

**EMISSION TESTING AT
COALINGA COGENERATION PLANT**

September 19 and 20, 1990

Prepared for

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Prepared by

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Report PS-90-2284/Project 6882-90

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SECTION 1

INTRODUCTION

At the request of Shell Western Exploration & Production, Inc., Pape & Steiner Environmental Services conducted a series of emission tests on the effluent of two gas turbines at the cogeneration plant located north of Coalinga, California. The tests were conducted on September 19 and 20, 1990 to determine compliance with Fresno County Air Pollution Control District rules and regulations.

Duplicate particulate, sulfate and SO₂ tests were conducted on the effluent of each HRSG serving each gas turbine (101A and 101B) using EPA Method 5/8. Duplicate NO_x, CO, CO₂ and O₂ tests were conducted using EPA Method 20. Duplicate hydrocarbon tests were conducted using EPA Method 18. A sample of the PUC natural gas fired in each turbine was collected and analyzed for CHNOS, specific gravity, moisture and Btu using ASTM Methods. Finally, a single test for H₂S in the fuel gas was conducted using EPA Method 11.

Section 2 of the report summarizes the test matrix for this program.

SECTION 2

TEST PROGRAM

Table 2-1 summarizes the tests performed on each unit. Extended sampling times were used to maximize the amount of particulate and SO₂ for subsequent analysis.

No upsets occurred during the test program and the data should be representative of emissions from this plant.

Section 3 summarizes the results of these tests.

TABLE 2-1. COALINGA COGENERATION PLANT TEST MATRIX

<u>Date</u>	<u>Unit #</u>	<u>Test #</u>	<u>Test Parameter</u>	<u>Test Time</u>
09/19/90	101A	1	Particulates/Sulfates/SO ₂ /HC NO _x /CO/CO ₂ /O ₂	10:30 am - 1:08 pm 10:30 am - 12:25 pm
		2	Particulates/Sulfates/SO ₂ /HC NO _x /CO/CO ₂ /O ₂	2:11 pm - 4:55 pm 2:20 pm - 4:15 pm
09/20/90	101B	1	Particulates/Sulfates/SO ₂ /HC NO _x /CO/CO ₂ /O ₂	9:35 am - 12:23 pm 9:35 am - 11:35 am
		2	Particulates/Sulfates/SO ₂ /HC NO _x /CO/CO ₂ /O ₂	1:25 pm - 4:02 pm 1:25 pm - 3:25 pm
09/20/90	101B	1	H ₂ S	11:15 am - 3:15 pm

SECTION 3

TEST RESULTS

Tables 3-1 and 3-2 summarize the results of the tests performed on Units 101A and 101B. All data are reported at 60°F and 29.92 inches Hg. The fuel gas H_2S measured 0.10 ppm.

TABLE 3-1. SUMMARY OF SOURCE EMISSION TEST DATA (60°F)

Unit Tested: SWEPI Coalinga Date: September 19, 1990
 Cogen Plant HRSG Unit 101A

Test Number	1	2	Average
Test Condition	Compl.	Compl.	
Barometric Pressure (in. Hg)	28.59	28.51	28.55
Stack Pressure (in. Hg)	28.57	28.49	28.53
Stack Area (ft ²)	15.67	15.67	15.67
Elapsed Sampling Time (min.)	140.00	140.00	140.00
Volume Gas Sampled (dscf)	111.422	111.939	111.681
F-Factor	8480.67	8480.67	8480.67
GAS DATA			
Average Gas Velocity (fps)	41.17	41.47	41.32
Average Gas Temperature (°F)	242.89	241.39	242.14
Gas Flowrate	24,991	25,113	25,052
Gas Analysis (Volume %)			
Carbon Dioxide, dry	3.37	3.38	3.38
Oxygen, dry	14.97	14.41	14.69
Water	8.59	8.74	8.67
EMISSION CONCENTRATION			
Filterable Particulate (gr/dscf)	0.0019	0.0013	0.0016
Total Particulate (gr/dscf)	0.0030	0.0016	0.0023
Total Sulfate	0.0001	0.0002	0.0001
CO (ppm)	3.70	3.37	3.54
SO ₂ (ppm)	0.22	0.17	0.19
NO _x (ppm)	35.24	33.34	34.29
>C ₁ HC (ppm)	24.91	27.53	26.22
EMISSION RATE - lb/hr			
Filterable Particulate	0.40	0.28	0.34
Total Particulate	0.65	0.34	0.49
Total Sulfate	0.02	0.04	0.03
CO	0.41	0.37	0.39
SO ₂	0.06	0.04	0.05
NO _x	6.41	6.09	6.25
>C ₁ HC	1.58	1.75	1.67
EMISSION FACTOR - lb/MMBtu			
Filterable Particulate	0.0079	0.0050	0.0065
Total Particulate	0.0129	0.0061	0.0095
Total Sulfate	0.0005	0.0007	0.0006
CO	0.0082	0.0068	0.0075
SO ₂	0.0011	0.0008	0.0009
NO _x	0.1278	0.1105	0.1191
>C ₁ HC	0.0315	0.0318	0.0316

TABLE 3-2. SUMMARY OF SOURCE EMISSION TEST DATA (60°F)

Unit Tested: SWEPI Coalinga Date: September 20, 1990
 Cogen Plant HRSG Unit 101B

Test Number	1	2	Average
Test Condition	Compl.	Compl.	
Barometric Pressure (in. Hg)	28.49	28.47	28.48
Stack Pressure (in. Hg)	28.47	28.44	28.46
Stack Area (ft ²)	15.67	15.67	15.67
Elapsed Sampling Time (min.)	140.00	140.00	140.00
Volume Gas Sampled (dscf)	111.285	111.364	111.325
F-Factor	8470.27	8470.27	8470.27
GAS DATA			
Average Gas Velocity (fps)	41.32	41.28	41.30
Average Gas Temperature (°F)	239.93	235.82	237.88
Gas Flowrate	24,997	25,041	25,019
Gas Analysis (Volume %)			
Carbon Dioxide, dry	3.45	3.23	3.34
Oxygen, dry	14.38	14.47	14.43
Water	8.98	9.17	9.08
EMISSION CONCENTRATION			
Filterable Particulate (gr/dscf)	0.0011	0.0008	0.0010
Total Particulate (gr/dscf)	0.0013	0.0011	0.0012
Total Sulfate	0.0001	0.0001	0.0001
CO (ppm)	6.01	7.39	6.70
SO ₂ (ppm)	0.20	0.17	0.18
NO _x (ppm)	24.54	23.37	23.96
>C ₁ HC (ppm)	21.96	17.64	19.80
EMISSION RATE - lb/hr			
Filterable Particulate	0.24	0.17	0.21
Total Particulate	0.27	0.23	0.25
Total Sulfate	0.02	0.02	0.02
CO	0.67	0.82	0.74
SO ₂	0.05	0.04	0.05
NO _x	4.46	4.26	4.36
>C ₁ HC	1.39	1.12	1.26
EMISSION FACTOR - lb/MMBtu			
Filterable Particulate	0.0044	0.0031	0.0038
Total Particulate	0.0049	0.0041	0.0045
Total Sulfate	0.0003	0.0005	0.0004
CO	0.0121	0.0150	0.0135
SO ₂	0.0009	0.0008	0.0009
NO _x	0.0808	0.0780	0.0794
>C ₁ HC	0.0252	0.0205	0.0229

SECTION 4

SAMPLING EQUIPMENT AND PROCEDURES

This section of the report describes the equipment and procedures used to conduct the particulate and gaseous tests on this program.

4.1 PRELIMINARY MEASUREMENTS

Before conducting the stack tests a series of preliminary measurements were made to determine:

- The location of the sampling site and the number and location of the sampling points to be used (EPA Method 1)
- The velocity, temperature, and pressure of the gases in the stack (EPA Method 2)
- The composition of the stack gases (EPA Method 3)
- The moisture content of the stack gases (EPA Method 4)

Using the results of these preliminary measurements and the calibration constants for the sampling train, a series of calculations were made to determine the value of K, a constant, and N_d , ideal nozzle diameter, required to run an isokinetic test according to the equation:

$$\Delta H = \left\{ \frac{60^2 \pi^2 K_p^2 C_p^2 (1 - B_{wo})^2 P_s MW_d}{576^2 K_o^2 MW_s P_m} \right\} (N_d^4) \left(\frac{T_m}{T_s} \right) (\Delta P)$$

where

$$K = \left\{ \frac{60^2 \pi^2 K_p^2 C_p^2 (1 - B_{wo})^2 P_s M W_d}{576^2 K_o^2 M W_s P_m} \right\}$$

An actual nozzle, whose diameter was as close as possible to the ideal nozzle diameter, was selected for the test. Isokinetic sampling rates for each sampling point in the stack were computed using the equation:

$$\Delta H = (K)(N_d^4) \left(\frac{T_m}{T_s} \right) (\Delta P)$$

Since K and N_d are known, and remain constant during a test, the only variables are the meter temperatures, the stack gas temperature and the velocity pressure for each sampling point.

4.2 PREPARATION OF THE PARTICULATE-SO_x SAMPLING TRAIN

All sampling train components were cleaned in the laboratory (soap and water, tap water rinse, distilled water rinse, and IPA rinse) to eliminate previous contamination. The sampling train components were sealed and transported to the sampling site in a mobile lab. The EPA Method 5/8 equipment used to measure particulates (filterable and total) and SO_x consisted of:

- A calibrated 316 stainless steel nozzle for isokinetic sampling
- A heated Pyrex glass sampling probe (6 feet long) equipped with an S-type pitot tube and a thermocouple to measure stack velocity pressure and temperature

- A heated Pyrex glass filter holder containing a weighed 100-mm Whatman 934 AH glass fiber filter
- A Pyrex glass impinger train in an icebath (impinger 1 contained 100 ml 80-percent IPA; a Pyrex glass filter holder containing a 47-mm Whatman 934 AH filter; bubbler 2 and impinger 3 each contained 100 ml of 3-percent H_2O_2 ; bubbler 4 contained a weighed amount of silica gel)
- An umbilical to connect the probe and sample box to the control module
- A control module containing a vacuum pump, a calibrated dry gas meter and a calibrated orifice meter to measure the pressure, temperature and flowrate throughout the train.

The sampling train was charged in the mobile lab using freshly prepared reagents. Each impinger and its contents was weighed to the nearest 0.1 gm on a calibrated electronic balance. Blanks of all filters and reagents were retained for subsequent analysis. The sampling point locations were marked on the probe using a high-temperature marker. The sampling train was completely assembled and lifted to the sampling site.

4.3 SAMPLING PROCEDURES FOR PARTICULATE-SO_x SAMPLING TRAIN

Prior to a test, the sampling train was heated and leak-checked at 15-inches Mercury to insure leakage was less than 0.02 or 4% of the average sampling rate. The S-type pitot tube was also leak-checked. The sampling train was installed on the unirail and the probe was inserted into the stack at the farthest point. An isokinetic sampling rate was calculated using an HP-41CV calculator for each sampling point on the traverse (4 points per traverse; 7 traverses). Each point was sampled

for an equal period of time (5.0 minutes) and all pertinent data was recorded on the data sheet for each point. The probe and sample box were maintained at 250°F throughout the traverse. The gases leaving the impinger train were maintained at <68°F. At the end of a traverse, the probe was withdrawn from the stack and the entire sampling train was transferred intact to the next sampling port. Another traverse of the stack was completed and the sampling train was withdrawn for the final leak check. This leak check was performed at 15-inches Mercury or at the highest vacuum achieved during the test. The S-type pitot tube was also checked at this time. The sampling train was then purged with ambient air for 15-minutes using the highest ΔH measured during the test. After the train was purged, the filter holder and impinger train were sealed with aluminum foil and lowered to the mobile lab for sample recovery.

4.4 SAMPLE RECOVERY PROCEDURES FOR PARTICULATE-SO_x SAMPLING TRAIN

Sample recovery for the nozzle and probe occurred on the stack. The nozzle and probe were brushed and rinsed three times using ACS reagent grade acetone into a polyethylene sample bottle. Sample recovery for the filter holder and impinger train occurred in the mobile lab. The 100-mm filter was removed from the 4-inch filter holder and sealed in its petri dish. The glass fibers stuck to the gasket were scraped off and put into the petri dish. The front half of the 4-inch glass filter holder was brushed and rinsed with acetone. Each impinger was removed from the icebath, wiped dry and weighed to the nearest 0.1 gm. The contents of impinger 1 were transferred to a polyethylene sample bottle. The back half of the 4-inch glass filter holder, the glass connectors, impinger 1, and the front half of the 2-inch filter holder were rinsed

with 80-percent IPA and the rinsings were transferred to this same bottle. The 47-mm filter from the 2-inch filter holder was sealed in its petri dish. The contents of bubbler 2 and impinger 3 were transferred to a polyethylene sample bottle. Distilled water rinsings of the back half of the 2-inch filter holder, bubbler 2, the connector, and impinger 3 were transferred to this same bottle. All sample bottles and petri dishes were marked and labeled. A chain-of-custody log was completed and the field data sheet was also labeled with the sample ID numbers. The sampling train was then recharged in preparation for the next test.

4.5 SAMPLING PROCEDURES FOR CONTINUOUS MONITORING

The continuous monitors used in the Pape & Steiner Mobile Monitoring Lab are shown in Table 4-1. Figure 4-1 is a schematic of the continuous monitoring system. The procedures used to continuously monitor stack gases for NO_x , CO, CO_2 , and O_2 strictly follow EPA Method 20.

Sample was taken from the stack (at 2 points) using a 316 stainless steel probe. A heated Balston filter holder and fiberglass filter (99.9999 percent efficiency retention of 0.6 micron particles) was connected to the outlet of the probe. Sample gas was transported through heated Teflon sample line (maintained at $>250^\circ\text{F}$) by a Teflon-lined diaphragm pump to a 316 stainless steel refrigeration type conditioner (Hankison Model E-4G-SS). The sample gas was passed through the conditioner two separate times under vacuum before entering the pump, then two additional times under pressure. The clean, dry sample gas ($\sim 35^\circ\text{F}$) was then transported to the continuous analyzer system through an unheated Teflon line. A series of flowmeters, valves and regulators maintain constant flow through the system at a constant pressure.

TABLE 4-1 . CONTINUOUS MONITORING LAB - TRAILER 3

NO_x CHEMILUMINESCENT ANALYZER -- THERMO ELECTRON MODEL 10

Response Time (0-90%)	1.5 sec -- NO mode; 1.7 sec -- NO _x mode
Zero Drift	Negligible after 1/2 hour warmup ^x
Linearity	+1% of full scale
Accuracy	Derived from the NO or NO ₂ calibration gas, +1% of full scale
Output	0-10 V
Operating Ranges	0-2, 5, 10, 25, 100, 250, 1000, 2500, and 10,000 ppm

O₂ ANALYZER, FUEL TYPE -- TELEDYNE MODEL 326

Response Time (0-90%)	60 seconds
Accuracy	+1% of scale at constant temperatures; +1% of scale of +5% of reading, whichever is greater, over the operating temperature range
Output	0-1 V
Operating Ranges	0-5%, 10%, 25% O ₂

CO₂/CO INFRARED ANALYZER -- ANARAD MODEL AR-600

Response Time (0-90%)	5 seconds
Zero Drift	+1%
Span Drift	+1%
Linearity	1%
Resolution	Less than 1% of full scale
Output	0-1 V
Operating Ranges	0-20% CO ₂ /0-10,000 ppm CO

CO GAS FILTER CORRELATION - THERMO ELECTRON MODEL 48

Response Time (0-95%)	1 minute
Zero Drift	+0.2 ppm CO
Span Drift	Less than 1% full scale in 24 hours
Linearity	+1% full scale, all ranges
Accuracy	+0.1 ppm CO
Output	0-10 V
Operating Ranges	1, 2, 5, 10, 20, 50, 100, 200, 500, and 1000 ppm

SO₂ UV ANALYZER -- DUPONT MODEL 400

Response Time (0-90%)	Less than 1 second
Zero Drift	Less than 1% full scale in 24 hours
Linearity	+1% full scale
Accuracy	+2% full scale
Output	0-5 V
Operating Ranges	0-100 ppm, 0-1000 ppm

STRIP CHART RECORDERS (2) -- LINSEIS MODEL 7025

Pen Response	0.35 seconds Full Scale
Input Spans	1, 2, 5, 10, 20, 50, 100, 200, 500 mV; 1, 2, 5, 10, 20, 50 V; Variable gain up to 2.5 times
Zero Set	Adjustable to 100% of Full Scale
Accuracy	0.35% of Span
Linearity	0.25% of Span
Chart Speed	1, 2, 5, 10, 20, 50, 100 cm/minute; 1, 2, 5, 10, 20, 50 cm/hour, LED indicator, forward/reverse
Recording Pen	Fiber tip
Chart Width	250 mm

SCOTSMAN TRAILER

Fully Insulated	Air conditioned	8-ft x 14-ft x 11-ft
-----------------	-----------------	----------------------

1. Filter 0.6 μ , 99.9999 percent efficient
2. Duct
3. 316 stainless steel probe
4. 3/8-inch, heated (250°F) Teflon
5. Four-pass conditioner-dryer, 316 stainless steel internals
6. 3/8-inch, unheated Teflon
7. Teflon-lined sample pump
8. 3/8-inch unheated Teflon
9. Rotameter
10. 1/4-inch Teflon tubing
11. Calibration gas manifold
12. Calibration gas selector valve
13. Calibration gas cylinders
14. Backpressure regulator
15. Auxiliary analysis port

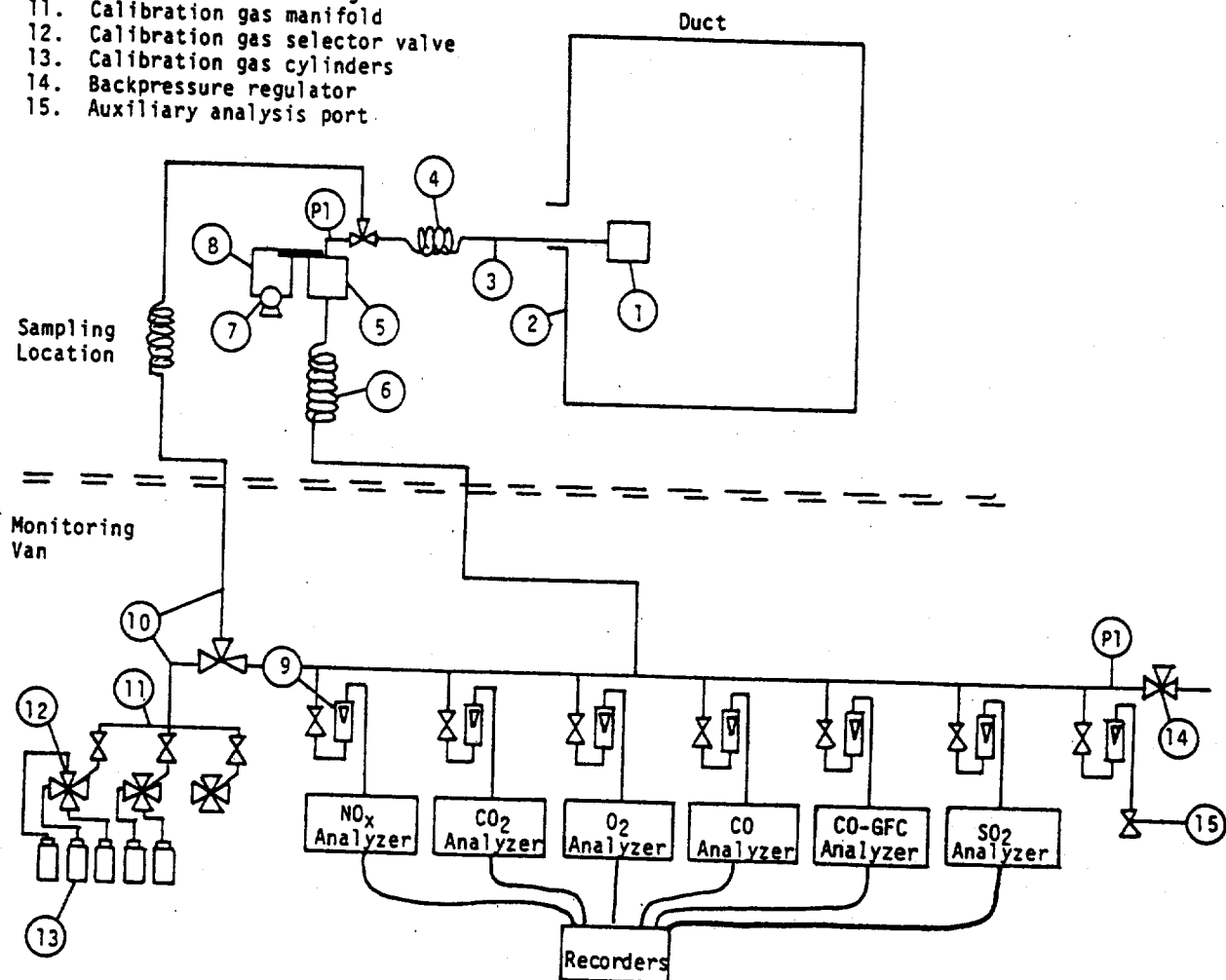


FIGURE 4-1. SCHEMATIC OF CONTINUOUS MONITORING SYSTEM

Calibrations of the continuous analyzers were performed using EPA Protocol 1 calibration gases ($\pm 1\%$) for NO_x and NBS certified calibration gases ($\pm 1\%$) for CO , CO_2 and O_2 . Copies of the gas certifications are included in the Appendix of this report. All pertinent data (date, time, test locations, analyzer range, cal gas value) were recorded on both the field data sheets and continuous analyzer strip charts in the field.

At the start of a test day, a leak-check was performed. The sample probe was removed from the stack and the end was sealed. A leak-check was successful only if pressure at the analyzer system and flow through the rotameters to the individual analyzers all dropped to zero. A mandatory leak-check was performed at the completion of each test day.

An initial calibration was performed at the start of a test period by introducing zero and span gases for each analyzer and making the necessary adjustments. A multipoint linearity check was performed on each analyzer to insure all points were within $\pm 2\%$ of full scale. An NO_2 to NO converter check was performed to insure converter efficiency was greater than 90%. And, finally, the upscale and downscale response time of the sampling system was measured to insure the sampling time per point could be set at 1-minute plus the system response time. Calibration gas values were recorded on the continuous monitor strip charts and field data sheets. A calibration check was completed at the end of a test and adjustments (if necessary) to the analyzers were made in preparation for another test.

An external calibration of the sampling system was performed at the start of a test day. EPA Protocol 1 gas was flowed through the entire sampling system from the probe tip. The response of the analyzers

had to be within $\pm 5\%$ of the certified tank value before testing could proceed. An external calibration was also performed at the end of each test day.

Test data was collected by recording 10-minute averages from the strip chart recordings onto the field data sheets. Data collected over the test period was averaged and reported. A fuel analysis was used to calculate the F-factor, dscf/MMBtu corrected to zero percent O_2 (standard conditions $60^\circ F$, 29.92 inches Mercury), as described in 40 CFR 60.45. The pollutant concentration and the F-factor were used to calculate an emission factor in lb/MMBtu.

4.6 SAMPLING PROCEDURES FOR HYDROCARBONS

The sampling train for hydrocarbons consisted of a probe (short piece of stainless steel), a Tygon sample line, a Tedlar bag and a hand pump. The entire train was purged with stack gas three times before collecting a sample. An integrated grab sample of the stack gases was collected over the test period. After sample collection, the Tedlar bag was lowered to the mobile lab for subsequent analysis. Duplicate grab samples were collected during the test series.

4.7 PREPARATION OF H_2S SAMPLING TRAIN

All sampling train components were cleaned in the laboratory (soap and water, tap water rinse, distilled water rinse, and IPA rinse) to eliminate previous contamination.

EPA Method 11, with cadmium sulfate as the absorbing solution, was used to collect H_2S . Samples were collected from the gas stream using the following sampling train:

- A Teflon sample line (3 feet long) to connect the impinger train to the duct
- An impinger train consisting of five midget impingers with glass connections (impinger 1 contained 15 mls of 3-percent H_2O_2 ; impingers 2, 3, and 4 each contained 15 mls of the 3 M cadmium sulfate absorbing solution; and, impinger 5 contained approximately 20 grams of silica gel)
- A control module containing a pump, control valves, gas meter, orifice meter, dual inclined manometer and temperature indicator with selector switch
- An umbilical cord to connect the control module and the sample train

4.8 SAMPLING PROCEDURES FOR H_2S

Tests were conducted in strict accordance with EPA Method 11. The entire sample train was assembled at the test site. An initial leak-check was performed at 5-inches Mercury vacuum to insure leakage was less than 0.002 cfm. After completing the leak-check, sample was drawn through the midget impinger train at approximately 0.13 cfm for 4 hours. A final leak-check was performed after completing each test. The impinger train was transported to the mobile lab for sample recovery.

4.9 SAMPLE RECOVERY PROCEDURES FOR H_2S

Recovery of the EPA Method 11 sample train was performed in the mobile lab. The contents of the hydrogen peroxide impinger were discarded. The contents of impingers 2, 3, and 4 were quantitatively transferred to a labelled polyethylene sample bottle.

SECTION 5

ANALYSIS PROCEDURES

This section of the report describes the procedures used to analyze the samples collected during the test program. The fuel gas was sent to Pacific Gas Technology for analysis. All other analyses were performed in the Pape & Steiner laboratory in Bakersfield.

5.1 ANALYSIS OF PARTICULATE-SO_x SAMPLES

5.1.1 Nozzle, Probe, Filter Holder Wash

The volume of the acetone washings was measured and the washings were transferred to clean, tared, aluminum weighing dishes. The dishes were placed on temperature-controlled water bath under a fume hood and gently heated to dryness (100°F). The dishes with the dry residue were desiccated and weighed repeatedly at 6-hour intervals until a constant weight was achieved (to the nearest 0.01 mg with a tolerance of <0.1 mg between weighings). The ACS reagent grade acetone blank was treated in the same manner.

5.1.2 Filter

The 100 mm filter was removed from its petri dish and transferred to an oven where it was heated for 2 hours at 105°C. The filter was then desiccated and weighed repeatedly at 6-hour intervals until a constant weight was achieved (to nearest 0.01 mg with a tolerance of <0.1 mg between weighings). An unused, tared blank filter was treated in the same manner.

5.1.3 Filterable Particulate Sulfate

The acetone washings residue and the 100 mm filter were combined and then leached with distilled water to remove sulfate and the leachate was diluted to 100 ml. An aliquot was passed through ion exchange resin and titrated against 0.01N BaCl₂ (which was previously standardized against 0.0100N H₂SO₄) using the barium-thorin titration procedure specified in EPA Method 8. The acetone blank and 100 mm filter blank were treated in an identical manner.

5.1.4 Condensable Particulate, Sulfate, and SO₂

The 47-mm glass fiber filter was leached with distilled water and the leachate was added to the contents and washings from impinger 1. The volume was measured and the entire volume was transferred to a clean, tared glass evaporating dish. The dish was placed on a temperature-controlled hot plate under a fume hood and gently heated to dryness (150°F). The dish with the dry residue was desiccated and weighed repeatedly at 6-hour intervals until a constant weight was achieved (to nearest 0.01 mg with a tolerance of <0.1 mg between weighings). The dry residue was dissolved in distilled water and diluted to 100 ml using distilled water and analyzed for sulfate using the barium-thorin titration procedure. A blank 47-mm filter and 80-percent IPA solution were treated in the same manner.

5.1.5 SO₂

The volume of contents and washings from bubbler 2 and impinger 3 was measured and an aliquot was analyzed for sulfate using the barium-thorin procedure. A 3-percent H₂O₂ blank was treated in the same manner.

5.2 ANALYSIS OF HYDROCARBON SAMPLES

The grab sample of hydrocarbons was analyzed using a Carle Model 211 AGC-FID. After purging the sample loop three times, a 1-ml sample was extracted from the Tedlar sample bag and injected onto a 6-foot long, 1/8-inch stainless steel column containing 80/100 mesh PoraPac Q, maintained at 150°C. The C₁ hydrocarbon was separated and the greater than C₁ hydrocarbons were backflushed to the detector for quantitation as a single peak. An HP Model 3390A reporting integrator was used to record and integrate the signal from the GC. A ±1 percent certified calibration gas (C₁-C₆ HC in N₂) was used to calibrate the GC before and after sample analysis to quantitate the C₁ and greater than C₁ hydrocarbons. The beginning and end calibrations must agree within ±5% for the data to be acceptable.

5.3 ANALYSIS PROCEDURES FOR H₂S

In the laboratory, the contents of the sample bottle were transferred to an iodine flask along with the water rinsings. A known amount of iodine was added to the sample and acidified with 3 M HCl. The iodine flask was immediately stoppered and shaken. The flask was placed in the dark for 30-minutes. Standard 0.01 N sodium thiosulfate was used to standardize the iodine solution used each day of testing. Samples were titrated with the same sodium thiosulfate solution to an iodine/starch blue endpoint. The blank and standard solutions were handled in exactly the same manner.

5.4 FUEL ANALYSIS

A sample of the fuel gas fired during this test program was collected and sent to Pacific Gas Technology (PGT) for analysis. Analysis

was performed by PGT in accordance with EPA Title 40 Section 60.45. The specific procedures are itemized in Table 5-1. The results appear at the end of this section.

TABLE 5-1. FUEL ANALYSIS METHODS
LABORATORY TEST PROCEDURES FOR FUEL OILS AND FUEL GASES

Reference: EPA Title 40, Section 60.45

FUEL OIL TESTS:

Sediment and Water, Vol. %	ASTM D4007-81
Gravity by Hydrometer (API)	ASTM D1298-80
API Gravity Corrected to 60°F	ASTM Table 5A
Gross Calorific Value (Btu/lb)	ASTM D2015-77
Ultimate Analysis (C, H, O, N, S, wt. %)	
Carbon, Hydrogen	ASTM D3178-73
Nitrogen (chemiluminescence detector)	ASTM D3431-80
Sulfur	ASTM D2622-82
Ash	ASTM D482
Oxygen	ASTM D3176-74

GASEOUS FUELS BY GAS-LIQUID CHROMATOGRAPHY:

Gas Analysis	ASTM D1945-81
Sulfur Analysis	CPA B16
Calculation of Gross Calorific Value	ASTM D3588-81
Component Weight %, F-factor calculations	EPA 40:60.45

PROCEDURES FOR SCRUBBER LIQUOR ANALYSIS:

Specific Gravity	ASTM D1429
Chlorides	ASTM D512-67

PACIFIC GAS TECHNOLOGY



RECEIVED

SEP 24 1990

Ans'd.....

4200 Easton Drive - Suite 5
Bakersfield, California 93309
805/324-1317
Fax: 805/324-2746

GAS ANALYSIS BY CHROMATOGRAPH

PAPE & STEINER ENVIRONMENTAL SERVICES
5801 Norris Road
Bakersfield, CA 93308

Attention: Jim Steiner

SAMPLED: SEPTEMBER 19, 1990

SUBMITTED: SEPTEMBER 21, 1990

REPORTED: SEPTEMBER 21, 1990

LAB # 3030-1

Sample ID : SWEPI/COALINGA
HRSG 101A
FUEL GAS

P&S ID # : 24761

ANALYZED GAS

MOLE %

WT %

CHONS WT %

OXYGEN	0.08	0.15	CARBON	72.14
NITROGEN	1.26	2.05	HYDROGEN	23.34
CARBON DIOXIDE	1.25	3.19	OXYGEN	2.47
HYDROGEN	ND	0.00	NITROGEN	2.05
CARBON MONOXIDE	ND	0.00	SULFUR	0.00
HYDROGEN SULFIDE	ND	0.00		
METHANE	93.59	87.04		
ETHANE	3.02	5.27		
PROPANE	0.59	1.51		
iso-BUTANE	0.06	0.20		
n-BUTANE	0.08	0.27		
iso-PENTANE	0.02	0.08		
n-PENTANE	0.02	0.08		
HEXANE +	0.03	0.10		

SPECIFIC GRAVITY * : 0.596

SPECIFIC VOLUME : 22.08 cu ft/lb

HYDROGEN SULFIDE : ppm
(Draeger)

TOTAL * DRY : 1023
BTU/cu ft

NET * DRY : 923
BTU/cu ft

WET : 1005

WET : 907

BTU/lb : 22585

BTU/lb : 20371

PACIFIC GAS TECHNOLOGY



RECEIVED

SEP 24 1990

Ans'd.....

4200 Easton Drive - Suite 5
Bakersfield, California 93309
805/324-1317
Fax: 805/324-2746

GAS ANALYSIS BY CHROMATOGRAPH

PAPE & STEINER ENVIRONMENTAL SERVICES
5801 Norris Road
Bakersfield, CA 93308

Attention: Jim Steiner

Sample ID : SWEPI/COALINGA
HRSG 101B
FUEL GAS

SAMPLED: SEPTEMBER 20, 1990

SUBMITTED: SEPTEMBER 21, 1990

REPORTED: SEPTEMBER 21, 1990

LAB # 3030-2

P&S ID # : 24762

ANALYZED GAS

	MOLE %	WT %	CHONS WT %
OXYGEN	0.02	0.04	CARBON 72.46
NITROGEN	0.94	1.53	HYDROGEN 23.47
CARBON DIOXIDE	1.34	3.43	OXYGEN 2.53
HYDROGEN	ND	0.00	NITROGEN 1.53
CARBON MONOXIDE	ND	0.00	SULFUR 0.00
HYDROGEN SULFIDE	ND	0.00	
METHANE	94.12	87.92	
ETHANE	2.87	5.03	
PROPANE	0.53	1.36	
iso-BUTANE	0.05	0.17	
n-BUTANE	0.07	0.24	
iso-PENTANE	0.02	0.08	
n-PENTANE	0.02	0.08	
HEXANE +	0.02	0.05	

SPECIFIC GRAVITY * : 0.593

HYDROGEN SULFIDE : ppm
(Draeger)

TOTAL * DRY : 1024
BTU/cu ft

WET : 1006

BTU/lb : 22713

SPECIFIC
VOLUME : 22.18 cu ft/lb

NET * DRY : 923
BTU/cu ft

WET : 907

BTU/lb : 20467

SECTION 6

QUALITY ASSURANCE

This section of the report describes the QA/QC procedures employed on the test program.

6.1 PARTICULATE/SO_x SAMPLING EQUIPMENT

A detailed record of repair and maintenance to each sampling train is kept. Preventative maintenance to each system is performed periodically to avoid complete component breakdown during a field test.

A detailed record of sampling system calibrations is also kept. Calibration data for the sampling nozzles, pitot tubes, dry gas meters and orifice meters are available for review. Results of the EPA Quality Assurance Branch biannual audits of the dry gas meter and orifice meter combinations are also logged and verify our in-house calibration data. The calibration data for the equipment used on this program can be found in the Appendix of this report.

6.2 LAB ANALYSIS

All field samples are assigned a label and an ID number. This ID is also affixed to a chain-of-custody log and to the field data sheet to eliminate any chance of sample mixup.

Prior to analysis, all glassware is thoroughly cleaned (soap and water, tap water rinse, distilled water rinse, IPA rinse) to eliminate any contamination. The evaporating dishes used to evaporate the washings

are treated the same as a sample (dried in an oven, desiccated and weighed repeatedly at 6-hour intervals until a constant weight is achieved). The glassware used to measure volumes and make transfers and dilutions are all NBS Class A to insure accurate measurements. All weighings are carried out on a Sartorius Research Model R160P electronic semi-micro balance supported by a marble table in a separate room from the main analytical laboratory. The balance is calibrated regularly against an NBS Class S-1 weight.

All reagents used in the field and in the laboratory are ACS reagent grade and blanks of these reagents are evaluated for every set of tests. Blanks are taken in the field from the squeeze bottles and not the original container. Records are kept on these blanks to insure consistent quality of the reagents. Prior to use, the IPA is also analyzed to insure no peroxides are present which could lead to high SO_3 and low SO_2 values.

A quality control program consisting of duplicate analyses (to measure precision), spikes (to measure recovery efficiency) or analysis of blind standards supplied by EPA's Quality Assurance Branch (to measure accuracy) is implemented for each test program. Table 6-1 summarizes the results of the QC checks on this program. Records of our lab's participation in the EPA bi-annual audits for SO_2 are kept on file and verify our in-house QA/QC effort.

6.3 QUALITY ASSURANCE OF HYDROCARBON ANALYSES

Each sample container is purged in the field with sample prior to the actual tests. A certified gas is used to calibrate the gas chromatograph used to measure the hydrocarbons. The calibration certificate for

the gas used appears at the end of this section. Duplicate analyses of some samples were conducted. The results of these quality assurance checks are included in Table 6-1.

6.4 CONTINUOUS MONITORS QUALITY ASSURANCE

The NO_x analyzer is calibrated before and after each test using an EPA Protocol 1 gas ($\pm 1\%$) traceable to NBS. The CO, CO₂ and O₂ analyzer are calibrated before and after each test using a NBS certified gas mixture ($\pm 1\%$). Copies of the calibration gas certificates appear in the Appendix of this report.

A sampling system check was performed at the beginning and end of each test day. This was done by introducing an EPA Protocol 1 gas at the sampling probe and measuring the system response. The purpose of this was to check the system for leaks and sample loss.

Multipoint calibration linearity checks of the continuous analyzers were performed on April 10, 13 and 25, 1990. These results were well within CARB limitations of $\pm 2\%$ of full scale. Tables 6-2 through 6-6 list the results of these checks.

All of the EPA Method 20 QA/QC checks (e.g., linearity, interference, response time, converter efficiency, etc.) were performed on the continuous monitoring system and the system passed these requirements.

TABLE 6-1. QA/QC RESULTS

<u>Unit #</u>	<u>Test #</u>	<u>Test Parameter</u>	<u>Dupl. (%)</u>	<u>Rec (%)</u>
101A	1	Filterable Sulfate	100.0	
	2	Filterable Sulfate		99.2
		EPA SO ₂ 0586 6XXX		100.1
101A	1	Condensible Sulfate	100.0	
	2	Condensible Sulfate		99.8
		EPA SO ₂ 0586 6XXX		100.1
101A	1	SO ₂	100.0	
	2	SO ₂		98.2
		EPA SO ₂ 0586 6XXX		100.1
101A	1	Hydrocarbon	108.8	
101B	1	Filterable Sulfate	100.0	
	2	Filterable Sulfate		100.0
101B	1	Condensible Sulfate	100.0	
	2	Condensible Sulfate		99.8
101B	1	SO ₂	100.0	
	2	SO ₂		100.7
101B	1	Hydrocarbon	96.6	

TABLE 6-2.

NO_x CALIBRATION SUMMARY

1. Station T-3

2. Analyzer NOX TECO
Model 10AR S/N _____

3. Calibration by JP Date 4-10-90

4. Calibrator Manufacturer ENVIRONICS
Model 201-1520 S/N 1122

5. NO_x Standard ALM 5595/ALM 7882/ALM 2355 Concentration 202ppm/2973ppm/8805
Cylinder Pressure 1150/1250/1200

NO_x CALIBRATION AND LINEARITY CHECKS

Calibration Points	Flow, Dil. 1 cc/min	Flow, Std 2 cc/min	0-25 ppm 3 (NO _x) ppm out	4 Chart ppm	% Difference + 2% Full Scale
Zero	8995	0	0	0	0
80% URL	8103.3	888.9	19.98	19.98	0
1	8325.6	667.2	14.99	15.0	+0.4
2	8550.5	445.0	9.99	10.0	+0.4
3	8772.8	222.8	5.00	5.0	0

Cross check Bottle ALM 7729 12.34ppm = (12.65ppm 1.24%)

Calibration Points	Flow, Dil. 1 cc/min	Flow, Std 2 cc/min	0-250 RANGE 3 (NO _x) ppm out	4 Chart ppm	% Difference + 2% Full Scale
Zero	9000	0	0	0	0
80% URL	8393.1	604.6	199.7	199.7	0
1	8545.5	453.7	149.9	150.5	+0.24%
2	8692.8	302.7	100.1	100.75	+0.26%
3	8842.7	151.8	50.1	51.0	+0.36%

Cross check Bottle LOWL 81.35ppm ALM 2361
Reading 84ppm = +1.00%

TABLE 6-2. (Concluded)
 NO_x CALIBRATION AND LINEARITY CHECKS

Calibration Points	Flow, Dil. 1 cc/min	Flow, Std 2 cc/min	0-2500 RANGE 3 (NO_x) ppm _{out}	4 Chart ppm	% Difference + 2% Full Scale
Zero	3916.6	—	0	0	0
80% URL	2087.4	908.1	2000	2000	0
1	3317.2	681.1	1501	1505	+16
2	3542	454.4	1002	1005	+12
3	3769.3	227.7	501.8	512	+4

TABLE 6-3.
CO CALIBRATION SUMMARY

1. Station T-3

2. Analyzer CO TECO
Model 48 S/N 13738-141

3. Calibration by JP Date 4/25/80

4. Calibrator Manufacturer ENVIRONICS
Model 201-1520 S/N 1122

5. CO Standard ALM6164/AWL 114/AWL 960 Concentration 200ppm/1003ppm/9992ppm
Cylinder Pressure 1900/1500/1600

CO CALIBRATION AND LINEARITY CHECKS

Calibration Points	Flow, Dil.	Flow, Std	0-20 RANGE		% Difference + 2% Full Scale
	1 cc/min	2 cc/min	3 (CO) _{out} ppm	4 Chart ppm	
Zero	9001	—	0	0	0
80% URL	8283.2	721.8	16.03	16.0	0
1	8463.0	541.5	12.03	12.08	+1.25%
2	8640.4	361.4	8.03	7.96	-.35%
3	8820.2	180.9	4.01	3.81	-1%

Calibration Points	Flow, Dil.	Flow, Std	0-100 RANGE		% Difference + 2% Full Scale
	1 cc/min	2 cc/min	3 (CO) _{out} ppm	4 Chart ppm	
Zero	9000	—	0	0	0
80% URL	8283.2	719.1	80.1	80.1	0
1	8460.5	539.4	60.1	60.0	-.1%
2	8640.4	360	40.1	39.8	-.3%
3	8820.2	180.6	20.1	19.8	-.3%

TABLE 6-3. (Concluded)
CO CALIBRATION AND LINEARITY CHECKS

Calibration Points	Flow, Dil. 1 cc/min	Flow, Std 2 cc/min	0-1000 RANGE		% Difference + 2% Full Scale
			3 (CO) out ppm	4 Chart ppm	
Zero	9000.09	—	0	0	0
80% URL	8275.7	725.5	801.0	801	0
1	8458.0	544.1	601	597	-1.4%
2	8637.9	363.2	401	399	-1.2%
3	8815.2	182.1	201	198	-1.3%

TABLE 6-4.
CO CALIBRATION SUMMARY

1. Station T-3

2. Analyzer ANALAN CU
Model AK602 S/N 2340

3. Calibration by JP Date 4-13-90

4. Calibrator Manufacturer ENVIRONICS
Model 201-1520 S/N 1122

5. CO Standard AKL-5660 Concentration 9942 PPM
Cylinder Pressure 1600

CO CALIBRATION AND LINEARITY CHECKS

Calibration Points	Flow, Dil.	Flow, Std	0 - 10,000 RANGE		% Difference + 2% Full Scale
	1 cc/min	2 cc/min	3 (CO) ppm _{out}	4 Chart ppm	
Zero	<u>1004</u>	<u>0</u>	<u>0</u>	<u>0</u>	<u>0</u>
80% URL	<u>202.2</u>	<u>810.7</u>	<u>7938</u>	<u>7938</u>	<u>0</u>
1	<u>402.0</u>	<u>609.3</u>	<u>5990</u>	<u>6100</u>	<u>-1.1%</u>
2	<u>596.9</u>	<u>407.8</u>	<u>4036</u>	<u>4100</u>	<u>+1.6%</u>
3	<u>801.7</u>	<u>203.6</u>	<u>2016</u>	<u>2090</u>	<u>-7.4%</u>

Calibration Points	Flow, Dil.	Flow, Std	3 (CO) ppm _{out}	4 Chart ppm	% Difference + 2% Full Scale
	1 cc/min	2 cc/min			
Zero					
80% URL					
1					
2					
3					

TABLE 6-5.
CO₂ CALIBRATION SUMMARY

1. Station T-3

2. Analyzer ANALAB
Model AK602 S/N 2340

3. Calibration by JP Date 4/13/90

4. Calibrator Manufacturer ENVIRONICS
Model 201-1520 S/N 1122

5. CO₂ Standard AAL-799 Concentration 200%
Cylinder Pressure 950

CO₂ CALIBRATION AND LINEARITY CHECKS

Calibration Points	Flow, Dil.	Flow, Std	0-20% RANGE		% Difference + 2% Full Scale
	1 cc/min	2 cc/min	3 (CO ₂) _{out}	4 Chart %	
Zero	<u>1009.0</u>	<u>0</u>	<u>0</u>	<u>0</u>	<u>0</u>
80% URL	<u>209.7</u>	<u>813.4</u>	<u>15.9%</u>	<u>15.9%</u>	<u>0</u>
1	<u>404.5</u>	<u>612.3</u>	<u>12.0</u>	<u>11.7</u>	<u>-1.5%</u>
2	<u>609.4</u>	<u>406.9</u>	<u>8.0</u>	<u>7.7</u>	<u>-1.5%</u>
3	<u>809.2</u>	<u>201.5</u>	<u>3.98</u>	<u>3.8</u>	<u>-.9%</u>

Forms 1.19 03/20/89

TABLE 6-6.
O₂ CALIBRATION SUMMARY

1. Station T-3

2. Analyzer TELEDYNE 07
Model 326A S/N 44535

3. Calibration by SP Date 4/13/90

4. Calibrator Manufacturer ENVIRONICS
Model 701-1520 S/N 1122

5. O₂ Standard A-14722 Concentration 45%
Cylinder Pressure 1850

O₂ CALIBRATION AND LINEARITY CHECKS

Calibration Points	Flow, Dil.	Flow, Std	0-25% RANGE		% Difference + 2% Full Scale
	1 cc/min	2 cc/min	3 (O ₂) _{out}	4 Chart %	
Zero	<u>1996</u>	<u>0</u>	<u>0</u>	<u>0</u>	<u>0</u>
80% URL	<u>1109</u>	<u>889.4</u>	<u>20</u>	<u>20</u>	<u>0</u>
1	<u>1331.3</u>	<u>667.3</u>	<u>15</u>	<u>75</u>	<u>0</u>
2	<u>1551.1</u>	<u>445.5</u>	<u>10.04</u>	<u>10.2</u>	<u>+1.64%</u>
3	<u>1777.4</u>	<u>223.1</u>	<u>5.03</u>	<u>5.23</u>	<u>+1.8%</u>

Calibration Points	Flow, Dil.	Flow, Std	0-10% RANGE		% Difference + 2% Full Scale
	1 cc/min	2 cc/min	3 (O ₂) _{out}	4 Chart %	
Zero	<u>5005.8</u>	<u>0</u>	<u>0</u>	<u>0</u>	<u>0</u>
80% URL	<u>4116.5</u>	<u>890</u>	<u>8.0</u>	<u>8.0</u>	<u>0</u>
1	<u>4341.4</u>	<u>667.6</u>	<u>6.0</u>	<u>6.1</u>	<u>+1%</u>
2	<u>4561.1</u>	<u>445.5</u>	<u>4.0</u>	<u>4.15</u>	<u>+1.5%</u>
3	<u>4786.1</u>	<u>223.1</u>	<u>2.0</u>	<u>2.12</u>	<u>+1.6%</u>

TABLE 6-5. (Concluded)
O₂ CALIBRATION AND LINEARITY CHECKS

Calibration Points	Flow, Dil.	Flow, Std	0-50%	Chart %	% Difference + 2% Full Scale
	1 cc/min	2 cc/min	3 (O ₂) out		
Zero		0	0	0	0
80% URL	6382.2	623.3	4.0	4.0	0
1	6539.6	467.7	3.0	3.03	+ .6%
2	6694.5	312	2.0	2.075	+ 1.6%
3	6849.3	156.5	1.0	1.05	+ 1.0%

Forms 1.17 03/20/89

APPENDIX A
PAPE & STEINER RAW DATA

SAMPLING POINT LOCATION DATA SHEET

Plant SWEPI

Date 9/19/90

Test Location HRSG 101 A, HRSG 101 B

Upstream Dist./Dia. 48" / 1.0 φ

Downstream Dist./Dia. 96" / 2.0 φ

No. of Sampling Points 28

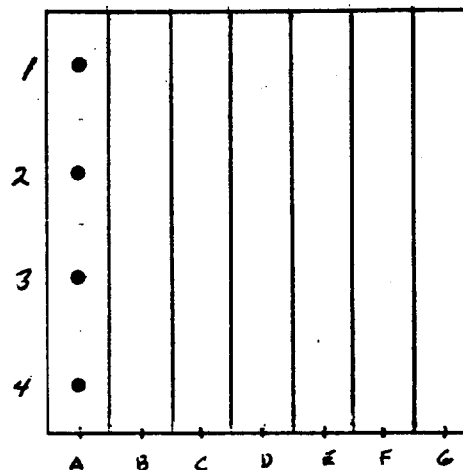
Stack Dimension 47.5 x 47.5

Coupling Length 7

7, 4 -inch MPT/FPT/Flange

need C-Clamps
100' power
50' rope
(pulley stand/wheel)

XEQ PNT



Sample Point	Dist	Sample Point	Dist	Sample Point	Dist	Sample Point	Dist
1	12.9						
2	24.8						
3	36.7						
4	48.6						

SAMPLING POINT RELOCATION:

VELOCITY TRAVERSE DATA SHEET

Plant SWEPI
 Date 9/19/90
 Test Location HRSG 101A
 Static Pressure (in. wg) -0.30
 Barometric Pressure 28.59
 Probe Type/Length 6/6'
 Pitot Coefficient 0.84
 Stack Dimension 47.5 x 47.5

Time: 9:59 Time: Time: Time:

Smpl Pt.	ΔP	Ts	Smpl Pt.	ΔP	Ts	Smpl Pt.	ΔP	Ts	Smpl Pt.	ΔP	Ts
6	0.39	280									
2	0.41	272									
3	0.38	262									
4	0.34	255									
10:02 E 1	0.40	235									
2	0.39	232									
3	0.39	227									
4	0.37	237									
10:06 C 1	0.39	237									
2	0.39	231									
3	0.39	224									
4	0.22	239									

SAMPLING POINT RELOCATION:

Avg. $\sqrt{\Delta P}$ = 0.6081
 Avg. ΔP = 0.37
 Avg. Ts = 244

PLANT SWEPI TEST TYPE MS/B FIELD TEST DATA SHEET (Page 1 of 3)

[IMPINGER VOLUMES/WEIGHTS] [GAS COMPOSITION]

Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO
80% IPA	667.1	553.4	113.7				
3% H ₂ O ₂	577.0	540.4	36.6				
3% H ₂ O ₂	549.0	538.6	10.4				
S.G.	832.6	767.3	65.3	Leakrate	cfm		inHg
		TOTAL	226.0	Initial	0.012		15 mg/L
				Final			

Date 9/19/90 Barometric Pressure 28.59
 Test Location 101A Static in.wg. -0.30
 Run Number 1 Probe Type/Length 6/6'
 Stack Diameter 41.5x47.5 Pitot Coefficient 0.84
 Operator JS Meter Box No./Y 644/1.0132
 Filter No. 77 Nozzle No./Size #270/1.3020

[TEMPERATURE ° F]

Sample Point	Time	ΔP in wg	ΔH in wg	Gas Meter Volume Ft ³	Stack	Probe	Oven	Imp.	Gas Meter IN OUT	Pump Vacuum in. Hg	ΔP	Comments
A	1 0	0.38	2.10	257.873	272	275	243	62	79 77	3.5	0.616	pitotok
	2 5	0.39	2.16	261.995	276	225	241	60	84 80	3.5	0.624	
	3 10	0.38	2.26	266.200	231	232	252	59	87 83	3.5	0.616	FAW 24751
	4 15	0.31	1.84	270.550	234	244	243	58	90 84	3.0	0.557	FLT 24752
	20			274.487								
B	1 0	0.40	2.36	274.487	241	246	249	62	90 87	4.0	0.632	10A 24753
	2 5	0.40	2.37	278.866	241	245	227	60	95 89	4.0	0.632	
	3 10	0.41	2.52	283.275	220	236	238	61	97 92	4.0	0.640	24754
	4 15	0.24	1.47	287.920	223	231	236	63	97 93	3.0	0.490	
	20			291.582	254				98 94			
E	1 11:00	0.41	2.45	291.582	240	246	236	65	95 94	4.0	0.640	24755
	2 5	0.40	2.40	296.115	239	242	258	64	99 95	4.0	0.632	
	3 10	0.40	2.45	300.645	228	244	254	66	101 98	4.0	0.632	
	4 15	0.37	2.28	305.240	223	251	246	66	102 97	4.0	0.608	HC1 24763
	20			309.744								

SWEEP

TEST TYPE

45/8

FIELD TEST

SHEET (Page

2 of

3

Date 9/19/90 Barometric Pressure 28.59
 Test Location 101A Static in.wg. -0.30
 Run Number 1 Probe Type/Length 6/6'
 Stack Diameter 42.5x41.5 Pitot Coefficient 0.84
 Operator JG Meter Box No./Y 644/1.013Z
 Filter No. 77 Nozzle No./Size 270/1.3020

IMPINGER VOLUMES/WEIGHTS			GAS COMPOSITION				
Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO
				Leakrate	cfm		"Hg
S.G.				Initial			
		TOTAL		Final			

[illegible]

Date	9/19/90	Barometric Pressure	28.51
Test Location	101A	Static in.wg.	-0.30
Run Number	3	Probe Type/Length	G/6'
Stack Diameter	47.5x47.5	Pitot Coefficient	0.84
Operator	JG	Meter Box No./Y	644 / 1.0132
Filter No.	78	Nozzle No./Size	370 / .3020

Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO
S.G.				Leakrate	cfm		"Hg
				Initial			
				Final			
		TOTAL					

[TEMPERATURE ° F]

[illegible]

Date	9/19/90	Barometric Pressure	28.5/
Test Location	101A	Static in. wg.	- 0.30
Run Number	2	Probe Type/Length	G/6'
Stack Diameter	42.5 x 47.5	Pitot Coefficient	0.84
Operator	JS	Meter Box No./Y	644/1.0/32
Filter No.	78	Nozzle No./Size	270/3020

Contents	Final	Initial	Net
S.G.		TOTAL	

Time	CO ₂	O ₂	C0

Leakrate	cfm	"Hg
Initial		
Final	0.009	11.5 mm Hg

[T E M P E R A T U R E ° F]												
Sample Point	Time	ΔP in wg	ΔH in wg	Gas Meter Volume Ft ³	Stack	Probe	Oven	Imp.	Gas Meter IN OUT	Pump Vacuum in. Hg	$\sqrt{\Delta P}$	Comments
4	15	0.37	2.29	488.125	235	220	234	55	111 111	9.5	0.608	
	20			492.580								
A 1	0	0.39	2.29	492.580	270	230	227	54	108 108	9.0	0.624	
2	5	0.40	2.33	497.004	274	237	235	55	108 108	9.5	0.632	
3	10	0.40	2.49	501.562	226	234	232	58	108 108	9.5	0.632	
4	15	0.33	2.04	506.119	232	232	233	60	108 107	8.0	0.574	
	20			510.373								
C 1	4:33	0.39	2.39	510.373	233	253	234	60	105 105	10.0	0.624	
2	5	0.40	2.44	514.905	239	238	235	57	108 105	10.0	0.632	
3	10	0.39	2.45	519.520	220	233	236	52	108 107	10.0	0.624	
4	15	0.24	1.51	524.130	221	232	255	52	109 108	6.0	0.490	pilot ok
	20			527.953								
	140		2.33	125.674	241.39				107.02		0.6174	surge for 15 min

PLANT SWEEP-101-B TEST TYPE M-5/8 FIELD TEST DATA SHEET (Page 1 of 3)

[IMPINGER VOLUMES/WEIGHTS] [GAS COMPOSITION]

Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO
80% IPA	671.7	558.0	113.7				
3% H ₂ O ₂	583.4	543.9	39.5				
3% H ₂ O ₂	560.2	543.1	17.1				
S.G.	864.9	798.3	66.6	Leakrate	cfm	"Hg	
		TOTAL	230.9	Initial	.003	15"	
				Final	.001	5.0"	

Date 9-20-90 Barometric Pressure 28.49
 Test Location 101-B Static in.wg. - .23
 Run Number 1 Probe Type/Length G-6
 Stack Diameter 47.5x47.5 Pitot Coefficient .087
 Operator SM Meter Box No./Y 644/1.0132
 Filter No. 79 Nozzle No./Size #270/1.3020

[TEMPERATURE ° F]

Sample Point	Time	ΔP in wg	ΔH in wg	Gas Meter Volume Ft ³	Stack	Probe	Oven	Imp.	Gas Meter IN OUT	Pump Vacuum in.Hg	ΔP	Comments
G-1	0.0	0.37	2.13	536.210	263	261	270	67	91 92	3.5	0.608	Pitot OK
-2	5.0	0.40	2.32	540.334	255	255	262	59	71 89	4.0	0.632	LOSS PUMP 0958 RESET - 0951
-3	10.0	0.40	2.38	544.749	247	230	244	56	100 96	4.0	0.632	
-4	15.0	0.34	2.04	549.262	245	266	232	57	102 99	3.5	0.583	
E-1	20.0	0.39	2.33	553.324	245	261	247	60	99 98	4.0	0.624	1011 LOSS OF PUMP Pitot OK LOSS OF PUMP 1019 RESET 1022
-2	25.0	0.40	2.41	557.772	245	230	237	54	105 103	4.0	0.632	
-3	30.0	0.40	2.45	562.328	231	257	238	55	103 101	4.5	0.632	FHW 24765
-4	35.0	0.37	2.25	566.941	239	264	242	57	105 103	4.0	0.608	MF 24766
A-1	40.0	0.42	2.55	571.332	239	270	231	60	103 103	4.5	0.648	IPA 24767
-2	45.0	0.40	2.46	575.999	232	268	241	60	107 105	4.5	0.632	
-3	50.0	0.40	2.49	580.670	224	240	265	61	107 104	4.5	0.632	
-4	55.0	0.25	1.53	585.239	238	235	246	63	108 107	3.0	0.500	AMF 24768
A-1	60.0	0.38	2.28	588.933	248	251	244	65	105 105	3.5	0.616	H ₂ O ₂ 24769

Date 9-20-90 Barometric Pressure 28.49
 Test Location 101-B Static in. wg. - .23
 Run Number 1 Probe Type/Length G-6'
 Stack Diameter 42.5x47.5 Pitot Coefficient 0.84
 Operator SM Meter Box No./Y 644/1.0132
 Filter No. 79 Nozzle No./Size #270/3020

Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO
				Leakrate	cfm	"Hg	
S.G.				Initial	.003	15"	
		TOTAL		Final	.001	50"	

[TEMPERATURE ° F]

[illegible]

PLANT Sweet TEST TYPE M-5/8 FIELD TEST DATA SHEET (Page 1 of 3)

[[INPINGER	VOLUMES/WEIGHTS	] [GAS COMPOSITION	]]
1	100	100	100
2	100	100	100
3	100	100	100
4	100	100	100
5	100	100	100
6	100	100	100
7	100	100	100
8	100	100	100
9	100	100	100
10	100	100	100
11	100	100	100
12	100	100	100
13	100	100	100
14	100	100	100
15	100	100	100
16	100	100	100
17	100	100	100
18	100	100	100
19	100	100	100
20	100	100	100
21	100	100	100
22	100	100	100
23	100	100	100
24	100	100	100
25	100	100	100
26	100	100	100
27	100	100	100
28	100	100	100
29	100	100	100
30	100	100	100
31	100	100	100
32	100	100	100
33	100	100	100
34	100	100	100
35	100	100	100
36	100	100	100
37	100	100	100
38	100	100	100
39	100	100	100
40	100	100	100
41	100	100	100
42	100	100	100
43	100	100	100
44	100	100	100
45	100	100	100
46	100	100	100
47	100	100	100
48	100	100	100
49	100	100	100
50	100	100	100
51	100	100	100
52	100	100	100
53	100	100	100
54	100	100	100
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65	100	100	100
66	100	100	100
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83	100	100	100
84	100	100	100
85	100	100	100
86	100	100	100
87	100	100	100
88	100	100	100
89	100	100	100
90	100	100	100
91	100	100	100
92	100	100	100
93	100	100	100
94	100	100	100
95	100	100	100
96	100	100	100
97			

Date 9-20-90 Barometric Pressure 28.47
 Test Location 101-B Static in.wg. - .35
 Run Number 2 Probe Type/Length G-6'
 Stack Diameter 42.5 x 40.5 Pitot Coefficient 0.84
 Operator SM Meter Box No./Y 64/1,0137
 Filter No. 80 Nozzle No./Size #270/3020

Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO
80% IPA	668.9	533.8	135.1				
30% H ₂ O ₂	571.0	530.4	40.6				
30% H ₂ O ₂	545.8	545.5	0.3				
S.G.	835.6	769.1	66.5	Leakrate Initial	cfm 0.13	"Hg 15"	
		TOTAL	242.5	Final	.008	11"	

[TEMPERATURE . F]

Sample Point	Time hrs	ΔP in wg	ΔH in wg	Gas Meter Volume Ft ³	Stack	Probe	Oven	Imp.	Gas Meter IN OUT	Pump Vacuum in. Hg	$f_{\Delta P}$	Comments
F-1	0.0	0.39	2.36	673.187	240	248	242	67	103 103	9.5	0.624	F.TOT O.K
-2	5.0	0.39	2.36	677.644	241	241	236	54	105 104	9.5	0.624	F4W 2 24771
-3	10.0	0.38	2.36	682.190	230	252	249	53	109 107	9.5	0.616	ME 2 24772
-4	15.0	0.37	2.26	686.905	242	246	231	55	110 109	9.0	0.608	IPA 2 24773
D-1	20.0	0.38	2.35	691.157	231	243	241	61	108 108	9.0	0.616	AME 2 24774
-2	25.0	0.38	2.38	695.705	224	247	270	50	110 110	9.0	0.616	H2O2 2 24775
-3	30.0	0.38	2.40	700.165	220	245	264	46	111 111	9.0	0.616	HC 2 24776
-4	35.0	0.36	2.23	704.759	236	241	250	47	113 111	9.0	0.600	
B-1	40.0	0.41	2.52	709.247	239	246	237	52	111 112	10.0	0.640	
-2	45.0	0.40	2.47	713.856	237	243	234	49	111 111	10.0	0.632	
-3	50.0	0.39	2.46	718.486	222	237	229	53	111 111	10.0	0.624	
-4	55.0	0.37	2.26	723.109	244	235	258	54	112 112	9.5	0.608	
G-1	60.0	0.35	2.16	727.594	237	251	230	54	110 111	8.5	0.592	

[TEMPERATURE.]

A-14

TEST TYPE M-5/8 FIELD TEST DATA SHEET (Page 3 of 3)

Date 9-20-90 Barometric Pressure 28.47
 Test Location 101-B Static in.wg. -.35
 Run Number 2 Probe Type/Length G-6'
 Stack Diameter 47.5475 Pitot Coefficient 0.84
 Operator Sm Meter Box No./Y 644/1.0132
 Filter No. 80 Nozzle No./Size #270/3020

Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO
S.G.				Leakrate	cfm		"Hg
				Initial	.013		15"
				Final	.008		11"
		TOTAL					

[TEMPERATURE ° F]

[illegible]

Date 9-20-90

Test Location Fuel Gas Line

Run Number 1

Stack Diameter 4"

Operator VVP

Filter No. NA

Barometric Pressure 28.49

Static in. wg. —

Probe Type/Length TEFLON

Pitot Coefficient NA

Meter Box No. / 8005 / 29875

Nozzle No./Size NA

Impinger Volumes/Weights				Gas Composition			
Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO
	106.3	105.3					
	104.0	101.5					
	82.2	81.5					
				Leak Rate	cfm	"Hg	
				Initial	0.002	Max	
S.G.	122.7	117.7	Total	Final			

Sample Point	IIS Time	ΔP in wg	ΔH in wg	Gas Meter Volume Ft ³	Temperature °F				Pump Vacuum in. Hg	√ΔP	Comments
					Stack	Probe	Oven	Imp.			
	0			784.512				60	92	92	
	10			785.85				63	93	92	24777
	20			787.16				62	93	92	
	30			788.50				60	93	92	24778
	40			789.83				59	93	92	
	50			791.17				61	94	92	
	60			792.48				63	95	93	
	70			793.81				63	95	93	
	80			795.15				64	95	93	
	90			796.47				66	96	93	
	100			797.81				66	96	93	
	110			799.14				62	96	93	
	120			800.470							

Date 9-20-90

Test Location	Fuel Gas Line

Run Number

Stack Diameter $\sim 4 \frac{1}{4}$ in.

Operator

Filter No. NH

Barometric Pressure 28.44

Static in. wg.

[illegible]

Pitot Coefficient $\frac{NH}{0.00514}$

Meter Box No. / 8

Nozzle No./Size
NH

Impinger Volumes/Weights				Gas Composition			
Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO
S.G.				Leak Rate		cfm	"Hg
				Initial			
				Final		0.002	Max
			Total				

Sample Point	Time	ΔP in wg	ΔH in wg	Gas Meter Volume Ft. ³	Temperature °F					Pump Vacuum in. Hg	$\sqrt{\Delta P}$	Comments	
					Stack	Probe	Oven	Imp.	Gas Meter				
									In				Out
	120			800.470				63	90	93			
	130			801.52				63	90	93			
	140			803.20				65	97	93			
	150			804.55				67	97	93			
	160			805.93				62	98	94			
	170			807.30				60	98	94			
	180			808.66				59	98	94			
	190			810.01				60	98	94			
	200			811.39				62	97	95			
	210			812.75				63	98	95			
	220			814.11				64	99	95			
	230			815.48				66	99	95			
	240			816.843									
	1515												
	TA			32.331					94.	50			

Plant SWEPI COALINGA COGEN APCD Witness/Number _____
 Date 9/19/90 Run No. #1 (PREF FOR 2) Generator Type Allison CTG "501" KBS
 Test Location HRS6101A OUTLET, Port B-3 "A-3" Burner Type _____
 Operator PCS O₂ Controller Type _____
 Fuel Type NATURAL GAS Trailer No. #3 Gas Cylinder Nos. NOX-AAL-13433 AAL-15365 AAL-2171
CO₂/CO/O₂-11-23410, CC12055,
CO-CC163, AAL-9891,

Time	Sample Point	Fuel Flow	Dry Uncorrected					Response Time		NO-NOx Converter Gas			Comments
			O2 %	CO2 %	CO ppm	SO2 ppm	NO ppm	NOx ppm	Up (sec)	Down (sec)	NO	NO2	
0830			15.0	14.71	80.7			81.9					SPAN GAS VALUES
			Ø	Ø	Ø			Ø					ZERO GAS
								41.4					NOx LIN / = (41.39 PPM)
			3.825					20.6					NOx LIN / = (20.04 PPM)
0913					36.0								NOx LIN / = (3.82 %)
			5.0										CO LIN / = (37.4 PPM)
			15.2	4.92	82.7			79.0					CO2 LIN / = (5.02 %)
0939			0.12										EXTERNAL CHECK
			15.0	5.02	82.1			81.9					LEAK CHECK - GOOD
			Ø	Ø	Ø			Ø					RECALIBRATE
1030	B-3												SPAN GAS VALUES
			15.03	3.36	4.20			34.8					START RUN #1 @ 1025
			14.98	3.34	3.85			34.8					
			14.98	3.34	3.80			35.1					
			14.95	3.34	4.00			35.2					
			14.93	3.32	3.80			35.1					
			14.93	3.32	3.85			35.3					
			14.90	3.29	3.75			35.1					
1130	B-3 A-3		14.91	3.28	3.80			35.2					CHANGE PROBE POSITION
			14.90	3.26	3.61			35.3					FROM B-3 TO A-3 @ 1140
			14.85	3.26	3.85			35.4					
			14.85	3.26	3.75			35.3					
			14.83	3.24	3.62			35.2					
			Ø	Ø	+0.25			+0.3					END RUN #1 @ 1225
			14.90	4.80	8.43			81.1					ZERO CHECK - NO ADJ
													SPAN CHECK - NO ADJ
24761													

—

Plant ~~SWEPT COALING COGEN~~

Date 9/19/90 Run No. #2

Test Location HRSG-101A OUTLET

Operator pes

Fuel Type NATURAL GAS Trailer No. 3

APCD Witness/Number

Generator Type Allison CTG "501" KB5

Burner Type

02 Controller Type

Gas Cylinder Nos.

NOX- AAL-13433, AAL-15365, AAL-2171
CO₂-CO-O₂- 1L-23410, CC12655
CO - CC163, AAL-9891

Time	Sample Point	Fuel Flow	Dry Uncorrected						Response Time		NO-NOx Converter Gas			Comments
			O2 %	CO2 %	CO ppm	SO2 ppm	NO ppm	NOx ppm	Up (sec)	Down (sec)	NO	NO2	NOx	
1255			15.0	5.02	8.21									SPAN GAS VALUES
			Ø	Ø	Ø									ZERO GAS
1420	A-3		14.85	3.36	3.38									START RUN # 2 @ 1415
1430	/		14.75	3.36	3.42									
1440	/		14.65	3.34	3.39									
1450	/		14.63	3.32	3.42									
1500	/		14.60	3.32	3.42									
1510	/		14.60	3.32	3.43									
1520	B-3		14.60	3.28	3.42									CHANGE PROBE POSITION
1530			14.60	3.30	3.39									FROM A-3 TO B-3 @ 1525
1540			14.58	3.27	3.42									
1550			14.55	3.24	3.40									
1600			14.55	3.24	3.40									
1610			14.55	3.22	3.44									END RUN # 2 @ 1615
1615			Ø	-0.08	+0.12									ZERO CHECK - NO ADJ
			15.45	4.80	8.24									SPAN CHECK - NO ADJ
			+0.15	4.70	8.36									EXTERNAL CHECK

CONTINUOUS MONITOR DATA SHEET

Plant SWEPI COALINGH

Date 9-20-90 Run No. 1

Test Location HDSG OUT

Operator VDP

Fuel Type NAT'L GAS Trailer No. 3

APCD Witness/Number

Client Rep

Generator Type

Burner Type

O₂ Controller Type

Dry Uncorrected

Time	Sample Point	O ₂ %	CO ₂ %	CO ppm	SO ₂ ppm	NO ppm	NO _x ppm	Comments	Miscellaneous Information
		15.0	14.71	8.21			81.9	SPAN VALUES	NO _x 13433, 2171, 13365
		0.0	0.0	0.0			0.0	CALC —	SO ₂ 86236, 9891
		15.0	14.71	8.21			81.9	ZERO	CO 23410, 12053
							41.38	SPAN	
							82.2	LINEARITY CHECKS	
							20.06	MID	
		15.0	14.71	8.21			81.8	HI	Wet Bulb: Dry Bulb:
		3.9	5.02	3.44			41.39	LOW	Barometric Press:
		0.15	4.90	8.40			25.0	RESET SPAN VALUES	
		15.0	5.02	37.4			24.8	EXT (BIAS) CHECK	RESPONSE TIME
							24.8	CAL ADJUST	Upscale: 48 Downscale: 43
							24.8		Upscale: 45 Downscale: 42
0935	PORT E	14.75	3.35	6.00			24.6		Upscale: 45 Downscale: 42
45		14.65	3.40	6.30			24.4		
55		14.60	3.40	6.60			24.2		
1005	CM PORT	14.60	3.40	6.10			25.0		
15		14.60	3.40	6.10			24.2		
25		14.50	3.40	6.30			24.2		
35		14.50	3.40	6.30			24.2		
45		14.40	3.35	6.80			24.2		
55		14.35	3.35	6.60			25.0		
1105		14.30	3.30	4.90			25.0		
15		14.25	3.30	5.10			0.2		
25		14.25	3.30	5.20			41.8		
1135	CAL ✓	0.0	-0.15	0.10			8.20	ZERO —	
		15.20	4.80	8.20				SPAN ✓	

PROCESS DATA

Fuel Flow:

Steam Flow:

Rating:

CONVERTER GAS

Cal Gas Values | Actual Values

NO

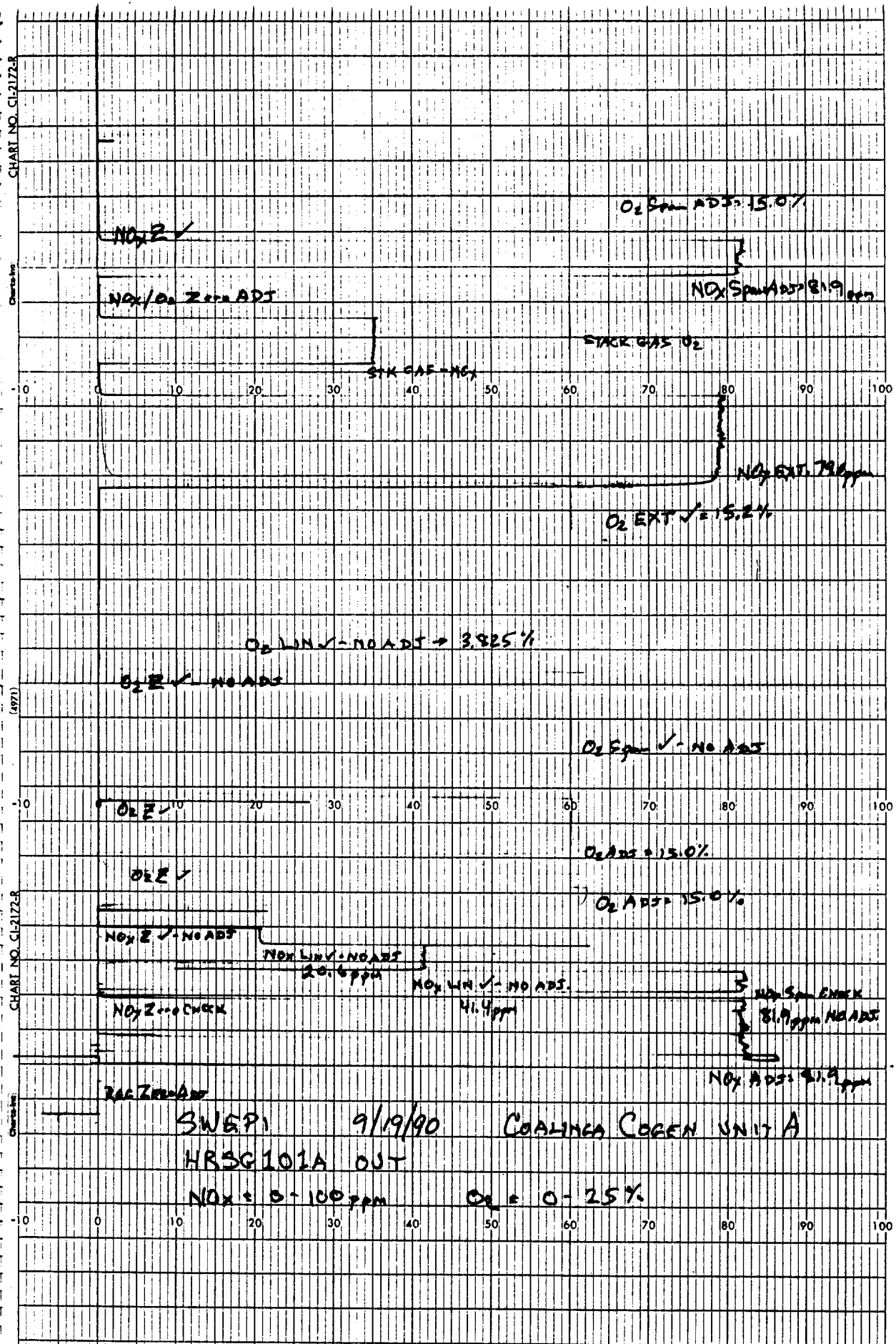
NO₂

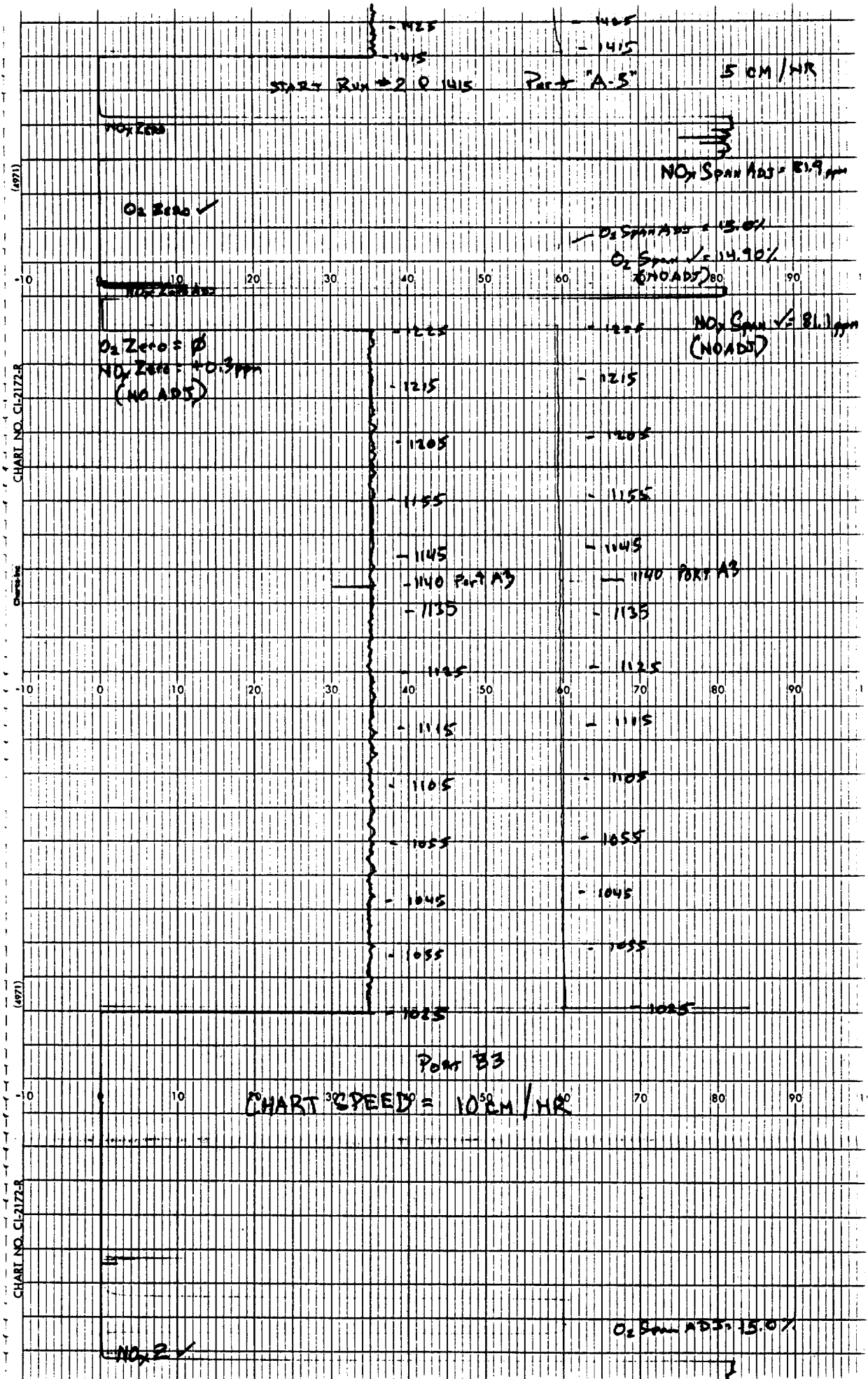
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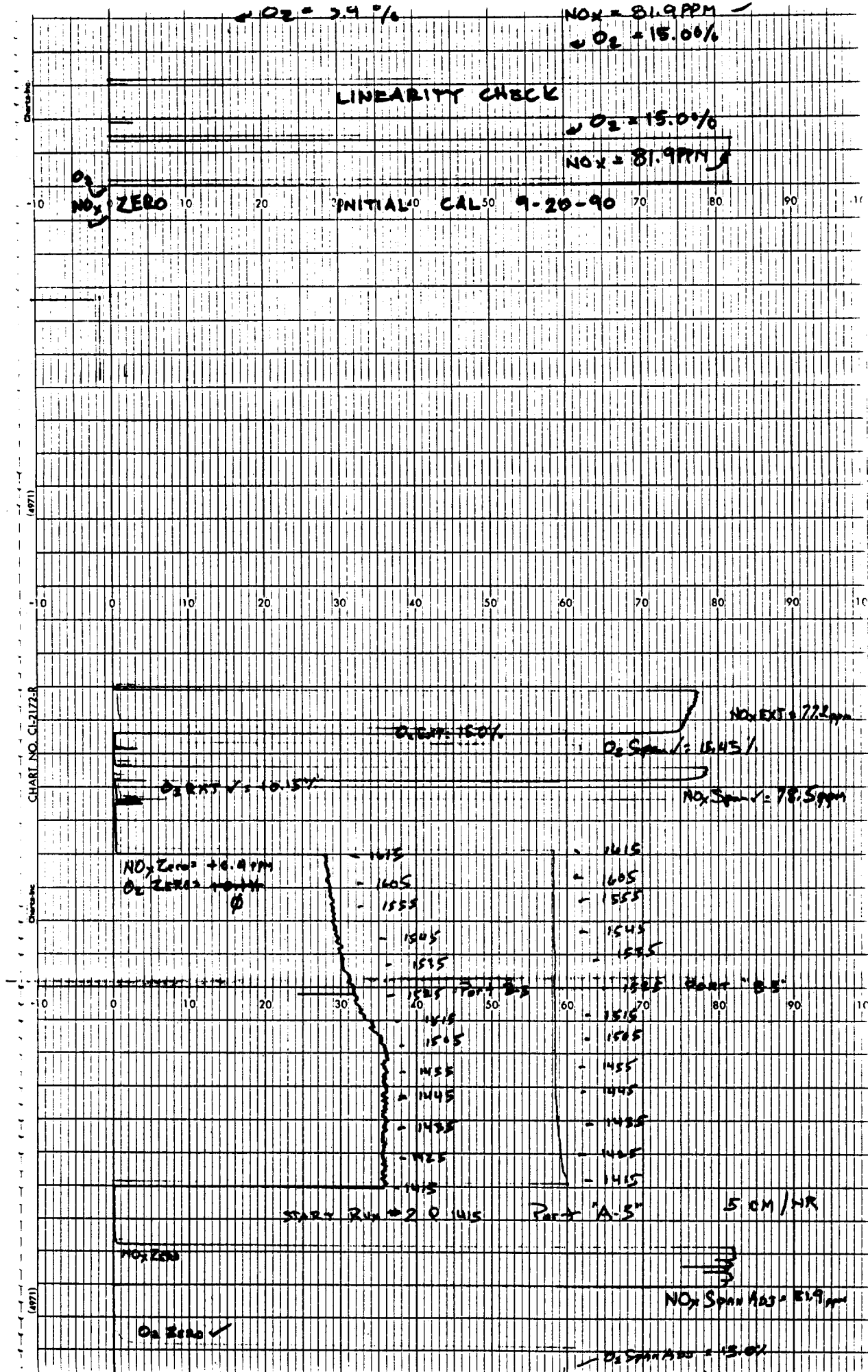
CONTINUOUS MONITOR DATA SHEET

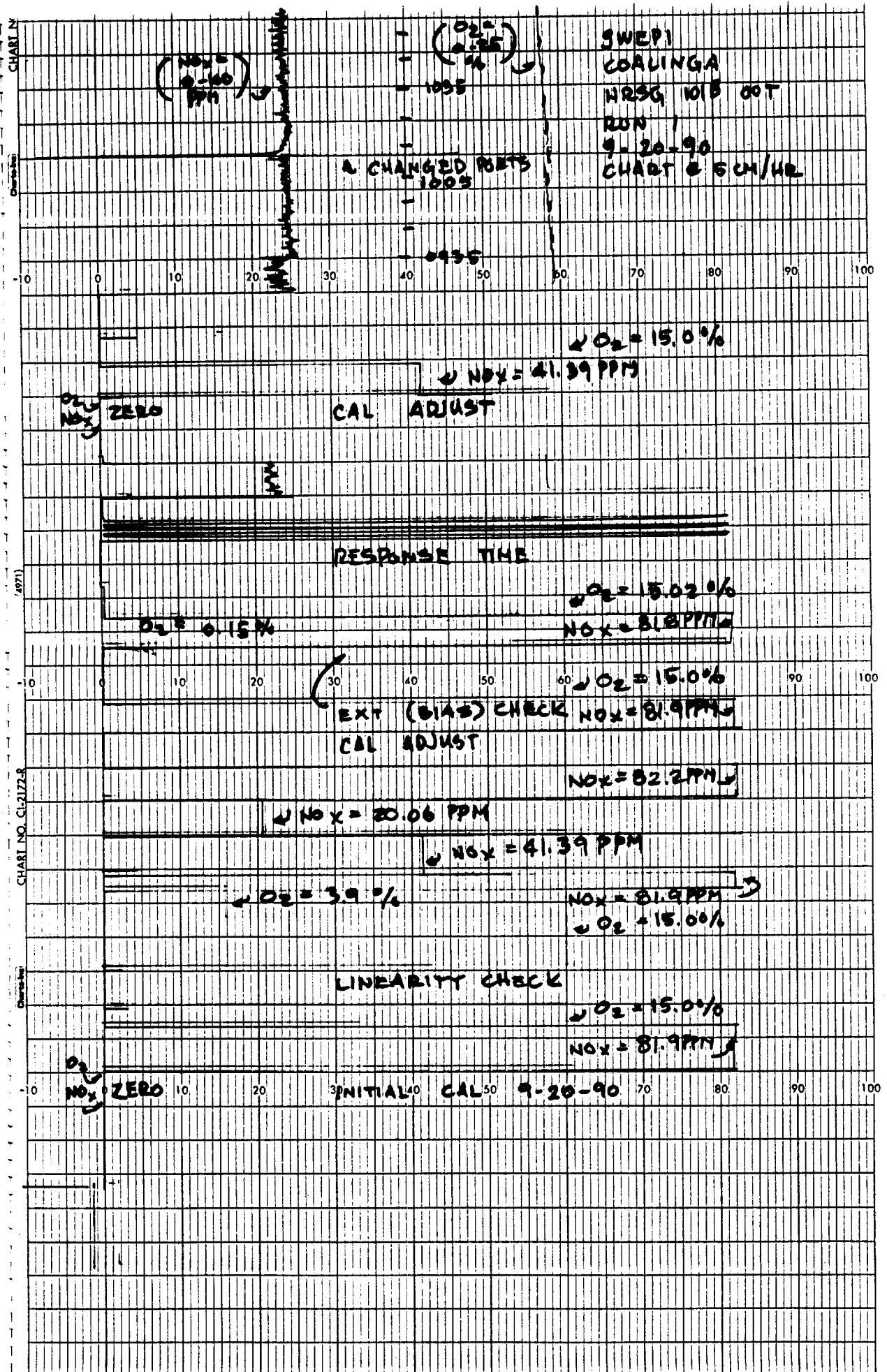
Plant SWEPI COALINGA APCD Witness/Number _____
 Date 9-20-90 Run No. 2 Client Rep _____
 Test Location HDEG 1018 Generator Type _____
 Operator VVM Burner Type _____
 Fuel Type N. GAS Trailer No. 3 O₂ Controller Type _____

Time	Sample Point	Dry Uncorrected						Comments	Miscellaneous Information
		O ₂ %	CO ₂ %	CO ppm	SO ₂ ppm	NO ppm	NO _x ppm		
		15.0	5.02	8.21			41.39	SPAN VALUES	CALIBRATION GASES
1325	CP1002F	14.50	3.35	5.60			25.4	DUN 2	NO _x _____
35		14.50	3.30	6.55			24.0		SO ₂ _____
45		14.45	3.30	6.70			24.0		CO _____
55		14.50	3.25	8.30			23.0		CO/CO ₂ /O ₂ _____
1405		14.50	3.20	9.00			23.0		Wet Bulb: _____ Dry Bulb: _____
15		14.45	3.20	8.10			23.0		Barometric Press: _____
25		14.45	3.20	8.60			23.4		
35		14.40	3.20	9.20			23.6		RESPONSE TIME
45		14.40	3.20	7.65			24.0		Upscale: _____ Downscale: _____
55		14.60	3.20	6.90			24.0		Upscale: _____ Downscale: _____
1505		14.60	3.20	6.40			25.0		Upscale: _____ Downscale: _____
15		14.60	3.20	6.40			25.0		
									PROCESS DATA
1525		0.10	-0.15	-0.02			0.8	ZERO ✓	Fuel Flow: _____
		15.05	4.85	8.36			43.2	SPAN ✓	Steam Flow: _____
		0.15	4.80	8.45			42.2	EXT (8145) ✓	Rating: _____
									CONVERTER GAS
									Cal Gas Values Actual Values
									NO _____
									NO ₂ _____
									Conv. Efficiency: _____









SWEPI
COALINGA
NRSG 1015 00T
RUN 1
9-20-90
CHART @ 5 CM/HR

(NOx = 2.46 PPM)

(O2 = 15.0%)

A CHANGED PORTS

NOx ZERO

CAL ADJUST

O2 = 15.0%

NOx = 41.39 PPM

RESPONSE TIME

O2 = 15.02%

NOx = 81.8 PPM

O2 = 15.0%

EXT (BIAS) CHECK NOx = 81.9 PPM

CAL ADJUST

O2 = 15.0%

NOx = 82.2 PPM

NOx = 20.06 PPM

NOx = 41.39 PPM

O2 = 15.0%

NOx = 81.9 PPM

O2 = 15.0%

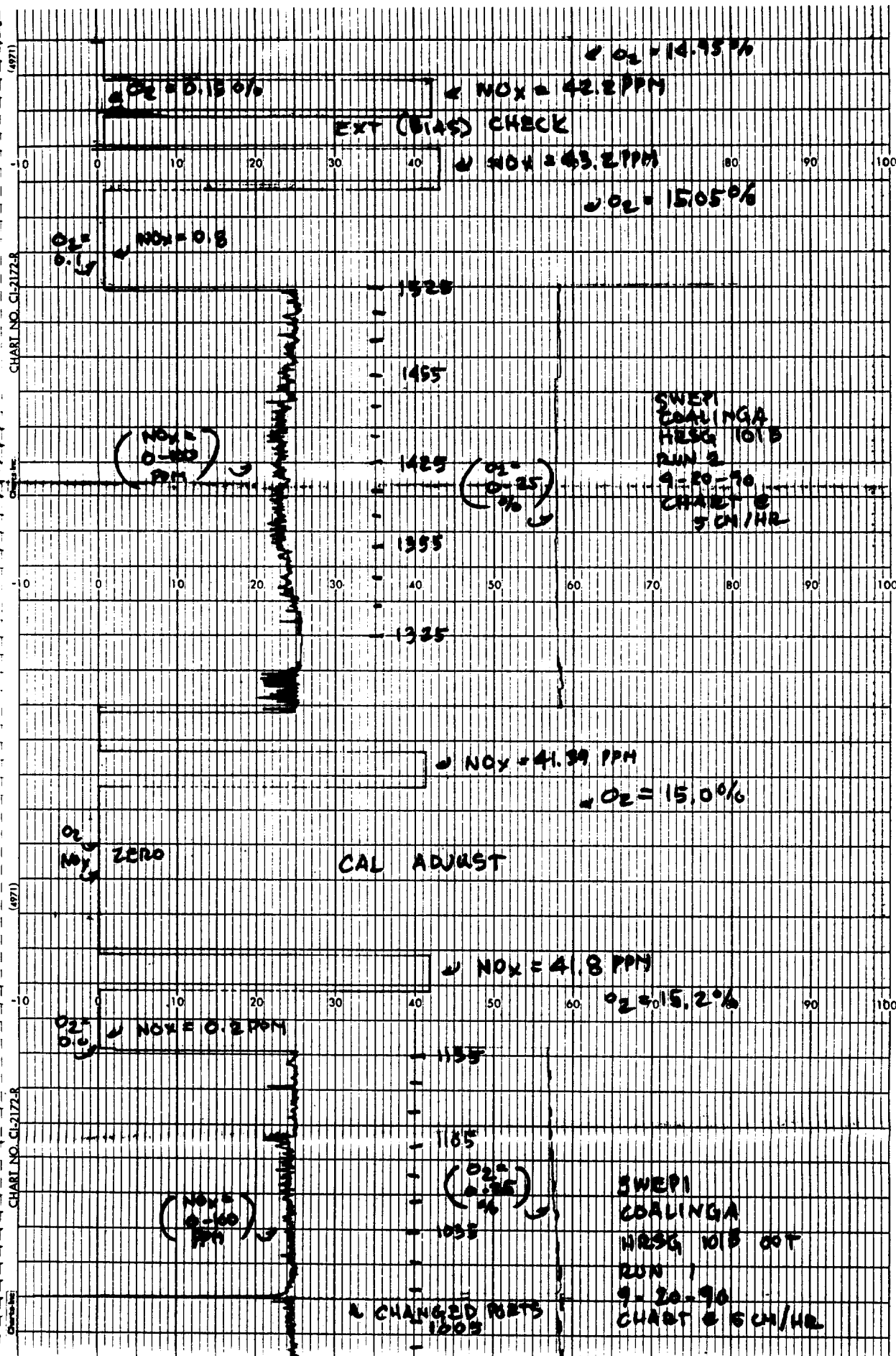
LINEARITY CHECK

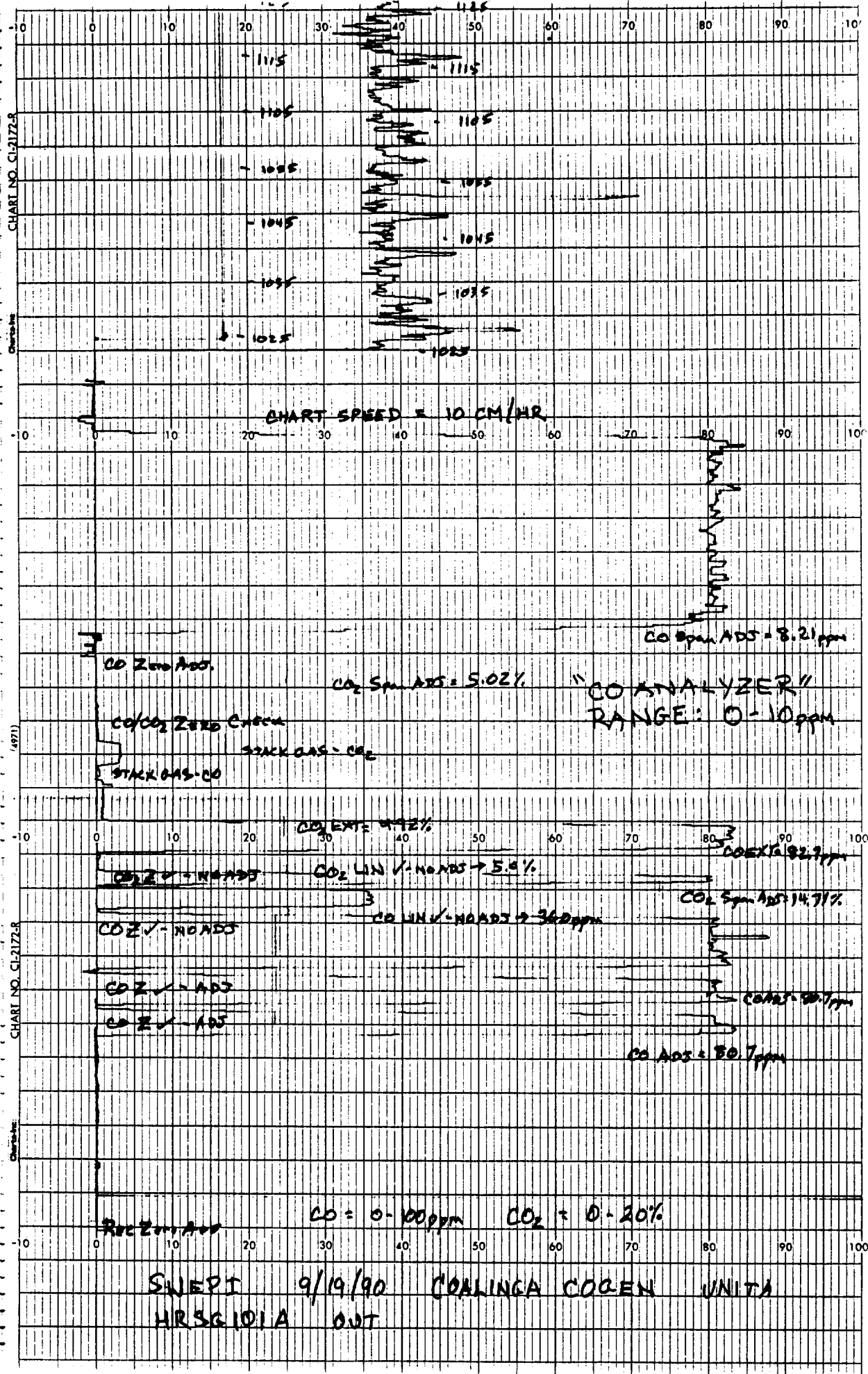
O2 = 15.0%

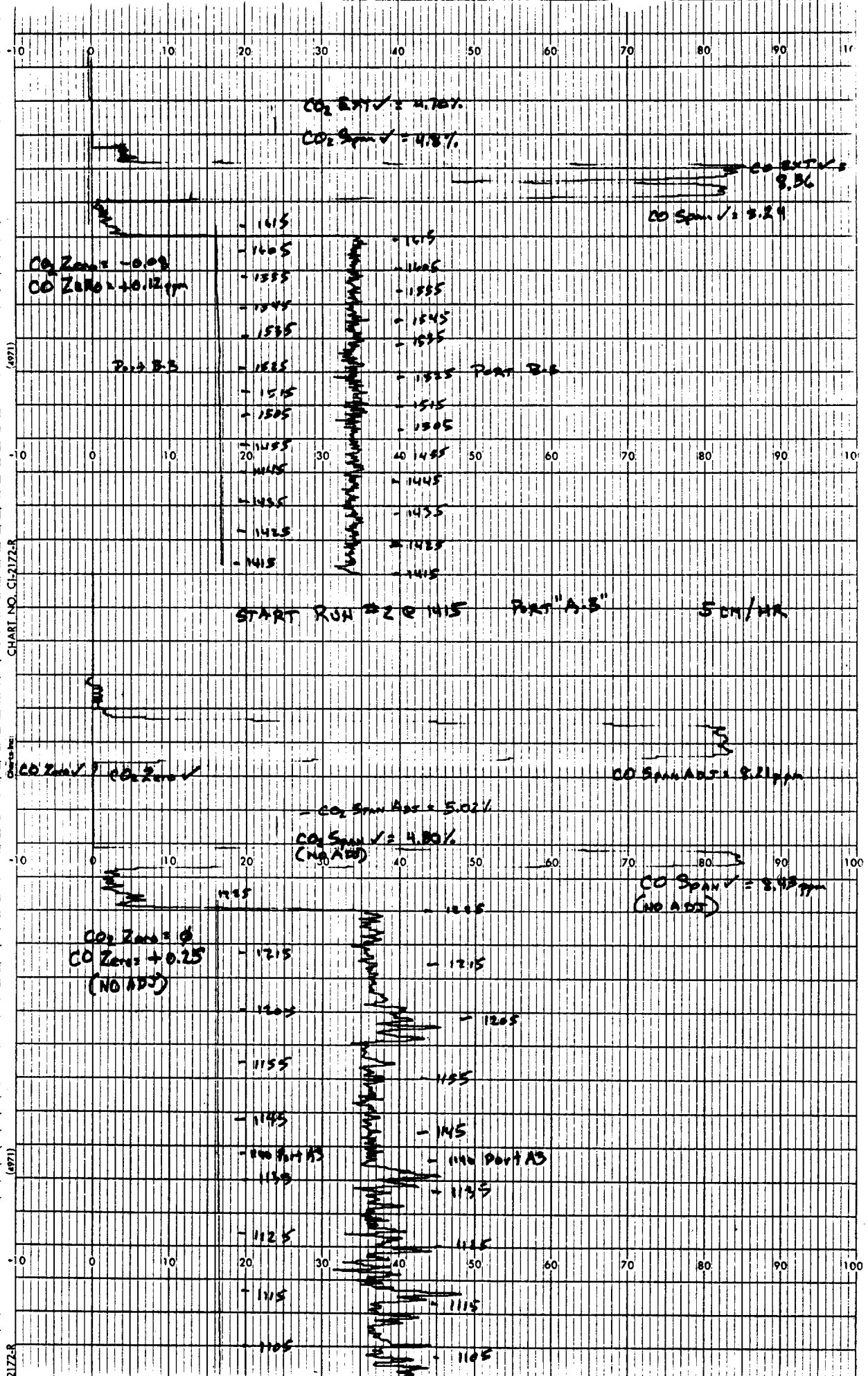
NOx = 81.9 PPM

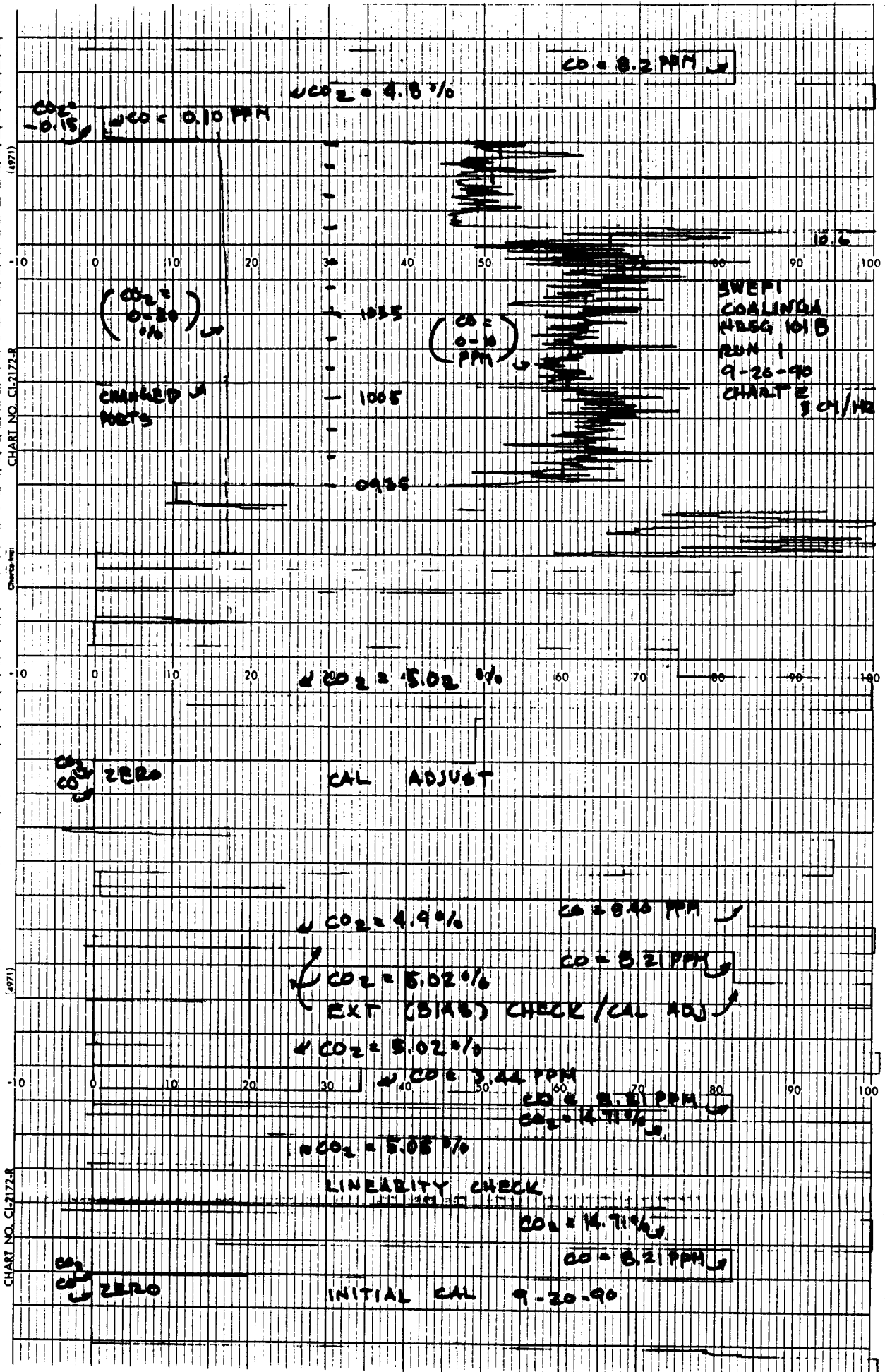
NOx ZERO

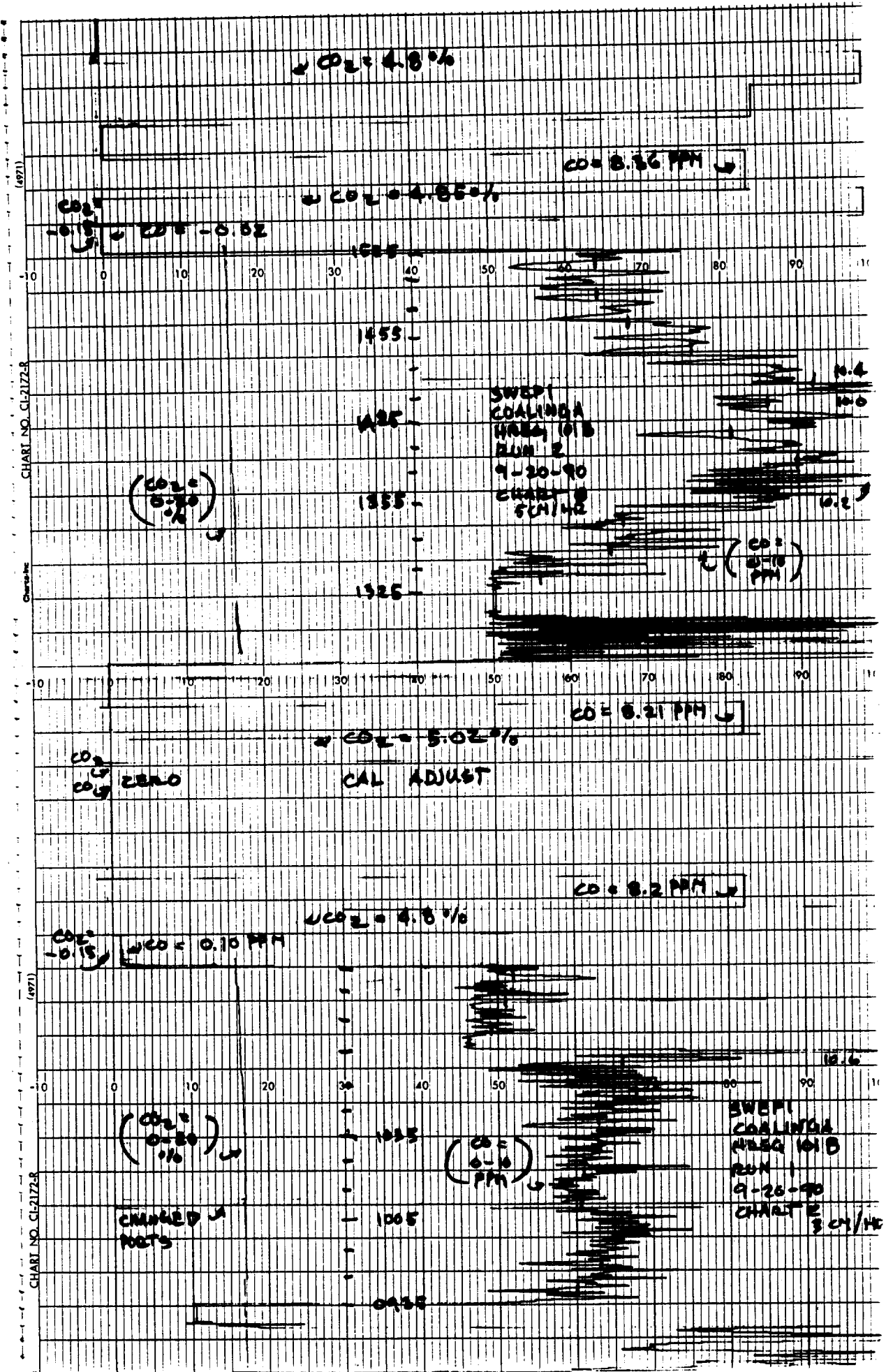
INITIAL CAL 9-20-90











A. CALIBRATION AND CORRECTION DATA

Company : SWEPI COALINGA Date : 9/19/90
 Station : HRSO 101A Test Run : 1
 Test Condition: COMPL

Concentration : Drift Uncorrected (A) / Corrected (B)											
Point #	%O ₂		%CO ₂		ppm CO		ppm SO ₂		ppm NOx		
	A	B	A	B	A	B	A	B	A	B	
1	15.03	15.03	3.36	3.37	4.20	4.19			34.80	34.81	
2	14.98	14.99	3.34	3.36	3.85	3.82			34.80	34.82	
3	14.98	15.00	3.34	3.37	3.80	3.75			35.10	35.14	
4	14.95	14.98	3.34	3.38	4.00	3.93			35.20	35.25	
5	14.93	14.97	3.32	3.37	3.80	3.71			35.10	35.16	
6	14.93	14.98	3.32	3.38	3.85	3.74			35.30	35.38	
7	14.90	14.95	3.29	3.36	3.75	3.62			35.10	35.19	
8	14.91	14.97	3.28	3.36	3.80	3.65			35.20	35.31	
9	14.90	14.97	3.26	3.36	3.61	3.44			35.30	35.42	
10	14.85	14.93	3.26	3.37	3.85	3.66			35.40	35.54	
11	14.85	14.94	3.26	3.38	3.75	3.54			35.30	35.45	
12	14.83	14.93	3.24	3.37	3.62	3.39			35.20	35.37	
MEAN		14.97		3.37		3.70					35.24

Concentration : Drift Uncorrected (A) / Corrected (B)											
Point #	%O ₂		%CO ₂		ppm CO		ppm SO ₂		ppm NOx		
	A	B	A	B	A	B	A	B	A	B	
Zero Check		0.00		0.00		0.25				0.30	
Span Check		14.90		4.80		8.43				81.10	
Cal. Gas		15.00		5.00		8.21				81.90	
Scf	-0.00056		-0.00333		-0.00030				-0.00112		
Zcf	0.00000		0.00000		0.02083				0.02500		

Scf, Span Drift Correction Factor = (% Drift / 100) / # of Readings
 Zcf, Zero Drift Correction Factor = Zero Drift / # of Readings
 Cz, Zero Corr. Concentration = measured value - [Zcf x (Point # - 0.5)]
 B, Corrected Concentration = Cz / [1 + (Scf x (Point # - 0.5))]

A. CALIBRATION AND CORRECTION DATA

Company : SWEPI COALINGA Date : 9/19/90
 Station : HRSG 101A Test Run : 2
 Test Condition: COMPL

Concentration : Drift Uncorrected (A) / Corrected (B)											
Point #	%O2		%CO2		ppm CO		ppm SO2		ppm NOx		
	A	B	A	B	A	B	A	B	A	B	
1	14.85	14.83	3.36	3.37	3.38	3.38			35.70	35.75	
2	14.75	14.69	3.36	3.38	3.42	3.41			35.70	35.86	
3	14.65	14.56	3.34	3.37	3.39	3.37			35.80	36.07	
4	14.63	14.50	3.32	3.37	3.42	3.40			35.80	36.17	
5	14.60	14.44	3.32	3.38	3.42	3.39			35.80	36.28	
6	14.60	14.40	3.32	3.39	3.43	3.39			34.90	35.47	
7	14.60	14.37	3.28	3.37	3.42	3.38			32.50	33.12	
8	14.60	14.33	3.30	3.40	3.39	3.34			31.00	31.67	
9	14.58	14.28	3.27	3.38	3.42	3.36			30.00	30.73	
10	14.55	14.21	3.24	3.37	3.40	3.33			29.20	29.98	
11	14.55	14.18	3.24	3.38	3.40	3.33			28.80	29.65	
12	14.55	14.14	3.22	3.37	3.44	3.36			28.40	29.32	
MEAN		14.41		3.38		3.37				33.34	

	%O2		%CO2		ppm CO		ppm SO2		ppm NOx	
	A	B	A	B	A	B	A	B	A	B
Zero Check		0.00		-0.08		0.12				0.40
Span Check		15.45		4.80		8.24				78.50
Cal. Gas		15.00		5.00		8.21				81.90
Scf		0.00250		-0.00200		-0.00091				-0.00387
Zcf		0.00000		-0.00667		0.01000				0.03333

Scf, Span Drift Correction Factor = (% Drift / 100) / # of Readings
 Zcf, Zero Drift Correction Factor = Zero Drift / # of Readings
 Cz, Zero Corr. Concentration = measured value - [Zcf x (Point # - 0.5)]
 B, Corrected Concentration = Cz / [1 + (Scf x (Point # - 0.5))]

A. CALIBRATION AND CORRECTION DATA

Company : SWEPI COALINGA Date : 09/20/90
 Station : HRSGL01B Test Run : 1
 Test Condition: COMPL

Concentration : Drift Uncorrected (A) / Corrected (B)										
Point #	%O2		%CO2		ppm CO		ppm SO2		ppm NOx	
	A	B	A	B	A	B	A	B	A	B
1	14.75	14.74	3.35	3.36	6.00	6.00			25.00	24.99
2	14.65	14.63	3.40	3.42	6.30	6.30			24.80	24.76
3	14.60	14.56	3.40	3.44	6.60	6.60			24.80	24.73
4	14.60	14.54	3.40	3.45	6.10	6.09			24.80	24.71
5	14.60	14.53	3.40	3.47	6.10	6.09			24.60	24.48
6	14.50	14.41	3.40	3.48	6.30	6.29			24.60	24.45
7	14.50	14.40	3.40	3.50	6.30	6.29			24.40	24.23
8	14.40	14.28	3.35	3.47	6.80	6.79			24.20	24.00
9	14.35	14.22	3.35	3.48	6.60	6.59			24.20	23.97
10	14.30	14.15	3.30	3.45	4.90	4.87			25.00	24.74
11	14.25	14.09	3.30	3.46	5.10	5.07			25.00	24.72
12	14.25	14.07	3.30	3.48	5.20	5.17			25.00	24.69
MEAN		14.38		3.45		6.01				24.54

	%O2	%CO2	ppm CO	ppm SO2	ppm NOx
Zero Check	0.00	-0.15	0.10		0.20
Span Check	15.20	4.80	8.20		41.80
Cal. Gas	15.00	5.00	8.21		41.39
Scf	0.00111	-0.00083	-0.00112		0.00042
Zcf	0.00000	-0.01250	0.00833		0.01667

Scf, Span Drift Correction Factor = (% Drift / 100) / # of Readings
 Zcf, Zero Drift Correction Factor = Zero Drift / # of Readings
 Cz, Zero Corr. Concentration = measured value - [Zcf x (Point # - 0.5)]
 B, Corrected Concentration = Cz / [1 + (Scf x (Point # - 0.5))]

A. CALIBRATION AND CORRECTION DATA

Company : SWEPI COALINGA

Date : 09/20/90

2

Test Run :
Test Condition: COMPL

Station : HRSGL01B

Concentration : Drift Uncorrected (A) / Corrected (B)											
Point #	%O2		%CO2		ppm CO		ppm SO2		ppm NOx		
	A	B	A	B	A	B	A	B	A	B	
1	14.50	14.50	3.35	5.60	5.60	5.60			25.40	25.34	
2	14.50	14.49	3.30	6.54	6.55	6.54			24.60	24.43	
3	14.45	14.44	3.30	6.68	6.70	6.68			24.00	23.71	
4	14.50	14.48	3.25	8.45	8.50	8.45			23.00	22.61	
5	14.50	14.48	3.20	8.94	9.00	8.94			23.00	22.49	
6	14.45	14.43	3.20	8.03	8.10	8.03			23.00	22.38	
7	14.45	14.42	3.20	8.52	8.60	8.52			23.40	22.67	
8	14.40	14.37	3.20	9.09	9.20	9.09			23.60	22.75	
9	14.40	14.36	3.20	7.55	7.65	7.55			24.00	23.04	
10	14.60	14.56	3.20	6.71	6.80	6.71			24.60	23.51	
11	14.60	14.55	3.20	6.30	6.40	6.30			25.00	23.79	
12	14.60	14.55	3.20	6.29	6.40	6.29			25.00	23.68	
MEAN		14.47	3.23	7.39						23.37	

	%O2		%CO2		ppm CO		ppm SO2		ppm NOx	
	A	B	A	B	A	B	A	B	A	B
Zero Check		0.10		-0.15		-0.02				0.80
Span Check		15.05		4.85		8.36				43.20
Cal. Gas		15.00		5.00		8.21				41.39
Scf		-0.00028				0.00173				0.00203
Zcf		0.00833				-0.00167				0.06667

Scf, Span Drift Correction Factor = (% Drift / 100) / # of Readings
Zcf, Zero Drift Correction Factor = Zero Drift / # of Readings
Cz, Zero Corr. Concentration = measured value - [Zcf x (Point # - 0.5)]
B, Corrected Concentration = Cz / [1 + (Scf x (Point # - 0.5))]

B. ZERO AND SPAN DRIFT PERCENT CALCULATIONS

Company : SWEPI COALINGA

Date : 9/19/90

Station : HRSG 101A

Run 1	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
Initial Span	15.00	5.00	8.21		81.90
Measured Span	14.90	4.80	8.43		81.10
Zero Drift	0.00	0.00	0.25		0.30
Final, Actual Span	14.90	4.80	8.18		80.80
Percent Drift	-0.7	-4.0	-0.4		-1.3
*****	*****	*****	*****	*****	*****
Run 2	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
Initial Span	15.00	5.00	8.21		81.90
Measured Span	15.45	4.80	8.24		78.50
Zero Drift	0.00	-0.08	0.12		0.40
Final, Actual Span	15.45	4.88	8.12		78.10
Percent Drift	3.0	-2.4	-1.1		-4.6
*****	*****	*****	*****	*****	*****
Run	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
Initial Span					
Measured Span					
Zero Drift					
Final, Actual Span					
Percent Drift					

Final, Actual Span = Measured Span - Zero Drift

Percent Drift = (Final, Actual Span - Initial Span) / Initial Span x 100

B. ZERO AND SPAN DRIFT PERCENT CALCULATIONS

Company : SWEPI COALINGA

Date : 09/20/90

Station : HRSG101B

Run 1	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
Initial Span	15.00	5.00	8.21		41.39
Measured Span	15.20	4.80	8.20		41.80
Zero Drift	0.00	-0.15	0.10		0.20
Final, Actual Span	15.20	4.95	8.10		41.60
Percent Drift	1.3	-1.0	-1.3		0.5
*****	*****	*****	*****	*****	*****
Run 2	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
Initial Span	15.00	5.00	8.21		41.39
Measured Span	15.05	4.85	8.36		43.20
Zero Drift	0.10	-0.15	-0.02		0.80
Final, Actual Span	14.95	5.00	8.38		42.40
Percent Drift	-0.3	0.0	2.1		2.4
*****	*****	*****	*****	*****	*****
Run	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
Initial Span					
Measured Span					
Zero Drift					
Final, Actual Span					
Percent Drift					

Final, Actual Span = Measured Span - Zero Drift

Percent Drift = (Final, Actual Span - Initial Span) / Initial Span x 100

SAMPLE HANDLING/LOG-IN

Date 9/19/90 Test Location SWEPI Coalina
101A

	Sample Type	Volume	Comments
1.	24751 <u>5/8</u> <u>FHW</u> <u>#1</u> Meth Sample Test		
2.	24752 <u>5/8</u> <u>FLT</u> <u>#1</u> Meth Sample Test		
3.	24753 <u>5/8</u> <u>80%IPA</u> <u>#1</u> Meth Sample Test		
4.	24754 <u>5/8</u> <u>AMF</u> <u>#1</u> Meth Sample Test		
5.	24755 <u>5/8</u> <u>H₂O₂</u> <u>#1</u> Meth Sample Test		
6.	24756 <u>5/8</u> <u>F4W</u> <u>#2</u> Meth Sample Test		
7.	24757 <u>5/8</u> <u>MF</u> <u>#2</u> Meth Sample Test		
8.	24758 <u>5/8</u> <u>IPA</u> <u>#2</u> Meth Sample Test		
9.	24759 <u>5/8</u> <u>AMF</u> <u>#2</u> Meth Sample Test		
10.	24760 <u>5/8</u> <u>H₂O₂</u> <u>#2</u> Meth Sample Test		
11.	24763 <u>GC</u> <u>HC</u> <u>1</u> Meth Sample Test		
12.	24764 <u>GC</u> <u>HC</u> <u>2</u> Meth Sample Test		

CHAIN OF CUSTODY

one

LW. + yc

SAMPLE HANDLING/LOG-IN

Date 9/20/90

Test Location 5WEPI Coalinga
101 B

		Sample Type	Volume	Comments
1.	24765	<u>5/8 FHW 1</u> Meth Sample Test		
2.	24766	<u>5/8 MF 1</u> Meth Sample Test		
3.	24767	<u>5/8 IPA 1</u> Meth Sample Test		
4.	24768	<u>5/8 AMF 1</u> Meth Sample Test		
5.	24769	<u>5/8 H2O2 1</u> Meth Sample Test		
6.	24770	<u>GC HC 1</u> Meth Sample Test		
7.	24771	<u>5/8 FHW 2</u> Meth Sample Test		
8.	24772	<u>5/8 MF 2</u> Meth Sample Test		
9.	24773	<u>5/8 IPA 2</u> Meth Sample Test		
10.	24774	<u>5/8 AMF 2</u> Meth Sample Test		
11.	24775	<u>5/8 H2O2 2</u> Meth Sample Test		
12.	24776	<u>GC HC 2</u> Meth Sample Test		

CHAIN OF CUSTODY

GM

LW & YC

SAMPLE HANDLING/LOG-IN

Date 9-20-90

Test Location SWEDI Coalingo
101A, 101B

	Sample Type	Volume	Comments
1.	24777 <u>H₂S</u> All Meth <u>Blank</u> Sample Test		
2.	24778 <u>H₂S</u> All Meth <u>Blank</u> Sample Test		
3.	24245 <u>516 FAW</u> All Meth <u>Blank</u> Sample Test		
4.	24246 <u>516 MF</u> All Meth <u>Blank</u> Sample Test		
5.	24247 <u>516 IPA</u> All Meth <u>Blank</u> Sample Test		
6.	24248 <u>516 AMF</u> All Meth <u>Blank</u> Sample Test		
7.	24249 <u>516 H₂O₂</u> All Meth <u>Blank</u> Sample Test		
8.			
9.			
10.			
11.			
12.			

CHAIN OF CUSTODY

WU

LW & YC

SAMPLE HANDLING/LOG-IN

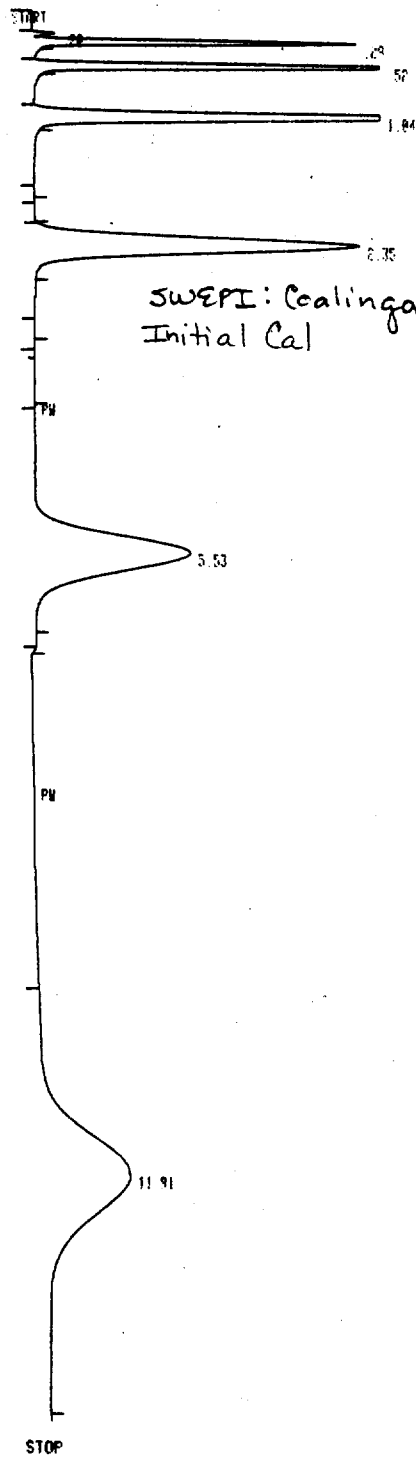
Date 9/19-20/90

Test Location SWEDI Coalinga
101A 101B

	Sample Type	Volume	Comments
1.	24761 <u>FG</u> <u>ALL</u> Meth Sample Test		
2.	24762 <u>FG</u> <u>ALL</u> Meth Sample Test		
3.			
4.			
5.			
6.			
7.			
8.			
9.			
10.			
11.			
12.			

CHAIN OF CUSTODY

Jim



Initial Cal → calibrated

RUN # 1 SEP/21/90 07:55:09

ESTD	RT	AREA	TYPE	CAL#	AMOUNT
	0.20	254	PV	2	1.000
	0.29	4611	VB	IR	21.190
	0.52	9505	PB		43.680
	1.04	14890	PB		68.427
	2.35	20344	BB		93.491
	5.53	23106	BB		106.550
	11.91	30515	PR		140.230

TOTAL AREA= 103310
MUL FACTOR= 1.0000E+00

Initial Cal → % Area

RUN # 1 SEP/21/90 07:55:09

AREAX	RT	AREA	TYPE	AR/HT	AREAX
	0.20	254	PV	0.033	0.246
	0.29	4611	VB	0.042	4.464
	0.52	9505	PB	0.045	9.201
	1.04	14890	PB	0.080	14.414
	2.35	20344	BB	0.180	19.693
	5.53	23106	BB	0.431	22.444
	11.91	30515	PR	1.019	29.539

TOTAL AREA= 103310
MUL FACTOR= 1.0000E+00



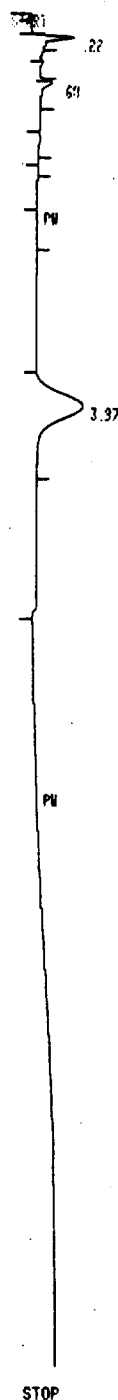
SWEPI: Coalinga
9/19/90
Unit 101A
Test 1a

RUN # 15
ID 24763-1a

SEP/21/90 13:48:17

ESTD	RT	AREA	TYPE	CAL#	AMOUNT
	0.18	722	PV	2	2.843
	0.64	381	BB		1.751
	3.93	5040	PB		23.161

TOTAL AREA= 6143
MUL FACTOR= 1.0000E+00



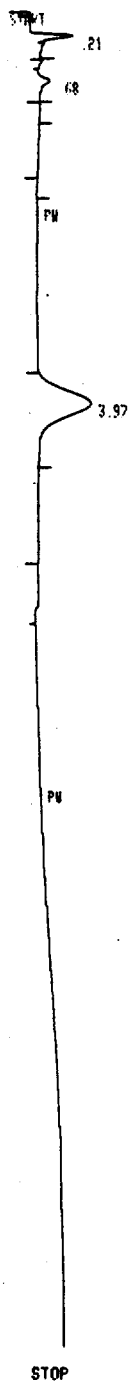
SWEPI: Coalinga
9/19/90
Unit 101A
Test 1b
(duplicate)

RUN # 16
ID 24763-1b
NO CALIB PEAKS FOUND

SEP/21/90 14:11:56

AREA2	RT	AREA	TYPE	AR/WT	AREA2	PPM
	0.22	784	PB	0.057	13.028	8.663
	0.68	169	BB	0.049	2.888	0.777
	3.97	5065	BB	0.310	84.164	28.276

TOTAL AREA= 6018
MUL FACTOR= 1.0000E+00



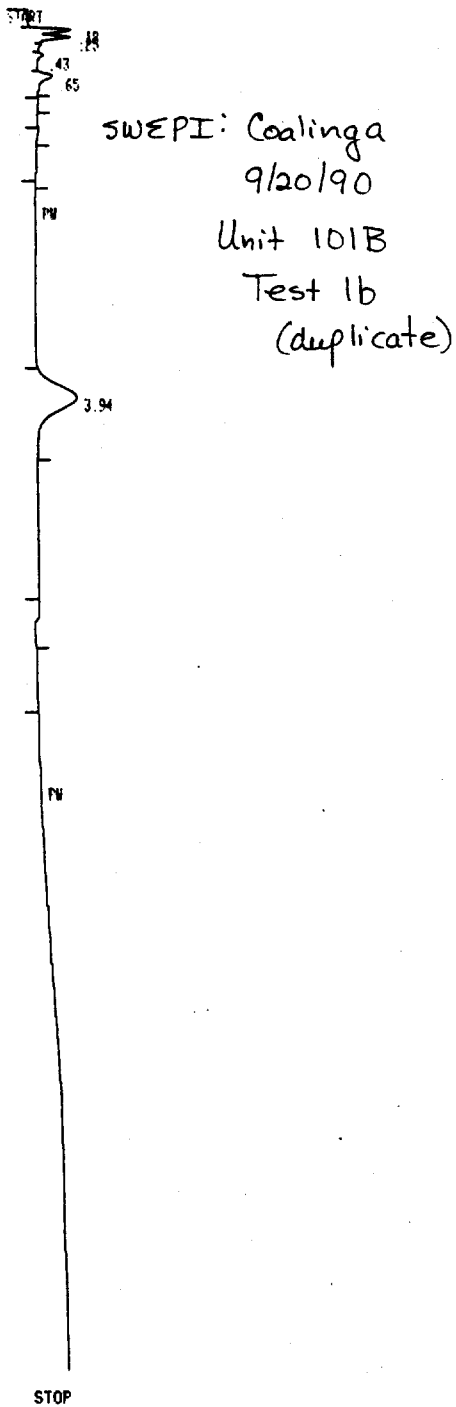
SWEPI: Coalinga
 9/19/90
 Unit 101A
 Test 2

RUN # 17
 ID 24764-2

SEP/21/90 14:35:39

ESTD	RT	AREA	TYPE	CAL#	AMOUNT
	0.21	522	PV	2	2.855
	0.68	326	PB		1.498
	3.97	5665	BR		26.833

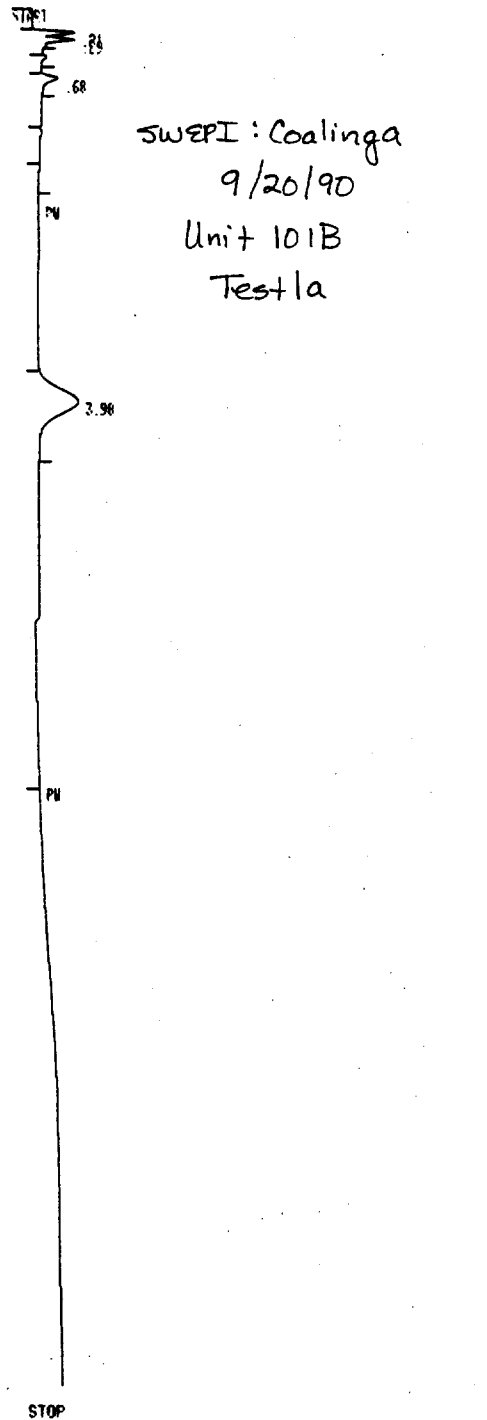
TOTAL AREA= 6513
 MUL FACTOR= 1.00000000



RUN # 19 SEP/21/90 15:25:51
ID 24770-1b

ESTD	RT	AREA	TYPE	CAL#	AMOUNT
	0.18	686	BV	2	2.701
	0.25	787	VV	1R	3.249 C ₁
	0.43	363	VV		1.668
	0.65	544	V8		2.500 } > C ₁
	3.94	4292	BB		19.724

TOTAL AREA= 6592
MUL FACTOR= 1.0000E+00



RUN # 18 SEP/21/90 14:59:46
ID 24770-1a

ESTD	RT	AREA	TYPE	CAL#	AMOUNT
	0.21	644	PV	2	2.535
	0.29	578	V8	1R	2.656 C ₁
	0.68	451	P8		2.073
	3.98	4328	BB		19.889 } > C ₁

TOTAL AREA= 6001
MUL FACTOR= 1.0000E+00



SWEPI: Coalinga
Unit 101B
9/20/90
Test 2

RUN # 20
ID 24776-2

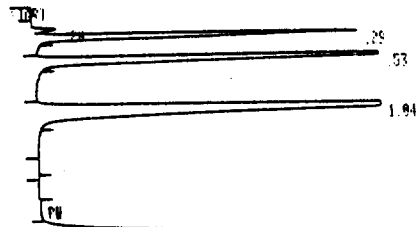
SEP/21/90 15:49:43

ESTD

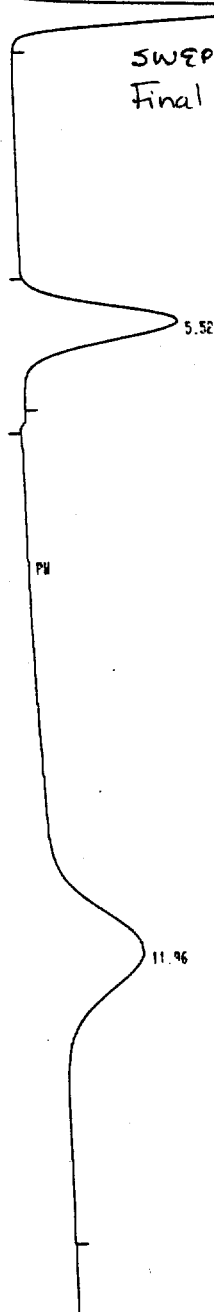
RT	AREA	TYPE	CAL#	AMOUNT
0.21	623	PV	2	2.453
0.28	512	VB	1R	2.353 c,
0.67	443	BB		2.036
3.97	3396	BB		15.686 } > c,

TOTAL AREA= 4974
MUL FACTOR= 1.0000E+00

DELETE ID



SWEEP: Coalinga 9/19-20/90
Final Cal



STOP

Final Cal

RUN # 21

SEP/21/90 16:18:58

ESTD	RT	AREA	TYPE	CAL#	AMOUNT
	0.29	198	PV	2	0.780
	0.29	4603	VB	1R	21.153
	0.53	9600	PB		44.117
	1.04	15006	PB		69.328
	2.35	20244	BB		93.031
	5.52	23258	BB		106.088
	11.96	28082	PD		132.730

TOTAL AREA= 101870
MR FACTOR= 1.000000

ANALYTICAL REPORT

SAMPLE TYPE : FHW ANALYSIS (g) DATE : 9/28/90
 SAMPLING METHOD : M5/8
 SAMPLE COMPONENT : ACETONE ANALYST : LW & YC
 REQUESTED BY : SWEPI COALINGA, 101A, 9/19/90
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Sample Volume (ml)	Analytical Result (total sample)	
		Uncorrected	Blank Corr. (g)
1	140	0.01395	0.01342
2	160	0.00990	0.00929
Blank	100	0.00038	

ANALYTICAL REPORT

SAMPLE TYPE : FILTERABLE PARTICULATE DATE : 9/28/90
 SAMPLING METHOD : M5/8
 SAMPLE COMPONENT : 100 mm FILTER ANALYST : LW & YC
 REQUESTED BY : SWEPI COALINGA, 101A, 9/19/90
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Filter No.	Analytical Result (total sample)	
		Uncorrected	Blank Corr. (g)
1	77	-0.00122	-0.00104
2	78	-0.00102	-0.00084
Blank	116	-0.00018	

ANALYTICAL REPORT

SAMPLE TYPE : CONDENSIBLE PARTICULATE DATE : 9/28/90
 SAMPLING METHOD : M5/8
 SAMPLE COMPONENT : 80% IPA + Amf ANALYST :
 REQUESTED BY : SWEPI COALINGA, 101A, 9/19/90
 ANALYTICAL METHOD : GRAVIMETRIC

		Test No.	Sample Volume	Analytical Result (total sample)	
				Uncorrected	Blank Corr. (g)
		1	350	0.00951	0.00834
		2	270	0.00319	0.00207
IPA	Blank		100	0.00006	
AMF	Blank		100	0.00087	
DI	Blank		100	-0.00009	

ANALYTICAL REPORT

SAMPLE TYPE : FILTERABLE SO4 DATE : 9/28/90
 SAMPLING METHOD : M5/8
 SAMPLE COMPONENT : FHW + MF ANALYST : LW & YC
 REQUESTED BY : SWEPI COALINGA, 101A, 9/19/90
 ANALYTICAL METHOD : BaCl2 Titration

Test No.	Sample Volume	Sample Aliquot	TITER mls or (Absorbance)	Analyt. Result (total sample) mg H2SO4
1	100	10	0.30	0.37
2	100	10	0.29	0.33
Blank	100	10	0.22	1.03

% Duplicate = 100.0 RUN NO. 1

% Recovery = 99.2 RUN NO. 2

% CONFIDENCE = 100.1 EPA SO2 LOT 0586 6XXX
 NORMALITY = 0.009560229

ANALYTICAL REPORT

SAMPLE TYPE : CONDENSIBLE SULFATE DATE : 9/28/90
 SAMPLING METHOD : M5/8
 SAMPLE COMPONENT : BHW + AMF ANALYST : LW & YC
 REQUESTED BY : SWEPI COALINGA, 101A, 9/19/90
 ANALYTICAL METHOD : BaCL2 Titration

Test No.	Sample Volume	Sample Aliquot	TITER mls or (Absorbance)	Analyt. Result (total sample) mg H2SO4
1	100	10	0.16	0.47
2	100	10	0.27	0.98
IPA Blank	100	10	0.06	0.28
AMF Blank	100	10	0.05	0.23
DI Blank	100	10	0.05	0.23

% Duplicate = 100.0 RUN NO. 1

% Recovery = 99.8 RUN NO. 2

% CONFIDENCE = 100.1 EPA SO2 LOT 0586 6XXX

NORMALITY = 0.009560229

ANALYTICAL REPORT

SAMPLE TYPE :SO2
 SAMPLING METHOD :M5/8
 SAMPLE COMPONENT :3% H2O2
 REQUESTED BY :SWEPI COALINGA, 101A, 9/19/90
 ANALYTICAL METHOD :BaCL2 Titration

DATE : 9/28/90
 ANALYST : LW & YC

Test No.	Sample Volume	Sample Aliquot	TITER mls or (Absorbance)	Analyt. Result (total sample) mg H2SO4
1	360	10	0.17	2.88
2	290	10	0.16	2.18
Blank			0.00	0.00

% Duplicate = 100.0 RUN NO. 1

% Recovery = 98.2 RUN NO. 2

% CONFIDENCE = 100.1 EPA SO2 LOT 0586 6XXX
 NORMALITY = 0.009606148

A N A L Y T I C A L R E P O R T

SAMPLE TYPE : FHW ANALYSIS (g) DATE : 9/28/90
 SAMPLING METHOD : M5/8
 SAMPLE COMPONENT : ACETONE ANALYST : LW & YC
 REQUESTED BY : SWEPI COALINGA, 101B, 9/20/90
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Sample Volume (ml)	Analytical Result (total sample)	
		Uncorrected	Blank Corr. (g)
1	150	0.00881	0.00824
2	200	0.00639	0.00563
Blank	100	0.00038	

ANALYTICAL REPORT

SAMPLE TYPE : FILTERABLE PARTICULATE DATE : 9/28/90
 SAMPLING METHOD : M5/8
 SAMPLE COMPONENT : 100 mm FILTER ANALYST : LW & YC
 REQUESTED BY : SWEPI COALINGA, 101B, 9/20/90
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Filter No.	Analytical Result (total sample)	
		Uncorrected	Blank Corr. (g)
1	79	-0.00078	-0.00060
2	80	-0.00044	-0.00026
Blank	116	-0.00018	

ANALYTICAL REPORT

SAMPLE TYPE : CONDENSIBLE PARTICULATE DATE : 9/28/90
 SAMPLING METHOD : M5/8
 SAMPLE COMPONENT : 80% IPA + Amf ANALYST :
 REQUESTED BY : SWEPI COALINGA, 101B, 9/20/90
 ANALYTICAL METHOD : GRAVIMETRIC

		Test No.	Sample Volume	Analytical Result (total sample)	
				Uncorrected	Blank Corr. (g)
		1	300	0.00201	0.00087
		2	290	0.00308	0.00195
IPA	Blank		100	0.00006	
AMF	Blank		100	0.00087	
DI	Blank		100	-0.00009	

ANALYTICAL REPORT

SAMPLE TYPE : FILTERABLE SO4 DATE : 9/28/90
 SAMPLING METHOD : M5/8
 SAMPLE COMPONENT : FHW + MF ANALYST : LW & YC
 REQUESTED BY : SWEPI COALINGA, 101B, 9/20/90
 ANALYTICAL METHOD : BaCl2 Titration

Test No.	Sample Volume	Sample Aliquot	TITER mls or (Absorbance)	Analyt. Result (total sample) mg H2SO4
1	100	10	0.26	0.19
2	100	10	0.25	0.14

Blank	100	10	0.22	1.03
-------	-----	----	------	------

% Duplicate = 100.0 RUN NO. 1

% Recovery = 100.0 RUN NO. 2

% CONFIDENCE = 100.1 EPA SO2 LOT 0586 6XXX
 NORMALITY = 0.009560229

ANALYTICAL REPORT

SAMPLE TYPE : CONDENSIBLE SULFATE DATE : 9/28/90
 SAMPLING METHOD : M5/8
 SAMPLE COMPONENT : BHW + AMF ANALYST : LW & YC
 REQUESTED BY : SWEPI COALINGA, 101B, 9/20/90
 ANALYTICAL METHOD : BaCL2 Titration

Test No.	Sample Volume	Sample Aliquot	TITER mls or (Absorbance)	Analyt. Result (total sample) mg H2SO4
1	100	10	0.15	0.42
2	100	10	0.21	0.70
IPA Blank	100	10	0.06	0.28
AMF Blank	100	10	0.05	0.23
DI Blank	100	10	0.05	0.23

% Duplicate = 100.0 RUN NO. 1

% Recovery = 99.8 RUN NO. 2

% CONFIDENCE = 100.1 EPA SO2 LOT 0586 6XXX

NORMALITY = 0.009560229

ANALYTICAL REPORT

SAMPLE TYPE : SO2
 SAMPLING METHOD : M5/8
 SAMPLE COMPONENT : 3% H2O2
 REQUESTED BY : SWEPI COALINGA, 101B, 9/20/90
 ANALYTICAL METHOD : BaCL2 Titration

DATE : 9/28/90
 ANALYST : LW & YC

Test No.	Sample Volume	Sample Aliquot	TITER mls or (Absorbance)	Analyt. Result (total sample) mg H2SO4
1	340	10	0.16	2.56
2	300	10	0.16	2.26
Blank			0.00	0.00

% Duplicate = 100.0 RUN NO. 1

% Recovery = 100.7 RUN NO. 2

% CONFIDENCE = 100.1 EPA SO2 LOT 0586 6XXX
 NORMALITY = 0.009606148

ANALYTICAL REPORT

SAMPLE TYPE Method 11 H₂S

DATE 9/26/90

SAMPLE COMPONENT CdSO₄ Abs. Solution

ANALYST SW.

REQUESTED BY SWPFI: Coalings 9/19-20/90

ANALYTICAL METHOD H₂S: I₂ Addition w/ Na₂S₂O₃ titration

Sample ID No.	Test No.	Sample Volume	mL I ₂ Added	Titer mLs	Sample Color	Normality of Iodine
	I	95	35	1.80	very pale yellow	$\frac{(2.225)(.01)}{25} = .00089$
	BI	95	35	2.50	clear	

SOURCE TEST CALCULATIONS

PLANT : SWEPI COALINGA
HRS 101A

RUN NO.: 1
DATE : SEPT 19, 1990

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	98.38 DEG. F	STATIC PRESS.	=	-0.30 in. H2O
STACK TEMP.	=	242.89 DEG. F	Cp	=	0.840
SQ.RT. dP	=	0.6136 in. H2O	STACK I.D.	=	inch
METER ORIFICE	=	2.26 in. H2O	DUCT LENGTH	=	47.5 inch
METER VOLUME	=	122.866 Cu.Ft.	DUCT WIDTH	=	47.5 inch
METER Y	=	1.0132	STACK AREA	=	15.668 Sq.Ft.
BAR. PRESSURE	=	28.59 in.Hg	TEST TIME	=	140.00 min.
COND. (Vlc)	=	226.0 ml	NOZZLE DIA.	=	0.3020 inch

GAS ANALYSIS	=	14.97 % O2	0.00 % CO
		3.37 % CO2	81.66 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times$
 $(Pb + (dH / 13.6)) / (Tm + 460) \dots\dots = 111.422 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic = 10.477 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots = 0.086$ | Lower
| Bws

Bws @ Saturated Conditions = Vapor Press. of H2O
@ Dew Point Temp. / (Ps, in.Hg.) $\dots\dots\dots = 1.000$ | value
| used.

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = 227.22$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)] = 29.14$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots\dots\dots = 28.18$

$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots = 28.57 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots\dots\dots = 41.17 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots\dots\dots = 38,707 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots\dots\dots = 24,991 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 100.31 \%$

SOURCE TEST CALCULATIONS

PLANT : SWEPI COALINGA
HRSG 101A

RUN NO.: 2
DATE : SEPT 19, 1990

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	107.02 DEG. F	STATIC PRESS.=	-0.30 in. H2O
STACK TEMP.	=	241.39 DEG. F	Cp	= 0.840
SQ.RT. dP	=	0.6174 in. H2O	STACK I.D.	= inch
METER ORIFICE	=	2.33 in. H2O	DUCT LENGTH	= 47.5 inch
METER VOLUME	=	125.674 Cu.Ft.	DUCT WIDTH	= 47.5 inch
METER Y	=	1.0132	STACK AREA	= 15.668 Sq.Ft.
BAR. PRESSURE	=	28.51 in.Hg	TEST TIME	= 140.00 min.
COND.(Vlc)	=	231.3 ml	NOZZLE DIA.	= 0.3020 inch

GAS ANALYSIS	:	14.41 % O2	0.00 % CO
		3.38 % CO2	82.21 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times (Pb + (dH / 13.6)) / (Tm + 460) \dots\dots = 111.939 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic = 10.722 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots = 0.087$ | Lower Bws

Bws @ Saturated Conditions = Vapor Press. of H2O
@ Dew Point Temp. / (Ps, in.Hg.) $\dots\dots\dots = 1.000$ | value used.

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = 197.57$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)] = 29.12$

$Ms = (Md \times (1-Bws)) + (18.0 \times Bws) \dots\dots\dots = 28.15$

$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots = 28.49 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots\dots\dots = 41.47 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots\dots\dots = 38,984 \text{ acf/min}$

$Qs(std) = Qs \times (1-Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots\dots\dots = 25,113 \text{ dscf/min}$

$I = (Ts+460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 100.29 \%$

SOURCE TEST CALCULATIONS

PLANT : SWEPI COALINGA
HRSGL01B

RUN NO.: 1
DATE : SEPT 20, 1990

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	105.98 DEG. F	STATIC PRESS.=	-0.23 in. H2O
STACK TEMP.	=	239.93 DEG. F	Cp	= 0.840
SQ.RT. dP	=	0.6155 in. H2O	STACK I.D.	= inch
METER ORIFICE	=	2.31 in. H2O	DUCT LENGTH	= 47.5 inch
METER VOLUME	=	124.804 Cu.Ft.	DUCT WIDTH	= 47.5 inch
METER Y	=	1.0132	STACK AREA	= 15.668 Sq.Ft.
BAR. PRESSURE	=	28.49 in.Hg	TEST TIME	= 140.00 min.
COND. (Vlc)	=	236.9 ml	NOZZLE DIA.	= 0.3020 inch
GAS ANALYSIS	=	14.38 % O2	0.00 % CO	
		3.45 % CO2	82.17 % N2	

$$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times (Pb + (dH / 13.6)) / (Tm + 460) \dots = 111.285 \text{ dscf}$$

$$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic = 10.982 \text{ scf}$$

$$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots = 0.090 \text{ | Lower Bws value used.}$$

$$Bws @ \text{ Saturated Conditions} = \text{Vapor Press. of H2O @ Dew Point Temp. / (Ps, in.Hg.)} \dots = 1.000$$

$$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = 196.64$$

$$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)] = 29.13$$

$$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots = 28.13$$

$$P(stack) = Pbar + [Pstatic / 13.6] \dots = 28.47 \text{ in. Hg}$$

$$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots = 41.32 \text{ ft/sec}$$

$$Qs = vs \times As \times 60 \dots = 38,846 \text{ acf/min}$$

$$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots = 24,997 \text{ dscf/min}$$

$$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 100.17 \%$$

SOURCE TEST CALCULATIONS

PLANT : SWEPI COALINGA
HRS G101B

RUN NO.: 2
DATE : SEPT 20, 1990

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	112.07 DEG. F	STATIC PRESS.	=	-0.35 in. H2O
STACK TEMP.	=	235.82 DEG. F	Cp	=	0.840
SQ. RT. dP	=	0.6158 in. H2O	STACK I.D.	=	inch
METER ORIFICE	=	2.35 in. H2O	DUCT LENGTH	=	47.5 inch
METER VOLUME	=	126.311 Cu.Ft.	DUCT WIDTH	=	47.5 inch
METER Y	=	1.0132	STACK AREA	=	15.668 Sq.Ft.
BAR. PRESSURE	=	28.47 in.Hg	TEST TIME	=	140.00 min.
COND. (Vlc)	=	242.5 ml	NOZZLE DIA.	=	0.3020 inch

GAS ANALYSIS	:	14.47 % O2	0.00 % CO
		3.23 % CO2	82.30 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times$ $(Pb + (dH / 13.6)) / (Tm + 460) \dots\dots$	=	111.364	dscf
$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic$	=	11.242	scf
$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots$	=	0.092	Lower Bws value used.
$Bws @ \text{Saturated Conditions} = \text{Vapor Press. of H2O}$ $@ \text{Dew Point Temp.} / (Ps, \text{ in.Hg.}) \dots\dots\dots$	=	1.000	
$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100$	=	199.39	
$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)]$	=	29.10	
$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots\dots\dots$	=	28.08	
$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots$	=	28.44 in. Hg	
$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460)$ $/ (Ms \times Ps)] \dots\dots\dots$	=	41.28	ft/sec
$Qs = vs \times As \times 60 \dots\dots\dots$	=	38,804	acf/min
$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460))$ $\times (Ps / 29.92) \dots\dots\dots$	=	25,041	dscf/min
$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60)$	=	100.06	%

EMISSION RATE CALCULATIONS

PLANT :SWEPI COALINGA
HRSG 101A

RUN NO.: 1
DATE : SEPT 19,1990
O2 CORR.: 15.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.01342 grams | Vm(std) 111.422 ft3
Mass Filter (MF)           0.00000 grams | Vw(std)  10.477 ft3
Back Half Wash (BHW)      0.00834 grams | Qs(std) 24,991 dscfm
Front Half Sulfate (FHS)   0.37 mg H2SO4 | Bws      0.086
Back Half Sulfate (BHS)   0.47 mg H2SO4 | CO2      3.37 %
H2O2 Catch (SO2)          2.88 mg H2SO4 | O2       14.97 %
*****
```

F-FACTOR

10E6 x [3.64(%H) + 1.53(%C) + 0.57(%S) + 0.14(%N) -
0.46(%O2)] / (Btu/lb) x [(Tstd + 460)/528] 8480.67 dscf/MMBtu

FILTERABLE PARTICULATE

```
-----
15.432 x (FHW + MF) / [Vm(std) + Vw(std)] ..... 0.0017 gr/scf
15.432 x (FHW + MF) / Vm(std) ..... 0.0019 gr/dscf
gr/dscf x (12 / %CO2) ..... 0.0066 @ 12% CO2
0.00857 x Qs(std) x gr/dscf ..... 0.40 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0079 lb/MMBtu
```

TOTAL PARTICULATE

```
-----
15.432 x (FHW + MF + BHW) / [(Vm(std) + Vw(std))] ... 0.0028 gr/scf
15.432 x (FHW + MF + BHW) / Vm(std) ..... 0.0030 gr/dscf
gr/dscf x (12 / %CO2) ..... 0.0107 @ 12% CO2
0.00857 x Qs(std) x gr/dscf ..... 0.65 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0129 lb/MMBtu
```

TOTAL SULFATE

```
-----
0.015432 x (FHS + BHS) / [Vm(std) + Vw(std)] ..... 0.0001 gr/scf
0.015432 x (FHS + BHS) / Vm(std) ..... 0.0001 gr/dscf
gr/dscf x (12 / %CO2) ..... 0.0004 @ 12% CO2
0.00857 x Qs(std) x gr/dscf ..... 0.02 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0005 lb/MMBtu
```

SULFUR DIOXIDE (SO2)

```
-----
1.60982 x [T(std) + 460] x (mg H2SO4) / [ 98.076 x  
Vm(std)] ..... 0.22 ppm
ppm x [(20.9 - Oxygen Corr.) / (20.9 - %O2)] ..... 0.22 @ O2 corr.
ppm x (1 - Bws) ..... 0.20 ppm (wet)
8.223E-5 x Qs(std) x 64.062 x ppm / [T(std) + 460].. 0.06 lb/hr
F-Factor x 64.062 x [1.3711E-6 / [T(std)+ 460]] x  
[20.9 / (20.9 - %O2)] x ppm ..... 0.0011 lb/MMBtu
lb/hr / (dscfm x 60 min/hr) ..... 3.72E-08 lb/dscf
```

SULFUR (S)

```
(lb/MMBtu SO2) / 2 ..... 0.0006 lb/MMBtu
(lb/MMBtu Total Sulfate) x (32 / 98.076) ..... 0.0002 lb/MMBtu
Total Sulfur ..... 0.0007 lb/MMBtu
```

EMISSION RATE CALCULATIONS

PLANT :SWEPI COALINGA
HRS 101A

RUN NO.: 2
DATE : SEPT 19, 1990
O2 CORR.: 15.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.00929 grams      | Vm(std) 111.939 ft3
Mass Filter (MF)           0.00000 grams      | Vw(std)  10.722 ft3
Back Half Wash (BHW)       0.00207 grams      | Qs(std)  25,113 dscfm
Front Half Sulfate (FHS)    0.33 mg H2SO4     | Bws       0.087
Back Half Sulfate (BHS)     0.98 mg H2SO4     | CO2       3.38 %
H2O2 Catch (SO2)           2.18 mg H2SO4     | O2        14.41 %
*****
```

F-FACTOR

$10E6 \times [3.64(\%H) + 1.53(\%C) + 0.57(\%S) + 0.14(\%N) - 0.46(\%O_2)] / (Btu/lb) \times [(Tstd + 460)/528] \dots\dots\dots 8480.67 \text{ dscf/MMBtu}$

FILTERABLE PARTICULATE

```
15.432 x (FHW + MF) / [Vm(std) + Vw(std)] ..... 0.0012 gr/scf
15.432 x (FHW + MF) / Vm(std) ..... 0.0013 gr/dscf
gr/dscf x (12 / %CO2) ..... 0.0045 @ 12% CO2
0.00857 x Qs(std) x gr/dscf ..... 0.28 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0050 lb/MMBtu
```

TOTAL PARTICULATE

```
15.432 x (FHW + MF + BHW) / [(Vm(std) + Vw(std))] ... 0.0014 gr/scf
15.432 x (FHW + MF + BHW) / Vm(std) ..... 0.0016 gr/dscf
gr/dscf x (12 / %CO2) ..... 0.0056 @ 12% CO2
0.00857 x Qs(std) x gr/dscf ..... 0.34 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0061 lb/MMBtu
```

TOTAL SULFATE

```
0.015432 x (FHS + BHS) / [Vm(std) + Vw(std)] ..... 0.0002 gr/scf
0.015432 x (FHS + BHS) / Vm(std) ..... 0.0002 gr/dscf
gr/dscf x (12 / %CO2) ..... 0.0006 @ 12% CO2
0.00857 x Qs(std) x gr/dscf ..... 0.04 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0007 lb/MMBtu
```

SULFUR DIOXIDE (SO2)

```
1.60982 x [T(std) + 460] x (mg H2SO4) / [ 98.076 x
Vm(std)] ..... 0.17 ppm
ppm x [(20.9 - Oxygen Corr.) / (20.9 - %O2)] ..... 0.15 @ O2 corr.
ppm x (1 - Bws) ..... 0.15 ppm (wet)
8.223E-5 x Qs(std) x 64.062 x ppm / [T(std) + 460].. 0.04 lb/hr
F-Factor x 64.062 x [1.3711E-6 / [T(std)+ 460]] x
[20.9 / (20.9 - %O2)] x ppm ..... 0.0008 lb/MMBtu
lb/hr / (dscfm x 60 min/hr) ..... 2.81E-08 lb/dscf
```

SULFUR (S)

```
(lb/MMBtu SO2) / 2 ..... 0.0004 lb/MMBtu
(lb/MMBtu Total Sulfate) x (32 / 98.076) ..... 0.0002 lb/MMBtu
Total Sulfur ..... 0.0006 lb/MMBtu
```

EMISSION RATE CALCULATIONS

PLANT :SWEPI COALINGA
HRSGL01B

RUN NO.: 1
DATE : SEPT 20,1990
O2 CORR.: 15.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.00824 grams      | Vm(std) 111.285 ft3
Mass Filter (MF)           0.00000 grams      | Vw(std)  10.982 ft3
Back Half Wash (BHW)       0.00087 grams      | Qs(std) 24,997 dscfm
Front Half Sulfate (FHS)    0.19 mg H2SO4    | Bws      0.090
Back Half Sulfate (BHS)    0.42 mg H2SO4    | CO2      3.45 %
H2O2 Catch (SO2)          2.56 mg H2SO4    | O2       14.38 %
*****
```

F-FACTOR

10E6 x [3.64(%H) + 1.53(%C) + 0.57(%S) + 0.14(%N) -
0.46(%O2)] / (Btu/lb) x [(Tstd + 460)/528] 8470.27 dscf/MMBtu

FILTERABLE PARTICULATE

15.432 x (FHW + MF) / [Vm(std) + Vw(std)] 0.0010 gr/scf
15.432 x (FHW + MF) / Vm(std) 0.0011 gr/dscf
gr/dscf x (12 / %CO2) 0.0040 @ 12% CO2
0.00857 x Qs(std) x gr/dscf 0.24 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0044 lb/MMBtu

TOTAL PARTICULATE

15.432 x (FHW + MF + BHW) / [(Vm(std) + Vw(std))] ... 0.0011 gr/scf
15.432 x (FHW + MF + BHW) / (Vm(std) 0.0013 gr/dscf
gr/dscf x (12 / %CO2) 0.0044 @ 12% CO2
0.00857 x Qs(std) x gr/dscf 0.27 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0049 lb/MMBtu

TOTAL SULFATE

0.015432 x (FHS + BHS) / [Vm(std) + Vw(std)] 0.0001 gr/scf
0.015432 x (FHS + BHS) / Vm(std) 0.0001 gr/dscf
gr/dscf x (12 / %CO2) 0.0003 @ 12% CO2
0.00857 x Qs(std) x gr/dscf 0.02 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0003 lb/MMBtu

SULFUR DIOXIDE (SO2)

1.60982 x [T(std) + 460] x (mg H2SO4) / [98.076 x
Vm(std)] 0.20 ppm
ppm x [(20.9 - Oxygen Corr.) / (20.9 - %O2)] 0.18 @ O2 corr.
ppm x (1 - Bws) 0.18 ppm (wet)
8.223E-5 x Qs(std) x 64.062 x ppm / [T(std) + 460].. 0.05 lb/hr
F-Factor x 64.062 x [1.3711E-6 / [T(std)+ 460]] x
[20.9 / (20.9 - %O2)] x ppm 0.0009 lb/MMBtu
lb/hr / (dscfm x 60 min/hr) 3.32E-08 lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 0.0005 lb/MMBtu
(lb/MMBtu Total Sulfate) x (32 / 98.076) 0.0001 lb/MMBtu
Total Sulfur 0.0006 lb/MMBtu

EMISSION RATE CALCULATIONS

PLANT :SWEPI COALINGA
HRSGL01B

RUN NO.: 2
DATE : SEPT 20,1990
O2 CORR.: 15.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.00563 grams   | Vm(std) 111.364 ft3
Mass Filter (MF)           0.00000 grams   | Vw(std)  11.242 ft3
Back Half Wash (BHW)       0.00195 grams   | Qs(std) 25,041 dscfm
Front Half Sulfate (FHS)    0.14 mg H2SO4  | Bws      0.092
Back Half Sulfate (BHS)     0.70 mg H2SO4  | CO2      3.23 %
H2O2 Catch (SO2)           2.26 mg H2SO4  | O2       14.47 %
*****
```

F-FACTOR

10E6 x [3.64(%H) + 1.53(%C) + 0.57(%S) + 0.14(%N) -
0.46(%O2)] / (Btu/lb) x [(Tstd + 460)/528] 8470.27 dscf/MMBtu

FILTERABLE PARTICULATE

```
15.432 x (FHW + MF) / [Vm(std) + Vw(std)] ..... 0.0007 gr/scf
15.432 x (FHW + MF) / Vm(std) ..... 0.0008 gr/dscf
gr/dscf x (12 / %CO2) ..... 0.0029 @ 12% CO2
0.00857 x Qs(std) x gr/dscf ..... 0.17 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0031 lb/MMBtu
```

TOTAL PARTICULATE

```
15.432 x (FHW + MF + BHW) / [(Vm(std) + Vw(std))] ... 0.0010 gr/scf
15.432 x (FHW + MF + BHW) / (Vm(std) ..... 0.0011 gr/dscf
gr/dscf x (12 / %CO2) ..... 0.0039 @ 12% CO2
0.00857 x Qs(std) x gr/dscf ..... 0.23 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0041 lb/MMBtu
```

TOTAL SULFATE

```
0.015432 x (FHS + BHS) / [Vm(std) + Vw(std)] ..... 0.0001 gr/scf
0.015432 x (FHS + BHS) / Vm(std) ..... 0.0001 gr/dscf
gr/dscf x (12 / %CO2) ..... 0.0004 @ 12% CO2
0.00857 x Qs(std) x gr/dscf ..... 0.02 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. 0.0005 lb/MMBtu
```

SULFUR DIOXIDE (SO2)

```
1.60982 x [T(std) + 460] x (mg H2SO4) / [ 98.076 x
Vm(std)] ..... 0.17 ppm
ppm x [(20.9 - Oxygen Corr.) / (20.9 - %O2)] ..... 0.16 @ O2 corr.
ppm x (1 - Bws) ..... 0.16 ppm (wet)
8.223E-5 x Qs(std) x 64.062 x ppm / [T(std) + 460].. 0.04 lb/hr
F-Factor x 64.062 x [1.3711E-6 / [T(std)+ 460]] x
[20.9 / (20.9 - %O2)] x ppm ..... 0.0008 lb/MMBtu
lb/hr / (dscfm x 60 min/hr) .....2.92E-08 lb/dscf
```

SULFUR (S)

```
(lb/MMBtu SO2) / 2 ..... 0.0004 lb/MMBtu
(lb/MMBtu Total Sulfate) x (32 / 98.076) ..... 0.0001 lb/MMBtu
Total Sulfur ..... 0.0006 lb/MMBtu
```

EMISSION RATE CALCULATIONS

PLANT : SWEPI COALINGA
SOURCE : HRSG 101A

Temp. Std. : 60 dF
Press. Std.: 29.92 in. Hg. 15 % O2 Correction

Run No.	1	2	AVERAGE
Date	9/19/90	9/19/90	
Oxygen (%)	14.97	14.41	14.69
Qs(std), dscfm	24,991	25,113	25,052
NOx, ppm	35.24	33.34	34.29
SO2, ppm			
CO, ppm	3.70	3.37	3.54
HC, ppm	24.91	27.53	26.22
F-Factor	8480.67	8480.67	8480.67

NOx, MW = 46.005			
NOx, lb/hr	6.41	6.09	6.25
NOx, ppm @ O2	35.06	30.31	32.69
NOx, lb/MMBtu	0.1278	0.1105	0.1191

SO2, MW = 64.058
SO2, lb/hr
SO2, ppm @ O2
SO2, lb/MMBtu

CO, MW = 28.010			
CO, lb/hr	0.41	0.37	0.39
CO, ppm @ O2	3.69	3.06	3.37
CO, lb/MMBtu	0.0082	0.0068	0.0075

HC, MW = 16.043			
HC, lb/hr	1.58	1.75	1.67
HC, ppm @ O2	24.79	25.03	24.91
HC, lb/MMBtu	0.0315	0.0318	0.0317

$$* \text{ lb/hr} = 8.223\text{E-}5 \times Qs(\text{std}) \times MW \times \text{ppm} / (T\text{std} + 460)$$

$$* \text{ ppm @ O2} = \text{ppm measured} \times [(20.9 - \text{O2\% correction}) / (20.9 - \text{\%O2 measured})]$$

$$* \text{ lb/MMBtu} = \text{F-Factor} \times MW \times [1.3711\text{E-}6 / (T\text{std} + 460)] \times [20.9 / (20.9 - \text{O2\%})] \times \text{ppm}$$

$$* \text{ lb/Bbl} = (\text{lb/MMBtu}) \times (\text{MMBtu/Bbl})$$

EMISSION RATE CALCULATIONS

PLANT : SWEPI COALINGA
SOURCE : HRSG 101B

Temp. Std. : 60 dF
Press. Std.: 29.92 in. Hg. 15 % O2 Correction

Run No.	1	2	AVERAGE
Date	9/20/90	9/20/90	
Oxygen (%)	14.38	14.47	14.43
Qs(std), dscfm	24,997	25,041	25,019
NOx, ppm	24.54	23.37	23.96
SO2, ppm			
CO, ppm	6.01	7.39	6.70
HC, ppm	21.96	17.64	19.80
F-Factor	8470.27	8470.27	8470.27

NOx, MW = 46.005			
NOx, lb/hr	4.46	4.26	4.36
NOx, ppm @ O2	22.21	21.44	21.83
NOx, lb/MMBtu	0.0808	0.0780	0.0794

SO2, MW = 64.058
SO2, lb/hr
SO2, ppm @ O2
SO2, lb/MMBtu

CO, MW = 28.010			
CO, lb/hr	0.67	0.82	0.74
CO, ppm @ O2	5.44	6.78	6.11
CO, lb/MMBtu	0.0121	0.0150	0.0135

HC, MW = 16.043			
HC, lb/hr	1.39	1.12	1.26
HC, ppm @ O2	19.87	16.19	18.03
HC, lb/MMBtu	0.0252	0.0205	0.0229

$$* \text{ lb/hr} = 8.223\text{E-}5 \times \text{Qs(std)} \times \text{MW} \times \text{ppm} / (\text{Tstd} + 460)$$

$$* \text{ ppm @ O2} = \text{ppm measured} \times [(\text{20.9} - \text{O2\% correction}) / (\text{20.9} - \text{\%O2 measured})]$$

$$* \text{ lb/MMBtu} = \text{F-Factor} \times \text{MW} \times [1.3711\text{E-}6 / (\text{Tstd} + 460)] \times [\text{20.9} / (\text{20.9} - \text{O2\%})] \times \text{ppm}$$

$$* \text{ lb/Bbl} = (\text{lb/MMBtu}) \times (\text{MMBtu/Bbl})$$

E. HYDROCARBON DATA
UNIT 101A

CALIBRATIONS

Methane Calibration gas = 21.19 ppm

	Area Count	ppm	
Initial Cal.	4611	21.19	C1
Final Cal. Check	4603	21.15	C1

% cal. diff. = 0.19
ppm/area count = 4.60E-03

SAMPLES

Run. No.		A R E A C O U N T S		p p m	
		1	2	1	2
HC	C1				
HC	>C1	381	326	1.75	1.50
	"	5040	5665	23.16	26.03
	"				
	"				
Total HC	>C1 =	5421	5991	24.91	27.53

Run. No.		l b / h r	
		1	2
HC	C1		
HC	>C1	0.11	0.10
	"	1.47	1.66
	"		
	"		
Total HC	>C1 =	1.58	1.75

E. HYDROCARBON DATA
UNIT 101B

CALIBRATIONS

Methane Calibration gas = 21.19 ppm

	Area Count	ppm	
Initial Cal.	4611	21.19	C1
Final Cal. Check	4603	21.15	C1

% cal. diff. = 0.19
ppm/area count = 4.60E-03

SAMPLES

		A R E A C O U N T S		p p m	
Run. No.		1	2	1	2
HC	C1	578	512		
HC	>C1	451	443	2.07	2.04
	"	4328	3396	19.89	15.61
	"				
	"				
Total HC	>C1 =	4779	3839	21.96	17.64

l b / h r

Run. No.		1	2
HC	C1		
HC	>C1	0.13	0.13
	"	1.26	0.99
	"		
	"		
Total HC	>C1 =	1.39	1.12

H₂S CALCULATIONS AT S_t

(Standard Temperature to be defined)

$$V_{m, std} = \frac{S_t}{29.92} (\gamma) (V_m) \left(\frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right)$$

$$\text{Blank CdSO}_4 = [N_{I_2}(\text{mls } I_2) - N_{Na_2S_2O_3}(\text{mls } Na_2S_2O_3)]$$

$$\text{ppm H}_2\text{S} = \frac{0.8039(S_t + 460) \left([N_{I_2}(\text{mls } I_2) - (N_{Na_2S_2O_3})(\text{mls } Na_2S_2O_3)] - \text{Blank} \right)}{V_{m, std}}$$

$$V_{m, std} = \frac{(60 + 460)}{29.92} (0.9875) (32.331) \left(\frac{28.49 + \frac{0}{13.6}}{94.56 + 460} \right)$$

$$= 28.5064$$

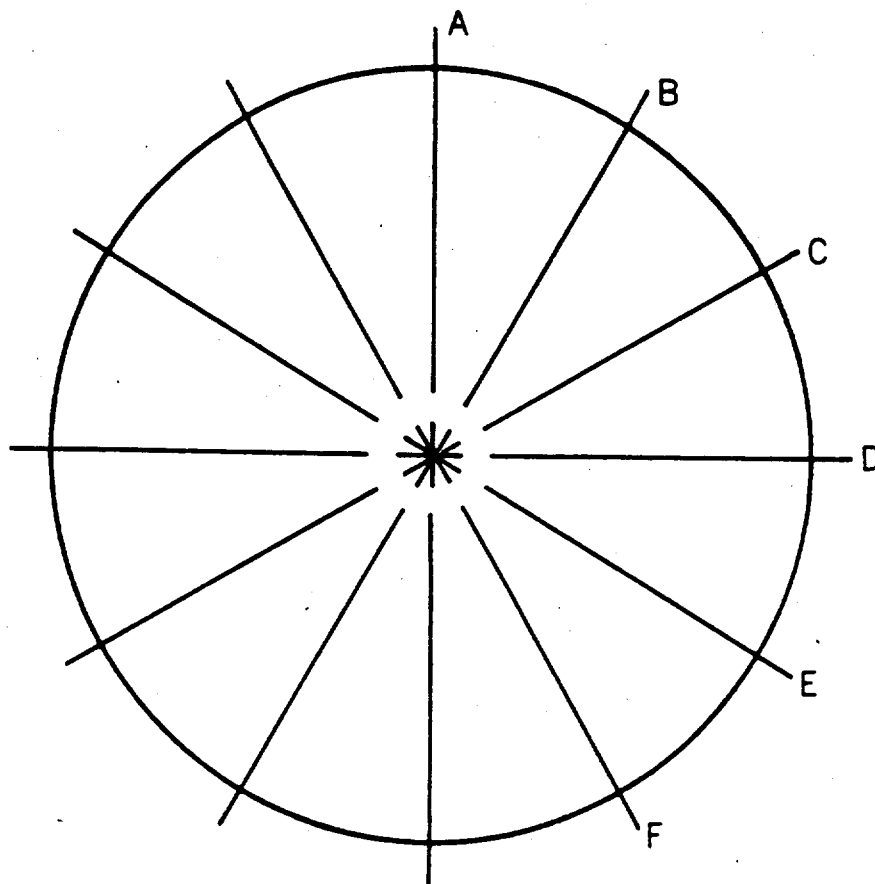
$$\text{Blank CdSO}_4 = [0.00089 (35.00) - 0.0100 (2.50)]$$

$$= 0.0062$$

$$\text{ppm H}_2\text{S} = \frac{0.8039(60 + 460) \left([0.00089 (35.00) - 0.0100 (1.80)] - 0.0062 \right)}{28.5064}$$

$$= 0.10$$

NOZZLE CALIBRATION DATA



DIAMETER (in.)

A 0.3015

B 0.3000

C 0.3041

D 0.3025

E _____

F _____

AVG. 0.3020

DATE 7-27-89

NOZZLE NO. 270

OPERATOR SM

DRY GAS METER / ORIFICE METER CALIBRATION DATA

Date8/16/90
 Bar. Press, in.Hg 29.69
 Meter Box No. 644

Dry Gas Meter No. ... 1008455
 Standard Test Meter # 69279
 Operator TD

STANDARD TEST METER			DRY TEST METER				Time t (min)
Press. dHs (in. H2O)	Temp. Ts (dF)	Volume Vs (ft3)	Press. dH (in. H2O)	Temp. Tdi (dF)	Temp. Tdo (dF)	Volume Vd (ft3)	
	67.0	91.560		99	96	44.501	80.0
2.0	67.0	58.418	0.5	99	97	10.178	
Avg/Net :	67.0	33.142			98	34.323	
	70.0	135.344		91	87	89.503	
3.0	76.0	92.168	1.0	83	82	45.118	77.0
Avg/Net :	73.0	43.176			86	44.385	
	68.0	58.038		100	97	1009.786	33.0
3.7	68.0	36.041	1.5	97	95	986.788	
Avg/Net :	68.0	21.997			97	22.998	
	68.0	35.860		99	96	986.606	
4.6	67.0	10.724	2.0	97	96	960.383	33.0
Avg/Net :	67.5	25.136			97	26.223	
	69.0	157.223		94	88	112.278	23.0
6.3	69.0	135.583	3.0	89	87	89.752	
Avg/Net :	69.0	21.640			90	22.526	

$$y = V_s \times (P_{bar} + (dH_s / 13.6)) \times (Avg. T_d + 460) / [V_d \times (P_{bar} + (dH / 13.6)) \times (T_s + 460)]$$

$$K_o = [(V_s/t) \times [(T_{do} + 460) / (T_s + 460)] \times [(P_{bar} + (dH_s/13.6)) / (P_{bar} + (dH/13.6))] / [((T_{do} + 460) \times dH) / (P_{bar} + (dH/13.6))] \times (Mm)]^{0.5}$$

dH :	0.5	1.0	1.5	2.0	3.0	Avg.	Std.Dev.
y :	1.0257	1.0010	1.0149	1.0186	1.0060	1.0132	0.0088
Ko :	0.7723	0.7243	0.7179	0.7123	0.7129	0.7279	0.0226
y :	0.87 % Relative Std. Dev.						
Ko :	3.11 % Relative Std. Dev.						

DRY GAS METER / ORIFICE METER CALIBRATION DATA

Date8/17/90
 Bar. Press, in.Hg 29.68
 Meter Box No.PORTABLE

Dry Gas Meter No. ... 6825354
 Standard Test Meter # 69279
 Operator TD

STANDARD TEST METER			DRY TEST METER				Time t (min)
Press. dHs (in. H2O)	Temp. Ts (dF)	Volume Vs (ft3)	Press. dH (in. H2O)	Temp. Tdi (dF)	Temp. Tdo (dF)	Volume Vd (ft3)	
	0.0	0.000		0	0	0.000	
0.0	0.0	0.000	0.5	0	0	0.000	0.0
Avg/Net :	0.0	0.000			0	0.000	
	0.0	0.000		0	0	0.000	
0.0	0.0	0.000	1.0	0	0	0.000	0.0
Avg/Net :	0.0	0.000			0	0.000	
	66.0	358.901		84	76	415.874	
-3.4	66.0	330.682	1.5	68	68	387.215	51.0
Avg/Net :	66.0	28.219			74	28.659	
	0.0	0.000		0	0	0.000	
0.0	0.0	0.000	2.0	0	0	0.000	0.0
Avg/Net :	0.0	0.000			0	0.000	
	0.0	0.000		0	0	0.000	
0.0	0.0	0.000	3.0	0	0	0.000	0.0
Avg/Net :	0.0	0.000			0	0.000	

$$y = V_s \times (P_{bar} + (dH_s / 13.6)) \times (Avg. T_d + 460) / [V_d \times (P_{bar} + (dH / 13.6)) \times (T_s + 460)]$$

$$K_o = [(V_s/t) \times [(T_{do} + 460) / (T_s + 460)] \times [(P_{bar} + (dH_s/13.6)) / (P_{bar} + (dH/13.6))] / [((T_{do} + 460) \times dH) / (P_{bar} + (dH/13.6))] \times (Mm)]^{0.5}$$

dH :	0.5	1.0	1.5	2.0	3.0	Avg.	Std.Dev.
y :			0.9875			0.9875	0.3950
Ko :			0.5748			0.5748	0.2299
y :	40.00 % Relative Std. Dev.						
Ko :	40.00 % Relative Std. Dev.						



Scott Specialty Gases

TELEX: 510-100-8831 (ScottGas)
FAX: 714-887-0549
PHONE: 714-887-2571

a division of

Scott Environmental Technology Inc. 2600 CAJON BLVD., SAN BERNARDINO, CA 92405

PAPE & STEINER
ATTN: SUE POWERS

Shipped From: Scott

Date Shipped: 5-10-89

Our Project No: 00252

Your PO No: SP2302-89 R12

Page 1 of 1

Expiration Date: 11-10-90

CERTIFICATE OF ANALYSIS - EPA PROTOCOL GASES*

Certified Per Traceability Protocol No. 1 Procedure No. G1

Cylinder No. AAL-15365

Cylinder Pressure 1900 psig

Certified Accuracy ± 1 % NBS Traceable

REFERENCE STD

COMPONENTS	CERTIFIED CONC	SRM/CRM NO.	CYL. NO.	CONC.
Nitric Oxide	19.78 PPM	SRM 2629 A	AAL-14755	23.33 PPM

NOX 20.04 PPM

GAS ANALYZER

MAKE/MODEL/SERIAL NO.	LAST CAL. DATE	ANALYTICAL PRINCIPLE
Thermo-Electron	5-2-89	Chemi-Luminescent
10 AR S/N 14853-150		

BALANCE GAS Nitrogen

ANALYZER READINGS: Z = Zero Gas T = Test Gas R = Reference Gas

Component	Nitric Oxide	Units	PPM
First Analysis Date 4-24-89			
Z 0.00	R 93.73	T	79.09
R 93.68	Z 0.08	T	79.02
Z 0.08	T 79.03	R	93.78
Mean Test Assay			19.68 PPM
Second Analysis Date 5-6-89			
Z 0.00	R 92.99	T	79.66
R 94.05	Z 0.01	T	79.78
Z 0.00	T 79.81	R	94.13
Mean Test Assay			19.78

Chronology: Date _____
Assay _____

Analyst Doug Hagberg/Carrie Boddy

Approved By:

Mean Test Assay

[Signature]



Scott Specialty Gases

TELEX: 510-100-8831 (ScottGas)

FAX: 714-887-0549

PHONE: 714-887-2571

a division of

Scott Environmental Technology Inc. 2600 CAJON BLVD., SAN BERNARDINO, CA 92405

PAPE & STEINER

ATTN: SUE POWERS

Shipped From: Scott SAN BERNARDINO

Date Shipped 7-17-89

Our Project No: 01341

Your P.O. No: SP2302-89 R20

Page 1 of 1

Expiration Date: 1-17-91

CERTIFICATE OF ANALYSIS - EPA PROTOCOL GASES

Certified Per Measurability Protocol No. 1 Procedure No. G1

Cylinder No. AAL-13433

Cylinder Pressure 1900 psig

Certified Accuracy ±1 % 100 Traceable

REFERENCE STD

COMPONENTS	CERTIFIED CONC	SRM/CRM NO.	CYL. NO.	CONC.
Nitric Oxide	81.59 PPM	SRM 1684 B	CAL-12787	94.80 PPM

NOX 81.90 PPM

GAS ANALYZER

MAKE/MODEL/SERIAL NO.	LAST CAL. DATE	ANALYTICAL PRINCIPLE
Thermo-Electron 10 AR S/N 14853-150	5-2-89	Chemi-Luminescent

BALANCE GAS Nitrogen

ANALYZER READINGS: Z = Zero Gas T = Test Gas R = Reference Gas

Component	Nitric Oxide	7-5-89	Units	PPM
First Analysis Date	Z	0.00	R	94.83
	R	-0.01	T	81.70
	Z	-0.03	T	81.63
	T	81.67	R	94.75
Mean Test Assay				81.68 PPM
Second Analysis Date	Z	0.00	R	94.50
	R	0.02	T	81.32
	Z	81.30	T	81.32
	T		R	94.43
Mean Test Assay				81.59 PPM

Chronology: Date
Assay

Analyst Doug Hagberg

Approved By:

[Signature]



Scott Specialty Gases

TELEX: 510-100-8831 (ScotGas)

FAX: 714-887-0549

PHONE: 714-887-2571

a division of

Scott Environmental Technology Inc. 2600 CAJON BLVD., SAN BERNARDINO, CA 92405

Pape & Steiner

Shipped From: Scott San Bernardino

Date Shipped 11/27/89

Our Project No: 3535

Your PO. No: SP2302-89 REL 35

Page 1 of 1

Expiration Date: 5/91

C to A G G o

CERTIFICATE OF ANALYSIS - EPA PROTOCOL GASES*

Certified For Traceability Protocol No. 1 Procedure No. G1

Cylinder No. AAAL 2171

Cylinder Pressure 1900 PSIG

Certified Accuracy ±1 % NBS Traceable

REFERENCE STD

GAS ANALYZER

COMPONENTS	CERTIFIED CONC	SRM/CRM NO.	CYL. NO.	CONC.	MAKE/MODEL/SERIAL NO.	LAST CAL. DATE	ANALYTICAL PRINCIPLE
Nitric Oxide	41.32 PPM	CRM 1684 B	ALM-3640	97.28 PPM	Thermo-Electron 10 AR	11/10/89	Chemi-Luminescent
NOX	41.39 PPM				S/N 14853-150		

BALANCE GAS Nitrogen

ANALYZER READINGS: Z = Zero Gas T = Test Gas R = Reference Gas

Component	Nitric Oxide	
First Analysis Date	11/13/89	Units
Z	0.0	R 97.23 T 41.21
R	97.14	Z 0.0 T 41.23
Z	0.0	T 41.27 R 97.20
		Mean Test Assay 41.27
Second Analysis Date	11/21/89	Units
Z	0.0	R 97.26 T 41.30
R	97.25	Z 0.05 T 41.33
Z	0.06	T 41.40 R 97.32
		Mean Test Assay 41.32

Component		Units
Date		
Z		R T
R		Z T
Z		T R
		Mean Test Assay
Date		
Z		R T
R		Z T
Z		T R
		Mean Test Assay

Chronology: Date _____
Assay _____

Analyst Lee Oldham

Approved By: R. D. Bryant



SCOTT-MARRIN, INC.

2001 THIRD ST. • UNIT H • RIVERSIDE, CA 92507
TELEPHONE (714) 784-1240

REPORT OF ANALYSIS
NIST TRACEABLE GAS MIXTURES

PAPE01

TO:

SUE POWERS
PAPE & STEINER ENVIRONMENTAL
5801 NORRIS RD.
BAKERSFIELD, CA 93308

DATE: 08/23/90

CUSTOMER ORDER NUMBER: SP-2750-90 REL2

PAGE 1

CYLINDER NUMBER	COMPONENT	CONCENTRATION (v/v)	NIST TRACEABLE REFERENCE STANDARD
CC73017	Carbon Dioxide	15.24 ± 0.15 %	SRM 1675b
	Oxygen	7.38 ± 0.07 %	SRM 2658a
	Carbon Monoxide	75.4 ± 0.8 ppm	SRM 1679c
	Nitrogen	Balance	
CC12055	Carbon Dioxide	14.71 ± 0.15 %	SRM 1675b
	Oxygen	3.82 ± 0.04 %	SRM 2658a
	Carbon Monoxide	37.4 ± 0.4 ppm	SRM 2614a
	Nitrogen	Balance	
CC7262	Oxygen	0.967 ± 0.010 %	SRM 2657
	Carbon Dioxide	9.53 ± 0.10 %	SRM 1675b
	Carbon Monoxide	394 ± 4 ppm	SRM 1680b
	Nitrogen	Balance	

ppm = umole/mole

% = mole-%

The above analyses are traceable to the National Institute of Standards and Technology by intercomparison with the reference standards listed above. Where indicated, volumetric and gravimetric reference standards are traceable thru use of our analytical balance. NIST Report No. MMAP 232.09/202491.

Analyst:

J.W. Gay

Approved:

J.T. Marrin

The only liability of this company for gas which fails to comply with this analysis shall be replacement or reanalysis thereof by the company without extra cost.

STANDARD CALIBRATION GASES IN ALUMINUM CYLINDERS

REPORT OF ANALYSIS

CUSTOMER ORDER NUMBER: SP-2750-90 REL2

PAGE 2

<XX>			
CYLINDER NUMBER	COMPONENT	CONCENTRATION(v/v)	NIST TRACEABLE REFERENCE STANDARD
-----	-----	-----	-----
CC28200	Carbon Dioxide	15.03 + 0.15 %	SRM 1675b
	Oxygen	7.61 + 0.08 %	SRM 2658a
	Carbon Monoxide	142.4 + 1.4 ppm	SRM 2636
	Nitrogen	Balance	

ppm = umole/mole

% = mole-%

The above analyses are traceable to the National Institute of Standards and Technology by intercomparison with the reference standards listed above. Where indicated, volumetric and gravimetric reference standards are traceable thru use of our analytical balance. NIST Report No. MMAP 232.09/202491.



Scott Specialty Gases

a division of

TELEX: 510-100-8831 (ScolGas)

FAX: 714-887-0549

PHONE: 714-887-2571

Scott Environmental Technology Inc. 2600 CAJON BLVD., SAN BERNARDINO, CA 92405

PAPE & STEINER
5801 NORRIS ROAD
BAKERSFIELD, CA 93308

Date: 2/14/90

Our Project No.: 5087

Your P.O. No.: SP 2546-90 REL# 5

Gentlemen:

Thank you for choosing Scott for your Specialty Gas needs. The analyses for the gases ordered, as reported by our laboratory, are listed below. Results are in volume percent, unless otherwise indicated.

ANALYTICAL REPORT

Cyl. No. 1L-23410 Analytical Accuracy ±1%
Component Concentration

CARBON DIOXIDE 5.02%

CARBON MONOXIDE 80.7 ppm

OXYGEN 15.0%

CO NIST TRACEABLE TO SRM 1679

NITROGEN BALANCE

Cyl. No. _____ Analytical Accuracy _____
Component Concentration

Cyl. No. _____ Analytical Accuracy _____
Component Concentration

Cyl. No. _____ Analytical Accuracy _____
Component Concentration

Analyst _____

Approved By *[Signature]*

The only liability of this Company for gas which fails to comply with this analysis shall be replacement thereof by the Company without extra cost.

PLUMSTEADVILLE, PENNSYLVANIA / TROY, MICHIGAN / HOUSTON, TEXAS / WHEELING, ILLINOIS
SOUTH PLAINFIELD, NEW JERSEY / FREMONT, CALIFORNIA / WAKEFIELD, MASSACHUSETTS / LONGMONT, COLORADO
BOSTON, MASSACHUSETTS / BATON ROUGE, LOUISIANA



Scott Specialty Gases

a division of

TELEX: 510-100-8831 (ScotGas)

FAX: 714-887-0549

PHONE: 714-887-2571

Scott Environmental Technology Inc. 2600 CAJON BLVD., SAN BERNARDINO, CA 92405

PAPE & STEINER
SUE POWERS

Date: 8/21/90

Our Project No.: 8369

Your P.O. No.: SP 25469 REL 19

Gentlemen:

Thank you for choosing Scott for your Specialty Gas needs. The analyses for the gases ordered, as reported by our laboratory, are listed below. Results are in volume percent, unless otherwise indicated.

ANALYTICAL REPORT

1300 psig
Cyl. No. AAL-9891 Analytical Accuracy ±1%
Component Concentration

CARBON MONOXIDE 3.484 ppm

NITROGEN BALANCE

*GRAVIMETRIC MASTER GAS

Cyl. No. _____ Analytical Accuracy _____
Component Concentration

Cyl. No. _____ Analytical Accuracy _____
Component Concentration

Cyl. No. _____ Analytical Accuracy _____
Component Concentration

Analyst _____

Approved By [Signature]

*CERTIFIED TO HAVE BEEN BLENDED AGAINST NIST CERTIFIED WEIGHTS AND VERIFIED TO BE CORRECT BY INDEPENDENT ANALYSIS.

The only liability of this Company for gas which fails to comply with this analysis shall be replacement thereof by the Company without extra cost.

PLUMSTEADVILLE, PENNSYLVANIA / TROY, MICHIGAN / HOUSTON, TEXAS / WHEELING, ILLINOIS
SOUTH PLAINFIELD, NEW JERSEY / FREMONT, CALIFORNIA / WAKEFIELD, MASSACHUSETTS / LONGMONT, COLORADO
BOSTON, MASSACHUSETTS / BATON ROUGE, LOUISIANA



SCOTT-MARRIN, INC.
2001 THIRD ST. • UNIT H • RIVERSIDE, CA 92507
TELEPHONE (714) 784-1240

REPORT OF ANALYSIS

PAPEØ1

TO: Pape & Steiner Environmental Services
5801 Norris Rd.
Bakersfield, CA 93308

DATE: 30 August 1990

IMPORTANT ANALYSIS REPORT

Please forward to user
of calibration gases.

CUSTOMER ORDER NUMBER: B-SP-2750-90 Rel. 2

~~~~~  
CYLINDER NUMBER CC92991  
COMPONENT CONCENTRATION(v/v)  
Carbon Monoxide  $3.24 \pm 0.07$  ppm  
Nitrogen Balance

CYLINDER NUMBER \_\_\_\_\_  
COMPONENT CONCENTRATION(v/v)  
Replicate 8/23/90 3.30 ppm 8/30/90 3.21 ppm  
Analysis 3.21 ppm 3.23 ppm  
Data On 3.25 ppm 3.25 ppm  
CO: Mean 3.25 ppm 3.23 ppm

Expiration Date CO: 2/30/92

CYLINDER NUMBER CC63352  
COMPONENT CONCENTRATION(v/v)  
Carbon Monoxide  $8.24 \pm 0.16$  ppm  
Nitrogen Balance

CYLINDER NUMBER \_\_\_\_\_  
COMPONENT CONCENTRATION(v/v)  
Replicate 8/23/90 8.24 ppm 8/30/90 8.23 ppm  
Analysis 8.22 ppm 8.30 ppm  
Data On 8.23 ppm 8.19 ppm  
CO: Mean 8.23 ppm 8.24 ppm

Expiration Date CO: 2/30/92

ANALYST

J.W. Gay

APPROVED

J.T. Marrin

The only liability of this company for gas which fails to comply with this analysis shall be replacement or reanalysis thereof by the company without extra cost.

SCOTT-MARRIN, INC.

2001 THIRD ST., UNIT 1

RIVERSIDE, CALIFORNIA 92507

## REPORT OF ANALYSIS

CUSTOMER ORDER NUMBER: B-SP-2750-90 Rel. 2

CYLINDER NUMBER CC86236

| COMPONENT       | CONCENTRATION(v/v) |
|-----------------|--------------------|
| Carbon Monoxide | 8.21 ± 0.16 ppm    |
| Nitrogen        | Balance            |

CYLINDER NUMBER \_\_\_\_\_

| COMPONENT         | CONCENTRATION(v/v) |
|-------------------|--------------------|
| Replicate 8/23/90 | 8.13 ppm           |
| Analysis          | 8.19 ppm           |
| Data On           | 8.24 ppm           |
| CO: Mean          | 8.19 ppm           |

Expiration Date CO: 2/30/92

CYLINDER NUMBER CC56541

| COMPONENT       | CONCENTRATION(v/v) |
|-----------------|--------------------|
| Carbon Monoxide | 825 ± 8 ppm        |
| Nitrogen        | Balance            |

CYLINDER NUMBER \_\_\_\_\_

| COMPONENT         | CONCENTRATION(v/v) |
|-------------------|--------------------|
| Replicate 8/24/90 | 825 ppm            |
| Analysis          | 822 ppm            |
| Data On           | 821 ppm            |
| CO: Mean          | 823 ppm            |

Expiration Date CO: 2/31/92

CYLINDER NUMBER CC56425

| COMPONENT       | CONCENTRATION(v/v) |
|-----------------|--------------------|
| Carbon Monoxide | 4130 ± 41 ppm      |
| Nitrogen        | Balance            |

CYLINDER NUMBER \_\_\_\_\_

| COMPONENT         | CONCENTRATION(v/v) |
|-------------------|--------------------|
| Replicate 8/24/90 | 4140 ppm           |
| Analysis          | 4110 ppm           |
| Data On           | 4130 ppm           |
| CO: Mean          | 4130 ppm           |

Expiration Date CO: 2/31/92

CYLINDER NUMBER CC92991

| COMPONENT | CONCENTRATION(v/v) |
|-----------|--------------------|
|-----------|--------------------|

CYLINDER NUMBER \_\_\_\_\_

| COMPONENT | CONCENTRATION(v/v) |
|-----------|--------------------|
|-----------|--------------------|

(The Carbon Monoxide analysis was performed in accordance with Section 3.0.4 of the revised )  
 (EPA traceability protocol No. 1 dated June 9, 1987. The analysis is traceable to the National )  
 Institute of Standards & Technology by direct intercomparison with SRM 2612, cylinder number )  
 FF11054 at 9.92 ppm Carbon Monoxide in Air. The analysis was performed using a Carle Model )  
 8000 gas chromatograph with catalytic methanation/flame ionization detection. The last multi- )  
 point calibration was performed 9/11/90. )

SCOTT-MARRIN, INC.

2001 THIRD ST., UNIT 1

RIVERSIDE, CALIFORNIA 92507

## REPORT OF ANALYSIS

CUSTOMER ORDER NUMBER: B-SP-2750-90 Rel. 2

CYLINDER NUMBER CC86236CYLINDER NUMBER CC63352

COMPONENT CONCENTRATION(v/v)

COMPONENT CONCENTRATION(v/v)

(The Carbon Monoxide analysis was performed in accordance with Section 3.0.4 of the revised )  
 (EPA traceability protocol No. 1 dated June 9, 1987. The analysis is traceable to the )  
 (National Institute of Standards & Technology by direct intercomparison with SRM 2612, )  
 (cylinder number FF11054 at 9.92 ppm Carbon Monoxide in Air. The analysis was performed )  
 (using a Carle Model 8000 gas chromatograph with catalytic methanation/flame ionization )  
 (detection. The last multipoint calibration was performed 9/11/90. )

CYLINDER NUMBER CC56541

CYLINDER NUMBER \_\_\_\_\_

COMPONENT CONCENTRATION(v/v)

COMPONENT CONCENTRATION(v/v)

(The Carbon Monoxide analysis was performed in accordance with Section 3.0.4 of the revised )  
 (EPA traceability protocol No. 1 dated June 9, 1987. The analysis is traceable to the )  
 (National Institute of Standards & Technology by direct intercomparison with GMIS, cylinder )  
 (number L382 at 1046 ppm Carbon Monoxide in Nitrogen. The analysis was performed using a )  
 (Carle Model 8000 gas chromatograph with catalytic methanation/flame ionization detection. )  
 (The last multipoint calibration was performed 9/11/90. )

CYLINDER NUMBER CC56425

CYLINDER NUMBER \_\_\_\_\_

COMPONENT CONCENTRATION(v/v)

COMPONENT CONCENTRATION(v/v)

(The Carbon Monoxide analysis was performed in accordance with Section 3.0.4 of the revised )  
 (EPA traceability protocol No. 1 dated June 9, 1987. The analysis is traceable to the )  
 (National Institute of Standards & Technology by direct intercomparison with GMIS, cylinder )  
 (number CC7245 at 5040 ppm Carbon Monoxide in Nitrogen. The analysis was performed using )  
 (a Carle Model 8000 gas chromatograph with catalytic methanation/flame ionization detection. )  
 (The last multipoint calibration was performed 9/11/90. )

CYLINDER NUMBER \_\_\_\_\_

CYLINDER NUMBER \_\_\_\_\_

COMPONENT CONCENTRATION(v/v)

COMPONENT CONCENTRATION(v/v)





# Scott Specialty Gases

a division of

TELEX: 510-100-8831 (ScotGas)

FAX: 714-887-0549

PHONE: 714-887-2571

Scott Environmental Technology Inc. 2800 CAJON BLVD., SAN BERNARDINO, CA 92405

PAPE & STEINER  
5801 NORRIS ROAD  
BAKERSFIELD, CA 93308

Date: 5/11/90  
Our Project No.: 5843  
Your P.O. No.: SP2546-90 REL# 10

Gentlemen:

Thank you for choosing Scott for your Specialty Gas needs. The analyses for the gases ordered, as reported by our laboratory, are listed below. Results are in volume percent, unless otherwise indicated.

## ANALYTICAL REPORT

CGA 350 Analytical  
Cyl. No. ALM-12308 Accuracy +1%  
Component Concentration  
METHANE 21.19 ppm  
ETHANE 21.98 ppm  
PROPANE 22.63 ppm  
n-BUTANE 22.33 ppm  
n-PENTANE 19.74 ppm  
n-HEXANE 19.48 ppm

NITROGEN BALANCE

Cyl. No. \_\_\_\_\_ Analytical Accuracy \_\_\_\_\_  
Component Concentration

Analyst \_\_\_\_\_

Cyl. No. \_\_\_\_\_ Analytical Accuracy \_\_\_\_\_  
Component Concentration

Cyl. No. \_\_\_\_\_ Analytical Accuracy \_\_\_\_\_  
Component Concentration

Approved By [Signature]

The only liability of this Company for gas which fails to comply with this analysis shall be replacement thereof by the Company without extra cost.

PLUMSTEADVILLE, PENNSYLVANIA / TROY, MICHIGAN / HOUSTON, TEXAS / WHEELING, ILLINOIS  
SOUTH PLAINFIELD, NEW JERSEY / FREMONT, CALIFORNIA / WAKEFIELD, MASSACHUSETTS / LONGMONT, COLORADO  
BOSTON, MASSACHUSETTS / BATON ROUGE, LOUISIANA

**APPENDIX B**  
**SWEPI COALINGA COGEN OPERATING DATA**

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/20/90 TIME: 08:52:09

09/20/90

09/20/90

09/20/90

0.74 RATIO

0.73 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 398.7873 MCF | 24 HR RUNNING  |
| FUEL GAS 1081.823 MCF | 24 HR PREVIOUS |
| FUEL GAS 3633.233 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 19811.15 MCF | MONTH RUNNING  |
| FUEL GAS 31982.18 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 404.9142 MCF | 24 HR RUNNING  |
| FUEL GAS 1098.213 MCF | 24 HR PREVIOUS |
| FUEL GAS 3687.500 MCF | 7 DAY RUNNING  |
| FUEL GAS 7874.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 21218.15 MCF | MONTH RUNNING  |
| FUEL GAS 33180.49 MCF | MONTH PREVIOUS |

0.74 RATIO

0.73 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 817.2148 MCF | 24 HR RUNNING  |
| FUEL GAS 2211.638 MCF | 24 HR PREVIOUS |
| FUEL GAS 7427.847 MCF | 7 DAY RUNNING  |
| FUEL GAS 15438.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 41730.47 MCF | MONTH RUNNING  |
| FUEL GAS 67386.09 MCF | MONTH PREVIOUS |

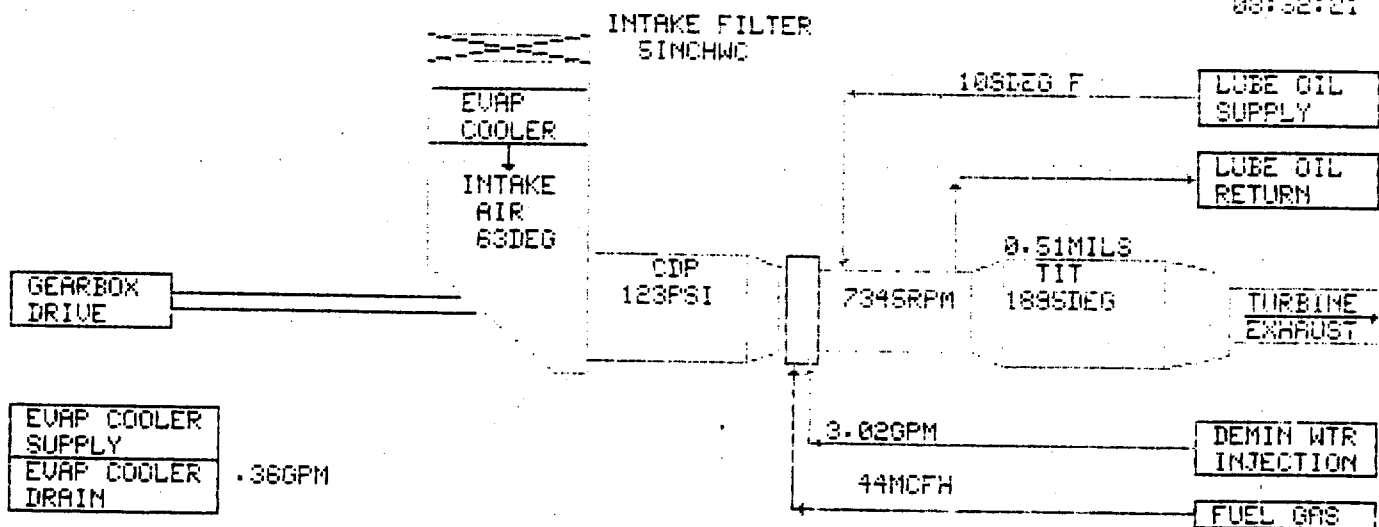
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DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/20/90 TIME: 08:52:25

ENGINE INSTRUMENTATION

20/SEP/90  
08:52:21



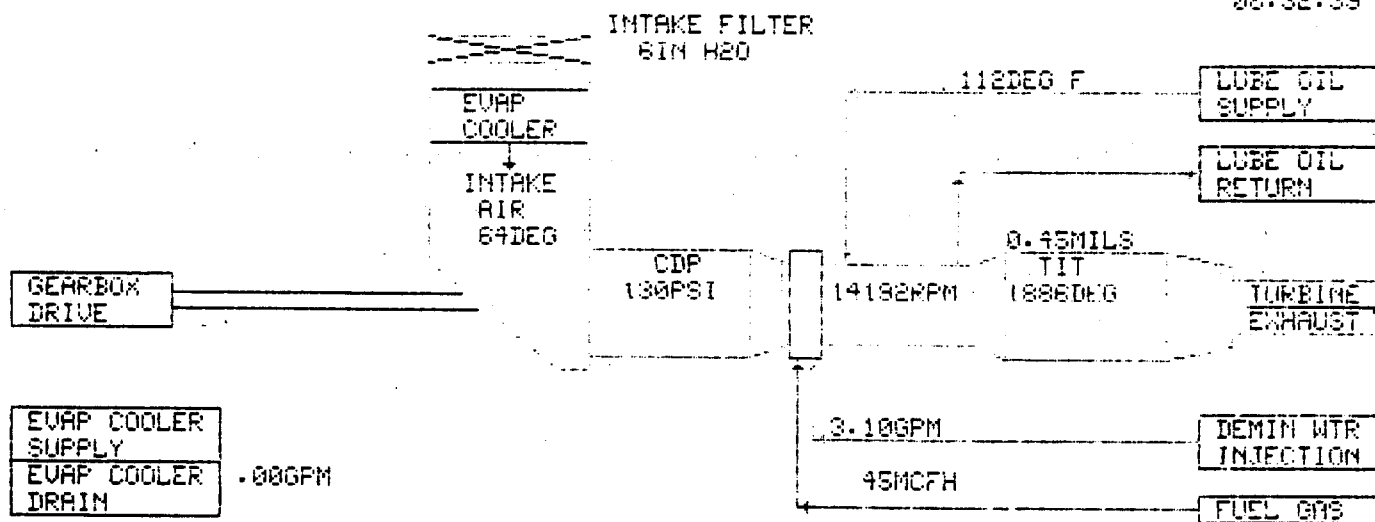
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/20/90 TIME: 08:52:44

10-1413 TURBINE INSTRUMENTATION

20/SEP/90  
08:52:39



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/19/90 TIME: 10:27:11

18 SEP 90

WATER, W. 2000

01:27:00

|                       |                |                       |                |
|-----------------------|----------------|-----------------------|----------------|
| FUEL GAS 475.1517 MCF | 24 HR RUNNING  | FUEL GAS 481.8123 MCF | 24 HR RUNNING  |
| FUEL GAS 1075.172 MCF | 24 HR PREVIOUS | FUEL GAS 1090.958 MCF | 24 HR PREVIOUS |
| FUEL GAS 2627.750 MCF | 7 DAY RUNNING  | FUEL GAS 2666.136 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.784 MCF | 7 DAY PREVIOUS | FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 18964.00 MCF | MONTH RUNNING  | FUEL GAS 20218.31 MCF | MONTH RUNNING  |
| FUEL GAS 31982.18 MCF | MONTH PREVIOUS | FUEL GAS 33160.43 MCF | MONTH PREVIOUS |

0.73 RATIO

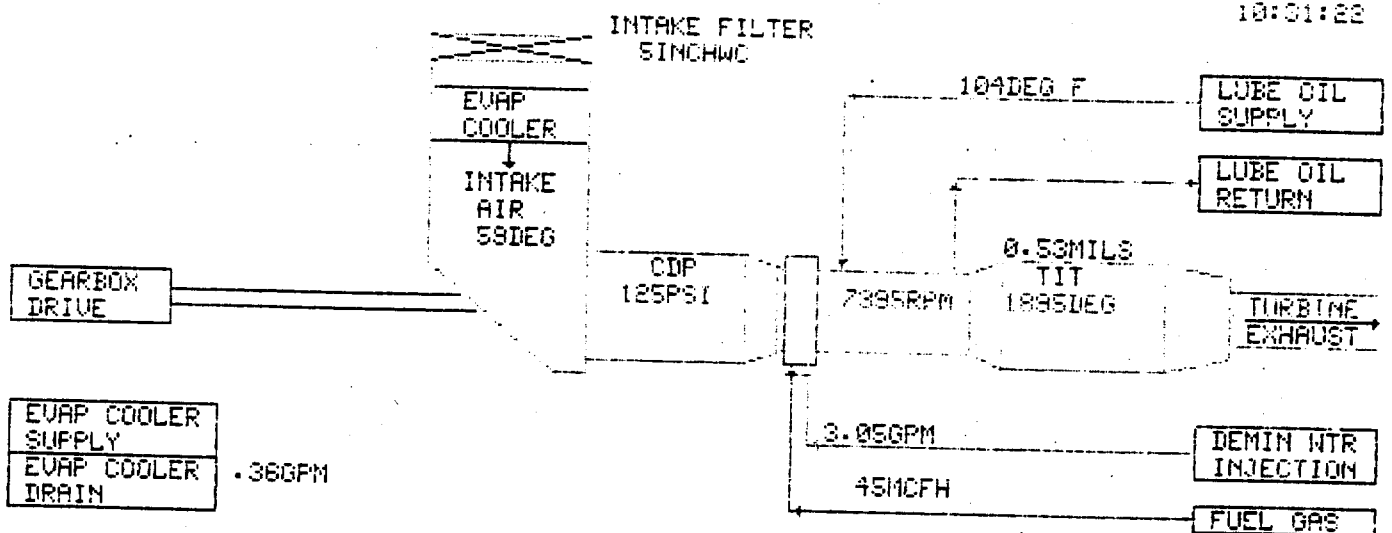
|                       |                |
|-----------------------|----------------|
| FUEL GAS 973.8858 MCF | 24 HR RUNNING  |
| FUEL GAS 2195.398 MCF | 24 HR PREVIOUS |
| FUEL GAS 5370.815 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 39645.33 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.73 RATIO

COPY IN PROGRESS

TIME: 10:31:25

19/SEP/90  
10:01:22



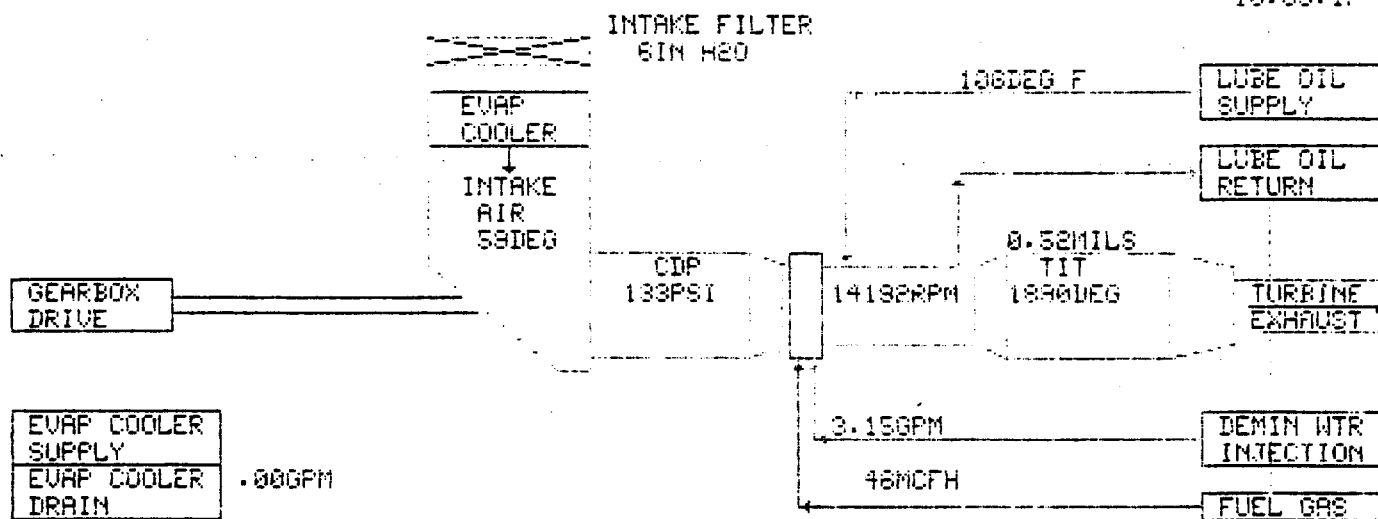
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/19/90 TIME: 10:33:19

FA-18 D TURBINE INSTRUMENTATION

19/SEP/90  
10:33:17



COPY IN PROGRESS



DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/19/90 TIME: 10:43:15

18/SEP/90

~~XXXXXXXXXXXX~~

~~XXXXXXXXXXXX~~

|                       |                |
|-----------------------|----------------|
| FUEL GAS 487.2579 MCF | 24 HR RUNNING  |
| FUEL GAS 1075.172 MCF | 24 HR PREVIOUS |
| FUEL GAS 2639.885 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.784 MCF | 7 DAY PREVIOUS |
| FUEL GAS 18975.42 MCF | MONTH RUNNING  |
| FUEL GAS 31982.18 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 494.2513 MCF | 24 HR RUNNING  |
| FUEL GAS 1090.959 MCF | 24 HR PREVIOUS |
| FUEL GAS 2678.468 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.377 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20231.35 MCF | MONTH RUNNING  |
| FUEL GAS 33180.93 MCF | MONTH PREVIOUS |

0.73 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 398.8928 MCF | 24 HR RUNNING  |
| FUEL GAS 2195.398 MCF | 24 HR PREVIOUS |
| FUEL GAS 5395.759 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 39671.63 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.74 RATIO

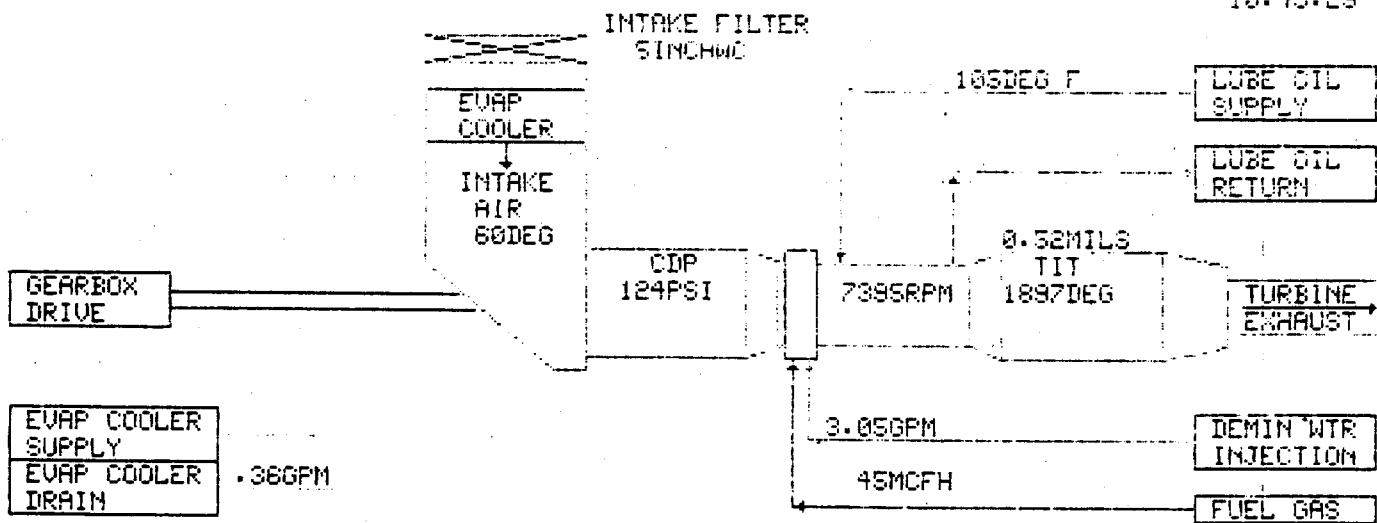
COPY IN PROGRESS

DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/19/90 TIME: 10:43:33

DS-100A TURBINE INSTRUMENTATION

19/SEP/90  
10:43:28



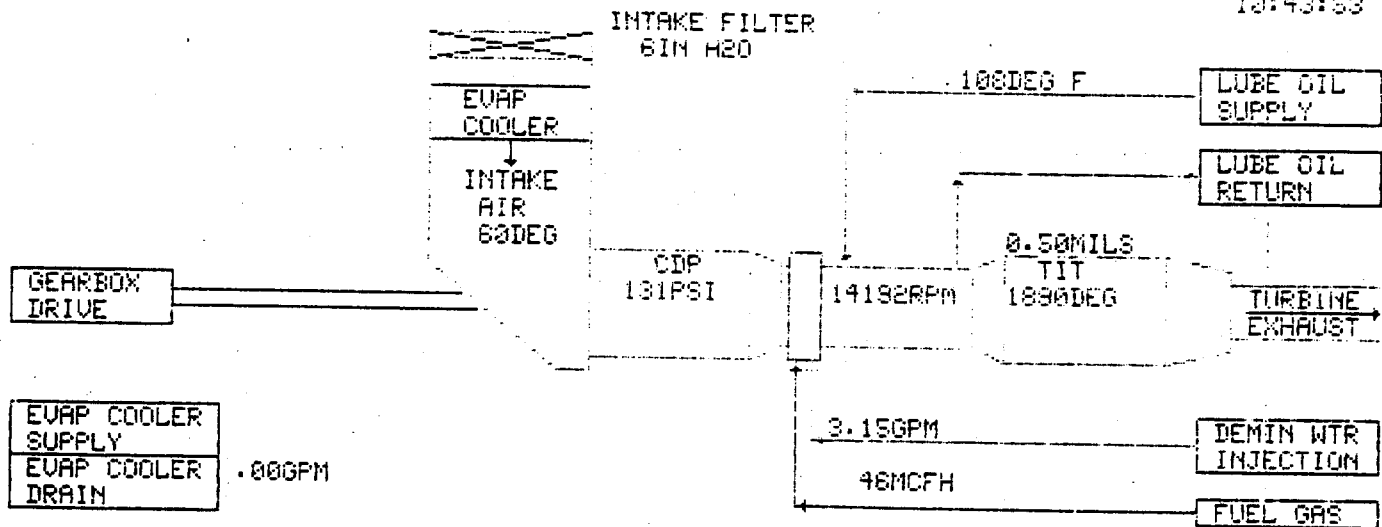
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/19/90 TIME: 10:43:55

TB-101D TURBINE INSTRUMENTATION

18/SEP/90  
10:43:53



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/19/90

TIME: 11:03:56

13 SEP 1990

~~XXXXXXXXXXXXXXXXXXXX~~

~~XXXXXXXXXXXX~~

11:03:56

|                       |                |
|-----------------------|----------------|
| FUEL GAS 502.9284 MCF | 24 HR RUNNING  |
| FUEL GAS 1075.172 MCF | 24 HR PREVIOUS |
| FUEL GAS 2655.485 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 18990.23 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 510.1555 MCF | 24 HR RUNNING  |
| FUEL GAS 1090.859 MCF | 24 HR PREVIOUS |
| FUEL GAS 2694.373 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20248.17 MCF | MONTH RUNNING  |
| FUEL GAS 33160.43 MCF | MONTH PREVIOUS |

0.73 BBT10

|                       |                |
|-----------------------|----------------|
| FUEL GAS 1030.859 MCF | 24 HR RUNNING  |
| FUEL GAS 2195.396 MCF | 24 HR PREVIOUS |
| FUEL GAS 5427.868 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 39705.62 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.74 BBT10

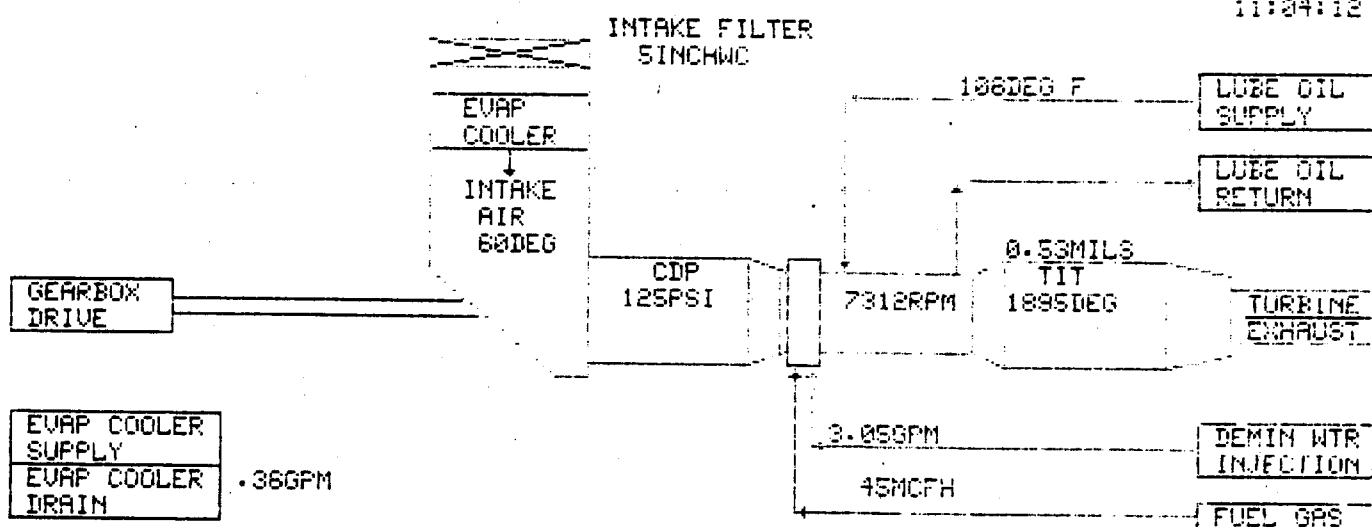
COPY IN PROGRESS

DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/19/90 TIME: 11:04:16

To-Intake Turbine Installation

18/SLP/90  
11:04:12



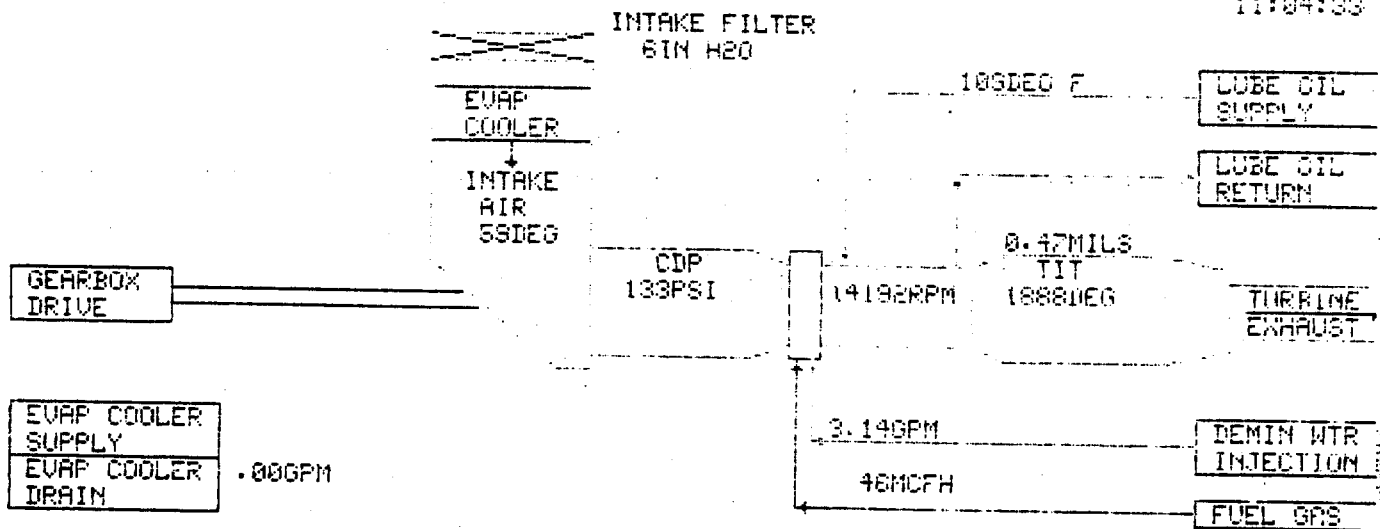
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/19/90 TIME: 11:04:37

GEARBOX TURBINE INSTRUMENTATION

19/SEP/90  
11:04:33



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/19/90 TIME: 11:25:33

19-SEP-90

~~CONFIDENTIAL~~

11:25:33

~~CONFIDENTIAL~~

~~CONFIDENTIAL~~

|                       |                |
|-----------------------|----------------|
| FUEL GAS 519.1915 MCF | 24 HR RUNNING  |
| FUEL GAS 1075.172 MCF | 24 HR PREVIOUS |
| FUEL GAS 2671.788 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 19005.58 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 536.7547 MCF | 24 HR RUNNING  |
| FUEL GAS 1090.953 MCF | 24 HR PREVIOUS |
| FUEL GAS 2711.903 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20265.71 MCF | MONTH RUNNING  |
| FUEL GAS 33160.43 MCF | MONTH PREVIOUS |

0.72 BBT10

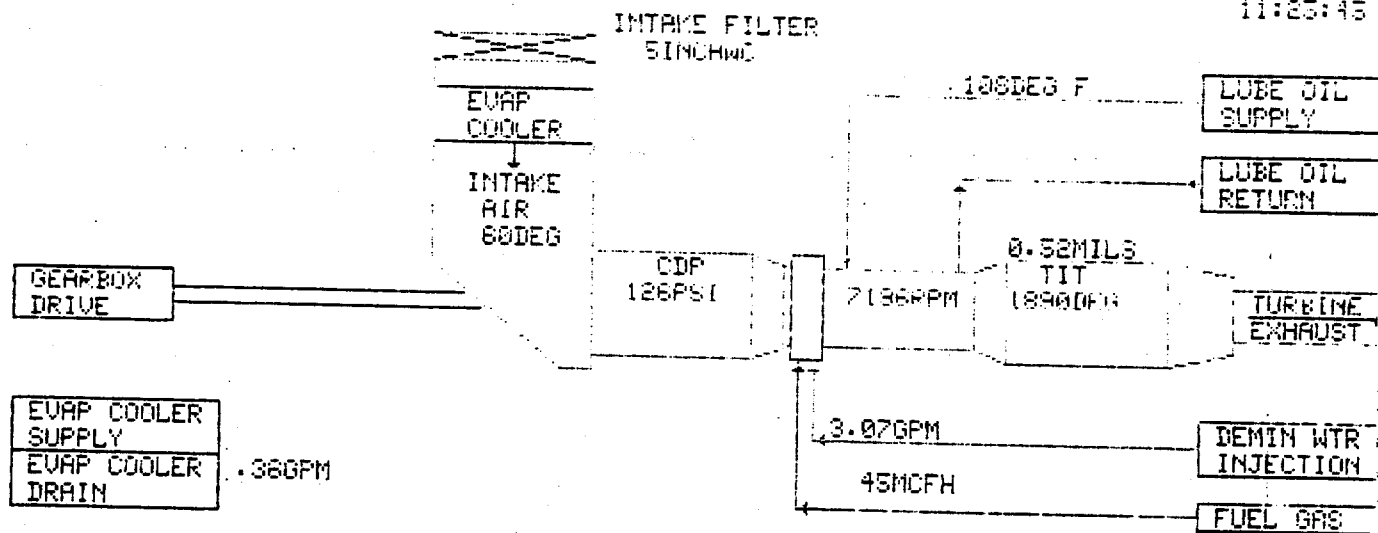
|                       |                |
|-----------------------|----------------|
| FUEL GAS 1064.023 MCF | 24 HR RUNNING  |
| FUEL GAS 2195.398 MCF | 24 HR PREVIOUS |
| FUEL GAS 5481.391 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 33741.11 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.72 BBT10

COPY IN PROGRESS

DATE: 09/19/90 TIME: 11:25:49

18/SEP/94  
11:25:45



**COPY IN PROGRESS**

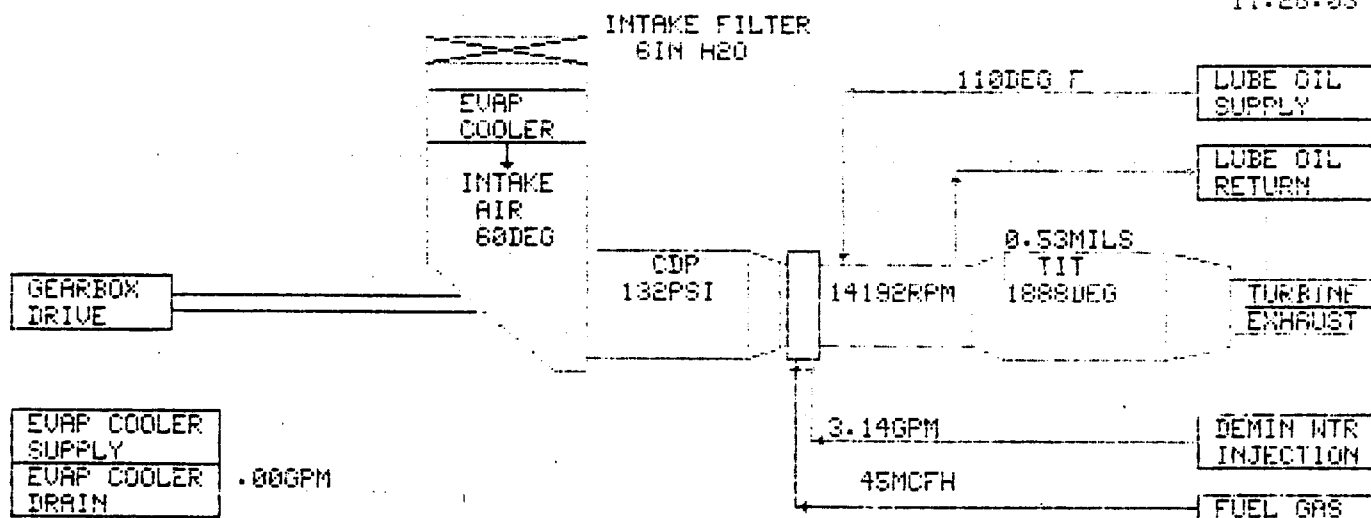


DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/19/90 TIME: 11:26:08

FOR LUBE TURBINE (WATER-ENTRAPPED)

19/SEP/90  
11:26:03



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/19/90 TIME: 11:45:47

18/SEP/90

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|                       |                |
|-----------------------|----------------|
| FUEL GAS 534.4415 MCF | 24 HR RUNNING  |
| FUEL GAS 1075.172 MCF | 24 HR PREVIOUS |
| FUEL GAS 2687.048 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 19019.91 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 542.2878 MCF | 24 HR RUNNING  |
| FUEL GAS 1090.858 MCF | 24 HR PREVIOUS |
| FUEL GAS 2726.530 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20282.04 MCF | MONTH RUNNING  |
| FUEL GAS 33160.49 MCF | MONTH PREVIOUS |

0.74 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 1095.219 MCF | 24 HR RUNNING  |
| FUEL GAS 2195.396 MCF | 24 HR PREVIOUS |
| FUEL GAS 5492.688 MCF | 7 DAY RUNNING  |
| FUEL GAS 15438.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 39774.31 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.74 RATIO

COPY IN PROGRESS

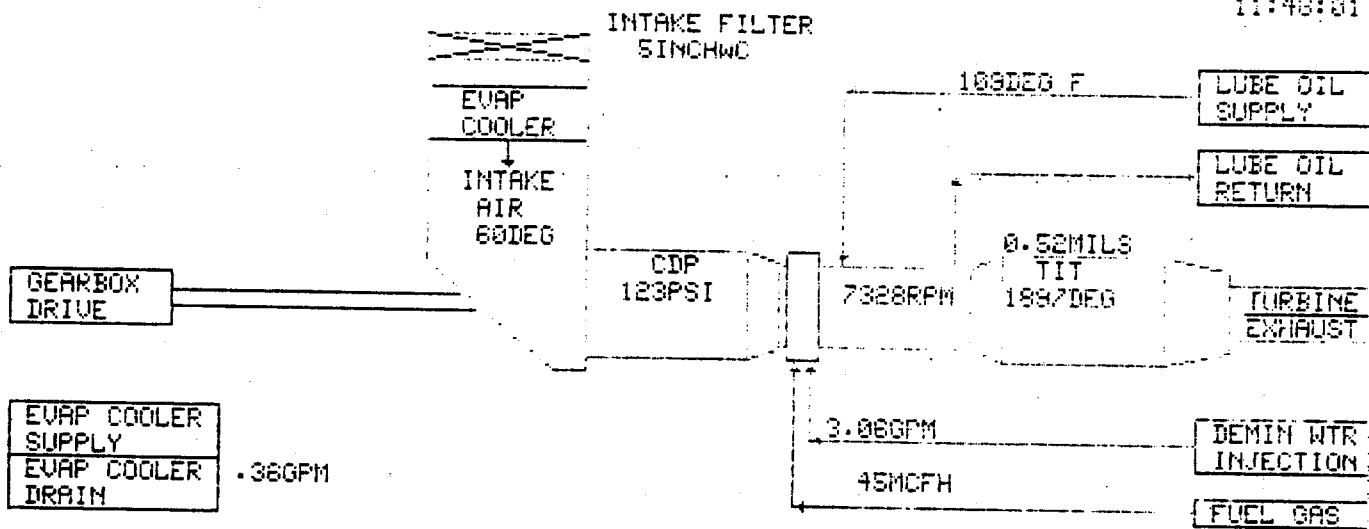
DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/19/90

TIME: 11:46:06

TURBINE INSTRUMENTATION

19/SEP/90  
11:48:01



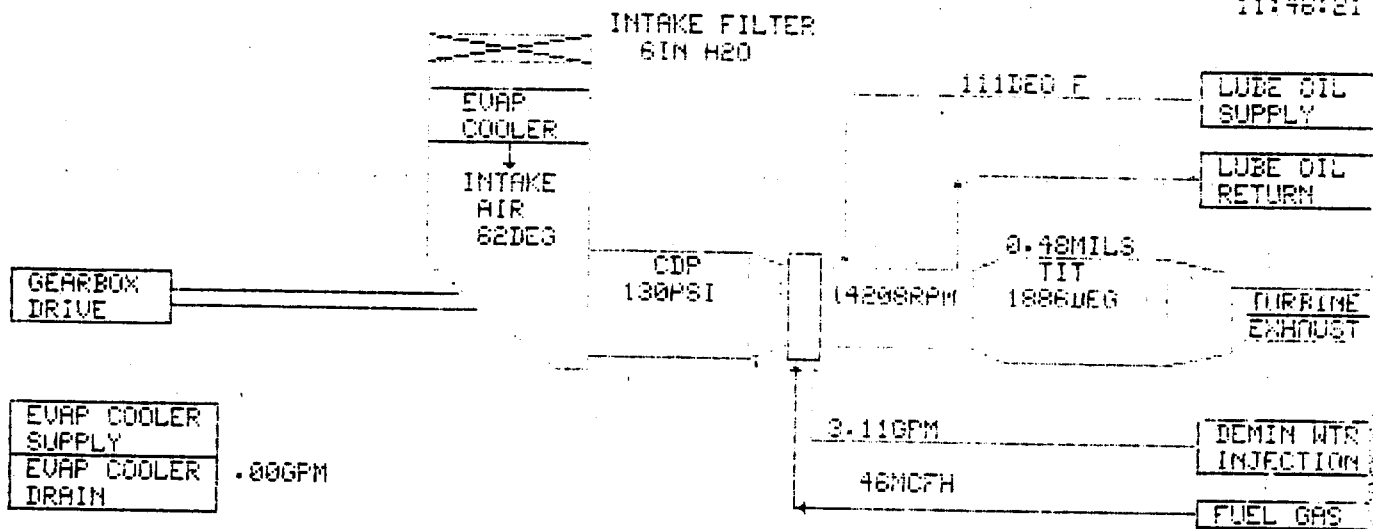
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/19/90 TIME: 11:46:26

T-1215 TURBINE INSTRUMENTATION

19/SEP/90  
11:46:21



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DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/19/90 TIME: 12:04:23

19/SEP/90

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11/09/90

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|-----------------------|----------------|
| FUEL GAS 548.4100 MCF | 24 HR RUNNING  |
| FUEL GAS 1075.172 MCF | 24 HR PREVIOUS |
| FUEL GAS 2701.015 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.784 MCF | 7 DAY PREVIOUS |
| FUEL GAS 19033.01 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 556.5137 MCF | 24 HR RUNNING  |
| FUEL GAS 1090.953 MCF | 24 HR PREVIOUS |
| FUEL GAS 2740.750 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20295.73 MCF | MONTH RUNNING  |
| FUEL GAS 33160.49 MCF | MONTH PREVIOUS |

0.72 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 1123.784 MCF | 24 HR RUNNING  |
| FUEL GAS 2195.396 MCF | 24 HR PREVIOUS |
| FUEL GAS 5521.145 MCF | 7 DAY RUNNING  |
| FUEL GAS 15429.59 MCF | 7 DAY PREVIOUS |
| FUEL GAS 39804.82 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.74 RATIO

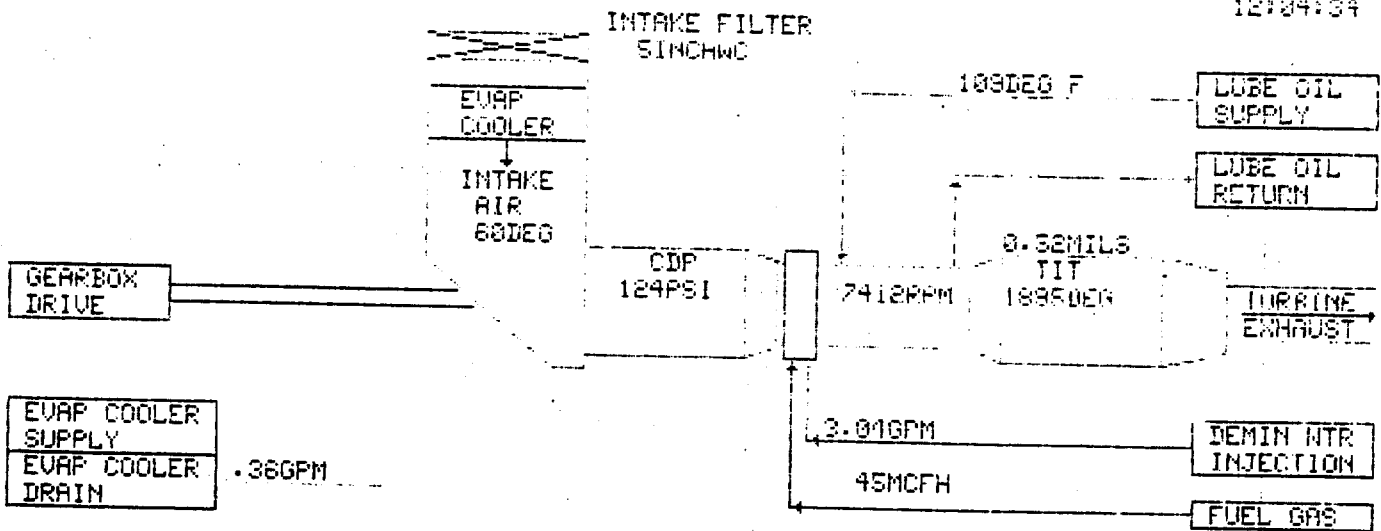
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DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/19/90 TIME: 12:04:39

1-181A CURRENT DISPOSITION

18/SEP/94  
12:04:39



COPY IN PROGRESS

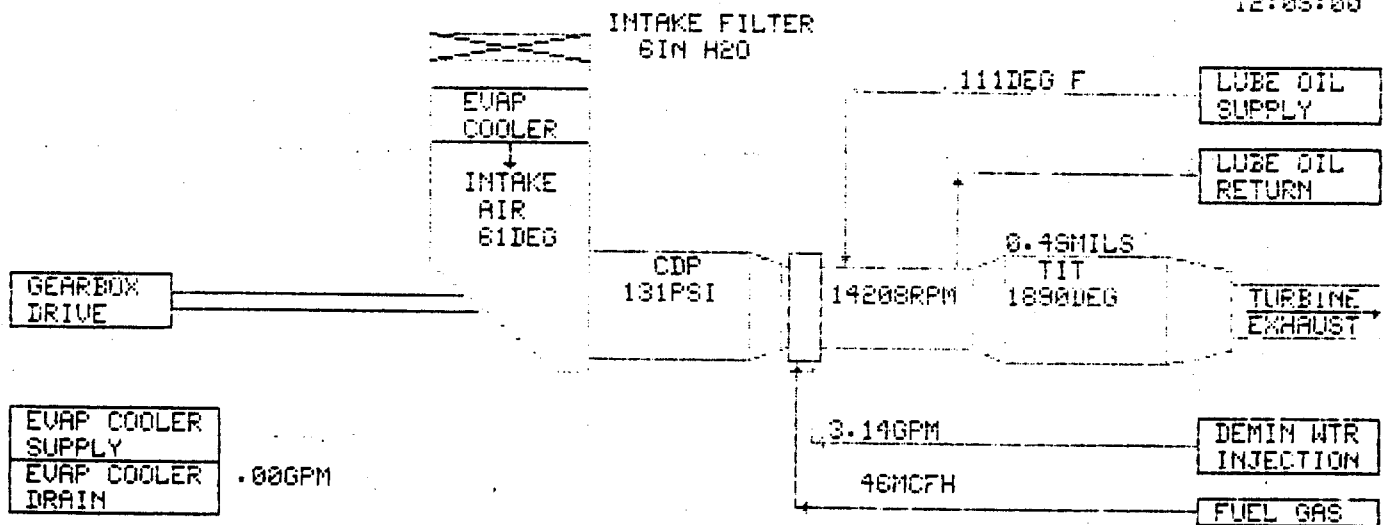
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DATE: 09/19/90

TIME: 12:05:05

TG-1015 TURBINE DIS-PUMINATION

19/SEP/90  
12:05:00



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DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/19/90 TIME: 12:37:17

18/SEP/90

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18/SEP/90

|                       |                |
|-----------------------|----------------|
| FUEL GAS 573.1163 MCF | 24 HR RUNNING  |
| FUEL GAS 1075.172 MCF | 24 HR PREVIOUS |
| FUEL GAS 2725.705 MCF | 7 DAY RUNNING  |
| FUEL GAS 7538.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 19056.21 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 581.6487 MCF | 24 HR RUNNING  |
| FUEL GAS 1090.859 MCF | 24 HR PREVIOUS |
| FUEL GAS 2765.876 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20322.35 MCF | MONTH RUNNING  |
| FUEL GAS 33160.49 MCF | MONTH PREVIOUS |

0.73 RATIO

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|-----------------------|----------------|
| FUEL GAS 1174.208 MCF | 24 HR RUNNING  |
| FUEL GAS 2195.396 MCF | 24 HR PREVIOUS |
| FUEL GAS 5571.372 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 39858.65 MCF | MONTH RUNNING  |
| FUEL GAS 87366.09 MCF | MONTH PREVIOUS |

0.73 RATIO

COPY IN PROGRESS

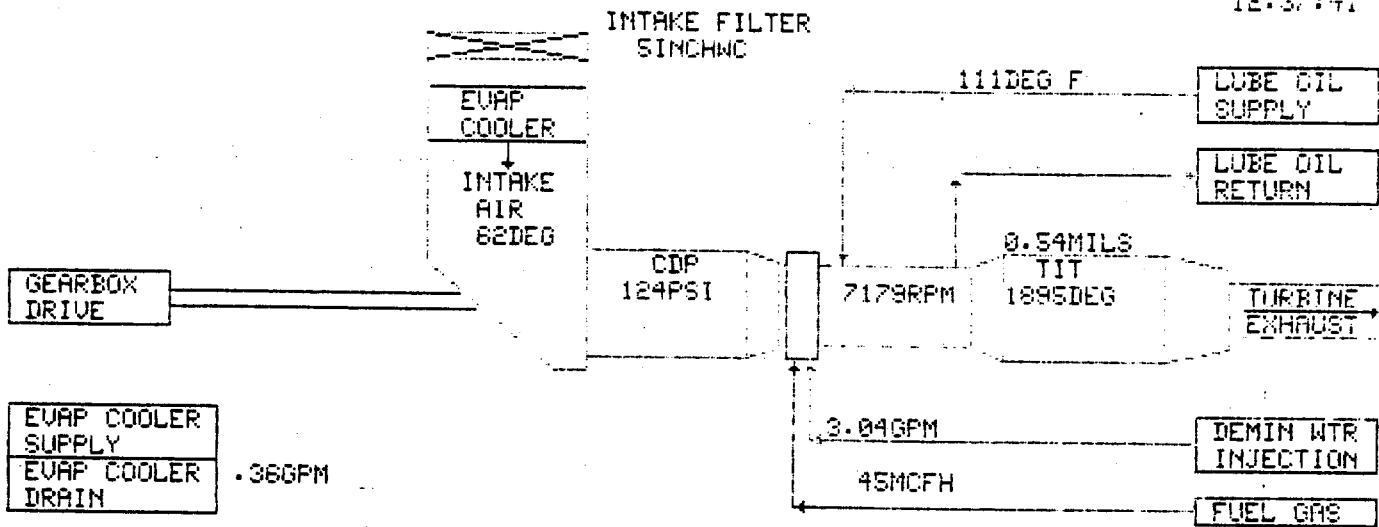


DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/19/90 TIME: 12:37:41

TG-1814 TURBINE INSTRUMENTATION

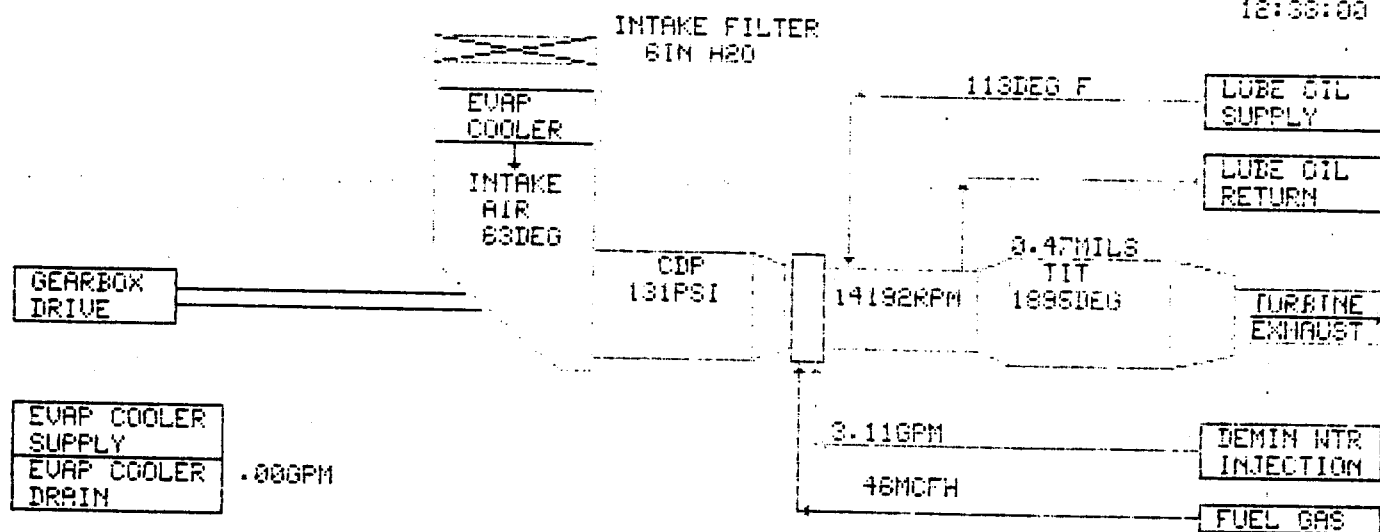
19/SEP/90  
12:37:41



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TIME: 12:38:05

19/SEP/90  
12:36:00



**COPY IN PROGRESS**

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/19/90 TIME: 12:59:23

19-SEP-90

0.73 99710

0.73 99710

|                       |                |
|-----------------------|----------------|
| FUEL GAS 589.6591 MCF | 24 HR RUNNING  |
| FUEL GAS 1075.172 MCF | 24 HR PREVIOUS |
| FUEL GAS 2742.237 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 19071.74 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 588.4753 MCF | 24 HR RUNNING  |
| FUEL GAS 1050.959 MCF | 24 HR PREVIOUS |
| FUEL GAS 2782.698 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20339.08 MCF | MONTH RUNNING  |
| FUEL GAS 33160.43 MCF | MONTH PREVIOUS |

0.73 99710

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|-----------------------|----------------|
| FUEL GAS 1207.903 MCF | 24 HR RUNNING  |
| FUEL GAS 2195.396 MCF | 24 HR PREVIOUS |
| FUEL GAS 5805.013 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.53 MCF | 7 DAY PREVIOUS |
| FUEL GAS 33890.52 MCF | MONTH RUNNING  |
| FUEL GAS 67386.09 MCF | MONTH PREVIOUS |

0.73 99710

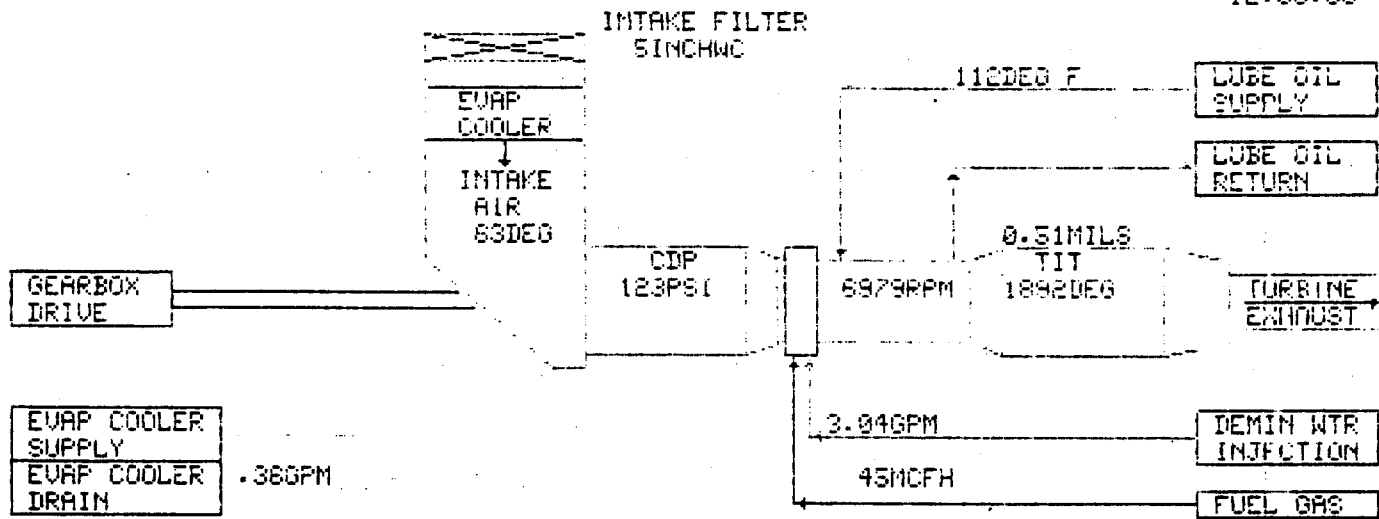
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DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/19/90 TIME: 12:59:41

TD-101A TURBINE INSTRUMENTATION

13/SEP/90  
12:33:38



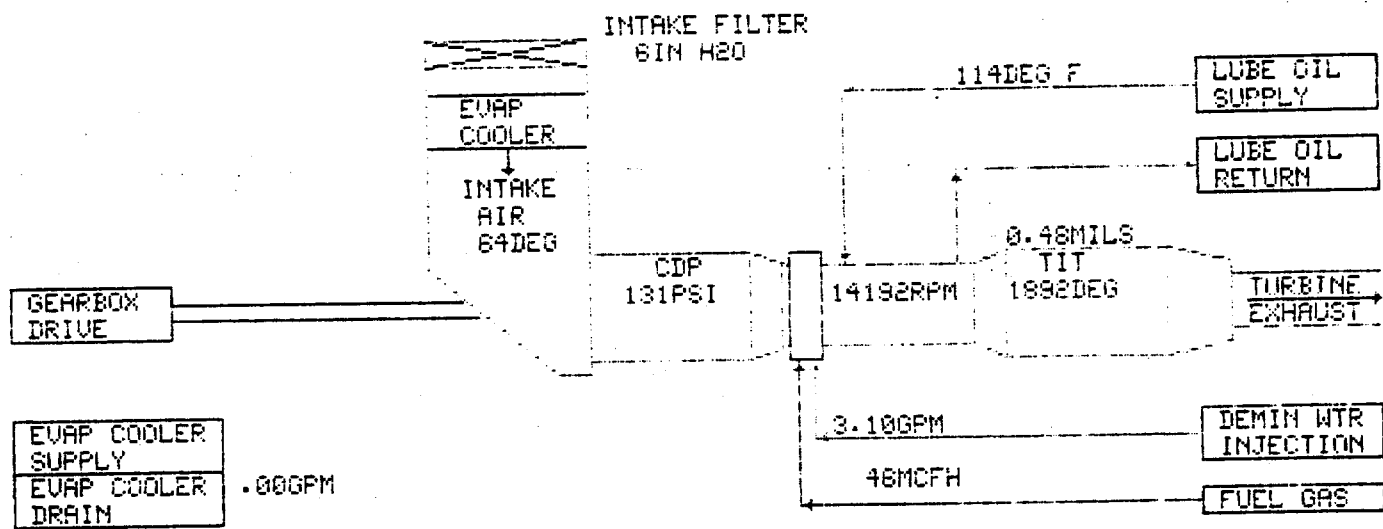
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/19/90 TIME: 13:00:00

T-1018 TURBINE INSTRUMENTATION

19/SEP/90  
12:53:53



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/19/90 TIME: 13:21:34

18/SEP/90

~~CONFIDENTIAL~~

18/SEP/90

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|-----------------------|----------------|
| FUEL GAS 606.2029 MCF | 24 HR RUNNING  |
| FUEL GAS 1075.172 MCF | 24 HR PREVIOUS |
| FUEL GAS 2758.788 MCF | 7 DAY RUNNING  |
| FUEL GAS 7538.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 19087.34 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 615.3093 MCF | 24 HR RUNNING  |
| FUEL GAS 1090.953 MCF | 24 HR PREVIOUS |
| FUEL GAS 2799.555 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20355.24 MCF | MONTH RUNNING  |
| FUEL GAS 33180.49 MCF | MONTH PREVIOUS |

0.73 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 1241.593 MCF | 24 HR RUNNING  |
| FUEL GAS 2195.396 MCF | 24 HR PREVIOUS |
| FUEL GAS 5638.810 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 39924.94 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.74 RATIO

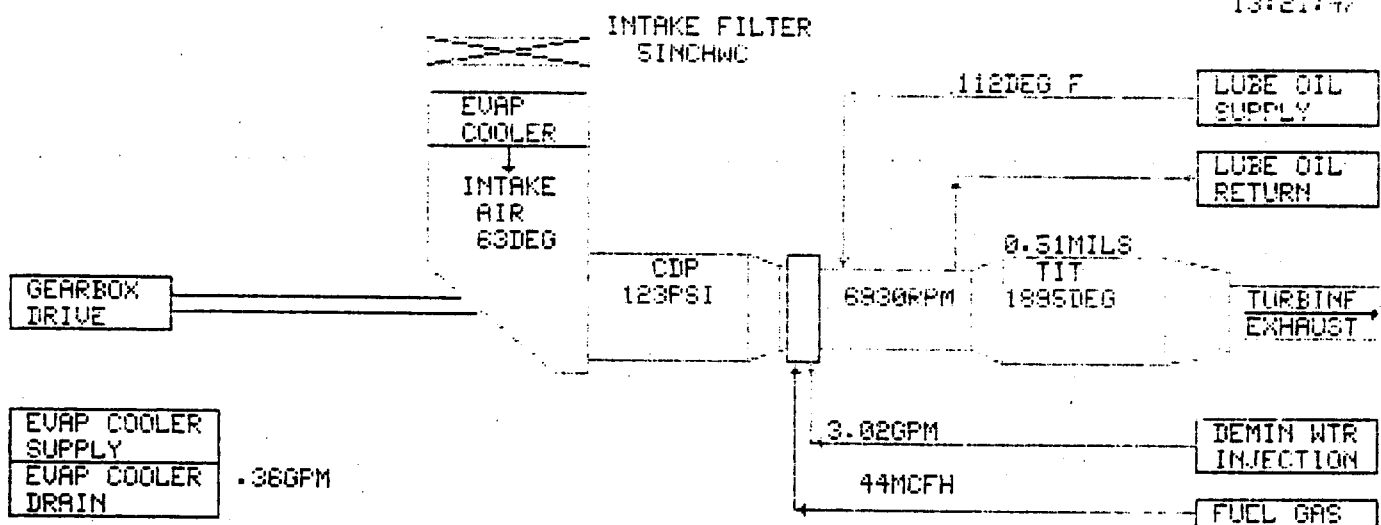
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DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/19/90 TIME: 13:21:51

TURBINE FUEL SYSTEM INSTRUMENTATION

18/SAP/90  
13:21:47



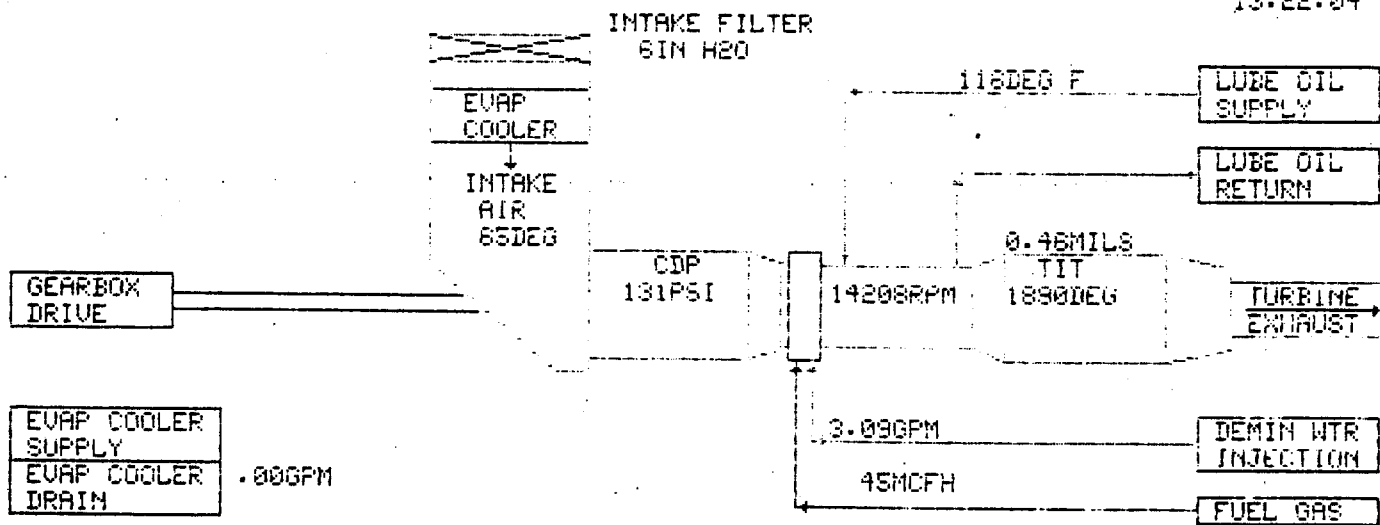
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/19/90 TIME: 13:22:09

TG-101B TURBINE INSTRUMENTATION

19/SEP/90  
13:22:04



COPY IN PROGRESS



DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/19/90 TIME: 13:41:15

SEP-90

**147000000**

**147000000**

**147000000**

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|-----------------------|----------------|
| FUEL GAS 620.8849 MCF | 24 HR RUNNING  |
| FUEL GAS 1673.172 MCF | 24 HR PREVIOUS |
| FUEL GAS 2773.473 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 19101.17 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 630.2517 MCF | 24 HR RUNNING  |
| FUEL GAS 1050.953 MCF | 24 HR PREVIOUS |
| FUEL GAS 2814.511 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20369.79 MCF | MONTH RUNNING  |
| FUEL GAS 33166.43 MCF | MONTH PREVIOUS |

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0.72 RATIO

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|-----------------------|----------------|
| FUEL GAS 1271.487 MCF | 24 HR RUNNING  |
| FUEL GAS 2195.396 MCF | 24 HR PREVIOUS |
| FUEL GAS 5668.771 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 39954.00 MCF | MONTH RUNNING  |
| FUEL GAS 67386.09 MCF | MONTH PREVIOUS |

0.73 RATIO

**COPY IN PROGRESS**

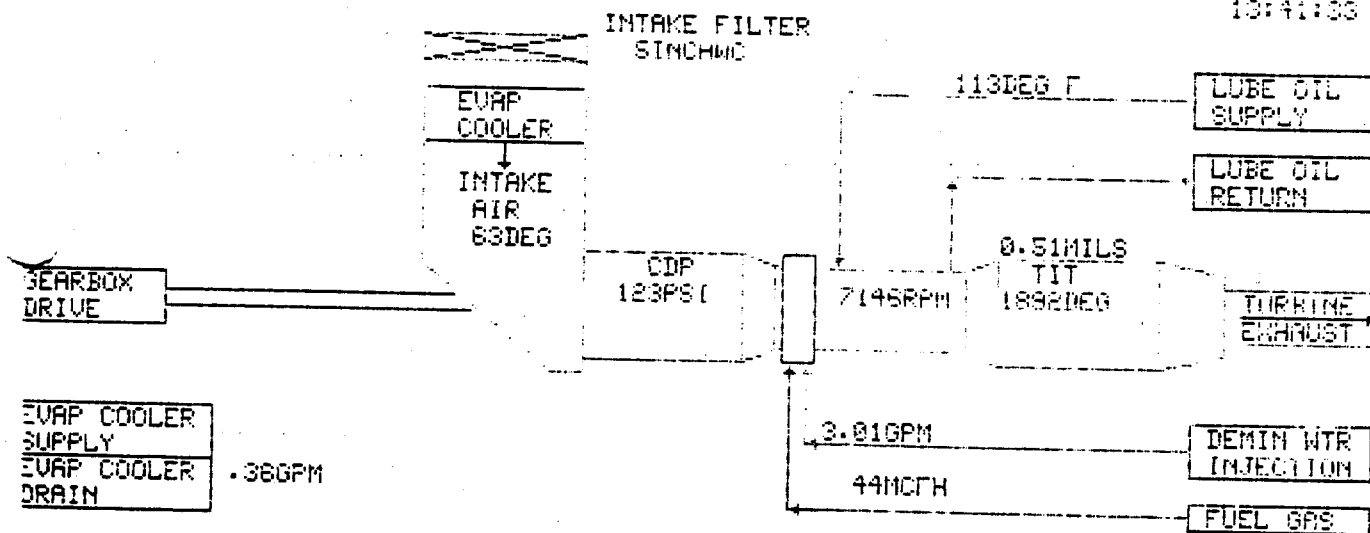
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DATE: 09/19/90

TIME: 13:41:37

70-101R TURBINE INSTRUMENTATION

13/SEP/90  
13:41:33



COPY IN PROGRESS

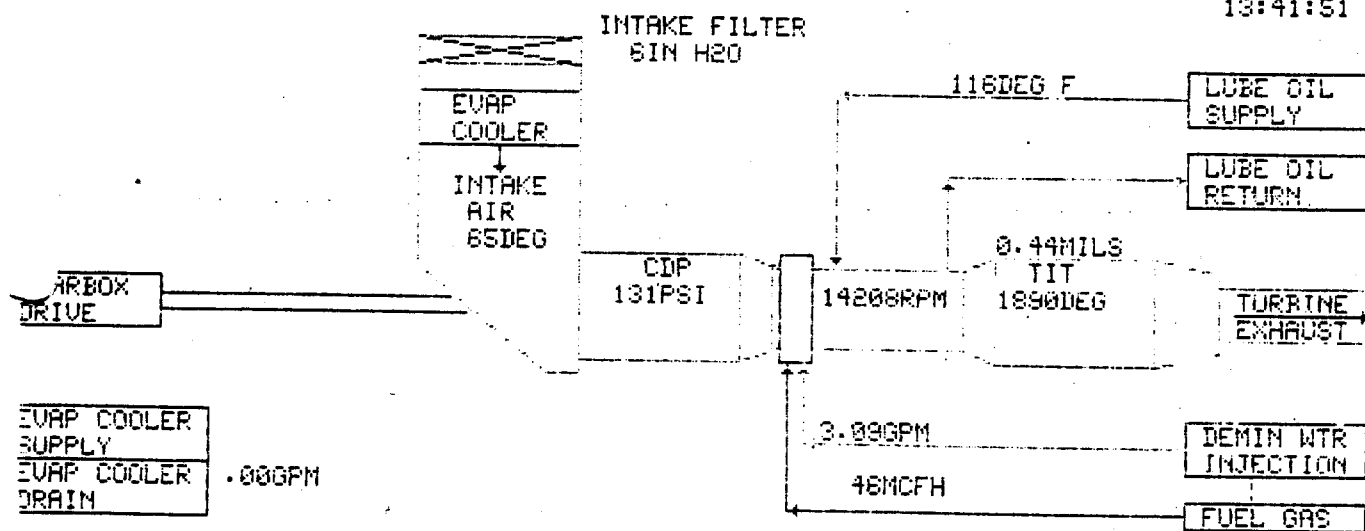
DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/19/90

TIME: 13:41:56

10-101B TURBINE INSTRUMENTATION

19/SEP/90  
13:41:51



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DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/19/90 TIME: 14:00:17

10/5/90 30

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FUEL GAS 635.0634 MCF 24 HR RUNNING  
FUEL GAS 1075.172 MCF 24 HR PREVIOUS

FUEL GAS 2787.654 MCF 7 DAY RUNNING  
FUEL GAS 7588.764 MCF 7 DAY PREVIOUS

FUEL GAS 19114.56 MCF MONTH RUNNING  
FUEL GAS 31982.16 MCF MONTH PREVIOUS

FUEL GAS 644.6689 MCF 24 HR RUNNING  
FUEL GAS 1090.959 MCF 24 HR PREVIOUS

FUEL GAS 2828.948 MCF 7 DAY RUNNING  
FUEL GAS 7674.877 MCF 7 DAY PREVIOUS

FUEL GAS 20383.43 MCF MONTH RUNNING  
FUEL GAS 33160.48 MCF MONTH PREVIOUS

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0.73 RATIO

FUEL GAS 1300.350 MCF 24 HR RUNNING  
FUEL GAS 2195.396 MCF 24 HR PREVIOUS

0.73 RATIO

FUEL GAS 5637.788 MCF 7 DAY RUNNING  
FUEL GAS 15436.58 MCF 7 DAY PREVIOUS

FUEL GAS 39980.85 MCF MONTH RUNNING  
FUEL GAS 67366.09 MCF MONTH PREVIOUS

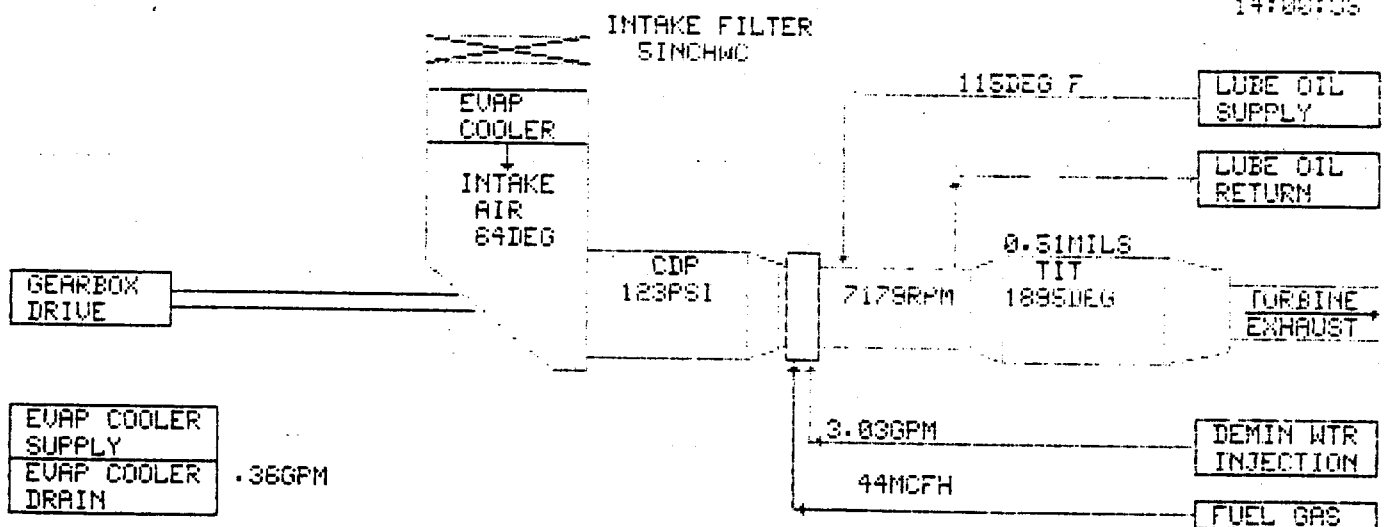
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DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/19/90 TIME: 14:00:39

PH-121A BLASTING INSTRUMENTATION

19/SEP/90  
14:00:35



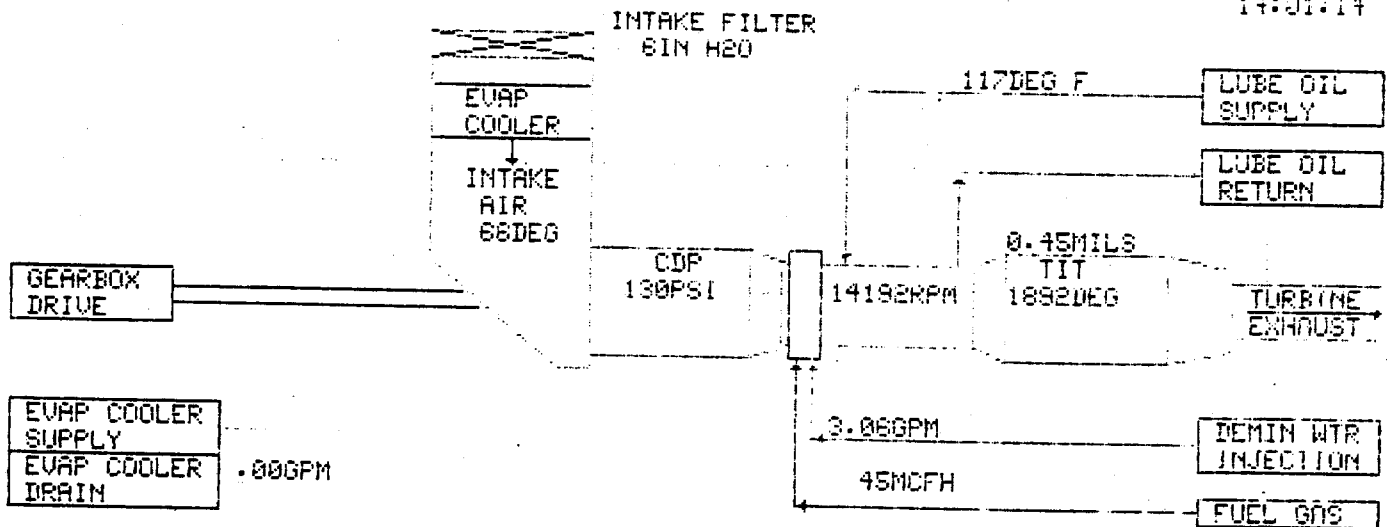
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/19/90 TIME: 14:01:19

TG-1012 TURBINE INSTRUMENTATION

19/SEP/90  
14:01:19



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/20/90 TIME: 09:33:34

20-SEP-90

ACR-2111-10-2-3-3

09:33:32

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|-----------------------|----------------|
| FUEL GAS 429.4771 MCF | 24 HR RUNNING  |
| FUEL GAS 1081.823 MCF | 24 HR PREVIOUS |
| FUEL GAS 3663.883 MCF | 7 DAY RUNNING  |
| FUEL GAS 7388.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 19940.26 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 436.0505 MCF | 24 HR RUNNING  |
| FUEL GAS 1036.213 MCF | 24 HR PREVIOUS |
| FUEL GAS 3716.628 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.377 MCF | 7 DAY PREVIOUS |
| FUEL GAS 21247.41 MCF | MONTH RUNNING  |
| FUEL GAS 33160.48 MCF | MONTH PREVIOUS |

0.74 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 879.7786 MCF | 24 HR RUNNING  |
| FUEL GAS 2211.638 MCF | 24 HR PREVIOUS |
| FUEL GAS 7490.572 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 41788.86 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.74 RATIO

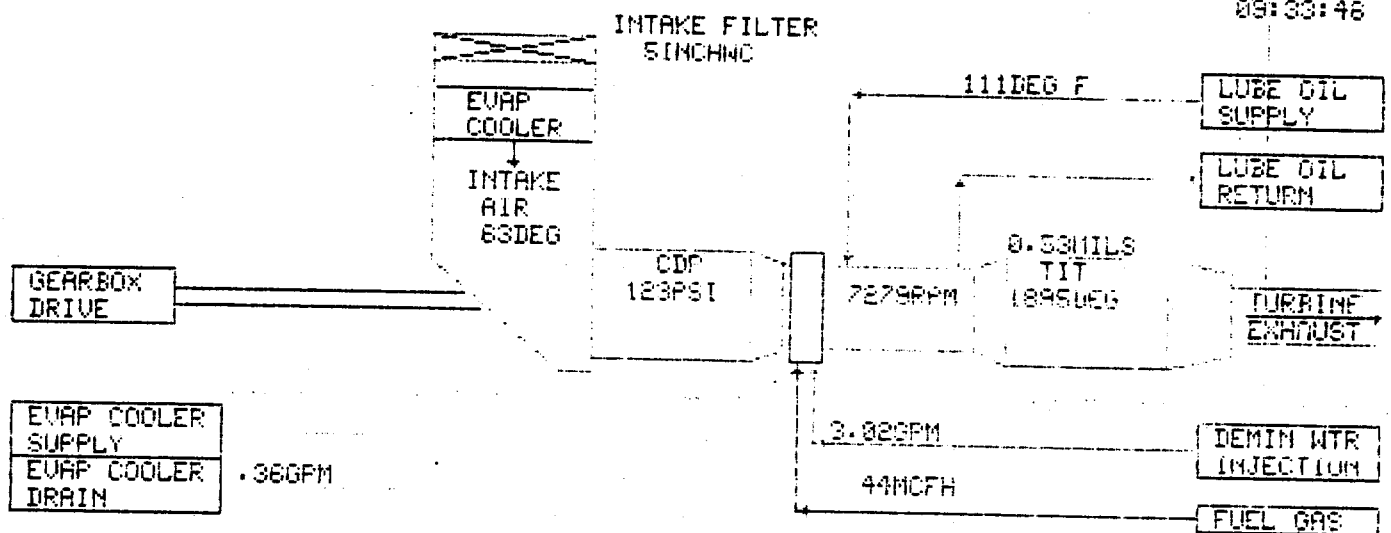
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DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/20/90 TIME: 09:33:50

TG-101A TURBINE INSTRUMENTATION

20/SEP/90  
09:33:46



COPY IN PROGRESS

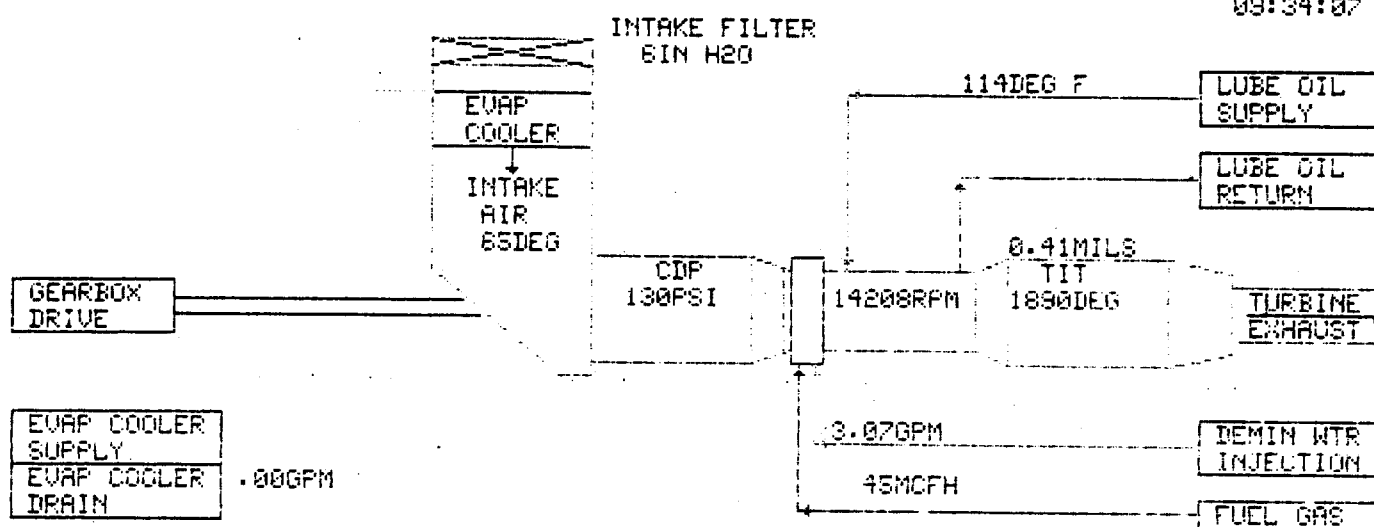


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DATE: 09/20/90 TIME: 09:34:12

TG-101B TURBINE INSTRUMENTATION

20/SEP/90  
09:34:07



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DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/20/90 TIME: 10:26:02

10/SEP/90

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1012-101

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|-----------------------|----------------|
| FUEL GAS 468.3777 MCF | 24 HR RUNNING  |
| FUEL GAS 1081.823 MCF | 24 HR PREVIOUS |
| FUEL GAS 3702.833 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 19977.15 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 475.5262 MCF | 24 HR RUNNING  |
| FUEL GAS 1066.213 MCF | 24 HR PREVIOUS |
| FUEL GAS 3758.094 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 21284.50 MCF | MONTH RUNNING  |
| FUEL GAS 33168.49 MCF | MONTH PREVIOUS |

0.73 BTU10

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|-----------------------|----------------|
| FUEL GAS 959.1521 MCF | 24 HR RUNNING  |
| FUEL GAS 2211.638 MCF | 24 HR PREVIOUS |
| FUEL GAS 7570.386 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 41862.47 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.73 BTU10

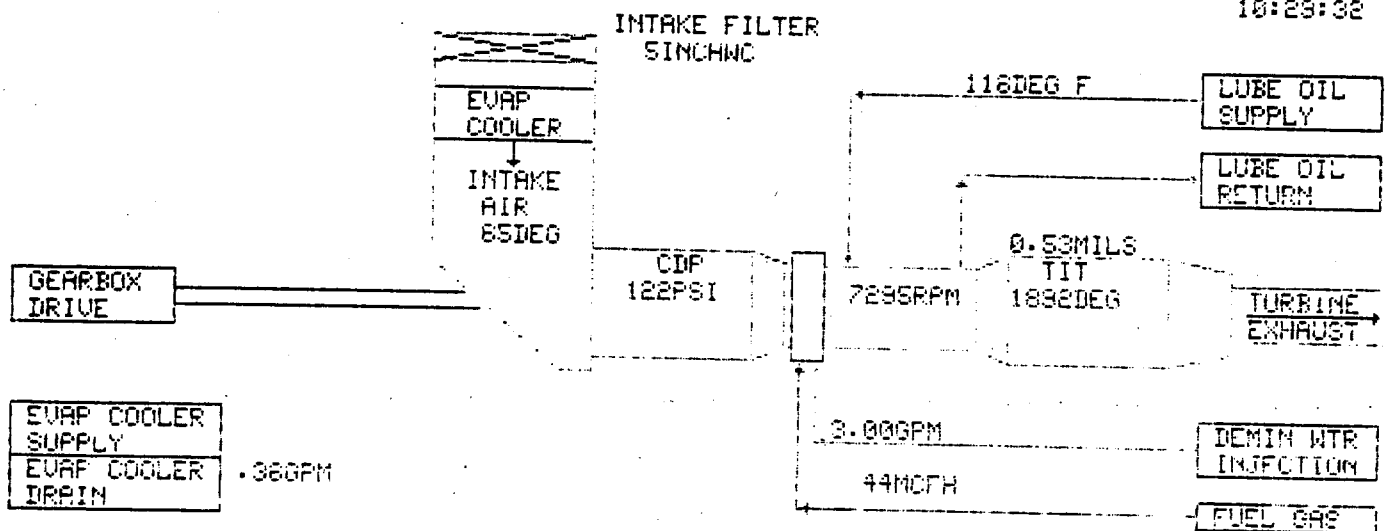
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DIAGRAM NUMBER: 2005      VERSION: 0

DATE: 09/20/90      TIME: 10:29:34

TG-101A TURBINE INSTRUMENTATION

28/SEP/90  
10:29:32



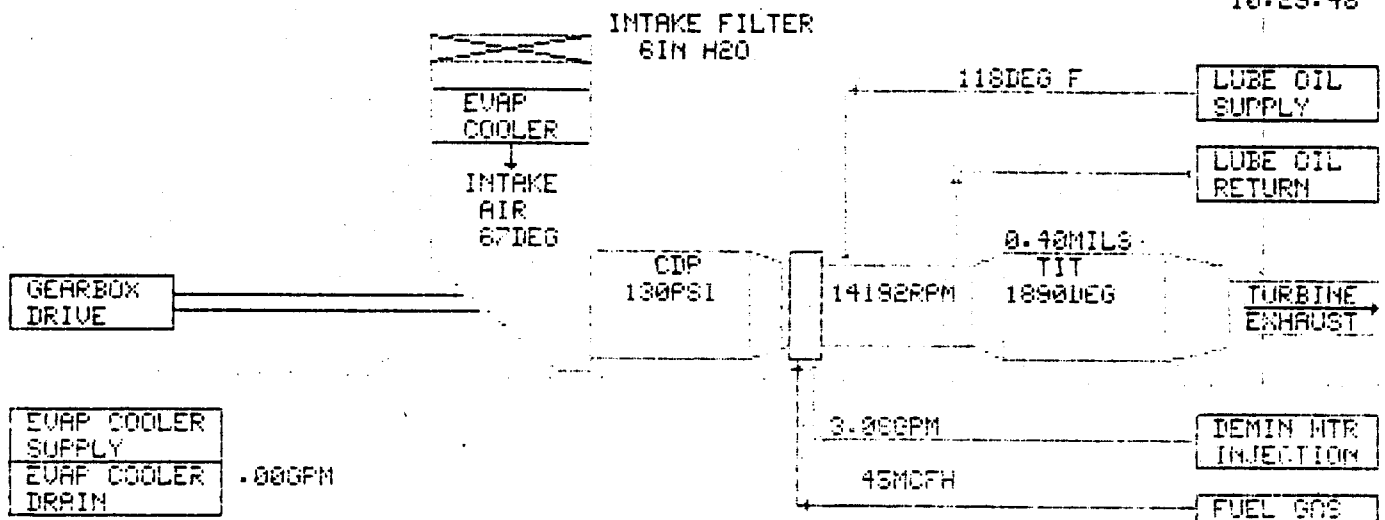
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/20/90 TIME: 10:29:50

TG-101B TURBINE INSTRUMENTATION

20/SEP/90  
10:29:48



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/20/90 TIME: 10:46:37

20/SEP/90

09/20/90 10:46:37

10:46:37

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|-----------------------|----------------|
| FUEL GAS 483.6721 MCF | 24 HR RUNNING  |
| FUEL GAS 1081.823 MCF | 24 HR PREVIOUS |
| FUEL GAS 3718.143 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.784 MCF | 7 DAY PREVIOUS |
| FUEL GAS 19991.65 MCF | MONTH RUNNING  |
| FUEL GAS 31982.18 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 491.0188 MCF | 24 HR RUNNING  |
| FUEL GAS 1090.213 MCF | 24 HR PREVIOUS |
| FUEL GAS 3773.573 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.677 MCF | 7 DAY PREVIOUS |
| FUEL GAS 21299.04 MCF | MONTH RUNNING  |
| FUEL GAS 33160.49 MCF | MONTH PREVIOUS |

0.73 88110

|                       |                |
|-----------------------|----------------|
| FUEL GAS 990.2777 MCF | 24 HR RUNNING  |
| FUEL GAS 2211.828 MCF | 24 HR PREVIOUS |
| FUEL GAS 7801.849 MCF | 7 DAY RUNNING  |
| FUEL GAS 15429.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 41831.44 MCF | MONTH RUNNING  |
| FUEL GAS 87388.09 MCF | MONTH PREVIOUS |

0.73 88110

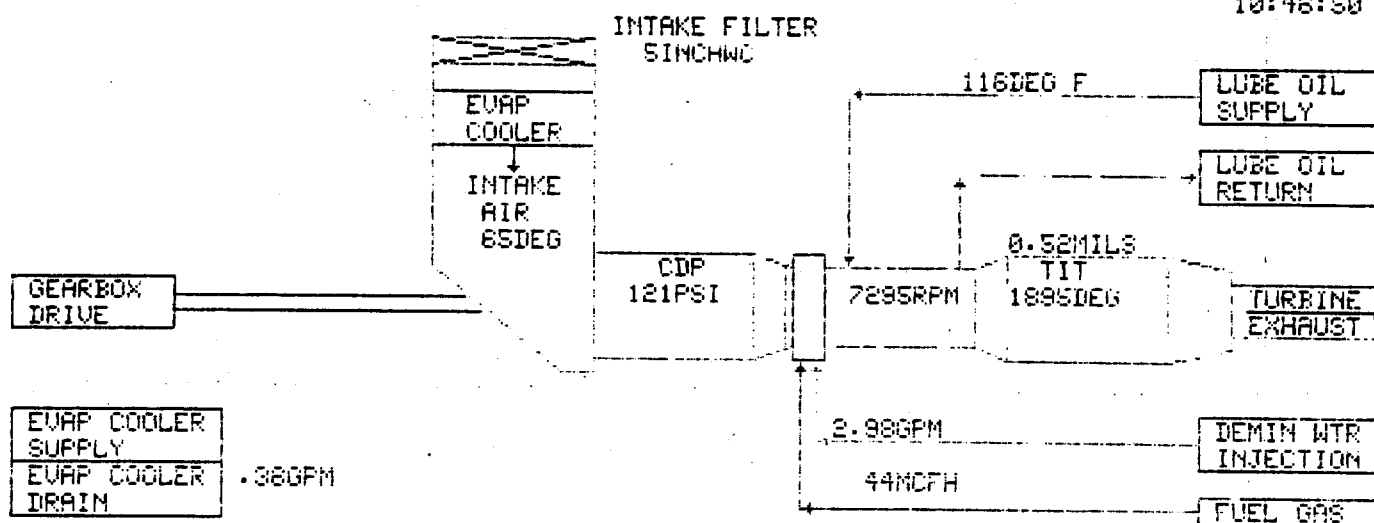
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DATE: 09/20/90 TIME: 10:46:55

TG-101A TURBINE INSTRUMENTATION

20/SEP/90  
10:46:50



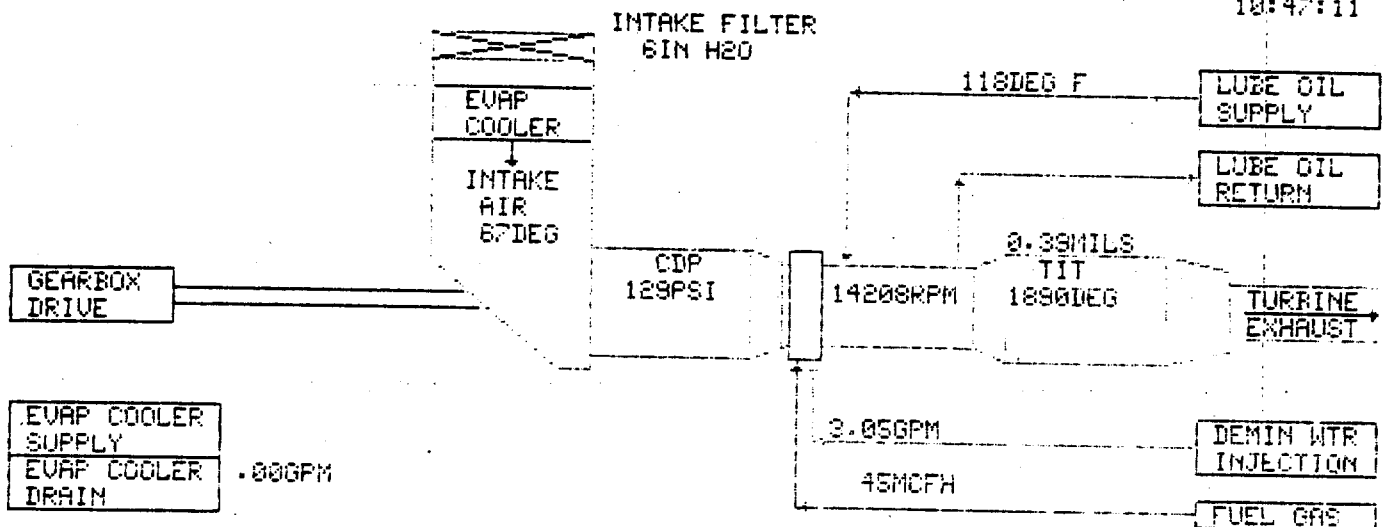
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/20/90 TIME: 10:47:13

TG-101B TURBINE INSTRUMENTATION

20/SEP/90  
10:47:11



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/20/90 TIME: 11:23:04

20/SEP/90

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11:23:03

|                       |                |
|-----------------------|----------------|
| FUEL GAS 510.6813 MCF | 24 HR RUNNING  |
| FUEL GAS 1081.823 MCF | 24 HR PREVIOUS |
| FUEL GAS 3745.143 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20017.27 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 518.4785 MCF | 24 HR RUNNING  |
| FUEL GAS 1098.213 MCF | 24 HR PREVIOUS |
| FUEL GAS 3801.024 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 21324.90 MCF | MONTH RUNNING  |
| FUEL GAS 33168.49 MCF | MONTH PREVIOUS |

0.72 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 1045.343 MCF | 24 HR RUNNING  |
| FUEL GAS 2211.638 MCF | 24 HR PREVIOUS |
| FUEL GAS 7858.774 MCF | 7 DAY RUNNING  |
| FUEL GAS 15438.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 41942.70 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.73 RATIO

COPY IN PROGRESS

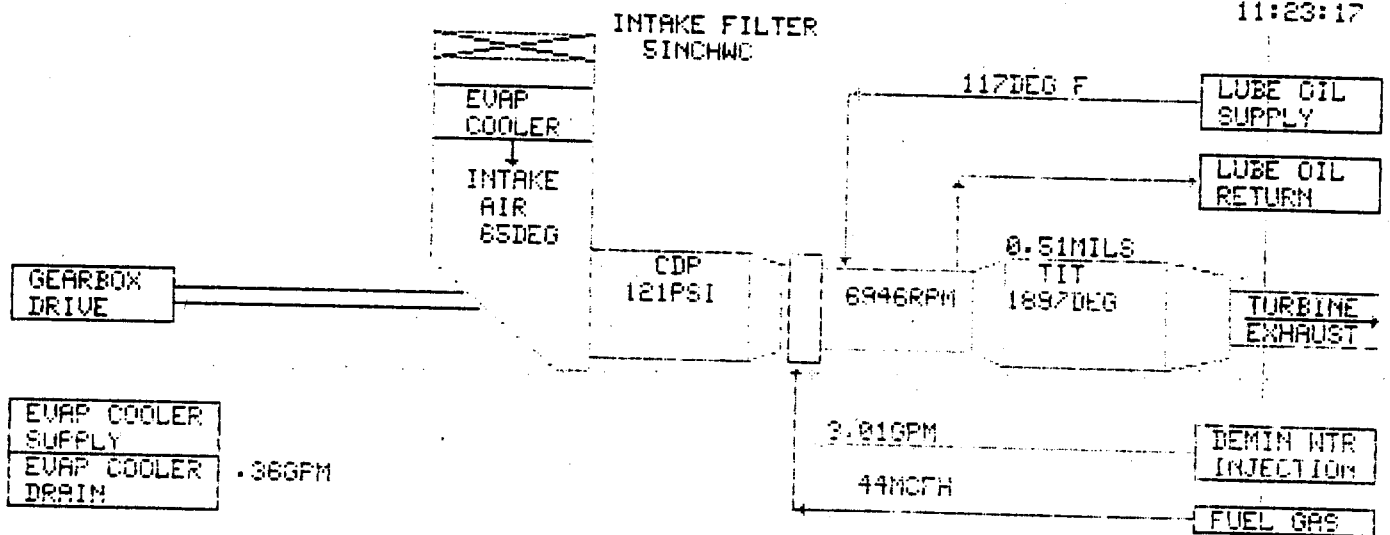


DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/20/90 TIME: 11:23:22

TG-181A TURBINE INSTRUMENTATION

20/SEP/90  
11:23:17



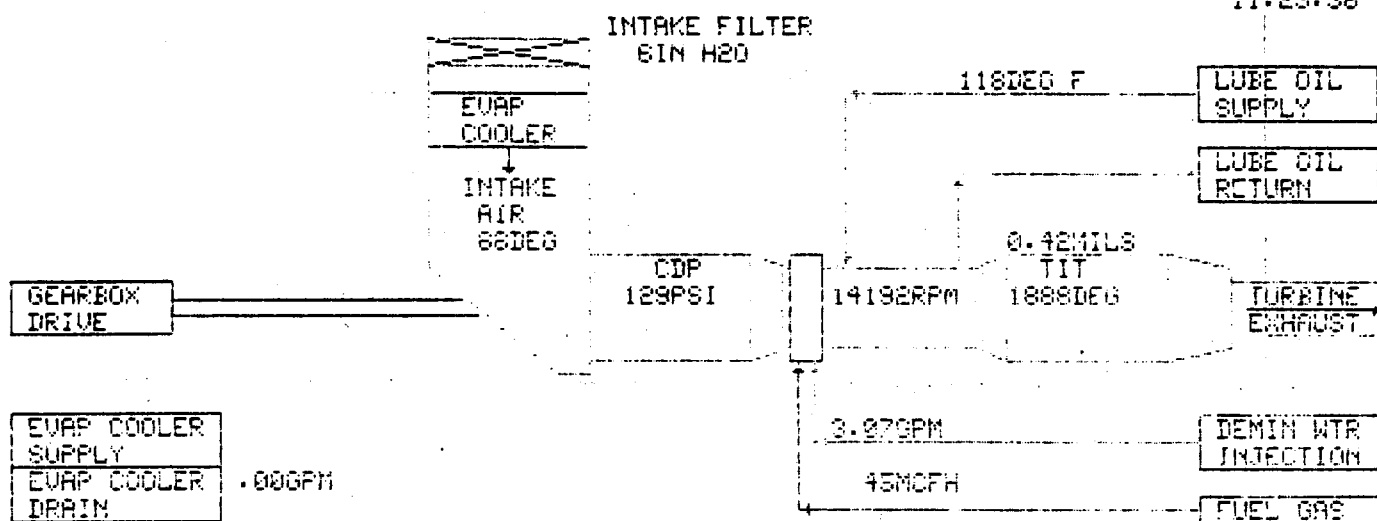
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DATE: 09/20/90 TIME: 11:23:40

TG-1015 TURBINE INSTRUMENTATION

20/SEP/90  
11:23:38



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DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/20/90 TIME: 11:39:57

09/20/90

09/20/90

11:39:55

|                       |                |
|-----------------------|----------------|
| FUEL GAS 523.1826 MCF | 24 HR RUNNING  |
| FUEL GAS 1081.823 MCF | 24 HR PREVIOUS |
| FUEL GAS 3757.648 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20029.14 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 531.2003 MCF | 24 HR RUNNING  |
| FUEL GAS 1090.213 MCF | 24 HR PREVIOUS |
| FUEL GAS 3813.748 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 21336.80 MCF | MONTH RUNNING  |
| FUEL GAS 33160.49 MCF | MONTH PREVIOUS |

0.73 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 1870.853 MCF | 24 HR RUNNING  |
| FUEL GAS 2211.938 MCF | 24 HR PREVIOUS |
| FUEL GAS 7882.401 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.59 MCF | 7 DAY PREVIOUS |
| FUEL GAS 41868.42 MCF | MONTH RUNNING  |
| FUEL GAS 67388.09 MCF | MONTH PREVIOUS |

0.73 RATIO

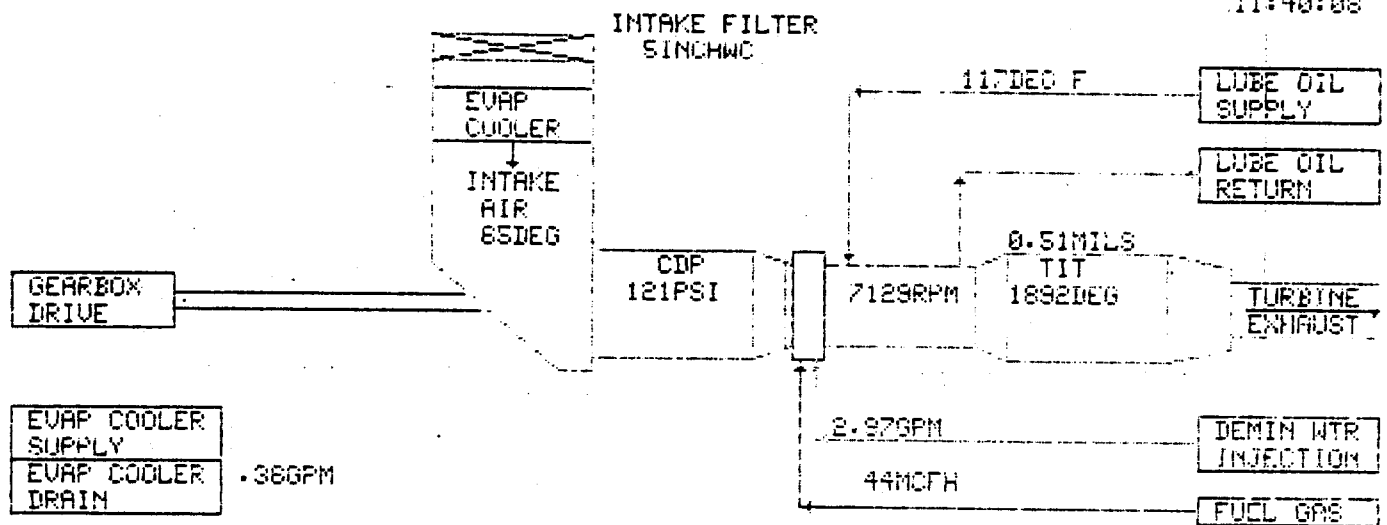
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DATE: 09/20/90 TIME: 11:40:12

TG-101A TURBINE INSTRUMENTATION

20/SEP/90  
11:40:08



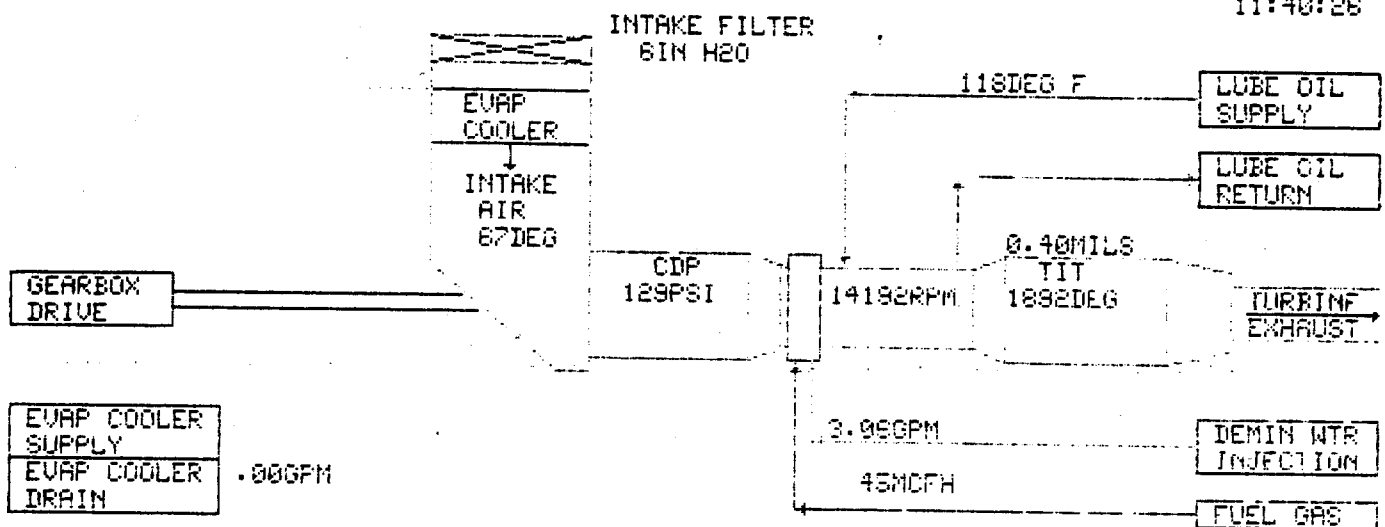
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/20/90 TIME: 11:40:31

TS-181B TURBINE INSTRUMENTATION

20/SEP/90  
11:40:26



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/20/90 TIME: 12:29:30

20/SEP/88

**GAS UTILIZATION**

12:29:30

|                       |                |                       |                |
|-----------------------|----------------|-----------------------|----------------|
| FUEL GAS 559.6349 MCF | 24 HR RUNNING  | FUEL GAS 568.4310 MCF | 24 HR RUNNING  |
| FUEL GAS 1081.823 MCF | 24 HR PREVIOUS | FUEL GAS 1098.213 MCF | 24 HR PREVIOUS |
| FUEL GAS 3794.102 MCF | 7 DAY RUNNING  | FUEL GAS 3850.952 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS | FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20063.97 MCF | MONTH RUNNING  | FUEL GAS 21371.89 MCF | MONTH RUNNING  |
| FUEL GAS 31982.18 MCF | MONTH PREVIOUS | FUEL GAS 33160.49 MCF | MONTH PREVIOUS |

**0.74 RATIO**

0.74 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 1145.263 MCF | 24 HR RUNNING  |
| FUEL GAS 2211.638 MCF | 24 HR PREVIOUS |
| FUEL GAS 7756.431 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.88 MCF | 7 DAY PREVIOUS |
| FUEL GAS 42036.10 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

**0.73 RATIO**

0.73 RATIO

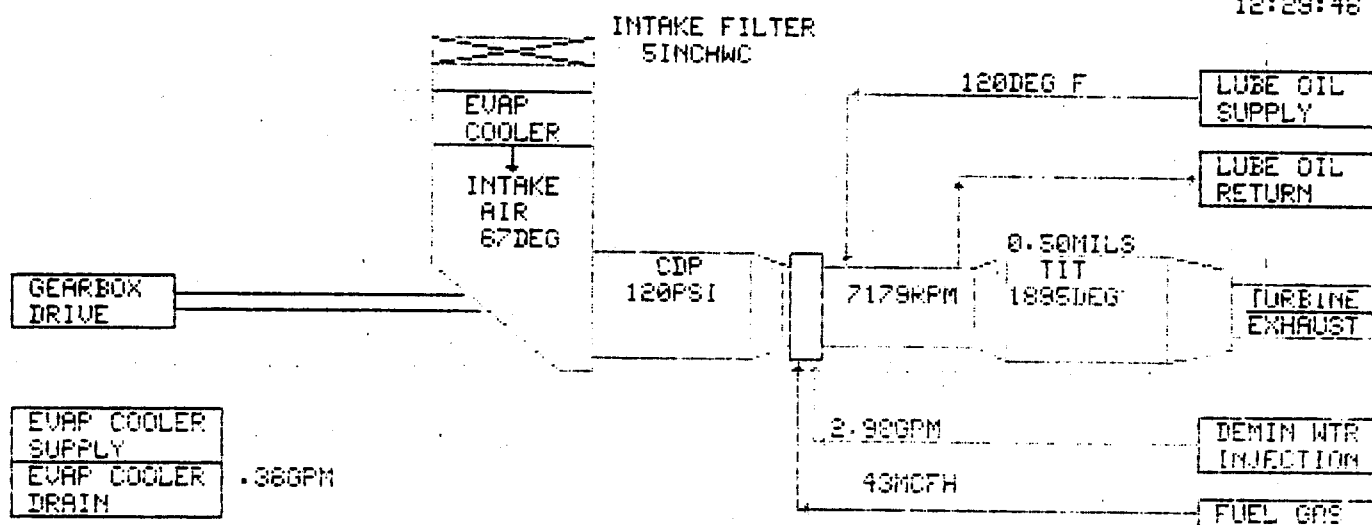
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DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/20/90 TIME: 12:29:51

TG-101A TURBINE INSTRUMENTATION

20/SEP/90  
12:29:46



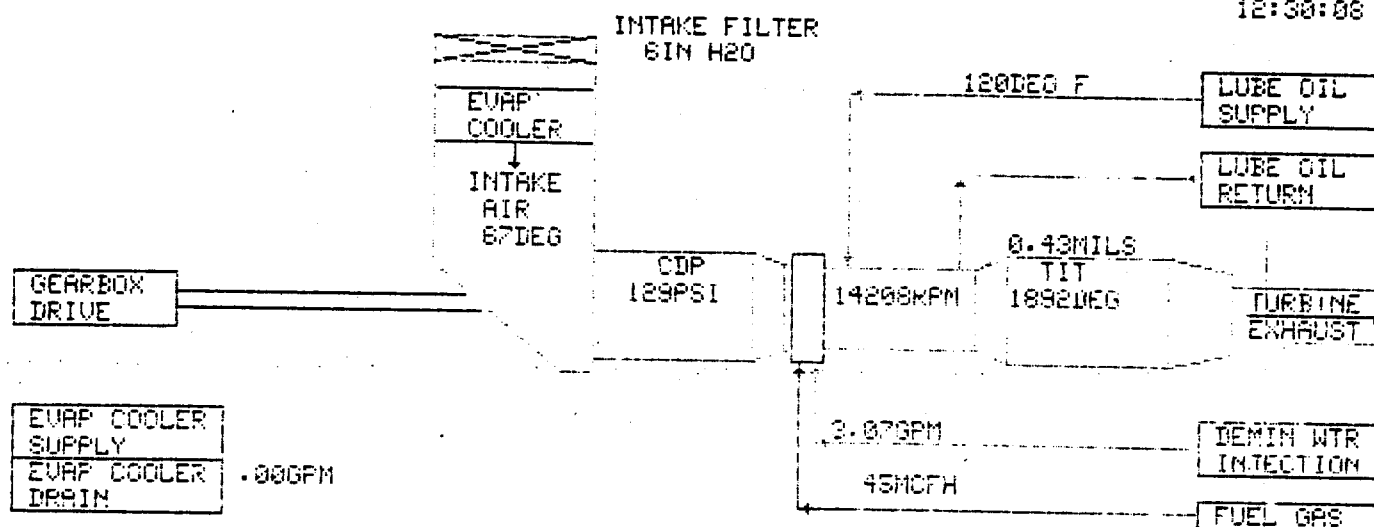
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DATE: 09/20/90 TIME: 12:30:08

TG-101B TURBINE INSTRUMENTATION

20/SEP/90  
12:30:08



COPY IN PROGRESS



DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/20/90 TIME: 12:48:01

10/SEP/90

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(214/15)

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|-----------------------|----------------|-----------------------|----------------|
| FUEL GAS 573.2182 MCF | 24 HR RUNNING  | FUEL GAS 582.3170 MCF | 24 HR RUNNING  |
| FUEL GAS 1081.823 MCF | 24 HR PREVIOUS | FUEL GAS 1098.213 MCF | 24 HR PREVIOUS |
| FUEL GAS 3807.681 MCF | 7 DAY RUNNING  | FUEL GAS 3864.831 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS | FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 28076.99 MCF | MONTH RUNNING  | FUEL GAS 21384.92 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS | FUEL GAS 33160.49 MCF | MONTH PREVIOUS |

0.72 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 1172.950 MCF | 24 HR RUNNING  |
| FUEL GAS 2211.638 MCF | 24 HR PREVIOUS |
| FUEL GAS 7784.898 MCF | 7 DAY RUNNING  |
| FUEL GAS 15438.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 42062.14 MCF | MONTH RUNNING  |
| FUEL GAS 67358.09 MCF | MONTH PREVIOUS |

0.74 RATIO

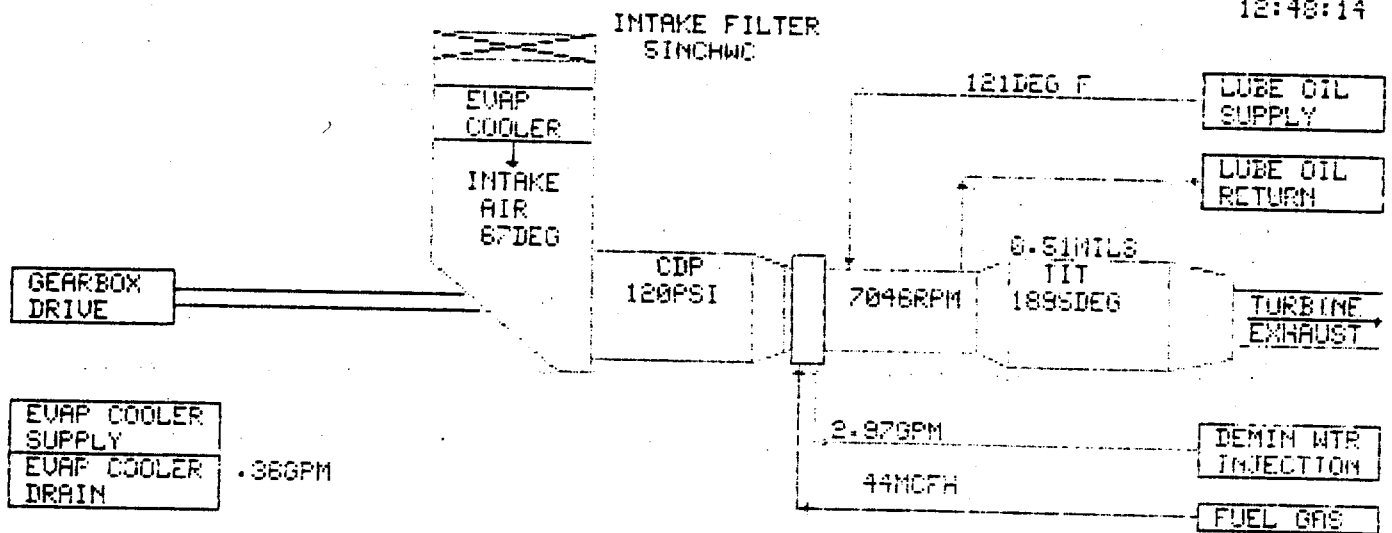
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DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/20/90 TIME: 12:48:19

TG-101A TURBINE INSTRUMENTATION

20/SEP/90  
12:48:14



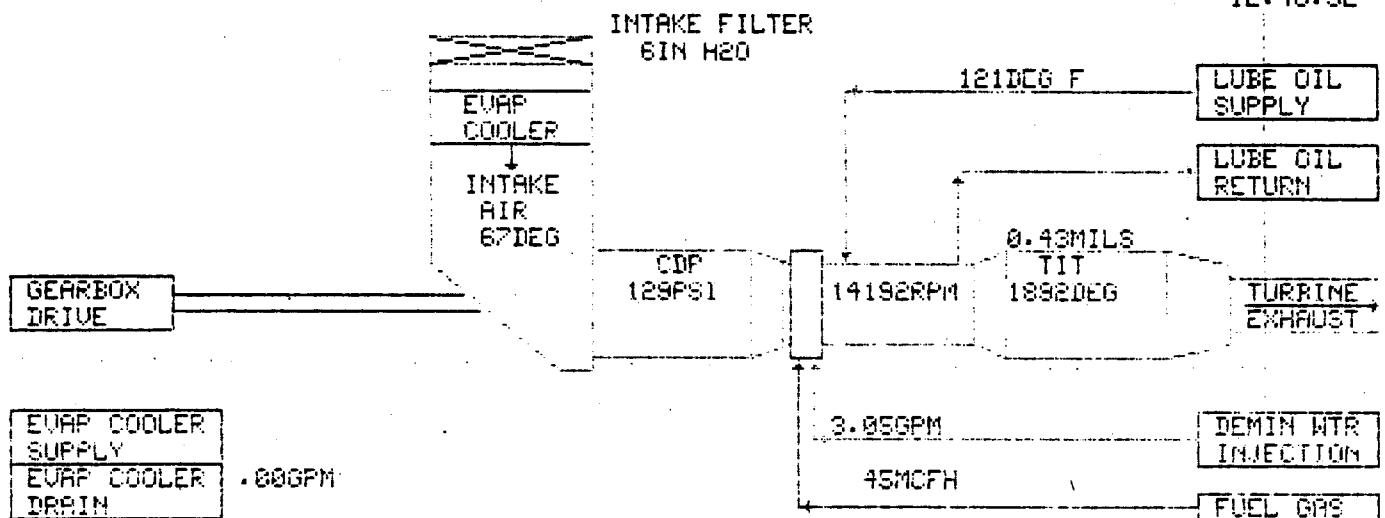
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/20/90 TIME: 12:48:36

TN-101B TURBINE INSTRUMENTATION

20/SEP/90  
12:48:32



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/20/90 TIME: 13:20:21

20/SEP/90

~~09/20/90 13:20:21~~

(3) 09:21

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|-----------------------|----------------|
| FUEL GAS 596.9731 MCF | 24 HR RUNNING  |
| FUEL GAS 1081.823 MCF | 24 HR PREVIOUS |
| FUEL GAS 3831.434 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20099.73 MCF | MONTH RUNNING  |
| FUEL GAS 31962.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 606.5720 MCF | 24 HR RUNNING  |
| FUEL GAS 1059.213 MCF | 24 HR PREVIOUS |
| FUEL GAS 3889.071 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 21407.71 MCF | MONTH RUNNING  |
| FUEL GAS 33160.49 MCF | MONTH PREVIOUS |

0.72 RATIO

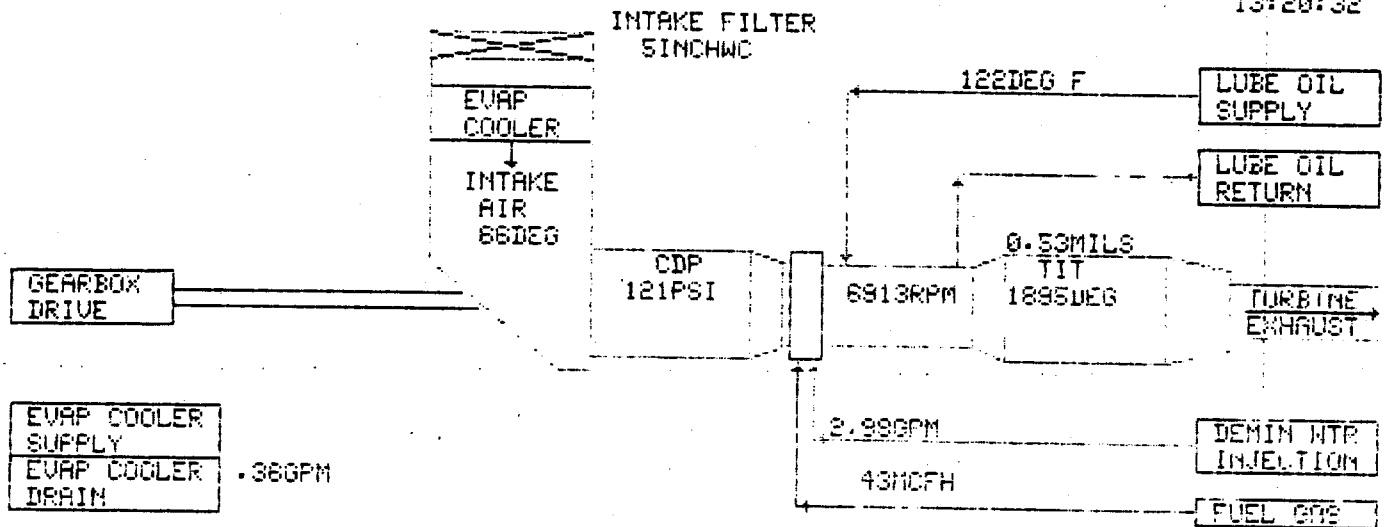
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|-----------------------|----------------|
| FUEL GAS 1221.430 MCF | 24 HR RUNNING  |
| FUEL GAS 2211.638 MCF | 24 HR PREVIOUS |
| FUEL GAS 7832.433 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 42107.63 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.73 RATIO

COPY IN PROGRESS

DATE: 09/20/90 TIME: 13:20:37

20/SEP/90  
13:20:32



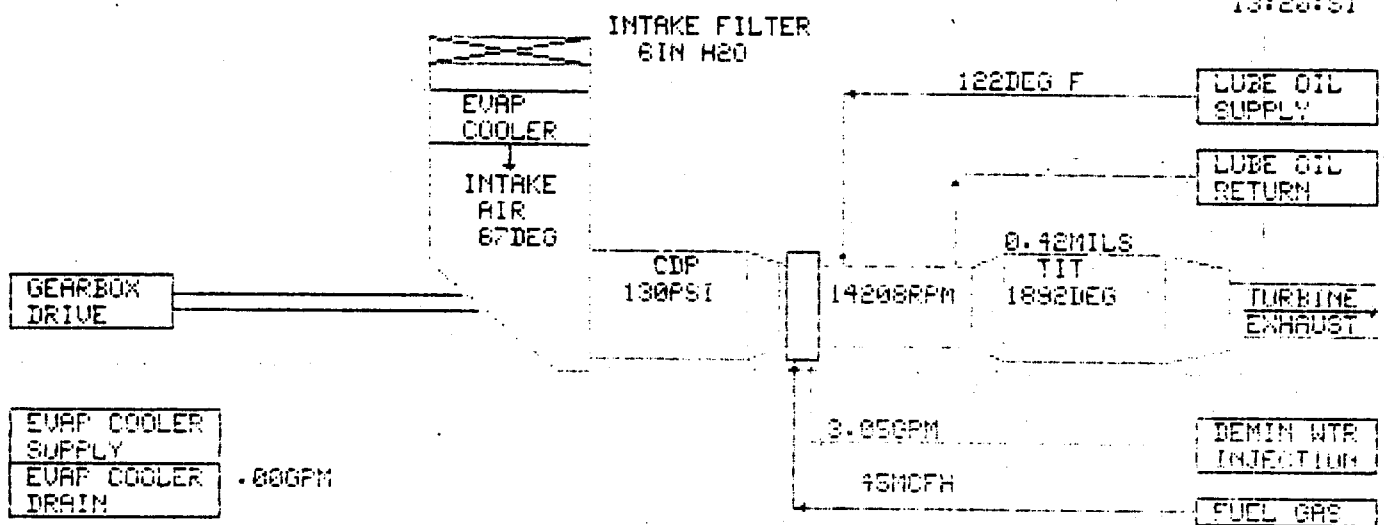
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DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/20/90 TIME: 13:20:56

TG-1018 TURBINE INSTRUMENTATION

20/SEP/90  
13:20:51



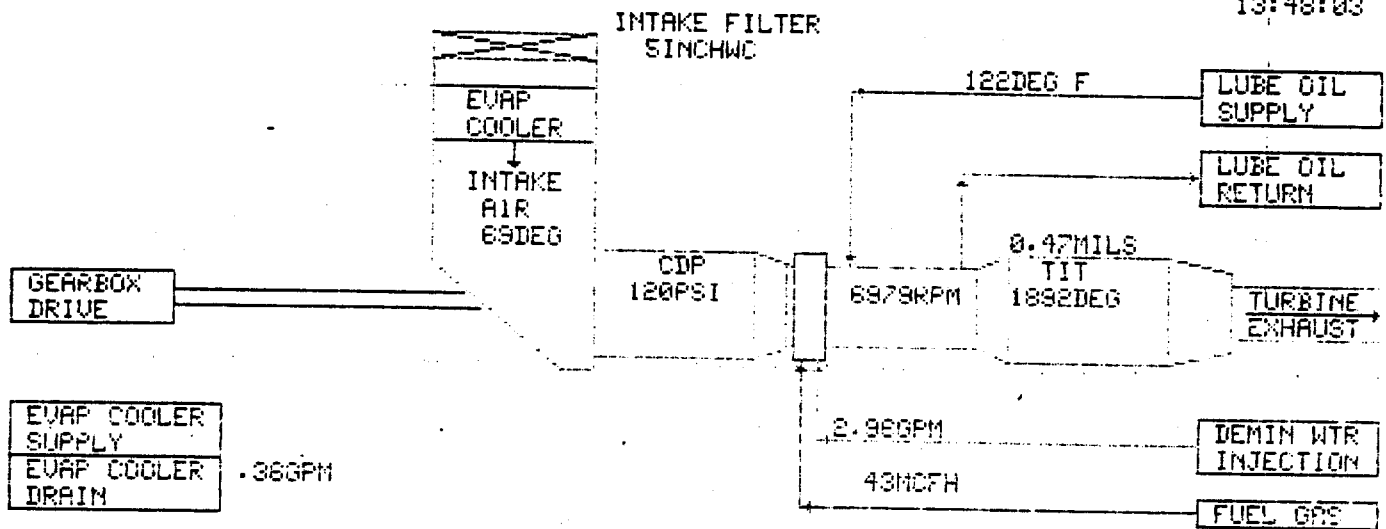
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DIAGRAM NUMBER: 2005 VERSION: 0

DATE: 09/20/90 TIME: 13:48:08

TG-101A TURBINE INSTRUMENTATION

20/SEP/90  
13:48:03



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/20/90 TIME: 13:47:52

09/20/90

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13:47:52

|                       |                |
|-----------------------|----------------|
| FUEL GAS 617.1351 MCF | 24 HR RUNNING  |
| FUEL GAS 1081.823 MCF | 24 HR PREVIOUS |
| FUEL GAS 3851.598 MCF | 7 DAY RUNNING  |
| FUEL GAS 7586.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20119.08 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 627.0920 MCF | 24 HR RUNNING  |
| FUEL GAS 1096.213 MCF | 24 HR PREVIOUS |
| FUEL GAS 3909.581 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 21427.07 MCF | MONTH RUNNING  |
| FUEL GAS 33160.49 MCF | MONTH PREVIOUS |

0.75 RATIO

|                       |                |
|-----------------------|----------------|
| FUEL GAS 1262.444 MCF | 24 HR RUNNING  |
| FUEL GAS 2211.638 MCF | 24 HR PREVIOUS |
| FUEL GAS 7873.543 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 42146.32 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.73 RATIO

COPY IN PROGRESS

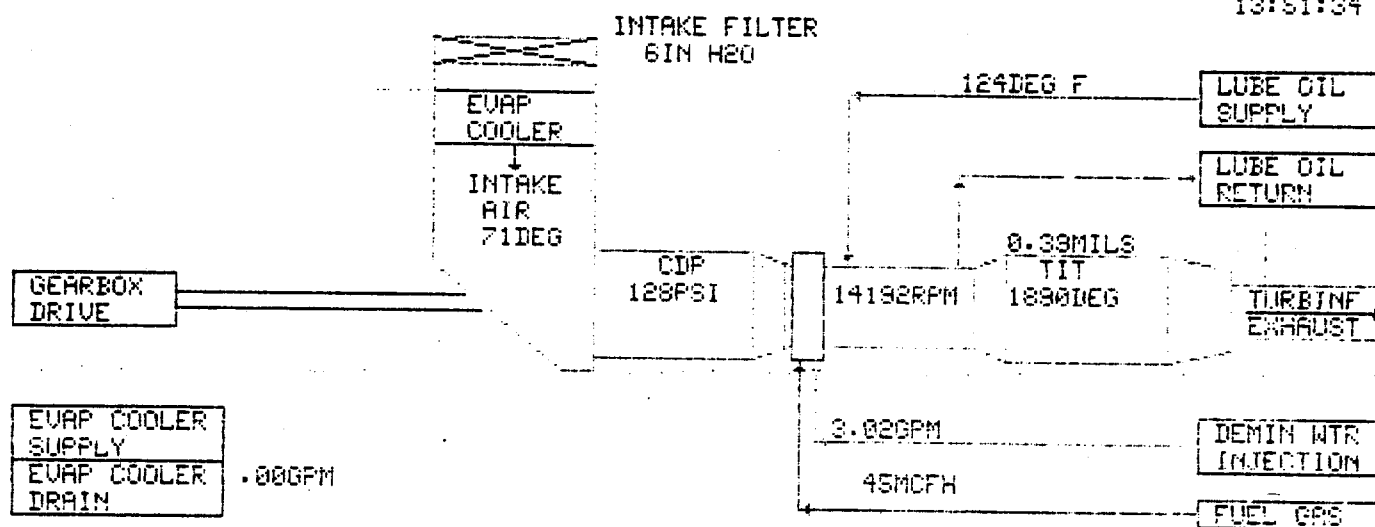


DIAGRAM NUMBER: 2011 VERSION: 0

DATE: 09/20/90 TIME: 13:51:36

TG-101B TURBINE INSTRUMENTATION

20/SEP/90  
13:51:34



COPY IN PROGRESS

DIAGRAM NUMBER: 3050 VERSION: 0

DATE: 09/20/90 TIME: 14:19:13

20 SEP 90

0.72 RATIO

14:19:13

|                       |                |
|-----------------------|----------------|
| FUEL GAS 640.0001 MCF | 24 HR RUNNING  |
| FUEL GAS 1081.823 MCF | 24 HR PREVIOUS |
| FUEL GAS 3874.468 MCF | 7 DAY RUNNING  |
| FUEL GAS 7588.764 MCF | 7 DAY PREVIOUS |
| FUEL GAS 20141.12 MCF | MONTH RUNNING  |
| FUEL GAS 31982.16 MCF | MONTH PREVIOUS |

|                       |                |
|-----------------------|----------------|
| FUEL GAS 650.3140 MCF | 24 HR RUNNING  |
| FUEL GAS 1098.213 MCF | 24 HR PREVIOUS |
| FUEL GAS 3932.815 MCF | 7 DAY RUNNING  |
| FUEL GAS 7674.877 MCF | 7 DAY PREVIOUS |
| FUEL GAS 21449.11 MCF | MONTH RUNNING  |
| FUEL GAS 33160.49 MCF | MONTH PREVIOUS |

0.72 RATIO

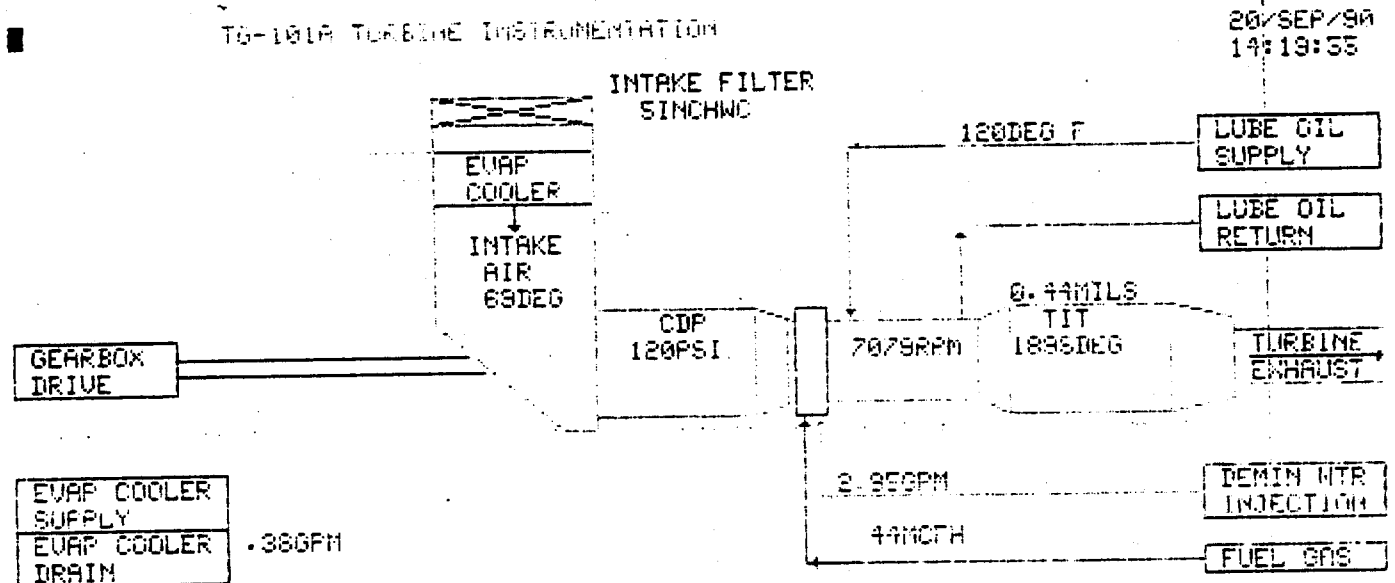
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|-----------------------|----------------|
| FUEL GAS 1308.840 MCF | 24 HR RUNNING  |
| FUEL GAS 2211.638 MCF | 24 HR PREVIOUS |
| FUEL GAS 7920.040 MCF | 7 DAY RUNNING  |
| FUEL GAS 15436.58 MCF | 7 DAY PREVIOUS |
| FUEL GAS 42190.41 MCF | MONTH RUNNING  |
| FUEL GAS 67366.09 MCF | MONTH PREVIOUS |

0.72 RATIO

COPY IN PROGRESS

DIAGRAM NUMBER: 2005 VERSION: 0

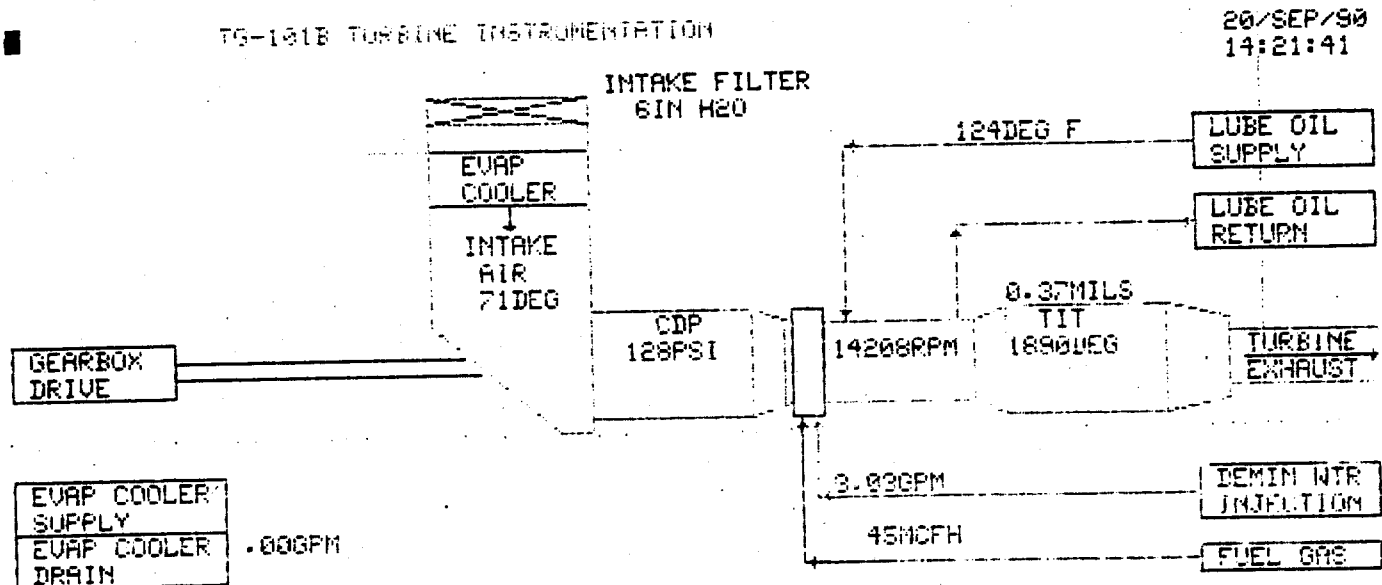
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DATE: 09/20/90 TIME: 14:21:43



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