

WA344

**SOURCE TEST REPORT AND RELATIVE ACCURACY AUDIT
SINGLE NATURAL GAS FIRED TURBINE
COALINGA COGENERATION COMPANY,
COALINGA, CALIFORNIA**

Prepared for:

**Coalinga Cogeneration Company
P.O. Box 81078
Bakersfield, California 93380**

For Submittal to:

**San Joaquin Valley Unified Air Pollution Control District
1999 Tuolumne St., Suite 200
Fresno, California 93721**

Test Dates:

March 4, 1993

Publication Date:

April 1, 1993

Prepared by:

**Engineering-Science, Inc.
2520 Pegasus Drive
Bakersfield, California 93308
(805)393-0272**

ES ENGINEERING-SCIENCE

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MAY 18 1993

San Joaquin Valley Unified
Air Pollution Control District



Coalinga Cogeneration Company

P.O. Box 81078, Bakersfield, CA 93380

(805) 392-2630

Gordon M. Thomson, Executive Director

May 17, 1993

CC-1349

Mr. Gary Martin
Source Test Supervisor
San Joaquin Valley Unified APCD
Central Region Office
1999 Tuolumne Street, Suite 200
Fresno, CA 93721

Re: **Non-Methane Hydrocarbon Source Test Results**

Dear Mr. Martin:

Pursuant to your conversation with Mervyn Soares on May 12, 1993, this letter is an addendum to the retest report for non-methane hydrocarbons ("NMHC") submitted April 16, 1993 (CC-1322). Coalinga Cogeneration Company's ("CCC") turbine fires on utility grade natural gas of which methane is the major component. Initial performance test results for NMHC emissions conducted in December 1991 on CCC's turbine were found to be non-detectable (see Attachment A). This is consistent with NMHC emissions test data for substantially identical gas turbines fired on utility grade natural gas.

Mid-Set Cogeneration Company ("Mid-Set") located within the jurisdiction of the San Joaquin Valley Unified APCD ("SJVUAPCD") operates a GE Frame 6 turbine in Fellows, California. The Mid-Set turbine is substantially identical to the turbine operating at CCC and equipped with ammonia and SCR for NOx reduction. Source tests conducted at Mid-Set confirm that NMHC emissions from a Frame 6 turbines are at non-detectable levels (see Attachment B).

Based on source test results from CCC and Mid-Set, it is extremely unlikely that NMHC emissions are present in detectable quantities in the turbine exhaust gas. Existing test data for GE Frame 6 turbines substantiates that the March 4, 1993, NMHC emissions data of 2.58 #/hour is improbable. Based on these observations and the April 5, 1993 data from the retest, we infer that CCC is in compliance with the NMHC permitted emission limit.

Mr. G. Martin
May 17, 1993
Page 2

If you have any questions, please contact Mervyn Soares at (805) 392-2643.

Sincerely,

A handwritten signature in cursive script, appearing to read "G. M. Thomson".

G. M. THOMSON
Executive Director

MAS:plc

cc: D. S. King - MOMI (w/attachment)
R. L. LaRue (w/attachment)
F. A. Maggio (w/attachment)
A. Wu - Texaco, UCP (w/attachment)

Attachment A

Initial Performance NMHC Emission Data

EMISSION DATA SUMMARY GAS COMPONENTS

COALINGA COGENERATION
STACK OUTLET

12-Dec-91

NITROGEN DIOXIDE

Run #	% O2	Corrected ppm (dry)	Corrected ppm (dry) @ 15% O2	lb/hr	lb/MMBtu
1	14.79	3.60	3.48	6.04	0.0127
2	14.53	3.55	3.29	5.91	0.0120
3	14.52	3.34	3.09	5.59	0.0113
4					
5					
6					
Average	14.61	3.50	3.28	5.85	0.0120

CARBON MONOXIDE

Run #	Corrected ppm (dry)	Corrected ppm (dry) @ 15% O2	lb/hr	lb/MMBtu
1	4.00	3.86	4.09	0.0086
2	3.06	2.83	3.10	0.0063
3	3.03	2.80	3.09	0.0062
4				
5				
6				
Average	3.36	3.17	3.42	0.0070

SULFUR DIOXIDE

Run #	Corrected ppm (dry)	Corrected ppm (dry) @ 15% O2	lb/hr	lb/MMBtu
1	0.19	0.18	0.44	0.0009
2	0.09	0.08	0.21	0.0004
3	0.12	0.11	0.28	0.0006
4				
5				
6				
Average	0.13	0.13	0.31	0.0006

HYDROCARBON (NON-METHANE)

Run #	Corrected ppm (dry)	Corrected ppm (dry) @ 15% O2	lb/hr	lb/MMBtu
1	0.00	0.00	0.00	0.0000
2	0.00	0.00	0.00	0.0000
3	0.00	0.00	0.00	0.0000
4				
5				
6				
Average	0.00	0.00	0.00	0.0000

Attachment B

Mid-Set Cogeneration Company

NMHC Emission Data

SUMMARY OF SOURCE TEST RESULTS FOR KCAPCD

Company: Mid-Set Cogeneration Company
 Test Date: April 27, 1989

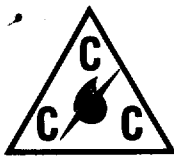
APCD # 4003597D
 Unit: Gas Turbine
 (Natural Gas)

EMISSIONS

	gr/SCF	ppm(v/v) ppm(v/v) @15%O2	lb/hr	lb/MMBTU	Other
Particulate	0.0012		2.37		
	0.0012		2.33		
	<u>0.0013</u>		<u>2.59</u>		
Mean	0.0012		2.43		
Sulfate	<0.00003		<0.058		
	<0.00003		<0.063		
	<u><0.00003</u>		<u><0.059</u>		
Mean	<0.00003		<0.060		
SO2 (wet)		<0.04	<0.04	<0.10	
		<0.05	<0.04	<0.12	
		<u><0.04</u>	<u><0.04</u>	<u><0.11</u>	
Mean		<0.04	<0.04	<0.11	
NOX as NO2 (dry)		9.2	8.4	15.25	0.029
		8.9	7.9	14.40	0.029
		<u>9.1</u>	<u>8.1</u>	<u>14.70</u>	<u>0.029</u>
Mean		9.1	8.1	14.78	0.029
HC		<1.0	<1.0	<0.57	<0.001
		<1.0	<1.0	<0.57	<0.001
		<u><1.0</u>	<u><1.0</u>	<u><0.57</u>	<u><0.001</u>
Mean:		<1.0	<1.0	<0.57	<0.001
CO		6.7	6.1	6.76	0.013
		6.8	6.1	6.70	0.013
		<u>6.5</u>	<u>5.8</u>	<u>6.39</u>	<u>0.013</u>
Mean:		6.7	6.0	6.62	0.013
NH3 Slip from SCR:		1.1	<1.0		
		2.1	1.9		
		<u>1.6</u>	<u>1.5</u>		
Mean:		1.6	1.5		

For Kern County Use Only:

Standard Conditions: 29.92 inches Hg & 60 deg F



Coalinga Cogeneration Company

P.O. Box 81078, Bakersfield, CA 93380

(805) 392-2630

Gordon M. Thomson, Executive Director

April 16, 1993

CC-1322

Mr. Gary Martin
Source Test Supervisor
San Joaquin Valley Unified APCD
Central Region Office
1999 Tuolumne Street, Suite 200
Fresno, CA 93721

RECEIVED

APR 21 1993

San Joaquin Valley Unified
Air Pollution Control District

Re: **Non-Methane Hydrocarbon Source Test Results**

Dear Mr. Martin:

Attached is an addendum to the 1993 source test report submitted by Coalinga Cogeneration Company ("CCC") dated April 1, 1993 (CC-1313). Pursuant to your request a retest for non-methane hydrocarbons ("NMHC") was conducted at CCC on April 5, 1993. The test results verified NMHC emissions from the gas turbine at CCC to be non-detectable. The test was performed by Engineering-Science, Inc., Bakersfield.

If you have any questions, please contact Mervyn Soares at (805) 392-2643.

Sincerely,

G. M. THOMSON
Executive Director

MAS:plc

cc: D. S. King - MOMI (w/attachment)
R. L. LaRue (w/attachment)



ENGINEERING-SCIENCE, INC.

2520 PEGASUS DRIVE
BAKERSFIELD, CA 93308
Tel: (805) 393-0272
Fax: (805) 393-8306

April 15, 1993

Coalinga Cogeneration Company
P.O. Box 81078
Bakersfield, CA 93380

Attention: Mervyn Soares

Subject: Retest results for Hydrocarbons at Coalinga Cogeneration Company.

Enclosed are the results from the retesting Engineering-Science, Inc. performed at Coalinga Cogeneration Company (District Permit # 3040170101R3) for hydrocarbon emissions. These results are an Addendum to the Source Test Report and Relative Accuracy Audit for the testing performed on March 4, 1993 and reported on April 1, 1993. We have included with Table 1 all calculations and supporting raw data.

Please feel free to call if you have any questions or need further assistance.

Sincerely,

A handwritten signature in dark ink, appearing to read 'Gary W. McRae', written over the printed name.

Gary W. McRae
Environmental Scientist

GWM/lkm
Enclosure

TABLE 1
HYDROCARBON DATA SUMMARY
HRSG STACK OUTLET, DISTRICT PERMIT # 3040170101R3
COALINGA COGENERATION COMPANY
COALINGA, CALIFORNIA
APRIL 5, 1993

RUN	O ₂	NON-METHANE HYDROCARBONS (NMHC) AS METHANE			
		ppm(v)	ppm(v)	lb/hr	lb/MMBtu
#	%	@ 15% O ₂			
1	14.48	ND	ND	ND	ND
2	14.47	ND	ND	ND	ND
3	14.46	ND	ND	ND	ND
AVG	14.47	ND	ND	ND	ND

Note: "ND" samples were non-detectable for all hydrocarbon compounds (C₂-C₆) with a detection limit of no greater than 0.50 ppm for each compound.

EMISSION CALCULATIONS HYDROCARBON COMPOUNDS

COALINGA COGENERATION
OUTLET STACK
APRIL 5, 1993

Hydrocarbon Compound	Molecular Weight	Molecular Formula	Laboratory Analysis, ppm as HC compound *			ppm HC as methane *		
			Run 1	Run 2	Run 3	Run 1	Run2	Run 3
C ₁ Methane	16.04	CH ₄						
C ₂ Ethane	30.07	C ₂ H ₆						
C ₃ Propane	44.09	C ₃ H ₈						
C ₄ Butane	58.12	C ₄ H ₁₀						
C ₅ Pentane	72.15	C ₅ H ₁₂						
C ₆ Hexane	86.17	C ₆ H ₁₄						
C ₆ + as Hexane	86.17	C ₆ H ₁₄						

Run 1	Run 2	Run 3	Average
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Stack Parameters

Stack Gas Oxygen, %	14.48	14.47	14.46	14.47
Stack Gas Flowrate, dscfm	220,976	224,684	224,336	223,332
F-Factor, dscf/MMBtu	8,517.09	8,517.09	8,517.09	8,517.09

Total Hydrocarbons, THC as methane

ppm	0.00	0.00	0.00	0.00	C ₁ -C ₆ + HC
ppm @ Oxygen Correction	0.00	0.00	0.00	0.00	
lb/hr	0.00	0.00	0.00	0.00	
lb/MMBtu	0.0000	0.0000	0.0000	0.0000	

Reactive Organic Compounds, ROC as methane

ppm	0.00	0.00	0.00	0.00	C ₂ -C ₆ + HC
ppm @ Oxygen Correction	0.00	0.00	0.00	0.00	
lb/hr	0.00	0.00	0.00	0.00	
lb/MMBtu	0.0000	0.0000	0.0000	0.0000	

Oxygen Correction : 15.0 %
Standard Temperature = 60 °F

Equations

HC corrected to methane, ppm = (MW of HC Compound / MW of Methane) x ppm value

ppm @ Oxygen Correction = ppm measured x [(20.9 - Oxygen Correction) / (20.9 - %Oxygen Measured)]

lb/hr = (0.00000137 lb-mole dR / ft³) x 60 min/hr x Qs(std) x (MW of Methane) x ppm / [T(std) + 460]

lb/MMBtu = F-Factor x (MW of Methane) x [(1.3711E-06 lb-mole dR/ft³) / [T(std) + 460]] x [20.9 / 20.9 - O₂%] x ppm



Performance Analytical Inc.
Environmental Testing and Consulting

PERFORMANCE ANALYTICAL INC.

RESULTS OF ANALYSIS

Client: Engineering Science, Inc.

Client Project ID: #WA344

PAI Project ID: #5103

Test code: EPA 18
Analyst: Ku-Jih Chen
Instrument ID: HP5890/FID #4
Verified by: Michael Taday

Matrix: Tedlar Bags
Date Received: 04/08/93
Date Analyzed: 04/08/93
Volume Analyzed: 1.0 ml

Client Sample ID	PAI Sample ID	C ₁ as Methane ppm	C ₂ as Ethane ppm	C ₃ as Propane ppm
BK9304001 (04/05/93)	9301133	ND < 0.50	ND < 0.50	ND < 0.40
BK9304002 (04/05/93)	9301134	ND < 0.50	ND < 0.50	ND < 0.40
BK9304003 (04/05/93)	9301135	ND < 0.50	ND < 0.50	ND < 0.40
BK9304003 (04/05/93)	Lab Duplicate	ND < 0.50	ND < 0.50	ND < 0.40
N/A (04/08/93)	Method Blank	ND < 0.50	ND < 0.50	ND < 0.40

Client Sample ID	PAI Sample ID	C ₄ as Butane ppm	C ₅ as Pentane ppm	C ₆ as Hexane ppm	C ₆ + as Hexane ppm
BK9304001 (04/05/93)	9301133	ND < 0.30	ND < 0.30	ND < 0.20	ND < 0.20
BK9304002 (04/05/93)	9301134	ND < 0.30	ND < 0.30	ND < 0.20	ND < 0.20
BK9304003 (04/05/93)	9301135	ND < 0.30	ND < 0.30	ND < 0.20	ND < 0.20
BK9304003 (04/05/93)	Lab Duplicate	ND < 0.30	ND < 0.30	ND < 0.20	ND < 0.20
N/A (04/08/93)	Method Blank	ND < 0.30	ND < 0.30	ND < 0.20	ND < 0.20

ND = Not Detected - Less Than Indicated Detection Limit

2520 Pegasus Drive
Bakersfield, CA 93308
(805) 393-0272

#5103

CHAIN OF CUSTODY RECORD

[illegible]

Page 1 of 1.

Coalinga Cogen

Test Location	HRSG Outlet

Test Method / Parameter	EPA Method 18 / HC
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ENGINEERING—SCIENCE, INC.

Note: Using a 10 liter sample bag, set the flowrate as follows: 15 min sample = 0.33 l/min; 30 min sample = 0.67 l/min; 60 min sample = 0.17 l/min.

Daily Logs for Mon 05 Apr 1993
 ***** Coalinga Cogeneration Company *****
 Coalinga, Fresno County, CA 93210

Fifteen Minute Log

Time hh:mm	CO						NOx (Stack)				
	O2 Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
09:30	14.48	6.04	5.55	.012	5.92	DAS Dn	4.90	4.51	.017	7.88	DAS Dn
	NH3 Slip										
	NH3	---15 min---		-----1 hr-----		NH3/NOx	---- SCR ----				
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
09:30	596.78	4.93	2.91	DAS Dn	DAS Dn	.915	42.80	738.71			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
09:30	304.00	5.85	3.66	.62	26.47						

Fifteen Minute Log

Run #1

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
09:45	14.49	6.19	5.70	.013	6.16	DAS Dn	4.37	4.03	.015	7.12	DAS Dn
		NH3 Slip									
	NH3	---15 min---		---1 hr---		NH3/NOx	--- SCR ---				
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
45	601.67	5.09	3.00	DAS Dn	DAS Dn	.930	42.45	738.96			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
09:45	303.91	5.92	3.73	.63	27.01						

Fifteen Minute Log

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
10:00	14.46	6.34	5.81	.013	6.42	6.29	4.18	3.83	.014	6.93	7.03
		NH3 Slip									
		NH3 SCFH		NH3		NH3/NOx	SCR				
		ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
10:00	607.23	5.13	3.07	5.11	3.04	.936	41.94	738.83			
		Air #/sec	Gas #/sec	H2O #/sec	Inj. Ratio	H2O gal/hr					
10:00	308.52	6.06	3.68	.61	26.66						

Run#1 O₂ = 14.48%
Fuel = 5.99 #/sec

Run #1 O₂ = 14.48%
 Fuel = 5.99 #/sec

One Hour Log

Time hh:mm	Gas mmBTU	O2 Pct	CO ppm	CO ppmC	#/mmBTU	#/hrC	NOx (Stack) ppm	ppmC	#/mmBTU	#/hrC
10:00	3446.00	14.48	6.21	5.70	.013	6.20	4.43	4.07	.015	7.24

Daily Logs for Run 03 Apr 2000
 ***** Coalinga Cogeneration Company *****
 Coalinga, Fresno County, CA 93210

	Air #/sec	Gas #/sec	H2O #/sec	NH3 SCFH	-- NH3 Slip -- ppmC #/hr	Inj. Ratio	H2O gal/hr	NH3/NOx Ratio	---- SCR ---- NOx	Temp
00	305.70	5.96	3.69	602.50	5.06 3.01	.62	26.74	.93	42.35	738.800

Fifteen Minute Log

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
10:15	14.45	6.87	6.10	.014	6.81	6.46	4.30	3.93	.015	7.19	7.08
NH3 Slip											
	NH3	ppmC <td>#/hr</td> <td>ppmC <td>#/hr</td> <td>NH3/NOx Ratio</td> <td>SCR</td> <td>NOx</td> <td>Temp</td> <td colspan="2"></td> </td>	#/hr	ppmC <td>#/hr</td> <td>NH3/NOx Ratio</td> <td>SCR</td> <td>NOx</td> <td>Temp</td> <td colspan="2"></td>	#/hr	NH3/NOx Ratio	SCR	NOx	Temp		
10:15	604.74	4.96	2.98	5.06	3.02	.930	42.00	739.05			
	Air #/sec	Gas #/sec	H2O #/sec	Inj. Ratio	H2O gal/hr						
10:15	309.01	6.12	3.57	.58	25.86						

Fifteen Minute Log

Run#

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
10:30	14.47	5.60	5.13	.011	5.71	6.27	4.25	3.90	.014	7.11	7.09
NH3 Slip											
	NH3	ppmC <td>#/hr</td> <td>ppmC <td>#/hr</td> <td>NH3/NOx Ratio</td> <td>SCR</td> <td>NOx</td> <td>Temp</td> <td colspan="2"></td> </td>	#/hr	ppmC <td>#/hr</td> <td>NH3/NOx Ratio</td> <td>SCR</td> <td>NOx</td> <td>Temp</td> <td colspan="2"></td>	#/hr	NH3/NOx Ratio	SCR	NOx	Temp		
10:30	621.61	5.06	3.03	5.06	3.02	.932	43.10	739.33			
	Air #/sec	Gas #/sec	H2O #/sec	Inj. Ratio	H2O gal/hr						
10:30	308.87	6.10	3.48	.57	25.17						

Fifteen Minute Log

Run # 2

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
10:45	14.46	5.65	5.18	.012	5.76	6.17	3.96	3.63	.013	6.61	6.96
NH3 Slip											
	NH3	ppmC <td>#/hr</td> <td>ppmC <td>#/hr</td> <td>NH3/NOx Ratio</td> <td>SCR</td> <td>NOx</td> <td>Temp</td> <td colspan="2"></td> </td>	#/hr	ppmC <td>#/hr</td> <td>NH3/NOx Ratio</td> <td>SCR</td> <td>NOx</td> <td>Temp</td> <td colspan="2"></td>	#/hr	NH3/NOx Ratio	SCR	NOx	Temp		
10:45	619.45	5.07	3.04	5.05	3.03	.938	42.64	739.36			
	Air #/sec	Gas #/sec	H2O #/sec	Inj. Ratio	H2O gal/hr						
10:45	308.84	6.09	3.52	.58	25.50						

Run # 2

O₂ = 14.47%

Fuel = 6.10 #/sec

Daily Logs for Mon 05 Apr 1995
 ***** Coalinga Cogeneration Company *****
 Coalinga, Fresno County, CA 93210

Fifteen Minute Log

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
11:00	14.46	5.49	5.03	.011	5.59	5.96	4.03	3.70	.014	6.73	6.91
		NH3 Slip									
		NH3		15 min		1 hr	NH3/NOx		SCR		
		SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp		
11:00	621.63	4.84	2.90	4.98	2.99	.932	43.07	739.33			
		Air	Gas	H2O	Inj.	H2O					
		#/sec	#/sec	#/sec	Ratio	gal/hr					
11:00	309.15	6.09	3.50	.57	25.35						

One Hour Log

Time	Gas	O2	CO				NOx (Stack)			
hh:mm	mmBTU	Pct	ppm	ppmC	#/mmBTU	#/hrC	ppm	ppmC	#/mmBTU	#/hrC
11:00	3476.00	14.46	5.85	5.36	.012	5.96	4.13	3.79	.014	6.91

	Air	Gas	H2O	NH3	-- NH3 Slip --	Inj.	H2O	NH3/NOx	---- SCR ----		
	#/sec	#/sec	#/sec	SCFH	ppmC	#/hr	Ratio	gal/hr	Ratio	NOx	Temp
11:00	309.00	6.10	3.52	616.90	4.98	2.99	.58	25.47	.93	42.70	739.300

Fifteen Minute Log

Run #3

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
11:15	14.46	5.55	5.09	.012	5.66	5.68	3.87	3.54	.013	6.45	6.72
		NH3 Slip									
		NH3		15 min		1 hr	NH3/NOx		SCR		
		SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp		
11:15	618.91	4.88	2.93	4.96	2.97	.936	42.70	739.25			
		Air	Gas	H2O	Inj.	H2O					
		#/sec	#/sec	#/sec	Ratio	gal/hr					
11:15	308.88	6.10	3.51	.58	25.43						

Fifteen Minute Log

Run #3

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
11:30	14.46	5.41	4.96	.011	5.52	5.63	3.96	3.63	.013	6.60	6.60
		NH3 Slip									
		NH3		15 min		1 hr	NH3/NOx		SCR		
		SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp		
11:30	619.15	4.93	2.96	4.93	2.96	.936	42.75	739.25			

Run #3

O₂ = 14.46%

Fuel = 6.10 #/sec

Cashin Corporation

MAINSCREEN: 1005 VER: 100 SUBSCREEN: 11 VER: 102 WINDOW: 0 VER: 0
DATE: 04/05/93 TIME: 09:30:45

US/HR/93	GROUP	POINT ID	HLARM	DESCRIPTION	TYPE	BOTH	UNIT	UNIT
1	FC286	FC286		CALC STM FLOW FROM FQ1201A1		128780		
2	FC287	FC287		CALC STM FLOW FROM FQ1202A1		86780		
3	DW	DW		GENERATOR LOAD		39.72	MM	
4	FOT	FOT		TOTAL FUEL FLOW (RAS)		5.94	LB/SEC	
5	WQJ	WQJ		H2O INJ FLOW (REDUNDANT INPUT)		3.813	LB/SEC	
6	FT404C	FT404C		NH3 TO NH3/AIR MIXER COMPENSTD		27.30	LB/HR	

COPY IN PROGRESS

Calbio Corporation Co.

MAINSCREEN: 1005 VER: 100 SUBSCREEN: 11 VER: 102 MINDUM: 0 VER: 0
DATE: 04/05/93 TIME: 10:02:22

GRP POS	POINT ID	GROUP 5012	DESCRIPTION	TYPE	VALUE	BOTH	UNITS
1	FC206	ALARM	CALC STM FLOW FROM F01201A1		132000		
2	FC207		CALC STM FLOW FROM F01202A1		85000		
3	DW		GENERATOR LOAD		40.81		MW
4	FOT		TOTAL FUEL FLOW (GAS)		6.16		LB/SEC
5	WQJ		H2O INJ FLOW (REDUNDANT INPUT)		3.774		LB/SEC
6	FT404C		NH3 TO NH3-AIR MIXER COMPENSTD		27.47		LB/HR

05/APR/93

GRP POS

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COPY-TH/ADDRESS

Coulter Cogeneration Co.

MAINSCREEN: 1005 VER: 100 SUBSCREEN: 11 VER: 102 WINDOW: 0 VER: 0
DATE: 04/06/93 TIME: 10:29:56

05/APR/93	GROUP 5012	POINT ID	ALARM	DESCRIPTION	TYPE	BOTH	VALUE	UNITS	10:29:55
1	FC206			CALC STM FLOW FROM F01201A1			130500		
2	FC207			CALC STM FLOW FROM F01202A1			86700		
3	DW			GENERATOR LOAD			40.16	MW	
4	F01			TOTAL FUEL FLOW (GAS)			6.02	LB/SEC	
5	WQJ			H2O INJ FLOW (REDUNDANT INPUT)			3.436	LB/SEC	
6	FT404C			NH3 TO NH3/AIR MIXER COMPENSTD			28.63	LB/HR	
7									
8									
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18									
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Carlini Corporation Co.

MAINSCREEN: 1005 VER: 100 SUBSCREEN: 11 VER: 102 WINDOW: 0 VER: 0
DATE: 04/05/93 TIME: 11:04:16

05/APR/93	GRP POS	POINT ID	ALARM	DESCRIPTION	TYPE	BOTH	VALUE	UNITS
1	FC206			CALC STM FLOW FROM FQ1201A1			127800	
2	FC207			CALC STM FLOW FROM FQ1202A1			86100	
3	DW			GENERATOR LOAD			40.25	MW
4	FQ1			TOTAL FUEL FLOW (GAS)			6.01	LB/SEC
5	WQJ			H2O IN-1 FLOW (REDUNDANT INPUT)			3.483	LB/SEC
6	FT404C			NH3 TO NH3-AIR MIXER COMPENSTD			28.77	LB/HR

COPY IN PROGRESS

Cadmus Concentration Co.

MAINSCREEN: 1005 VER: 100 SUBSCREEN: 11 VER: 102 WINDOW: 0 VER: 0
DATE: 04/06/93 TIME: 11:30:08

GRP POS	POINT ID	ALARM	DESCRIPTION	TYPE	BOTH	VALUE	UNITS
1	FC206		CALC STM FLOW FROM FQ1201A1			133800	
2	FC207		CALC STM FLOW FROM FQ1202A1			87000	
3	DW		GENERATOR LOAD			40.41	MW
4	FOT		TOTAL FUEL FLOW (GAS)			6.24	LB/SEC
5	WQ1		H2O INJ FLOW (REDUNDANT INPUT)			3.578	LB/SEC
6	FT404C		NH3 TO NH3/AIR MIXER COMPENSTD			27.09	LB/HR

05/APR/93 GROUP 5012

19

COPY IN PROGRESS



Coalinga Cogeneration Company

P.O. Box 81078, Bakersfield, CA 93380

(805) 392-2630

Gordon M. Thomson, Executive Director

VIA FEDERAL EXPRESS

April 8, 1993

CC-1313

Mr. Gary Martin
San Joaquin Valley Unified APCD - Central Region
1999 Tuolumne Street, Suite 200
Fresno, CA 93721

Re: **Annual Compliance Source Test Report**
Relative Accuracy Audit - CEM System

Dear Mr. Martin:

Pursuant to Permit to Operate (PTO) number 3040170101R3, attached is the 1993 annual compliance source test report and a relative accuracy audit (RA) of the continuous emission monitoring (CEM) system for Coalinga Cogeneration Company (CCC). The source testing and audit were conducted at the CCC facility on March 4, 1993.

In accordance with CCC's PTO, the gas turbine was tested under normal operating conditions fired on natural gas. Testing was performed by Engineering Science, Inc., Bakersfield, California.

As verified by the emission data, CO emissions from gas turbines are extremely low. As a result of such low stack gas concentration for CO you had agreed during the initial certification of the CEM system that the calculation method for the determination of relative accuracy as specified in Performance Specification No. 4 does not apply. Since the absolute difference between the reference method CO concentrations and those of the plant CEM differ by approximately 1 ppm the plant instrument is considered sufficiently accurate.

As per your verbal approval on April 2, 1993, a retest for non-methane hydrocarbons has been scheduled for April 5, 1993.

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San Joaquin Valley Unified
Air Pollution Control District

Mr. G. Martin
April 8, 1993
Page 2

If you have any questions, please contact Karen White-Fallon at (805) 392-2720 or Mervyn Soares at (805) 392-2643.

Sincerely,

A handwritten signature in cursive script, appearing to read "G. M. Thomson".

G. M. THOMSON
Executive Director

KWF:plc

Attachment

WA344

**SOURCE TEST REPORT AND RELATIVE ACCURACY AUDIT
SINGLE NATURAL GAS FIRED TURBINE
COALINGA COGENERATION COMPANY,
COALINGA, CALIFORNIA**

Prepared for:

**Coalinga Cogeneration Company
P.O. Box 81078
Bakersfield, California 93380**

For Submittal to:

**San Joaquin Valley Unified Air Pollution Control District
1999 Tuolumne St., Suite 200
Fresno, California 93721**

Test Dates:

March 4, 1993

Publication Date:

April 1, 1993

Prepared by:

**Engineering-Science, Inc.
2520 Pegasus Drive
Bakersfield, California 93308
(805)393-0272**

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APR - 9 1993

**San Joaquin Valley Unified
Air Pollution Control District**

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APPENDIX C	PLANT DATA

SECTION 1

INTRODUCTION

**SOURCE TEST REPORT AND RELATIVE ACCURACY AUDIT
SINGLE NATURAL GAS FIRED TURBINE
COALINGA COGENERATION COMPANY,
COALINGA, CALIFORNIA**

SECTION 1

INTRODUCTION

Engineering-Science, Inc. (ES), Bakersfield, California conducted source testing of a single natural gas fired General Electric Frame 6, 42.7 MW (Gross) combustion gas turbine operated by Coalinga Cogeneration Company (CCC), Coalinga, California. NO_x emissions are controlled by ammonia injection and Selective Catalytic Reduction (SCR). A Relative Accuracy Audit of the CCC Continuous Emission Monitoring (CEM) system was conducted simultaneously with the source test. Testing was conducted to demonstrate compliance with annual testing requirements in Permit to Operate number 3040170101R3 issued by the San Joaquin Valley Unified Air Pollution Control District (District).

Testing consisted of Continuous Emission Monitoring (CEM) for Nitrogen Oxides (NO_x), Carbon Monoxide (CO), and Oxygen (O₂); non-methane hydrocarbons (NMHC); and ammonia slip (NH₃ slip). Testing procedures for NO_x, CO, and O₂ were conducted in accordance with EPA Methods published in 40 CFR, Part 60, Appendix A and Appendix B, dated July 1990 and CARB Method 100. NH₃ slip testing was conducted in accordance with BAAQMD Method ST-1b as published in the Bay Area Air Quality Management District Manual of Procedures. NMHC testing was conducted in accordance with EPA Method 18. The turbine was operated at 100% load condition and fired on natural gas. The test program is summarized in Table 1-1. Relative accuracy calculations are in accordance with 40 CFR, Part 60, Appendix B, Performance Specifications 2 (NO_x), 3 (O₂), and 4 (CO).

Testing was performed March 4, 1993. Ten CEM test runs of 30 minute duration were performed. These 10 runs were used for compliance determination and

TABLE 1-1
SUMMARY OF SOURCE TESTING
COMPLIANCE AND RELATIVE ACCURACY TESTING
HRSG STACK OUTLET, DISTRICT PERMIT # 3040170101R3
COALINGA COGENERATION COMPANY
COALINGA, CALIFORNIA
MARCH 4, 1993

Source Test Parameters and Methodology					
Natural Gas					
Nitrogen Oxides NO _x	Carbon Monoxide CO	Oxygen O ₂	Non-methane hydrocarbons NMHC	Ammonia Slip NH ₃	Exhaust Gas Flow Rate
10 30-minute* runs for compliance and Relative Accuracy determination CARB Method 100	10 30-minute* runs for compliance and Relative Accuracy determination CARB Method 100	10 30-minute* runs for Relative Accuracy determination and O ₂ correction CARB Method 100	Triplicate 30 minute runs for compliance determination EPA Method 18	Triplicate 30 minute runs for compliance determination BAAQMD Method ST-1b	Single fuel Sample Analyzed by ASTM Method D-3588 F-Factor calculations in accordance with 40 CFR, Part 60, Appendix A

* Note: The ten Relative Accuracy Test runs are averaged for compliance determination.

Relative Accuracy calculations are accordance with Title 40 CFR, Part 60, Appendix B, Performance Specifications 2 (NO_x), 3 (O₂), and 4 (CO).

to calculate the Relative Accuracy of the CCC NO_x, CO, and O₂ analyzers. The CCC CEM system was operated in its normal mode. Triplicate 30 minute duration ammonia slip test runs (BAAQMD Method ST-1b) and triplicate 30-minute hydrocarbon test runs (EPA Method 18) were also performed for compliance determination.

In addition to the compliance and RA testing, a sample of natural gas was collected and analyzed for Carbon (C), Hydrogen (H), Oxygen (O), Nitrogen (N), Sulfur (S), and heating value (Btu). Fuel consumption data was supplied by CCC plant personnel. This data was used to determine exhaust gas pollutant mass emission rates (lb/hr) in accordance with F-Factor calculation methods specified in 40 CFR, Part 60, Appendix A.

Ms. Karen White-Fallon of CCC coordinated plant activities and was responsible for supplying ES with plant operating data. The ES testing team was comprised of Mssrs. Gary McRae, Troy Delfino, and Cesario Mangaoang.

SECTION 2

SUMMARY OF RESULTS

SECTION 2

SUMMARY OF RESULTS

The following Tables present the parameters and emission data measured by Engineering-Science, Inc. at Coalinga Cogeneration Company on March 4, 1993. Emission measurements were made of the exhaust gases of the single 42.7 MW natural gas fired turbine, District Permit No. 3040170101R3.

Table 2-1 summarizes the NO_x and CO emissions in parts per million (ppm), ppm @ 15% O₂, pounds per hour (lb/hr), and pounds per million British Thermal units (lb/MMBtu). Table 2-2 summarizes the NMHC emissions in ppm, lb/hr, and lb/MMBtu. Ammonia slip in ppm and lb/hr is also presented in Table 2-2. Relative Accuracy of the CCC NO_x, CO, and O₂ monitors are presented in Tables 2-3 through 2-5, respectively.

TABLE 2-1
 NITROGEN OXIDE AND CARBON MONOXIDE DATA SUMMARY
 HRSG STACK OUTLET, DISTRICT PERMIT # 3040170101R3
 COALINGA COGENERATION COMPANY
 COALINGA, CALIFORNIA
 MARCH 4, 1993

RUN #	O ₂ %	NITROGEN OXIDE (NO _x)			CARBON MONOXIDE (CO)				
		ppm(v)	ppm(v) @ 15% O ₂	lb/hr lb/MMBtu	ppm(v)	ppm(v) @ 15% O ₂	lb/hr lb/MMBtu		
1	14.48	2.21	2.03	3.50	0.0074	10.66	9.79	10.28	0.0218
2	14.54	3.58	3.32	5.69	0.0122	9.17	8.50	8.88	0.0189
3	14.53	3.62	3.35	5.73	0.0123	8.85	8.19	8.52	0.0183
4	14.52	3.66	3.39	5.77	0.0124	8.18	7.57	7.85	0.0169
5	14.59	3.95	3.69	6.27	0.0135	7.97	7.45	7.70	0.0166
6	14.53	3.78	3.50	5.92	0.0128	7.99	7.40	7.63	0.0165
7	14.57	4.10	3.82	6.43	0.0140	7.37	6.87	7.04	0.0153
8	14.56	4.33	4.03	6.72	0.0148	7.44	6.93	7.02	0.0154
9	14.56	4.30	4.00	6.65	0.0146	7.67	7.13	7.22	0.0159
10	14.61	4.12	3.86	6.46	0.0141	7.77	7.28	7.42	0.0162
AVG	14.55	3.77	3.50	5.91	0.0128	8.31	7.71	7.96	0.0172

TABLE 2-2
HYDROCARBON DATA SUMMARY
HRSG STACK OUTLET, DISTRICT PERMIT # 3040170101R3
COALINGA COGENERATION COMPANY
COALINGA, CALIFORNIA
MARCH 4, 1993

RUN #	O ₂ %	NON-METHANE HYDROCARBONS (NMHC) AS METHANE				AMMONIA SLIP		
		ppm(v)	ppm(v) @ 15% O ₂	lb/hr	lb/MMBtu	ppm(v)	ppm(v) @ 15% O ₂	lb/hr
1	14.48	5.37	4.94	2.96	0.0063	1.71	1.57	1.00
2	14.54	8.60	7.97	4.76	0.0102	0.67	0.62	0.39
3	14.53	ND	ND	ND	ND	0.91	0.84	0.53
AVG	14.52	4.66	4.30	2.58	0.0055	1.10	1.01	0.64

Note: "ND" samples were non-detectable for all hydrocarbon compounds (C₂-C₆) with a detection limit of 1 ppm for each compound.

TABLE 2-3
 NO_x RELATIVE ACCURACY DATA SUMMARY
 DISTRICT PERMIT # 3040170101R3
 COALINGA COGENERATION COMPANY
 COALINGA, CALIFORNIA
 MARCH 4, 1993

Run #	Reference Method (ES) Values ppm	Plant CEM Values ppm	Difference
1	2.21	2.35	0.14
2	3.58	3.62	0.04
3	3.62	3.68	0.06
4	3.66	3.75	0.09
5	3.95	3.99	0.04
6	3.78	3.86	0.08
7	4.10	4.24	0.14
8	4.33	4.05	-0.28
9	4.30	4.18	-0.12
10	4.12	4.02	-0.10

RELATIVE ACCURACY PERCENT = 2.79

TABLE 2-4
CO RELATIVE ACCURACY DATA SUMMARY
DISTRICT PERMIT # 3040170101R3
COALINGA COGENERATION COMPANY
COALINGA, CALIFORNIA
MARCH 4, 1993

Run #	Reference Method (ES) Values ppm	Plant CEM Values ppm	Difference
1	10.66	9.37	-1.29
2	9.17	7.92	-1.25
3	8.85	7.49	-1.36
4	8.18	6.91	-1.27
5	7.97	6.60	-1.37
6	7.99	6.76	-1.23
7	7.37	6.06	-1.31
8	7.44	6.37	-1.07
9	7.67	6.25	-1.42
10	7.77	6.59	-1.18

RELATIVE ACCURACY PERCENT = 16.22

TABLE 2-5
O₂ RELATIVE ACCURACY DATA SUMMARY
DISTRICT PERMIT # 3040170101R3
COALINGA COGENERATION COMPANY
COALINGA, CALIFORNIA
MARCH 4, 1993

Run #	Reference Method (ES) Values %	Plant CEM Values %	Difference
1	14.48	14.51	0.03
2	14.54	14.54	0.00
3	14.53	14.56	0.03
4	14.52	14.56	0.04
5	14.59	14.56	-0.03
6	14.53	14.55	0.02
7	14.57	14.58	0.01
8	14.56	14.59	0.03
9	14.56	14.57	0.01
10	14.61	14.57	-0.04

RELATIVE ACCURACY PERCENT = 0.20

SECTION 3

SAMPLING AND ANALYSIS PROCEDURES

SECTION 3

SAMPLING AND ANALYSIS PROCEDURES

Continuous Emissions Monitoring

Sample Extraction and Conditioning

Sampling is performed using a system which delivers a conditioned, continuous gas sample to the gas analyzers. The gas sample is extracted through a stainless steel probe, then passes through a heated (250°F) Teflon sample line, a sample condenser (for moisture removal), an in-line filter (for particulate removal), and a stainless steel pump. The clean, dry sample is then transported via unheated Teflon line to the analyzer manifold (located within the mobile van) for sample distribution to the continuous emissions monitors.

Continuous Emissions Monitors (CEMS)

Table 3-1 describes the CEMS used in the mobile van to analyze the exhaust gases. Calibrations of the CEMS are performed using EPA Protocol 1 or NIST certified calibration gases. Copies of gas certifications are included in the Report appendix.

Prior to performing the emissions testing, a leak check of the sample system is performed. A check of sampling system bias is performed by injecting calibration gas (for each parameter) at the sample probe and then observing instrument response. A response within ± 5 percent of instrument range is considered acceptable. The leak check is repeated at the conclusion of the test day to verify the validity of the tests.

Before each test run, an initial calibration of the analyzers is performed by introducing zero and span gases and making appropriate adjustments. During each test run, analyzer response data is recorded for each instrument. At the conclusion of the test run, a calibration check is performed to verify acceptable zero and span drift limits.

TABLE 3-1
CEM INSTRUMENT SPECIFICATIONS
CEM VAN # 3

PARAMETER	MANUFACTURER	MODEL NO.	ANALYZER PRINCIPLE	SENSITIVITY / ACCURACY	LINEARITY	SPECIAL NOTES	RESPONSE TIME	NOISE	PRECISION
O ₂	MSA Instruments	4000	Electroconductivity Detection	+ - 0.01%	< 2%	Galvanic Fuel Cell	90% Full Scale in 20 sec.	+ - 1%	
CO ₂	Infrared Industries	732	Non - Dispersive Infrared		< 2%		90% Full Scale in 20 sec.		
NO _x	Thermo Environmental Instruments Inc.	10	Chemiluminescent	0.05 ppm	+ - 1% from 0.05 to 10,000	High range has O ₂ feed.	Approx. 1.5 sec NO mode Approx. 1.7 sec NO _x mode	< 1% of Full Scale	
CO	Thermo Environmental Instruments Inc.	48	Gas Filter Correlation	0.1 ppm	< + - 1%		95% Full Scale in < 60 sec.	< 0.05 ppm	> + - 0.1ppm
Gas Dilution System	Enviroincs, Inc.	Series 2000	Computerized Mass Flow Controllers	+ - 0.05% Full Scale	NA	Operated between 10% and 90% of flow controller full scale operating range.	+ - 2.0% of target flow in 30 seconds	NA	+ - 0.2% Full Scale
CO ₂ / High CO	Fuji - Milton Roy	ZRH	Non - Dispersive Infrared	2% of Full Scale / week	1% of Full Scale	CO ₂ Range : 0 - 20 % CO Range : 0 - 1 %	90% Full Scale in 3 sec.	< 0.5% of Full Scale	CO ₂ : .5% Full Scale CO: 1% Full Scale

Ammonia (BAAQMD Method ST-1B)

General

Testing is conducted in accordance with BAAQMD Method ST-1b. Sample gas is collected in a solution of 0.1 Normal hydrochloric acid which absorbs the ammonia.

Sampling Train

The impinger train is kept in an icebath during the test run. Impingers 1 and 2 contain 100 milliliters of 0.1 N HCl, impinger 3 is empty, and impinger 4 contains a tared amount of silica gel. The impingers are weighed before and after sampling to allow calculation of percent moisture in the gas stream. The probe and sample box are connected to the control module using an umbilical line. The control module consists of a vacuum pump, a calibrated dry gas meter, and a calibrated orifice meter. The control module components measure pressure, temperature, and flowrate throughout the train.

Sampling Procedure

A leak check is performed before sampling begins by bringing the sample train to 15-inches of mercury vacuum. Leakage has to be less than 0.02 cfm or 4% of the average sampling rate prior to beginning a test. After sampling is complete, a final leak check is performed on the sampling train. This leak check is performed at 15-inches of mercury vacuum or at the highest vacuum achieved during the test. All pertinent data is recorded on field data sheets.

Sample Recovery

Each impinger is removed from the icebath, wiped dry, and weighed to allow calculation of percent moisture in the gas stream. A polyethylene bottle labeled as NH_3 is used to collect the contents of the impingers and the distilled water rinses of the impingers

and their connectors . A chain-of-custody form is filled out with sample numbers for tracking purposes.

Sample Analysis for Ammonia

The volume of the NH_3 sample bottle is measured and an aliquot is transferred to a 250 milliliter beaker using a 100 milliliter NBS class A pipet. A Teflon stir bar is carefully placed in the beaker and NH_3 ionic strength adjuster (ISA) solution is added until a blue color persists. The ammonia content is determined using a specific ion electrode. The electrode is rinsed with distilled water, immersed in the liquid, and allowed to reach a stable ppm (and millivolt) reading. The ion selective electrode (ISE) meter is calibrated with 1 ppm, 10 ppm and 100 ppm standards (3-point calibration) prior to sample analysis. Quality Control, duplicate, spike, and blank (0.1 N HCl impinger solution) samples are also analyzed.

Non-methane Hydrocarbons (EPA Method 18)

Integrated samples are collected through a 316 stainless steel probe and teflon line directly into a new Tedlar bag by utilizing an evacuated chamber to draw the exhaust gas into the bag. The Tedlar bags are purged twice with the exhaust gas before collecting each sample. At the conclusion of sampling, the Tedlar bag is closed off, labeled, and delivered to the laboratory along with a chain-of-custody form. Non-methane Hydrocarbon (NMHC) analysis is performed by Gas Chromatography equipped with Flame Ionization Detection (GC/FID).

Fuel Gas

A fuel gas sample is collected in a stainless steel gas sample cylinder, properly labeled, and delivered to the laboratory with an accompanying chain-of-custody form.

Samples are analyzed by gas chromatography for CHONS (carbon, hydrogen, oxygen, nitrogen, and sulfur) and heating value in accordance with ASTM Method D-3588.

SECTION 4
CALCULATIONS

NOMENCLATURE

A_s	= Cross-sectional area of stack (ft ²)
A_n	= Cross-sectional area of nozzle (ft ²)
B_{ws}	= Water vapor in the gas stream, proportion by volume (dimensionless)
C_p	= Pitot tube coefficient (dimensionless)
dH	= Average pressure differential across the orifice meter (inches of water)
M_d	= Dry molecular weight of stack gas (lb/lb-mole)
M_s	= Wet molecular weight of stack gas (lb/lb-mole)
N	= Normality of titrant (milliequivalents/ml)
dP	= Velocity pressure of stack gas (inches of water)
P_b	= Barometric pressure at sampling site (in. Hg)
P_s	= Absolute stack gas pressure (in. Hg)
P_{std}	= Standard absolute pressure (29.92 in. Hg)
$Q_s(std)$	= Dry volumetric stack gas flow rate, standard conditions (dscfm)
T_s	= Stack temperature (°F)
V_m	= Dry gas volume as measured by dry gas meter (dcf)
$V_m(std)$	= Dry gas volume as measured by dry gas meter, corrected to standard conditions (dscf)
$V_w(std)$	= Volume of water vapor in the gas stream, corrected to standard conditions (scf)
V_{lc}	= Volume of water vapor condensed in impingers and silica gel (ml)
$T(std)$	= Standard temperature (°F)
T_m	= Meter temperature (°F)
$SQ.RT.dP$	= Square root of velocity pressure (dimensionless)
y	= Dry gas meter calibration factor (dimensionless)
P_{static}	= Static pressure of stack (in. H ₂ O)
P_{stack}	= Static pressure of stack (in. Hg)
I	= Isokinetic sample rate (percent)
vs	= Average velocity of the stack gas (ft/sec)
Q_s	= Actual stack gas flow rate at stack conditions (ft ³ /min)
Θ	= Total sampling time (min)
% O ₂	= Percent oxygen by volume (dry basis)
% CO ₂	= Percent carbon dioxide by volume (dry basis)
% CO	= Percent carbon monoxide by volume (dry basis)
% N ₂	= Percent nitrogen by volume (dry basis)
Z_{cf}	= Zero drift correction factor
S_{cf}	= Span drift correction factor
C_z	= Zero correction concentration
MW	= Molecular weight (lb/lb-mole)
ppm	= Parts per million by volume

lb/MMBtu	= Emission concentration, pounds per million British thermal units
dscf/MMBtu	= Fuel factor, dry standard cubic feet per million British thermal units
gr/scf	= Emission concentration, grains per standard cubic foot
lb/hr	= Emission rate, pounds per hour
FHW	= Front Half Wash of sampling train
MF	= Mass Filter of sampling train
BHW	= Back Half Wash of Sampling train
gr/dscf	= Emission concentration, grains per dry standard cubic foot
ng	= Mass unit, nanograms
mg	= Mass unit, milligrams
g	= Mass unit, grams
ml	= Unit of volume, milliliters
L	= Unit of volume, liters
ul	= Unit of volume, microliters
H ₂ SO ₄	= Chemical formula, sulfuric acid
BaCl ₂	= Chemical formula, barium chloride
NaOH	= Chemical formula, sodium hydroxide
H ₂ S	= Chemical formula, hydrogen sulfide
FHS	= Front Half Sulfate of sampling train
BHS	= Back Half Sulfate of sampling train
F-Factor	= Fuel factor, volume of generated gases per unit of heat content (dscf/MMBtu)
°F	= Degrees Fahrenheit
°R	= Degrees Rankine
°C	= Degrees Celsius
98.076	= Molecular weight of sulfuric acid
64.062	= Molecular weight of sulfur dioxide
46.006	= Molecular weight of nitrogen dioxide
28.010	= Molecular weight of carbon monoxide
60	= Conversion factor, minutes per hour
460	= Conversion factor, °F to °R
15.432	= Conversion factor, grains per gram
0.000143	= Conversion factor, pounds per grain
32/98.076	= Conversion factor, equivalent weight of SO ₂ to MW of H ₂ SO ₄
1.60982	= Ideal Gas Law (lb-mole x dscf/ dscf/ °R x mg)
0.00000137	= Ideal Gas Law (lb-mole x °R/ft ³)
0.280	= Molecular weight of N ₂ or CO, divided by 100
0.320	= Molecular weight of O ₂ , divided by 100
0.440	= Molecular weight of CO ₂ , divided by 100
18.0	= Molecular weight of H ₂ O
32.064	= Equivalent weight of SO ₂
85.49	= Pitot tube constant, ft/sec x [(lb/lb-mole) x (in.Hg)/((°R) x (in.H ₂ O))] ^{0.5}
8.223E-05	= Ideal gas constant (1.37E-06 lb-mole °R/ft ³) x (60 min/hr)

RELATIVE ACCURACY CALCULATIONS – NOx (ppm)

COALINGA COGENERATION COMPANY
OUTLET STACK

04-Mar-93

Run No.	RM Test Values		Plant CEM Values		Difference d
	Runs not Used for RA	Runs Used for RA	Runs not Used for RA	Runs Used for RA	
1		2.21		2.35	0.14
2		3.58		3.62	0.04
3		3.62		3.68	0.06
4		3.66		3.75	0.09
5		3.95		3.99	0.04
6		3.78		3.86	0.08
7		4.10		4.24	0.14
8		4.33		4.05	-0.28
9		4.30		4.18	-0.12
10		4.12		4.02	-0.10
11					
12					

$\overline{RM} : 3.77$

$\overline{d} : 0.01$

Standard Deviation (Std.Dev.) : 0.13

t-VALUES TABLE			
n	t0.975	n	t0.975
2	12.706	10	2.262
3	4.303	11	2.228
4	3.182	12	2.201
5	2.776	13	2.179
6	2.571	14	2.160
7	2.447	15	2.145
8	2.365	16	2.131
9	2.306		

CONFIDENCE COEFFICIENT

$$CC = t_{0.975} \times [\text{Std.Dev.} / (\text{Sq.Rt. } n)] = 0.10$$

Where : CC = 2.5 percent error Confidence Coefficient.

n , number of valid test runs = 10

t0.975, t-Value from table = 2.262

RELATIVE ACCURACY

$$RA (\%) = (| \overline{d} | + | CC |) / \overline{RM} \times 100 = \boxed{2.79}$$

RELATIVE ACCURACY CALCULATIONS – CO (ppm)

COALINGA COGENERATION COMPANY
OUTLET STACK

04–Mar–93

Run No.	RM Test Values		Plant CEM Values		Difference d
	Runs not Used for RA	Runs Used for RA	Runs not Used for RA	Runs Used for RA	
1		10.66		9.37	–1.29
2		9.17		7.92	–1.25
3		8.85		7.49	–1.36
4		8.18		6.91	–1.27
5		7.97		6.60	–1.37
6		7.99		6.76	–1.23
7		7.37		6.06	–1.31
8		7.44		6.37	–1.07
9		7.67		6.25	–1.42
10		7.77		6.59	–1.18
11					
12					

$\overline{RM}$: 8.31

$\overline{d}$: –1.28

Standard Deviation (Std.Dev.) : 0.10

t–VALUES TABLE			
n	t0.975	n	t0.975
2	12.706	10	2.262
3	4.303	11	2.228
4	3.182	12	2.201
5	2.776	13	2.179
6	2.571	14	2.160
7	2.447	15	2.145
8	2.365	16	2.131
9	2.306		

CONFIDENCE COEFFICIENT

$$CC = t_{0.975} \times [\text{Std.Dev.} / (\text{Sq.Rt. } n)] = 0.07$$

Where : CC = 2.5 percent error Confidence Coefficient.

n , number of valid test runs = 10

t0.975, t–Value from table = 2.262

RELATIVE ACCURACY

$$RA (\%) = (| \overline{d} | + | CC |) / \overline{RM} \times 100 = 16.22$$

RELATIVE ACCURACY CALCULATIONS – O2 (%)

COALINGA COGENERATION COMPANY
OUTLET STACK

04-Mar-93

Run No.	RM Test Values		Plant CEM Values		Difference d
	Runs not Used for RA	Runs Used for RA	Runs not Used for RA	Runs Used for RA	
1		14.48		14.51	0.03
2		14.54		14.54	0.00
3		14.53		14.56	0.03
4		14.52		14.56	0.04
5		14.59		14.56	-0.03
6		14.53		14.55	0.02
7		14.57		14.58	0.01
8		14.56		14.59	0.03
9		14.56		14.57	0.01
10		14.61		14.57	-0.04
11					
12					

$\overline{RM}$: 14.55

$\overline{d}$: 0.01

Standard Deviation (Std.Dev.) : 0.03

t-VALUES TABLE			
n	t0.975	n	t0.975
2	12.706	10	2.262
3	4.303	11	2.228
4	3.182	12	2.201
5	2.776	13	2.179
6	2.571	14	2.160
7	2.447	15	2.145
8	2.365	16	2.131
9	2.306		

CONFIDENCE COEFFICIENT

CC = t0.975 x [Std.Dev. / (Sq.Rt. n)] = 0.02
 Where : CC = 2.5 percent error Confidence Coefficient.
 n , number of valid test runs = 10
 t0.975, t-Value from table = 2.262

RELATIVE ACCURACY

RA (%) = ($|\overline{d}|$ + |CC|) / $\overline{RM}$ x 100 = 0.20

EMISSION CALCULATIONS GAS COMPONENTS

COALINGA COGENERATION COMPANY OUTLET STACK

DATA :

	Run 1	Run 2	Run 3	Run 4	Run 5	Run 6
Date	04-Mar-93	04-Mar-93	04-Mar-93	04-Mar-93	04-Mar-93	04-Mar-93
Oxygen (%)	14.48	14.54	14.53	14.52	14.59	14.53
Qs(std), dscfm	217,656	218,592	217,320	216,608	218,073	215,647
F-Factor, dscf/MMBtu	8,517.09	8,517.09	8,517.09	8,517.09	8,517.09	8,517.09
NOx, ppm	2.21	3.58	3.62	3.66	3.95	3.78
CO, ppm	10.66	9.17	8.85	8.18	7.97	7.99

CALCULATIONS :

NOx, lb/hr	3.50	5.69	5.73	5.77	6.27	5.92
NOx, ppm @ 15 %O2	2.03	3.32	3.35	3.39	3.69	3.50
NOx, lb/MMBtu	0.0074	0.0122	0.0123	0.0124	0.0135	0.0128
CO, lb/hr	10.28	8.88	8.52	7.85	7.70	7.63
CO, ppm @ 15 %O2	9.79	8.50	8.19	7.57	7.45	7.40
CO, lb/MMBtu	0.0218	0.0189	0.0183	0.0169	0.0166	0.0165
SO2, lb/hr						
SO2, ppm @ 15 %O2						
SO2, lb/MMBtu						
HC, lb/hr						
HC, ppm @ 15 %O2						
HC, lb/MMBtu						

EQUATIONS :

$$\text{lb/hr} = (0.00000137 \text{ Lb-Mole } ^\circ\text{R} / \text{ft}^3) \times 60 \text{ min/hr} \times Qs(\text{std}) \times MW \times \text{ppm} / [T(\text{std}) + 460]$$

$$\text{ppm @ 15 \%O}_2 = \text{ppm measured} \times [(20.9 - 15 \%O_2) / (20.9 - \%O_2 \text{ measured})]$$

$$\text{lb/MMBtu} = F\text{-Factor} \times MW \times [(1.3711\text{E}-6 \text{ Lb-Mole } ^\circ\text{R} / \text{ft}^3) / (T(\text{std}) + 460)] \times [20.9 / (20.9 - O_2\%)] \times \text{ppm}$$

CONSTANTS :

Standard Temp. T(std):
Oxygen Correction :

60 °F
15 % O2

NOx, MW = 46.005 lb/lb-mole
CO, MW = 28.010 lb/lb-mole

SO2, MW = 64.058 lb/lb-mole
HC, MW = 16.043 lb/lb-mole

EMISSION CALCULATIONS GAS COMPONENTS

COALINGA COGENERATION COMPANY OUTLET STACK

DATA :

	Run 7	Run 8	Run 9	Run 10
Date	04-Mar-93	04-Mar-93	04-Mar-93	04-Mar-93
Oxygen (%)	14.57	14.56	14.56	14.61
Qs(std), dscfm	215,700	213,118	212,745	215,754
F-Factor, dscf/MMBtu	8,517.09	8,517.09	8,517.09	8,517.09
NOx, ppm	4.10	4.33	4.30	4.12
CO, ppm	7.37	7.44	7.67	7.77
SO2, ppm				
HC (non-methane), ppm				

CALCULATIONS :

NOx, lb/hr	6.43	6.72	6.65	6.46
NOx, ppm @ 15 %O2	3.82	4.03	4.00	3.86
NOx, lb/MMBtu	0.0140	0.0148	0.0146	0.0141
CO, lb/hr	7.04	7.02	7.22	7.42
CO, ppm @ 15 %O2	6.87	6.93	7.13	7.28
CO, lb/MMBtu	0.0153	0.0154	0.0159	0.0162
SO2, lb/hr				
SO2, ppm @ 15 %O2				
SO2, lb/MMBtu				
HC, lb/hr				
HC, ppm @ 15 %O2				
HC, lb/MMBtu				

EQUATIONS :

$$\text{lb/hr} = (0.00000137 \text{ Lb-Mole } ^\circ\text{R} / \text{ft}^3) \times 60 \text{ min/hr} \times Q_s(\text{std}) \times \text{MW} \times \text{ppm} / [T(\text{std}) + 460]$$

$$\text{ppm @ 15 \%O}_2 = \text{ppm measured} \times [(20.9 - 15 \%O_2) / (20.9 - \%O_2 \text{ measured})]$$

$$\text{lb/MMBtu} = \text{F-Factor} \times \text{MW} \times [(1.3711\text{E}-6 \text{ Lb-Mole } ^\circ\text{R} / \text{ft}^3) / (T(\text{std}) + 460)] \times [20.9 / (20.9 - O_2\%)] \times \text{ppm}$$

CONSTANTS :

Standard Temp. T(std): 60 °F
Oxygen Correction : 15 % O2

NOx, MW = 46.005 lb/lb-mole SO2, MW = 64.058 lb/lb-mole
CO, MW = 28.010 lb/lb-mole HC, MW = 16.043 lb/lb-mole

GAS ANALYZER DATA

COALINGA COGENERATION COMPANY
OUTLET STACK

Date : 04-Mar-93
Run No. : 1

Point #	O2, %		CO2, %		NOx, ppm		CO, ppm		SO2, ppm	
	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading
1	14.50	14.50			2.20	2.20	10.40	10.40		
2	14.50	14.50			2.40	2.40	10.40	10.39		
3	14.48	14.48			2.23	2.23	11.00	10.99		
4	14.47	14.47			2.15	2.15	11.00	10.99		
5	14.46	14.46			2.14	2.14	10.60	10.58		
6	14.45	14.45			2.15	2.15	10.65	10.62		
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MEAN :	14.48				2.21		10.66			

Zero Check	0.00	0.00	0.20
Span Check	15.14	8.46	12.54
Initial Span Value	15.14	8.46	12.54
Drift, Percent	0.0	0.0	-1.6
Zero Drift, Zcf	0.00000	0.00000	0.03333
Span Drift, Scf	0.00000	0.00000	-0.00266

Drift, Percent = [(Span Check - Zero Check) - Calib. Gas] / Calib. Gas x 100

Zero Drift Correction Factor, Zcf = Zero Check / # of Readings

Span Drift Correction Factor, Scf = (% Drift / 100) / # of Readings

Cz, Zero Corr. Concentration = measured value - [Zcf x (Point # - 0.5)]

Drift Corrected Reading = Cz / [1 + (Scf x (Point # - 0.5))]

GAS ANALYZER DATA

**COALINGA COGENERATION COMPANY
OUTLET STACK**

Date : 04-Mar-93

Run No. : 2

Point #	O2, %		CO2, %		NOx, ppm		CO, ppm		SO2, ppm	
	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading
1	14.54	14.54			3.30	3.30	9.70	9.70		
2	14.54	14.54			3.60	3.60	9.50	9.50		
3	14.54	14.54			3.70	3.70	9.10	9.10		
4	14.54	14.54			3.65	3.65	8.90	8.90		
5	14.54	14.54			3.63	3.63	8.90	8.90		
6	14.54	14.54			3.60	3.60	8.90	8.90		
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30										
MEAN :	14.54				3.58		9.17			

Zero Check	0.00	0.00	0.00
Span Check	15.14	8.46	12.54
Initial Span Value	15.14	8.46	12.54
Drift, Percent	0.0	0.0	0.0
Zero Drift, Zcf	0.00000	0.00000	0.00000
Span Drift, Scf	0.00000	0.00000	0.00000

Drift, Percent = $[(\text{Span Check} - \text{Zero Check}) - \text{Calib. Gas}] / \text{Calib. Gas} \times 100$

Zero Drift Correction Factor, Zcf = $\text{Zero Check} / \# \text{ of Readings}$

Span Drift Correction Factor, Scf = $(\% \text{ Drift} / 100) / \# \text{ of Readings}$

Cz, Zero Corr. Concentration = $\text{measured value} - [\text{Zcf} \times (\text{Point \#} - 0.5)]$

Drift Corrected Reading = $\text{Cz} / [1 + (\text{Scf} \times (\text{Point \#} - 0.5))]$

GAS ANALYZER DATA

COALINGA COGENERATION COMPANY
OUTLET STACK

Date : 04-Mar-93
Run No. : 3

Point #	O2, %		CO2, %		NOx, ppm		CO, ppm		SO2, ppm	
	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading
1	14.53	14.53			3.80	3.79	9.00	9.00		
2	14.53	14.53			3.80	3.78	8.30	8.31		
3	14.53	14.53			3.40	3.37	9.20	9.21		
4	14.53	14.53			3.55	3.50	9.00	9.02		
5	14.53	14.53			3.75	3.68	8.90	8.92		
6	14.53	14.53			3.70	3.62	8.60	8.63		
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MEAN :	14.53				3.62		8.85			

Zero Check	0.00		
Span Check	15.14	0.00	0.00
Initial Span Value	15.14	8.67	12.50
Drift, Percent	0.0	8.46	12.54
Zero Drift, Zcf	0.00000	2.5	-0.3
Span Drift, Scf	0.00000	0.00000	0.00000
		0.00414	-0.00053

Drift, Percent = $[(\text{Span Check} - \text{Zero Check}) - \text{Calib. Gas}] / \text{Calib. Gas} \times 100$

Zero Drift Correction Factor, Zcf = $\text{Zero Check} / \# \text{ of Readings}$

Span Drift Correction Factor, Scf = $(\% \text{ Drift} / 100) / \# \text{ of Readings}$

Cz, Zero Corr. Concentration = $\text{measured value} - [\text{Zcf} \times (\text{Point \#} - 0.5)]$

Drift Corrected Reading = $\text{Cz} / [1 + (\text{Scf} \times (\text{Point \#} - 0.5))]$

GAS ANALYZER DATA

**COALINGA COGENERATION COMPANY
OUTLET STACK**

**Date : 04-Mar-93
Run No. : 4**

Point #	O2, %		CO2, %		NOx, ppm		CO, ppm		SO2, ppm	
	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading
1	14.50	14.50			4.05	4.05	7.70	7.70		
2	14.50	14.50			3.40	3.39	8.80	8.80		
3	14.50	14.50			3.70	3.68	8.30	8.30		
4	14.52	14.52			3.80	3.78	7.80	7.80		
5	14.55	14.55			3.25	3.22	8.10	8.10		
6	14.57	14.57			3.90	3.86	8.40	8.40		
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30										
MEAN :	14.52				3.66		8.18			

Zero Check	0.00	0.00	0.00
Span Check	15.14	8.55	12.54
Initial Span Value	15.14	8.46	12.54
Drift, Percent	0.0	1.1	0.0
Zero Drift, Zcf	0.00000	0.00000	0.00000
Span Drift, Scf	0.00000	0.00177	0.00000

Drift, Percent = $[(\text{Span Check} - \text{Zero Check}) - \text{Calib. Gas}] / \text{Calib. Gas} \times 100$

Zero Drift Correction Factor, Zcf = $\text{Zero Check} / \# \text{ of Readings}$

Span Drift Correction Factor, Scf = $(\% \text{ Drift} / 100) / \# \text{ of Readings}$

Cz, Zero Corr. Concentration = $\text{measured value} - [\text{Zcf} \times (\text{Point \#} - 0.5)]$

Drift Corrected Reading = $\text{Cz} / [1 + (\text{Scf} \times (\text{Point \#} - 0.5))]$

GAS ANALYZER DATA

**COALINGA COGENERATION COMPANY
OUTLET STACK**

**Date : 04-Mar-93
Run No. : 5**

Point #	O2, %		CO2, %		NOx, ppm		CO, ppm		SO2, ppm	
	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading
1	14.57	14.57			3.62	3.62	7.95	7.95		
2	14.59	14.59			4.05	4.05	8.00	8.00		
3	14.59	14.59			3.90	3.90	8.25	8.25		
4	14.59	14.59			4.30	4.30	7.80	7.80		
5	14.59	14.59			4.10	4.10	8.00	8.00		
6	14.59	14.59			3.75	3.75	7.80	7.80		
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MEAN :	14.59				3.95		7.97			

Zero Check	0.00	0.00	0.00
Span Check	15.14	8.46	12.54
Initial Span Value	15.14	8.46	12.54
Drift, Percent	0.0	0.0	0.0
Zero Drift, Zcf	0.00000	0.00000	0.00000
Span Drift, Scf	0.00000	0.00000	0.00000

Drift, Percent = $[(\text{Span Check} - \text{Zero Check}) - \text{Calib. Gas}] / \text{Calib. Gas} \times 100$

Zero Drift Correction Factor, Zcf = $\text{Zero Check} / \# \text{ of Readings}$

Span Drift Correction Factor, Scf = $(\% \text{ Drift} / 100) / \# \text{ of Readings}$

Cz, Zero Corr. Concentration = $\text{measured value} - [\text{Zcf} \times (\text{Point \#} - 0.5)]$

Drift Corrected Reading = $\text{Cz} / [1 + (\text{Scf} \times (\text{Point \#} - 0.5))]$

GAS ANALYZER DATA

COALINGA COGENERATION COMPANY
OUTLET STACK

Date : 04-Mar-93
Run No. : 6

Point #	O2, %		CO2, %		NOx, ppm		CO, ppm		SO2, ppm	
	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading
1	14.52	14.52			4.00	4.00	7.50	7.50		
2	14.52	14.53			3.60	3.60	8.00	8.00		
3	14.50	14.52			3.80	3.80	8.10	8.10		
4	14.50	14.53			3.70	3.70	8.15	8.15		
5	14.48	14.52			3.55	3.55	8.40	8.40		
6	14.48	14.53			4.00	4.00	7.80	7.80		
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MEAN :		14.53				3.78		7.99		

Zero Check	0.00	0.00	0.00
Span Check	15.08	8.46	12.54
Initial Span Value	15.14	8.46	12.54
Drift, Percent	-0.4	0.0	0.0
Zero Drift, Zcf	0.00000	0.00000	0.00000
Span Drift, Scf	-0.00066	0.00000	0.00000

Drift, Percent = [(Span Check - Zero Check) - Calib. Gas] / Calib. Gas x 100

Zero Drift Correction Factor, Zcf = Zero Check / # of Readings

Span Drift Correction Factor, Scf = (% Drift / 100) / # of Readings

Cz, Zero Corr. Concentration = measured value - [Zcf x (Point # - 0.5)]

Drift Corrected Reading = Cz / [1 + (Scf x (Point # - 0.5))]

GAS ANALYZER DATA

COALINGA COGENERATION COMPANY
OUTLET STACK

Date : 04-Mar-93
Run No. : 7

Point #	O2, %		CO2, %		NOx, ppm		CO, ppm		SO2, ppm	
	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading
1	14.55	14.55			4.00	3.99	7.80	7.80		
2	14.55	14.55			4.20	4.18	7.00	7.00		
3	14.58	14.58			4.20	4.17	7.80	7.80		
4	14.58	14.58			3.70	3.66	8.00	8.00		
5	14.58	14.58			4.40	4.35	6.80	6.80		
6	14.58	14.58			4.30	4.24	6.80	6.80		
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30										
MEAN :		14.57				4.10		7.37		

Zero Check	0.00	0.00	0.00
Span Check	15.14	8.60	12.54
Initial Span Value	15.14	8.46	12.54
Drift, Percent	0.0	1.7	0.0
Zero Drift, Zcf	0.00000	0.00000	0.00000
Span Drift, Scf	0.00000	0.00276	0.00000

Drift, Percent = $[(\text{Span Check} - \text{Zero Check}) - \text{Calib. Gas}] / \text{Calib. Gas} \times 100$

Zero Drift Correction Factor, Zcf = $\text{Zero Check} / \# \text{ of Readings}$

Span Drift Correction Factor, Scf = $(\% \text{ Drift} / 100) / \# \text{ of Readings}$

Cz, Zero Corr. Concentration = $\text{measured value} - [\text{Zcf} \times (\text{Point \#} - 0.5)]$

Drift Corrected Reading = $\text{Cz} / [1 + (\text{Scf} \times (\text{Point \#} - 0.5))]$

GAS ANALYZER DATA

**COALINGA COGENERATION COMPANY
OUTLET STACK**

Date : 04-Mar-93
Run No. : 8

Point #	O2, %		CO2, %		NOx, ppm		CO, ppm		SO2, ppm	
	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading
1	14.55	14.55			4.30	4.31	7.40	7.40		
2	14.55	14.55			4.40	4.42	7.00	7.00		
3	14.55	14.55			4.20	4.23	7.80	7.80		
4	14.55	14.55			4.25	4.29	7.75	7.75		
5	14.58	14.58			4.25	4.30	7.50	7.50		
6	14.60	14.60			4.40	4.46	7.20	7.20		
7										
8										
9										
10										
11										
12										
13										
14										
15										
16										
17										
18										
19										
20										
21										
22										
23										
24										
25										
26										
27										
28										
29										
30										
MEAN :	14.56				4.33		7.44			

Zero Check	0.00	0.00	0.00
Span Check	15.14	8.33	12.54
Initial Span Value	15.14	8.46	12.54
Drift, Percent	0.0	-1.5	0.0
Zero Drift, Zcf	0.00000	0.00000	0.00000
Span Drift, Scf	0.00000	-0.00256	0.00000

Drift, Percent = [(Span Check - Zero Check) - Calib. Gas] / Calib. Gas x 100

Zero Drift Correction Factor, Zcf = Zero Check / # of Readings

Span Drift Correction Factor, Scf = (% Drift / 100) / # of Readings

Cz, Zero Corr. Concentration = measured value - [Zcf x (Point # - 0.5)]

Drift Corrected Reading = Cz / [1 + (Scf x (Point # - 0.5))]

GAS ANALYZER DATA

COALINGA COGENERATION COMPANY
OUTLET STACK

Date : 04-Mar-93
Run No. : 9

Point #	O2, %		CO2, %		NOx, ppm		CO, ppm		SO2, ppm	
	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading
1	14.55	14.55			4.15	4.16	7.90	7.90		
2	14.55	14.55			4.27	4.29	7.70	7.70		
3	14.55	14.55			4.27	4.30	7.60	7.60		
4	14.55	14.55			4.20	4.24	7.70	7.70		
5	14.55	14.55			4.30	4.35	7.60	7.60		
6	14.58	14.58			4.40	4.46	7.50	7.50		
7										
8										
9										
10										
11										
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25										
26										
27										
28										
29										
30										
MEAN :		14.56				4.30		7.67		

Zero Check	0.00	-0.13	0.00
Span Check	15.14	8.46	12.54
Initial Span Value	15.14	8.46	12.54
Drift, Percent	0.0	1.5	0.0
Zero Drift, Zcf	0.00000	-0.02167	0.00000
Span Drift, Scf	0.00000	0.00256	0.00000

Drift, Percent = [(Span Check - Zero Check) - Calib. Gas] / Calib. Gas x 100

Zero Drift Correction Factor, Zcf = Zero Check / # of Readings

Span Drift Correction Factor, Scf = (% Drift / 100) / # of Readings

Cz, Zero Corr. Concentration = measured value - [Zcf x (Point # - 0.5)]

Drift Corrected Reading = Cz / [1 + (Scf x (Point # - 0.5))]

GAS ANALYZER DATA

**COALINGA COGENERATION COMPANY
OUTLET STACK**

Date : 04-Mar-93
Run No. : 10

Point #	O2, %		CO2, %		NOx, ppm		CO, ppm		SO2, ppm	
	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading	Instrument Reading	Drift Corrected Reading
1	14.60	14.60			4.30	4.30	7.40	7.40		
2	14.60	14.60			3.80	3.79	8.10	8.10		
3	14.60	14.60			4.10	4.09	7.60	7.60		
4	14.61	14.61			4.60	4.58	7.50	7.50		
5	14.61	14.61			3.70	3.68	8.20	8.20		
6	14.62	14.62			4.30	4.27	7.80	7.80		
7										
8										
9										
10										
11										
12										
13										
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20										
21										
22										
23										
24										
25										
26										
27										
28										
29										
30										
MEAN :		14.61				4.12		7.77		

Zero Check	0.00	0.00	0.00
Span Check	15.14	8.53	12.54
Initial Span Value	15.14	8.46	12.54
Drift, Percent	0.0	0.8	0.0
Zero Drift, Zcf	0.00000	0.00000	0.00000
Span Drift, Scf	0.00000	0.00138	0.00000

Drift, Percent = [(Span Check - Zero Check) - Calib. Gas] / Calib. Gas x 100

Zero Drift Correction Factor, Zcf = Zero Check / # of Readings

Span Drift Correction Factor, Scf = (% Drift / 100) / # of Readings

Cz, Zero Corr. Concentration = measured value - [Zcf x (Point # - 0.5)]

Drift Corrected Reading = Cz / [1 + (Scf x (Point # - 0.5))]

AMMONIA CALCULATIONS

Company Name :	COALINGA COGENERATION	O2 Correction :	15 %
Source :	OUTLET STACK	Standard Temp. :	60 °F
Date :	MARCH 4, 1993	Standard Press. :	29.92 "Hg

	<u>Run 1</u>	<u>Run 2</u>	<u>Run 3</u>
Tm, °F	77.17	82.50	79.00
Y, meter correction factor	0.9980	0.9980	0.9980
Vm, ft3	20.013	19.958	19.864
Pb, in.Hg.	29.52	29.52	29.52
dH, in.H2O	1.30	1.30	1.30
O2, percent	14.48	14.54	14.53
Qs(std), dscfm	217656	218592	217320
Vm(std), dscf	19.138	18.898	18.931
mg AMMONIA	0.67	0.26	0.35
ppm AMMONIA	1.71	0.67	0.91
ppm AMMONIA @ 15.0 %O2	1.57	0.62	0.84
lb/hr AMMONIA	1.00	0.39	0.53

EQUATIONS :

$$Vm(std), dscf = [T(std) + 460 / 29.92] \times Vm \times Y \times (Pb + (dH / 13.6)) / (Tm + 460)$$

$$ppm \text{ AMMONIA} = 1.60982 \times (Temp.Std. + 460) \times (mg \text{ AMMONIA}) / (MW \times Vm, std)$$

Where : 1.60982 = Ideal Gas Law Factor

Where MW of AMMONIA = 17.08 Lb/Lb-Mole

$$ppm \text{ AMMONIA @ corrected O2\%} = ppm \text{ AMMONIA} \times [20.9 - O2 \text{ correction} / (20.9 - \%O2 \text{ measured})]$$

$$lb/hr = (0.00000137 \text{ Lb-Mole } ^\circ R / ft^3) \times 60 \text{ min/hr} \times Qs(std) \times MW \times ppm / [T(std) + 460]$$

EMISSION CALCULATIONS HYDROCARBON COMPOUNDS

SALINAS RIVER COGENERATION
OUTLET STACK
MARCH 3, 1993

Hydrocarbon Compound		Molecular Weight	Molecular Formula	Laboratory Analysis, ppm as HC compound *			ppm HC as methane *		
				Run 1	Run 2	Run 3	Run 1	Run2	Run 3
C ₁	Methane	16.04	CH ₄						
C ₂	Ethane	30.07	C ₂ H ₆						
C ₃	Propane	44.09	C ₃ H ₈						
C ₄	Butane	58.12	C ₄ H ₁₀						
C ₅	Pentane	72.15	C ₅ H ₁₂						
C ₆	Hexane	86.17	C ₆ H ₁₄	1	1.6		5.37	8.60	
C ₆ +	as Hexane	86.17	C ₆ H ₁₄						

	Run 1	Run 2	Run 3	Average	
<u>Stack Parameters</u>					
Stack Gas Oxygen, %	14.48	14.54	14.53	14.52	
Stack Gas Flowrate, dscfm	217,656	218,592	217,320	217,856	
F-Factor, dscf/MMBtu	8,517.09	8,517.09	8,517.09	8,517.09	
<u>Total Hydrocarbons, THC as methane</u>					
ppm	5.37	8.60	0.00	4.66	C ₁ -C ₆ + HC
ppm @ Oxygen Correction	4.94	7.97	0.00	4.30	
lb/hr	2.96	4.76	0.00	2.58	
lb/MMBtu	0.0063	0.0102	0.0000	0.0055	
<u>Reactive Organic Compounds, ROC as methane</u>					
ppm	5.37	8.60	0.00	4.66	C ₂ -C ₆ + HC
ppm @ Oxygen Correction	4.94	7.97	0.00	4.30	
lb/hr	2.96	4.76	0.00	2.58	
lb/MMBtu	0.0063	0.0102	0.0000	0.0055	
Oxygen Correction : 15.0 %					
Standard Temperature = 60 °F					

Equations

HC corrected to methane, ppm = (MW of HC Compound / MW of Methane) x ppm value

ppm @ Oxygen Correction = ppm measured x [(20.9 - Oxygen Correction) / (20.9 - %Oxygen Measured)]

lb/hr = (0.00000137 lb-mole dR / ft³) x 60 min/hr x Qs(std) x (MW of Methane) x ppm / [T(std) + 460]]

lb/MMBtu = F-Factor x (MW of Methane) x [(1.3711E-06 lb-mole dR/ft³) / [T(std) + 460)] x [20.9 / 20.9 - O2%] x ppm

FUEL BASED CALCULATIONS

COALINGA COGENERATION COMPANY
OUTLET STACK

04-Mar-93

FUEL ANALYSIS DATA								
Run #	Fuel Value (%), Moisture & Ash Free					GCV		
	Carbon	Hydrogen	Nitrogen	Oxygen	Sulfur	BTU/lb, dry	ft3/lb	lb/gal
1	72.37	22.72	1.00	3.90	0.00	22,175	20.920	
2	72.37	22.72	1.00	3.90	0.00	22,175	20.920	
3	72.37	22.72	1.00	3.90	0.00	22,175	20.920	
4	72.37	22.72	1.00	3.90	0.00	22,175	20.920	
5	72.37	22.72	1.00	3.90	0.00	22,175	20.920	
6	72.37	22.72	1.00	3.90	0.00	22,175	20.920	

CALCULATIONS									
Run #	Stack Gas Oxygen %	Fuel Gas Flowrate		Fuel Oil Flowrate		Solid Fuel lb/hr	Heat Input MMBTU/hr	F-Factor dscf/MMBTU	Qs(std) dscfm
		lb/hr	ft3/hr	lb/hr	gal/hr				
1	14.48	21,240					470.999	8,517.09	217,656
2	14.54	21,132					468.604	8,517.09	218,592
3	14.53	21,042					466.608	8,517.09	217,320
4	14.52	21,006					465.810	8,517.09	216,608
5	14.59	20,916					463.814	8,517.09	218,073
6	14.53	20,880					463.016	8,517.09	215,647

$$\text{Heat Input, MMBTU/hr} = (\text{lb/hr fuel gas}) \times \text{BTU/lb} \times \text{MM}/1\text{E}+06$$

$$= (\text{ft3/hr fuel gas}) \times \text{BTU/lb} / (\text{ft3/lb fuel gas}) \times \text{MM}/1\text{E}+06$$

$$= (\text{lb/hr fuel oil}) \times \text{BTU/lb} \times \text{MM}/1\text{E}+06$$

$$= (\text{gal/hr fuel oil}) \times \text{lb/gal} \times \text{BTU/lb} \times \text{MM}/1\text{E}+06$$

$$= (\text{lb/hr solid fuel}) \times \text{BTU/lb} \times \text{MM}/1\text{E}+06$$

$$\text{F-Factor, dscf/MMBTU} = 1\text{E}+06 [(3.64 \text{ scf/lb})/\% \times (\% \text{ H}) + (1.53 \text{ scf/lb})/\% \times (\% \text{ C}) + (0.57 \text{ scf/lb})/\% \times (\% \text{ S}) + (0.14 \text{ scf/lb})/\% \times (\% \text{ N}) - (0.46 \text{ scf/lb})/\% \times (\% \text{ O}_2)] / (\text{BTU/lb}) \times [(\text{Tstd} + 460) / 528]$$

$$\text{Qs(std), dscfm} = \text{MMBTU/hr} \times [\text{F-Factor} \times (20.9 / (20.9 - \% \text{O}_2)) \times (\text{hr} / 60 \text{ min})]$$

$$\text{GCV} = \text{Gross Calorific Value of fuel, Btu/lb, dry}$$

$$\text{Standard Temperature} = 60 \text{ }^{\circ}\text{F}$$

FUEL BASED CALCULATIONS

COALINGA COGENERATION COMPANY
OUTLET STACK

04-Mar-93

FUEL ANALYSIS DATA								
Run #	Fuel Value (%), Moisture & Ash Free					GCV		
	Carbon	Hydrogen	Nitrogen	Oxygen	Sulfur	BTU/lb, dry	ft3/lb	lb/gal
7	72.37	22.72	1.00	3.90	0.00	22,175	20.920	
8	72.37	22.72	1.00	3.90	0.00	22,175	20.920	
9	72.37	22.72	1.00	3.90	0.00	22,175	20.920	
10	72.37	22.72	1.00	3.90	0.00	22,175	20.920	

CALCULATIONS									
Run #	Stack Gas Oxygen %	Fuel Gas Flowrate		Fuel Oil Flowrate		Solid Fuel lb/hr	Heat Input MMBTU/hr	F-Factor dscf/MMBTU	Qs(std) dscfm
		lb/hr	ft3/hr	lb/hr	gal/hr				
7	14.57	20,754					460.222	8,517.09	215,700
8	14.56	20,538					455.432	8,517.09	213,118
9	14.56	20,502					454.634	8,517.09	212,745
10	14.61	20,628					457.428	8,517.09	215,754

$$\text{Heat Input, MMBTU/hr} = (\text{lb/hr fuel gas}) \times \text{BTU/lb} \times \text{MM}/1\text{E}+06$$

$$= (\text{ft3/hr fuel gas}) \times \text{BTU/lb} / (\text{ft3/lb fuel gas}) \times \text{MM}/1\text{E}+06$$

$$= (\text{lb/hr fuel oil}) \times \text{BTU/lb} \times \text{MM}/1\text{E}+06$$

$$= (\text{gal/hr fuel oil}) \times \text{lb/gal} \times \text{BTU/lb} \times \text{MM}/1\text{E}+06$$

$$= (\text{lb/hr solid fuel}) \times \text{BTU/lb} \times \text{MM}/1\text{E}+06$$

$$\text{F-Factor, dscf/MMBTU} = 1\text{E}+06 [(3.64 \text{ scf/lb})/\% \times (\% \text{ H}) + (1.53 \text{ scf/lb})/\% \times (\% \text{ C}) + (0.57 \text{ scf/lb})/\% \times (\% \text{ S}) + (0.14 \text{ scf/lb})/\% \times (\% \text{ N}) - (0.46 \text{ scf/lb})/\% \times (\% \text{ O}_2)] / (\text{BTU/lb}) \times [(\text{Tstd} + 460) / 528]$$

$$\text{Qs(std), dscfm} = \text{MMBTU/hr} \times [\text{F-Factor} \times (20.9 / (20.9 - \% \text{O}_2))] \times (\text{hr} / 60 \text{ min})$$

$$\text{GCV} = \text{Gross Calorific Value of fuel, Btu/lb, dry}$$

$$\text{Standard Temperature} = 60 \text{ }^{\circ}\text{F}$$

SECTION 5
QUALITY ASSURANCE

SECTION 5

QUALITY ASSURANCE

The report is reviewed for technical and editorial quality and for compliance with project requirements. Calculations are performed by computer programs designed for source testing. At least one set of calculations are performed manually to check results.

All equipment used in testing has been checked for proper maintenance and calibrated prior to testing. Test equipment calibrations are included in the Report appendix. The dry gas meter accuracy is expressed as gamma and is determined as the difference between the meter box dry gas meter and the wet test meter used for calibration. The results of the orifice calibration are expressed as the delta H@ (dH@) at various pressure drops (inches of water), as specified in EPA publication APTD-0576. EPA Quality Assurance Branch annual audits are performed with an orifice check of each of the dry gas meters used for volumetric sampling.

The analyzers employed for continuous monitoring of NO_x, CO, SO₂, CO₂, O₂, and HC are California Air Resources Board (CARB) approved instruments. Sampling system bias checks of the continuous monitor sampling system are performed using either EPA protocol 1 or NIST certified calibration gases. Calibration certificates are included in the report. All other required checks of the continuous monitor system are also performed.

All field samples are labeled and logged in on a chain-of-custody sheet. Chain-of-custody sheets remain with samples and document sample movement.

SAMPLE SYSTEM BIAS CHECK

COMPANY COALINGA COGEN.

DATE 3/4/93

TEST LOCATION HRSO OUTLET STACK OPERATOR T. DELFINO

COMMENTS: POST-TEST CHECK

Parameter	Instrument Full Scale	Span Gas Value	Scale	Internal Response	System Response	Percent Difference
O2 (%)	0-25%	0.00	Zero	0.00		
		15.14	Upscale	15.14	15.05	-0.36
CO2 (%)		0.00	Zero			
			Upscale			
NOx (ppm)	0-10	0.00	Zero	0.00		
		8.46	Upscale	8.53	8.38	-1.50
CO (ppm)	0-20	0.00	Zero	0.00		
		12.54	Upscale	12.54	12.50	-0.20
SO2 (ppm)		0.00	Zero			
			Upscale			
HC (ppm)		0.00	Zero			
			Upscale			
		0.00	Zero			
			Upscale			

Percent Difference = [(System Response - Internal Response) / Instrument Full Scale] x 100

Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 867-2571 FAX: (909) 867-0540

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
ENGINEERING SCIENCE
P.O. BOX 2007
IRVINDALE, CA 91706

Assay Laboratory
Scott Specialty Gases
2600 Cajon Boulevard
San Bernardino, CA 92411

Purchase Order BK042
Scott Project # 0223658

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol 1 Procedure #G1, Section Number 3.0.4

Cylinder Number ALM011324
Cylinder Pressure 1900 psig

Certification Date 2/2/93
Previous Certification Dates

Expiration Date 8/2/93

ANALYZED CYLINDER

Components
Nitric Oxide
Carbon Monoxide

Certified Concentration
12.50 ppm
12.54 ppm

Analytical Uncertainty*
± 1 % NIST Traceable

Balance Gas: Nitrogen
NOX

12.7 ppm

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type
GMS
GMS
Expiration Date
3/93
3/93

Cylinder Number
ALM006975
ALM026614

Concentration
22.52 ppm Nitric Oxide
96.23 ppm Carbon Monoxide

INSTRUMENTATION

Instrument/Model/Serial #
TECO / 10AR / 38644-258
Honey / OPE-135D / 56565502

Last Date Calibrated
11/12/92
11/20/92

Analytical Principle
Chemi-Luminescent
NDIR

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components

First Triad Analysis

Date: 1/22/93 Response Units: mv
Z1= 0.06 R1= 89.87 T1= 49.98
R2= 90.06 Z2= 0.18 T2= 50.02
Z3= 0.20 T3= 50.02 R3= 90.05
Avg. Conc. of Cust Cyl. 12.50 ppm

Second Triad Analysis

Date: 2/2/93 Response Units: mv
Z1= 0.00 R1= 89.99 T1= 50.08
R2= 90.23 Z2= 0.06 T2= 50.14
Z3= 0.10 T3= 50.12 R3= 90.61
Avg. Conc. of Cust Cyl. 12.50 ppm

Calibration Curve

Concentration= $Ax + Bx + C$
A = -0.000050429
B = -1.04899
C = -0.29251

Carbon Monoxide

Date: 1/26/93 Response Units: mv
Z1= 0.00 R1= 97.0 T1= 13.2
R2= 97.0 Z2= 0.00 T2= 13.2
Z3= 0.00 T3= 13.2 R3= 97.0
Avg. Conc. of Cust Cyl. 12.52 ppm

Date: 2/2/93 Response Units: mv
Z1= 0.00 R1= 97.0 T1= 13.3
R2= 97.0 Z2= 0.00 T2= 13.2
Z3= 0.00 T3= 13.2 R3= 97.0
Avg. Conc. of Cust Cyl. 12.53 ppm

Concentration= $Ax + Bx + Cx + Dx + E$
A = -0.0000000689
B = -0.000002034
C = -0.0006717
D = -0.93957
E = -0.004735

Date: Response Units:
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Date: Response Units:
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Concentration=

Special Notes

Analyst: Joseph De La Torre



Scott Specialty Gases, Inc.

FAX 714-887-0549
PHONE: 714-887-2571

2600 CAJON BLVD., SAN BERNARDINO, CA 92411

ENGINEERING SCIENCE

ATTN: GARY MCRAE

2520 PEGASUS

BAKERSFIELD

CA 93308

Shipped From: Scott
Date Shipped: 10/14/92
Our Project No.: 22021
Your P.O. No.: BK033
Page 1 of 1
Expiration Date: 4/94

SAN BERNARDINO, CA

CERTIFICATE OF ANALYSIS - ERA PROTOCOL GASES

Certified Per Traceability Protocol No. 1 Procedure No. G1 Cylinder No. A1M011705 Cylinder Pressure 2000 PSIG Certified Accuracy $\pm 1\%$ % NIST Traceable

REFERENCE STD

CERTIFIED CONC

8.002%

SRM/CRM NO.

CRM1675

CYL. NO.

A1M001136

CONC.

14.08%

GAS ANALYZER

LAST CAL. DATE

9/17/92

MAKE/MODEL/SERIAL NO.

OPE-135C

ANALYTICAL PRINCIPLE

INFRA-RED

PARAMAGNETIC

8/27/92

BALANCE GAS NITROGEN

ANALYZER READINGS: Z = Zero Gas T = Test Gas R = Reference Gas

Component CARBON DIOXIDE

First Analysis Date 10/6/92 Units mv

Z 0.00 R 95.5 T 67.3

R 95.5 Z 0.00 T 67.2

Z 0.00 T 67.3 R 95.5

Mean Test Assay 8.002%

Second Analysis Date Units mv

Z R T

R Z T

Z T R

Mean Test Assay

Component OXYGEN

Date 10/6/92 Units mv

Z 0.00 R 83.7 T 61.3

R 83.7 Z 0.00 T 61.3

Z 0.01 T 61.2 R 83.7

Mean Test Assay 15.14%

Date Units mv

Z R T

R Z T

Z T R

Mean Test Assay

Chronology: Date Assay

Analyst J. DE LA TORRE

Approved By:

A. F. Lange

A. F. LANGE, Ph.D., MANAGER, QA



Scott Specialty Gases, Inc.

2600 CAJON BLVD., SAN BERNARDINO, CA 92411

ENGINEERING SCIENCE

2520 PEGASUS

BAKERSFIELD, CA 93308-5003

FAX 714-887-0549
PHONE: 714-887-2571

Shipped From: Scott SAN BERNARDINO, CA
Date Shipped: 10/5/92
Our Project No: 0221822
Your P.O. No: BKG0001
Page 1 of 1
Expiration Date: 4/94

CERTIFICATE OF ANALYSIS - EPA PROTOCOL GASES

Certified Per Traceability Protocol No. 1 Procedure No. GL Cylinder No. ALM027375 Cylinder Pressure 1800 PSIG Certified Accuracy ±1% % NIST Traceable

REFERENCE STD

COMPONENTS
CARBON DIOXIDE 3.994 %
OXYGEN 4.002 %

SRM/CRM NO. CYL. NO. CONC.

SRM2626A CAL-7539 3.9198%

CRM2657 AAL-20176 2.002 %

GAS ANALYZER

LAST CAL. DATE 6/3/92
ANALYTICAL PRINCIPLE INFERA RED

MAKE/MODEL/SERIAL NO. HORIBA PRI2000
406004

BECKMAN 755
100410

6/3/92 PARAMAGNETIC

NITROGEN

BALANCE GAS ANALYZER READINGS: Z = Zero Gas T = Test Gas R = Reference Gas

Component CARBON DIOXIDE
First Analysis Date 10/5/92 Units mv
Z 00.0 R 78.2 T 79.4
R 78.2 Z 00.0 T 79.4
Z 00.0 T 79.4 R 78.2
Mean Test Assay 3.994%
Second Analysis Date Units mv
Z R T
R Z T
Z T R
Mean Test Assay

Component OXYGEN
Date 10/5/92 Units mv
Z 00.0 R 40.0 T 80.0
R 40.0 Z 00.0 T 80.0
Z 00.0 T 80.0 R 40.0
Mean Test Assay 4.002 %
Date Units mv
Z R T
R Z T
Z T R
Mean Test Assay

Component
Date Units mv
Z R T
R Z T
Z T R
Mean Test Assay
Date Units mv
Z R T
R Z T
Z T R
Mean Test Assay

Chronology: Date Assay

Analyst F. VILLAMAS

Approved By: A.F. LANGE, Ph.D., MANAGER, QA

Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 887-2571 FAX: (909) 887-0549

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
ENGINEERING SCIENCE
2520 PEGASUS
BAKERSFIELD, CA 93308-2200

Assay Laboratory
Scott Specialty Gases
2600 Cajon Boulevard
San Bernardino, CA 92411

Purchase Order BK034
Scott Project # 23659.003

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol 1 Procedure #G1, Section Number 3.0.4

Cylinder Number ALM022850
Cylinder Pressure 1900psig

Certification Date 02-03-93
Previous Certification Dates NONE

Expiration Date 08-93

ANALYZED CYLINDER

Comments
Carbon Monoxide
Nitric Oxide

Certified Concentration
8.352 ppm
8.338 ppm

Analytical Uncertainty*
± 1 % NIST Traceable
± 2 % NIST Traceable

Balance Gas: Nitrogen

NOX

8.46 ppm

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type
SRM1677
GMS
Expiration Date
10-93
03-93

Cylinder Number
CAL5078
ALM6975

Concentration
9.900 ppm
22.52 ppm

INSTRUMENTATION

Instrument/Model/Serial #
Horiba / OPE-135D / 56565502
TECO / 10AR / 14853-150

Last Date Calibrated
06-03-92
10-29-92

Analytical Principle
NDIR
Chemi-Luminescent

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Comments
Carbon Monoxide

First Triad Analysis

Date: 01-37-93 **Response Units:** MV
Z1= 0.00 R1= 19.5 T1= 16.5
R2= 19.5 Z2= 0.04 T2= 16.5
Z3= 0.07 T3= 16.5 R3= 19.5
Avg. Conc. of Cust Cyl. 8.352 ppm

Second Triad Analysis

Date: 02-03-93 **Response Units:** MV
Z1= 0.00 R1= 19.5 T1= 16.5
R2= 19.5 Z2= 0.00 T2= 16.5
Z3= 0.00 T3= 16.5 R3= 19.5
Avg. Conc. of Cust Cyl. 8.352 ppm

Calibration Curve

Concentration= Ax^2+Bx+C
A = -0.0005011
B = 0.5059
C = -0.01002

Nitric Oxide

Date: 01-22-93 **Response Units:** MV
Z1= 0.02 R1= 89.87 T1= 33.46
R2= 90.41 Z2= 0.18 T2= 33.57
Z3= 0.20 T3= 33.57 R3= 90.45
Avg. Conc. of Cust Cyl. 8.347 ppm

Date: 02-02-93 **Response Units:** MV
Z1= 0.00 R1= 90.40 T1= 33.49
R2= 90.42 Z2= 0.00 T2= 33.42
Z3= 0.00 T3= 33.39 R3= 90.40
Avg. Conc. of Cust Cyl. 8.328 ppm

Concentration= Ax^2+Bx+C
A = -0.000504296
B = 1.0489680
C = -0.292506

Date: **Response Units:**
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Date: **Response Units:**
Z1= R1= T1=
R2= Z2= T2=
Z3= T3= R3=
Avg. Conc. of Cust Cyl.

Concentration=

Special Notes

Joseph De La Torre
Analyst Joseph De La Torre



Scott Specialty Gases, Inc.

2600 CAJON BOULEVARD, SAN BERNARDINO, CA 92411

(909) 887-2571 FAX: (909) 887-0549

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
ENGINEERING SCIENCE
P.O. BOX 2007
IRVINDALE, CA 91706

Assay Laboratory
Scott Specialty Gases
2600 Cajon Boulevard
San Bernardino, CA 92411

Purchase Order BK042
Scott Project # 0223658

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol 1 Procedure #G1, Section Number 3.0.4

Cylinder Number AAL 2534
Cylinder Pressure 1900 psig

Certification Date 2/2/93
Previous Certification Dates

Expiration Date 8/2/93

ANALYZED CYLINDER

Components
Carbon Monoxide
Nitric Oxide

Certified Concentration
18.56 ppm
22.75 ppm

Analytical Uncertainty*
± 1 % NIST Traceable

Balance Gas: Nitrogen
NOX

23.2 ppm

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type
CRM-1678
GMS

Expiration Date
2/94
3/93

Cylinder Number
AAL-5970
ALM 006975

Concentration
47.20 ppm Carbon Monoxide
22.52 ppm Nitric Oxide

INSTRUMENTATION

Instrument/Model/Serial #
Horiba / OPE-135D / 56565502
TECO / 10AR / 14853-150

Last Date Calibrated
12/17/92
1/20/93

Analytical Principle
NDIR
Chemi-Luminescent

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components

First Triad Analysis

Second Triad Analysis

Calibration Curve

Zero Gas

Date: 1/26/93 **Response Units:** mv
Z1= 0.02 R1= 89.55 T1= 90.54
R2= 90.03 Z2= 0.13 T2= 90.60
Z3= 0.12 T3= 90.63 R3= 90.12
Avg. Conc. of Cust Cyl. 22.69 ppm

Date: 2/1/93 **Response Units:** mv
Z1= 0.00 R1= 89.26 T1= 90.78
R2= 89.16 Z2= -0.23 T2= 90.14
Z3= -0.20 T3= 90.12 R3= 89.25
Avg. Conc. of Cust Cyl. 22.80 ppm

Concentration= $Ax + Bx + C$
A = -0.00008618
B = -0.23997
C = -0.019484

Carbon Monoxide

Date: 1/26/93 **Response Units:** mv
Z1= 0.00 R1= 20.9 T1= 8.40
R2= 20.9 Z2= 0.00 T2= 8.30
Z3= 0.00 T3= 8.33 R3= 20.9
Avg. Conc. of Cust Cyl. 18.52 ppm

Date: 2/2/93 **Response Units:** mv
Z1= 0.00 R1= 20.9 T1= 8.40
R2= 20.9 Z2= 0.00 T2= 8.30
Z3= 0.00 T3= 8.33 R3= 20.9
Avg. Conc. of Cust Cyl. 18.59 ppm

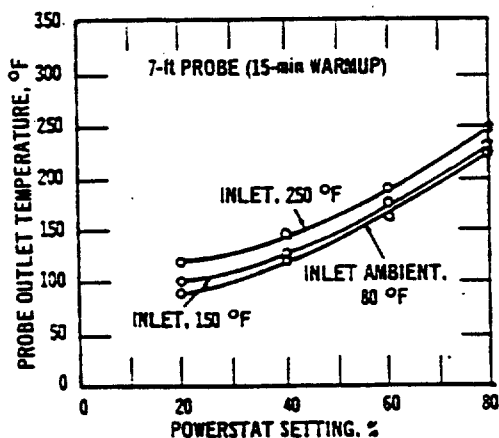
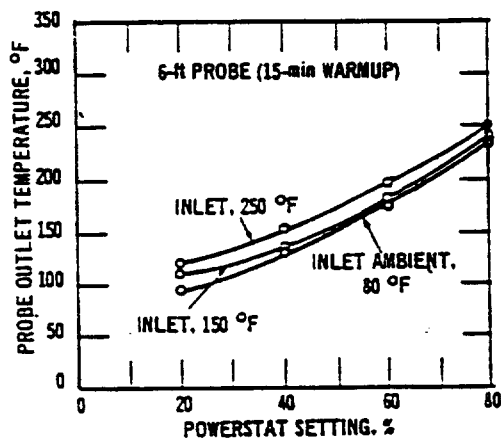
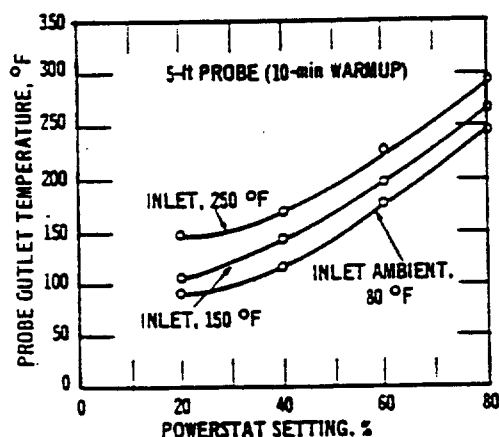
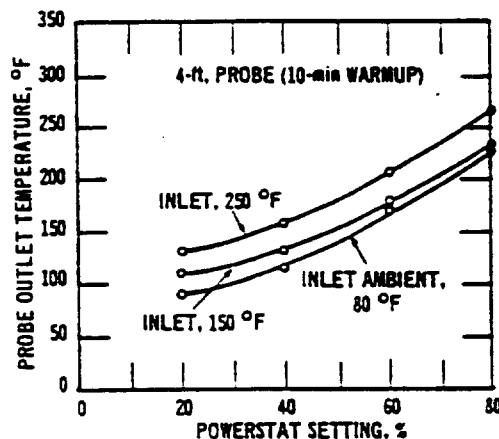
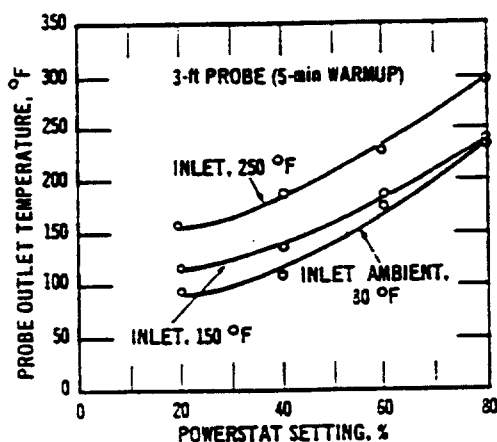
Concentration= $Ax + Bx + Cx + DX$
A = -0.0000000089
B = -0.0000000084
C = -0.0006117
D = 0.99997
E = -0.004733

Special Notes

Analyst: Joseph De La Torre

PROBE HEAT CALIBRATION

Sample probes are constructed as outlined in EPA publication PB-209 022 "Maintenance, Calibration, and Operation of Isokinetic Source Sampling Equipment". The Figures below from this publication are used to determine probe heat settings to maintain a probe temperature of 250 °F.



NOTE: Flow rate held constant at 0.75; 50% change in flow rate has little effect on probe temperature.

DRY GAS METER AND ORIFICE CALIBRATION

Meter Box # Brown IV Barometric Press. 29.38 IN. HG.

Date 18-Jan-93 Performed by T. Delfino

Calibration Meter Y 1.00014

	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
VACUUM (°Hg)	3	5	5	5	5	5
dHw (°H2O)	0.00	0.00	0.00	0.00	0.00	0.00
dHd (°H2O)	0.50	1.00	1.50	2.00	3.00	4.00
INITIAL WTM	866.883	873.433	931.482	833.099	947.264	977.798
FINAL WTM	873.178	931.327	946.881	866.342	977.357	1011.223
INITIAL DGM	918.813	925.631	986.853	884.158	3.643	36.108
FINAL DGM	925.371	986.665	1003.242	918.243	35.647	71.736
TEMP. WTM (°F)	62.0	58.0	58.0	59.0	57.0	57.0
TEMP. DGM (°F)	75.0	82.0	83.0	76.0	87.0	88.0
TEST TIME (MIN.)	15.0	101.0	22.0	41.0	31.0	30.0
CALCULATIONS :						
NET VOLUME WTM (Vw)	6.296	57.902	15.401	33.248	30.097	33.430
NET VOLUME DGM (Vd)	6.558	61.034	16.389	34.085	32.004	35.628
Y	0.983	0.990	0.981	1.002	0.988	0.985
ACCEPTABLE Y RANGE = 0.968 TO 1.008						
dH@	1.56	1.63	1.63	1.65	1.68	1.70
ACCEPTABLE dH@ RANGE = 1.49 TO 1.79						

AVERAGE Y = 0.988

AVERAGE dH@ = 1.64

CALCULATIONS :

$$Y = (Vw (Pb - (dHw / 13.6)) \times (Td + 460)) / (Vd (Pb + (dHd / 13.6)) \times (Tw + 460))$$

$$dH@ = 0.0317 \times dHd / (Pb (Td + 460)) \times ((Tw + 460) \times \text{time}) / Vw \wedge 2$$

POST TEST METER CALIBRATION

Meter Box # Brown IV Barometric Press. 30.03 IN. HG.

Date 22-MAR-93 Performed by J-POLHAMUS

	RUN 1	RUN 2	RUN 3
VACUUM ("Hg)	10	10	10
dHw ("H2O)	0.00	0.00	0.00
dHd ("H2O)	2.50	2.50	2.50
INITIAL WTM	12.201	25.782	39.255
FINAL WTM	25.782	39.255	52.780
INITIAL DGM	641.554	655.452	669.370
FINAL DGM	655.452	669.370	683.463
TEMP. WTM (°F)	72.0	72.0	73.0
TEMP. DGM (°F)	74.0	79.0	83.0
TEST TIME (MIN.)	15.0	15.0	15.0
CALCULATIONS :			
NET VOLUME WTM (Vw)	13.581	13.473	13.525
NET VOLUME DGM (Vd)	13.898	13.918	14.093
Y	0.975	0.975	0.972

AVERAGE Y = 0.974

PRETEST Y = 0.988

DIFFERENCE, % = 1.4%

WHERE :

$$Y = (Vw (Pb - (dHw / 13.6)) \times (Td + 460)) / (Vd (Pb + (dHd / 13.6)) \times (Tw + 460))$$

Thermometer / Pyrometer Calibration

Date : 18-Jan-93
Calibrated by : T. Delfino

I.D. : Brown IV Pyrometer

Reference Point #	Reference * Temperature °F	Pyrometer Temperature °F	Temperature difference ** %
1	10	10	0.00
2	32	33	-3.13
3	60	60	0.00
4	100	100	0.00
5	200	200	0.00
6	300	300	0.00
7	400	399	0.25
8	500	498	0.40
9	700	700	0.00
10	900	899	0.11
11	1000	998	0.20
12	1200	1197	0.25
13	1400	1396	0.29
14	1600	1595	0.31
15	1700	1693	0.41
16	1900	1895	0.26

* Digital Calibrator Thermometer, S/N 28494/991
-60 °F to 1999 °F

** Allowable % difference = 5 %

**2520 Pegasus Drive
Bakersfield, CA 93308
(805) 393-0272**

[illegible]

**2520 Pegasus Drive
Bakersfield, CA 93308
(805) 393-0272**

[illegible]

**2520 Pegasus Drive
Bakersfield, CA 93308
(805) 393-0272**

[illegible]

APPENDIX A

FIELD DATA

ENGINEERING-SCIENCE, INC.
CEM FIELD DATA SHEET

PLANT COALINGA COGEN CEM VAN NO. 3 DATE 3/4/93
TEST LOCATION HRSO BUTLER STACK OPERATOR T DELFINO

O₂, %
Calibration Gases :
High 20.9 Cyl. # 49574
Mid 15.14 Cyl. # ALMD11705
Low 4.002 Cyl. # ALMD27375

CO₂, %
Calibration Gases :
High _____ Cyl. # _____
Mid _____ Cyl. # _____
Low _____ Cyl. # _____

NO_x, ppm
Calibration Gases :
High 23.2 Cyl. # AN2534
Mid 12.7 Cyl. # MS11324
Low 8.46 Cyl. # AS22850

CO, ppm
Calibration Gases :
High 18.56 Cyl. # AN2534
Mid 12.54 Cyl. # ALMD11324
Low 8.352 Cyl. # ALMD22850

SO₂, ppm
Calibration Gases :
High _____ Cyl. # _____
Mid _____ Cyl. # _____
Low _____ Cyl. # _____

Calibration Gases :
High _____ Cyl. # _____
Mid _____ Cyl. # _____
Low _____ Cyl. # _____

TIME	SAMPLE POINT	O ₂ (%)	CO ₂ (%)	NO _x (ppm)	CO (ppm)	SO ₂ (ppm)	COMMENTS / RUN #
		<u>15.14</u>		<u>8.46</u>	<u>12.54</u>		Span gas values used for test.
		<u>20.9</u>		<u>23.2</u>	<u>18.56</u>		HIGH LINEARITY Check
		<u>15.14</u>		<u>12.58</u>	<u>12.42</u>		MID
		<u>4.07</u>		<u>8.43</u>	<u>8.45</u>		LOW
<u>0815-0820</u>	<u>Run-1</u>	<u>14.50</u>		<u>2.20</u>	<u>10.40</u>		<u>Run-1</u>
<u>0820-0825</u>		<u>14.50</u>		<u>2.40</u>	<u>10.40</u>		
<u>0825-0830</u>		<u>14.48</u>		<u>2.23</u>	<u>11.00</u>		
<u>0830-0835</u>		<u>14.47</u>		<u>2.15</u>	<u>11.00</u>		
<u>0835-0840</u>		<u>14.46</u>		<u>2.14</u>	<u>10.60</u>		
<u>0840-0845</u>		<u>14.45</u>		<u>2.15</u>	<u>10.65</u>		
		<u>14.48</u>		<u>2.21</u>	<u>10.68</u>		ALC.
		<u>14.48</u>		<u>2.21</u>	<u>10.68</u>		
<u>CALIBRATE</u>		<u>0.0</u>		<u>0.00</u>	<u>0.20</u>		Zero Check
		<u>15.14</u>		<u>8.46</u>	<u>12.54</u>		SPAN Check

ENGINEERING-SCIENCE, INC.
CEM FIELD DATA SHEET

Page 2 of 4

PLANT TEST LOCATION COALINGA COGEN 3 CEM VAN NO. 3 DATE 3/4/93
HRS OUTLET STACK OPERATOR T. DEUFINO

TIME	SAMPLE POINT	O2 (%)	CO2 (%)	NOx (ppm)	CO (ppm)	SO2 (ppm)	COMMENTS / RUN #
		15.14		8.46	12.54		Span gas values used for test.
0900-0905	RUN-2	14.54		3.30	9.70		RUN-2
0905-0910		14.54		3.60	7.50		
0910-0915		14.54		3.70	9.10		
0915-0920		14.54		3.65	8.90		
0920-0925		14.54		3.63	8.90		
0925-0930		14.54		3.60	8.90		
		$\bar{x} = 14.54$		$\bar{x} = 3.58$	$\bar{x} = 9.17$		
CALIBRATE		0.00		0.00	0.00		ZERO CHECK
		15.14		8.46	12.54		SPAN CHECK
0945-0950	RUN-3	14.53		3.80	9.0		RUN-3
0950-0955		14.53		3.80	8.3		
0955-1000		14.53		3.40	9.2		
1000-1005		14.53		3.55	9.0		
1005-1010		14.53		3.75	8.9		
1010-1015		14.53		3.70	8.6		
		$\bar{x} = 14.53$		$\bar{x} = 3.67$	$\bar{x} = 8.83$		AVG.
CALIBRATE		0.00		0.00	0.00		ZERO CHECK
		15.14		8.67	12.50		SPAN CHECK
1030-1035	RUN-4	14.50		4.05	7.70		RUN-4
1035-1040		14.50		3.40	8.40		
1040-1045		14.50		3.70	8.30		
1045-1050		14.52		3.80	7.80		
1050-1055		14.55		3.25	9.10		
1055-1100		14.57		3.90	8.40		
		$\bar{x} = 14.52$		$\bar{x} = 3.68$	$\bar{x} = 8.35$		AVG.
CALIBRATE		0.00		0.00	0.00		ZERO CHECK
		15.14		8.55	12.54		CHECK SPAN

ENGINEERING-SCIENCE, INC.
CEM FIELD DATA SHEET

PLANT COMINGAR COGEN CEM VAN NO. 3 DATE 3/4/93
TEST LOCATION HRSG OUTLET OPERATOR T. DELFINO

TIME	SAMPLE POINT	O2 (%)	CO2 (%)	NOx (ppm)	CO (ppm)	SO2 (ppm)	COMMENTS / RUN #
		15.14		8.46	12.54		Span gas values used for test.
1115 - 1120	Run-5	14.57		3.62	7.95		Run-5
1120 - 1125		14.59		4.05	8.00		
1125 - 1130		14.59		3.96	8.25		
1130 - 1135		14.59		4.30	7.80		
1135 - 1140		14.59		4.10	8.00		
1140 - 1145		14.59		3.75	7.80		
Calibrate		$\bar{x} = 14.59$		$\bar{x} = 3.95$	$\bar{x} = 7.97$		AVG.
		0.00		0.00	0.00		Zero Check
		15.14		8.46	12.54		Span Check
1200 - 1205	Run-6	14.52		4.00	7.50		Run-6
1205 - 1210		14.52		3.60	8.00		
1210 - 1215		14.50		3.80	8.10		
1215 - 1220		14.50		3.70	8.15		
1220 - 1225		14.48		3.55	8.40		
1225 - 1230		14.48		4.00	7.80		
Calibrate		$\bar{x} = 14.50$		$\bar{x} = 3.78$	$\bar{x} = 7.99$		AVG.
		0.00		0.00	0.00		Zero Check
		15.08		8.46	12.54		Span Check
1245 - 1250	Run-7	14.55		4.00	7.80		Run-7
1250 - 1255		14.55		4.00	7.00		
1255 - 1300		14.58		4.20	7.80		
1300 - 1305		14.58		3.70	8.00		
1305 - 1310		14.58		4.40	6.80		
1310 - 1315		14.58		4.30	6.80		
Calibrate		$\bar{x} = 14.57$		$\bar{x} = 4.13$	$\bar{x} = 7.29$		AVG.
		0.00		0.00	0.00		Zero Check
		15.14		8.46	12.54		Span Check

ENGINEERING-SCIENCE, INC.
CEM FIELD DATA SHEET

Page 4 of 4

PLANT TEST LOCATION COALINGA COGEN CEM VAN NO. 3 DATE 3/4/93
HRS6 OUTLET STACK OPERATOR T. DELFINO

TIME	SAMPLE POINT	O2 (%)	CO2 (%)	NOx (ppm)	CO (ppm)	SO2 (ppm)	COMMENTS / RUN #
		15.14		8.46	12.54		Span gas values used for test.
1330 - 1345	RUN-8	14.55		4.30	7.40		RUN-8
1345 - 1350		14.55		4.40	7.00		
1350 - 1355		14.55		4.20	7.80		
1355 - 1400		14.55		4.25	7.75		
		14.55		4.25	7.50		
		14.55		4.40	7.20		
		$\bar{x} = 14.56$		$\bar{x} = 4.30$	$\bar{x} = 7.44$		AVG.
CALIBRATE		0.00		0.00	0.00		ZERO check
		15.14		8.33	12.54		SPAN check
1415 - 1420	RUN-9	14.55		4.15	7.90		RUN-9
1420 - 1425		14.55		4.27	7.70		
1425 - 1430		14.55		4.27	7.60		
1430 - 1435		14.55		4.20	7.70		
1435 - 1440		14.55		4.30	7.60		
1440 - 1445		14.55 14.55		4.40	7.50		
		$\bar{x} = 14.56$		$\bar{x} = 4.27$	$\bar{x} = 7.67$		AVG.
CALIBRATE		0.00		0.00	0.00		ZERO check
		15.14		8.46	12.54		SPAN check
1500 - 1505	RUN-10	14.60		4.30	7.40		RUN-10
1505 - 1510		14.60		3.80	8.10		
1510 - 1515		14.60		4.10	7.40		
1515 - 1520		14.61		4.60	7.5		
1520 - 1525		14.61		3.70	8.0		
1525 - 1530		14.62		4.30	7.80		
		$\bar{x} = 14.61$		$\bar{x} = 4.13$	$\bar{x} = 7.77$		AVG.
CALIBRATION		0.0		0.00	0.00		ZERO check
		15.14		8.53	12.54		SPAN check
		15.05		8.38	12.50		SYSTEM BIAS CK ✓

CO = 12.94 mm

CO = 0.0 mm
CO = 0.03 mm

Calculated CO = (0.20 mm) full scale

LOW CO = 8.45 mm

HIGH CO = 12.42 mm

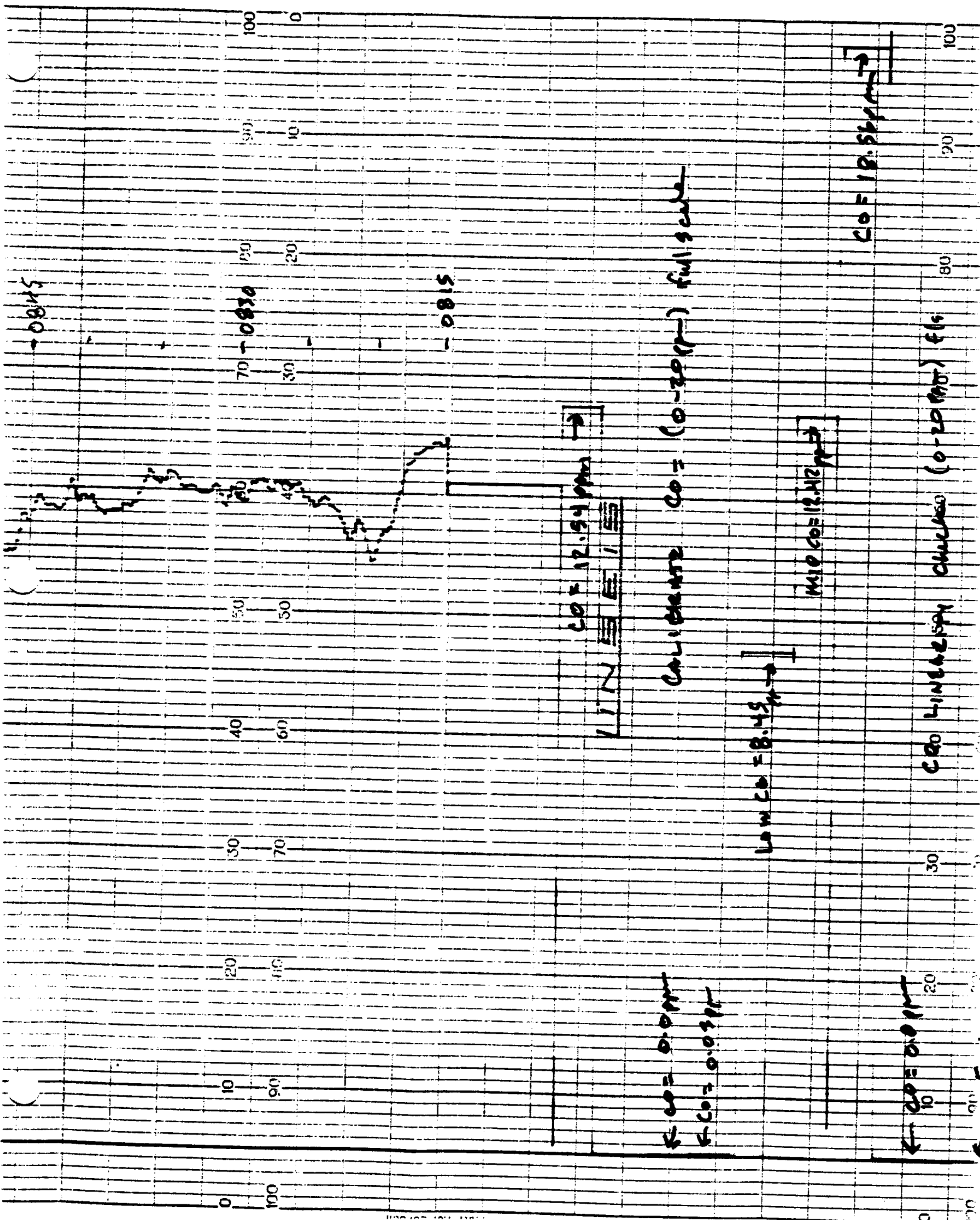
CO = 18.56 mm

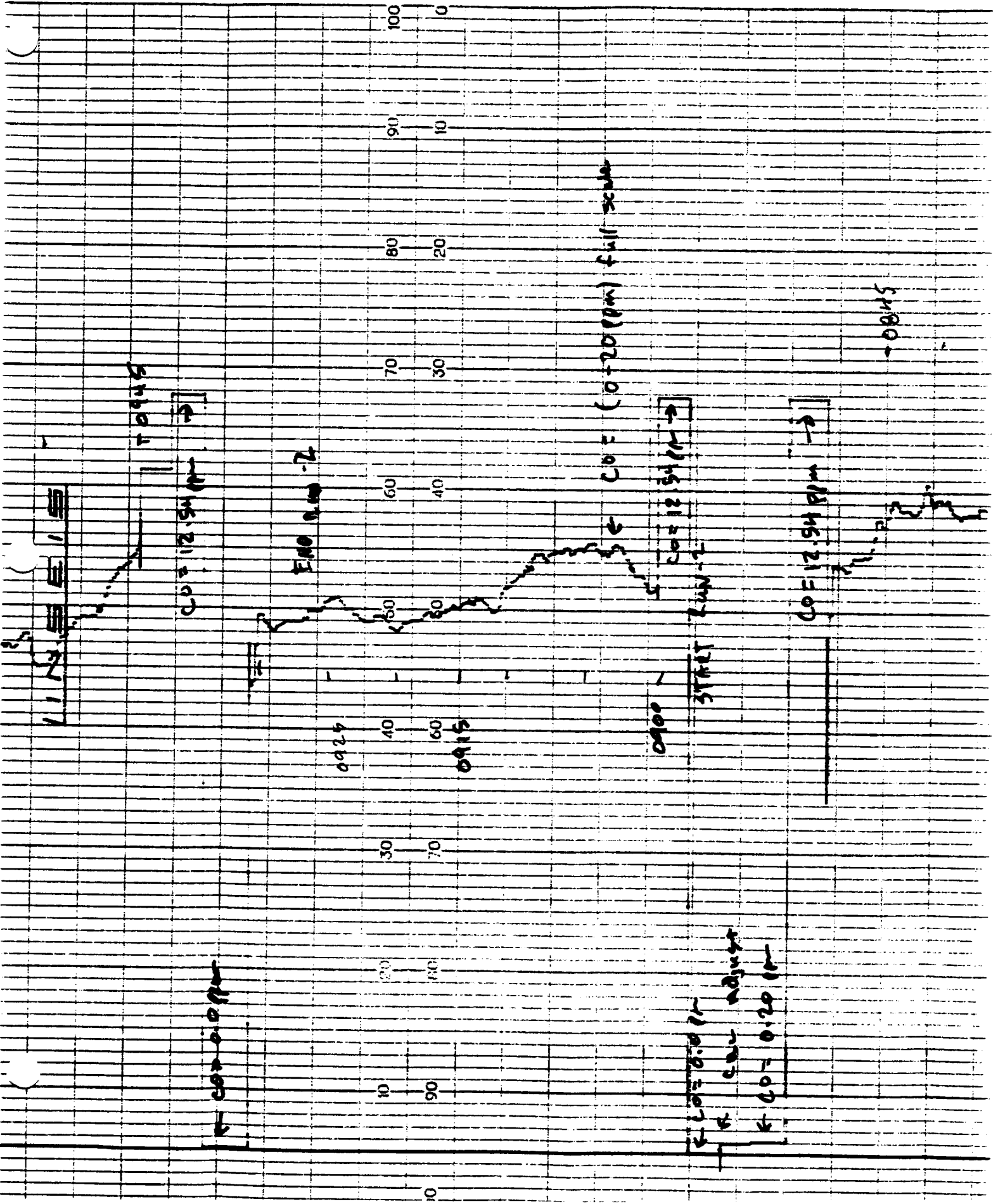
CO = 0.0 mm

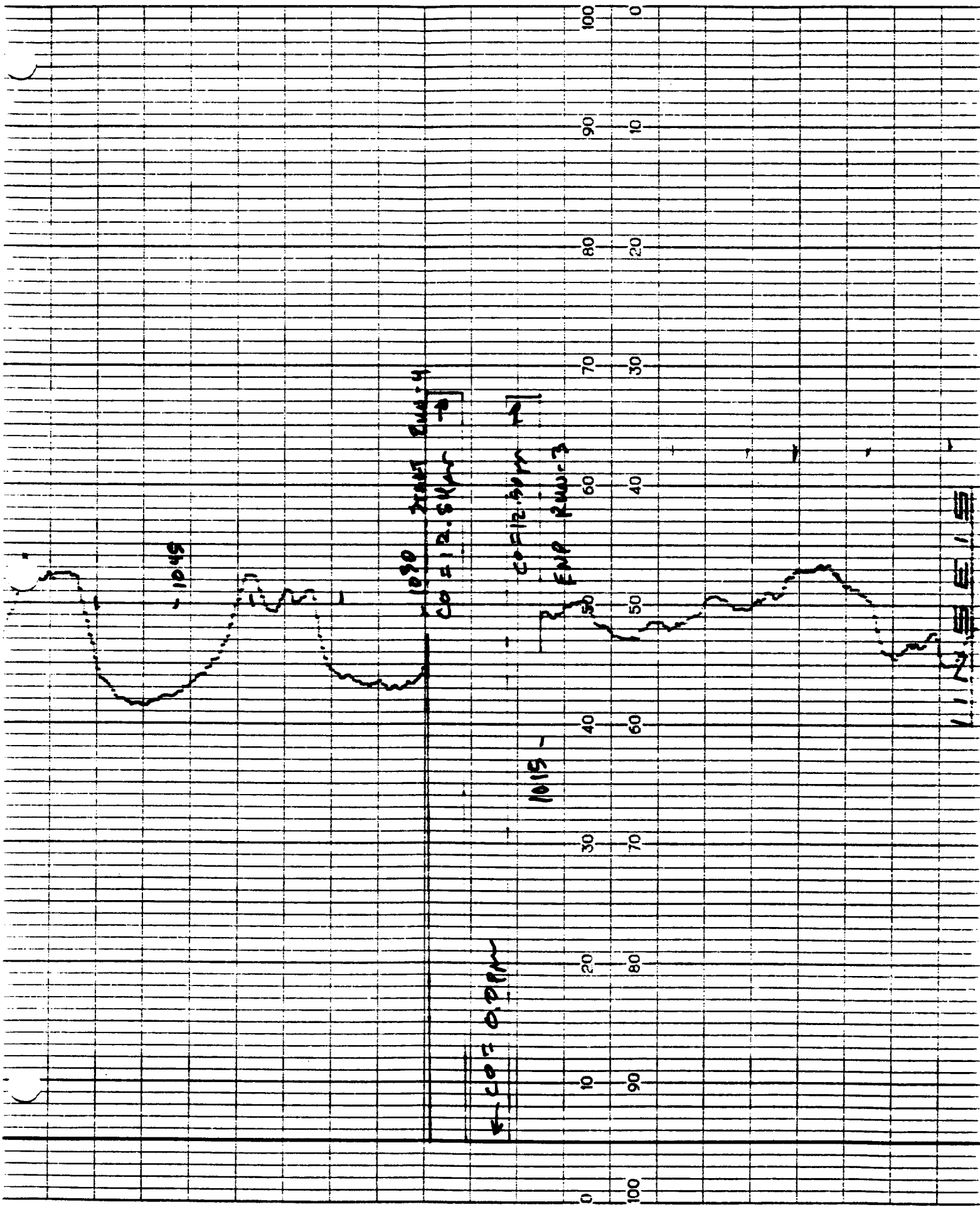
5 days duration
Zero offset

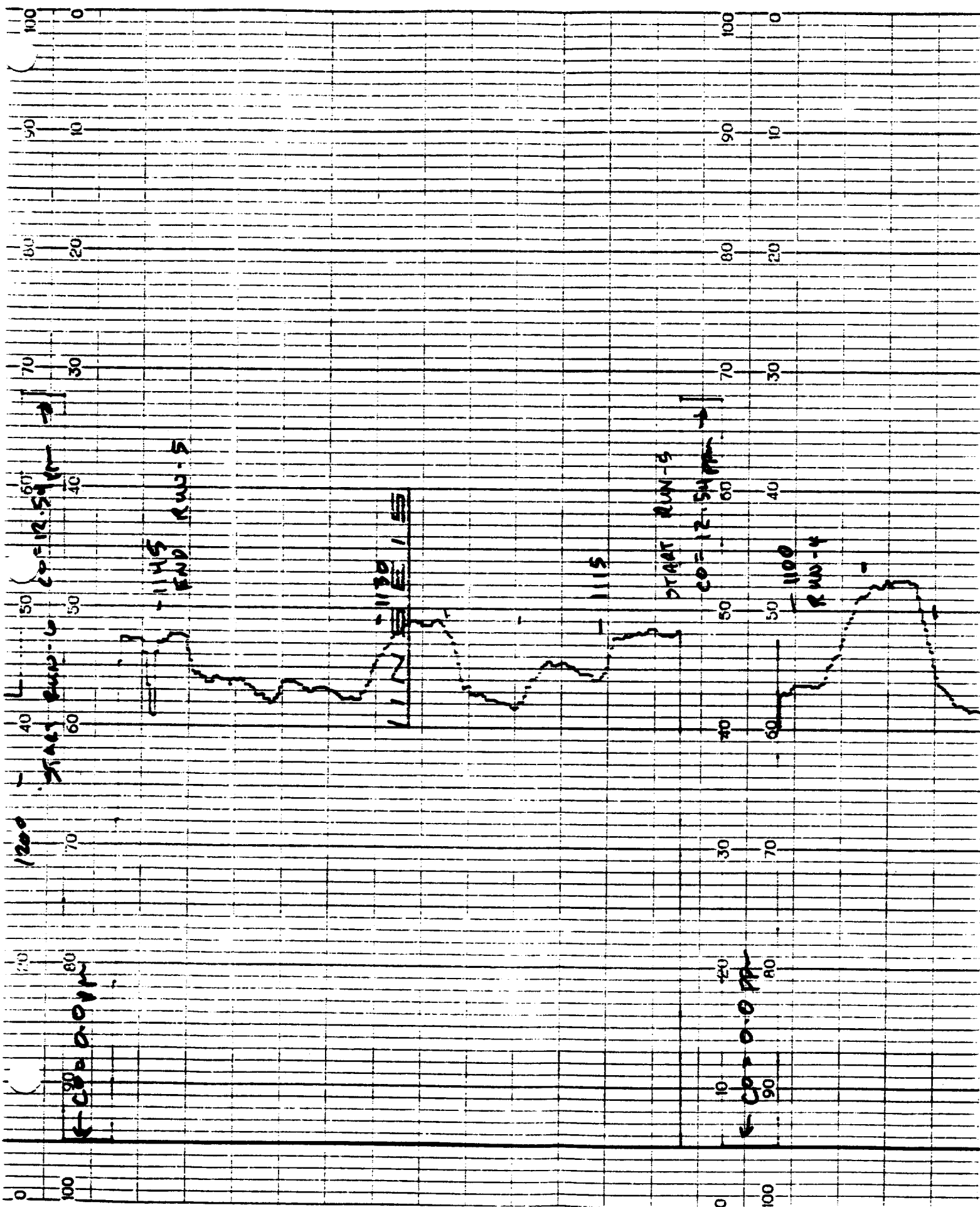
CO LINEARITY CHECK (0.20 mm) FL

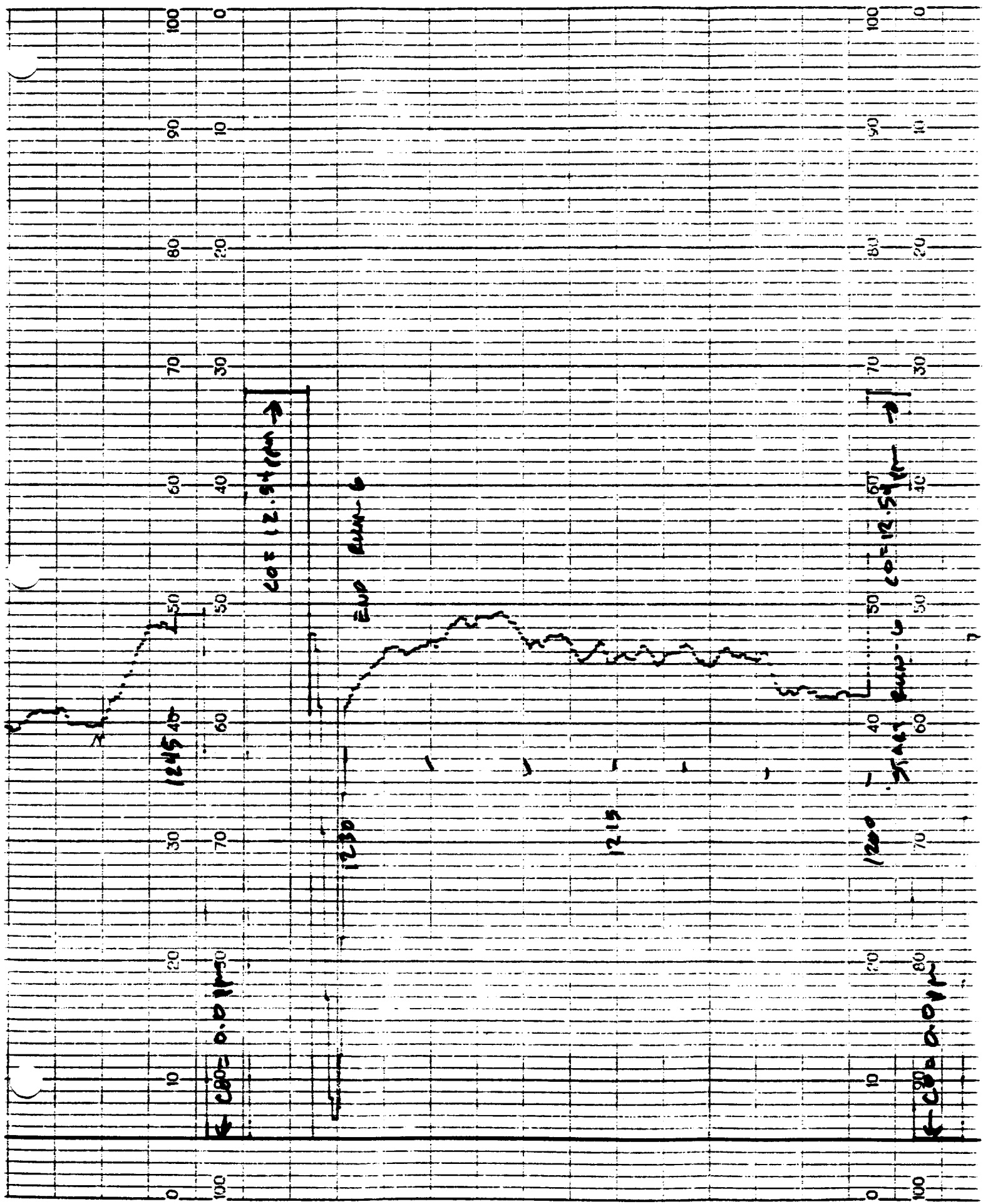
COMINGA COGEN
Hess Outlet Stack
2/4/93

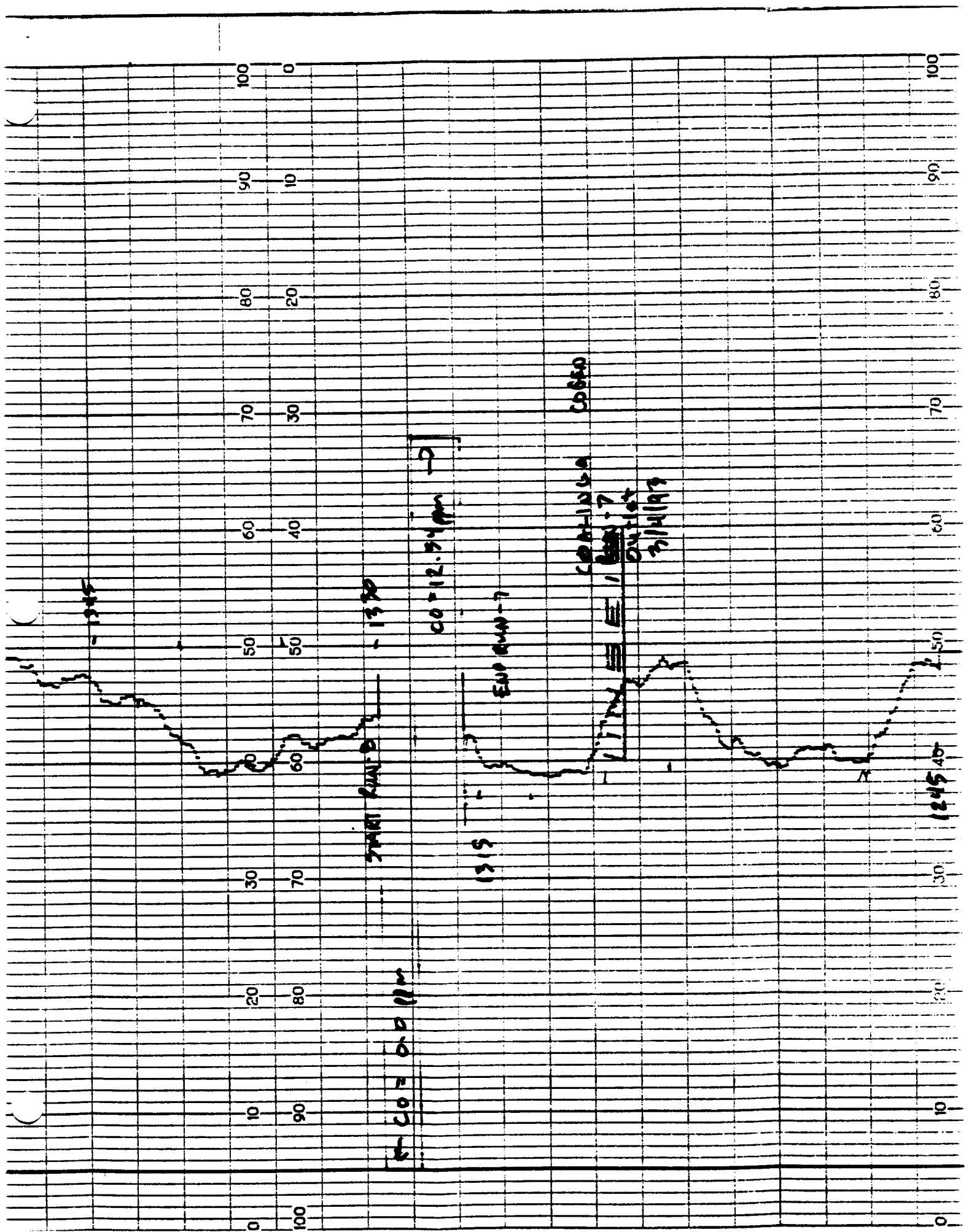


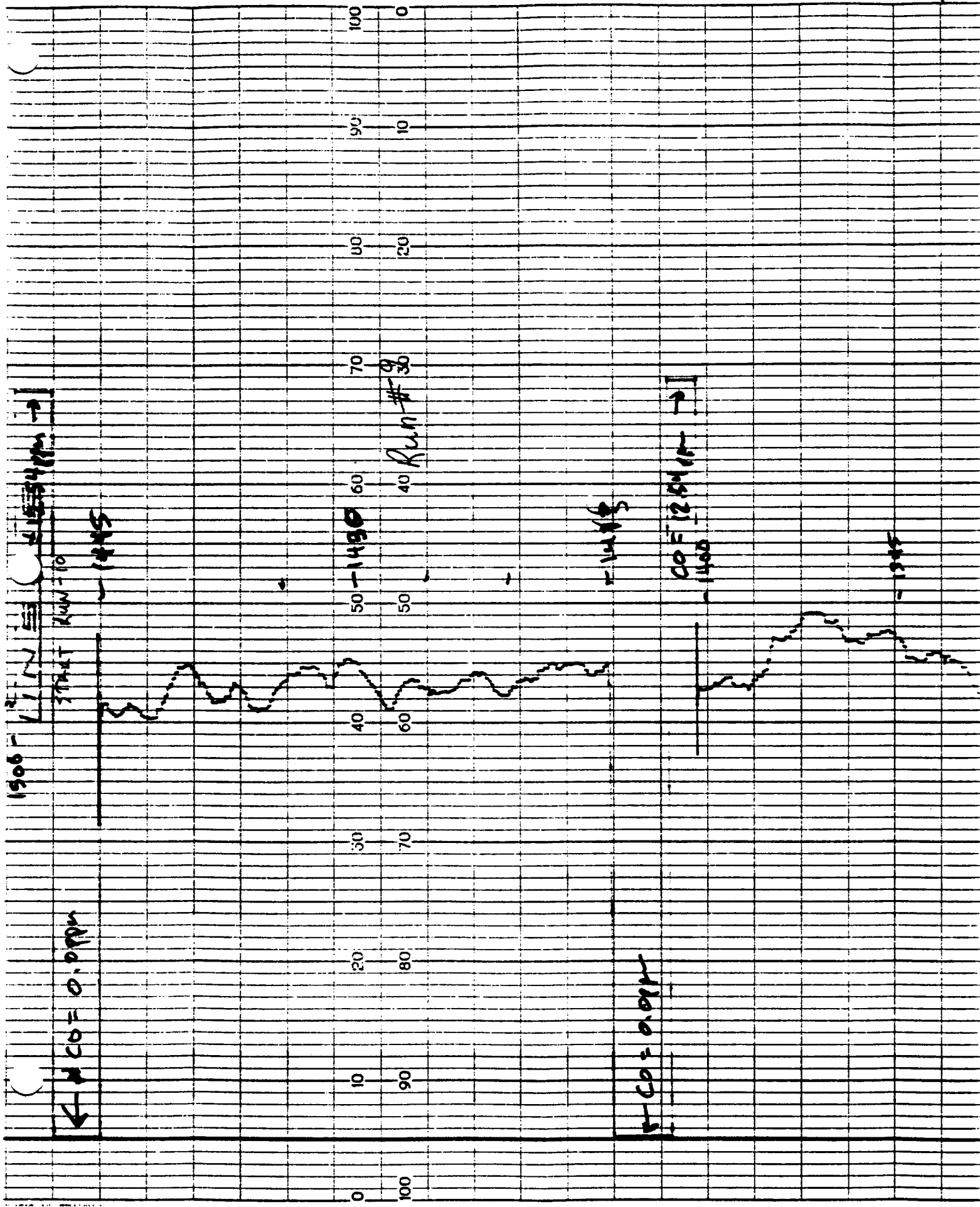








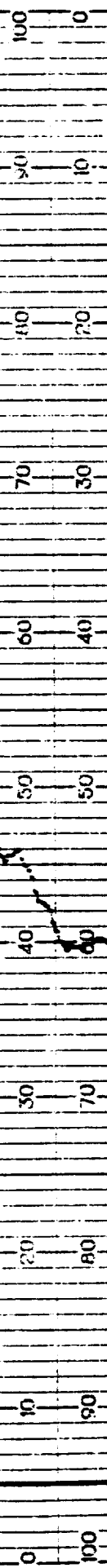




END CO = 12.59ppm →
 SAMPLE SYSTEM BINS CHECK
 CO = 12.59ppm →

← CO = 0.01ppm

1300-1120-10
 END RUN-10



Run #10

1500-1120-10
 START RUN-10

← CO = 0.01ppm

1445

O₂ = 15.14%

NOT = 8.46 ppm

CHANGE NOT TO (0-10 ppm) Full scale + calibration

← O₂ = 0.0%

← NOT = 0.0 ppm

LOW NOT = 8.46 ppm

MID NOT = 0.50 ppm

HIGH NOT = 23.2 ppm

NOT LINEARITY CHECK (0-25 ppm) 1/16

20 ← LOW O₂ = 4.07%

100

90

80

70

60

50

40

30

20

10

0

← NOT = 0.0 ppm

MID O₂ = 15.14% →

HIGH O₂ = 20.9% →

100

90

80

70

60

50

40

30

20

10

0

O₂ LINEARITY CHECK (0-25%) Analysis

O₂ = 20.9% →

NOT = 8.46 ppm

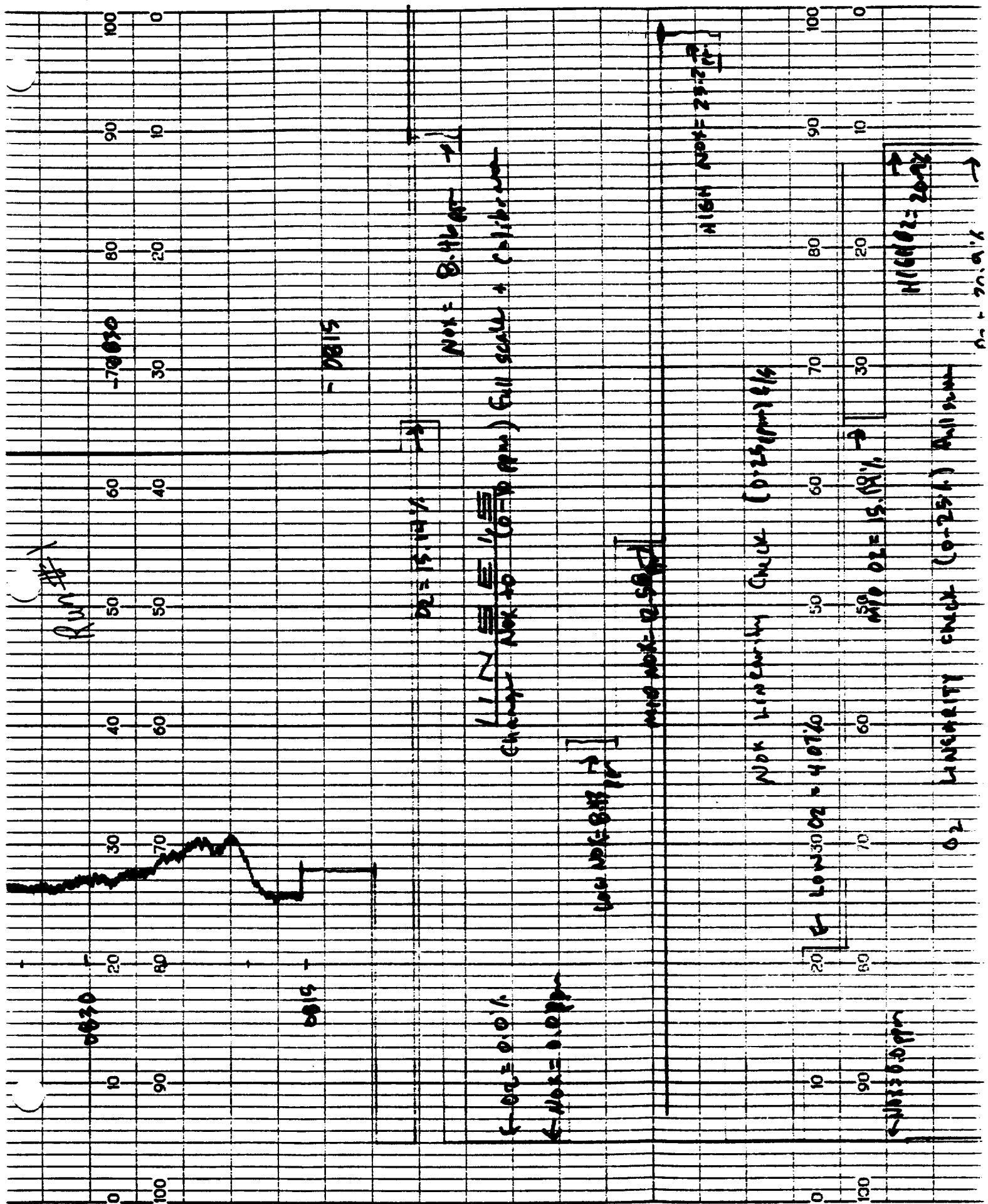
← NOT = 0.0 ppm

← O₂ = 0.0%

← 2.5 chart division zero offset

INITIAL CALIBRATION

COALINGA CODED
HASE OUTLET STACK
3/4/93



02 = 15.14% →

← 02 = 0.0%

NOX = 0.46 ppb →

END RUN-2

← 0025

← 0015

← 02 = (0.25%) + 13

← 0900

NOX = 0.46 ppb

02 = 15.14% →

NOX = 0.35 ppb →

← 0845

NOX = 10-10 ppm (H) →

0900

START RUN-2

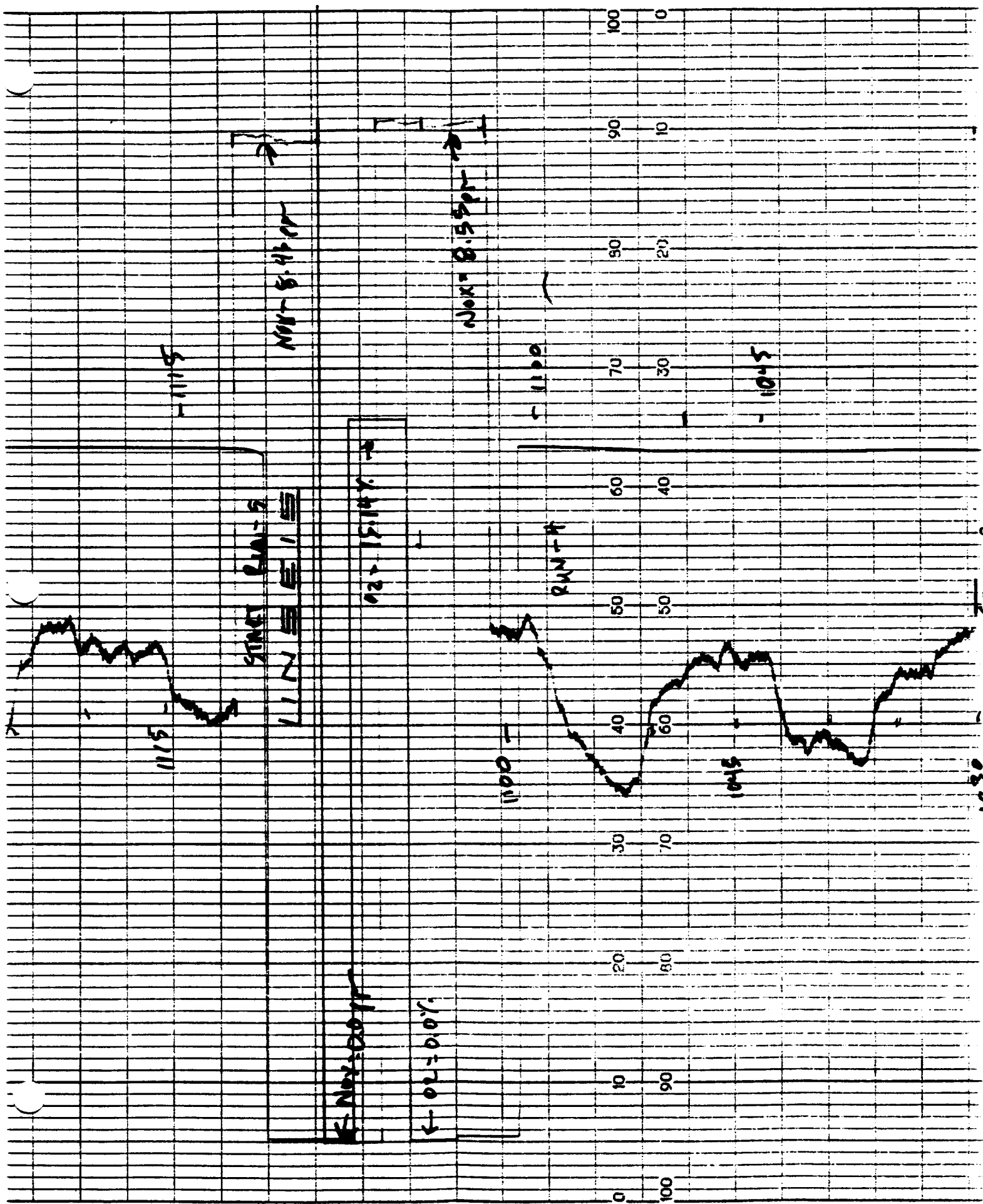
NOX = 0.0 ppb

← 02 = 0.0%

0015

RUN #1

0030



0 10 20 30 40 50 60 70 80 90 100

$\leftarrow N_{\text{K}} = 0.84\%$

$\leftarrow \sigma_L = 0.00\%$

1200

9005 END-6

$\sigma_L = 15.14\%$

-11200

1215

-1215

1145

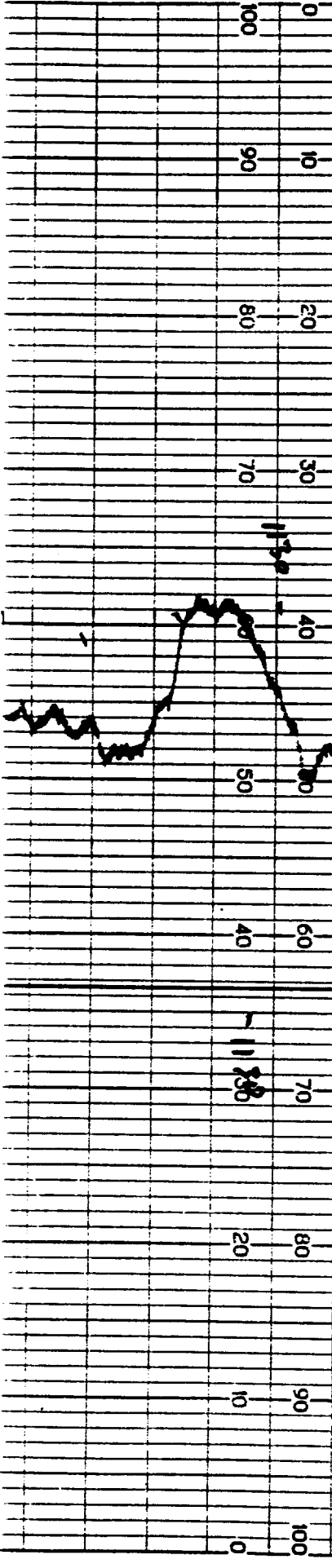
-1145

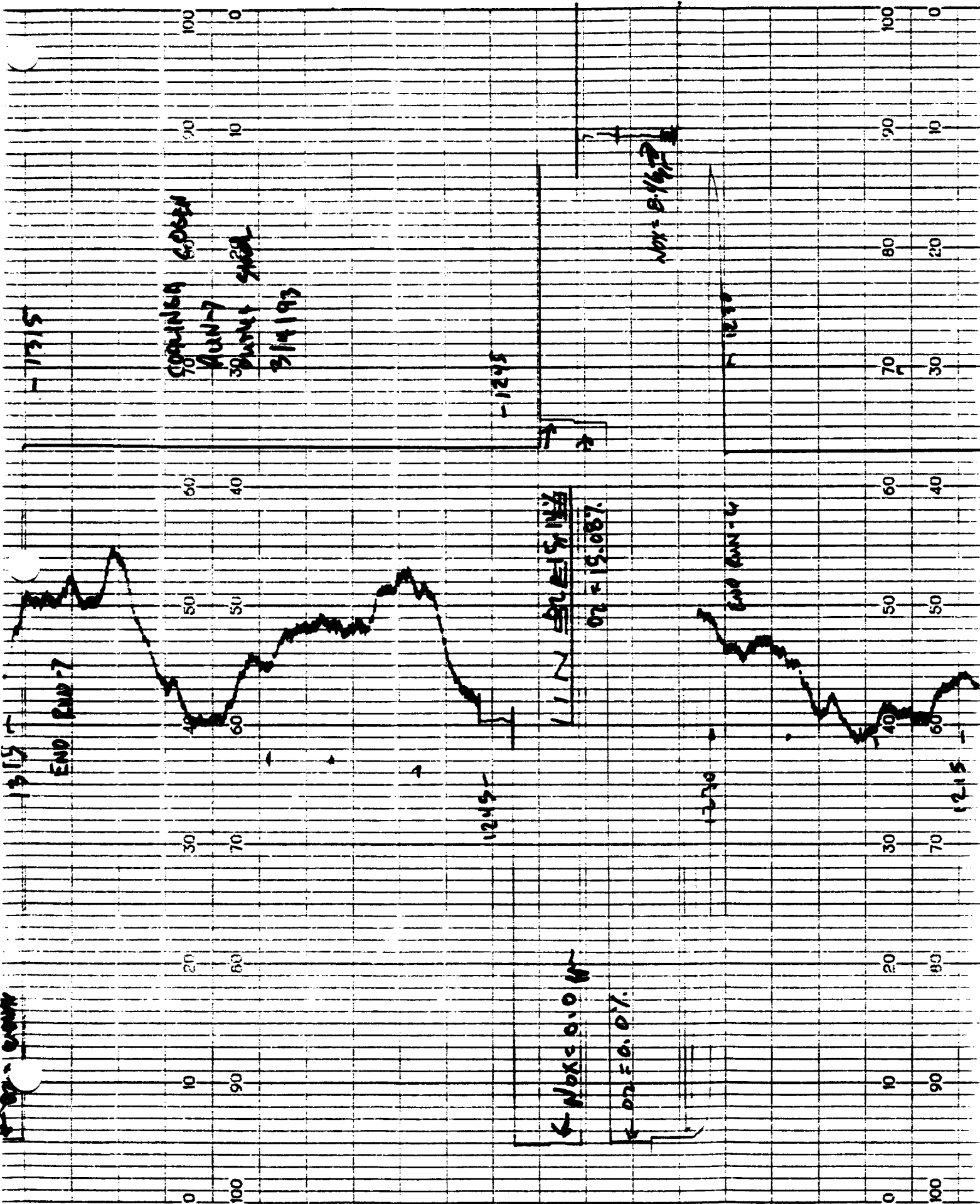
END END-5

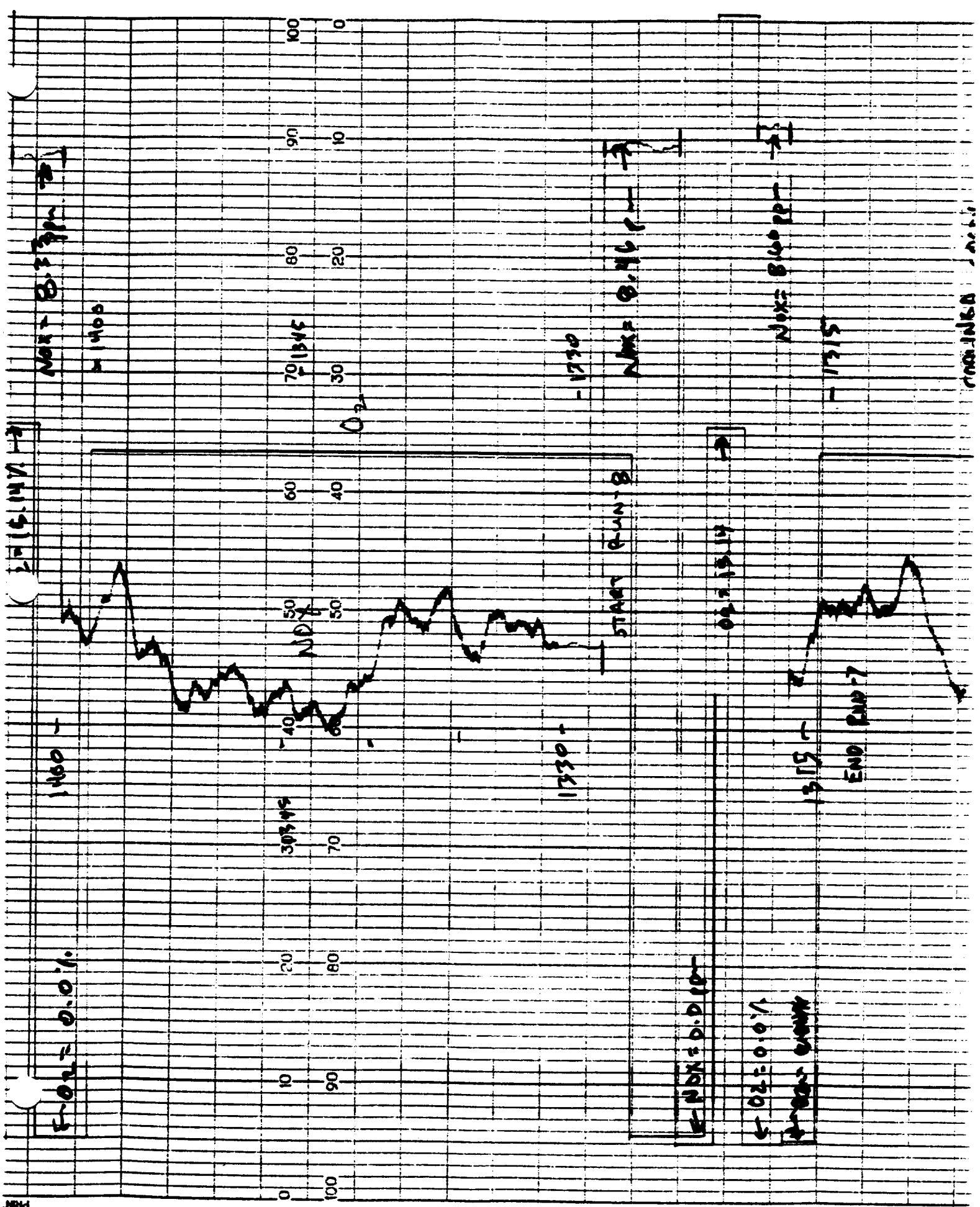
$N_{\text{K}} = 0.46\%$

1130

-1130







EXT. 0.2 = 15.061

11.11.55

EXT. MAX. 8.38

SAMPLE SYSTEM DMS CHECK

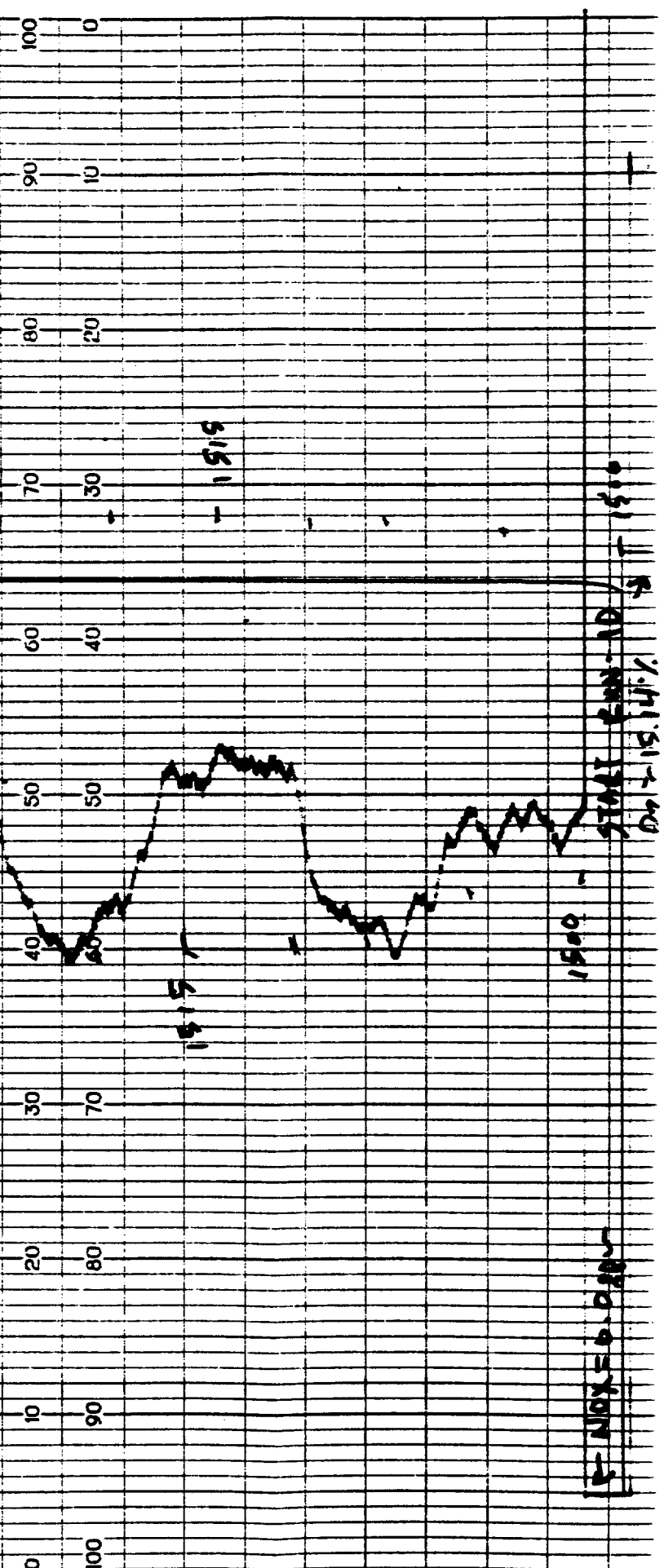
0.2 = 15.14V

0.2 = 0.0%

NOX = 8.53

END RUN - 10

15.30



Page 1 of 1

ENGINEERING—SCIENCE, INC.

$$\begin{array}{r} 3493 \\ \hline \end{array}$$

K-FACTOR:

Nozzle # / Size N/A

TOTAL:	35.1
--------	------

[illegible]

Page 1 of 1

ENGINEERING—SCIENCE, INC.

K-FACTOR:

Nozzle # / Size N/A

TOTAL: 35.2[illegible]

Page 1 of 1

ENGINEERING—SCIENCE, INC.

K-FACTOR:

Nozzle # / Size N/A

[illegible]

Page 1 of 1Date 3-4-93

Note: Using a 10 liter sample bag, set the flowrate as follows: 15 min sample = 0.67 l/min; 30 min sample = 0.33 l/min; 60 min sample = 0.17 l/min.

APPENDIX B

LABORATORY DATA

Project # WA 344

Company: Coalinga Logen

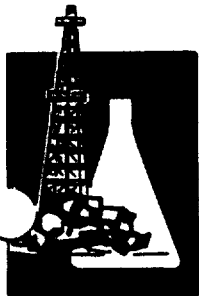
Analysis For: NH_3

Sample Dates:

Source: Outlet stack

Method and Handling: Samples collected by BAAGWD ST-1b. Analyzed by Ion Selective Electrode (ISE). Calibrated ISE Meter w/ 1ppm, 10ppm, and 100ppm standards. 1ppm = 76.9 mV, 10ppm = 21.6 mV, 100ppm = -36.8 mV. ISE Meter calculated slope = -59.0 mV. ISE Meter corrects slope automatically for blank water value.

Identification		Raw Data						Comments/Descriptions
Sample ID Number	Run Number	Total Sample Volume, ml	Aliquot Sample Volume, ml	MV (millivolts)	PPM	mg/sample		
BK9303021	1a	351	100	61.4	1.96	.688	> 93.9 % Dup	
BK9303021	1b	351	100	62.8	1.84	.646		
BK9303022	2a	303	100	79.9	.848	.257		
BK9303022	2ap	303	100	45.5	3.83	—	Added 50 ml of 10 ppm Std = 333 ppm sample 3.83 / (3.33 + .848) × 100 = 91.7% Rec	
BK9303023	3	310	100	73.9	1.13	.350		
BK9303024	B1	100	100	152.0	0.000	0.000		
	QC	100	100	-37.3	102	102% Conf		
							Analyst LM Date 3/25/93	



oilwell research, inc.
ANALYTICAL LABORATORIES

Established 1949

California State Approved
Testing Laboratory

3161 Pegasus Drive
P.O. Box 80475
Bakersfield, CA
93380-0475
805 392-8811

NPDES Permit Analysis
Injection Water Quality
Reservoir Fluid Analysis
Natural Gas Analysis
Enhanced Recovery
Drilling & Production Support

PRECISION ANALYSIS / QUALITY SERVICE

March 11, 1993

**Attention: Mr. Gary McRae
ENGINEERING SCIENCE, INC.
2520 Pegasus Drive
Bakersfield, CA 93308**

Ref: Lab No. 93-1853

Enclosed please find your report of analysis performed on the samples submitted to our lab on March 4, 1993.

All measureable results greater than the detection limits were rechecked and a blank run to verify the results.

We thank you for this opportunity to be of service. If you should have any questions concerning this report, or require further analysis, please do not hesitate to call.

Respectfully submitted,

**Ronald P. Hoff
RPH/sj**

enclosures

Attention: Mr. Gary McRae
ENGINEERING SCIENCE, INC.
2520 Pegasus Drive
Bakersfield, CA 93308

Report Date: March 11, 1993
Sampled: March 4, 1993
Submitted: March 4, 1993
Lab No. 93-1853-1

LABORATORY TEST REPORT

Project Name: Coalinga Cogen Compliance

Project No.: WA344

Sample ID: Run #1

Control No. BK93030025

Analyzed For: Trace Hydrocarbons

Method: EPA 18

<u>Component</u>	<u>Found</u>	<u>Units</u>	<u>MDL</u>
Methane	ND	ppm	1.0
Ethane	ND	ppm	1.0
Propane	ND	ppm	1.0
Butane	ND	ppm	1.0
Pentane	ND	ppm	1.0
Hexanes +	1.0	ppm	1.0

ND: None Detected
MDL: Method Detection Limit

Date Analyzed: 10-Mar-93
Analyst: S. Harris

Attention: Mr. Gary McRae
ENGINEERING SCIENCE, INC.
2520 Pegasus Drive
Bakersfield, CA 93308

Report Date: March 11, 1993
Sampled: March 4, 1993
Submitted: March 4, 1993
Lab No. 93-1853-2

LABORATORY TEST REPORT

Project Name: Coalinga Cogen Compliance

Project No.: WA344

Sample ID: Run #2

Control No. BK93030026

Analyzed For: Trace Hydrocarbons

Method: EPA 18

<u>Component</u>	<u>Found</u>	<u>Units</u>	<u>MDL</u>
Methane	ND	ppm	1.0
Ethane	ND	ppm	1.0
Propane	ND	ppm	1.0
Butane	ND	ppm	1.0
Pentane	ND	ppm	1.0
Hexanes +	1.6	ppm	1.0

ND: None Detected
MDL: Method Detection Limit

Date Analyzed: 10-Mar-93
Analyst: S. Harris

Attention: Mr. Gary McRae
ENGINEERING SCIENCE, INC.
2520 Pegasus Drive
Bakersfield, CA 93308

Report Date: March 11, 1993
Sampled: March 4, 1993
Submitted: March 4, 1993
Lab No. 93-1853-3

LABORATORY TEST REPORT

Project Name: Coalinga Cogen Compliance

Project No.: WA344

Sample ID: Run #3

Control No. BK93030027

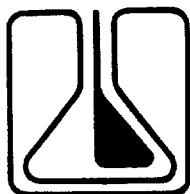
Analyzed For: Trace Hydrocarbons

Method: EPA 18

<u>Component</u>	<u>Found</u>	<u>Units</u>	<u>MDL</u>
Methane	ND	ppm	1.0
Ethane	ND	ppm	1.0
Propane	ND	ppm	1.0
Butane	ND	ppm	1.0
Pentane	ND	ppm	1.0
Hexanes +	ND	ppm	1.0

ND: None Detected
MDL: Method Detection Limit

Date Analyzed: 10-Mar-93
Analyst: S. Harris



ZALCO LABORATORIES, INC.

Analytical & Consulting Services

ENGINEERING SCIENCE
2520 Pegasus Drive
Bakersfield, CA 93308

Lab. No.: 035013_001
Received: Mar 4, 1993
Reported: Mar 4, 1993

Attention: Gary McRae

Sample Description: Coalinga Cogen WA344 BK9303020 Fuel
Gas Sample 3/4/93

* CHROMATOGRAPHIC ANALYSIS (Z 1635) *

Components	Mole %	Wt %	CHONS	Wt %
Hydrogen	0.000	0.000	CARBON	72.37
Carbon Dioxide	2.157	5.243	HYDROGEN	22.72
Oxygen	.049	.087	OXYGEN	3.90
Nitrogen	.649	1.004	NITROGEN	1.00
Carbon Monoxide	0.000	0.000	SULFUR	0.00
Hydrogen Sulfide	0.000	0.000		
Methane	88.563	78.481	Totals	99.99
Ethane	7.540	12.523	Total H/C	.31
Propane	.907	2.210		
IsoButane	.046	.146		
N-Butane	.071	.229		
IsoPentane	.008	.031		
N-Pentane	.006	.024		
Hexanes+	.005	.023		
Totals =	100.000	100.000		

SPECIFIC GRAVITY (Air = 1) .6263
SPECIFIC VOLUME, cu.ft./lb * 20.92
GROSS CALORIFIC VALUE, BTU/cu.ft. * 1041.89
GROSS CALORIFIC VALUE, BTU/cu.ft. ** 1059.91
GROSS CALORIFIC VALUE, BTU/lb ** 22175.10
NET CALORIFIC VALUE, BTU/cu.ft. ** 956.81
NET CALORIFIC VALUE, BTU/lb ** 20017.99
DSCF EXHAUST PER SCF FUEL (0% Oxygen) 9.0074
COMPRESSIBILITY FACTOR 'Z' (60 F, 1 ATM) .9976
EPA 'F' Factor @ 68 F: 8647.843 DSCF / MM Btu.
KCAPCD 'F' Factor @ 60 F: 8518.126 DSCF / MM Btu.

* Water Saturated

** Dry Gas @ 60 F, 14.73 psia

Analyst

Jim Etherton
Laboratory Director

4309 Armour Avenue Bakersfield, California 93308

(805) 395-0539

FAX (805) 395-3069

APPENDIX C

PLANT DATA

***** Coalinga Cogeneration Company *****
Coalinga, Fresno County, CA 93210

	Air #/sec	Gas #/sec	H2O #/sec	Inj. Ratio	H2O gal/hr
08:00	313.81	5.89	3.90	.66	28.25

One Hour Log

Time hh:mm	Gas	O2	CO			NOx (Stack)				
	mmBTU	Pct	ppm	ppmC	#/mmBTU	#/hrC	ppm	ppmC	#/mmBTU	#/hrC
08:00	3579.00	14.49	8.37	7.70	.017	8.34	3.56	3.28	.012	5.83

Time hh:mm	Air	Gas	H2O	NH3	NH3 Slip		Inj. Ratio	H2O gal/hr	NH3/NOx Ratio	SCR NOx	Temp
	#/sec	#/sec	#/sec	SCFH	ppmC	#/hr					
08:00	314.80	5.93	3.83	632.60	4.11	2.51	.65	27.74	.92	43.97	733.800

Description	Date	Time hh:mm	Zero			Upscale			Fail	
			Expected	Actual	%Drift	Expected	Actual	%Drift	1 Dy	5 Dy
NOx ppm (SCR)	03/04/93	08:12	0.000	-.310	-.31	82.800	83.033	.23		

Description	Date	Time hh:mm	Zero			Upscale			Fail	
			Expected	Actual	%Drift	Expected	Actual	%Drift	1 Dy	5 Dy
O2 pct	03/04/93	08:12	0.000	.020	.02	14.850	14.902	.05		

Description	Date	Time hh:mm	Zero			Upscale			Fail	
			Expected	Actual	%Drift	Expected	Actual	%Drift	1 Dy	5 Dy
CO ppm	03/04/93	08:12	0.000	.039	.08	39.300	39.387	.17		

Description	Date	Time hh:mm	Zero			Upscale			Fail	
			Expected	Actual	%Drift	Expected	Actual	%Drift	1 Dy	5 Dy
NOx ppm (STACK)	03/04/93	08:12	0.000	-.020	-.20	7.840	7.913	.73		

Fifteen Minute Log

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		Other	Other	Other	Other	Other	Other	Other	Other	Other	Other
08:15	Other	Other	Other	Other	Other	Maint	Other	Other	Other	Other	Maint

Time hh:mm	NH3 SCFH	NH3 Slip		NH3/NOx		SCR NOx	Temp
		Other	Other	Maint	Maint		
08:15	659.89	Other	Other	Maint	Maint	Other	734.23

	Air #/sec	Gas #/sec	H2O #/sec	Inj. Ratio	H2O gal/hr
08:15	313.21	5.88	3.99	.68	28.86

Fifteen Minute Log

Daily Logs for the of the 1999
 ***** Coalinga Cogeneration Company *****
 Coalinga, Fresno County, CA 93210

Time hr/mm	CO						NOx (Stack)				
	O2 Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
08:30	14.50	9.50	8.76	.020	9.40	9.09	2.39	2.21	.008	3.88	4.27
	NH3 Slip										
	NH3	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
08:30	660.45	6.18	3.75	5.57	3.39	.998	42.25	734.10			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
08:30	312.55	5.89	3.93	.67	28.48						

RA Run #

RA Run #1

Fifteen Minute Log

Time hh/mm	CO						NOx (Stack)				
	O2 Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
08:45	14.51	9.23	8.53	.019	9.18	9.12	2.31	2.13	.008	3.76	4.10
	NH3 Slip										
	NH3	ppmC	#/hr	ppmC	#/hr	Ratio	SCR	NOx	Temp		
08:45	658.96	6.16	3.74	5.77	3.51	.999		42.08	734.20	RA Run # 1	
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
08:45	312.71	5.91	3.89	.66	28.18						

RA Run #1

Fifteen Minute Log

Time hh:mm	CO						NOx (Stack)				
	O2 Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
09:00	14.53	8.37	7.75	.017	8.33	8.97	2.93	2.71	.010	4.78	4.14
	NH3 Slip										
	NH3	---15 min---		---1 hr---		NH3/NOx	--- SCR ---				
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
09:00	636.94	4.69	2.85	5.67	3.45	.950	42.73	734.33			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
09:00	312.89	5.90	3.82	.65	27.65						

One Hour Log

Time hr/mm	Gas mmBTU	O2 Pct	CO				NOx (Stack)			
			ppm	ppmC	#/mmBTU	#/hrC	ppm	ppmC	#/mmBTU	#/hrC
09:00	3451.00	14.51	9.03	8.33	.019	8.96	2.55	2.35	.009	4.15
	Air	Gas	H2O	NH3	NH3 Slip	Inj.	H2O	NH3/NOx	SCR	
	#/sec	#/sec	#/sec	SCFH	ppmC	Ratio	gal/hr	Ratio	NOx	Temp

***** Coalinga Cogeneration Company *****
Coalinga, Fresno County, CA 93210

09:00 312.80 5.89 3.91 654.10 5.67 3.44 .66 28.29 .98 42.40 734.200

Fifteen Minute Log

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		15 min ppm	15 min ppmC	15 min #/mmBTU	1 hr #/hrC	1 hr #/hrC	15 min ppm	15 min ppmC	15 min #/mmBTU	1 hr #/hrC	1 hr #/hrC
09:15	14.53	8.27	7.66	.017	8.23	8.79	3.53	3.27	.012	5.76	4.55
		NH3 Slip									
	NH3	15 min	1 hr	NH3/NOx		SCR					
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
09:15	600.61	3.38	2.05	5.10	3.10	.908	42.25	734.33			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
09:15	312.42	5.89	3.86	.66	27.97						

RA Run#2

Fifteen Minute Log

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		15 min ppm	15 min ppmC	15 min #/mmBTU	1 hr #/hrC	1 hr #/hrC	15 min ppm	15 min ppmC	15 min #/mmBTU	1 hr #/hrC	1 hr #/hrC
09:30	14.54	7.57	7.02	.016	7.49	8.31	3.71	3.44	.013	6.01	5.08
		NH3 Slip									
	NH3	15 min	1 hr	NH3/NOx		SCR					
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
09:30	603.63	3.27	1.98	4.37	2.65	.901	42.87	734.52			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
09:30	311.72	5.85	3.81	.65	27.61						

RA Run#2

Fifteen Minute Log

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		15 min ppm	15 min ppmC	15 min #/mmBTU	1 hr #/hrC	1 hr #/hrC	15 min ppm	15 min ppmC	15 min #/mmBTU	1 hr #/hrC	1 hr #/hrC
09:45	14.54	8.23	7.64	.017	8.18	8.06	3.50	3.25	.012	5.71	5.56
		NH3 Slip									
	NH3	15 min	1 hr	NH3/NOx		SCR					
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
09:45	591.76	3.20	1.94	3.64	2.20	.904	41.90	734.34			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
09:45	311.60	5.88	3.88	.66	28.07						

Fifteen Minute Log

***** Coalinga Cogeneration Company *****
Coalinga, Fresno County, CA 93210

Time hh:mm	CO						NOx (Stack)				
	O2 Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
1:00	14.56	7.49	6.96	.016	7.43	7.83	3.68	3.42	.012	5.98	5.87
NH3 Slip											
	NH3	-15 min	-1 hr	NH3/NOx			SCR				
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
10:00	597.95	3.06	1.85	3.23	1.96	.897	42.69	734.19			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
10:00	311.56	5.85	3.81	.65	27.60						

RA Run# 3

RA Run# 3

One Hour Log

Time hh:mm	Gas		O2 Pct	CO				NOx (Stack)			
	mmBTU			ppm	ppmC	#/mmBTU	#/hrC	ppm	ppmC	#/mmBTU	#/hrC
10:00	3453.00		14.54	7.89	7.32	.016	7.83	3.60	3.35	.012	5.87
Air Gas H2O NH3 -- NH3 Slip -- Inj. H2O NH3/NOx -- SCR --											
#/sec #/sec #/sec SCFH ppmC #/hr Ratio gal/hr Ratio NOx Temp											
10:00	311.80	5.87	3.84	598.50	3.23	1.95	.65	27.81	.90	42.42	734.300

Fifteen Minute Log

Time hh:mm	CO						NOx (Stack)				
	O2 Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
10:15	14.56	7.49	6.97	.016	7.42	7.63	3.68	3.42	.013	5.96	5.92
NH3 Slip											
	NH3	ppmC	#/hr	ppmC	#/hr	NH3/NOx	SCR	NOx	Temp		
10:15	593.33	3.00	1.81	3.13	1.89	.895	42.52	733.59			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
10:15	310.82	5.84	3.80	.65	27.54						

RA Run # 3

RA Run# 3

Fifteen Minute Log

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
1:30	14.57	7.26	6.77	.015	7.20	7.56	3.93	3.67	.013	6.39	6.01
NH3 Slip											
NH3											
SCFH											
15 min 1 hr NH3/NOx SCR											
ppmC #/hr ppmC #/hr Ratio NOx Temp											

Alarm: Maint Request recorded Thu 04 Mar 1993 1021

Clear: Maint Request recorded Thu 04 Mar 1993 1026

***** Coalinga Cogeneration Company *****
Coalinga, Fresno County, CA 93210

10:30 583.62 2.95 1.77 3.05 1.84 .889 42.38 733.57

	Air #/sec	Gas #/sec	H2O #/sec	Inj. Ratio	H2O gal/hr
10:30	309.92	5.83	3.75	.64	27.14

Fifteen Minute Log

Time hh:mm	O2 Pct	CO				NOx (Stack)					
		15 min ppm	1 hr ppmC	15 min #/mmBTU	1 hr #/hrC	15 min ppm	1 hr ppmC	15 min #/mmBTU	1 hr #/hrC		
10:45	14.56	6.93	6.44	.014	6.86	7.23	3.76	3.50	.013	6.10	6.11
NH3 Slip											
	NH3 SCFH	15 min ppmC	1 hr #/hr	15 min ppmC	1 hr #/hr	NH3/NOx Ratio	SCR NOx	Temp			
10:45	587.95	2.85	1.72	2.97	1.79	.890	42.56	733.97			
	Air #/sec	Gas #/sec	H2O #/sec	Inj. Ratio	H2O gal/hr						
10:45	309.63	5.84	3.72	.64	26.92						

RA Run #4

Fifteen Minute Log

Time hh:mm	O2 Pct	CO				NOx (Stack)					
		15 min ppm	1 hr ppmC	15 min #/mmBTU	1 hr #/hrC	15 min ppm	1 hr ppmC	15 min #/mmBTU	1 hr #/hrC		
11:00	14.55	6.88	6.39	.014	6.80	7.07	3.74	3.47	.013	6.06	6.13
NH3 Slip											
	NH3 SCFH	15 min ppmC	1 hr #/hr	15 min ppmC	1 hr #/hr	NH3/NOx Ratio	SCR NOx	Temp			
11:00	583.75	2.76	1.65	2.89	1.74	.889	42.41	734.43			
	Air #/sec	Gas #/sec	H2O #/sec	Inj. Ratio	H2O gal/hr						
11:00	309.03	5.83	3.72	.64	26.90						

RA Run #4

One Hour Log

Time hh:mm	Gas mmBTU	O2 Pct	CO				NOx (Stack)				
			ppm	ppmC	#/mmBTU	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	
11:00	3457.00	14.56	7.13	6.63	.015	7.06	3.76	3.50	.013	6.11	
	Air #/sec	Gas #/sec	H2O #/sec	NH3 SCFH	NH3 Slip ppmC	1 hr #/hr	Inj. Ratio	H2O gal/hr	NH3/NOx Ratio	SCR NOx	Temp
11:00	309.90	5.84	3.75	587.20	2.89	1.74	.64	27.13	.89	42.47	733.900

Fifteen Minute Log

CO	NOx (Stack)
----	-------------

DAILY LOGS FOR THE 04 MAR 1990
 ***** Coalinga Cogeneration Company *****
 Coalinga, Fresno County, CA 93210

Time	O2	-----15 min-----					1 hr	-----15 min-----					1 hr
hh:mm	Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC
11:15	14.56	6.84	6.36	.014	6.74	6.90	6.90	3.79	3.53	.013	6.13	6.17	6.17
		NH3 Slip -----											
	NH3	-----15 min-----		-----1 hr-----		NH3/NOx		----- SCR -----					
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio		NOx	Temp				
11:15	585.10	2.85	1.71	2.85	1.71	.890		42.44	734.82				
	Air	Gas	H2O	Inj.	H2O								
	#/sec	#/sec	#/sec	Ratio	gal/hr								
11:15	309.30	5.82	3.70	.64	26.78								

F i f t e e n M i n u t e L o g

Time	O2	----- CO -----					1 hr	----- NOx (Stack) -----					1 hr
hh:mm	Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC
11:30	14.56	6.69	6.22	.014	6.58	6.75	6.75	3.95	3.67	.013	6.37	6.37	6.17
		NH3 Slip -----											
	NH3	-----15 min-----		-----1 hr-----		NH3/NOx		----- SCR -----					
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio		NOx	Temp				
11:30	581.91	2.84	1.70	2.82	1.70	.886		42.45	735.13				
	Air	Gas	H2O	Inj.	H2O								
	#/sec	#/sec	#/sec	Ratio	gal/hr								
11:30	308.76	5.81	3.67	.63	26.59								

RA Run # 5

F i f t e e n M i n u t e L o g

Time	O2	----- CO -----					1 hr	----- NOx (Stack) -----					1 hr
hh:mm	Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC
11:45	14.55	6.50	6.04	.013	6.40	6.63	6.63	4.02	3.73	.014	6.48	6.48	6.26
		NH3 Slip -----											
	NH3	-----15 min-----		-----1 hr-----		NH3/NOx		----- SCR -----					
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio		NOx	Temp				
11:45	583.69	2.86	1.71	2.83	1.69	.885		42.65	735.02				
	Air	Gas	H2O	Inj.	H2O								
	#/sec	#/sec	#/sec	Ratio	gal/hr								
11:45	308.59	5.81	3.65	.63	26.42								

RA Run # 5

F i f t e e n M i n u t e L o g

Time	O2	----- CO -----					1 hr	----- NOx (Stack) -----					1 hr
hh:mm	Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC
11:00	14.56	6.61	6.15	.014	6.52	6.56	6.56	4.10	3.81	.014	6.62	6.62	6.40
		NH3 Slip -----											
	NH3	-----15 min-----		-----1 hr-----		NH3/NOx		----- SCR -----					
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio		NOx	Temp				

DAILY LOG FOR THE COALINGA COGENERATION PLANT
 ***** Coalinga Cogeneration Company *****
 Coalinga, Fresno County, CA 93210

12:00 578.64 2.69 1.61 2.81 1.68 .880 42.54 734.97

	Air #/sec	Gas #/sec	H2O #/sec	Inj. Ratio	H2O gal/hr
12:00	308.65	5.81	3.67	.63	26.55

One Hour Log

Time hh:mm	Gas	O2	CO		NOx (Stack)	
	mmBTU	Pct	ppm	ppmC #/mmBTU	#/hrC	ppm ppmC #/mmBTU #/hrC
12:00	3461.00	14.56	6.66	6.19 .014	6.56	3.96 3.69 .014 6.40

12:00	Air	Gas	H2O	NH3	-- NH3 Slip --	Inj.	H2O	NH3/NOx	---- SCR ----
	#/sec	#/sec	#/sec	SCFH	ppmC #/hr	Ratio	gal/hr	Ratio	NOx Temp
12:00	308.80	5.81	3.67	582.30	2.81 1.68	.63	26.59	.88	42.52 735.000

Fifteen Minute Log

Time hh:mm	O2 Pct	CO				NOx (Stack)			
		ppm	ppmC #/mmBTU	#/hrC	ppm	ppmC #/mmBTU	#/hrC	#/hrC	
12:15	14.55	6.61	6.14 .014	6.49	6.50	3.82	3.55 .013	6.16 6.41	

12:15	NH3	NH3 Slip		NH3/NOx	SCR
	SCFH	ppmC #/hr	ppmC #/hr		
12:15	584.19	2.70 1.61	2.77 1.66	.886	42.71 735.03

12:15	Air	Gas	H2O	Inj.	H2O
	#/sec	#/sec	#/sec	Ratio	gal/hr
12:15	308.17	5.80	3.71	.64	26.87

RA RUN #6

Fifteen Minute Log

Time hh:mm	O2 Pct	CO				NOx (Stack)			
		ppm	ppmC #/mmBTU	#/hrC	ppm	ppmC #/mmBTU	#/hrC	#/hrC	
12:30	14.54	6.91	6.41 .014	6.79	6.55	3.89	3.61 .013	6.27 6.38	

12:30	NH3	NH3 Slip		NH3/NOx	SCR
	SCFH	ppmC #/hr	ppmC #/hr		
12:30	571.83	2.64 1.57	2.72 1.63	.883	42.04 735.28

12:30	Air	Gas	H2O	Inj.	H2O
	#/sec	#/sec	#/sec	Ratio	gal/hr
12:30	307.45	5.80	3.73	.64	26.99

RA RUN #6

Fifteen Minute Log

CO NOx (Stack)

***** Coalinga Cogeneration Company *****
Coalinga, Fresno County, CA 93210

Time	02	-----15 min-----					1 hr	-----15 min-----					1 hr
hh:mm	Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC
12:45	14.56	6.37	5.93	.013	6.26	6.52	6.52	3.95	3.68	.013	6.37	6.35	6.35
		NH3 Slip											
	NH3	-----15 min-----		-----1 hr-----		NH3/NOx		----- SCR -----					
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio		NOx	Temp				
12:45	577.83	2.86	1.70	2.72	1.63	.886		42.36	735.71				
	Air	Gas	H2O	Inj.	H2O								
	#/sec	#/sec	#/sec	Ratio	gal/hr								
12:45	307.17	5.80	3.68	.63	26.61								

Fifteen Minute Log

Time	02	----- CO -----					1 hr	----- NOx (Stack) -----					1 hr
hh:mm	Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC
13:00	14.58	5.98	5.58	.013	5.88	6.36	6.36	4.29	4.01	.015	6.92	6.43	6.43
		NH3 Slip											
	NH3	-----15 min-----		-----1 hr-----		NH3/NOx		----- SCR -----					
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio		NOx	Temp				
13:00	574.83	2.68	1.59	2.72	1.62	.875		42.80	735.85				
	Air	Gas	H2O	Inj.	H2O								
	#/sec	#/sec	#/sec	Ratio	gal/hr								
13:00	306.32	5.78	3.60	.62	26.07								

RA RUN #7

One Hour Log

Time	Gas	02	----- CO -----				----- NOx (Stack) -----			
hh:mm	mmBTU	Pct	ppm	ppmC	#/mmBTU	#/hrC	ppm	ppmC	#/mmBTU	#/hrC
13:00	3457.00	14.56	6.47	6.01	.013	6.36	3.99	3.71	.014	6.43
	Air	Gas	H2O	NH3	-- NH3 Slip --	Inj.	H2O	NH3/NOx	----- SCR -----	
	#/sec	#/sec	#/sec	SCFH	ppmC	#/hr	Ratio	gal/hr	Ratio	NOx
13:00	307.30	5.79	3.68	577.20	2.72	1.62	.63	26.63	.88	42.48

Fifteen Minute Log

Time	02	----- CO -----					1 hr	----- NOx (Stack) -----					1 hr
hh:mm	Pct	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	#/hrC
13:15	14.58	6.14	5.73	.013	6.01	6.23	6.23	4.18	3.91	.014	6.70	6.56	6.56
		NH3 Slip											
	NH3	-----15 min-----		-----1 hr-----		NH3/NOx		----- SCR -----					
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio		NOx	Temp				
13:15	574.41	2.86	1.69	2.76	1.64	.881		42.61	735.97				
	Air	Gas	H2O	Inj.	H2O								
	#/sec	#/sec	#/sec	Ratio	gal/hr								
13:15	305.32	5.75	3.61	.63	26.14								

RA RUN #7

***** Coalinga Cogeneration Company *****
Coalinga, Fresno County, CA 93210

F i f t e e n M i n u t e L o g

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		-----15 min-----			1 hr		-----15 min-----			1 hr	
12:30	14.57	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
		6.38	5.95	.013	6.23	6.09	4.00	3.73	.014	6.40	6.60
		----- NH3 Slip -----									
	NH3	----15 min----		-----1 hr-----		NH3/NOx	---- SCR ----				
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
13:30	570.57	2.87	1.70	2.82	1.67	.885	42.17	735.98			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
13:30	304.90	5.74	3.68	.64	26.65						

F i f t e e n M i n u t e L o g

Time hh:mm	O2 Pct	CO					NOx (Stack)							
		15 min ppm	15 min ppmC	15 min #/mmBTU	1 hr #/hrC	1 hr #/hrC	15 min ppm	15 min ppmC	15 min #/mmBTU	1 hr #/hrC	1 hr #/hrC			
13:45	14.58	5.99	5.59	.013	5.80	5.98	4.12	3.84	.014	6.55	6.64			
		NH3 Slip												
	NH3	15 min	1 hr	NH3/NOx		SCR								
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp						
13:45	579.21	2.70	1.60	2.78	1.65	.879	43.17	736.00	RA Run #8					
	Air	Gas	H2O	Inj.	H2O									
	#/sec	#/sec	#/sec	Ratio	gal/hr									
13:45	304.47	5.70	3.64	.64	26.33									

RA Run #8

F i f t e e n M i n u t e L o g

Time hh:mm	O2 Pct	CO					NOx (Stack)							
		15 min ppm	15 min ppmC	15 min #/mmBTU	1 hr #/hrC	1 hr #/hrC	15 min ppm	15 min ppmC	15 min #/mmBTU	1 hr #/hrC	1 hr #/hrC			
14:00	14.59	6.75	6.31	.014	6.57	6.15	3.98	3.72	.014	6.35	6.50			
		NH3 Slip												
	NH3	15 min	1 hr	NH3/NOx		SCR								
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp						
14:00	565.97	2.68	1.59	2.78	1.64	.881	42.05	736.11	RA Run # 8					
	Air	Gas	H2O	Inj.	H2O									
	#/sec	#/sec	#/sec	Ratio	gal/hr									
14:00	304.69	5.71	3.72	.65	26.95									

RA Run #8

O n e H o u r L o g

Time	Gas	O2	CO	NOx (Stack)
------	-----	----	----	-------------

Daily Logs for Unit 04 Mar 1995
 ***** Coalinga Cogeneration Company *****
 Coalinga, Fresno County, CA 93210

hh:mm	mmBTU	Pct	ppm	ppmC	#/mmBTU	#/hrC	ppm	ppmC	#/mmBTU	#/hrC
14:00	3459.00	14.58	6.31	5.89	.013	6.15	4.07	3.80	.014	6.50

	Air	Gas	H2O	NH3	-- NH3 Slip --	Inj.	H2O	NH3/NOx	---- SCR ----
	#/sec	#/sec	#/sec	SCFH	ppmC	#/hr	Ratio	gal/hr	Ratio
									NOx
									Temp
14:00	304.80	5.72	3.66	572.50	2.78	1.64	.64	26.52	.88
									42.50
									736.000

Fifteen Minute Log

Time	O2	CO	NOx (Stack)
hh:mm	Pct	ppm	ppmC
14:15	14.58	6.35	5.93

Time	NH3	NH3 Slip	NH3/NOx	SCR
hh:mm	SCFH	ppmC	#/hr	Ratio
14:15	569.61	2.78	1.64	2.76

Time	Air	Gas	H2O	Inj.	H2O
hh:mm	#/sec	#/sec	#/sec	Ratio	gal/hr
14:15	304.61	5.71	3.67	.64	26.58

Fifteen Minute Log

Time	O2	CO	NOx (Stack)
hh:mm	Pct	ppm	ppmC
14:30	14.57	6.31	5.89

Time	NH3	NH3 Slip	NH3/NOx	SCR
hh:mm	SCFH	ppmC	#/hr	Ratio
14:30	569.45	2.70	1.60	2.72

Time	Air	Gas	H2O	Inj.	H2O
hh:mm	#/sec	#/sec	#/sec	Ratio	gal/hr
14:30	304.66	5.70	3.64	.64	26.35

RA Run #9

Fifteen Minute Log

Time	O2	CO	NOx (Stack)
hh:mm	Pct	ppm	ppmC
14:45	14.57	6.19	5.77

Time	NH3	NH3 Slip	NH3/NOx	SCR
hh:mm	SCFH	ppmC	#/hr	Ratio
14:45	570.77	2.69	1.59	2.71

Time	Air	Gas	H2O	Inj.	H2O
hh:mm	#/sec	#/sec	#/sec	Ratio	gal/hr
14:45	304.95	5.69	3.65	.64	26.40

RA Run #9

***** Coalinga Cogeneration Company *****
Coalinga, Fresno County, CA 93210

Fifteen Minute Log

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		-----15 min-----		1 hr		-----15 min-----		1 hr			
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
15:00	14.58	6.00	5.60	.013	5.80	6.02	4.14	3.87	.014	6.56	6.60
		----- NH3 Slip -----									
	NH3	----15 min----		-----1 hr-----		NH3/NOx	---- SCR ----				
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
15:00	574.55	2.70	1.60	2.72	1.61	.879	42.79	736.16			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
15:00	304.99	5.68	3.64	.64	26.37						

One Hour Log

Time hh:mm	Gas mmBTU	O2 Pct	CO				NOx (Stack)			
			ppm	ppmC	#/mmBTU	#/hrC	ppm	ppmC	#/mmBTU	#/hrC
15:00	3464.00	14.58	6.21	5.80	.013	6.02	4.16	3.88	.014	6.60
	Air	Gas	H2O	NH3	NH3 Slip	Inj.	H2O	NH3/NOx	SCR	
	#/sec	#/sec	#/sec	SCFH	ppmC	#/hr	Ratio	gal/hr	Ratio	NOx Temp
15:00	304.80	5.70	3.65	571.10	2.72	1.61	.64	26.42	.88	42.56 736.100

Fifteen Minute Log

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
15:15	14.56	6.65	6.19	.014	6.46	6.09	4.00	3.72	.014	6.37	6.55
		NH3 Slip									
	NH3	15 min		1 hr		NH3/NOx	SCR				
	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
15:15	566.93	2.54	1.50	2.66	1.57	.878	42.21	736.23	RA Run #10		
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
15:15	305.26	5.72	3.71	.65	26.85						

RA Run #10

Fifteen Minute Log

Time hh:mm	O2 Pct	CO					NOx (Stack)				
		ppm	ppmC	#/mmBTU	#/hrC	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC
15:30	14.58	6.52	6.08	.014	6.36	6.15	4.04	3.77	.014	6.46	6.51
		NH3 Slip									
	NH3	15 min		1 hr		NH3/NOx	SCR				

RA Run #10

***** Coalinga Cogeneration Company *****
Coalinga, Fresno County, CA 93210

	SCFH	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp
15:30	568.81	2.58	1.53	2.63	1.56	.878	42.31	736.07

	Air #/sec	Gas #/sec	H2O #/sec	Inj. Ratio	H2O gal/hr
15:30	305.55	5.74	3.70	.65	26.82

Fifteen Minute Log

Time hh:mm	O2 Pct	CO				NOx (Stack)					
		ppm	ppmC	#/mmBTU	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	
15:45	14.57	6.30	5.87	.013	6.14	6.19	4.19	3.91	.014	6.70	6.52
NH3 Slip											
	NH3	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
15:45	573.73	2.75	1.63	2.64	1.57	.879	42.62	735.99			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
15:45	305.75	5.73	3.68	.64	26.62						

Fifteen Minute Log

Time hh:mm	O2 Pct	CO				NOx (Stack)					
		ppm	ppmC	#/mmBTU	#/hrC	ppm	ppmC	#/mmBTU	#/hrC	#/hrC	
16:00	14.57	6.56	6.11	.014	6.33	6.32	4.10	3.82	.014	6.49	6.50
NH3 Slip											
	NH3	ppmC	#/hr	ppmC	#/hr	Ratio	NOx	Temp			
16:00	567.38	2.79	1.64	2.66	1.58	.882	42.31	736.11			
	Air	Gas	H2O	Inj.	H2O						
	#/sec	#/sec	#/sec	Ratio	gal/hr						
16:00	303.53	5.69	3.66	.64	26.47						

One Hour Log

Time hh:mm	Gas mmBTU	O2 Pct	CO			NOx (Stack)				
			ppm	ppmC	#/mmBTU	#/hrC	ppm	ppmC	#/mmBTU	#/hrC
16:00	3448.00	14.57	6.51	6.06	.014	6.32	4.08	3.81	.014	6.50
	Air	Gas	H2O	NH3	NH3 Slip	Inj.	H2O	NH3/NOx	SCR	
	#/sec	#/sec	#/sec	SCFH	ppmC	#/hr	Ratio	gal/hr	Ratio	NOx Temp
16:00	305.00	5.72	3.69	569.20	2.66	1.58	.64	26.69	.88	42.36 736.100

m: Maint Request recorded Thu 04 Mar 1993 1603

MAINSCREEN: 1251 VER: 100

SUBSCREEN: DATE: 03/04/93

11 VER: 102 TIME: 09:07:41

WINDOW:

0 VER: 0

04/MAR/93

10 MINUTE TREND

09:07:40

X1:FQT

TOTAL FUEL FLOW (GAS)

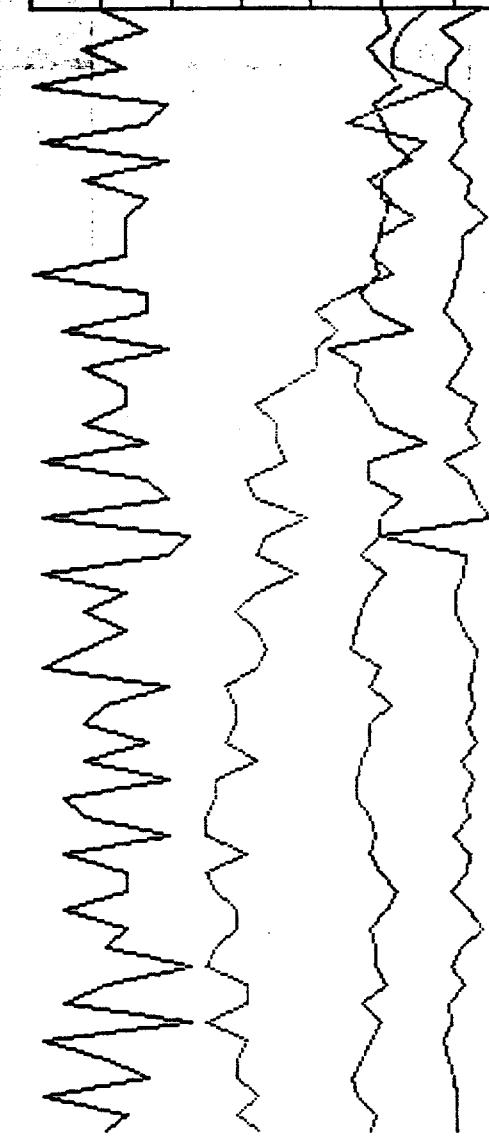
X2:DW

GENERATOR LOAD

Y1:FY205KLB CALC STEAM FLOW TO WHITTIER

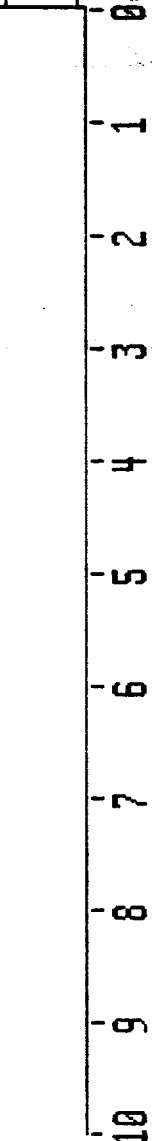
Y2:FY206KLB CALC STEAM FLOW TO SANTA FE

6.50
82.00



X1= 5.87 LB/SEC
Y1= 82 KLBS/H
X2= 40.16 MW
Y2= 133 KLBS/H

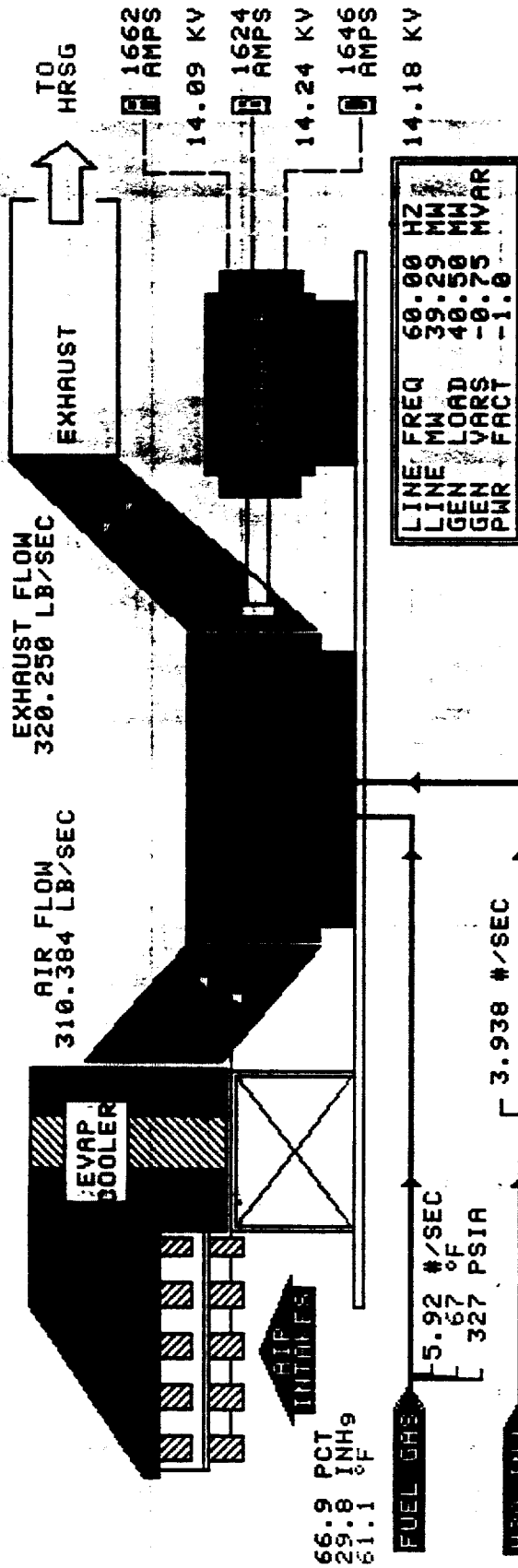
5.50
70.00



COPY IN PROGRESS

MAINSCREEN: 2001 VER: 0 SUBSCREEN: 299 VER: 100 WINDOW: 0 VER: 0
 DATE: 03/04/93 TIME: 09:08:52

TURBINE/GENERATOR



T/G TEMPERATURES	
INLET FLG.	55 °F
DISCH TEMP	656 °F
LUBE SYST	131 °F
EXHAUST	1003 °F

TOTAL FIRED HRS	11173.8
FIRED STARTS	37
PEAK FIRED HRS	0

VIBRATION	0.33 IN/S
(MAX SELECT)	84 DEG
IGV ANGLE	

MAINSCREEN: 1251 VER: 100

SUBSCREEN: DATE: 03/04/93

11 VER: 102 TIME: 10:08:28

0 VER: 0

04/MAR/93

10 MINUTE TREND

10:08:28

X1:FQT

TOTAL FUEL FLOW (GAS)

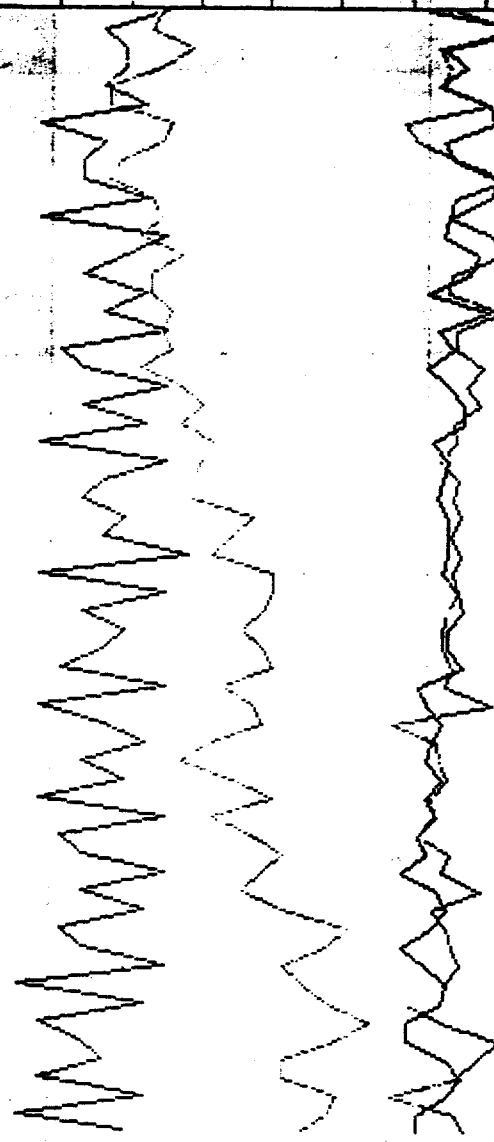
X2:DW

GENERATOR LOAD

Y1:FY205KLB CALC STEAM FLOW TO WHITTIER

Y2:FY206KLB CALC STEAM FLOW TO SANTA FE

5.50 11.50
80.00 147.00



X1= 5.83 LB/SEC
Y1= 79 KLBBS/H
X2= 39.81 MW
Y2= 139 KLBBS/H

5.50 11.50
80.00 147.00

10 9 8 7 6 5 4 3 2 1 0

COPY IN PROGRESS

MAINSCREEN: 1251 VER: 100

SUBSCREEN: DATE: 03/04/93

11 VER: 102 TIME: 11:24:07

WINDOW:

0 VER: 0

04/MAR/93

X1:FOT

TOTAL FUEL FLOW (GAS)

Y1:FY205KLB CALC STEAM FLOW TO WHITTIER

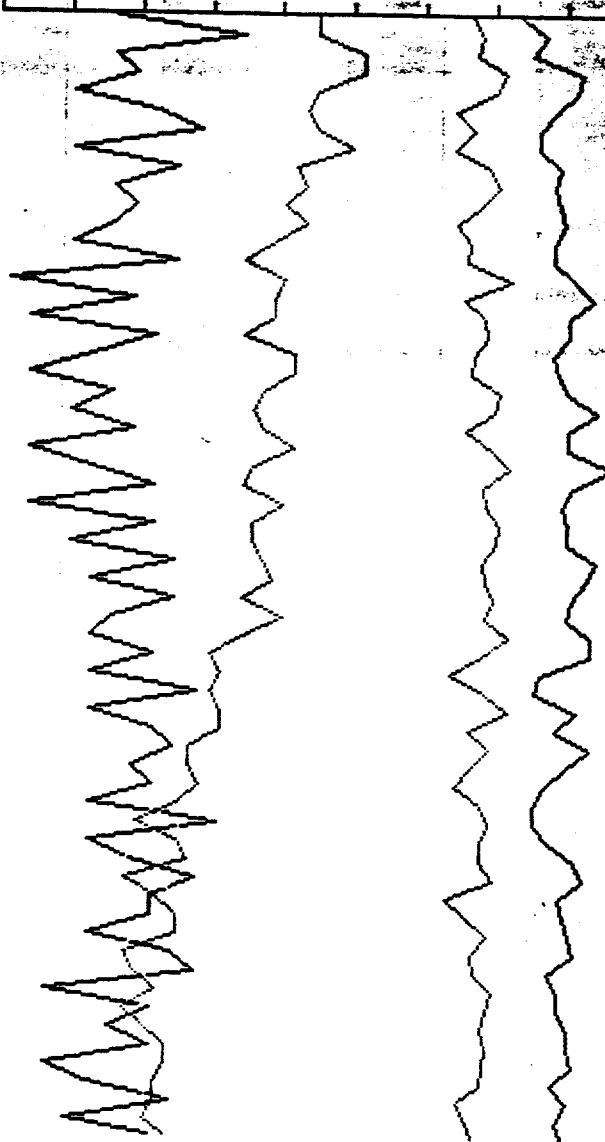
10 MINUTE TREND

X2:DW

Y2:FY206KLB CALC STEAM FLOW TO SANTA FE

11:24:07

6.50
52.00



X1= 5.85 LB/SEC
Y1= 81 KLBS/H
X2= 39.38 MW
Y2= 134 KLBS/H

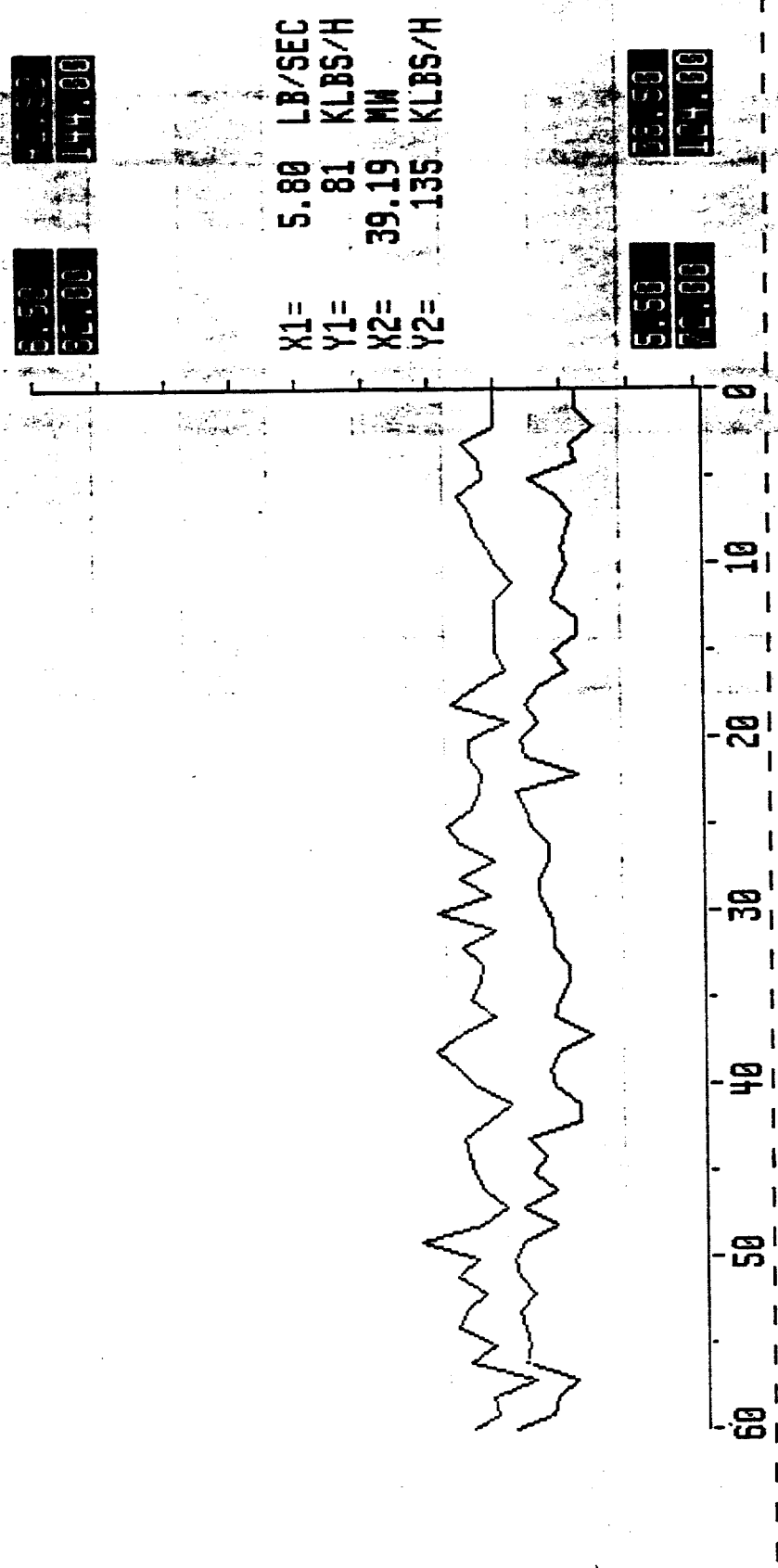
5.50
22.00

10 9 8 7 6 5 4 3 2 1 0

COPY IN PROGRESS

MAINSCREEN: 1252 VER: 100 SUBSCREEN: 11 VER: 102 WINDOW: 0 VER: 0
DATE: 03/04/93 TIME: 11:29:06

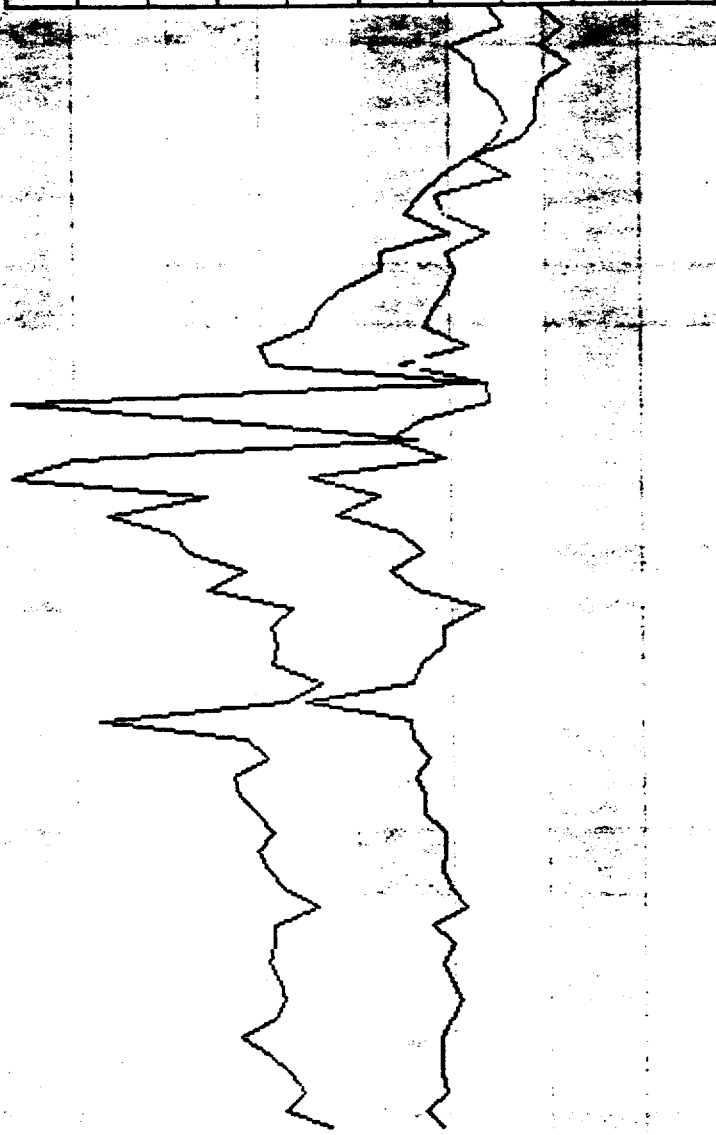
04/MAR/93 60 MINUTE TREND 11:29:06
X1:FQT TOTAL FUEL FLOW (GAS) X2:DW GENERATOR LOAD
Y1:FY205KLB CALC STEAM FLOW TO WHITTIER Y2:FY206KLB CALC STEAM FLOW TO SANTA FE



MAINSCREEN: 1257 VER: 100 SUBSCREEN: 11 VER: 102 WINDOW: 0 VER: 0
DATE: 03/04/93 TIME: 11:29:22

04/MAR/93 10 HOUR TREND 11:29:21
X1:FOT TOTAL FUEL FLOW (GAS) GENERATOR LOAD
Y1:FY205KLB CALC STEAM FLOW TO WHITTIER Y2:FY206KLB CALC STEAM FLOW TO SANTA FE

5.50 5.78 LB/SEC
52.00 79 KLBS/H
39.03 MW
136 KLBS/H



5.50 5.78
52.00 79
39.03 MW
136 KLBS/H

HOURS 10 9.0 8.0 7.0 6.0 5.0 4.0 3.0 2.0 1.0 0

MAINSCEEN: 1252 VER: 100

SUBSCREEN: 11 DATE: 03/04/93

VER: 102 WINDOW: 0

VER: 0

04/MAR/93

X1:FQT

TOTAL FUEL FLOW (GAS)

Y1:FY205KLB CALC STEAM FLOW TO WHITTIER

60 MINUTE TREND

X2:DW

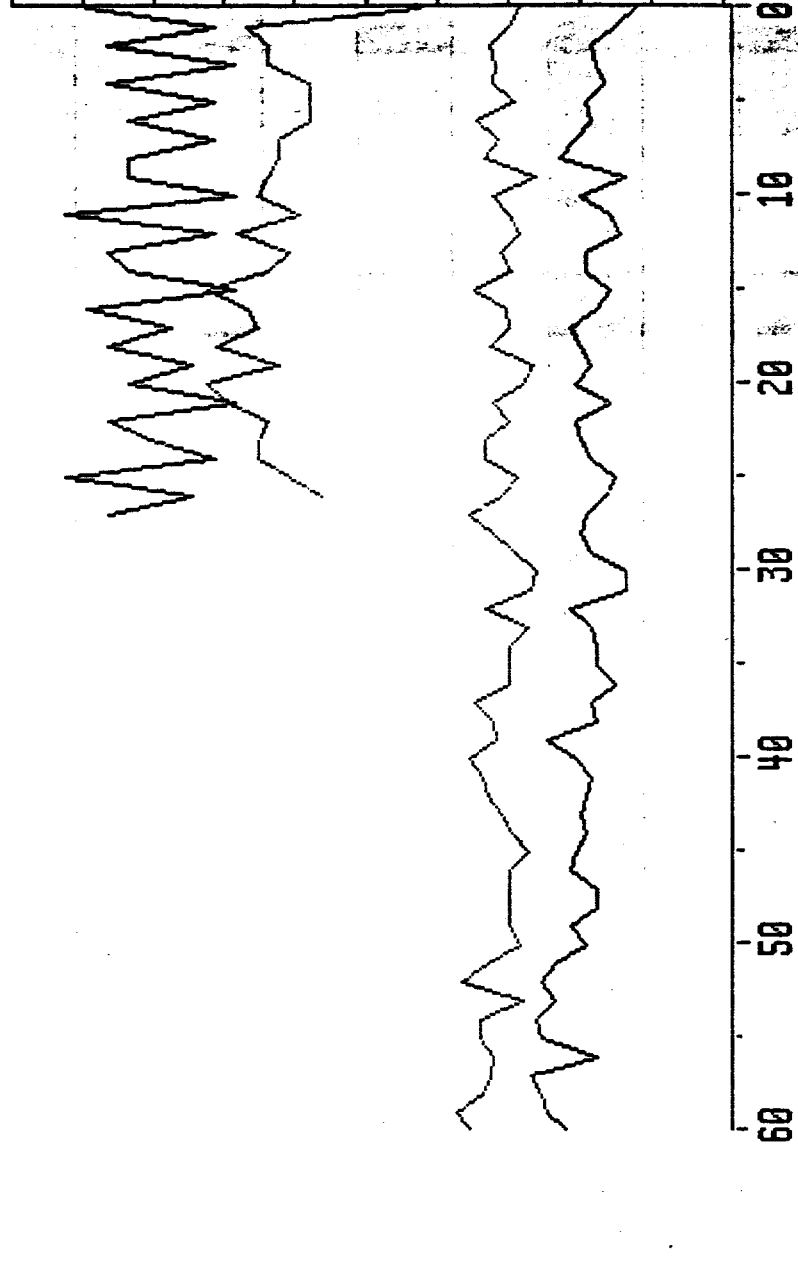
GENERATOR LOAD

Y2:FY206KLB CALC STEAM FLOW TO SANTA FE

12:05:23

5.50 12.50
32.00 144.00

X1= 5.81 LB/SEC
Y1= 79 KLBS/H
X2= 39.19 MW
Y2= 133 KLBS/H



5.50 39.50
72.00 124.00

MAINSCEEN: 1252 VER: 100

SUBSCREEN: DATE: 03/04/93

11 VER: 102

WINDOW:

0 VER: 0

TIME: 13:37:06

04/MAR/93

60 MINUTE TREND

13:37:05

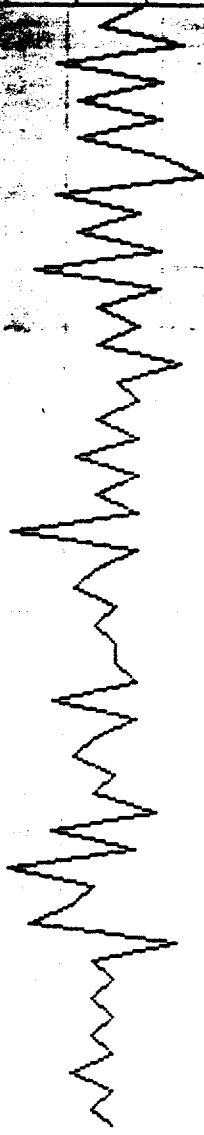
X1:FOT TOTAL FUEL FLOW (GAS)

X2:DN GENERATOR LOAD

Y1:FY205KLB CALC STEAM FLOW TO WHITTIER

Y2:FY200KLB CALC STEAM FLOW TO SANTA FE

5.50
82.00



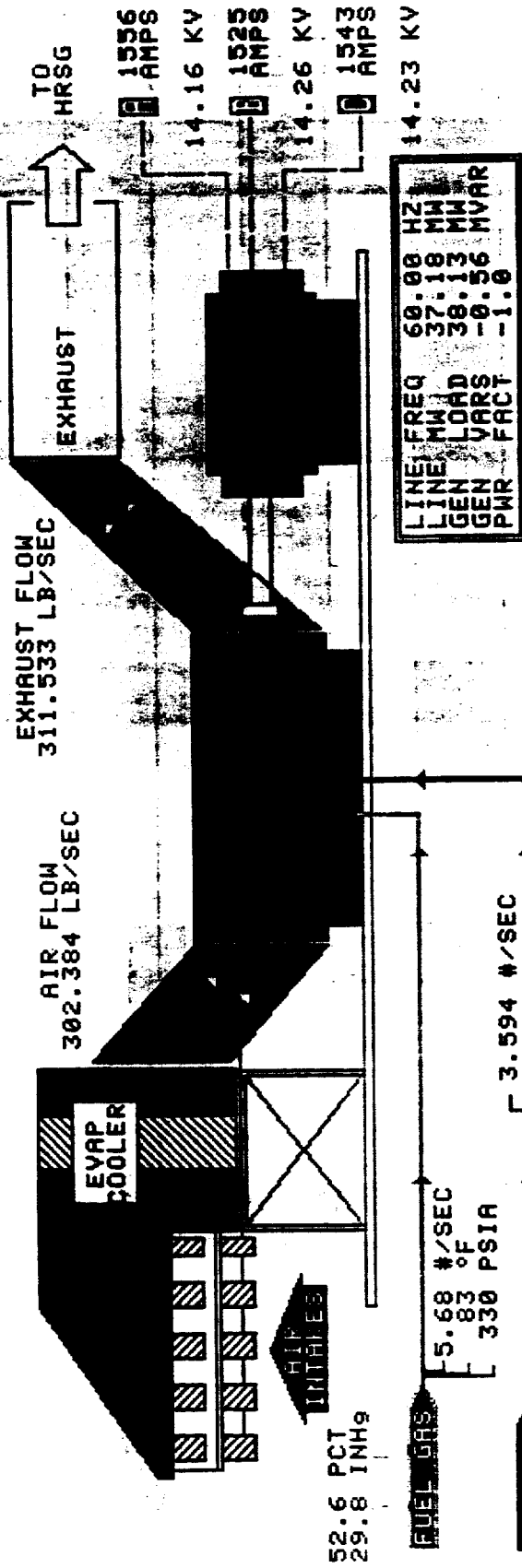
X1= 5.68 LB/SEC
Y1= 80 KLBS/H
X2= 38.00 MM
Y2= 130 KLBS/H

5.50
82.00



MAINSCREEN: 2001 VER: 0 SUBSCREEN: 299 VER: 100 WINDOW: 0 VER: 0
 DATE: 03/04/93 TIME: 13:37:38

TURBINE/GENERATOR



T/G TEMPERATURES	
INLET FLG.	69 °F
DISCH TEMP	673 °F
LUBE SYST	137 °F
EXHAUST	1012 °F

TOTAL FIRED HRS	11178.3
FIRED STARTS	37
PEAK FIRED HRS	0

COPY IN PROGRESS

MAINSCEEN: 1252 VER: 100

SUBSCREEN: DATE: 03/04/93

11 VER: 102 TIME: 14:30:20

WINDOW:

0 VER: 0

04/MAR/93

X1:FQT

TOTAL FUEL FLOW (GAS)

Y1:FY205KLB CALC STEAM FLOW TO WHITTIER

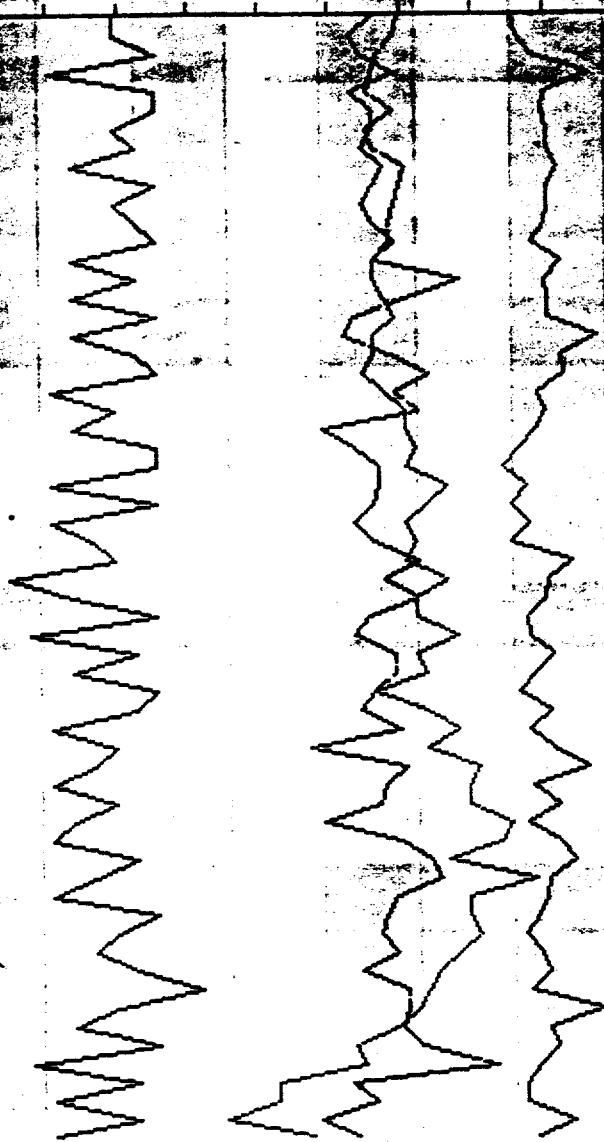
60 MINUTE TREND

X2:DN

GENERATOR LOAD

Y2:FY206KLB CALC STEAM FLOW TO SANTA FE

14:30:20



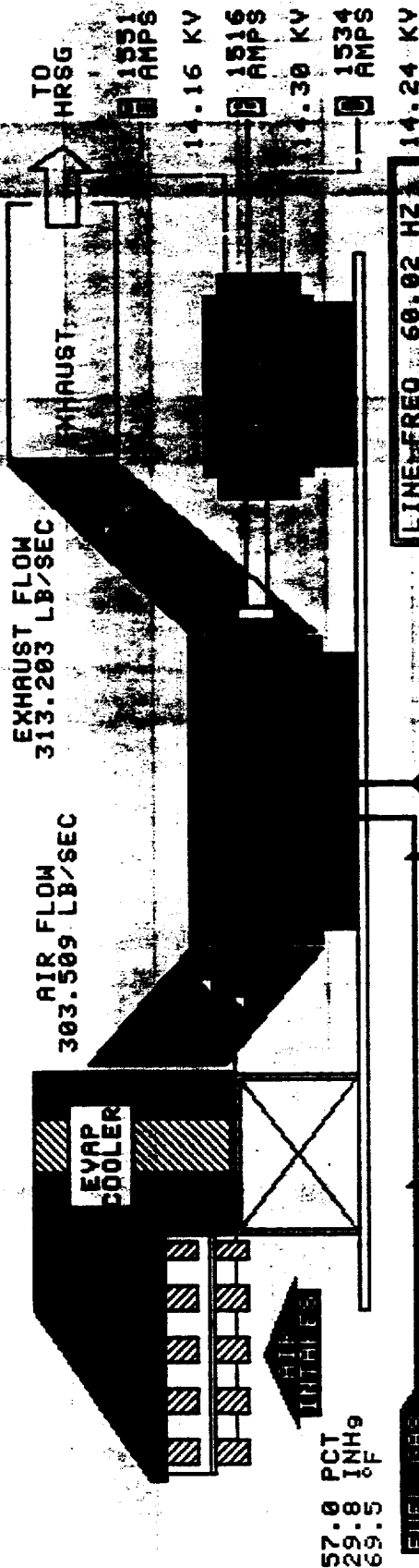
X1= 5.75 LB/SEC
Y1= 80 KLBS/H
X2= 38.16 MW
Y2= 134 KLBS/H

5.50 5.50
52.00 52.00
35.50 35.50
72.00 72.00

60 50 40 30 20 10

MAINSCREEN: 2001 VER: 0 SUBSCREEN: 299 VER: 100 WINDOW: 0 VER: 0
 DATE: 03/04/93 TIME: 14:30:48

TURBINE/GENERATOR



LINE FREQ 60.02 HZ
 LINE MW 37.19 MW
 GEN LOAD 38.19 MW
 GEN VAR 0.21 MVAR
 PWR FACT 1.00

T/G TEMPERATURES	
INLET FLG.	67 °F
DISCH TEMP	672 °F
LUBE SYST	131 °F
EXHAUST	1011 °F

TOTAL FIRED HRS 11179.2
 FIRED STARTS 37
 PEAK FIRED HRS 0

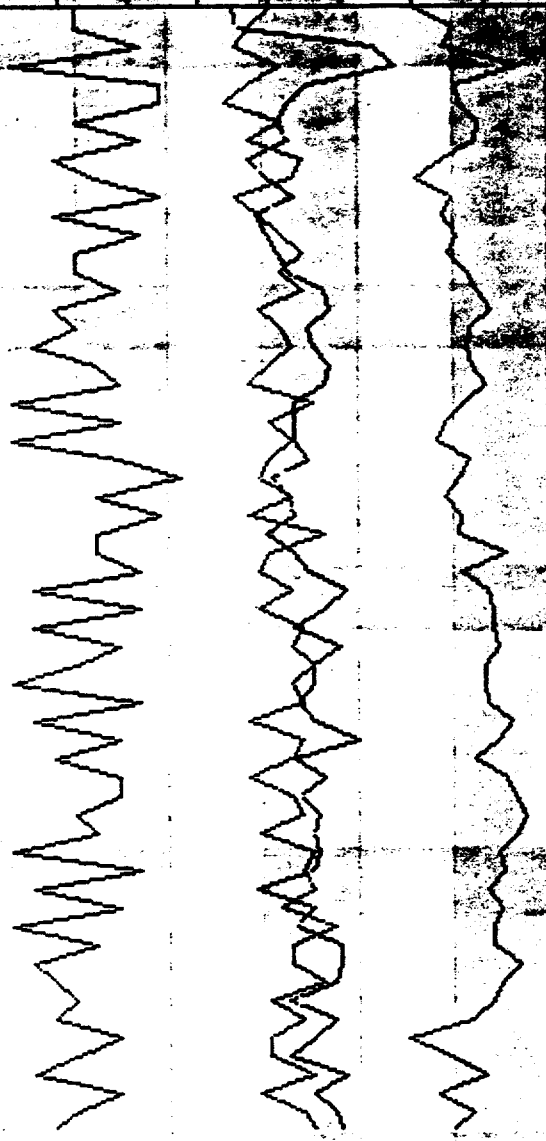
VIBRATION 0.30 IN/S
 <MAX SELECT
 IGV ANGLE 84 DEG

MAINSCREEN: 1252 VER: 100 SUBSCREEN: 11 VER: 102 WINDOW: 0 VER: 0
DATE: 03/04/93 TIME: 15:30:36

04/MAR/93 60 MINUTE TREND 15:30:36
X1:FOT TOTAL FUEL FLOW (GAS) X2:DN
Y1:FY205KLB CALC STEAM FLOW TO WHITTIER Y2:FY206KLB CALC STEAM FLOW TO SANTA FE

5.63 79 37.81 134
5.63 79 37.81 134

X1= 5.63 LB/SEC
Y1= 79 KLS/H
X2= 37.81 MM
Y2= 134 KLS/H

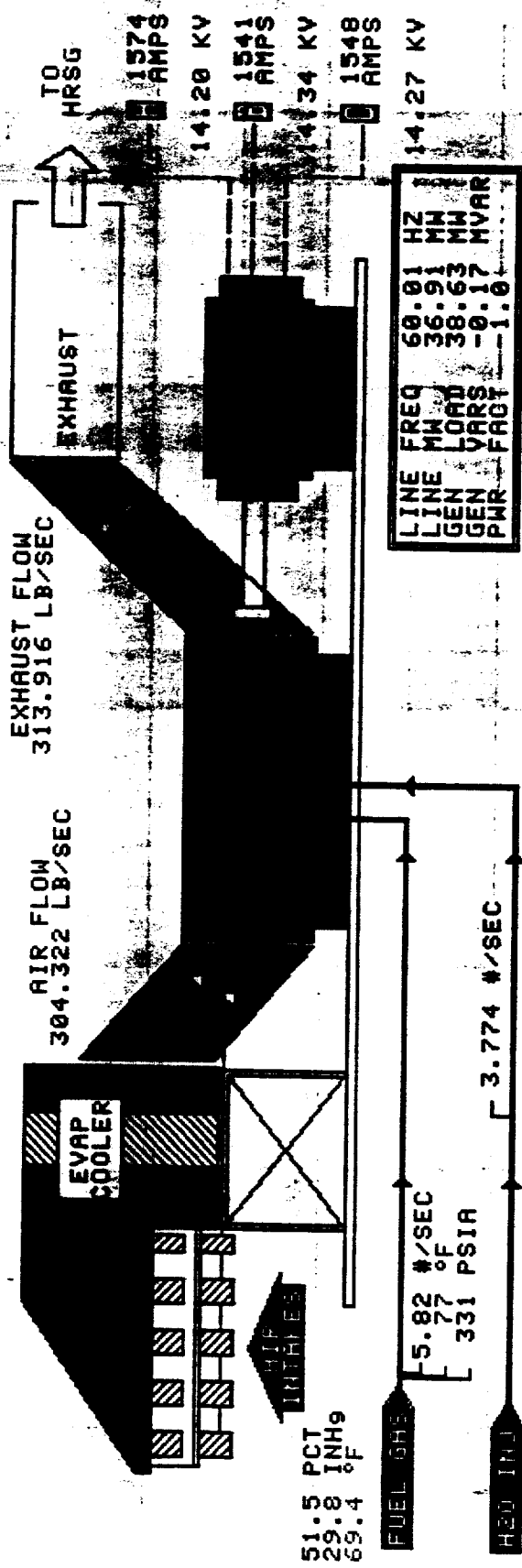


5.63 79 37.81 134
5.63 79 37.81 134

60 50 40 30 20 10

MAINSCREEN: 2001 VER: 0 SUBSCREEN: 299 VER: 100 WINDOW: 0 VER: 0
 DATE: 03/04/93 TIME: 15:31:32

TURBINE/GENERATOR



T/G TEMPERATURES	
INLET FLG.	66 °F
DISCH TEMP	671 °F
LUBE SYST	127 °F
EXHAUST	1013 °F

TOTAL FIRED HRS	11180.2
FIRED STARTS	37
PEAK FIRED HRS	0

VIBRATION	0.29 IN/S
<MAX SELECT	
IGV ANGLE	84 DEG

FROM P-102A/B