

Note: This is a reference cited in *AP 42, Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at www.epa.gov/ttn/chief/ap42/

The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.



EVALUATOR CMC

EVALUATION DATE 7/14/92

METHOD 5: SECONDARY EMISSIONS TEST REPORT EVALUATION

STATE: WY

FACILITY: FMC-WYOMING CORP

TEST DATE: 5/24/88

PROCESS(ES) TESTED: resque plant gas fired calciner - wet scrubbers
M-22

SAMPLING DURATION

must have at least 3 runs, each ≥ 1 hour duration, with sampling ≥ 2 minutes at each traverse point, and total sampling volume ≥ 30 dscf 3

SAMPLING TEMPERATURE

both probe and filter must be maintained at $248 \pm 25^\circ\text{F}$ or other temperature specified in NSPS 2

PRODUCTION RATE

is process or production rate during testing representative of normal rates 3

BACK-HALF

if any, what method was used to catch and recover condensable matter 3

WY - H₂O

CONTROL DEVICE(S)

are devices described, and their efficiencies given 2

no

EQUIPMENT were a borosilicate glass probe liner and a glass fiber filter used 2

no doc.

METHOD 1

are calculations accurate, and is figure provided 3

CALIBRATION were both pre- and post-test calibrations performed for meter box 2

pitot tube 2

METHODS 2,3

are data and calculations included for gas velocity, cyclonic flow, and molecular weight determination, and is source of barometric pressure noted 2

no

temperature sensor 2

nozzle (3 #) 2

METHOD 4

are data and calculations included for moisture content determination, and is moisture content realistic ($< \text{saturation}$) 3

LEAK CHECKS both pre- and post-test 3

BLANKS were filter and reagent blanks analyzed, and were any problems addressed 3

FIELD DATA is field data on standard forms, and does raw data correspond with printout 3

SAMPLE PREP

filter desiccation and tare weights documented 2

no doc.

BOILER TESTS

calculation of F_0 from Orsat accurate N/A

ISOKINETICS within $100 \pm 10\%$ for all runs 3

EVALUATOR CmcEVALUATION DATE 7/14/92

METHOD 5: SECONDARY EMISSIONS TEST REPORT EVALUATION

STATE: WYFACILITY: FPMC Wyoming Corp.TEST DATE: 6/1, 2/89PROCESS(ES) TESTED: RA-23resgen plant - gas fired boiler w/ wet scrubbers

SAMPLING DURATION

must have at least 3 runs, each $\geq \frac{1}{2}$ hour duration, with sampling ≥ 2 minutes at each traverse point, and total sampling volume ≥ 30 dscf

SAMPLING TEMPERATURE

both probe and filter must be maintained at $248 \pm 25^\circ\text{F}$ or other temperature specified in NSPS

PRODUCTION RATE

is process or production rate during testing representative of normal rates

BACK-HALF

if any, what method was used to catch and recover condensable matter

CONTROL DEVICE(S)

are devices described, and their efficiencies given

EQUIPMENT were a borosilicate glass probe liner and a glass fiber filter used

METHOD 1

are calculations accurate, and is figure provided

CALIBRATION were both pre- and post-test calibrations performed for meter box

METHODS 2,3

are data and calculations included for gas velocity, cyclonic flow, and molecular weight determination, and is source of barometric pressure noted

pitot tube

temperature sensor

nozzle (3 #)

METHOD 4

are data and calculations included for moisture content determination, and is moisture content realistic ($< \text{saturation}$)

LEAK CHECKS both pre- and post-test

FIELD DATA is field data on standard forms, and does raw data correspond with printout

BLANKS were filter and reagent blanks analyzed, and were any problems addressed

SAMPLE PREP

filter desiccation and tare weights documented

BOILER TESTS

calculation of F_0 from Orsat accurateISOKINETICS within $100 \pm 10\%$ for all runs

File Copy

*Don
File:*

MEMORANDUM

TO: FMC Soda Ash Plant Compliance File

THROUGH: Chuck Collins, Air Quality Administrator
Bernie Dailey, Air Quality Supervisor

FROM: Lee Gribovicz, Division Air Quality Engineer *LG*

SUBJECT: Review of Sesqui Plant Gas Calciner Tests

DATE: November 1, 1988

By letter of January 4, 1988 the Division requested that FMC provide updated tests on RA-22 and RA-23 sources, which exhaust direct gas fired trona calciner kilns in the sesqui portion of the plant. These sources had very dated tests (6-10 years old) which showed emissions close to the allowable for these stacks. Because recent test results for another similar calciner (RA-24) had shown marginal results and because significant opacities had been noted in recent inspections of these two sources, it was felt that a confirmation of the current compliance status was appropriate. By letter of April 13, 1988 FMC scheduled this testing for the last part of May and the first part of June. The tests were conducted as planned, but because of other conflicts, the Division was unable to have an observer present during the test work.

The test reports for this test work were submitted separately, with the test report for RA-22 submitted under June 6, 1988 cover and the RA-23 report under June 15, 1988 cover. I have reviewed these test reports, and copies of my review worksheets are attached to this memo. I have had the opportunity to observe FMC's test crew numerous times and I am confident that proper procedure was followed. I can find no problems with the protocol evidenced in the test reports, therefore I must conclude that the reports are accurate (I did catch and correct a number of arithmetical errors). Test production rates were documented and reported, and I find that testing was conducted at representative conditions. As shown in the table below, both stacks tested well in compliance with their respective allowables. These tests should be accepted as confirmation of current compliance of the two stacks.

	<u>RA-22</u>	<u>RA-23</u>
Date of Testing	5/24-26/88	6/1-2/88
Measured Emission Rate (pph)	20.32	29.89
Allowable Emission Rate (pph)	32.0	35.0
Tested Production Rate (TPH)	26.6	30.5
Design Production Rate (TPH)	35	50

STACK EMISSION REVIEW

COMPANY FMC Iron Plant LOCATION Green River WY
 TESTING FIRM FMC Env. Dept TESTS CONDUCTED BY Ted Brown
 DATE TESTED 5/24-26/88 Simon Ree
 TEST OBSERVED BY Not Observed Keith Noe
 TEST EVALUATED BY Lee Kuhn

STACK DATA

Stack ht (ft) _____
 Stack dia (ft) Two stacks, each 3.5 ft dia
 Process venting through stack RA-22A & RA-22B
(R-9 Calciner Kilm)

TRAVERSE POINTS

Nozzle diameter: Test 1 0.18" Test 2 _____ Test 3 _____
 Location of sampling ports 32.5 ft (9.3 dia) downstream; 5.7 ft (1.6 dia) upstream
 Number of traverse points per test: Test 1 36 per stack Test 2 _____ Test 3 _____
72 per test
 Do sampling points follow EPA guidelines? Yes ☒ No _____

Comments:

EMISSIONS

	Test 1	Test 2	Test 3
Process wt rate (ton/hr)	<u>26.8</u>	<u>27.6</u>	<u>25.5</u> → <u>26.6 avg / 35 design</u>
Allowable emission (lb/hr)	<u>32.0</u>	<u>32.0</u>	<u>32.0</u> <u>section 25 limit</u>
Measured emission (lb/hr)	<u>22.43</u>	<u>18.61</u>	<u>19.92</u> → <u>20.32 avg</u>
% Isokinetic	<u>104%</u>	<u>105%</u>	<u>106%</u>

Comments and recommendations:

Test was run @ ~76% of design production rate
Emissions are 64% of allowable ∴ accept test
10/2/88

TSP
DATA SHEET

Total
RA-77 A+B

$P_{std} = 29.92$ in Hg

$T_{std} = 528^{\circ}R$

	Test 1	Test 2	Test 3
P_{bar} = barometric pressure at site (in Hg)	<u>23.99</u>	<u>24.06</u>	<u>24.00</u>
P_s = absolute stack gas pressure (in Hg)	<u>23.99</u>	<u>24.06</u>	<u>24.00</u>
T_s = absolute average stack gas temp. ($^{\circ}R$)	<u>585.0</u>	<u>578.8</u>	<u>580.2</u>
T_m = absolute average dry gas meter temp. ($^{\circ}R$)	<u>553.9</u>	<u>548.1</u>	<u>553.4</u>
V_{ic} = total volume of water collected (ml)	<u>133.4</u>	<u>123.2</u>	<u>140.9</u>
V_m = volume of gas through dry gas meter (ft^3)	<u>56.480</u>	<u>50.447</u>	<u>50.467</u>
ΔH = average pressure drop across orifice (in H_2O)	<u>0.401</u>	<u>0.334</u>	<u>0.328</u>
C_p = pitot tube coefficient	<u>0.84</u>		
$(\sqrt{\Delta P})_{ave}$ = average velocity head of stack gas (in H_2O)	<u>0.638</u>	<u>0.568</u>	<u>0.566</u>
A_s = cross-sectional area of stack (ft^2)	<u>19.2423</u>		
M_n = total amount of particulate collected (g) <i>with Back Half Included</i>	<u>0.2327</u>	<u>0.1952</u>	<u>0.2115</u>
θ = total sampling time (min.)	<u>144</u>		
A_n = cross-sectional area of nozzle (ft^2)	<u>1.767×10^{-4}</u>		

ORSAT ANALYSIS

	Test 1	Test 2	Test 3
% CO_2	<u>1.1</u>	<u>1.4</u>	<u>1.3</u>
% O_2	<u>15.1</u>	<u>12.6</u>	<u>15.1</u>
% CO	<u>—</u>	<u>—</u>	<u>—</u>
% N_2	<u>83.8</u>	<u>86.0</u>	<u>83.6</u>

Final Test RA-77 A + B

CALCULATIONS

1. $V_{w \text{ std}}$ = volume of water vapor in gas @ STP (ft^3)

$$V_{w \text{ std}} = 0.0474 \text{ ft}^3/\text{ml} \cdot V_{ic}$$

$$V_{w \text{ std}} = \underline{6.32}, \underline{5.84}, \underline{6.68} \text{ ft}^3$$

2. $V_{m \text{ std}}$ = volume of gas sample through dry gas meter @ STP (ft^3)

$$V_{m \text{ std}} = \left(\frac{17.65 \text{ } ^\circ\text{R}}{\text{in Hg}} \right) V_m \left(\frac{P_{\text{bar}} + \frac{H}{13.6}}{T_m} \right)$$

$$V_{m \text{ std}} = \underline{43.73}, \underline{39.13}, \underline{38.67} \text{ ft}^3$$

3. B_{wo} = proportion by volume of water vapor in gas stream (dimensionless)

$$B_{wo} = \frac{V_{w \text{ std}}}{V_{w \text{ std}} + V_{m \text{ std}}}$$

$$B_{wo} = \underline{0.13}, \underline{0.13}, \underline{0.15}$$

4. Molecular weight (lb/lb mole)

$$M_d = 0.44 (\% \text{ CO}_2) + .32 (\% \text{ O}_2) + .28 (\% \text{ N}_2 + \% \text{ CO})$$

$$M_d = \underline{28.78}, \underline{28.73}, \underline{28.81} \text{ lb/lb mole}$$

$$M_s = M_d (1 - B_{wo}) + 18 B_{wo}$$

$$M_s = \underline{27.40}, \underline{27.39}, \underline{27.22} \text{ lb/lb mole}$$

5. V_s = stack gas velocity (ft/sec)

$$V_s = 85.48 C_p (\sqrt{\Delta p})_{\text{ave}} \sqrt{\frac{T_s}{P_s M_s}}$$

$$V_s = \underline{43.21}, \underline{38.26}, \underline{38.30} \text{ ft/sec}$$

6. Q_s = volumetric flow rate, dry basis, @ STP (ft^3/min)

$$Q_s = 60 (1 - B_{wo}) V_s \cdot A_s \left(\frac{520}{T_s} \right) \left(\frac{P_s}{29.92} \right)$$

$$Q_s = \underline{31,498}, \underline{28,196}, \underline{27,525} \text{ ft}^3 \text{ min}$$

$$Q = \underline{49,891} \quad \underline{44,173} \quad \underline{44,219} \quad \left. \vphantom{\begin{matrix} 49,891 \\ 44,173 \\ 44,219 \end{matrix}} \right\} \underline{46,094} \text{ avg two stacks}$$

PARTICULATE
CALCULATIONS (CONTINUED)

Total
Test RA-72A+B

7. C_s = concentration (lb/ft³)

$$C_s = 2.205 \times 10^{-3} \frac{M_n}{V_m \text{ std}}$$

$$C_s = \frac{1.19 \times 10^{-5}}{1.10 \times 10^{-5}}, \frac{1.21 \times 10^{-5}}{1.21 \times 10^{-5}} \text{ lb/ft}^3$$

grains/dscf

0.083	0.077	0.085
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!

8. E = emission rate lb/hr

$$E = C_s \cdot Q_s \cdot 60$$

$$E = 22.43, 18.61, 19.92 \text{ lb/hr}$$

9. % Isokinetic

$$I = 1.667 T_s \left(0.00267 V_{ic} + \frac{V_m}{T_m} \left[P_{bar} + \frac{\Delta H}{13.6} \right] \right)$$

$$I = \frac{\Theta V_s P_s A_n}{103.71, 104.85, 106.15 \%}$$

TSP
DATA SHEET

RA-22A
Only

West Scrubbers
X-27

$P_{std} = 29.92$ in Hg

$T_{std} = 528^{\circ}R$

	Test 1	Test 2	Test 3
P_{bar} = barometric pressure at site (in Hg)	<u>23.99</u>	<u>24.06</u>	<u>24.00</u>
P_s = absolute stack gas pressure (in Hg)	<u>23.99</u>	<u>24.06</u>	<u>24.00</u>
T_s = absolute average stack gas temp. ($^{\circ}R$)	<u>583.6</u>	<u>578.4</u>	<u>579.9</u>
T_m = absolute average dry gas meter temp. ($^{\circ}R$)	<u>561.1</u>	<u>537.5</u>	<u>563.1</u>
V_{ic} = total volume of water collected (ml)	<u>use moisture from both stacks</u>		
V_m = volume of gas through dry gas meter (ft^3)	<u>25.476</u>	<u>22.658</u>	<u>20.509</u>
ΔH = average pressure drop across orifice (in H_2O)	<u>0.311</u>	<u>0.271</u>	<u>0.213</u>
C_p = pitot tube coefficient	<u>0.84</u>	<u>—————→</u>	
$(\sqrt{\Delta P})_{ave}$ = average velocity head of stack gas (in H_2O)	<u>0.569</u>	<u>0.507</u>	<u>0.449</u>
A_s = cross-sectional area of stack (ft^2)	<u>9.6211</u>	<u>—————→</u>	
M_n = total amount of particulate collected (g)	<u>volume calculation only</u>		
θ = total sampling time (min.)	<u>72</u>	<u>—————→</u>	
A_n = cross-sectional area of nozzle (ft^2)	<u>1.767×10^{-4}</u>	<u>—————→</u>	

ORSAT ANALYSIS

	Test 1	Test 2	Test 3
% CO_2	<u>1.1</u>	<u>1.4</u>	<u>1.3</u>
% O_2	<u>15.1</u>	<u>12.6</u>	<u>15.1</u>
% CO	<u>—</u>	<u>—</u>	<u>—</u>
% N_2	<u>83.8</u>	<u>86.0</u>	<u>83.6</u>

RA-72A
only

CALCULATIONS

1. $V_{w \text{ std}}$ = volume of water vapor in gas @ STP (ft^3)

$$V_{w \text{ std}} = 0.0474 \text{ ft}^3/\text{ml} \cdot V_{ic}$$

$$V_{w \text{ std}} = \text{not calculated} \text{ ft}^3$$

2. $V_{m \text{ std}}$ = volume of gas sample through dry gas meter @ STP (ft^3)

$$V_{m \text{ std}} = \left(\frac{17.65 \text{ } ^\circ\text{R}}{\text{in Hg}} \right) V_m \left(\frac{P_{\text{bar}} + \frac{H}{13.6}}{T_m} \right)$$

$$V_{m \text{ std}} = 19.21, 17.92, 15.44 \text{ ft}^3$$

3. B_{wo} = proportion by volume of water vapor in gas stream (dimensionless)

$$B_{wo} = \frac{V_{w \text{ std}}}{V_{w \text{ std}} + V_{m \text{ std}}}$$

$$B_{wo} = 0.13, 0.13, 0.15$$

assume T_{wo}
stack average
is applicable

4. Molecular weight (lb/lb mole)

$$M_d = 0.44 (\% \text{ CO}_2) + .32 (\% \text{ O}_2) + .28 (\% \text{ N}_2 + \% \text{ CO})$$

$$M_d = 28.78, 28.73, 28.81 \text{ lb/lb mole}$$

$$M_s = M_d (1 - B_{wo}) + 18 B_{wo}$$

$$M_s = 27.40, 27.93, 27.72 \text{ lb/lb mole}$$

5. V_s = stack gas velocity (ft/sec)

$$V_s = 85.48 C_p (\sqrt{\Delta p})_{ave} \sqrt{\frac{T_s}{P_s M_s}}$$

$$V_s = 38.49, 34.14, 30.38 \text{ ft/sec}$$

6. Q_s = volumetric flow rate, dry basis, @ STP (ft^3/min)

$$Q_s = 60 (1 - B_{wo}) V_s \cdot A_s \left(\frac{520}{T_s} \right) \left(\frac{P_s}{29.92} \right)$$

$$Q_s = 14,063, 12,588, 10,920 \text{ ft}^3 \text{ min}$$

$$Q_a = 22,221, 19,708, 17,535 \} 19,871 \text{ avg}$$

43%
of total

TSP
DATA SHEET

RA-22B
Only

East Scrubber
X-26

$P_{std} = 29.92$ in Hg

$T_{std} = 528^{\circ}R$

	Test 1	Test 2	Test 3
P_{bar} = barometric pressure at site (in Hg)	<u>23.99</u>	<u>24.06</u>	<u>24.00</u>
P_s = absolute stack gas pressure (in Hg)	<u>23.99</u>	<u>24.06</u>	<u>24.00</u>
T_s = absolute average stack gas temp. ($^{\circ}R$)	<u>586.4</u>	<u>579.1</u>	<u>580.5</u>
T_m = absolute average dry gas meter temp. ($^{\circ}R$)	<u>546.7</u>	<u>558.8</u>	<u>543.8</u>
V_{ic} = total volume of water collected (ml)	<u>use mixture from both stacks</u>		
V_m = volume of gas through dry gas meter (ft^3)	<u>31.043</u>	<u>27.788</u>	<u>29.958</u>
ΔH = average pressure drop across orifice (in H_2O)	<u>0.492</u>	<u>0.398</u>	<u>0.443</u>
C_p = pitot tube coefficient	<u>0.84</u>		
$(\sqrt{\Delta P})_{ave}$ = average velocity head of stack gas (in H_2O)	<u>0.707</u>	<u>0.629</u>	<u>0.682</u>
A_s = cross-sectional area of stack (ft^2)	<u>9.6211</u>		
M_n = total amount of particulate collected (g)	<u>volume calculation only</u>		
θ = total sampling time (min.)	<u>72</u>		
A_n = cross-sectional area of nozzle (ft^2)	<u>1.767×10^{-4}</u>		

ORSAT ANALYSIS

	Test 1	Test 2	Test 3
% CO_2	<u>1.1</u>	<u>1.4</u>	<u>1.3</u>
% O_2	<u>15.1</u>	<u>12.6</u>	<u>15.1</u>
% CO	<u>—</u>	<u>—</u>	<u>—</u>
% N_2	<u>83.8</u>	<u>86.0</u>	<u>83.6</u>

CALCULATIONS

RA-22B
only

1. $V_{w \text{ std}}$ = volume of water vapor in gas @ STP (ft^3)

$$V_{w \text{ std}} = 0.0474 \text{ ft}^3/\text{ml} \cdot V_{ic}$$

$$V_{w \text{ std}} = \text{not calculated} \text{ ft}^3$$

2. $V_{m \text{ std}}$ = volume of gas sample through dry gas meter @ STP (ft^3)

$$V_{m \text{ std}} = \left(\frac{17.65 \text{ } ^\circ\text{R}}{\text{in Hg}} \right) V_m \left(\frac{P_{\text{bar}} + \frac{H}{13.6}}{T_m} \right)$$

$$V_{m \text{ std}} = 24.00, 21.14, 23.37 \text{ ft}^3$$

3. B_{wo} = proportion by volume of water vapor in gas stream (dimensionless)

$$B_{wo} = \frac{V_{w \text{ std}}}{V_{w \text{ std}} + V_{m \text{ std}}}$$

$$B_{wo} = 0.13, 0.13, 0.15$$

4. Molecular weight (lb/lb mole)

$$M_d = 0.44 (\% \text{ CO}_2) + .32 (\% \text{ O}_2) + .28 (\% \text{ N}_2 + \% \text{ CO})$$

$$M_d = 28.78, 28.73, 28.81 \text{ lb/lb mole}$$

$$M_s = M_d (1 - B_{wo}) + 18 B_{wo}$$

$$M_s = 27.40, 27.33, 27.27 \text{ lb/lb mole}$$

5. V_s = stack gas velocity (ft/sec)

$$V_s = 85.48 \text{ Cp } (\sqrt{\Delta p})_{\text{ave}} \sqrt{\frac{T_s}{P_s M_s}}$$

$$V_s = 47.94, 42.38, 46.16 \text{ ft/sec}$$

6. Q_s = volumetric flow rate, dry basis, @ STP (ft^3/min)

$$Q_s = 60 (1 - B_{wo}) V_s \cdot A_s \left(\frac{520}{T_s} \right) \left(\frac{P_s}{29.92} \right)$$

$$Q_s = 17,431, 15,608, 16,579 \text{ ft}^3 \text{ min}$$

$$Q_a = 27,677, 24,465, 26,648 \left\{ 26,263 \text{ avg } \left(\frac{57\%}{\text{of total}} \right) \right.$$

Assume
Two stack
average is
applicable

STACK EMISSION REVIEW

COMPANY J MC Trona Plant LOCATION Green River, WY
 TESTING FIRM JMC Env. Dept. TESTS CONDUCTED BY Fred Brown
 DATE TESTED 6/1-2/88 Simon Lee
 TEST OBSERVED BY Not Observed Kurt Horrie
 TEST EVALUATED BY Lee Kibowicz

STACK DATA

Stack ht (ft) _____
 Stack dia (ft) two stacks, each 3.0 ft dia
 Process venting through stack RA-23A + RA-23B

TRAVERSE POINTS

Nozzle diameter: Test 1 0.18" Test 2 _____ Test 3 _____
 Location of sampling ports 23 ft (7.67 dia) downstream; 8 ft (2.67 dia) upstream
 Number of traverse points per test: Test 1 16 per stack Test 2 _____ Test 3 _____
32 per test
 Do sampling points follow EPA guidelines? Yes X No _____

Comments:

EMISSIONS

	Test 1	Test 2	Test 3
Process wt rate (ton/hr)	<u>29.4</u>	<u>30.9</u>	<u>31.3</u> → <u>30.5 avg / 50 design</u>
Allowable emission (lb/hr)	<u>35</u>	<u>35</u>	<u>35</u> Section 25 allowable
Measured emission (lb/hr)	<u>31.28</u>	<u>29.62</u>	<u>28.78</u> → <u>29.89 avg</u>
% Isokinetic	<u>104%</u>	<u>102%</u>	<u>105%</u>

Comments and recommendations:

Test was run @ 61% of design production rate
Emissions are 85% of allowable
test is low enough below allowable to accept
6/2/88

TSP
DATA SHEET

Total Cond
RA-73 A+B

$P_{std} = 29.92$ in Hg

$T_{std} = 528^{\circ}R$

		Test 1	Test 2	Test 3
P_{bar}	= barometric pressure at site (in Hg)	<u>24.04</u> →		<u>24.17</u>
P_s	= absolute stack gas pressure (in Hg)	<u>24.04</u> →		<u>24.17</u>
T_s	= absolute average stack gas temp. ($^{\circ}R$)	<u>607.4</u>	<u>605.4</u>	<u>598.8</u>
T_m	= absolute average dry gas meter temp. ($^{\circ}R$)	<u>546.8</u>	<u>561.2</u>	<u>556.3</u>
V_{ic}	= total volume of water collected (ml)	<u>424.1</u>	<u>421.0</u>	<u>438.0</u>
V_m	= volume of gas through dry gas meter (ft^3)	<u>74.865</u>	<u>76.450</u>	<u>76.431</u>
ΔH	= average pressure drop across orifice (in H_2O)	<u>0.847</u>	<u>0.855</u>	<u>0.847</u>
C_p	= pitot tube coefficient	<u>0.84</u> →		
$(\sqrt{\Delta P})_{ave}$	= average velocity head of stack gas (in H_2O)	<u>1.127</u>	<u>1.136</u>	<u>1.128</u>
A_s	= cross-sectional area of stack (ft^2)	<u>14.1372</u> →		
M_n	= total amount of particulate collected (g)	<u>0.3941</u>	<u>0.3676</u>	<u>0.3644</u>
θ	= total sampling time (min.)	<u>12.8</u> →		
A_n	= cross-sectional area of nozzle (ft^2)	<u>1.767×10^{-4}</u> →		

ORSAT ANALYSIS

	Test 1	Test 2	Test 3
% CO_2	<u>3.6</u>	<u>3.5</u>	<u>4.6</u>
% O_2	<u>14.5</u>	<u>14.8</u>	<u>13.2</u>
% CO	<u>/</u>	<u>/</u>	<u>/</u>
% N_2	<u>81.9</u>	<u>81.7</u>	<u>82.2</u>

CALCULATIONS

Total Test
RA-73A+B

1. $V_{w \text{ std}}$ = volume of water vapor in gas @ STP (ft^3)

$$V_{w \text{ std}} = 0.0474 \text{ ft}^3/\text{ml} \cdot V_{ic}$$

$$V_{w \text{ std}} = \underline{20.10}, \underline{19.96}, \underline{20.76} \text{ ft}^3$$

2. $V_{m \text{ std}}$ = volume of gas sample through dry gas meter @ STP (ft^3)

$$V_{m \text{ std}} = \left(\frac{17.65 \text{ }^\circ\text{R}}{\text{in Hg}} \right) V_m \left(\frac{P_{\text{bar}} + \frac{H}{13.6}}{T_m} \right)$$

$$V_{m \text{ std}} = \underline{58.74}, \underline{57.95}, \underline{58.76} \text{ ft}^3$$

3. B_{wo} = proportion by volume of water vapor in gas stream (dimensionless)

$$B_{wo} = \frac{V_{w \text{ std}}}{V_{w \text{ std}} + V_{m \text{ std}}}$$

$$B_{wo} = \underline{0.26}, \underline{0.26}, \underline{0.26}$$

4. Molecular weight (lb/lb mole)

$$M_d = 0.44 (\% \text{ CO}_2) + .32 (\% \text{ O}_2) + .28 (\% \text{ N}_2 + \% \text{ CO})$$

$$M_d = \underline{29.16}, \underline{29.15}, \underline{29.26} \text{ lb/lb mole}$$

$$M_s = M_d (1 - B_{wo}) + 18 B_{wo}$$

$$M_s = \underline{26.29}, \underline{26.30}, \underline{26.32} \text{ lb/lb mole}$$

5. V_s = stack gas velocity (ft/sec)

$$V_s = 85.48 \text{ Cp } (\sqrt{\Delta p})_{\text{ave}} \sqrt{\frac{T_s}{P_s M_s}}$$

$$V_s = \underline{79.37}, \underline{79.82}, \underline{78.58} \text{ ft/sec}$$

6. Q_s = volumetric flow rate, dry basis, @ STP (ft^3/min)

$$Q_s = 60 (1 - B_{wo}) V_s \cdot A_s \left(\frac{520}{T_s} \right) \left(\frac{P_s}{29.92} \right)$$

$$Q_s = \underline{34,937}, \underline{35,294}, \underline{35,081} \text{ ft}^3 \text{ min}$$

$$Q_a = \underline{67,286}, \underline{67,709}, \underline{66,650} \text{ } \left. \vphantom{\begin{matrix} 67,286 \\ 67,709 \\ 66,650 \end{matrix}} \right\} \text{ avg } 67,215$$

PARTICULATE
CALCULATIONS (CONTINUED)

Total Test
RA-23A & B

7. C_s = concentration (lb/ft³)

$$C_s = 2.205 \times 10^{-3} \frac{M_n}{V_{m \text{ std}}}$$

$$C_s = \underline{1.49 \times 10^{-5}}, \underline{1.40 \times 10^{-5}}, \underline{1.37 \times 10^{-5}} \text{ lb/ft}^3$$

grams/sec
0.104 0.098 0.096

8. E = emission rate lb/hr

$$E = C_s \cdot Q_s \cdot 60$$

$$E = \underline{31.78}, \underline{29.62}, \underline{28.78} \text{ lb/hr}$$

9. % Isokinetic

$$I = \frac{1.667 T_s \left(0.00267 V_{ic} + \frac{V_m}{T_m} [P_{bar} + \frac{\Delta H}{13.6}] \right)}{\theta V_s P_s A_n}$$

$$I = \underline{104.04}, \underline{102.48}, \underline{104.54} \%$$

TSP
DATA SHEET

RA-23A West Scrubber
only X-13

$P_{std} = 29.92$ in Hg

$T_{std} = 528^{\circ}R$

	Test 1	Test 2	Test 3
P_{bar} = barometric pressure at site (in Hg)	24.04 →		24.17
P_s = absolute stack gas pressure (in Hg)	24.04 →		24.17
T_s = absolute average stack gas temp. ($^{\circ}R$)	607.7	606.4	598.4
T_m = absolute average dry gas meter temp. ($^{\circ}R$)	538.1	562.6	530.7
V_{ic} = total volume of water collected (ml)	Use moisture from both stacks		
V_m = volume of gas through dry gas meter (ft^3)	40.403	40.169	41.447
ΔH = average pressure drop across orifice (in H_2O)	1.008	0.961	1.021
C_p = pitot tube coefficient	0.84 →		
$(\sqrt{\Delta P})_{ave}$ = average velocity head of stack gas (in H_2O)	1.230	1.205	1.241
A_s = cross-sectional area of stack (ft^2)	7.0686		
M_n = total amount of particulate collected (g)	volume calculation only		
θ = total sampling time (min.)	64		
A_n = cross-sectional area of nozzle (ft^2)	1.767×10^{-4}		

ORSAT ANALYSIS

	Test 1	Test 2	Test 3
% CO_2	3.6	3.5	4.6
% O_2	14.5	14.8	13.2
% CO	/	/	/
% N_2	81.9	81.7	82.2

CALCULATIONS

RA-23A
only

West Scrubber
X-13

1. $V_{w \text{ std}}$ = volume of water vapor in gas @ STP (ft^3)

$$V_{w \text{ std}} = 0.0474 \text{ ft}^3/\text{ml} \cdot V_{\text{ic}}$$

$$V_{w \text{ std}} = \text{not calculated} \text{ ft}^3$$

2. $V_{m \text{ std}}$ = volume of gas sample through dry gas meter @ STP (ft^3)

$$V_{m \text{ std}} = \left(\frac{17.65 \text{ } ^\circ\text{R}}{\text{in Hg}} \right) V_m \left(\frac{P_{\text{bar}} + \frac{H}{13.6}}{T_m} \right)$$

$$V_{m \text{ std}} = 31.96, 30.38, 32.21 \text{ ft}^3$$

3. B_{wo} = proportion by volume of water vapor in gas stream (dimensionless)

$$B_{wo} = \frac{V_{w \text{ std}}}{V_{w \text{ std}} + V_{m \text{ std}}}$$

$$B_{wo} = 0.26, 0.26, 0.26$$

4. Molecular weight (lb/lb mole)

$$M_d = 0.44 (\% \text{ CO}_2) + .32 (\% \text{ O}_2) + .28 (\% \text{ N}_2 + \% \text{ CO})$$

$$M_d = 29.16, 29.15, 29.26 \text{ lb/lb mole}$$

$$M_s = M_d (1 - B_{wo}) + 18 B_{wo}$$

$$M_s = 26.29, 26.30, 26.32 \text{ lb/lb mole}$$

5. V_s = stack gas velocity (ft/sec)

$$V_s = 85.48 \text{ Cp } (\sqrt{\Delta p})_{\text{ave}} \sqrt{\frac{T_s}{P_s M_s}}$$

$$V_s = 86.60, 84.74, 86.42 \text{ ft/sec}$$

6. Q_s = volumetric flow rate, dry basis, @ STP (ft^3/min)

$$Q_s = 60 (1 - B_{wo}) V_s \cdot A_s \left(\frac{520}{T_s} \right) \left(\frac{P_s}{29.92} \right)$$

$$Q_s = 19,061, 18,704, 19,304 \text{ ft}^3 \text{ min}$$

$$Q_a = 36,727, 35,911, 36,651$$

$$\text{avg } 36,440$$

(54% of total)

Assume
two stacks
average
moisture

TSP
DATA SHEET

RA-23B
only

East Scrubber
X12

$P_{std} = 29.92$ in Hg

$T_{std} = 528^{\circ}R$

	Test 1	Test 2	Test 3
P_{bar} = barometric pressure at site (in Hg)	<u>24.04</u> →		<u>24.17</u>
P_s = absolute stack gas pressure (in Hg)	<u>24.04</u> →		<u>24.17</u>
T_s = absolute average stack gas temp. ($^{\circ}R$)	<u>607.1</u>	<u>604.5</u>	<u>599.1</u>
T_m = absolute average dry gas meter temp. ($^{\circ}R$)	<u>555.6</u>	<u>559.8</u>	<u>561.9</u>
V_{ic} = total volume of water collected (ml)	use moisture from both stacks		
V_m = volume of gas through dry gas meter (ft^3)	<u>34.462</u>	<u>36.281</u>	<u>34.984</u>
ΔH = average pressure drop across orifice (in H_2O)	<u>0.688</u>	<u>0.749</u>	<u>0.673</u>
C_p = pitot tube coefficient	<u>0.84</u> →		
$(\sqrt{\Delta P})_{ave}$ = average velocity head of stack gas (in H_2O)	<u>1.024</u>	<u>1.067</u>	<u>1.015</u>
A_s = cross-sectional area of stack (ft^2)	<u>7.0686</u> →		
M_n = total amount of particulate collected (g)	volume calculation only		
θ = total sampling time (min.)	<u>64</u> →		
A_n = cross-sectional area of nozzle (ft^2)	<u>1.767×10^{-4}</u> →		

ORSAT ANALYSIS

	Test 1	Test 2	Test 3
% CO_2	<u>3.6</u>	<u>3.5</u>	<u>4.6</u>
% O_2	<u>14.5</u>	<u>14.8</u>	<u>13.2</u>
% CO	<u>—</u>	<u>—</u>	<u>—</u>
% N_2	<u>81.9</u>	<u>81.7</u>	<u>82.2</u>

CALCULATIONS

RA-73B
only

East Scrubber
X-12

1. $V_{w \text{ std}}$ = volume of water vapor in gas @ STP (ft^3)

$$V_{w \text{ std}} = 0.0474 \text{ ft}^3/\text{ml} \cdot V_{ie}$$

$$V_{w \text{ std}} = \text{not calculated} \text{ ft}^3$$

2. $V_{m \text{ std}}$ = volume of gas sample through dry gas meter @ STP (ft^3)

$$V_{m \text{ std}} = \left(\frac{17.65 \text{ } ^\circ\text{R}}{\text{in Hg}} \right) V_m \left(\frac{P_{\text{bar}} + \frac{H}{13.6}}{T_m} \right)$$

$$V_{m \text{ std}} = 26.37, 27.56, 26.61 \text{ ft}^3$$

3. B_{wo} = proportion by volume of water vapor in gas stream (dimensionless)

$$B_{wo} = \frac{V_{w \text{ std}}}{V_{w \text{ std}} + V_{m \text{ std}}}$$

$$B_{wo} = 0.26, 0.26, 0.26$$

4. Molecular weight (lb/lb mole)

$$M_d = 0.44 (\% \text{ CO}_2) + .32 (\% \text{ O}_2) + .28 (\% \text{ N}_2 + \% \text{ CO})$$

$$M_d = 29.16, 29.15, 29.26 \text{ lb/lb mole}$$

$$M_s = M_d (1 - B_{wo}) + 18 B_{wo}$$

$$M_s = 26.29, 26.30, 26.32 \text{ lb/lb mole}$$

5. V_s = stack gas velocity (ft/sec)

$$V_s = 85.48 \text{ Cp } (\sqrt{\Delta p})_{\text{ave}} \sqrt{\frac{T_s}{P_s M_s}}$$

$$V_s = 72.06, 74.92, 70.72 \text{ ft/sec}$$

6. Q_s = volumetric flow rate, dry basis, @ STP (ft^3/min)

$$Q_s = 60 (1 - B_{wo}) V_s \cdot A_s \left(\frac{520}{T_s} \right) \left(\frac{P_s}{29.92} \right)$$

$$Q_s = 15,876, 16,588, 15,779 \text{ ft}^3 \text{ min}$$

$$Q_a = 30,561, 31,775, 29,994 \left\{ \text{avg } 30,777 \right. \\ \left. (46\% \text{ of total}) \right.$$

Assume
two stack
average
mixture

FMC Wyoming Corporation

Box 872
Green River Wyoming 82935
307 875 2580

June 6, 1988

Mr. Lee Gribovicz
District II Engineer
Air Quality Division
Department of Environmental Quality
210 Lincoln Street
Lander, Wyoming 82520



RE: Compliance Test Report
Emission Source: RA-22 A&B

Dear Mr. Gribovicz:

Per the Air Quality Division's request of January 4, 1988, compliance tests were run on emission source RA-22 A&B. These tests were run on May 24, 25, and 26, 1988. Enclosed you will find the compliance report for this testwork. Following the same format that we have used for other reports of this nature, this report contains the following information:

- Summary of the test results
- Sampling and Analysis procedures
- Appendix which includes field data, laboratory worksheets, and calculations for each test. Diagram showing locations of sample ports, and the location and number of points in each sample diameter are also included.

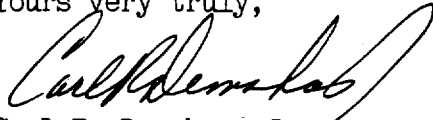
The section which contains the calculation of feedrate to the unit, has been separated from the main report and marked "Confidential" as provided for in § 35-11-1101 of the Wyoming Environmental Quality Act. Included in this separate packet are the control room logsheets of operating parameters monitored during the testwork. We consider this information to be trade secret and proprietary as it is not available to the public or to our competitors. We would appreciate you treating it as such.

Mr. Lee Gribovicz
June 6, 1988

Page 2

If you have any questions concerning this report, or need any additional information, give me a call.

Yours very truly,



Carl R. Demshar, Jr.
Environmental Manager

jc

cc: Charles Collins, DEQ - Cheyenne
JW Coykendall*, JF Herink* - Green River

* Summary Table I included with cover letter.

COMPLIANCE TEST REPORT

EMISSION SOURCE RA-22 A&B

FMC WYOMING CORPORATION

GREEN RIVER, WYOMING

June 6, 1988

COMPLIANCE TEST REPORT

EMISSION SOURCE: RA-22 A&B

FMC WYOMING CORPORATION
GREEN RIVER, WYOMING

TEST DATE: MAY 24 - 26, 1988
REPORT DATE: JUNE 6, 1988

COMPLIANCE TEST REPORT
EMISSION SOURCE: RA-22 A&B

Section

Introduction

Summary of Results

Sampling and Analysis Procedures

Calculation of Production Rate, and Control Room Logsheets
(Included in separate packet marked "CONFIDENTIAL")

APPENDIX

Section A-1 Test Data

- Field Data Sheets
- Laboratory Data Sheets
- Test Calculations
- Preliminary Test Data

Section A-2, Stack Information

- Drawing showing location of sample ports, and locations of sampling points per traverse.

Introduction

In an effort to verify compliance of source RA-22 A&B, compliance tests were conducted on May 24, 25, and 26, 1988. FMC Wyoming Corporation personnel taking part in the testwork were:

Ted Brown	Environmental Engineer
Simon Lee	Environmental Engineering Aide
Kieth Norris	Senior Laboratory Analyst

Summary of Results

This section summarizes the results of the compliance tests performed on emission source RA-22 A&B. Table I is a general summary showing the individual test results in relation to the maximum allowable emission for this source. Table II is a summary of the results obtained from each compliance tests. Details of the individual tests, including field data sheets, laboratoty data sheets, and calculation sheets can be found in the Appendix.

From Table I, it can be seen that the individual test results, as well as the three-test average, are well below the allowable emission rate for this particular unit.

TABLE I

Comparison of Compliance Test Results
With Allowable Emission Rates

<u>Emission Source</u>	<u>Test Number</u>	<u>Emission Rate, lb/hr</u>	
		<u>Compliance Test</u>	<u>Allowable</u>
RA-22 A&B	88-06-S-P	22.4	32.0
RA-22 A&B	88-07-S-P	18.6	32.0
RA-22 A&B	88-08-S-P	<u>19.0</u>	<u>32.0</u>
	Average:	20.0	32.0

TABLE II

SUMMARY OF STACK SAMPLING CALCULATIONSStack: RA-22 A & B

Test Code Number	TEST 1 ----- 88-06-SP	TEST 2 ----- 88-07-SP	TEST 3 ----- 88-08-SP
Barometric Pressure at site, (in Hg)	23.99	24.06	24.00
Absolute stack gas pressure, (in Hg)	23.99	24.06	24.00
Absolute average stack gas temp. A, (R)	583.6	578.4	579.9
Absolute average stack gas temp. B, (R)	586.4	579.1	580.5
Absolute average dry gas meter temp., (R)	553.9	548.1	553.4
Total volume of water collected, (ml)	133.4	123.2	140.9
Volume of gas through dry gas meter, (ft ³)	56.480	50.447	50.423
Average pressure drop across orifice, (in H ₂ O)	0.401	0.334	0.328
Pitot tube coefficient	0.84	0.84	0.84
Average velocity head of stack gas A, (in H ₂ O)	0.568	0.507	0.449
Average velocity head of stack gas B, (in H ₂ O)	0.708	0.629	0.682
Cross sectional area of stack, (ft ²)	9.621	9.621	9.621
Front half particulate collected, (gm)	0.2322	0.1878	0.2073
Back half particulate collected, (gm)	0.0005	0.0074	0.0042
Total particulate collected, (gm)	0.2327	0.1952	^{0.2115} 0.2015
Total sampling time, (min)	144	144	144
Cross sectional area of nozzle, (ft ² *10 ⁻⁴)	1.7672	1.7672	1.7672
Gas volume A, (acfm)	22180	19706	17533
Gas volume B, (acfm)	27713	24463	26646
Gas volume A, (scfm)	16151	14520	12854
Gas volume B, (scfm)	20083	18004	19514
Percent isokinetic	104.14	105.30	106.62
Emission rate, (lb/hr)	22.44	18.62	18.98

Sampling and Analysis Procedure

Compliance testing on emission source RA-22 A&B was conducted on May 24, 25, and 26 using EPA Method No. 5, "Determination of Particulate Emissions from Stationary Sources". This unit consists of two stacks, RA-22A and RA-22B. Each emission test consisted of traversing two sample diameters in each stack with 18 points being sampled on each diameter. Each point was sampled for two minutes resulting in a sample time of 72 minutes for each stack, with the total time for each emission sample being 144 minutes. One sample train was used for each emission test. Figure 1, located in Section A-2 of the Appendix, shows the location of the sample ports in relation to the nearest flow disturbance (an expansion, contraction, or bend in the stack). This diagram also shows the location of the sample points in each sample diameter.

Control room logsheets, containing operating data pertinent to the unit during the testwork, can be found in the Confidential Section of this report.

Calculation of Production Rate:

Emission Source: RA-22 A&B

Test Date: May 24, 25, and 26, 1988

Test No. 88-06-S-P	26.8 tons per hour
--------------------	--------------------

Test No. 88-07-S-P	27.6 tons per hour
--------------------	--------------------

Test No. 88-08-S-P	25.5 tons per hour
--------------------	--------------------

Details of these calculations, along with the control room logsheets which contain the data used in these calculations, can be found in the Confidential packet.

APPENDIX

Section A-1, Test Data

- Field Data Sheets
- Laboratory Data Sheets
- Test Calculations
- Preliminary Test Data

STACK SAMPLING FIELD DATA

Company FMC W. Corp.

Assumed Moisture, % 0.10

Plant Location Green River, WY

Probe Tip Diameter, in. 0.18

Run No. 88-06-S-P

Probe Length, ft. 5

Sampling Location RA-22A-B

Ambient Temperature, °F 5

Date 5-24-88

Bar. Pressure, in. Hg. 23.99

Start Time 09:45

Initial Leak Check, CFS

Finish Time 10:21

CFM 0.16 at 15 in. Hg.

Filter No.

Final Leak Check, CFS

CFM at in. Hg.

RA-22B "East" X-26

Point No.	Time (min)	Dry Gas Meter FT ³	Pitot		Orifice ΔH		Dry Gas Temp. °F		Pump Vacuum in. Hg Gauge	Sample Box Temp. °F	Impinger Temp. °F	Stack Press. in. Hg	Stack Temp. °F
			in. H ₂ O		in. H ₂ O		Inlet Outlet						
			P	VP	Desired	Actual							
1	0	464.719	0.29	0.538	0.26	0.26	68	65	1.0	233	76		126
2	2	465.3	0.28	0.529	0.25	0.25	70	66	1.0	237	76		126
3	4	466.0	0.29	0.538	0.26	0.26	73	67	1.2	241	76		126
4	6	466.6	0.28	0.529	0.25	0.25	74	68	1.2	242	76		126
5	8	467.3	0.27	0.520	0.24	0.24	76	69	1.0	244	76		126
6	10	467.9	0.26	0.510	0.23	0.23	78	70	1.0	236	77		126
7	12	468.5	0.25	0.500	0.22	0.22	79	71	0.9	242	77		128
8	14	469.1	0.20	0.487	0.17	0.17	79	73	0.8	243	77		127
9	16	469.6	0.17	0.462	0.15	0.15	80	74	0.6	244	77		126
10	18	470.1	0.31	0.557	0.27	0.27	83	74	1.8	244	76		126
11	20	470.8	0.70	0.837	0.61	0.61	89	76	2.5	248	75		127
12	22	471.8	0.94	0.969	0.81	0.81	91	76	3.0	244	75		128
13	24	472.9	1.0	1.000	0.86	0.86	93	77	3.0	248	74		128
14	26	474.0	0.9	0.985	0.84	0.84	94	79	3.0	247	73		128
15	28	475.2	0.98	0.990	0.85	0.85	95	80	3.0	244	73		127
16	30	476.3	0.94	0.969	0.81	0.81	96	81	3.0	222	73		127
17	32	477.4	0.97	0.985	0.84	0.84	97	82	3.0	229	73		125
18	34	478.5	0.97	0.985	0.84	0.84	97	82	3.0	236	73		125
	36	479.7											
Total													
Average													
total	V _m	56.480	25.497		17.7		86.7°F						126.4°F
average			15.8708		ΔH 0.492		54.67°F						58.64°F

10389154316-

74.981 x 1.0389

31.043

45.827 = 0.678

72

45.827 = 0.678

72

Orsat: 1.1 %CO₂

15.1 %O₂

Stk. Area 9.621

Water 133.4

Catch 0.2337

6242 ✓

4550 ✓

1.0389/54.345-

74.881 x 1.0389

31.043

$\frac{45.927}{72} = 0.638$

$\frac{28.9}{72} = 0.401$

OrseA: 1.1 8CO₂
15.1 % O₂

Stk Area 9.621
Water 33.4
Catch 0.2337

6242 ✓

112.2
9.000
72

4550 ✓

total	V _m	56.480	25.497	17.7	86.7°F							✓	126.4°F
average			15.702	ΔH 0.492	546.7°F							✓	586.4°F

0.707 Avg. ΔH: 0.401 Avg. T_m: 553.92°F

[illegible]

STACK SAMPLING FIELD DATA

Company SMC Wy. Corp.

Plant Location Green River, WY

Run No. 88-06-S-7

Sampling Location RA-22A+B

Date 5-24-88

Start Time 11:30AM

Finish Time 12:06 PM

Filter No.

Assumed Moisture, % 70

Probe Tip Diameter, in. .18

Probe Length, ft. 5

Ambient Temperature, °F _____

Bar. Pressure, in. Hg. 23.99

Initial Leak Check, CFS

CEM _____ at _____ in. Hg.

Final Leak Check, CFS _____
CEM _____ at _____ in. Hg

RA-2.2 A "West" X-27

[illegible]

[illegible]

TEST NO. 88-06-S-P

DATE 05/24/88

VELOCITY AND VOLUME DETERMINATION

DRY GAS VOLUME

$$Vmstd = (17.71 \text{ deg R/in. Hg}) * Vm * (Pbar + \Delta H / 13.6) / Tm$$

Where $Vmstd$ = Volume (ft³) of gas sample at 70F and 29.92 in. Hg

Vm = Volume (ft³) of gas at meter conditions

Tm = Average dry gas meter temperature (R)

$Pbar$ = Barometric pressure (in. Hg)

ΔH = Pressure drop across orifice (in. WG)

$$Vmstd = 17.71 * 56.48 * (23.99 + 0.401 / 13.6) / 553.9 = 43.376 \text{ ft}^3$$

VOLUME OF WATER VAPOR

$$Vwstd = (0.0474 \text{ ft}^3/\text{ml}) * Vlc$$

Where $Vwstd$ = Volume (ft³) of water vapor

Vlc = Total volume of water collected (ml)

$$Vwstd = .00474 * 133.4 = 6.323 \text{ ft}^3$$

MOISTURE CONTENT

$$Bwc = Vwstd * 100 / (Vwstd + Vmstd)$$

Where Bwc = Percent moisture

$$Bwc = 6.32 * 100 / (6.32 + 43.38) = 12.723 \text{ percent}$$

CONCENTRATION

$$Cs' = (15.43 \text{ grains/gm}) * Mn / (Vmstd + Vwstd)$$

Where Cs' = Concentration (grains/scf)

Mn = Total particulate collected (gm)

$$Cs' = 15.43 * 0.2327 / (43.38 + 6.32) = 0.0722 \text{ grains/scf}$$

STACK VELOCITY

Where V = Stack velocity (ft/sec)

Ts = Stack absolute temperature (R)

ΔP = Average pitot reading (in. WG)

Mw = Molecular wt. of stack gas (lb/lb mole)

Kp = Pitot tube coefficient

$$Mw = 0.13 * 12.72 + 0.44 * 0.96 + 0.32 * 13.18 + 0.25 * 73.14 = 27.408 \text{ lb/mole}$$

$$RA-22A \quad V = 0.84 * 85.48 * 0.558 * \text{SQRT}(583.6 / (27.41 * 23.99)) = 38.423 \text{ ft/sec}$$

$$RA-22B \quad V = 0.84 * 85.48 * 0.708 * \text{SQRT}(586.4 / (27.41 * 23.99)) = 48.008 \text{ ft/sec}$$

STACK VOLUME

$$ACFM = V * A * 60 \quad \text{AND} \quad SCFM = ACFM * 530 * Ps / (Ts * 29.92)$$

Where $ACFM$ = Actual cubic ft per minute at stack conditions

A = Stack area (ft²)

$SCFM$ = Standard cubic ft. per min. (29.92 in. Hg & 530 R)

$$RA-22A \quad ACFM = 38.42 * 9.621 * 60 = 22180 \text{ acfm}$$

$$RA-22B \quad ACFM = 48.01 * 9.621 * 60 = 27713 \text{ acfm}$$

$$RA-22A \quad SCFM = 22180 * 530 * 23.99 / (583.6 * 29.92) = 16151 \text{ scfm}$$

$$RA-22B \quad SCFM = 27713 * 530 * 23.99 / (586.4 * 29.92) = 20083 \text{ scfm}$$

CALCULATED DUST LOAD

$$\text{lb/hr} = Cs' * SCFM * 60 / 7000 \text{ grains/lb}$$

$$\text{DUST LOAD} = 0.0722 * 36234 * 60 / 7000 = 22.44 \text{ lb/hr}$$

ISOKINETIC RATE

LABORATORY DATA

Company FMC WYO
 Sampling Location RA 22A-B

Run No.: 88-06-S-P
 Date: 5-24-88

MOISTURE COLLECTED

		GM/ML	Water Weight/Volume Gain GM/ML
IMPINGER 1	Final Weight/Volume	<u>661.8</u>	
	Initial Weight/Volume	<u>552.9</u>	
	Increase	<u>108.9</u>	<u>108.9</u>
IMPINGER 2	Final Weight/Volume	<u>555.7</u>	
	Initial Weight/Volume	<u>544.3</u>	
	Increase	<u>11.4</u>	<u>11.4</u>
IMPINGER 3	Final Weight/Volume	<u>440.7</u>	
	Initial Weight/Volume	<u>439.2</u>	
	Increase	<u>1.5</u>	<u>1.5</u>
IMPINGER 4	Final Weight/Volume	<u>655.1</u>	
	Initial Weight/Volume	<u>643.5</u>	
	Increase	<u>11.6</u>	<u>11.6</u>
TOTAL MOISTURE CATCH			<u>133.4</u> ✓

PARTICULATE COLLECTED

FRONT-HALF ANALYSIS (Nozzle, Probe, Cyclone, Filter Front-Half)

Filter & Particulates	<u>0.7700</u>
Filter Tare Weight	<u>0.5978</u>
Particulate	<u>0.1922</u>
Washings	<u>0.0400</u>
Particulate Catch	<u>0.2322</u>
Acetone Blank	<u>- 0 -</u>
TOTAL FRONT CATCH	<u>0.2322</u>

BACK-HALF ANALYSIS (Impingers, Filter Back-Half)

1BH Extractable Weight	<u>75.5480</u>
Boil Down Weight	<u>75.5475</u>
Impinger Catch	<u>0.0005</u>
Water Blank	<u>- 0 -</u>
TOTAL BACK CATCH	<u>0.0005</u>
TOTAL TRAIN CATCH	<u>0.2327</u> ✓

15

75.1200
 75.0800

0.0400

1B
 74.9800
 74.9800

0.0000

STACK SAMPLING FIELD DATA

Company SMC Wy Corp

Plant Location Green River, WY.

Run No. 88-07-S-P

Sampling Location R9 RA-22AB

Date 05/25/88

Start Time 09:53

Finish Time 10:28

Filter No. _____

Assumed Moisture, % 10

Probe Tip Diameter, in. 18

Probe Length, ft. 5

Ambient Temperature, °F _____

Bar. Pressure, in. Hg. 24.06

Initial Leak Check, CFS
CFM 0.004 at 15 in. Hg.

Final Leak Check, CFS
CFM _____ at _____ in. Hg.

RA-22A West X-27

Point No.	Time (min)	Dry Gas Meter FT ³	Pitot in. H ₂ O		Orifice ΔH in. H ₂ O		Dry Gas Temp. °F		Pump Vacuum in. Hg Gauge	Sample Box Temp. °F	Impinger Temp. °F	Stack Press. in. Hg	Stack Temp. °F
			P	VP	Desired	Actual	Inlet	Outlet					
1	0	519.290	.12	0.346	0.11	0.11	58	53	1.8	231	69	—	119
2	2	519.7	.14	0.374	0.12	0.12	59	54	1.7	230	66	—	119
3	4	520.2	.16	0.400	0.14	0.14	61	55	1.7	238	64	—	118
4	6	520.7	.12	0.346	0.11	0.11	63	57	1.6	236	64	—	118
5	8	521.1	.03	0.173	0.03	0.03	63	59	0	237	66	—	119
6	10	521.3	.03	0.173	0.03	0.03	63	59	0	243	66	—	118
7	12	521.4	.03	0.173	0.03	0.03	64	61	0	240	67	—	118
8	14	521.6	.03	0.173	0.03	0.03	65	61	0	238	67	—	118
9	16	521.8	.03	0.173	0.03	0.03	67	63	0	242	67	—	118
10	18	522.0	.29	0.538	0.25	0.25	71	64	2.1	241	64	—	118
11	20	522.6	.47	0.685	0.41	0.41	76	65	2.8	243	60	—	119
12	22	523.4	.52	0.701	0.45	0.45	79	67	3.0	243	58	—	119
13	24	524.3	.52	0.701	0.45	0.45	81	68	3.0	245	56	—	118
14	26	525.1	.51	0.714	0.44	0.44	82	69	3.0	250	55	—	118
15	28	525.9	.48	0.693	0.41	0.41	83	70	2.9	248	54	—	118
16	30	526.8	.46	0.678	0.40	0.40	84	72	2.9	247	54	—	118
17	32	527.6	.46	0.678	0.40	0.40	85	73	2.9	249	54	—	118
18	34	528.4	.46	0.678	0.40	0.40	86	74	2.9	252	55	—	117
	36	529.2											

889/48.558: 50.447

21.810 x 1.07457
22.658
0.568

Orsat
%CO₂ = 1.4
%CO = 12.6
%O₂ = 0.0

Stack Area: 9.651
Water 123.2
Catch = 0.1952

578.8

total Vm 50.447 18.24 9.74 77.5°F 5578
average 0.507 ΔH 0.271 537.5°F 5784

Avg. ΔH = 0.334 Avg. Tm = 548.1°F

STACK SAMPLING FIELD DATA

Company FMCW, Corp.

Plant Location Green River, WY

Run No. 88-07-S-P

Sampling Location R-9 RA-22A-B

Date 05/25/88

Start Time 10:47

Finish Time

Filter No. _____

Assumed Moisture, % 10

Probe Tip Diameter, in. .078

Probe Length, ft. 5

Ambient Temperature, °F

Bar. Pressure, in. Hg. 24.06

Initial Leak Check, CFS _____
CFM at in. Hg

Final Leak Check, CFS _____
CFM _____ at _____ in. Hg

RA-22A West X-27

[illegible]

Assumed Moisture, % 10

Probe Tip Diameter, in. 1/8

Probe Length, ft. 5

Ambient Temperature, °F

Bar. Pressure, in. Hg. 24.06

Initial Leak Check, CFS

CFM at in. Hg

Final Leak Check, CFS

CFM. at in. Hg

RA-22B EAST X-26

[illegible]

STACK SAMPLING FIELD DATA

Company fmc Wy. Corp.

Assumed Moisture, % 10

Plant Location Green River, WY

Probe Tip Diameter, in. .18

Run No. 88-07-S-P .

Probe Length, ft. 5

Sampling Location R-9 RA-22A-B

Ambient Temperature, °F _____

Date 05/25/88

Bar. Pressure, in. Hg. 24.06

Start Time 12:21

Initial Leak Check, CFS _____
CFM _____ at _____ in. Hg.

Finish Time 13:03

Final Leak Check, CFS
CFM 2.00 / at 5.0 in. Hg.

Filter No. _____

RA-22B EAST X-26

[illegible]

TEST NO. 88-07-S-P

DATE 05/25/88

VELOCITY AND VOLUME DETERMINATION

DRY GAS VOLUME

$$Vmstd = (17.71 \text{ deg R/in. Hg}) * Vm * (Pbar + \Delta H / 13.6) / Tm$$

Where Vmstd=Volume(ft3) of gas sample at 70F and 29.92 in. Hg

Vm=Volume (ft3) of gas at meter conditions

Tm=Average dry gas meter temperature (R)

Pbar=Barometric pressure (in. Hg)

deltaH=Pressure drop across orifice (in. WG)

$$Vmstd = 17.71 * 50.45 * (24.06 + 0.334 / 13.6) / 548.1 = 39.258 \text{ ft}^3$$

VOLUME OF WATER VAPOR

$$Vwstd = (0.0474 \text{ ft}^3/\text{ml}) * Vlc$$

Where Vwstd=Volume (ft3) of water vapor

Vlc=Total volume of water collected (ml)

$$Vwstd = .00474 * 123.2 = 5.840 \text{ ft}^3$$

MOISTURE CONTENT

$$Bwc = Vwstd * 100 / (Vwstd + Vmstd)$$

Where Bwc=Percent moisture

$$Bwc = 5.84 * 100 / (5.84 + 39.26) = 12.949 \text{ percent}$$

CONCENTRATION

$$Cs' = (15.43 \text{ grains/gm}) * Mn / (Vmstd + Vwstd)$$

Where Cs'=Concentration (grains/scf)

Mn=Total particulate collected (gm)

$$Cs' = 15.43 * 0.1952 / (39.26 + 5.84) = 0.0668 \text{ grains/scf}$$

STACK VELOCITY

Where V=Stack velocity (ft/sec)

Ts=Stack absolute temperature (R)

deltaP=Average pitot reading (in. WG)

Mw=Molecular wt. of stack gas (lb/lb mole)

Kp=Pitot tube coefficient

$$Mw = 0.18 * 12.95 + 0.44 * 1.22 + 0.32 * 10.97 + 0.28 * 74.86 = 27.339 \text{ lb/mole}$$

$$RA-22A \quad V = 0.84 * 85.48 * 0.507 * \sqrt{578.4 / (27.34 * 24.06)} = 34.137 \text{ ft/sec}$$

$$RA-22B \quad V = 0.84 * 85.48 * 0.629 * \sqrt{579.1 / (27.34 * 24.06)} = 42.377 \text{ ft/sec}$$

STACK VOLUME

$$ACFM = V * A * 60 \quad \text{AND} \quad SCFM = ACFM * 530 * Ps / (Ts * 29.92)$$

Where ACFM=Actual cubic Ft per minute at stack conditions

A=Stack area (ft2)

SCFM=Standard cubic ft. per min. (29.92 in. Hg & 530 R)

$$RA-22A \quad ACFM = 34.14 * 9.621 * 60 = 19706 \text{ acfm}$$

$$RA-22B \quad ACFM = 42.38 * 9.621 * 60 = 24463 \text{ acfm}$$

$$RA-22A \quad SCFM = 19706 * 530 * 24.06 / (578.4 * 29.92) = 14520 \text{ scfm}$$

$$RA-22B \quad SCFM = 24463 * 530 * 24.06 / (579.1 * 29.92) = 18004 \text{ scfm}$$

CALCULATED DUST LOAD

$$\text{lb/hr} = Cs' * SCFM * 60 / 7000 \text{ grains/lb}$$

$$\text{DUST LOAD} = 0.0668 * 32524 * 60 / 7000 = 18.62 \text{ lb/hr}$$

ISOKINETIC RATE

$$I = 105.3018 \%$$

2

LABORATORY DATA

Company _____

Run No. 88-07-S-4

Sampling Location R#22A-B

Date 5-25-88

MOISTURE COLLECTED

		GM/ML	Water Weight/Volume Gain GM/ML
IMPINGER 1	Final Weight/Volume	<u>682.7</u>	
	Initial Weight/Volume	<u>579.1</u>	
	Increase	<u>103.6</u>	<u>103.6</u>
IMPINGER 2	Final Weight/Volume	<u>555.7</u>	
	Initial Weight/Volume	<u>546.4</u>	
	Increase	<u>9.3</u>	<u>9.3</u>
IMPINGER 3	Final Weight/Volume	<u>435.6</u>	
	Initial Weight/Volume	<u>434.2</u>	
	Increase	<u>1.4</u>	<u>1.4</u>
IMPINGER 4	Final Weight/Volume	<u>643.0</u>	
	Initial Weight/Volume	<u>634.1</u>	
	Increase	<u>8.9</u>	<u>8.9</u>
	TOTAL MOISTURE CATCH		<u>123.2</u>

PARTICULATE COLLECTED

FRONT-HALF ANALYSIS (Nozzle, Probe, Cyclone, Filter Front-Half)

25	74.3840	Filter & Particulates	<u>0.6890</u>
	74.3486	Filter Tare Weight	<u>0.5342</u>
	<u>.0354</u>	Particulate	<u>0.1548</u>
		Washings	<u>0.0354</u>
		Particulate Catch	<u>0.1902</u>
		Acetone Blank	<u>0.0024</u>
		TOTAL FRONT CATCH	<u>0.1878</u>

~~Acetone Blank~~
~~one~~
~~not milled~~

BACK-HALF ANALYSIS (Impingers, Filter Back-Half)

2B	74.7540	Extractable Weight	<u>75.4690</u>
	74.7516	Boil Down Weight	<u>75.4526</u>
	<u>.0024</u>	Impinger Catch	<u>0.0074</u>
		Water Blank	<u>X</u>
		TOTAL BACK CATCH	<u>0.0074</u>
		TOTAL TRAIN CATCH	<u>0.1952</u>

Separate
blanks for
each impinger
of dedicated
water bottles

STACK SAMPLING FIELD DATA

Company SMCWy Corp. Assumed Moisture, % 10
 Plant Location Green River Wy. Probe Tip Diameter, in. .18
 Run No. 88-08-S-P Probe Length, ft. 5
 Sampling Location RA-22 A+B R-9 Ambient Temperature, °F _____
 Date 5-26-88 Bar. Pressure, in. Hg. 24.00
 Start Time 10:03 Initial Leak Check, CFS _____
 Finish Time 10:39 CFM 2.00 at 15 in. Hg.
 Filter No. _____ Final Leak Check, CFS _____
 CFM _____ at _____ in. Hg.

RA-22 B "EAST" X-26

Point No. West Port	Time (min)	Dry Gas Meter FT ³	Pitot in. H ₂ O		Orifice ΔH in. H ₂ O		Dry Gas Temp. OF		Pump Vacuum in. Hg Gauge	Sample Box Temp. OF	Impinger Temp. OF 740F	Stack Press. in. Hg	Stack Temp. OF
			P	VP	in. H ₂ O		Inlet 63	Outlet 62					
					Desired	Actual							
					*								
1	0	568.864	0.29	0.538	0.25	0.25	66	61	2.6	227	73		121
2	2	569.5	0.31	0.557	0.27	0.27	67	62	2.7	236	72		120
3	4	570.1	0.25	0.500	0.22	0.22	70	63	2.2	235	71		120
4	6	570.7	0.21	0.458	0.18	0.18	71	64	2.0	243	70		121
5	8	571.2	0.24	0.490	0.21	0.21	73	66	2.2	256	69		122
6	10	571.8	0.25	0.500	0.22	0.22	75	67	2.2	240	68		121
7	12	572.4	0.21	0.458	0.18	0.18	76	68	2.1	239	68		121
8	14	573.0	0.15	0.387	0.13	0.13	77	69	2.0	243	68		121
9	16	573.4	0.14	0.374	0.12	0.12	78	70	2.0	235	69		123
10	18	573.9	0.39	0.624	0.33	0.33	62	72	3.0	243	67		121
11	20	574.6	0.60	0.894	0.69	0.69	87	73	4.2	246	64		121
12	22	575.6	0.90	0.949	0.78	0.78	89	74	4.7	249	62		121
13	24	576.7	0.90	0.949	0.78	0.78	90	76	4.9	256	61		121
14	26	577.8	0.89	0.943	0.77	0.77	92	77	4.9	256	60		121
15	28	578.9	0.82	0.905	0.71	0.71	92	78	4.6	257	60		120
16	30	580.0	0.83	0.911	0.71	0.71	93	79	4.6	249	61		120
17	32	581.0	0.83	0.911	0.71	0.71	94	80	4.6	242	61		120
18	34	582.1	0.83	0.911	0.71	0.71	95	81	4.8	253	62		121
	36	583.2			*								
50.467 10389 48.577 50.423 74.876 21.093 79.958 70.529 60.467 0.566 0.150 %CO₂ = 1.3 %O₂ = 15.1 %CO = 0.0 Stack Area = 9.621 Water = 140.9 Catch = 0.2015													

Avg. ΔH = 0.358 Avg. Tm = 553.4

Company fmc Wy. Corp.

Assumed Moisture, % 10

Plant Location Green River, WY

Probe Tip Diameter, in. .18

Run No. 88-08-S-P

Probe Length, ft. 5

Sampling Location RA-22 A+B

Ambient Temperature, OF _____

Date 5-26-88

Bar. Pressure, in. Hg. 24.00

Start Time 10:54

Initial Leak Check, CFS _____
CFM _____ at _____ in. Hg.

Finish Time 11:30

Final Leak Check, CFS _____
CFM _____ at _____ in. Hg.

Filter No. _____

RA-22 B "EAST" X-26

[illegible]

STACK SAMPLING FIELD DATA

Company FMC Wy. Corp.

Assumed Moisture, % 10

Plant Location Green River Wy.

Probe Tip Diameter, in. .18

Run No. 88-08-S-P

Probe Length, ft. 5

Sampling Location RA-22 A+B R-9

Ambient Temperature, °F

Date 05-26-88

Bar. Pressure, in. Hg. 24.00

Start Time 11:50

Initial Leak Check, CFS

Finish Time 12:26

CFM at in. Hg.

Filter No.

Final Leak Check, CFS

RA-22 A "West" X-27

Point No. East Port	Time (min)	Dry Gas Meter FT ³	Pitot in. H ₂ O		Orifice ΔH in. H ₂ O		Dry Gas Temp. OF		Pump Vacuum in. Hg Gauge	Sample Box Temp. OF	Impinger Temp. OF	Stack Press. in. Hg	Stack Temp. OF
			P	VP	Desired	Actual	Inlet	Outlet					
1	0	597.7	.12	0.346	.11	.11	98	96	2.1	243	91		117
2	2	598.4	.12	0.346	.11	.11	99	96	2.1	253	89		118
3	4	598.8	.12	0.346	.11	.11	99	97	2.1	254	88		119
4	6	599.3	.11	0.332	.10	.10	100	97	2.1	255	87		119
5	8	599.7	.08	0.283	.07	.07	99	97	1.0	248	85		117
6	10	600.0	.04	0.200	.03	.03	98	97	0.5	267	85		120
7	12	600.3	.02	0.141	.01	.01	98	97	0.6	251	85		120
8	14	600.5	.02	0.141	.01	.01	98	97	0.8	248	85		119
9	16	600.7	.02	0.141	.01	.01	98	98	0.8	255	85		119
10	18	601.0	.21	0.458	.18	.18	100	98	2.9	252	82		120
11	20	601.5	.45	0.671	0.39	0.39	105	98	3.8	249	76		121
12	22	602.4	.48	0.693	0.42	0.42	106	98	4.0	255	75		120
13	24	603.2	.47	0.686	0.41	0.41	107	99	4.0	261	75		120
14	26	604.0	.45	0.671	0.39	0.39	108	99	4.0	246	75		119
15	28	604.8	.42	0.648	0.36	0.36	108	99	3.8	246	76		119
16	30	605.6	.42	0.648	0.36	0.36	108	100	3.8	248	75		119
17	32	606.4	.42	0.648	0.36	0.36	109	100	3.8	245	75		118
18	34	607.2	.42	0.648	0.36	0.36	109	101	3.8	259	75		118
	36	608.0											
70509													
											</		

Company fmc wy. Corp.

Assumed Moisture, % 10

Plant Location Green River WY

Probe Tip Diameter, in. .18

Run No. 88-08-S-P

Probe Length, ft. 5

Sampling Location RA-22 A+B R-9

Ambient Temperature, °F _____

Date 5-26-88

Bar. Pressure, in. Hg. 24.00

Start Time 12:39

Initial Leak Check, CFS

Finish Time 13:15

CFM _____ at _____ in. Hg.

Filter No.

Final Leak Check, CFS CFM, 004 at 5.5 in. Hg.

RA-22A "West" X-27

[illegible]

VELOCITY AND VOLUME DETERMINATION

DRY GAS VOLUME

$$Vmstd = (17.71 \text{ deg R/in. Hg}) * Vm * (Pbar + \Delta H / 13.6) / Tm$$

Where $Vmstd$ = Volume (ft³) of gas sample at 70F and 29.92 in. Hg Vm = Volume (ft³) of gas at meter conditions Tm = Average dry gas meter temperature (R) $Pbar$ = Barometric pressure (in. Hg) ΔH = Pressure drop across orifice (in. WG)

$$Vmstd = 17.71 * 50.42 * (24.00 + 0.328 / 13.6) / 553.4 = 38.766 \text{ ft}^3$$

VOLUME OF WATER VAPOR

$$Vwstd = (0.0474 \text{ ft}^3/\text{ml}) * Vlc$$

Where $Vwstd$ = Volume (ft³) of water vapor Vlc = Total volume of water collected (ml)

$$Vwstd = .00474 * 140.9 = 6.679 \text{ ft}^3$$

MOISTURE CONTENT

$$Bwo = Vwstd * 100 / (Vwstd + Vmstd)$$

Where Bwo = Percent moisture

$$Bwo = 6.68 * 100 / (6.68 + 38.77) = 14.696 \text{ percent}$$

CONCENTRATION

$$Cs' = (15.43 \text{ grains/gm}) * Mn / (Vmstd + Vwstd)$$

Where Cs' = Concentration (grains/scf) Mn = Total particulate collected (gm)

$$Cs' = 15.43 * 0.2015 / (38.77 + 6.68) = 0.0684 \text{ grains/scf}$$

STACK VELOCITY

Where V = Stack velocity (ft/sec) Ts = Stack absolute temperature (R) ΔP = Average pitot reading (in. WG) Mw = Molecular wt. of stack gas (lb/lb mole) Kp = Pitot tube coefficient

$$Mw = 0.18 * 14.70 + 0.44 * 1.11 + 0.32 * 12.88 + 0.28 * 71.31 = 27.223 \text{ lb/mole}$$

$$\text{RA-22A } V = 0.84 * 85.48 * 0.449 * \text{SQRT}(579.9 / (27.22 * 24.00)) = 30.373 \text{ ft/sec}$$

$$\text{RA-22B } V = 0.84 * 85.48 * 0.682 * \text{SQRT}(580.5 / (27.22 * 24.00)) = 46.159 \text{ ft/sec}$$

STACK VOLUME

$$ACFM = V * A * 60 \quad \text{AND} \quad SCFM = ACFM * 530 * Ps / (Ts * 29.92)$$

Where $ACFM$ = Actual cubic Ft per minute at stack conditions A = Stack area (ft²) $SCFM$ = Standard cubic ft. per min. (29.92 in. Hg & 530 R)

$$\text{RA-22A } ACFM = 30.37 * 9.621 * 60 = 17533 \text{ acfm}$$

$$\text{RA-22B } ACFM = 46.16 * 9.621 * 60 = 26646 \text{ acfm}$$

$$\text{RA-22A } SCFM = 17533 * 530 * 24.00 / (579.9 * 29.92) = 12854 \text{ scfm}$$

$$\text{RA-22B } SCFM = 26646 * 530 * 24.00 / (580.5 * 29.92) = 19514 \text{ scfm}$$

CALCULATED DUST LOAD

$$\text{lb/hr} = Cs' * SCFM * 60 / 7000 \text{ grains/lb}$$

$$\text{DUST LOAD} = 0.0684 * 32368 * 60 / 7000 = 18.98 \text{ Lb/Hr}$$

ISOKINETIC RATE

$$I = 106.619 \%$$

LABORATORY DATA

Company FMC

Run No. 88-08-S-P

Sampling Location RA 22A B

Date 5-26-88

MOISTURE COLLECTED

		GM/ML	Water Weight/Volume Gain GM/ML
IMPINGER 1	Final Weight/Volume	685.2	
	Initial Weight/Volume	565.4	
	Increase	119.8	119.5
IMPINGER 2	Final Weight/Volume	576.4	
	Initial Weight/Volume	565.9	
	Increase	10.5	10.5
IMPINGER 3	Final Weight/Volume	449.4	
	Initial Weight/Volume	448.3	
	Increase	1.1	1.1
IMPINGER 4	Final Weight/Volume	626.9	
	Initial Weight/Volume	617.1	
	Increase	9.8	9.8
	TOTAL MOISTURE CATCH		140.9

PARTICULATE COLLECTED

FRONT-HALF ANALYSIS (Nozzle, Probe, Cyclone, Filter Front-Half)

35

75.6571
75.6250
0.0321

Filter & Particulates	0.7072
Filter Tare Weight	0.5317
Particulate	0.1755
Washings	0.0321
Particulate Catch	0.2076
Acetone Blank	0.0003

TOTAL FRONT CATCH 0.2073

BACK-HALF ANALYSIS (Impingers, Filter Back-Half)

3B

73.7849
73.7846
0.0003

3BH

Extractable Weight	73.3101
Boil Down Weight	73.3059
Impinger Catch	0.0042
Water Blank	0.0000

TOTAL BACK CATCH 0.0042

TOTAL TRAIN CATCH 0.2115

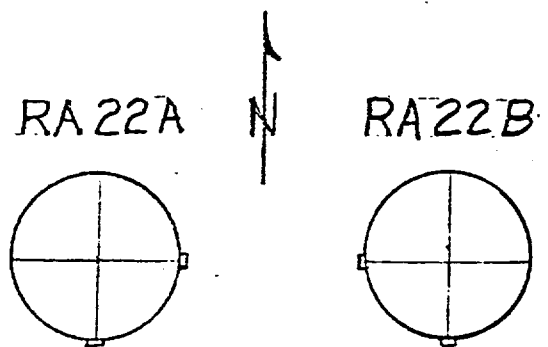
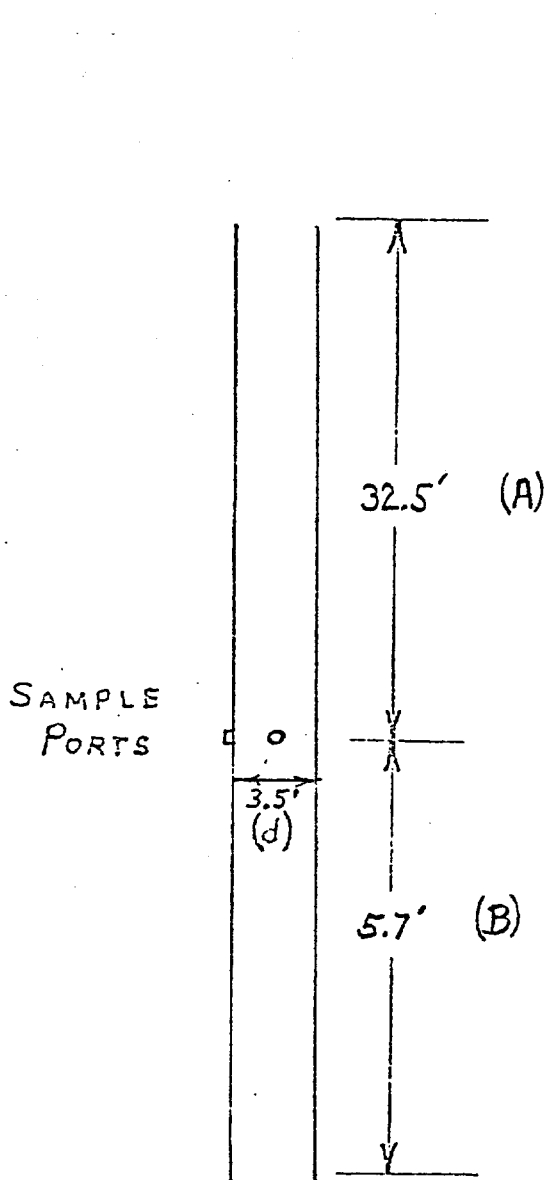
Section A-2, Information

- Drawing showing location of sample ports and number of points per traverse

FMC Corporation

Industrial Chemical Division
Box 872
Green River Wyoming 82935
(307) 875 2580

RA 22 A & B



$$\frac{B}{d} = 1.6$$

NO. OF POINTS PER TRAVERSE = 36*
NO. OF POINTS PER DIAMETER = 18
NO. OF DIAMETERS PER RUN = 4 (2 EACH DUCT)
SAMPLE TIME PER POINT = 2 MINUTES

TRAVERSE POINTS ON EACH DIAMETER

	% OF DIAMETER	DISTANCE FROM INSIDE WALL (IN.)	DISTANCE FROM COUPLING (IN.)
1	1.4	1.00**	4.00**
2	4.4	1.84	4.84
3	7.5	3.15	6.15
4	10.9	4.58	7.58
5	14.6	6.13	9.13
6	18.8	7.90	10.90
7	23.6	9.91	12.91
8	29.6	12.43	15.43
9	38.2	16.04	19.04
10	61.8	25.96	28.96
11	70.4	29.57	32.57
12	76.4	32.09	35.09
13	81.2	34.10	37.10
14	85.4	35.87	38.87
15	89.1	37.42	40.42
16	92.5	38.85	41.85
17	95.6	40.15	43.15
18	98.6	41.00**	44.00**

* VERBAL FROM WOODY RUSSELL
ON MARCH 1, 1977

** ADJUSTED TO MAINTAIN
1 INCH MINIMUM FROM WALL

H
~~John~~
John
with:-

June 15, 1988

FMC

RECEIVED

JUN 16 1988

ALL QUALITY BOOKS

LANDER WYOMING

Dear Mr. Gribovicz:

Included in this report is the following information:

- Summary of the test results
- Sampling and analysis procedures
- Appendix which includes:
 - o Field data
 - o Laboratory worksheet
 - o Calculations for each test
- Diagram showing
 - o Location of sample ports
 - o Location and number of sample points in each diameter

A CONFIDENTIAL Section is included with the report which contains the control room logsheets of operating parameters monitored during the testwork. As provided for in § 35-11-1101 of the Wyoming Environmental Quality Act, we consider this information to be trade secret and proprietary as it is not available to the public or our competitors. We would appreciate you treating it as such.

Mr. Lee Gribovicz
June 15, 1988

Page 2

If you have any questions concerning this report, or need any additional information, give me a call.

Yours very truly,



Carl R. Demshar, Jr.
Environmental Manager

jc

cc: Charles Collins, DEQ - Cheyenne
JW Coykendall*, JF Herink* - Green River

* Summary Table I included with cover letter.

COMPLIANCE TEST REPORT

EMISSION SOURCE RA-23 A&B

FMC WYOMING CORPORATION

GREEN RIVER, WYOMING

June 15, 1988

COMPLIANCE TEST REPORT

EMISSION SOURCE: RA-23 A&B

FMC WYOMING CORPORATION
GREEN RIVER, WYOMING

TEST DATE: JUNE 1 and 2, 1988
REPORT DATE: JUNE 15, 1988

COMPLIANCE TEST REPORT
EMISSION SOURCE: RA-23 A&B

Section

Introduction

Summary of Results

Sampling and Analysis Procedures

Calculation of Production Rate, and Control Room Logsheets
(Included in separate packet marked "CONFIDENTIAL")

APPENDIX

Section A-1 Test Data

- Field Data Sheets
- Laboratory Data Sheets
- Test Calculations
- Preliminary Test Data

Section A-2, Stack Information

- Drawing showing location of sample ports, and locations of sampling points per traverse.

Introduction

In an effort to demonstrate compliance of emission source RA-23 A&B, emission tests were run on June 1 and 2, 1988.

FMC Wyoming Corporation personnel taking part in the testwork were:

Ted Brown	Environmental Engineer
Simon Lee	Environmental Engineering Aide
Kieth Norris	Senior Laboratory Analyst

Summary of Results

This section summarizes the results of the compliance tests performed on emission source RA-23 A&B. Table I is a general summary showing the individual test results in relation to the maximum allowable emission for this source. Table II is a summary of the results obtained from each compliance test. Details of the individual tests, including field data sheets, laboratory data sheets, and calculation sheets can be found in the Appendix.

From Table I, it can be seen that the individual test results, as well as the three-test average, are well below the allowable emission rate for this particular unit.

TABLE I

Comparison of Compliance Test Results
With Allowable Emission Rates

<u>Emission Source</u>	<u>Test Number</u>	<u>Emission Rate, lb/hr</u>	
		<u>Compliance Test</u>	<u>Allowable</u>
RA-23 A&B	88-09-S-P	31.3	35.0
RA-23 A&B	88-10-S-P	28.2	35.0
RA-23 A&B	88-11-S-P	<u>28.8</u>	<u>35.0</u>
	Average:	29.4	35.0

TABLE II

SUMMARY OF STACK SAMPLING CALCULATIONSStack: RA-23 A & B

	TEST 1 -----	TEST 2 -----	TEST 3 -----
Test Code Number	88-09-SP	88-10-SP	88-11-SP
Barometric Pressure at site, (in Hg)	24.04	24.04	24.17
Absolute stack gas pressure, (in Hg)	24.04	24.04	24.17
Absolute average stack gas temp. A, (R)	607.7	606.4	598.4
Absolute average stack gas temp. B, (R)	607.1	604.5	599.1
Absolute average dry gas meter temp., (R)	546.8	561.2	556.3
Total volume of water collected, (ml)	423.8	421.0	438.0
Volume of gas through dry gas meter, (ft ³)	74.865	76.449	76.431
Average pressure drop across orifice, (in H ₂ O)	0.847	0.855	0.846
Pitot tube coefficient	0.84	0.84	0.84
Average velocity head of stack gas A, (in H ₂ O)	1.230	1.205	1.240
Average velocity head of stack gas B, (in H ₂ O)	1.023	1.067	1.014
Cross sectional area of stack, (ft ²)	7.069	7.069	7.069
Front half particulate collected, (gm)	0.3934	0.3670	0.3646
Back half particulate collected, (gm)	0.0007	0.0006	0.0001
Total particulate collected, (gm)	0.3941	0.3676	0.3647
Total sampling time, (min)	128	128	128
Cross sectional area of nozzle, (ft ² *10 ⁻⁴)	1.7672	1.7672	1.7672
Gas volume A, (acfm)	36723	36267	36619
Gas volume B, (acfm)	30528	32063	29962
Gas volume A, (scfm)	25733	25468	26200
Gas volume B, (scfm)	21413	22587	21412
Percent isokinetic	104.56	108.21	105.12
Emission rate, (lb/hr)	31.29	28.20	28.81

Sampling and Analysis Procedure

Compliance testing on emission source RA-23 A&B was conducted on June 1 and 2 using EPA Method No. 5, "Determination of Particulate Emissions from Stationary Sources". This unit consists of two stacks, RA-23A and RA-23B. Each emission test consisted of traversing two sample diameters in each stack with 16 points being sampled on each diameter. Each point was sampled for two minutes resulting in a sample time of 64 minutes for each stack, with the total time for each emission sample being 128 minutes. One sample train was used for each emission test. Figure 1, located in Section A-2 of the Appendix, shows the location of the sample ports in relation to the nearest flow disturbance (an expansion, contraction, or bend in the stack). This diagram also shows the location of the sample points in each sample diameter.

Control room logsheets, containing operating data pertinent to the unit during the testwork, can be found in the Confidential Section of this report.

Calculation of Production Rate:

Emission Source: RA-23 A&B

Test Date: June 1, and 2, 1988

Test No. 88-09-S-P	29.4 tons per hour
Test No. 88-10-S-P	30.9 tons per hour
Test No. 88-11-S-P	31.3 tons per hour

Details of these calculations, along with the control room logsheets which contain the data used in these calculations, can be found in the Confidential packet.

APPENDIX

Section A-1, Test Data

- Field Data Sheets
- Laboratory Data Sheets
- Test Calculations
- Preliminary Test Data

STACK SAMPLING FIELD DATA

Company FMC W. Corp.
 Plant Location Green River, W. Y.
 Run No. 88-09-S-P
 Sampling Location RA-23A+B
 Date 6-1-88
 Start Time 09:42 / 10:21
 Finish Time 10:14 / 10:53
 Filter No. _____

Assumed Moisture, % 20
 Probe Tip Diameter, in. .18 (1.76715)
 Probe Length, ft. 5
 Ambient Temperature, °F _____
 Bar. Pressure, in. Hg. 24.04
 Initial Leak Check, CFS _____
 CFM .012 at 15 in. Hg.
 Final Leak Check, CFS _____
 CFM _____ at _____ in. Hg.

RA-23A "West" X-13

Point No.	Time (min)	Dry Gas Meter FT ³	Pitot in. H ₂ O		Orifice ΔH in. H ₂ O		Dry Gas Temp. °F		Pump Vacuum in. Hg Gauge	Sample Box Temp. °F	Impinger Temp. °F	Stack Press. in. Hg	Stack Temp. °F
			P	VP	Desired	Actual	Inlet	Outlet					
South													
1	0	629.910	1.15	1.012	0.75	0.75	65	55	3.4	230	47		116
2	4	631.9	1.2	1.095	0.79	0.79	72	58	4.2	237	46		149
3	8	634.0	1.5	1.25	0.98	0.98	76	61	5.2	240	43		157
4	12	636.3	1.8	1.342	1.18	1.18	79	63	6.0	233	45		151
5	16	638.9	1.9	1.378	1.24	1.24	82	66	7.0	247	45		153
6	20	641.6	2.2	1.483	1.44	1.44	84	68	8.3	246	44		156
7	24	644.5	2.1	1.449	1.38	1.38	85	70	9.0	239	45		150
8	28	647.4	2.1	1.449	1.38	1.38	86	72	9.0	256	46		150
	32	650.3											
North													
1	0	650.3	0.89	0.943	0.59	0.59	83	75	4.5	247	53		145
2	4	652.3	1.05	1.025	0.69	0.69	87	77	5.0	244	51		150
3	8	654.3	1.3	1.140	0.85	0.85	90	78	6.0	245	48		147
4	12	656.6	1.45	1.204	0.95	0.95	91	79	6.8	244	48		147
5	16	659.0	1.60	1.265	1.05	1.05	92	80	7.2	243	45		144
6	20	661.5	1.50	1.225	0.98	0.98	93	81	7.1	238	46		143
7	24	664.0	1.45	1.204	0.95	0.95	93	81	7.1	243	48		150
8	28	666.4	1.40	1.183	0.92	0.92	94	82	7.2	245	51		153
	32	668.8											
1.0389 x 72.06 = 74.865													
ORSAT													
%CO ₂ = 3.6													
%O ₂ = 14.5													
%CO = 0.0													
Stack Area = 700													
Water = 455.8													
424.1													
2478													
78.1°F													
538.1°R													
147.7°F													
607.7°F													
total V _m 74.865													
VP 1.230													
ΔH 1.008													

Aug. ΔH 0.847

Aug. Tm: 546.8°R

Company fmc Wy. Corp.

Assumed Moisture, % 20

Plant Location Green River, W.V.

Probe Tip Diameter, in. .18

Run No. 88-09-S-P.

Probe Length, ft. 5

Sampling Location RA-23 A+B R-13

Ambient Temperature, °F

Date 6-1-88

Bar. Pressure, in. Hg.

Start Time 11:04 / 11:45

Initial Leak Check, CFS

Finish Time 11:36 / 12:17

CFM at in. Hg.

Filter No. /

Final Leak Check, CFS
CFM .002 at 9.0 in. Hg.

RA-23-B "EAST" X-12

[illegible]

TEST NO. 88-09-S-P

DATE 06/01/88

VELOCITY AND VOLUME DETERMINATION

DRY GAS VOLUME

$$Vmstd = (17.71 \text{ deg R/in. Hg}) * Vm * (Pbar + \Delta H / 13.6) / Tm$$

Where $Vmstd$ = Volume (ft³) of gas sample at 70F and 29.92 in. Hg

Vm = Volume (ft³) of gas at meter conditions

Tm = Average dry gas meter temperature (R)

$Pbar$ = Barometric pressure (in. Hg)

ΔH = Pressure drop across orifice (in. WG)

$$Vmstd = 17.71 * 74.87 * (24.04 + 0.847 / 13.6) / 546.8 = 58.442 \text{ ft}^3$$

VOLUME OF WATER VAPOR

$$Vwstd = (0.0474 \text{ ft}^3/\text{ml}) * Vlc$$

Where $Vwstd$ = Volume (ft³) of water vapor

Vlc = Total volume of water collected (ml)

$$Vwstd = .00474 * 423.8 = 20.088 \text{ ft}^3$$

MOISTURE CONTENT

$$Bwo = Vwstd * 100 / (Vwstd + Vmstd)$$

Where Bwo = Percent moisture

$$Bwo = 20.09 * 100 / (20.09 + 58.44) = 25.580 \text{ percent}$$

CONCENTRATION

$$Cs' = (15.43 \text{ grains/gm}) * Mn / (Vmstd + Vwstd)$$

Where Cs' = Concentration (grains/scf)

Mn = Total particulate collected (gm)

$$Cs' = 15.43 * 0.3941 / (58.44 + 20.09) = 0.0774 \text{ grains/scf}$$

STACK VELOCITY

Where V = Stack velocity (ft/sec)

Ts = Stack absolute temperature (R)

ΔP = Average pitot reading (in. WG)

Mw = Molecular wt. of stack gas (lb/lb mole)

Kp = Pitot tube coefficient

$$Mw = 0.18 * 25.58 + 0.44 * 2.68 + 0.32 * 10.79 + 0.28 * 60.95 = 26.302 \text{ lb/mole}$$

$$\text{RA-23A } V = 0.84 * 85.48 * 1.230 * \text{SQR}(607.7 / (26.30 * 24.04)) = 86.582 \text{ ft/sec}$$

$$\text{RA-23B } V = 0.84 * 85.48 * 1.023 * \text{SQR}(607.1 / (26.30 * 24.04)) = 71.976 \text{ ft/sec}$$

STACK VOLUME

$$ACFM = V * A * 60 \quad \text{AND} \quad SCFM = ACFM * 530 * Ps / (Ts * 29.92)$$

Where $ACFM$ = Actual cubic Ft per minute at stack conditions

A = Stack area (ft²)

$SCFM$ = Standard cubic ft. per min. (29.92 in. Hg & 530 R)

$$\text{RA-23A } ACFM = 86.58 * 7.069 * 60 = 36723 \text{ acfm}$$

$$\text{RA-23B } ACFM = 71.98 * 7.069 * 60 = 30528 \text{ acfm}$$

$$\text{RA-23A } SCFM = 36723 * 530 * 24.04 / (607.7 * 29.92) = 25733 \text{ scfm}$$

$$\text{RA-23B } SCFM = 30528 * 530 * 24.04 / (607.1 * 29.92) = 21413 \text{ scfm}$$

CALCULATED DUST LOAD

$$\text{lb/hr} = Cs' * SCFM * 60 / 7000 \text{ grains/lb}$$

$$\text{DUST LOAD} = 0.0774 * 47147 * 60 / 7000 = 31.29 \text{ Lb/Hr}$$

ISOKINETIC RATE

$$I = 104.5606 \%$$

LABORATORY DATA

Company FMC

Run No.: 88-09.5-0

Sampling Location RA 23A & B

Date: 6-1-88

MOISTURE COLLECTED

		GM/ML	Water Weight/Volume Gain GM/ML
IMPINGER 1	Final Weight/Volume	<u>820.5</u>	
	Initial Weight/Volume	<u>574.0</u>	
	Increase	<u>246.5</u>	<u>246.5</u>
IMPINGER 2	Final Weight/Volume	<u>717.8</u>	
	Initial Weight/Volume	<u>563.0</u>	
	Increase	<u>154.8</u>	<u>154.8</u>
IMPINGER 3	Final Weight/Volume	<u>459.6</u>	
	Initial Weight/Volume	<u>455.8</u>	
	Increase	<u>3.8</u>	<u>3.8</u>
IMPINGER 4	Final Weight/Volume	<u>633.2</u>	
	Initial Weight/Volume	<u>614.2</u>	
	Increase	<u>19.0</u>	<u>19.0</u>
TOTAL MOISTURE CATCH			<u>423.0</u>

424.1

PARTICULATE COLLECTED

FRONT-HALF ANALYSIS (Nozzle, Probe, Cyclone, Filter Front-Half)

15	75.1022	Filter & Particulates	<u>0.9083</u>
	75.0830	Filter Tare Weight	<u>0.5338</u>
	<u>0.0192</u>	Particulate	<u>0.3745</u>
		Washings	<u>0.0192</u>
		Particulate Catch	<u>0.3937</u>
		Acetone Blank	<u>0.0003</u>
TOTAL FRONT CATCH			<u>0.3934</u>

BACK-HALF ANALYSIS (Impingers, Filter Back-Half)

1B	74.9746	Extractable Weight	<u>75.5495</u>
	74.9743	Boil Down Weight	<u>75.5488</u>
	<u>0.0003</u>	Impinger Catch	<u>0.0007</u>
		Water Blank	<u>-0-</u>

TOTAL BACK CATCH

TOTAL TRAIN CATCH

0.0007

0.3941

Some volume blank as washings

STACK SAMPLING FIELD DATA

Company MC Wy Corp.

Plant Location Green River W.Y.

Run No. 88-10-S-P.

Sampling Location RA-23A+B

Date 6-1-88

Start Time 13:54 / 14:40

Finish Time 14:26 / 15:12

Filter No. _____

RA-23-B "Eos +"

Assumed Moisture, % 20

Probe Tip Diameter, in. 18

Probe Length, ft. 5

Ambient Temperature, °F

Bar. Pressure, in. Hg. _____

Initial Leak Check, CFS _____
CFM at in. Hg.

Final Leak Check, CFS
CFM 001 at 9 in. Hg.

Point No.	Time (min)	Dry Gas Meter FT ³	Pitot in. H ₂ O		Orifice ΔH in. H ₂ O		Dry Gas Temp. °F		Pump Vacuum in. Hg Gauge	Sample Box Temp. °F	Impinger Temp. °F	Stack Press. in. Hg	Stack Temp. °F
			P	V _F			Inlet	Outlet					
					Desired	Actual							
1	0	740.9	0.80	1.074	0.52	0.52	101	96	3.8	267	57		143
2	4	742.4	0.94	1.090	0.64	0.64	104	97	4.1	265	57		143
3	8	744.8	1.15	1.072	0.75	0.75	106	97	4.6	272	53		143
4	12	746.9	1.15	1.072	0.75	0.75	106	97	4.9	268	52		145
5	16	749.1	1.2	1.095	0.79	0.79	106	97	5.1	269	52		143
6	20	751.4	1.15	1.072	0.75	0.75	106	97	5.0	272	52		144
7	24	753.0	1.2	1.095	0.79	0.79	106	97	5.3	271	54		144
8	28	755.9	0.89	1.038	0.58	0.58	105	96	5.0	273	54		145
	32	757.8											
1	0	757.8	1.10	1.049	0.72	0.72	97	93	5.0	265	54		140
2	4	759.9	1.10	1.049	0.72	0.72	102	95	5.2	275	48		146
3	8	762.1	1.10	1.049	0.72	0.72	103	96	5.4	275	48		147
4	12	764.3	1.10	1.049	0.72	0.72	103	96	5.7	278	49		146
5	16	766.4	1.30	1.140	0.85	0.85	104	95	6.2	272	51		145
6	20	768.6	1.40	1.183	0.92	0.92	104	95	7.0	274	51		147
7	24	771.1	1.40	1.183	0.92	0.92	104	95	7.2	276	51		146
8	28	773.4	1.30	1.140	0.85	0.85	104	95	7.0	265	52		145
	32	*775.822											
Total			17.07		11.99			3195					2312
Average			1067°		ΔH = 0.749			99.8°F					144.5°
								559.8°R					604.5K

VELOCITY AND VOLUME DETERMINATION

DRY GAS VOLUME

$$Vmstd = (17.71 \text{ deg R/in. Hg}) * Vm * (Pbar + \Delta H / 13.6) / Tm$$

Where $Vmstd$ = Volume (ft³) of gas sample at 70F and 29.92 in. Hg Vm = Volume (ft³) of gas at meter conditions Tm = Average dry gas meter temperature (R) $Pbar$ = Barometric pressure (in. Hg) ΔH = Pressure drop across orifice (in. WG)

$$Vmstd = 17.71 * 76.45 * (24.04 + 0.855 / 13.6) / 561.2 = 58.149 \text{ ft}^3$$

VOLUME OF WATER VAPOR

$$Vwstd = (0.0474 \text{ ft}^3/\text{ml}) * Vlc$$

Where $Vwstd$ = Volume (ft³) of water vapor Vlc = Total volume of water collected (ml)

$$Vwstd = .00474 * 521.0 = 24.695 \text{ ft}^3$$

MOISTURE CONTENT

$$Bwc = Vwstd * 100 / (Vwstd + Vmstd)$$

Where Bwc = Percent moisture

$$Bwc = 24.70 * 100 / (24.70 + 58.15) = 29.809 \text{ percent}$$

CONCENTRATION

$$Cs' = (15.43 \text{ grains/gm}) * Mn / (Vmstd + Vwstd)$$

Where Cs' = Concentration (grains/scf) Mn = Total particulate collected (gm)

$$Cs' = 15.43 * 0.3676 / (58.15 + 24.70) = 0.0685 \text{ grains/scf}$$

STACK VELOCITY

Where V = Stack velocity (ft/sec) Ts = Stack absolute temperature (R) ΔP = Average pitot reading (in. WG) Mw = Molecular wt. of stack gas (lb/lb mole) Kp = Pitot tube coefficient

$$Mw = 0.18 * 29.81 + 0.44 * 2.46 + 0.32 * 10.39 + 0.28 * 57.35 = 25.828 \text{ lb/mole}$$

$$RA-23A \quad V = 0.84 * 85.48 * 1.205 * \text{SQRT}(606.4 / (25.83 * 24.04)) = 85.507 \text{ ft/sec}$$

$$RA-23B \quad V = 0.84 * 85.48 * 1.067 * \text{SQRT}(604.5 / (25.83 * 24.04)) = 75.596 \text{ ft/sec}$$

STACK VOLUME

$$ACFM = V * A * 60 \quad \text{AND} \quad SCFM = ACFM * 530 * Ps / (Ts * 29.92)$$

Where $ACFM$ = Actual cubic Ft per minute at stack conditions A = Stack area (ft²) $SCFM$ = Standard cubic ft. per min. (29.92 in. Hg & 530 R)

$$RA-23A \quad ACFM = 85.51 * 7.069 * 60 = 36267 \text{ acfm}$$

$$RA-23B \quad ACFM = 75.60 * 7.069 * 60 = 32063 \text{ acfm}$$

$$RA-23A \quad SCFM = 36267 * 530 * 24.04 / (606.4 * 29.92) = 25468 \text{ scfm}$$

$$RA-23B \quad SCFM = 32063 * 530 * 24.04 / (604.5 * 29.92) = 22587 \text{ scfm}$$

CALCULATED DUST LOAD

$$\text{lb/hr} = Cs' * SCFM * 60 / 7000 \text{ grains/lb}$$

$$\text{DUST LOAD} = 0.0685 * 48055 * 60 / 7000 = 28.20 \text{ Lb/Hr}$$

ISOKINETIC RATE

$$I = 108.2138 \%$$

LABORATORY DATA

Company FMC

Run No.: 88-10-5-P

Sampling Location RR-23A#B

Date: 6-1-88

MOISTURE COLLECTED

		GM/ML	Water Weight/Volume Gain GM/ML
IMPINGER 1	Final Weight/Volume	<u>807.3</u>	
	Initial Weight/Volume	<u>560.1</u>	
	Increase	<u>247.2</u>	<u>247.2</u>
IMPINGER 2	Final Weight/Volume	<u>694.7</u>	
	Initial Weight/Volume	<u>543.9</u>	
	Increase	<u>150.8</u>	<u>150.8</u>
IMPINGER 3	Final Weight/Volume	<u>426.2</u>	
	Initial Weight/Volume	<u>422.1</u>	
	Increase	<u>4.1</u>	<u>4.1</u>
IMPINGER 4	Final Weight/Volume	<u>646.9</u>	
	Initial Weight/Volume	<u>628.0</u>	
	Increase	<u>18.9</u>	<u>18.9</u>
TOTAL MOISTURE CATCH			<u>421.0</u> ✓

PARTICULATE COLLECTED

FRONT-HALF ANALYSIS (Nozzle, Probe, Cyclone, Filter Front-Half)

25	74.9989	Filter & Particulates	<u>0.8994</u>
	74.9960	Filter Tare Weight	<u>0.5350</u>
	<u>0.0029</u>	Particulate	<u>0.3644</u>
		Washings	<u>0.0029</u>
		Particulate Catch	<u>0.3673</u>
		Acetone Blank	<u>0.0003</u>
TOTAL FRONT CATCH			<u>0.3670</u>

BACK-HALF ANALYSIS (Impingers, Filter Back-Half)

2B	74.7538	1BH	Extractable Weight	<u>75.4553</u>
	74.7535		Boil Down Weight	<u>75.4547</u>
	<u>0.0003</u>		Impinger Catch	<u>0.0006</u>
			Water Blank	<u>-0-</u>
TOTAL BACK CATCH				<u>0.0006</u>
TOTAL TRAIN CATCH				<u>0.3676</u> ✓

STACK SAMPLING FIELD DATA

Company MC Wy. Corp.

Plant Location Green River WY

Run No. 88-11-S-P. 1

Sampling Location RA-23A+B

Date 6-2-88

Start Time 10:37 / 11:16

Finish Time 11:09 / 11:48

Filter No.

Assumed Moisture, % 20

Probe Tip Diameter, in. 1.76715

Probe Length, ft. 5

Ambient Temperature, °F

Bar. Pressure, in. Hg. 24.17

Initial Leak Check, CFS CFM, 020 at 15 in. Hg.

Final Leak Check, CFS _____
CFM _____ at _____ in. Hg.

RA-23 "A" West X-12

Point No.	Time (min)	Dry Gas Meter FT ³	Pitot in. H ₂ O		Orifice ΔH in. H ₂ O		Dry Gas Temp. OF		Pump Vacuum in. Hg Gauge	Sample Box Temp. OF	Impinger Temp. OF	Stack Press. in. Hg	Stack Temp. OF
			P	VP	Desired	Actual	Inlet	Outlet					
1	0	779.605	1.1	1.049	0.72	0.72	76	69	3.3	238	69		109
2	4	781.7	1.2	1.095	0.78	0.78	85	70	3.5	262	70		114
3	8	783.9	1.32	1.162	0.88	0.88	87	73	4.0	261	70		114.5
4	12	786.2	1.75	1.311	1.14	1.14	90	75	5.2	256	69		114
5	16	788.8	1.70	1.304	1.11	1.11	92	77	5.3	260	67		114.2
6	20	791.4	2.1	1.449	1.37	1.37	95	79	6.5	270	66		114.2
7	24	794.3	2.3	1.516	1.50	1.50	97	97	7.1	263	65		114.3
8	28	797.3	2.1	1.449	1.37	1.37	99	84	7.3	248	67		114.3
	32	800.2											
1	0	800.2	0.82	0.905	0.53	0.53	95	87	3.2	243	69		109
2	4	802.2	1.1	1.049	0.72	0.72	100	89	4.0	256	65		139
3	8	804.3	1.4	1.183	0.91	0.91	103	90	5.0	265	68		143
4	12	806.6	1.6	1.265	1.04	1.04	104	91	5.8	254	70		143
5	16	809	1.75	1.311	1.14	1.14	105	92	6.1	257	69		144
6	20	811.9	1.8	1.342	1.17	1.17	106	93	6.6	266	71		144
7	24	814.5	1.45	1.204	0.94	0.94	106	94	5.9	268	62		142
8	28	817.0	1.55	1.249	1.01	1.01	107	95	6.1	278	60		142
	32	819.5											
389 x 13.569 = 76.431													
Orsat %CO₂ = 4.6 %CO = 13.2 %O₂ = 40 Stack Area = 7.089 Water = 138.0													
26.006 11.2													
5904 90.7°F 550.7°E													
38.4 598.4													
total	Vm	76.431	79.842	16.33	90.7°F								
average		112.44	ΔH = 1.021	550.7°E									

STACK SAMPLING FIELD DATA

Company FMC Wy Corp.

Assumed Moisture, % 20

Plant Location Green River Wy.

Probe Tip Diameter, in. 1/8

Run No. 88-11-S-P

Probe Length, ft. 5

Sampling Location RA-23A+B

Ambient Temperature, °F _____

Date 6-2-88

Bar. Pressure, in. Hg. _____

Start Time 11:52 / 12:30

Initial Leak Check, CFS

Finish Time 12:24 / 13:02

CFM _____ at _____ in. Hg.

Filter No. _____

Final Leak Check, CFS

CFM 0.012 at 8.0 in. Hg.

RA-23"B East X-12

Point No.	Time (min)	Dry Gas Meter FT ³	Pitot in. H ₂ O		Orifice ΔH in. H ₂ O		Dry Gas Temp. °F		Pump Vacuum in. Hg Gauge	Sample Box Temp. °F	Impinger Temp. °F	Stack Press. in. Hg	Stack Temp. °F
			P	VP	Desired	Actual	Inlet	Outlet					
SOUTH													
1	0	819.5	0.91	0.954	0.60	0.60	102	95	4.2	246	67		123
2	4	821.6	0.99	0.995	0.64	0.64	105	96	4.4	233	69		142
3	8	823.6	1.1	1.049	0.72	0.72	108	97	5.0	291	67		144
4	12	825.7	1.1	1.049	0.72	0.72	108	97	5.0	251	66		144
5	16	827.9	1.1	1.049	0.72	0.72	108	98	5.2	263	68		143
6	20	830.0	1.05	1.025	0.68	0.68	107	97	5.1	258	71		145
7	24	832.2	1.05	1.025	0.68	0.68	107	97	5.2	267	70		145
8	28	834.3	1.0	1.000	0.65	0.65	107	97	5.3	250	71		144
	32	836.4											
WEST													
1	0	836.4	0.68	0.825	0.45	0.45	101	96	4.1	263	77		109
2	4	838.2	0.99	0.995	0.64	0.64	105	97	5.0	264	76		139
3	8	841.9	0.99	0.995	0.64	0.64	106	97	5.0	265	66		141
4	12	842.2	1.2	1.095	0.78	0.78	107	98	6.0	267	61		141
5	16	844.4	1.2	1.095	0.78	0.78	107	98	6.3	270	63		143
6	20	846.7	1.2	1.095	0.78	0.78	107	98	6.2	268	62		142
7	24	849.0	1.1	1.049	0.72	0.72	107	97	6.1	261	59		140
8	28	851.2	0.88	0.938	0.57	0.57	107	97	5.9	259	59		140
	32	853.74											
Total													
Average													
			16.233		10.77		101.9°F						159.1°F
			10:01A		ΔH: 0.673		561.9°E						599.1°F

VELOCITY AND VOLUME DETERMINATION

DRY GAS VOLUME

$$Vmstd = (17.71 \text{ deg R/in. Hg}) * Vm * (Pbar + \Delta H / 13.6) / Tm$$

Where $Vmstd$ = Volume (ft³) of gas sample at 70F and 29.92 in. Hg Vm = Volume (ft³) of gas at meter conditions Tm = Average dry gas meter temperature (R) $Pbar$ = Barometric pressure (in. Hg) ΔH = Pressure drop across orifice (in. WG)

$$Vmstd = 17.71 * 76.43 * (24.17 + 0.846 / 13.6) / 556.3 = 58.962 \text{ ft}^3$$

VOLUME OF WATER VAPOR

$$Vwstd = (0.0474 \text{ ft}^3/\text{ml}) * Vlc$$

Where $Vwstd$ = Volume (ft³) of water vapor Vlc = Total volume of water collected (ml)

$$Vwstd = .00474 * 438.0 = 20.761 \text{ ft}^3$$

MOISTURE CONTENT

$$Bwc = Vwstd * 100 / (Vwstd + Vmstd)$$

Where Bwc = Percent moisture

$$Bwc = 20.76 * 100 / (20.76 + 58.96) = 26.042 \text{ percent}$$

CONCENTRATION

$$Cs' = (15.43 \text{ grains/gm}) * Mn / (Vmstd + Vwstd)$$

Where Cs' = Concentration (grains/scf) Mn = Total particulate collected (gm)

$$Cs' = 15.43 * 0.3647 / (58.96 + 20.76) = 0.0706 \text{ grains/scf}$$

STACK VELOCITY

Where V = Stack velocity (ft/sec) Ts = Stack absolute temperature (R) ΔP = Average pitot reading (in. WG) Mw = Molecular wt. of stack gas (lb/lb mole) Kp = Pitot tube coefficient

$$Mw = 0.18 * 26.04 + 0.44 * 3.40 + 0.32 * 9.76 + 0.28 * 60.79 = 26.331 \text{ lb/mole}$$

$$RA-23A \quad V = 0.84 * 85.48 * 1.240 * \sqrt{598.4 / (26.33 * 24.17)} = 86.336 \text{ ft/sec}$$

$$RA-23B \quad V = 0.84 * 85.48 * 1.014 * \sqrt{599.1 / (26.33 * 24.17)} = 70.642 \text{ ft/sec}$$

STACK VOLUME

$$ACFM = V * A * 60 \quad \text{AND} \quad SCFM = ACFM * 530 * Ps / (Ts * 29.92)$$

Where $ACFM$ = Actual cubic Ft per minute at stack conditions A = Stack area (ft²) $SCFM$ = Standard cubic ft. per min. (29.92 in. Hg & 530 R)

$$RA-23A \quad ACFM = 86.34 * 7.069 * 60 = 36619 \text{ acfm}$$

$$RA-23B \quad ACFM = 70.64 * 7.069 * 60 = 29962 \text{ acfm}$$

$$RA-23A \quad SCFM = 36619 * 530 * 24.17 / (598.4 * 29.92) = 26200 \text{ scfm}$$

$$RA-23B \quad SCFM = 29962 * 530 * 24.17 / (599.1 * 29.92) = 21412 \text{ scfm}$$

CALCULATED DUST LOAD

$$\text{lb/hr} = Cs' * SCFM * 60 / 7000 \text{ grains/lb}$$

$$\text{DUST LOAD} = 0.0706 * 47612 * 60 / 7000 = 28.81 \text{ Lb/Hr}$$

ISOKINETIC RATE

$$I = 105.1219 \%$$

3

LABORATORY DATA

Company FMC

Run No.: 88-11-S-P

Sampling Location RA-23A & B

Date: 6-2-88

MOISTURE COLLECTED

		GM/ML	Water Weight/Volume Gain GM/ML
IMPINGER 1	Final Weight/Volume	<u>832.6</u>	
	Initial Weight/Volume	<u>566.4</u>	
	Increase	<u>266.2</u>	<u>266.2</u>
IMPINGER 2	Final Weight/Volume	<u>717.4</u>	
	Initial Weight/Volume	<u>568.0</u>	
	Increase	<u>149.4</u>	<u>149.4</u>
IMPINGER 3	Final Weight/Volume	<u>447.1</u>	
	Initial Weight/Volume	<u>442.8</u>	
	Increase	<u>4.3</u>	<u>4.3</u>
IMPINGER 4	Final Weight/Volume	<u>666.5</u>	
	Initial Weight/Volume	<u>648.4</u>	
	Increase	<u>18.1</u>	<u>18.2</u>
	TOTAL MOISTURE CATCH		<u>438.0</u>

PARTICULATE COLLECTED

FRONT-HALF ANALYSIS (Nozzle, Probe, Cyclone, Filter Front-Half)

Filter & Particulates	<u>0.9311</u>
Filter Tare Weight	<u>0.5760</u>
Particulate	<u>0.3551</u>
Washings	<u>0.0095</u>
Particulate Catch	<u>0.3646</u>
Acetone Blank	<u>0.0003</u>
TOTAL FRONT CATCH	<u>0.3649</u>

BACK-HALF ANALYSIS (Impingers, Filter Back-Half)

Extractable Weight	<u>72.8116</u>
Boil Down Weight	<u>72.8115</u>
Impinger Catch	<u>0.0001</u>
Water Blank	<u>- 0 -</u>
TOTAL BACK CATCH	<u>0.0001</u>
TOTAL TRAIN CATCH	<u>0.3647</u>

0.7644

3S

73.3410
73.3315
0.0095

3B

74.8803
74.8800
0.0003

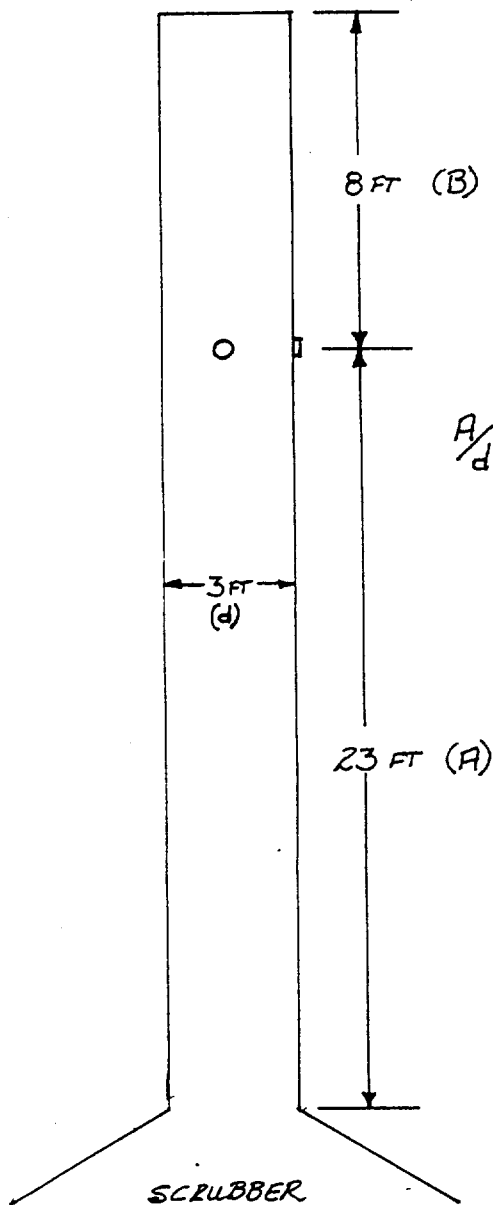
Section A-2, Information

- Drawing showing location of sample ports and number of points per traverse

RA-23A&B

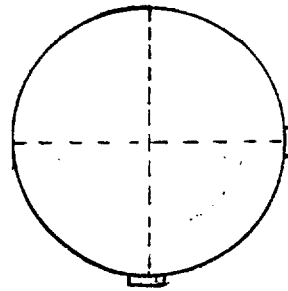
ONE UNIT -

TWO IDENTICAL SCRUBBERS, DUCTS, AND FANS

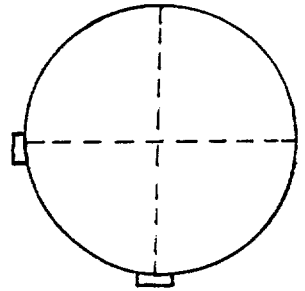


$$A/d = 7.7$$

RA-23A



RA-23B



No. OF POINTS PER TRAVERSE = 16

No. OF POINTS PER DIAMETER = 8

No. OF DIAMETERS PER RUN = 4 (2 PER STACK)

TRAVERSE POINTS ON EACH DIAMETER

	<u>% OF DIAMETER</u>	<u>DISTANCE FROM INSIDE WALL, (IN.)</u>	<u>DISTANCE FROM COUPLING, (IN.)</u>
1	3.3	1.18	4.18
2	10.5	3.78	6.78
3	19.4	6.98	9.98
4	32.3	11.63	14.63
5	67.7	24.37	29.37
6	80.6	29.02	32.02
7	89.5	32.20	35.20
8	96.7	34.81	37.81