$	120	$4.0 \times 10^{-8}$	370	$1.3 \times 10^{-7}$	$6.8 \times 10^{-8}$	$8.6 \times 10^{-11}$
OCDD	<190	$<5.7 \times 10^{-8}$	400	$1.3 \times 10^{-7}$	400	$1.4 \times 10^{-7}$	$1.1 \times 10^{-7}$	$1.4 \times 10^{-10}$



**Table 5**  
**Summary of Polynuclear Aromatic Hydrocarbons (PAH) Emissions**  
**Unit #2 Stack**  
**January 25-26, 1990**  
**Kern River Cogeneration Company**  
**Bakersfield, California**

Furans	Run #1		Run #2		Run #3		Average Emission Rates	
	ug/ sample	lb/hr	ug/ sample	lb/hr	ug/ sample	lb/hr	lb/hr	lb/MMBTU
Napthalene ✓	4.9	1.4 x 10 <sup>-3</sup>	0.5	<1.7 x 10 <sup>-4</sup>	4.6	1.6 x 10 <sup>-3</sup>	1.1 x 10 <sup>-3</sup>	1.3 x 10 <sup>-6</sup>
Acenaphthylene	<0.063	<1.9 x 10 <sup>-5</sup>	<0.046	<1.6 x 10 <sup>-5</sup>	0.37	1.3 x 10 <sup>-4</sup>	<5.5 x 10 <sup>-5</sup>	7.0 x 10 <sup>-8</sup>
Acenaphthene	<0.045	<1.3 x 10 <sup>-5</sup>	<0.35	<1.2 x 10 <sup>-4</sup>	<0.063	<2.0 x 10 <sup>-5</sup>	<5.1 x 10 <sup>-5</sup>	6.5 x 10 <sup>-8</sup>
Fluorene	<0.51	<1.5 x 10 <sup>-4</sup>	<0.37	<1.2 x 10 <sup>-4</sup>	<0.58	<2.0 x 10 <sup>-5</sup>	1.0 x 10 <sup>-4</sup>	1.2 x 10 <sup>-7</sup>
Phenanthrene	2.2	6.6 x 10 <sup>-4</sup>	1.2	<4.1 x 10 <sup>-4</sup>	2.7	9.1 x 10 <sup>-4</sup>	6.6 x 10 <sup>-4</sup>	8.4 x 10 <sup>-7</sup>
Anthracene	<0.17	<5.2 x 10 <sup>-5</sup>	<0.040	<1.3 x 10 <sup>-5</sup>	0.82	2.8 x 10 <sup>-4</sup>	1.2 x 10 <sup>-4</sup>	1.5 x 10 <sup>-7</sup>
Fluoranthene	<0.51	1.5 x 10 <sup>-4</sup>	0.30	1.0 x 10 <sup>-4</sup>	0.44	1.5 x 10 <sup>-4</sup>	1.3 x 10 <sup>-4</sup>	1.7 x 10 <sup>-7</sup>
Benzo (a)anthracene ✓	<0.18	5.5 x 10 <sup>-5</sup>	<0.090	<3.0 x 10 <sup>-5</sup>	<0.015	<5.1 x 10 <sup>-6</sup>	3.0 x 10 <sup>-5</sup>	<3.8 x 10 <sup>-8</sup>
Chrysene	<0.19	5.8 x 10 <sup>-5</sup>	<0.094	<3.2 x 10 <sup>-5</sup>	<0.062	<2.1 x 10 <sup>-5</sup>	3.7 x 10 <sup>-5</sup>	<4.7 x 10 <sup>-8</sup>
Pyrene	0.33	1.0 x 10 <sup>-4</sup>	0.37	1.2 x 10 <sup>-4</sup>	0.63	2.0 x 10 <sup>-4</sup>	1.4 x 10 <sup>-4</sup>	1.8 x 10 <sup>-7</sup>
Benzo (b)fluoranthene ✓	0.71	2.1 x 10 <sup>-4</sup>	0.31	1.0 x 10 <sup>-4</sup>	<0.15	<5.1 x 10 <sup>-5</sup>	1.2 x 10 <sup>-4</sup>	<1.5 x 10 <sup>-7</sup>
Benzo (k)fluoranthene ✓	<0.19	5.8 x 10 <sup>-5</sup>	<0.040	<1.3 x 10 <sup>-5</sup>	<0.14	<4.8 x 10 <sup>-5</sup>	4.0 x 10 <sup>-5</sup>	<5.0 x 10 <sup>-8</sup>
Benzo (a)pyrene ✓	0.55	1.6 x 10 <sup>-4</sup>	0.11	3.7 x 10 <sup>-5</sup>	<0.11	<3.8 x 10 <sup>-5</sup>	7.8 x 10 <sup>-5</sup>	<9.9 x 10 <sup>-8</sup>
Dibenzo (a, h) anthracene ✓	0.045	1.3 x 10 <sup>-5</sup>	<0.015	<5.1 x 10 <sup>-6</sup>	<0.014	<4.8 x 10 <sup>-6</sup>	7.6 x 10 <sup>-6</sup>	<9.7 x 10 <sup>-9</sup>
Benzo (g,h,i) perylene	<0.034	1.1 x 10 <sup>-8</sup>	<0.020	<6.7 x 10 <sup>-6</sup>	<0.0072	<2.5 x 10 <sup>-6</sup>	3.1 x 10 <sup>-6</sup>	<3.9 x 10 <sup>-9</sup>
Indeno (1,2,3-c,d) pyrene	<0.043	1.3 x 10 <sup>-8</sup>	<0.025	8.5 x 10 <sup>-6</sup>	<0.0056	<2.0 x 10 <sup>-6</sup>	3.5 x 10 <sup>-6</sup>	<4.5 x 10 <sup>-9</sup>

**Table 6**  
**Summary of Arsenic, Hydrogen Chloride and Formaldehyde Emissions**  
**Unit #2 Stack**  
**January 25-26, 1990**  
**Kern River Cogeneration Company**  
**Bakersfield, California**

Parameter	Run #1 lb/hr	Run #2 lb/hr	Run #3 lb/hr	Average Emission Rates	
				lb/hr	lb/MMBTU
Arsenic	$4.5 \times 10^{-4}$	$2.3 \times 10^{-4}$	$8.4 \times 10^{-5}$	$2.5 \times 10^{-4}$	$3.2 \times 10^{-7}$
Hydrogen Chloride	$5.0 \times 10^{-1}$	$4.2 \times 10^{-1}$	$4.7 \times 10^{-1}$	$4.6 \times 10^{-1}$	$5.9 \times 10^{-4}$
Formaldehyde	$5.7 \times 10^{-2}$	$6.4 \times 10^{-2}$	$4.7 \times 10^{-2}$	$5.6 \times 10^{-2}$	$7.1 \times 10^{-5}$

Table 7

Summary of Benzene, and Selected Volatile Emissions

Unit #2 Stack Outlet

January 25-26, 1990

Kern River Cogeneration Company

Bakersfield, California

Parameter	Run #1	Run #2	Run #3	Average Emissions Rate	
	ppm	ppm	ppm	lb/hr	lb/MMBTU
✓ Benzene	<0.11	<0.11	<0.11	<0.53	<6.8 x 10 <sup>-4</sup>
✓ Acrolein	<0.11	<0.11	<0.11	<0.38	<4.8 x 10 <sup>-4</sup>
✓ 1-3 Butadiene	<0.11	<0.11	<0.11	<0.37	<4.7 x 10 <sup>-4</sup>
✓ Propylene	<0.10	<0.10	<0.10	<0.27	<3.3 x 10 <sup>-4</sup>
Toluene	<0.066	<0.066	<0.066	<0.37	<4.7 x 10 <sup>-4</sup>
Xylene	<0.056	<0.056	<0.056	<0.37	<4.7 x 10 <sup>-4</sup>

**Table 8**  
**Summary of Trace Elements**  
**Fuel Sample**  
**January 25-26, 1990**  
**Kern River Cogeneration Company**  
**Bakersfield, California**

Parameter	Results mg/l
Arsenic	<0.001
Beryllium	<0.010
Cadmium	0.110
Chloride	0.500
Chromium	0.290
Copper	0.540
Mercury	0.050
Manganese	0.050
Nickel	1.20
Lead	<1.0
Selenium	<0.002
Zinc	4.8

**Appendix A**  
**Field Data Sheets**

Plant KRECC  
 Date 1-26-90  
 Test Site KRECC  
 Run Number TRACE ELEMENTS  
 Operator TR

Ambient Temp 60  
 Barometer 30.44  
 Stack Pressure -.101  
 Stack H<sub>2</sub>O +.03  
 Stack Dia 10.75

Meter # 98 1.749  
 Meter Gamma 1.030  
 Meter Box # 30  
 Nozzle Diameter 1.5  
 Probe Length 1.5

Probe Mat'l Teflon  
 Filter Number 202  
 Pump Box # 1  
 PPS LEAK 0.01 @ 5" HG  
 POST LEAK 1.2 @ 5" HG

#1

FIELD DATA

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (Vh)	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H; "H <sub>2</sub> O)		TEMPERATURES						PUMP VAC. "Hg
					Desired	Actual	STACK (T/s)	METER INLET	METER OUT	IMPINGER	FILTER		
1	0	0914	348.035	.65	1.58	1.0	304	54	44				3
2	10	0924	356.9	.64	1.56	1.0	308	51	44				3
3	20	0934	304.9	.65	1.58	1.0	308	53	46				3
4	30	0944	371.3	.74	1.81	1.8	305	57	46				3
5	40	0954	378.6	.65	1.58	1.0	308	60	50				3
6	50	1004	385.8	.59	1.44	1.44	314	52	47				3
	60	1014	394.256				PORT CHANGE						
7	0	1017	394.256	.59	1.44	1.44	314	54	49				3
8	10	1027	402.5	.59	1.44	1.44	312	55	50				3
9	20	1037	406.8	.55	1.34	1.34	312	57	51				3
10	30	1047	410.1	.59	1.44	1.44	313	48	49				3
11	40	1057	415.5	.59	1.44	1.44	308	47	46				3
12	50	1107	420.8	.59	1.44	1.44	311	45	45				3
	60	1117	426.383				PORT CHANGE						
AVERAGE / SUM	2h0		100.98	7830		1.48	295	56					

PORT A  
 PORT B  
 PORT C

1h0: 101

TRUCK RECORDS #1

Page 2 of 2  
Run Number 1 TRACE 0271  
Operator JZ

Plant KRCC  
Date 7-26-90  
POST LEAK RATE, ASES @ 5" Hg

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V <sub>m</sub> )	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H, "H <sub>2</sub> O)		TEMPERATURES					PUMP VAC. "Hg	
					Desired	Actual	STACK (T <sub>s</sub> )	METER INLET	METER OUT	IMPINGER	FILTER		
13	0	1144	426.383	.54	1.72	1.3	297	47	47				2.5
14	10	1151	432.7	.63	1.54	1.5	297	48	45				3
15	20	1201	439.1	.81	1.98	2.0	297	57	49				3
16	30	1211	446.7	.64	1.56	1.6	299	56	50				3
17	40	1221	454.1	.65	1.59	1.6	300	56	51				3
18	50	1231	461.9	.54	1.32	1.3	314	59	53				3
	60	1241	468.825				CHANGE	CHANGE	56				
19	0	1245	468.825	.53	1.29	1.3	312	58	56				3
20	10	1255	476.3	.57	1.39	1.3	308	64	57				3
21	20	1305	482.9	.63	1.54	1.5	309	63	58				3
22	30	1315	489.5	.59	1.44	1.4	307	56	55				3
23	40	1325	495.8	.59	1.44	1.4	307	56	55				3
24	50	1335	502.8	.61	1.45	1.5	317	60	57				3
	60	1345	509.615			END	RUN	#1					
AVERAGE /SUM	040		100.980	.780		1.48	295						

Point 1

TRACE ELEMENTS #2

$K = 2.27$

Plant KRCC  
 Date 2-5-90  
 Test Site KRCC GOSWAMI #2  
 Run Number 2 TRACE ELEMENTS  
 Operator IK

Ambient Temp 75  
 Barometer 29.44  
 Stack Pressure .67  
 Stack H<sub>2</sub>O & O<sub>2</sub>  
 Stack Dia 16.75

Meter #88 1.629  
 Meter Gamma 0.994  
 Meter Box #2A42  
 Nozzle Diameter  
 Probe Length

Probe Mat'l  
 Filter Number  
 Samp Box #  
 FIB LEAK 0.00035 MG  
 POST LEAK

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (Vol)	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H; "H <sub>2</sub> O)		TEMPERATURES				PUMP VAC. "Hg	
					Desired	Actual	STACK (Tb)	METER INLET	METER OUT	IMPINGER		FILTER
1	0	1455	416.790	.67	1.52	1.5	298	75				1
2	10	1505	424.1	.71	1.61	1.6	292	81				1
3	20	1515	431.1	.74	1.68	1.7	292	82				1
4	30	1525	438.7	.67	1.52	1.5	290	84				1
5	40	1535	445.9	.66	1.50	1.5	290	83				1
6	50	1545	453.3	.69	1.57	1.6	294	87				1
	60	1555				PORT CHANGE						
7	0	1600	460.956	.61	1.38	1.4	291	86				1
8	10	1610	467.5	.61	1.38	1.4	291	90				1
9	20	1620	474.6	.59	1.34	1.3	293	92				1
10	30	1630	482.4	.59	1.34	1.3	293	92				1
11	40	1640	488.0	.68	1.54	1.5	291	92				1
12	50	1650	495.3	.63	1.43	1.4	292	90				1
	60	1700	501.592			PORT CHANGE						
AVERAGE / SUM	240		170.029	828		1.5	295	83				

PHW = 279.7



TRACE elem. #2

Page 2 of 2  
Run Number 2 TRACE ELEM.  
Operator TR

Plant KRCC  
Date 1-25-90  
POST LEAK RATE 0.002

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (Vm)	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H, "H2O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (Tps)	MEISER INLET	MEISER OUT	IMPINGER	FILTER	
13	0	1706	501.572	.74	1.68	1.7	290	80				/
14	10	1716	608.3	.65	1.48	1.5	291	78				/
15	20	1726	514.7	.65	1.48	1.5	290	77				/
16	30	1736	521.0	.72	1.63	1.6	290	77				/
17	40	1746	528.7	.63	1.43	1.4	287	76				/
18	50	1756	525.6	.68	1.54	1.5	293	86				/
	60	1806	543.002			POET	CHANGE					
19	0	1811	543.002	0.10	1.71	1.71	297	86				/
20	10	1821	550.1	0.18	1.77	1.77	299	86				/
21	20	1831	557.3	0.75	1.70	1.70	299	87				
22	30	1841	542.8	0.72	1.63	1.63	300	86				
23	40	1851	573.1	0.74	1.67	1.7	300	86				
24	50	1861	579.8	0.75	1.70	1.70	255	86				
	60	1911	586.813			END	Run #2					
AVERAGE /SUM	240		170.02	0.528		1.6	292	83				

TRACE ELEMENTS #3

FIELD DATA

PAGE 1 OF 2

ES ENGINEERING & SCIENCE COMPANIES

Meter #10 1.629  
 Meter Gamma 0.994  
 Meter Box #1 (1) #2  
 Nozzle Diameter 2  
 Probe Length

Probe Mat'l  
 Filter Number  
 Sump Box #  
 PRE LEAK GOOD @ 5 MG  
 POST LEAK

Ambient Temp 71.0  
 Barometer 29.94  
 Stack Pressure .107  
 Stack H2O % .06  
 Stack Dia 1.075

Plant KCC  
 Date 1-25-90  
 Test Site COAL #2  
 Run Number TRACE ELEM. #3  
 Operator TR

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V/m)	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H; "H2O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (Tb)	METER INLET	METER OUT	DIP THERM	FILTER	
1	0	2000	587.628	.68	1.54	1.5	292	82				1
2	10	2010	594.6	.73	1.66	1.7	293	82				1
3	20	2020	602.1	.79	1.79	1.8	290	82				1
4	30	2030	609.0	.72	1.63	1.6	293	82				1
5	40	2040	617.0	.71	1.61	1.6	293	82				1
6	50	2050	625.1	.81	1.83	1.8	294	82				1
	60	2100	631.665			Filter	CHANGE					
7	0	2106	631.665	.71	1.61	1.6	295	78				.5
8	10	2116	638.4	.68	1.54	1.5	298	80				.5
9	20	2126	645.3	.72	1.63	1.6	297	82				.5
10	30	2136	651.9	.71	1.61	1.6	295	78				1
11	40	2146	658.9	.74	1.68	1.7	294	76				1
12	50	2156	666.5	.71	1.61	1.6	297	75				1
	60	2206	673.549			Filter	CHANGE					
AVERAGE / SUM	240		172.284	.858		1.6	295	80				

MW = 281.5

$K = 2.27$

TRACE ELEMENTS #3

Plant KRCC  
 Date 1-25-90  
 POST LEAK RATE 0.005025" Hg  
 Page 2 of 2  
 Run Number 3 TRACE ELEM.  
 Operator TR

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (Vn)	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H, "H2O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (Tn)	METER INLET	METER OUT	IMPINGER	FILTER	
13	0	2213	673.549	.75	1.70	1.7	298	72				/
14	10	2223	686.3	.73	1.66	1.7	296	76				/
15	20	2233	687.1	.71	1.61	1.6	297	81				/
16	30	2243	694.4	.78	1.77	1.8	296	81				/
17	40	2253	701.8	.78	1.77	1.8	296	81				/
18	50	2303	709.3	.59	1.34	1.3	297	78				/
	60	2313	715.861		POCT CHANGE							
19	0	2318	715.861	.71	1.61	1.6	297	78				/
20	10	2328	722.2	.65	1.48	1.5	295	78				/
21	20	2338	730.1	.65	1.48	1.5	296	82				/
22	30	2348	737.6	.69	1.57	1.6	293	85				/
23	40	2358	745.4	.73	1.66	1.7	295	86				/
24	50	2408	753.5	.71	1.61	1.6	294	84				/
	60	2418	759.912			END	RUN #5					
AVERAGE / SUM	avg		692.1	0.74		1.6	295	80				

ENGINEERING-SCIENCE, INC.

TRAIN RECOVERY SHEET

DATE 1-25-90

TRACE # 1  
 RUN# \_\_\_\_\_ METHOD \_\_\_\_\_

FACILITY Kree T#2

TYPE \_\_\_\_\_

TECHNICIAN RR

IMP. SOLUTION HNO<sub>3</sub> KMnO<sub>4</sub>

SOLUTION	VOL. (ml)	DESCRIPTION
NOZZLE-PROBE RINSE		✓
UMBILICAL RINSE		✓

NOZZLE-PROBE RINSE

UMBILICAL RINSE

	FINAL (g)	INITIAL (g)	NET (g)
IMPINGER # <u>1</u> HNO <sub>3</sub> /H <sub>2</sub> O ✓	<u>265</u>	<u>100</u>	<u>165</u>
IMPINGER # <u>2</u> HNO <sub>3</sub> /H <sub>2</sub> O ✓	<u>150</u>	<u>100</u>	<u>50</u>
IMPINGER # <u>3</u> MT			
IMPINGER # <u>4</u> KMnO <sub>4</sub> /H <sub>2</sub> SO <sub>4</sub>	<u>105</u>	<u>100</u>	<u>5</u>
DESCRIPTION			
IMPINGER RINSE			

IMPINGER # 1

IMPINGER # 2

IMPINGER # 3

IMPINGER # 4

DESCRIPTION

IMPINGER RINSE

SILICA GEL  
(DESCRIPTION)

SILICA GEL (DESCRIPTION)	FINAL (g)	INITIAL (g)	NET (g)
<u>1/8 away</u> ↳	<u>849.3</u>	<u>814.7</u>	<u>34.6</u>
TOTAL MOISTURE			

FILTER#  
(DESCRIPTION)

FIELD BLANKS

252.6  
(g)

DISPOSITION/COMMENTS

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ENGINEERING-SCIENCE, INC.

TRAIN RECOVERY SHEET

DATE 1-15-90

FACILITY RACE TR V

TECHNICIAN RR

RUN# TRACE # 2 METHOD ✓

TYPE \_\_\_\_\_

IMP. SOLUTION HNO<sub>3</sub> KNO<sub>3</sub>

NOZZLE-PROBE RINSE

UMBILICAL RINSE

SOLUTION	VOL. (ml)	DESCRIPTION
		/
		/

IMPINGER # 1

IMPINGER # 2

IMPINGER # 3

IMPINGER # 4

	FINAL (g)	INITIAL(g)	NET(g)
HNO <sub>3</sub> /HNO <sub>3</sub>	76.7	100	15.7
HNO <sub>3</sub> /HNO <sub>3</sub>	170	100	70
MT	10	0	10
KMnO <sub>4</sub> /HNO <sub>3</sub>	105	100	5

DESCRIPTION

IMPINGER RINSE

SILICA GEL  
(DESCRIPTION)

	FINAL (g)	INITIAL(g)	
2/3 used	824.0	791.9	32.7

FILTER#  
(DESCRIPTION)

	<b>TOTAL MOISTURE</b>	
--	-----------------------	--

FIELD BLANKS

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

2.79.7  
(g)

DISPOSITION/COMMENTS

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

ENGINEERING-SCIENCE, INC.

TRAIN RECOVERY SHEET

DATE 1-26-90

FACILITY KELL

TECHNICIAN RO/RD

RUN# 3 METHOD \_\_\_\_\_

TYPE TRACE ELEMENTS

IMP. SOLUTION H<sub>2</sub>O/HNO<sub>3</sub>

NOZZLE-PROBE RINSE

UMBILICAL RINSE

SOLUTION	VOL. (ml)	DESCRIPTION

IMPINGER # 1

IMPINGER # 2

IMPINGER # 3

IMPINGER # 4

DESCRIPTION

IMPINGER RINSE

	FINAL (g)	INITIAL (g)	NET (g)
HNO <sub>3</sub> /H <sub>2</sub> O	<u>205</u>	<u>100</u>	<u>105</u>
HNO <sub>3</sub> /H <sub>2</sub> O	<u>130</u>	<u>100</u>	<u>30</u>
MT	<u>10</u>	<u>0</u>	<u>10</u>
KMnO <sub>4</sub>	<u>100</u>	<u>100</u>	

SILICA GEL (DESCRIPTION)

FILTER# (DESCRIPTION)

FIELD BLANKS

DISPOSITION/COMMENTS

	FINAL (g)	INITIAL (g)	
	<u>858.3</u>	<u>821.7</u>	<u>36.6</u>
TOTAL MOISTURE			

~~181.6~~ (g)

281.6

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_



Box B  $k = 2.43$

DIXON #1

Plant KACC

Date 11/26/90

POST LEAK RATE 0.005 @ 20" Hg

Page 2 of 2  
 Run Number 1  
 Operator W. J. J. / S. K.

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (Vn)	VELOCITY HEAD (delta P)	ORIFICE PRESSURE (delta H, "H2O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (Tn)	MEISER INLET	MEISER OUT	IMPINGER	FILTER	
13	120	1142	484.778	1.8	4.37	2.0	300	63	59	50	230	19
14	130	1152	492.0	1.7	4.13	2.0	300	58	55		250	19
15	140	1202	499.5	1.6	3.89	2.0	299	60	55		248	19
16	150	1212	507.1	1.7	4.13	2.0	305	63	56		252	19
17	160	1222	514.8	1.7	4.13	2.0	312	63	57		249	19
18	170	1232	522.4	1.7	4.13	2.0	312	65	58		242	19
19	180	1242	530.163				<i>part</i>					
20	190	1249	530.163	1.8	4.37	1.9	311	63	59		252	19
21	200	1259	537.6	1.8	4.37	1.9	310	67	60		240	19
22	210	1309	545.2	1.8	4.37	1.9	310	69	62		240	19
23	220	1319	552.9	1.7	4.13	1.9	311	69	63		252	19
24	230	1329	560.6	1.7	4.13	1.9	308	69	64		252	19
24	230	1339	568.5	1.1	2.67	1.9	315	76	69		230	19
240	240	1349	575.941									
AVERAGE /SUM	240		173.407	1.05		1.75	303	61				

HW = 29.0



Plant KACC  
 Date 11/26/80  
 Test Site Stack #2  
 Run Number 2  
 Operator DM/SLK

Ambient Temp 70  
 Barometer  
 Stack Pressure  
 Stack H<sub>2</sub>O % 8  
 Stack Dia 167.5"

Meter #10 1.74  
 Meter Gamma 1.01  
 Meter Box # 24 #3  
 Nozzle Diameter 1.59  
 Probe Length

Probe Mat'l  
 Filter Number  
 Samp Box #  
 FRS LEAK  (N)  
 POST LEAK

Box B  
 $k = 2.43 (.189)^4$   
 $k = 0.79$

FIELD DATA

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V/m)	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H; WED)		TEMPERATURES				FUMP VAC. "Hg	
					Desired	Actual	STACK (T/s)	METER INLET	METER OUT	INDINGER		FILTER
1	0	1502	576.425	1.7	1.34	1.3	305	76	69	49	250	9
2	10	1512	582.4	1.7	1.34	1.3	303	76	69	49	250	9
3	20	1522	588.4	1.7	1.34	1.3	307	76	68	49	250	9
4	30	1532	595.0	1.7	1.34	1.3	308	80	72	49	249	10
5	40	1542	600.9	1.7	1.34	1.3	309	81	73	50	247	9
6	50	1552	608.1	1.7	1.34	1.3	309	83	75	50	250	10
	60	1602	614.515	1.7	1.34	1.3	309	79	76	50		9
7	60	1609	614.515	1.7	1.34	1.3	309	79	76	50	241	9
8	70	1619	621.3	1.7	1.34	1.3	304	83	77	50	238	10
9	80	1629	627.9	1.7	1.34	1.3	302	84	77	50	240	11
10	90	1639	634.5	1.7	1.34	1.3	301	83	78	50	234	11
11	100	1649	641.8	1.7	1.34	1.3	301	82	77	50	264	11
12	110	1659	647.8	1.7	1.34	1.3	300	81	77	50	238	11
	120	1709	654.172									
AVERAGE /SUM	240		158.887	1.3038		1.3	301					

(N) = 205.4

Box B

DIXON # 2

K 0:79

ES ENGINEERING-SCIENCE COMPANIES

KARCE

Page 2 of 2  
Run Number 2  
Operator [Signature]

Plant  
Date 11/20/89  
POST LEAK RATE 0.007

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS MEIER READING (V <sub>m</sub> )	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H, "H <sub>2</sub> O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (T <sub>m</sub> )	MEIER INLET	MEIER OUT	IMPINGER	FILTER	
13	120	1715	654.172	1.7	1.34	1.3	300	77	75	49	266	11
14	130	1725	660.7	1.7	1.34	1.3	300	79	75	49	249	11
15	140	1735	667.0	1.7	1.34	1.3	299	79	75	49	243	11
16	150	1745	673.4	1.7	1.34	1.3	300	79	75	50	255	11
17	160	1755	679.0	1.7	1.34	1.3	300	79	74	50	254	11
18	170	1805	686.5	1.7	1.34	1.3	299	79	74	48	236	11
	180	1815	693.068		post change							
1	180	1824	693.068	1.7	1.34	1.3	301	76	72	48	252	11
2	190	1834	699.9	1.7	1.34	1.3	300	75	70	47	233	11
3	200	1844	705.1	1.7	1.34	1.3	301	74	70	47	222	11
4	210	1854	712.6	1.7	1.34	1.3	301	70	69	47	232	11
5	220	1904	719.3	1.7	1.34	1.3	300	73	70	47	237	11
6	230	1914	726.9	1.7	1.34	1.3	300	73	70	46	224	11
	240	1924	735.911		END TEST							
AVERAGE /SUM	240		158.867	1.3038		1.3	301					
								72				

Box B  
 Dioxin #3

Plant KACC  
 Date 1/26/90  
 Test Site Stack #2  
 Run Number 3  
 Operator ASD

Ambient Temp 65  
 Barometer  
 Stack Pressure  
 Stack H2O & S  
 Stack Dia 167.5"

Meter #19  
 Meter Gamma 1.01  
 Meter Box # 2-1-#3  
 Nozzle Diameter 0.189  
 Probe Length

$K = 0.79$

Probe Mat'l  
 Filter Number  
 Samp Box #  
 PPS LEAK 0.002  
 POST LEAK 15

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (Vn)	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H; "H2O)		TEMPERATURES						PUMP VAC. "Hg
					Desired	Actual	STACK (Tn)	METER INLET	METER OUT	DIPPER	FILTER		
1	0	2002	735.472	1.6	1.26	1.3	300	77	75	49	240	13	
2	10	2012	743.2	1.6	1.26	1.3	297	77	75	49	243	12	
3	20	2022	750.2	1.6	1.26	1.3	295	77	75	49	250	9	
4	30	2032	756.2	1.8	1.42	1.4	295	77	75	49	250	10	
5	40	2042	762.7	1.8	1.42	1.4	295	77	75	49	250	10	
6	50	2052	769.3	1.8	1.42	1.4	295	77	75	49	250	10	
	60	2102	775.984			part	change						
7	60	2110	775.984	1.8	1.42	1.4	295	78	76	50	250	11	
8	70	2120	782.6	1.8	1.42	1.4	295	78	76	50	250	11	
9	80	2130	789.7	1.7	1.34	1.3	297	78	76	50	250	11	
10	90	2140	796.5	1.7	1.34	1.3	297	78	76	50	250	11	
11	100	2150	803.5	1.7	1.34	1.3	295	78	76	50	249	11	
12	110	2200	810.8	1.7	1.34	1.3	296	78	76	50	250	11	
	120	2210	816.780										
AVERAGE / SUM	240		154.17	1.302		1.3	296		76				

MAN = 166.1

Box Dixon #3

K = 0.79



Plant KREC  
 Date 1-26-90  
 POST LEAK RATE 0.0042 12 "Hg  
 Page 2 of 2  
 Run Number 3  
 Operator SK

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V <sub>m</sub> )	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H, "H <sub>2</sub> O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (T <sub>s</sub> )	METER INLET	METER OUT	IMPINGER	FILTER	
13	170	2215	816.780	1.7	1.34	1.3	296	78	76	50	250	11
14	130	2225	823.9	1.6	1.34	1.3	295	78	76	50	249	11
15	140	2235	829.8	1.7	1.34	1.3	296	78	76	50	249	10
16	150	2245	836.8	1.7	1.34	1.3	296	78	76	50	249	10
17	160	2255	843.0	1.7	1.34	1.3	295	78	76	50	250	10
18	170	2305	849.5	1.7	1.34	1.3	295	78	76	50	250	10
	180	2310	853.744									
19	180	2318	853.744	1.7	1.34	1.3	295	78	76	50	250	10
20	190	2328	856.9	1.7	1.34	1.3	296	78	76	50	250	10
21	200	2338	861.9	1.7	1.34	1.3	296	78	76	50	250	10
22	210	2348	872.5	1.7	1.34	1.3	296	78	77	50	251	10
23	220	2358	878.9	1.7	1.34	1.3	296	78	76	50	250	10
24	230	2408	885.2	1.7	1.34	1.3	296	78	76	50	250	10
	240	2418	891.639									
AVERAGE /SUM			156.17	1.3052		1.3	296					

20  
 156.17  
 1.3052

ENGINEERING-SCIENCE, INC.

TRAIN RECOVERY SHEET

DIOXIN-1

DATE 1-25-90

RUN# \_\_\_\_\_ METHOD \_\_\_\_\_

FACILITY KRCC T#V

TYPE \_\_\_\_\_

TECHNICIAN RP

IMP. SOLUTION \_\_\_\_\_

SOLUTION	VOL. (ml)	DESCRIPTION
NOZZLE-PROBE RINSE		/
UMBILICAL RINSE		/

NOZZLE-PROBE RINSE

UMBILICAL RINSE

	FINAL (g)	INITIAL (g)	NET (g)
IMPINGER # <u>1</u>	HW 310	100	210
IMPINGER # <u>2</u>	HW 120	100	20
IMPINGER # <u>3</u>	MT 0	0	0
IMPINGER # _____			
DESCRIPTION			
IMPINGER RINSE			

IMPINGER # 1

IMPINGER # 2

IMPINGER # 3

IMPINGER # \_\_\_\_\_

DESCRIPTION

IMPINGER RINSE

SILICA GEL (DESCRIPTION)	FINAL (g)	INITIAL (g)	NET (g)
<u>1/3 silica</u>	835.4	786.4	49.0

SILICA GEL (DESCRIPTION)

FILTER# (DESCRIPTION)

TOTAL MOISTURE

FIELD BLANKS

289.0 (g)

DISPOSITION/COMMENTS

\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

ENGINEERING-SCIENCE, INC.

TRAIN RECOVERY SHEET

DATE 1-26-90

RUN# 2 METHOD \_\_\_\_\_

FACILITY KRCL TAV

TYPE DIOXIN

TECHNICIAN RS/RR

IMP. SOLUTION \_\_\_\_\_

NOZZLE-PROBE RINSE

UMBILICAL RINSE

SOLUTION	VOL. (ml)	DESCRIPTION

IMPINGER # 1

IMPINGER # 2

IMPINGER # 3

IMPINGER # \_\_\_\_\_

DESCRIPTION

IMPINGER RINSE

	FINAL (g)	INITIAL (g)	NET (g)
HW	390	100	290
HW	40	100	-60
MT	20	0	20

SILICA GEL  
(DESCRIPTION)

FILTER#  
(DESCRIPTION)

FIELD BLANKS

DISPOSITION/COMMENTS

	FINAL (g)	INITIAL (g)	
1/3 used	837.6	792.2	45.4
TOTAL MOISTURE			

295.4 (g)

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

ENGINEERING-SCIENCE, INC.

TRAIN RECOVERY SHEET

DATE 1-26-90

RUN# 3 METHOD \_\_\_\_\_

FACILITY KRL TAV

TYPE Dioxin

TECHNICIAN RO/RD

IMP. SOLUTION \_\_\_\_\_

NOZZLE-PROBE RINSE

UMBILICAL RINSE

SOLUTION	VOL. (ml)	DESCRIPTION

IMPINGER # 1

IMPINGER # 2

IMPINGER # 3

IMPINGER # \_\_\_\_\_

DESCRIPTION

IMPINGER RINSE

	FINAL (g)	INITIAL (g)	NET (g)
H <sub>2</sub> O	315	100	215
H <sub>2</sub> O	5	100	-95
MT	0	0	0

SILICA GEL  
(DESCRIPTION)

FILTER#  
(DESCRIPTION)

	FINAL (g)	INITIAL (g)	
1/3 used	868.8	821.9	46.9
	TOTAL MOISTURE		

FIELD BLANKS

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

166.9 (g)

DISPOSITION/COMMENTS

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

$K=2.29$   
 ACC #1  
 UVA

Plant KRECC  
 Date 2-26-89  
 Test Site KRECC COGSL #2  
 Run Number 1 ACC  
 Operator JL

Ambient Temp 60  
 Barometer 29.94  
 Stack Pressure .01  
 Stack H<sub>2</sub>O .03  
 Stack Dia 167.5

Meter # 1629  
 Meter Gains 0.994  
 Meter Box # KRECC #2  
 Nominal Diameter 2  
 Probe Length

Probe Mat'l TKUN  
 Filter Number  
 Sump Box # 0.002  
 PPG LEAK  
 POST LEAK

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V <sub>m</sub> )	VELOCITY HEAD (delta P)	ORIFICE PRESSURE (delta H; H <sub>2</sub> O)		TEMPERATURES						PUMP VAC. "Hg
					Desired	Actual	STACK (T <sub>st</sub> )	METER INLET	METER OUT	INLET	FILTER		
1	0	0920	231.482	1.7	3.86	3.9	268	50					1
2	10	0930	238.8	.71	1.61	1.6	283	50					5
3	20	0940	244.7	1.7	3.86	3.9	283	50					6
4	30	0950	253.2	1.7	3.86	3.9	281	50					6
5	40	1000	263.5	1.7	3.86	3.9	314	50					6
6	50	1010	273.9	1.7	3.86	3.9	312	50					6
	60	1020	287.340				PORT	CHANGE					6
7	0	1024	282.340	2.0	4.54	4.5	312	50					6
8	10	1037	291.5	2.0	4.54	4.5	312	50					6
9	20	1047	300.2	2.0	4.54	4.5	313	50					6
10	30	1057	308.7	2.0	4.54	4.5	308	50					6
11	40	1107	317.5	2.0	4.54	4.5	311	50					6
12	50	1117	328.7	2.0	4.54	4.5	312	50					6
	60	1127	334.98				PORT	CHANGE					
AVERAGE / SUM	240		104.6	1.800		2.9	290						60

PORT A

PORT B

104.674 1.8



HCC #1  
CUBI

Plant KCC  
Date 7-28-96  
POST LEAK RATE 0.0002 2 Hg

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V <sub>m</sub> )	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H, "H <sub>2</sub> O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (T <sub>s</sub> )	METER INLET	METER OUT	IMPINGER	FILTER	
13	0	1144	334.786	.71	1.61	1.6	295	60				2
14	10	1154	342.5	.71	1.61	1.6	294	62				2
15	20	1204	349.1	.75	1.70	1.7	294	70				2
16	30	1214	356.6	.75	1.70	1.7	298	71				2
17	40	1234	362.4	.65	1.48	1.5	300	73				2
18	50	1234	369.6	.72	1.63	1.6	288	70				2
	60	1244	375.869				PORT CHANGE					
19	6	1248	375.869	.73	1.60	1.7	285	75				2
20	10	1258	382.2	.74	1.68	1.7	287	79				2
21	20	1308	389.3	.78	1.77	1.8	288	80				2
22	30	1318	396.5	.72	1.63	1.6	287	79				2
23	40	1328	403.2	.70	1.59	1.6	287	76				2
24	50	1338	410.2	.52	1.18	1.2	294	77				2
	60	1348	416.156				END RUN #1					
AVERAGE	240		1844.6	1.0901		2.9	2900	60				

PORT C  
PORT D  
PORT E

Plant KRCC  
 Date 1-25-90  
 Test Site CA-701 P2  
 Run Number 2 HQ  
 Operator \_\_\_\_\_

Ambient Temp 75  
 Barometer 29.44  
 Stack Pressure 1.17  
 Stack H2O & O2 \_\_\_\_\_  
 Stack Dia. 16.75

Meter # 1010  
 Meter Gamma 1-0-30  
 Meter Box # BL000000  
 Nozzle Diameter \_\_\_\_\_  
 Probe Length \_\_\_\_\_

Probe Mat # 1  
 Filter Number \_\_\_\_\_  
 Sump Box # \_\_\_\_\_  
 FPM LEAK 00010251H  
 POST LEAK \_\_\_\_\_

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V <sub>m</sub> )	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H; W2O)		STACK (70)	TEMPERATURE				PUMP VAC. "Hg
					Desired	Actual		METER INLET	METER OUT	DEFINER	FILTER	
1	0	1500	511.127	.78	1.90	1.9	306	64	65			5
2	10	1510	517.7	.71	1.73	1.7	302	65	63			4.5
3	20	1520	525.2	.68	1.54	1.6	304	70	66			4.5
4	30	1530	532.2	.68	1.66	1.7	308	72	68			5
5	40	1540	539.3	.72	1.76	1.8	309	75	71			5
6	50	1550	546.2	.73	1.78	1.8	309	79	72			6
7	60	1600	553.320	.78	1.90	1.9	306	77	73			6
8	0	1605	553.300	.72	1.76	1.8	302	82	76			7
9	10	1615	562.3	.77	1.88	1.9	300	83	78			4.5
10	20	1625	570.4	.71	1.73	1.7	300	83	79			5
11	30	1635	579.5	.76	1.85	1.9	301	74	73			3.5
12	40	1645	587.1	.76	1.85	1.9	302	73	72			
	50	1655	593.1	.75	1.86	1.9						
	60	1705	599.149									
AVERAGE /SUM	240		716.57	.8643		1.8	300					

HCC #2  
 GWN

K=2.44

CHANG

P

Plant KCC  
 Date 1-25-90  
 POST LEAK RATE 0.600

Page 2 of 2  
 Run Number 2 KCC  
 Operator TK

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V <sub>m</sub> )	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H, "H <sub>2</sub> O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (Tb)	MEIER INLET	MEIER OUT	IMPINGER	FILTER	
13	0	1709	599.149	.78	1.90	1.9	299	68	68			5
14	10	1719	606.4	.74	1.81	1.8	299	69	66			5
15	20	1729	613.9	.78	1.90	1.9	300	69	65			5
16	30	1739	621.1	.78	1.90	1.9	300	69	65			5
17	40	1749	629.8	.74	1.81	1.8	296	71	65			6
18	50	1759	637.2	.69	1.68	1.7	295	72	65			4.5
	60	1809	644.461				CHANGE					
19	0	1811	644.461	0.80	1.81	1.81	297	72	65			4.5
20	10	1821	652.1	0.77	1.81	1.81	297	70	64			5
21	20	1831	659.0	0.78	1.90	1.90	297	70	64			5
22	30	1841	665.5	0.78	1.90	1.90	299	70	64			5
23	40	1851	672.2	0.77	1.81	1.81	253	70	64			5
24	50	1901	680.6	0.74	1.81	1.81	255	70	64			5
	60	1911	687.701				END RUN #2					
AVERAGE / SUM	240		176.571	0.768	1.81	1.81	300					10

HCC #2  
 CWV

Plant KRCC

Date 1-25-50

Test Site OLAN #2

Run Number 111 #3

Operator IT

Ambient Temp 70

Barometer 29.44

Stack Pressure .07

Stack H<sub>2</sub>O 0.00

Stack Dia 16.75

Meter # 1.749

Meter Gamma 1.030

Meter Box # 302 #3

Nozzle Diameter .25

Probe Length

Probe Mat'l

Filter Number

Sump Box #

Probe Leak 001025 #6

POST LEAK

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V <sub>m</sub> )	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H; H <sub>2</sub> O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (T <sub>g</sub> )	METER INLET	METER OUT	IMPINGER	FILTER	
1	0	2002	689.512	.75	1.83	1.8	294	62	61			5
2	10	2012	696.6	.85	2.07	2.1	291	65	63			5
3	20	2022	704.1	.71	1.73	1.7	292	66	61			5
4	30	2032	711.7	.71	1.73	1.7	293	66	61			5
5	40	2042	719.2	.80	1.95	2.0	294	66	61			5
6	50	2052	727.5	.75	1.83	1.8	294	66	60			5
	60	2102	735.321				MARKS					
7	0	2107	735.321	.75	1.83	1.8	295	62	60			4.5
8	10	2117	742.0	.71	1.73	1.7	298	64	59			5
9	20	2127	749.6	.81	1.98	2.0	297	65	59			5
10	30	2137	756.4	.74	1.81	1.8	277	65	59			5
11	40	2147	763.6	.78	1.90	1.9	294	64	59			5
12	50	2157	771.2	.75	1.83	1.8	297	66	59			5
	60	2207	779.358				MARKS					
							MARKS					
AVERAGE /SUM	240		722.68	8072		1.83	295		60			

HCC #3  
Civ 87

K=2.44

File #3  
Curb

Page 2 of 2  
Run Number KCC 3  
Operator TR

Plant KCC  
Date 1-25-90  
POST LEAK RATE 0.001 @ 5" HG

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V <sub>m</sub> )	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H, "H <sub>2</sub> O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (T <sub>s</sub> )	MEIER INLET	MEIER OUT	IMPINGER	FILTER	
13	0	2214	778.350	.75	1.83	1.0	297	60	57			5
14	10	2224	784.2	.69	1.68	1.7	296	62	57			5
15	20	2234	791.2	.80	1.95	2.0	297	64	58			5
16	30	2244	798.7	.78	1.90	1.9	296	64	58			5
17	40	2254	805.8	.78	1.90	1.9	296	64	58			5
18	50	2304	813.9	.74	1.81	1.8	297	63	57			5
	60	2314	820.891		POOR CHANGE							
19	0	2320	820.891	.74	1.81	1.8	297	63	57			5
20	10	2330	826.8	.72	1.76	1.8	295	63	57			5
21	20	2340	834.5	.69	1.68	1.7	296	66	58			5
22	30	2350	840.7	.75	1.83	1.8	293	67	60			5
23	40	2400	847.9	.75	1.83	1.8	295	68	60			5
24	50	2410	854.8	.76	1.85	1.9	294	66	60			5
	60	2420	862.189		END RUN #3							
AVERAGE /SUM	610		172.60	.9672		1.8	295	60				

ENGINEERING-SCIENCE, INC.

TRAIN RECOVERY SHEET

Cr # 1

DATE 1-25-90

FACILITY KRCC T# V

TECHNICIAN RP

RUN# \_\_\_\_\_ METHOD \_\_\_\_\_

TYPE \_\_\_\_\_

IMP. SOLUTION NaHCO<sub>3</sub>

SOLUTION	VOL. (ml)	DESCRIPTION
NOZZLE-PROBE RINSE		✓
UMBILICAL RINSE		✓

NOZZLE-PROBE RINSE

UMBILICAL RINSE

	FINAL (g)	INITIAL (g)	NET (g)
NaHCO <sub>3</sub>	375	100	275
NaHCO <sub>3</sub>	100	100	0
MT	0	0	0

IMPINGER # 1

IMPINGER # 2

IMPINGER # 3

IMPINGER # \_\_\_\_\_

DESCRIPTION

IMPINGER RINSE

SILICA GEL (DESCRIPTION)	FINAL (g)	INITIAL (g)	NET (g)
<u>1/5 used</u>	827.0	788.9	38.1

SILICA GEL (DESCRIPTION)

FILTER# (DESCRIPTION)

	<b>TOTAL MOISTURE</b>	
--	-----------------------	--

FIELD BLANKS

\_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

313.1 (g)

DISPOSITION/COMMENTS

\_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

ENGINEERING-SCIENCE, INC.

TRAIN RECOVERY SHEET

*W & Y*

DATE 1-25-90

FACILITY KACE # TV

TECHNICIAN KN

RUN# \_\_\_\_\_ METHOD \_\_\_\_\_

TYPE \_\_\_\_\_

IMP. SOLUTION NaHCO<sub>3</sub>

NOZZLE-PROBE RINSE

UMBILICAL RINSE

SOLUTION	VOL. (ml)	DESCRIPTION
		✓
		✓

IMPINGER # 1

IMPINGER # ✓

IMPINGER # 3

IMPINGER # \_\_\_\_\_

	FINAL (g)	INITIAL (g)	NET (g)
NaHCO <sub>3</sub>	345	100	245
NaHCO <sub>3</sub>	110	100	10
MT	0	0	0

DESCRIPTION

IMPINGER RINSE

SILICA GEL (DESCRIPTION)

	FINAL (g)	INITIAL (g)	
1/3 rxn	856.7	814.0	42.7

FILTER# (DESCRIPTION)

	TOTAL MOISTURE	
--	----------------	--

FIELD BLANKS

\_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

297.7 (g)

DISPOSITION/COMMENTS

\_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

ENGINEERING-SCIENCE, INC.

TRAIN RECOVERY SHEET

CR #3

DATE 1-26-90

FACILITY KACE #TV

TECHNICIAN PR

RUN# \_\_\_\_\_ METHOD \_\_\_\_\_

TYPE \_\_\_\_\_

IMP. SOLUTION \_\_\_\_\_

SOLUTION	VOL. (ml)	DESCRIPTION
NOZZLE-PROBE RINSE		✓
UMBILICAL RINSE		✓

NOZZLE-PROBE RINSE

UMBILICAL RINSE

IMPINGER # 1

IMPINGER # 2

IMPINGER # 3

IMPINGER # \_\_\_\_\_

	FINAL (g)	INITIAL (g)	NET (g)
<u>Na<sub>2</sub>CO<sub>3</sub></u>	<u>360</u>	<u>100</u>	<u>260</u>
<u>Na<sub>2</sub>CO<sub>3</sub></u>	<u>100</u>	<u>100</u>	<u>0</u>
<u>NET</u>	<u>0</u>	<u>0</u>	<u>0</u>

DESCRIPTION

IMPINGER RINSE

SILICA GEL  
(DESCRIPTION)

	FINAL (g)	INITIAL (g)	
<u>1/3 cup</u>	<u>872.1</u>	<u>782.8</u>	<u>34.3</u>

FILTER #  
(DESCRIPTION)

TOTAL MOISTURE

FIELD BLANKS

299.3 (g)

DISPOSITION/COMMENTS











ENGINEERING SCIENCE COMPANIES

Plant KRCC  
 Date 11/24/90  
 Test Site AD-1-A #2  
 Run Number 1-15  
 Operator STB

Ambient Temp 65  
 Barometer  
 Stack Pressure  
 Stack H<sub>2</sub>O &  
 Stack Dia 16.5"

Meter # 2000  
 Meter Gamma 0.97  
 Meter Box # 259  
 Nozzle Diameter 2.59  
 Probe Length

Probe Mat'l  
 Filter Number  
 Sump Box #  
 FIVE LEAK 0.00215" Hg  
 POST LEAK 0.001216" Hg

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS MEIER READING (V <sub>m</sub> )	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H; "H <sub>2</sub> O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (T <sub>s</sub> )	MEIER INLET	MEIER OUT	IMPINGER	FILTER	
1	0	0915	376.395	3.113	3.90	6.0	NA	AA	AA	NA	8°	
2	10	0918	478.534					50				
3	20	0935	397.3	1.5	3.5	3.5		50				
4	30	0945	406.9	1.6	3.73	3.7		50				
5	40	0955	417.1	1.6	3.73	3.7		50				
6	50	1005	427.4	1.6	3.73	3.7		56		45		12
7	60	1015	437.589	1.7	3.96	4.0		60		45		12
8	70	1030	447.7	1.7	3.96	4.0		60		45		13
9	80	1040	455.5	1.6	3.73	3.7		60		45		12
10	90	1050	468.2	1.6	3.73	3.7		60		45		12
11	100	1100	479.1	1.6	3.73	3.7		60		45		12
12	110	1110	489.1	1.6	3.73	3.7		60		45		12
	120	1120	499.297									
AVERAGE /SUM	240		255.21	1.3031		4.1	995					

*Handwritten notes:*  
 K = 2.79  
 MV.33  
 FIELD DATA

*Handwritten notes:*  
 Meter #10 2.00

*Handwritten notes:*  
 Ambient Temp 65

*Handwritten notes:*  
 Stack Dia 16.5"

PC = 2.33

WALKING #1

Plant KPCC  
 Date 11/20/90  
 POST LEAK RATE 0.007 @ 16" Hg

Page 2 of 2  
 Run Number AS  
 Operator ggg/glc

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V <sub>m</sub> )	VELOCITY HEAD (delta P)	ORIFICE PRESSURE (delta H, "H <sub>2</sub> O)		TEMPERATURES					PUMP VAC. "Hg
					Desired	Actual	STACK (Tb)	METER INLET	METER OUT	IMPINGER	FILTER	
13	120	<del>1127</del> 1130	499.297	<del>2.1</del> 1.9	<del>4.43</del> 4.43	4.4	300	60		50	N/A	15
14	130	<del>1137</del> 1130	510.1	1.9	4.43	4.4	300	60		50		15
15	140	<del>1147</del> 1147	521.2	1.9	4.43	4.4	300	60		50		15
16	150	1157	532.0	2.2	5.13	4.4	295	60		50		15
17	160	1207	542.1	2.2	5.13	4.4	305	60		50		15
18	170	1217	554.1	2.2	5.13	4.4	310	60		50		15
19	180	1227	565.198		part							
19	180	1237	565.198	2.2	5.13	4.4	310	60		50		15
20	190	<del>1245</del> 1245	575.9	2.2	5.13	4.3	311	60		50		14
21	200	<del>1255</del> 1255	587.0	2.3	5.36	4.3	310	68		50		14
22	210	<del>1307</del> 1307	598.0	2.0	4.66	4.3	310	70		50		15
23	220	<del>1317</del> 1317	609.2	2.0	4.66	4.3	311	70		50		14
24	230	<del>1325</del> 1325	620.4	2.0	4.66	4.3	308	70		50		15
24	240	<del>1337</del> 1337	631.603		end		sum	#1				
AVERAGE /SUM	240		255.21	1.3031		4.1	295	60				

Box A  
K = 2.33

FIELD DATA *UNUSUAL #2*

Plant KRIC Ambient Temp 70 Probe Mat'l Probe Mat'l  
 Date 11/21/90 Barometer 30.97 Filter Number 49  
 Test Site 22.1 #2 Stack Pressure 9 Meter Gamma 2.00 Sump Box # 0.001  
 Run Number 2 Stack H2O & Stack Dia 167.57 Meter Box # 2.39 Nozzle Diameter 2.39 Probe Length POST LEAK  
 Operator 211/3K

TRAVERSE POINT NUMBER	ELAPSED TIME (mins)	CLOCK TIME	GAS METER READING (V <sub>m</sub> )	VELOCITY HEAD (delta p)	ORIFICE PRESSURE (delta H, "H <sub>2</sub> O)		TEMPERATURES				PUMP VAC. "Hg	
					Desired	Actual	STACK (T <sub>s</sub> )	METER INLET	METER OUT	IMPINGER		FILTER
1	0	1500	640.47	1.5	4.19	4.2	305	70		49	NA	11
2	10	1510	652.4	1.9	4.43	4.4	303	70		49		12
3	20	1520	662.8	1.9	4.43	4.4	303	70		49		12
4	30	1530	674.1	2.0	4.66	4.7	308	70		49		12
5	40	1540	685.6	2.0	4.66	4.7	309	72		50		12
6	50	1550	697.2	2.0	4.66	4.7	309	72		50		11
7	60	1600	709.181	2.0	<i>Part change</i>		<i>change</i>					11
	60	1607	709.181	2.2	5.13	5.1	309	72		50		11
8	70	1613	724.6	2.2	5.13	5.1	309	72		50		11
9	80	1623	736.6	2.3	5.13	5.1	303	72		50		11
10	90	1633	748.6	2.2	4.66	4.7	302	72		50		11
11	100	1643	761.3	2.2	5.13	5.1	301	72		50		11
12	110	1653	772.4	2.2	5.13	5.1	301	72		50		11
	120	1707	784.540									
AVERAGE /SUM	240		984.31	1.4311		4.8	303			part change		

TMA Inc.

02/06/90 14:48:48

REPORT

WORK ORDER # AD-010034

REPORT Engineering Science  
TO 75 N. Fair Oaks Ave.  
P. O. Box 7107  
Pasadena, CA 91109

ATTEN H. Doriada

CLIENT ENGINEER SCI SAMPLES 3  
COMPANY Engineering Science  
FACILITY

WORK ID WA 005 KRCC

TAKEN BY ES Staff  
TRANS BY ES Staff

TYPE Gas

P. O. # WA 005

INVOICE under separate cover

SAMPLE IDENTIFICATION

01 900159  
02 900160  
03 900161

PREPARED Thermo Analytical, Inc.

BY 160 Taylor Street  
Monrovia, CA 91016

ATTEN Ms. Carole Harris  
PHONE 818-357-3247

CONTACT REM

CERTIFIED BY *Robert M. ...*

This report is for the sole and exclusive use of the client to whom it is addressed and represents only those samples herein described. Samples not destroyed in testing are retained a maximum of 30 days unless otherwise requested.

TEST CODES and NAMES used on this report

VGA A Volatile Organics by GC/MS

SAMPLE ID 900159

FRACTION 01A TEST CODE VDA A NAME Volatile Organics by GC/MS  
 Date & Time Collected 01/25/90 Category

VOLATILE ORGANIC RESULTS

COMPOUND	RESULT	DET LIMIT	COMPOUND	RESULT	DET LIMIT
Chloromethane	ND	0.25	1,1,2,2-Tetrachloroethane	ND	0.25
Bromomethane	ND	0.25	1,2-Dichloropropane	ND	0.25
Vinyl chloride	ND	0.25	trans-1,3-Dichloropropene	ND	0.25
Chloroethane	ND	0.25	1,1-Dichloroethane	ND	0.25
Methylene chloride	ND	0.25	1,1,1-Trichloroethane	ND	0.25
Acetone	ND	0.25	2,2,4-Trimethylpentane	ND	0.25
Acrolein	ND	0.25	Benzene	ND	0.25
Acrylonitrile	ND	0.25	1,2-Dichloropropane	ND	0.25
Carbon disulfide	ND	0.25	trans-1,3-Dichloropropene	ND	0.25
1,1-Dichloroethane	ND	0.25	1,1-Dichloroethane	ND	0.25
1,1-Dichloroethane	ND	0.25	1,1,1-Trichloroethane	ND	0.25
1,2-Dichloroethane	ND	0.25	2-Chloroethyl Vinyl Ether	ND	0.25
Chloroform	ND	0.25	Bromoform	ND	0.25
1,2-Dichloroethane	ND	0.25	2-Hexanone	ND	0.25
Methylethyl ketone	ND	0.25	4-Methyl-2-Pentanone	ND	0.25
1,1,1-Trichloroethane	ND	0.25	Tetrachloroethane	ND	0.25
Carbon tetrachloride	ND	0.25	Toluene	ND	0.25
Vinyl acetate	ND	0.25	Chlorobenzene	ND	0.25
Bromodichloromethane	ND	0.25	Ethyl benzene	ND	0.25
			Styrene	ND	0.25
			Xylenes (Total)	ND	0.25

NOTE: All results reported in mg/M3 unless otherwise specified  
 ND = Not detected at the specified limits

SURROGATE COMPOUNDS % RECOVERY

- DB-Toluene NA
- Bromofluorobenzene NA
- 1,2-Dichloroethane-d4 NA

ANALYST TZ  
 DATE INJECTED 01/30/90



TMA Inc.

REPORT

Work Order # AD-0034  
Continued From Above

Results by Sample

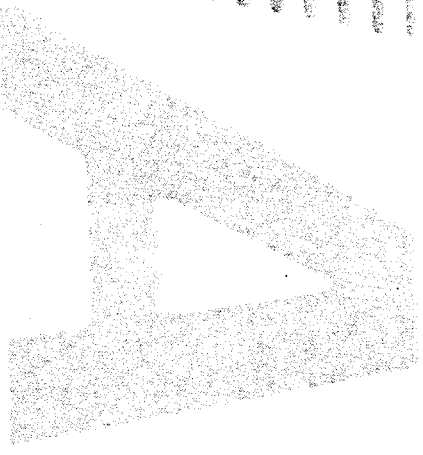
SAMPLE ID 900159

FRACTION Q1A TEST CODE VDA A NAME Volatile Organics by GC/MS  
Date & Time Collected 01/25/90 Category

TENTATIVELY IDENTIFIED VOLATILE COMPOUNDS

COMPOUND	APPR. CONC. mg/M3
1,3 Butadiene	ND
Propylene	ND

Small, illegible table with multiple columns and rows of data, possibly a reference list or detailed analysis table.



Received: 01/30/90

SAMPLE ID 900160

TMA Inc.

Results by Sample

REPORT

Work Order # A0-0034

FRACTION 02A TEST CODE VDA A NAME Volatile Organics by GC/MS  
Date & Time Collected 01/25/90 Category

VOLATILE ORGANIC RESULTS

COMPOUND	RESULT	DET LIMIT	COMPOUND	RESULT	DET LIMIT
Chloromethane	ND	0.25	1,1,2,2-Tetrachloroethane	ND	0.25
Bromomethane	ND	0.25	1,2-Dichloropropane	ND	0.25
Vinyl chloride	ND	0.25	trans-1,3-Dichloropropene	ND	0.25
Chloroethane	ND	0.25	Trichloroethene	ND	0.25
Methylene chloride	ND	0.25	Dibromochloromethane	ND	0.25
Acetone	ND	0.25	1,1,2-Trichloroethane	ND	0.25
Acrolein	ND	0.25	Benzene	ND	0.25
Acrylonitrile	ND	0.25	1,3-Dichloropropane	ND	0.25
Carbon disulfide	ND	0.25	2-Chloroethyl Vinyl Ether	ND	0.25
1,1-Dichloroethane	ND	0.25	Bromoform	ND	0.25
1,1-Dichloroethane	ND	0.25	2-Hexanone	ND	0.25
1,2-Dichloroethane	ND	0.25	4-Methyl-2-Pentanone	ND	0.25
Chloroform	ND	0.25	Tetrachloroethene	ND	0.25
1,2-Dichloroethane	ND	0.25	Toluene	ND	0.25
Methyleneethyl ketone	ND	0.25	Chlorobenzene	ND	0.25
1,1,1-Trichloroethane	ND	0.25	Ethyl benzene	ND	0.25
Carbon tetrachloride	ND	0.25	Styrene	ND	0.25
Vinyl acetate	ND	0.25	Xylenes (Total)	ND	0.25
Bromodichloromethane	ND	0.25			

NOTE: All results reported in mg/M3 unless otherwise specified  
ND = Not detected at the specified limits  
NA = Not Analyzed

SURROGATE COMPOUNDS % RECOVERY

dg-Toluene	NA
Bromofluorobenzene	NA
1,2-Dichloroethane-d4	NA

ANALYST TZ  
DATE INJECTED 01/30/90

Page 5  
Received: 01/30/90

SAMPLE ID 900160

TMA Inc.

Results by Sample

REPORT

Work Order # A0-0034  
Continued From Above

FRACTION 02A TEST CODE VOA A NAME Volatile Organics by GC/MS  
Date & Time Collected 01/25/90 Category

TENTATIVELY IDENTIFIED VOLATILE COMPOUNDS

COMPOUND	APPR. CONC. mg/M3
1,3 Butadiene	ND
Propylene	ND



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Received: 01/30/90

SAMPLE ID 900161

FRACTION 03A TEST CODE VDA A NAME Volatile Organics by GC/MS  
Date & Time Collected 01/25/90 Category

VOLATILE ORGANIC RESULTS

COMPOUND	RESULT	DET LIMIT	COMPOUND	RESULT	DET LIMIT
Chloromethane	ND	0.25	1,1,2,2-Tetrachloroethane	ND	0.25
Bromomethane	ND	0.25	1,2-Dichloropropane	ND	0.25
Vinyl chloride	ND	0.25	trans-1,3-Dichloropropene	ND	0.25
Chloroethane	ND	0.25	Trichloroethene	ND	0.25
Methylene chloride	ND	0.25	Dibromochloroethane	ND	0.25
Acetone	ND	0.25	1,1,2-Trichloroethane	ND	0.25
Acrolein	ND	0.25	Benzene	ND	0.25
Acrylonitrile	ND	0.25	1,1-Dichloroethene	ND	0.25
Carbon disulfide	ND	0.25	2-Chloroethyl Vinyl Ether	ND	0.25
1,1-Dichloroethene	ND	0.25	Bromoform	ND	0.25
1,1-Dichloroethane	ND	0.25	2-Hexanone	ND	0.25
1,2-Dichloroethene	ND	0.25	4-Methyl-2-Pentanone	ND	0.25
Chloroform	ND	0.25	1-Trichloroethene	ND	0.25
1,2-Dichloroethane	ND	0.25	Toluene	ND	0.25
Methylethyl ketone	ND	0.25	Chlorobenzene	ND	0.25
1,1,1-Trichloroethane	ND	0.25	Ethyl benzene	ND	0.25
Carbon tetrachloride	ND	0.25	Styrene	ND	0.25
Vinyl acetate	ND	0.25	Xylenes (Total)	ND	0.25
Bromodichloroethane	ND	0.25			

NOTE: All results reported in mg/M3 unless otherwise specified  
 NIJ = Not detected at the specified limits  
 NA = Not Analyzed

SURROGATE COMPOUNDS % RECOVERY

d8-Toluene	NA
Bromofluorobenzene	NA
1,2-Dichloroethane-d4	NA

ANALYST TZ  
DATE INJECTED 01/30/90

TMA Inc.

Results by Sample

REPORT

Work Order # AD-0034  
Continued From Above

Page 7  
Received: 01/30/90

SAMPLE ID 900161

FRACTION 03A TEST CODE VDA A NAME Volatile Organics by GC/MS  
Date & Time Collected 01/25/90 Category

TENTATIVELY IDENTIFIED VOLATILE COMPOUNDS

COMPOUND	APPR.	CONC.	mg/M3
1,3 Butadiene	ND		
Propylene	ND		

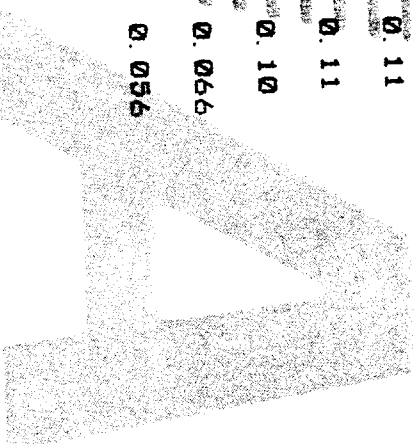


Engineering Science

SUMMARY OF RESULTS

Compound/Sample#	900159	900160	900161	Detection Limit
Benzene	ND	ND	ND	0.11
Acrolein	ND	ND	ND	0.11
1-3 Butadiene	ND	ND	ND	0.10
Propylene	ND	ND	ND	0.066
Toluene	ND	ND	ND	0.056
Xylene	ND	ND	ND	

Results given in ppm



**Appendix C**  
**Detailed Results**

Plant: KRCC

Source: UNIT 2 STACK OUTLET

Date: 1/25/90

Run: DIOXINS 2

Standard Temp = 60 deg F

Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches) 167.50  
STACK CROSS-SECTIONAL AREA (sq feet) 153.02  
BAROMETRIC PRESSURE (inches Hg) 29.44  
OXYGEN CONTENT (%) 14.4  
CARBON DIOXIDE CONTENT (%) 4.7  
MOISTURE CONTENT (%) 8.2  
STACK TEMPERATURE (deg F) 301  
STACK STATIC PRESSURE (inches water) 0.08  
DRY STACK GAS MOLECULAR WEIGHT 29.33  
VELOCITY PRESSURE (sq ft inches water) 1.30  
PILOT TUBE CORRECTION FACTOR 0.84  
VELOCITY (ft per sec) 89.04  
EXHAUST GAS FLOW RATE (ACFM) 817,465  
EXHAUST GAS FLOW RATE (DSCFM) 504,928

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF) 158.887  
DRY GAS VOLUME SAMPLED (DSCF) 154.841  
DRY GAS METER TEMPERATURE (deg F) 72  
DRY GAS METER GAMMA 1.01  
AVERAGE ORIFICE PRESSURE (inches water) 1.30  
TOTAL RUN TIME (min) 240  
NOZZLE DIAMETER (inches) 0.188  
ISOKINETIC (%) 102.0

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mis) 295.40



Engineering-Science, Pasadena, California

Plant: KRCC  
Source: UNIT 2 STACK OUTLET  
Date: 1/25/90  
Run: DIOXINS 1  
Standard Temp = 60 deg F      Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches)	167.50
STACK CROSS-SECTIONAL AREA (sq feet)	153.02
BAROMETRIC PRESSURE (inches Hg)	29.44
OXYGEN CONTENT (%)	14.4
CARBON DIOXIDE CONTENT (%)	4.7
MOISTURE CONTENT (%)	7.2
STACK TEMPERATURE (deg F)	303
STACK STATIC PRESSURE (inches water)	0.08
DRY STACK GAS MOLECULAR WEIGHT	29.33
VELOCITY PRESSURE (sq rt inches water)	1.05
PITOT TUBE CORRECTION FACTOR	0.84
VELOCITY (ft per sec)	71.88
EXHAUST GAS FLOW RATE (ACFM)	659,904
EXHAUST GAS FLOW RATE (DSCFM)	410,658

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF)	173.407
DRY GAS VOLUME SAMPLED (DSCF)	172.752
DRY GAS METER TEMPERATURE (deg F)	61
DRY GAS METER GAMMA	1.01
AVERAGE ORIFICE PRESSURE (inches water)	1.75
TOTAL RUN TIME (min)	240
NOZZLE DIAMETER (inches)	0.225
ISOKINETIC (%)	97.1

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mls)	289.00
--------------------------	--------

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: UNIT 2 STACK OUTLET  
Date: 1/26/90  
Run: TRACE 3  
Standard Temp = 60 deg F      Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches)	167.50
STACK CROSS-SECTIONAL AREA (sq feet)	153.02
BAROMETRIC PRESSURE (inches Hg)	29.44
OXYGEN CONTENT (%)	14.4
CARBON DIOXIDE CONTENT (%)	4.7
MOISTURE CONTENT (%)	7.4
STACK TEMPERATURE (deg F)	295
STACK STATIC PRESSURE (inches water)	0.05
DRY STACK GAS MOLECULAR WEIGHT	29.33
VELOCITY PRESSURE (sq rt inches water)	0.85
PITOT TUBE CORRECTION FACTOR	0.84
VELOCITY (ft per sec)	57.91
EXHAUST GAS FLOW RATE (ACFM)	531,654
EXHAUST GAS FLOW RATE (DSCFM)	333,529

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF)	172.284
DRY GAS VOLUME SAMPLED (DSCF)	162.911
DRY GAS METER TEMPERATURE (deg F)	80
DRY GAS METER GAMMA	0.99
AVERAGE ORIFICE PRESSURE (inches water)	1.60
TOTAL RUN TIME (min)	240
NOZZLE DIAMETER (inches)	0.245
ISOKINETIC (%)	95.1

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mls)	281.60
--------------------------	--------

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: UNIT 2 STACK OUTLET  
Date: 1/25/90  
Run: TRACE 2  
Standard Temp = 60 deg F      Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches)	167.50
STACK CROSS-SECTIONAL AREA (sq feet)	153.02
BAROMETRIC PRESSURE (inches Hg)	29.44
OXYGEN CONTENT (%)	14.4
CARBON DIOXIDE CONTENT (%)	4.7
MOISTURE CONTENT (%)	7.5
STACK TEMPERATURE (deg F)	295
STACK STATIC PRESSURE (inches water)	0.05
DRY STACK GAS MOLECULAR WEIGHT	29.33
VELOCITY PRESSURE (sq rt inches water)	0.82
PITOT TUBE CORRECTION FACTOR	0.84
VELOCITY (ft per sec)	55.87
EXHAUST GAS FLOW RATE (ACFM)	512,977
EXHAUST GAS FLOW RATE (DSCFM)	321,517

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF)	170.023
DRY GAS VOLUME SAMPLED (DSCF)	159.845
DRY GAS METER TEMPERATURE (deg F)	83
DRY GAS METER GAMMA	0.99
AVERAGE ORIFICE PRESSURE (inches water)	1.50
TOTAL RUN TIME (min)	240
NOZZLE DIAMETER (inches)	0.245
ISOKINETIC (%)	96.8

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mls)	279.70
--------------------------	--------

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: UNIT 2 STACK OUTLET  
Date: 1/25/90  
Run: TRACE 1  
Standard Temp = 60 deg F      Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches)	167.50
STACK CROSS-SECTIONAL AREA (sq feet)	153.02
BAROMETRIC PRESSURE (inches Hg)	29.44
OXYGEN CONTENT (%)	14.4
CARBON DIOXIDE CONTENT (%)	4.7
MOISTURE CONTENT (%)	6.7
STACK TEMPERATURE (deg F)	295
STACK STATIC PRESSURE (inches water)	0.05
DRY STACK GAS MOLECULAR WEIGHT	29.33
VELOCITY PRESSURE (sq rt inches water)	0.78
PITOT TUBE CORRECTION FACTOR	0.84
VELOCITY (ft per sec)	53.06
EXHAUST GAS FLOW RATE (ACFM)	487,114
EXHAUST GAS FLOW RATE (DSCFM)	308,169

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF)	160.980
DRY GAS VOLUME SAMPLED (DSCF)	165.983
DRY GAS METER TEMPERATURE (deg F)	56
DRY GAS METER GAMMA	1.04
AVERAGE ORIFICE PRESSURE (inches water)	1.48
TOTAL RUN TIME (min)	240
NOZZLE DIAMETER (inches)	0.245
ISOKINETIC (%)	104.9

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mls)	254.60
--------------------------	--------

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: UNIT 2 STACK OUTLET  
Date: 1/26/90  
Run: DIOXINS 3  
Standard Temp = 60 deg F      Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches)	167.50
STACK CROSS-SECTIONAL AREA (sq feet)	153.02
BAROMETRIC PRESSURE (inches Hg)	29.44
OXYGEN CONTENT (%)	14.4
CARBON DIOXIDE CONTENT (%)	4.7
MOISTURE CONTENT (%)	4.9
STACK TEMPERATURE (deg F)	296
STACK STATIC PRESSURE (inches water)	0.08
DRY STACK GAS MOLECULAR WEIGHT	29.33
VELOCITY PRESSURE (sq rt inches water)	1.30
PITOT TUBE CORRECTION FACTOR	0.84
VELOCITY (ft per sec)	88.17
EXHAUST GAS FLOW RATE (ACFM)	809,512
EXHAUST GAS FLOW RATE (DSCFM)	521,248

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF)	156.467
DRY GAS VOLUME SAMPLED (DSCF)	151.345
DRY GAS METER TEMPERATURE (deg F)	76
DRY GAS METER GAMMA	1.01
AVERAGE ORIFICE PRESSURE (inches water)	1.30
TOTAL RUN TIME (min)	240
NOZZLE DIAMETER (inches)	0.188
ISOKINETIC (%)	96.5

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mls)	166.90
--------------------------	--------

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: UNIT 2 STACK OUTLET  
Date: 1/25/90  
Run: CR 3  
Standard Temp = 60 deg F      Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches)	167.50
STACK CROSS-SECTIONAL AREA (sq feet)	153.02
BAROMETRIC PRESSURE (inches Hg)	29.44
OXYGEN CONTENT (%)	14.4
CARBON DIOXIDE CONTENT (%)	4.7
MOISTURE CONTENT (%)	7.3
STACK TEMPERATURE (deg F)	295
STACK STATIC PRESSURE (inches water)	0.08
DRY STACK GAS MOLECULAR WEIGHT	29.33
VELOCITY PRESSURE (sq rt inches water)	0.87
PITOT TUBE CORRECTION FACTOR	0.84
VELOCITY (ft per sec)	59.25
EXHAUST GAS FLOW RATE (ACFM)	543,989
EXHAUST GAS FLOW RATE (DSCFM)	341,819

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF)	172.677
DRY GAS VOLUME SAMPLED (DSCF)	176.815
DRY GAS METER TEMPERATURE (deg F)	60
DRY GAS METER GAMMA	1.04
AVERAGE ORIFICE PRESSURE (inches water)	1.80
TOTAL RUN TIME (min)	250
NOZZLE DIAMETER (inches)	0.250
ISOKINETIC (%)	92.9

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mls)	299.30
--------------------------	--------

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: UNIT 2 STACK OUTLET  
Date: 1/25/90  
Run: CR 2  
Standard Temp = 60 deg F      Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches)	167.50
STACK CROSS-SECTIONAL AREA (sq feet)	153.02
BAROMETRIC PRESSURE (inches Hg)	29.44
OXYGEN CONTENT (%)	14.4
CARBON DIOXIDE CONTENT (%)	4.7
MOISTURE CONTENT (%)	7.2
STACK TEMPERATURE (deg F)	300
STACK STATIC PRESSURE (inches water)	0.08
DRY STACK GAS MOLECULAR WEIGHT	29.33
VELOCITY PRESSURE (sq rt inches water)	0.86
PITOT TUBE CORRECTION FACTOR	0.84
VELOCITY (ft per sec)	58.76
EXHAUST GAS FLOW RATE (ACFM)	539,451
EXHAUST GAS FLOW RATE (DSCFM)	336,949

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF)	176.574
DRY GAS VOLUME SAMPLED (DSCF)	177.394
DRY GAS METER TEMPERATURE (deg F)	70
DRY GAS METER GAMMA	1.04
AVERAGE ORIFICE PRESSURE (inches water)	1.80
TOTAL RUN TIME (min)	240
NOZZLE DIAMETER (inches)	0.250
ISOKINETIC (%)	98.5

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mls)	297.70
--------------------------	--------

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: UNIT 2 STACK OUTLET  
Date: 1/25/90  
Run: CR 1  
Standard Temp = 60 deg F      Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches)	167.50
STACK CROSS-SECTIONAL AREA (sq feet)	153.02
BAROMETRIC PRESSURE (inches Hg)	29.44
OXYGEN CONTENT (%)	14.4
CARBON DIOXIDE CONTENT (%)	4.7
MOISTURE CONTENT (%)	7.5
STACK TEMPERATURE (deg F)	296
STACK STATIC PRESSURE (inches water)	0.08
DRY STACK GAS MOLECULAR WEIGHT	29.33
VELOCITY PRESSURE (sq rt inches water)	0.88
PITOT TUBE CORRECTION FACTOR	0.84
VELOCITY (ft per sec)	60.00
EXHAUST GAS FLOW RATE (ACFM)	550,837
EXHAUST GAS FLOW RATE (DSCFM)	344,878

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF)	184.674
DRY GAS VOLUME SAMPLED (DSCF)	179.364
DRY GAS METER TEMPERATURE (deg F)	66
DRY GAS METER GAMMA	0.99
AVERAGE ORIFICE PRESSURE (inches water)	1.80
TOTAL RUN TIME (min)	240
NOZZLE DIAMETER (inches)	0.250
ISOKINETIC (%)	97.3

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mls)	313.10
--------------------------	--------



Engineering-Science, Pasadena, California

Plant: KRCC  
Source: UNIT 2 STACK OUTLET  
Date: 1/26/90  
Run: AS 3  
Standard Temp = 60 deg F      Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches)	167.50
STACK CROSS-SECTIONAL AREA (sq feet)	153.02
BAROMETRIC PRESSURE (inches Hg)	29.44
OXYGEN CONTENT (%)	14.4
CARBON DIOXIDE CONTENT (%)	4.7
MOISTURE CONTENT (%)	7.2
STACK TEMPERATURE (deg F)	296
STACK STATIC PRESSURE (inches water)	0.10
DRY STACK GAS MOLECULAR WEIGHT	29.33
VELOCITY PRESSURE (sq rt inches water)	1.41
PITOT TUBE CORRECTION FACTOR	0.84
VELOCITY (ft per sec)	96.07
EXHAUST GAS FLOW RATE (ACFM)	882,045
EXHAUST GAS FLOW RATE (DSCFM)	554,057

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF)	261.977
DRY GAS VOLUME SAMPLED (DSCF)	248.080
DRY GAS METER TEMPERATURE (deg F)	70
DRY GAS METER GAMMA	0.97
AVERAGE ORIFICE PRESSURE (inches water)	4.50
TOTAL RUN TIME (min)	240
NOZZLE DIAMETER (inches)	0.240
ISOKINETIC (%)	91.3

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mls)	414.50
--------------------------	--------

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: UNIT 2 STACK OUTLET  
Date: 1/25/90  
Run: AS 2  
Standard Temp = 60 deg F      Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches)	167.50
STACK CROSS-SECTIONAL AREA (sq feet)	153.02
BAROMETRIC PRESSURE (inches Hg)	29.44
OXYGEN CONTENT (%)	14.4
CARBON DIOXIDE CONTENT (%)	4.7
MOISTURE CONTENT (%)	7.4
STACK TEMPERATURE (deg F)	303
STACK STATIC PRESSURE (inches water)	0.10
DRY STACK GAS MOLECULAR WEIGHT	29.33
VELOCITY PRESSURE (sq rt inches water)	1.43
PITOT TUBE CORRECTION FACTOR	0.84
VELOCITY (ft per sec)	97.93
EXHAUST GAS FLOW RATE (ACFM)	899,107
EXHAUST GAS FLOW RATE (DSCFM)	558,179

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF)	284.365
DRY GAS VOLUME SAMPLED (DSCF)	268.973
DRY GAS METER TEMPERATURE (deg F)	71
DRY GAS METER GAMMA	0.97
AVERAGE ORIFICE PRESSURE (inches water)	4.80
TOTAL RUN TIME (min)	240
NOZZLE DIAMETER (inches)	0.240
ISOKINETIC (%)	98.2

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mls)	465.20
--------------------------	--------

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: UNIT 2 STACK OUTLET  
Date: 1/25/90  
Run: AS 1  
Standard Temp = 60 deg F      Standard Press = 29.92 in Hg

-----  
FLOW DATA  
-----

STACK DIAMETER (inches)	167.50
STACK CROSS-SECTIONAL AREA (sq feet)	153.02
BAROMETRIC PRESSURE (inches Hg)	29.44
OXYGEN CONTENT (%)	14.4
CARBON DIOXIDE CONTENT (%)	4.7
MOISTURE CONTENT (%)	7.4
STACK TEMPERATURE (deg F)	295
STACK STATIC PRESSURE (inches water)	0.10
DRY STACK GAS MOLECULAR WEIGHT	29.33
VELOCITY PRESSURE (sq rt inches water)	1.30
PITOT TUBE CORRECTION FACTOR	0.84
VELOCITY (ft per sec)	88.55
EXHAUST GAS FLOW RATE (ACFM)	812,946
EXHAUST GAS FLOW RATE (DSCFM)	510,472

-----  
SAMPLING DATA  
-----

DRY GAS VOLUME SAMPLED (DCF)	255.205
DRY GAS VOLUME SAMPLED (DSCF)	245.599
DRY GAS METER TEMPERATURE (deg F)	61
DRY GAS METER GAMMA	0.97
AVERAGE ORIFICE PRESSURE (inches water)	4.10
TOTAL RUN TIME (min)	240
NOZZLE DIAMETER (inches)	0.240
ISOKINETIC (%)	98.1

-----  
LABORATORY DATA  
-----

MOISTURE RECOVERED (mls)	419.90
--------------------------	--------

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: HRSG STACK OUTLET 2  
Date: 1/23/90  
Run: 1 (FUEL OIL)  
Standard Temperature = 520 Deg. R

-----  
FUEL DATA  
-----

HYDROGEN CONTENT (%)	15.12
CARBON CONTENT (%)	84.81
OXYGEN CONTENT (%)	0.10
NITROGEN CONTENT (%)	0.03
SULFUR CONTENT (%)	0.04
GROSS CALORIFIC VALUE (BTU/LB)	19440
FUEL CONSUMPTION (LBS/SEC)	11.26
F FACTOR (DSCF/MMBTU)	9362

-----  
POLLUTANT DATA  
-----

NOX (PPM)	42.0
SO2 (PPM)	0.0
CO (PPM)	14.9
CH4 (PPM)	0.0
NMHC (PPM AS CH4)	0.0
OXYGEN (%)	14.3
CARBON DIOXIDE (%)	4.7

-----  
EMISSIONS DATA BY O2  
-----

NOX (LBS/HR)	117.154
NOX (LBS/MMBTU)	0.149
SO2 (LBS/HR)	0.000
SO2 (LBS/MMBTU)	0.000
CO (LBS/HR)	25.306
CO (LBS/MMBTU)	0.032
CH4 (LBS/HR)	0.000
CH4 (LBS/MMBTU)	0.000
NMHC (LBS/HR)	0.000
NMHC (LBS/MMBTU)	0.000
CALCULATED STACK FLOW (DSCFM)	383789

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: HRSG STACK OUTLET 2  
Date: 1/23/90  
Run: 2 (FUEL OIL)  
Standard Temperature = 520 Deg. R

-----  
FUEL DATA  
-----

HYDROGEN CONTENT (%)	15.12
CARBON CONTENT (%)	84.81
OXYGEN CONTENT (%)	0.10
NITROGEN CONTENT (%)	0.03
SULFUR CONTENT (%)	0.04
GROSS CALORIFIC VALUE (BTU/LB)	19440
FUEL CONSUMPTION (LBS/SEC)	11.21
F FACTOR (DSCF/MMBTU)	9362

-----  
POLLUTANT DATA  
-----

NOX (PPM)	36.4
SO2 (PPM)	0.0
CO (PPM)	17.9
CH4 (PPM)	0.0
NMHC (PPM AS CH4)	0.0
OXYGEN (%)	14.5
CARBON DIOXIDE (%)	4.4

-----  
EMISSIONS DATA BY O2  
-----

NOX (LBS/HR)	104.241
NOX (LBS/MMBTU)	0.133
SO2 (LBS/HR)	0.000
SO2 (LBS/MMBTU)	0.000
CO (LBS/HR)	31.212
CO (LBS/MMBTU)	0.040
CH4 (LBS/HR)	0.000
CH4 (LBS/MMBTU)	0.000
NMHC (LBS/HR)	0.000
NMHC (LBS/MMBTU)	0.000
CALCULATED STACK FLOW (DSCFM)	394025

Engineering-Science, Pasadena, California

Plant: KRCC  
Source: HRSG STACK OUTLET 2  
Date: 1/23/90  
Run: 3 (FUEL OIL)  
Standard Temperature = 520 Deg. R

-----  
FUEL DATA  
-----

HYDROGEN CONTENT (%)	15.12
CARBON CONTENT (%)	84.81
OXYGEN CONTENT (%)	0.10
NITROGEN CONTENT (%)	0.03
SULFUR CONTENT (%)	0.04
GROSS CALORIFIC VALUE (BTU/LB)	19440
FUEL CONSUMPTION (LBS/SEC)	11.29
F FACTOR (DSCF/MMBTU)	9362

-----  
POLLUTANT DATA  
-----

NOX (PPM)	36.3
SO2 (PPM)	0.0
CO (PPM)	17.3
CH4 (PPM)	0.0
NMHC (PPM AS CH4)	0.0
OXYGEN (%)	14.6
CARBON DIOXIDE (%)	4.6

-----  
EMISSIONS DATA BY O2  
-----

NOX (LBS/HR)	106.359
NOX (LBS/MMBTU)	0.135
SO2 (LBS/HR)	0.000
SO2 (LBS/MMBTU)	0.000
CO (LBS/HR)	30.863
CO (LBS/MMBTU)	0.039
CH4 (LBS/HR)	0.000
CH4 (LBS/MMBTU)	0.000
NMHC (LBS/HR)	0.000
NMHC (LBS/MMBTU)	0.000
CALCULATED STACK FLOW (DSCFM)	403136

ENGINEERING SCIENCE, INC.  
Pasadena, California

MOBILE SOURCE TEST VAN  
CONTINUOUS EMISSIONS MONITORS DATA  
CALIBRATION DRIFT CORRECTION

Project No. WA Turbine # Source Name KRCC

Test Location HREG End out Date 1/25/90

Test No.	Parameter	$\bar{C}$	$C_0$	$C_m$	$C_{ms}$	$C_{gas}$
1	NOx	46.5	0.05	51.4	51.4	46.3
	CO	13.1	0	12.95	12.91	13.1
	CO <sub>2</sub>	4.8	0	9.75	9.8	4.8
	O <sub>2</sub>	14.3	0	14.4	14.66	14.4
2	NOx	45.6	0	44.3	43.7	45.0
	CO	13.0	-0.1	21.8	21.83	13.1
	CO <sub>2</sub>	4.7	0.02	9.6	9.64	4.7
	O <sub>2</sub>	14.0	0	14.35	14.64	14.3
3	NOx	45.3	0	44.3	43.7	44.7
	CO	12.5	-0.1	21.8	21.83	12.6
	CO <sub>2</sub>	4.5	0.02	9.4	9.64	4.5
	O <sub>2</sub>	14.0	0	14.35	14.64	14.3

$$C_{gas} = (\bar{C} - C_0) (C_{ms} / (C_m - C_0))$$

$C_{gas}$  - corrected gas concentration, ppm or % vol(dry)

$\bar{C}$  - analyzer gas concentration, ppm or % vol(dry)

$C_0$  - average of initial and final zero drift, ppm or % vol(dry)

$C_m$  - average of initial and final span drift, ppm or % vol(dry)

$C_{ms}$  - span gas cylinder concentration, ppm or % vol(dry)





**ENGINEERING SCIENCE  
Pasadena, California  
SUMMARY OF CEM DATA**

Project KRCC source Test Date Jan 25, 1970 Sheet 2 of 2  
 Plant KRCC Location Unit # 2 Stack outlet  
 Operator DSW

Time	NO		NO <sub>x</sub>		SO <sub>2</sub>		CO		CO <sub>2</sub>		O <sub>2</sub>		Conc.	
	Chart	Conc. (ppm)	Chart	Conc. (ppm)	Chart	Conc. (ppm)	Chart	Conc. (ppm)	Chart	Conc. (%)	Chart	Conc. (%)	Chart	Conc.
Run # 2														
1030-1045			45.5	45.5		26.2	13.1	23.8	4.8	56.2	4.1			
1045-1100			45.4	45.4		26.1	13.1	23.6	4.7	56.1	4.0			
1100-1115			45.6	45.4		25.6	12.8	23.3	4.7	56.1	4.0			
1115-1130			45.7	45.7		25.8	12.9	23.1	4.4	56.1	4.0			
Ave. Conc.				45.6			13.0		4.7		14.0			
Run # 3														
1130-1145			45.5	45.5		25.3	12.7	23.0	4.4	56.1	4.0			
1145-1200			45.3	45.3		25.3	12.7	22.9	4.4	56.0	4.0			
1200-1215			45.2	45.2		24.9	12.5	22.4	4.5	56.0	4.0			
1215-1230			45.3	45.3		24.5	12.3	22.3	4.5	56.0	4.0			
Ave. Conc.				45.3			12.5		4.5		14.0			
Mid. Calc.			0.1	0		-0.3	0	-0.2	0	0	0			
			44.8	43.7		43.6	21.83	46.8	9.64	57	4.66			
								48.2	9.64	58.4	4.66			



ENGINEERING SCIENCE  
Pasadena, California

ANALYZER CALIBRATION ERROR

Facility: RCC Source Test

Source: RCC

Location: Unit 2 stack outlet Fuel oil

Date: 1/25/90

Operator: DJW

Time: \_\_\_\_\_

Sheet 4 of \_\_\_\_\_

Run No.	Species	Full Scale	Cylinder Value	Analyzer Reading	Absolute Diff.	Diff. ± Span
Zero	NO <sub>x</sub>	0-100 ppm	0	0	0	0
Upscale			51.4	51.2	-0.2	0.2
Zero	NO <sub>x</sub>	0-100 ppm	0	0	0	0
Upscale			13.55	13.1	0.5	0.5
Zero	NO <sub>x</sub>	0-100 ppm	0	0	0	0
Upscale			43.7	44.5	0.8	0.8
Zero	O <sub>2</sub>	0-25%	0	0	0	0
Upscale			14.6	14.8	0.1	0.4
Zero	O <sub>2</sub>	0-25%	0	0	0	0
Upscale			3.04	3.1	0.04	0.2
Zero	O <sub>2</sub>					
Upscale						

Run No.	Species	Full Scale	Cylinder Value	Analyzer Reading	Absolute Diff.	Diff. ± Span
Zero	CO	0-50 ppm	0	0	0	0
Upscale			12.9	13.0	0.1	0.2
Zero	CO	0-50 ppm				
Upscale						
Zero	CO					
Upscale						
Zero	CO <sub>2</sub>	0-20%	0	0	0	0
Upscale			9.44	9.8	0.2	0.8
Zero	CO <sub>2</sub>	0-20%	0	0	0	0
Upscale			3.4	3.4	0.2	1.0
Zero						
Upscale						

ENGINEERING SCIENCE  
Pasadena, California

CALIBRATION DRIFT TEST

Facility: KRCC Source Test  
 Source: #12 Stack outlet, Fuel oil fired  
 Location: Bakersfield CA

Date: 1/25/90  
 Operator: DJW  
 Time: \_\_\_\_\_  
 Sheet: 5 of \_\_\_\_\_

Run No.	Specie	Full Scale	Initial Response	Final Response	Drift
0920-1020					
Zero	NO <sub>x</sub>	0-100	0	0.1	0.1
Upscale		ppm	51.2	51.9	0.7
Zero	NO <sub>x</sub>				
Upscale					
Zero	CO	0-50	0	0	0
Upscale		ppm	13.0	12.9	-0.2
Zero	CO				
Upscale					
Zero	O <sub>2</sub>	0-25%	0	0	0
Upscale			14.8	14.4	-1.0
Zero	CO <sub>2</sub>	0-20%	0	0	0
Upscale			9.8	9.7	-0.5

Run No.	Specie	Full Scale	Initial Response	Final Response	Drift
243					
Zero	NO <sub>x</sub>	0-100	0	0	0
Upscale		ppm	43.7	44.8	1.1
Zero	NO <sub>x</sub>				
Upscale					
Zero	CO	0-50	0	-0.2	
Upscale		ppm	12.9		
Zero	CO	0-50	0	0.2	0.4
Upscale		ppm	21.8	21.8	0
Zero	O <sub>2</sub>	0-25%	0	0	0
Upscale			14.4	14.3	0.4
Zero	CO <sub>2</sub>	0-20%	0	0.04	0.2
Upscale			9.7	9.4	1.5

ENGINEERING SCIENCE  
Pasadena, California

CALIBRATION DRIFT TEST

Facility: KREC  
 Source: Unit #2 Stand outside Fuel oil fired  
 Location: Bakersfield, CA  
 Date: 1/25/90  
 Operator: D.S.W.  
 Time: \_\_\_\_\_  
 Sheet 1 of \_\_\_\_\_

Run No. 4  
1307-1407

Run No.	Species	Full Scale	Initial Response	Final Response	Drift (% Span)
Zero	NO <sub>x</sub>				
Upscale	NO <sub>x</sub>				
Zero	NO <sub>x</sub>				
Upscale	NO <sub>x</sub>				
Zero	CO				
Upscale	CO				
Zero	CO				
Upscale	CO				
Zero	O <sub>2</sub>				
Upscale	O <sub>2</sub>				
Zero	CO <sub>2</sub>				
Upscale	CO <sub>2</sub>				

Run No.	Species	Full Scale	Initial Response	Final Response	Drift (% Span)
Zero	NO <sub>x</sub>	0-100	0	0	0
Upscale	NO <sub>x</sub>	100	44.8	45.0	0.12
Zero	NO <sub>x</sub>				
Upscale	NO <sub>x</sub>				
Zero	CO	0-50	0.2	-0.19	-2.2
Upscale	CO	50	21.8	21.6	-0.14
Zero	CO				
Upscale	CO				
Zero	O <sub>2</sub>	0-25%	6	0	0
Upscale	O <sub>2</sub>	25%	14.3	14.8	2.0
Zero	CO <sub>2</sub>	0-20%	0.04	0	-0.2
Upscale	CO <sub>2</sub>	20%	9.4	9.6	1.0

**Appendix D**  
**Example Calculations**

Client KERN UNIT # ✓  
 Subject Sample Comp - New  
F film DSCFM

Job No. \_\_\_\_\_  
 By PR  
 Checked \_\_\_\_\_

Sheet 1 of 4  
 Date \_\_\_\_\_  
 Rev. \_\_\_\_\_

Table 1

Flow print out - average values  
 DSCFM - Fuel oil print out, average values

Run # 1	383 729
# 2	394 025
# 3	<u>403 136</u>

393 650 diff <sup>3</sup>/min

Table 2

Lab results, no comp.

Table 3 lb/hr trace elements:

Parameter	1	2	3	4
Run #				
TS #	900201	900202	900203	(Blank) 900204
ml (HNO <sub>3</sub> )	620	780	780	700
ml (KMnO <sub>4</sub> )	180	150	180	130
As	4.69	1.38	4.85	4.1
Be	< 0.13	2.4	< 0.16	< 0.14
Cd	< 4.96	< 6.24	< 6.24	< 5.6
(WAS) Cr <sup>5</sup>	0.11	0.204	0.32	< 0.64
Cr total	11	< 5.95	8	< 7.0
Cu	18.4	75.94	9.12	5.4
Hg	0.03	0.09	0.028	0.072
Mn	262.24	133.16	160.048	46.8
Ni	49.6	2496	20	< 6.6
Pb	12.91	12.57	7.18	7.16
Se	< 0.13	< 0.16	< 0.16	< 0.14
Zn	246.8	2696.4	99.88	468.8

Client ICERN UNIT # 2  
 Subject W/F Factor

Job No. \_\_\_\_\_  
 By RA  
 Checked \_\_\_\_\_

Sheet 2 of 4  
 Date \_\_\_\_\_  
 Rev. \_\_\_\_\_

**F Factor DSCFM**

Run #	DSCFM
1	383789
2	394025
3	403176

Run #	Metals	Cu
1	166.674 ft <sup>3</sup>	178.642 ft <sup>3</sup>
2	159.701	178.079
3	162.755	177.497

Average # 393650 DSCFM

$$\text{lb/hr} = \frac{\text{mg sample} \times \frac{10^{-6} \text{ gram}}{\text{mg}} \times \frac{1 \text{ lb}}{453.59 \text{ gram}}}{\text{DSCFM (ft}^3)} \times \frac{\text{DSCFM ft}^3}{\text{min}} \times \frac{60 \text{ min}}{\text{hr}}$$

$$= 1.32 \times 10^{-7} \left( \frac{\text{ug}}{\text{DSCFM}} \right) \text{ DSCFM}$$

	Run # 1 lb/hr	Run # 2 lb/hr	Run # 3 lb/hr	Ave	lb/MMBtu
As	1.47 x 10 <sup>-3</sup>	4.51 x 10 <sup>-4</sup>	1.56 x 10 <sup>-3</sup>	1.2 x 10 <sup>-3</sup>	1.5 x 10 <sup>-6</sup>
Ba	< 4.06 x 10 <sup>-5</sup>	7.55 x 10 <sup>-4</sup>	< 5.13 x 10 <sup>-5</sup>	< 2.9 x 10 <sup>-4</sup>	3.7 x 10 <sup>-7</sup>
Cd	< 1.55 x 10 <sup>-3</sup>	< 2.04 x 10 <sup>-3</sup>	< 2.00 x 10 <sup>-3</sup>	< 1.9 x 10 <sup>-3</sup>	2.4 x 10 <sup>-7</sup>
Co	3.26 x 10 <sup>-5</sup>	6.67 x 10 <sup>-5</sup>	1.03 x 10 <sup>-4</sup>	6.8 x 10 <sup>-5</sup>	8.6 x 10 <sup>-8</sup>
Cr (total)	3.40 x 10 <sup>-3</sup>	< 1.95 x 10 <sup>-3</sup>	2.57 x 10 <sup>-3</sup>	2.7 x 10 <sup>-3</sup>	3.4 x 10 <sup>-6</sup>
Cu	5.75 x 10 <sup>-3</sup>	8.48 x 10 <sup>-3</sup>	2.93 x 10 <sup>-3</sup>	5.7 x 10 <sup>-3</sup>	7.3 x 10 <sup>-6</sup>
Hg	9.48 x 10 <sup>-6</sup>	7.94 x 10 <sup>-5</sup>	7.70 x 10 <sup>-5</sup>	1.5 x 10 <sup>-6</sup>	2.0 x 10 <sup>-9</sup>
Mn	8.10 x 10 <sup>-2</sup>	4.16 x 10 <sup>-2</sup>	5.14 x 10 <sup>-2</sup>	5.8 x 10 <sup>-2</sup>	7.4 x 10 <sup>-5</sup>
Ni	1.55 x 10 <sup>-2</sup>	8.16 x 10 <sup>-1</sup>	6.42 x 10 <sup>-3</sup>	2.8 x 10 <sup>-1</sup>	3.5 x 10 <sup>-4</sup>
Pb	4.65 x 10 <sup>-3</sup>	4.11 x 10 <sup>-3</sup>	2.30 x 10 <sup>-3</sup>	3.0 x 10 <sup>-3</sup>	4.4 x 10 <sup>-3</sup>
Se	< 2.06 x 10 <sup>-5</sup>	5.73 x 10 <sup>-5</sup>	5.13 x 10 <sup>-5</sup>	4.8 x 10 <sup>-5</sup>	6.1 x 10 <sup>-8</sup>
Zn	7.71 x 10 <sup>-2</sup>	8.8 x 10 <sup>-1</sup>	9.20 x 10 <sup>-2</sup>	3.3 x 10 <sup>-1</sup>	4.2 x 10 <sup>-5</sup>

MMBtu/hr = 787.32 MMBtu/hr



Client ICRCC  
 Subject Dioxins/Furans  
NEW DSCFM

Job No. \_\_\_\_\_  
 By PK  
 Checked \_\_\_\_\_

Sheet 4 of 4  
 Date \_\_\_\_\_  
 Rev. \_\_\_\_\_

	SPICED Blank	Run # 1	Run # 2	Run # 3	Method	
Furans		picogram	picogram	picogram	picogram	
TCDF	<16	26	45	1600	<1.2	
Pc CDF	<14	19	170	2200	<1.3	
Hx CDF	<3.3	14	94	1100	<0.59	
Hp CDF	<20	76	110	660	<1.3	
OCDF	52	<72	120	250	44	
Dioxins						
TCDD	<15	<9.2	<19	160	<1.0	
Pc CDD	<9.4	4.2	<14	340	<1.5	
Hx CDD	<7.0	43	43	370	<1.9	
Hp CDD	90	240	210	460	<11	
OCDD	1600	1600	2400	2500	<190	
DSCFM =	393 GSD	40712	24994	51317		
DSCF (FP)		Run #1	#2	#3		
		172.70V	174.841	151.345		
lb/hr =	$\frac{\text{picogram} \times \frac{10^{-12} \text{ gram}}{\text{pg}} \times \frac{1 \text{ lb}}{453.59 \text{ grams}} \times 393 \text{ GSD} \times \frac{60 \text{ min}}{\text{hr}}}{\text{DSCF (FP)}} \times \frac{\text{min}}{\text{hr}}$					
TCDF	$7.8 \times 10^{-9}$	<del><math>7.8 \times 10^{-9}</math></del>	$1.5 \times 10^{-8}$	$5.5 \times 10^{-7}$	$1.9 \times 10^{-7}$	$7.4 \times 10^{-10}$
Pc CDF	$5.7 \times 10^{-9}$	<del><math>9.0 \times 10^{-7}</math></del>	$4.0 \times 10^{-8}$	$2.6 \times 10^{-7}$	$7.7 \times 10^{-7}$	$3.4 \times 10^{-10}$
Hx CDF	$4.2 \times 10^{-9}$	<del><math>7.3 \times 10^{-7}</math></del>	$3.0 \times 10^{-8}$	$3.8 \times 10^{-7}$	$1.4 \times 10^{-7}$	$1.8 \times 10^{-10}$
Hp CDF	$2.3 \times 10^{-8}$	<del><math>4.0 \times 10^{-7}</math></del>	$3.7 \times 10^{-8}$	$4.3 \times 10^{-7}$	$1.0 \times 10^{-7}$	$1.2 \times 10^{-10}$
OCDF	< $5.4 \times 10^{-9}$	< $9.4 \times 10^{-7}$	$2.2 \times 10^{-8}$	$6.7 \times 10^{-8}$	$3.1 \times 10^{-8}$	$4.0 \times 10^{-11}$
TCDD	< $4.5 \times 10^{-9}$		$2.6 \times 10^{-9}$	$5.5 \times 10^{-8}$	$2.2 \times 10^{-8}$	$7.8 \times 10^{-11}$
Pc CDD	< $2.8 \times 10^{-9}$		< $4.7 \times 10^{-9}$	$1.2 \times 10^{-7}$	< $4.7 \times 10^{-8}$	$5.4 \times 10^{-11}$
Hx CDD	$1.3 \times 10^{-8}$		$1.4 \times 10^{-8}$	$1.3 \times 10^{-7}$	$5.2 \times 10^{-8}$	$6.6 \times 10^{-11}$
Hp CDD	$3.3 \times 10^{-8}$		$4.0 \times 10^{-8}$	$1.3 \times 10^{-7}$	$6.8 \times 10^{-8}$	$8.6 \times 10^{-11}$
OCDD	< $5.7 \times 10^{-9}$		$1.3 \times 10^{-7}$	$1.4 \times 10^{-7}$	$1.1 \times 10^{-7}$	$1.4 \times 10^{-10}$

Client KRCC AB XXK  
 Subject NEW DSCFM

Job No. \_\_\_\_\_  
 By RL  
 Checked \_\_\_\_\_

Sheet 3 of 4  
 Date \_\_\_\_\_  
 Rev. \_\_\_\_\_

Asenic

Run #	ug/l	g	ug	DSCF	DSCFM	lb/hr
1	7.54	.835	7.14	245.599	393.650	45 x 10 <sup>-4</sup>
2	1.57	.790	1.20	268.973		2.3 x 10 <sup>-4</sup>
3	0.40	1.110	0.40	248.080		8.4 x 10 <sup>-5</sup>
4 Blank	< 0.40	.830	< 0.73			

$Q_{me} = 2.5 \times 10^{-4}$   
 $= 3.2 \times 10^{-7}$

$$\begin{aligned}
 \text{lb/hr} &= \frac{\text{ug sample} \times 10^{-6} \text{ gram}}{\text{ug}} \times \frac{1 \text{ lb}}{453.59 \text{ gram}} \times \frac{\text{DSCFM ft}^3}{\text{min}} \times \frac{60 \text{ min}}{\text{hr}} \\
 &= \frac{\text{ug}}{\text{DSCF (ft}^3)} \times \frac{393.650 \times 10^{-6} \times 60}{453.59} \\
 &= 0.417 \frac{\text{ug}}{\text{DSCF}}
 \end{aligned}$$

A. Field Data Summary

This form is required for Kern County use. Other forms may be used to present the data on the following pages.

ARSENIC

Station KREE MS 588 UNIT YHNSG

Run # 1 ✓ 3

Vlc	- Volume of water collected, ml	<u>419.90</u>	<u>465.70</u>	<u>414.5</u>
Vm	- Gas volume, meter cond., dcf	<u>755.25</u>	<u>784.25</u>	<u>761.977</u>
Y	- Meter calibration factor	<u>0.97</u>	<u>0.97</u>	<u>0.97</u>
Pbar	- Barometric pressure, in Hg.	<u>29.44</u>	<u>29.44</u>	<u>29.44</u>
Pg	- Stack static pressure, in H2O	<u>0.10</u>	<u>0.10</u>	<u>0.10</u>
ΔH	- Avg meter press. diff., in H2O	<u>4.10</u>	<u>4.80</u>	<u>4.50</u>
Tm	- Absolute meter temperature, °R	<u>521</u>	<u>531</u>	<u>520</u>
Vm(std)	- Standard sample gas vol, dscf	<u>745.599</u>	<u>768.973</u>	<u>748.050</u>
Bws	- Water vapor part in gas stream	<u>7.4</u>	<u>7.4</u>	<u>7.5</u>
CO2	- Dry concentration, volume %	<u>4.7</u>	<u>4.7</u>	<u>4.7</u>
O2	- Dry concentration, volume %	<u>14.4</u>	<u>14.4</u>	<u>14.4</u>
Md	- Mol wt stack gas, dry, g/gmole	<u>29.32</u>	<u>29.32</u>	<u>29.32</u>
Ms	- Mol wt stack gas, wet, g/gmole	<u>28.48</u>	<u>28.48</u>	<u>28.50</u>
Cp	- Pitot tube coeff., dimensionless	<u>0.84</u>	<u>0.84</u>	<u>0.84</u>
Δp	- Avg of square roots of each Ap	<u>1.30</u>	<u>1.43</u>	<u>1.41</u>
Ts	- Absolute stack temperature, °R	<u>755</u>	<u>763</u>	<u>750</u>
A	- Area of stack, square feet	<u>153.02</u>	<u>153.02</u>	<u>153.02</u>
Qstd	- Volumetric flowrate, dscfm	<u>510.539</u>	<u>558.251</u>	<u>554.129</u>
An	- Area of nozzle, square feet	<u>3.12 × 10<sup>-4</sup></u>	<u>3.12 × 10<sup>-4</sup></u>	<u>3.12 × 10<sup>-4</sup></u>
t	- Sampling time, minutes	<u>240</u>	<u>240</u>	<u>240</u>
I	- Isokinetic variation, percent	<u>98.5</u>	<u>98.6</u>	<u>91.6</u>

KACE MS788

Aerosol  $\mu\text{g}/\text{ft}^3 \times \text{ft}^3 = \mu\text{g sample}$

$$16/\text{hr} = \frac{\mu\text{g} \times 10^{-3} \text{ ng}/\mu\text{g}}{\text{PSCF}(\text{ft}^3)} \times \frac{\text{ft}^3}{152.19 \text{ gram} \times 10^3 \frac{\text{ng}}{\text{gram}}} \times \frac{\text{ft}^3}{\text{min}} \times \frac{60 \text{ min}}{\text{hr}}$$

$$\text{PSCF} = \frac{\mu\text{g}}{\text{PSCF}}$$

900/20 = 45 (avg) = 2000

Aerosol	PSCF	$\mu\text{g}/\text{ft}^3$	$\text{ft}^3$	$\mu\text{g}$	$\text{ft}^3/\text{hr}$
1	0.12	1.0	100	100	100
2	0.15	1.0	100	150	100
3	0.18	1.0	100	180	100
4	0.20	1.0	100	200	100

↓  
 PSCF values  
 0.12  
 0.15  
 0.18  
 0.20



# Proc Chloride

2/3 UIC

NaCl	2000	@ 100	ml	< 1 mg/l
NaCl	2000	@ 100	ml	1.7 mg/l
NaCl	2000	@ 100	ml	1.7 mg/l
NaCl	2000	@ 100	ml	1.6 mg/l

mg	lb/h
1.7	0.43
1.65	0.37
1.6	0.4

$$1.5 \frac{lb}{h} = \frac{1.5 \times 60 \text{ min}}{60 \text{ min}} \times \frac{1.7 \text{ mg}}{1 \text{ min}} \times \frac{60 \text{ min}}{h}$$

A	A	A	A
179.24	240.14	186.02	240.87
177.24	234.09	187.99	337.070
185.15	241.91	189.90	344.94 ✓

Formaldehyde

Blank	Conc	Vol	mg
	< 0.1	@ 100 ul	
Run 1	0.15	195 ul	0.03
2	0.15	190 ul	0.03
3	0.10	210 ul	0.02



0.32 1/4



RR-f

Trace Elements in ug

9/26/01	A	B	C = 10 ml	D = 0.1 ml	=	Total ug
As	ND	ND	ND	0.00	=	4.7 ✓
Ba	ND	ND	ND	ND	=	ND < 0.00
Cd	ND	ND	ND	ND	=	ND < 0.15
Co	ND	ND	ND	ND	=	0.11
Cu	ND	ND	ND	90.2	=	90.2 (11)
Cr	ND	ND	ND	18.4	=	18.4
Hg	ND	ND	ND	ND	=	0.07
Mn	ND	ND	ND	20.2	=	20.2
Ni	ND	ND	ND	49.6	=	49.6
Pb	ND	ND	ND	12.9	=	12.9
Se	ND	ND	ND	ND	=	ND < 0.4
Zn	ND	ND	ND	24.8	=	24.8

where 49.6, 12.9, 24.8, 18.4, 20.2, 90.2, 4.7 are not extracted out values are abnormal

where A = 100 ug for white filter  
 B = 100 ug for white filter  
 C = 100 ug for white filter  
 D = 100 ug for white filter

1/1 4/26/01 49.6 ug/g 12.9 ug/g 24.8 ug/g 18.4 ug/g 20.2 ug/g 90.2 ug/g 4.7 ug/g

16/11 - 13/11/2007 ug  
DSCFM

12/11/07  
13/11/07  
14/11/07  
15/11/07  
16/11/07  
17/11/07  
18/11/07  
19/11/07  
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29/11/07  
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31/11/07

f ucrs

not reported

12/11/07  
13/11/07  
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15/11/07  
16/11/07  
17/11/07  
18/11/07  
19/11/07  
20/11/07  
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28/11/07  
29/11/07  
30/11/07  
31/11/07



900Y0V

900Y03

Hand eye / 16/16

Hand eye / 16/16

A.S. 1000  
B. 1000  
C. 1000

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1000  
1000

WCAS

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~~PRINT~~

3-23-KR

KRCC FUEL OIL

lb/hr emissions  $\rightarrow$  lb/MMBTU

$$\text{Fuel Consumption Ave} = \frac{11.21 + 11.26 + 11.29}{3} = 11.25 \text{ lbs/sec}$$

$$\text{Gross Calorific Value} = 19440 \text{ BTU/lb fuel.}$$

$$\therefore \approx 11.25 \frac{\text{lbs fuel}}{\text{sec}} \times \frac{3600 \text{ sec}}{\text{hr}} \times 19440 \frac{\text{BTU}}{\text{lb fuel}} \times \frac{\text{MMBTU}}{10^6 \text{ BTU}}$$

$$\approx 787.32 \text{ MMBTU/hr.}$$

$\therefore \rightarrow$  From KRCC tables for any element or parameter w/ lb/hr value divide the average value:

$$= \frac{\text{lbs/hr Element}}{\text{MMBTU/hr}}$$

$$= \text{lbs Element/MMBTU}$$

$\leftarrow$  Add new column.

$\downarrow$   
Since no process data = inspection of real time

Example Table 6

$$\text{Arsenic} \approx \frac{9.57 \times 10^{-4} \text{ lb/hr}}{787.32 \text{ MMBTU/hr}}$$

$$= 1.22 \times 10^{-6}$$

KRCC AB 1588

Table 4

lb/hr computation;

DSCFM = ~~427~~ / 133 ft<sup>3</sup>/min ave

TDF = 557 picogram/sample

#/hr =  $\frac{\text{mg} \cdot 10^{-9} \frac{\text{mg}}{\text{mg}}}{\text{ft}^3 \times 0.078317 \frac{\text{m}^3}{\text{ft}^3}} \times \frac{23.69}{\text{MW}} \times 1.58 \times 10^{-7} \text{ MW} \cdot Q$

=  $\frac{\text{picogram}}{\text{ft}^3} \times Q \cdot \frac{10^{-9} \times 23.69 \times 1.58 \times 10^{-7}}{0.078317}$

=  $1.786 \times 10^{-13} \frac{\text{picogram}}{\text{ft}^3} \cdot Q$

- 1 milligram
- 10<sup>-3</sup> microgram
- 10<sup>-6</sup> nanogram
- 10<sup>-9</sup> picogram

A. Field Data Summary

This form is required for Kern County use. Other forms may be used to present the data on the following pages.

CHROMIUM+6

HCL

	Station	142CC	ABX88	UNIT 2 HRSG
	Run #	1	✓	3
Vlc	- Volume of water collected, ml	313.1	297.7	299.3
Vm	- Gas volume, meter cond., dcf	184.674	176.514	172.677
Y	- Meter calibration factor	0.99	1.04	1.04
Pbar	- Barometric pressure, in Hg.	29.44	29.44	29.44
Pg	- Stack static pressure, in H2O	0.08	0.08	0.08
ΔH	- Avg meter press. diff., in H2O	1.80	1.80	1.80
Ta	- Absolute meter temperature, °R	524	520	520
Vm(std)	- Standard sample gas vol, dscf	178.64✓	178.079	177.497
Bws	- Water vapor part in gas stream	7.5	7.✓	7.3
CO2	- Dry concentration, volume %	4.7	4.7	4.7
O2	- Dry concentration, volume %	14.4	14.4	14.4
Md	- Mol wt stack gas, dry, g/gmole	29.3✓	29.3✓	29.3✓
Ms	- Mol wt stack gas, wet, g/gmole	28.47	28.50	28.49
Cp	- Pitot tube coeff., dimensionless	0.84	0.84	0.84
Δp	- Avg of square roots of each Ap	0.88	0.84	0.87
Ts	- Absolute stack temperature, °R	756	760	755
A	- Area of stack, square feet	153.0✓	153.0✓	153.0✓
Qstd	- Volumetric flowrate, dscfm	344.837	337.070	341.92✓
An	- Area of nozzle, square feet	3.41 × 10 <sup>-4</sup>	3.41 × 10 <sup>-4</sup>	3.41 × 10 <sup>-4</sup>
e	- Sampling time, minutes	240	240	240
I	- Isokinetic variation, percent	96.9	98.8	93.2✓

A. Field Data Summary

This form is required for Kern County use. Other forms may be used to present the data on the following pages.

		TRACE		
		KRCE	AS X88	UNIT 7 HR5G
		Station	1	2
		Run #	1	2
Vlc	- Volume of water collected, ml		254.6	279.7
Vm	- Gas volume, meter cond., dcf		160.980	170.073
Y	- Meter calibration factor		1.04	0.99
Pbar	- Barometric pressure, in Hg.		29.44	29.44
Pg	- Stack static pressure, in H2O		0.05	0.05
ΔH	- Avg meter press. diff., in H2O		1.48	1.50
Tm	- Absolute meter temperature, °R		516	523
Vm(std)	- Standard sample gas vol, dscf		106.674	115.501
Bws	- Water vapor part in gas stream		6.6	7.5
CO2	- Dry concentration, volume %		4.7	4.7
O2	- Dry concentration, volume %		14.4	14.4
Md	- Mol wt stack gas, dry, g/gmole		29.32	29.32
Ms	- Mol wt stack gas, wet, g/gmole		28.57	28.44
Cp	- Pitot tube coeff., dimensionless		0.84	0.84
Ap	- Avg of square roots of each Ap		0.78	0.82
Ts	- Absolute stack temperature, °R		755	755
A	- Area of stack, square feet		153.02	153.02
Qstd	- Volumetric flowrate, dscfm		308.274	321.479
An	- Area of nozzle, square feet		$3.27 \times 10^{-4}$	$3.27 \times 10^{-4}$
e	- Sampling time, minutes		240	240
I	- Isokinetic variation, percent		105.3	96.4

A. Field Data Summary

This form is required for Kern County use. Other forms may be used to present the data on the following pages.

		DIOXINS		
		KRCC	MBV588	UNIT 2 HRSG
		1	2	3
		Run #		
V1c	- Volume of water collected, ml	<u>289.0</u> ✓	<u>295.4</u> ✓	<u>146.90</u> ✓
Vm	- Gas volume, meter cond., dcf	<u>173.407</u> ✓	<u>158.887</u> ✓	<u>156.167</u> ✓
Y	- Meter calibration factor	<u>1.01</u> ✓	<u>1.01</u> ✓	<u>1.01</u> ✓
Pbar	- Barometric pressure, in Hg.	<u>29.44</u> ✓	<u>29.44</u> ✓	<u>29.44</u> ✓
Pg	- Stack static pressure, in H2O	<u>0.08</u> ✓	<u>0.08</u> ✓	<u>0.08</u> ✓
ΔH	- Avg meter press. diff., in H2O	<u>1.75</u> ✓	<u>1.20</u> ✓	<u>1.20</u> ✓
Tm	- Absolute meter temperature, °R	<u>521</u> ✓	<u>522</u> ✓	<u>526</u> ✓
Vm(std)	- Standard sample gas vol, dscf	<u>171.75</u> ✓	<u>154.84</u> ✓	<u>151.054</u> ✓
Bws	- Water vapor part in gas stream	<u>7.2</u> ✓	<u>8.2</u> ✓	<u>4.9</u> ✓
CO2	- Dry concentration, volume %	<u>4.7</u> ✓	<u>4.7</u> ✓	<u>4.7</u> ✓
O2	- Dry concentration, volume %	<u>14.4</u> ✓	<u>14.4</u> ✓	<u>14.4</u> ✓
Md	- Mol wt stack gas, dry, g/gmole	<u>29.32</u> ✓	<u>29.32</u> ✓	<u>29.32</u> ✓
Ms	- Mol wt stack gas, wet, g/gmole	<u>28.50</u> ✓	<u>28.39</u> ✓	<u>28.77</u> ✓
Cp	- Pitot tube coeff., dimensionless	<u>0.82</u> ✓	<u>0.82</u> ✓	<u>0.82</u> ✓
Ap	- Avg of square roots of each Ap	<u>1.05</u> ✓	<u>1.20</u> ✓	<u>1.20</u> ✓
Ts	- Absolute stack temperature, °R	<u>763</u> ✓	<u>761</u> ✓	<u>756</u> ✓
A	- Area of stack, square feet	<u>153.62</u> ✓	<u>153.62</u> ✓	<u>153.62</u> ✓
Qstd	- Volumetric flowrate, dscfm	<u>210.71</u> ✓	<u>204.994</u> ✓	<u>221.317</u> ✓
An	- Area of nozzle, square feet	<u>2.76 x 10<sup>-4</sup></u> ✓	<u>1.92 x 10<sup>-4</sup></u> ✓	<u>1.92 x 10<sup>-4</sup></u> ✓
e	- Sampling time, minutes	<u>240</u> ✓	<u>240</u> ✓	<u>240</u> ✓
I	- Isokinetic variation, percent	<u>97.1</u> ✓	<u>101.4</u> ✓	<u>96.0</u> ✓

**Appendix E**  
**Quality Assurance Data**

ENGINEERING SCIENCE, INC.  
75 W. Fair Oaks Ave.  
Pasadena, California  
(818) 440-6000

CHAIN OF CUSTODY RECORD

Paul Pang Du Air Filter

Project No.	Project Name	Project Manager	ANALYSIS REQUIRED				SENT TO: TMA-ARLI
WAB889	KRCC	DPB	As	Pb	Cd	Hg	SHIPPED VIA:
Samples Collected By:			Phone:				SHIPPED BY:
ES Lab No.	Test Date	Sample Description (Container, Media, Volume, etc.)	As	Pb	Cd	Hg	Remarks
900201-A		1/2 Air Filter, Run 1	✓				
900201-B		1/2 Air Filter, Run 1	✓				
900201-C		K Mn O4 Solution, Run 1	✓				
900201-D		HNO3/H2O2 Solution, Run 1	✓				
900202-A		1/2 Air Filter, Run 2	✓				
900202-B		1/2 Air Filter, Run 2	✓				
900202-C		K Mn O4 Solution, Run 2	✓				
900202-D		HNO3/H2O2 Solution, Run 2	✓				
900203-A		1/2 Air Filter, Run 3	✓				
900203-B		1/2 Air Filter, Run 3	✓				
Relinquished by:	Date/Time	Received by:	Reason for Exchange:				Comments:
James D. ... Phone: (818) 440-6000	2-2-90 12:05	DPB	Relinquished				
Relinquished by:	Date/Time	Received by:	Reason for Exchange:				Comments:
La ... Phone:	2-7-90 11:00	DPB	Relinquished				
Relinquished by:	Date/Time	Received by:	Reason for Exchange:				Comments:
Phone:			Relinquished				
Relinquished by:	Date/Time	Received by:	Reason for Exchange:				Comments:
Phone:			Relinquished				

All Metals = Be, Cd, Ni, As, Cu, Pb, Mn, Hg, Cr, P, Se, Zn, Ni



ENGINEERING SCIENCE, INC.  
 75 N. Fair Oaks Av.  
 Pasadena, California  
 (818) 440-6000

CHAIN OF CUSTODY RECORD

Use The Pass Page On Air Filters

Project No. WPA087		Project Name KRCC		Project Manager DPB		ANALYSIS REQUIRED				SENT TO: TMA-ARLI		
Samples Collected By:						AS	AS	AS	AS	AS	AS	SHIPPED VIA:
Test Date						SH	SH	SH	SH	SH	SH	SHIPPED BY:
ES Lab No.	Test Date	Sample Description (Container, Media, Volume, etc.)				Remarks						
900203-C		KMnO4 Solution, Run 3										
900203-D		HNO3/H2O2 Solution, Run 3										
900204-A		K2Cr2O7 Filter, Blank										
900204-B		K2Cr2O7 Filter, Blank										
900204-C		KMnO4, Blank										
900204-D		HNO3/H2O2, Blank										
900170		Carb. 423 Train										
900171		" " "										
900172		" " "										
900173		" " "										
Relinquished by:		Date/Time		Received by:		Reason for Exchange:		Comments:				
Zhang (616) 440-6014		2-2-90		J. DeLuca		Delivery		Comments: If questions call Kamiro 440-6014 or Shanley 440-6161				
Relinquished by:		Date/Time		Received by:		Reason for Exchange:		Comments:				
DeLuca		2-7-90		Bob TMA		TMA		Comments:				
Relinquished by:		Date/Time		Received by:		Reason for Exchange:		Comments:				
Phone:		Date/Time		Received by:		Reason for Exchange:		Comments:				
Relinquished by:		Date/Time		Received by:		Reason for Exchange:		Comments:				
Phone:		Date/Time		Received by:		Reason for Exchange:		Comments:				

\* All Metals Be, Cd, Ni, As, Cu, Pb, Mn, Hg, Cr, P, Se, Zn, Ni

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Pasadena, California  
(818) 440-6000

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CHAIN OF CUSTODY RECORD

Project No.	Project Name		Project Manager	SENT TO:
	KRCC Toxic Hot Spots			
90152	1-25-90	1 lb glass of fuel oil sample.	DENNIS BEJAR	
ES Lab No.	Test Date	Sample Description (Container, Media, Volume, etc.)	Phone:	Remarks

ES Lab No.	Test Date	Sample Description	ANALYSIS REQUIRED		Reason for Exchange:	Comments:
			**Metals**	Slide		
			Metals	Slide		
			Metals	Slide		
			Metals	Slide		
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			Metals	Slide		
			Metals	Slide		
			Metals	Slide		

Relinquished by:	Date/Time	Received by:	Reason for Exchange:	Comments:
H. Damiana Phone: (619) 440-6054	1/29/90 0800 hrs	S. Ruby Of: ES	To TMA North	* Ship 700ml of fuel oil to Dr. Karsten at Nevada for analysis.
Shirley Ruby Phone: 440-6161	1/29/90 1:34 PM	Robert McKREX Of:	To TMA North	Comments: Rush analysis of Oncoy A Spec. It was Bette and Summer.
Relinquished by:	Date/Time	Received by:	Reason for Exchange:	Comments:
Phone:		Of:		
Relinquished by:	Date/Time	Received by:	Reason for Exchange:	Comments:
Phone:		Of:		

\* 588 Metals: Pb, Cd, Cr, Cu, Be, Hg, As, Mn, Ni, Zn, Se

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CHAIN OF CUSTODY RECORD

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Project No.		Project Name		Project Manager		ANALYSIS REQUIRED					SENT TO:	
Samples Collected By:		KRCR HUT STAFF		DJB							SHIPPED VIA: RUSH	
Phone:		PACOUR & CREW		Phone:							SHIPPED BY:	
ES Lab No.	Test Date	Sample Description (Container, Media, Volume, etc.)	✓	✓	✓	✓	✓	✓	✓	✓	✓	Remarks
	1-15-90	900148 @ 1000 ml	✓	✓	✓	✓	✓	✓	✓	✓	✓	C/O WCA-S
		900149 @ 1000 ml	✓	✓	✓	✓	✓	✓	✓	✓	✓	MESSRS. PWS OUSON
		900150 @ 850 ml	✓	✓	✓	✓	✓	✓	✓	✓	✓	JACIK WASHINGTON
		900151 @ 1000 ml	✓	✓	✓	✓	✓	✓	✓	✓	✓	Chridge - ion chromatography
												Or - with PWS
		4 Samples										Total Cr
		Total Cr										Total Cr
		Total Cr										c/o P. RUSKIUO
												S. KIRBY
												D. REEVES
Relinquished by:		Date/Time		Received by:		Reason for Exchange:		Comments:				
Phone:		1-29-90		Senior D. Kambhata		DELIVERY						
Relinquished by:		Date/Time		Received by:		Reason for Exchange:		Comments:				
Phone:				Mary Caldwell		ANALYSIS		8:45 A.M. / 1-29-90		14701		
Relinquished by:		Date/Time		Received by:		Reason for Exchange:		Comments:				
Phone:												
Relinquished by:		Date/Time		Received by:		Reason for Exchange:		Comments:				
Phone:												

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CHAIN OF CUSTODY RECORD

Project No.	Project Name	Project Manager	ANALYSIS REQUIRED						SENT TO: ARLI	SHIPPED VIA: CAR		
			Phenol	Nitrobenzene	Xylene	Toluene	Benzene	Remarks				
WA005	KRC	H. Deranda										
Samples Collected By: Phone:												
ES Lab No.	Test Date	Sample Description (Container, Media, Volume, etc.)	Phenol	Nitrobenzene	Xylene	Toluene	Benzene					
900/59	1/25/90	Turbine # 2 Stack outlet sample	✓	✓	✓	✓	✓					
900/60	1/25/90	" # 2 " outlet sample	✓	✓	✓	✓	✓					
900/61	1/25/90	" # 2 " outlet sample	✓	✓	✓	✓	✓					
Relinquished by: H. Deranda Phone: (818) 440-6054			Date/Time 1/30/90 0930			Received by: <i>Steven D. Kalkreuth</i> Of: E S				Reason for Exchange: Delivery to Lab		
Relinquished by:			Date/Time			Received by:				Reason for Exchange:		
Phone:						Of:				Comments:		
Relinquished by:			Date/Time			Received by:				Reason for Exchange:		
Phone:						Of:				Comments:		
Relinquished by: <i>Steven D. Kalkreuth</i> Phone: 440 6211			Date/Time 1-30-90 10:15 AM			Received by: <i>Brian Davis</i> Of: TMA				Reason for Exchange: Analysis		

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**POST-TEST METER BOX  
CALIBRATION WORKSHEET**

Meter Box No. BLUE # 1 Date 2-12-90 Box Operator sk

Barometric Pressure (P<sub>b</sub>) 29.25 Ambient Temp 61 Published Y<sub>1</sub> 0.9738

Project No. WA005 H Run 4.0 Vacuum Run 17" Calibration Operator Init. sk  
KRCC

Run#		V <sub>w</sub> (ft <sup>3</sup> )	V <sub>a</sub> (ft <sup>3</sup> )	T <sub>w</sub> (°F)	T <sub>a</sub> (°F)	T <sub>1</sub> (min.)	Y <sub>1</sub> (each)
01	Initial	497.253	453.645	61	70	7.43	
	Final	509.782	466.596	61	70	7.54	0.9743
	Net	12529	12951	61	70	7.55	
02	Initial	509.782	466.596	61	70	7.56	
	Final	526.175	483.570	61	75	8.10	0.9819
	Net	16.393	16.974	61	75	8.11	
03	Initial	526.175	483.570	61	75	8.12	
	Final	539.877	498.084	61	78	8.23	0.9652
	Net	13.702	14.514	61	78	8.24	
		<b>FINAL LEAK CHECK</b>		<b>FINAL METER READING</b>		<b>Y<sub>1</sub> AVERAGE</b>	
		<u>26 " ,005</u> "Hg CFM		498.084		0.9738	

**METER BOX CALIBRATION HISTORY**

Date Last Calibration 9-6-89

Calibrated by A. GARVER

H of Calibration @ 2.00

Y<sub>1</sub> of Calibration 0.97

**ENGINEERING SCIENCE**  
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**POST-TEST METER BOX  
CALIBRATION WORKSHEET**

Meter Box No. BU# 2 Date 2-2-90 Box Operator SK

Barometric Pressure (P<sub>b</sub>) 29.32 Ambient Temp 62 Published Y<sub>1</sub> 0.9857

Project No. WA 005 H Run 2.8 Vacuum Run 10 Calibration Operator Init. SK  
K ACC

Run#		V <sub>w</sub> (ft <sup>3</sup> )	V <sub>a</sub> (ft <sup>3</sup> )	T <sub>w</sub> (°F)	T <sub>a</sub> (°F)	T <sub>1</sub> (min.)	Y <sub>1</sub> (each)
01	Initial	343.555	865.286	55	60	9.20	
	Final	354.192	875.880	55	60	9.32	1.0067
	Net	10.637	10.594	55	60	9.33	
02	Initial	354.192	875.880	55	60	9.34	
	Final	364.813	886.722	55	60	9.45	0.9822
	Net	10.621	10.842	55	60	9.46	
03	Initial	364.813	886.722	55	60	9.47	
	Final	375.046	897.360	55	62	10.00	0.9682
	Net	10.233	10.638	55	62	10.01	
<b>FINAL LEAK CHECK</b>				<b>FINAL METER READING</b>		<b>Y<sub>1</sub> AVERAGE</b>	
<u>27</u> " <u>600</u> "Hg CFM				<u>1.001</u>		<u>0.9857</u>	

**METER BOX CALIBRATION HISTORY**

Date Last Calibration 10-12-89

Calibrated by SK

H of Calibration @ 1.920

Y<sub>1</sub> of Calibration 1.001

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**POST-TEST METER BOX  
CALIBRATION WORKSHEET**

Meter Box No. BUE#3 Date 2-2-98 Box Operator SK

Barometric Pressure (P<sub>b</sub>) 29.32 Ambient Temp 68 Published Y<sub>1</sub> 1.0259

Project No. WA005 H Run 4.2 Vacuum Run 17 Calibration Operator Init. SK  
KRCC

Run#		V <sub>w</sub> (ft <sup>3</sup> )	V <sub>v</sub> (ft <sup>3</sup> )	T <sub>w</sub> (°F)	T <sub>v</sub> (°F)	T <sub>1</sub> (min.)	Y <sub>1</sub> (each)
01	Initial	305.874	981.128	59	65	8.33	
	Final	319.190	994.360	59	65	8.43	1.0074
	Net	13.316	13.232	59	65	8.44	
02	Initial	319.190	994.360	59	65	8.45	
	Final	330.380	005.296	60	68	8.53	1.0281
	Net	11.190	10.936	60	68	8.54	
03	Initial	330.380	005.296	60	68	8.55	
	Final	343.555	017.948	62	68	9.05	1.0423
	Net	13.175	12.652	62	68	9.06	
		<b>FINAL LEAK CHECK</b>		<b>FINAL METER READING</b>		<b>Y<sub>1</sub> AVERAGE</b>	
		<u>27</u> "Hg	<u>1.002</u> CM	<u>017.948</u>		<u>1.0259</u>	

**METER BOX CALIBRATION HISTORY**

Date Last Calibration 10-17-89

Calibrated by A. GARVER

H of Calibration @ 1.749

Y<sub>1</sub> of Calibration 1.036

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**POST-TEST METER BOX  
CALIBRATION WORKSHEET**

Meter Box No. YELLOW #1 Date 2-9-90 Box Operator sk

Barometric Pressure (P<sub>b</sub>) 29.44 Ambient Temp 60 Published Y<sub>i</sub> 1.0301

Project No. WA 005 H Run 4.0 Vacuum Run 15" Calibration Operator Init. sk  
KRCC

Run#		V <sub>w</sub> (ft <sup>3</sup> )	V <sub>a</sub> (ft <sup>3</sup> )	T <sub>w</sub> (°F)	T <sub>a</sub> (°F)	T <sub>i</sub> (min.)	Y <sub>i</sub> (each)
01	Initial	162.040	305.690	60	70	11.07	
	Final	473.577	317.964	60	70	11.17	0.9486
	Net	11.537	12.274	60	70	11.18	
02	Initial	473.577	317.964	60	70	11.19	
	Final	485.910	329.360	60	73	11.28	1.0983
	Net	12.333	11.396	60	73	11.29	
03	Initial	485.910	329.360	60	73	11.30	
	Final	497.252	340.432	60	75	11.38	1.0435
	Net	11.342	11.072	60	75	11.39	
<b>FINAL LEAK CHECK</b>				<b>FINAL METER READING</b>		<b>Y<sub>i</sub> AVERAGE</b>	
		<u>25"</u> "Hg	<u>.002</u> CFM	340.432		1.0301	

**METER BOX CALIBRATION HISTORY**

Date Last Calibration 10-17-89

Calibrated by A. GARVER

H of Calibration @ 1.712

Y<sub>i</sub> of Calibration 1.038



**ENGINEERING SCIENCE**  
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**POST-TEST METER BOX  
CALIBRATION WORKSHEET**

Meter Box No. RED #2 Date 2-2-90 Box Operator sk

Barometric Pressure (P<sub>b</sub>) 29.32 Ambient Temp 86 Published Y<sub>1</sub> \_\_\_\_\_

Project No. WMJUS H Run 4.7 Vacuum Run 14 Calibration Operator Init. sk  
KRCE

Run#		V <sub>w</sub> (ft <sup>3</sup> )	V <sub>d</sub> (ft <sup>3</sup> )	T <sub>w</sub> (°F)	T <sub>a</sub> (°F)	T <sub>1</sub> (min.)	Y <sub>1</sub> (each)
01	Initial	265.680	172.433	56	75	7.33	
	Final	278.342	185.064	56	75	7.43	1.0273
	Net	12.662	12.631	56	75	7.44	
02	Initial	278.342	185.064	56	75	7.45	
	Final	294.205	201.236	56	80	7.56	1.0146
	Net	15.863	16.172	56	80	7.57	
03	Initial	294.205	201.236	56	80	7.58	
	Final	305.773	213.168	56	86	8.07	1.0139
	Net	11.568	11.932	56	86	8.08	
		<b>FINAL LEAK CHECK</b>		<b>FINAL METER READING</b>		<b>Y<sub>1</sub> AVERAGE</b>	
		<u>26</u> " "Hg	<u>.003</u> CFM	213.168		1.0186	

**METER BOX CALIBRATION HISTORY**

Date Last Calibration 10-16-89

Calibrated by A. GARUBR

H of Calibration @ 1.629

Y<sub>1</sub> of Calibration 0.9921