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**AB 2588 TOXIC EMISSIONS TEST RESULTS ON
A GAS-FIRED COGENERATION FACILITY**

**DEXZEL COMBINED CYCLE FACILITY
AUTHORITY TO OPERATE PERMIT NO. 488001 (A)**

Prepared for:

DIAMOND (DEXZEL) ENERGY, INC.

**Attn: Mr. Bruce Wertz
633 West Fifth Street, Suite 2800
Los Angeles, California 90071**

Date Submitted:

July 8, 1992


Richard J. Vacherot



Air Measurement Services, Inc.

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July 8, 1992

Mr. Bruce Wertz
Diamond (Dexzel) Energy, Inc.
633 West Fifth Street, Suite 2800
Los Angeles, California 90071

Dear Mr. Wertz:

Please find enclosed three copies of the source test report entitled, "AB 2588 Toxic Emissions Test Results on a Gas-Fired Cogeneration Facility" for submittal to Kern County Air Pollution Control District (KCAPCD).

If you have any questions, please call me at (805) 498-8781.

Sincerely,

HORIZON AIR MEASUREMENT SERVICES, INC.

Richard J. Vacherot
President

RV:lmg

Enclosures

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1. INTRODUCTION

Under the requirements of AB 2588 "Air Toxics 'Hot Spots' Information and Assessment Act of 1987", DEXZEL, INC. is required to conduct an emissions testing program on the combined cycle facility located in Bakersfield, California. The major components of the cogeneration facility include a 29.1 megawatt (MW) natural gas-fired General Electric Model LM-2500 Combustion Gas Turbine Generator (CGTG) with an un-fired Heat Recovery Steam Generator (HRSG).

From May 27 through May 29, 1992, HORIZON AIR MEASUREMENT SERVICES, INC. completed the emissions testing program in accordance with the procedures of the Test Plan which had been approved by Kern County APCD. Mr. Luis Parades observed all testing conducted on May 29, 1992. Testing was conducted at the cogeneration system exhaust stack to quantify concentration and emission rate of the following compounds:

<u>Parameter</u>	<u>Test Method</u>
Flow Rate	CARB Method 1/2 (in conjunction with Method 429)
Moisture	CARB Method 4 (in conjunction with Method 429)
Fixed Gases	CARB Method 3
Acetaldehyde	CARB Method 430
Formaldehyde	CARB Method 430
Acrolein	CARB Method 430
Benzene	CARB Method 410A
Ethyl Benzene	CARB 410A/PID-GC
Propylene	CARB Method 422/FID-GC
Toluene	CARB Method 422/PID-GC
Xylenes	CARB Method 422/PID-GC
Naphthalene	CARB Method 429
Polycyclic Aromatic Hydrocarbons	CARB Method 429
Ammonia	BAAQMD Method ST-1B

Three, replicate test runs were conducted under normal operating conditions for each parameter of interest. In addition to the cogeneration system stack, the headspace of a stock tank and wash tank was quantified for concentration of the following compounds:

<u>Parameter</u>	<u>Test Method</u>
Benzene	CARB Method 410A
Toluene	CARB Method 422/PID-GC
Xylenes	CARB Method 422/PID-GC
Ethyl Benzene	CARB Method 422/PID-GC
Hydrogen Sulfide	EPA Method 11
C ₁ -C ₆ Hydrocarbons	EPA Method 18

Three, replicate test runs were conducted for each parameter of interest at each of one stock/wash tanks. The results of the testing program are summarized in Section 2. Emission source information is provided in Section 3. Section 4 and 5 detail the sampling/analytical and QA/QC procedures, respectively.

2. SUMMARY OF RESULTS

Can not field
blank corrected

2.1 Cogeneration Stack

2.1.1 Speciated VOC's (Benzene, Toluene, Xylene, Ethyl Benzene, Propylene)

Three, replicate 60-minute test runs were completed for benzene, toluene, xylene, ethyl benzene (BTXE) and propylene emissions determination. All three test runs were conducted during the PAH Run #2. The results of the three test runs are provided in Table 2-1. All xylene and ethyl benzene samples were below the detection limit of 0.2 parts per billion, by volume (ppb, v/v). Benzene concentration and emission rate averaged 0.33 ppb and 0.00051 pounds per hour (lb/hr), respectively. The standard deviation between the three test runs, based on concentration, was 0.07 ppb. Toluene concentrations and emission rates averaged 2.74 ppb and 0.0050 lbs/hour, respectively. The standard deviation of the measured concentrations is 0.82 ppb. Propylene concentration and emission rate averaged 2.92 ppb and 0.0024 lbs/hour, respectively. The standard deviation was 0.04 ppb.

No sampling or analytical problems were encountered during VOC testing. All field blank values were below the detection limit with the exception of toluene, which was measured at 0.28 ppb. Reported concentrations and emission rates are not blank corrected.

2.1.2 Aldehydes (Formaldehyde, Acetaldehyde, Acrolein)

The results of the three, replicate 120-minute test runs for aldehyde are provided in Table 2-2. All reported values are field blank corrected. Formaldehyde concentration and emission rate average 11 ppb and 0.0064 lbs/hr, respectively. Formaldehyde concentration standard deviation is 5.5 ppb. The average sample formaldehyde concentration was only 36 percent greater than those of the average field blank. This is less than the desired 5:1 ratio between sample and field blank concentration. This was due to the fact that the observed formaldehyde concentrations (11 ppb average) were well below the target concentration of 1 ppm used for pre-test protocol calculations. All DNPH solutions were pre-test blank-checked within 48 hours of use and all

TABLE 2-1
Summary of Concentration and Emission Rates
Benzene, Toluene, Xylene, Ethyl Benzene and Propylene
Dexzel Corporation
May 28, 1992

	TEST RUN #			
	1	2	3	
Date	5/28/92	5/28/92	5/28/92	
Time	0900-1000	1005-1105	1108-1208	
STACK GAS CHARACTERISTICS				
Temperature (°F)	197	197	197	
Moisture (%)	8.9	8.9	8.9	
Fixed Gases (%)				
O ₂	14.6	14.6	14.6	
CO ₂	3.6	3.6	3.6	
N ₂	81.8	81.8	81.8	
Flow Rate				
dscfm	124,020	124,020	124,020	
acfm	171,508	171,508	171,508	
EMISSIONS				FIELD BLANK
Concentration (ppb)				
Benzene	0.34	0.26	0.40	<0.1
Toluene	3.68	2.17	2.37	0.28
Xylene	<0.2	<0.2	<0.2	<0.2
Propylene	2.83	3.39	2.54	<0.1
Ethyl Benzene	<0.2	<0.2	<0.2	<0.2
Emission Rates (lb/hr)				
Benzene	0.00052	0.00040	0.00061	<0.00015
Toluene	0.0067	0.0039	0.0043	0.00051
Xylene	<0.00041	<0.00041	<0.00041	<0.00021
Propylene	0.0023	0.0028	0.0021	<0.00008
Ethyl Benzene	<0.00041	<0.00041	<0.00041	<0.00021

Note: Values preceded by "<" are below detection limit values.

Note: Values are not blank corrected.

TABLE 2-2
Summary of Concentration and Emission Rates
Aldehydes
Dexzel Corporation
May 27/28, 1992

	TEST RUN #		
	1	2	3
Date	5/27/92	5/28/92	5/28/92
Time	1713-1913	0856-1056	1339-1539
STACK GAS CHARACTERISTICS			
Temperature (°F)	197	197	197
Moisture (%)	7.1	8.8	8.0
Fixed Gases (%)			
O ₂	14.6	14.6	14.5
CO ₂	3.6	3.6	3.7
N ₂	81.8	81.8	81.8
Flow Rate			
dscfm	126,843	124,020	122,956
acfm	171,990	171,508	168,551
EMISSIONS			
Concentration (ug/dscf)			
Formaldehyde	0.59	0.20	0.37
Acetaldehyde	1.2	*	*
Acrolein	0.21	0.25	0.32
Concentration (ppb)			
Formaldehyde	17	6	11
Acetaldehyde	24	*	*
Acrolein	3	4	5
Emission Rates (lb/hr)			
Formaldehyde	0.0099	0.0033	0.0061
Acetaldehyde	0.021	*	*
Acrolein	0.004	0.004	0.005

Note: Values preceded by "<" are below detection limit values.

Note: Values are field blank corrected.

* Field blank value exceeded that of the sample.

samples were extracted within one week of collection. The sample spike was within 93.6 percent of its true value.

Two of the three acetaldehyde runs' (Run 2 and 3) sample concentration was below that of the field blank. Run #1 field-blank corrected values were 24 ppb and 0.021 lbs/hr. The sample spike recovery was 108.1 percent.

Acrolein concentration and emission rate averaged 4 ppb and 0.004 lbs/hr, respectively. The acrolein concentration standard deviation was 1 ppb. The average acrolein sample concentration was 8.5 times the average field blank value. Two of the three field blanks were below the detection limit. The sample spike was 100.5 percent of its true value.

2.1.3 Polycyclic Aromatic Hydrocarbons (PAH's)

The results of the three, replicate 180-minute PAH test runs are provided in Table 2-3. All values preceded by "<" were below the detection; reported values are detection limit values. Reported values are not field blank corrected. Blank train values are provided in parenthesis adjacent to the corresponding sample value. All blank train values were below the detection limit with the exception of naphthalene and phenanthrene. No sampling or analytical problems were encountered during the test program.

2.1.4 Ammonia

The results of the three, replicate 60-minute ammonia test runs are provided in Table 2-4. The average ammonia concentration and emission rate was 0.97 ppm and 0.31 lbs/hr, respectively. The concentration standard deviation is 0.24 ppm. No sampling or analytical problems were encountered during the ammonia testing.

Two Runs
Below
Field Blank

TABLE 2-3
Summary of Emission Rates
Polycyclic Aromatic Hydrocarbons
May 27/28, 1992

	RUN #		
	1	2	3
Date	5/27/92	5/28/92	5/28/92
Time	1353-1800	0831-1154	1253-1610
STACK GAS CHARACTERISTICS			
Temperature (°F)	197	197	197
Moisture (%)	7.2	8.9	8.1
Fixed Gases (%)			
O ₂	14.6	14.6	14.5
CO ₂	3.6	3.6	3.7
N ₂	81.8	81.8	81.8
Flow Rate (dscfm)	126,843	124,020	122,956
(acfm)	171,990	171,508	168,551
PAH SPECIES EMISSIONS (mg/hr)			
Naphthalene	258 (170)	179 (157)	190 (155)
Acenaphthylene	<2.7 (<2.7)	2.6 (<2.5)	<2.0 (<2.5)
Acenaphthene	<4.0 (<2.7)	<2.5 (<2.5)	<2.5 (<2.5)
Fluorene	15 (<2.7)	4.3 (<2.5)	6.5 (<2.5)
Phenanthrene	77 (13)	38 (12)	30 (12)
Anthracene	<4.4 (<3.3)	<3.0 (<3.1)	<2.5 (<3.0)
Fluoranthene	10 (<3.3)	7.0 (<3.1)	3.6 (<3.0)
Pyrene	3.7 (<3.3)	4.2 (<3.1)	2.0 (<3.0)
Benz (a) Anthracene	<4.4 (<4.4)	<3.5 (<4.1)	<4.0 (<4.0)
Benz (b) Fluoranthene	<2.2 (<4.4)	<1.5 (<2.0)	<1.5 (<2.0)
Benzo (k) Fluoranthene	<2.2 (<2.2)	<1.5 (<2.0)	<1.5 (<2.0)
Benzo (a) Pyrene	3.0 (<2.2)	<2.0 (<2.0)	<2.0 (<2.0)
Benzo (g,h,i) Perylene	<2.7 (<2.7)	<2.0 (<2.5)	<2.0 (<2.0)
Chrysene	<4.9 (<4.4)	<4.0 (<4.1)	<4.0 (<4.0)
Dibenz (a,h) Anthracene	<4.4 (<4.4)	<4.0 (<4.1)	<4.0 (<4.0)
Indeno (1,2,3-cd) Pyrene	<4.4 (<4.4)	<4.0 (<4.1)	<4.0 (<4.0)

Note: Values preceded by "<" are below the detection limit values.

Note: Blank train values are provided in parenthesis.

TABLE 2-4
Summary of Emission Rates
Ammonia
Dexzel Cogeneration
May 27/28, 1992

	RUN #		
	1	2	3
Date	05/27/92	05/28/92	05/28/92
Time	1748-1848	1100-1200	1445-1545
STACK GAS CHARACTERISTICS			
Temperature (°F)	197	197	197
Moisture (%)	7.2	8.9	8.1
Fixed Gases (%)			
O ₂	14.6	14.6	14.5
CO ₂	3.6	3.6	3.7
N ₂	81.8	81.8	18.8
Flow Rate (dscfm)	126,843	124,020	122,956
(acfm)	171,990	171,508	168,551
AMMONIA EMISSIONS			
Concentration (mg/dscf)	0.014	0.023	0.020
Concentration (ppm)	0.72	1.2	1.0
Emission Rate (lbs/hr)	0.235	0.383	0.319

2.2 Jerry Lee Wash Tank #T-402

The results, on a weight fraction basis, of the Jerry Lee Wash Tank #T-402 testing are provided in Table 2-5. Benzene, xylenes and toluene were all below the detection limit. Toluene concentration averaged 41.4 ppm, v/v or 0.00027 weight fraction of toluene to weight fraction headspace gas (wt/wt). Hydrogen sulfide (H₂S) concentration averaged 7.6 ppm, v/v or 0.000018 wt/wt. Toluene and H₂S concentration standard deviation was 1.6 ppm and 1.9 ppm, respectively. No sampling or analytical problems were encountered during any phase of the testing.

2.3 Ferne Lease Stock Tank #5395

The results, on a weight fraction basis, of the Ferne Lease Wash Tank #5395 are provided in Table 2-5. Xylene and ethylbenzene were below the detection limit for all test runs. Benzene concentration averaged 0.098 ppm, v/v or 5.4×10^{-7} wt/wt. Toluene concentration averaged 54.0 ppm, v/v or 0.00035 wt/wt. Hydrogen sulfide concentration averaged 1.1 ppm, v/v or 2.7×10^{-6} wt/wt. The standard deviation of benzene, toluene and hydrogen sulfide concentration was 0.007 ppb, 54 ppb and 1.1 ppb, respectively. No sampling or analytical problems were encountered during the Ferne Lease Stack Tank testing.

TABLE 2-5

Summary of Pollutant Weight Fractions - Tank Headspace
Jerry Lee Wash Tank #T-402 and Ferne Lease Stock Tank #5395
Dexzel Cogeneration
May 29, 1992

	WEIGHT FRACTION (wt fraction pollutant/wt fraction headspace gas)		
Run #	1	2	3
JERRY LEE WASH TANK #T-402			
Benzene	$< 2.2 \times 10^{-7}$	$< 2.2 \times 10^{-7}$	$< 2.2 \times 10^{-7}$
Toluene	2.7×10^{-4}	2.8×10^{-4}	2.6×10^{-4}
Xylenes	$< 1.3 \times 10^{-6}$	$< 1.3 \times 10^{-6}$	$< 1.3 \times 10^{-6}$
Ethylbenzene	$< 6.0 \times 10^{-7}$	$< 6.0 \times 10^{-7}$	$< 6.0 \times 10^{-7}$
Hydrogen Sulfide	1.8×10^{-5}	1.4×10^{-5}	2.3×10^{-5}
FERNE LEASE STACK TANK #5395			
Benzene	5.2×10^{-7}	5.2×10^{-7}	5.8×10^{-7}
Toluene	3.6×10^{-4}	3.4×10^{-4}	3.5×10^{-4}
Xylenes	$< 1.3 \times 10^{-6}$	$< 1.3 \times 10^{-6}$	$< 1.3 \times 10^{-6}$
Ethylbenzene	$< 6.0 \times 10^{-7}$	$< 6.0 \times 10^{-7}$	$< 6.0 \times 10^{-7}$
Hydrogen Sulfide	3.6×10^{-6}	2.6×10^{-6}	1.9×10^{-6}

3. EMISSION SOURCE INFORMATION

3.1 Facility Description

The facility consists of a single natural gas fired General Electric Model LM-2500 turbine equipped with a 29.1 MW electrical generator located at Dexzel Combined Cycle Facility, Bakersfield, California. The facility controls nitrogen oxides emissions using a Babcock-Hitachi selective catalytic reduction (SCR) control system equipped with water and ammonia injection. The gas turbine is equipped with a heat recovery steam generator (HRSG). The Dexzel Combined Cycle Facility is owned by Dexzel Incorporated and operated by UC Operating Services (UCOS).

3.2 Emissions Source Description

3.2.1 Cogeneration System Stack

The single exhaust stack (95 inches in diameter) sampling location is approximately three diameters (25 feet) downstream of the HRSG entry into the base of the stack and one half diameter upstream (approximately 4 feet) of the stack exit. Twenty-four traverse points were used for velocity determination and PAH sample collection.

3.2.2 Stock Tanks

The stock tanks (3) act as a collection point for crude oil heated to a minimum of 165°F in preparation for shipment to the refinery. There are two "Ferne Lease Stock Tanks", each equipped with vapor recovery. Each tank is 21 feet in diameter by 16 feet high with a fixed roof and contains heating coils.

The "Jerry Lee Lease Stock Tank" is also 21 feet in diameter and 16 feet high with a fixed roof and heating coils. One of the Ferne lease stock tanks' headspace, Tank #5395, was tested.

3.2.3 Wash Tank

The wash tanks act as a gathering point for oil/water separation prior to being stored and heated for shipment. There are two wash tanks at the facility.

One wash tank is a "Ferne Lease Wash Tank" equipped with vapor recovery. This bolted wash tank is 15 feet in diameter by 24 feet high with a fixed roof and contains no heating coils. The second wash is a "Jerry Lee Wash Tank" with no vapor recovery. The bolted wash tank is 21 feet in diameter by 24 feet high with a fixed roof and no heating coil. The Jerry Lee Wash tank, Tank #T-402, headspace was tested.

3.3 Process Data

3.3.1 Cogeneration System

All replicate test runs were conducted as close to normal, maximum rated load as possible during the test period. All other operating parameters were set at "normal" operating values. Table 3-1 provides the operating parameter values which were monitored by Dexzel, Inc. during each test run.

3.3.2 Stock and Wash Tanks

Each of the stock and wash tanks were tested under normal operating conditions. Stock and wash tank levels were noted on each, respective, field data sheet (Appendix C).

TABLE 3-1

System Operating Parameters
Dexzel Cogeneration System
May 27/28, 1992

	TEST RUN #		
	1	2	3
Time	(1353-1800)	(0831-1154)	(1253-1610)
Output, MW	22.2	22.4	22.2
Fuel Flow, scfh	239,543	241,414	243,521
Ammonia Flow, lb/hr	6.16	6.45	5.56
SCR Inlet Temp, °F	725.6	725.8	725.1
SCR Pressure Drop, in H ₂ O	0.6287	0.6254	0.6269
Steam Flow lbs/hr	73,276	73,832	73,953
CTG Water Injection, gpm	16.16	16.28	16.18

Note: Test Run #'s correspond to PAH test run numbers. Aldehyde and ammonia test runs were completed within the corresponding numbered PAH test run. All speciated VOC test runs were conducted during PAH Test Run #2.

4. SOURCE TEST PROCEDURES

The compounds and parameters of interest, the associated test methodology, the number of replicate test runs and test run duration is provided in Table 4-1. The specific sampling/analytical procedures to be utilized for each parameter of interest are detailed in subsequent subsections.

4.1 Polycyclic Aromatic Hydrocarbons (PAH) - CARB Method 429

HORIZON used a sampling train that conformed to CARB Method 429 specifications for PAH determination. Stack gases were withdrawn through a glass buttonhook nozzle and a heated glass lined probe followed by a filter assembly containing a pre weighed glass fiber filter. A thermocouple and pitot tube was connected to the probe per CARB Method 429. The cyclone bypass and filter assembly were maintained at approximately 250 degrees Fahrenheit ($\pm$ 25 degrees Fahrenheit).

Following the filter assembly were three foot 5/8" OD Teflon tube, a water cooled condenser and sorbent module (XAD) followed by three glass impingers. The sorbent module contained approximately 150 grams of pre-cleaned, blank checked XAD-2 resin. The condensing coil and sorbent module were mounted vertically and their temperature maintained at 60 degrees Fahrenheit or less. The first impinger was of the modified design with the exception of having the stem cut to six inches. The second and third impingers were of the modified Greenburg Smith design. The first impinger contained 100 ml of distilled deionized water. The second impinger was empty. The last contained a pre-weighed amount of silica gel. An umbilical cord connected the last impinger to the flow control console containing a leakless, lubricated vane pump, dry gas meter, calibrated orifice, and a 0-5 inch magnahelic gauge.

TABLE 4-1
Compounds/Parameters of Interest
Dexzel, Inc.

PARAMETER	NUMBER OF REPLICATE TESTS PER SOURCE	NOMINAL TEST RUN DURATION (minutes)	TEST METHOD
Flow Rate	3	180	CARB Method 1/2 (in conjunction with Method 429)
Fixed Gases (CO ₂ , O ₂ , CO, N ₂)	3	180	CARB Method 3
Moisture	3	180	CARB Method 4 (in conjunction with Method 429)
Acetaldehyde	3	120	CARB Method 430
Acrolein	3	120	CARB Method 430
Formaldehyde	3	120	CARB Method 430
Benzene	3	60	CARB Method 410
Propylene	3	60	CARB Method 422/FID-GC Analysis
Toluene	3	60	CARB Method 422/PID-GC Analysis
Xylenes	3	60	CARB Method 422/PID-GC Analysis
Ethyl Benzene	3	60	CARB Method 422/PID-GC Analysis
Polycyclic Aromatic Hydrocarbons	3	180	CARB Method 429
Hydrogen Sulfide	3	30 - 60	Modified CARB Method 15
Ammonia	3	60	BAAQMD Method ST-1

A leak check of the pitot tube lines and sampling trains was conducted prior to and after each sampling run and prior to and after either changing any of the constituents of the train or disconnecting the umbilical cord to facilitate transport of the train. Leak checks prior to each sampling run were conducted at 15 inches mercury vacuum to insure a leak rate of no greater than 0.02 cfm. Leak checks at the conclusion of each run were conducted at the highest vacuum reached during that test run.

Upon completion of the sample run, the nozzle, probe, and front half of the filter holder were brushed and rinsed with acetone, hexane, and methylene chloride (sample container #1). The filter was replaced in its original glass petri dish pending analysis. The sorbent module (XAD) was capped off with ground glass fittings, covered with pre-treated aluminum foil and refrigerated pending analysis. The back half of the filter housing, Teflon jumper and the water condenser were subsequently rinsed with acetone, hexane, and methylene chloride into sample container #2. The volume of water collected in the first three impingers were determined volumetrically. The moisture collected in the silica gel in the last impinger was determined gravimetrically with a calibrated balance accurate to 0.1 grams. These two measurements were used to calculate stack gas moisture content as per CARB Method 429. After the impinger #1 contents were collected in Container #3, the impinger was rinsed with acetone, hexane and methylene chloride and added to container #3. After impingers 2 and 3 contents were placed in container #4, the impingers and all connecting glassware was rinsed with distilled, deionized water into container #4.

All sample bottles and filter containers were sealed with Teflon tape and all liquid levels are marked. All sample bottles were amber glass jars with Teflon-lined caps. All samples were kept on ice pending analyses. A blank train was assembled on-site, leak-checked, recovered and analyzed in the exact manner as the samples. Field blanks of all sorbent filters and solutions were obtained and analyzed in the same manner as the samples.

All samples were extracted per CARB Method 429 by Zenon Laboratories. The sample portion extracts were combined, as allowed by CARB, for each sample and analyzed using selective ion low resolution mass spectrometry. All reported emission results are accompanied by the blank train values. Any elevated field blank values are identified and discussed.

4.2 Aldehydes (Formaldehyde, Acrolein, Acetaldehyde) - CARB Method 430

Aldehydes (formaldehyde, acrolein, acetaldehyde) emissions were determined in accordance with CARB Method 430 "Determination of Formaldehyde Emissions from Stationary Sources". In this method stack gas is withdrawn from the stack through a series of midjet impingers containing an aqueous acidic solution of 2,4-dinitrophenyl-hydrazine (DNPH) solution (used within 48 hours of preparation). Aldehydes react with DNPH by nucleophilic addition on the carbonyl followed by 1,2 elimination of water and the formulation of 2,4 dinitrophenyl hydrazone.

HORIZON used a sampling train which conforms to CARB Method 430 specifications. Stack gases were withdrawn from a single traverse point through a heated Teflon probe followed by a Teflon sample line. Following the probe were three glass midjet impingers. The first two impingers contained 10 ml of 0.05% DNPH/2N HCL reagent; the third impinger contained a weighed amount of silica gel.

An umbilical cord was connected between the last impinger and the flow control system. The control system consisted of a calibrated rotometer equipped with a needle valve, an accumulator and a vacuum pump. Prior to and at the conclusion of each test run, the probe inlet flow was measured using a SKC bubble meter to confirm the rotometer setting flow rate, during the test run. The sample flow was maintained at 250 cubic centimeters (cc) per minute throughout the test run as indicated on the rotometer. Rotometer sampling rate was recorded at 10-minute intervals over each 120-minute test run. The impingers were kept on ice during sampling to maintain a sample temperature of less than 60°F at the last impinger.

A leak check of the sampling train was conducted prior to and at the conclusion of each test run by plugging the probe tip and turning on the sampling pump. If the rotometer indicates no flow, the sample system was deemed leak-free. Upon completion of the test run the sample line was rinsed with 2 ml of impinger solution into the first impinger. The sample line was then rinsed with 1 ml of reagent water into the first impinger. The impinger contents were then combined into a leaktight septum vial which was weighed and refrigerated pending analysis.

Prior to field sampling, four reagent blanks of the impinger solution were analyzed to verify anticipated reagent blank levels (reagent blank levels were expected to be 0.8 μg formaldehyde per 10 ml of solution). In addition, three field blanks were carried through all the required steps for sample preparation and analysis. A field blank consists of an impinger and sample line which is similar to a sampling impinger. One matrix spike was also conducted as specified in Method 430. All reported emission values were field blank-corrected.

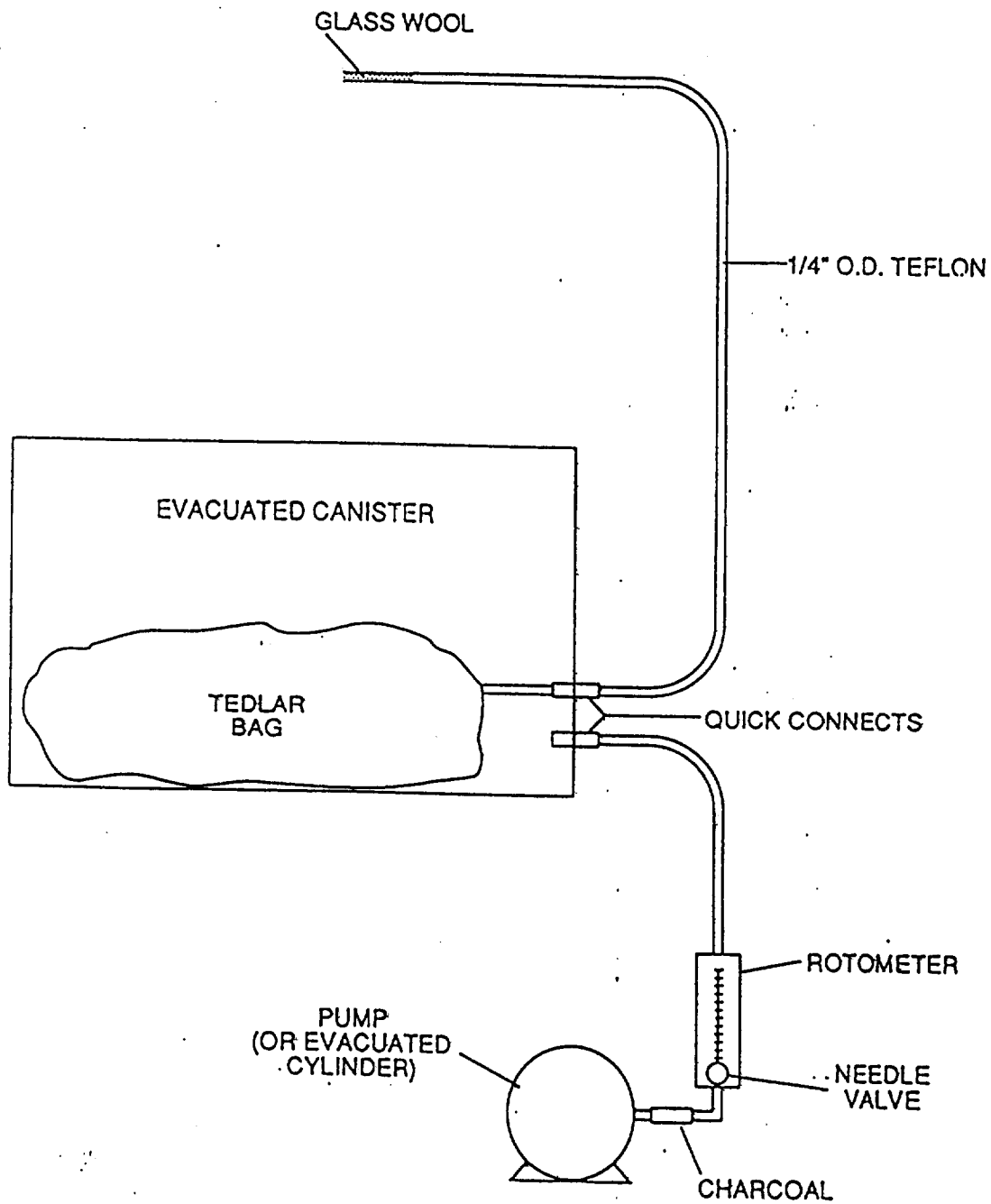
4.3 Benzene - CARB Method 410A

Benzene emissions were determined in accordance with CARB Method 410A entitled "Determination of Benzene from Stationary Sources". A stack gas sample was collected using the Tedlar bag - evacuated canister system as depicted in Figure 4-1.

The evacuated canister ("lung") sampling system is capable of collecting an integrated, representative sample while ensuring sample integrity. The system consisted of a 1/4" O.D. Teflon probe/sample line, containing glass wool to remove particulate, a 10-liter leak-free, non-reactive Tedlar bag contained in a leak-free evacuation drum. All system components coming in contact with sample were constructed of Teflon, glass or stainless steel. The sample was collected by evacuating the canister at a constant rate over the sampling period using a rotometer/needle valve and a vacuum pump.

Prior to each sampling run, the evacuated canister which contains the Tedlar bag was leak checked at 2" Hg vacuum. The sample train upstream of the Tedlar bag was then purged with stack gas. At the conclusion of each test run, each Tedlar bag sample was sealed and stored in an opaque container pending analyses.

All samples were analyzed within 48 hours using gas chromatography in accordance with CARB Method 410 using a gas chromatograph equipped with a photoionization detector. A field blank sample was also collected and analyzed for benzene, propylene, toluene and xylenes.



TEDLAR BAG - EVACUATED CANISTER
SAMPLING SYSTEM

4.4 Propylene

Propylene concentration was determined from the Tedlar bag samples collected for benzene as described in Section 4.3. The sample was analyzed within 48 hours using a gas chromatograph equipped with a flame ionization detector.

4.5 Toluene, Xylenes and Ethyl Benzene

Toluene and xylene samples were collected in accordance with CARB Method 410/422. The Tedlar bag samples collected for benzene/propylene were also analyzed for toluene and xylenes using appropriate photoionization detection/gas chromatographic techniques.

4.6 Fixed Gases (O₂, CO₂, N₂)

Fixed gas determination were conducted in accordance with CARB Method 3. A Tedlar bag sample was collected using the evacuated canister collection system as described in Section 4.3. Subsequent samples were analyzed on-site using an Orsat analyzer for O₂, CO₂ and N₂ concentration.

4.7 Ammonia - BAAQMD Method ST-1B

HORIZON used a sampling train that conformed to BAAQMD Method ST-1B specifications for ammonia determination (Figure 4-2). Stack gases were withdrawn through a stainless steel straight nozzle and a heated glass lined probe followed by a three foot 5/8" O.D. Teflon tube.

Following the Teflon tube was four glass impingers. The first and second impingers were of the modified Greenburg Smith design, containing 100 mls of 0.1 N HCl. The third impinger was empty. The last contained a pre-weighed amount of silica gel. An umbilical cord connected the last impinger to the flow control console containing a leakless, lubricated vane pump, dry gas meter, calibrated orifice, and a dual 0-5 inch H₂O magnahelic gauge.

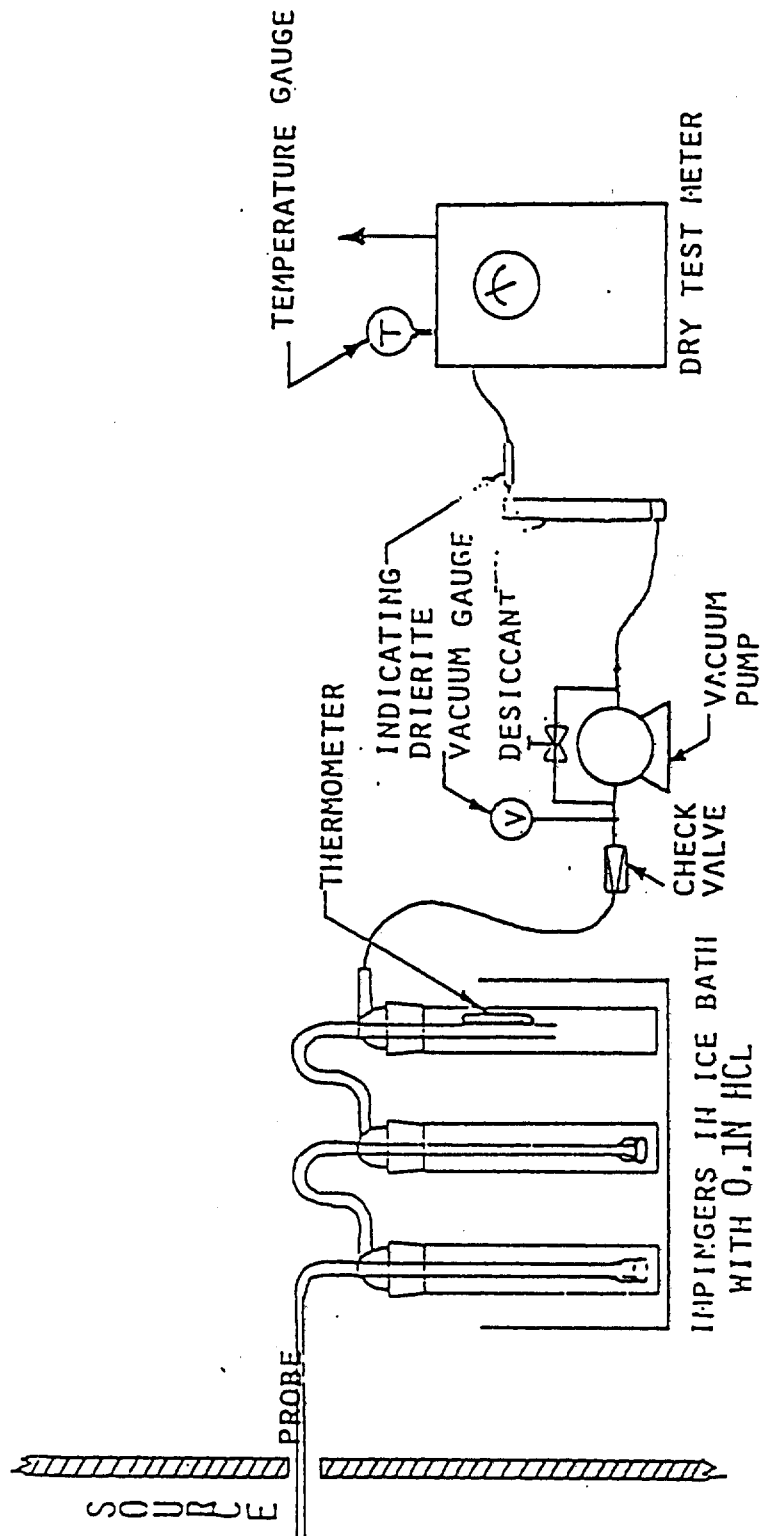


Figure 4-2
AMMONIA SAMPLING TRAIN

A leak check of the pitot tube lines and sampling trains was conducted prior to and after each sampling run and prior to and after either changing any of the constituents of the train or disconnecting the umbilical cord to facilitate transport of the train.

Leak checks prior to each sampling run were conducted at 15 inches mercury vacuum to insure a leak rate of no greater than 0.02 cfm. Leak checks at the conclusion of each run were conducted at the highest vacuum reached during the test run.

Upon completion of the sample run the nozzle was removed. The nozzle and probe were brushed and rinsed with deionized water. The volume of water collected in the first two impingers were determined volumetrically. The moisture collected in the silica gel in the last impinger was determined gravimetrically with a calibrated balance. These two measurements were used to calculate stack gas moisture as per BAAQMD Method ST-1B. The impinger contents were then collected and all connecting glassware and impingers were rinsed with deionized water and placed in the same container.

All sample bottles were sealed with Teflon tape and all liquid levels were marked. All samples were refrigerated pending analyses. The ammonia concentration was determined using BAAQMD Method ST-1 by West Coast Analytical. Field blanks of all solutions were obtained and analyzed in the same manner as the samples.

4.8 Hydrogen Sulfide

Hydrogen sulfide (H_2S) emissions were determined using US EPA Method 11 "Determination of Hydrogen Sulfide Content of Fuel Gas Streams in Petroleum Refineries". In this method, H_2S is collected from the tank headspace in a series of midjet impingers and absorbed in pH 3.0 cadmium sulfate ($CdSO_4$) to form cadmium sulfide (CdS). The latter compound is then measured idiometrically.

The sampling apparatus consisted of a 1/4" OD Teflon probe, a sampling valve, a series of six midjet impingers, a calibrated dry gas meter, a vane pump and a calibrated orifice.

The first impinger contained 15 ml of three percent hydrogen peroxide solution; the second impinger was empty; the third, fourth and fifth impinger each contained 15 ml of cadmium sulfate solution. Glass/quartz wool was placed in the second impinger to remove particulate and H_2O_2 .

mist, respectively. The sixth impinger contained silica gel. A leak check was conducted prior to and at the conclusion of each test run.

The sampling/probe line was purged with tank headspace gas prior to each test run. Sample was collected for 30-minutes at a nominal rate of one liter per minute (lpm) over each test run. At the conclusion of the test run the impinger train was purged with scrubbed ambient air at one lpm for fifteen to twenty minutes. The contents of the third, fourth and fifth impingers was released into a 500 ml iodine flask. Samples were analyzed per Method 11, on site, approximately 30 minutes after collection.

4.9 Speciated Hydrocarbons (C₁-C₇)

Speciated hydrocarbon samples were collected from the tank headspace in accordance with EPA Method 18, using the evacuated canister - Tedlar bag procedure detailed in Section 4.3. Subsequent samples were analyzed for C₁-C₇ hydrocarbon species using GC-FID techniques.

APPENDIX A

Computer Printout of Results

EXCEL COGENERATION
HILDALE, CA

PAH'S

		RUN	RUN	RUN	RUN	RUN
RUN NUMBER	*****	1	2	3	1A	1A
DATE OF RUN	*****	5-27-92	5-28-92	5-28-92	5-27-92	5-27-92
LOCK TIME: INITIAL	*****	1353	831	1253		
LOCK TIME: FINAL	*****	1800	1154	1610		
WG. STACK TEMPERATURE	DEGREES F	196.5	197	197.4	198	195
WG. SQUARE DELTA P	INCHES H2O	0.9247	0.9183	0.9042	0.9032	0.9463
NOZZLE DIAMETER	INCHES	na	0.236	0.236	0.214	0.237
BAROMETRIC PRESSURE	IN. HG.	30.05	30.02	30.05	30.05	30.05
SAMPLING TIME	MIN.	180	180	180	90	90
SAMPLE VOLUME	CUBIC FEET	145.546	156.434	154.338	63.891	81.655
AVG. METER TEMP.	DEGREES F	92	90	90	91	93
WG. DELTA H	IN. H2O	2.05	2.43	2.32	1.53	2.57
3M CALIB. FACTOR [Y]	*****	1.0016	1.0016	1.0016	1.0016	1.0016
WATER COLLECTED	MILLILITERS	229	309	276	101	128
CO 2	PERCENT	3.6	3.6	3.7	3.6	3.6
2	PERCENT	14.6	14.6	14.5	15.6	15.6
CO	PERCENT	0.0	0.0	0.0	0.0	0.0
N 2	PERCENT	81.8	81.8	81.8	80.8	80.8
CK AREA	SQUARE INCHES	7088	7088	7088	7088	7088
STATIC PRESSURE	INCHES WG.	-0.30	-0.30	-0.32	-0.30	-0.30
PITOT COEFFICIENT	*****	0.84	0.84	0.84	0.84	0.84
SAMPLE VOLUME DRY	DSCF	138.64	149.60	147.65	60.88	77.72
WATER AT STD.	SCF	10.8	14.6	13.0	4.7	6.0
MOISTURE	PERCENT	7.2	8.9	8.1	7.2	7.2
MOLE FRACTION DRY GAS	*****	0.93	0.91	0.92	0.93	0.93
MOLECULAR WT. DRY	LB/LB MOLE	29.16	29.16	29.17	29.20	29.20
EXCESS AIR	PERCENT	209	209	204	272	272
MOLECULAR WT. WET	LB/LB MOLE	28.35	28.17	28.27	28.39	28.39
STACK GAS PRESSURE	INCHES HG.	30.03	30.00	30.03	30.03	30.03
STACK VELOCITY	AFPM	3494	3484	3424	3415	3569
VOLUMETRIC FLOWRATE, DRY STD.	DSCFM	126843	124020	122956	123676	129892
VOLUMETRIC FLOWRATE, ACTUAL	ACFM	171990	171508	168551	168072	175685
ISOKINETIC RATIO	PERCENT	ERR	107	106	106	105

DEXZEL

CALCULATIONS FOR GRAIN LOADING AND EMISSION RATES

RUN NUMBER 1
 DATE OF RUN 5-27-92
 CLOCK TIME: INITIAL 1353
 CLOCK TIME: FINAL 1800

RUN 2
 5-28-92
 831
 1154

RUN 3
 5-28-92
 1253
 1610

PAH EMISSION RATES

	WEIGHT (ug)	CONC. (mg/dscf)	EMISSION RATE (mg/hr)	WEIGHT (ug)	CONC. (mg/dscf)	EMISSION RATE (mg/hr)	WEIGHT (ug)	CONC. (mg/dscf)	EMISSION RATE (mg/hr)
NAPHTHALENE	4.700	3.39E-05	258.002	3.600	2.41E-05	179.067	3.800	2.57E-05	189.870
ACENAPHTHYLENE	* 0.050	3.61E-07	2.745	0.052	3.48E-07	2.587 *	0.040	2.71E-07	1.999
ACENAPHTHENE	* 0.072	5.19E-07	3.952 *	0.050	3.34E-07	2.487 *	0.050	3.39E-07	2.498
FLUORENE	0.270	1.95E-06	14.821	0.086	5.75E-07	4.278	0.130	8.80E-07	6.496
PHENANTHRENE	1.400	1.01E-05	76.852	0.760	5.08E-06	37.803	0.600	4.06E-06	29.980
ANTHRACENE	* 0.080	5.77E-07	4.392 *	0.060	4.01E-07	2.984 *	0.050	3.39E-07	2.498
FLUORANTHENE	0.190	1.37E-06	10.430	0.140	9.36E-07	6.964	0.071	4.81E-07	3.548
PYRENE	0.068	4.90E-07	3.733	0.084	5.62E-07	4.178	0.041	2.78E-07	2.049
BENZ(A)ANTHRACENE	* 0.080	5.77E-07	4.392 *	0.070	4.68E-07	3.482 *	0.080	5.42E-07	3.997
CHRYSENE	* 0.090	6.49E-07	4.940 *	0.080	5.35E-07	3.979 *	0.080	5.42E-07	3.997
BENZO(b)FLUORANTHENE	* 0.040	2.89E-07	2.196 *	0.030	2.01E-07	1.492 *	0.030	2.03E-07	1.499
BENZO(k)FLUORANTHENE	* 0.040	2.89E-07	2.196 *	0.030	2.01E-07	1.492 *	0.030	2.03E-07	1.499
BENZO(a)PYRENE	0.055	3.97E-07	3.019 *	0.040	2.67E-07	1.990 *	0.040	2.71E-07	1.999
BENZO(G,H,I)PERYLENE	* 0.050	3.61E-07	2.745 *	0.040	2.67E-07	1.990 *	0.040	2.71E-07	1.999
DIBENZ(A,H)ANTHRACENE	* 0.080	5.77E-07	4.392 *	0.080	5.35E-07	3.979 *	0.080	5.42E-07	3.997
INDENO[1,2,3-cd]PYRENE	* 0.080	5.77E-07	4.392 *	0.080	5.35E-07	3.979 *	0.080	5.42E-07	3.997

* - sample was below the reportable limit.

DEXZEL

CALCULATIONS FOR GRAIN LOADING AND EMISSION RATES

RUN NUMBER *****
 DATE OF RUN *****
 CLOCK TIME: INITIAL *****
 CLOCK TIME: FINAL *****

BLANK TRAINS

RUN 2
 5-28-92
 831
 1154

RUN 3
 5-28-92
 1253
 1610

PAH EMISSION RATES

	WEIGHT (ug)	CONC. (mg/dscf)	EMISSION RATE (mg/hr)	WEIGHT (ug)	CONC. (mg/dscf)	EMISSION RATE (mg/hr)	WEIGHT (ug)	CONC. (mg/dscf)	EMISSION RATE (mg/hr)
NAPHTHALENE	3.100	2.24E-05	170.172	3.100	2.07E-05	157.706	3.100	2.10E-05	154.894
ACENAPHTHYLENE	*	3.61E-07	2.745 *	0.050	3.34E-07	2.544 *	0.050	3.39E-07	2.498
ACENAPHTHENE	*	3.61E-07	2.745 *	0.050	3.34E-07	2.544 *	0.050	3.39E-07	2.498
FLUORENE	*	3.61E-07	2.745 *	0.050	3.34E-07	2.544 *	0.050	3.39E-07	2.498
PHENANTHRENE	0.230	1.66E-06	12.626	0.230	1.54E-06	11.701	0.230	1.56E-06	11.492
ANTHRACENE	0.060	4.33E-07	3.294 *	0.060	4.01E-07	3.052 *	0.060	4.06E-07	2.998
FLUORANTHENE	0.060	4.33E-07	3.294 *	0.060	4.01E-07	3.052 *	0.060	4.06E-07	2.998
PYRENE	0.060	4.33E-07	3.294 *	0.060	4.01E-07	3.052 *	0.060	4.06E-07	2.998
BENZ(A)ANTHRACENE	0.080	5.77E-07	4.392 *	0.080	5.35E-07	4.070 *	0.080	5.42E-07	3.997
CHRYSENE	0.080	5.77E-07	4.392 *	0.080	5.35E-07	4.070 *	0.080	5.42E-07	3.997
BENZO(b)FLUORANTHENE	0.040	2.89E-07	2.196 *	0.040	2.67E-07	2.035 *	0.040	2.71E-07	1.999
BENZO(k)FLUORANTHENE	0.040	2.89E-07	2.196 *	0.040	2.67E-07	2.035 *	0.040	2.71E-07	1.999
BENZO(a)PYRENE	0.040	2.89E-07	2.196 *	0.040	2.67E-07	2.035 *	0.040	2.71E-07	1.999
BENZO(G,H,I)PERYLENE	0.050	3.61E-07	2.745 *	0.050	3.34E-07	2.544 *	0.050	3.39E-07	2.498
DIBENZ(A,H)ANTHRACENE	0.080	5.77E-07	4.392 *	0.080	5.35E-07	4.070 *	0.080	5.42E-07	3.997
INDENO[1,2,3-cd]PYRENE	0.080	5.77E-07	4.392 *	0.080	5.35E-07	4.070 *	0.080	5.42E-07	3.997

* - sample was below the reportable limit.

DEXZEL

Cogeneration Facility
 PLANT: DEXZEL, INC.
 LOCATION: OILDALE, CA

ALDEHYDES

		RUN 1	RUN 2	RUN 3
RUN NUMBER	*****	1	2	3
DATE OF RUN	*****	5-27-92	5-28-92	5-28-92
CLOCK TIME: INITIAL	*****	1713	856	1339
CLOCK TIME: FINAL	*****	1913	1056	1539
AVG. STACK TEMPERATURE	DEGREES F	197	197	197
AVG. SQUARE DELTA P	INCHES H2O	0.9247	0.9183	0.9042
NOZZLE DIAMETER	INCHES	NA	NA	NA
BAROMETRIC PRESSURE	IN. HG.	30.07	30.02	30.05
SAMPLING TIME	MIN.	120	120	120
SAMPLE VOLUME	CUBIC FEET	1.085	1.064	1.095
AVG. METER TEMP.	DEGREES F	87	76	87
AVG. DELTA H	IN. H2O	NA	NA	NA
WGM CALIB. FACTOR [Y]	*****	1.0000	1.0000	1.0000
WATER COLLECTED	MILLILITERS	NA	NA	NA
CO 2	PERCENT	3.6	3.6	3.7
CO 2	PERCENT	14.6	14.6	14.5
CO	PERCENT	0.0	0.0	0.0
N 2	PERCENT	81.8	81.8	81.8
STACK AREA	SQUARE INCHES	7088.0	7088.0	7088.0
STATIC PRESSURE	INCHES WG.	-0.30	-0.30	-0.32
PITOT COEFFICIENT	*****	0.84	0.84	0.84
SAMPLE VOLUME DRY	DSCF	1.04	1.04	1.05
WATER AT STD.	SCF	0.0	0.0	0.0
MOISTURE	PERCENT	7.2	8.9	8.1
MOLE FRACTION DRY GAS	*****	0.93	0.91	0.92
MOLECULAR WT. DRY	LB/LB MOLE	29.16	29.16	29.17
EXCESS AIR	PERCENT	209	209	204
MOLECULAR WT. WET	LB/LB MOLE	28.36	28.17	28.27
STACK GAS PRESSURE	INCHES HG.	30.05	30.00	30.03
STACK VELOCITY	AFPM	3493	3484	3424
VOLUMETRIC FLOWRATE, DRY STD.	DSCFM	126843	124020	122956
VOLUMETRIC FLOWRATE, ACTUAL	ACFM	171990	171508	168551

TRAIN LOADING AND EMISSION RATES

FORMALDAHYDE BLANK TRAIN	ug/sample	1.11	1.11	1.11
TOTAL FORMALDAHYDE WEIGHT	ug/sample	1.72	1.32	1.50
FORMALDAHYDE CONCENTRATION	ug/dscf	0.58862	0.20284	0.37293
FORMALDAHYDE CONCENTRATION	ppb	17	6	11
ORMALDAHYDE EMISSION RATE	mg/hr	4479.7	1509.4	2751.3
ORMALDAHYDE EMISSION RATE	lb/hr	0.0099	0.0033	0.0061

ACETALDAHYDE BLANK	ug/sample	0.30	0.30	0.30
TOTAL ACETALDAHYDE WEIGHT	ug/sample	1.59	0.11	0.23
CETALDAHYDE CONCENTRATION	ug/dscf	1.24478	-0.18352	-0.06694
ACETALDAHYDE CONCENTRATION	ppb	24	-4	-1
ACETALDAHYDE EMISSION RATE	mg/hr	9473.5	-1365.6	-493.8
CETALDAHYDE EMISSION RATE	lb/hr	0.0209	-0.0030	-0.0011

ACROLEIN BLANK	ug/sample	0.07	0.07	0.07
TOTAL ACROLEIN WEIGHT	ug/sample	0.29	0.33	0.40
ACROLEIN CONCENTRATION	ug/dscf	0.21229	0.25114	0.31556
ACROLEIN CONCENTRATION	ppb	3	4	5
ACROLEIN EMISSION RATE	mg/hr	1615.6	1868.7	2328.0
ACROLEIN EMISSION RATE	lb/hr	0.004	0.004	0.005

EMISSION RATES - SPECIATED VOLATILE ORGANIC COMPOUNDS
 PLANT: DEXZEL, INC.
 LOCATION: OILDALE, CA

SAMPLE LOCATION: COGENERATION STACK
 CONTAMINANT: BENZENE 78.0

RUN #		1	2	3	Field Blank
DATE		5-28-92	5-28-92	5-28-92	5-28-92
SAMPLE VOLUME	standard liters				
CONCENTRATION	ug/liter	0.0011	0.0009	0.0013	0.0003
CONCENTRATION	ppm, v/v	0.00034	0.00026	0.00040	0.00010
FLOWRATE	scfm	124020	124020	124020	124020
EMISSION RATE	grams/second	0.000066	0.000050	0.000077	0.000019
EMISSION RATE	lbs/hour	0.00052	0.00040	0.00061	0.00015

SAMPLE LOCATION: COGENERATION STACK
 CONTAMINANT: PROPYLENE 42.0

RUN #		1	2	3	Field Blank
DATE		5-28-92	5-28-92	5-28-92	5-28-92
SAMPLE VOLUME	standard liters				
CONCENTRATION	ug/liter	0.0050	0.0060	0.0045	0.0002
CONCENTRATION	ppm, v/v	0.0028	0.0034	0.0025	0.0001
FLOWRATE	scfm	124020	124020	124020	124020
EMISSION RATE	grams/second	0.000294	0.000352	0.000264	0.000010
EMISSION RATE	lbs/hour	0.00233	0.00279	0.00209	0.00008

SAMPLE LOCATION: COGENERATION STACK
CONTAMINANT:TOLUENE 92.0

RUN #		1	2	3	Field Blank
DATE		5-28-92	5-28-92	5-28-92	5-28-92
SAMPLE VOLUME	standard liters				
CONCENTRATION	ug/liter	0.0143	0.0084	0.0092	0.0011
CONCENTRATION	ppm,v/v	0.00368	0.00217	0.00237	0.00028
FLOWRATE	scfm	124020	124020	124020	124020
EMISSION RATE	grams/second	0.000836	0.000493	0.000539	0.000064
EMISSION RATE	lbs/hour	0.00662	0.00391	0.00427	0.00050

SAMPLE LOCATION: COGENERATION STACK
CONTAMINANT:XYLENES 106.0

RUN #		1	2	3	Field Blank
DATE		5-28-92	5-28-92	5-28-92	5-28-92
SAMPLE VOLUME	standard liters				
CONCENTRATION	ug/liter	< 0.0009	< 0.0009	< 0.0009	< 0.0004
CONCENTRATION	ppm,v/v	< 0.00020	< 0.00020	< 0.00020	< 0.00010
FLOWRATE	scfm	124020	< 124020	< 124020	< 124020
EMISSION RATE	grams/second	< 0.000052	< 0.000052	< 0.000052	< 0.000026
EMISSION RATE	lbs/hour	< 0.00041	< 0.00041	< 0.00041	< 0.00021

SAMPLE LOCATION: COGENERATION STACK
CONTAMINANT:ETHYLBENZ 106.0

RUN #		1	2	3	Field Blank
DATE		5-28-92	5-28-92	5-28-92	5-28-92
SAMPLE VOLUME	standard liters				
CONCENTRATION	ug/liter	< 0.0009	< 0.0009	< 0.0009	< 0.0004
CONCENTRATION	ppm,v/v	< 0.00020	< 0.00020	< 0.00020	< 0.00010
FLOWRATE	scfm	124020	124020	124020	124020
EMISSION RATE	grams/second	< 0.000052	< 0.000052	< 0.000052	< 0.000026
EMISSION RATE	lbs/hour	< 0.00041	< 0.00041	< 0.00041	< 0.00021

DPVZEL

AMMONIA SLIP TESTING
 PLANT: DEXZEL COGENERATION PLANT
 LOCATION: OILDALE, CA

		Run 1	Run 2	Run 3
IN NUMBER	*****	Ammonia	Ammonia	Ammonia
DATE OF RUN	*****	5-27-92	5-28-92	5-28-92
CLOCK TIME: INITIAL	*****	1748	1100	1445
CLOCK TIME: FINAL	*****	1848	1200	1545
AVG. STACK TEMPERATURE	DEGREES F	NA	NA	NA
AVG. SQUARE DELTA P	INCHES H2O	NA	NA	NA
NOZZLE DIAMETER	INCHES	NA	NA	NA
BAROMETRIC PRESSURE	IN. HG.	30.07	30.05	30.05
SAMPLING TIME	MIN.	60	60	60
SAMPLE VOLUME	CUBIC FEET	45.982	45.283	47.116
AVG. METER TEMP.	DEGREES F	NA	NA	NA
AVG. DELTA H	IN. H2O	1.70	1.70	1.70
IN CALIB. FACTOR [Y]	*****	0.9788	0.9788	0.9788
WATER COLLECTED	MILLILITERS	34	89	96
CO 2	PERCENT	3.6	3.6	3.7
O 2	PERCENT	14.6	14.6	14.5
	PERCENT	0.0	0.0	0.0
	PERCENT	81.8	81.8	81.8
STACK AREA	SQUARE INCHES	7088	7088	7088
STATIC PRESSURE	INCHES WG.	-0.30	-0.30	-0.30
WOT COEFFICIENT	*****	0.84	0.84	0.84
SAMPLE VOLUME DRY	DSCF	51.345	50.531	52.577
WATER AT STD.	SCF	1.6	4.2	4.5
WISTURE	PERCENT	3.0	7.7	7.9
MOLE FRACTION DRY GAS	*****	0.97	0.92	0.92
MOLECULAR WT.DRY	LB/LB MOLE	29.16	29.16	29.17
CESS AIR	PERCENT	208.71	208.71	204.36
MOLECULAR WT. WET	LB/LB MOLE	28.83	28.30	28.28
STACK GAS PRESSURE	INCHES HG.	30.05	30.03	30.03
STACK VELOCITY	AFPM	3493	3484	3424
VOLUMETRIC FLOWRATE, DRY STD.	DSCFM	126843	124020	122956
VOLUMETRIC FLOWRATE, ACTUAL	ACFM	171990	171508	168551

EMISSION RATES

monia				
Concentration	mg/sample	0.72	1.18	1.03
Concentration	ppm	0.72	1.21	1.01
Concentration	mg/dscf	0.0140	0.0234	0.0196
Emission Rate	lbs/hr	0.2353	0.3831	0.3186

LOCATION: OILDALE, CA

JERRY LEE WASH TANK #T-402

RUN #:	1	2	3
DATE:	5-29-92	5-29-92	5-29-92
START TIME:	842	956	1108
END TIME:	912	1026	1138

DGM Volume	liters	29.42	29.59	29.54
DGM Temp.	F	80	84	87
Standard Temp.	F	60	60	60
Bar. Press.	inches	30.00	30.00	30.00
Standard Press	inches	29.92	29.92	29.92
DGM Cal Factor	Y	1.0437	1.0437	1.0437
Standard DGM Volume		29.65	29.60	29.39

Iodide, sample	ml	50	50	50
Iodide, blank	ml	50	50	50
Iodide, Std.	N	0.0110	0.0110	0.0110
Titrant, sample	ml	45.82	46.2	45.3
Titrant, blank	ml	47.68	47.68	47.68
Titrant, Std.	N	0.010	0.010	0.010

H2S Conc.	mg/dscm	10.7	8.5	13.8
H2S Conc.	ppm	7.5	6.0	9.7

PERNE LEASE TANK #5395

RUN #:	1	2	3
DATE:	5-29-92	5-29-92	5-29-92
START TIME:	907	1039	1202
END TIME:	1007	1140	1302

DGM Volume	liters	60.15	62.5	61.65
DGM Temp.	F	86	90	98
Standard Temp.	F	60	60	60
Bar. Press.	inches	30.00	30.00	30.00
Standard Press	inches	29.92	29.92	29.92
DGM Cal Factor	Y	1.0386	1.0386	1.0386
Standard DGM Volume		59.66	61.54	59.83

Iodide, sample	ml	50	50	50
Iodide, blank	ml	50	50	50
Iodide, Std.	N	0.0110	0.0110	0.0110
Titrant, sample	ml	46.93	47.1	47.3
Titrant, blank	ml	47.68	47.68	47.68
Titrant, Std.	N	0.010	0.010	0.010

H2S Conc.	mg/dscm	2.1	1.6	1.1
H2S Conc.	ppm	1.5	1.1	0.8

HEAD SPACE MOLECULAR WEIGHT

FACILITY:DEXZEL

SOURCE: JERRY LEE TANK #T-402

RUN #: 1

	Concentration,v/v (ppm)	MW	Weight Fraction
C1	886000	16	
C2	101	30	12.5
C3	4.4	44	0.8
C4	48.5	58	11.6
C5	9.9	72	2.9
C6	19.3	86	6.9
C7	59.2	100	24.4
	242.3	MWtnmhc	59.1
		MWthc	16.0
Benzene	0.04 *	78	2.2E-07 *
Toluene	41	92	2.7E-04
Xylenes	0.18 *	106	1.3E-06 *
E.benzene	0.08 *	106	6.0E-07 *
H2S	7.4	34	1.8E-05

FACILITY:DEXZEL

SOURCE: JERRY LEE TANK #T-402

RUN #: 2

	Concentration,v/v (ppm)	MW	Weight Fraction
C1	882000	16	
C2	44.6	30	5.5
C3	3	44	0.5
C4	42.2	58	10.1
C5	4.1	72	1.2
C6	28.8	86	10.2
C7	91	100	37.6
	213.7	MWtnmhc	65.2
		MWthc	16.0
Benzene	0.04 *	78	2.2E-07 *
Toluene	43.2	92	2.8E-04
Xylenes	0.18 *	106	1.3E-06 *
E.benzene	0.08 *	106	6.0E-07 *
H2S	5.9	34	1.4E-05

RUN #:

3

	Concentration, v/v (ppm)	MW	Weight Fraction
C1	838000	16	
C2	90.8	30	11.2
C3	4.1	44	0.7
C4	44.8	58	10.7
C5	9.4	72	2.8
C6	20.8	86	7.4
C7	53.9	100	22.2
	223.8	MWtnmhc	55.1
		MWthc	16.0
Benzene	0.04 *	78	2.2E-07 *
Toluene	40	92	2.6E-04
Xylenes	0.18 *	106	1.3E-06 *
E.benzene	0.08 *	106	6.0E-07 *
H2S	9.6	34	2.3E-05

HEAD SPACE MOLECULAR WEIGHT

FACILITY:DEXZEL

SOURCE: FERNE LEASE TANK # 5395

RUN #: 1

	Concentration,v/v (ppm)	MW	Weight Fraction
C1	445000	16	
C2	76.5	30	9.5
C3	7.9	44	1.4
C4	198	58	47.4
C5	29.4	72	8.7
C6	56.1	86	19.9
C7	81.2	100	33.5
	449.1	MWtnmhc	120.5
		MWthc	16.1
Benzene	0.094	78	5.2E-07
Toluene	56.2	92	3.6E-04
Xylenes	0.18 *	106	1.3E-06 *
E.benzene	0.08 *	106	6.0E-07 *
H2S	1.5	34	3.6E-06

FACILITY:DEXZEL

SOURCE: FERNE LEASE TANK # 5395

RUN #: 2

	Concentration,v/v (ppm)	MW	Weight Fraction
C1	445000	16	
C2	79.4	30	9.8
C3	8.3	44	1.5
C4	195	58	46.7
C5	28.5	72	8.5
C6	48	86	17.0
C7	66.7	100	27.5
	425.9		
		MWtnmhc	111.0
		MWthc	16.1
Benzene	0.095	78	5.2E-07
Toluene	52.5	92	3.4E-04
Xylenes	0.18 *	106	1.3E-06 *
E.benzene	0.08 *	106	6.0E-07 *
H2S	1.1	34	2.6E-06

FACILITY:DEXZEL
SOURCE: FERNE LEASE TANK # 5395

RUN #: 3

	Concentration,v/v (ppm)	MW	Weight Fraction
C1	440000	16	
C2	78.1	30	9.7
C3	8	44	1.5
C4	191	58	45.7
C5	26.7	72	7.9
C6	45.4	86	16.1
C7	61.1	100	25.2
	410.3	MWtnmhc	106.1
		MWthc	16.1
Benzene	0.106	78	5.8E-07
Toluene	53.4	92	3.5E-04
Xylenes	0.18 *	106	1.3E-06 *
E.benzene	0.08 *	106	6.0E-07 *
H2S	0.8	34	1.9E-06

APPENDIX B

Laboratory Data

Zenon Environmental Laboratories - Certificate of Analysis

Client Information
Name: Horizon Air Measurement
Project: D02-001

Lab Information
Contact: RM
Project: AN920566
Date: 92/07/01

Notes:
 "-" = Not Analysed
 "<" = Less than Method Detection Limit
 All results are method blank corrected
 CARB429 PAH analyses are corrected for internal recoveries
 "NS" = Surrogates not spiked

Component	Units:	Client ID: Lab ID:	METHOD BLANK	D201-FB 014573 92	D201-BT 014574 92	D201-1 014575 92	D201-2 014576 92	D201-3 014577 92
Naphthalene	ug		<0.1	3.3	3.1	4.7	3.6	3.8
Acenaphthylene			<0.05	<0.05	<0.05	<0.05	0.052	<0.04
Acenaphthene			<0.05	<0.05	<0.05	<0.072	<0.05	<0.05
Fluorene			<0.05	<0.05	<0.05	0.27	0.086	0.13
Phenanthrene			<0.1	0.26	0.23	1.4	0.76	0.6
Anthracene			<0.1	<0.08	<0.06	<0.08	<0.06	<0.05
Fluoranthene			<0.1	<0.08	<0.06	0.19	0.14	0.071
Pyrene			<0.1	<0.08	<0.06	0.068	0.084	0.041
Benz(a)anthracene			<0.1	<0.1	<0.08	<0.08	<0.07	<0.08
Chrysene			<0.1	<0.1	<0.08	<0.09	<0.08	<0.08
Benzo(b)fluoranthene			<0.05	<0.05	<0.04	<0.04	<0.03	<0.03
Benzo(k)fluoranthene			<0.05	<0.05	<0.04	<0.04	<0.03	<0.03
Benzo(a)pyrene			<0.05	<0.05	<0.04	0.055	<0.04	<0.04
Indeno(1,2,3-c,d)pyrene			<0.1	<0.1	<0.08	<0.08	<0.08	<0.08
Dibenzo(a,h)anthracene			<0.1	<0.1	<0.08	<0.08	<0.08	<0.08
Benzo(g,h,i)perylene			<0.05	<0.05	<0.05	<0.05	<0.04	<0.04
INTERNAL RECOVERIES	%							
Naphthalene-2H8			50	41	53	64	71	62
Acenaphthylene-2H8			55	47	58	64	67	68
Acenaphthene-2H10			55	43	59	63	66	70
Fluorene-2H10			70	69	85	120	120	100
Phenanthrene-2H10			69	73	87	82	85	88
Anthracene-2H10			62	64	74	52	58	62
Fluoranthene-2H10			74	69	82	63	63	67
Pyrene-2H10			75	67	82	66	66	68
Benz(a)anthracene-2H12			91	78	93	100	110	110
Chrysene-2H12			92	71	81	78	91	90
Benzo(b)fluoranthene-2H12			100	85	97	100	100	110
Benzo(k)fluoranthene-2H12			88	77	78	69	78	76
Benzo(a)pyrene-2H12			90	67	79	64	79	76
Indeno(1,2,3-c,d)pyrene-2H12			78	69	95	92	90	92
Dibenzo(a,h)anthracene-2H14			94	89	110	97	100	100
Benzo(g,h,i)perylene-2H12			95	73	89	76	84	82
SURROGATE RECOVERIES	%							
Benzo(e)pyrene-2H12			NS	68	72	79	92	89
Terphenyl-2H14			NS	68	78	82	86	86



AtmAA Inc.

21354 Nordhoff St., Suite 113, Chatsworth, CA 91311 (818) 718-6070 • FAX (818) 718-9779

environmental consultants
laboratory services

LABORATORY ANALYSIS REPORT

DNPH solutions were analyzed for formaldehyde, acetaldehyde, and acrolein by high performance liquid chromatography.

Report Date : June 12, 1992
Date Received : May 29, 1992
Date Analyzed : June 4, 1992
P.O. No. : Verbal
Client Proj. # : D02-001

AtmAA Lab. No.	Sample ID	ug/sample		
		Formal.	Acetal.	Acrolein
91502-29	FB 1	0.63	0.22	<0.02
91502-30	FB 2	0.50	0.12	<0.02
91502-31	FB 3	0.54	0.11	0.07
91502-32	1A	1.72	1.59	0.29
91502-33	2A	1.32	0.11	0.33
91502-34	3A/BB	1.50	0.23	0.40
REPEAT:				
91502-29	FB 1	0.62	0.19	<0.02
91502-29 spiked		4.25	6.11	5.49
ug spiked		3.87	5.45	5.46
% recovery		93.6	108.1	100.5
Det. Limit		0.06	0.02	0.02

Dr. Kochy Fung
Air Programs Director

Client/Project Name		Project Location	
Dexzel Inc.		Oildale, CA	
Project No.		Field Logbook No.	
Doe-001			
Sampler: (Signature)		Chain of Custody Tape No.	
Sample No./ Identification	Date	Time	Lab Sample Number
FB1	5-27-92		91502-29
FB2	↓		91502-30
FB3	↓		91502-31
1A	↓		91502-32
1B	↓		
2A	5/28/92		91502-33
2B	↓		
3A/BB	↓		91502-34
Relinquished by: (Signature)			
Date		Time	
5/27/92		1215	
Received by: (Signature)			
Date		Time	
5-29-92		1432	
Relinquished by: (Signature)			
Date		Time	
Relinquished by: (Signature)			
Date		Time	
Sample Disposal Method:			
Disposed of by: (Signature)			
ANALYTICAL LABORATORY			
SAMPLE COLLECTOR			
HORIZON AIR MEASUREMENT SERVICES 996 Lawrence Drive, Suite 108 Newbury Park, CA 91320 (805) 498-8781			
Nº 1125			

LABORATORY ANALYSIS REPORT

DNPH solutions were analyzed for aldehydes by high performance liquid chromatography.

Report Date : May 26, 1992
Date Shipped : May 26, 1992
Date Analyzed : May 26, 1992
P.O. No. :
Client Proj. # :

DNPH Blank	ug/ml		
	HCHO	CH3CHO	Acrolein
1	0.09	<0.01	<0.01
2	0.08	<0.01	<0.01
3	0.08	<0.01	<0.01
4	0.08	<0.01	<0.01
Average	0.08	<0.01	<0.01

3.838

8.023

10.287

12.159

11.727

CHROMATOGRAM	1	MEMORIZED					
PKNO	TIME	RRT	AREA	MK	IDNO	CONC	NAME
1	3.838	0.3273	20183		2	0.1031	HCHO
4	11.727	1	138785		1	1.3307	HXNAL
TOTAL			158968			1.4338	

mg ml extract

02/05/26 11:16:54

3.689

79.8756

107174

11.593

CHROMATOGRAM	1	MEMORIZED					
PKNO	TIME	RRT	AREA	MK	IDNO	CONC	NAME
1	3.689	0.3182	16858		2	0.0863	HCHO
4	11.593	1	135118		1	1.3008	HXNAL
TOTAL			151976			1.3871	

mg ml extract

02/05/26 11:33:33

3.788

79.8756

10.256

11.713

CHROMATOGRAM	1	MEMORIZED					
PKNO	TIME	RRT	AREA	MK	IDNO	CONC	NAME
1	3.788	0.3234	17313		2	0.0886	HCHO
4	11.713	1	138273		1	1.3265	HXNAL
TOTAL			155586			1.4151	

mg ml extract

02/05/26 11:50:20

3.775

8.243

10.254

11.713

CHROMATOGRAM	1	MEMORIZED					
PKNO	TIME	RRT	AREA	MK	IDNO	CONC	NAME
1	3.775	0.3223	17900		2	0.0916	HCHO
3	8.7	0.7428	1743		4	0.0537	ACTONE
5	11.713	1	136949		1	1.3157	HXNAL
TOTAL			156592			1.461	

mg ml extract



AtmAA Inc.

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environmental consultants
laboratory services

LABORATORY ANALYSIS REPORT

Benzene, Toluene, Ethylbenzene, m + p-xylenes, o-xylene, & Propylene
Analysis in Tedlar Bag Samples

Report Date: June 4, 1992
Client: Horizon/Dexzel
P.O. No.: Verbal
Source Location: Oildale, CA
Source Test Date: May 28, 1992

Date Received: May 29, 1992
Date Analyzed: May 30, & June 1, 1992

ANALYSIS DESCRIPTION

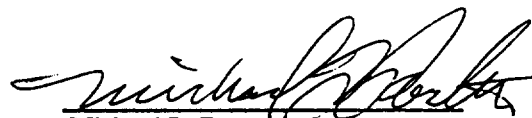
Benzene, toluene, ethylbenzene, m + p-xylenes, o-xylene, and propylene were analyzed by photoionization detection/gas chromatography (PID/GC).

AtmAA Lab No.:	91502-19	91502-20	91502-21	91502-22
Sample I.D.:	D201-1	D201-2	D201-3	D201-FB
	BTXEP	BTXEP	BTXEP	BTXEP

Components:

(Concentration in ppb, v/v)

Benzene	0.34	0.26	0.40	<0.1
Toluene	3.68	2.17	2.37	0.28
Ethylbenzene	<0.2	<0.2	<0.2	<0.1
m + p-xylenes	<0.2	<0.2	<0.2	<0.1
o-xylene	<0.2	<0.2	<0.2	<0.1
Propylene	2.83	3.39	2.54	<0.1


Michael L. Porter
Laboratory Director

QUALITY ASSURANCE SUMMARY
(Repeat Analysis)

P.O. No.: Verbal
Client Proj. No.: D02-001

Components:	Sample ID	Repeat	Analysis	Mean Conc.	% Diff. From Mean
		Run #1	Run #2		
(Concentration in ppb, v/v)					
Benzene	3-BTXEP	0.39	0.41	0.40	3.2
	FB-BTXE	< 0.1	< 0.1	---	---
Toluene	3-BTXEP	2.34	2.40	2.37	1.3
	FB-BTXE	0.24	0.31	0.28	13
Ethylbenzene	3-BTXEP	< 0.2	< 0.2	---	---
	FB-BTXE	< 0.1	< 0.1	---	---
m + p-xylenes	3-BTXEP	< 0.2	< 0.2	---	---
	FB-BTXE	< 0.1	< 0.1	---	---
o-xylene	3-BTXEP	< 0.2	< 0.2	---	---
	FB-BTXE	< 0.1	< 0.1	---	---
Propylene	3-BTXEP	2.74	2.35	2.54	7.7

A set of 4 Tedlar bag samples, laboratory numbers 91502-(19-22) was analyzed for benzene, toluene, ethylbenzene, m + p-xylenes, o-xylene, and propylene. Agreement between repeat analysis is a measure of precision and is shown above in the column "% Difference from Mean." Repeat analyses are an important part of AtmAA's quality assurance program. The average % Difference from Mean for 4 repeat measurements from the sample set of 4 Tedlar bag samples is 6.3%.



Client/Project Name				Project Location		ANALYSES	
Dorco Inc.				Orlando, CA			
Project No.		Field Logbook No.		B.T.C. people			
D02-001							
Sampler: (Signature)		Chain of Custody Tape No.		B.T.C. people			
[Signature]							
Sample No./ Identification	Date	Time	Lab Sample Number	Type of Sample	B.T.C. people		
D001-1-BTXEP	5/20/92		91502-19	10 lb Tedlar bag	B.T.C. people		
D001-2-BTXEP			91502-20				
D001-3-BTXEP			91502-21				
D001-F6-BDOP			91502-22				
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		
					B.T.C. people		

June 12, 1992

HORIZON AIR MEASUREMENT
996 Lawrence Drive
Suite 108
Newbury Park, CA 91320

Attn: Rich Vacherot

JOB NO. 21502

S

WCAS

**WEST COAST
ANALYTICAL
SERVICE, INC.**

ANALYTICAL CHEMISTS

LABORATORY REPORT

Samples Received: Four (4) Liquid Samples

Date Received: 6-2-92

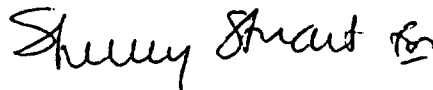
Purchase Order No: Proj#: D02-001/Proj. Nm: Dexzel Cogeneration

The samples were analyzed as follows:

<u>Samples Analyzed</u>	<u>Analysis</u>	<u>Results</u>
Four (4) liquids	Ammonia by BAAQMD No.1	Table 1

Page 1 of 2


Michael Shelton
Technical Director


D. J. Northington, Ph.D.
President

This report is to be reproduced in its entirety.

WEST COAST ANALYTICAL SERVICE, INC.

HORIZON AIR MEASUREMENT
Mr. Rich Vacherot

Job #21502
June 12, 1992

LABORATORY REPORT

Table 1

Ammonia by BAAQMD No.1

<u>Sample ID</u>	<u>Parts Per Million (mg/L)</u>	<u>Sample Volume (L)</u>	<u>Total mg</u>
D02-001-NH ₃ -1	1.4	0.50	0.72
D02-001-NH ₃ -2	2.3	0.52	1.18
D02-001-NH ₃ -3	1.9	0.54	1.03
D02-001-NH ₃ -FB	ND	0.28	ND<0.03
Detection Limit	0.1	----	----

ND - Not Detected

Date Analyzed: 6-11-92

Matrix Spike/Matrix Spike Duplicate Quality Control Summary

Sample: D02-001-NH3-3
Units: Total mg
Method: BAAQMD No.1

<u>Analyte</u>	<u>Sample Result</u>	<u>Amount Spiked</u>	<u>MS Result</u>	<u>% Rec MS</u>	<u>MSD Result</u>	<u>% Rec MSD</u>	<u>RPD</u>
AMMONIA	1.03	4.32	5.72	109	5.83	111	2

QC Limits

<u>Analyte</u>	<u>Warning</u>	<u>RPD Control</u>	<u>% Recovery Control</u>
AMMONIA	15	25	50-150

RD

RD

CLIENT: Pexel Corp
 UNIT : WASH / STOCK TANKS
 METHOD: EPA 11

DATE: 5/28/92
 JOB NO.: D02-001
 SAMPLE ID: _____

Run#	Tank	Time	Vol-end	Vol-begin	Titrant Volume		
Iodine Standardization							
Normality of Sodium thiosulfate = 0.0100 N							
			24.95	2.2	22.75		
			23.4	0.7	22.7		
			$(25 \times 0.0100) / 22.73 \text{ ml} = 0.010999$				
#1	BLANK	1020	48.3	0.62	47.68		
#2	BLANK	1010	47.8	0.10	47.70		
#1	JL WASH TANK	1020	45.72	0.10	45.82		
#1	FRANK LEAK STOCK TANK	1020 1100	47.75	0.82	46.93		
#2	JL WASH TANK	1130	46.80	0.60	46.2		
#2	FRANK LEAK STOCK TANK	1230	47.7	0.60	47.10		
#3	JL WASH TANK	1230	45.4	0.1	45.3		
#3	FRANK LEAK STOCK TANK	1350	47.6	0.3	47.3		



AtmAA Inc.

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environmental consultants
laboratory services

LABORATORY ANALYSIS REPORT

C1-C6 Hydrocarbons Analysis in Tedlar Bag Samples

Report Date: June 4, 1992
Client: Horizon/Dexzel
P.O. No.: Verbal
Source Location: Oildale, CA
Source Test Date: May 28, 1992

Date Received: May 29, 1992
Date Analyzed: May 30, 1992

ANALYSIS DESCRIPTION

C1-C6 hydrocarbons are analyzed by FID/GC using a non-polar capillary column temperature programmed from -60 to +210 degrees C. Eluted peaks are grouped by carbon number for quantitation.

AtmAA Lab No.:	91502-23	91502-23	91502-24	91502-25	91502-25	91502-26
Sample I.D.:	DEX-JL	repeat	DEX-JL	DEX-JL	repeat	DEX-FER
	TB-1		TB-2	TB-3		TB-1

(ppmv as component)

Component:

C1	886000	886000	882000	838000		445000
C2	101	91.7	44.6	90.8	90.3	76.5
C3	4.36	3.76	2.97	4.06	3.91	7.90
C4	48.5	47.9	42.2	44.8	43.7	198
C5	9.89	9.80	4.12	9.35	8.72	29.4
C6	19.3	19.6	28.8	20.8	18.8	56.1

LABORATORY ANALYSIS REPORT

C1-C6 Hydrocarbons Analysis in Tedlar Bag Samples

Report Date: June 4, 1992
Client: Horizon/Dexzel
P.O. No.: Verbal
Source Location: Oildale, CA
Source Test Date: May 28, 1992

Date Received: May 29, 1992
Date Analyzed: May 30, 1992

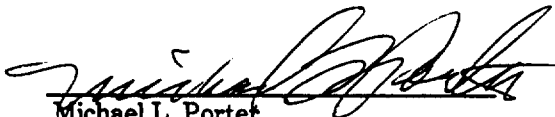
ANALYSIS DESCRIPTION

C1-C6 hydrocarbons are analyzed by FID/GC using a non-polar capillary column temperature programmed from -60 to +210 degrees C. Eluted peaks are grouped by carbon number for quantitation.

AtmAA Lab No.:	91502-27	91502-28	91502-28
Sample I.D.:	DEX-FER	DEX-FER	repeat
	TB-2	TB-3	

(ppmv as component)

Component:			
C1	445000	440000	443000
C2	79.4	78.1	78.2
C3	8.29	8.03	8.15
C4	195	191	190
C5	28.5	26.7	26.7
C6	48.0	45.4	45.0


Michael L. Porter
Laboratory Director





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LABORATORY ANALYSIS REPORT

Benzene, Toluene, Ethylbenzene, m + p-xylenes, & o-xylene,
Analysis in Tedlar Bag Samples

Report Date: June 4, 1992
Client: Horizon/Dexzel
P.O. No.: Verbal
Source Location: Oildale, CA
Source Test Date: May 28, 1992

Date Received: May 29, 1992
Date Analyzed: May 30, 1992

ANALYSIS DESCRIPTION

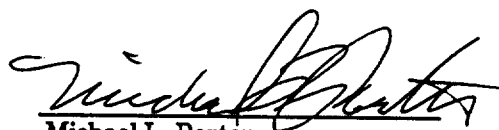
Benzene, toluene, ethylbenzene, m + p-xylenes, and o-xylene were analyzed by photoionization detection/
gas chromatography (PID/GC).

AtmAA Lab No.:	91502-23	91502-24	91502-25	91502-26	91502-27	91502-28
Sample I.D.:	DEX-JL	DEX-JL	DEX-JL	DEX-FER	DEX-FER	DEX-FER
	TB-1	TB-2	TB-3	TB-1	TB-2	TB-3

Components:

(Concentration in ppb, v/v)

Benzene	< 40	< 40	< 40	93.7	95.4	106
Toluene	41000	43200	40000	56200	52500	53400
Ethylbenzene	< 80	< 80	< 80	< 80	< 80	< 80
m + p-xylenes	< 100	< 100	< 100	< 100	< 100	< 100
o-xylene	< 80	< 80	< 80	< 80	< 80	< 80


Michael L. Porter
Laboratory Director

QUALITY ASSURANCE SUMMARY
(Repeat Analysis)

P.O. No.: Verbal
Client Proj. No.: D02-001

Components:	Sample ID	Repeat	Analysis	Mean Conc.	% Diff. From Mean
		Run #1	Run #2		
(Concentration in ppb, v/v)					
Benzene	JL-TB-3	< 40	< 40	---	---
	FER-TB-3	102	111	106	4.2
Toluene	JL-TB-3	39500	40400	40000	1.1
	FER-TB-3	52600	54200	53400	1.5
Ethylbenzene	JL-TB-3	< 80	< 80	---	---
	FER-TB-3	< 80	< 80	---	---
m+ p-xylenes	JL-TB-3	< 100	< 100	---	---
	FER-TB-3	< 100	< 100	---	---
o-xylene	JL-TB-3	< 80	< 80	---	---
	FER-TB-3	< 80	< 80	---	---

A set of 6 Tedlar bag samples, laboratory numbers 91502-(23-28) was analyzed for benzene, toluene, ethylbenzene, m + p-xylenes, and o-xylene. Agreement between repeat analysis is a measure of precision and is shown above in the column "% Difference from Mean." Repeat analyses are an important part of AtmAA's quality assurance program. The average % Difference from Mean for 3 repeat measurements from the sample set of 6 Tedlar bag samples is 2.3%.





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LABORATORY ANALYSIS REPORT

C7 Hydrocarbons Analysis in Tedlar Bag Samples

Report Date: June 4, 1992
Client: Horizon/Dexzel
P.O. No.: Verbal
Source Location: Oildale, CA
Source Test Date: May 28, 1992

Date Received: May 29, 1992
Date Analyzed: May 30, 1992

ANALYSIS DESCRIPTION

C7 hydrocarbons are analyzed by FID/GC using a non-polar capillary column temperature programmed from -60 to +210 degrees C. Eluted peaks are grouped by carbon number for quantitation.

AtmAA Lab No.:	91502-23	91502-23	91502-24	91502-25	91502-25	91502-26
Sample I.D.:	DEX-JL	repeat	DEX-JL	DEX-JL	repeat	DEX-FER
	TB-1		TB-2	TB-3		TB-1
	(ppmv as componet)					
Component:						
C7		59.2	91.0	53.9	56.7	81.2
>C7 as C7					207	

LABORATORY ANALYSIS REPORT

C7 Hydrocarbons Analysis in Tedlar Bag Samples

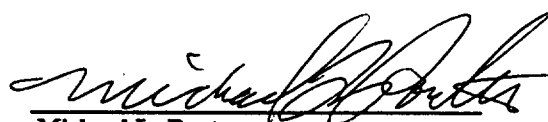
Report Date: June 4, 1992
Client: Horizon/Dexzel
P.O. No.: Verbal
Source Location: Oildale, CA
Source Test Date: May 28, 1992

Date Received: May 29, 1992
Date Analyzed: May 30, 1992

ANALYSIS DESCRIPTION

C7 hydrocarbons are analyzed by FID/GC using a non-polar capillary column temperature programmed from -60 to +210 degrees C. Eluted peaks are grouped by carbon number for quantitation.

AtmAA Lab No.:	91502-27	91502-28	91502-28
Sample I.D.:	DEX-FER	DEX-FER	repeat
	TB-2	TB-3	
	(ppmv as component)		
Component:			
C7	66.7	62.8	61.1
> C7 as C7			285


Michael L. Porter
Laboratory Director



CHAIN OF CUSTODY RECORD

Client/Project Name		Project Location		ANALYSES	
Dexal		Oildale, CA			
Project No.		Field Logbook No.			
D02-001					
Sampler (Signature)		Chain of Custody Tape No.			
<i>[Signature]</i>					
Sample No./ Identification	Date	Time	Lab Sample Number	Type of Sample	REMARKS
DEX-SL-TB-1	5/20/92		91502-23	Tedlar bag	
DEX-JL-TB-2			91502-24		
DEX-JL-TB-3			91502-25		
DEX-JL-TB-4			91502-26		
DEX-JL-TB-5			91502-27		
DEX-JL-TB-6			91502-28		
DEX-JL-TB-7					
DEX-JL-TB-8					
DEX-JL-TB-9					
DEX-JL-TB-10					
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DEX-JL-TB-256					
DEX-JL-TB					

APPENDIX C

Field Data

METHOD 2 GAS VELOCITY AND VOLUME DATA FORM

PLANT DEXZELL (CO-GEN)

DATE 5-27-92

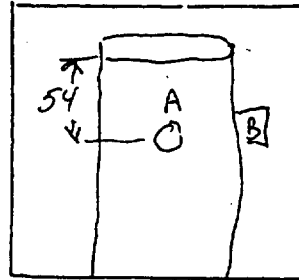
RUN NO. INITIAL TRAVERSE

STACK DIAMETER, in. 95"

BAROMETRIC PRESSURE, in. Hg. 30.05

STATIC PRESSURE IN STACK (P_s), in. Hg. -0.33

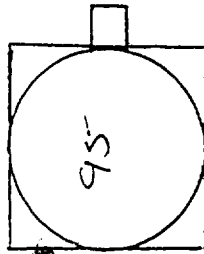
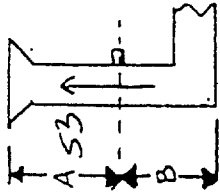
OPERATORS R. H. ADP, RV



SCHEMATIC OF STACK CROSS SECTION

Field data					
Traverse point number	Position, in.	Velocity head (Δp_s), in. H_2O	Stack temp., °F	Cyclonic flow determination	
				Δp_s at 0° reference	Angle (α) which yields a null Δp
1	2.00	0.68	197	5	→
2	6.37	0.92	199	3	
3	11.21	0.88	199	0	
4	16.82	0.94	199	0	→
5	23.75	0.98	199	0	
6	33.82	1.25	196	0	
7	61.18	1.00	196	0	→
8	71.25	0.86	197	0	
9	78.19	0.88	197	0	
10	83.79	0.92	197	0	
11	88.64	0.98	196	0	
12	93.01	1.10	195	5	
B-1		0.68	194	3	
2	SAME	0.86	194	3	
3	AS	0.86 ^{0.90}	196	3	
4	ABOVE	0.90	198	0	
5		0.84	193	0	
6		0.74	200	0	
7		0.74	200	0	
8		0.70	198	0	
9		0.80	198	3	
10		0.86	197	0	
11		1.00	198	3	
12		1.00	199	3	
PEAK ✓ - OK				Average angle (α)	

PLANT: DEXTEL
 LOCATION: BAKERSFIELD
 COUNTY: KERN
 UNIT: COGER
 DATE: 5-27-92
 RUN NO/METHOD: 1 PAK pg 1
 COLD BOX NO.: 3 10016 17959
 METER BOX NO.: Y = 0.9904 AND = 1.7698
 METER FACTOR: 31
 PITOT #/FACTOR: 0.840
 PYROMETER #: 10-1
 MAGNEHELIC FACTOR: ΔPO-5 ΔH0-5



FILTER NO. PAH-1
 AMBIENT TEMP.: 85
 BAROMETRIC PRESS., IN. HG.: 30.05
 ASSUMED MOISTURE: 5%
 HEATER BOX SETTING: 250
 PROBE LENGTH, FT.: 10' 9/1655
 NOZZLE DIAMETER, IN.: 0.214 (-2)
 PROBE HEATER SETTING: 250
 APPROX. WIND VEL., MPH: 0-10
 SAMPLE BOX TEMP., (F): <60
 DRI-RRITE WT.: —
 STATIC PRESSURE: -0.30 "H2O
0.65 SET = 20" 8 1/2" FIAW 73

TRAVERSE POINT NUMBER	DISTANCE INCHES	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O		PRESSURE DIFF ORIFICE METER (ΔH)	DRY GAS SAMPLE VOLUME (VM), FT.	GAS SAMPLE TEMP. @ DRY GAS METER		PUMP VACUUM IN. HG	TEMP. LAST IMPINGER (F)
						R2H	ΔP			INLET (Tm),	OUTLET (TM)		
1				1353 00	199	0.68P	1.32 RH	466.122	89	91	460-24	<60	
2	84	✓ - CLK		7.5	198	0.72	1.35 RH	471.4/472	87	89	12	<60	
3	84	✓ - CLK		15.0	198	0.76	1.40 RH	477.2	88	90	8.0	<60	
4				22.5	198	0.80	1.50	482.4	88 RH	94	8.0	<60	
5				30.0	198	0.76	1.40	486.80	85	93	9.0	<60	
6				37.5	198	0.74	1.40	491.80	89	95	9.0	<60	
7				45.0	197	0.70	1.30	498.20	89	96	8.0	<60	
8				52.5	199	0.74	1.40	502.20	90	94	8.0	<60	
9				60.0	198	0.84	1.50	507.16	90	95	10	<60	
10				67.5	198	0.96	1.80	512.50	90	95	11	<60	
11				75.0	197	1.05	1.98	519.0	90	94	11.5	<60	
12				82.5	196	1.10	2.05	524.0	90	93	12.0	<60	
STOP				90.0				530.013					
AVERAGE					198		1.529	63.891		91.1			
PITOT LEAK CHECK:													
BEFORE:				TOP ΔP = 0.82	SAMPLE TRAIN LEAK:								
AFTER:				ΔP = 0.52	CFM@ 15 IN. HG.								
				TOP ΔP = 0.66	CFM@ 12 IN. HG.								
				ΔP = 0.655									
COMMENTS: PURGE													

(011

58

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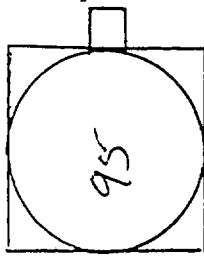
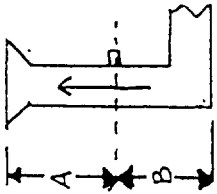
57

58

58

57

PLANT: Dez 28 11
LOCATION: Baigersville
COUNTY: Kane
UNIT: Cogeco
DATE: 5-27-92
RUN NO/METHOD: PAH #1 eq 2
COLD BOX NO.:
METER BOX NO.: 1
METER FACTOR: P=1.0016
PITOT #/FACTOR: 0.54
PYROMETER #:
MAGNEHELIC FACTOR: ΔP ΔH



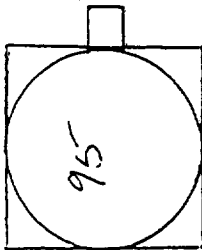
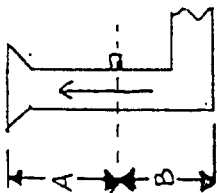
FILTER NO.:
AMBIENT TEMP.: 85
BARAMETRIC PRESS. IN. HG.:
ASSUMED MOISTURE: 5%
HEATER BOX SETTING: 250
PROBE LENGTH, FT.: 10' 9 1/2
NOZZLE DIAMETER, IN.: 0.237
PROBE HEATER SETTING: 250
APPROX. WIND VEL., MPH: 0-10
SAMPLE BOX TEMP., (F): 260
DRI-PRITE WT.:
STATIC PREASURE: "H2O

TRAVERSE POINT NUMBER	DISTANCE INCHES	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O		PRESSURE DIFF ORIFICE METER (ΔH) IN. H2O	DRY GAS SAMPLE VOLUME (VM), FT.	GAS SAMPLE TEMP. @ DRY GAS METER		PUMP VACUUM IN. HG.	TEMP. LAST IMPINGER (F)
						ΔP	√ΔP			INLET (Tm),	OUTLET (Tm)		
B - 1				1630 00	195	0.76		2.20	530.337	89	91	11	<60
2				7.5	198	0.90		2.60	536.50	91	95	13	<60
3				15.0	195	0.86		2.22	544.0	90	95	11	<60
4				22.5	197	0.88		2.80	550.9	91	94	14	<60
5				30.0	194	0.98		2.80	556.5	91	93	14	<60
6				37.5	192	1.00		2.90	564.2	91	93	15	<60
7				45.0	194	0.90		2.60	570.9	91	94	14.5	<60
8				52.5	190	0.86		2.42	578.1	92	93	14	<60
9				60.0	198	0.84		2.40	585.2	92	97	13	<60
10				67.5	196	0.86		2.42	591.40	92	95	13	<60
11				75.0	195	0.90		2.80	598.40	92	95	13.5	<60
12				82.5	196	0.92		2.65	604.6	92	94	14.0	<60
STOP	ZERO			90.0					611.992				
AVERAGE	SPAN						0.9463						
					195		0.9589	2.568	81.655		92.6		
PITOT LEAK CHECK:													
BEFORE: TOP ΔP= 196.5 BOTTOM ΔP= 198													
AFTER: TOP ΔP= 196.5 BOTTOM ΔP= 198													
SAMPLE TRAIN LEAK: BEFORE= 0.015 CFM@ 15 IN. HG. AFTER= 0.017 CFM@ 15 IN. HG.													
COMMENTS: PURGE													

4.5
13
56
57
54
57
52
52

1.96.5 0.9217 2.048 146.546 91.9

PLANT: Dex Bell
 LOCATION: Bakersfield
 COUNTY: KERN
 UNIT: CO-GEN
 DATE: 5-28-92
 RUN NO/METHOD: 2 PAH 191
 COLD BOX NO.: 5
 METER BOX NO.: 1
 METER FACTOR: Y=1.0016, AND=1.1959
 PITOT #/FACTOR: 0.840
 PYROMETER #: 10-1
 MAGNEHELIC FACTOR: AP 0.5 ΔH 0.5



FILTER NO.: PAH-2
 AMBIENT TEMP.: 77
 BAROMETRIC PRESS., IN. HG.: 30.02
 ASSUMED MOISTURE: 5%
 HEATER BOX SETTING: 250
 PROBE LENGTH, FT.: 16' #1 g/luss
 NOZZLE DIAMETER, IN.: 0.236
 PROBE HEATER SETTING: 250
 APPROX. WIND VEL., MPH: 0-10
 SAMPLE BOX TEMP., (F): 60
 DRI-RRITE WT.: 2.2 PT #4
 STATIC PRESSURE: - 0.30 "H2O

TRAVERSE POINT NUMBER	DISTANCE INCHES	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O		PRESSURE DIFF ORIFICE METER (ΔH) IN. H2O	DRY GAS SAMPLE VOLUME (VM), FT. 6/4.712-6/13.365	GAS SAMPLE TEMP. @ DRY GAS METER		PUMP VACUUM IN. HG	TEMP. LAST IMPINGER (F)
						ΔP	√ΔP			INLET (Tm),	OUTLET (Tm)		
1	52			831 00	195	0.70		2.00	613.305	80	84	8.0	60
2	52			75	195	0.70		2.00	614.712/615.330	82	91	8.0	60
3	53			156	196	0.74		2.15	624.9	83	93	8.5	60
4	53			225	197	0.76		2.20	631.6	84	93	9.0	60
5	53			30.0	196	0.76		2.2	637.20	85	91	9.0	60
6	54			37.5	196	0.74		2.15	643.70	87	92	8.5	60
7	53			45.0	196	0.72		2.05	649.9	87	93	8.0	60
8	52			52.5	196	0.68		1.90	655.2	88	93	8.0	60
9	53			60.0	197	0.70		2.00	661.8	88	93	8.0	60
10	53			67.5	197	0.84		2.50	667.1	89	93	10	60
11	53			75.0	197	0.94		2.7	674.5	89	93	11	60
12	53			82.5	197	1.00		2.8	681.3	89	93	11.5	60
STOP	ZERO			90.0					688.107				
	SPAN								695.33				
AVERAGE	53				195.4		0.8778	2.220	74.184		88.8		

PITOT LEAK CHECK:

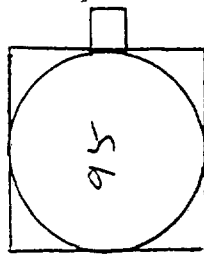
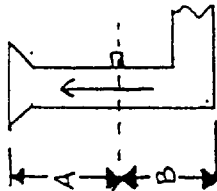
BEFORE: TOP ΔP= 0.46
 ΔP= 0.46
 AFTER: TOP ΔP= 0.46
 ΔP= 0.46

SAMPLE TRAIN LEAK:

BEFORE= 0.015 CFM@ 15 IN. HG.
 AFTER= 0.017 CFM@ 13 IN. HG.

COMMENTS: PURGE

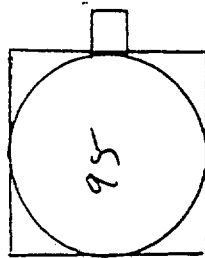
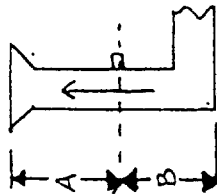
PLANT: DEXTEL
LOCATION: BAKERSFIELD
COUNTY: KERN
UNIT: GO-GEN
DATE: 5-28-92 pg 3
RUN NO/METHOD: PAH #2
COLD BOX NO.: 5
METER BOX NO.: 1
METER FACTOR: Y=1.0016
PITOT #/FACTOR: 0.840
PYROMETER #: 10-1
MAGNETIC FACTOR: AP 0-5 AH 0-5



FILTER NO. PAH-2
AMBIENT TEMP.: 79
BAROMETRIC PRESS., IN. HG.:
ASSUMED MOISTURE: 5%
HEATER BOX SETTING: 250
PROBE LENGTH, FT.: 10' #1
NOZZLE DIAMETER, IN.: 0.236
PROBE HEATER SETTING: 250
APPROX. WIND VEL., MPH: 0-10
SAMPLE BOX TEMP., (F): 660
DRI-RRITE WT.:
STATIC PRESSURE: "H2O

TRAVERSE POINT NUMBER	DISTANCE INCHES <i>Coll Temp</i>	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O		PRESSURE DIFF ORIFICE METER (ΔH) IN. H2O	DRY GAS SAMPLE VOLUME (VM), FT.	GAS SAMPLE TEMP. @ DRY GAS METER		PUMP VACUUM IN. HG.	TEMP. LAST IMPINGER (F)
						ΔP	√ΔP			INLET (Tm),	OUTLET (Tm)		
1	53			1024 00	197	0.800	0.68	2.25	688.107	89	88	9.0	660
2	53			7.5	196	0.70		2.00	694.90	89	91	10.0	660
3	52			15.0	200	0.84		2.40	700.60	88	93	10.5	660
4	52			22.5	200	0.90		2.60	707.35	90	96	11.0	660
5	53			30.0	200	1.10		3.15	715.4	90	96	12.0	660
6	53			37.5	200	1.05		3.0	722.6	90	92	11.5	660
7	53			45.0	199	1.05		3.0	728.5	90	92	11.5	660
8	54			52.5	197	1.00		2.40	735.8	89	90	10.0	660
9	55			60.0	198	0.84		2.40	743.1	89	92	10.5	660
10	55			67.5	197	0.98		2.80	749.1	89	91	11.2	660
11	54			75.0	199	1.05		3.0	755.9	89	91	11.7	660
12	54			82.5	200	1.00		2.85	763.1	89	91	11.5	660
STOP	ZERO			90.0					770.357				
AVERAGE	SPAN				198.6		0.958	2.64	82.250				
PITOT LEAK CHECK:													
BEFORE:				TOP ΔP=	197	BOTTOM ΔP=	0.9183	BEFORE=	2.43	CFM@		IN. HG.	
AFTER:				TOP ΔP=		BOTTOM ΔP=		AFTER=		CFM@		IN. HG.	
COMMENTS:										PURGE			

PLANT: DEX 2811
 LOCATION: BALCESSIC 10
 COUNTY: KERN
 UNIT: COGEN
 DATE: 5-28-92
 RUN NO/METHOD: 3 PAH 891
 COLD BOX NO.: 6
 METER BOX NO.: 1
 METER FACTOR: 1=1.0016 ΔHP=1.7957
 PITOT #/FACTOR: 0.846
 PYROMETER #: 70-1
 MAGNETIC FACTOR: ΔPO-5 ΔH0-5



FILTER NO. PAH-3
 AMBIENT TEMP.: 82
 BAROMETRIC PRESS., IN. HG.: 30.07
 ASSUMED MOISTURE: 576
 HEATER BOX SETTING: 250
 PROBE LENGTH, FT.: 10' 9 1/2
 NOZZLE DIAMETER, IN.: 0.236
 PROBE HEATER SETTING: 250
 APPROX. WIND VEL., MPH: 0-10
 SAMPLE BOX TEMP., (F): 660
 DRI-RRITE WT.:
 STATIC PRESSURE: -0.32 "H2O

TRAVERSE POINT NUMBER	DISTANCE INCHES	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O		PRESSURE DIFF ORIFICE METER (ΔH) IN. H2O	DRY GAS SAMPLE VOLUME (VM), FT.	GAS SAMPLE TEMP. @ DRY GAS METER		PUMP VACUUM IN. HG.	TEMP. LAST IMPINGER (F)
						ΔP	√ΔP			INLET (Tm),	OUTLET (Tm)		
1	53			1253	199	0.68		1.90	771.607	89	89	9.0	660
2	53			75	197	0.70		2.00	777.7	87	91	9.5	660
3	54			150	197	0.74		2.15	783.3	88	89	10.0	660
4	53			225	198	0.74		2.15	788.8	88	89	10.0	660
5	52			300	196	0.72		2.10	796.1	88	88	10	660
6	53			375	196	0.72		2.10	802.0	88	88	10	660
7	52			450	196	0.70		2.00	807.7	87	88	9.5	660
8	53			525	196	0.74		2.15	813.6	86	89	10.0	660
9	53			600	196	0.78		2.20	820.5	88	90	10.5	660
10	54			675	197	0.80		2.25	825.8	87	90	10.5	660
11	55			750	197	0.97		2.60	833.60	88	93	11.5	660
12	55			825	198	0.94		2.30	839.1	89	94	10.5	660
STOP	ZERO			90					845.486				
AVERAGE	SPAN				196.9			2.14	73.875		53.8		

PITOT LEAK CHECK:

BEFORE: TOP ΔP= 0.48
 ΔP= 0.48
 AFTER: TOP ΔP= 0.55
 ΔP= 0.54/5

BOTTOM ΔP= 0.62
 ΔP= 0.62
 BOTTOM ΔP= 0.32
 ΔP= 0.325

SAMPLE TRAIN LEAK:

BEFORE= 0.012 CFM@ 15 IN. HG.
 AFTER= 0.010 CFM@ 11 IN. HG.

PURGE

COMMENTS:

PLANT: D5x2511

LOCATION:

COUNTY:

UNIT :

DATE: 5-28-92

RUN NO METHOD: 3

COLD BOX NO.:

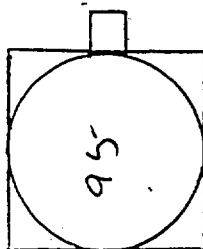
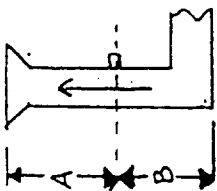
METER BOX NO.:

METER FACTOR: $Y = 1.0016$

PITOT #/FACTOR: 6.846

PYROMETER #: 10-1

MAGNETIC FACTOR: ΔP 0-5' ΔH 0-5'



FILTER NO. 1A4-3

AMBIENT TEMP.:

BARAMETRIC PRESS.,IN.HG.:

ASSUMED MOISTURE:

HEATER BOX SETTING:

PROBE LENGTH, FT. 10' 9/16SS

NOZZLE DIAMETER, IN.: 0.238

PROBE HEATER SETTING:

APPROX. WIND VEL., MPH:

SAMPLE BOX TEMP.,(F):

DRI-RRITE WT.:

STATIC PREASURE: "H2O

TRAVERSE POINT NUMBER	DISTANCE INCHES	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O		PRESSURE DIFF ORIFICE METER (ΔH)	DRY GAS SAMPLE VOLUME (VM), FT.	GAS SAMPLE TEMP. @ DRY GAS METER		PUMP VACUUM IN. HG	TEMP. LAST IMPINGER (F)
						ΔP	√ΔP			INLET (Tm),	OUTLET (Tm)		
1	53			1440	195	0.63		1.80	845.486	90.	91	9.5	<60
2	54			75	198	0.88		2.50	852.10	40.	96	9.0	<60
3	56			150	198	0.86		2.40	857.6	91	96	8.5	<60
4	58			225	198	0.86		2.40	864.7	91	93	8.5	<60
5	56			300	198	0.90		2.65	870.8	91	92	9.5	<60
6	54			375	198	1.05		3.00	878.0	89	91	10.5	<60
7	53			450	198	0.90		2.65	884.1	90	91	9.5	<60
8	52			525	198	0.88		2.50	891.9	89	90	9.0	<60
9	52			600	198	0.86		2.40	898.6	89	91	8.5	<60
10	53			675	198	0.86		2.40	905.2	90	91	8.5	<60
11	53			750	198	0.90		2.65	912.0	91	91	9.5	<60
12	53			825	198	0.90		2.65	919.0	90	91	9.5	<60
STOP	ZERO			90					925.945				
AVERAGE	SPAN				197.8		0.937	2.50	80.459	910	879		

PITOT LEAK CHECK:

BEFORE: TOP ΔP= _____ ΔP= _____

AFTER: TOP ΔP= _____ ΔP= _____

SAMPLE TRAIN LEAK:

BEFORE= _____ IN. HG.

AFTER= _____ IN. HG.

COMMENTS: _____

PURGE _____

METHOD 8 - PARTICULATE CLEAN-UP SHEET

Date 5/22/92
 Run No. 1-PAH
 Sample Recovered by RV
 Sample Box No. _____

Client Dexal Inc.
 WO No. DOZ-001
 Plant Dexal Cogeneration

PARTICULATE - FRONT HALF

Nozzle & Probe Acetone Wash
 Cyclone & Flask Acetone Wash

Lab No. _____ Residue: _____ mg
 Lab No. _____ Residue: _____ mg

Filter No.	Lab No.	Weight	
_____	_____	_____ mg	Total Filter Particulate _____ mg
_____	_____	_____ mg	
_____	_____	_____ mg	
_____	_____	_____ mg	Front Half Total _____ mg

MOISTURE

Impinger No.	Final Weight	Initial Weight	Net Weight
<u>1</u>	<u>896</u>	<u>100</u>	<u>196</u>
<u>2</u>	<u>0</u>	<u>0</u>	<u>0</u>

Total Imp. Gain 196 g

SILICA GEL

Container No.	Final Weight	Initial Weight	Net Weight
<u>Si Gel</u>	<u>268</u>	<u>235</u>	<u>33</u>
_____	_____	_____	_____
_____	_____	_____	_____

Total Si. Gel Gain 33 g

Total Moisture 229 g

METHOD 8 - PARTICULATE CLEAN-UP SHEET

Date 5/28/92
 In No. 2 - PAH
 Sample Recovered by RV
 Sample Box No. _____

Client Dexal
 WO No. DA-001
 Plant COGENERATION

PARTICULATE - FRONT HALF

Nozzle & Probe Acetone Wash
 Cyclone & Flask Acetone Wash

Lab No. _____ Residue: _____ mg
 Lab No. _____ Residue: _____ mg

Filter No.	Lab No.	Weight	
_____	_____	_____ mg	Total Filter Particulate _____ mg
_____	_____	_____ mg	
_____	_____	_____ mg	
_____	_____	_____ mg	Front Half Total _____ mg

MOISTURE

Impinger No.	Final Weight	Initial Weight	Net Weight
<u>1</u>	<u>485.0^W</u>	<u>100</u>	<u>385.28^W</u>
<u>2</u>	<u>326.8^W</u>	<u>0</u>	<u>0</u>
_____	_____	_____	_____
Total Imp. Gain			<u>273^W</u> <u>386.0</u> g

SILICA GEL

Container No.	Final Weight	Initial Weight	Net Weight
<u>Si Gel</u>	<u>321.5</u>	<u>285.5</u>	<u>36</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
Total Si. Gel Gain			<u>36.0</u> g
Total Moisture			<u>321.5</u> <u>309</u> g

818582-3335-00 7.1, 88

METHOD 8 - PARTICULATE CLEAN-UP SHEET

Date Dental 5/25/92
 Run No. 3 PHA
 Sample Recovered by RV
 Sample Box No. _____

Client Dental
 WO No. P2201
 Plant Orville, CA

PARTICULATE - FRONT HALF

Nozzle & Probe Acetone Wash	Lab No. _____	Residue: _____ mg
Cyclone & Flask Acetone Wash	Lab No. _____	Residue: _____ mg

Filter No.	Lab No.	Weight	
_____	_____	_____ mg	Total Filter Particulate _____ mg
_____	_____	_____ mg	
_____	_____	_____ mg	
_____	_____	_____ mg	Front Half Total _____ mg

MOISTURE

Impinger No.	Final Weight	Initial Weight	Net Weight
<u>1</u>	<u>348.5</u>	<u>200</u>	<u>248.5</u>
<u>2</u>	<u>0</u>	<u>0</u>	<u>0</u>
_____	_____	_____	_____

Total Imp. Gain 248.5 g

SILICA GEL

Container No.	Final Weight	Initial Weight	Net Weight
<u>Si 64</u>	<u>350</u>	<u>319.4</u>	<u>30.6</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Total Si. Gel Gain 30.6 g

Total Moisture 276.1 g

CLIENT: DexcellDATE: 5-28-92UNIT : COGENJOB NO.: W02-001METHOD: FORMIC ALHYDESAMPLE ID: DEX-CG-Form-2

BARO = 30.02

Time SAMPLE	DATA	SET POINT CC/min	ACTUAL Flow	AMBIEN Temp			
00	856	53	248	75.8			
10	906	53	248	74.3			
20	916	53	248	74.4			
30	926	53	248	75.8			
40	936	53	248	75.0			
50	946	53	248	75.2			
60	956	53	248	75.5			
70	1006	53	248	75.8			
80	1016	53	248	76.4			
90	1026	53	248	76.1			
100	1036	53	248	77.4			
110	1046	53	248	78.8			
STOP 120	1056						
AVERAGE		53	248	75.9			
CALIBRATION CC/min							
		ROTO setting	C ₁	C ₂	C ₃	Avg	
BEGINNING		53	248	248	248	248	} 250.9
ENDING			252	253	256	253.7	

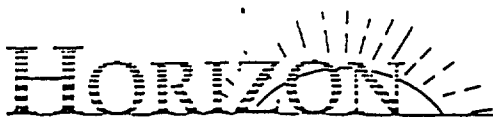
BEGINNING leak ✓ - Roto = Ø (ok)

CLIENT: DexellDATE: 5-28-92UNIT : COGENJOB NO.: W02-001METHOD: Formaldehyde #3

SAMPLE ID: _____

		Rotometer		SKC	Ambient		
Time		cc/min	cc/min		°F		
		5					
00	1339 1334 R*	53	256		82.5		
10	1344 1344 R*	53	256		84.2		
20	1354 1354 R*	53	256		84.3		
30	1409	53	256		85.3		
40	1419	53	256		86.1		
50	1429	53	256		88.1		
60	1439	53	256		88.3		
70	1449	53	256		86.8		
80	1459	53	256		87.2		
90	1509	53	256		86.8		
100	1519	53	256		85.6		
110	1529	53	256		86.7		
STOP 110	1539						
		CALIBRATION cc/min					
		C1	C2	C3	Avg		
Beginning		0.257	0.256	0.256	256	} 258.5 R*	
Ending		0.261	0.261	0.261	261		

Beg leak ✓ - OK
End leak ✓ - OK



Air Measurement Services

SAMPLE DATA SHEETS

DATE: 5/28/92

RUN NO.: #1, 2 & 3

CLIENT: DEXZEL

LOCATION: BARTERSFIELD, CA

PROJECT NO.: DDZ-003

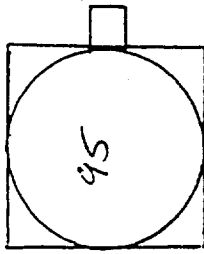
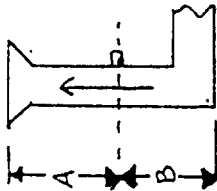
AMBIENT TEMP: 90°

OPERATOR: AF

SORBENT TYPE	PUMP NO.	START TIME	FINISH TIME	ELAPSED TIME	COMMENTS
11 - TDLAC BTX #1		0900	1000	1 hr	150 cc/r
TXR #2		1005	1105	1 hr	
BTX #3		1108	1208	1 hr	

REMARKS: All bags taken during PAH #2 run

PLANT: DECEL
 LOCATION: BATES 515.10
 COUNTY: KERN
 UNIT: COGEN
 DATE: 5-27-92
 RUN NO/METHOD: 1 NH3
 COLD BOX NO.:
 METER BOX NO.: 2 $\Delta H = 1.7041$
 METER FACTOR: Y = 0.9788
 PITOT #/FACTOR: NA
 PYROMETER #: NA
 MAGNETIC FACTOR: ΔP NA ΔH



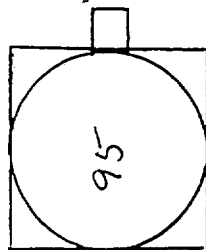
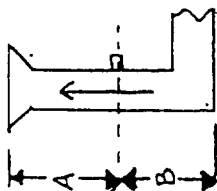
FILTER NO. NA
 AMBIENT TEMP.: 85
 BAROMETRIC PRESS., IN. HG.: 30.05 30.07
 ASSUMED MOISTURE: 5%
 HEATER BOX SETTING: NA
 PROBE LENGTH, FT.: 5' 9/16"
 NOZZLE DIAMETER, IN.: NA
 PROBE HEATER SETTING: NA
 APPROX. WIND VEL., MPH: 0-10
 SAMPLE BOX TEMP., (F): 60
 DRI-RITE WT.: —
 STATIC PRESSURE: — "H2O —

TRAVERSE POINT NUMBER	DISTANCE INCHES	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O	HEAD IN. H2O	DIFF ORIFICE METER (ΔH)	DRY GAS SAMPLE VOLUME (VM), FT.	GAS SAMPLE TEMP. @ DRY GASMETER INLET (Tm), (Tm)	PUMP VACUUM IN. HG.	TEMP. LAST IMPINGER (F)
Center of Stack				1748 00	NA	NA	NA	1.7	580.575	96	100	60
				05								
				1758 10				1.70	588.40	99	104	60
				15								
				1808 20				1.70	595.20	99	103	60
				25								
				1818 30				1.70	603.90	98	102	60
				35								
				1828 40				1.70	610.90	99	103	60
				45								
				1838 50				1.70	618.40	98	103	60
				55								
STOP	ZERO			1848 60	V	V	V		626.557			
	SPAN											
AVERAGE				60 min				1.70	45.982		100.3	

PITOT LEAK CHECK:				SAMPLE TRAIN LEAK:			
BEFORE:	TOP ΔP =	NA	BOTTOM ΔP =	NA	BEFORE =	0.017	CFM @ 15" IN. HG.
AFTER:	ΔP =	NA	ΔP =	NA	AFTER =	0.01	CFM @ 6" IN. HG.
	TOP ΔP =	NA	BOTTOM ΔP =	NA	COMMENTS:		
	ΔP =	NA	ΔP =	NA	PURGE /850 - 1910		

PLANT: DEXELL
LOCATION: BALCONSFIELD
COUNTY: KERN
UNIT: CO-GEN
DATE: 5-28-92
RUN NO./METHOD: 2 NH3
COLD BOX NO.: 2
METER BOX NO.: 2
METER FACTOR: Y = 0.9788 $\Delta H^0 = -1704$
PITOT #/FACTOR: N/A
PYROMETER #: N/A
MAGNETIC FACTOR: ΔP ΔH 0-5

FILTER NO.: NA
AMBIENT TEMP.: 80
BAROMETRIC PRESS., IN. HG.: 30.05
ASSUMED MOISTURE: 5%
HEATER BOX SETTING: —
PROBE LENGTH, FT.: 5' 9/16
NOZZLE DIAMETER, IN.: NA
PROBE HEATER SETTING: NA
APPROX. WIND VEL., MPH: 0-10
SAMPLE BOX TEMP., (F): 660
DRI-RRITE WT.:
STATIC PREASURE: NA "H2O



TRAVERSE POINT NUMBER	DISTANCE INCHES	O ₂ (%)	CO ₂ (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H ₂ O		PRESSURE DIFF ORIFICE METER (ΔH)	DRY GAS SAMPLE VOLUME (VM), FT. ³	GAS SAMPLE TEMP. @ DRY GAS METER		PUMP VACUUM IN. HG	TEMP. LAST IMPINGER (F)
						ΔP	√ΔP			INLET (Tm),	OUTLET (TM)		
Center				1100 sec	N/A	N/A	N/A	IN. H ₂ O 1.70	640.697	90	92	8	< 60
				10				1.7	647.1	91	92	8	60
				20				1.7	655.0	91	91	8	< 60
				30				1.7	662.5	91	91	8	60
				40				1.7	671.5	90	90	8	< 60
				50				1.7	678.3	90	91	8	60
				STOP 60					685.980				
	ZERO							1.70	45.283		90.8		
	SPAN												
AVERAGE													

PITOT LEAK CHECK:

BEFORE: TOP ΔP = N/A BOTTOM ΔP = N/A

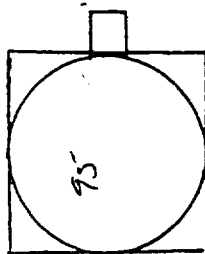
AFTER: TOP ΔP = N/A BOTTOM ΔP = N/A

SAMPLE TRAIN LEAK:

BEFORE = 0.005 CFM @ 15 IN. HG.

AFTER = 0.007 CFM @ 10 IN. HG.

COMMENTS: PURGE LROZ - 4922



TRAVERSE POINT NUMBER	DISTANCE INCHES	O ₂ (%)	CO ₂ (%)	SAMPLE TIME MIN.	STACK TEMP. (T _s), F	VELOCITY IN. H ₂ O		PRESSURE DIFF ORIFICE METER (ΔH)	DRY GAS SAMPLE VOLUME (VM), FT. 	GAS SAMPLE TEMP. @ DRY GAS METER		PUMP VACUUM IN. HG	TEMP. LAST IMPINGER (F)
						ΔP	√ΔP			INLET (T _m),	OUTLET (T _m)		
				1445	NA	NA	NA	1.7	701.687	93	92	8	<60
				16				1.7	709.2	93	94	8	<60
				20				1.7	716.6	93	94	8	<60
				30				1.7	724.6	94	94	8	<60
				40				1.7	733.3	94	94	8	<60
				50				1.7	740.4	93	94	8	<60
				STOP	60				748.803				
	ZERO							1.7	747.116		93.4		
	SPAN												
AVERAGE													
PITOT LEAK CHECK:									SAMPLE TRAIN LEAK:				
BEFORE:									CFM@ 15 IN. HG.				
AFTER:									CFM@ 10 IN. HG.				
COMMENTS:									PURGE 1547 - 1607				

1000. 347-2717 x 765
- 60318-3082220.5-

METHOD 8 - PARTICULATE CLEAN-UP SHEET

Date 5/22/92
 Run No. 1-NH3
 Sample Recovered by AP
 Sample Box No. _____

Client Dexzel Inc
 WO No. D02-001
 Plant Dexzel Corporation

PARTICULATE - FRONT HALF

Nozzle & Probe Acetone Wash
 Cyclone & Flask Acetone Wash

Lab No. _____ Residue: _____ mg
 Lab No. _____ Residue: _____ mg

Filter No.	Lab No.	Weight	
_____	_____	_____ mg	Total Filter Particulate _____ mg
_____	_____	_____ mg	
_____	_____	_____ mg	
_____	_____	_____ mg	Front Half Total _____ mg

MOISTURE

Impinger No.	Final Weight	Initial Weight	Net Weight
<u>1</u>	<u>226.5</u>	<u>200</u>	<u>26.5</u>
<u>2</u>	_____	_____	_____
_____	_____	_____	_____
Total Imp. Gain			<u>26.5</u> g

SILICA GEL

Container No.	Final Weight	Initial Weight	Net Weight
<u>Si-600</u>	<u>289.7</u>	<u>282.7</u>	<u>7.0</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
Total Si. Gel Gain			<u>7.0</u> g
Total Moisture			<u>27.5</u> g

METHOD 8 - PARTICULATE CLEAN-UP SHEET

Date 5/28/92
 In No. 2-NH3
 Sample Recovered by RV
 Sample Box No. _____

Client Dexzel
 WO No. DOZ-001
 Plant Cogenaration

PARTICULATE - FRONT HALF

Nozzle & Probe Acetone Wash
 Cyclone & Flask Acetone Wash

Lab No. _____ Residue: _____ mg
 Lab No. _____ Residue: _____ mg

Filter No.	Lab No.	Weight	
_____	_____	_____ mg	Total Filter Particulate _____ mg
_____	_____	_____ mg	
_____	_____	_____ mg	
_____	_____	_____ mg	Front Half Total _____ mg

MOISTURE

Impinger No.	Final Weight	Initial Weight	Net Weight
<u>142</u>	<u>273.5</u>	<u>200</u>	<u>73.5</u>
_____	_____	_____	_____
_____	_____	_____	_____

Total Imp. Gain 73.5 g

SILICA GEL

Container No.	Final Weight	Initial Weight	Net Weight
<u>Si gel</u>	<u>284.10</u>	<u>268.3</u>	<u>15.7</u>
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Total Si. Gel Gain 15.7 g

Total Moisture 79.2 g

ORSAT DATA SHEET METHOD 3

Facility: Dexzel Cogeneration

Job #: DDZ-001

Source: COGENERATION STACK

Date: 5/27/92

Run #: 1

By: RV

Gas	Run	1		2		3		Average Net Volume
		Actual Reading	Net	Actual Reading	Net	Actual Reading	Net	
CO ₂			36		36		36	36
O ₂ (Net is Actual O ₂ minus Actual CO ₂ Reading)		18.2	14.6	18.2	14.6	18.2	14.6	14.6
CO (Net is Actual CO minus Actual O ₂ reading)								
N ₂ (Net is 100 minus Actual CO reading)								

ORSAT DATA SHEET METHOD 3

Facility: Detroit Cogeneration

Job #: D02-001

Source: Cogeneration Stack

Date: 5/28/92

Run #: 2

By: RV

Gas \ Run	1		2		3		Average Net Volume
	Actual Reading	Net	Actual Reading	Net	Actual Reading	Net	
CO ₂		36		36		36	36
O ₂ (Net is Actual O ₂ minus Actual CO ₂ Reading)	18.2	14.6	18.2	14.6	18.2	14.6	14.6
CO (Net is Actual CO minus Actual O ₂ reading)							
N ₂ (Net is 100 minus Actual CO reading)							

ORSAT DATA SHEET METHOD 3

Facility: Detroit Cogeneration

Job #: 202-001

Source: Cogeneration Smoke

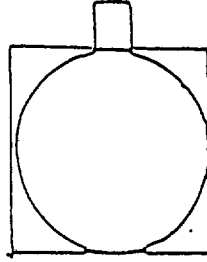
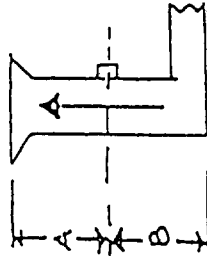
Date: 5/28/92

Run #: 3

By: RV

Gas \ Run	1		2		3		Average Net Volume
	Actual Reading	Net	Actual Reading	Net	Actual Reading	Net	
CO ₂		3.7		3.6		3.7	3.7
O ₂ (Net is Actual O ₂ minus Actual CO ₂ Reading)	18.0	14.3	18.2	14.6	18.2	14.5	14.5
CO (Net is Actual CO minus Actual O ₂ reading)							
N ₂ (Net is 100 minus Actual CO reading)							81.8

DOZ-CO1



PLANT: DEXTEL
 LOCATION: BAZESFIELD
 COUNTY: KIEW
 UNIT: Energy Loss Valve Tank
 DATE: 5/29/92
 RUN NO/METHOD: 1 HES
 COLD BOX NO.: 10487
 METER BOX NO.: 4-1006
 METER FACTOR: 1.7759
 PITOT #/ FACTOR: —
 PYROMETER #: —
 MAGNEHEUC FACTOR: ΔP — ΔH SKC

FILTER NO. —
 AMBIENT TEMP.: —
 BARAMETRIC PRESS., IN. HG.: 29
 ASSUMED MOISTURE: 2%
 HEATER BOX SETTING: —
 PROBE LENGTH, FT.: 70
 NOZZLE DIAMETER, IN.: —
 PROBE HEATER SETTING: —
 APPROX. WIND VEL., MPH: 0-5
 SAMPLE BOX TEMP., (F): 90
 STATIC PREASURE: — "H₂O
 OFFSET: — in. PORT DIA.: — in. (M / F)

TRAVERSE POINT NUMBER	DISTANCE INCHES	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O		PRESSURE DIFF ORIFICE METER (ΔH) IN. H2O	DRY GAS SAMPLE VOLUME (VM), FT.	GAS SAMPLE TEMP. @ DRY - GAS METER		PUMP VACUUM IN. HG	TEMP. LAST IMPINGER (F)
						ΔP	√ΔP			INLET (Tm),	OUTLET (Tm)		
Style	START			0842				1.0847	927.002	74	73	41	
				0852					927.340	87	80	41	
				0902					927.691	84	81	41	
	SOP			0912					928.041				
				"					"		"		
				30 min					1,039		80		
	ZERO						pos cal	1.0647	2742				
	SPAN												
AVERAGE													
PITOT LEAK CHECK:								SAMPLE TRAIN LEAK:					
BEFORE:				TOP ΔP =		BOTTOM ΔP =		BEFORE =		CFM @		IN. HG.	
AFTER:				ΔP =		ΔP =		AFTER =		CFM @		IN. HG.	
								COMMENTS:		PURGE		15.	

PLANT: DEXCEL
LOCATION: DARESFIELD
COUNTY: KEWA
UNIT: Terry Lee Wash Truck
DATE: 5/25/92
RUN NO/METHOD: 2 H₂S
COLD BOX NO.:
METER BOX NO.: 1
METER FACTOR: $y = +.0074$ $WC = 1.7959$
PITOT #/FACTOR: 1.0433
PYROMETER #:
MAGNETHEUIC FACTOR: $\Delta P - \Delta H$ SEC

FILTER NO. _____

AMBIENT TEMP.: _____

BAROMETRIC PRESS., IN. HG.: _____

ASSUMED MOISTURE: _____

HEATER BOX SETTING: _____

PROBE LENGTH, FT. _____

NOZZLE DIAMETER, IN.: _____

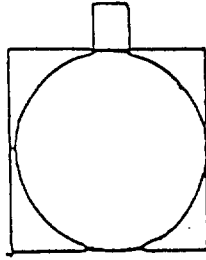
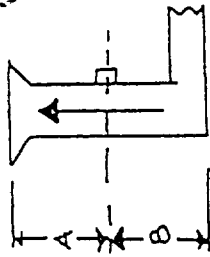
PROBE HEATER SETTING: _____

APPROX. WIND VEL., MPH: _____

SAMPLE BOX TEMP., (F): _____

STATIC PREASURE: _____

OFFSET: _____ in.



MAGNETIC FACTOR: $\Delta P - \Delta H$ SEC

TRAVERSE POINT NUMBER	DISTANCE INCHES	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O		PRESSURE DIFF ORIFICE METER (ΔH) IN. H2O	DRY GAS SAMPLE VOLUME (VM), FT.	GAS SAMPLE TEMP. @ DRY GAS METER		PUMP VACUUM IN. HG	TEMP. LAST IMPINGING (F)
						ΔP	√ΔP			INLET (Tm), °F	OUTLET (Tm), °F		
				START →	0956			1.054	928.901	85	84	1	
					1006				929.250	85	84	1	
					1016				929.598	84	83	1	
				STOP	1026				929.946				
								1.054	1.045		84		
									29.541				
	ZERO												
	SPAN												
AVERAGE													

PITOT LEAK CHECK:

BEFORE: TOP ΔP = _____
ΔP = _____

AFTER: TOP ΔP = _____
ΔP = _____

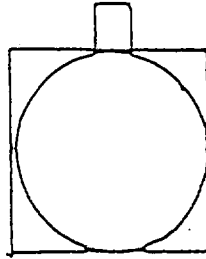
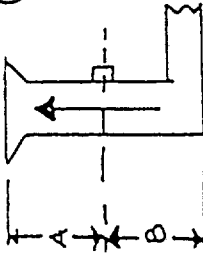
SAMPLE TRAIN LEAK:

BEFORE = 0 CFM @ 4.5 IN. HG.
AFTER = 0 CFM @ 4.5 IN. HG.

COMMENTS: PURGE 15 min

NOV 1964

PLANT:	DEXCEL
LOCATION:	BARKSFIELD
COUNTY:	KEEN
UNIT:	TERRY LEE WEST TOWN
DATE:	5/29/92
RUN NO/METHOD:	3 / HCS
COLD BOX NO.:	-
METER BOX NO.:	1
METER FACTOR:	y = 1.0016 H ₂ O 1.7959
PITOT #/FACTOR:	-
PYROMETER #:	-
MAGNETIC FACTOR:	ΔP - ΔH SKC



FILTER NO.:
 AMBIENT TEMP.:
 BARAMETRIC PRESS.,IN.HG.:
 ASSUMED MOISTURE:
 HEATER BOX SETTING:
 PROBE LENGTH,FT.:
 NOZZLE DIAMETER,IN.:
 PROBE HEATER SETTING:
 APPROX.WIND VEL.,MPH:
 SAMPLE BOX TEMP.,(F):
 STATIC PREASURE:
 OFFSET: in.

OFFSET: (in.) PORT DIA.: (in.) (M / F)

OFFSET: (in.

[illegible]

TRAGE	PITOT LEAK CHECK:
-------	-------------------

BEFORE:

TOP ΔP=

AFTER:

$$\frac{\text{TOP } \Delta P}{\Delta P} =$$

SAMPLE TRAIN LEAK:

BEFORE= 0 CFM@ 4 IN. HG.

AFTER= 0 CFM@ 4 IN. HG.

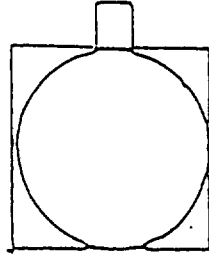
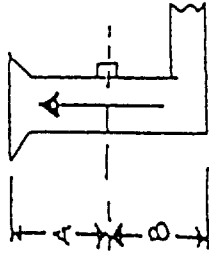
COMMENTS:

PURGE 3mm



DUC-001

PLANT: Dexel
 LOCATION: BARREFIELD CR
 COUNTY: Kern
 UNIT: FERNER WASH TANK
 DATE: 5/24/92
 RUN NO/METHOD: 1 H2S
 COLD BOX NO.: 2
 METER BOX NO.: 10998
 METER FACTOR: 1.0386
 PITOT #/FACTOR: 1.0386
 PYROMETER #: -
 MAGNEHEUC FACTOR: ΔP - ΔH SKC



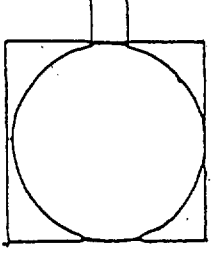
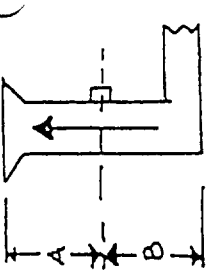
FILTER NO.: -
 AMBIENT TEMP.: -
 BARMETRIC PRESS., IN. HG.: -
 ASSUMED MOISTURE: 2%
 HEATER BOX SETTING: -
 PROBE LENGTH, FT.: teflon
 NOZZLE DIAMETER, IN.: -
 PROBE HEATER SETTING: -
 APPROX. WIND VEL., MPH: 0-5
 SAMPLE BOX TEMP., (F): 85°
 STATIC PREASURE: - "H2O
 OFFSET: - in. PORT DIA.: - in. (M / F)

TRAVERSE POINT NUMBER	DISTANCE INCHES	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O		PRESSURE DIFF ORIFICE METER (ΔH) IN. H2O	DRY GAS SAMPLE VOLUME (VM), FT.	GAS SAMPLE TEMP. @ DRY- GAS METER		PUMP VACUUM IN. HG.	TEMP. LAST IMPINGER (F)
						ΔP	√ΔP			INLET (Tm), 82	OUTLET (Tm) 82		
		START	—	0907				1.044	759.908	82	82	1	
				0917					760.262	85	82	1	
				0927					760.615	92	86	1	
				0937					760.942	90	87	1	
				0947					761.306	88	87	1	
				0957				1	761.669	88	87		
				1007					762.032				
	ZERO	STOP	—						=		=		
	SPAN							1.034	2.124		86		
AVERAGE													
PITOT LEAK CHECK:													
BEFORE:						BOTTOM ΔP=		BEFORE=		SAMPLE TRAIN LEAK:			
						ΔP=				CFM@		7 IN. HG.	
AFTER:						BOTTOM ΔP=		AFTER=		CFM@		7 IN. HG.	
						ΔP=				COMMENTS:			
										PURGE 15			

11002000

10-1-201

PLANT: Dexzel
LOCATION: Barefield CA
COUNTY: KEEN
UNIT: Flare West Tank
DATE: 5/25/92
RUN NO/METHOD: 2 H₂S
COLD BOX NO.: -
METER BOX NO.: 244
METER FACTOR: 1 = 0.9788 HE = 1.7041
PITOT #/FACTOR: 1.0386
PYROMETER #: -
MAGNETIC FACTOR: ΔP - ΔH SEC



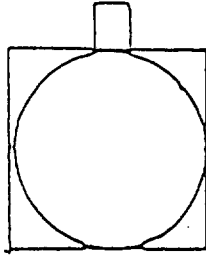
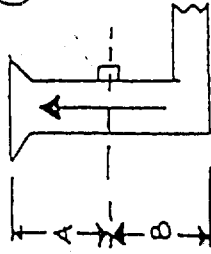
FILTER NO. -
AMBIENT TEMP.: -
BAROMETRIC PRESS., IN. HG.: -
ASSUMED MOISTURE: 2%
HEATER BOX SETTING: -
PROBE LENGTH, FT.: Teflon
NOZZLE DIAMETER, IN.: -
PROBE HEATER SETTING: -
APPROX. WIND VEL., MPH: 0-5
SAMPLE BOX TEMP., (F): 90
STATIC PREASURE: "H₂O
OFFSET: - in. PORT DIA.: - in. (M / F)

TRAVERSE POINT NUMBER	DISTANCE INCHES	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O		PRESSURE DIFF ORIFICE METER (ΔH) IN.H2O	DRY GAS SAMPLE VOLUME (VM), FT.	GAS SAMPLE TEMP. @ DRY GAS METER		PUMP VACUUM IN.HG	TEMP. LAST IMPINGER (F)
						ΔP	HEAD ΔP			INLET (Tm),	OUTLET (TM)		
			START	1039				103 1/2	762.586	90	89	1	
				1049					762.944	90	89	1	
				1059					763.301	90	89	1	
				1109					763.676	91	89	1	
				1119					764.042	91	90	1	
				1129					764.397	91	90		
				4:29 1140					764.793		=		
	ZERO								=				
	SPAN								2.207		90		
AVERAGE				6 min					62.502				
PITOT LEAK CHECK:													
BEFORE:						BOTTOM ΔP=		SAMPLE TRAIN LEAK: CFM@ 4.5 IN. HG.					
						ΔP=		CFM@ 4.5 IN. HG.					
AFTER:						BOTTOM ΔP=		COMMENTS: PURGE 15min					
						ΔP=							

HORIZON

101-001

PLANT: Dexzel
 LOCATION: Batesfield
 COUNTY: KEEN
 UNIT: Emk ~~3/29/92~~ Nbr D-4
 DATE: 3/29/92
 RUN NO/METHOD: 3 H₂S
 COLD BOX NO.: -
 METER BOX NO.: 2
 METER FACTOR: ~~1.001~~ 1.001
 PITOT #/FACTOR: 40.93870 HC = 1.7015
 PYROMETER #: Y=1.0386
 MAGNEHELIC FACTOR: ΔP - ΔH SEC



FILTER NO.: -
 AMBIENT TEMP.: -
 BARMETRIC PRESS., IN. HG.: -
 ASSUMED MOISTURE: 2%
 HEATER BOX SETTING: -
 PROBE LENGTH, FT.: 7.410
 NOZZLE DIAMETER, IN.: -
 PROBE HEATER SETTING: -
 APPROX. WIND VEL., MPH: 0-5
 SAMPLE BOX TEMP., (F): 90
 STATIC PREASURE: - "H₂O
 OFFSET: - in. PORT DIA.: - in. (M / F)

TRAVERSE POINT NUMBER	DISTANCE INCHES	O2 (%)	CO2 (%)	SAMPLE TIME MIN.	STACK TEMP. (Ts), F	VELOCITY IN. H2O		PRESSURE DIFF ORIFICE METER (ΔH) IN. H2O	DRY GAS SAMPLE VOLUME (VM), FT.	GAS SAMPLE TEMP. @ DRY GAS METER		PUMP VACUUM IN. HG	TEMP. LAST IMPINGER (F)
						ΔP	√ΔP			INLET (Tm), 95	OUTLET (Tm) 94		
				1202				1,014	765.451			1	
				1212					765.820	97	95	1	
				1222					766.178	99	96	1	
				1232					766.535	100	97	1	
				1242					766.904	101	98	1	
				1252					767.260	102	99	1	
	ZERO			1302					767.628				
	SPAN								=		98		
AVERAGE									2.177				
PITOT LEAK CHECK:						SAMPLE TRAIN LEAK:							
BEFORE:						BOTTOM ΔP=		BEFORE=		CFM@		6 1/2 IN. HG.	
AFTER:						ΔP=		AFTER=		CFM@		6 1/2 IN. HG.	
TOP ΔP=						BOTTOM ΔP=		COMMENTS:		PURGE		15.	
ΔP=						ΔP=							
TOP ΔP=						ΔP=							
ΔP=						ΔP=							

HORIZON

INTEGRATED BAG SAMPLING DATA FORM

Run number 1

Date 5-29-92 Plant Dexzel

Sampling location JERRY LEE NON VAPOR RECOVERY TANK T-402

Barometric pressure _____

Ambient temp. °F 75 TANK Stack temp. °F 132

Operator PH. AP. RV

OIL & WATER

[illegible]

a

$$\% \text{ Dev.} = \left(\frac{Q - Q_{avg}}{Q_{avg}} \right) 100; \text{ must be } \leq 10\%.$$

Tank level
about 1/2 full

leak ✓ - OK

INTEGRATED BAG SAMPLING DATA FORM

Run number 2

Date: 5-29-92

Plant Dierzell

Sampling location: JERRY LEE TANK. T-402

Barometric pressure

Ambient temp. ° 80

TANK
stack temp. °F 132

Operator

[illegible]

2

$$\% \text{ Dev.} = \left(\frac{Q - Q_{avg}}{Q_{avg}} \right) 100; \text{ must be } \leq 10\%.$$

TANK ABOUT
1/2 Full
END
4' from TOP

Quality Assurance Handbook M3-4.3

1/21/10 ✓ OK

INTEGRATED BAG SAMPLING DATA FORM

Run number 3

Date 5-29-92 Plant Dexzel

Sampling location: JERRY LEE TANK # T-402

Barometric pressure _____

Ambient temp. °F Stack temp. °F 130

Operator RH, AP, RV

Time	Traverse point	Rate meter flow, rate (Q), cm^3/min	% Dev. ^a
1105		300	
1115		300	
1125		300	
1135		300	
		Avg =	

$$\% \text{ Dev.} = \left(\frac{Q - Q_{\text{avg}}}{Q_{\text{avg}}} \right) 100; \text{ must be } \leq 10\%.$$

TANK LEVAL
4' FROM TOP

Quality Assurance Handbook M3-4.3

LEAK ✓ - OK

INTEGRATED BAG SAMPLING DATA FORM

Run number 1

Date. 5-29-92

Plant Dryas

Sampling location: FERNE 5395 (VAPOR RECOVERY)

Barometric pressure

Ambient temp. °F 75

TANK
Stack temp. °F 110

Operator 1224, AP, RV

CRUDE OIL

	Time	Traverse point	Rate meter flow, rate ($\dot{Q}$), cm^3/min	% Dev. ^a
	840	12" ABOVE TANK	300 cc/min	
	850 10		300	
	900 20		300	
910 STOP	30		300	
			Avg =	

$$\% \text{ Dev.} = \left(\frac{Q - Q_{\text{avg}}}{Q_{\text{avg}}} \right) 100; \text{ must be } \leq 10\%.$$

TANK level
1/6' FROM TOP

12/11/20 ✓ - OK

INTEGRATED BAG SAMPLING DATA FORM

Run number 2

Date: 5-29-92 Plant DOXCEL

Sampling location 7

Barometric pressure Ferne Tank 5395

Ambient temp. °R 80 Tank Stack temp. °C 110

Operator _____

Time	Traverse point	Rate meter flow, rate ($\dot{Q}$), cm^3/min	% Dev. ^a
915		300	
925		300	
935		306	
945		308	
		Avg =	

a

$$\% \text{ Dev.} = \left(\frac{Q - Q_{avg}}{Q_{avg}} \right) 100; \text{ must be } \leq 10\%.$$

TANK LEVEL
About 6' FROM TOP

1EAK ✓ -OK

INTEGRATED BAG SAMPLING DATA FORM

Run number 3

Date: 5-29-92 Plant

Sampling location: FERNE TANK # 5395

Barometric pressure _____

Ambient temp. °F Stack temp. °F 116

Operator _____

Time	Traverse point	Rate meter flow, rate (Q), cm^3/min	% Dev. ^a
1156		300	
1206		300	
1216		300	
1226		300	
		Avg =	

a

$$\% \text{ Dev.} = \left(\frac{Q - Q_{avg}}{Q_{avg}} \right) 100; \text{ must be } \leq 10\%.$$

TANK EVAL
6' FROM TOP

Quality Assurance Handbook M3-4.3

19AK ✓ - OK

APPENDIX D

Operating Data

TURBINE GAS GEN. SPEED 9766 RPM AT NOON

WED. 1200

	CTG MW	FUEL FLW CORR. SCFH	NH3 FLW # HR	EXH. FLW # HR	SCR INLT TEMP °F	SCR DP "H2O	H.P STM FLW # HR	CTG NOX WTR INJ. GPM
01	22.20	239020	5.39	537987	724	.6218	73668	16.30
30	22.28	240366	5.5	538072	724.6	.6253	73489	16.46
02	22.34	240882	4.9	540599	726	.6267	73838	16.45
30	22.26	240561	5.0	536847	725.8	.6260	73501	16.35
02	22.22	239683	4.97	538063	725.8	.6267	73571	16.29
30	22.19	239827	4.76	539860	725.2	.6267	73418	16.19
00	22.26	239197	5.43	538975	725.8	.6267	73025	16.08
00	22.22	240500	5.49	538031	725.2	.6260	72812	16.18
00	22.26	238862	5.72	537660	724.8	.6287	73609	16.12
00	22.21	239973	6.94	539627	725.4	.6300	73775	16.05
00	22.17	238387	6.84	535490	725.8	.6307	73041	16.24
00	22.22	239517	7.54	537061	726.2	.6333	73802	16.17
00	22.2	239742	7.74	539983	726.6	.6300	72429	16.14
330	22.25	239687	7.87	538103	725.8	.6280	72924	16.10
30	22.23	238748	7.36	538226	725.6	.6300	73559	16.03
330	22.2	239408	7.13	537132	726.2	.6280	73429	15.90
00		5/28	THUR.					
00	22.5	243237	6.24	540909	726.4	.6253	74198	16.36
00	22.52	242929	6.07	541861	726.2	.6247	74286	16.47
00	22.5	242812	5.68	541640	725.8	.6247	74006	16.44
00	22.48	242627	6.32	540960	725.8	.6227	74172	16.54
00	22.5	241878	6.05	541367	725.4	.6267	73541	16.20
30	22.5	241330	5.94	541435	725	.6227	74194	16.46
00	22.45	241483	5.81	539820	725.3	.6230	74008	16.25
00	22.35	241400	5.32	539954	725.3	.6267	74182	16.38
00	22.32	241048	5.87	539651	725.3	.6260	74047	16.26
330	22.20	239786	5.36	539820	725.2	.6263	73726	16.32
00	22.30	239894	5.10	540073	725.0	.6267	73892	16.35
00	22.27	240226	7.66	536390	725.2	.6273	74300	16.20
00	22.21	247931	5.29	539202	725	.6267	73627	16.04
00	22.20	247893	6.01	539287	725	.627	73628	16.05
00	22.18	247871	6.67	539567	725	.628	74453	16.07
00	22.20	239923	6.26	539659	725	.612	74282	16.06
1700	22.18	2475626	6.14	540109	725.2	.614	73401	16.1

APPENDIX E

Calibration Data

Magnehelic Gauge Bi-Monthly Calibration

0" - 1" Range

Date: 05-22-92

Barometric Pressure: 29.17

Calibrated by: A. Pecaut

Target	1.0"	1.0"
Magnehelic serial #	R90207MR96	R910710SC117
Leak Check (y/n):	Yes	Yes
	reference gauge	reference gauge
	0.20 0.20	0.20 0.20
	0.40 0.40	0.40 0.40
	0.60 0.59	0.60 0.60
	0.80 0.78	0.80 0.79
Correction Factor:	1.00 0.98	1.00 0.99

1.0169

1.0084

Date:

5/22/92

Calibrated by:

Paul D. H.

HORIZON

Magnehelic Gauge Calibration Data

0-5.0" Range

Date: 05-22-92

Barometric Pressure: 29.17 "Hg

Calibrated by: A. Pecaut

Reference serial # R81207CS28

R81117LG11

reference gauge

reference gauge

1.00 0.980

1.00 1.00

2.00 1.950

2.00 1.90

3.00 2.900

3.00 2.90

4.00 3.850

4.00 3.95

5.00 4.900

5.00 4.95

Corection Factor

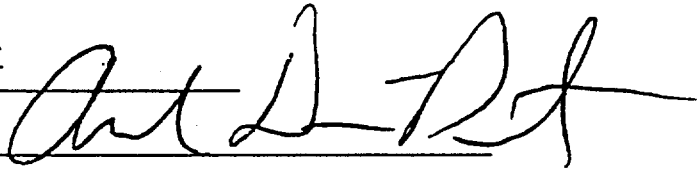
1.0288

1.0204

Date:

5/22/92

Calibrated by:



HORIZON

Magnehelic Gauge Bi-Monthly Calibration Data
0"-5" Range

Date: 01-10-92

Barometric Pressure: 29.23 "Hg

Calibrated by: A. Pecaut

RANGE		0-5.0"		0-5.0"		0-5.0"		0-5.0"		0-5.0"	
Magnehelic serial # R81207CS28		R81117LG11		R890412RR9		R89041319888		4911022MP159			
Leak Check (y/n): Yes		Yes		Yes		Yes		Yes			
reference	gauge	reference	gauge	reference	gauge	reference	gauge	reference	gauge	reference	gauge
1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2.0	2.1	2.0	2.1	2.0	2.1	2.0	2.1	2.0	2.1	2.0	2.0
3.0	3.1	2.9	3.0	3.0	3.1	3.0	3.1	3.0	3.1	3.0	2.9
=====											
Corection Factor		0.976		0.975		0.962		0.968		1.017	

Date: 1-16-92

Calibrated by: Ant D. Pef

Control Box Calibration Data

ate: 05-04-92 Calibrated by: A. Pecaut
 DGM number: 1 Barometric Pressure: 29.18

rifice setting (H)	Gas Volumes			Temperatures			Time (min)	Y	H ₀
	Wet Test (cu.ft)	Dry Gas Initial (cu.ft)	Dry Gas Final (cu.ft)	DGM Initial (F)	DGM final (F)	WTM (F)			
0.5	4.406	298.832	303.355	87	89	72	11	1.0022	1.7486
1	5.595	304.154	309.883	86	87	72	10	1.0007	1.7972
1	6.178	309.883	316.194	86	87	72	11	1.0031	1.7836
1	6.151	316.194	322.482	86	87	72	11	1.0023	1.7993
1.5	6.870	392.426	399.422	87	87	77	10	0.9965	1.8202
2	7.908	400.230	408.230	88	89	77	10	1.0046	1.8266
AVERAGE								1.0016	1.7959

alibrated by:

A. D. Pecaut

reviewed by:

Phil D. Heller

HORIZON

Control Box Calibration Data

Date: 06-24-92 Calibrated by: A. Pecaut

DGM number: 1 Barometric Pressure: 29.07

Gas Volumes

Temperatures Time

Y

SKC reading (lpm.)	Wet Test (cu.ft)	Dry Gas Initial (cu.ft)	Dry Gas Final (cu.ft)	DGM Initial (F)	DGM final (F)	WTM (F)	(min)	
1.05	1.134	75.998	77.088	81	81	78	30	1.0434
1.06	1.141	77.137	78.233	81	81	78	30	1.0441

AVERAGE								1.0437

Calibrated by:

Reviewed by:

Control Box Calibration Data

Date: 05-22-92 Calibrated by: A. Pecaut
DGM number: 2 Barometric Pressure: 29.27

Orifice setting (H)	Gas Volumes			Temperatures			Time	Y	He
	Wet Test (cu.ft)	Dry Gas Initial (cu.ft)	Dry Gas Final (cu.ft)	DGM Initial (F)	DGM final (F)	WTM (F)	(min)		
0.5	2.10708	537.702	539.852	72	75	74	5.00	0.9779	1.6298
1	5.81056	540.209	546.137	75	80	75	10	0.9823	1.7082
1	2.90138	546.137	549.117	79	81	75	5	0.9803	1.7048
1	8.07066	549.117	557.447	81	84	75	14	0.9800	1.7194
1.5	6.96546	557.917	565.151	83	87	75	10	0.9772	1.7585
2	7.99561	565.652	573.976	85	89	76	10	0.9754	1.7795
AVERAGE								0.9788	1.7041

Calibrated by: A. Pecaut
Reviewed by: Robert J. Halk

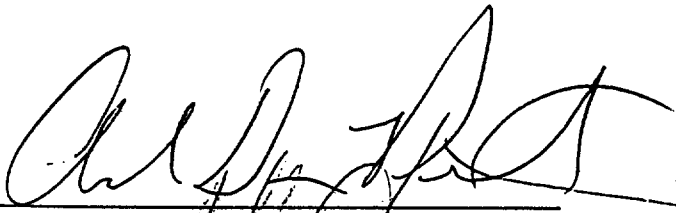
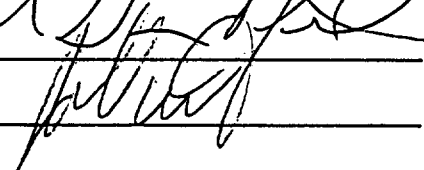
HORIZON

Control Box Calibration Data

Date: 06-24-92 Calibrated by: A. Pecaut
DGM number: 2 Barometric Pressure: 29.07

	Gas Volumes			Temperatures		Time		
SKC reading (lpm.)	Wet Test (cu.ft)	Dry Gas Initial (cu.ft)	Dry Gas Final (cu.ft)	DGM Initial (F)	DGM final (F)	WTM (F)	(min)	Y
1.05	1.149	336.093	337.200	76	78	78	30	1.0333
1.05	1.543	337.283	338.760	78	80	78	40	1.0439

AVERAGE								1.0386

Calibrated by: 
Reviewed by: 

Control Box Calibration Data

Date: 05-22-92
 Meter Box Number: 3
 Orifice Number: 1112
 GM Number: NA

Calibrated by: A. Pecaut
 Barometric Pressure: 29.27
 Wet Test Meter Cf: 0.9746

Orifice setting (H)	Gas Volumes			Temperatures			Time	Y	H _e
	Wet Test (cu.ft)	Dry Gas Initial (cu.ft)	Dry Gas Final (cu.ft)	DGM Initial (F)	DGM final (F)	WTM (F)	(min)		
0.5	2.916	561.355	564.364	89	90	74	7.0	0.9707	1.7049
1	6.352	564.662	571.202	88	91	74	11.0	0.9716	1.7744
1	2.887	571.202	574.161	90	91	74	5.0	0.9778	1.7716
1	3.458	574.161	577.722	91	91	74	6.0	0.9741	1.7765
1.5	7.020	578.038	585.233	90	93	74	10.0	0.9784	1.7945
2	8.090	585.587	594.158	92	94	74	10.0	0.9479	1.7967
AVERAGE								0.9701	1.7698

Calibrated by:

Reviewed by:

HORIZON

Thermocouple Calibration Data

Date: 3-24-92
 Calibrated by: A. Pecaut

Termocouple ID	Ice Water		Ambient Air		Boiling Water	
	reference	Tc	reference	Tc	reference	Tc
Cold Box #1	33	33	66	66	204	206
Cold Box #2	33	34	65	64	204	205
Cold Box #3	33	33	67	67	204	206
Cold Box #4	33	34	67	67	203	205
Cold Box #5	33	33	68	67	204	204
Filter Box #1	33	34	68	68	206	208
Filter Box #2	33	33	67	67	206	209
DGM #1 In	35	35	67	69	203	204
DGM #1 Out	34	35	67	68	202	203
DGM #2 In	34	34	67	68	202	203
DGM #2 Out	35	35	67	67	204	205
DGM #3 In	34	35	68	68	204	206
DGM #3 Out	33	33	68	67	204	204

Calibrated by: _____

Reviewed by: _____

HORIZON

Thermocouple Calibration Data

Date: 02/28/92
Calibrated by: A. Pecaut

Termocouple ID	Ice Water		Ambient Air		Boiling Water	
	reference	Tc	reference	Tc	reference	Tc
3-1	32	32	68	67	205	208
3-2	32	32	69	67	205	210
3-3	32	32	70	69	203	206
3-4	32	32	70	70	204	208
3-5	32	32	70	69	205	209
5-1	***	***	70	75	***	***
5-2	31	32	70	70	203	206
5-3	30	31	70	70	203	207
5-4	30	32	70	71	203	207
5-5	31	31	70	71	202	206

Calibrated by: _____

Reviewed by: _____

HORIZON

MANUFACTURER'S CALIBRATION CERTIFICATE

The following record shows the accuracy of your digital flowmeter
at tested flow rates compared to NBS (NIST) calibrated standard
TN 242118 TELEDYNE HFM-1A #1337.

CALIBRATION DATE: 01/18/91

INTERNAL UNIT #: 5548

CALIBRATION FLOW (ml/min)

50.21

498.71

2979.87

SERIAL #: 311114

% ERROR

-0.65

0.53

0.65

PRESSURE (mb): 1017

TEMPERATURE (C): 23

REL. HUMIDITY (%): 54

CALIBRATED BY: LVL

NOZZLE CALIBRATION

Date 5/22/91

Calibrated by AP

Nozzle identification number	D_1 , in.	D_2 , in.	D_3 , in.	ΔD , in.	D_{avg}
C-1	.142	.141	.143	.002	.142
C-2	.214	.215	.213	.002	.214
C-3	.307	.308	.308	.001	.308
C-4	.492	.496	.494	.004	.494

where:

$D_{1,2,3}$ = nozzle diameter measured on a different diameter, in.
Tolerance = measure within 0.001 in.

ΔD = maximum difference in any two measurements, in.
Tolerance = 0.004 in.

D_{avg} = average of D_1 , D_2 , and D_3 .

Nozzle calibration data.

NOZZLE CALIBRATION

Date 5/26/92

Calibrated by AP

Nozzle identification number	D_1 , in.	D_2 , in.	D_3 , in.	ΔD , in.	D_{avg}
GLASS #3	0.236	0.236	0.237	0.001	0.236
#13	0.236	0.237	0.237	0.001	0.237

where:

$D_{1,2,3}$ = nozzle diameter measured on a different diameter, in.
Tolerance = measure within 0.001 in.

ΔD = maximum difference in any two measurements, in.
Tolerance = 0.004 in.

D_{avg} = average of D_1 , D_2 , and D_3 .

Nozzle calibration data.

TYPE S PITOT TUBE INSPECTION DATA FORM

Tubing diameter, D_t 0.378 in.

Pitot Tube Assembly Level? Yes / No

Pitot Tube Openings Damaged? Yes / No

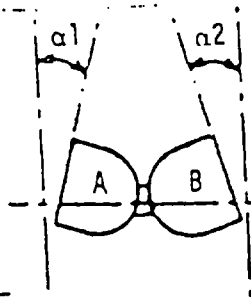
A-SIDE PLANE

NOTE:

$P_A =$ 0.563 in.

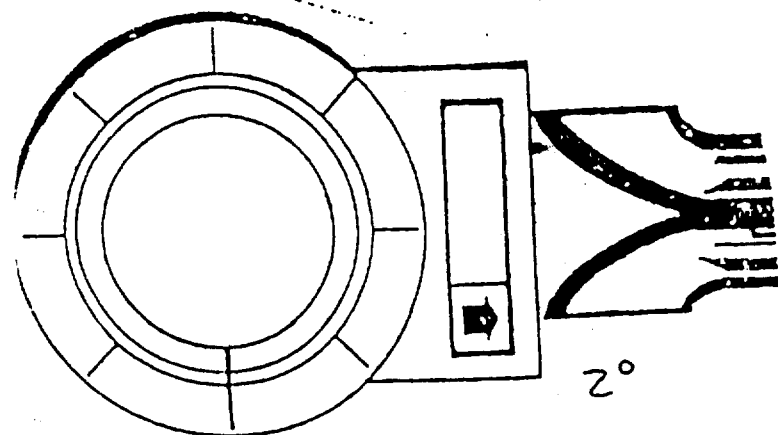
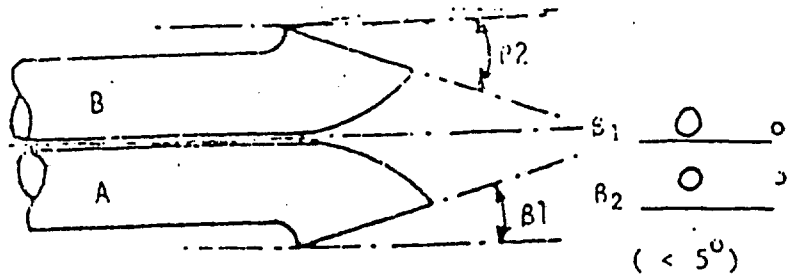
$P_B =$ 0.564 in.

$$\begin{cases} 1.05 D_t < P < 1.50 D_t \\ P_A = P_B \end{cases}$$



$$\begin{aligned} \alpha_1 &= \frac{2}{1}^\circ \\ \alpha_2 &= \frac{1}{1}^\circ \end{aligned}$$

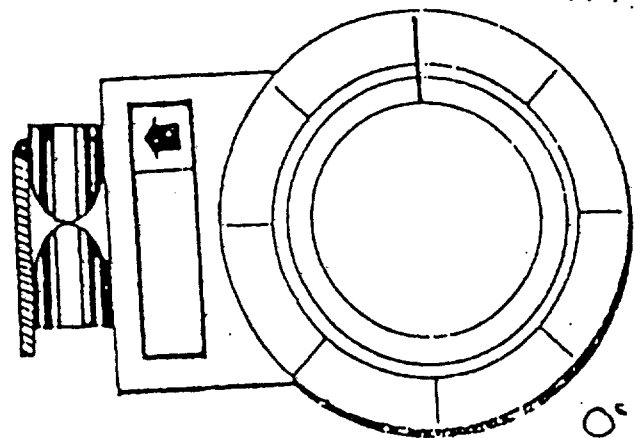
($< 10^\circ$)



Level Position to Find γ

$$Z = A \sin \gamma$$

0.035 in. ($< 1/8$ in.)



Level Position to find θ

$$W = A \sin \theta$$

0 in. ($< 1/32$ in.)

Comments Used to be pitot ID# S-3

Checked by: AP

Date: 11/22/91

Calibration Required? No

APPENDIX F

Calculations

Facility Deerl Cogeneration
 Source SMC
 Run 2-PAH

Job No. 102-001
 Date 7/7/92
 Calc/Review PK

SAMPLE CALCULATIONS

Particulate Isokinetic Sampling

1. Calculations for stack volume and Isokinetic Ratio

Time	Dry Gas Meter ft ³	Pitot ΔP , in. H ₂ O	Orifice ΔH , in. H ₂ O	Dry Gas Temp °F In Out	Stack Static Pressure in. H ₂ O	Stack Temp °F
------	----------------------------------	---	---	------------------------------	---	------------------

T	VM	ΔP	PM	TMI TMO	PST	TS
1. DN - Nozzle Diameter, inches					<u>0.236</u>	in.
2. PB = Barometric Pressure, inches Hg					<u>30.02</u>	in. Hg
3. TT = Net Sampling Time, minutes					<u>180</u>	min.
4. VM = VM final - VM initial = Sample Gas Volume, ft ³					<u>156.434</u>	ft ³
4A. VML = Use only if any final or intermediate leak check rate is over 0.02 cfm						

LI = Leak rate after any given sampling period, cfm

TLI = Total time of sampling period in which leak occurred, min.

VM = VM - [(L1 - 0.02) TL1 + (L2 - 0.02) TL2 + (L3 - 0.02) TL3 + L4 + 0.02) TL4]

= () - [(- 0.02)() + (- 0.02)() + (- 0.02)() + () + (- 0.02)()]

= () - [() + () + () + ()]

= () - () = _____ ft³

5. TM = Average Dry Gas Temperature at Meter, °F

TM = $\frac{\text{Avg. TMI} + \text{Avg. TMO}}{2}$ = 90 °F

6. PM = Average Orifice Pressure Drop, inches H₂O

PM = Avg. ΔH

= 243 ÷ 13.6 = _____ in. Hg

7. Volume of dry gas sampled at standard conditions, ^a dscf

VMSTD = $520 (Y) (VM) (PB + \frac{PM}{13.6})$
 $29.92 (TM + 460)$

Y = dry gas meter calibration factor

= $\frac{520 () () ()}{29.92 ()}$ = 149.518 ft³

Job No. D02-001
Run No. 2-PH

8. VW = Total Water Collected = gm H₂O Silica gel + ml Imp. H₂O = ml
() + () = 309

9. Volume of water vapor at standard conditions, scf

VW gas = 0.04715 × VW = scf = 0.04715 (309) = 14.569 ft³

10. Percent moisture in stack gas

$$\% M = \frac{100 \times \text{VW gas}}{\text{VMSTD} + \text{VW gas}} = \frac{100 (\underline{14.569})}{(\underline{149.518}) + (\underline{14.569})} = \frac{()}{()} = 8.88$$

$$= \underline{8.88} \%$$

11. Mole fraction of dry gas

$$\text{MD} = \frac{100 - \%M}{100} = \frac{100 - (\underline{8.88})}{100} = \underline{0.9112}$$

12. Molecular weight of dry stack gas

$$\text{MWD} = (\% \text{CO}_2 \times \frac{44}{100}) + (\% \text{O}_2 \times \frac{32}{100}) + [(\% \text{CO} + \% \text{N}_2) \times \frac{28}{100}]$$

$$= (\underline{3.6} \times 0.44) + (\underline{14.6} \times 0.32) + (\underline{81.8} \times 0.28)$$

$$= () + () + () = \underline{29.16} \text{ lb/lb mole dry}$$

12A. %EA = % Excess Air = $\frac{[(\% \text{O}_2 - 0.5 (\% \text{CO})) \times 100]}{[(0.264 (\% \text{N}_2))] - (\% \text{O}_2) + 0.5 (\% \text{CO})}$

$$= \frac{() \times 100}{[(0.264 ()) - () + 0.5 ()]}$$

$$= \frac{() \times 100}{() - () + ()} = \underline{\quad\quad\quad} \%$$

13. Molecular weight of wet stack gas

$$\text{MW} = \text{MWD} \times \text{MD} + 18 (1 - \text{MD})$$

$$= (\underline{29.16}) (\underline{0.9112}) + 18 (1 - \underline{0.9112})$$

$$= () + () = \underline{28.169} \text{ lb/lb mole wet}$$

14. AS, = Stack Area, square inches

$$\text{Circular, } = \left(\frac{\text{Stack diameter}}{2} \right)^2 \pi = \left(\frac{\underline{95}}{2} \right)^2 \pi = \underline{7088} \text{ sq. in.}$$

Rectangular, = Length × width = () () = sq. in.

15. PS = Stack Pressure, absolute, inches Hg = PB ± AV PST

PST = Stack static pressure

Job No. D02-001
Run No. 2-PAH

$$\text{PST in. Hg} = \frac{\text{PST in. H}_2\text{O}}{13.6} = \frac{30}{13.6} = 0.022 \text{ in. Hg}$$

$$\text{PS} = \text{PB} \pm \text{Avg. PST} = (0.022) (30.02) = 30.04 \text{ in. Hg}$$

$$16. \text{ TS} = \text{Average Stack Temperature, } 197^\circ\text{F} + 460 = 657^\circ\text{R}$$

$$\text{TS} = \text{Average TS} \quad \sqrt{\text{TS}_{\text{AV}} + 460} = 25.632$$

$$17. \text{ SDE}_{\text{AV}} = (\sqrt{\Delta P})_{\text{AV}} \times \sqrt{\text{TS}_{\text{AV}} + 460} = (0.9183) (25.632) = 23.538$$

$$18. \text{ Stack gas velocity at stack conditions, afpm}$$

$$\text{VS} = 5130^{(e)} \times C_p \times \text{Avg. (SDE)} \times \left[\frac{1}{\text{PS} \times \text{MW}} \right]^{\frac{1}{2}} = \text{afpm} \quad C_p = \text{pitot tube coefficient}$$

$$= 5130 \times (0.84) \times (23.538) \times \left[\frac{1}{(30.04)(28.169)} \right]^{\frac{1}{2}} = 3489 \text{ afpm}$$

$$19. \text{ Stack gas volumetric flow rate at standard conditions, }^c \text{ dscfm}$$

$$Q_s = \frac{520 \times \text{VS} \times \text{AS} \times \text{MD} \times \text{PS}}{(29.92)(144)(\text{TS} + 460)} = \text{dscfm}$$

$$= \frac{520 (3489) \times (7088) \times (0.9112) \times (30.04)}{29.92 \times 144 (657)} = 124,186 \text{ dscfm}$$

$$20. \text{ Stack gas volumetric flow rate at stack conditions, }^d \text{ acfm}$$

$$Q_a = \frac{29.92 \times Q_s (\text{TS} + 460)}{(520) (\text{PS}) (\text{MD})} = \text{acfm}$$

$$= \frac{29.92 (124,186) (657)}{520 (30.04) (0.9112)} = 171,736 \text{ acfm}$$

$$21. \text{ Percent isokinetics}$$

$$\% I = \frac{1,039^{(f)} \times (\text{TS} + 460) \times \text{VMSTD}}{\text{VS} \times \text{TT} \times \text{PS} \times \text{MD} \times (\text{DN})^2} = 1067$$

^a Dry standard cubic feet at 68°F (528R) and 29.92 in. Hg.

^b Standard conditions at 68°F (528R) and 29.92 in. Hg.

^c Dry standard cubic feet per minute at 68°F (528) and 29.92 in. Hg.

^d Actual cubic feet per minute

$$^e 5130 = 85.5 \frac{\text{ft}}{\text{sec}} \left[\frac{(1\text{b}/1\text{b mole})(\text{in. Hg})}{(^{\circ}\text{R})(\text{in. H}_2\text{O})} \right]^{\frac{1}{2}} \times 60 \text{ sec/min}$$

$$^f 1039 = \frac{29.92 \text{ in. Hg}}{528 \text{ DegR}} \times \frac{144 \text{ in.}^2}{\text{ft}^2} \times \frac{4}{\pi} \times 100$$

EMISSION RATE Example Calculations

1. PAH - Run #1

$$\text{Naphthalene} = \frac{4.7 \mu\text{g}}{\text{sample}} \times \frac{\text{sample}}{138.64 \text{ dscf}} \times \frac{126843 \text{ dscf}}{\text{min}} \times \frac{60 \text{ min}}{1 \text{ hr}} \times \frac{1 \text{ mg}}{1000 \mu\text{g}}$$
$$\text{mg/hr} = 258 \text{ mg/hr}$$

2 Aldehydes - Formaldehyde - Run #1

$$\text{mg/hr} = \left(\frac{1.72 \mu\text{g/sample} - 1.11 \mu\text{g/blank}}{1.04 \text{ dscf/sample}} \right) \times \frac{126,843 \text{ dscf}}{\text{min}} \times \frac{60 \text{ min}}{1 \text{ hr}} \times \frac{1 \text{ mg}}{1000 \mu\text{g}}$$

$$\text{mg/hr} = 4464 \text{ mg/hr}$$

3. BENZENE - Run #1

$$\text{lbs/hr} = 0.00034 \text{ ppm} \times 0.0422 \times 78 \times \frac{1 \text{ m}^3}{35.31 \text{ ft}^3} \times \frac{1 \text{ lb}}{453,590 \text{ mg}} \times \frac{124,020 \text{ dscf}}{\text{min}}$$
$$\times \frac{60 \text{ min}}{1 \text{ hr}} = 0.00052 \text{ lbs/hour}$$

4. Ammonia - Run #1

$$\text{lbs/hr} = 0.72 \text{ mg/sample} \times \frac{\text{SAMPLE}}{51.345 \text{ dscf}} \times \frac{126843 \text{ dscf}}{\text{min}} \times \frac{60 \text{ min}}{1 \text{ hr}} \times \frac{1 \text{ lb}}{453,590 \text{ mg}}$$

$$\text{lbs/hr} = 0.2353 \text{ lbs/hour}$$

WEIGHT FRACTION CALCULATIONS

In order to convert tank headspace chemical concentrations for the AB 2588 program from parts per million volume to parts per million weight, the tank headspace sample will be analyzed for C₁ through C₆ hydrocarbons in addition to the specific AB 2588 listed substances. The following calculations will be followed to convert the volumetric concentrations to weight fractions.

First the total nonmethane hydrocarbon concentration will be determined.

$$C_{NMHC} = \sum_{n=2}^6 C_n$$

where:

C_{NMHC} = Total volumetric nonmethane hydrocarbon concentration
 C_n = Volumetric concentration of C₂ to C₆ hydrocarbons

Next, an average molecular weight of the nonmethane hydrocarbons will be determined. This is accomplished by multiplying the molecular weight of the C₂ to C₆ hydrocarbons by a ratio of each hydrocarbon concentration to the total nonmethane hydrocarbon concentration. The equation to be used is presented below.

$$MW_{NMHC} = \frac{\sum_{n=2}^6 C_n MW_n}{C_{NMHC}}$$

where:

MW_{NMHC} = Average molecular weight of total nonmethane hydrocarbons
 MW_n = Molecular weight of each C₂ to C₆ hydrocarbon

MW_{C_2} = 30 lb/lb-mole
 MW_{C_3} = 44 lb/lb-mole
 MW_{C_4} = 58 lb/lb-mole
 MW_{C_5} = 72 lb/lb-mole
 MW_{C_6} = 86 lb/lb-mole

The molecular weights of C_2 to C_6 hydrocarbons were calculated using the carbon to hydrogen ratio of $C_N H_{2N+2}$.

Next, an average total hydrocarbon molecular weight is calculated. The average molecular weight is simply the concentration of the methane and nonmethane hydrocarbons multiplied by their respective molecular weights, with the sum divided by the total hydrocarbon concentration. The equation reads as follows:

$$MW_{THC} = \frac{(C_{CH_4})(MW_{CH_4}) + (C_{NMHC})(MW_{NMHC})}{C_{CH_4} + C_{NMHC}}$$

where:

- C_{CH_4} = Volumetric concentration of methane
 MW_{CH_4} = Molecular weight of methane (16 lb/lb-mole)

Finally, the weight fraction of each AB 2588 compound can be determined. The following equation is utilized.

$$Wt_i = \frac{(C_i)(MW_i)}{(C_{CH_4} + C_{NMHC})(MW_{THC})}$$

where:

- Wt_i = Weight fraction of the AB 2588 compound
 C_i = Volumetric concentration of the AB 2588 compound
 MW_i = Molecular weight of the AB 2588 compound

APPENDIX G

Correspondences

RESOURCE MANAGEMENT AGENCY

RANDALL L. ABBOTT
DIRECTOR

DAVID PRICE III
ASSISTANT DIRECTOR



Air Pollution Co.
WILLIAM J. RC
Environmental Health &
STEVE McALLEY.
Planning & Development
TED JAMES, AIC

AIR POLLUTION CONTROL DISTRICT

May 18, 1992

Mr. Bruce Wertz
Diamond Energy, Inc.
623 W. Fifth St., Suite 2800
Los Angeles, CA 90071

Subject: Biennial Toxic Emission Inventory Plan (BTEIP)
Air Toxics Hot Spots Information and Assessment Act

Regarding: Diamond Energy/Dexzel Cogeneration Source Test

Received: April 27, 1992

Dear Mr. Wertz:

As required by AB2588, the District has reviewed and conditionally approved the source test protocol, subject to the following conditions:

1. CARB Method 430:

The District requires Dexzel Cogeneration to use the revised CARB 430 Formaldehyde test method. As stated in the method, the Pre-Test Protocol must be submitted for District review and approval at least 48 hours before the source sampling is scheduled to begin.

2. Stock/Wash Tank Sampling and Analysis:

A. Emissions Calculations:

The District requires the emission rates of AB2588 toxic compounds, from petroleum product storage tanks, to be calculated in terms of pounds of toxic per pound of Total Organic Gas (TOG). Please submit sample calculation for determination of TOG emissions from crude storage tanks and the application of source test data to the TOG calculation.

Post 44 brand fax transmitted memo 7/87	1st page - 2
John Haley	From: Miss Pinedas
Dexzel Cogeneration	To: CC: AICD
805-399-5894	805-861-3682
805-399-5894	805-861-2000

Dexzel Cogeneration
May 18, 1992
Page 2

B. Hydrogen Sulfide:

The District requires the use of ST-28 or EPA method 11 for sampling and analysis of Hydrogen Sulfide. OK

3. QA/QC Audit:

A. Field Inspection:

Please note the District will perform a QA/QC audit of the Dexzel source test. The audit will consist of a field inspection of sampling equipment and methodology to ensure strict conformance with CARB approved procedures. ✓

B. Laboratory Data:

The analytical results will be audited for conformance to CARB approved analytical procedures. Please submit copies, when available, of GC and HPLC chromatograms for all calibration, blank, and sample analysis. The District also requires sample calculations of concentrations and emission rates as derived from GC and HPLC chromatograms, i.e. strip charts. ✓

The District requires the additional information by May 25, this will allow the District two days for review prior to testing.

The District may find it necessary to request additional information and/or require an on-site inspection in the course of reviewing the BTEIP.

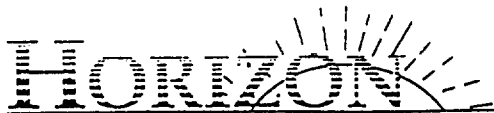
Thank you for your cooperation. Should you have any questions, please contact Mr. Luis Paredes or myself, at (805) 861-3682.

Sincerely,

WILLIAM J. RODDY
AIR POLLUTION CONTROL OFFICER



William Weese
Supervisor Technical Services
Compliance Division



Air Measurement Services, Inc.

(805) 498-8781

D2-01-C1

May 20, 1992

Mr. Luis R. Paredes
Kern County Air Pollution Control District
2700 "M" Street, Suite 275
Bakersfield, CA 93301

Dear Mr. Paredes:

In response to your comments, dated May 18, 1992, concerning the Dexel Cogeneration Source Test Plan, HORIZON is submitting the following Pre-test Protocol for aldehyde testing per our conversation earlier this morning.

We are basing all Planned Sample Volume (PSV) and Planned Sample Time (PST) upon formaldehyde, since formaldehyde is expected to have the highest blank value.

According to our calculations (Table 1) based upon a typical DNPH reagent blank level of 60 ng/ml and your stated sample rate requirement of 100 cc/min, a sample run time of four hours will be required to ensure a TAC of 1 ppm formaldehyde.

Within 48 hours of the start of the test program, four pre-test blanks will be obtained and analyzed to ensure anticipated reagent blank levels are within the expected levels used for the PSV and PST calculations.

Sincerely,

HORIZON AIR MEASUREMENT SERVICES, INC.

Richard J. Vacherot
President

RV:pve

TABLE 1
Sample Volume/ Time Calculations
Method 430

3.5.1 Planned Sample Volume (PSV)

Assume:

$$\begin{aligned} \text{TAC} &= 1 \text{ ppm} \\ &= 1.25 \text{ mg HCHO/dscm} \\ &= 1.83 \text{ mg HC}_3\text{CHO/dscm} \end{aligned}$$

$$\text{ESTFB} = 1.5 \times 60 \text{ mg HCHO/ml} \times 30 \text{ ml} = 2700 \text{ mg}$$

$$\begin{aligned} \text{where, } C_{\text{RB}} &= 10 \text{ mg HCHO/ml} \\ V_{\text{ST}} &= 30 \text{ ml} \\ R &= 95\% \end{aligned}$$

$$\text{PSV}_{\text{HClO}} = \frac{10 \times 2700}{1000} \times \frac{100}{95} \times \frac{1}{1.25}$$

$$\text{PSV}_{\text{HClO}} (\text{liters}) = 22.74 \text{ liters}$$

3.5.2 Planned Sample Time (PST)

$$\text{PST (minutes)} = \frac{22.74 \text{ liters}}{0.1 \text{ L/min}}$$

$$\begin{aligned} &= 227 \text{ minutes} \\ &= 3.78 \text{ hours (4 hours)} \end{aligned}$$

Fresno

Kern

Kings

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San Joaquin Valley
Unified Air Pollution Control District

May 26, 1992

Merced

San Joaquin

Stanislaus

Tulare

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DM STEARNS

Councilmember, City of Clovis

JOE HAMMOND

Supervisor, Kings County

LYDE GOULD

Supervisor, Tulare County

MEL McLAUGHLIN

Councilmember, City of Wasco

Mr. John Dydo
Diamond Energy, Inc.
633 W. 5th, Suite 2800
Los Angeles, CA 90071

Subject: Biennial Toxic Emission Inventory Plan (BTEIP)
Air Toxics Hot Spots Information and Assessment Act

Regarding: Dexzel Source Test, CARB method 430 flow rate

Date Received: May 20, 1992

Dear Mr. Dydo :

As required by AB2588, the District has reviewed and approved the Source Test Protocol revisions listed below:

CARB method 430:

The flow rate will be changed from 100 ml/min to 250 ml/min.

Thank you for your cooperation. Should you have any questions, please contact Mr. Luis Paredes or myself at (805) 831-3682.

Sincerely,

DAVID L. CROW
EXECUTIVE DIRECTOR/APCO

MARK BOESE
DEPUTY APCO

William H. Weese
William H. Weese
Toxic Assessment Manager
Southern Region

DEXZEL, INC.

FILE#

DATE: MAY 29 1992

DISTRIBUTION:

HORIZON

JOHN HALEY - LUFT

WW/tp