

**EMISSIONS TEST RESULTS
AT COMPRESSOR STATION 6, UNIT A
NEAR ROSALIA, WASHINGTON**

Prepared For:

PACIFIC GAS TRANSMISSION COMPANY

Prepared By:

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**CARNOT
Tustin, California**

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CR 82100-2265R

REPORT CERTIFICATION

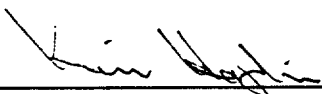
The sampling and analysis performed for this report was carried out under my direction and supervision.



Kevin C. Hopkins
Senior Engineer

Date 1/15/91

I have reviewed all testing details and results in this test report and hereby certify that the test report is authentic and accurate.



Kevin C. Hopkins
Senior Engineer

Date 1/15/91

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SECTION 1.0

INTRODUCTION AND SUMMARY

Carnot was contracted by Pacific Gas Transmission (PGT) Company to conduct an emissions test of its natural gas fired turbine at Compression Station 6 Unit A, near Rosalia, Washington. The tests were conducted to comply with the requirements of the Spokane County Air Pollution Control Authority.

This document presents the test results for the 1990 annual compliance tests at Compressor Station 6, Unit A. All tests were performed with the turbine operating at full load. Table 1-1 presents a summary of the three tests.

The tests were performed by Kevin Hopkins and Mike Schmidt of Carnot. Unit operations were coordinated by Carmen Acton of PGT.

TABLE 1-1
RESULTS SUMMARY - PGT STATION 6 UNIT A

Test No.	5-6A	6-6A	7-6A	Average
Date	12/10/90	12/10/90	12/10/90	—
Time	1105/1205	1220/1320	1335/1445	—
Fuel Flow, scfh	109,300	110,500	110,240	110,013
Exhaust, °F	947	946	945	946
Turbine Inlet, °F	1375	1375	1375	1375
Gas Producer Speed, %	102	102	102	102
rpm	11,076	11,091	11,100	11,089
Gas Producer Compressor Discharge, psi	203	203	203	203
Barometric Pressure, in Hg	27.66	27.66	27.63	27.65
Wet Bulb, °F	43.8	43.5	43.0	43.4
Dry Bulb, °F	45.5	44.0	43.5	44.3
Humidity, lb H ₂ O/lb dry air	0.0057	0.0059	0.0058	0.0058
ISO Factor	1.0700	1.0790	1.0792	1.0761
O ₂ , %	15.28	15.30	15.33	15.30
CO ₂ , %	3.00	3.00	3.00	3.00
Exhaust Flow, dscfm*	58,690	59,550	59,730	59,320
Exhaust Flow, dscfm**	62,100	62,780	62,630	62,530
NO _x , ppm	162.0	161.6	162.9	162.2
ppm @ 15% O ₂	170.1	170.3	172.5	171.0
ppm ISO @ 15% O ₂	182.0	183.8	186.2	184.0
lb/hr ⁺	69.15	69.99	70.76	69.97
lb/hr ⁺⁺	73.17	73.79	74.20	73.72
CO, ppm	1	1	1	1
ppm @ 15% O ₂	1	1	1	1
lb/hr ⁺	0.26	0.26	0.26	0.26
lb/hr ⁺⁺	0.28	0.27	0.27	0.27
SO ₂ , ppm	0.00	0.00	0.00	0.00
ppm @ 15% O ₂	0.00	0.00	0.00	0.00
lb/hr ⁺	0.00	0.00	0.00	0.00

* Exhaust flows are calculated using the measured fuel flow and the EPA O₂ based emission factor.

** Exhaust flows are calculated using the measured fuel flow and the EPA CO₂ based emission factor.

+ Mass emissions rates are calculated using the exhaust flow rate based on the O₂ F-Factor and the measured species concentration.

++ Mass emissions rates are calculated using the exhaust flow rate based on CO₂ F-Factor and the measured species concentration.

SECTION 2.0

UNIT DESCRIPTION

PGT Compressor Station 6, Unit A is a Solar Mars gas turbine engine which is rated at 14,600 hp (ISO).

The following operating parameters were recorded at 15 minute intervals during each test:

- Fuel flow rate
- Exhaust temperature
- Gas producer speed (NGP)
- Gas producer compressor discharge pressure (PCP)
- Power turbine inlet temperature (T-5)
- Inlet pressure

Data sheets documenting unit operation are provided in Appendix D of this report.

SECTION 3.0

TEST DESCRIPTION

3.1 TEST CONDITIONS

Table 3-1 presents the average test conditions during the tests. Also shown are the average ambient conditions.

3.2 SAMPLE LOCATION

Pacific Gas Transmission Company Compressor Station 6, Unit A, near Rosalia, Washington, is a Solar gas turbine which exhausts to a stack which measured 7'3" by 7'3". The sample plane was located two equivalent duct diameters downstream of a 90° bend, and approximately 1.5 duct diameters upstream of the stack exit. A sketch of the sample location is provided in Appendix C.

3.3 TEST PROCEDURES

Test procedures used at Compressor Station 6 are presented in Table 3-2. Detailed test methods can be found in Appendix A. Modifications to standard procedures are discussed in the following sections.

3.3.1 Preliminary Diluent Traverse

In accordance with EPA Method 20, a preliminary diluent traverse was performed in order to select sample points for subsequent tests. A 30-point grid was traversed at two minutes per point. Neither O₂ nor CO₂ varied by more than 1% of the overall average, indicating a well-mixed exhaust flow. For the three remaining tests, the probe was placed at port D point number 4.

3.3.2 NO_x, CO, O₂, SO₂, and CO₂ Measurements

NO_x, CO, O₂, and CO₂ measurements were made at full load. Triplicate 60-minute runs were performed.

SO₂ emissions were calculated based on a fuel sulfur analysis, performed by Truesdail Laboratories in Irvine California.

TABLE 3-1
SUMMARY OF TEST CONDITIONS

Fuel Flow	110,013 scfh
Exhaust Temperature	946 °F
Turbine Inlet, °F	1375 °F
Gas Producer Speed	102 %
Gas Producer Speed	11089 rpm
Compressor Discharge	203 psi
Barometric pressure	27.65 in Hg
Wet Bulb Temperature	43.4 °F
Dry Bulb Temperature	44.3 °F

3.3.3 Exhaust Gas Flow

Exhaust gas flow was calculated using measured fuel flow, fuel analysis, measured excess O₂, and stoichiometric calculation. Calculation procedures are documented in EPA Method 19. Specific calculations are presented in Appendix E.

3.3.4 Fuel Analysis

Fuel analysis (composition, HHV) for use in stoichiometric flow rate calculations, was performed by Truesdail Laboratories.

Exhaust gas flow was also calculated using measured excess CO₂, measured fuel flow, fuel analysis and stoichiometric calculation.

TABLE 3-2
TEST PROCEDURES

Parameter	Measurement Technique	Reference Method	Comments
NO _x	Chemiluminescence	EPA 20	Triplicate 1-hour runs
CO	Nondispersive infrared absorption	EPA 10	Triplicate 1-hour runs
O ₂	Electrochemical cell	EPA 20	Triplicate 1-hour runs
SO ₂	Fuel Analysis	---	Duplicate fuel samples collected during testing
CO ₂	Nondispersive infrared absorption	EPA 3A	Triplicate 1-hour runs
Exhaust gas flow rate	Fuel flow measurement and stoichiometric calculation	EPA 19	

SECTION 4.0

RESULTS

The results of the compliance tests are presented in Table 4-1A, 4-1B and 4-2. Tables 4-1A and 4-1B provide the results of the fuel analysis. Table 4-2 presents the results summary.

Raw data and calculation procedures can be found in Appendix C, D, E and F of this report.

TABLE 4-1A
NATURAL GAS ANALYSIS

Species	% Volume
O ₂	0.0
N ₂	0.0
CH ₄	97.3
CO ₂	0.4
C ₂ H ₆	2.0
C ₃ H ₈	0.2
n-C ₄ H ₁₀	ND
i-C ₄ H ₁₀	ND
He	ND
H ₂ S	<0.1ppm

ND - Not Detected

TABLE 4-1B
NATURAL GAS ANALYSIS

HHV, Btu/Scf	1,025
HHV, Btu/lb	23,673
Density, lb/scf	0.0433
Molecular Weight, lb/lb-mole	16.43
EPA F-Factor, DSCF/MMBtu @ 60 °F	
O ₂ Based:	8,453
CO ₂ Based:	998

TABLE 4-2
RESULTS SUMMARY - PGT STATION 6 UNIT A

Test No.	5-6A	6-6A	7-6A	Average
Date	12/10/90	12/10/90	12/10/90	—
Time	1105/1205	1220/1320	1335/1445	—
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Exhaust, °F	947	946	945	946
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ppm ISO @ 15% O ₂	182.0	183.8	186.2	184.0
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CO, ppm	1	1	1	1
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lb/hr ⁺⁺	0.28	0.27	0.27	0.27
SO ₂ , ppm	0.00	0.00	0.00	0.00
ppm @ 15% O ₂	0.00	0.00	0.00	0.00
lb/hr ⁺	0.00	0.00	0.00	0.00

* Exhaust flows are calculated using the measured fuel flow and the EPA O₂ based emission factor.

** Exhaust flows are calculated using the measured fuel flow and the EPA CO₂ based emission factor.

+ Mass emissions rates are calculated using the exhaust flow rate based on the O₂ F-Factor and the measured species concentration.

++ Mass emissions rates are calculated using the exhaust flow rate based on the CO₂ F-Factor and the measured species concentration.

APPENDIX A
MEASUREMENT PROCEDURES

Extractive Continuous Emissions Monitoring System
Oxygen (O₂) by Continuous Analyzer
NO/NO_x by Continuous Analyzer
Carbon Monoxide (CO) by NDIR/Gas Filter Correlation

Extractive Continuous Emissions Monitoring System

O₂, CO, CO₂, NO, and NO_x are measured using an extractive continuous emissions monitoring (CEM) package, shown in the following figure. This package is comprised of three basic subsystems. They are: (1) the sample acquisition and conditioning system, (2) the calibration gas system, and (3) the analyzers themselves. This section presents a description of the sampling and calibration systems. Descriptions of the analyzers used in this program and the corresponding reference test methods follow. Information regarding quality assurance information on the system, including calibration routines and system performance data follows.

The sample acquisition and conditioning system contains components to extract a representative sample from the stack or flue, transport the sample to the analyzers, and remove moisture and particulate material from the sample. In addition to performing the tasks above, the system must preserve the measured species and deliver the sample for analysis intact. The sample acquisition system extracts the sample through a stainless steel probe. The probe is insulated or heated as necessary to avoid condensation.

Where water soluble NO₂ and/or SO₂ are to be measured, the sample is drawn from the probe through a heated Teflon sample line into a supercooled (approximately -20 °C) water removal trap. The trap consists of stainless steel flasks in a bath of dry ice and antifreeze. If dry ice is not locally available, ice and rock salt are used. This design removes the water vapor by condensation and freezes the liquid quickly. The contact between the sample and liquid water is minimized. Since the solubility of the NO₂ and SO₂ in ice is negligible, these species are conserved. This system meets the requirements of EPA Method 20. The sample is then drawn through a Teflon transport line and particulate filter, into the sample pump. The pump is a dual head, diaphragm pump. All sample-wetted components of the pump are stainless steel or Teflon. The pressurized sample leaving the pump flows through a stainless steel refrigerated (38 °F) compressed air dryer for final moisture removal. A drain line and valve are provided to constantly expel any condensed moisture from the dryer. After the dryer, the sample is directed into a distribution manifold. Excess sample is vented through a back-pressure regulator, maintaining a constant pressure of 5-6 psig to the analyzers.

The calibration system is comprised of two parts: the analyzer calibration, and the system bias check (dynamic calibration). The analyzer calibration equipment includes pressurized cylinders of certified span gas. The gases used are, as a minimum, certified to 1% by the manufacturer where necessary, to comply with reference method requirements. EPA Protocol 1 gases are used. The cylinders are equipped with pressure regulators which supply the calibration gas to the analyzers at the same pressure and flow rate as the sample. The selection of zero, span, or sample gas directed to each analyzer is accomplished by operation of the sample/calibration selector valves.

The system bias check is accomplished by transporting the same gases used to zero and span the analyzers to the sample conditioner inlet (probe exit). The span gas is exposed to the same elements as the sample and the system response is documented. Where the supercooled moisture removal system is used, water is added to the knockout flasks before the pre-test check. The analyzer indications for the system calibration check must agree within 5% of the analyzer calibration. Values are adjusted and changes/repairs are made to the system to compensate for any difference in analyzer readings. Specific information on the analytical equipment and test methods used is provided in the following pages.

Method:	Oxygen (O ₂) by Continuous Analyzer
Applicable Ref. Methods:	EPA 3A, EPA 20, ARB 100, BA ST-14
Principle:	A sample is continuously drawn from the flue gas stream, conditioned, and conveyed to the instrument for direct readout of O ₂ concentration.
Analyzer:	Teledyne Model 326A
Measurement Principle:	Electrochemical cell
Ranges:	0-5, 0-10, 0-25% O ₂
Accuracy:	1% of full scale
Output:	0-100 mV, linear
Interferences:	Halogens and halogenated compounds will cause a positive interference. Acid gases will consume the fuel cell and cause a slow calibration drift.
Response Time:	90% <7 seconds
Sampling Procedure	The stack dimensions are described in Section 3.2. A 5 x 6 matrix will be used as specified in EPA Method 20 for a preliminary O ₂ traverse. Subsequent tests will be performed using the eight sample points with the lowest O ₂ level. A representative flue gas sample is collected and conditioned using the CEM system described previously.
Analytical Procedure:	An electrochemical cell is used to measure O ₂ concentration. Oxygen in the flue gas diffuses through a Teflon membrane and is reduced on the surface of the cathode. A corresponding oxidation occurs at the anode internally, and an electric current is produced that is proportional to the concentration of oxygen. This current is measured and conditioned by the instrument's electronic circuitry to give an output in percent O ₂ by volume.
Special Calibration Procedure:	The measurement cells used with the O ₂ instrument have to be replaced on a regular basis. After extended use, the cell tend to produce a nonlinear response. Therefore, a three-point calibration is performed at the start of each test day to check for linearity. If the response is not linear ($\pm$ 2% of scale), the cell is replaced.

Method: NO/NOx by Continuous Analyzer

Applicable Ref. Methods: EPA 7E, EPA 20; ARB 100, BA ST-13A

Principle: A sample is continuously drawn from the flue gas stream, conditioned, and conveyed to the instrument for direct readout of NO or NOx.

Analyzer: Teco Model No. 10AR

Measurement Principle: Chemiluminescence

Accuracy: 1% of full scale

Ranges: 0-2.5, 0-10, 0-25, 0-100, 0-250, 0-1000, 0-2500, 0-10,000 ppm

Output: 0-10 mV

Inferences: Compounds containing nitrogen (other than ammonia) may cause interference.

Response Time: 90%, 1.5 seconds (NO mode) and 1.7 seconds (NOx mode)

Sampling Procedure: A representative flue gas sample is collected and conditioned using the CEM system described previously. Method 20 procedures for selecting sample points are used.

Analytical Procedure: The oxides of nitrogen monitoring instrument is a chemiluminescent nitric oxide analyzer. The operational basis of the instrument is the chemiluminescent reaction of NO and ozone (O₃) to form NO₂ in an excited state. Light emission results when excited NO₂ molecules revert to their ground state. The resulting chemiluminescence is monitored through an optical filter by a high sensitivity photomultiplier tube, the output of which is electronically processed so it is linearly proportional to the NO concentration. The output of the instrument is in ppmV.

When NO₂ is expected to be present in the flue gas, a supercooled water dropout flask will be placed in the sample line to avoid loss of NO₂. Since NO₂ is highly soluble in water, "freezing out" the water will allow the NO₂ to reach the analyzers for analysis. The analyzer measures NO only. In the NOx mode, the gas is passed through a moly converter which converts NO₂ to NO and a total NOx measurement is obtained. NO₂ is determined as the difference between NO and NOx. Use of a moly converter instead of a stainless steel converter eliminates NH₃ interference; NH₃ is converted to NO with a stainless converter, but not with a moly converter.

Method: Carbon Monoxide (CO) by NDIR/Gas Filter Correlation

Applicable
Ref. Methods: EPA 10; ARB 1-100; BA ST-6

Principle: A sample is continuously drawn from the flue gas stream, conditioned, and conveyed to the instrument for direct readout of CO concentration.

Analyzer: TECO, Model 48

Measurement
Principle: NDIR/Gas Filter Correlation

Precision: 0.1% ppm

Ranges: 0-5, 0-10, 0-25, 0-50, 0-100, 0-250, 0-500, 0-1000, 0-5000 ppm

Output: 0-100 mV

Interferences: Negligible interference from water and CO₂

Rise/Fall
Times (0-95%) 1 minute @ 1 lpm flow, 30 second integration time

Sampling
Procedure: A representative flue gas sample is collected and conditioned using the CEM system described previously. Sample point selection has been described previously.

Analytical
Procedure: Radiation from an infrared source is chopped and then passed through a gas filter which alternates between CO and N₂ due to rotation of a filter wheel. The radiation then passes through a narrow band-pass filter and a multiple optical pass sample cell where absorption by the sample gas occurs. The IR radiation exits the sample cell and falls on a solid state IR detector.

APPENDIX B
QUALITY ASSURANCE

Appendix B.1

Quality Assurance Program Summary

QUALITY ASSURANCE PROGRAM SUMMARY

Carnot ensures the quality and validity of its emission measurement and reporting procedures through a rigorous quality assurance (QA) program. The program is developed and administered by an internal QA Officer, and encompasses seven major areas:

1. Development and use of an internal QA manual.
2. QA reviews of reports, laboratory work, and field testing.
3. Equipment calibration and maintenance.
4. Chain of custody.
5. Training.
6. Knowledge of current test methods.
7. Agency certification.

Each of these areas is discussed individually below.

Quality Assurance Manual. Carnot has prepared a QA Manual according to EPA guidelines. The manual serves to document and formalize all of Carnot's QA efforts. The manual is constantly updated, and each member of the Source Test Division is required to read and understand its contents. The manual includes details on the other six QA areas discussed below.

QA Reviews. Carnot's review procedure includes review of each source test report by the QA Officer, and spot check reviews of laboratory and field work.

The most important review is the one that takes place before a test program begins. The QA Officer works closely with Source Test Division personnel to prepare and review test protocols. Test protocol review includes selection of appropriate test procedures, evaluation of any interferences or other restrictions that might preclude use of standard test procedures, and evaluation and/or development of alternate procedures.

Equipment Calibration and Maintenance. The equipment used to conduct the emissions measurements is maintained according to the manufacturer's instructions to ensure proper operation. In addition to the maintenance program, calibrations are carried out on each measurement device according to the schedule outlined by the California Air Resources Board (CARB). The schedule for maintenance and calibrations are given in Tables B-1 and B-2. Quality control checks are also conducted in the field for each test program. The following is a partial list of checks made as part of each CEM system test series.

Sample acquisition and conditioning system leak check.

2-point analyzer calibrations (all analyzers)

3-point analyzer calibrations (analyzers with potential for linearity errors).

Complete system calibration check ("dynamic calibration" through entire sample system).

Periodic analyzer calibration checks (once per hour) are conducted at the start and end of each test run. Any change between pre- and post-test readings are recorded.

TABLE B-1.
SAMPLING INSTRUMENTS AND EQUIPMENT CALIBRATION SCHEDULE

Instrument Type	Frequency of Calibration	Standard of Comparison or Method of Calibration	Acceptance Limits
Orifice Meter (large)	12 months	Calibrated dry test meter	$\pm 2\%$ of volume measured
Dry Gas Meter	12 months or when repaired	Calibrated dry test meter	$\pm 2\%$ of volume measured
S-Type Pitot (for use with EPA type sampling train)	6 months	EPA Method 2	Cp constant ($+5\%$) over working range. Difference between the average Cp for each leg must be less than 2%
Vacuum Gauges Pressure Gauges	6 months	Manometer	$\pm 3\%$
Field Barometer	6 months	Mercury barometer	$\pm 0.2''$ Hg
Temperature Measurement	6 months	NBS mercury thermometer or NBS calibrated platinum RTD	± 4 F for $<400^{\circ}\text{F}$ $\pm 1.5\%$ for $>400^{\circ}\text{F}$
Temperature Readout Devices	6 months	Precision potentiometer	$\pm 2\%$ full scale reading
Analytical Balance	12 months (checked prior to each use)	Should be performed by manufacturer or qualified laboratory	± 0.3 mg of stated weight
Probe Nozzles	12 months	Nozzle diameter check micrometer	Range $< \pm 0.10$ mm for three measurements
Continuous Analyzers	Depends on use, frequency, and performance	As specified by manufacturers operating manuals, EPA NBS gases, and/or ref. methods	Satisfy all limits specified in operating specifications

TABLE B-2.
EQUIPMENT MAINTENANCE SCHEDULE
 Based on Manufacturer's Specifications
 and Carnot Experience

Equipment	Performance Requirement	Maintenance Interval	Corrective Action
Pumps	1. Absence of leaks 2. Ability to draw mfr required vacuum and flow	Every 500 hrs of operation or 6 months whichever is less	1. Visual insp. 2. Clean 3. Replace worn parts 4. Leak check
Flow Measuring Device	1. Free mechanical movement 2. Absence of malfunction	Every 500 hrs of operation or 6 months whichever is less After each test, if used in H ₂ S sampling or other corrosive atmospheres	1. Visual insp. 2. Clean 3. Calibrate
Sampling Instruments	1. Absence of malfunction 2. Proper response to zero, span gas	As required by manufacturer	As recommended by manufacturer
Integrated Sampling Tanks	Absence of leaks	Depends on nature of use	1. Steam clean 2. Leak check
Mobile Van Sampling Systems	Absence of leaks	Depends on nature of use	1. Change filters 2. Change gas dryer 3. Leak check 4. Check for system contamination
Sampling Lines	Sample degradation less than two percent	After each test or test series	Blow filtered air thru line until dry

All calibrations are conducted using gases certified by the manufacturer to be + 1% of label value (NBS traceable).

Calibration and CEM performance data are fully documented, and are included in each source test report.

Chain of Custody. Carnot maintains full chain of custody documentation on all samples and data sheets. In addition to normal documentation of changes between field sample custodians, laboratory personnel, and field test personnel, Carnot documents every individual who handles any test component in the field (e.g., probe wash, impinger loading and recovery, filter loading and recovery, etc.).

Samples are stored in a locked area to which only Source Test Division personnel have access. Neither other Carnot employees nor cleaning crews have keys to this area.

Data sheets are copied immediately upon return from the field, and this first generation copy is placed in locked storage. Any notes made on original sheets are initialed and dated.

Training. Personnel training is essential to ensure quality testing. Carnot has formal and informal training programs which include:

1. Attendance at EPA-sponsored training courses.
2. Enrollment in EPA correspondence courses.
3. A requirement for all technicians to read and understand Carnot's QA Manual.
4. In-house training and QA meetings on a regular basis.
5. Maintenance of training records.

Knowledge of Current Test Methods. With the constant updating of standard test methods and the wide variety of emerging test methods, it is essential that any qualified source tester keep abreast of new developments. Carnot subscribes to services which provide updates on EPA and CARB reference methods, and on EPA, CARB, and SCAQMD rules and regulations. Additionally, source test personnel regularly attend and present papers at testing and emission-related seminars and conferences. Carnot personnel maintain membership in the Air Pollution Control Association, the Source Evaluation Society, and the ASME Environmental Control Division.

Appendix B.2
Equipment Calibration

SPAN GAS RECORD

Date 12/9/90

Client/Location PGT Station 6 Unit A

By _____

Gas	Span Cylinder		Aux. Span Cylinder	
	Cylinder No.	Concentration	Cylinder No.	Concentration
Zero	AAL-6181	N ₂	—	—
NOx	ALM-2854	146.4 ppm	ALM-7351	229.8 ppm
O ₂	ALM-11553	8.00%	ALM-14399	12.49%
CO	ALM-12686	55.04 ppm	ALM-5658	88.25 ppm
CO ₂	ALM-11553	22.51 ppm	ALM-14399	14.95%
SO ₂	✓	✓	✓	✓

INSTRUMENT LINEARITY

	Analyzer				
	O ₂	CO ₂	NOx NOx	CO CO	SO ₂
Analyzer Range	25%	25%	250 ppm	100 ppm	✓
Set to High STD ^{MID} (80-90% of Range)	8.00%	High 22.5%	145.0 ppm	High O ₂ 55.8 ppm	
As-Found Low STD ^{LOW} (50-60% of Range)	12.63%	14.75%	230.0 ppm	54.5 ppm	
Actual Value of Low STD	12.49%	14.95%	229.8 ppm	55.8 ppm	
Difference in % of Full Scale Range	+1.1%	+1.3%	+0.1%	-2.3%	

Allowable deviation is 2% of full scale (2 squares on strip chart).



CEM PERFORMANCE DATA

By K. Hopkins Location PGT - Station 6 Unit A Date 12/9/96

System Configuration

Analyzers in Service NO_x (NO + NO₂), O₂, CO₂, COProbe: Length 10' Liner Material S. S. Heated (Y/N) YSample Line: Length 150' Material TeflonOn-Stack Conditioner: In Service (Y/N) Y Coolant ICE

System Flow Rate (from file): _____ cfm

System Leak Check

Pre-Test: 0.00 cfh Post-Test: _____ cfhLeak Rate (%) = $\frac{\text{Post Test (cfh)}}{\text{System Flow Rate (cfm)} \times 60} \times 100 = \underline{\hspace{2cm}} \%$

System Response Time Check

Upscale

Downscale

1	2	3	Avg
<u>30</u> sec	<u>25</u> sec	____ sec	<u>30</u> sec
<u>30</u> sec	<u>30</u> sec	____ sec	<u>30</u> sec



Scott Specialty Gases, Inc.

FAX: 714-887-0549
PHONE: 714-887-2571

2600 CAJON BLVD., SAN BERNARDINO, CA 92405

CARNOT

15891 RED HILL AVE, SUITE 110
10811N, CA 92680

JIM MULLIGAN

CERTIFICATE OF ANALYSIS - EPA PROTOCOL GASES

Certified for Traceability Protocol No. 1 Process Gas No. G1

Cylinder No. ALM-2854

Cylinder Pressure 1900 psig

Certified Accuracy $\pm 1\%$ 11105 Traceable

Shipped From: Scott SAN BERNARDINO,
Date Shipped 11/12/90
Our Protocol No: 10003
Your PO No: 6693
Pics 1 of 1
Expiration Date: 5/92

REFERENCE STD

COMPONENTS	CERTIFIED CONC	SN/VCN/NO.	CYL. NO.	CONC.	MAKE/MODEL/SERIAL NO.	LAST CAL. DATE	ANALYTICAL PRINCIPLE
NITRIC OXIDE	143.5 ppm	CRM1685B	CAL-5827	236 ppm	THERMO-ELECTRON	9/3/90	CHEMI-LUMINESC
NOX	146.4 ppm				10 AR 14853-150		

BALANCE GAS - NITROGEN

ANALYZER READINGS: Z = Zero Gas T = Test Gas R = Reference Gas

Component NITRIC OXIDE

Final Analysis Date	10/27/90	Units	mv
Z	0.00	N	94.40
N	94.10	Z	0.00
Z	-0.02	T	57.30

Mean Test Assay 143.3 ppm

Second Analysis Date	11/3/90	Units	mv
Z	0.00	N	94.40
N	94.40	Z	0.01
Z	0.00	T	57.48

Mean Test Assay 143.5 ppm

Component	Date	Units
Z		N
N		Z
Z		T

Mean Test Assay

Component	Date	Units
Z		N
N		Z
Z		T

Mean Test Assay

Chronology: Date _____

Assay _____

Analyst L. OLDFHAM

Approved By: _____

256



Scott Specialty Gases, Inc.

FAX: 714-887-0549
PHONE: 714-887-2571

2600 CAJON BLVD., SAN BERNARDINO, CA 92405

6/15/90

CARNOT

15991 RED HILL AVE

SUITE 110

TUSTIN

CA 92680-0000

FORMERLY ENERGY SYS ASSOC

PROJECT #: 02-07371

PO #: 6102

CYLINDER #: ALM011553

ANALYTICAL ACCURACY: +/-1%

COMPONENT	REQUESTED CONCENTRATION	ANALYSIS 1 (MOLES) U/M
CARBON DIOXIDE	22.5 PCT	22.51 PCT
ARGON	8.0 PCT	8.000 PCT
NITROGEN	BALANCE GAS	N/A

NOTES: GRAVIMETRIC MASTER GAS-CERTIFIED TO HAVE BEEN
BLENDED AGAINST NIST CERTIFIED WEIGHTS AND
VERIFIED TO BE CORRECT BY INDEPENDENT
ANALYSIS.

CO2 TRACEABLE TO CRM1675

O2 TRACEABLE TO CRM2658

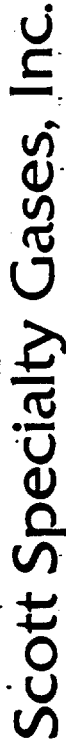
DATE OF ANALYSIS: 6/15/90

ANALYST:

MAYNARD JOHNSON

APPROVED BY:

ROBERT SHEALY



2600 CAJON BLVD., SAN BERNARDINO, CA 92405

TUSTIN, CA

CERTIFICATE OF ANALYSIS - EPA PROTOCOL GASES:

1 Procedure No. G1

Call No. ALM-12686

Cylinder Pressure 1900 psi

Carroll Agency $\frac{\pm 1\%}{\pm 1\%}$ "HDS Theobald"

Expiration Date: 11/91

$$\text{Pr} \approx \frac{1}{\alpha} \frac{1}{\alpha}$$

your po 110: _____

6450

5/24/90

SAN BERNARDINO, CA

REFERENCE STD

GAS ANALYZER

ANALYTICAL PRINCIPLE

**CERTIFIED
COMPONENTS
CO/LO**

SPW/CB 110.

001, 110,

21103

11. KENNEDY, J. H. 1960. *Journal of the Royal Microscopical Society* 80: 1-10.

DATE
LAST CAL.

<u>COMPONENTS</u>	<u>CONC</u>
CARBON MONOXIDE	55.84 ppm

Color	GMS
55.84 ppm	

ALM-7531

258.7 ppm

HORIBA AIA 24

4/30/90

INFRA _ RED

TRACEABLE TO CRM2636

4564403

ALANOE GAS

VALVE-BEADINGS: Z = Zero Gas T = Test Gas R = Reference Gas

CARBON MONOXIDE

Component	5/15/90	Units	ppm
mf Analysis Date	00.0	h	22.9
	95.0	z	22.9
	00.0	T	95.0
			55.84 ppm

Mean Test Assy 55.84 ppm

Second Analysis Date	5/22/90	Units	ppm
00.0	R	95.0	22.9
95.0	Z	00.0	22.9
00.0	T	22.9	95.0

55.84 ppm

Component: _____

Date _____ Units: _____
 Z _____ R _____ T _____
 R _____ Z _____ T _____
 Z _____ T _____ R _____

Utah Post Office

Mean Test Assay

Date	Units
Z	R
R	Z
Z	T
	R

Mean Test Assay

Chronology: Date _____
Assay _____

Analyst P. VILLIMAS/M. JOHNSON

Approved By:

R. S. Leary

APPENDIX C

RAW DATA

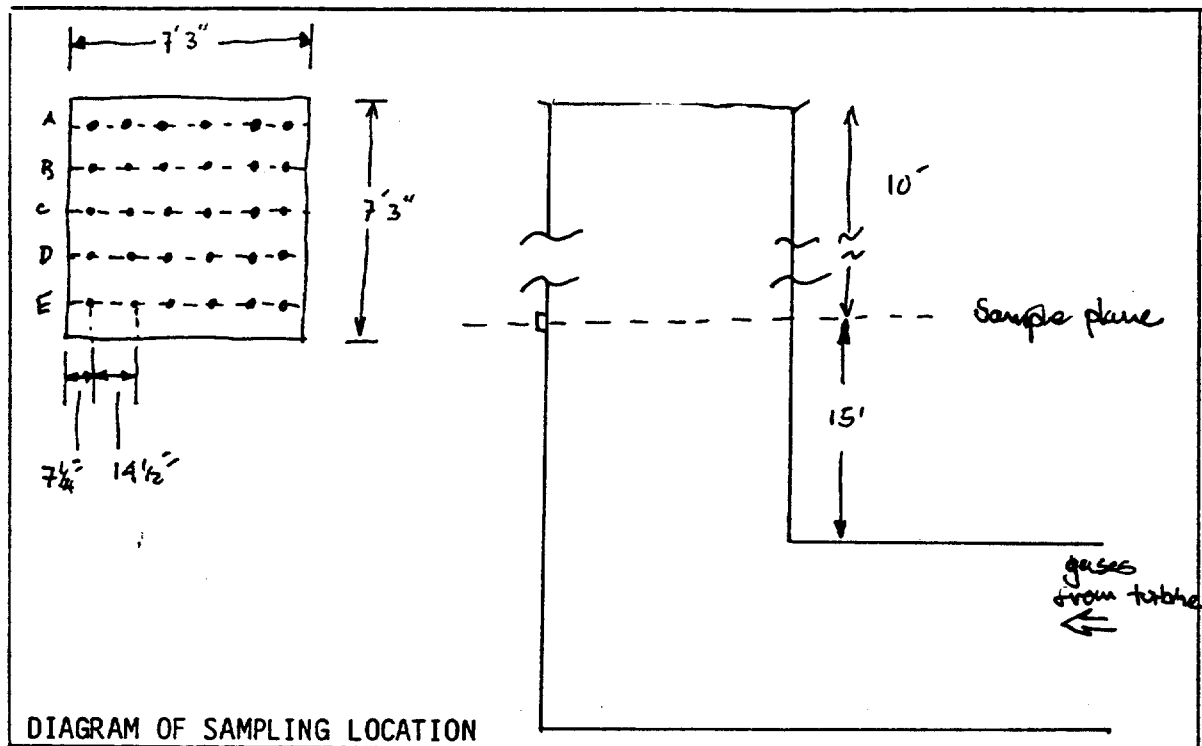
SAMPLING POINT LOCATION DATA EPA Method 1

Plant PGT Station 6 Unit A

Data by _____

Date _____

Test Location Stack, Solar Mars Turbine



Upstream Dist./Dia. _____

Downstream Dist./Dia. _____

Coupling Length _____

No. of Sampling Pts. _____

Stack Dimension 87" x 87"

Stack Area, ft² 52.6 ft²

Sample Point	% of Diameter	In. from near Wall	In. from Nozzle*
1	7 1/4"		
2	14 1/2 21 3/4"		
3	28 1/4 36 1/4"		
4	36 1/4 50 3/4"		
5	50 3/4 65 1/4"		
6	65 1/4 79 3/4"		

*Inches from wall plus
coupling length



CONTINUOUS EMISSIONS MEASUREMENTS

pg. 1 of 3

Client PGT/Station 6 Unit A
Date 12/10/90
Test Location Stack
Ambient Temperature, DB/WB _____
Operator KCH/MS

Test No(s) O₂/CO₂ Traverse
Barometric Pressure 27.66 in Hg
Duct Static Pressure _____
Fuel Nat. Gas

Test No.	Sample Time	Point	Dry, Uncorrected							Corrected to 15% O ₂ , Dry		
			O ₂	CO ₂	CO	NO _x	NO	NO ₂	SO ₂	CO	NO _x	SO ₂
	858	Pre-test calibration	0.0 12.5	0.0 15.0	0.0 5.6	0.0 14.5						
	902 904	A-6	15.45	3.00	4.5	165						
	904 906	A-5	15.45	3.00	2	162.5						
	906 908	A-4	15.45	3.00	1	161.5					175.9	
	908 910	A-3	15.5	3.0	1	161.5						
	910 912	A-2	15.50	3.0	1	160.0						
	912 914	A-1	AIR in-leakage									
		Cal AS FOUND	6.0 12.6	0.0 15.0								
	917 919	B-6	15.45	3.00	1	163.8					177.3	
	919 921	B-5	15.45	3.00	1	163.8						
	921 923	B-4	15.45	3.00	1	163.8						
	923 925	B-3	15.45	3.00	1	163.8						
	925 927	B-2	15.45	3.0	1	162.5						
		B-1	AIR in-leakage									
Span Gas Concentration			2.5	15.0	35.8	146.4						

Comments: _____

Client PGT/Station 6 Unit A

Date 12/10/90

Test Location Stack

Ambient Temperature, DB/WB 43.5/42.5

Operator KCH/MS @09:42

Test No(s) O₂/CO₂ Traverse (Cont'd)

Barometric Pressure _____

Duct Static Pressure _____

Fuel Nat. Gas

Test No.	Sample Time	Point	Dry, Uncorrected							Corrected to % Dry		
			O ₂	CO ₂	CO	NO _x	NO	NO ₂	SO ₂	CO	NO _x	SO ₂
		CAL AS FOUND	0.0	0.0								
	932		12.6	15.0		14.6						
	934	C-6	15.33	3.00	1	162.5						
	934		15.33	3.00	1	162.5						
	936	C-5	15.33	3.00	1	162.5						
	936		15.33	3.00	1	162.5						
	938	C-4	15.33	3.00	1	162.5						
	938		15.33	3.00	1	162.5						
	940	C-3	15.33	3.00	1	162.5						
	940		15.33	3.00	1	161.3						
	942	C-2	15.33	3.00	1	161.3						
	942		15.33	3.00	1	161.3						
	944	C-1	15.5	3.00	1	160.0						
	944		15.5	3.00	1	160.0						
	945	CAL AS FOUND	12.65	14.95								
	947		15.33	3.03	1	162.5						
	949	D-6	15.33	3.03	1	162.5						
	949		15.33	3.03	1	162.5						
	951	D-5	15.33	3.03	1	162.5					172.1	
	951		15.33	3.03	1	162.5						
	953	D-4	15.33	3.03	1	162.5						
	953		15.33	3.03	1	161.3						
	955	D-3	15.33	3.03	1	161.3						
	955		15.33	3.00	1	161.3						
	957	D-2	15.33	3.00	1	161.3						
	957		15.33	3.00	1	161.3						
		D-1										
Span Gas Concentration												

Comments: _____

CONTINUOUS EMISSIONS MEASUREMENTS

Client PCA/Station 6 Unit A

Date 12/10/90

Test Location Stack

Ambient Temperature, DB/WB (See below)

Operator KCH/

Test No(s) 5-6A

Barometric Pressure 27.66

Duct Static Pressure _____

Fuel _____

Test No.	Sample Time	Point	Dry, Uncorrected							Corrected to 15% O ₂ , Dry			WB/DB
			O ₂	CO ₂	CO	NO _x	NO	NO ₂	SO ₂	CO	NO _x	SO₂	
	1059 1104	Pre test Analyzer cal	0.0 12.5	0.0 15.0	0.0 5.5	0.0 146.4							WB/DB
	1105 1115	D-4	15.31	3.00	1	161.3					170.3		
	1115 1125		15.30	3.00	1	162.8					171.5		43.5/45
	1125 1135		15.30	3.06	1	162.3					170.0		
	1135 1145		15.28	3.00	1	161.3					169.3		44/46
	1145 1155		15.25	3.00	1	162.3					169.5		
	1155 1205		15.25	3.00	1	161.8					169.0		
	1206	Post test cal As Found	0.0 12.38	0.0 15.0	0.0 5.5	0.0 145.0							
		% Drift (% of span)	0 -96	0 0	0 0	0 -96							
		Average:	15.28	3.00	1	162.0					170.1		
Span Gas Concentration			12.5	15.0	5.8	146.4							

Comments: Probe place @ port which measured lowest O₂ and highest CO₂. No variation in point-to-point variation was measured. Point 4 was selected as representative



CONTINUOUS EMISSIONS MEASUREMENTS

Client PGIT/Station 6 Unit A

Test No(s) 6-6A

Date 12/10/90

Barometric Pressure 27.66

Test Location Stack

Duct Static Pressure _____

Ambient Temperature, DB/WB (See below)

Fuel _____

Operator _____

Test No.	Sample Time	Point	Dry, Uncorrected							Corrected to 15% O ₂ , Dry		
			O ₂	CO ₂	CO	NOx	NO	NO ₂	SO ₂	CO	NOx	SO ₂
	1213	Pre-test CALIBRATION	0/12.5	0/15	0/56.5	0/146.4						
	1220 1230	D-4	15.30	3.00	1	163.8					172.6	
	1230 1240		15.30	3.00	1	162.3					171.0	
	1240 1250		15.30	3.00	1	161.3					170.0	
	1250 1300		15.30	3.00	1	160.8					169.4	
	1300 1310		15.30	3.00	1	160.8					169.4	
	1310 1320		15.30	3.00	1	160.3					168.9	
		Post-test cal As Found	0.0/12.5	0.0/15.0	0.0/56.5	0.5/145						
		Drift % of Span	0/0	0/0	0/0	0.34%/ -1.6%						
		Average	15.30	3.00	1	161.6					170.3	
Span Gas Concentration			12.5	15.0	55.8	146.4						

WB/DB

43.5/44.0

Comments: _____

APPENDIX D
UNIT OPERATING DATA

PGIT - Station 6 A
December 1990

KCV
12/9

Test No.	5-6A	#1					
Date		12/10					
Time		11:00	11:15	11:30	11:45	12:00	
Data By:		CTA	CTA	CTA	CTA	CTA	
Fuel Flow Rate SCF MBCF x 1000		99755 1090	99781 1097	997809 1093	997836 1092	997864 1094	
Exhaust Temp.		948°F	947°	946.7	946°F	947°	
T-5		1375°F	1375°	1375°	1375°	1375°	
Gas Producer Speed (NGP)		102% 1106 rpm	102% 11080	102% 11080	102% 11086	102% 11074	
Gas Producer Comp Discharge (PCP)		202 PSI	203 PSI	203 PSI	203 PSI	202 PSI	
Inlet pressure		14.0/14.1 PSIA	14.1 PSIA	14.1 PSIA	14.1 PSIA	14.1 PSIA	
Rel Humidity		86%	86%	88%	86%	81/82%	
T-1 (Ambient)		46°F	46°F	45°	46°F	45°	
Barometric		940 millibars	940	940	940	940	
		27.5 10" Hg					
Ambient		44°					

KCH
12/9

PGT - Station 6 A
December 1990

Test No.	Oz Traverse						
Date	12/10						
Time	9:15	9:42					
Data By:	GTA	GTA					
Fuel Flow Rate	$\times 1000$ msec	1102 997561	1093 997611				
Exhaust Temp.		950°F	949°				
T-5		1375°F	1375				
Gas Producer Speed (NGP)		102% 11118 RPM	102 11099				
Gas Producer Comp Discharge (PLP)		204 PSE	203 PSE				
Inlet pressure		14.2 PSIA	14.0 PSIA				

Rel Humidity 87% 85%

Ambient T° 40°F 40°

T-1 44°F 46°F

Bar - 940 m. l. b. bars 940
27 (~~28~~) Hg
 $\frac{7.5}{10}$

SCREEN DUMP

TIME: 10 DEC 1990 11:05:03.5

ANALOG DATA

AVG	1375	*F	NGP SPEED	102	%	SUCTION PRS	660	PSI
MAX	1426	*F	NGP SPEED	11054	RPM	DISCHG PRS	738	PSI
MIN	1314	*F	NPT SPEED	76	%	DISCHG TEMP.	61	*F
+ COMP	115	*F	NPT SPEED	7210	RPM	COMP.THRST OUT	176	*F
CTIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	176	*F
TEMP	46	*F	GV DRIVE	-2	MA	BUF.GAS FIL DP	1	PSI
THRUST	167	*F	GV POS.	-4.4	V	BUF.AIR DP	25	PSI
THRUST	169	*F	BV DRIVE	4	MA	SEAL VNT PR	1	PSI
G.2BRG DRN	215	*F	BV POS.	4.9	V	BUF.GAS DP	23	PSI
R INLET DP	1	H2O	ENGINE PCD	202	PSI			
L TNK PRS	1	H2O	FUEL ACTUATOR	25	MA			
L TANK TEMP.	165	*F	OIL PRESS.	41.9	PSI	COALESCER	1	H2O
BE OILTEMP	146	*F	BAT.VOLT	24.3	V	AMBT PRESS	14.0	PSIA
ARTR PRES	-0	PSI	GAS FUEL PRS	368	PSI	REL HUMIDITY	86	%
RV HYD PRS	975	PSI	OIL FILTER DP	18	PSI			

SCREEN DUMP TIME: 10 DEC 1990 11:15:22.6

ANALOG DATA

AVG	1376	*F	NGP SPEED	102	%	SUCTION PRS	660	PSI
MAX	1427	*F	NGP SPEED	11080	RPM	DISCHG PRS	738	PSI
MIN	1311	*F	NPT SPEED	76	%	DISCHG TEMP.	61	*F
+ COMP	115	*F	NPT SPEED	7210	RPM	COMP.THRST OUT	177	*F
CTIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	177	*F
TEMP	46	*F	GV DRIVE	-2	MA	BUF.GAS FIL DP	0	PSI
THRUST	167	*F	GV POS.	-4.4	V	BUF.AIR DP	25	PSI
THRUST	169	*F	BV DRIVE	4	MA	SEAL VNT PR	1	PSI
G.2BRG DRN	216	*F	BV POS.	4.9	V	BUF.GAS DP	23	PSI
R INLET DP	1	H2O	ENGINE PCD	203	PSI			
L TNK PRS	1	H2O	FUEL ACTUATOR	25	MA			
L TANK TEMP.	165	*F	OIL PRESS.	41.9	PSI	COALESTER	1	H2O
BE OILTEMP	144	*F	BAT.VOLT	24.3	V	AMBT PRESS	14.1	PSIA
ARTR PRES	-0	PSI	GAS FUEL PRS	368	PSI	REL HUMIDITY	86	%
RV HYD PRS	976	PSI	OIL FILTER DP	19	PSI			

SCREEN DUMP TIME: 10 DEC 1990 11:30:18.8

ANALOG DATA

AVG	1375	°F	NGP SPEED	102	%	SUCTION PRS	658	PSI
MAX	1426	°F	NGP SPEED	11080	RPM	DISCHG PRS	739	PSI
MIN	1309	°F	NPT SPEED	76	%	DISCHG TEMP.	61	°F
+ COMP	120	°F	NPT SPEED	7214	RPM	COMP.THRST OUT	177	°F
TIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	177	°F
TEMP	45	°F	GV DRIVE	-2	MA	BUF.GAS FIL DP	1	PSI
THRUST	169	°F	GV POS.	-4.4	V	BUF.AIR DP	25	PSI
THRUST	171	°F	BV DRIVE	4	MA	SEAL VNT PR	1	PSI
NG.2BRG DRN	216	°F	BV POS.	4.9	V	BUF.GAS DP	23	PSI
ER INLET DP	1	H2O	ENGINE PCD	203	PSI			
IL TNK PRS	1	H2O	FUEL ACTUATOR	25	MA			
IL TANK TEMP.	167	°F	OIL PRESS.	42.1	PSI			
BE OILTEMP	146	°F	BAT.VOLT	24.3	V	COALESCER	1	H2O
PARTR PRES	-0	PSI	GAS FUEL PRS	369	PSI	AMBT PRESS	14.1	PSIA
ERVO HYD PRS	976	PSI	OIL FILTER DP	19	PSI	REL HUMIDITY	88	%

SCREEN DUMP TIME: 10 DEC 1990 11:45:04.7

ANALOG DATA

AVG	1376	°F	NGP SPEED	102	%	SUCTION PRS	658	PSI
MAX	1423	°F	NGP SPEED	11080	RPM	DISCHG PRS	739	PSI
MIN	1312	°F	NPT SPEED	76	%	DISCHG TEMP.	62	°F
+ COMP	122	°F	NPT SPEED	7219	RPM	COMP.THRST OUT	178	°F
TIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	176	°F
TEMP	45	°F	GV DRIVE	-2	MA	BUF.GAS FIL DP	1	PSI
THRUST	168	°F	GV POS.	-4.5	V	BUF.AIR DP	25	PSI
THRUST	171	°F	BV DRIVE	4	MA	SEAL VNT PR	1	PSI
NG.2BRG DRN	217	°F	BV POS.	4.9	V	BUF.GAS DP	23	PSI
ER INLET DP	1	H2O	ENGINE PCD	203	PSI			
IL TNK PRS	1	H2O	FUEL ACTUATOR	25	MA			
IL TANK TEMP.	167	°F	OIL PRESS.	42.0	PSI			
BE OILTEMP	145	°F	BAT.VOLT	24.3	V	COALESCER	1	H2O
PARTR PRES	-0	PSI	GAS FUEL PRS	369	PSI	AMBT PRESS	14.1	PSIA
ERVO HYD PRS	976	PSI	OIL FILTER DP	18	PSI	REL HUMIDITY	86	%

PGIT - Station 6 A
December 1990

Test No.	6-6A	#2					
Date		12/10/90					
Time		12:20	12:30	12:35	12:50	1:05	1:20
Data By:		CTA		CTA			
Fuel Flow Rate mscfd SCF/hr $\times 100$		99790 1098	99720 1104	99727 1105	997955 1108	99783 1109	998011 1108
Exhaust Temp.		947°F	947°F	947	946°	945	945°
T-5		1375°F	1375°F	1375°F	1375°F	1375°	1376
Gas Producer Speed (NGP)		102% 11099 rpm	102 11093	102 11093	102 11080	102 11093	102 11086
Gas Producer Comp Discharge (PLP)		203 PSI	202	202	203	203	203
Inlet pressure		14.1 PSIA	14.1	14.1	14.1	14.1	14.1

Barometer

940 940 940 940 939 939

Rel Humidity

83% 83% 80% 83% 86 85%

T-1 (Ambient)

45°F 45°F 46° 45° 45° 440

SCREEN DUMP TIME: 10 DEC 1990 12:20:28.0

ANALOG DATA

AVG	1375	"F	NGP SPEED	102	%	SUCTION PRS	656	PSI
MAX	1426	"F	NGP SPEED	11093	RPM	DISCHG PRS	739	PSI
MIN	1314	"F	NPT SPEED	77	%	DISCHG TEMP	62	"F
+ COMP	124	"F	NPT SPEED	7267	RPM	COMP.THRST OUT	178	"F
ATIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	177	"F
TEMP	45	"F	GV DRIVE	-2	MA	BUF.GAS FIL DP	1	PSI
THRUST	167	"F	GV POS.	-4.5	V	BUF.AIR DP	25	PSI
THRUST	171	"F	BV DRIVE	4	MA	SEAL VNT PR	1	PSI
NG.2BRG DRN	218	"F	BV POS.	4.9	V	BUF.GAS DP	23	PSI
IR INLET DP	1	H2O	ENGINE PCD	203	PSI			
IL TNK PRS	1	H2O	FUEL ACTUATOR	25	MA			
IL TANK TEMP.	167	"F	OIL PRESS.	42.0	PSI			
UBE OILTEMP	145	"F	BAT.VOLT	24.3	V	COALESCER	1	H2O
IARTR PRES	-0	PSI	GAS FUEL PRS	368	PSI	AMBT PRESS	14.0	PSIA
ERVO HYD PRS	976	PSI	OIL FILTER DP	19	PSI	REL HUMIDITY	83	%

SCREEN DUMP TIME: 10 DEC 1990 12:30:15.6

ANALOG DATA

AVG	1373	"F	NGP SPEED	102	%	SUCTION PRS	656	PSI
MAX	1427	"F	NGP SPEED	11099	RPM	DISCHG PRS	738	PSI
MIN	1311	"F	NPT SPEED	77	%	DISCHG TEMP	62	"F
+ COMP	124	"F	NPT SPEED	7285	RPM	COMP.THRST OUT	179	"F
ATIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	177	"F
TEMP	45	"F	GV DRIVE	-2	MA	BUF.GAS FIL DP	1	PSI
THRUST	167	"F	GV POS.	-4.5	V	BUF.AIR DP	25	PSI
THRUST	171	"F	BV DRIVE	4	MA	SEAL VNT PR	1	PSI
NG.2BRG DRN	218	"F	BV POS.	4.9	V	BUF.GAS DP	23	PSI
IR INLET DP	1	H2O	ENGINE PCD	203	PSI			
IL TNK PRS	1	H2O	FUEL ACTUATOR	26	MA			
IL TANK TEMP.	167	"F	OIL PRESS.	42.1	PSI			
UBE OILTEMP	145	"F	BAT.VOLT	24.3	V	COALESCER	1	H2O
IARTR PRES	-0	PSI	GAS FUEL PRS	368	PSI	AMBT PRESS	14.1	PSIA
ERVO HYD PRS	976	PSI	OIL FILTER DP	18	PSI	REL HUMIDITY	84	%

SCREEN DUMP TIME: 10 DEC 1990 12:49:21.4

ANALOG DATA

AVG	1375	°F	NGP SPEED	102	%	SUCTION PRS	655	PSI
MAX	1427	°F	NGP SPEED	11080	RPM	DISCHG PRS	739	PSI
MIN	1317	°F	NPT SPEED	77	%	DISCHG TEMP.	62	°F
1 + COMP	127	°F	NPT SPEED	7280	RPM	COMP.THRST OUT	178	°F
ACTIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	177	°F
TEMP	45	°F	GV DRIVE	-2	MA	BUF.GAS FIL DP	1	PSI
2 THRUST	167	°F	GV POS.	-4.5	V	BUF.AIR DP	25	PSI
THRUST	171	°F	BV DRIVE	4	MA	SEAL VNT PR	1	PSI
NG.2BRG DRN	217	°F	BV POS.	4.9	V	BUF.GAS DP	23	PSI
R INLET DP	1	H2O	ENGINE PCD	202	PSI			
IL TNK PRS	1	H2O	FUEL ACTUATOR	26	MA			
L TANK TEMP.	166	°F	OIL PRESS.	42.0	PSI			
WEE OILTEMP	145	°F	BAT.VOLT	24.3	V	COALESCER	1	H2O
PARTR PRES	-0	PSI	GAS FUEL PRS	368	PSI	AMBT PRESS	14.1	PSIA
ERVO HYD PRS	976	PSI	OIL FILTER DP	18	PSI	REL HUMIDITY	84	%

SCREEN DUMP TIME: 10 DEC 1990 13:04:35.6

ANALOG DATA

5 AVG	1376	°F	NGP SPEED	102	%	SUCTION PRS	656	PSI
5 MAX	1427	°F	NGP SPEED	11093	RPM	DISCHG PRS	738	PSI
5 MIN	1314	°F	NPT SPEED	77	%	DISCHG TEMP.	62	°F
1 + COMP	128	°F	NPT SPEED	7280	RPM	COMP.THRST OUT	179	°F
ACTIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	177	°F
1 TEMP	45	°F	GV DRIVE	-2	MA	BUF.GAS FIL DP	2	PSI
2 THRUST	167	°F	GV POS.	-4.5	V	BUF.AIR DP	25	PSI
7 THRUST	171	°F	BV DRIVE	3	MA	SEAL VNT PR	1	PSI
NG.2BRG DRN	217	°F	BV POS.	4.9	V	BUF.GAS DP	24	PSI
IR INLET DP	1	H2O	ENGINE PCD	203	PSI			
IL TNK PRS	1	H2O	FUEL ACTUATOR	25	MA			
IL TANK TEMP.	167	°F	OIL PRESS.	42.0	PSI			
WEE OILTEMP	145	°F	BAT.VOLT	24.3	V	COALESCER	1	H2O
PARTR PRES	-0	PSI	GAS FUEL PRS	366	PSI	AMBT PRESS	14.1	PSIA
ERVO HYD PRS	975	PSI	OIL FILTER DP	19	PSI	REL HUMIDITY	86	%

SCREEN DUMP TIME: 10 DEC 1990 13:19:58.4

ANALOG DATA

AVG	1375	°F	NGP SPEED	102	%	SUCTION PRS	657	PSI
MAX	1420	°F	NGP SPEED	11086	RPM	DISCHG PRS	738	PSI
MIN	1321	°F	NPT SPEED	77	%	DISCHG TEMP.	62	°F
+ COMP	128	°F	NPT SPEED	7267	RPM	COMP.THRST OUT	178	°F
TIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	177	°F
TEMP	44	°F	GV DRIVE	-2	MA	BUF.GAS FIL DP	1	PSI
THRUST	167	°F	GV POS.	-4.5	V	BUF.AIR DP	25	PSI
THRUST	171	°F	BV DRIVE	3	MA	SEAL VNT PR	1	PSI
IG.2BRG DRN	218	°F	BV POS.	4.9	V	BUF.GAS DP	23	PSI
IR INLET DP	1	H2O	ENGINE PCD	203	PSI			
IL TNK PRS	1	H2O	FUEL ACTUATOR	25	MA			
IL TANK TEMP.	167	°F	OIL PRESS.	42.1	PSI			
UBE OILTEMP	145	°F	BAT.VOLT	24.3	V	COALESCER	1	H2O
ARTR PRES	-0	PSI	GAS FUEL PRS	369	PSI	AMBT PRESS	14.1	PSIA
ERVO HYD PRS	973	PSI	OIL FILTER DP	19	PSI	REL HUMIDITY	86	%

KCH
12/9

PGT - Station 6 A
December 1990

Test No.	7-6A 100%	# 3					
Date		12/10					
Time		13:35	13:50	14:05	14:20	14:35	
Data By:		CTA					
Fuel Flow Rate	$\times 100$ $\frac{\text{SCFH}}{\text{MSEC}}$	1105 998040	1103 998066	1106 998094	1101 998121	1097 998149	
Exhaust Temp.	°F	945	945	945	945	945	
T-5	°F	1376	1375	1375	1375	1375	
Gas Producer Speed (NGP)		102 11106rpm	102 11099	102 11099	102 11106	102 11093	
Gas Producer Comp Discharge (PLD) PSI		204 PSI	203	203	204	203	✓ ✓ ✓ ✓
Inlet pressure	PSIA	14.1 PSIA	14.1	14.1	14.1	14.1	

Barometer 938.5 939 939 938.5 938.5

Rel. Humidity 91% 90/91% ~~90%~~^{91%} 92% 91%

T-1 (Ambient) 43°F 43°F 43°F 43°F 44°

SCREEN DUMP TIME: 10 DEC 1990 13:40:19.8

Printer
Problems
unable to get
13:35 Printed

ANALOG DATA

AVG	1376	°F	NGP SPEED	102	%	SUCTION PRS	657	PSI
MAX	1421	°F	NGP SPEED	11099	RPM	DISCHG PRS	737	PSI
MIN	1314	°F	NPT SPEED	77	%	DISCHG TEMP.	62	°F
+ COME	129	°F	NPT SPEED	7276	RPM	COMP.THRST OUT	178	°F
TIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	177	°F
TEMP	43	°F	GV DRIVE	-2	MA	BUF.GAS FIL DP	1	PSI
THRUST	167	°F	GV POS.	-4.5	V	BUF.AIR DP	25	PSI
THRUST	171	°F	BV DRIVE	3	MA	SEAL VNT PR	1	PSI
NG.2BRG DRN	218	°F	BV POS.	4.9	V	BUF.GAS DP	23	PSI
R INLET DP	1	H2O	ENGINE PCD	203	PSI			
L TNK PRS	1	H2O	FUEL ACTUATOR	25	MA			
L TANK TEMP.	166	°F	OIL PRESS.	42.0	PSI			
BE OILTEMP	144	°F	BAT.VOLT	24.3	V	COALESCER	1	H2O
ARTR PRES	-0	PSI	GAS FUEL PRS	369	PSI	AMBT PRESS	14.1	PSIA
ERVO HYD PRS	976	PSI	OIL FILTER DP	19	PSI	REL HUMIDITY	91	%

SCREEN DUMP TIME: 10 DEC 1990 13:50:39.0

ANALOG DATA

AVG	1376	°F	NGP SPEED	102	%	SUCTION PRS	657	PSI
MAX	1420	°F	NGP SPEED	11099	RPM	DISCHG PRS	738	PSI
MIN	1318	°F	NPT SPEED	77	%	DISCHG TEMP.	62	°F
+ COMP	128	°F	NPT SPEED	7258	RPM	COMP.THRST OUT	179	°F
TIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	177	°F
TEMP	43	°F	GV DRIVE	-2	MA	BUF.GAS FIL DP	0	PSI
THRUST	167	°F	GV POS.	-4.5	V	BUF.AIR DP	25	PSI
THRUST	171	°F	BV DRIVE	3	MA	SEAL VNT PR	1	PSI
NG.2BRG DRN	218	°F	BV POS.	4.9	V	BUF.GAS DP	23	PSI
R INLET DP	1	H2O	ENGINE PCD	204	PSI			
L TNK PRS	1	H2O	FUEL ACTUATOR	25	MA			
L TANK TEMP.	167	°F	OIL PRESS.	42.0	PSI			
BE OILTEMP	145	°F	BAT.VOLT	24.3	V	COALESCER	1	H2O
ARTK PRES	-0	PSI	GAS FUEL PRS	370	PSI	AMBT PRESS	14.1	PSIA
ERVO HYD PRS	976	PSI	OIL FILTER DP	19	PSI	REL HUMIDITY	91	%

SCREEN DUMP TIME: 10 DEC 1990 14:04:29.8

ANALOG DATA

AVG	1375	"F	NGP SPEED	102	%	SUCTION PRS	657	PSI
MAX	1421	"F	NGP SPEED	11099	RPM	DISCHG PRS	739	PSI
MIN	1317	"F	NPT SPEED	77	%	DISCHG TEMP.	62	"F
+ COMP	129	"F	NPT SPEED	7258	RPM	COMP.THRST OUT	178	"F
TIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	177	"F
TEMP	43	"F	GV DRIVE	-2	MA	BUF.GAS FIL DP	1	PSI
THRUST	167	"F	GV POS.	-4.5	V	BUF.AIR DP	25	PSI
THRUST	171	"F	BV DRIVE	3	MA	SEAL VNT PR	1	PSI
G.2BRG DRN	218	"F	BV POS.	5.0	V	BUF.GAS DP	23	PSI
R INLET DP	1	H2O	ENGINE PCD	204	PSI			
L TNK PRS	1	H2O	FUEL ACTUATOR	25	MA			
L TANK TEMP.	167	"F	OIL PRESS.	42.1	PSI			
BE OILTEMP	145	"F	BAT.VOLT	24.3	V	COALESCER	1	H2O
ARTR PRES	-0	PSI	GAS FUEL PRS	369	PSI	AMBT PRESS	14.1	PSIA
RVO HYD PRS	976	PSI	OIL FILTER DP	19	PSI	REL HUMIDITY	91	%

SCREEN DUMP TIME: 10 DEC 1990 14:19:25.5

ANALOG DATA

AVG	1376	"F	NGP SPEED	102	%	SUCTION PRS	657	PSI
MAX	1421	"F	NGP SPEED	11106	RPM	DISCHG PRS	739	PSI
MIN	1317	"F	NPT SPEED	77	%	DISCHG TEMP.	62	"F
+ COMP	129	"F	NPT SPEED	7249	RPM	COMP.THRST OUT	178	"F
TIVE TC	17		NPT EXT.SET	99	%	COMP.THRST IN	177	"F
TEMP	43	"F	GV DRIVE	-2	MA	BUF.GAS FIL DP	1	PSI
THRUST	167	"F	GV POS.	-4.5	V	BUF.AIR DP	25	PSI
THRUST	171	"F	BV DRIVE	4	MA	SEAL VNT PR	1	PSI
G.2BRG DRN	218	"F	BV POS.	4.9	V	BUF.GAS DP	23	PSI
R INLET DP	1	H2O	ENGINE PCD	204	PSI			
L TNK PRS	1	H2O	FUEL ACTUATOR	25	MA			
L TANK TEMP.	166	"F	OIL PRESS.	42.0	PSI			
BE OILTEMP	145	"F	BAT.VOLT	24.3	V	COALESCER	1	H2O
ARTR PRES	-0	PSI	GAS FUEL PRS	369	PSI	AMBT PRESS	14.0	PSIA
RVO HYD PRS	976	PSI	OIL FILTER DP	18	PSI	REL HUMIDITY	91	%

APPENDIX E
EMISSIONS CALCULATIONS

GAS FUEL "F" FACTOR CALCULATIONS

Source - PGT Station 6
 BY - KCH
 DATE - 01/15/91
 TIME - 11:56
 Reference
 Temp, °F 60

SPECIES	VOL.%	lb./lb-mol. (Fuel)			N	S
		C	H	O		
CH4	97.3000	11.676	3.892	0.000	0.000	0.000
C2H6	2.0000	0.480	0.120	0.000	0.000	0.000
C3H8	0.2000	0.072	0.016	0.000	0.000	0.000
C4H10 - I	0.0000	0.000	0.000	0.000	0.000	0.000
C4H10 - N	0.0000	0.000	0.000	0.000	0.000	0.000
C5H12 - I	0.0000	0.000	0.000	0.000	0.000	0.000
C5H12 - N	0.0000	0.000	0.000	0.000	0.000	0.000
C6H6	0.0000	0.000	0.000	0.000	0.000	0.000
CO2	0.4000	0.048	0.000	0.128	0.000	0.000
N2	0.0000	0.000	0.000	0.000	0.000	0.000
H2S	1.00E-05	0.000	0.000	0.000	0.000	0.000
Total	99.90	12.276	4.028	0.128	0.000	0.00000
WT.%		74.708	24.513	0.779	0.000	0.00002

GAS MW = 16.432 lb/lb-mole
 HHV = 1025.00 Btu/SCF
 23672.55 Btu/lb
 DENSITY = 0.0433 lb/SCF

F - FACTOR: (O2 based)
 @ 68 °F= 8,583 DSCF/MMBtu @ 0% O2
 @ 60 °F= 8,453 DSCF/MMBtu @ 0% O2

F - FACTOR: (CO2 based)
 @ 68 °F= 1013.04 DSCF/MMBtu
 @ 60 °F= 997.69 DSCF/MMBtu

O2 BASED

TEST NO	FUEL FLOW (SCFH)	EXHAUST O2 (% dry)	EXHAUST FLOW (DSCFM)	SO2 lb/hr	SO2 ppm	SO2 ppm @15%O2
5-6A	109300	15.28	58,694	0.001	0.000	0.000
6-6A	110500	15.30	59,550	0.001	0.000	0.000
7-6A	110240	15.33	59,730	0.001	0.000	0.000

CO2 BASED

TEST NO	FUEL FLOW (SCFH)	EXHAUST O2 (% dry)	EXHAUST FLOW (DSCFM)	SO2 lb/hr	SO2 ppm	SO2 ppm @15%O2
5-6A	109300	3.00	62,097	0.001	0.000	0.000
6-6A	110500	3.00	62,778	0.001	0.000	0.000
7-6A	110240	3.00	62,631	0.001	0.000	0.000

EMISSION CALCULATIONS

1. Sample Volume and Isokinetics

- a. Sample gas volume, dscf

$$V_{m \text{ std}} = 0.03342 V_m [P_{\text{bar}} + (H/13.6)] (T_{\text{ref}}/T_m) (Y)$$

- b. Water vapor volume, scf

$$V_{w \text{ std}} = 0.0472 V_{lc} (T_{\text{ref}}/528^{\circ}\text{R})$$

- c. Moisture content, nondimensional

$$B_{wo} = V_{w \text{ std}} / (V_{m \text{ std}} + V_{w \text{ std}})$$

- d. Stack gas molecular weight, lb/lb mole

$$MW_{\text{dry}} = 0.44(\% \text{ CO}_2) + 0.32(\% \text{ O}_2) + 0.28(\% \text{ N}_2)$$

$$MW_{\text{wet}} = MW_{\text{dry}} (1 - B_{wo}) + 18 (B_{wo})$$

- e. Absolute stack pressure, iwg

$$P_s = P_{\text{bar}} + P_{\text{sg}}/13.6$$

- f. Stack velocity, ft/sec

$$V_s = 2.90 C_p \sqrt{\Delta P T_s} \sqrt{\frac{29.92 \times 28.95}{P_s MW_{\text{wet}}}}$$

- g. Actual stack gas flow rate, wacfm

$$Q = (V_s)(A_s)(60)$$

- h. Standard stack gas flow rate, dscfm

$$Q_{sd} = Q (1 - B_{wo}) (T_{\text{ref}}/T_s) (P_s/29.92)$$

- i. Percent isokinetic

$$I = \frac{17.32 \times T_s (V_{m \text{ std}})}{(1 - B_{wo})^0 \times V_s \times P_s \times D_n^2} \times \frac{528^{\circ}\text{R}}{T_{\text{ref}}}$$

2. Particulate Emissions

- a. Grain loading, gr/dscf

$$C = 0.01543 (M_n/V_{m \text{ std}})$$

- b. Grain loading at 12% CO₂, gr/dscf

$$C_{12\% \text{ CO}_2} = C (12\% \text{ CO}_2)$$

c. Mass emissions, lb/hr

$$M = C \times Q_{sd} \times (60 \text{ min/hr}) / (7000 \text{ gr/lb})$$

3. Gaseous Emissions, lb/hr

$$M = \text{ppm} \times 10^{-6} \frac{MW_i \text{ lb/lb mole}}{SV} \times Q_{sd} \times 60 \text{ min/hr}$$

where SV = specific molar volume of an ideal gas:

$$\begin{aligned} 385.3 \text{ ft}^3/\text{lb mole for } T_{ref} &= 528 \text{ }^\circ\text{R} \\ 379.5 \text{ ft}^3/\text{lb mole for } T_{ref} &= 520 \text{ }^\circ\text{R} \end{aligned}$$

4. Emissions Rates, lb/10⁶ Btu

a. Fuel factor at 68 °F, dscf/10⁶ Btu at 0% O₂

$$F_{68} = \frac{10^6 [3.64(\%H) + 1.53(\%C) + 0.14(\%N) + 0.57(\%S) - 0.46(\%O_2, \text{fuel})]}{HHV, \text{ Btu/lb}}$$

b. Fuel factor at 60 °F

$$F_{60} = F_{68} (520 \text{ }^\circ\text{R} / 528 \text{ }^\circ\text{R})$$

c. Gaseous emission factor

$$\text{lb/10}^6 \text{ Btu}_i = \text{ppm}_i \times 10^{-6} \times \frac{MW_i \text{ lb}}{\text{lb mole}} \times \frac{1}{SV} \times F \times \frac{20.9}{20.9 - \%O_2}$$

d. Particulate emission factor

$$\text{lb/10}^6 \text{ Btu} = C \times \frac{1 \text{ lb}}{7000 \text{ gr}} \times F \times \frac{20.9}{20.9 - \%O_2}$$

These calculations are routinely performed on Carnot's computer.

Nomenclature:

A_s	= stack area, ft^2
B_{wo}	= flue gas moisture content
$C_{12\% \text{ CO}_2}$	= particulate grain loading, gr/dscf corrected to 12% CO_2
C	= particulate grain loading, gr/dscf
C_p	= pitot calibration factor, dimensionless
D_n	= nozzle diameter, in.
F	= fuel F factor, $\text{dscf}/10^6 \text{ Btu}$ at 0% O_2
H	= orifice pressure differential, iwg
I	= % isokinetics
M_n	= mass of collected particulate, mg
M_i	= mass emissions of species i , lb/hr
MW	= molecular weight of flue gas
MW_i	= molecular weight of species i :
	NO_x : 46
	CO : 28
	SO_2 : 64
	HC : 16
θ	= sample time, min.
ΔP	= average velocity head, iwg $= (\sqrt{\Delta P})^2$
P_{bar}	= barometric pressure, in.Hg
P_s	= stack absolute pressure, in.Hg.
P_{sg}	= stack static pressure, iwg
Q	= wet stack gas flow rate at actual conditions, wacfm
Q_{sd}	= dry stack gas flow rate at standard conditions, dscfm
SV	= specific molar volume of an ideal gas at std conditions, $\text{ft}^3/\text{lb mole}$
T_m	= meter temperature, $^{\circ}\text{R}$
T_{ref}	= reference temperature, $^{\circ}\text{R}$
T_s	= stack temperature, $^{\circ}\text{R}$
V_s	= stack velocity, ft/sec
V_{lc}	= volume of liquid collected in impingers, ml
V_m	= dry meter volume uncorrected, dcf
$V_{m \text{ std}}$	= dry meter volume at standard conditions, dscf
$V_{w \text{ std}}$	= volume of water vapor at standard conditons, scf
Y	= meter calibration coefficient

CARNOT

SUBJECT Calculation of ISO Factors

JOB NO. _____

SHEET NO. 1 of 2

COMPUTED BY K. Hopkins

DATE _____

CHECKED BY _____

DATE _____

$$ISO = \left(\frac{29.92}{B.P.} \right)^{1/2} \left(\frac{288^{\circ}K}{T_{amb}} \right)^{1.53} 14(H - 0.00633) e$$

B.P. : Barometric pressure, in Hg

T_{amb} : Ambient Temperature, K (same as dry bulb temperature)

H : humidity, lb H₂O / lb dry air

Example:

Test No. 5-6A

T wet bulb = ~~46°F~~ 43.8°F

T dry bulb = ~~48°F~~ 45.5°F = 280.5 K

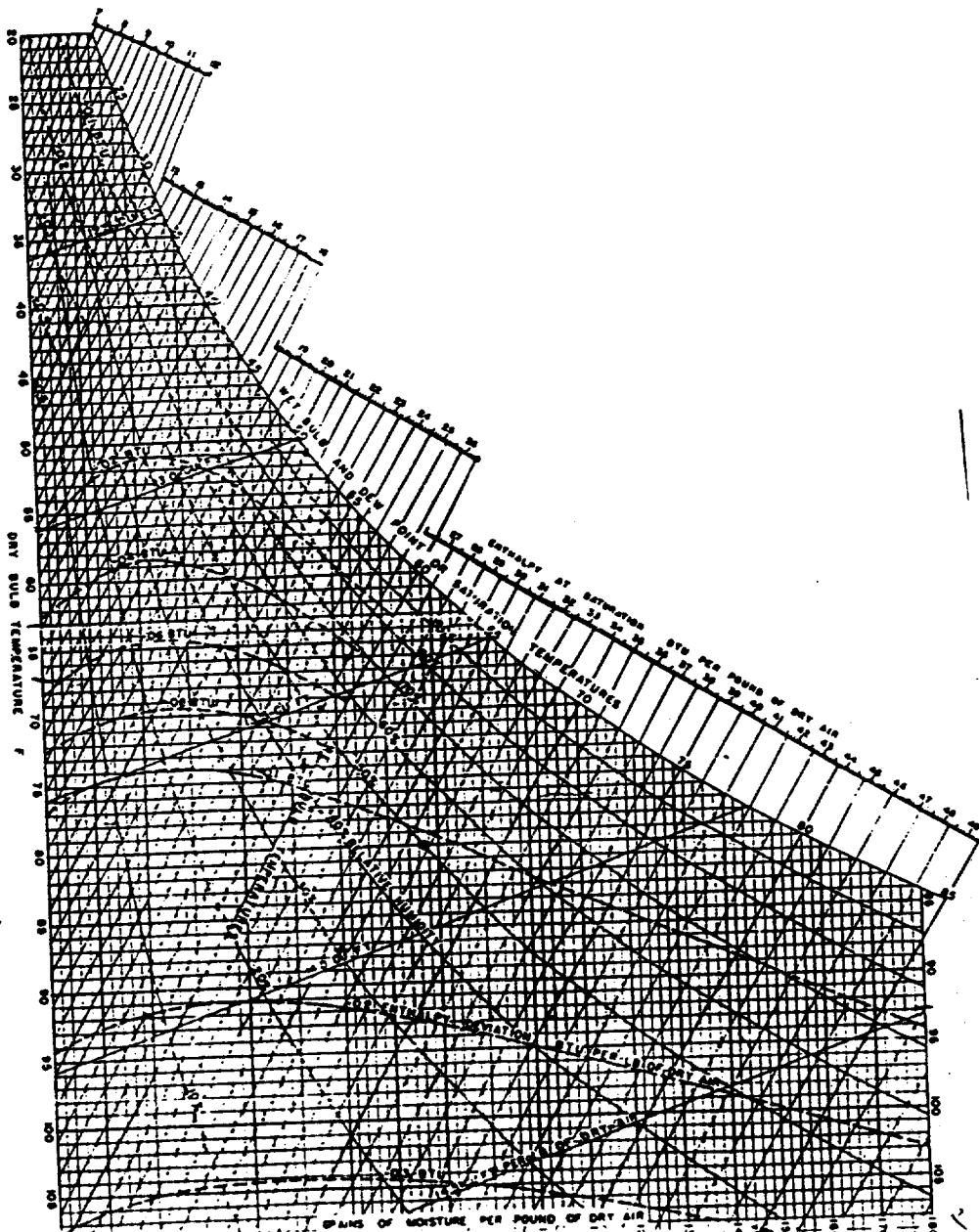
B.P. = 27.66 in Hg

From psychrometric chart (see attached)

H = 0.0057 lb H₂O / lb air

$$\underline{\underline{ISO = 1.0700}}$$

FIG. A-1 Psychrometric chart, normal temperatures, English units, $p = 1$ atm.
(Carrier Corporation.)



CARNOT

SUBJECT Calculation of EPA "F-Factor" and Exhaust Flow,
and NO_x mass emissions

JOB NO. 82100

SHEET NO. 1 of 3

COMPUTED BY K. Hopkins

DATE 1/4/91

CHECKED BY _____

DATE _____

GIVEN: 1. Natural Gas Fuel Analysis:

Species	CH ₄	C ₂ H ₆	C ₃ H ₈	CO ₂	H ₂ S
Vol%	97.3	2.0	0.2	0.4	1×10^{-5}

$$HHV = 1025 \text{ Btu/scf}$$

2. Fuel flow for test 5-64

$$Q_f = 109,300 \text{ scfh}$$

3. Exhaust O₂ = 15.28%

FIND: 1. "F-Factor" @ 60°F

2. Exhaust Flow rate, @ d scfh

Step 1. Convert from Volume % to Atom Weight %

	%VOL	C	H	O	S
CH ₄	97.3	11.676	3.892	0.00	0.00
C ₂ H ₆	2.0	0.480	0.120	0.00	0.00
C ₃ H ₈	0.2	0.072	0.016	0.00	0.00
CO ₂	0.4	0.048	0.00	0.128	0.00
H ₂ S	1×10^{-5}	0.00	0.00	0.00	0.00

$$\sum 12.276 + 4.028 + 0.128 + 0.00 = 16.432 \text{ lb/lb-mole}$$

$$\text{Wt\%: } 74.708 \quad \frac{24.513}{25.513} \quad 0.779 \quad 0.00 \quad \text{H}$$

SUBJECT _____

JOB NO. _____

SHEET NO. 2 of 3

COMPUTED BY _____

DATE _____

CHECKED BY _____

DATE _____

Step 2. Calculate EPA "F-Factor"

From 40 CFR Pt 60, App. A, Meth 19, Eq. 19-13

$$F_{68} = \frac{10^6 \left\{ (3.64)(\%H) + (1.53)(\%C) + (0.14)(\%N) + (0.57)(\%S) - (0.46)(\%O_2 \text{ fuel}) \right\}}{HHV, \text{ Btu/lb}}$$

Specific Molar Volume of an ideal gas @ 60°F

$$SV = 379.5 \frac{\text{ft}^3}{\text{lb mole}}$$

$$HHV, \frac{\text{Btu}}{\text{lb}} = \frac{\left(1025 \frac{\text{Btu}}{\text{ft}^3} \right) \left(379.5 \frac{\text{ft}^3}{\text{lb mole}} \right)}{16.432 \frac{\text{lb}}{\text{lb mole}}} = 23,672.55 \frac{\text{Btu}}{\text{lb}}$$

$$F_{68} = \frac{10^6 \left\{ (3.64)(28.513) + (1.53)(74.708) + (0.14)(0.6) + (0.57)(0.0) - (0.46)(0.0) \right\}}{23,672.55}$$

$$F_{68} = 8582.6 \text{ dscf/MMBtu @ 0\% O}_2$$

$$F_{60} = (8582.6) \left(\frac{526}{520} \right) = 8452.6 \text{ dscf/MMBtu @ 0\% O}_2$$

SUBJECT _____ JOB NO. _____

SHEET NO. 3 of 3

COMPUTED BY _____ DATE _____ CHECKED BY _____ DATE _____

Step 3 Compute Exhaust flow

$$Q_{\text{Exhaust}} = (F_{60})(HHV)(Q_f)(10^{-6})\left(\frac{1}{60}\right)\left(\frac{20.9}{20.9 - \%O_2}\right)$$

$$= (8452.6)(1025)(109,300)(10^{-6})\left(\frac{1}{60}\right)\left(\frac{20.9}{20.9 - 15.20\%}\right)$$

$$\underline{Q_{\text{Exhaust}} = 58,694 \text{ dscfm}}$$

Step 4 Compute NO_x in lb/hr

$$\dot{M}_{NO_x} = (NO_x, \text{ppm dry}) \times 10^{-6} \left(\frac{46 \frac{\text{lb}}{\text{lb-mole}}}{379.5 \frac{\text{ft}^3}{\text{lb-mole}}} \right) \times Q_{\text{Exhaust}} \times 60$$

$$\dot{M}_{NO_x} = (162.0)(10^{-6})\left(\frac{46}{379.5}\right)(58,694)(60)$$

$$\underline{\dot{M}_{NO_x} = 69.15 \text{ lb/hr}} \Rightarrow \text{test No. 5-6A}$$

CARNOT

SUBJECT Calculation of Exhaust Flow Based JOB NO. _____
on CO₂ based F-Factor SHEET NO. 1 of 1
COMPUTED BY K. Hopkins DATE _____ CHECKED BY _____ DATE _____

CO₂ based F-Factor

$$F_{60} = 10^6 (\%C)(0.321) / HHV$$

$$= 10^6 (74.700)(0.321) / 23,672.55$$

$$= 1,013.04 \text{ dscf} / 10^6 \text{ Btu}$$

$$F_{60} = \left(\frac{520}{528} \right) F_{68} = 997.69 \text{ dscf} / 10^6 \text{ Btu}$$

$$Q_{\text{exhaust}} = (F_{60})(HHV)(Q_f)(10^{-6})(1/60) \left(\frac{100}{\% \text{ CO}_2} \right)$$

Test 5-6A

$$Q_{\text{exhaust}} = (997.69)(1025)(109,300)(10^{-6})(1/60) \left(\frac{100}{3.00} \right)$$
$$= 62,097 \text{ dscfm}$$

CARNOT

SUBJECT Calculation of Exhaust SO₂ Concentration JOB NO. 82100

SHEET NO. 1 of 2

COMPUTED BY K. Hopkins DATE _____ CHECKED BY _____ DATE _____

- Given:
1. "F-Factor" @ 60°F
 2. HHV, Btu/scf
 3. Exhaust O₂
 4. Fuel Flow, scfh
 5. Wt% of Sulfur in Natural Gas

FIND: Exhaust Concentration of SO₂

Assume: All sulfur in reactants is found as SO₂ in products

$$\text{"F-Factor"} = 8,453 \text{ DSCF/MMBtu @ } 0\% \text{ O}_2$$

$$Q_f = 109,300 \text{ scfh}$$

$$\text{HHV} = 1025 \text{ Btu/scf}$$

$$\text{O}_2 = 15.28 \%$$

$$\text{Wt\% S} = 2.0 \times 10^{-5} \%$$

$$\text{MW}_{\text{SO}_2} = 64 \text{ lb/lb-mole}$$

$$Q_{\text{exhaust}} = (F_{60})(\text{HHV})(Q_f)(10^{-6})\left(\frac{1}{60}\right)\left(\frac{20.9}{20.9 - \% \text{O}_2}\right)$$

$$\dot{m}_{\text{SO}_2} = (Q_f)(P_f) \frac{\text{Wt\% S}}{100}$$

$$\text{ppm SO}_2 = (\dot{m}_{\text{SO}_2})(10^6)(379.5) / (64 Q_{\text{exhaust}}(60))$$

CARNOT

SUBJECT _____ JOB NO. _____

SHEET NO. 2 of 2

COMPUTED BY _____ DATE _____ CHECKED BY _____ DATE _____

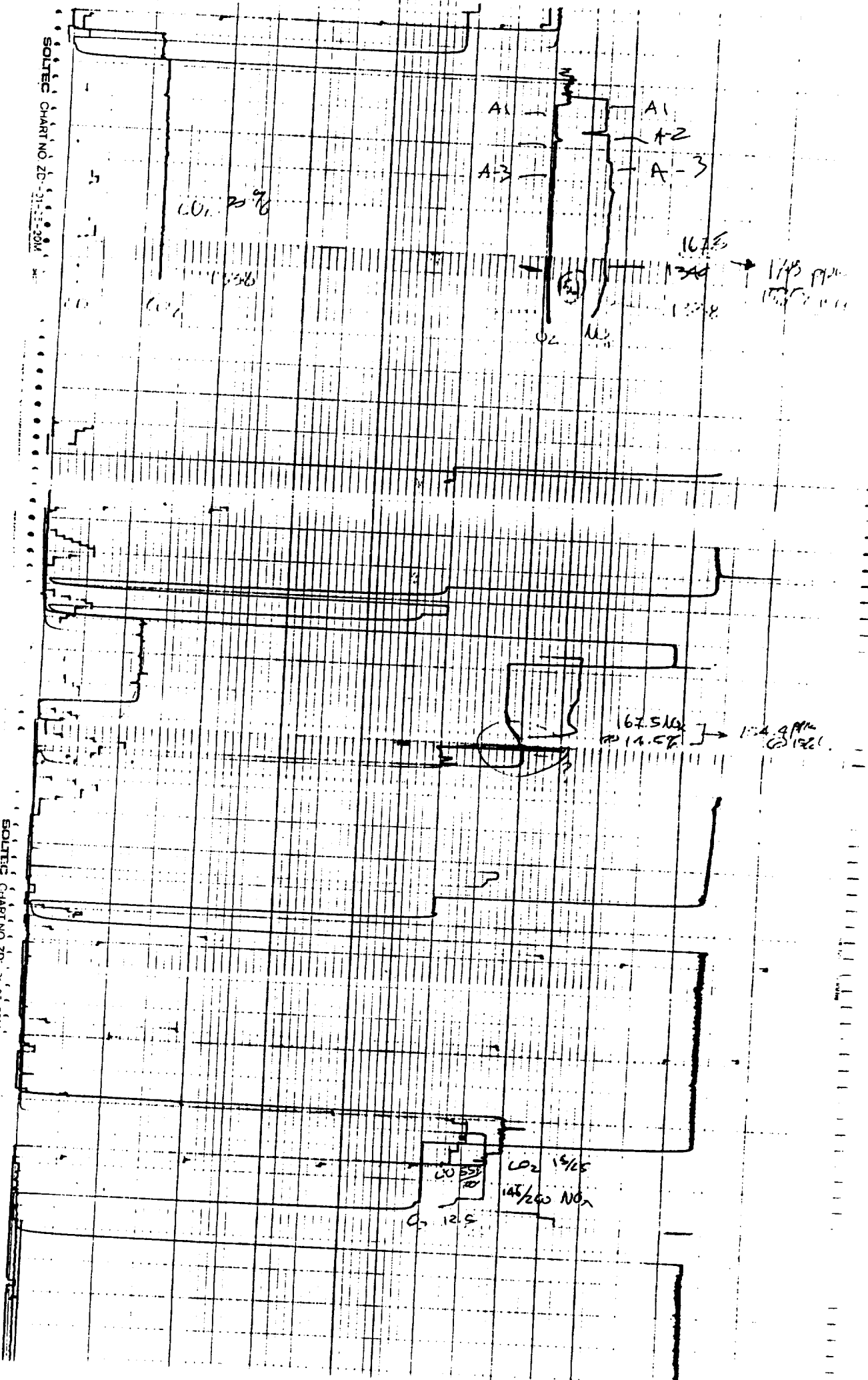
$$\text{ppm SO}_2 = \frac{(Q_f)(P_f)\left(\frac{\text{wt\% S}}{100}\right)(10^6)(379.5)}{(6A)(F_{60})(HHV)(Q_f)(10^{-6})\left(\frac{1}{60}\right)\left(\frac{20.9}{20.9 - O_2}\right)60}$$

$$\text{ppm SO}_2 = \frac{(2.88 \times 10^9)(P_f)(\text{wt\% S})(20.9 - \%O_2)}{(F_{60})(HHV)}$$

APPENDIX F
STRIP CHARTS

SOLTEC CHART NO. ZD-01-25-20M

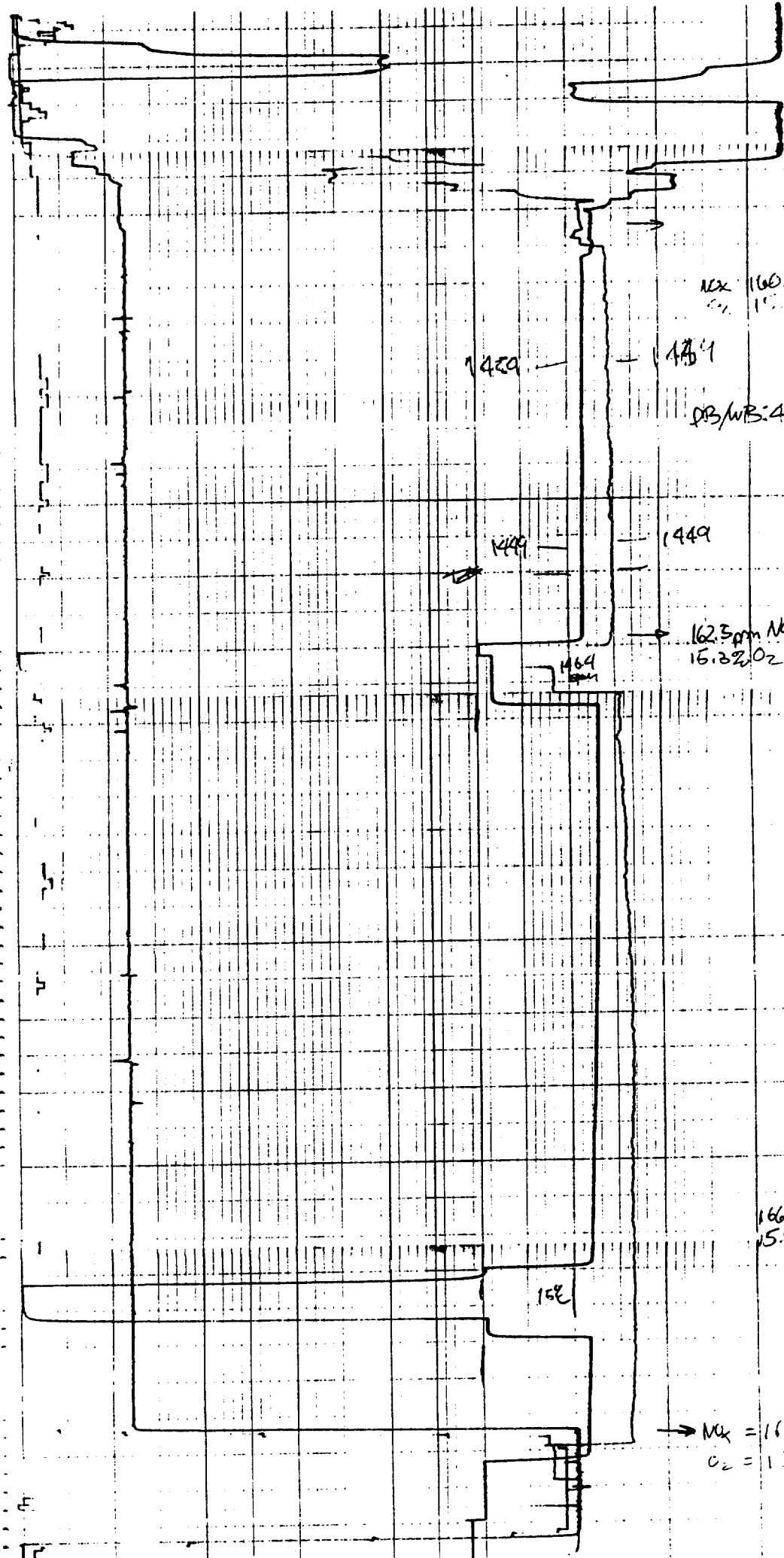
SOLTEC CHART NO. ZD-01-25-20M



25-20M

2020

SOLETC CHART NO. 201-10-25-20M



10x 100.0cm
15.2%

16.1%

1459 — 1464

DB/WB: 45/44

1449 — 1449

162.3pm N₂
15.2% O₂ → 17.2 ft

1464

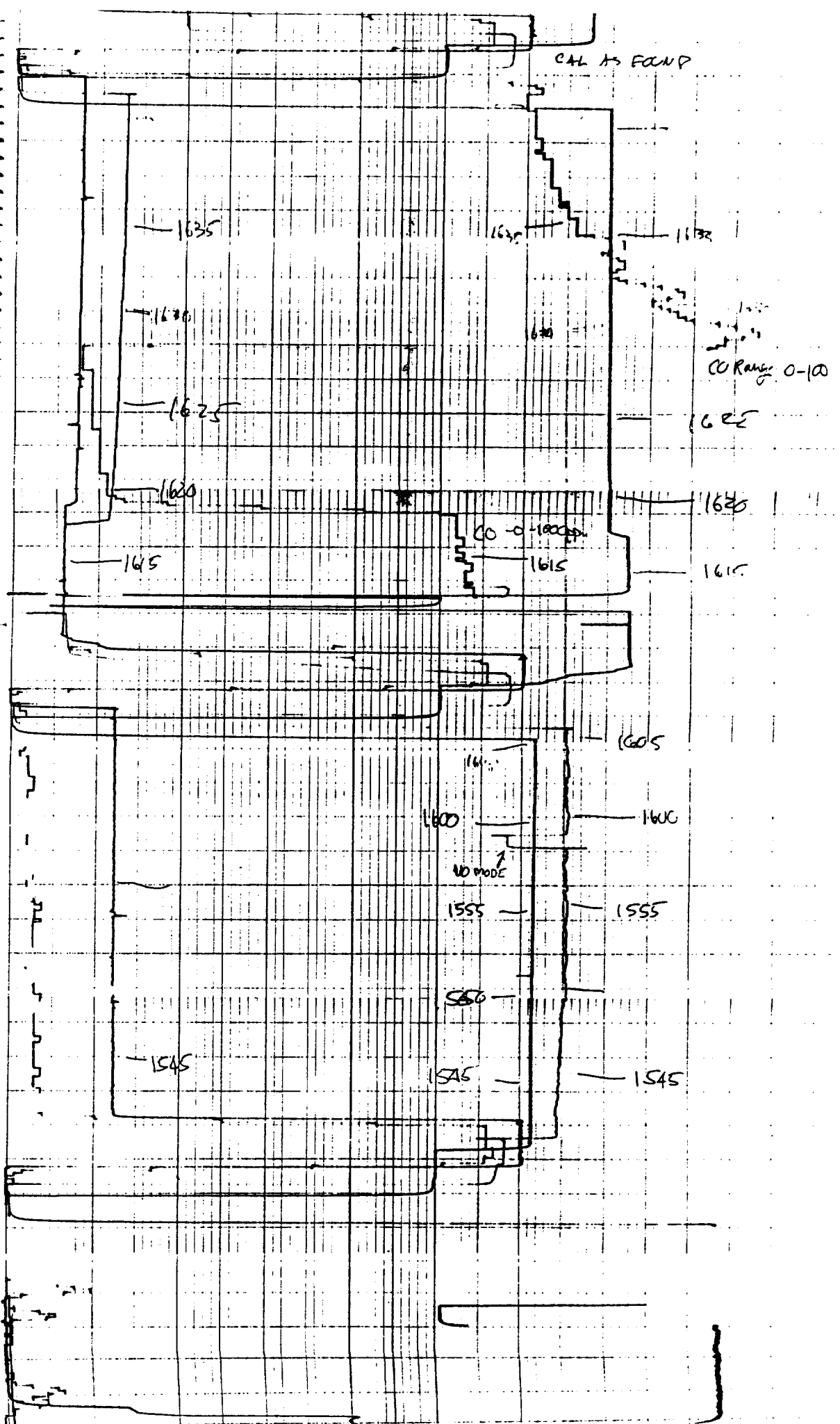
166.3pm
15.5%

168

→ M_K = 165.0
O₂ = 15.2% → 17.2 ft
@ 15.2%

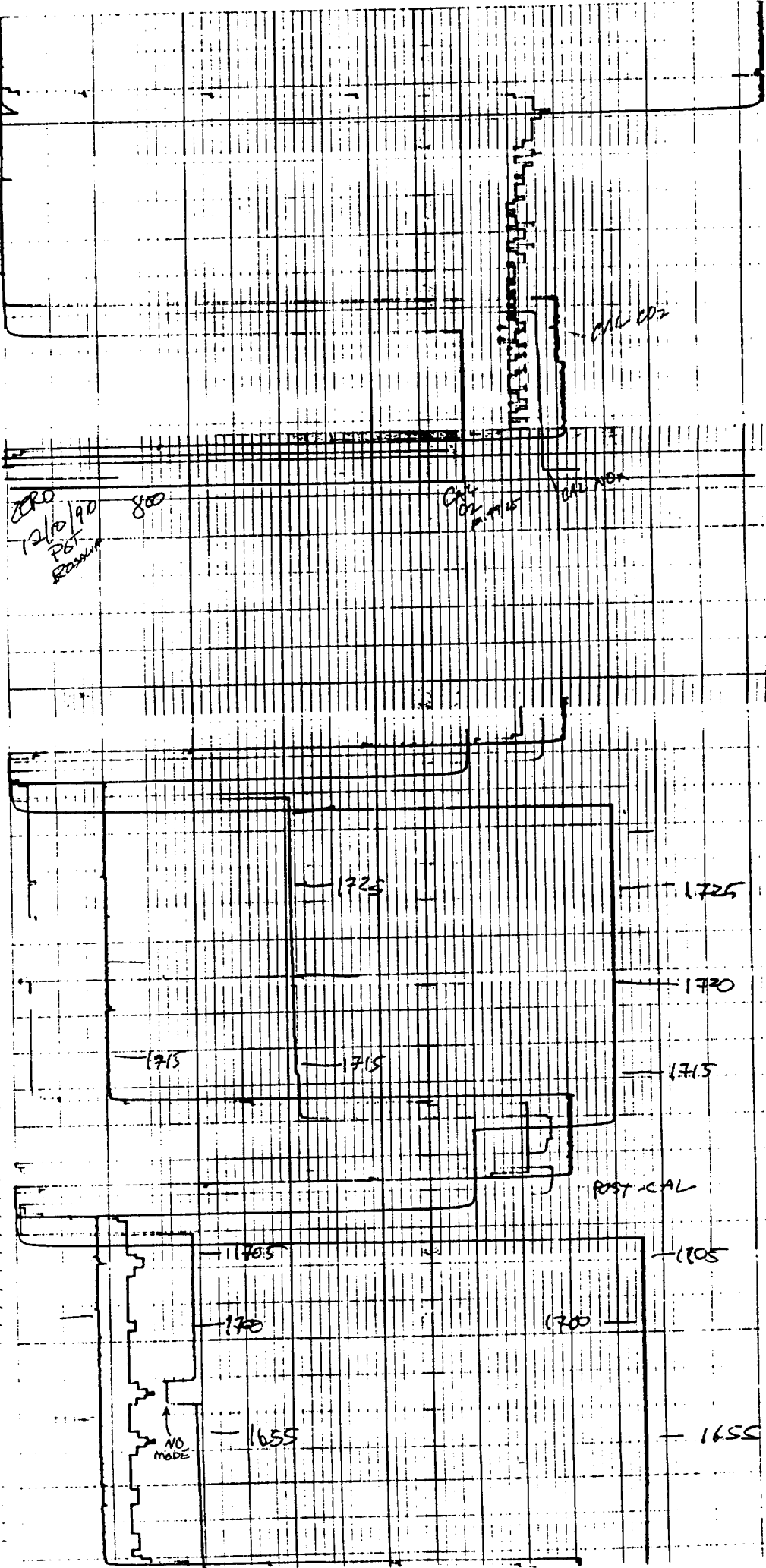
SOUEC CHART NO. ZD1-01-25-20M

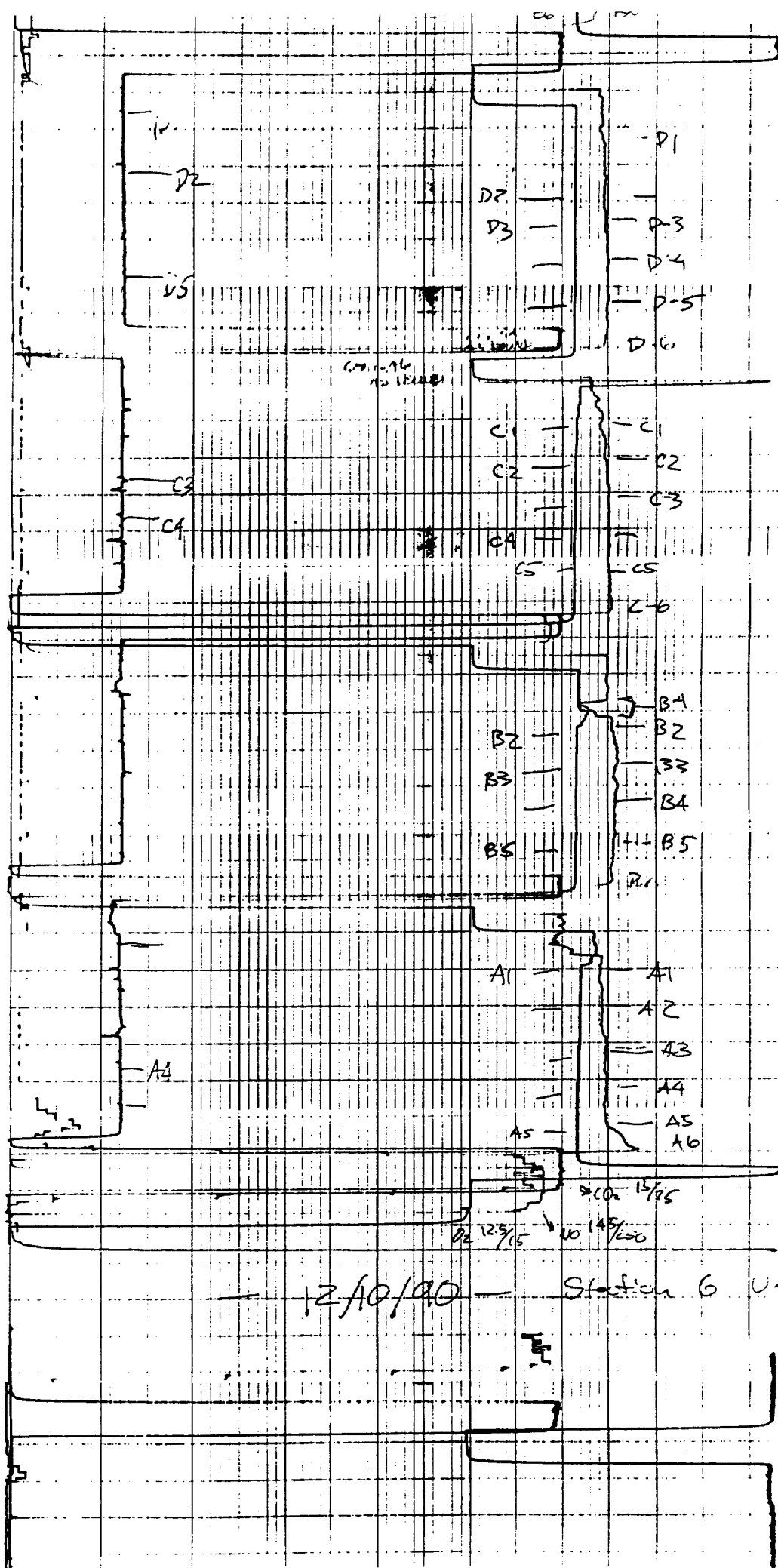
SOUEC CHART NO. ZD1-01-25-20M



SOURCE CHART NO. ZD-01-25-20M

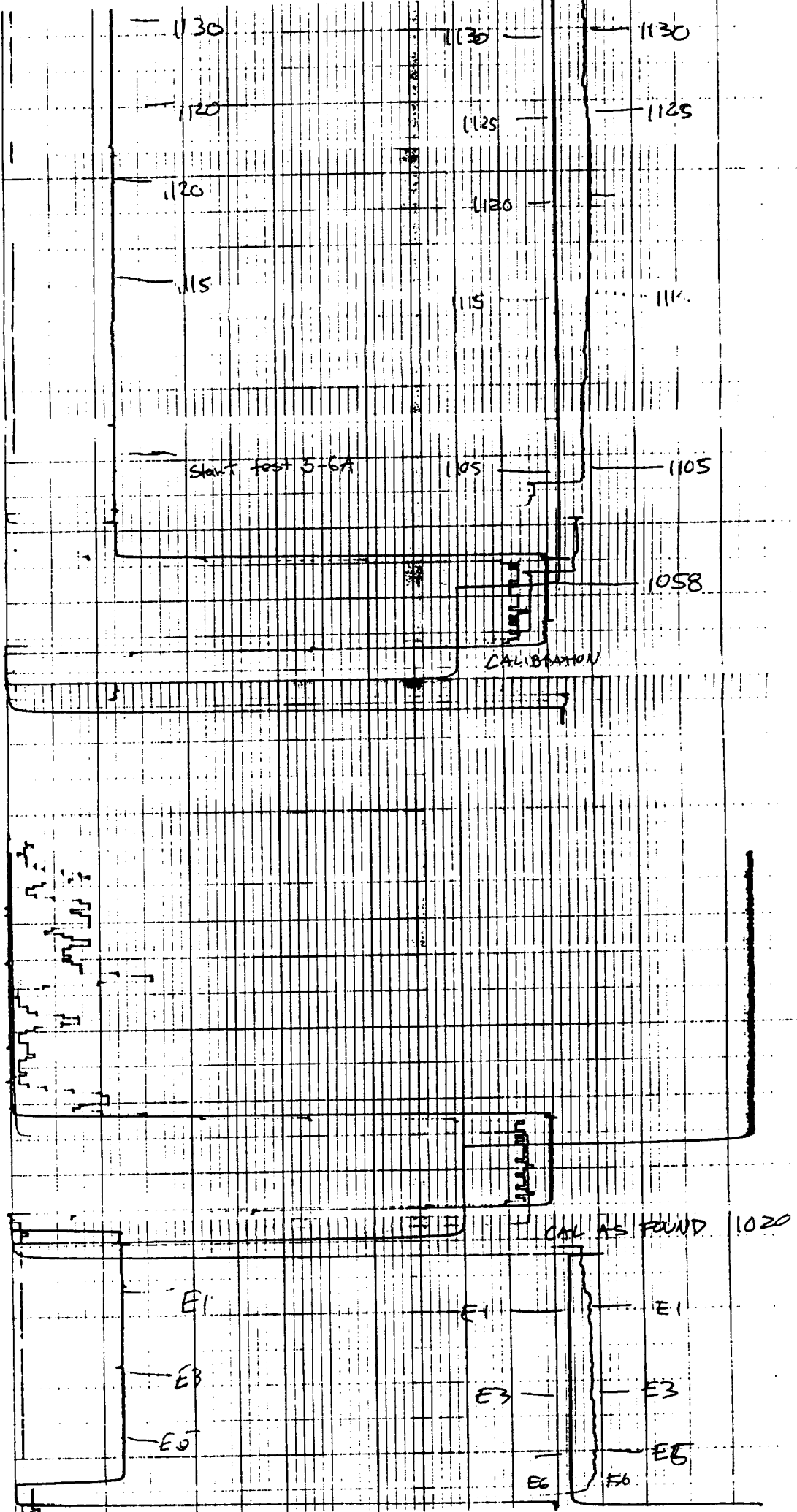
SOURCE CHART NO. ZD-01-25-20M





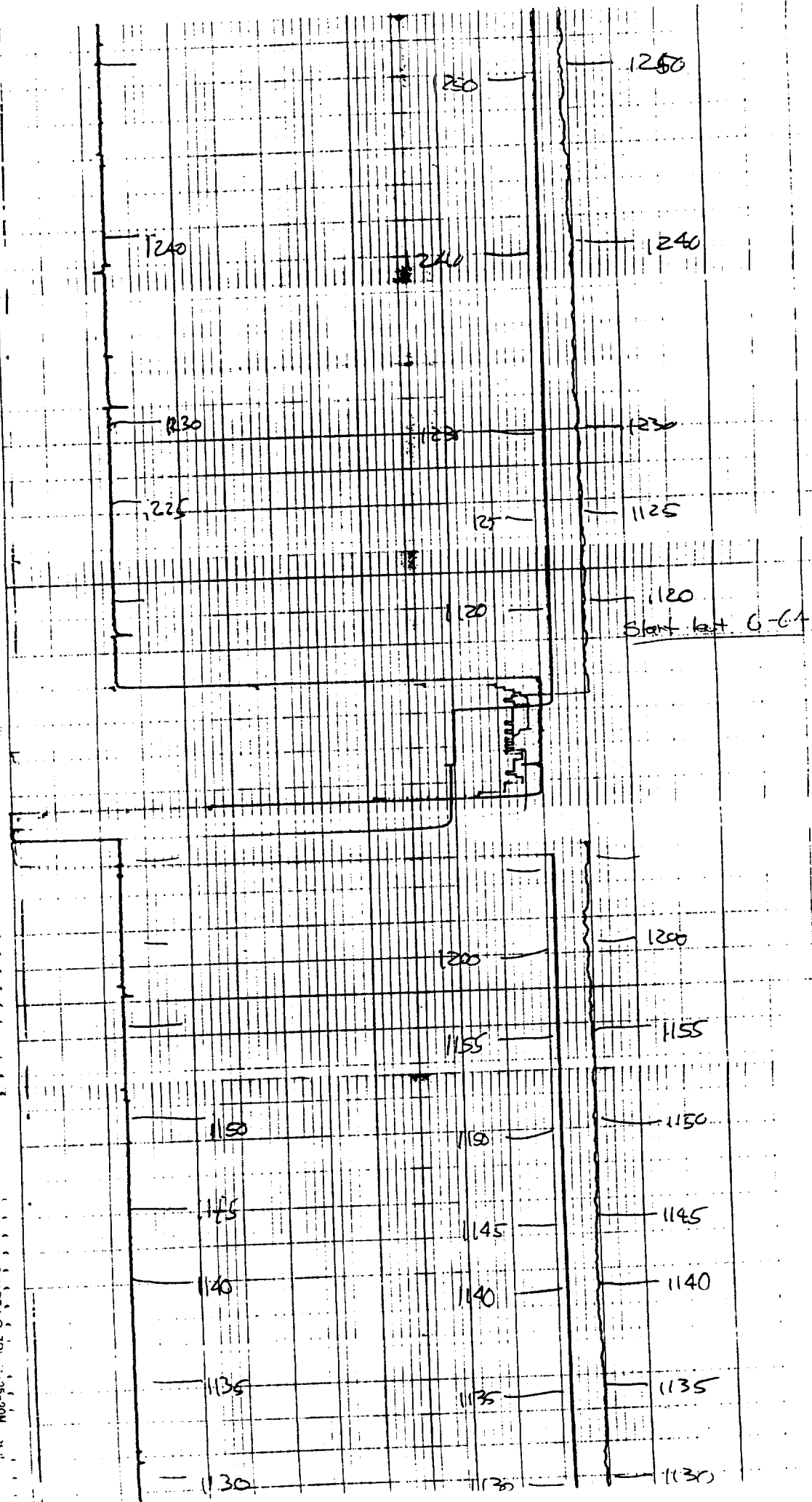
SOLEC CHART NO. 201-01-55-20M

SOLEC



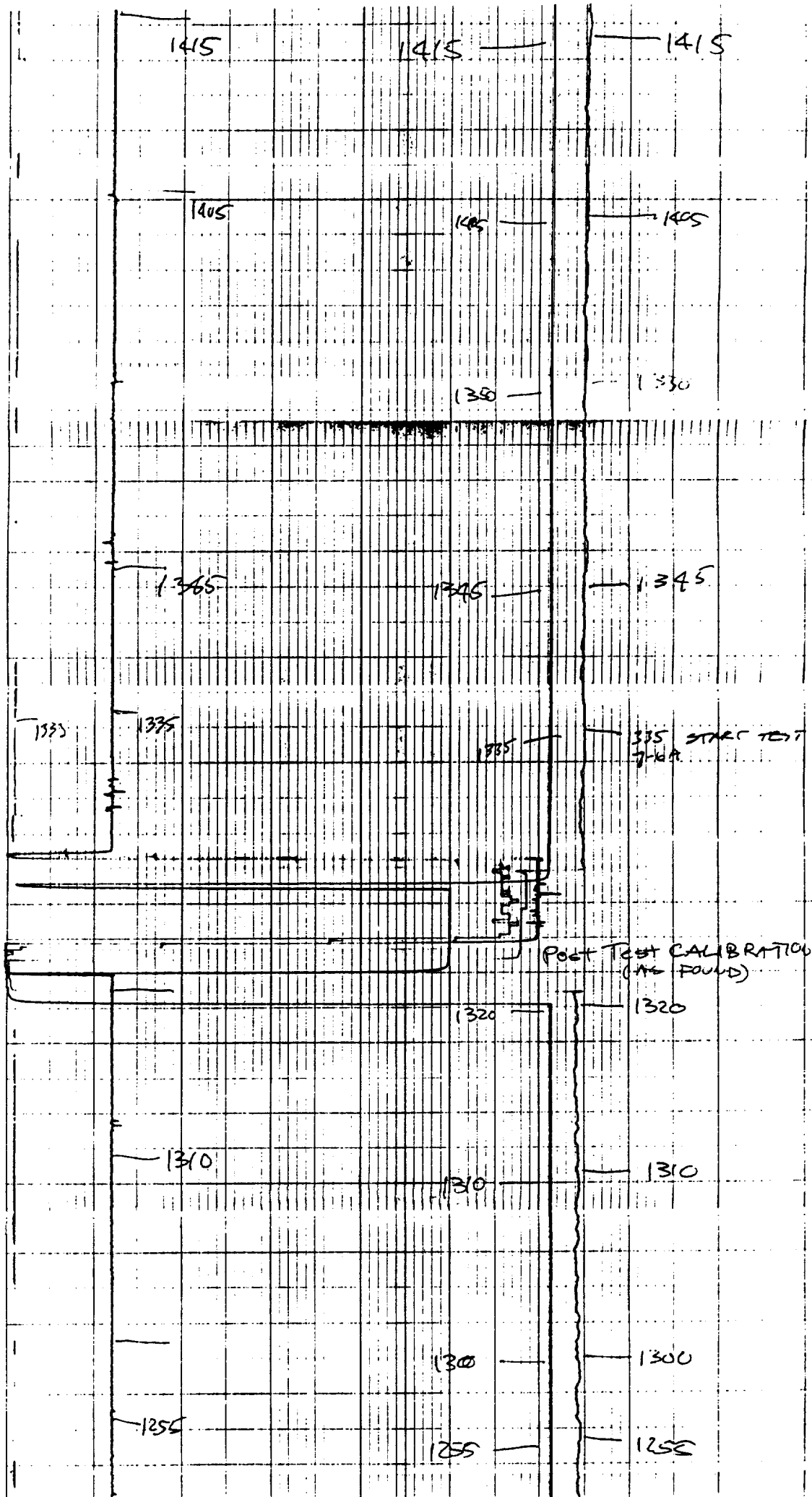
SOLTEC CHART NO. ZD1-01-25-20M

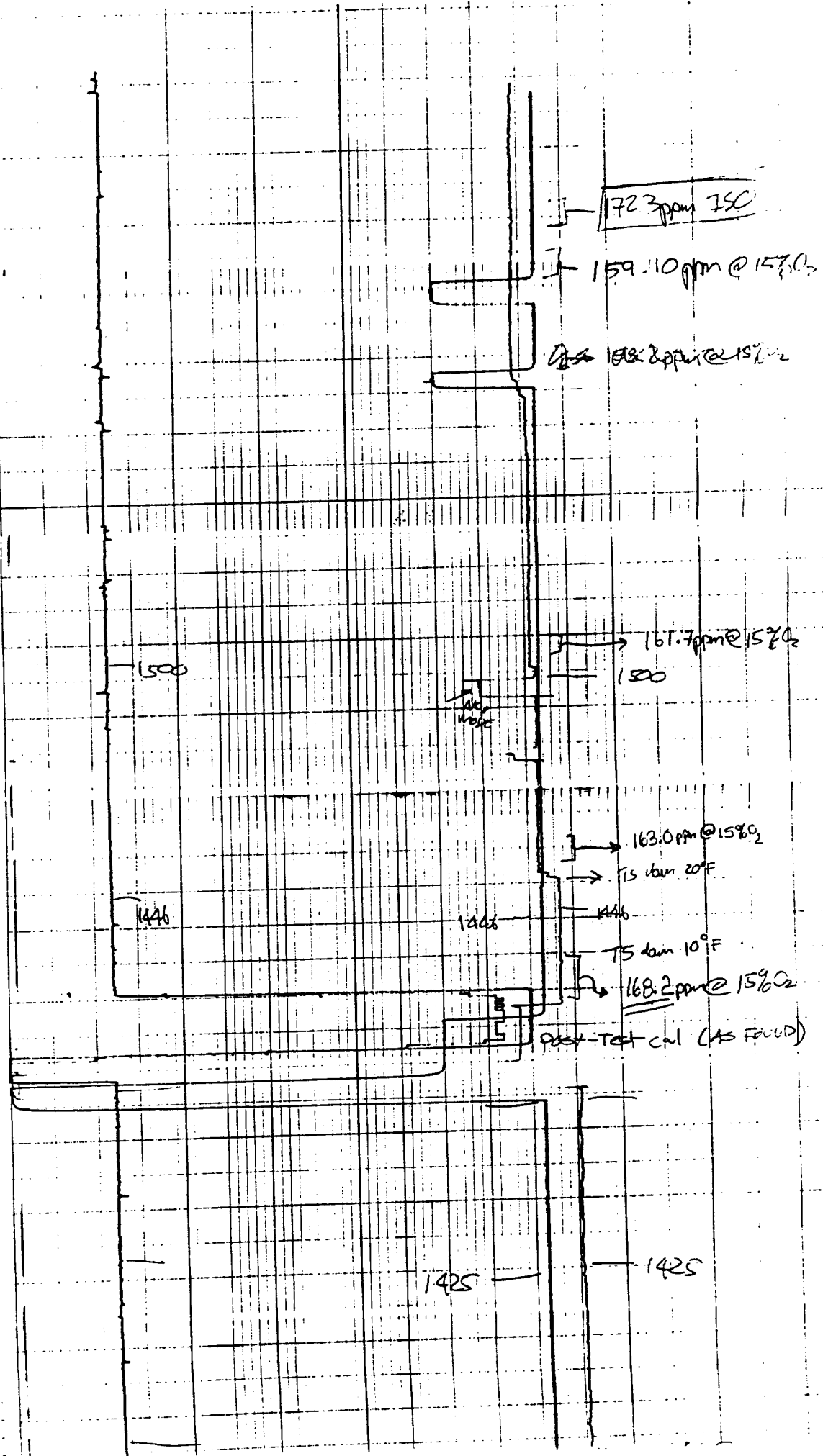
SOLTEC CHART NO. ZD1-01-25-20M



SOITEC CHART NO. ZDI-01-25-20M

SOITEC CHART NO. ZDI-01-25-20M





SOLTEC CHART NO ZD:-3:-:-20M

APPENDIX G
LABORATORY RESULTS

CARNOT
LN 42525

12-17-90

Sample ID

Bag 1-Fuel-6A

<u>COMPONENT</u>	<u>CONCENTRATION</u>	<u>DL</u>
	%v/v	%v/v
Helium (He)	ND	0.1
Oxygen (O ₂)	1.1	0.1
Nitrogen (N ₂)	4.1	0.1
Methane (CH ₄)	92.2	0.1
Carbon dioxide (CO ₂)	0.4	0.1
Ethane (C ₂ H ₆)	1.9	0.1
Propane (C ₃ H ₈)	0.2	0.1
n-Butane (n-C ₄ H ₁₀)	ND	0.1
i-Butane (i-C ₄ H ₁₀)	ND	0.1
n-Pentane (n-C ₅ H ₁₂)	ND	0.1
i-Pentane (i-C ₅ H ₁₂)	ND	0.1
Specific Gravity	0.592	
Heat Value, BTU/SCF		
High	972	
Low	876	
Hydrogen Sulfide (H ₂ S), ppmv	ND	0.1 ppm

ND = not detected
DL = detection limit

CARNOT

SUBJECT Air Correction of Natural Gas Sample JOB NO. _____

SHEET NO. _____ of _____

COMPUTED BY _____ DATE _____ CHECKED BY _____ DATE _____

Component	Concentration		Corrected to 0% O ₂
He	ND		ND
O ₂	1.1	- 1.1 =	0.0
N ₂	4.1	-(1.1)(3.76) =	0.0
CH ₄	92.2	$\times \frac{99.9}{99.9 - (1.1)(1)}$	97.3
CO ₂	0.4	$\times \frac{99.9}{99.9 - (1.1)(1)}$	0.42
C ₂ H ₆	1.4		2.06
C ₂ H ₄	0.2		0.2
C ₂ H ₂	ND		ND
n-C ₄ H ₁₀	ND		ND
i-C ₄ H ₁₀	ND		ND
n-C ₅ H ₁₂	ND		ND
i-C ₅ H ₁₂	ND		ND
	<u>99.9</u>		<u>99.9</u>

O₂ : 1.1 %

N₂ : (1.1)(3.76) = 4.1 %



CERTIFICATION OF SAMPLE RECEIPT

Samples:

Sample No.
(Project No.)
Test No.

82400

P.O.# 6907

Complete Description

1- Fuel - 6A

3 bags for

1- Fuel - 11A

1- Fuel - 16K1

HHV, composition, H₂S, Sulfor

Chain of Custody Prior to Shipment:

Released by	Time and Date	Received by	Time and Date
<i>[Signature]</i>	12/17/90	<i>[Signature]</i>	12/17/90

Samples shipped to:

Trues Dail

Samples shipped from Carnot by:

Carrier:

Date

Air Bill No.

Samples received by:

Company:

Date