
**Montana Refining Company, Inc.
Great Falls, Montana**

**Diesel Hydrotreater Heater (HTU) H1701 &
Hydrogen Plant Reformer Heater H1810 Stacks**

NO_x/CO Compliance Emission Test Report

10/08/08

By:

Ed Wadington

**Energy & Environmental Measurement Corporation (EEMC)
1744 Mullooney Lane, Billings, Montana 59101
Phone: (406) 252-4450 Fax: (406) 252-6350**

**3730 N. Pellegrino Drive, Tucson, Arizona 85749
Phone: (520) 749-2167 Fax: (520) 749-3582**

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FIELD OBSERVATION CHECKLIST

Test Date: 10/08/08

Plant Name: Montana Refining Company, Inc.

Plant Address: 1900 10th Street N.E.
Great Falls, Montana 59404

Sources Tested: HTU (Diesel Hydrotreater Heater) H1701 &
Hydrogen Plant Reformer Heater H1810 Stacks

Plant Contact: Ray Martinich / Environmental Engineer

Phone: (406) 761-4100 refinery; (406) 454-9862 direct line
Fax: (406) 761-0174

Observers & Affiliation: Ray Martinich - Montana Refining Company
No State Observers

EEMC Field Team:
Team Leader: Dave Wang
Other Members: Jason Wiggs
John Adams

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INTRODUCTION

Montana Refining Company, Inc., Great Falls, Montana contracted with Energy & Environmental Measurement Corporation (EEMC) to conduct a series of NO_x/CO compliance emission tests on their Hydrogen Plant Reformer Heater (H1810) and Diesel Hydrotreater Heater (H1701) Stacks located at Great Falls, Montana. This report contains all field data, calculations and results.

Test Chronolog 10/08/08

Time	Run #	Source	Test Description
07:45-08:44	1-NO _x /CO	Hydrogen Plant	EPA Methods #7E, #10 & #19
08:52-09:51	2-NO _x /CO	Hydrogen Plant	EPA Methods #7E, #10 & #19
09:59-10:58	3-NO _x /CO	Hydrogen Plant	EPA Methods #7E, #10 & #19
07:45-08:45	1-GF/H ₂ O	Hydrogen Plant	EPA Methods #1-4
08:52-09:52	2-GF/H ₂ O	Hydrogen Plant	EPA Methods #1-4
09:59-10:59	3-GF/H ₂ O	Hydrogen Plant	EPA Methods #1-4
11:35-12:34	4-NO _x /CO	Hydrotreater (HTU)	EPA Methods #7E, #10 & #19
12:42-13:41	5-NO _x /CO	Hydrotreater (HTU)	EPA Methods #7E, #10 & #19
13:49-14:48	6-NO _x /CO	Hydrotreater (HTU)	EPA Methods #7E, #10 & #19
11:35-12:35	4-GF/H ₂ O	Hydrotreater (HTU)	EPA Methods #1-4
12:42-13:42	5-GF/H ₂ O	Hydrotreater (HTU)	EPA Methods #1-4
13:49-14:49	6-GF/H ₂ O	Hydrotreater (HTU)	EPA Methods #1-4

TEST METHODS/PROCEDURES

Gas Flow / Moisture Sampling

EPA Methods #1-4^[1] were utilized for determination of stack gas velocity, density and moisture. Note section tabulated - Stack Parameters for a description of the sampling locations, etc.

The sample train consisted of a SS pitobe assembly (S-type pitot tube and a Type K thermocouple) leading to a set of four Greenburg-Smith impingers where flue gas moisture was condensed (1&2-150 ml H₂O₂, 3-empty, and 4-silica gel). The dried gases were then pulled, via an umbilical cord, to a RAC type meter box for gas volume metering. A meter box orifice slip stream was utilized for collection of an integrated bag sample and analyzed via orsat and a Servomex oxygen analyzer. A total of three one-hour tests were conducted concurrent with the NO_x/CO testing.

TEST METHODS/PROCEDURES - continued

Upon completion of the test run, CO₂ / O₂ concentrations were determined by triplicate orsat analysis (integrated bag), and moisture determination was via gravimetric analysis of the impinger liquid gain.

NO_x Emissions

EPA Method #7E^[1] was utilized for determination of stack gas NO_x concentration. The stack gases were extracted from the stream, and conveyed to an CAI (Model 400) Chemiluminescent analyzer. EPA Protocol 1 calibration gases were utilized for instrument span checks. Zero was checked with zero N₂ gas. Results were recorded via an integrating logger on a one-minute basis.

CO Emissions

EPA Method #10^[1] was utilized for determination of gas stream carbon monoxide concentration. A CAI (Model 100) NDIR analyzer was utilized. Span gases were EPA Protocol 1 CO in N₂. Calibration results are included with each test run as per the method.

Fuel Analysis

In order to develop an Fd factor a fuel analysis was conducted by Montana Refining. The results and subsequent calculations (Fd) are included the this report (lbs/MMBtu).

Units of Reporting

The data is reported with the following units:

- 1) NO_x/CO
ppm v/v Dry - parts per million on a volume basis with and without water
PPH - pounds per hour
TPY - tons per year
lb/MMBtu - pounds per million British Thermal Units
- 2) Gas Flow
Flow - FPS - feet per second
Volume - AWCfm - actual wet cubic feet per minute
SDCFH - dry standard* cubic feet per hour,
(* @ 68 °F and 29.92 Hg)
- 3) CO₂/O₂ - % v/v - percent on a volume basis

RESULTS

The Data Summaries Section contains pertinent results. Field data & calculations are included as tabulated.

REFERENCES

- ^[1] Federal Register, Pt. 60, App. A. Methods #1-4, #7E, #10 & #19, 7/1/07.

COMPLIANCE STATEMENT

Montana Refining Company, Inc.
Diesel Hydrotreater Heater (HTU) H1701 &
Hydrogen Plant Reformer Heater H1810 Stacks
Great Falls, Montana

Emission Limits:

Hydrogen Plant Heater

NO _x	@	1.9 lb/hr, 8.3 TPY & 0.08 lbs/MMBtu
CO	@	0.93 lb/hr, 4.1 TPY

Hydrotreater Heater

NO _x	@	1.42 lb/hr, 6.2 TPY & 0.0716 lbs/MMBtu
CO	@	0.79 lb/hr, 6.2 TPY

Measured Emissions (10/08/08):

Hydrogen Plant Reformer Heater H1810

NO _x	@	0.88 lb/hr, 3.85 TPY & 0.037 lbs/MMBtu	PASS
CO	@	0.03 lb/hr, 0.1 TPY	PASS

Diesel Hydrotreater Heater (HTU) H1701

NO _x	@	0.76 lb/hr, 2.85 TPY & 0.053 lbs/MMBtu	PASS
CO	@	0.01 lb/hr, 0.04 TPY	PASS

Example: lbs/hr → tons/year

$(0.88 \text{ lbs/hr}) (24 \text{ hrs/day}) (365 \text{ days/year}) / (2000 \text{ lbs/ton}) = 3.85 \text{ tons/year}$

Summary of Montana Refining Company, Inc.
Hydrogen Plant Reformer Heater H1810
Great Falls, Montana
NO_x/CO Emission Data
10/8/2008

Time	Run#	EPA Method #7E - NO _x Emissions			EPA Method #10 - CO Emissions		
		ppm v/v D	PPH	lbs/MMBtu	ppm v/v D	PPH	lbs/MMBtu
07:45-08:44	1-NO _x /CO	27.2	0.87	0.036	1.4	0.03	0.001
08:52-09:51	2-NO _x /CO	27.8	0.88	0.037	1.9	0.04	0.002
09:59-10:58	3-NO _x /CO	<u>27.7</u>	<u>0.88</u>	<u>0.037</u>	<u>1.8</u>	<u>0.03</u>	<u>0.001</u>
Mean 1-3		27.6	0.88	0.037	1.7	0.03	0.001

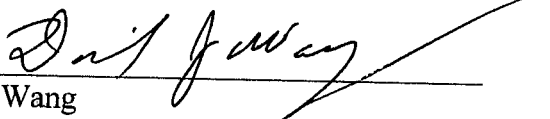
Time	Run#	EPA Methods #1-4 Gas Stream Characteristics					%CO ₂	O ₂
		AWCFM	ADCFM	DSCFH	T(s) °F	%H ₂ O v/v		
07:45-08:45	1-GF/H ₂ O	8,845.6	7,632.0	267,678.6	334	13.72	v/v Dry	5.2
08:52-09:52	2-GF/H ₂ O	8,821.6	7,565.4	265,341.7	334	14.24	13.0	5.3
09:59-10:59	3-GF/H ₂ O	<u>8,829.6</u>	<u>7,567.0</u>	<u>265,063.2</u>	<u>335</u>	<u>14.30</u>	13.1	<u>5.2</u>
Mean 1-3		8,832.3	7,588.1	266,027.8	334	14.09	<u>13.2</u>	<u>5.2</u>

MONTANA REFINING Heaters 10-8-08

<u>EPA Methods #1-4 Gas Stream Characteristics</u>							
	AWCFM	ADCFM	DSCFH	T(s)	%H ₂ O	%CO ₂ %O ₂	
				°F	v/v	v/v Dry	
11:35-12:35	4-GF/H2O	5,998.2	5,518.9	142,423.5	619	7.99	9.4 2.9
12:42-13:42	5-GF/H2O	6,080.2	5,645.5	145,553.0	620	7.15	9.5 2.8
13:49-14:49	6-GF/H2O	<u>6,115.8</u>	<u>5,658.9</u>	<u>145,901.6</u>	<u>620</u>	<u>7.47</u>	<u>9.5</u> <u>2.8</u>
Mean 4-6		6,064.7	5,607.8	144,626.0	620	7.54	9.5 2.8

Review and Certification

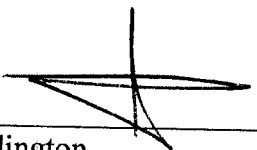
All work, calculations, and other activities and tasks performed and documented in this report were carried out under my direction and supervision. This test project conforms to EEMC's Quality Manual and to the requirements of ASTM D-7036.



David Wang
Division Manager, EEMC

Date 10 - 19 - 08

I have reviewed all testing details, calculations, results, conclusions and other appropriate written materials contained herein, and hereby certify that the presented material is authentic and accurate.



Ed Wadington
President, EEMC

Date 11 / 11 / 08

I have reviewed, and accept, the production and test data contained in this report, and hereby certify that it is authentic.

Signature

Date

Name (Printed)

Title

Company

STACK PARAMETERS

Montana Refining Company, Inc.
Great Falls, Montana

Hydrogen Plant Reformer Heater Stack

Diameter of Stack @ 35 inches (2.917 ft.)
Area of Stack @ 6.683 sq. ft.

Distance to upstream flow disturbance @ ~6 ft. (toward process)
Distance to downstream flow disturbance @ 3.0 ft. (toward stack exit)

Number of diameters upstream @ ~6 ft. / 3 ft. = -2 d
Number of diameters downstream @ 3.0 ft. / 3 ft. = 1.0 d

Number of sample ports = 2 @ 90°

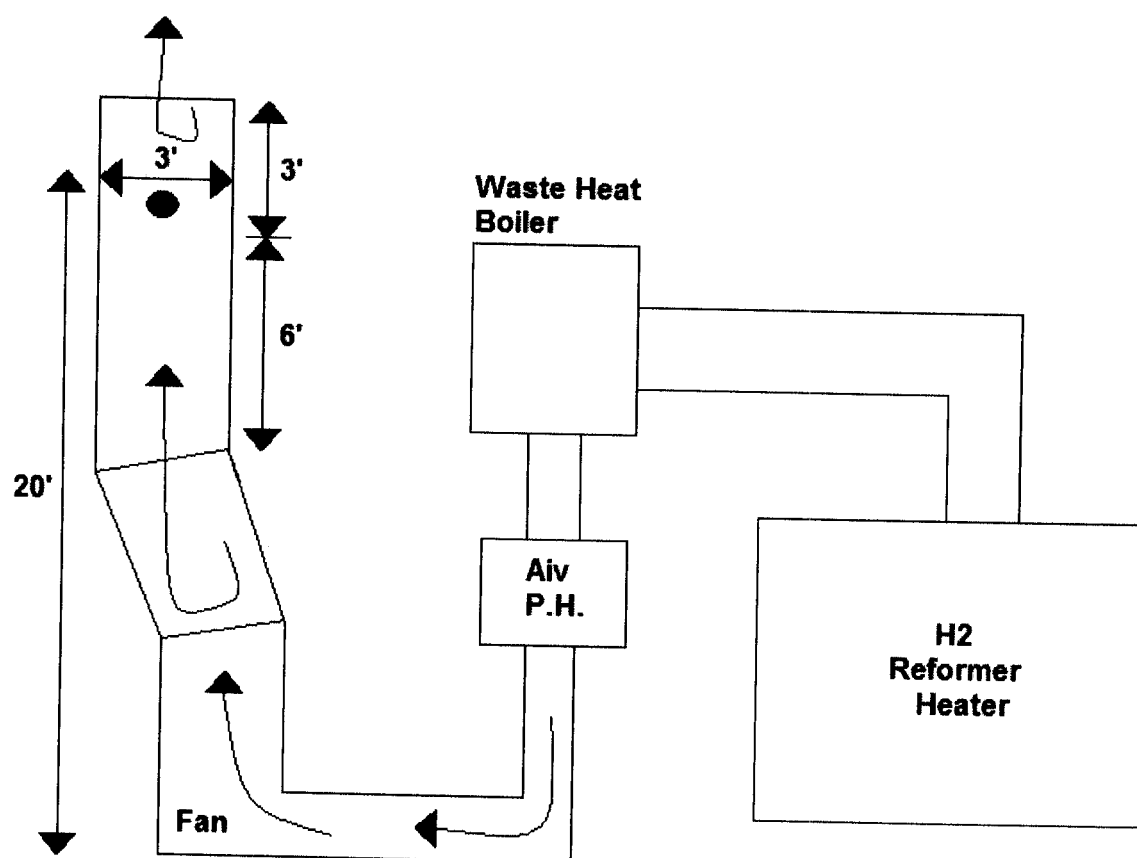
Number of NO_x/CO/Gas Flow sample (traverse) points: 24(12/traverse)

Location of traverse points: (from inside wall)

- 1) 0.735 (1.0) inches
- 2) 2.35 inches
- 3) 4.13 inches
- 4) 6.20 inches
- 5) 9.00 inches
- 6) 12.82 inches
- 7) 23.18 inches
- 8) 27.00 inches
- 9) 29.63 inches
- 10) 31.75 inches
- 11) 33.59 inches
- 12) 35.24(35.0) inches

The NO_x/CO sample probe was located at the center of the gas stream after a three point stratification test validated this strategy.

**Hydrogen Plant Reformer Heater Stack
Montana Refining Company**



STACK PARAMETERS

Montana Refining Company, Inc.
Great Falls, Montana

Diesel Hydrotreater Heater Stack (HTU)

Diameter of Stack @ 33 inches (2.75 ft.)

Area of Stack @ 5.94 sq. ft.

Distance to upstream flow disturbance @ ~6 ft. (toward process)

Distance to downstream flow disturbance @ 15 ft. (toward stack exit)

Number of diameters upstream @ ~6 ft. / 3 ft. = 17.5 d

Number of diameters downstream @ 15 ft. / 3 ft. = 6.5 d

Number of sample ports = 2 @ 90°

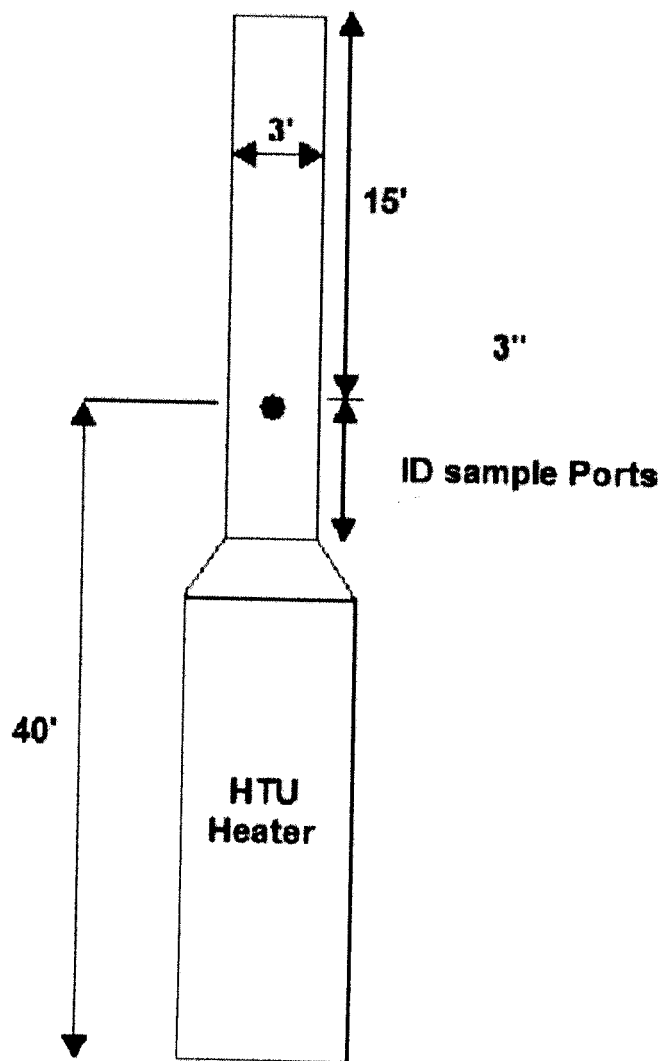
Number of NO_x/CO/Gas Flow sample (traverse) points: 24(12/traverse)

Location of traverse points: (from inside wall)

- 1) 0.69 (1.0) inches
- 2) 2.21 inches
- 3) 3.89 inches
- 4) 5.84 inches
- 5) 8.25 inches
- 6) 11.75 inches
- 7) 21.25 inches
- 8) 24.75 inches
- 9) 27.16 inches
- 10) 29.11 inches
- 11) 30.79 inches
- 12) 32.31(32.0) inches

The NO_x/CO sample probe was located at the center of the gas stream after a three point stratification test validated this strategy.

Diesel Hydrotreater Heater Stack (HTU)
Montana Refining Company





NO_x EXAMPLE CALCULATIONS

COMPANY NAME: <u>Montana Refining Co.</u>	SPECIES: <u>NO_x</u>
PLANT LOCATION: <u>Great Falls, Montana</u>	TEST DATE: <u>10/8/08</u>
SOURCE TESTED: <u>H₂ Plant Reformer H1810</u>	

Run #1

Calculate the "Calibration Corrected NO_x Value", C_{GAS} - EPA Reference Method #7E

$$C_{GAS} = \frac{(C_{Mean} - C_0)[C_{MA}/(C_M - C_0)]}{\text{corrected gas concentration, ppm v/v dry}}$$

$$C_{Mean} = \text{average gas ppm from analyzer}$$

$$C_{Mean} = \underline{27.12}$$

$$C_0 = \text{average of initial and final (post) system bias calibration check for zero calibration gas, ppm}$$

$$C_0 = \underline{0.15}$$

$$C_{MA} = \text{actual concentration of upscale calibration gas, ppm}$$

$$C_{MA} = \underline{50.2}$$

$$C_M = \text{average of initial and final (post) system bias calibration check for upscale calibration gas, ppm}$$

$$C_M = \underline{49.95}$$

$$C_{GAS} = \frac{(27.12 - 0.15)[50.2 / (49.95 - 0.15)]}{\text{corrected gas concentration, ppm v/v dry}}$$

$$= \underline{27.2}$$

F_d Calculations - EPA Reference Method #19

Oxygen based F factor dry basis.

$$E = C_d F_d [20.9 / (20.9 - \%O_2)]$$

Where:

$$E = \text{emission rate in lbs/mmBtu}$$

$$C_d = \text{concentration in lbs/scf}$$

To convert from ppm v/v dry to lbs/scf multiply ppm by 1.194×10^{-7}

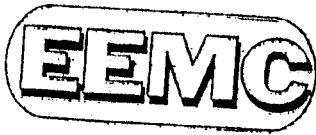
$$F_d = \text{fuel factor on a dry basis}$$

$$= \text{scf/mmBtu for natural / fuel gas as supplied / calculated.}$$

NO_x Example:

$$E = (27.2 \text{ ppm v/v dry})(1.194 \times 10^{-7})(8.258 \text{ scf/mmBtu})[20.9 / (20.9 - 5.2 \%O_2)]$$

$$= \underline{0.036} \text{ lbs/mmBtu}$$



CO EXAMPLE CALCULATIONS

COMPANY NAME: <u>Montana Refining</u>	SPECIES: <u>CO</u>
PLANT LOCATION: <u>Great Falls, Montana</u>	TEST DATE: <u>10/8/89</u>
SOURCE TESTED: <u>H2 Plant Reformer H1810</u>	

Calculate the "Calibration Corrected CO Value", C_{GAS} - EPA Reference Method #10

$$C_{GAS} = (C_{Mean} - C_0) [C_{MA} / (C_M - C_0)]$$

corrected gas concentration, ppm v/v dry

$$C_{Mean} = \text{average gas ppm from analyzer}$$

$$C_{Mean} = \underline{1.59}$$

$$C_0 = \text{average of initial and final (post) system bias calibration check for zero calibration gas, ppm}$$

$$C_0 = \underline{0.2}$$

$$C_{MA} = \text{actual concentration of upscale calibration gas, ppm}$$

$$C_{MA} = \underline{43.8}$$

$$C_M = \text{average of initial and final (post) system bias calibration check for upscale calibration gas, ppm}$$

$$C_M = \underline{43.355}$$

$$C_{GAS} = \frac{(1.59 - 0.2) [43.8]}{(43.355 - 0.2)}$$

$$= \underline{1.41}$$

F_d Calculations - EPA Reference Method #19

Oxygen based F factor dry basis.

$$E = C_d F_d [20.9 / (20.9 - \%O_2)]$$

Where:

$$E = \text{emission rate in lbs/mmBtu}$$

$$C_d = \text{concentration in lb/scf}$$

To convert from ppm v/v dry to lb/scf multiply ppm by 7.27×10^{-8}

$$F_d = \text{fuel factor on a dry basis}$$

$$= \underline{8.258} \text{ scf/mmBtu for natural / fuel gas as supplied / calculated.}$$

CO Example:

$$E = \frac{(1.4 \text{ ppm v/v dry})(7.27 \times 10^{-8})(8.258)}{0.001 \text{ lb/mmBtu}} [20.9 / (20.9 - 5.2 \%O_2)]$$



MASS FLOW EXAMPLE CALCULATIONS

COMPANY NAME: Montana Refining Co.
PLANT LOCATION: Great Falls, Montana
SOURCE TESTED: H2 Plant Refinery, H1810

SPECIES: NOx / CO
TEST DATE: 10/8/08

Definitions:

PPH based on MW, Molecular Weight, MW = 46/28 for species NOx / CO
Gas Flow (GF) units are awcfm, scdfh, or what is compatible to concentration.

Concentration units are ppm v/v dry or wet, compatible to gas flow.

Volume/Mole, V/M = (359 cu.ft./lb-mole @ STP) $\left(\frac{T_s \text{ } ^\circ\text{A}}{492^\circ\text{A}} \right) \left(\frac{29.92\text{Hg}}{\text{Ps} \text{ "Hg}} \right)$

Ts °A = Temperature Stack, degrees Absolute

Ps "Hg = Pressure Stack, inches mercury

pph = $(60 \times 10^{-6}) (MW / (V/M)) (Gas \text{ Flow}) (Concentration)$

Run # 1 PPH Basis (Species = NOx, MW = 46)
NOx
$$= (60 \times 10^{-6}) (46 \text{ MW}) / (659.082 \text{ V/M}) (7,632 \text{ GF}) (27.2 \text{ ppmv/v}) = 0.87$$

$$V/M = (359 \text{ cu.ft./lb-mole @ STP}) \left(\frac{794 \text{ } ^\circ\text{A}}{492^\circ\text{A}} \right) \left(\frac{29.92\text{Hg}}{26.30 \text{ "Hg}} \right) = 659.082$$

CO
$$= (60 \times 10^{-6}) (28 \text{ MW}) / (659.082 \text{ V/M}) (7,632 \text{ GF}) (1.4 \text{ ppmv/v}) = 0.03$$

$$V/M = (359 \text{ cu.ft./lb-mole @ STP}) \left(\frac{\text{Ts } ^\circ\text{A}}{492^\circ\text{A}} \right) \left(\frac{29.92\text{Hg}}{\text{Ps "Hg}} \right) =$$

$$= (60 \times 10^{-6}) ((\text{MW}) / (\text{V/M})) (\text{GF}) (\text{ppmv/v}) =$$

$$V/M = (359 \text{ cu.ft./lb-mole @ STP}) \left(\frac{\text{Ts } ^\circ\text{A}}{492^\circ\text{A}} \right) \left(\frac{29.92\text{Hg}}{\text{Ps "Hg}} \right) =$$

$$= (60 \times 10^{-6}) ((\text{MW}) / (\text{V/M})) (\text{GF}) (\text{ppmv/v}) =$$

$$V/M = (359 \text{ cu.ft./lb-mole @ STP}) \left(\frac{\text{Ts } ^\circ\text{A}}{492^\circ\text{A}} \right) \left(\frac{29.92\text{Hg}}{\text{Ps "Hg}} \right) =$$

$$= (60 \times 10^{-6}) ((\text{MW}) / (\text{V/M})) (\text{GF}) (\text{ppmv/v}) =$$

$$V/M = (359 \text{ cu.ft./lb-mole @ STP}) \left(\frac{\text{Ts } ^\circ\text{A}}{492^\circ\text{A}} \right) \left(\frac{29.92\text{Hg}}{\text{Ps "Hg}} \right) =$$

Compliance Data
EPA Methods #7E & 10

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Hydrogen Plant Reformer Heater H1810

Run #: 1-NO_x/CO
Time: 07:45-08:44
Date: 10/08/08

#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry	#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry
1	7:45	27.5	1.5	31	8:15	26.9	1.8
2	7:46	26.0	1.4	32	8:16	26.5	1.7
3	7:47	26.8	1.5	33	8:17	26.3	1.6
4	7:48	27.7	1.5	34	8:18	26.9	1.5
5	7:49	27.5	1.5	35	8:19	25.9	1.9
6	7:50	26.8	1.6	36	8:20	26.9	1.7
7	7:51	27.3	1.4	37	8:21	27.7	1.6
8	7:52	26.2	1.5	38	8:22	28.7	1.7
9	7:53	26.7	1.5	39	8:23	29.3	1.8
10	7:54	27.9	1.4	40	8:24	25.1	1.5
11	7:55	26.5	1.6	41	8:25	24.3	1.6
12	7:56	27.1	1.2	42	8:26	26.3	1.5
13	7:57	26.4	1.4	43	8:27	28.1	1.9
14	7:58	26.4	1.4	44	8:28	29.4	1.8
15	7:59	27.6	1.5	45	8:29	30.8	1.7
16	8:00	26.8	1.4	46	8:30	29.3	1.8
17	8:01	27.8	1.3	47	8:31	24.5	1.6
18	8:02	27.4	1.5	48	8:32	25.0	1.7
19	8:03	27.0	1.3	49	8:33	27.5	1.5
20	8:04	27.2	1.3	50	8:34	28.9	1.9
21	8:05	27.4	1.3	51	8:35	30.1	1.8
22	8:06	27.0	1.4	52	8:36	30.7	1.8
23	8:07	26.9	1.6	53	8:37	25.7	1.7
24	8:08	26.7	1.5	54	8:38	24.0	1.5
25	8:09	26.4	1.2	55	8:39	25.6	1.7
26	8:10	27.7	1.6	56	8:40	27.4	1.8
27	8:11	27.3	1.6	57	8:41	28.2	2.0
28	8:12	27.6	1.8	58	8:42	28.8	1.9
29	8:13	27.8	1.7	59	8:43	25.2	1.8
30	8:14	27.5	1.7	60	8:44	24.3	1.6
				Averages:		27.12	1.59

Client: Montana Refining Company, Inc.
Source: Hydrogen Plant Reformer Heater H1810

Test #: 1-NOx/CO
Date: 10/8/2008

Instrument Calibration Checks

NO_x Instrument

Calibration Span, CS: 100.7 ppm v/v Dry

NO_x Calibration Error Tests

Time	Tank Value C _v	Instrument Resp., C _{Dir}	System CE, SCE ($< 2\%$ of span)
7:16	0.0	0.0	0.0
7:20	50.2	50.1	-0.1
7:24	100.7	100.3	-0.4

Initial System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _i ($< 5\%$ of span)
7:33	0.0	0.1	0.1
7:31	50.2	50.0	-0.2

Post System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _f ($< 5\%$ of span)	Drift, D (SB _f - SB _i) ($< 3\%$ of span)
8:46	0.0	0.2	0.2	0.1
8:48	50.2	49.9	-0.3	-0.1

CO Instrument

Calibration Span, CS: 93.5 ppm v/v Dry

CO Calibration Error Tests

Time	Tank Value C _v	Instrument Resp., C _{Dir}	System CE, SCE ($< 2\%$ of span)
7:16	0	0.1	0.1
7:18	43.8	43.6	-0.2
7:22	93.5	93.1	-0.4

Initial System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _i ($< 5\%$ of span)
7:29	0	0.2	0.2
7:27	43.8	43.5	-0.3

Post System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _f ($< 5\%$ of span)	Drift, D (SB _f - SB _i) ($< 3\%$ of span)
8:46	0	0.2	0.2	0.0
8:50	43.8	43.5	-0.3	0.0

Instrument Response Times:

	Zero	High
NO _x	27	25 seconds
CO	27	29 seconds

Client: Montana Refining Company, Inc.
Source: Hydrogen Plant Reformer Heater H1810

Test #: 1-NOx/CO
Date: 10/8/2008

Data From Concurrent Run:

Ps	26.301 IN Hg
Gas Flow	7,632.0 adcfm
Avg. Temp	334 Deg. F 794 Deg. A (R)
NOx Molecular Wt.	46
CO Molecular Wt.	28
Oxygen	5.2 % v/v dry
cu.ft/lb-mole	
Act Conditions	659.082 ft ³ /#mole
Fd Factor (O ₂ Basis)	8,258 dscf/mmBtu

Calculations:

Averages:

NO _x	27.12 ppm v/v Dry
CO	1.59 ppm v/v Dry

Calibration Corrected Values:

NO _x	27.2 ppm v/v Dry
CO	1.4 ppm v/v Dry

Mass Flow:

NO _x	0.87 PPH
CO	0.03 PPH

NO _x	0.036 lb/mmBTU
CO	0.001 lb/mmBTU

Compliance Data
EPA Methods #7E & 10

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Hydrogen Plant Reformer Heater H1811

Run #: 2-NO_x/CO
Time: 08:52-09:51
Date: 10/08/08

#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry	#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry
1	8:52	26.1	1.7	31	9:22	30.7	2.3
2	8:53	28.2	1.7	32	9:23	31.4	2.4
3	8:54	29.2	1.7	33	9:24	25.1	2.6
4	8:55	30.6	1.6	34	9:25	24.4	2.6
5	8:56	30.6	1.7	35	9:26	26.8	2.7
6	8:57	24.8	1.6	36	9:27	28.7	2.9
7	8:58	24.3	1.8	37	9:28	30.0	3.0
8	8:59	26.7	1.6	38	9:29	31.3	3.1
9	9:00	28.3	1.8	39	9:30	27.2	3.1
10	9:01	29.5	1.5	40	9:31	24.2	2.4
11	9:02	30.9	1.3	41	9:32	25.1	2.5
12	9:03	27.7	1.6	42	9:33	27.3	2.3
13	9:04	24.4	1.7	43	9:34	28.3	2.4
14	9:05	24.9	1.5	44	9:35	29.2	2.3
15	9:06	27.1	1.7	45	9:36	28.1	2.6
16	9:07	28.1	1.7	46	9:37	25.1	2.5
17	9:08	29.4	1.8	47	9:38	25.5	2.2
18	9:09	28.9	1.4	48	9:39	27.3	2.7
19	9:10	25.0	1.7	49	9:40	28.1	2.5
20	9:11	24.6	1.3	50	9:41	29.0	2.4
21	9:12	26.4	1.4	51	9:42	30.0	2.5
22	9:13	27.1	1.5	52	9:43	29.8	2.2
23	9:14	28.0	1.6	53	9:44	25.6	2.7
24	9:15	29.3	1.7	54	9:45	25.3	2.7
25	9:16	30.0	1.8	55	9:46	27.3	2.2
26	9:17	25.3	1.9	56	9:47	29.0	2.5
27	9:18	24.2	1.9	57	9:48	30.3	2.3
28	9:19	26.2	2.0	58	9:49	32.0	2.4
29	9:20	28.1	1.9	59	9:50	31.3	2.7
30	9:21	29.0	2.0	60	9:51	25.2	2.5
Averages:						27.69	2.11

Client: Montana Refining Company, Inc.
Source: Hydrogen Plant Reformer Heater H1810

Test #: 2-NOx/CO
Date: 10/8/2008

Instrument Calibration Checks

NO_x Instrument

Calibration Span, CS: 100.7 ppm v/v Dry

NO_x Calibration Error Tests

Time	Tank Value C_v	Instrument Resp., C_{Dir}	System CE, SCE ($< 2\%$ of span)
7:16	0.0	0.0	0.0
7:20	50.2	50.1	-0.1
7:24	100.7	100.3	-0.4

Initial System Bias Check

Time	Tank Value C_v	Instrument Resp., C_s	System Bias, SB_i ($< 5\%$ of span)
8:46	0.0	0.2	0.2
8:48	50.2	49.9	-0.3

Post System Bias Check

Time	Tank Value C_v	Instrument Resp., C_s	System Bias, SB_r ($< 5\%$ of span)	Drift, D ($SB_r - SB_i$) ($< 3\%$ of span)
9:53	0.0	0.2	0.2	0.0
9:55	50.2	49.9	-0.3	0.0

CO Instrument

Calibration Span, CS: 93.5 ppm v/v Dry

CO Calibration Error Tests

Time	Tank Value C_v	Instrument Resp., C_{Dir}	System CE, SCE ($< 2\%$ of span)
7:16	0	0.1	0.1
7:18	43.8	43.6	-0.2
7:22	93.5	93.1	-0.4

Initial System Bias Check

Time	Tank Value C_v	Instrument Resp., C_s	System Bias, SB_i ($< 5\%$ of span)
8:46	0	0.2	0.2
8:50	43.8	43.5	-0.3

Post System Bias Check

Time	Tank Value C_v	Instrument Resp., C_s	System Bias, SB_r ($< 5\%$ of span)	Drift, D ($SB_r - SB_i$) ($< 3\%$ of span)
9:53	0	0.2	0.2	0.0
9:57	43.8	43.5	-0.3	0.0

Instrument Response Times:

	Zero	High
NO _x	27	25 seconds
CO	27	29 seconds

Client: Montana Refining Company, Inc.
Source: Hydrogen Plant Reformer Heater H1810

Test #: 2-NOx/CO
Date: 10/8/2008

Data From Concurrent Run:

Ps	26.301 IN Hg
Gas Flow	7,565.4 adcfm
Avg. Temp	334 Deg. F 794 Deg. A (R)
NOx Molecular Wt.	46
CO Molecular Wt.	28
Oxygen	5.3 % v/v dry
cu.ft/lb-mole	
Act Conditions	659.082 ft ³ /#mole
Fd Factor (O ₂ Basis)	8,258 dscf/mmBtu

Calculations:

Averages:

NO _x	27.69 ppm v/v Dry
CO	2.11 ppm v/v Dry

Calibration Corrected Values:

NO _x	27.8 ppm v/v Dry
CO	1.9 ppm v/v Dry

Mass Flow:

NO _x	0.88 PPH
CO	0.04 PPH

NO _x	0.037 lb/mmBTU
CO	0.002 lb/mmBTU

Compliance Data
EPA Methods #7E & 10

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Hydrogen Plant Reformer Heater H18

Run #: 3-NO_x/CO
Time: 09:59-10:58
Date: 10/08/08

#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry	#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry
1	9:59	24.9	2.3	31	10:29	29.4	1.9
2	10:00	27.1	2.4	32	10:30	27.8	1.7
3	10:01	28.2	2.6	33	10:31	25.3	1.8
4	10:02	29.5	2.5	34	10:32	25.7	2.0
5	10:03	28.4	2.2	35	10:33	27.4	1.9
6	10:04	24.6	2.3	36	10:34	27.8	1.3
7	10:05	25.1	2.5	37	10:35	28.9	1.4
8	10:06	26.7	2.3	38	10:36	29.9	1.4
9	10:07	27.6	2.6	39	10:37	29.3	1.5
10	10:08	28.4	2.4	40	10:38	25.1	1.6
11	10:09	29.3	2.7	41	10:39	25.0	1.6
12	10:10	30.0	2.5	42	10:40	27.3	1.5
13	10:11	25.8	1.7	43	10:41	29.0	1.6
14	10:12	24.8	1.8	44	10:42	30.1	1.6
15	10:13	27.0	1.8	45	10:43	31.3	1.6
16	10:14	29.0	2.1	46	10:44	28.8	1.9
17	10:15	29.9	2.0	47	10:45	24.7	1.8
18	10:16	31.2	1.9	48	10:46	25.6	1.7
19	10:17	30.8	2.1	49	10:47	28.2	1.7
20	10:18	25.2	1.9	50	10:48	29.3	1.7
21	10:19	25.2	1.7	51	10:49	30.7	1.8
22	10:20	27.7	2.1	52	10:50	30.3	1.8
23	10:21	29.1	2.1	53	10:51	25.6	1.9
24	10:22	30.2	1.9	54	10:52	24.4	1.9
25	10:23	31.1	1.8	55	10:53	26.2	2.0
26	10:24	26.6	1.9	56	10:54	27.6	1.8
27	10:25	24.6	1.8	57	10:55	28.7	2.0
28	10:26	25.8	1.8	58	10:56	26.8	2.0
29	10:27	27.5	1.9	59	10:57	27.0	2.5
30	10:28	28.5	1.7	60	10:58	26.6	2.8
Averages:						27.66	1.95

Client: Montana Refining Company, Inc.
Source: Hydrogen Plant Reformer Heater H1810

Test #: 3-NOx/CO
Date: 10/8/2008

Instrument Calibration Checks

NO_x Instrument

Calibration Span, CS: 100.7 ppm v/v Dry

NO_x Calibration Error Tests

Time	Tank Value C _v	Instrument Resp., C _{Dir}	System CE, SCE ($< 2\%$ of span)
7:16	0.0	0.0	0.0
7:20	50.2	50.1	-0.1
7:24	100.7	100.3	-0.4

Initial System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _i ($< 5\%$ of span)
9:53	0.0	0.2	0.2
9:55	50.2	49.9	-0.3

Post System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _f ($< 5\%$ of span)	Drift, D (SB _f - SB _i) ($< 3\%$ of span)
11:00	0.0	0.2	0.2	0.0
11:02	50.2	50.0	-0.2	0.1

CO Instrument

Calibration Span, CS: 93.5 ppm v/v Dry

CO Calibration Error Tests

Time	Tank Value C _v	Instrument Resp., C _{Dir}	System CE, SCE ($< 2\%$ of span)
7:16	0	0.1	0.1
7:18	43.8	43.6	-0.2
7:22	93.5	93.1	-0.4

Initial System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _i ($< 5\%$ of span)
9:53	0	0.2	0.2
9:57	43.8	43.5	-0.3

Post System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _f ($< 5\%$ of span)	Drift, D (SB _f - SB _i) ($< 3\%$ of span)
11:00	0	0.2	0.2	0.0
11:04	43.8	43.6	-0.2	0.1

Instrument Response Times:

	Zero	High
NO _x	27	25 seconds
CO	27	29 seconds

Client: Montana Refining Company, Inc.
Source: Hydrogen Plant Reformer Heater H1810

Test #: 3-NOx/CO
Date: 10/8/2008

Data From Concurrent Run:

Ps	26.301 IN Hg
Gas Flow	7,567.0 adcfm
Avg. Temp	335 Deg. F 795 Deg. A (R)
NOx Molecular Wt.	46
CO Molecular Wt.	28
Oxygen	5.3 % v/v dry
cu.ft/lb-mole	
Act Conditions	659.912 ft ³ /#mole
Fd Factor (O ₂ Basis)	8,258 dscf/mmBtu

Calculations:

Averages:	
NO _x	27.66 ppm v/v Dry
CO	1.95 ppm v/v Dry
Calibration Corrected Values:	
NO _x	27.7 ppm v/v Dry
CO	1.8 ppm v/v Dry
Mass Flow:	
NO _x	0.88 PPH
CO	0.03 PPH
NO _x	0.037 lb/mmBTU
CO	0.001 lb/mmBTU

Montana Refining Company
NO_x/CO Computer Logger Data
10/08/08

Time	NO _x -PPM v/v Dry	CO-PPM v/v Dry	Comments
7:15	0.0	0.1	Initial Calibration Information:
7:16	<u>0.0</u>	<u>0.1</u>	Response Check
7:17	0.0	29.9	
7:18	0.0	<u>43.6</u>	Response Check
7:19	29.9	22.4	
7:20	<u>50.1</u>	0.2	Response Check
7:21	16.4	78.6	
7:22	0.1	<u>93.1</u>	Response Check
7:23	67.4	22.5	
7:24	<u>100.3</u>	0.1	Response Check
7:25	36.8	0.1	<u>NO_x Tanks:</u>
7:26	0.0	34.6	LL31587 @ 100.7 ppm; Exp. 08/11/10
7:27	0.0	<u>43.5</u>	AL88466 @ 51.6 ppm; Exp. 03/19/09
7:28	0.0	12.4	ET0001887 @ 50.2 ppm; Exp. 10/15/09
7:29	0.0	<u>0.2</u>	NO _x Instrument: CAI 400
7:30	32.6	0.2	
7:31	<u>50.0</u>	0.2	<u>CO Tanks:</u>
7:32	14.6	0.2	ER0000536 @ 43.8 ppm; Exp. 10/02/2009
7:33	<u>0.1</u>	0.2	ER0000533 @ 93.5 ppm; Exp. 10/02/2009
7:34	40.1	0.2	CO Instrument: CAI 100
7:35	47.4	0.2	
7:36	<u>47.4</u>	0.2	NO _x Conversion Efficiency Check
7:37	17.5	0.2	
7:38	27.6	0.5	
7:39	26.1	1.6	Stratification Test
7:40	26.9	1.5	Stratification Test
7:41	27.6	1.3	Stratification Test
7:42	27.0	1.2	Stratification Test
7:43	27.2	1.3	Stratification Test
7:44	28.0	1.3	Stratification Test
7:45	27.5	1.5	Start Run 1
7:46	26.0	1.4	Plant Reformer 1810
7:47	26.8	1.5	
7:48	27.7	1.5	
7:49	27.5	1.5	
7:50	26.8	1.6	
7:51	27.3	1.4	
7:52	26.2	1.5	
7:53	26.7	1.5	
7:54	27.9	1.4	
7:55	26.5	1.6	
7:56	27.1	1.2	
7:57	26.4	1.4	
7:58	26.4	1.4	
7:59	27.6	1.5	
8:00	26.8	1.4	
8:01	27.8	1.3	
8:02	27.4	1.5	
8:03	27.0	1.3	
8:04	27.2	1.3	
8:05	27.4	1.3	
8:06	27.0	1.4	

Montana Refining Company
NO_x/CO Computer Logger Data
10/08/08

Time	NO _x -PPM	CO-PPM	Comments
	v/v Dry	v/v Dry	
8:07	26.9	1.6	
8:08	26.7	1.5	
8:09	26.4	1.2	
8:10	27.7	1.6	
8:11	27.3	1.6	
8:12	27.6	1.8	
8:13	27.8	1.7	
8:14	27.5	1.7	
8:15	26.9	1.8	
8:16	26.5	1.7	
8:17	26.3	1.6	
8:18	26.9	1.5	
8:19	25.9	1.9	
8:20	26.9	1.7	
8:21	27.7	1.6	
8:22	28.7	1.7	
8:23	29.3	1.8	
8:24	25.1	1.5	
8:25	24.3	1.6	
8:26	26.3	1.5	
8:27	28.1	1.9	
8:28	29.4	1.8	
8:29	30.8	1.7	
8:30	29.3	1.8	
8:31	24.5	1.6	
8:32	25.0	1.7	
8:33	27.5	1.5	
8:34	28.9	1.9	
8:35	30.1	1.8	
8:36	30.7	1.8	
8:37	25.7	1.7	
8:38	24.0	1.5	
8:39	25.6	1.7	
8:40	27.4	1.8	
8:41	28.2	2.0	
8:42	28.8	1.9	
8:43	25.2	1.8	
8:44	24.3	1.6	End Run 1
8:45	2.9	0.3	
8:46	<u>0.2</u>	0.2	
8:47	28.7	0.2	
8:48	<u>49.9</u>	0.2	
8:49	15.3	32.6	
8:50	0.2	<u>43.5</u>	
8:51	5.5	0.8	
8:52	26.1	1.7	Start Run 2
8:53	28.2	1.7	
8:54	29.2	1.7	
8:55	30.6	1.6	
8:56	30.6	1.7	
8:57	24.8	1.6	
8:58	24.3	1.8	

Montana Refining Company
NO_x/CO Computer Logger Data
10/08/08

Time	NO _x -PPM	CO-PPM	Comments
	v/v Dry	v/v Dry	
8:59	26.7	1.6	
9:00	28.3	1.8	
9:01	29.5	1.5	
9:02	30.9	1.3	
9:03	27.7	1.6	
9:04	24.4	1.7	
9:05	24.9	1.5	
9:06	27.1	1.7	
9:07	28.1	1.7	
9:08	29.4	1.8	
9:09	28.9	1.4	
9:10	25.0	1.7	
9:11	24.6	1.3	
9:12	26.4	1.4	
9:13	27.1	1.5	
9:14	28.0	1.6	
9:15	29.3	1.7	
9:16	30.0	1.8	
9:17	25.3	1.9	
9:18	24.2	1.9	
9:19	26.2	2.0	
9:20	28.1	1.9	
9:21	29.0	2.0	
9:22	30.7	2.3	
9:23	31.4	2.4	
9:24	25.1	2.6	
9:25	24.4	2.6	
9:26	26.8	2.7	
9:27	28.7	2.9	
9:28	30.0	3.0	
9:29	31.3	3.1	
9:30	27.2	3.1	
9:31	24.2	2.4	
9:32	25.1	2.5	
9:33	27.3	2.3	
9:34	28.3	2.4	
9:35	29.2	2.3	
9:36	28.1	2.6	
9:37	25.1	2.5	
9:38	25.5	2.2	
9:39	27.3	2.7	
9:40	28.1	2.5	
9:41	29.0	2.4	
9:42	30.0	2.5	
9:43	29.8	2.2	
9:44	25.6	2.7	
9:45	25.3	2.7	
9:46	27.3	2.2	
9:47	29.0	2.5	
9:48	30.3	2.3	
9:49	32.0	2.4	
9:50	31.3	2.7	

Montana Refining Company
NO_x/CO Computer Logger Data
10/08/08

Time	NO _x -PPM	CO-PPM	Comments
	v/v Dry	v/v Dry	
9:51	25.2	2.5	End Run 2
9:52	3.5	0.4	
9:53	<u>0.2</u>	<u>0.2</u>	
9:54	30.4	0.2	
9:55	<u>49.9</u>	0.2	
9:56	11.3	33.4	
9:57	0.2	<u>43.5</u>	
9:58	12.2	8.5	
9:59	24.9	2.3	Start Run 3
10:00	27.1	2.4	
10:01	28.2	2.6	
10:02	29.5	2.5	
10:03	28.4	2.2	
10:04	24.6	2.3	
10:05	25.1	2.5	
10:06	26.7	2.3	
10:07	27.6	2.6	
10:08	28.4	2.4	
10:09	29.3	2.7	
10:10	30.0	2.5	
10:11	25.8	1.7	
10:12	24.8	1.8	
10:13	27.0	1.8	
10:14	29.0	2.1	
10:15	29.9	2.0	
10:16	31.2	1.9	
10:17	30.8	2.1	
10:18	25.2	1.9	
10:19	25.2	1.7	
10:20	27.7	2.1	
10:21	29.1	2.1	
10:22	30.2	1.9	
10:23	31.1	1.8	
10:24	26.6	1.9	
10:25	24.6	1.8	
10:26	25.8	1.8	
10:27	27.5	1.9	
10:28	28.5	1.7	
10:29	29.4	1.9	
10:30	27.8	1.7	
10:31	25.3	1.8	
10:32	25.7	2.0	
10:33	27.4	1.9	
10:34	27.8	1.3	
10:35	28.9	1.4	
10:36	29.9	1.4	
10:37	29.3	1.5	
10:38	25.1	1.6	
10:39	25.0	1.6	
10:40	27.3	1.5	
10:41	29.0	1.6	
10:42	30.1	1.6	

Montana Refining Company
NO_x/CO Computer Logger Data
10/08/08

Time	NO _x -PPM	CO-PPM	Comments
	v/v Dry	v/v Dry	
10:43	31.3	1.6	
10:44	28.8	1.9	
10:45	24.7	1.8	
10:46	25.6	1.7	
10:47	28.2	1.7	
10:48	29.3	1.7	
10:49	30.7	1.8	
10:50	30.3	1.8	
10:51	25.6	1.9	
10:52	24.4	1.9	
10:53	26.2	2.0	
10:54	27.6	1.8	
10:55	28.7	2.0	
10:56	26.8	2.0	
10:57	27.0	2.5	
10:58	26.6	2.8	End Run 3
10:59	5.2	0.6	
11:00	<u>0.2</u>	<u>0.2</u>	
11:01	29.6	0.2	
11:02	<u>50.0</u>	0.2	
11:03	11.5	26.7	
11:04	0.2	<u>43.6</u>	
11:05	0.1	7.8	
11:06	0.1	0.2	Initial Calibrations:
11:07	<u>0.1</u>	<u>0.2</u>	Diesel Hydrotreater Heater 1701
11:08	29.9	0.2	
11:09	<u>50.0</u>	26.6	Response Check
11:10	12.4	<u>43.5</u>	Response Check
11:11	0.3	20.0	
11:12	36.6	0.3	
11:13	<u>100.4</u>	45.4	Response Check
11:14	24.7	<u>93.1</u>	Response Check
11:15	0.1	23.6	
11:16	29.6	0.2	
11:17	<u>49.9</u>	0.2	
11:18	17.5	0.2	
11:19	<u>0.2</u>	0.2	
11:20	0.2	32.4	
11:21	0.2	<u>43.5</u>	
11:22	0.2	15.3	
11:23	0.2	<u>0.3</u>	
11:24	8.8	0.7	
11:25	43.3	1.6	
11:26	42.2	1.7	
11:27	43.1	1.8	
11:28	41.2	1.7	
11:29	41.8	1.8	
11:30	43.3	1.8	
11:31	41.4	1.7	
11:32	43.0	1.5	
11:33	42.5	1.6	
11:34	43.2	1.7	Diesel Hydrotreater Heater 1701

Montana Refining Company
NO_x/CO Computer Logger Data
10/08/08

Time	NO _x -PPM	CO-PPM	Comments
	v/v Dry	v/v Dry	
11:35	42.9	1.7	Start Run 4
11:36	41.9	1.8	
11:37	41.6	1.7	
11:38	41.5	1.6	
11:39	40.4	1.9	
11:40	40.4	1.5	
11:41	44.1	1.5	
11:42	45.8	1.8	
11:43	44.1	1.6	
11:44	25.6	1.8	
11:45	40.6	1.5	
11:46	43.1	1.6	
11:47	43.3	1.8	
11:48	42.7	1.7	
11:49	45.1	1.6	
11:50	44.2	1.6	
11:51	43.6	1.5	
11:52	43.6	1.7	
11:53	44.3	1.7	
11:54	44.5	1.5	
11:55	43.9	1.7	
11:56	43.8	1.5	
11:57	43.3	1.9	
11:58	43.5	1.5	
11:59	45.5	1.8	
12:00	45.3	1.9	
12:01	44.4	1.5	
12:02	44.7	1.5	
12:03	44.0	1.5	
12:04	42.5	1.5	
12:05	44.6	1.5	
12:06	45.2	1.6	
12:07	39.3	1.6	
12:08	37.7	1.8	
12:09	42.7	1.5	
12:10	45.9	1.4	
12:11	45.7	1.5	
12:12	45.1	1.6	
12:13	44.8	1.6	
12:14	42.9	1.6	
12:15	42.3	1.7	
12:16	43.1	1.7	
12:17	43.1	1.6	
12:18	43.7	1.7	
12:19	42.5	1.7	
12:20	42.4	1.7	
12:21	43.7	1.7	
12:22	45.0	1.7	
12:23	44.0	1.7	
12:24	44.1	1.7	
12:25	44.1	1.7	
12:26	45.7	1.8	

Montana Refining Company
NO_x/CO Computer Logger Data
10/08/08

Time	NO _x -PPM	CO-PPM	Comments
	v/v Dry	v/v Dry	
12:27	44.4	1.8	
12:28	44.2	1.8	
12:29	45.4	1.8	
12:30	44.3	1.9	
12:31	43.5	1.9	
12:32	45.0	2.0	
12:33	44.5	2.0	
12:34	45.7	2.0	End Run 4
12:35	14.3	0.6	
12:36	<u>0.2</u>	<u>0.3</u>	
12:37	31.5	0.3	
12:38	<u>49.9</u>	0.3	
12:39	12.6	27.8	
12:40	0.2	<u>43.5</u>	
12:41	21.5	8.7	
12:42	43.7	1.8	Start Run 5
12:43	45.1	1.8	
12:44	44.1	1.9	
12:45	43.9	2.1	
12:46	45.1	1.9	
12:47	45.8	1.8	
12:48	44.9	1.8	
12:49	45.0	1.8	
12:50	44.9	1.8	
12:51	46.3	2.0	
12:52	45.2	1.7	
12:53	44.7	1.8	
12:54	40.9	1.8	
12:55	39.0	2.0	
12:56	40.4	1.7	
12:57	45.9	2.1	
12:58	45.7	1.9	
12:59	45.0	2.0	
13:00	45.2	1.7	
13:01	44.1	1.8	
13:02	43.8	2.0	
13:03	45.0	2.1	
13:04	45.0	1.7	
13:05	45.9	1.7	
13:06	45.1	1.9	
13:07	42.9	1.6	
13:08	43.1	1.5	
13:09	45.7	1.6	
13:10	44.2	1.5	
13:11	43.1	1.6	
13:12	43.4	1.5	
13:13	43.5	1.5	
13:14	43.7	1.3	
13:15	44.2	1.4	
13:16	45.7	1.7	
13:17	44.1	1.6	
13:18	43.9	1.4	

Montana Refining Company
NO_x/CO Computer Logger Data
10/08/08

Time	NO _x -PPM	CO-PPM	Comments
	v/v Dry	v/v Dry	
13:19	46.0	1.4	
13:20	44.1	1.4	
13:21	42.9	1.5	
13:22	43.7	1.5	
13:23	44.3	1.6	
13:24	45.4	1.5	
13:25	46.5	1.4	
13:26	43.9	1.4	
13:27	42.8	1.6	
13:28	44.7	1.6	
13:29	44.0	1.4	
13:30	44.1	1.4	
13:31	44.3	1.4	
13:32	44.1	1.5	
13:33	44.5	1.5	
13:34	44.8	1.7	
13:35	43.7	1.4	
13:36	43.6	1.4	
13:37	43.4	1.5	
13:38	44.3	1.5	
13:39	45.3	1.6	
13:40	45.7	1.6	
13:41	45.8	1.6	End Run 5
13:42	10.4	0.4	
13:43	<u>0.2</u>	<u>0.2</u>	
13:44	34.0	0.2	
13:45	<u>49.9</u>	0.2	
13:46	20.5	35.2	
13:47	0.2	<u>43.5</u>	
13:48	16.8	7.9	
13:49	42.8	1.7	Start Run 6
13:50	44.4	1.7	
13:51	45.0	1.8	
13:52	44.0	1.5	
13:53	42.2	1.7	
13:54	42.3	1.7	
13:55	44.2	1.6	
13:56	42.6	1.6	
13:57	44.5	1.7	
13:58	45.5	1.9	
13:59	45.1	1.8	
14:00	45.1	1.9	
14:01	43.3	1.8	
14:02	42.4	1.8	
14:03	43.3	1.9	
14:04	44.3	1.9	
14:05	45.2	1.8	
14:06	43.5	1.7	
14:07	42.8	1.7	
14:08	43.5	1.6	
14:09	43.3	1.7	
14:10	45.9	1.9	

Montana Kenning Company
NO_x/CO Computer Logger Data
10/08/08

Time	NO _x -PPM	CO-PPM	Comments
	v/v Dry	v/v Dry	
14:11	44.1	1.6	
14:12	43.4	1.8	
14:13	44.1	1.8	
14:14	44.3	1.6	
14:15	45.6	1.6	
14:16	43.8	1.7	
14:17	43.5	1.8	
14:18	43.0	2.0	
14:19	43.8	2.0	
14:20	43.4	2.0	
14:21	43.5	2.1	
14:22	43.6	1.7	
14:23	43.4	1.8	
14:24	44.5	1.8	
14:25	45.6	2.0	
14:26	45.2	1.9	
14:27	44.4	1.8	
14:28	43.0	1.8	
14:29	42.7	2.0	
14:30	43.7	1.8	
14:31	44.2	2.0	
14:32	44.1	1.9	
14:33	42.5	1.7	
14:34	43.5	1.9	
14:35	45.9	2.0	
14:36	43.6	1.9	
14:37	42.4	1.9	
14:38	43.9	1.8	
14:39	45.5	1.7	
14:40	42.9	1.7	
14:41	42.8	1.8	
14:42	44.2	2.1	
14:43	43.7	1.7	
14:44	43.8	1.8	
14:45	44.1	1.9	
14:46	42.6	1.7	
14:47	43.1	1.8	
14:48	42.7	1.7	End Run 6
14:49	9.4	0.5	
14:50	<u>0.3</u>	<u>0.2</u>	
14:51	32.8	0.2	
14:52	<u>50.0</u>	0.2	
14:53	17.7	36.2	
14:54	0.3	<u>43.5</u>	
14:55	0.3	13.6	
14:56	0.3	0.3	
14:57	0.2	0.2	



EPA METHODS # 1 - 4
GAS FLOW / MOISTURE
EXAMPLE CALCULATION

COMPANY NAME: Montana Refining Co.
PLANT LOCATION: Great Falls, Montana
SOURCE TESTED: Plant Reformer H1810

TEST DATE: 10/8/08
RUN #: 1 GF/H2O

$$P_m^{\text{Hg}} = 26.30 \text{ Pb}^{\text{Hg}} + (2.0 \text{ } \Delta H \text{ "H}_2\text{O}/13.6) = 26.447 \text{ Pm}^{\text{Hg}}$$

$$P_s^{\text{Hg}} = 26.30 \text{ Pb}^{\text{Hg}} + (0.02 \text{ Static "H}_2\text{O}/13.6) = 26.301 \text{ Ps}^{\text{Hg}}$$

$$1) V_m(\text{std}) = \left(\frac{42.763}{3} V_m \right) (17.65) \left(\frac{1.01}{2} Y \right) \left(\frac{26.447 \text{ Pm}^{\text{Hg}}}{524. \text{ Tm}^{\circ}\text{A}} \right) = 38.475 \text{ dscf}$$

$$2) V_w(\text{std}) = (0.04707) (130.0 \text{ ml}) = 6.119 \text{ scf}$$

$$3) Bws = \left(\frac{6.119 \text{ scf}}{6.119 \text{ scf} + 38.475 \text{ dscf}} \right) = .1372 \text{ Bws} \times 100 = 13.72 \% \text{H}_2\text{O}$$

$$4) V_m(\text{actual}) = \frac{\left(\frac{Y}{1 - Bws} \right) \left(\frac{V_m}{1} \right) \left(\frac{\text{Ts}^{\circ}\text{A}}{\text{Tm}^{\circ}\text{A}} \right) \left(\frac{\text{Pm}^{\text{Hg}}}{\text{Ps}^{\text{Hg}}} \right)}{\left(\frac{1}{1} \right) \left(\frac{1}{1} \right) \left(\frac{1}{1} \right) \left(\frac{1}{1} \right)} = \text{awcf}$$

$$5) M_d = 0.44 \left(\frac{13.0}{1} \% \text{CO}_2 \right) + 0.32 \left(\frac{5.2}{1} \% \text{O}_2 \right) + 0.28 \left(\frac{81.3}{1} \% \text{N}_2 + \% \text{CO} \right) = 30.29 \text{ lb/lb mole}$$

$$6) M_s = \left(\frac{30.29 \text{ lb/lb mole}}{1} \right) (1 - .1372 \text{ Bws}) + (18 \times .1372 \text{ Bws}) = 28.60 \text{ lb/lb mole}$$

$$7a) \text{Area} = (3.1416) \left(\frac{2.917 \text{ ft.}/2}{\text{dia } 3} \right)^2 = 6.683 \text{ sq.ft.}$$

$$7b) \text{Area} = \left(\frac{\text{ft.}}{3} \right) \left(\frac{\text{ft.}}{3} \right) = \text{sq.ft.}$$

$$8) V_s = (85.49) \left(\frac{.94 \text{ cp}}{2} \right) \left(\frac{\text{Avg SQRT } .299_{AP}}{1} \right) \left(\frac{794 \text{ Ts}^{\circ}\text{A}}{\sqrt{26.301 \text{ Ps}^{\text{Hg}} (28.60 \text{ lb/lb mole})}} \right) = 22.06 \text{ fps}$$

$$9a) \text{AWCFM} = (22.06 \text{ fps}) (6.683 \text{ sq.ft.}) (60 \text{ sec/min}) = 8,845.6 \text{ awcfm}$$

$$9b) \text{ADCFM} = (8,845.6 \text{ awcfm}) (1 - .1372 \text{ Bws}) = 7,624.9 \text{ adcfm}$$

$$10a) Q_{sw} = 3600 (22.06 \text{ fps}) (6.683 \text{ sq.ft.}) \left(\frac{528^{\circ}\text{A}}{794. \text{ Ts}^{\circ}\text{A}} \right) \left(\frac{26.301 \text{ Ps}^{\text{Hg}}}{29.92 \text{ "Hg}} \right) = 310,244.6 \text{ wscf/hr}$$

$$10b) Q_{sd} = (1 - .1372 \text{ Bws}) (310,244.6 \text{ wscf/hr}) = 267,678.6 \text{ dcsf/hr}$$

EPA Methods #1-4
Field Data & Calculations
Gas Flow/Moisture

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Hydrogen Plant Reformer Heater H1810

Test #: 1-GF/H₂O
Time: 07:45-08:45
Date: 10/08/08

Sample Point #	Clock Time (min.)	Meter Reading (cu.ft.)	Delta P ("H ₂ O)	Delta H ("H ₂ O)	Meter Temp. Deg. F	Stack Temp. Deg. F	SQRT Delta P
1	5	984.000	0.09	2.0	64	334	0.300
2	10		0.09	2.0	64	334	0.300
3	15		0.09	2.0	64	334	0.300
4	20		0.08	2.0	65	333	0.283
5	25		0.08	2.0	65	333	0.283
6	30		0.08	2.0	65	333	0.283
7	35		0.08	2.0	65	333	0.283
8	40		0.09	2.0	64	334	0.300
9	45		0.10	2.0	64	334	0.316
10	50		0.10	2.0	64	335	0.316
11	55		0.10	2.0	64	335	0.316
12	60		0.09	2.0	65	335	0.300
1		1,026.763	0.09			335	0.300
2			0.09			335	0.300
3			0.09			335	0.300
4			0.08			334	0.283
5			0.08			334	0.283
6			0.09			334	0.300
7			0.10			334	0.316
8			0.10			333	0.316
9			0.10			333	0.316
10			0.09			333	0.300
11			0.09			334	0.300
12			0.08			334	0.283

Client: Montana Refining Company, Inc.
Source: Hydrogen Plant Reformer Heater H1810

Test #: 1-GF/H2O
Date: 10/08/08

FIELD DATA INPUT: (CONTINUED)

Barometric Pressure (Pb) 26.30 in. Hg
Static Pressure 0.02 in H₂O
Meter Cal. Factor 1.01 Y
Pitot Factor (cp) 0.84

Orsat
%CO₂ Average 13.0 %
%O₂ Average 5.2 %

Total Test Time 60 min
Sample Time Interval 5 min
Meter Volume (Vm) 42.763 dcf
Water Volume 130 ml

Stack Dimensional Data:

Circular
Diameter 2.917 ft

Rectangular
Width 0.000 ft
Length 0.000 ft

FIELD DATA AVERAGES:

Average Delta H 2.0 in. H₂O

Average SQRT Dp 0.299 in. H₂O

Average Meter
Temperature (Tm) 64 deg F
Temperature (Tm) 524 deg A (R)

Average Stack
Temperature (Ts) 334 deg F
Temperature (Ts) 794 deg A (R)

Pressure Meter (Pm) 26.447 in. Hg

Pressure Stack (Ps) 26.301 in. Hg

Moisture (Bws) 0.1372

CALCULATIONS:

Standard Meter
Volume, Vm(std) 38.475 dscf

Stack Gas:
Velocity (Vs) 22.06 fps

Actual Meter
Volume, Vm(actual) 76.273 awcf
Volume Water
Vapor, Vw(std) 6.119 scf

Volume (actual conditions) 8,845.6 awcfm
7,632.0 adcfm

Percent Moisture 13.72 %

Volume (std. Conditions)
(@ 68 deg F & 29.9 "Hg) 310,244.1 wscf/hr
5,170.7 wscfm
267,678.6 dscf/hr
4,461.3 dscfm

Gas Density:

Dry (Md) 30.29 lb/lb-mole
Wet (Ms) 28.60 lb/lb-mole

Stack Area 6.683 sq.ft.

PARTICULATE FIELD DATA

COMPANY NAME: MT Refining Co. RUN #: 1
 PLANT LOCATION: Great Falls DATE: 10/08/08
 SOURCE TESTED: Hydrogen Plant Reformer Heater (H1810) START TIME: 0745
 METER BOX OPERATOR: RW TECHNICIANS: DW END TIME: 0845

EQUIPMENT / IDENTIFICATION CHECKS:

☒ PITOTS, PRE-TEST 120 PITOT
☒ PITOTS, POST-TEST 88 METER BOX
☒ ORSAT SAMPLING SYSTEM 1.01 Y FACTOR
☒ TEDLAR BAG 15 PRE 14 POST
☒ THERMOCOUPLE @ °F .000 PRE .000 POST
26.30 BAROMETRIC PRESSURE ("Hg) +0.02 STATIC PRESSURE ("H2O) 35" STACK DIMENSIONS
 NOZZLE # 60 TEST TIME
 NOZZLE DIA. M
 T/C READOUT
 TRAIN LEAK TEST VACUUM ("Hg)
 TRAIN LEAK TEST (ft3/min)
 STACK DIMENSIONS

Sample Point	Time (min)	Dry Gas Meter Reading (ft³)	Pitot Reading ΔP ("H ₂ O)	Meter ΔH	Meter Temp. Tm (°F)	Pump Vacuum (Hg)	Filter Box (°F)	Imp. Exit (°F)	Stack Temp. (°F)	% CO ₂	% O ₂
		<u>984.000</u>									
1	5		<u>.09</u>	<u>2</u>	<u>64</u>	<u>4</u>	<u>—</u>	<u>40</u>	<u>334</u>		
2	10		<u>.09</u>		<u>64</u>	<u>4</u>		<u>40</u>	<u>334</u>		
3	15		<u>.09</u>		<u>64</u>	<u>4</u>		<u>40</u>	<u>334</u>		
4	20		<u>.08</u>		<u>65</u>	<u>4</u>		<u>40</u>	<u>333</u>		
5	25		<u>.08</u>		<u>65</u>	<u>4</u>		<u>41</u>	<u>333</u>		
6	30		<u>.08</u>		<u>65</u>	<u>4</u>		<u>41</u>	<u>333</u>		
7	35		<u>.08</u>		<u>65</u>	<u>4</u>		<u>41</u>	<u>333</u>		
8	40		<u>.09</u>		<u>64</u>	<u>4</u>		<u>41</u>	<u>334</u>		
9	45		<u>.10</u>		<u>64</u>	<u>4</u>		<u>40</u>	<u>334</u>		
10	50		<u>.10</u>		<u>64</u>	<u>4</u>		<u>40</u>	<u>335</u>		
11	55	<u>1,026.763</u>	<u>.10</u>		<u>64</u>	<u>4</u>		<u>40</u>	<u>335</u>		
12	60	<u>26.763</u>	<u>.09</u>		<u>65</u>	<u>4</u>		<u>40</u>	<u>335</u>		
		<u>+42.763</u>									
1			<u>.09</u>						<u>335</u>		
2			<u>.09</u>						<u>335</u>		
3			<u>.09</u>						<u>335</u>		
4			<u>.08</u>						<u>334</u>		
5			<u>.08</u>						<u>334</u>		
6			<u>.09</u>						<u>334</u>		
7			<u>.10</u>						<u>334</u>		
8			<u>.10</u>						<u>333</u>		
9			<u>.10</u>						<u>333</u>		
10			<u>.09</u>						<u>333</u>		
11			<u>.09</u>						<u>334</u>		
12			<u>.08</u>						<u>334</u>		



MOISTURE DETERMINATION

COMPANY NAME:	MT Refining Co.	RUN #	1
PLANT LOCATION:	Great Falls	TEST DATE:	10/08/08
SOURCE TESTED:	#1810	Start Time:	
Weighed By:	JWZ	Balance Level:	☒
		Balance Zeroed:	☒
		End Time:	

Weight (grams)

Impinger #1

Final Weight 708
Initial Weight 643
Weight Gain 65 ✓

Impinger #2

Final Weight 649
Initial Weight 607
Weight Gain 42 ✓

Impinger #3

Final Weight 537
Initial Weight 532
Weight Gain 5 ✓

Impinger #4 (if applicable)

Final Weight _____
Initial Weight _____
Weight Gain _____

Silica Gel Impinger

Final Weight 804
Initial Weight 786
Weight Gain 18 ✓

Total Mass of Moisture Captured: 130 ✓ grams

Notes:

EPA Methods #1-4
Field Data & Calculations
Gas Flow/Moisture

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Hydrogen Plant Reformer Heater H1810

Test #: 2-GF/H₂O
Time: 08:52-09:52
Date: 10/08/08

Sample Point #	Clock Time (min.)	Meter Reading (cu.ft.)	Delta P ("H ₂ O)	Delta H ("H ₂ O)	Meter Temp. Deg. F	Stack Temp. Deg. F	SQRT Delta P
1	5	30.150	0.08	2.0	65	334	0.283
2	10		0.08	2.0	65	334	0.283
3	15		0.08	2.0	65	334	0.283
4	20		0.08	2.0	64	334	0.283
5	25		0.09	2.0	64	335	0.300
6	30		0.09	2.0	64	335	0.300
7	35		0.09	2.0	64	335	0.300
8	40		0.10	2.0	65	334	0.316
9	45		0.10	2.0	65	333	0.316
10	50		0.09	2.0	65	333	0.300
11	55		0.09	2.0	66	333	0.300
12	60		0.08	2.0	66	334	0.283
1		73.698	0.08			334	0.283
2			0.08			334	0.283
3			0.08			334	0.283
4			0.09			333	0.300
5			0.09			333	0.300
6			0.09			333	0.300
7			0.09			333	0.300
8			0.10			334	0.316
9			0.10			334	0.316
10			0.10			335	0.316
11			0.09			335	0.300
12			0.09			335	0.300

Client: Montana Refining Company, Inc.
Source: Hydrogen Plant Reformer Heater H1810

Test #: 2-GF/H2O
Date: 10/08/08

FIELD DATA INPUT: (CONTINUED)

Barometric Pressure (Pb)	26.30 in. Hg	<u>Orsat</u>	
Static Pressure	0.02 in H ₂ O	%CO ₂ Average	13.1 %
Meter Cal. Factor	1.01 Y	%O ₂ Average	5.3 %
Pitot Factor (cp)	0.84		
Total Test Time	60 min	<u>Stack Dimensional Data:</u>	
Sample Time Interval	5 min	Circular	
Meter Volume (Vm)	43.548 dcf	Diameter	2.917 ft
Water Volume	138 ml	Rectangular	
		Width	0.000 ft
		Length	0.000 ft

FIELD DATA AVERAGES:

Average Delta H	2.0 in. H ₂ O	Average SQRT Dp	0.298 in. H ₂ O
Average Meter		Average Stack	
Temperature (Tm)	65 deg F	Temperature (Ts)	334 deg F
Temperature (Tm)	525 deg A (R)	Temperature (Ts)	794 deg A (R)
Pressure Meter (Pm)	26.447 in. Hg	Pressure Stack (Ps)	26.301 in. Hg
		Moisture (Bws)	0.1424

CALCULATIONS:

Standard Meter		<u>Stack Gas:</u>	
Volume, Vm(std)	39.107 dscf	Velocity (Vs)	22.00 fps
Actual Meter		Volume (actual conditions)	8,821.6 awcfm
Volume, Vm(actual)	77.996 awcf		7,565.4 adcfm
Volume Water		Volume (std. Conditions)	309,400.3 wscf/hr
Vapor, Vw(std)	6.496 scf	(@ 68 deg F & 29.9 "Hg)	5,156.7 wscfm
Percent Moisture	14.24 %		265,341.7 dscf/hr
<u>Gas Density:</u>			4,422.4 dscfm
Dry (Md)	30.31 lb/lb-mole		
Wet (Ms)	28.56 lb/lb-mole		
Stack Area	6.683 sq.ft.		

PARTICULATE FIELD DATA

COMPANY NAME: MT Refining Co. RUN #: 2
 PLANT LOCATION: Great Falls DATE: 10/03/08
 SOURCE TESTED: H1810 START TIME: 852
 METER BOX OPERATOR: JW TECHNICIANS: DW END TIME: 952

EQUIPMENT / IDENTIFICATION CHECKS:

☒ PITOTS, PRE-TEST 120 PITOT
☒ PITOTS, POST-TEST 38 METER BOX
☒ ORSAT SAMPLING SYSTEM 1.01 Y FACTOR
☒ TEDLAR BAG 15 PRE 15 POST
☒ THERMOCOUPLE @ °F 200 PRE 200 POST
26.30 BAROMETRIC PRESSURE ("Hg) +0.02 STATIC PRESSURE ("H2O)
 NOZZLE # C60 TEST TIME
 NOZZLE DIA. M T/C READOUT
 TRAIN LEAK TEST VACUUM ("Hg)
 TRAIN LEAK TEST (ft3/min)
35" STACK DIMENSIONS

Sample Point	Time (min)	Dry Gas Meter Reading (ft³)	Pitot Reading ΔP ("H₂O)	Meter ΔH	Meter Temp. Tm (°F)	Pump Vacuum (Hg)	Filter Box (°F)	Imp. Exit (°F)	Stack Temp. (°F)	% CO2	% O2
		<u>30.150</u>									
1	5		<u>.08</u>	<u>2</u>	<u>65</u>	<u>4</u>	<u>—</u>	<u>41</u>	<u>334</u>		
2	10		<u>.08</u>		<u>65</u>	<u>4</u>		<u>41</u>	<u>334</u>		
3	15		<u>.08</u>		<u>65</u>	<u>4</u>		<u>41</u>	<u>334</u>		
4	20		<u>.08</u>		<u>64</u>	<u>4</u>		<u>41</u>	<u>334</u>		
5	25		<u>.09</u>		<u>64</u>	<u>4</u>		<u>42</u>	<u>335</u>		
6	30		<u>.09</u>		<u>64</u>	<u>4</u>		<u>42</u>	<u>335</u>		
7	35		<u>.09</u>		<u>64</u>	<u>4</u>		<u>42</u>	<u>335</u>		
8	40		<u>.10</u>		<u>65</u>	<u>4</u>		<u>42</u>	<u>334</u>		
9	45		<u>.10</u>		<u>65</u>	<u>4</u>		<u>41</u>	<u>333</u>		
10	50		<u>.09</u>		<u>65</u>	<u>4</u>		<u>41</u>	<u>333</u>		
11	55		<u>.09</u>		<u>66</u>	<u>4</u>		<u>41</u>	<u>333</u>		
12	60	<u>73.698</u>	<u>.08</u>		<u>66</u>	<u>4</u>		<u>41</u>	<u>334</u>		
		<u>+43.548</u>									
		<u>✓</u>									
1			<u>.08</u>						<u>334</u>		
2			<u>.08</u>						<u>334</u>		
3			<u>.08</u>						<u>334</u>		
4			<u>.09</u>						<u>333</u>		
5			<u>.09</u>						<u>333</u>		
6			<u>.09</u>						<u>333</u>		
7			<u>.09</u>						<u>333</u>		
8			<u>.10</u>						<u>334</u>		
9			<u>.10</u>						<u>334</u>		
10			<u>.10</u>						<u>335</u>		
11			<u>.09</u>						<u>335</u>		
12			<u>.09</u>						<u>335</u>		



MOISTURE DETERMINATION

COMPANY NAME:	MT Refining Co.	RUN #	2
PLANT LOCATION:	Great Falls	TEST DATE:	10/02/08
SOURCE TESTED:	H1810	Start Time:	
Weighed By:	JW	Balance Level:	☒
		Balance Zeroed:	☒
		End Time:	

Weight (grams)

Impinger #1

Final Weight 214
Initial Weight 647
Weight Gain 62 ✓

Impinger #2

Final Weight 673
Initial Weight 633
Weight Gain 40 ✓

Impinger #3

Final Weight 511
Initial Weight 503
Weight Gain 8 ✓

Impinger #4 (if applicable)

Final Weight _____
Initial Weight _____
Weight Gain _____

Silica Gel Impinger

Final Weight 821
Initial Weight 798
Weight Gain 23 ✓

Total Mass of Moisture Captured: 138 ✓ grams

Notes:

EPA Methods #1-4
Field Data & Calculations
Gas Flow/Moisture

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Hydrogen Plant Reformer Heater H1810

Test #: 3-GF/H₂O
Time: 09:59-10:59
Date: 10/08/08

Sample Point #	Clock Time (min.)	Meter Reading (cu.ft.)	Delta P ("H ₂ O)	Delta H ("H ₂ O)	Meter Temp. Deg. F	Stack Temp. Deg. F	SQRT Delta P
1	5	78.530	0.08	2.0	65	334	0.283
2	10		0.08	2.0	65	334	0.283
3	15		0.09	2.0	65	334	0.300
4	20		0.09	2.0	64	335	0.300
5	25		0.09	2.0	64	335	0.300
6	30		0.08	2.0	64	335	0.283
7	35		0.08	2.0	64	335	0.283
8	40		0.08	2.0	64	334	0.283
9	45		0.10	2.0	63	334	0.316
10	50		0.10	2.0	63	335	0.316
11	55		0.10	2.0	63	336	0.316
12	60		0.09	2.0	63	336	0.300
1		121.183	0.09			335	0.300
2			0.08			335	0.283
3			0.08			335	0.283
4			0.09			334	0.300
5			0.09			334	0.300
6			0.10			334	0.316
7			0.10			334	0.316
8			0.10			334	0.316
9			0.09			336	0.300
10			0.09			336	0.300
11			0.09			334	0.300
12			0.08			334	0.283

Client: Montana Refining Company, Inc.
Source: Hydrogen Plant Reformer Heater H1810

Test #: 3-GF/H2O
Date: 10/08/08

FIELD DATA INPUT: (CONTINUED)

Barometric Pressure (Pb)	26.30 in. Hg	<u>Orsat</u>	
Static Pressure	0.02 in H ₂ O	%CO ₂ Average	13.2 %
Meter Cal. Factor	1.01 Y	%O ₂ Average	5.2 %
Pitot Factor (cp)	0.84		
Total Test Time	60 min	<u>Stack Dimensional Data:</u>	
Sample Time Interval	5 min	Circular	
Meter Volume (Vm)	42.653 dcf	Diameter	2.917 ft
Water Volume	136 ml	Rectangular	
		Width	0.000 ft
		Length	0.000 ft

FIELD DATA AVERAGES:

Average Delta H	2.0 in. H ₂ O	Average SQRT Dp	0.298 in. H ₂ O
Average Meter		Average Stack	
Temperature (Tm)	64 deg F	Temperature (Ts)	335 deg F
Temperature (Tm)	524 deg A (R)	Temperature (Ts)	795 deg A (R)
Pressure Meter (Pm)	26.447 in. Hg	Pressure Stack (Ps)	26.301 in. Hg
		Moisture (Bws)	0.1430

CALCULATIONS:

Standard Meter		<u>Stack Gas:</u>	
Volume, Vm(std)	38.376 dscf	Velocity (Vs)	22.02 fps
Actual Meter		Volume (actual conditions)	8,829.6 awcfm
Volume, Vm(actual)	76.688 awcf		7,567.0 adcfm
Volume Water		Volume (std. Conditions)	309,292.0 wscf/hr
Vapor, Vw(std)	6.402 scf	(@ 68 deg F & 29.9 "Hg)	5,154.9 wscfm
Percent Moisture	14.30 %		265,063.2 dscf/hr
<u>Gas Density:</u>			4,417.7 dscfm
Dry (Md)	30.32 lb/lb-mole		
Wet (Ms)	28.56 lb/lb-mole		
Stack Area	6.683 sq.ft.		

PARTICULATE FIELD DATA

COMPANY NAME: MT Refining Co. RUN #: 3
 PLANT LOCATION: Great Falls DATE: 10/09/08
 SOURCE TESTED: H1810 START TIME: 959
 METER BOX OPERATOR: JW TECHNICIANS: DW END TIME: 1039

EQUIPMENT / IDENTIFICATION CHECKS:

☒ PITOTS, PRE-TEST 120 PITOT — NOZZLE # 60 TEST TIME
☒ PITOTS, POST-TEST 88 METER BOX — NOZZLE DIA.
☒ ORSAT SAMPLING SYSTEM 1.01 Y FACTOR — T/C READOUT
☒ TEDLAR BAG 15 PRE 13 POST M
☒ THERMOCOUPLE @ °F 000 PRE 000 POST TRAIN LEAK TEST VACUUM ("Hg)
26.30 BAROMETRIC PRESSURE ("Hg) +10.2 STATIC PRESSURE ("H2O) 35" STACK DIMENSIONS

Sample Point	Time (min)	Dry Gas Meter Reading (ft³)	Pitot Reading ΔP ("H₂O)	Meter ΔH	Meter Temp. Tm (°F)	Pump Vacuum (Hg)	Filter Box (°F)	Imp. Exit (°F)	Stack Temp. (°F)	% CO2	% O2
		<u>78.530</u>									
1	5		<u>.08</u>	<u>2</u>	<u>65</u>	<u>4</u>	<u>—</u>	<u>43</u>	<u>334</u>		
2	10		<u>.08</u>		<u>65</u>	<u>4</u>		<u>43</u>	<u>334</u>		
3	15		<u>.09</u>		<u>65</u>	<u>4</u>		<u>43</u>	<u>334</u>		
4	20		<u>.09</u>		<u>64</u>	<u>4</u>		<u>44</u>	<u>335</u>		
5	25		<u>.09</u>		<u>64</u>	<u>4</u>		<u>44</u>	<u>335</u>		
6	30		<u>.08</u>		<u>64</u>	<u>4</u>		<u>44</u>	<u>335</u>		
7	35		<u>.08</u>		<u>64</u>	<u>4</u>		<u>44</u>	<u>335</u>		
8	40		<u>.08</u>		<u>64</u>	<u>4</u>		<u>45</u>	<u>334</u>		
9	45		<u>.10</u>		<u>63</u>	<u>4</u>		<u>45</u>	<u>334</u>		
10	50		<u>.10</u>		<u>63</u>	<u>4</u>		<u>45</u>	<u>335</u>		
11	55		<u>.10</u>		<u>63</u>	<u>4</u>		<u>44</u>	<u>336</u>		
12	60	<u>121.183</u>	<u>.09</u>		<u>63</u>	<u>4</u>		<u>44</u>	<u>336</u>		
		<u>+42.653</u>									
1			<u>.09</u>						<u>335</u>		
2			<u>.08</u>						<u>335</u>		
3			<u>.08</u>						<u>335</u>		
4			<u>.09</u>						<u>334</u>		
5			<u>.09</u>						<u>334</u>		
6			<u>.10</u>						<u>334</u>		
7			<u>.10</u>						<u>334</u>		
8			<u>.10</u>						<u>336</u>		
9			<u>.09</u>						<u>336</u>		
10			<u>.09</u>						<u>334</u>		
11			<u>.09</u>						<u>334</u>		
12			<u>.08</u>						<u>334</u>		



MOISTURE DETERMINATION

COMPANY NAME:	<u>MT Refining Co.</u>	RUN #	<u>3</u>
PLANT LOCATION:	<u>Great Falls</u>	TEST DATE:	<u>10/08/08</u>
SOURCE TESTED:	<u>H1310</u>	Start Time:	
Weighed By:	<u>JW</u>	Balance Level:	<u>✓</u>
		Balance Zeroed:	<u>✓</u>
		End Time:	

Weight (grams)

Impinger #1

Final Weight 711
Initial Weight 648
Weight Gain 63 ✓

Impinger #2

Final Weight 682
Initial Weight 633
Weight Gain 49 ✓

Impinger #3

Final Weight 529
Initial Weight 526
Weight Gain 3 ✓

Impinger #4 (if applicable)

Final Weight _____
Initial Weight _____
Weight Gain _____

Silica Gel Impinger

Final Weight 822
Initial Weight 801
Weight Gain 21 ✓

Total Mass of Moisture Captured: 136 ✓ grams

Notes:

Compliance Data
EPA Methods #7E & 10

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Diesel Hydrotreater Heater (HTU) H1701

Run #: 4-NO_x/CO
Time: 11:35-12:34
Date: 10/08/08

#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry	#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry
1	11:35	42.9	1.7	31	12:05	44.6	1.5
2	11:36	41.9	1.8	32	12:06	45.2	1.6
3	11:37	41.6	1.7	33	12:07	39.3	1.6
4	11:38	41.5	1.6	34	12:08	37.7	1.8
5	11:39	40.4	1.9	35	12:09	42.7	1.5
6	11:40	40.4	1.5	36	12:10	45.9	1.4
7	11:41	44.1	1.5	37	12:11	45.7	1.5
8	11:42	45.8	1.8	38	12:12	45.1	1.6
9	11:43	44.1	1.6	39	12:13	44.8	1.6
10	11:44	25.6	1.8	40	12:14	42.9	1.6
11	11:45	40.6	1.5	41	12:15	42.3	1.7
12	11:46	43.1	1.6	42	12:16	43.1	1.7
13	11:47	43.3	1.8	43	12:17	43.1	1.6
14	11:48	42.7	1.7	44	12:18	43.7	1.7
15	11:49	45.1	1.6	45	12:19	42.5	1.7
16	11:50	44.2	1.6	46	12:20	42.4	1.7
17	11:51	43.6	1.5	47	12:21	43.7	1.7
18	11:52	43.6	1.7	48	12:22	45.0	1.7
19	11:53	44.3	1.7	49	12:23	44.0	1.7
20	11:54	44.5	1.5	50	12:24	44.1	1.7
21	11:55	43.9	1.7	51	12:25	44.1	1.7
22	11:56	43.8	1.5	52	12:26	45.7	1.8
23	11:57	43.3	1.9	53	12:27	44.4	1.8
24	11:58	43.5	1.5	54	12:28	44.2	1.8
25	11:59	45.5	1.8	55	12:29	45.4	1.8
26	12:00	45.3	1.9	56	12:30	44.3	1.9
27	12:01	44.4	1.5	57	12:31	43.5	1.9
28	12:02	44.7	1.5	58	12:32	45.0	2.0
29	12:03	44.0	1.5	59	12:33	44.5	2.0
30	12:04	42.5	1.5	60	12:34	45.7	2.0
				Averages:		43.31	1.68

Client: Montana Refining Company, Inc.
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 4-NOx/CO
Date: 10/8/2008

Instrument Calibration Checks

NO_x Instrument

Calibration Span, CS: 100.7 ppm v/v Dry

NO_x Calibration Error Tests

Time	Tank Value C _v	Instrument Resp., C _{Dir}	System CE, SCE ($< 2\%$ of span)
11:07	0.0	0.1	0.1
11:09	50.2	50.0	-0.2
11:13	100.7	100.4	-0.3

Initial System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _i ($< 5\%$ of span)
11:19	0.0	0.2	0.2
11:17	50.2	49.9	-0.3

Post System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _f ($< 5\%$ of span)	Drift, D (SB _f - SB _i) ($< 3\%$ of span)
12:36	0.0	0.2	0.2	0.0
12:38	50.2	49.9	-0.3	0.0

CO Instrument

Calibration Span, CS: 93.5 ppm v/v Dry

CO Calibration Error Tests

Time	Tank Value C _v	Instrument Resp., C _{Dir}	System CE, SCE ($< 2\%$ of span)
11:07	0	0.2	0.2
11:10	43.8	43.5	-0.3
11:14	93.5	93.1	-0.4

Initial System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _i ($< 5\%$ of span)
11:23	0	0.3	0.3
11:21	43.8	43.5	-0.3

Post System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _f ($< 5\%$ of span)	Drift, D (SB _f - SB _i) ($< 3\%$ of span)
12:36	0	0.3	0.3	0.0
12:40	43.8	43.5	-0.3	0.0

Instrument Response Times:

	Zero	High
NO _x	27	24 seconds
CO	25	27 seconds

Client: Montana Refining Company, Inc.
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 4-NOx/CO
Date: 10/8/2008

Data From Concurrent Run:

Ps	26.298 IN Hg
Gas Flow	5,518.9 adcfm
Avg. Temp	619 Deg. F 1079 Deg. A (R)
NOx Molecular Wt.	46
CO Molecular Wt.	28
Oxygen	2.9 % v/v dry
cu.ft/lb-mole	
Act Conditions	895.756 ft ³ /#mole
Fd Factor (O ₂ Basis)	8,714 dscf/MMBtu

Calculations:

Averages:	
NO _x	43.31 ppm v/v Dry
CO	1.68 ppm v/v Dry
Calibration Corrected Values:	
NO _x	43.5 ppm v/v Dry
CO	1.4 ppm v/v Dry
Mass Flow:	
NO _x	0.74 PPH
CO	0.01 PPH
NO _x	0.053 lb/MMBTU
CO	0.001 lb/MMBTU

Compliance Data
EPA Methods #7E & 10

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Diesel Hydrotreater Heater (HTU) H1701

Run #: 5-NO_x/CO
Time: 12:42-13:41
Date: 10/08/08

#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry	#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry
1	12:42	43.7	1.8	31	13:12	43.4	1.5
2	12:43	45.1	1.8	32	13:13	43.5	1.5
3	12:44	44.1	1.9	33	13:14	43.7	1.3
4	12:45	43.9	2.1	34	13:15	44.2	1.4
5	12:46	45.1	1.9	35	13:16	45.7	1.7
6	12:47	45.8	1.8	36	13:17	44.1	1.6
7	12:48	44.9	1.8	37	13:18	43.9	1.4
8	12:49	45.0	1.8	38	13:19	46.0	1.4
9	12:50	44.9	1.8	39	13:20	44.1	1.4
10	12:51	46.3	2.0	40	13:21	42.9	1.5
11	12:52	45.2	1.7	41	13:22	43.7	1.5
12	12:53	44.7	1.8	42	13:23	44.3	1.6
13	12:54	40.9	1.8	43	13:24	45.4	1.5
14	12:55	39.0	2.0	44	13:25	46.5	1.4
15	12:56	40.4	1.7	45	13:26	43.9	1.4
16	12:57	45.9	2.1	46	13:27	42.8	1.6
17	12:58	45.7	1.9	47	13:28	44.7	1.6
18	12:59	45.0	2.0	48	13:29	44.0	1.4
19	13:00	45.2	1.7	49	13:30	44.1	1.4
20	13:01	44.1	1.8	50	13:31	44.3	1.4
21	13:02	43.8	2.0	51	13:32	44.1	1.5
22	13:03	45.0	2.1	52	13:33	44.5	1.5
23	13:04	45.0	1.7	53	13:34	44.8	1.7
24	13:05	45.9	1.7	54	13:35	43.7	1.4
25	13:06	45.1	1.9	55	13:36	43.6	1.4
26	13:07	42.9	1.6	56	13:37	43.4	1.5
27	13:08	43.1	1.5	57	13:38	44.3	1.5
28	13:09	45.7	1.6	58	13:39	45.3	1.6
29	13:10	44.2	1.5	59	13:40	45.7	1.6
30	13:11	43.1	1.6	60	13:41	45.8	1.6
				Averages:		44.32	1.65

Client: Montana Refining Company, Inc.
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 5-NOx/CO
Date: 10/8/2008

Instrument Calibration Checks

NO_x Instrument

Calibration Span, CS: 100.7 ppm v/v Dry

NO_x Calibration Error Tests

Time	Tank Value C _v	Instrument Resp., C _{Dir}	System CE, SCE ($< 2\%$ of span)
11:07	0.0	0.1	0.1
11:09	50.2	50.0	-0.2
11:13	100.7	100.4	-0.3

Initial System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _i ($< 5\%$ of span)
12:36	0.0	0.2	0.2
12:38	50.2	49.9	-0.3

Post System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _f ($< 5\%$ of span)	Drift, D (SB _f - SB _i) ($< 3\%$ of span)
13:43	0.0	0.2	0.2	0.0
13:45	50.2	49.9	-0.3	0.0

CO Instrument

Calibration Span, CS: 93.5 ppm v/v Dry

CO Calibration Error Tests

Time	Tank Value C _v	Instrument Resp., C _{Dir}	System CE, SCE ($< 2\%$ of span)
11:07	0	0.2	0.2
11:10	43.8	43.5	-0.3
11:14	93.5	93.1	-0.4

Initial System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _i ($< 5\%$ of span)
12:36	0	0.3	0.3
12:40	43.8	43.5	-0.3

Post System Bias Check

Time	Tank Value C _v	Instrument Resp., C _S	System Bias, SB _f ($< 5\%$ of span)	Drift, D (SB _f - SB _i) ($< 3\%$ of span)
13:43	0	0.2	0.2	-0.1
13:47	43.8	43.5	-0.3	0.0

Instrument Response Times:

	Zero	High
NO _x	27	24 seconds
CO	25	27 seconds

Client: Montana Refining Company, Inc.
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 5-NOx/CO
Date: 10/8/2008

Data From Concurrent Run:

Ps	26.298 IN Hg
Gas Flow	5,645.5 adcfm
Avg. Temp	620 Deg. F 1080 Deg. A (R)
NOx Molecular Wt.	46
CO Molecular Wt.	28
Oxygen	2.8 % v/v dry
cu.ft/lb-mole	
Act Conditions	896.586 ft ³ /#mole
Fd Factor (O ₂ Basis)	8,714 dscf/MMBtu

Calculations:

Averages:

NO _x	44.32 ppm v/v Dry
CO	1.65 ppm v/v Dry

Calibration Corrected Values:

NO _x	44.6 ppm v/v Dry
CO	1.4 ppm v/v Dry

Mass Flow:

NO _x	0.78 PPH
CO	0.01 PPH

NO _x	0.054 lb/MMBTU
CO	0.001 lb/MMBTU

Compliance Data
EPA Methods #7E & 10

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Diesel Hydrotreater Heater (HTU) H1701

Run #: 6-NO_x/CO
Time: 13:49-14:48
Date: 10/08/08

#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry	#	Time	NO _x - ppm v/v Dry	CO - ppm v/v Dry
1	13:49	42.8	1.7	31	14:19	43.8	2.0
2	13:50	44.4	1.7	32	14:20	43.4	2.0
3	13:51	45.0	1.8	33	14:21	43.5	2.1
4	13:52	44.0	1.5	34	14:22	43.6	1.7
5	13:53	42.2	1.7	35	14:23	43.4	1.8
6	13:54	42.3	1.7	36	14:24	44.5	1.8
7	13:55	44.2	1.6	37	14:25	45.6	2.0
8	13:56	42.6	1.6	38	14:26	45.2	1.9
9	13:57	44.5	1.7	39	14:27	44.4	1.8
10	13:58	45.5	1.9	40	14:28	43.0	1.8
11	13:59	45.1	1.8	41	14:29	42.7	2.0
12	14:00	45.1	1.9	42	14:30	43.7	1.8
13	14:01	43.3	1.8	43	14:31	44.2	2.0
14	14:02	42.4	1.8	44	14:32	44.1	1.9
15	14:03	43.3	1.9	45	14:33	42.5	1.7
16	14:04	44.3	1.9	46	14:34	43.5	1.9
17	14:05	45.2	1.8	47	14:35	45.9	2.0
18	14:06	43.5	1.7	48	14:36	43.6	1.9
19	14:07	42.8	1.7	49	14:37	42.4	1.9
20	14:08	43.5	1.6	50	14:38	43.9	1.8
21	14:09	43.3	1.7	51	14:39	45.5	1.7
22	14:10	45.9	1.9	52	14:40	42.9	1.7
23	14:11	44.1	1.6	53	14:41	42.8	1.8
24	14:12	43.4	1.8	54	14:42	44.2	2.1
25	14:13	44.1	1.8	55	14:43	43.7	1.7
26	14:14	44.3	1.6	56	14:44	43.8	1.8
27	14:15	45.6	1.6	57	14:45	44.1	1.9
28	14:16	43.8	1.7	58	14:46	42.6	1.7
29	14:17	43.5	1.8	59	14:47	43.1	1.8
30	14:18	43.0	2.0	60	14:48	42.7	1.7
				Averages:		43.82	1.80

Client: Montana Refining Company, Inc.
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 6-NOx/CO
Date: 10/8/2008

Instrument Calibration Checks

NO_x Instrument

Calibration Span, CS: 100.7 ppm v/v Dry

NO_x Calibration Error Tests

Time	Tank Value C _v	Instrument Resp., C _{Dir}	System CE, SCE ($< 2\%$ of span)
11:07	0.0	0.1	0.1
11:09	50.2	50.0	-0.2
11:13	100.7	100.4	-0.3

Initial System Bias Check

Time	Tank Value C _v	Instrument Resp., C _s	System Bias, SB _i ($< 5\%$ of span)
13:43	0.0	0.2	0.2
13:45	50.2	49.9	-0.3

Post System Bias Check

Time	Tank Value C _v	Instrument Resp., C _s	System Bias, SB _f ($< 5\%$ of span)	Drift, D (SB _f - SB _i) ($< 3\%$ of span)
14:50	0.0	0.3	0.3	0.1
14:52	50.2	50.0	-0.2	0.1

CO Instrument

Calibration Span, CS: 93.5 ppm v/v Dry

CO Calibration Error Tests

Time	Tank Value C _v	Instrument Resp., C _{Dir}	System CE, SCE ($< 2\%$ of span)
11:07	0	0.2	0.2
11:10	43.8	43.5	-0.3
11:14	93.5	93.1	-0.4

Initial System Bias Check

Time	Tank Value C _v	Instrument Resp., C _s	System Bias, SB _i ($< 5\%$ of span)
13:43	0	0.2	0.2
13:47	43.8	43.5	-0.3

Post System Bias Check

Time	Tank Value C _v	Instrument Resp., C _s	System Bias, SB _f ($< 5\%$ of span)	Drift, D (SB _f - SB _i) ($< 3\%$ of span)
14:50	0	0.2	0.2	0.0
14:54	43.8	43.5	-0.3	0.0

Instrument Response Times:

	Zero	High
NO _x	27	24 seconds
CO	25	27 seconds

Client: Montana Refining Company, Inc.
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 6-NOx/CO
Date: 10/8/2008

Data From Concurrent Run:

Ps	26.298 IN Hg
Gas Flow	5,658.9 adcfm
Avg. Temp	620 Deg. F 1080 Deg. A (R)
NOx Molecular Wt.	46
CO Molecular Wt.	28
Oxygen	2.8 % v/v dry
cu.ft/lb-mole	
Act Conditions	896.586 ft ³ /#mole
Fd Factor (O ₂ Basis)	8,714 dscf/MMBtu

Calculations:

Averages:

NO _x	43.82 ppm v/v Dry
CO	1.80 ppm v/v Dry

Calibration Corrected Values:

NO _x	44.0 ppm v/v Dry
CO	1.6 ppm v/v Dry

Mass Flow:

NO _x	0.77 PPH
CO	0.02 PPH

NO _x	0.053 lb/MMBTU
CO	0.001 lb/MMBTU

EPA Methods #1-4
Field Data & Calculations
Gas Flow/Moisture

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 4-GF/H₂O
Time: 11:35-12:35
Date: 10/08/08

Sample Point #	Clock Time (min.)	Meter Reading (cu.ft.)	Delta P ("H ₂ O)	Delta H ("H ₂ O)	Meter Temp. Deg. F	Stack Temp. Deg. F	SQRT Delta P
1	5	125.000	0.04	2.0	70	619	0.200
2	10		0.04	2.0	70	619	0.200
3	15		0.03	2.0	70	619	0.173
4	20		0.04	2.0	70	618	0.200
5	25		0.04	2.0	71	618	0.200
6	30		0.04	2.0	71	618	0.200
7	35		0.04	2.0	71	618	0.200
8	40		0.03	2.0	71	619	0.173
9	45		0.04	2.0	70	619	0.200
10	50		0.04	2.0	70	620	0.200
11	55		0.04	2.0	71	620	0.200
12	60		0.04	2.0	71	620	0.200
1		167.758	0.04			620	0.200
2			0.04			620	0.200
3			0.04			620	0.200
4			0.03			621	0.173
5			0.03			621	0.173
6			0.04			621	0.200
7			0.04			620	0.200
8			0.04			620	0.200
9			0.04			619	0.200
10			0.04			619	0.200
11			0.04			619	0.200
12			0.04			618	0.200

Client: Montana Refining Company, Inc.
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 4-GF/H2O
Date: 10/08/08

FIELD DATA INPUT: (CONTINUED)

Barometric Pressure (Pb) 26.30 in. Hg
Static Pressure -0.03 in H₂O
Meter Cal. Factor 1.01 Y
Pitot Factor (cp) 0.84

Orsat
%CO₂ Average 9.4 %
%O₂ Average 2.9 %

Total Test Time 60 min
Sample Time Interval 5 min
Meter Volume (Vm) 42.758 dcf
Water Volume 70 ml

Stack Dimensional Data:

Circular
Diameter 2.750 ft

Rectangular
Width 0.000 ft
Length 0.000 ft

FIELD DATA AVERAGES:

Average Delta H 2.0 in. H₂O

Average SQRT Dp 0.196 in. H₂O

Average Meter
Temperature (Tm) 71 deg F
Temperature (Tm) 531 deg A (R)

Average Stack
Temperature (Ts) 619 deg F
Temperature (Ts) 1079 deg A (R)

Pressure Meter (Pm) 26.447 in. Hg

Pressure Stack (Ps) 26.298 in. Hg

Moisture (Bws) 0.0799

CALCULATIONS:

Standard Meter
Volume, Vm(std) 37.963 dscf
Actual Meter
Volume, Vm(actual) 95.915 awcf
Volume Water
Vapor, Vw(std) 3.295 scf

Stack Gas:

Velocity (Vs) 16.83 fps

Volume (actual conditions) 5,998.2 awcfm
5,518.9 adcfm

Percent Moisture 7.99 %

Volume (std. Conditions)
(@ 68 deg F & 29.9 "Hg) 154,791.3 wscf/hr
2,579.9 wscfm
142,423.5 dscf/hr
2,373.7 dscfm

Gas Density:

Dry (Md) 29.62 lb/lb-mole
Wet (Ms) 28.69 lb/lb-mole

Stack Area 5.940 sq.ft.

PARTICULATE FIELD DATA

COMPANY NAME: MRC RUN #: 4
 PLANT LOCATION: Great Falls DATE: 10/08/08
 SOURCE TESTED: H1201 START TIME: 1135
 METER BOX OPERATOR: DW TECHNICIANS: DW JA END TIME: 1235

EQUIPMENT / IDENTIFICATION CHECKS:

☒ PITOTS, PRE-TEST 170 PITOT
☒ PITOTS, POST-TEST SR METER BOX
☒ ORSAT SAMPLING SYSTEM 1.01 Y FACTOR
☒ TEDLAR BAG 15 PRE 15 POST
☒ THERMOCOUPLE @ °F 000 PRE 000 POST
26.30 BAROMETRIC PRESSURE ("Hg) -03 STATIC PRESSURE ("H2O) 33"
 NOZZLE # 60 TEST TIME
 NOZZLE DIA. M T/C READOUT
 TRAIN LEAK TEST VACUUM ("Hg)
 TRAIN LEAK TEST (ft3/min)
 STACK DIMENSIONS

Sample Point	Time (min)	Dry Gas Meter Reading (ft³)	Pitot Reading ΔP ("H₂O)	Meter ΔH	Meter Temp. Tm (°F)	Pump Vacuum (Hg)	Filter Box (°F)	Imp. Exit (°F)	Stack Temp. (°F)	% CO2	% O2
		<u>125.000</u>									
1	5		<u>.04</u>	<u>2</u>	<u>70</u>	<u>4</u>	<u>—</u>	<u>48</u>	<u>619</u>	<u>9.4</u>	<u>2.9</u>
2	10		<u>.04</u>		<u>70</u>	<u>4</u>		<u>48</u>	<u>619</u>		
3	15		<u>.03</u>		<u>70</u>	<u>4</u>		<u>48</u>	<u>619</u>		
4	20		<u>.04</u>		<u>70</u>	<u>4</u>		<u>47</u>	<u>618</u>		
5	25		<u>.04</u>		<u>71</u>	<u>4</u>		<u>47</u>	<u>618</u>		
6	30		<u>.04</u>		<u>71</u>	<u>4</u>		<u>47</u>	<u>618</u>		
7	35		<u>.04</u>		<u>71</u>	<u>4</u>		<u>46</u>	<u>618</u>		
8	40		<u>.03</u>		<u>71</u>	<u>4</u>		<u>46</u>	<u>619</u>		
9	45		<u>.04</u>		<u>70</u>	<u>4</u>		<u>46</u>	<u>619</u>		
10	50		<u>.04</u>		<u>70</u>	<u>4</u>		<u>46</u>	<u>620</u>		
11	55		<u>.04</u>		<u>71</u>	<u>4</u>		<u>47</u>	<u>620</u>		
12	60	<u>167.758</u>	<u>.04</u>		<u>71</u>	<u>4</u>		<u>47</u>	<u>620</u>		
		<u>+42.758</u>	<u>.04</u>		<u>71</u>	<u>4</u>		<u>47</u>	<u>620</u>		
		<u>✓</u>									
1			<u>.04</u>						<u>620</u>		
2			<u>.04</u>						<u>620</u>		
3			<u>.04</u>						<u>621</u>		
4			<u>.03</u>						<u>621</u>		
5			<u>.03</u>						<u>621</u>		
6			<u>.04</u>						<u>621</u>		
7			<u>.04</u>						<u>620</u>		
8			<u>.04</u>						<u>620</u>		
9			<u>.04</u>						<u>619</u>		
10			<u>.04</u>						<u>619</u>		
11			<u>.04</u>						<u>619</u>		
12			<u>.04</u>						<u>618</u>		



MOISTURE DETERMINATION

COMPANY NAME:	MRC	RUN #	4
PLANT LOCATION:	Great Falls	TEST DATE:	10/08/08
SOURCE TESTED:	H1201	Start Time:	
Weighed By:	JW	Balance Level:	☒
		Balance Zeroed:	☒
		End Time:	

Weight (grams)

Impinger #1

Final Weight 657
Initial Weight 626
Weight Gain 31 ✓

Impinger #2

Final Weight 265
Initial Weight 243
Weight Gain 22 ✓

Impinger #3

Final Weight 518
Initial Weight 517
Weight Gain 1 ✓

Impinger #4 (if applicable)

Final Weight _____
Initial Weight _____
Weight Gain _____

Silica Gel Impinger

Final Weight 812
Initial Weight 796
Weight Gain 16 ✓

Total Mass of Moisture Captured: 20 ✓ grams

Notes:

EPA Methods #1-4
Field Data & Calculations
Gas Flow/Moisture

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 5-GF/H₂O
Time: 12:42-13:42
Date: 10/08/08

Sample Point #	Clock Time (min.)	Meter Reading (cu.ft.)	Delta P ("H ₂ O)	Delta H ("H ₂ O)	Meter Temp. Deg. F	Stack Temp. Deg. F	SQRT Delta P
1	5	172.010	0.04	2.0	71	620	0.200
2	10		0.04	2.0	71	620	0.200
3	15		0.04	2.0	71	620	0.200
4	20		0.04	2.0	71	621	0.200
5	25		0.04	2.0	72	621	0.200
6	30		0.04	2.0	72	621	0.200
7	35		0.04	2.0	72	621	0.200
8	40		0.04	2.0	72	621	0.200
9	45		0.03	2.0	72	620	0.173
10	50		0.04	2.0	72	620	0.200
11	55		0.04	2.0	72	620	0.200
12	60		0.04	2.0	72	620	0.200
1		215.431	0.04			619	0.200
2			0.04			619	0.200
3			0.04			619	0.200
4			0.04			619	0.200
5			0.04			620	0.200
6			0.04			620	0.200
7			0.04			620	0.200
8			0.04			620	0.200
9			0.04			620	0.200
10			0.04			621	0.200
11			0.04			621	0.200
12			0.04			621	0.200

Client: Montana Refining Company, Inc.
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 5-GF/H2O
Date: 10/08/08

FIELD DATA INPUT: (CONTINUED)

Barometric Pressure (Pb) 26.30 in. Hg
Static Pressure -0.03 in H₂O
Meter Cal. Factor 1.01 Y
Pitot Factor (cp) 0.84

Orsat
%CO₂ Average 9.5 %
%O₂ Average 2.8 %

Total Test Time 60 min
Sample Time Interval 5 min
Meter Volume (Vm) 43.421 dcf
Water Volume 63 ml

Stack Dimensional Data:
Circular
Diameter 2.750 ft
Rectangular
Width 0.000 ft
Length 0.000 ft

FIELD DATA AVERAGES:

Average Delta H 2.0 in. H₂O

Average SQRT Dp 0.199 in. H₂O

Average Meter
Temperature (Tm) 72 deg F
Temperature (Tm) 532 deg A (R)

Average Stack
Temperature (Ts) 620 deg F
Temperature (Ts) 1080 deg A (R)

Pressure Meter (Pm) 26.447 in. Hg

Pressure Stack (Ps) 26.298 in. Hg

Moisture (Bws) 0.0715

CALCULATIONS:

Standard Meter
Volume, Vm(std) 38.480 dscf
Actual Meter
Volume, Vm(actual) 96.428 awcf
Volume Water
Vapor, Vw(std) 2.965 scf

Stack Gas:
Velocity (Vs) 17.06 fps
Volume (actual conditions) 6,080.2 awcfm
5,645.5 adcfm
Volume (std. Conditions)
(@ 68 deg F & 29.9 "Hg) 156,761.4 wscf/hr
2,612.7 wscfm
145,553.0 dscf/hr
2,425.9 dscfm

Percent Moisture 7.15 %

Gas Density:
Dry (Md) 29.63 lb/lb-mole
Wet (Ms) 28.80 lb/lb-mole

Stack Area 5.940 sq.ft.

PARTICULATE FIELD DATA

COMPANY NAME: MRC RUN #: 3
 PLANT LOCATION: Great Falls DATE: 10/08/08
 SOURCE TESTED: H1201 START TIME: 1242
 METER BOX OPERATOR: JW TECHNICIANS: DW JA END TIME: 1342

EQUIPMENT / IDENTIFICATION CHECKS:

☒ PITOTS, PRE-TEST 170 PITOT
☒ PITOTS, POST-TEST 30 METER BOX
☒ ORSAT SAMPLING SYSTEM 1.01 Y FACTOR
☒ TEDLAR BAG 15 PRE 14 POST
☒ THERMOCOUPLE @ °F 000 PRE 000 POST
26.30 BAROMETRIC PRESSURE ("Hg) -0.03 STATIC PRESSURE ("H2O) 33" STACK DIMENSIONS
 NOZZLE # C60 TEST TIME
 NOZZLE DIA. M
 T/C READOUT
 TRAIN LEAK TEST VACUUM ("Hg)
 TRAIN LEAK TEST (ft3/min)
 TRAIN LEAK TEST (ft3/min)

Sample Point	Time (min)	Dry Gas Meter Reading (ft³)	Pitot Reading ΔP ("H₂O)	Meter ΔH	Meter Temp. Tm (°F)	Pump Vacuum (Hg)	Filter Box (°F)	Imp. Exit (°F)	Stack Temp. (°F)	% CO₂	% O₂
		<u>172.010</u>									
1	5		<u>.04</u>	<u>2</u>	<u>71</u>	<u>4</u>	<u>—</u>	<u>49</u>	<u>620</u>	<u>9.5</u>	<u>2.8</u>
2	10		<u>.04</u>		<u>71</u>	<u>4</u>		<u>49</u>	<u>620</u>		
3	15		<u>.04</u>		<u>71</u>	<u>4</u>		<u>49</u>	<u>620</u>		
4	20		<u>.04</u>		<u>71</u>	<u>4</u>		<u>49</u>	<u>621</u>		
5	25		<u>.04</u>		<u>72</u>	<u>4</u>		<u>49</u>	<u>621</u>		
6	30		<u>.04</u>		<u>72</u>	<u>4</u>		<u>49</u>	<u>621</u>		
7	35		<u>.04</u>		<u>72</u>	<u>4</u>		<u>50</u>	<u>621</u>		
8	40		<u>.04</u>		<u>72</u>	<u>4</u>		<u>50</u>	<u>621</u>		
9	45		<u>.03</u>		<u>72</u>	<u>4</u>		<u>50</u>	<u>620</u>		
10	50		<u>.04</u>		<u>72</u>	<u>4</u>		<u>51</u>	<u>620</u>		
11	55		<u>.04</u>		<u>72</u>	<u>4</u>		<u>51</u>	<u>620</u>		
12	60	<u>215.431</u>	<u>.04</u>		<u>72</u>	<u>4</u>		<u>51</u>	<u>620</u>		
		<u>+43.421</u>									
		<u>✓</u>									
1			<u>.04</u>						<u>619</u>		
2			<u>.04</u>						<u>619</u>		
3			<u>.04</u>						<u>619</u>		
4			<u>.04</u>						<u>619</u>		
5			<u>.04</u>						<u>620</u>		
6			<u>.04</u>						<u>620</u>		
7			<u>.04</u>						<u>620</u>		
8			<u>.04</u>						<u>620</u>		
9			<u>.04</u>						<u>620</u>		
10			<u>.04</u>						<u>621</u>		
11			<u>.04</u>						<u>621</u>		
12			<u>.04</u>						<u>621</u>		



MOISTURE DETERMINATION

COMPANY NAME:	<u>MRC</u>	RUN #	<u>3</u>
PLANT LOCATION:	<u>Great Falls</u>	TEST DATE:	<u>10/08/08</u>
SOURCE TESTED:	<u>H1201</u>	Start Time:	
Weighed By:	<u>JW</u>	Balance Level:	☒
		Balance Zeroed:	☒
		End Time:	

Weight (grams)

Impinger #1

Final Weight 634
Initial Weight 601
Weight Gain 33 ✓

Impinger #2

Final Weight 698
Initial Weight 683
Weight Gain 15 ✓

Impinger #3

Final Weight 516
Initial Weight 516
Weight Gain 0 ✓

Impinger #4 (if applicable)

Final Weight _____
Initial Weight _____
Weight Gain _____

Silica Gel Impinger

Final Weight 298
Initial Weight 283
Weight Gain 15 ✓

Total Mass of Moisture Captured: 63 ✓ grams

Notes:

EPA Methods #1-4
Field Data & Calculations
Gas Flow/Moisture

Client: Montana Refining Company, Inc.
Location: Great Falls, Montana
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 6-GF/H₂O
Time: 13:49-14:49
Date: 10/08/08

Sample Point #	Clock Time (min.)	Meter Reading (cu.ft.)	Delta P ("H ₂ O)	Delta H ("H ₂ O)	Meter Temp. Deg. F	Stack Temp. Deg. F	SQRT Delta P
1	5	220.000	0.04	2.0	72	621	0.200
2	10		0.04	2.0	72	621	0.200
3	15		0.04	2.0	72	621	0.200
4	20		0.04	2.0	72	621	0.200
5	25		0.04	2.0	71	620	0.200
6	30		0.04	2.0	71	620	0.200
7	35		0.04	2.0	71	620	0.200
8	40		0.04	2.0	71	620	0.200
9	45		0.04	2.0	70	619	0.200
10	50		0.04	2.0	70	619	0.200
11	55		0.04	2.0	70	619	0.200
12	60		0.04	2.0	70	619	0.200
1		263.340	0.04			620	0.200
2			0.04			620	0.200
3			0.04			620	0.200
4			0.04			621	0.200
5			0.04			621	0.200
6			0.04			621	0.200
7			0.04			621	0.200
8			0.04			621	0.200
9			0.04			620	0.200
10			0.04			620	0.200
11			0.04			620	0.200
12			0.04			620	0.200

Client: Montana Refining Company, Inc.
Source: Diesel Hydrotreater Heater (HTU) H1701

Test #: 6-GF/H2O
Date: 10/08/08

FIELD DATA INPUT: (CONTINUED)

Barometric Pressure (Pb)	26.30 in. Hg	<u>Orsat</u>	
Static Pressure	-0.03 in H ₂ O	%CO ₂ Average	9.5 %
Meter Cal. Factor	1.01 Y	%O ₂ Average	2.8 %
Pitot Factor (cp)	0.84		
Total Test Time	60 min	<u>Stack Dimensional Data:</u>	
Sample Time Interval	5 min	Circular	
Meter Volume (Vm)	43.340 dcf	Diameter	2.750 ft
Water Volume	66 ml	Rectangular	
		Width	0.000 ft
		Length	0.000 ft

FIELD DATA AVERAGES:

Average Delta H	2.0 in. H ₂ O	Average SQRT Dp	0.200 in. H ₂ O
Average Meter		Average Stack	
Temperature (Tm)	71 deg F	Temperature (Ts)	620 deg F
Temperature (Tm)	531 deg A (R)	Temperature (Ts)	1080 deg A (R)
Pressure Meter (Pm)	26.447 in. Hg	Pressure Stack (Ps)	26.298 in. Hg
		Moisture (Bws)	0.0747

CALCULATIONS:

Standard Meter		<u>Stack Gas:</u>	
Volume, Vm(std)	38.480 dscf	Velocity (Vs)	17.16 fps
Actual Meter			
Volume, Vm(actual)	96.763 awcf	Volume (actual conditions)	6,115.8 awcfm
Volume Water			5,658.9 adcfm
Vapor, Vw(std)	3.107 scf		
Percent Moisture	7.47 %	Volume (std. Conditions)	157,680.3 wscf/hr
		(@ 68 deg F & 29.9 "Hg)	2,628.0 wscfm
<u>Gas Density:</u>			145,901.6 dscf/hr
Dry (Md)	29.63 lb/lb-mole		2,431.7 dscfm
Wet (Ms)	28.76 lb/lb-mole		
Stack Area	5.940 sq.ft.		

PARTICULATE FIELD DATA

COMPANY NAME: MRG RUN #: 6
 PLANT LOCATION: Great Falls DATE: 10/08/08
 SOURCE TESTED: H 1201 START TIME: 1349
 METER BOX OPERATOR: JW TECHNICIANS: DW, JA END TIME: 1449

EQUIPMENT / IDENTIFICATION CHECKS:

☒ PITOTS, PRE-TEST 120 PITOT
☒ PITOTS, POST-TEST 38 METER BOX
☒ ORSAT SAMPLING SYSTEM 1.01 Y FACTOR
☒ TEDLAR BAG 15 PRE 15 POST
☒ THERMOCOUPLE @ °F 000 PRE 000 POST
26.30 BAROMETRIC PRESSURE ("Hg) -0.03 STATIC PRESSURE ("H2O) 331 STACK DIMENSIONS
 NOZZLE # 60 TEST TIME
 NOZZLE DIA. M
 T/C READOUT
 TRAIN LEAK TEST VACUUM ("Hg)
 TRAIN LEAK TEST (ft3/min)
 STACK DIMENSIONS

Sample Point	Time (min)	Dry Gas Meter Reading (ft³)	Pitot Reading ΔP ("H ₂ O)	Meter ΔH	Meter Temp. Tm (°F)	Pump Vacuum (Hg)	Filter Box (°F)	Imp. Exit (°F)	Stack Temp. (°F)	% CO ₂	% O ₂
		<u>220.000</u>									
1	5		<u>.04</u>	<u>2</u>	<u>72</u>	<u>4</u>	<u>—</u>	<u>49</u>	<u>621</u>	<u>9.5</u>	<u>2.8</u>
2	10		<u>.04</u>		<u>72</u>	<u>4</u>		<u>49</u>	<u>621</u>		
3	15		<u>.04</u>		<u>72</u>	<u>4</u>		<u>49</u>	<u>621</u>		
4	20		<u>.04</u>		<u>72</u>	<u>4</u>		<u>49</u>	<u>621</u>		
5	25		<u>.04</u>		<u>71</u>	<u>4</u>		<u>50</u>	<u>620</u>		
6	30		<u>.04</u>		<u>71</u>	<u>4</u>		<u>50</u>	<u>620</u>		
7	35		<u>.04</u>		<u>71</u>	<u>4</u>		<u>50</u>	<u>620</u>		
8	40		<u>.04</u>		<u>71</u>	<u>4</u>		<u>50</u>	<u>620</u>		
9	45		<u>.04</u>		<u>70</u>	<u>4</u>		<u>51</u>	<u>619</u>		
10	50		<u>.04</u>		<u>70</u>	<u>4</u>		<u>51</u>	<u>619</u>		
11	55		<u>.04</u>		<u>70</u>	<u>4</u>		<u>51</u>	<u>619</u>		
12	60	<u>263.340</u>	<u>.04</u>		<u>70</u>	<u>4</u>		<u>51</u>	<u>619</u>		
		<u>+ 43.340</u>									
		<u>✓</u>									
1			<u>.04</u>						<u>620</u>		
2			<u>.04</u>						<u>620</u>		
3			<u>.04</u>						<u>620</u>		
4			<u>.04</u>						<u>621</u>		
5			<u>.04</u>						<u>621</u>		
6			<u>.04</u>						<u>621</u>		
7			<u>.04</u>						<u>621</u>		
8			<u>.04</u>						<u>621</u>		
9			<u>.04</u>						<u>620</u>		
10			<u>.04</u>						<u>620</u>		
11			<u>.04</u>						<u>620</u>		
12			<u>.04</u>						<u>620</u>		



MOISTURE DETERMINATION

COMPANY NAME:	MRC	RUN #	6
PLANT LOCATION:	Great Falls	TEST DATE:	10/08/08
SOURCE TESTED:	H1201	Start Time:	
Weighed By:	JW	Balance Level:	☒
		Balance Zeroed:	☒
		End Time:	

Weight (grams)

Impinger #1

Final Weight 651
Initial Weight 620
Weight Gain 31 ✓

Impinger #2

Final Weight 734
Initial Weight 712
Weight Gain 22 ✓

Impinger #3

Final Weight 507
Initial Weight 506
Weight Gain 1 ✓

Impinger #4 (if applicable)

Final Weight _____
Initial Weight _____
Weight Gain _____

Silica Gel Impinger

Final Weight 823
Initial Weight 811
Weight Gain 12 ✓

Total Mass of Moisture Captured: 66 ✓ grams

Notes:



ORSAT SHEET

COMPANY NAME:	MRC	TEST DATE:	10 - 8 - 08
PLANT LOCATION:	Great Falls		
SOURCE TESTED:	H 1810 H 1701		

	Gas	1	2	3	Average
Run # H 1810 1	Total CO ₂ + O ₂				
	CO ₂	13.0	13.0	12.9	13.0
	O ₂	5.1	5.2	5.2	5.2
Run # 2	Total CO ₂ + O ₂				
	CO ₂	13.1	13.1	13.0	13.1
	O ₂	5.3	5.2	5.3	5.3
Run # 3	Total CO ₂ + O ₂				
	CO ₂	13.2	13.2	13.2	13.2
	O ₂	5.2	5.1	5.2	5.2
Run # H 1701 4	Total CO ₂ + O ₂				
	CO ₂	9.4	9.4	9.3	9.4
	O ₂	2.9	2.9	3.0	2.9
Run # 5	Total CO ₂ + O ₂				
	CO ₂	9.5	9.5	9.4	9.5
	O ₂	2.8	2.8	2.9	2.8
Run # 6	Total CO ₂ + O ₂				
	CO ₂	9.5	9.5	9.4	9.5
	O ₂	2.8	2.8	2.8	2.8
Run #	Total CO ₂ + O ₂				
	CO ₂				
	O ₂				
Run #	Total CO ₂ + O ₂				
	CO ₂				
	O ₂				
Run #	Total CO ₂ + O ₂				
	CO ₂				
	O ₂				

Notes:

Montana Refining Company,inc.
Hydrogen Plant Reformer Heater Stack &
Diesel Hydrotreater Heater (HTU)
Process Data
10/08/08

Source	Fuel Flow scfh	Btu Content Btu/scf (Nominal)
Hydrogen Plant Heater	62,903	300
Diesel Hydrotreater Heater	6,173	1,000

EEMC

From: "Ray Martinich" <rmartinich@montanarefining.com>
To: <eemc@bresnan.net>
Sent: Tuesday, October 14, 2008 2:33 PM
Subject: Process data during testing

Dave,

Here is the process data for the HTU and hydrogen plant during the testing last week:

1) HTU unit feed rate 4,000 barrel per day (5,000 bpd max) – 80% of capacity

We could not go to higher feed rate because it would cause pressure problems in a downstream fuel gas unit (NaHS unit). At time of testing, HTU feed was gas oil, which provides the greater heater firing rate as opposed to diesel as HTU feed. HTU heater fuel firing rate during testing was approx. 148 mscfd – the average firing rate for the previous 12 months was approx. 135 mscfd.

2) Hydrogen plant production rate is dependent on the HTU rate – the H2 plant heater firing rate was at 82% of rated.

Please let me know if you need anything else.

Thanks.

Ray Martinich
Montana Refining Company, Inc.
1900 10th Street NE
Great Falls, MT 59404
(406) 454-9862 direct
(406) 761-4100 refinery
rmartinich@montanarefining.com

No virus found in this incoming message.

Checked by AVG - <http://www.avg.com>

Version: 8.0.173 / Virus Database: 270.8.0/1724 - Release Date: 10/14/2008 2:02 AM

The "City Gas" report is for natural gas, which is the sole fuel for the HTU heater. The hydrogen plant heater is fired primarily on vent gas from the unit and supplemented with natural gas. The fuel gas rates at the time of testing are as follows:

HTU heater fuel: average of 6,173 scfh natural gas over the test period

Hydrogen plant heater: average of 1,658 scfh natural gas and 62,903 scfh vent gas (natural gas has a nominal BTU content of 1,000 BTU/scf while the vent gas has a nominal BTU content of 300 BTU/scf)

/

Calculation of Fd Factor

Source: Hydrogen Plant Reformer Heater H1810
 Type of Fuel: Vent Gas
 Sample Taken: 10/08/08

Compound		Mole % *	Mol Wt	Weight Lbs	Wt Fract	Wt of H Lbs	Wt of C Lbs	Wt of N Lbs	Wt of O Lbs
Hydrogen	H ₂	50.39	2.0160	1.0159	0.0559	1.0159	0.0000	0.0000	0.0000
Carbon Dioxide	CO ₂	29.91	44.0100	13.1634	0.7245	0.0000	3.5925	0.0000	9.5706
Oxygen	O ₂	0.24	31.9988	0.0768	0.0042	0.0000	0.0000	0.0000	0.0768
Nitrogen	N ₂	4.09	28.0134	1.1457	0.0631	0.0000	0.0000	1.1457	0.0000
Carbon Monoxide	CO	2.53	28.0100	0.7087	0.0390	0.0000	0.3039	0.0000	0.4048
Methane	CH ₄	12.83	16.0400	2.0579	0.1133	0.5173	1.5410	0.0000	0.0000
Ethane	C ₂ H ₆	0.00	30.0700	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Ethylene	C ₂ H ₄	0.00	28.5400	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
n-Propane	C ₃ H ₈	0.00	44.1000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Propylene	C ₃ H ₆	0.00	42.5100	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
iso-butane	iC ₄ H ₁₀	0.00	58.1200	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
n-butane	nC ₄ H ₁₀	0.00	58.1200	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
1-butene	C ₄ H ₈	0.00	56.6800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
iso-butylene	C ₄ H ₈	0.00	58.1200	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
trans-2-butene	C ₄ H ₈	0.00	56.6800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
cis-2-Butene	C ₄ H ₈	0.00	56.6800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
1,3 Butadiene	C ₄ H ₆	0.00	54.5200	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
iso-pentane	iC ₅ H ₁₂	0.00	72.1500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
n-pentane	nC ₅ H ₁₂	0.00	72.1500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
C6+	C ₆ H ₁₄	0.00	87.1800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
hexane	C ₆ H ₁₄	0.00	87.1800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Hydrogen Sulfide	H ₂ S	0.00	34.0800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
		99.99		18.1684	1.0000	1.5332	5.4374	1.1457	10.0522
			Percent(w/w%)		100.00	8.44	29.93	6.31	55.33

Calculation of Fd Factor

Source: Hydrogen Plant Reformer Heater H1810
 Type of Fuel: Vent Gas
 Sample Taken: 10/08/08

% of Fuel by Weight		Molecular Weights utilized for calculations:	
%H	8.4388	H	1.008
%C	29.9278	C	12.011
%N	6.3060	N	14.007
%O	55.3279	O	15.999

Compound		Wt Fraction	Standard Btu/lb**	Sample Btu/lb
Hydrogen	H ₂	0.0559	61,095	3,415
Carbon Dioxide	CO ₂	0.7245	0	0
Oxygen	O ₂	0.0042	0	0
Nitrogen	N ₂	0.0631	0	0
Carbon Monoxide	CO	0.0390	4,347	170
Methane	CH ₄	0.1133	23,875	2,705
Ethane	C ₂ H ₆	0.0000	22,323	0
Ethylene	C ₂ H ₄	0.0000	21,636	0
n-Propane	C ₃ H ₈	0.0000	21,669	0
Propylene	C ₃ H ₆	0.0000	21,048	0
iso-butane	iC ₄ H ₁₀	0.0000	21,271	0
n-butane	nC ₄ H ₁₀	0.0000	21,321	0
1-butene	C ₄ H ₈	0.0000	20,854	0
iso-butylene	C ₄ H ₁₀	0.0000	20,737	0
trans-2-butene	C ₄ H ₈	0.0000	20,854	0
cis-2-butene	C ₄ H ₈	0.0000	20,854	0
n-pentene	C ₅ H ₁₀	0.0000	20,720	0
iso-pentane	iC ₅ H ₁₂	0.0000	21,047	0
n-pentane	nC ₅ H ₁₂	0.0000	21,095	0
C6+	C ₆ H ₁₄	0.0000	20,966	0
hexane	C ₆ H ₁₄	0.0000	20,966	0
Total				6,290 Btu/lb

GCV 6,290 Btu/lb

Fd = $[(3.64\%H + 1.53\%C + 0.14\%N - 0.46\%O)] \times 1000000 / GCV$
 Fd = 8,258

* From Montana Refining Fuel Analysis

Montana Refining Gas Report

Sample Name: MISC **H₂ Vent R**
 Date: 10/8/2008 7:41:02 AM
 Data Acquisition Time: 10/8/2008 7:23:54 AM
 Operator: gcmachine

Sample Number: 1
 Study:
 Cycle: 1
 Reprocess Number: mrci-001: 7362

Instrument Name: Autosystem 1

Software Version: Qate:

Sequence File: C:\Tcd\data\Autosystem1\MISC\A1_MISC.seq
 Inst Method: c:\tcd\method\td1 from C:\Tcd\data\Autosystem1\MISC\A1_TCD1_2008_10_08_MISC

Channel: A
 Raw Data File: C:\Tcd\data\Autosystem1\MISC\A1_TCD1_2008_10_08_MISC_001.raw
 Result File: C:\Tcd\data\Autosystem1\MISC\A1_TCD1_2008_10_08_MISC_001.rst
 Proc Method: c:\tcd\method\td1 from C:\Tcd\data\Autosystem1\MISC\A1_TCD1_2008_10_08_MISC
 Calib Method: c:\tcd\method\td1 from C:\Tcd\data\Autosystem1\MISC\A1_TCD1_2008_10_08_MISC
 Report Format File: c:\tcd\method\td1_MISC_tcd1.rpt

Channel: B
 Raw Data File: C:\Tcd\data\Autosystem1\MISC\A1_TCD2_2008_10_08_MISC_001.raw
 Result File: C:\Tcd\data\Autosystem1\MISC\A1_TCD2_2008_10_08_MISC_001.rst
 Proc Method: c:\tcd\method\td2 from C:\Tcd\data\Autosystem1\MISC\A1_TCD2_2008_10_08_MISC
 Calib Method: c:\tcd\method\td2 from C:\Tcd\data\Autosystem1\MISC\A1_TCD2_2008_10_08_MISC
 Report Format File: c:\tcd\method\td2_MISC_tcd2.rpt

A/B	Component Name	Concentration Amount	Normalized
B	C5+, C6+	0.0000	0.00
B	Propane	0.0000	0.00
B	Propylene	0.0000	0.00
B	i-Butane	0.0000	0.00
B	Propadiene	0.0000	0.00
B	n-Butane	0.0000	0.00
B	Butane 1	0.0000	0.00
B	i-Butylene	0.0000	0.00
B	t-Butylene 2	0.0000	0.00
B	c-Butene 2	0.0000	0.00
B	1,3-Butadiene	0.0000	0.00
B	i-Pentane	0.0000	0.00
B	n-Pentane	0.0000	0.00
A	Hydrogen	48.4078	50.38
A	Carbon Dioxide	28.7386	29.91
A	Ethylene	0.0000	0.00
A	Ethane	0.0000	0.00
A	H2S	0.0000	0.00
A	Oxygen	0.2320	0.24
A	Nitrogen	3.9328	4.09
A	Methane	12.3299	12.83
A	Carbon Monoxide	2.4281	2.53
		98.0702	100.00

Operator: **H₂ Plant Vent Tank**

Calculation of Fd Factor

Source:

Diesel Hydrotreater Heater (HTU) H1701

Type of Fuel:

Fuel Gas

Sample Taken:

09/20/07

Compound		Mole % *	Mol Wt	Weight Lbs	Wt Fract	Wt of H Lbs	Wt of C Lbs	Wt of N Lbs	Wt of O Lbs
Hydrogen	H ₂	0.00	2.0160	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Carbon Dioxide	CO ₂	0.13	44.0100	0.0572	0.0033	0.0000	0.0156	0.0000	0.0416
Oxygen	O ₂	0.19	31.9988	0.0608	0.0035	0.0000	0.0000	0.0000	0.0608
Nitrogen	N ₂	7.31	28.0134	2.0478	0.1167	0.0000	0.0000	2.0478	0.0000
Carbon Monoxide	CO	0.00	28.0100	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Methane	CH ₄	89.62	16.0400	14.3750	0.8189	3.6135	10.7642	0.0000	0.0000
Ethane	C ₂ H ₆	1.75	30.0700	0.5262	0.0300	0.1058	0.4204	0.0000	0.0000
Ethylene	C ₂ H ₄	0.00	28.5400	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
n-Propane	C ₃ H ₈	0.73	44.1000	0.3219	0.0183	0.0589	0.2630	0.0000	0.0000
Propylene	C ₃ H ₆	0.00	42.5100	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
iso-butane	iC ₄ H ₁₀	0.11	58.1200	0.0639	0.0036	0.0111	0.0528	0.0000	0.0000
n-butane	nC ₄ H ₁₀	0.13	58.1200	0.0756	0.0043	0.0131	0.0625	0.0000	0.0000
1-butene	C ₄ H ₈	0.00	56.6800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
iso-butylene	C ₄ H ₁₀	0.00	58.1200	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
trans-2-butene	C ₄ H ₈	0.00	56.6800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
cis-2-Butene	C ₄ H ₈	0.00	56.6800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
1,3 Butadiene	C ₄ H ₆	0.00	54.5200	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
iso-pentane	iC ₅ H ₁₂	0.00	72.1500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
n-pentane	nC ₅ H ₁₂	0.00	72.1500	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
C6+	C ₆ H ₁₄	0.03	87.1800	0.0262	0.0015	0.0042	0.0217	0.0000	0.0000
hexane	C ₆ H ₁₄	0.00	87.1800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Hydrogen Sulfide	H ₂ S	0.00	34.0800	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
		100.00		17.5546	1.0001	3.8066	11.6002	2.0478	0.1024
		Percent(w/w%)			100.01	21.68	66.08	11.67	0.58

Calculation of Fd Factor

Source: Diesel Hydrotreater Heater (HTU) H1701
 Type of Fuel: Fuel Gas
 Sample Taken: 09/20/07

% of Fuel by Weight		Molecular Weights utilized for calculations:	
%H	21.6843	H	1.008
%C	66.0807	C	12.011
%N	11.6653	N	14.007
%O	0.5833	O	15.999

Compound		Wt Fraction	Standard Btu/lb	Sample Btu/lb
Hydrogen	H ₂	0.0000	61,095	0
Carbon Dioxide	CO ₂	0.0033	0	0
Oxygen	O ₂	0.0035	0	0
Nitrogen	N ₂	0.1167	0	0
Carbon Monoxide	CO	0.0000	4,347	0
Methane	CH ₄	0.8189	23,875	19,551
Ethane	C ₂ H ₆	0.0300	22,323	670
Ethylene	C ₂ H ₄	0.0000	21,636	0
n-Propane	C ₃ H ₈	0.0183	21,669	397
Propylene	C ₃ H ₆	0.0000	21,048	0
iso-butane	iC ₄ H ₁₀	0.0036	21,271	77
n-butane	nC ₄ H ₁₀	0.0043	21,321	92
1-butene	C ₄ H ₈	0.0000	20,854	0
iso-butylene	C ₄ H ₁₀	0.0000	20,737	0
trans-2-butene	C ₄ H ₈	0.0000	20,854	0
cis-2-butene	C ₄ H ₈	0.0000	20,854	0
n-pentene	C ₅ H ₁₀	0.0000	20,720	0
iso-pentane	iC ₅ H ₁₂	0.0000	21,047	0
n-pentane	nC ₅ H ₁₂	0.0000	21,095	0
C6+	C ₆ H ₁₄	0.0015	20,966	31
hexane	C ₆ H ₁₄	0.0000	20,966	0
		Total	20,817 Btu/lb	

GCV 20,817 Btu/lb

Fd = $[(3.64\%H + 1.53\%C + 0.14\%N - 0.46\%O)] \times 1000000 / GCV$

Fd = 8,714

* From Montana Refining Fuel Analysis

Montana Refining Gas Report

Sample Name: MISC *City Gas*
 Date: 10/8/2008 8:58:43 AM
 Data Acquisition Time: 10/8/2008 8:41:38 AM
 Operator: gcmachine

Sample Number: 1
 Study:
 Cycle: 1
 Reprocess Number: mrci-001: 7366

Instrument Name: Autosystem 1

Software Version: Date:

Sequence File: C:\Tcsequences\A1_MISC.seq

Inst Method: c:\tcmethods\la1_tcd1 from C:\Tcddata\Autosystem1\MISCA1_TCD1_2008_10_08_MISC

Channel:A

Raw Data File: C:\Tcddata\Autosystem1\MISCA1_TCD1_2008_10_08_MISC_001-20081008-084143.

Result File: C:\Tcddata\Autosystem1\MISCA1_TCD1_2008_10_08_MISC_001-20081008-085843.

Proc Method: c:\tcmethods\la1_tcd1 from C:\Tcddata\Autosystem1\MISCA1_TCD1_2008_10_08_MISC

Calib Method: c:\tcmethods\la1_tcd1 from C:\Tcddata\Autosystem1\MISCA1_TCD1_2008_10_08_MISC

Report Format File: c:\tcmethods\la1_MISC_tcd1.rpt

Channel:B

Raw Data File: C:\Tcddata\Autosystem1\MISCA1_TCD2_2008_10_08_MISC_001-20081008-084144.

Result File: C:\Tcddata\Autosystem1\MISCA1_TCD2_2008_10_08_MISC_001-20081008-085852.

Proc Method: c:\tcmethods\la1_tcd2 from C:\Tcddata\Autosystem1\MISCA1_TCD2_2008_10_08_MISC

Calib Method: c:\tcmethods\la1_tcd2 from C:\Tcddata\Autosystem1\MISCA1_TCD2_2008_10_08_MISC

Report Format File: c:\tcmethods\la1_MISC_tcd2.rpt

<u>A/B</u>	<u>Component Name</u>	<u>Concentration Amount</u>	<u>Normalized</u>
B	C5+,C6+	0.0334	0.03
B	Propane	0.7411	0.73
B	Propylene	0.0000	0.00
B	i-Butane	0.1072	0.11
B	Propadiene	0.0000	0.00
B	n-Butane	0.1341	0.13
B	Butene 1	0.0000	0.00
B	i-Butylene	0.0000	0.00
B	t-Butene 2	0.0000	0.00
B	c-Butene 2	0.0000	0.00
B	1,3-Butadiene	0.0000	0.00
B	i-Pentane	0.0000	0.00
B	n-Pentane	0.0000	0.00
A	Hydrogen	0.0033	0.00
A	Carbon Dioxide	0.1279	0.13
A	Ethylene	0.0000	0.00
A	Ethane	1.7808	1.75
A	H2S	0.0000	0.00
A	Oxygen	0.1905	0.19
A	Nitrogen	7.4307	7.31
A	Methane	91.0828	89.62
A	Carbon Monoxide	0.0000	0.00
		101.6416	100.00

Operator: *City Gas - Low Pressure*

EQUIPMENT CALIBRATION

**Montana Refining Company, Inc.
Diesel Hydrotreater Heater (HTU) H1701 &
Hydrogen Plant Reformer Heater H1810 Stacks
Great Falls, Montana**

10/08/08

- 1) Meter Box
8-R
08/18/08 @ 1.01 (Full Profile)
10/14/08 @ 1.02 (@ 2.0"H₂O Delta H and 7.0" Hg Vacuum)
- 2) Thermocouple (M) and Dial Thermometers
Note attached following sheets.
- 3) Pitot Tube (S-type, #170)
A S-Type pitot was utilized as manufactured by EEMC. Note attached data sheets for specifications.
- 4) Barometer (aneroid)
The aneroid barometer was calibrated with a mercury wall barometer prior to and after the test series. See attached data sheet.
- 5) NO_x/CO
EPA Protocol 1 span gases were utilized for calibration. N₂ zero gas was employed. Instrument calibration drift and bias determinations follow each run. NO_x converter efficiency is noted on the computer/logger.

METER BOX CALIBRATION

Date: 8-18-08 Calibrated By: [Signature] Dry Gas Meterbox ID: 819
 Barometric Pressure, Pb: 26.62 Vacuum: _____

Orifice Manometer Setting Δ H in. H ₂ O	0.5	1.0	2.0	3.0	4.0	5.0
Gas Volume Wet Test Meter V _w , ft ³	5	5	7.5	10		
Gas Volume Dry Gas Meter M Final	533.891	539.048	546.775	557.058		
M Initial	529.000	534.100	539.300	547.000		
V _d , ft ³	4.891	4.948	7.475	10.058		
Wet Test Meter t _w F°	74	74	74	74		
t _w A°	534	534	534	534		
Dry Gas Meter Outlet, t _{mo}						
1)	73	73	74	74		
2)	73	74	74	75		
3)	73	74	74	75		
Dry Gas Meter Inlet, t _{mi}						
1)	75	75	76	76		
2)	75	75	76	77		
3)	75	76	76	77		
Mean t _m F°	74	75	75	76		
t _m A°	534	535	535	536		
Time θ minutes	727.12	536.93	577.62	633.55		
Results, Y = $\frac{(V_w)(P_b)(t_m)}{V_d (P_b + \Delta H/13.6)(t_w)}$	1.02	1.01	1.00	.99		
ΔH @ = $\frac{.0317(H)}{P_b(t_m)} \left[\frac{(t_w)\theta}{V_w} \right]^2$	1.87	2.02	2.09	2.12		

Averages: Y = 1.01 ΔH = 2.03

Notes:

$P_b + \Delta H/13.6 = P_m$

28.97 = molecular weight of air

y = ratio of accuracy of wet test meter to dry test meter. Tolerance = ± 0.01.

ΔH = Orifice pressure differential that gives 0.75 cfm of air at 70 °F and 29.92 in. of Hg in H₂O. Tolerance ± 0.15.

Revised 5-25-07 af

METER BOX CALIBRATION

Date: 10-14-08 Calibrated By: DJW Dry Gas Meterbox ID: 8R
 Barometric Pressure, Pb: 26.55 Vacuum: 7"

Orifice Manometer Setting Δ H in. H ₂ O	2.0 -0.5	2.0 1.0	2.0 -2.0	<i>post test</i>		
Gas Volume Wet Test Meter V _w , ft ³	5	5	5			
Gas Volume Dry Gas Meter M Final	729.883	734.778	739.718			
M Initial	725.000	729.883	734.778			
V _d , ft ³	4.883	4.895	4.940			
Wet Test Meter t _w F°	73	73	73			
t _w A°	533	533	533			
Dry Gas Meter Outlet, t _{mo}						
1)	73	73	74			
2)	73	73	74			
3)	73	74	74			
Dry Gas Meter Inlet, t _{mi}						
1)	75	76	76			
2)	76	76	77			
3)	76	76	77			
Mean						
t _m F°	74	75	75			
t _m A°	534	535	535			
Time θ minutes						
Results, Y = $\frac{(V_w)(P_b)(t_m)}{V_d(P_b + \Delta H/13.6)(t_w)}$	1.02	1.02	1.01			
ΔH @ $= \frac{.0317(H)}{P_b(t_m)} \left[\frac{(t_w)\theta}{V_w} \right]^2$						

Averages: Y = 1.02 ΔH = _____

Notes:

$P_b + \Delta H/13.6 = P_m$

28.97 = molecular weight of air

y = ratio of accuracy of wet test meter to dry test meter. Tolerance = ± 0.01.

ΔH = Orifice pressure differential that gives 0.75 cfm of air at 70 °F and 29.92 in. of Hg in H₂O. Tolerance ± 0.15.

Revised 5-25-07 af



1744 Mallowney Lane
Billings, MT 59101

3730 N. Pellegrino Drive
Tucson, AZ 85749

Thermocouple Calibration

Date: 8-25-08
Ambient Temperature: 73 °F
Calibrator: dfw

Thermocouple No.: M
Barometric Pressure: 26.60 "Hg
Reference: Mercury in glass: x
Other: _____

Reference Point No. ^a	Source ^b (specify)	Reference Thermocouple Temperature		Thermocouple Potentiometer Temperature		Difference ^c
		°F	°C	°F	°C	
	water	50	10.0	50	10	0
	"	100	37.8	100	37.8	0
	"	150	65.6	150	65.6	0
	"	200	93.3	199	92.8	.1
	oven	250	121.1	249	120.6	.1
	"	300	148.9	300	148.9	0
	"	350	176.7	350	176.7	0
	"	400	204.4	400	204.4	0
	"	450	232.2	449	231.7	.1
	"	500	260.0	497	258.3	.3
	"	550	287.8	546	285.6	.4
	"	600	315.6	596	313.3	.4
	"	650	343.3	645	340.6	.4
	"	700	371.1	696	368.9	.3
	"	750	398.9	744	395.6	.5
	"	800	426.7	794	423.3	.5
	"	850	454.4	844	451.1	.5

^a Every 30°C (50°F) for each reference point

^b Type of Calibration system used

^c $[(\text{Ref. Temp. } ^\circ\text{C} + 273) - (\text{Test Therm. Temp. } ^\circ\text{C} + 273)] / (\text{Ref. Temp. } ^\circ\text{C} + 273) \times 100 < 1.5\%$



1744 Mullooney Lane
Billings, MT 59101

3730 N. Pellegrino Drive
Tucson, AZ 85749

Thermocouple Calibration

Date: 10-14-08
Ambient Temperature: 73 °F
Calibrator: dfw

Thermocouple No.: M
Barometric Pressure: 26.55 "Hg
Reference: Mercury in glass: x
Other: _____

Reference Point No. ^a	Source ^b (specify)	Reference Thermocouple Temperature		Thermocouple Potentiometer Temperature		Difference ^c
		°F	°C	°F	°C	
	water	50	10.0	50	10	0
	"	100	37.8	100	37.8	0
	"	150	65.6	150	65.6	0
	"	200	93.3	198	92.2	.3
	oven	250	121.1	248	120	.3
	"	300	148.9	300	148.9	0
	"	350	176.7	350	176.7	0
	"	400	204.4	400	204.4	0
	"	450	232.2	448	231.1	.2
	"	500	260.0	497	258.3	.3
	"	550	287.8	546	285.6	.4
	"	600	315.6	596	313.3	.4
	"	650	343.3	645	340.6	.4
	"	700	371.1	696	368.9	.3
	"	750	398.9	744	395.6	.5
	"	800	426.7	795	423.9	.4
	"	850	454.4	844	451.1	.5

^a Every 30°C (50°F) for each reference point

^b Type of Calibration system used

^c [(Ref. Temp: °C + 273) - (Test Therm. Temp: °C + 273)] / (Ref. Temp: °C + 273) x 100 < 1.5%



Sample Train Temperature Calibration Data
Dial Thermometers

Ref. No. 8R

Standard: Glass Thermometer X

Date 10-4-08

PRE-TEST

Thermometer	Boiling Water <u>207</u>	Ambient <u>73</u>	Acceptable Range +/- 2°F
Impinger	<u>207</u>	<u>72</u>	
Meter 1	<u>206</u>	<u>73</u>	
Meter 2	<u>205</u>	<u>72</u>	
Collection Box	<u>205</u>	<u>72</u>	

Date 10-14-08

POST-TEST

Thermometer	Boiling Water <u>207</u>	Ambient <u>72</u>	Acceptable Range +/- 2°F
Impinger	<u>206</u>	<u>71</u>	
Meter 1	<u>207</u>	<u>72</u>	
Meter 2	<u>206</u>	<u>71</u>	
Collection Box	<u>205</u>	<u>71</u>	

Revised 5-10-07 af



TYPE S PITOT TUBE INSPECTION DATA FORM

Pitot Number 170

Date 10-14-08

Pitot tube assembly level? X yes no

Pitot tube openings damaged? yes (explain below) X no

$\alpha_1 = .5^\circ (<10^\circ)$, $\alpha_2 = 0^\circ (<10^\circ)$, $\beta_1 = .5^\circ (<5^\circ)$, $\beta_2 = 1.0^\circ (<5^\circ)$

$\gamma = 0^\circ$, $\theta = 0^\circ$, $A = .960$ (in.)

$z = A \sin \gamma = 0$ (in.); < 0.32 ($< 1/8$ in.)

$w = A \sin \theta = 0$ (in.); $< .08$ ($< 1/32$ in.)

$P_A = .480$ (in.) $P_b = .480$ (in.)

$D_t = .375$ (in.)

Comments: _____

Calibration required? yes X no

Signature 

Revised 5-10-07 af



TYPE S PITOT TUBE INSPECTION DATA FORM

Pitot Number 170

Date 10-4-08

Pitot tube assembly level? X yes no

Pitot tube openings damaged? yes (explain below) X no

$\alpha_1 = .5^\circ (<10^\circ)$, $\alpha_2 = 0^\circ (<10^\circ)$, $\beta_1 = .5^\circ (<5^\circ)$, $\beta_2 = 1.0^\circ (<5^\circ)$

$\gamma = 0^\circ$, $\theta = 0^\circ$, $A = .960$ (in.)

$z = A \sin \gamma = 0$ (in.); < 0.32 ($< 1/8$ in.)

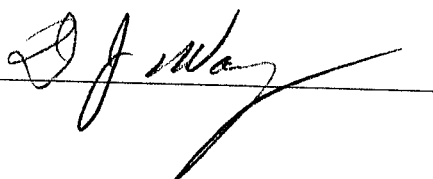
$w = A \sin \theta = 0$ (in.); $< .08$ ($< 1/32$ in.)

$P_A = .480$ (in.) $P_b = .480$ (in.)

$D_t = .375$ (in.)

Comments: _____

Calibration required? yes X no

Signature 

Revised 5-10-07 af



BAROMETER CALIBRATION

[illegible]



AMERICAN INDUSTRIAL GASES, INC.
AMERICAN RARE GASES, INC.

6055 BRENT DR. TOLEDO, OH 43611
419-729-7732 FAX 419-729-2411

THE AMERICAN GAS GROUP

www.americangasgroup.com

ANALYTICAL REPORT

Certificate ID: 101507010 Date: 10/15/2007
Customer Name: General Distributing - Billings
Customer Address: 1327 S 29th St.
Billings MT 59102
Purchase Order: 121010 Work Order: 067784-02
Lot Number: 1001HG07 Product Name: 2-Component Mixture, EPA Protocol
Size: 16A Pressure: 2200 psig @ 90 Deg F
Content: NA
Serial #: ET0001857
Analysis Date: 10/15/2007
Shelf Life: 24 months Expiration Date: 10/15/2009

<u>Component</u>	<u>Nominal</u>	<u>Actual</u>	<u>Accuracy</u>	<u>Method</u>
Nitrogen Oxides (NOx)	50 ppm	50.2 ppm	+/- 1% rel	Chemiluminescence
Nitrogen	Balance	Balance		

<u>REFERENCE STANDARD</u>	<u>Std Type</u>	<u>Std #</u>	<u>Cyl #</u>	<u>Concentration</u>	<u>Exp Date</u>
	GMIS	0329SH07	EB0005004	251.0000	6/14/2009

<u>INSTRUMENTATION</u>	<u>Instrument / ID</u>	<u>Component</u>
	Rosemount 951A	NOx

Note: * ANALYZED ACCORDING TO EPA TRACEABILITY PROTOCOL FOR ASSAY AND CERTIFICATION
OF GASEOUS CALIBRATION STANDARDS - SEPTEMBER 1997:G1
* DO NOT USE STANDARD WHEN PRESSURE IS BELOW 150 PSIG



Issued by: Josh Jones



CERTIFICATION OF ANALYSIS

Interference Free Multi-Component EPA Protocol Gases

Note: Analytical uncertainty and NIST traceability are in compliance with EPA-600/R-97/121
Section 2.2, Procedure G-1

Customer: VALLEY WELDERS & INDUSTRIAL SUPPLY
Location: LA PORTE, TX

P.O. Number: 82493
Item Number:

Assay Date: 19-Sep-2008

Expiration Date: 19-Mar-2009

Cylinder S/N: AL88466
Shipping Order Number: 30580498
Transfer Number:
Lot Number: SFS124405
Valve: CGA 660
Cylinder Pressure*: 2000 PSIG
*Cylinder should not be used when
gas pressure is below 150 psig

Components	Requested Concentration	Assay Concentration
Nitrogen	Balance	Balance
Nitrogen Dioxide	55 ppm	51.6 ± 1.3 ppm

Reference Standard(s) Employed For Analysis

Certified Concentration and Uncertainty	Component	Balance	Cyl. No.	SRM/PRM/Mix No.	Exp. Date	Sample No.	Type
51.4 ± 1.2 ppm	Nitrogen Dioxide	Nitrogen	EB0009973	SFS119543	12-Jul-2010	BI	GMIS

Anal Data

Component: Nitrogen Dioxide		FIRST TRIAD ANALYSIS 11-Sep-2008				SECOND TRIAD ANALYSIS 19-Sep-2008			
Information		Trial 1	Trial 2	Trial 3	Units	Trial 1	Trial 2	Trial 3	Units
Method: Fourier Transform IR	Zero	0.010	0.011	0.015	ppm	Zero	-0.025	-0.013	-0.015
Manufacturer: MKS Instruments	Reference	51.326	51.325	51.331	ppm	Reference	51.232	51.234	51.257
Model Number: 2031	Candidate	51.581	51.794	51.666	ppm	Candidate	51.235	51.178	51.275
Serial Number: 10387278	Result	51.66	51.87	51.74	ppm	Result	51.40	51.34	51.42
IPR Last Calibrated: 4-Sep-2008	Evaluation	Valid	Valid	Valid		Evaluation	Valid	Valid	Valid
Analytical Principle: FTIR		Mean Analytical Result: 51.76 ppm				Mean Analytical Result: 51.39 ppm			

Analyst: Thuan Tran

Approved by: Tan Ngo

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

Airgas Specialty Gases
 12722 S. Wentworth Avenue
 Chicago, IL 60628
 1-773-785-3000
 FAX: 1-773-785-1928
 www.airgas.com

Part Number: E02NI99E80A2906 Reference Number: 54-124146707-2
 Cylinder Number: LL31587 Cylinder Volume: 83 Cu.Ft.
 Laboratory: ASG - Chicago - IL Cylinder Pressure: 2215 PSIG
 Analysis Date: Aug 11, 2008 Valve Outlet: 660

Expiration Date: Aug 11, 2010

Certification performed in accordance with "EPA Traceability Protocol (Sept. 1997)" using the assay procedures listed. Analytical Methodology does not require correction for analytical interferences. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.
 Do Not Use This Cylinder below 150 psig, i.e. 1 Mega Pascal

ANALYTICAL RESULTS				
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty
NITRIC OXIDE	98.00 PPM	100.6 PPM	G1	+/- 1% NIST Traceable
NITROGEN	Balance			

Total oxides of nitrogen 100.7 PPM For Reference Only

CALIBRATION STANDARDS				
Type	Lot ID	Cylinder No	Concentration	Expiration Date
NTRM/NO	11106	CC207573	93.2PPM NITRIC OXIDE/	Jan 01, 2010
ANALYTICAL EQUIPMENT				
Instrument/Make/Model	Analytical Principle			Last Multipoint Calibration
Thermo 6700	FTIR			Aug 04, 2008

Triad Data Available Upon Request

Notes:

Richard N. Dyle

QA Approval



SPECIALTY GASES OF AMERICA, INC.
AMERICAN INDUSTRIAL GASES, INC.
AMERICAN RARE GASES, INC.

6055 BRENT DR. TOLEDO, OH 43611
419-729-7732 FAX 419-729-2411

THE AMERICAN GAS GROUP

www.americangasgroup.com

ANALYTICAL REPORT

Certificate ID: 100206L008 Date: 10/2/2006
Customer Name: General Distributing
Customer Address: 103 Bridger Center Dr
Bozeman MT 59772
406-454-1351
Purchase Order: 107478 Work Order: 054213-03
Lot Number: 0921SA06 Product Name: 3-Component Mixture, EPA Protocol
Size: 16A Pressure: 2000 psig @ 70 degF
Content: NA
Serial #: ER0000536
Analysis Date: 10/2/2006
Shelf Life: 36 months Expiration Date: 10/2/2009

<u>Component</u>	<u>Nominal</u>	<u>Actual</u>	<u>Accuracy</u>	<u>Method</u>
Carbon Monoxide	43 ppm	43.8 ppm	+/- 0.1 ppm	NDIR
Oxygen	8.6%	8.63%	+/- 0.03%	Paramagnetic
Nitrogen	Balance	Balance		

<u>REFERENCE STANDARD</u>	<u>Std Type</u>	<u>Std #</u>	<u>Cyl #</u>	<u>Concentration</u>	<u>Exp Date</u>
	GMIS	1011BC05	EB0000910	99.5 ppm	2/8/2008
	GMIS	1206BJ05	EB0001482	9.985%	2/7/2008

<u>INSTRUMENTATION</u>	<u>Instrument / ID</u>	<u>Component</u>
	Horiba VA-3000	CO
	Rosemount 755R	O2

Note: * ANALYZED ACCORDING TO EPA TRACEABILITY PROTOCOL FOR ASSAY AND CERTIFICATION OF GASEOUS CALIBRATION STANDARDS - SEPTEMBER 1997:G1
* DO NOT USE STANDARD WHEN PRESSURE IS BELOW 150 PSIG



Issued by: Duncan Lam



AMERICAN INDUSTRIAL GASES, INC.
AMERICAN RARE GASES, INC.

6055 BRENT DR. TOLEDO, OH 43611
419-729-7732 FAX 419-729-2411

THE AMERICAN GAS GROUP

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ANALYTICAL REPORT

Certificate ID: 100206L010 Date: 10/2/2006
Customer Name: General Distributing
Customer Address: 103 Bridger Center Dr
Bozeman MT 59772
406-454-1351
Purchase Order: 107478 Work Order: 054213-00
Lot Number: 0921BB06 Product Name: 2-Component Mixture, EPA Protocol
Size: 16A Pressure: 2000 psig @ 70 degF
Content: NA
Serial #: ER0000533
Analysis Date: 10/2/2006
Shelf Life: 36 months Expiration Date: 10/2/2009

<u>Component</u>	<u>Nominal</u>	<u>Actual</u>	<u>Accuracy</u>	<u>Method</u>
Carbon Monoxide	97 ppm	93.5 ppm	+/- 0.2 ppm	NDIR
Nitrogen	Balance	Balance		

<u>REFERENCE STANDARD</u>	<u>Std Type</u>	<u>Std #</u>	<u>Cyl #</u>	<u>Concentration</u>	<u>Exp Date</u>
	GMIS	1011BC05	EB0000910	99.5 ppm	2/8/2008

<u>INSTRUMENTATION</u>	<u>Instrument / ID</u>	<u>Component</u>
	Horiba VA-3000	CO

Note: * ANALYZED ACCORDING TO EPA TRACEABILITY PROTOCOL FOR ASSAY AND CERTIFICATION OF GASEOUS CALIBRATION STANDARDS - SEPTEMBER 1997:G1
* DO NOT USE STANDARD WHEN PRESSURE IS BELOW 150 PSIG



Issued by:

Duncan Lam

CHEMILUMINESCENT NO/NO_x ANALYZER



Model 400 CLD

FEATURES

- Sensitivity to 3 ppm NO/NO_x Full Scale
- Automatic High Voltage Shutdown with Loss of Ozone Air
- Complete Digital Presentation Including Sample & Air Pressure (No Gauges)
- Five Ranges
- Remote Operation Capability
- Sample Pump (Optional)
- CE Approved

CLD OPTIONS

- 19 Inch Rack Mount Slides
- Remote In-line Sample Filter
- Built-in Sample Pump

APPLICATIONS

- Stack Gases (CEM)
- Source Monitoring
- Scrubber Efficiency
- Process Chemical Gas Analysis
- Personnel Safety
- Power Plant Stack De-Nitrification
- Vehicle Emissions
- Low NO_x Applications

 **California Analytical Instruments, Inc.**



CALIFORNIA ANALYTICAL
INSTRUMENTS, INC.

ANALYZER ASSEMBLY & CALIBRATION CHECKLIST

ASSEMBLY NUMBER: 110556-1 MODEL NUMBER: 400 CLD

SERIAL NUMBER: P12023

ASSEMBLY COMPLETED BY: _____ DATE: _____

CHECKLIST:

- ☐ Front panel assembly complete per CAI assembly drawings
- ☐ Rear panel assembly complete per CAI assembly drawings
- ☐ Solenoid valves leak tested where applicable
- ☐ Oven assembly complete per CAI assembly drawings
- ☐ Sealants applied to fitting per MFG'S specifications
- ☐ Fittings tightened per MFG'S specifications
- ☐ PCB's pre-tested
- ☐ RTD's, T/C's and heaters pre-tested
- ☐ Mechanical parts & assemblies installed per CAI assembly drawings
- ☐ Electrical parts & assemblies installed per CAI assembly drawing

COMMENTS: _____

CALIBRATION COMPLETED BY: Jon Woods DATE: 12-20-03

☒ Pre burn-in complete

☒ Burn-In:

In date: 12-18-03 Out date: 12-22-03

☒ Final test complete

COMMENTS: _____

0-1VDC out put



CALIFORNIA ANALYTICAL
INSTRUMENTS, INC.

400 CLD QA Check List

Customer: EEMC Corp

S/N: P12023

Sales Order: 12007

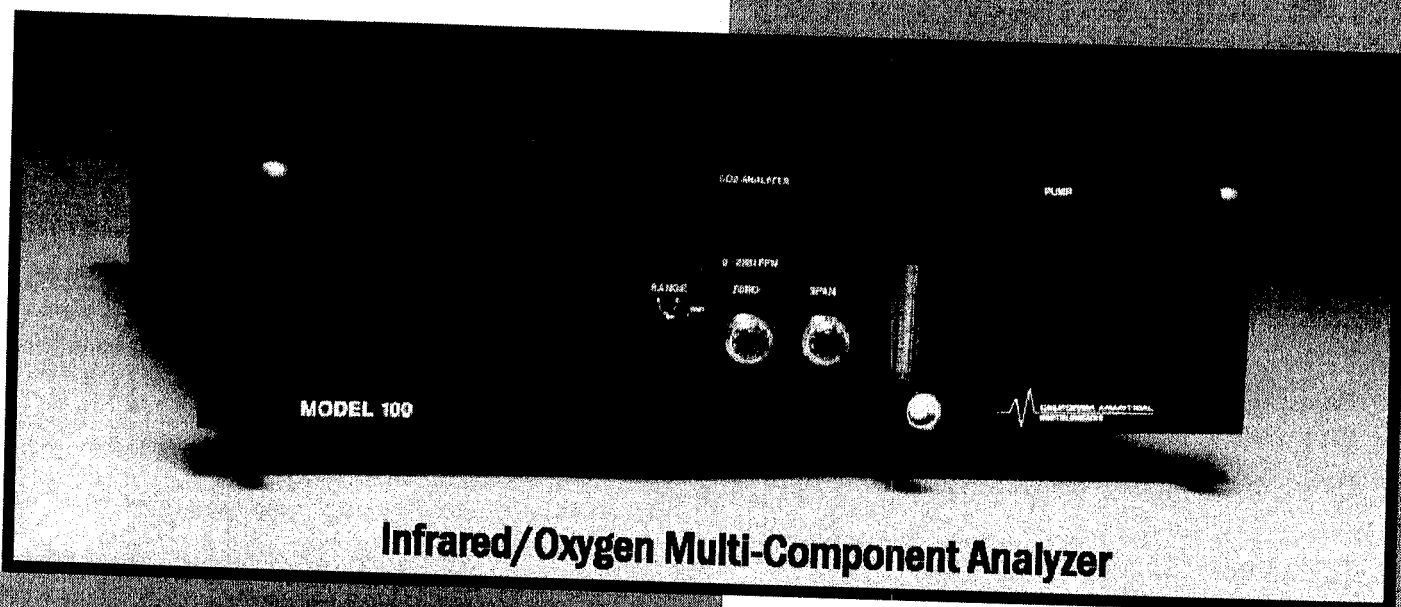
Date: 12-20-03

By: Jon Woods

1. PS Voltages Ref. +12 V ✓ -12 V ✓ +5 V ✓
+20 V ✓ +12.000 V ✓ AC Wiring ✓
2. PGA (Zero) Adjust ✓
3. Sample Pressure Zero and Span Adjust ✓
4. Air Pressure Zero and Span Adjust ✓
5. O2/Air Lamp Set at 2.0 PSI +/- 0.5 ✓
6. Cell Temperature Span Adjust ✓
7. Converter Temperature Span Adjust ✓
8. Cell Heater Temperature 46 °C
9. Converter Heater Temperature 205 °C
10. Solenoid Valves Leak Check NA
11. Air Pressure Regulator Set to 25 PSI ✓
12. O2/Air Pressure 12.75 PS Flow Rate 600 cc/Min
13. Sample Pressure 3.85 PS Flow Rate 188 cc/Min
14. Converter By Pass Flow Rate 247 cc/Min
15. Sample By Pass Flow Rate 62 cc/Min
16. EPC By Pass Flow Rate 1500 cc/Min
17. Calibrate 0-1V VDC &/or 4-20 MADC Output ✓ 0-1VDC
18. Amplifier Gain Adjust ✓
19. Front Panel Displays Zero and Span Adjusted ✓
20. 3,000 ppm Range Adjusted N/A
21. Remote Range Change Tested ✓
22. Remote NO/NOx Solenoid Tested ✓
23. Remote Mode Tested ✓
24. Remote Sample Pressure and
Converter Temperature Output Tested ✓
25. Response Time NO Mode (0-90% FS) 1.5 Seconds
26. Response Time NOx Mode (0-90% FS) 1.8 Seconds
27. NOx Converter Efficiency 97 %
28. CO2 Quench Value 2.2 %
29. Noise Level Range 1 61 % FS
30. Front Panel Dial Settings Number Zero 6.00 Span 5.00

100/200/300 SERIES

NDIR/O₂



Infrared/Oxygen Multi-Component Analyzer

APPLICATIONS

- Stack Gases (CEM)
- Combustion Efficiency
- Process Chemical Gas Analysis
- Vehicle Emissions
- EPA Compliance
- Controlled Atmospheres
- Landfill Emissions

OPTIONS

- Two or Three NDIR Channels or One to Two NDIR Channels And Oxygen
- Choice of Paramagnetic or Fuel Cell Technology for Oxygen
- Alarms
- 19 Inch Rack Mount

FEATURES

- From ppm to 100%
- Single Beam Optics
- No Optical or Mechanical Adjustments Required
- Microflow Detector
- Unmatched Reliability
- Excellent Stability
- Lowest Sensitivity to Vibration
- Digital Concentration Display
- Linear or Nonlinear Output



1312 West Grove Avenue
Orange, CA 92865-4134
Phone: 714-974-5560 Fax: 714-921-2531
www.gasanalyzers.com

Listing of Quality Control Procedures
EPA #1-4, #5, #6, #8, #17, #201A & #202 Testing Methodology
Particulates/SO₂/SO₃/Condensable Particulates

I. Calibration of Equipment

A. Meter box (meter)

The meter box is calibrated with a wet test meter prior to and after the test series. In addition the initial test includes a profile covering pertinent Delta H values (completed at least every six months).

The post meter box calibration includes a triplicate calibration at the mean Delta H at the maximum meter vacuum experienced during the test series.*

*If an orifice slip stream is utilized the meter calibration is conducted at the maximum slip stream flow rate encountered during testing.

B. Thermometers

- 1) Dry gas meter (2)
- 2) Silica gel impinger effluent (1)

These dial thermometers are checked at ambient and water boiling conditions prior to and after the test series. If they are off more than +/- 5.4 °F for the Dry Gas Meter thermometer or Collection Box thermometer or +/-2.0 °F for the Impinger thermometer they are adjusted or replaced (if not correctable). In addition, all thermometers in the field are daily checked prior to sampling utilizing ambient temperatures (reference glass thermometers and/or an Omega Simulator (thermocouple)).

C. Manometer (vertical/inclined)

This device is a primary standard. It is leak checked prior to and during field utilization. During use it is operated at level conditions (bubble indicator).

D. Vacuum Gauge

The vacuum gauge is an indicator of train vacuum - it does not affect the sample. Performance is checked each time the unit is utilized. If it is suspect, it is discarded and replaced.

E. Meter Box Leak Integrity

The meter box is placed under positive pressure just prior to field testing to determine if a leak exists. This procedure is repeated prior to each meter calibration.

II. Sampling - continued

C. Temperature (Thermocouple)

An electronic simulator is utilized for field determination of response accuracy at the stack temperature.

D. Temperature

Dial - Train Thermometers are checked against ambient air to determine continued field integrity.

E. Orsat

Ambient air is analyzed in the field to assess orsat performance.

F. Impinger balance

The balance is zeroed and checked for accuracy with standard weights.

G. Probe cleaning

After probe wash/clean out the probe is visually inspected.

H. Sample Removal

The samples are placed into glass or inert plastic bottles for removal to the laboratory. Labeling includes (minimum):

- | | |
|---------------|-----------------------|
| a) Date | d) Sample description |
| b) Run # | e) Source I.D. |
| c) Level mark | |

I. Post Purge

Upon completion of Method #8 sampling a 15 minute post purge is conducted utilizing carbon filtered ambient air or tank N₂.

III. Laboratory Analysis

A. Particulates

The laboratory balance is calibrated (with S weights) just prior to each act of weighing. Standard interim weights are utilized to determine if the calibration has been successful (+/- 0.2mg).

B. Sample Weighing

- 1) Filters (initial - tare)

The desiccated filters are tared to a constant weight (+/- 0.5 mg).

IV. Post Sampling

A. Particulates

Samples are washed from each train component three times utilizing the specified wash material (acetone, ester, or MeCl₂). The resultant captures are removed to EEMC's laboratory for analysis.

B. SO₂/SO₃

- 1) SO₂ samples are usually analyzed in the field and reanalyzed in the EEMC's laboratory
- 2) SO₃ samples can also be evaluated in the field but are usually returned to EEMC's laboratory for analysis.

If SO₃ is sampled/captured, a post sample purge of the 80%IPA Solution is conducted prior to analysis (15minutes with air or N₂)

This document is not designed to be a redundant dissertation of EPA methods. Instead, it is a brief commentary on general practices as routinely employed and almost all of which are described in EPA reference methods and quality control manuals.

**Listing of Quality Control Procedures
for EPA Methods #3A & 7E Testing Methodology**

I. Calibration of Equipment (NO_x in N₂ or Air)

A) Zero and Span

EPA Protocol 1 calibration gases are utilized for instrument zero/span purposes. The filtered air or N₂ tank is utilized for zero purposes.

B) Chemiluminescents instrumentation or equivalent is utilized for NO_x concentration determination. Converter efficiency is determined utilizing tank gas containing NO/NO₂ as per Method #7E.

Interferences have been determined (by the vendors) to meet selectivity requirements.

C) All calibrations must be drawn through the sample interface. All instruments are checked for linearity via EPA Protocol 1 gases before each test series (zero and three calibration gas concentrations).

D) Sample Moisture

Moisture removal is via a thermoelectric cooler at the head of the interface and in the case of heavy moisture additionally at the terminal end of the interface prior to injection to the instruments.

II. Sampling (NO_x)

A) The results are recorded on an integrating computer/logger on a minute by minute basis.

B) Sample Interface

The interface is leak checked prior to and after each sampling session.

Listing of Quality Control Procedures EPA Method #10 Testing Methodology

I. Calibration of Equipment (CO in N₂)

A) Zero and Span

EPA Protocol 1 gases are utilized for cell CO calibration. Linearity is initially determined by the introduction of zero and three calibration gas concentrations (~0% of scale, ~30% of scale, and one at high span ~60-90% of scale).

B) Interferences (CO₂)

The NDIR Monitor utilized does not respond significantly to CO₂. A high concentration of CO₂ (~12%) when injected into the CO NDIR Monitors does not indicate any interference (<0.1% of scale or 5ppm v/v @ 0-5000 pp, v/v span). Ascarite as a result is not normally utilized in the sample train.

C) Sample Flow

The monitors pump their own gas sample. The flow rate is maintained during the sample run.

D) Sample Interface

The interface is leak checked prior to and after each sampling session. All calibrations must be drawn through the sample interface.

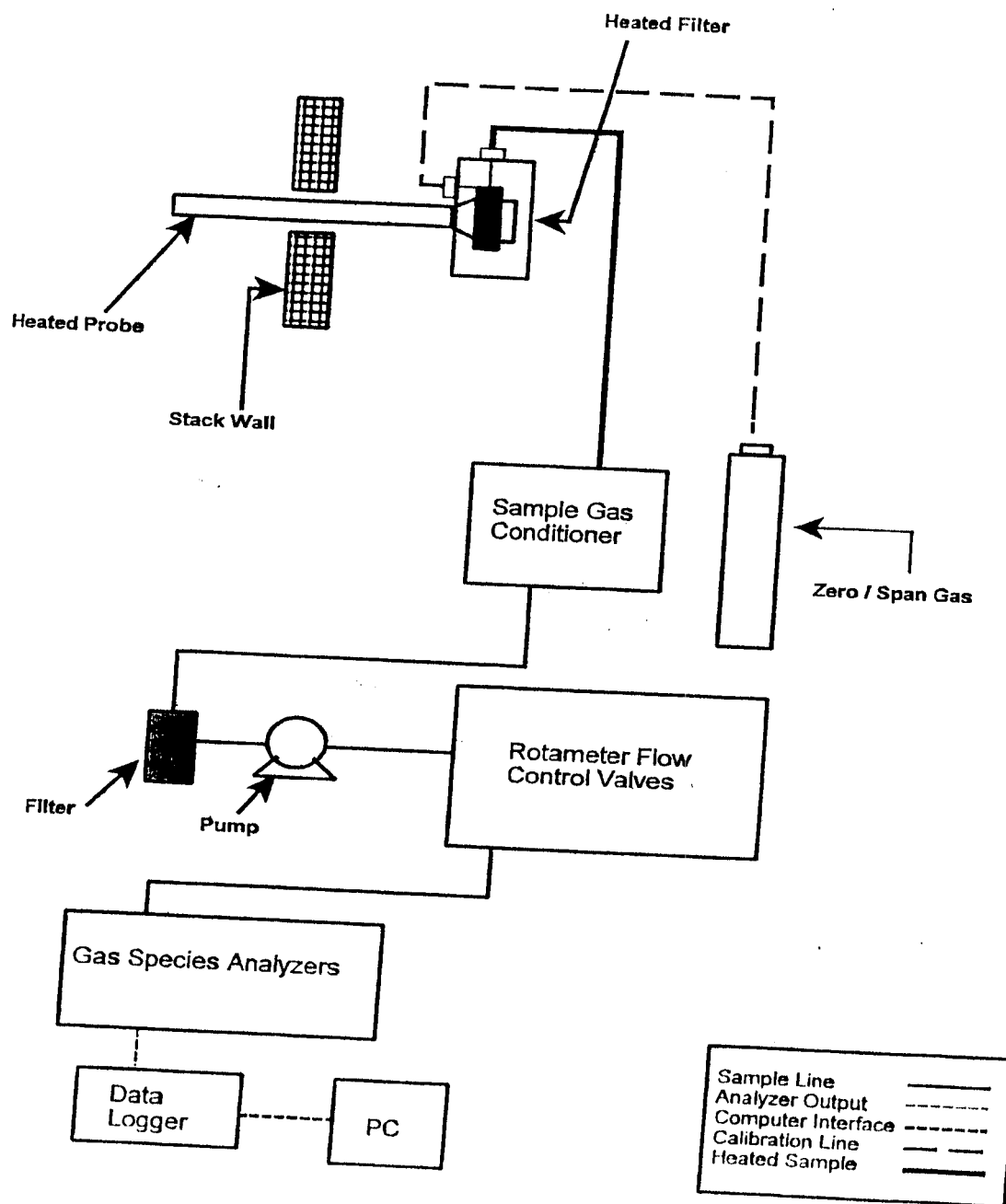
E) Sample Moisture

Moisture removal is via a thermoelectric cooler at the head of the interface and in the case of heavy moisture additionally at the terminal end of the interface prior to injection to the instruments.

II Sampling (CO)

CO instrument data is computer logged automatically utilizing one minute integrations.

EPA Methods #
 3A / 6C / 7E / 10
 O_2 & CO_2 / SO_2 / NO_x / CO
 Example Sampling Train



EPA Methods #1-4 Gas Flow / CO₂ / O₂ / Moisture Example Sampling Train

