

### 9.5.3 Meat Rendering Plants

Total VOC emissions of the wet cooker,  
blood furnace, hydrolizer, and melt  
tank

TRC Environmental Corporation for IBP, Inc.

August 1996

1996 (post section publication) source  
test data.

Note: This material is related to a section in AP42, *Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at [www.epa.gov/ttn/chief/ap42/](http://www.epa.gov/ttn/chief/ap42/)

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May 4, 1998

Mr. Ed Surla  
Compliance Data Section Chief  
Indiana Department of Environmental Management  
P.O. Box 6015  
Indianapolis, IN 46206-6015

RE: IBP, inc. - Logansport, Indiana  
VOC Test Reports

Dear Mr. Surla:

This letter replaces my original letter dated February 13, 1998, for the VOC Test Report for the above referenced facility. Please find enclosed a copy of that report. The testing was conducted on August 20-22, 1996, by TRC Environmental Corporation. Testing was conducted at other IBP facilities as well to verify the validity and accuracy of the data collected at the Logansport facility in 1996. VOC emission rates found on similar rendering systems indicate that data collected at Logansport is representative of VOC from pork rendering systems. Volatile organic carbon testing was completed per the Indiana Compliance Sampling Methods and was approved through protocol submittals and was witnessed by Mr. Pat Powlen of IDEM (Indiana Department of Environmental Management). As shown in the detailed testing report on page 3-5, the average VOC (Total Hydrocarbons as Methane) emission rate from are as follows:

|                               |                         |
|-------------------------------|-------------------------|
| Inedible Steam Cooker         | 1.50 lbs/hr as methane  |
| Blood Natural Gas fired Dryer | 0.138 lbs/hr as methane |
| Hair Steam Hydrolizer         | 0.107 lbs/hr as methane |
| Melt Tank                     | 154.35 ppmv as methane  |

The melt tank vents to room air and will not be covered in the VOC emission rate calculations.

If you have any questions concerning the testing results or procedures used please contact me at 402-241-3647 or you may contact Mr. Scott Miller, TRC Project Manager, at 630-810-1122.

Sincerely,

A handwritten signature in cursive script, appearing to read 'Rechelle Kruse'.

Rechelle Kruse  
Air Pollution Control Engineer

Enclosure

c: Darrell Schmidt (without test report)  
Janet Schroeder (without test report)  
Dallas Safriet (with test report)

RK98-491/LO-Stack Test

IBP, inc. P.O. BOX 515, DAKOTA CITY, NEBRASKA 68731 TELEPHONE: 402-494-2061

**FINAL REPORT  
TOTAL VOC EMISSIONS OF  
THE WET COOKER,  
BLOOD FURNACE,  
HYDROLIZER, AND  
MELT TANK**

Prepared for

**IBP, Inc.  
Logansport, Indiana**

Prepared by

**TRC ENVIRONMENTAL CORPORATION  
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(630) 810-1122**

August 1996

**TRC Project No. 20974-0000-00000**

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## LIST OF ACRONYMS AND ABBREVIATIONS

|                     |                                       |
|---------------------|---------------------------------------|
| acfm                | actual cubic feet per minute          |
| afmp                | actual feet per minute                |
| CEM                 | continuous emission monitor           |
| CEMS                | continuous emission monitoring system |
| cf                  | cubic feet                            |
| CO <sub>2</sub>     | carbon dioxide                        |
| dscf                | dry standard cubic feet               |
| EPA                 | Environmental Protection Agency       |
| °F                  | degrees Fahrenheit                    |
| ft                  | feet                                  |
| in H <sub>2</sub> O | inches of water                       |
| in Hg               | inches of mercury                     |
| lb/hr               | pounds per hour                       |
| O <sub>2</sub>      | oxygen                                |
| ppm (v)             | parts per million volume              |
| QA/QC               | Quality Assurance/Quality Control     |
| scfm                | standard cubic feet per minute        |
| TGNMO               | total gaseous non-methane organics    |
| THC                 | total hydrocarbons                    |
| TRC                 | TRC Environmental Corporation         |
| VOC                 | volatile organic compound             |

## PROGRAM SUMMARY

The IBP, Inc. facility located in Logansport, Indiana has a Wet Cooker, Blood Furnace, Hydrolizer, and Melt Tank in their rendering operations. TRC Environmental Corporation (TRC) was contracted by IBP, Inc. to conduct emission testing on the Wet Cooker, Blood Furnace, Hydrolizer, and Melt Tank. The major objectives of the test program were to collect representative flue gas samples and determine the emission rates of volatile organic compounds (VOC's) at the Wet Cooker, Blood Furnace, Hydrolizer, and Melt Tank exhausts.

TRC accomplished this objective through the use of acceptable test methods performed by trained and experienced staff. IBP, Inc. personnel were responsible for maintaining the proper operations during the emission test series. The emission test program was conducted on August 20-23, 1996. The emission tests included sampling for total gaseous non-methane organics (TGNMO), total hydrocarbons (THC), volumetric flow rates, and moisture content of the Wet Cooker, Blood Furnace, Hydrolizer, and Melt Tank flue gas following USEPA Methods 1 (Sampling Location Selection), 2 (Flow Rate), 3 (CO<sub>2</sub> and O<sub>2</sub> for Molecular Weight), 4 (Moisture), 18 (Methane), and 25 (TGNMO), and 25A (THC).

## **SECTION I**

### **INTRODUCTION**

#### **1.1 Project Scope**

The IBP, Inc. facility operates a Wet Cooker, Blood Furnace, Hydrolizer, and Melt Tank at its Logansport, Indiana facility. The Wet Cooker is for cooking the main waste pieces, Blood Furnace dries the blood, Hydrolizer cooks the hair, and the Melt Tank melts the fat and oils. The gas stream from each system enters the Spray Tower, gets scrubbed with water, and then exits to the atmosphere. The Melt Tank directly vents to the atmosphere and is not currently in line with the Spray Tower.

TRC was contracted by IBP, Inc. to conduct (THC) emission testing for determination of volatile organic compound (VOC) emission rates of the Wet Cooker, Blood Furnace, Hydrolizer, and Melt Tank exhausts. The major objective of the test program was to collect representative flue gas samples and determine emission rates of (VOC's) at the Wet Cooker, Blood Furnace, Hydrolizer, and Melt Tank exhausts. Three 1-hour tests were conducted at the Wet Cooker and Blood Furnace exhausts, simultaneously with flow rates, CO<sub>2</sub> and O<sub>2</sub> for molecular weight, and moisture. One 1-hour and 40-minute run was conducted on the Hydrolizer, and two flow runs. One 1-hour run was performed on the Melt Tank, flow was not measured from the open vent.

#### **1.2 Sampling Locations**

Sampling for TGNMO was conducted on the Wet Cooker exhaust. The inside stack dimension was measured to be 10 inches in diameter; therefore, the stack area equals 78.5 square inches. (THC) was conducted on the Blood Furnace, Hydrolizer, and Melt Tank exhausts. The inside stack dimension of the Blood Furnace was measured to be 18"; therefore, the stack area equals 254.5 square inches. The inside stack dimension of the

Hydrolizer was measured to be 8"; therefore, the stack area equals 50.3 square inches. The Melt Tank has an open vent and flow was not measured. Stack gas velocity, moisture, and volumetric flow rates were measured simultaneously with the TGNMO and (THC) sampling. The required number of sample points and the sample point locations for the velocity traverses of each source were calculated according to 40 CFR Part 60, Appendix A, Method 1.

## **SECTION 2**

### **SUMMARY OF RESULTS**

On August 20-23, 1996, testing was conducted to determine emission rates of the Wet Cooker, Blood Furnace, Hydrolizer, and Melt Tank exhausts at the IBP, Inc. plant in Logansport, Indiana. All testing was completed in accordance with approved test methodologies.

Table 2-1 summarizes the data for the Wet Cooker from August 22, 1996, table 2-2 summarizes the data for the Blood Furnace from August 20, 1996, table 2-3 summarizes the data for the Hydrolizer from August 21, 1996, and table 2-4 summarizes the data for the Melt Tank from August 22, 1996, at the IBP, Inc. plant located in Logansport, Indiana.

Raw field data sheets are located in Appendix A, this includes CEM's data sheets, CEM's one minute averages, flow rate data sheets, and moisture data sheets.

Process data recorded by IBP, Inc. is located in Appendix B.

Laboratory results and data sheets are located in Appendix C.

Equipment calibration data sheets are located in Appendix D.

Calculation formulas can be found in Appendix E.

All test procedures were conducted as stated in Section 3. No anomalous data is reported.

**Table 2-1 VOC Emission Rates for the Wet Cooker**

| WET COOKER EXHAUST EMISSION RATE RESULTS     |         |         |         |
|----------------------------------------------|---------|---------|---------|
|                                              | TEST #1 | TEST #2 | TEST #3 |
| Total Hydrocarbons Lbs/Hr<br>TGNMO as Carbon | 1.300   | 0.900   | 2.200   |

AVG = 1.500 lbs/hr TGNMO as carbon

**Table 2-2 VOC Emission Rates for the Blood Furnace**

| BLOOD FURNACE EXHAUST EMISSION RATE RESULTS                |         |         |         |
|------------------------------------------------------------|---------|---------|---------|
|                                                            | TEST #1 | TEST #2 | TEST #3 |
| Total Hydrocarbons Lbs/Hr as<br>Methane (CH <sub>4</sub> ) | .223    | .120    | .072    |

AVG = .138 lbs/hr as Methane (CH<sub>4</sub>)

**Table 2-3 VOC Emission Rates for the Hydrolizer**

| HYDROLIZER EXHAUST EMISSION RATE RESULTS                |         |
|---------------------------------------------------------|---------|
|                                                         | TEST #1 |
| Total Hydrocarbons Lbs/Hr as Methane (CH <sub>4</sub> ) | .107    |

**Table 2-4 VOC Concentrations for the Melt Tank**

| MELT TANK CONCENTRATION (PPM)                                          |         |
|------------------------------------------------------------------------|---------|
|                                                                        | TEST #1 |
| Total Hydrocarbon Concentration<br>Cpmmv as Methane (CH <sub>4</sub> ) | 154.35  |

## **SECTION 3**

### **FIELD SAMPLING PROCEDURES**

#### **3.1 Field Sampling Summary**

After consideration of the program requirements, TRC provided a team of two experienced professionals to conduct the field effort. The personnel and their responsibilities during this test program were as follows:

Scott R. Miller - Team Leader and Continuous Emission Monitoring (CEM) Operator

Dave Wells - TGNMO Train Operator and Volumetric Flow Rate Measurements

##### **3.1.1 Pre-Sampling Preparation**

Equipment was inspected for proper operation and durability prior to calibration. All calibrations were performed prior to and at the conclusion of the emissions test program as shown below:

- Pitot tubes (QA Handbook Section 3.12, pp. 1-13 and USEPA Reference Method 2) - measured for appropriate spacing and dimensions or calibrated in a wind tunnel. Rejection criteria given on the calibration sheet. Post-test check to inspect for damage.
- Thermocouples (QA Handbook Section 3.4.2, pp. 15-18) - verified against a mercury-in-glass thermometer at three points including the anticipated measurement range. Acceptance limits - impinger  $\pm 2^{\circ}\text{F}$ ; DGM  $\pm 5.4^{\circ}\text{F}$ ; stack  $\pm 1.5$  percent of stack temperature.
- Field barometer (QA Handbook Section 3.4.2, pp. 18-19) - compared against a mercury-in-glass barometer or use the airport station's barometric pressure and correct for elevation. Acceptance criteria -  $\pm 0.02$  in. Hg; post-test check - same.

## **3.2 Sampling Methods**

### **3.2.1 Flow Rate Measurements**

Velocity measurements at the sampling locations were made following EPA Reference Methods 1 and 2 simultaneously with the TGNMO and (THC) sampling. A Type-S pitot tube with an attached water manometer was used to measure the exhaust velocities at the sampling ports. An attached Type-K thermocouple with remote digimite was used to determine gas temperature.

### **3.2.2 CO<sub>2</sub> and O<sub>2</sub> Measurement**

Tedlar Bag<sup>®</sup> flue gas samples were taken concurrently with the TGNMO and (THC) sampling. A Fyrite was used to determine percent by volume of CO<sub>2</sub> and O<sub>2</sub>.

### **3.2.3 Moisture Measurement**

Moisture was measured simultaneously using the wet bulb / dry bulb technique stated in USEPA Method 4 for each test run. The difference between the wet bulb temperature and the dry bulb temperature was used to get the percent moisture. The calculation formulas are shown in Appendix E.

### **3.2.4 Total Hydrocarbons**

TRC conducted (TGNMO) testing at the Wet Cooker exhaust following (USEPA RM25), and (THC) monitoring at the Blood Furnace, Hydrolizer, and Melt Tank exhausts following (USEPA RM25A). TRC followed procedures outlined in the EPA publication 340/1-83-016 regarding setup and operation of its (THC) analyzer.

#### 3.2.4.1 USEPA Method 25 Train for Total Gaseous Non-Methane Organics

TGNMO sampling as conducted following the criteria of USEPA Reference Test Method 25. Flue gas was sampled from the Wet Cooker exhaust at a constant rate through a heated probe and filter and a chilled condensate trap by means of an evacuated sample tank. The heated probe and oven were kept at a temperature of  $\geq 265^{\circ}\text{F}$  and  $250 \pm 5^{\circ}\text{F}$  respectively during the sampling. After completion of each test run, the trap and tank were sealed, labeled and documented on the chain-of-custody record. All traps were kept under dry ice until the moment of analysis. Three one-hour tests were conducted. A schematic representation of the sampling train is included as Figure 3-1.

Leak checks on the Method 25 train were performed before each sampling run. All leak checks and leakage rates are documented on the relevant field test data sheet. Copies of the field data sheets and summary calculations are included in Appendix A.

#### 3.2.4.2 USEPA RM25A Train for Total Hydrocarbons

The (THC) analyzer system consists of three subsystems: sample acquisition, sample analysis, and a data acquisition system. The sample acquisition sample line is designed to deliver a representative sample of the stack gas stream to the sample analysis subsystem. A heat traced sample line was used to eliminate in-line condensation prior to the (THC) analyzer as shown in figure 3-2.

Sample analysis was achieved using a JUM VE-7 total hydrocarbon analyzer. Accurate interpretation of each analyzers response requires the systematic calibration of the instrument against gases of known concentrations. A calibration equation is determined from a linear regression of known gas concentrations versus instrument response. The equation used to convert instrument signal to concentration units follows:

$$\text{Concentration} = m (\text{response}) + b$$

where:  $m$  = slope of calibration curve  
response = instrument signal (volts)  
 $b$  = y-intercept of calibration curve

The data acquisition subsystem consists of an ESC 8800 Datalogger and an Esterline Angus strip chart recorder. The average total hydrocarbon concentration for each test run was calculated from average measurements recorded at one-minute intervals over the entire duration of each test run. Once the (THC) system was set up it was connected to a power source and brought on line. Sample line and signal wires were run between the sampling and (THC) system location, and the sample probe was selected and placed in the stack facing away from the gas stream.

The initial phase of the instrumental analysis method required the calibration of the (THC) analyzer system. Prior to the start of the first test run, system calibration using zero and three (3) upscale propane in nitrogen gas was performed. Following these initial system checks, further calibrations were performed at the end of each test run using a zero and an upscale propane in nitrogen gas.

### 3.2.5 Methane

Tedlar bag<sub>®</sub> samples were taken simultaneously with the (THC) sampling for determination of Methane. The methane fraction will be subtracted from the hydrocarbon total. The total hydrocarbon data is being reported as Propane ( $C_3H_8$ ), which has three Carbons. The Methane ( $CH_4$ ) fraction has only one Carbon; therefore, only 1/3 of the Methane concentration will be subtracted from the Propane concentration. For example:

THC (as  $C_3H_8$ ) = 100 ppm. There are three Carbons in propane.

Methane ( $CH_4$ ) = 60 ppm. There is only one Carbon in methane.

Methane equivalent to Propane would be  $1 / 3 = .333$  ppm as propane.

100 ppm propane - 60 ppm methane (which is equivalent to 20 ppm propane) = 80 ppm propane.

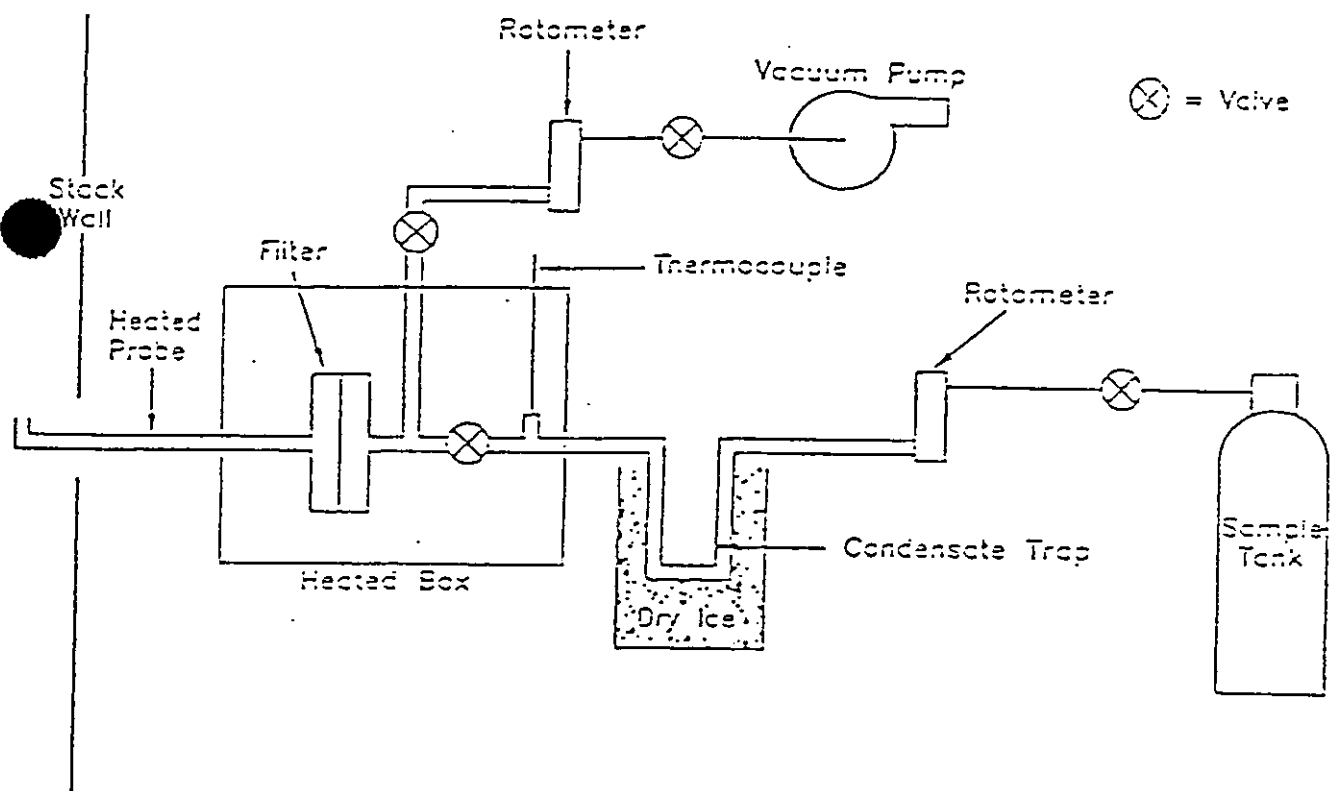


Figure 3-1 Method 25 Sampling Train

No post-test recovery is needed for this method

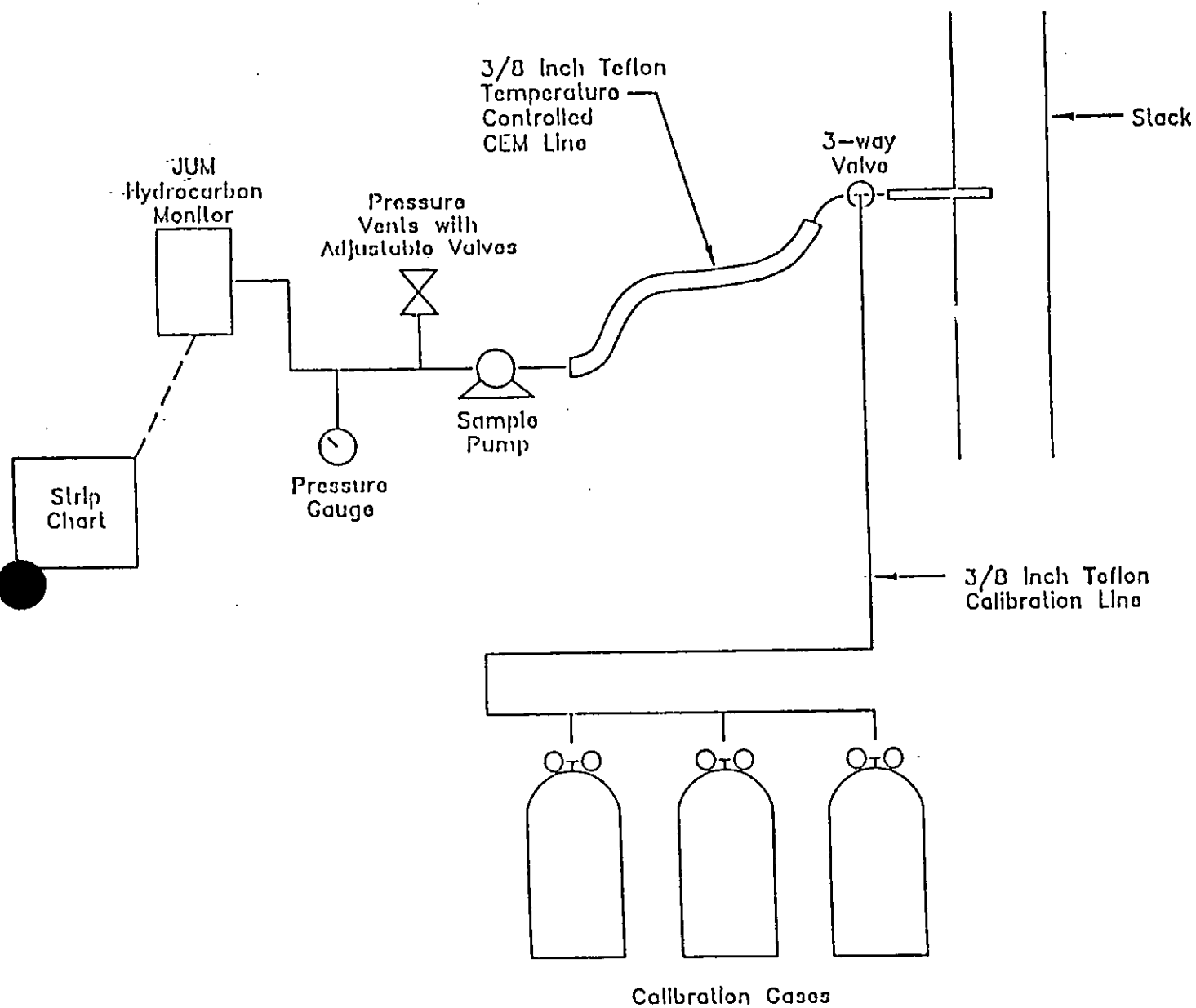


Figure 3-2 Method 25A Sampling Train

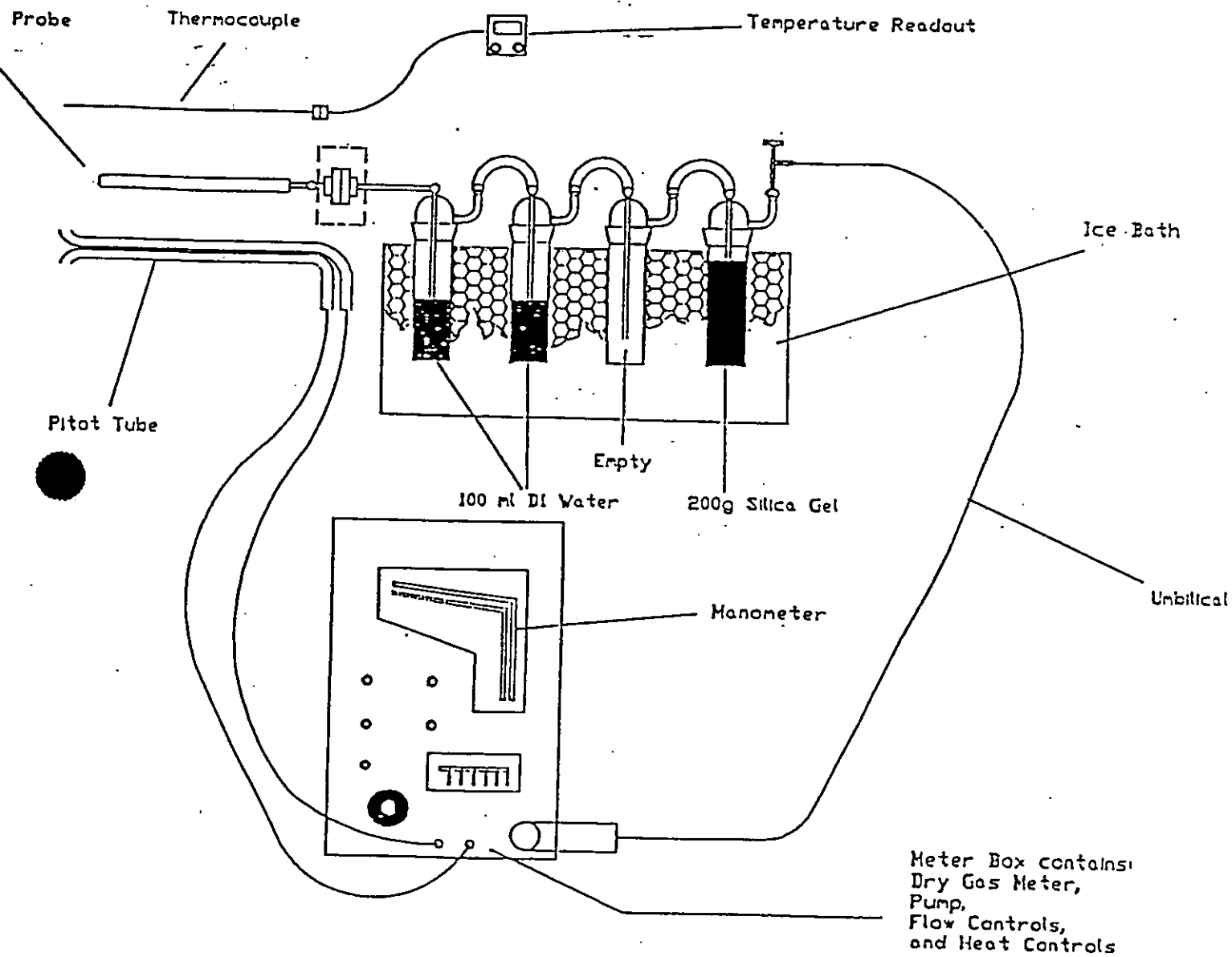


Figure 3-3 Method 2 and 4 Sampling Train

## SECTION 4 DATA REPORTING

### 4.1 Data Reporting

A flow chart depicting the measurement data reporting scheme is shown in Figure 4-1. Figure 4-2 presents the analytical data validation and reporting scheme routinely used at TRC.

All data was reported in standard units depending on the measurement and the ultimate use of the data. The bulk of the data was computer processed and reported as follows:

- Gas Properties:
  - a. Moisture %
  - b. Flow rate, dscfm and acfm
  - c. Pressure, in. Hg
  - d. Temperature, °F
- Total Gaseous non-methane Organics as PPMC
- Total Hydrocarbons: lbs/hr as Propane.

Results of the testing conducted at the IBP plant on the Wet Cooker exhaust are contained in Table 4-1.

Results of the testing conducted at the IBP plant on the Blood Furnace exhaust are contained in Table 4-2.

Results of the testing conducted at the IBP plant on the Hydrolizer exhaust are contained in Table 4-3.

Results of the testing conducted at the IBP plant on the Melt Tank exhaust are contained in Table 4-4.

**Table 4-1. Test Results - Wet Cooker Exhaust**

| Summary of Emission Rates<br>Wet Cooker Exhaust     |           |           |           |          |
|-----------------------------------------------------|-----------|-----------|-----------|----------|
| Run No.                                             | 2         | 3         | 4         |          |
| Date                                                | 22-Aug-96 | 22-Aug-96 | 22-Aug-96 |          |
| Start Time                                          | 09:44     | 10:54     | 12:27     |          |
| Stop Time                                           | 10:44     | 11:54     | 13:27     | AVERAGES |
| Barometric Pressure, in. Hg                         | 29.50     | 29.50     | 29.50     | 29.50    |
| Moisture, % (Wet /Dry Bulb Method)                  | 3.8       | 3.7       | 3.8       | 3.8      |
| Dry Mole Fraction, 100-%M                           | 0.9620    | 0.9630    | 0.9620    | 0.9623   |
| CO <sub>2</sub> , %                                 | 0.0       | 0.0       | 0.0       | 0.0      |
| O <sub>2</sub> , %                                  | 20.9      | 20.9      | 20.9      | 20.9     |
| N <sub>2</sub> , %                                  | 79.1      | 79.1      | 79.1      | 79.1     |
| Dry Molecular Weight, lb/lb mole                    | 28.84     | 28.84     | 28.84     | 28.84    |
| Wet Molecular Weight, lb/lb mole                    | 28.42     | 28.44     | 28.42     | 28.43    |
| Stack Area, sq. in. (10" Dia.)                      | 78.5      | 78.5      | 78.5      | 78.5     |
| Static Pressure, in. of H <sub>2</sub> O            | 1.05      | 1.05      | 1.05      | 1.05     |
| Stack Pressure, in. of Hg                           | 29.58     | 29.58     | 29.58     | 29.58    |
| Avg. Stack Temp., F                                 | 92.0      | 94.0      | 95.0      | 93.7     |
| Avg. Sqroot of Delta P                              | 1.0575    | 1.0498    | 1.0516    | 1.0530   |
| SDE Average                                         | 24.846    | 24.709    | 24.774    | 24.776   |
| Pitot Coefficient                                   | 0.84      | 0.84      | 0.84      | 0.84     |
| Stack Gas Velocity, afpm                            | 3692.5    | 3671.6    | 3681.9    | 3682.0   |
| Stack Flowrate, wet acfm                            | 2,013     | 2,002     | 2,007     | 2,007    |
| Stack Flowrate, dry scfm                            | 1,831     | 1,816     | 1,816     | 1,821    |
| Stack Flowrate, dry scf/hr                          | 109,862   | 108,957   | 108,953   |          |
| <b>Total Hydrocarbon Data, Method 25</b>            |           |           |           |          |
| Concentration, ppm as Carbon                        |           |           |           |          |
| Condensable                                         | 169       | 94        | 460       | 241      |
| Non-Condensable                                     | 206       | 173       | 193       | 191      |
| TOTAL (ppm) less Blank                              | 375       | 267       | 653       | 432      |
| Concentration, lb/dscf x 10 <sup>-6</sup> as Carbon | 11.668    | 8.307     | 20.317    | 13.431   |
| Emission Rate, lbs/hr as Carbon                     | 1.3       | 0.9       | 2.2       | 1.5      |

**Table 4-2. Test Results - Blood Furnace Exhaust**

**IBP Logansport, IA (Blood Furnace)**

| Run No.                                      | 1          | 2          | 3          |                 |
|----------------------------------------------|------------|------------|------------|-----------------|
| Date                                         | 20-Aug-96  | 20-Aug-96  | 20-Aug-96  |                 |
| Start Time                                   | 13:42      | 14:50      | 16:02      |                 |
| Stop Time                                    | 14:42      | 15:50      | 17:02      | <b>AVERAGES</b> |
| Barometric Pressure, in. Hg                  | 29.30      | 29.30      | 29.30      | 29.30           |
| Moisture, % (Wet/Dry Bulb)                   | 17.7       | 17.8       | 17.9       | 17.8            |
| Dry Mole Fraction, 100-%M                    | 0.8230     | 0.8220     | 0.8210     | 0.8220          |
| CO2 at Stack, % dry                          | 1.5        | 1.5        | 1.0        | 1.3             |
| O2 at Stack, % dry                           | 18.5       | 18.5       | 19.5       | 18.8            |
| CO + N2, % dry                               | 80.0       | 80.0       | 79.5       | 79.8            |
| Dry Molecular Weight, lb/lb mole             | 28.98      | 28.98      | 28.94      | 28.97           |
| Wet Molecular Weight, lb/lb mole             | 27.04      | 27.03      | 26.98      | 27.01           |
| Stack Diameter, in                           | 18         | 18         | 18         |                 |
| Stack Area, sq. in. (@ pitot meas. location) | 254.5      | 254.5      | 254.5      | 254.5           |
| Static Pressure, in. of H2O                  | 1.55       | 1.55       | 1.55       | 1.55            |
| Stack Pressure, in. of Hg                    | 29.41      | 29.41      | 29.41      | 29.41           |
| Avg. Stack Temp., F                          | 195.0      | 193.0      | 199.0      | 195.7           |
| Avg. Sqrroot of Delta P                      | 0.6321     | 0.6307     | 0.6361     | 0.6330          |
| SDE Average                                  | 16.177     | 16.117     | 16.329     | 16.208          |
| Pitot Coefficient                            | 0.84       | 0.84       | 0.84       | 0.84            |
| Stack Gas Velocity, afpm                     | 2472.0     | 2463.3     | 2497.8     | 2477.7          |
| Stack Flowrate, wet acfm                     | 4,368      | 4,353      | 4,414      | 4,378           |
| Stack Flowrate, dry scfm                     | 2,849      | 2,844      | 2,854      | 2,849           |
| Stack Flowrate, dry scf/hr                   | 170,946    | 170,655    | 171,262    |                 |
| Stack Flowrate, wet scf/hr                   | 2.0771E+05 | 2.0761E+05 | 2.0860E+05 |                 |
| Total Hydrocarbons ppmv as CH4               | 31.52      | 16.91      | 10.08      | 19.50           |
| Total Hydrocarbons Lb/Hr as CH4              | 0.223      | 0.120      | 0.072      | 0.138           |

**Calculations**

|                                 |         |         |         |
|---------------------------------|---------|---------|---------|
| Analyte                         | CH4     | CH4     | CH4     |
| FWhc lbs/lb-mole                | 16      | 16      | 16      |
| Stack Flowrate, dry scf/hr      | 170,946 | 170,655 | 171,262 |
| Moisture, %                     | 17.7    | 17.8    | 17.9    |
| Cppmv                           | 37.83   | 22.20   | 21.48   |
| Cppmv minus CH4                 | 31.52   | 16.91   | 10.08   |
| Hydrocarbons Emissions (lbs/hr) | 0.223   | 0.120   | 0.072   |

$$\text{Lbs/Hr} = \text{Cppmv minus CH4} * \text{FWhc} * (\text{Stack Flowrate}(\text{dscf/hr}) / 60) * (1.554 * 10^{-7})$$

**Table 4-3. Test Results - Hydrolizer Exhaust**

**IBP Logansport, IA (Hydrolizer)**

| Run No.                                      | 1         | 2 Flow only |          |
|----------------------------------------------|-----------|-------------|----------|
| Date                                         | 21-Aug-96 | 21-Aug-96   |          |
| Start Time                                   | 09:18     | 10:36       |          |
| Stop Time                                    | 11:16     | 11:16       | Averages |
| Barometric Pressure, in. Hg                  | 29.50     | 29.50       | 29.50    |
| Moisture, % (Wet/Dry Bulb)                   | 31.0      | 31.0        | 31.00    |
| Dry Mole Fraction, 100-%M                    | 0.6900    | 0.6900      | 0.69     |
| CO2 at Stack, % dry                          | 15.0      | 15.0        | 15.00    |
| O2 at Stack, % dry                           | 2.0       | 2.0         | 2.00     |
| CO + N2, % dry                               | 83.0      | 83.0        | 83.00    |
| Dry Molecular Weight, lb/lb mole             | 30.48     | 30.48       | 30.48    |
| Wet Molecular Weight, lb/lb mole             | 26.61     | 26.61       | 26.61    |
| Stack Diameter, in                           | 8         | 8           | 8.00     |
| Stack Area, sq. in. (@ pitot meas. location) | 50.3      | 50.3        | 50.27    |
| Static Pressure, in. of H2O                  | 0.89      | 0.90        | 0.90     |
| Stack Pressure, in. of Hg                    | 29.57     | 29.57       | 29.57    |
| Avg. Stack Temp., F                          | 212.0     | 212.0       | 212.00   |
| Avg. Sqroot of Delta P                       | 1.0992    | 1.1221      | 1.11     |
| SDE Average                                  | 28.495    | 29.088      | 28.79    |
| Pitot Coefficient                            | 0.84      | 0.84        | 0.84     |
| Stack Gas Velocity, afpm                     | 4377.6    | 4468.7      | 4423.15  |
| Stack Flowrate, wet acfm                     | 1,528     | 1,560       | 1543.97  |
| Stack Flowrate, dry scfm                     | 819       | 836         | 827.14   |
| Stack Flowrate, dry scf/hr                   | 49,117    | 50,141      | 49,629   |
| Stack Flowrate, wet scf/hr                   | 71,184    | 72,667      | 71,925   |
| Total Hydrocarbons ppmv as C3H8              | 52.14     |             |          |
| Total Hydrocarbons Lb/Hr as C3H8             | 0.107     |             |          |

**Calculations**

|                                 |        |
|---------------------------------|--------|
| Analyte                         | CH4    |
| FWhc lbs/lb-mole                | 16     |
| Stack Flowrate, dry scf/hr      | 49,629 |
| Moisture, %                     | 31.0   |
| Cppmv                           | 67.71  |
| Cppmv minus CH4                 | 52.14  |
| Hydrocarbons Emissions (lbs/hr) | 0.107  |

$$\text{Lbs/Hr} = \text{Cppmv minus CH4} \cdot \text{FWhc} \cdot (\text{Stack Flowrate(dscf/hr)} / 60) \cdot (1.554 \cdot 10^{-7})$$

**Table 4-4. Test Results - Melt Tank Exhaust**

**IBP Logansport, IA (Melt Tank)**

|                                 |           |
|---------------------------------|-----------|
| Run No.                         | 1         |
| Date                            | 22-Aug-96 |
| Start Time                      | 12:45     |
| Stop Time                       | 13:15     |
| Barometric Pressure, in. Hg     | 29.50     |
| Total Hydrocarbons ppmv as C3H8 | 154.35    |

**Calculations**

|                            |        |
|----------------------------|--------|
| Analyte                    | CH4    |
| FWhc lbs/lb-mole           | 16     |
| Stack Flowrate, dry scf/hr | n/a    |
| Moisture, %                | n/a    |
| Cppmv                      | 229.95 |
| Cppmv minus CH4            | 154.35 |

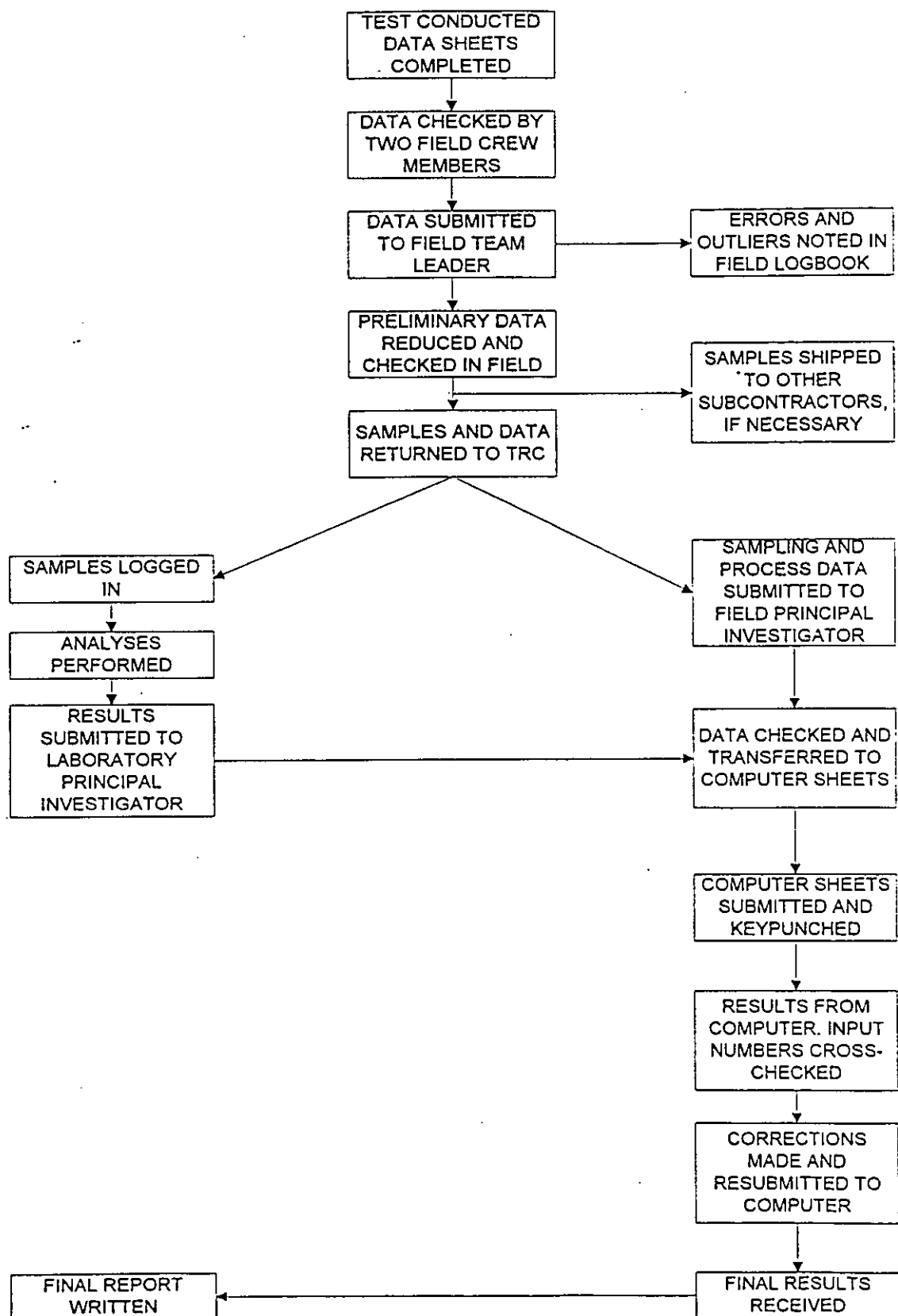


Figure 4-1. Measurement Data Flow Scheme

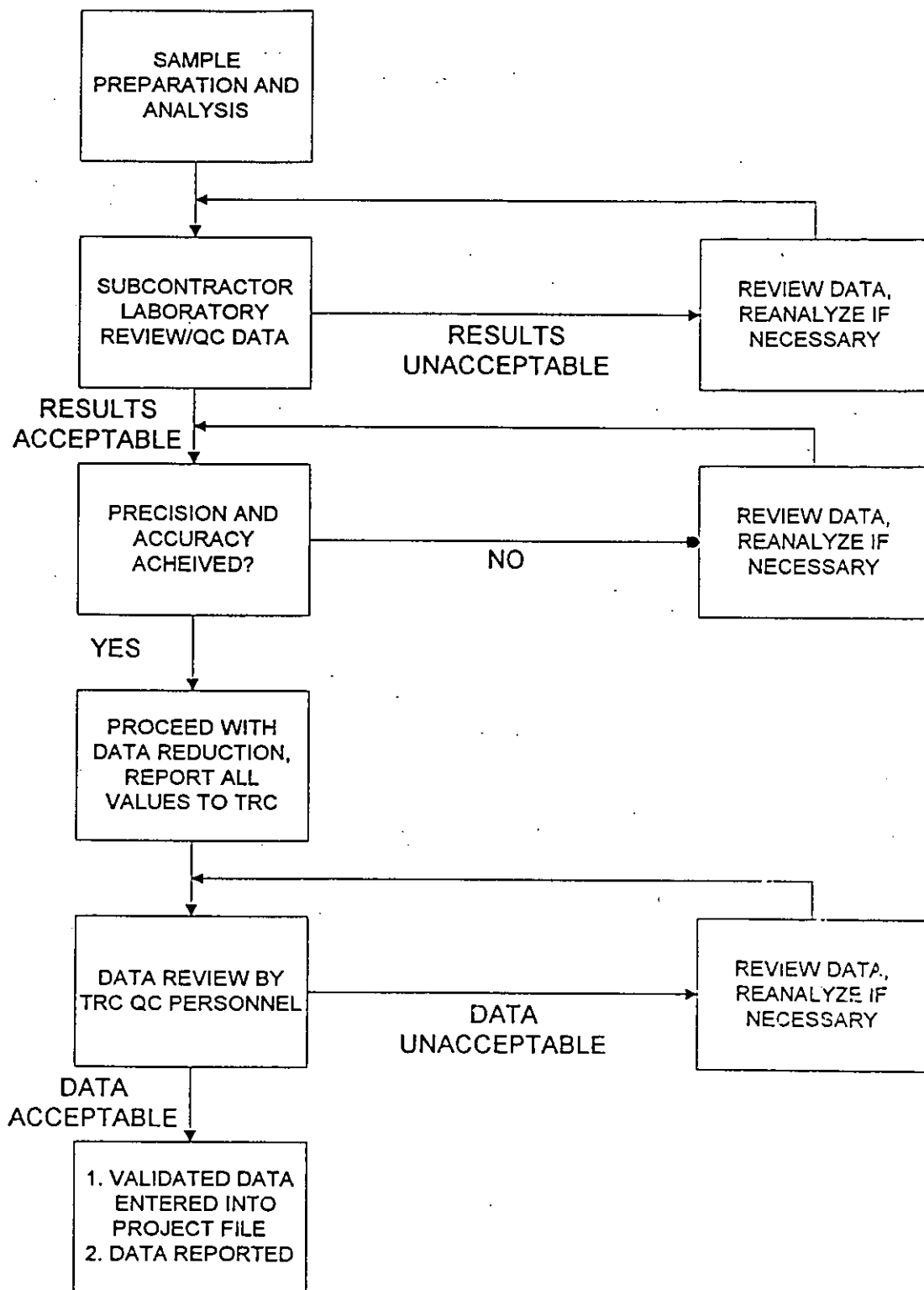


Figure 4-2. Analytical Data Report Scheme

## **APPENDIX A**

### **RAW FIELD DATA SHEETS AND DATA LOGGER PRINTOUTS**

## WET BULB / DRY BULB MOISTURE DETERMINATION

Client IBP Logansport  
 Date 8/22/1996  
 Project Number 20974-0000-00000  
 Plant Logansport, IN  
 Sampling Location exhaust stack  
 Source Wet Cooler  
 Run Number 2

Barometric Pressure 29.5  
 Static Pressure 1.05  
 Temperature (Dry) 92  
 Temperature (Wet) 84  
 S. V. P. (at T wet) 0.59  
 (Water Saturation Vapor Pressure (PSII))  
 PST 0.0772  
 PS 29.5772  
 Vapor Pressure 1.115  
 %Moisture 3.7581  
 Md 0.9624

## WET BULB / DRY BULB MOISTURE DETERMINATION

Client IBP Logansport  
 Date 8/22/1996  
 Project Number 20974-0000-00000  
 Plant Logansport, IN  
 Sampling Location exhaust stack  
 Source Wet Cooler  
 Run Number 3

Barometric Pressure 29.5  
 Static Pressure 1.05  
 Temperature (Dry) 94  
 Temperature (Wet) 84  
 S. V. P. 0.59  
 (Water Saturation Vapor Pressure (PSII))  
 PST 0.0772  
 PS 29.5772  
 Vapor Pressure 1.0991  
 %Moisture 3.6822  
 Md 0.9632

## WET BULB / DRY BULB MOISTURE DETERMINATION

Client IBP Logansport  
 Date 8/22/1996  
 Project Number 20974-0000-00000  
 Plant Logansport, IN  
 Sampling Location exhaust stack  
 Source Wet Cooler  
 Run Number 4

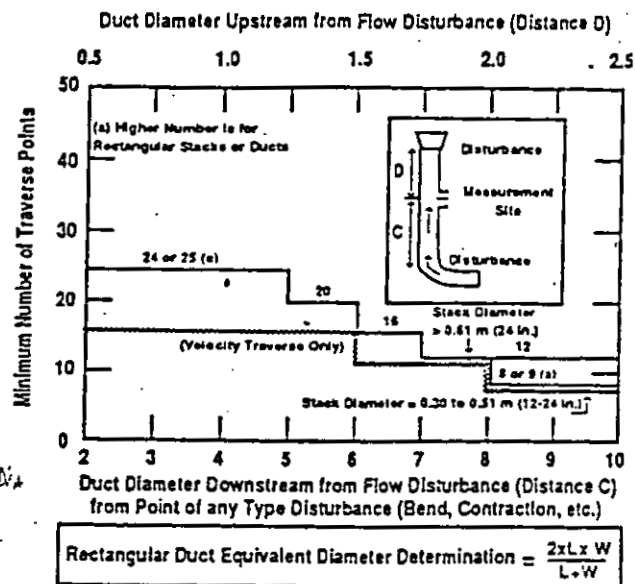
Barometric Pressure 29.5  
 Static Pressure 1.05  
 Temperature (Dry) 95  
 Temperature (Wet) 85  
 S. V. P. 0.6  
 (Water Saturation Vapor Pressure (PSII))  
 PST 0.0772  
 PS 29.5772  
 Vapor Pressure 1.1094  
 %Moisture 3.7508  
 Md 0.9625

# Traverse Point Location for Circular and Rectangular Ducts

Project No.: 20974  
 Client: IBP Logan Port Ind  
 Date: 8-20-96  
 Sampling Location: WET COOKER  
 Internal Stack Diameter: 10"  
 Nipple Length: 0  
 Total Stack Diameter: 10"  
 Nearest Upstream Disturbance (C): 24' ~~24.5~~ 28.8 ft  
 Nearest Downstream Disturbance (D): 32' 9.2 ft  
 Calculator: SM

GROUND level  
TS = 120°F 7.5% MOISTURE

| Traverse Point Number | Fraction of Stack ID<br>( $\frac{1}{100}$ ) | Stack ID | Traverse Point<br>(1 = 2 = Point) | Nipple Length | Traverse Point<br>Inside of Far Wall to Outside<br>of Port Nipple<br>(3 = 4 = Point) |
|-----------------------|---------------------------------------------|----------|-----------------------------------|---------------|--------------------------------------------------------------------------------------|
| 1                     | .032                                        | 10"      | .32                               | N/A           | .5                                                                                   |
| 2                     | .105                                        |          | 1.05                              |               | 1.05                                                                                 |
| 3                     | .194                                        |          | 1.94                              |               | 1.9                                                                                  |
| 4                     | .323                                        |          | 3.23                              |               | 3.2                                                                                  |
| 5                     | .677                                        |          | 6.77                              |               | 6.8                                                                                  |
| 6                     | .806                                        |          | 8.06                              |               | 8.1                                                                                  |
| 7                     | .895                                        |          | 8.95                              |               | 9.0                                                                                  |
| 8                     | .968                                        |          | 9.68                              |               | 9.5                                                                                  |
| 9                     |                                             |          |                                   |               |                                                                                      |
| 10                    |                                             |          |                                   |               |                                                                                      |
| 11                    |                                             |          |                                   |               |                                                                                      |
| 12                    |                                             |          |                                   |               |                                                                                      |
| 13                    |                                             |          |                                   |               |                                                                                      |
| 14                    |                                             |          |                                   |               |                                                                                      |
| 15                    |                                             |          |                                   |               |                                                                                      |
| 16                    |                                             |          |                                   |               |                                                                                      |
| 17                    |                                             |          |                                   |               |                                                                                      |
| 18                    |                                             |          |                                   |               |                                                                                      |
| 19                    |                                             |          |                                   |               |                                                                                      |
| 20                    |                                             |          |                                   |               |                                                                                      |
| 21                    |                                             |          |                                   |               |                                                                                      |
| 22                    |                                             |          |                                   |               |                                                                                      |
| 23                    |                                             |          |                                   |               |                                                                                      |
| 24                    |                                             |          |                                   |               |                                                                                      |



Location of Traverse Points in Circular Stacks

|    | 4    | 6    | 8    | 10   | 12   | 14   | 16   | 18   | 20   | 22   | 24   |
|----|------|------|------|------|------|------|------|------|------|------|------|
| 1  | 5.7  | 4.4  | 3.2  | 2.6  | 2.1  | 1.3  | 1.5  | 1.4  | 1.3  | 1.1  | 1.1  |
| 2  | 25.0 | 14.6 | 10.5 | 8.2  | 6.7  | 5.7  | 4.9  | 4.4  | 3.9  | 3.5  | 3.2  |
| 3  | 75.0 | 29.6 | 19.4 | 14.6 | 11.8 | 9.9  | 8.5  | 7.5  | 6.7  | 6.0  | 5.5  |
| 4  | 93.3 | 70.4 | 32.3 | 22.6 | 17.7 | 14.6 | 12.5 | 10.9 | 9.7  | 8.7  | 7.9  |
| 5  |      | 85.4 | 67.7 | 34.2 | 25.0 | 20.1 | 16.9 | 14.6 | 12.9 | 11.6 | 10.5 |
| 6  |      | 95.6 | 80.6 | 65.8 | 35.6 | 26.9 | 22.0 | 18.8 | 16.5 | 14.6 | 13.2 |
| 7  |      |      | 89.5 | 77.4 | 64.4 | 36.6 | 28.3 | 23.6 | 20.4 | 18.0 | 16.1 |
| 8  |      |      | 96.8 | 85.4 | 75.0 | 63.4 | 37.5 | 29.6 | 25.0 | 21.5 | 19.4 |
| 9  |      |      |      | 91.8 | 82.3 | 73.1 | 62.5 | 38.2 | 30.6 | 26.2 | 23.0 |
| 10 |      |      |      | 97.4 | 88.2 | 79.9 | 71.7 | 61.8 | 38.8 | 31.5 | 27.2 |
| 11 |      |      |      |      | 93.3 | 85.4 | 78.0 | 70.4 | 61.2 | 39.3 | 32.3 |
| 12 |      |      |      |      | 97.9 | 90.1 | 83.1 | 76.4 | 69.4 | 60.7 | 39.8 |
| 13 |      |      |      |      |      | 94.3 | 87.5 | 81.2 | 75.0 | 68.5 | 60.2 |
| 14 |      |      |      |      |      | 98.2 | 91.5 | 85.4 | 79.6 | 73.8 | 67.7 |
| 15 |      |      |      |      |      |      | 95.1 | 89.1 | 83.5 | 78.2 | 72.8 |
| 16 |      |      |      |      |      |      | 98.4 | 92.5 | 87.1 | 82.0 | 77.0 |
| 17 |      |      |      |      |      |      |      | 95.6 | 90.3 | 85.4 | 80.6 |
| 18 |      |      |      |      |      |      |      | 98.6 | 93.3 | 88.4 | 83.9 |
| 19 |      |      |      |      |      |      |      |      | 96.1 | 91.3 | 86.8 |
| 20 |      |      |      |      |      |      |      |      | 98.7 | 94.0 | 89.5 |
| 21 |      |      |      |      |      |      |      |      |      | 96.5 | 92.1 |
| 22 |      |      |      |      |      |      |      |      |      | 98.9 | 94.5 |
| 23 |      |      |      |      |      |      |      |      |      |      | 96.8 |
| 24 |      |      |      |      |      |      |      |      |      |      | 98.9 |

Location of Traverse Points in Rectangular Stacks

|    | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    | 10   | 11   | 12   |
|----|------|------|------|------|------|------|------|------|------|------|------|
| 1  | 25.0 | 16.7 | 12.5 | 10.0 | 8.3  | 7.1  | 6.3  | 5.6  | 5.0  | 4.5  | 4.2  |
| 2  | 75.0 | 50.0 | 37.5 | 30.0 | 25.0 | 21.4 | 18.8 | 15.7 | 15.0 | 13.5 | 12.5 |
| 3  |      | 83.3 | 62.5 | 50.0 | 41.7 | 35.7 | 31.3 | 27.8 | 25.0 | 22.7 | 20.8 |
| 4  |      |      | 87.5 | 70.0 | 58.3 | 50.0 | 43.8 | 38.9 | 35.0 | 31.8 | 29.2 |
| 5  |      |      |      | 90.0 | 75.0 | 64.3 | 56.3 | 50.0 | 45.0 | 40.9 | 37.5 |
| 6  |      |      |      |      | 91.7 | 78.5 | 68.8 | 61.1 | 55.0 | 50.0 | 45.8 |
| 7  |      |      |      |      |      | 92.9 | 81.3 | 72.2 | 65.0 | 59.1 | 54.2 |
| 8  |      |      |      |      |      |      | 93.8 | 83.3 | 75.0 | 68.2 | 62.5 |
| 9  |      |      |      |      |      |      |      | 94.4 | 85.0 | 77.3 | 70.8 |
| 10 |      |      |      |      |      |      |      |      | 95.0 | 85.4 | 79.2 |
| 11 |      |      |      |      |      |      |      |      |      | 95.5 | 87.5 |
| 12 |      |      |      |      |      |      |      |      |      |      | 95.8 |

# VELOCITY TRAVERSE

|                                                                                   |                                                        |
|-----------------------------------------------------------------------------------|--------------------------------------------------------|
| Plant: <u>IBP</u>                                                                 | Date: <u>8/22/96</u>                                   |
| Unit Number: <u>WET COOKER</u>                                                    | Stack Diameter (in.): <u>10"</u>                       |
| Load Condition: <u>norm/PEAK</u>                                                  | Stack Gauge Pressure ("H <sub>2</sub> O): <u>+1.05</u> |
| Run No.: <u>2</u>                                                                 | Operators: <u>SM/DW</u>                                |
| Project No.: <u>20774-0</u>                                                       |                                                        |
| Barometric Pressure at Ground Level ("Hg): <u>29.50</u>                           |                                                        |
| Pitot Tube ID:                                                                    |                                                        |
| Pitot Tube Coefficient: <u>.84</u>                                                | Port Change Pitot Leak Check <u>Pass</u> <u>Fail</u>   |
| Estimated Stack CO <sub>2</sub> %: <u>0.0</u> %: <u>11.0</u> %:                   | Port #1 <u>—</u> <u>—</u>                              |
| Platform Elevation (feet): <u>ground</u>                                          | Port #2 <u>—</u> <u>—</u>                              |
| Schematic of Stack Cross Section:                                                 | Port #3 <u>—</u> <u>—</u>                              |
|  | Port #4 <u>—</u> <u>—</u>                              |
| <u>WET Bulb = 84°F DRY Bulb = 92°F</u>                                            | <u>SDP avg = 1.0575</u><br><u>TS avg</u>               |

| Traverse Point Number | Velocity Head (In H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1                     | 1.00                                | 107             |
| 2                     | 1.05                                | 107             |
| 3                     | 1.10                                | 107             |
| 4                     | 1.10                                | 107             |
| 5                     | 1.10                                | 108             |
| 6                     | 1.15                                | 107             |
| 7                     | 1.10                                | 107             |
| 8                     | 1.15                                | 107             |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              |                                     |                 |

| Traverse Point Number | Velocity Head (In H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1                     | 1.15                                | 104             |
| 2                     | 1.15                                | 104             |
| 3                     | 1.10                                | 104             |
| 4                     | 1.10                                | 105             |
| 5                     | 1.15                                | 104             |
| 6                     | 1.20                                | 103             |
| 7                     | 1.15                                | 103             |
| 8                     | 1.15                                | 103             |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              |                                     |                 |

## VELOCITY TRAVERSE

|                                                                 |                                                        |
|-----------------------------------------------------------------|--------------------------------------------------------|
| Plant: <u>28P</u>                                               | Date: <u>8/22/96</u>                                   |
| Unit Number: <u>WET COOKER</u>                                  | Stack Diameter (in.): <u>10"</u>                       |
| Load Condition: <u>PEAK / NORM</u>                              | Stack Gauge Pressure ("H <sub>2</sub> O): <u>+1.05</u> |
| Run No.: <u>3</u>                                               | Operators: <u>DW / SM</u>                              |
| Project No.: <u>20974-0</u>                                     |                                                        |
| Barometric Pressure at Ground Level ("Hg): <u>29.50</u>         |                                                        |
| Pitot Tube ID:                                                  |                                                        |
| Pitot Tube Coefficient: <u>.84</u>                              | Port Change Pitot Leak Check                           |
| Estimated Stack CO <sub>2</sub> %: <u>0.2</u> %: <u>11.0</u> %: | <u>Pass</u> <u>Fail</u>                                |
| Platform Elevation (feet): <u>6'</u>                            | Port #1 <u>—</u> <u>—</u>                              |
| Schematic of Stack Cross Section:                               | Port #2 <u>—</u> <u>—</u>                              |
| <u>SEE P1</u>                                                   | Port #3 <u>—</u> <u>—</u>                              |
| <u>WET Bulb &gt;</u>                                            | Port #4 <u>—</u> <u>—</u>                              |
| <u>Dry Bulb =</u>                                               | <u>√ΔPavg = 1.0498</u>                                 |

| Traverse Point Number | Velocity Head (in H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1                     | 1.15                                | 106             |
| 2                     | 1.15                                | 106             |
| 3                     | 1.20                                | 106             |
| 4                     | 1.15                                | 106             |
| 5                     | 1.10                                | 106             |
| 6                     | 1.15                                | 105             |
| 7                     | 1.10                                | 105             |
| 8                     | 1.10                                | 105             |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              |                                     |                 |

| Traverse Point Number | Velocity Head (in H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1                     | 1.10                                | 103             |
| 2                     | 1.00                                | 104             |
| 3                     | 1.05                                | 104             |
| 4                     | 1.15                                | 104             |
| 5                     | 1.20                                | 104             |
| 6                     | 1.05                                | 103             |
| 7                     | 1.00                                | 103             |
| 8                     | 1.00                                | 103             |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              |                                     |                 |

## VELOCITY TRAVERSE

|                                                                            |                                                        |
|----------------------------------------------------------------------------|--------------------------------------------------------|
| Plant: <u>IBP</u>                                                          | Date: <u>8/22/96</u>                                   |
| Unit Number: <u>WET COOKER</u>                                             | Stack Diameter (in.): <u>10"</u>                       |
| Load Condition: <u>PeAK / NORM</u>                                         | Stack Gauge Pressure ("H <sub>2</sub> O): <u>+1.05</u> |
| Run No.: <u>4</u>                                                          | Operators: <u>DW/gm</u>                                |
| Project No.: <u>20974-0</u>                                                |                                                        |
| Barometric Pressure at Ground Level ("Hg): <u>29.50</u>                    |                                                        |
| Pitot Tube ID:                                                             |                                                        |
| Pitot Tube Coefficient: <u>.84</u>                                         | Port Change Pitot Leak Check                           |
| Estimated Stack CO <sub>2</sub> %: <u>0.0</u> %: <u>11.0</u> %: <u>0.0</u> | <u>Pass</u> <u>Fail</u>                                |
| Platform Elevation (feet):                                                 | Port #1 <u>—</u> <u>—</u>                              |
| Schematic of Stack Cross Section:                                          | Port #2 <u>—</u> <u>—</u>                              |
|                                                                            | Port #3 <u>—</u> <u>—</u>                              |
|                                                                            | Port #4 <u>—</u> <u>—</u>                              |
| <u>WET Bulb</u><br><u>DRY Bulb</u>                                         | <u>√ ΔPavg 1.0516</u><br><u>Ts</u>                     |

| Traverse Point Number | Velocity Head (In H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1                     | 1.0                                 | 106             |
| 2                     | 1.05                                | 106             |
| 3                     | 1.1                                 | 106             |
| 4                     | 1.1                                 | 105             |
| 5                     | 1.1                                 | 105             |
| 6                     | 1.15                                | 105             |
| 7                     | 1.15                                | 103             |
| 8                     | 1.1                                 | 103             |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              |                                     |                 |

| Traverse Point Number | Velocity Head (In H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1                     | 1.1                                 | 103             |
| 2                     | 1.1                                 | 104             |
| 3                     | 1.05                                | 104             |
| 4                     | 1.15                                | 105             |
| 5                     | 1.15                                | 105             |
| 6                     | 1.20                                | 104             |
| 7                     | 1.1                                 | 104             |
| 8                     | 1.1                                 | 104             |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              |                                     |                 |

# Method 25 Field Data

Project Number: 20974-0 Client: IBP  
 Facility: IBP LOGANS Sample Location: WET COOKER  
 Location: LOGANSLOTT Operator: DW  
 Date: 8/21/90 Run Number: R2  
 Tank Number: 274 Trap Number: ATA Sample I.D. R2

|           | Tank Vacuum           |                         | Barometric Pressure |            | Ambient Temperature |
|-----------|-----------------------|-------------------------|---------------------|------------|---------------------|
|           | Manometer<br>mm/cm Hg | Gauge<br>mm/cm Hg/in Hg | mm/cm Hg/in. Hg     |            | C/F                 |
| Pretest   | <u>738</u>            | <u>30</u>               | <u>29.50</u>        | <u>749</u> | <u>90°F</u>         |
| Post Term | <u>738</u>            | <u>4</u>                | <u>29.50</u>        | <u>749</u> | <u>90°F</u>         |

Pretest Leak Rate (mm/cm Hg/5 min):

5 Hg/5min

WET Bulb 84  
 DRY 93

| Clock Time   | Sample Time | Gauge Vacuum<br>mm/cm Hg | Flowmeter Setting<br>mL | Temperature  |            | Comments |
|--------------|-------------|--------------------------|-------------------------|--------------|------------|----------|
|              |             |                          |                         | Probe<br>C/F | Box<br>C/F |          |
| <u>9:44</u>  | <u>0</u>    | <u>30</u>                | <u>130</u>              | <u>120</u>   | <u>120</u> |          |
|              |             | <u>29.5</u>              |                         |              |            |          |
| <u>9:54</u>  | <u>10</u>   | <u>25</u>                |                         |              |            |          |
|              |             | <u>22.5</u>              |                         |              |            |          |
| <u>10:04</u> | <u>20</u>   | <u>20</u>                |                         |              |            |          |
|              |             | <u>18</u>                |                         |              |            |          |
| <u>10:14</u> | <u>30</u>   | <u>16</u>                |                         |              |            |          |
|              |             | <u>14</u>                |                         |              |            |          |
| <u>10:24</u> | <u>40</u>   | <u>12</u>                |                         |              |            |          |
|              |             | <u>10</u>                |                         |              |            |          |
| <u>10:34</u> | <u>50</u>   | <u>8</u>                 |                         |              |            |          |
|              |             | <u>6</u>                 |                         |              |            |          |
| <u>10:44</u> | <u>60</u>   | <u>4</u>                 |                         |              |            |          |
|              |             |                          |                         |              |            |          |
|              |             |                          |                         |              |            |          |
|              |             |                          |                         |              |            |          |
|              |             |                          |                         |              |            |          |
|              |             |                          |                         |              |            |          |
|              |             |                          |                         |              |            |          |
|              |             |                          |                         |              |            |          |

TRC

# Method 25 Field Data

Project Number: 20974-0 Client: IBP  
 Facility: IBP Sample Location: WET COOKER  
 Location: LOGANS PORT Operator: DEW  
 Date: 8/22/96 Run Number: R3  
 Tank Number: 105 Trap Number: CE Sample I.D.: 6213

|           | Tank Vacuum             |                          | Barometric Pressure |     | Ambient Temperature |
|-----------|-------------------------|--------------------------|---------------------|-----|---------------------|
|           | Manometer<br>(mm/cm Hg) | Gauge<br>mm/cm Hg/in. Hg | mm/cm Hg/in. Hg     |     | C/F                 |
| Pretest   | 738                     | 29                       | 29.58               | 749 | 90°F                |
| Post Term | 58                      | 3                        |                     | 749 | 90°F                |

Pretest Leak Rate (mm/cm Hg/5 min): 6

| Clock Time | Sample Time | Gauge Vacuum<br>mm/cm Hg | Flowmeter Setting<br>mL | Temperature  |            | Comments |
|------------|-------------|--------------------------|-------------------------|--------------|------------|----------|
|            |             |                          |                         | Probe<br>C/F | Box<br>C/F |          |
| 10:44      | 0           | 29                       | 130                     | 120          | 120        |          |
|            |             | 27                       |                         | ↓            | ↓          |          |
| 11:04      | 10          | 25                       |                         | ↓            | ↓          |          |
|            |             | 22.5                     |                         |              |            |          |
| 11:14      | 20          | 20                       |                         |              |            |          |
|            |             | 17.5                     |                         |              |            |          |
| 11:24      | 30          | 15                       |                         |              |            |          |
|            |             | 13                       |                         |              |            |          |
| 11:34      | 40          | 11                       |                         |              |            |          |
|            |             | 9                        |                         |              |            |          |
| 11:44      | 50          | 7                        |                         |              |            |          |
|            |             | 5                        |                         |              |            |          |
| 11:54      | 60          | 3                        |                         |              |            |          |
|            |             |                          |                         |              |            |          |
|            |             |                          |                         |              |            |          |
|            |             |                          |                         |              |            |          |
|            |             |                          |                         |              |            |          |
|            |             |                          |                         |              |            |          |
|            |             |                          |                         |              |            |          |
|            |             |                          |                         |              |            |          |
|            |             |                          |                         |              |            |          |
|            |             |                          |                         |              |            |          |

# Method 25 Field Data

Project Number: 20974-0 Client: IBP  
 Facility: IBP Sample Location: WET COOKER  
 Location: Logans Port Operator: DW  
 Date: 8/22/96 Run Number: R4  
 Tank Number: 154 Trap Number: ATC Sample I.D. R4

|           | Tank Vacuum           |                         | Barometric Pressure |     | Ambient Temperature |
|-----------|-----------------------|-------------------------|---------------------|-----|---------------------|
|           | Manometer<br>mm/cm Hg | Gauge<br>mm/cm Hg/in Hg | mm/cm Hg/in. Hg     |     | C/F                 |
| Pretest   | 7840                  | 30                      | 29.50               | 749 | 90°F                |
| Post Term |                       | 3                       |                     | 749 | 90°F                |

Pretest Leak Rate (mm/cm Hg/5 min): 8

| Clock Time | Sample Time      | Gauge Vacuum<br>mm/cm Hg | Flowmeter Setting<br>mL | Temperature    |              | Comments |
|------------|------------------|--------------------------|-------------------------|----------------|--------------|----------|
|            |                  |                          |                         | Probe<br>°C/°F | Box<br>°C/°F |          |
| 12:27      | 0                | 30                       | 130                     | 120            | 120          |          |
|            | <del>10</del>    | 27.5                     | ↓                       | ↓              | ↓            |          |
| 37         | 10               | 2.5                      | ↓                       | ↓              | ↓            |          |
|            | 20               | 22.5                     | ↓                       | ↓              | ↓            |          |
| 47         |                  | 20                       | ↓                       | ↓              | ↓            |          |
|            | 30               | 17.5                     |                         |                |              |          |
| 57         | 30               | 15                       |                         |                |              |          |
|            | <del>40</del>    | 12.5                     |                         |                |              |          |
| 1307       | 40               | 11.0                     |                         |                |              |          |
|            | 450              | 9                        |                         |                |              |          |
| 1317       | 50               | 7                        |                         |                |              |          |
|            | <del>60</del> 55 | 5                        |                         |                |              |          |
| 1327       | 60               | 3                        |                         |                |              |          |
|            |                  |                          |                         |                |              |          |
|            |                  |                          |                         |                |              |          |
|            |                  |                          |                         |                |              |          |
|            |                  |                          |                         |                |              |          |
|            |                  |                          |                         |                |              |          |
|            |                  |                          |                         |                |              |          |
|            |                  |                          |                         |                |              |          |
|            |                  |                          |                         |                |              |          |

## Method 25 Field Data

Project Number: 20974-0 Client: IBP  
Facility: IBP Sample Location: WET COOKER  
Location: LOG ANSLEY Operator: DW  
Date: 8/22/96 Run Number: BLANK  
Tank Number: 221 Trap Number: CL Sample I.D. BLANK

|           | Tank Vacuum           |                         | Barometric<br>Pressure<br>mm/cm Hg/in. Hg | Ambient<br>Temperature<br>C/F. |
|-----------|-----------------------|-------------------------|-------------------------------------------|--------------------------------|
|           | Manometer<br>mm/cm Hg | Gauge<br>mm/cm Hg/in Hg |                                           |                                |
| Pretest   | 0                     | 0                       | 749                                       | 90°F                           |
| Post Term | 0                     | 0                       | 749                                       | 90°F                           |

Pretest Leak Rate (mm/cm Hg/5 min): N/A

[illegible]

**TRC**

# Orsat Analysis

Project No. 20974-0  
 Name DBP  
 Facility LOGANSFORD, IN  
 Source WET COOKER  
 Sample Location EXHAUST STACK  
 GC Checkoff - Pretest \_\_\_\_\_

Date 8/22/96  
 Run 1-3 or 2-4  
 Operator DW, SM  
 Comments: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

Great Leak Checked (Yes/No)

Expiration Date of Reagents \_\_\_\_\_

Purge System with Sample Gas YES

Ambient Air Check CO<sub>2</sub> 0.0 O<sub>2</sub> 20.9

Audit Gas Check (measured/actual): CO<sub>2</sub> 1 O<sub>2</sub> 1 CO 1

| Sample Point  | Time  | CO <sub>2</sub> Reading 1 | (CO <sub>2</sub> ) Reading 2 |      | (CO) Reading 3 |     | F <sub>C</sub> |
|---------------|-------|---------------------------|------------------------------|------|----------------|-----|----------------|
|               |       |                           | Actual                       | Net  | Actual         | Net |                |
| <del>R1</del> |       |                           |                              |      |                |     |                |
| R2            | 10.00 | 0.0                       |                              | 20.9 |                |     |                |
| R3            | 11.30 | 0.0                       |                              | 20.9 |                |     |                |
| R4            | 13.00 | 0.0                       |                              | 20.9 |                |     |                |
|               |       |                           |                              |      |                |     |                |

Net CO<sub>2</sub> reading = Reading 2 - Reading 1 (Actual)

Net CO reading = Reading 3 - Reading 2 (Actual)

## CO Validation

Calculate F<sub>C</sub>

$$F_C = \frac{20.9 - \%O_2}{\%CO_2}$$

Fuel \_\_\_\_\_

Reported F<sub>C</sub> \_\_\_\_\_

## Expected F<sub>C</sub> Ranges

|                    |               |
|--------------------|---------------|
| Anthracite/Lignite | 1.015 - 1.130 |
| Bituminous         | 1.033 - 1.230 |
| Distillate Oil     | 1.250 - 1.413 |
| Residual Oil       | 1.270 - 1.370 |
| Natural Gas        | 1.500 - 1.535 |
| Wood Bark          | 1.000 - 1.120 |
| Municipal Garbage  | 1.040 - 1.177 |

Other \_\_\_\_\_

**TRC**

Run 1

DATE:

20-Aug-96

CLIENT REP: Rechelle Kruse

PLANT:

IBP

WITNESSED?: yes

GC TYPE

BURNER TYPE: N/A

OPERATOR:

SM, DW

GENERATOR TYPE: N/A

TEST LOCATION:

Blood Furnace

O2 GENERATOR TYPE: N/A

## CALIBRATION GASES

| O2  | CO2 | CO  | SO2 | NOx | THC outlet |
|-----|-----|-----|-----|-----|------------|
| 0   | 0   | 0   | 0   | 0   | 0          |
| N/A | N/A | N/A | N/A |     | 29.68      |
| N/A | N/A | N/A | N/A |     | 49.42      |
|     |     |     |     |     | 83.47      |

| END TIME | SAMPLE POINT | O2 wet | CO2 ppm | SO2 ppm | THC Outlet ppm | CO ppm | NOx ppm | COMMENTS |
|----------|--------------|--------|---------|---------|----------------|--------|---------|----------|
| 14:42    | 1            |        |         |         | 12.97          |        |         |          |
|          |              |        |         |         |                |        |         |          |
|          |              |        |         |         |                |        |         |          |
|          | AVERAGES     | ERR    | ERR     | ERR     | 12.97          | ERR    | ERR     |          |

Barometric Pres:

29.3

## EFFLUENT GAS CONCENTRATION, WET BASIS, PPM

|           | O2  | CO2 | SO2 | THC Outlet | CO  | NOx |
|-----------|-----|-----|-----|------------|-----|-----|
| PRE ZERO  | 0   |     | 0   | 0          | 0   | 0   |
| POST ZERO | 0   |     | 0   | 1          |     | 0   |
| ACT SPAN  | N/A | N/A | N/A | 29.68      | N/A | N/A |
| PRE SPAN  | 0   |     | 0   | 31.7       |     | 0   |
| POST SPAN | 0   |     | 0   | 28         |     | 0   |

|          |     |     |     |       |     |     |
|----------|-----|-----|-----|-------|-----|-----|
| GAS CONC | ERR | ERR | ERR | 12.61 | ERR | ERR |
|----------|-----|-----|-----|-------|-----|-----|

## EFFLUENT GAS CONC CALCULATION

$$\text{GAS CONC.} = (\text{Avg Stk Conc} - \text{Avg Zero Cal}) * (\text{Span Conc} / (\text{Avg Span Cal} - \text{Avg Zero Cal}))$$

Run 2

DATE:

20-Aug-96

CLIENT REP: Rechelle Kruse

PLANT:

IBP

WITNESSED?: yes

GC TYPE

BURNER TYPE: N/A

OPERATOR:

SM, DW

GENERATOR TYPE: N/A

TEST LOCATION:

Blood Furnace

O2 GENERATOR TYPE: N/A

## CALIBRATION GASES

| O2  | CO2 | CO  | SO2 | NOx | THC outlet |
|-----|-----|-----|-----|-----|------------|
| 0   | 0   | 0   | 0   | 0   | 0          |
| N/A | N/A | N/A | N/A |     | 29.68      |
| N/A | N/A | N/A | N/A |     | 49.42      |
|     |     |     |     |     | 83.47      |

| END TIME | SAMPLE POINT | O2 wet | CO2 ppm | SO2 ppm | THC Outlet ppm | CO ppm | NOx ppm | COMMENTS |
|----------|--------------|--------|---------|---------|----------------|--------|---------|----------|
| 15:50    | 1            |        |         |         | 8.67           |        |         |          |
|          |              |        |         |         |                |        |         |          |
|          |              |        |         |         |                |        |         |          |
|          | AVERAGES     | ERR    | ERR     | ERR     | 8.67           | ERR    | ERR     |          |

Barometric Pres:

29.3

## EFFLUENT GAS CONCENTRATION, WET BASIS, PPM

|           | O2  | CO2 | SO2 | THC Outlet | CO  | NOx |
|-----------|-----|-----|-----|------------|-----|-----|
| PRE ZERO  | 0   |     | 0   | 1          | 0   | 0   |
| POST ZERO | 0   |     | 0   | 1          |     | 0   |
| ACT SPAN  | N/A | N/A | N/A | 29.68      | N/A | N/A |
| PRE SPAN  | 0   |     | 0   | 28         |     | 0   |
| POST SPAN | 0   |     | 0   | 35.5       |     | 0   |

|          |     |     |     |      |     |     |
|----------|-----|-----|-----|------|-----|-----|
| GAS CONC | ERR | ERR | ERR | 7.40 | ERR | ERR |
|----------|-----|-----|-----|------|-----|-----|

## EFFLUENT GAS CONC CALCULATION

$$\text{GAS CONC.} = (\text{Avg Stk Conc} - \text{Avg Zero Cal}) * (\text{Span Conc} / (\text{Avg Span Cal} - \text{Avg Zero Cal}))$$

Run 3

DATE:

20-Aug-96

CLIENT REP: Rechelle Kruse

PLANT:

IBP

WITNESSED?: yes

DC TYPE

BURNER TYPE: N/A

OPERATOR:

SM, DW

GENERATOR TYPE: N/A

TEST LOCATION:

Blood Furnace

O2 GENERATOR TYPE: N/A

## CALIBRATION GASES

| O2  | CO2 | CO  | SO2 | NOx | THC outlet |
|-----|-----|-----|-----|-----|------------|
| 0   | 0   | 0   | 0   | 0   | 0          |
| N/A | N/A | N/A | N/A |     | 29.68      |
| N/A | N/A | N/A | N/A |     | 49.42      |
|     |     |     |     |     | 83.47      |

| END TIME | SAMPLE POINT | O2 wet | CO2 ppm | SO2 ppm | THC Outlet ppm | CO ppm | NOx ppm | COMMENTS |
|----------|--------------|--------|---------|---------|----------------|--------|---------|----------|
| 17:02    | 1            |        |         |         | 8.25           |        |         |          |
|          |              |        |         |         |                |        |         |          |
|          |              |        |         |         |                |        |         |          |
|          | AVERAGES     | ERR    | ERR     | ERR     | 8.25           | ERR    | ERR     |          |

Barometric Pres:

29.3

## EFFLUENT GAS CONCENTRATION, WET BASIS, PPM

|           | O2  | CO2 | THC Inlet | THC Outlet | CO  | NOx |
|-----------|-----|-----|-----------|------------|-----|-----|
| PRE ZERO  | 0   |     | 0         | 1          | 0   | 0   |
| POST ZERO | 0   |     | 0         | 0.5        |     | 0   |
| ACT SPAN  | N/A | N/A | N/A       | 49.42      | N/A | N/A |
| PRE SPAN  | 0   |     | 0         | 50         |     | 0   |
| POST SPAN | 0   |     | 0         | 55         |     | 0   |
| GAS CONC  | ERR | ERR | ERR       | 7.16       | ERR | ERR |

## EFFLUENT GAS CONC CALCULATION

$$\text{GAS CONC.} = (\text{Avg Stk Conc} - \text{Avg Zero Cal}) * (\text{Span Conc} / (\text{Avg Span Cal} - \text{Avg Zero Cal}))$$

### Calculations

|                                 |        |        |        |
|---------------------------------|--------|--------|--------|
| Analyte                         | C3H8   | C3H8   | C3H8   |
| FWhc lbs/lb-mole                | 44     | 44     | 44     |
| Stack Flowrate, dry scf/hr      | 35,298 | 35,298 | 35,298 |
| Moisture, %                     | 17.7   | 17.8   | 17.9   |
| Cppmv                           | 12.61  | 7.40   | 7.16   |
| Cppmv minus CH4                 | 10.51  | 5.64   | 3.36   |
| Hydrocarbons Emissions (lbs/hr) | 0.423  | 0.227  | 0.135  |

$$\text{Lbs/Hr} = \text{Cppmv minus CH4} \cdot \text{FWhc} \cdot (\text{Stack Flowrate(dscf/hr)} / 60) \cdot (1.554 \cdot 10^4)$$

## WET BULB / DRY BULB MOISTURE DETERMINATION

Client IBP Logansport  
 Date 8/20/1996  
 Project Number 20974-0000-00000  
 Plant Logansport, IN  
 Sampling Location roof vent  
 Source Blood Furnace  
 Run Number 1

Barometric Pressure 29.3  
 Static Pressure 1.55  
 Temperature (Dry) 199  
 Temperature (Wet) 139  
 S. V. P. (at Twet) 2.9  
 (Water Saturation Vapor Pressure (PSI))  
 PST 0.1140  
 PS 29.4140  
 Vapor Pressure 5.2126  
 % Moisture 17.7215  
 Md 0.8228

## WET BULB / DRY BULB MOISTURE DETERMINATION

Client IBP Logansport  
 Date 8/20/1996  
 Project Number 20974-0000-00000  
 Plant Logansport, IN  
 Sampling Location roof vent  
 Source Blood Furnace  
 Run Number 2

Barometric Pressure 29.3  
 Static Pressure 1.55  
 Temperature (Dry) 193  
 Temperature (Wet) 136  
 S. V. P. (at Twet) 2.9  
 (Water Saturation Vapor Pressure (PSI))  
 PST 0.1140  
 PS 29.4140  
 Vapor Pressure 5.2484  
 % Moisture 17.8431  
 Md 0.8216

## WET BULB / DRY BULB MOISTURE DETERMINATION

Client IBP Logansport  
 Date 8/20/1996  
 Project Number 20974-0000-00000  
 Plant Logansport, IN  
 Sampling Location roof vent  
 Source Blood Furnace  
 Run Number 3

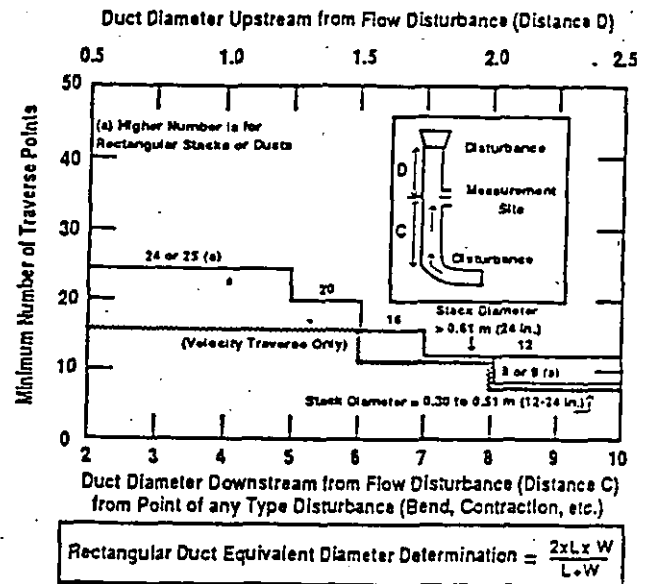
Barometric Pressure 29.3  
 Static Pressure 1.55  
 Temperature (Dry) 195  
 Temperature (Wet) 140  
 S. V. P. (at Twet) 2.9  
 (Water Saturation Vapor Pressure (PSI))  
 PST 0.1140  
 PS 29.4140  
 Vapor Pressure 5.2699  
 % Moisture 17.9162  
 Md 0.8208

# Traverse Point Location for Circular and Rectangular Ducts

Project No.: 20974-0000-00000  
 Client: IBP LOGANSFORT IND.  
 Date: 8-20-96  
 Sampling Location: BLOOD FURNACE  
 Internal Stack Diameter: 18"  
 Nipple Length: 0  
 Total Stack Diameter: 18"  
 Nearest Upstream Disturbance (C): 14' 9.3 Dia  
 Nearest Downstream Disturbance (D): 20' 13.3 Dia  
 Calculator: SM

Roof level  
 TS = 194°F

| Traverse Point Number | Fraction of Stack ID<br>( $\frac{1}{100}$ ) | Stack ID | Traverse Point<br>(1 x 2 = Point) | Nipple Length | Traverse Point<br>Inside of Far Wall to Outside of Port Nipple<br>(3 x 4 = Point) |
|-----------------------|---------------------------------------------|----------|-----------------------------------|---------------|-----------------------------------------------------------------------------------|
| 1                     | .044                                        | 18"      | .792                              | N/A           | .8                                                                                |
| 2                     | .146                                        |          | 2.63                              |               | 2.6                                                                               |
| 3                     | .296                                        |          | 5.33                              |               | 5.3                                                                               |
| 4                     | .444                                        |          | 8.07                              |               | 8.0                                                                               |
| 5                     | .594                                        |          | 10.82                             |               | 10.8                                                                              |
| 6                     | .746                                        |          | 13.58                             |               | 13.6                                                                              |
| 7                     |                                             |          |                                   |               |                                                                                   |
| 8                     |                                             |          |                                   |               |                                                                                   |
| 9                     |                                             |          |                                   |               |                                                                                   |
| 10                    |                                             |          |                                   |               |                                                                                   |
| 11                    |                                             |          |                                   |               |                                                                                   |
| 12                    |                                             |          |                                   |               |                                                                                   |
| 13                    |                                             |          |                                   |               |                                                                                   |
| 14                    |                                             |          |                                   |               |                                                                                   |
| 15                    |                                             |          |                                   |               |                                                                                   |
| 16                    |                                             |          |                                   |               |                                                                                   |
| 17                    |                                             |          |                                   |               |                                                                                   |
| 18                    |                                             |          |                                   |               |                                                                                   |
| 19                    |                                             |          |                                   |               |                                                                                   |
| 20                    |                                             |          |                                   |               |                                                                                   |
| 21                    |                                             |          |                                   |               |                                                                                   |
| 22                    |                                             |          |                                   |               |                                                                                   |
| 23                    |                                             |          |                                   |               |                                                                                   |
| 24                    |                                             |          |                                   |               |                                                                                   |



Location of Traverse Points in Circular Stacks

|    | 4    | 6    | 8    | 10   | 12   | 14   | 16   | 18   | 20   | 22   | 24   |
|----|------|------|------|------|------|------|------|------|------|------|------|
| 1  | 5.7  | 4.4  | 3.2  | 2.6  | 2.1  | 1.3  | 1.6  | 1.4  | 1.3  | 1.1  | 1.1  |
| 2  | 25.0 | 14.6 | 10.5 | 8.2  | 6.7  | 5.7  | 4.9  | 4.4  | 3.9  | 3.5  | 3.2  |
| 3  | 75.0 | 29.6 | 19.4 | 14.6 | 11.8 | 9.9  | 8.5  | 7.5  | 6.7  | 6.0  | 5.5  |
| 4  | 93.3 | 70.4 | 32.3 | 22.6 | 17.7 | 14.6 | 12.5 | 10.9 | 9.7  | 8.7  | 7.9  |
| 5  |      | 85.4 | 67.7 | 34.2 | 25.0 | 20.1 | 16.9 | 14.6 | 12.9 | 11.6 | 10.5 |
| 6  |      | 95.6 | 80.6 | 65.8 | 35.6 | 26.9 | 22.0 | 18.8 | 16.5 | 14.6 | 13.2 |
| 7  |      |      | 89.5 | 77.4 | 64.4 | 36.6 | 28.3 | 23.6 | 20.4 | 18.0 | 16.1 |
| 8  |      |      | 96.8 | 85.4 | 75.0 | 63.4 | 37.5 | 29.6 | 25.0 | 21.6 | 19.4 |
| 9  |      |      |      | 91.8 | 82.3 | 73.1 | 62.5 | 38.2 | 30.6 | 26.2 | 23.0 |
| 10 |      |      |      | 97.4 | 88.2 | 79.9 | 71.7 | 61.8 | 38.8 | 31.5 | 27.2 |
| 11 |      |      |      |      | 93.3 | 85.4 | 78.0 | 70.4 | 61.2 | 39.3 | 32.3 |
| 12 |      |      |      |      | 97.9 | 90.1 | 83.1 | 76.4 | 69.4 | 60.7 | 39.8 |
| 13 |      |      |      |      |      | 94.3 | 87.5 | 81.2 | 75.0 | 68.5 | 60.2 |
| 14 |      |      |      |      |      | 98.2 | 91.5 | 85.4 | 79.6 | 73.8 | 67.7 |
| 15 |      |      |      |      |      |      | 95.1 | 89.1 | 83.5 | 78.2 | 72.8 |
| 16 |      |      |      |      |      |      | 98.4 | 92.5 | 87.1 | 82.0 | 77.0 |
| 17 |      |      |      |      |      |      |      | 95.6 | 90.3 | 85.4 | 80.6 |
| 18 |      |      |      |      |      |      |      | 98.6 | 93.3 | 88.4 | 83.9 |
| 19 |      |      |      |      |      |      |      |      | 96.1 | 91.3 | 86.8 |
| 20 |      |      |      |      |      |      |      |      | 98.7 | 94.0 | 89.5 |
| 21 |      |      |      |      |      |      |      |      |      | 96.5 | 92.1 |
| 22 |      |      |      |      |      |      |      |      |      | 98.3 | 94.5 |
| 23 |      |      |      |      |      |      |      |      |      |      | 96.8 |
| 24 |      |      |      |      |      |      |      |      |      |      | 98.9 |

Location of Traverse Points in Rectangular Stacks

|    | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    | 10   | 11   | 12   |
|----|------|------|------|------|------|------|------|------|------|------|------|
| 1  | 25.0 | 16.7 | 12.5 | 10.0 | 8.3  | 7.1  | 6.3  | 5.6  | 5.0  | 4.5  | 4.2  |
| 2  | 75.0 | 50.0 | 37.5 | 30.0 | 25.0 | 21.4 | 18.8 | 15.7 | 15.0 | 13.5 | 12.5 |
| 3  |      | 83.3 | 62.5 | 50.0 | 41.7 | 35.7 | 31.3 | 27.8 | 25.0 | 22.7 | 20.8 |
| 4  |      |      | 87.5 | 70.0 | 58.3 | 50.0 | 43.8 | 38.9 | 35.0 | 31.8 | 29.2 |
| 5  |      |      |      | 90.0 | 75.0 | 64.3 | 56.3 | 50.0 | 45.0 | 40.9 | 37.5 |
| 6  |      |      |      |      | 91.7 | 78.6 | 68.8 | 61.1 | 55.0 | 50.0 | 45.8 |
| 7  |      |      |      |      |      | 92.9 | 81.3 | 72.2 | 65.0 | 59.1 | 54.2 |
| 8  |      |      |      |      |      |      | 93.8 | 83.3 | 75.0 | 68.2 | 62.5 |
| 9  |      |      |      |      |      |      |      | 94.4 | 85.0 | 77.3 | 70.8 |
| 10 |      |      |      |      |      |      |      |      | 95.0 | 85.4 | 79.2 |
| 11 |      |      |      |      |      |      |      |      |      | 95.5 | 87.5 |
| 12 |      |      |      |      |      |      |      |      |      |      | 95.8 |

## VELOCITY TRAVERSE

|                                                                             |                                                       |
|-----------------------------------------------------------------------------|-------------------------------------------------------|
| Place <u>IBP Logans Port</u>                                                | Date <u>8-20-96</u>                                   |
| Unit Number: <u>Blood Freezer</u>                                           | Stack Diameter (in.): <u>18.0</u>                     |
| Load Condition: <u>Normal/Peak</u>                                          | Stack Gauge Pressure (H <sub>2</sub> O): <u>+1.55</u> |
| Run No.: <u>1</u>                                                           | Operators: <u>SM/DW</u>                               |
| Project No.: <u>20974</u>                                                   |                                                       |
| Barometric Pressure at Ground Level (H <sub>2</sub> O): <u>29.30</u>        |                                                       |
| Pitot Tube ID:                                                              |                                                       |
| Pitot Tube Coefficient: <u>1.84</u>                                         | Port Change Pitot<br>Leak Check                       |
| Estimated Stack CO <sub>2</sub> %: <u>1.0</u> %: <u>19.0</u> %: <u>    </u> | Pass                                                  |
| Platform Elevation (feet): <u>25'</u>                                       | Fail                                                  |
| Schematic of Stack Cross Section:                                           |                                                       |
| <u>O<sub>2</sub> 18.5%</u>                                                  | Port #1                                               |
| <u>CO<sub>2</sub> 1.5%</u>                                                  | Port #2                                               |
|                                                                             | Port #3                                               |
|                                                                             | Port #4                                               |
| <u>195 Dry Bulb</u>                                                         | $\sqrt{AP} =$ <u>6.321</u>                            |
| <u>140 Wet Bulb</u>                                                         | TS = <u>195°F</u>                                     |
| <u>17% m</u>                                                                |                                                       |

| Transverse<br>Point<br>Number | Velocity<br>Head<br>(In H <sub>2</sub> O) | Stick<br>Temp.<br>(°F) |
|-------------------------------|-------------------------------------------|------------------------|
| 1A                            | .37                                       | 195                    |
| 2                             | .40                                       | 195                    |
| 3                             | .42                                       | 195                    |
| 4                             | .39                                       | 195                    |
| 5                             | .40                                       | 195                    |
| 6                             | .39                                       | 195                    |
|                               |                                           |                        |
|                               |                                           |                        |
|                               |                                           |                        |
|                               |                                           |                        |
|                               |                                           |                        |
|                               |                                           |                        |
|                               |                                           |                        |
|                               |                                           |                        |
| Average:                      | .3950                                     | 196                    |

| Traverse<br>Point<br>Number | Velocity<br>Head<br>(In H <sub>2</sub> O) | Stack<br>Temp.<br>(F) |
|-----------------------------|-------------------------------------------|-----------------------|
| 1 B                         | .37                                       | 195                   |
| 2                           | .40                                       | 195                   |
| 3                           | .41                                       | 195                   |
| 4                           | .43                                       | 195                   |
| 5                           | .46                                       | 195                   |
| 6                           | .36                                       | 195                   |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
| Average:                    | .4050                                     | 195                   |

**VELOCITY TRAVERSE**

| VELOCITY TEST LOG                                                                                                         |                                                                                                                                                                                                                                                                                                                                                                                                                                              |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
|---------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------|--------------|------------|------|------|---------|--|--|--|--|---------|--|--|--|--|---------|--|--|--|--|---------|--|--|--|--|
| Plant: IBP Loganston                                                                                                      | Date: 8/20/96                                                                                                                                                                                                                                                                                                                                                                                                                                |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Unit Number: BIOD FURNACE                                                                                                 | Stack Diameter (in.): 18"                                                                                                                                                                                                                                                                                                                                                                                                                    |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Load Condition: Norm / part                                                                                               | Stack Gauge Pressure ("H <sub>2</sub> O): +1.55                                                                                                                                                                                                                                                                                                                                                                                              |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Run No.: 2                                                                                                                | Operators: SM/Div                                                                                                                                                                                                                                                                                                                                                                                                                            |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Project No.: 20974-0                                                                                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                              |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Barometric Pressure at Ground Level ("Hg): 29.30                                                                          |                                                                                                                                                                                                                                                                                                                                                                                                                                              |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Pitot Tube ID:                                                                                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                              |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Pitot Tube Coefficient: .84                                                                                               | <table border="1"> <thead> <tr> <th>Port</th> <th>Change Pitot</th> <th>Leak Check</th> <th>Pass</th> <th>Fail</th> </tr> </thead> <tbody> <tr> <td>Port #1</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>Port #2</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>Port #3</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>Port #4</td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table> | Port       | Change Pitot | Leak Check | Pass | Fail | Port #1 |  |  |  |  | Port #2 |  |  |  |  | Port #3 |  |  |  |  | Port #4 |  |  |  |  |
| Port                                                                                                                      | Change Pitot                                                                                                                                                                                                                                                                                                                                                                                                                                 | Leak Check | Pass         | Fail       |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Port #1                                                                                                                   |                                                                                                                                                                                                                                                                                                                                                                                                                                              |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Port #2                                                                                                                   |                                                                                                                                                                                                                                                                                                                                                                                                                                              |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Port #3                                                                                                                   |                                                                                                                                                                                                                                                                                                                                                                                                                                              |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Port #4                                                                                                                   |                                                                                                                                                                                                                                                                                                                                                                                                                                              |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Estimated Stack CO <sub>2</sub> %: <u>1</u> 0.2% <u>9</u> H <sub>2</sub> O %: <u>  </u>                                   |                                                                                                                                                                                                                                                                                                                                                                                                                                              |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Platform Elevation (feet): 25'                                                                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                              |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |
| Schematic of Stack Cross Section:<br><br>$O_2 = 18.5$<br>$CO_2 = 1.5$<br><br>Dry Bulb - 193<br>Wet Bulb - 136      17% RH | $\sqrt{Sping} = .6307$<br><br>$T_{avg} = 193$                                                                                                                                                                                                                                                                                                                                                                                                |            |              |            |      |      |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |         |  |  |  |  |

| Traverse<br>Point<br>Number | Velocity<br>Head<br>(In H <sub>2</sub> O) | Stack<br>Temp.<br>(F) |
|-----------------------------|-------------------------------------------|-----------------------|
| 1                           | .34                                       |                       |
| 2                           | .40                                       |                       |
| 3                           | .41                                       |                       |
| 4                           | .42                                       |                       |
| 5                           | .41                                       |                       |
| 6                           | .37                                       |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
| Average:                    |                                           |                       |

| Traverse<br>Point<br>Number | Velocity<br>Head<br>(In H <sub>2</sub> O) | Stack<br>Temp.<br>(F) |
|-----------------------------|-------------------------------------------|-----------------------|
| 1                           | .41                                       |                       |
| 2                           | .44                                       |                       |
| 3                           | .43                                       |                       |
| 4                           | .36                                       |                       |
| 5                           | .41                                       |                       |
| 6                           | .38                                       |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
| Average:                    |                                           |                       |

# VELOCITY TRAVERSE

|                                                                             |                                                           |
|-----------------------------------------------------------------------------|-----------------------------------------------------------|
| Plant: <u>IBP Loganport</u>                                                 | Date: <u>8/20/90</u>                                      |
| Unit Number: <u>Blood Furnace</u>                                           | Stack Diameter (in.): <u>18"</u>                          |
| Load Condition: <u>Norm / Peat</u>                                          | Stack Gauge Pressure (in. H <sub>2</sub> O): <u>41.55</u> |
| Run No.: <u>3</u>                                                           | Operators: <u>Sm / DW</u>                                 |
| Project No.: <u>20974-0</u>                                                 |                                                           |
| Barometric Pressure at Ground Level (in. Hg): <u>29.70</u>                  |                                                           |
| Pitot Tube ID:                                                              |                                                           |
| Pitot Tube Coefficient: <u>.84</u>                                          | Port Change Pitot<br>Leak Check                           |
| Estimated Stack CO <sub>2</sub> %: <u>1.0</u> O <sub>2</sub> %: <u>19.5</u> | Pass                                                      |
| Platform Elevation (feet):                                                  | Fail                                                      |
| Schematic of Stack Cross Section:                                           | Port #1                                                   |
| $O_2 = 19.5$                                                                | Port #2                                                   |
| $CO_2 = 1.0$                                                                | Port #3                                                   |
| WET Bulb = 139                                                              | Port #4                                                   |
| Dry Bulb = 199                                                              |                                                           |
| 17% RH                                                                      |                                                           |
|                                                                             | $\sqrt{\Delta P_{avg}} = .6361$                           |
|                                                                             | $T_{avg} = 199.0^\circ F$                                 |

| Traverse Point Number | Velocity Head (in H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1A                    | .35                                 | 199             |
| 2                     | .38                                 | 199             |
| 3                     | .41                                 | 199             |
| 4                     | .43                                 | 199             |
| 5                     | .44                                 | 199             |
| 6                     | .44                                 | 199             |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              | .4083                               | 199             |

| Traverse Point Number | Velocity Head (in H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1B                    | .38                                 | 199             |
| 2                     | .41                                 | 199             |
| 3                     | .41                                 | 199             |
| 4                     | .40                                 | 199             |
| 5                     | .40                                 | 199             |
| 6                     | .41                                 | 199             |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              | .4017                               | 199             |

# Orsat Analysis

Project No. 20974-0  
 Vent IBP  
 From LOGANSPORT, IN  
 Source BLOOD FURNACE  
 Sample Location Roof EXHAUST  
 QC Checkoff - Pretest \_\_\_\_\_

Date 8/20/96  
 Run 1-3  
 Operator DW, SM  
 Comments: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

Orsat Leak Checked Yes/no

Expiration Date of Reagents \_\_\_\_\_

Purge System with Sample Gas YES

Ambient Air Check CO<sub>2</sub> 0.0 O<sub>2</sub> 20.9

Audit Gas Check (measured/actual): CO<sub>2</sub> 1 O<sub>2</sub> 1 CO 1

| Sample Point | Time  | CO <sub>2</sub> Reading 1 | (CO <sub>2</sub> ) Reading 2 |      | (CO) Reading 3 |     | F <sub>C</sub> |
|--------------|-------|---------------------------|------------------------------|------|----------------|-----|----------------|
|              |       |                           | Actual                       | Net  | Actual         | Net |                |
| R1           | 14:00 | 1.5                       | 20                           | 18.5 |                |     |                |
| R2           | 15:10 | 1.5                       | 20                           | 18.5 |                |     |                |
| R3           | 16:30 | 1.0                       | 20.5                         | 19.5 |                |     |                |
|              |       |                           |                              |      |                |     |                |
|              |       |                           |                              |      |                |     |                |

Net CO<sub>2</sub> reading = Reading 2 - Reading 1 (Actual)

Expected F<sub>C</sub> Ranges

Net CO reading = Reading 3 - Reading 2 (Actual)

## QC Validation

Calculate F<sub>C</sub>

$$F_C = \frac{20.9 - \%O_2}{\%CO_2}$$

|                    |               |
|--------------------|---------------|
| Anthracite/Lignite | 1.015 - 1.130 |
| Bituminous         | 1.033 - 1.230 |
| Distillate Oil     | 1.250 - 1.413 |
| Residual Oil       | 1.210 - 1.370 |
| Natural Gas        | 1.500 - 1.836 |
| Wood Bark          | 1.000 - 1.120 |
| Municipal Garbage  | 1.040 - 1.177 |

Other \_\_\_\_\_

Fuel \_\_\_\_\_

Reported F<sub>C</sub> \_\_\_\_\_

**TRC**

R1> INIT 02  
VEL NAME: VOC ?  
VEL TYPE: 9?  
E HOURLY AVERAGES: Y?

R1>  
.81240 - .84620  
7.349 ✓ 5.189  
5.612 ✓ 5.625 ✓  
.00380 - .00140  
.00340 - .00110  
.00380 - .00280  
.00340 - .00280

- 08/20/96 DAY= 233 12:42:02 - START Run#1 Blood Furnace

.88010 - .81240  
8.615 ✓ 9.349  
15.74 ✓ 5.612  
.00210 - .00380  
.00140 - .00340  
.00310 - .00380  
.00170 - .00340

- 08/20/96 DAY= 233 12:43:02

.89150 - .88010  
7.672 ✓ 8.615  
12.87 ✓ 15.74  
.00200 - .00210  
.00040 - .00140  
.00070 - .00310  
.00370 - .00170

- 08/20/96 DAY= 233 12:44:02

01 - .86000 - .89150  
02 7.229 ✓ 7.672  
03 9.109 ✓ 12.87  
04 - .00330 - .00200  
05 - .00410 - .00240  
06 - .00110 - .00370  
07 - .00310 - .00070

Tue 8/20/96 DAY= 233 12:45:02

01 - .63510 - .86000  
02 7.192 ✓ 7.229  
03 8.773 ✓ 9.109  
04 - .00520 - .00330  
05 - .00700 - .00410  
06 - .00040 - .00110

Page Average 8.01 ppm

07 -.22220 -.22210

Tue - 08/20/96 DAY= 233 12:46:02

01 -.21230 -.63510  
02 6.795 ✓ 7.192  
03 8.814 8.793  
04 .00000 -.00500  
05 .00000 -.00700  
06 -.20170 -.00040  
07 -.00310 -.00020

Tue - 08/20/96 DAY= 233 12:47:02

01 -.77860 -.91230  
02 6.375 ✓ 6.795  
03 8.912 8.814  
04 -.00010 -.00500  
05 -.00980 -.00050  
06 -.00240 -.00170  
07 -.00110 -.00310

Tue - 08/20/96 DAY= 233 12:48:02

01 -.91230 -.77860  
02 6.343 ✓ 6.375  
03 8.922 8.912  
04 -.00610 -.00310  
05 -.00680 -.00980  
06 -.20170 -.00240  
07 -.20140 -.00110

Tue - 08/20/96 DAY= 233 12:49:02

01 -.80000 -.91230  
02 6.427 ✓ 6.343  
03 8.932 8.922  
04 -.00800 -.00610  
05 -.00950 -.00680  
06 -.00040 -.20170  
07 -.00170 -.00140

Tue - 08/20/96 DAY= 233 12:50:02

01 -.90230 -.85000  
02 6.247 ✓ 6.427  
03 8.950 8.932  
04 -.00870 -.00680  
05 -.01170 -.00950  
06 -.00240 -.00040  
07 -.00340 -.00170

Tue - 08/20/96 DAY= 233 12:51:02

01 -.94610 -.90230  
02 6.206 ✓ 6.247  
03 8.811 8.950  
04 .00210 -.00370  
05 .00050 -.01170  
06 -.00140 -.00240  
07 -.20140 -.00340

Tue - 08/20/96 DAY= 233 12:52:02

01 -.77860 -.94610  
02 6.343 ✓ 6.206

Page 2 Average 6.27

Tue - 08/20/96 DAY= 233 12:59:02

01 -.74450 - .54610  
02 5.991 ✓ 5.962  
03 8.760 8.802  
04 -.00070 -.00000  
05 .00070 -.00070  
06 .0010 - .00170  
07 -.00240 -.00210

Tue - 08/20/96 DAY= 233 13:00:02

01 -.81230 - .74460  
02 5.837 ✓ 5.991  
03 8.787 8.760  
04 -.00000 -.00070  
05 -.00040 -.00070  
06 -.00240 -.00210  
07 -.00240 -.00240

Tue - 08/20/96 DAY= 233 13:01:02

01 -.90200 - .51230  
02 5.341 ✓ 5.307  
03 8.831 8.797  
04 .00040 -.00000  
05 .00000 -.00040  
06 -.00110 -.00240  
07 -.00240 -.00240

Tue - 08/20/96 DAY= 233 13:02:02

01 .00040 - .00200  
02 17.19 ✓ 5.341  
03 8.829 8.831  
04 .00000 .00040  
05 .00000 .00000  
06 -.00070 -.00110  
07 -.00140 -.00240

Tue - 08/20/96 DAY= 233 13:03:02

01 -.85150 - .77040  
02 26.48 ✓ 17.19  
03 8.874 8.889  
04 -.00040 .00000  
05 -.00040 .00000  
06 -.00200 -.00070  
07 -.00040 -.00140

Tue - 08/20/96 DAY= 233 13:04:02

01 -.34620 - .55150  
02 28.76 ✓ 26.48  
03 8.884 8.874  
04 -.00040 -.00040  
05 -.00040 -.00040  
06 .00030 -.00280  
07 .0010 - .00040

Tue - 08/20/96 DAY= 233 13:05:02

01 -.39140 - .94620  
02 29.01 ✓ 28.76  
03 8.880 8.884

P34 AUG= 16.928

03 8.356 8.311  
04 -.00710 -.00210  
05 -.00910 -.00650  
06 -.00110 -.00140  
07 -.00040 -.00140

Tue - 08/20/96 DAY= 233 12:53:02

01 -.81230 -.77650  
02 6.166 ✓ 5.546  
03 8.943 8.656  
04 -.00540 -.00710  
05 -.00610 -.00910  
06 -.00310 -.00110  
07 -.00110 -.00040

Tue - 08/20/96 DAY= 233 12:54:02

01 -.80200 -.81230  
02 6.061 ✓ 6.166  
03 8.776 8.943  
04 -.00070 -.00540  
05 -.00100 -.00610  
06 -.00240 -.00310  
07 -.00240 -.00110

Tue - 08/20/96 DAY= 233 12:55:02

01 -.81230 -.80200  
02 5.592 ✓ 6.061  
03 8.769 8.776  
04 -.00000 -.00070  
05 -.00070 -.00100  
06 -.00240 -.00240  
07 -.00280 -.00240

Tue - 08/20/96 DAY= 233 12:56:02

01 -.74460 -.81230  
02 5.023 ✓ 5.592  
03 8.841 8.769  
04 -.00630 -.00000  
05 -.00310 -.00070  
06 -.00140 -.00240  
07 -.00270 -.00280

Tue - 08/20/96 DAY= 233 12:57:02

01 -.86680 -.74460  
02 6.293 ✓ 5.023  
03 8.832 8.841  
04 -.00200 -.00630  
05 -.00300 -.00310  
06 -.00210 -.00140  
07 -.00110 -.00270

Tue - 08/20/96 DAY= 233 12:58:02

01 -.86680 -.86680  
02 5.962 ✓ 6.293  
03 8.832 8.832  
04 -.00000 -.00200  
05 -.00070 -.00300  
06 -.00170 -.00210  
07 -.00210 -.00110

Pg3 Avg = 6.016

35 -.00070 -.00040  
06 -.00350 -.00250  
07 -.00240 -.00210

Tue - 08/20/96 DAY= 233 13:06:02

01 .001610 -.00140  
02 .00161 ✓ 29.01  
03 8.775 8.000  
04 -.00040 -.00070  
05 -.00040 -.00070  
06 -.00170 -.00350  
07 -.00240 -.00240

Tue - 08/20/96 DAY= 233 13:07:03

01 -.00570 -.04610  
02 28.29 ✓ 27.61  
03 8.860 8.775  
04 .00000 -.00040  
05 .00000 -.00040  
06 -.00110 -.00170  
07 -.00130 -.00240

Tue - 08/20/96 DAY= 233 13:08:02

01 -.01230 -.00570  
02 28.71 ✓ 28.29  
03 8.794 8.860  
04 -.00070 .00000  
05 -.00070 .00000  
06 -.00070 -.00110  
07 .00000 -.00180

Tue - 08/20/96 DAY= 233 13:09:03

01 -.02280 -.01230  
02 28.57 ✓ 28.71  
03 8.804 8.794  
04 .00000 -.00070  
05 .00000 -.00070  
06 -.00000 -.00070  
07 -.00010 -.00000

Tue - 08/20/96 DAY= 233 13:10:02

01 -.07330 -.02280  
02 28.20 ✓ 28.57  
03 8.766 8.804  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00350  
07 -.00140 -.00310

Tue - 08/20/96 DAY= 233 13:11:02

01 -.04610 -.07330  
02 .00161 ✓ 28.20  
03 .00161 8.766  
04 -.00040 .00000  
05 -.00040 .00000  
06 -.00140 -.00070  
07 -.00290 -.00140

Pg 5 Avg = 23.40

Tue - 08/20/96 DAY= 233 13:12:02

01 -.33340 - .34510  
02 5.718 ✓ 7.051  
03 8.776 8.851  
04 -.00100 -.00040  
05 -.00070 -.00040  
06 -.00240 -.00140  
07 [REDACTED] 40 -.00280

Tue - 08/20/96 DAY= 233 13:13:05

01 -.78860 - .53540  
02 24.92 ✓ 5.718  
03 8.883 8.776  
04 -.00110 -.00100  
05 -.00110 -.00070  
06 -.00110 -.00240  
07 -.00110 -.00140

Tue - 08/20/96 DAY= 233 13:14:02

01 -.77950 - 78860  
02 28.84 ✓ 24.92  
03 8.772 8.883  
04 -.00110 -.00110  
05 -.00270 -.00110  
06 -.00210 -.00110  
07 -.00140 -.00110

Tue - 08/20/96 DAY= 233 13:15:02

01 -.02290 - .77950  
02 [REDACTED] 41 ✓ 28.84  
03 [REDACTED] 88 8.772  
04 -.00190 -.00110  
05 -.00210 -.00270  
06 -.00210 -.00210  
07 -.00140 -.00140

Tue - 08/20/96 DAY= 233 13:16:02

01 -.00000 - .02290  
02 29.94 ✓ 29.41  
03 8.535 8.883  
04 -.00040 -.00190  
05 -.00040 -.00210  
06 -.00280 -.00210  
07 -.00240 -.00140

Tue - 08/20/96 DAY= 233 13:17:02

01 -.78860 - .88880  
02 29.64 ✓ 29.94  
03 8.791 8.835  
04 .00000 -.00240  
05 .00000 -.00040  
06 -.00280 -.00280  
07 [REDACTED] 240 -.00240

Tue - 08/20/96 DAY= 233 13:18:02

01 -.74460 - .78860  
02 30.64 ✓ 29.64  
03 8.992 8.791  
04 -.00070 .00000  
05 -.00070 .00000

Pg. 6 Avg = 25.572

25 -.22250 -.00220  
27 -.00240 -.00240

Tue - 08/20/96 DAY= 233 13:19:02

01 -.99430 -.74450  
02 30.03 / 30.64  
03 72 3.892  
04 .00000 -.00070  
05 .00000 -.00070  
06 -.00350 -.00250  
07 -.00450 -.00240

Tue - 08/20/96 DAY= 233 13:20:02

01 -.74470 -.99430  
02 10.40 / 32.03  
03 8.961 8.870  
04 .00000 .00000  
05 .00000 .00000  
06 -.00310 -.00350  
07 -.00170 -.00450

Tue - 08/20/96 DAY= 233 13:21:02

01 -.00210 -.74470  
02 5.246 / 10.40  
03 8.837 8.961  
04 -.00240 .00000  
05 -.00040 .00000  
06 -.00240 -.00310  
07 -.00070 -.00170

Tue - 08/20/96 DAY= 233 13:22:03

01 -.01230 -.00210  
02 5.904 / 5.246  
03 8.843 8.837  
04 -.00070 -.00040  
05 -.00070 -.00040  
06 -.00210 -.00240  
07 -.00040 -.00070

Tue - 08/20/96 DAY= 233 13:23:02

01 -.04620 -.01230  
02 5.545 / 5.904  
03 8.819 8.843  
04 -.00040 -.00070  
05 -.00040 -.00070  
06 -.00170 -.00210  
07 -.00210 -.00040

Tue - 08/20/96 DAY= 233 13:24:02

01 -.73520 -.04620  
02 5.244 / 5.545  
03 8.319 8.819  
04 .00000 -.00040  
05 .00000 -.00040  
06 -.00140 -.00170  
07 -.00270 -.00210

Tue - 08/20/96 DAY= 233 13:25:02

Pg 6 Avg = 16.72

02 5.019 5.244  
03 9.932 9.791  
04 -.00070 .00000  
05 -.00070 .00000  
06 -.00170 -.00140  
07 -.00310 -.00270

Tu 08/20/96 DAY= 233 13:25:02

01 -.77850 -.77850  
02 4.531 5.019  
03 8.752 8.832  
04 .00200 -.00070  
05 .00000 -.00070  
06 -.00360 -.00170  
07 -.00240 -.00310

Tue - 08/20/96 DAY= 233 13:27:02

01 -.76870 -.77850  
02 4.538 4.531  
03 8.767 8.752  
04 .00000 .00000  
05 .00000 .00000  
06 -.00370 -.00390  
07 -.00240 -.00240

Tue - 08/20/96 DAY= 233 13:28:02

01 -.84620 -.76870  
02 4.482 4.538  
03 8.794 8.767  
04 .00000 .00000  
05 -.00040 .00000  
06 -.00380 -.00370  
07 -.00170 -.00240

Tue - 08/20/96 DAY= 233 13:29:02

01 -.91230 -.84620  
02 4.143 4.482  
03 8.333 8.794  
04 .00000 -.00040  
05 .00000 -.00040  
06 -.00240 -.00380  
07 -.00140 -.00170

Tue - 08/20/96 DAY= 233 13:30:02

01 -.73520 -.91230  
02 4.282 4.143  
03 8.792 8.333  
04 .00000 .00000  
05 .00000 .00000  
06 -.00310 -.00240  
07 -.00210 -.00140

Tu 08/20/96 DAY= 233 13:31:02

01 -.91230 -.73520  
02 3.666 4.282  
03 8.794 8.792  
04 .00000 .00000  
05 .00000 .00000  
06 -.00290 -.00310

Pg 7 Avg = 4.380

01 - .80210 - .80210

Tue - 09/20/96 DAY= 233 13:32:02

01 - .77850 - .81230  
02 ✓ 3.496 3.666  
03 8.264 8.794  
04 0.0000 0.0000  
05 0.0000 0.0000  
06 - .00140 - .00280  
07 - .00140 - .00210

Tue - 09/20/96 DAY= 233 13:33:02

01 - .83550 - .77850  
02 ✓ 3.351 3.466  
03 8.245 8.264  
04 0.0000 0.0000  
05 0.0000 0.0000  
06 - .00410 - .00140  
07 - .00270 - .00140

Tue - 09/20/96 DAY= 233 13:34:02

01 - .84610 - .83550  
02 ✓ 3.168 3.351  
03 8.733 8.845  
04 0.0000 0.0000  
05 0.0000 0.0000  
06 - .00140 - .00410  
07 - .00140 - .00270

Tue - 09/20/96 DAY= 233 13:35:02

01 - .81230 - .84610  
02 ✓ 3.531 3.168  
03 8.719 8.733  
04 0.0000 0.0000  
05 0.0000 0.0000  
06 - .00340 - .00140  
07 - .00110 - .00140

Tue - 09/20/96 DAY= 233 13:36:02

01 - .83550 - .81230  
02 ✓ 3.271 3.531  
03 8.733 8.719  
04 - .00040 0.0000  
05 - .00040 0.0000  
06 - .00540 - .00340  
07 - .00310 - .00110

Tue - 09/20/96 DAY= 233 13:37:02

01 - .81230 - .83550  
02 ✓ 3.382 3.271  
03 8.743 8.733  
04 - .00040 0.0000  
05 - .00040 0.0000  
06 - .00340 - .00540  
07 - .00170 - .00310

Tue - 09/20/96 DAY= 233 13:38:02

01 - .85000 - .81230  
02 ✓ 3.307 3.382

3.857

Page no =

03 8.789 8.743  
04 -.00240 -.00040  
05 -.00380 -.00000  
06 -.00340 -.00340  
07 -.00340 -.00170

Tue - 08/20/96 DAY= 233 13:39:02

01 .04620 -.38000  
02 ✓ 22.07 6.807  
03 6.713 6.709  
04 -.00000 -.00240  
05 -.00040 -.00360  
06 -.00070 -.00340  
07 -.00240 -.00340

Tue - 08/20/96 DAY= 233 13:40:02

01 -.99000 -.94620  
02 ✓ 24.53 22.07  
03 9.790 8.713  
04 -.00040 -.00000  
05 -.00410 -.00040  
06 -.00230 -.00070  
07 -.00170 -.00240

Tue - 08/20/96 DAY= 233 13:41:02

01 -.82300 -.88000  
02 ✓ 27.32 24.53  
03 8.672 8.790  
04 -.00380 -.00040  
05 .00000 -.00410  
06 .00190 -.00230  
07 -.00140 -.00170

Page 24.54  
avg

Tue - 08/20/96 DAY= 233 13:42:02 — STOP R1

01 -.88010 -.82300  
02 15.59 27.02  
03 8.636 8.672  
04 -.00240 -.00380  
05 -.00240 -.00350  
06 -.00170 -.00190  
07 -.00380 -.00140

Tue - 08/20/96 DAY= 233 13:43:02

01 -.90240 -.88010  
02 4.091 15.59  
03 8.673 8.636  
04 -.00000 -.00240  
05 -.00040 -.00240  
06 -.00240 -.00170  
07 -.00370 -.00380

Tue - 08/20/96 DAY= 233 13:44:02

01 .00040 -.90240  
02 5.263 4.091  
03 10.57+ 8.673  
04 -.00040 -.00000  
05 -.00110 -.00040  
06 -.00410 -.00240  
07 -.00210 -.00370

Tue - 08/20/96 DAY= 233 13:45:02

01 -.77650 -.81240  
02 6.191 5.063  
03 8.778 10.57+  
04 -.00140 -.00040  
05 .00210 -.00110  
06 .00110 -.00410  
07 -.00310 -.00210

Tue - 08/20/96 DAY= 233 13:46:02

01 -.77860 -.77850  
02 1.530 6.191  
03 8.715 9.778  
04 -.00310 -.00140  
05 -.00440 -.00210  
06 -.00240 -.00110  
07 -.00240 -.00310

Tue - 08/20/96 DAY= 233 13:47:02

01 -.77860 -.77860  
02 6.069 1.530  
03 11.17+ 8.715  
04 -.00110 -.00310  
05 -.00170 -.00440  
06 -.00240 -.00240  
07 -.00210 -.00240

Tue - 08/20/96 DAY= 233 13:48:02

01 .0030 -.77860  
02 26.51 6.069  
03 8.715 11.17+  
04 -.00240 -.00110  
05 -.00240 -.00170  
06 -.00310 -.00240  
07 -.00280 -.00210

Tue - 08/20/96 DAY= 233 13:49:02

01 -.00290 -.04630  
02 29.33 26.51  
03 8.644 8.715  
04 -.00280 -.00240  
05 -.00550 -.00240  
06 -.00040 -.00310  
07 -.00140 -.00280

Tue - 08/20/96 DAY= 233 13:50:02

01 .78860 -.00290  
02 33.42 29.33  
03 10.96+ 8.644  
04 -.00180 -.00280  
05 -.00520 -.00550  
06 .0010 -.00040  
07 .00140 -.00140

Tue - 08/20/96 DAY= 233 13:51:02

01 -.01240 -.78860  
02 31.70 33.42  
03 9.184 10.96+

START RZ  
BLOOD FURNACE  
CH # 2 0-100

32.56

05 - .00360 - .00520  
06 - .00140 - .00210  
07 - .00170 - .00140

Tue - 08/20/96 DAY= 233 13:52:02

01 - .00520 - .01240  
02 - .0051 31.70  
03 3.713 9.194  
04 - .00360 - .00170  
05 - .00930 - .00360  
06 - .00180 - .00140  
07 - .00210 - .00170

Tue - 08/20/96 DAY= 233 13:53:02

01 - .77060 - .85720  
02 ✓ 30.59 30.61  
03 8.740 8.719  
04 - .00710 - .00380  
05 - .00880 - .00930  
06 - .00210 - .00180  
07 - .00140 - .00210

Tue - 08/20/96 DAY= 233 13:54:02

01 - .01240 - .77060  
02 ✓ 11.09 30.59  
03 8.801 8.740  
04 - .00530 - .00710  
05 - .00950 - .00880  
06 - .00110 - .00210  
07 - .00140 - .00140

Tue - 08/20/96 DAY= 233 13:55:02

01 - .00210 - .01240  
02 ✓ 4.307 11.09  
03 8.732 8.801  
04 - .00540 - .00530  
05 - .00850 - .00950  
06 - .00110 - .00110  
07 - .00210 - .00140

Tue - 08/20/96 DAY= 233 13:56:02

01 - .04620 - .00010  
02 ✓ 4.259 4.307  
03 8.773 8.732  
04 - .00820 - .00540  
05 - .01050 - .00850  
06 - .00260 - .00110  
07 - .00170 - .00210

Tue - 08/20/96 DAY= 233 13:57:02

01 - .03560 - .04620  
02 ✓ 4 4.258  
03 8.777 8.773  
04 - .00770 - .00820  
05 - .01070 - .01050  
06 - .00110 - .00260  
07 - .00140 - .00170

Tue - 08/20/96 DAY= 233 13:58:02

14.00

01 -.73870 -.93560  
02 ✓19.63 3.174  
03 8.664 8.677  
04 -.00760 -.00770  
05 -.01060 -.01070  
06 -.00110 -.00110  
07 0.00140 -.00140

Tue - 06/20/96 DAY= 233 13:09:02

01 -.84630 -.78870  
02 ✓26.32 19.63  
03 8.658 8.664  
04 -.00210 -.00760  
05 -.00440 -.01060  
06 -.00110 -.00110  
07 -.00110 -.00040

Tue - 06/20/96 DAY= 233 14:00:02

01 -.85730 -.84630  
02 ✓27.19 26.32  
03 8.626 8.658  
04 -.00240 -.00210  
05 -.00520 -.00440  
06 -.00110 -.00110  
07 -.00000 -.00110

Tue - 06/20/96 DAY= 233 14:01:02

01 -.88010 -.85730  
02 ✓27.19 27.19  
03 8.626 8.626  
04 -.00310 -.00240  
05 -.00530 -.00520  
06 -.00110 -.00110  
07 -.00070 -.00000

Tue - 06/20/96 DAY= 233 14:02:02

01 -.85730 -.88010  
02 ✓26.27 27.19  
03 8.594 8.658  
04 -.00150 -.00310  
05 -.00310 -.00530  
06 -.00110 -.00110  
07 -.00140 -.00070

Tue - 06/20/96 DAY= 233 14:03:02

01 -.83560 -.85730  
02 ✓4.038 26.27  
03 8.597 8.594  
04 -.00170 -.00130  
05 -.00100 -.00310  
06 -.00070 -.00110  
07 -.00070 -.00140

Tue - 06/20/96 DAY= 233 14:04:03

01 -.81240 -.83560  
02 ✓3.139 4.038  
03 8.671 8.597  
04 -.00140 -.00170  
05 -.00140 -.00100

26 -.00240 -.00070  
27 .00070 -.00070

Tue - 06/20/96 DAY= 233 14:05:02

01 -.84630 -.81240  
02 3.139  
03 8.671  
04 -.00070 -.00140  
05 -.00070 -.00140  
06 -.00040 -.00240  
07 -.00070 .00070

Tue - 06/20/96 DAY= 233 14:06:02

01 -.83560 -.84630  
02 3.307 3.312  
03 8.592 8.614  
04 -.00140 -.00070  
05 -.00100 -.00070  
06 -.00170 -.00040  
07 -.00310 -.00070

Tue - 06/20/96 DAY= 233 14:07:02

01 -.68020 -.83560  
02 3.224 3.307  
03 8.631 8.592  
04 -.00070 -.00140  
05 -.00040 -.00100  
06 -.00140 -.00170  
07 -.00170 -.00310

Tue - 06/20/96 DAY= 233 14:08:02

01 -.88020 -.88020  
02 3.258 3.224  
03 8.622 8.631  
04 .00000 -.00070  
05 .00000 -.00040  
06 -.00040 -.00140  
07 -.00040 -.00170

Tue - 06/20/96 DAY= 233 14:09:02

01 -.83560 -.88020  
02 3.379 3.258  
03 8.633 8.622  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00040  
07 -.00040 -.00040

Tue - 06/20/96 DAY= 233 14:10:02

01 -.81250 -.83560  
02 3.326 3.379  
03 8.633  
04 .00000 .00000  
05 .00000 .00000  
06 -.00210 -.00170  
07 -.00000 -.00040

Tue - 06/20/96 DAY= 233 14:11:02

02 ✓3.459 3.326  
03 8.535 8.619  
04 .00000 .00000  
05 .00000 .00000  
06 .00110 -.00210  
07 .00070 -.00000

Tu 08/20/96 DAY= 233 14:12:02

01 -.86900 -.71090  
02 ✓3.474 3.459  
03 8.583 8.535  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 .00110  
07 -.00170 .00070

Tue - 08/20/96 DAY= 233 14:13:02

01 -.67710 -.86900  
02 ✓3.511 3.474  
03 8.569 8.583  
04 .00000 .00000  
05 .00000 .00000  
06 .00040 -.00110  
07 -.00040 -.00170

Tue - 08/20/96 DAY= 233 14:14:02

01 -.71090 -.67710  
02 ✓3.716 3.511  
03 8.598 8.569  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 .00040  
07 -.00070 -.00040

Tue - 08/20/96 DAY= 233 14:15:02

01 -.86900 -.71090  
02 ✓3.764 3.716  
03 8.670 8.598  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00110  
07 -.00040 -.00070

Tue - 08/20/96 DAY= 233 14:16:02

01 -.84630 -.86900  
02 ✓3.714 3.764  
03 8.613 8.670  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00070  
07 -.00040 -.00040

Tu 08/20/96 DAY= 233 14:17:02

01 -.00220 -.84630  
02 ✓3.672 3.714  
03 8.614 8.613  
04 .00000 .00000  
05 .00000 .00000  
06 -.00240 -.00140

3.62

07 - .00040 - .00040

Tue - 08/20/96 DAY= 233 14:18:03

01 - .00020 - .00020  
02 ✓ 3.733 3.672  
03 8.541 3.514  
04 .00000 .00000  
05 .00000 .00000  
06 - .00040 - .00040  
07 - .00070 .00040

Tue - 08/22/96 DAY= 233 14:19:02

01 - .00020 - .00020  
02 ✓ 6.457 3.783  
03 8.527 8.541  
04 .00000 .00000  
05 .00000 .00000  
06 - .00070 - .00040  
07 - .00040 - .00070

Tue - 08/20/96 DAY= 233 14:20:02

01 - .00020 - .00020  
02 ✓ 3.790 6.457  
03 8.516 9.527  
04 .00000 .00000  
05 .00000 .00000  
06 - .00070 - .00070  
07 - .00040 - .00040

Tue - 08/20/96 DAY= 233 14:21:02

01 - .00000 - .00020  
02 ✓ 3.720 3.790  
03 8.530 8.516  
04 .00000 .00000  
05 .00000 .00000  
06 - .00040 - .00070  
07 - .00070 - .00040

Tue - 08/20/96 DAY= 233 14:22:02

01 - .00020 - .00000  
02 ✓ 3.561 3.720  
03 8.533 8.530  
04 .00000 .00000  
05 .00000 .00000  
06 - .00070 - .00040  
07 .00000 - .00070

Tue - 08/20/96 DAY= 233 14:23:02

01 - .00020 - .00020  
02 ✓ 3.416 3.561  
03 8.534 8.533  
04 .00000 .00000  
05 .00000 .00000  
06 - .00140 - .00070  
07 - .00040 .00000

Tue - 08/20/96 DAY= 233 14:24:02

01 - .00000 - .00020  
02 ✓ 3.720 3.416

272.613  
28 29.736

4.06

03 8.573 8.534  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00140  
07 -.00040 -.00040

Tue - 08/20/96 DAY= 233 14:25:02

01 -.84630 -.83560  
02 ✓ 3.832 3.723  
03 8.633 8.573  
04 .00000 .00000  
05 .00000 .00000  
06 -.00000 -.00070  
07 -.00070 -.00040

Tue - 08/20/96 DAY= 233 14:25:02

01 -.84630 -.84630  
02 ✓ 4.011 3.832  
03 8.596 8.633  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00000  
07 -.00110 -.00070

Tue - 08/20/96 DAY= 233 14:27:02

01 -.86900 -.84630  
02 ✓ 4.378 4.011  
03 8.626 8.596  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00170  
07 -.00040 -.00110

Tue - 08/20/96 DAY= 233 14:29:02

01 -.88020 -.86900  
02 ✓ 3.942 4.378  
03 8.635 8.626  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00110  
07 -.00070 -.00040

Tue - 08/20/96 DAY= 233 14:29:02

01 -.83560 -.88020  
02 ✓ 4.017 3.942  
03 8.651 8.635  
04 .00000 .00000  
05 .00000 .00000  
06 .00040 .00000  
07 .00070 -.00070

Tue - 08/20/96 DAY= 233 14:30:03

01 .00000 -.83560  
02 ✓ 4.004 4.017  
03 8.593 8.651  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 .00040  
07 -.00070 .00070

$$27.904 / 7 = 3.986$$

Tue - 02/20/96 DAY= 233 14:31:02

01 -.89020 -.89020  
02 3.976 4.004  
03 8.560 8.583  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00040  
07 -.00040 -.00070

Tue - 02/20/96 DAY= 233 14:32:02

01 -.86500 -.89020  
02 3.617 3.976  
03 8.643 8.560  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 .00000  
07 .00000 -.00040

Tue - 02/20/96 DAY= 233 14:33:03

01 -.84630 -.86900  
02 3.551 3.617  
03 8.624 8.643  
04 .00000 .00000  
05 .00000 .00000  
06 .00040 .00000  
07 .00040 .00000

Tue - 02/20/96 DAY= 233 14:34:02

01 -.84630 -.84630  
02 3.501 3.551  
03 8.565 8.624  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 .00040  
07 .00000 .00040

Tue - 02/20/96 DAY= 233 14:35:02

01 -.81250 -.89020  
02 3.829 3.921  
03 8.488 8.565  
04 .00000 .00000  
05 .00000 .00000  
06 -.00000 -.00040  
07 -.00040 .00000

Tue - 02/20/96 DAY= 233 14:36:02

01 -.86920 -.81250  
02 3.686 3.829  
03 8.481 8.488  
04 .00000 .00000  
05 .00000 .00000  
06 .00040 -.00000  
07 .00000 -.00040

Tue - 02/20/96 DAY= 233 14:37:03

01 -.88020 -.86900  
02 3.522 3.686  
03 8.456 8.481

$25 \frac{592}{2} = 3.0951$

01 .00000 .00000  
02 .00000 .00000  
03 -.00040 -.00040  
07 -.00070 .00000

Tue - 08/29/96 DAY= 233 14:36:02

01 .00000 .00000  
02 .00000 .00000  
03 3.449 3.456  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00040  
07 -.00040 -.00070

Tue - 08/29/96 DAY= 233 14:39:02

01 -.00020 -.00020  
02 3.734 4.105  
03 9.503 8.449  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00110  
07 -.00040 -.00040

Tue - 08/29/96 DAY= 233 14:40:02

01 -.00000 -.00000  
02 2.780 3.734  
03 8.487 9.503  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00170  
07 .00000 -.00040

Tue - 08/29/96 DAY= 233 14:41:02

01 -.00020 -.00000  
02 -.00000 2.783  
03 8.474 8.487  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00040  
07 -.00110 .00000

Tue - 08/29/96 DAY= 233 14:42:02

01 -.00000 .00000  
02 -3.661 -.00000  
03 8.532 8.474  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00070  
07 -.00070 -.00110

Tue - 08/29/96 DAY= 233 14:43:02

01 -.00020 -.00000  
02 -3.661 -3.661  
03 8.547 8.532  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00040  
07 -.00110 -.00070

Tue - 08/29/96 DAY= 233 14:44:02

pg Aug. 2.30

01 -.83020 -.83020  
02 -3.614- -3.614-  
03 8.599 8.547  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00070  
07 .00070 -.00110

Tue - 02/20/96 DAY= 233 14:45:02

01 -.90240 -.88020  
02 -3.607- -3.614-  
03 8.679 8.599  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00140  
07 -.00040 -.00070

Tue - 02/20/96 DAY= 233 14:46:02

01 -.88020 -.90240  
02 -3.621- -3.607-  
03 8.789 8.679  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00040  
07 -.00070 -.00040

Tue - 02/20/96 DAY= 233 14:47:02

01 -.88020 -.88020  
02 .00000 -3.621-  
03 .00000 8.789  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 .00000  
07 -.00040 -.00070

Tue - 02/20/96 DAY= 233 14:48:02

01 -.90240 -.88020  
02 -3.606- -3.620-  
03 9.171 8.956  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00140  
07 -.00240 -.00040

Tue - 02/20/96 DAY= 233 14:49:02

01 -.88020 -.90240  
02 -3.609- -3.606-  
03 9.330 9.171  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00070  
07 .00000 -.00040

Tue - 02/20/96 DAY= 233 14:50:02

— STOP R2

Pg Avg = 0

Page

DCN#R1>

01 -.83540 -.99160  
02 .4339 22.89  
03 8.561 8.534  
04 -.00270 -.00760  
05 -.00370 -.00890  
06 -.00140 -.00350  
07 -.00270 -.00140

Tue - 08/20/96 DAY= 233 15:02:02

01 -.91390 -.83540  
02 19.93 ✓ .4339  
03 8.557 8.561  
04 -.00710 -.00270  
05 -.00950 -.00370  
06 -.00210 -.00140  
07 -.00340 -.00270

Tue - 08/20/96 DAY= 233 15:03:03 - Start Run #3 1503 End time 1623 Blood Furnace.

01 -.85710 -.91390  
02 19.93 ✓ 19.93  
03 8.524 8.557  
04 -.00140 -.00710  
05 -.00520 -.00950  
06 -.00210 -.00210  
07 -.00240 -.00340

Tue - 08/20/96 DAY= 233 15:04:02

01 -.84610 -.85710  
02 12.70 ✓ 27.63  
03 8.598 8.524  
04 -.00710 -.00140  
05 -.00910 -.00520  
06 -.00170 -.00210  
07 -.00140 -.00240

Tue - 08/20/96 DAY= 233 15:05:02

01 -.86000 -.84610  
02 6.355 ✓ 12.70  
03 8.640 8.598  
04 -.00410 -.00710  
05 -.00540 -.00910  
06 -.00110 -.00170  
07 170 -.00140

Tue - 08/20/96 DAY= 233 15:06:02

01 -.90220 -.86000  
02 12.78 ✓ 6.355  
03 8.770 8.640  
04 -.00570 -.00410

Pg Avg = 15.98

06 -.00140 -.00110  
07 -.00070 -.00170

Tue - 08/20/96 DAY= 233 15:07:05

01 -.81230 -.90220  
02 3.863 ✓ 12.78  
03 8.44 8.770  
04 -.00140 -.00070  
05 -.00240 -.00040  
06 -.00170 -.00240  
07 -.00070 -.00070

Tue - 08/20/96 DAY= 233 15:08:02

01 -.84610 -.81230  
02 3.153 ✓ 2.863  
03 8.822 8.944  
04 -.00440 -.00140  
05 -.00340 -.00240  
06 -.00170 -.00170  
07 -.00170 -.00070

Tue - 08/20/96 DAY= 233 15:09:02

01 -.87990 -.84610  
02 3.169 ✓ 3.153  
03 8.908 8.822  
04 -.00070 -.00440  
05 -.00110 -.00340  
06 -.00280 -.00170  
07 -.00170 -.00170

Tue - 08/20/96 DAY= 233 15:10:02

01 -.80200 -.87990  
02 3.025 ✓ 3.169  
03 8.912 8.822  
04 -.00030 -.00070  
05 -.00040 -.00110  
06 -.00110 -.00280  
07 -.00210 -.00170

Tue - 08/22/96 DAY= 233 15:11:02

01 -.80000 -.80200  
02 2.959 ✓ 3.025  
03 8.919 8.812  
04 -.00140 -.00030  
05 -.00170 -.00040  
06 -.00380 -.00110  
07 -.00340 -.00210

Tue - 08/20/96 DAY= 233 15:12:02

01 -.81230 -.80000  
02 2.959 ✓ 2.959  
03 8.908 8.919  
04 -.00040 -.00140  
05 -.00340 -.00170  
06 -.00210 -.00380  
07 -.00040 -.00340

Tue - 08/22/96 DAY= 233 15:13:02

Pg Avg = 5.00

01 -.88888 - .91220  
02 3.118 ✓ 2.859  
03 8.993 8.938  
04 -.00070 -.00340  
05 -.00200 -.00340  
06 -.00210 -.00210  
07 -.00070 -.00040

Tu - 08/20/96 DAY= 233 15:14:02

01 -.84610 -.86880  
02 3.153 ✓ 3.118  
03 8.951 8.893  
04 .00000 -.00070  
05 .00000 -.00200  
06 -.00210 -.00210  
07 -.00240 -.00070

Tue - 08/20/96 DAY= 233 15:15:02

01 -.77840 -.84610  
02 2.837 ✓ 3.153  
03 8.919 8.951  
04 .00000 .00000  
05 .00000 .00000  
06 -.00240 -.00210  
07 -.00240 -.00040

Tue - 08/20/96 DAY= 233 15:16:02

01 -.83540 -.77840  
02 2.639 ✓ 2.857  
03 8.977 8.919  
04 .00000 .00000  
05 .00000 .00000  
06 -.00240 -.00240  
07 -.00070 -.00240

Tue - 08/20/96 DAY= 233 15:17:02

01 -.84610 -.83540  
02 2.781 ✓ 2.639  
03 8.961 8.977  
04 -.00110 .00000  
05 -.00110 .00000  
06 -.00210 -.00240  
07 -.00240 -.00070

Tue - 08/20/96 DAY= 233 15:18:02

01 -.77840 -.84610  
02 2.844 ✓ 2.781  
03 8.970 8.961  
04 .00000 -.00110  
05 .00000 -.00110  
06 -.00110 -.00210  
07 -.00340 -.00240

Tu - 08/20/96 DAY= 233 15:19:02

01 -.90220 -.77840  
02 2.751 ✓ 2.844  
03 8.971 8.970  
04 .00000 .00000  
05 .00000 .00000  
06 -.00540 -.00110

pg 114 2.578

07 - .00470 - .00340

Tue - 08/20/96 DAY= 233 15:20:02

01 - .77840 - .90220  
02 2.722✓ 2.751  
03 8.897 8.871  
04 .00000 .00000  
05 .00000 .00000  
06 -.00380 - .00540  
07 -.00280 - .00470

Tue - 08/20/96 DAY= 233 15:21:02

01 -.81230 - .77840  
02 2.616✓ 2.722  
03 8.913 8.897  
04 .00000 .00000  
05 .00000 .00000  
06 -.00280 - .00380  
07 -.00210 - .00250

Tue - 08/20/96 DAY= 233 15:22:02

01 -.90220 - .81230  
02 2.756✓ 2.616  
03 8.825 8.913  
04 .00000 .00000  
05 .00000 .00000  
06 -.00210 - .00280  
07 -.00140 - .00210

Tue - 08/20/96 DAY= 233 15:23:02

01 -.81230 - .90220  
02 2.607✓ 2.756  
03 -.0363 8.825  
04 .00000 .00000  
05 .00000 .00000  
06 -.00340 - .00210  
07 -.00070 - .00140

Tue - 08/20/96 DAY= 233 15:24:02

01 -.86880 - .81230  
02 2.591✓ 2.607  
03 -.0044 - .0363  
04 .00000 .00000  
05 .00000 .00000  
06 -.00470 - .00340  
07 -.00170 - .00070

Tue - 08/20/96 DAY= 233 15:25:02

01 -.83540 - .86880  
02 2.934✓ 2.591  
03 -.0031 - .0044  
04 .00000 .00000  
05 .00000 .00000  
06 -.00410 - .00470  
07 -.00170 - .00170

Tue - 08/20/96 DAY= 233 15:26:03

01 -.84610 - .83540  
02 2.802✓ 2.934

Pg Avg 2.747

33 -.0031 -.0031  
04 .00020 .00000  
05 .00000 .00000  
06 -.00170 -.00410  
07 -.00280 -.00170

Tue - 08/20/96 DAY= 233 15:27:02

01 -.00200 -.04610  
02 2.997 3.004  
03 -.0031 -.0031  
04 .00000 .00000  
05 .00000 .00000  
06 -.00310 -.00170  
07 -.00110 -.00280

Tue - 09/20/96 DAY= 233 15:28:02

01 -.77840 -.00200  
02 3.314 2.997  
03 -.0031 -.0031  
04 .00000 .00000  
05 .00000 .00000  
06 -.00210 -.00310  
07 -.00240 -.00110

Tue - 08/20/96 DAY= 233 15:29:02

01 -.73520 -.77840  
02 3.442 3.314  
03 -.0031 -.0031  
04 .00000 .00000  
05 .00000 .00000  
06 -.00310 -.00210  
07 -.00170 -.00240

Tue - 08/20/96 DAY= 233 15:30:02

01 -.97990 -.73520  
02 3.141 3.442  
03 -.0041 -.0031  
04 .00000 .00000  
05 .00000 .00000  
06 -.00550 -.00310  
07 -.00380 -.00170

Tue - 08/20/96 DAY= 233 15:31:02

01 -.06000 -.97990  
02 3.065 3.141  
03 -.0031 -.0041  
04 .00000 .00000  
05 .00000 .00000  
06 -.00370 -.00550  
07 -.00240 -.00380

Tue - 09/20/96 DAY= 233 15:32:02

01 .00040 -.06000  
02 2.952 3.065  
03 -.0037 -.0031  
04 .00000 .00000  
05 .00000 .00000  
06 -.00440 -.00370  
07 -.00210 -.00240

$Pg_{avg} = 3.152$

Tue - 08/20/96 DAY= 233 15:33:03

01 -.74460 -.93540  
02 3.936 ✓ 2.952  
03 -.0024 -.0037  
04 .00000 .00000  
05 .00000 .00000  
06 .00110 -.00440  
07 -.00240 -.00210

Tue - 08/20/96 DAY= 233 15:34:02

01 -.74460 -.74460  
02 7.519 ✓ 3.836  
03 -.0017 -.0024  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00110  
07 -.00170 -.00240

Tue - 08/20/96 DAY= 233 15:35:02

01 -.76860 -.74460  
02 5.237 ✓ 7.513  
03 -.0017 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00140  
07 -.00110 -.00170

Tue - 08/20/96 DAY= 233 15:36:02

01 .00090 -.76860  
02 5.286 ✓ 5.237  
03 -.0029 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00390 -.00170  
07 -.00210 -.00110

Tue - 08/20/96 DAY= 233 15:37:02

01 -.06880 -.07990  
02 6.155 ✓ 5.266  
03 -.0024 -.0029  
04 .00000 .00000  
05 .00000 .00000  
06 -.00270 -.00390  
07 -.00240 -.00210

Tue - 08/20/96 DAY= 233 15:38:02

01 -.77840 -.86830  
02 9.229 ✓ 6.355  
03 -.0029 -.0024  
04 .00000 .00000  
05 .00000 .00000  
06 .00040 -.00270  
07 -.00110 -.00240

Tue - 08/20/96 DAY= 233 15:39:02

01 -.93540 -.77840  
02 10.99 ✓ 9.229  
03 -.0021 -.0029

Py Avg = 7.022

05 .00000 .00000  
06 -.00210 -.00240  
07 -.00240 -.00110

Tue - 08/20/96 DAY= 233 15:40:02

01 -.81230 -.83540  
02 11.47 ✓ 10.99  
03 -.0014 -.0021  
04 .00000 .00000  
05 .00000 .00000  
06 -.00210 -.00210  
07 -.00210 -.00240

Tue - 08/20/96 DAY= 233 15:41:02

01 -.87990 -.81230  
02 10.79 ✓ 11.47  
03 -.0014 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00210  
07 -.00340 -.00210

Tue - 08/20/96 DAY= 233 15:42:02

01 -.80200 -.87990  
02 10.80 ✓ 10.79  
03 .0007 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00140  
07 -.00210 -.00340

Tue - 08/20/96 DAY= 233 15:43:02

01 -.87990 -.80200  
02 10.90 ✓ 10.80  
03 -.0021 -.0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00310 -.00140  
07 -.00240 -.00210

Tue - 08/20/96 DAY= 233 15:44:02

01 -.81230 -.87990  
02 17.93 ✓ 10.90  
03 .0007 -.0021  
04 .00000 .00000  
05 .00000 .00000  
06 -.00240 -.00310  
07 -.00380 -.00240

Tue - 08/20/96 DAY= 233 15:45:02

01 -.91380 -.81230  
02 22.86 ✓ 17.83  
03 .0000 .0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00410 -.00240

Pg 15 = 14.108

01 - .00110 - .00000

Tue - 08/20/96 DAY= 233 15:46:02

01 - .77840 - .91380  
02 27.51 ✓ 22.36  
03 .0004 .0000  
04 .0000 .0000  
05 .0000 .0000  
06 -.00070 -.00410  
07 -.00070 -.00110

Tue - 08/20/96 DAY= 233 15:47:02

01 - .74460 - .77840  
02 20.52 ✓ 27.51  
03 -.0000 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00070  
07 -.00110 -.00070

Tue - 08/20/96 DAY= 233 15:48:02

01 - .77840 - .74460  
02 25.64 ✓ 20.52  
03 .0004 -.0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00310 -.00170  
07 -.00140 -.00110

Tue - 08/20/96 DAY= 233 15:49:02

01 -.95710 - .77840  
02 27.34 ✓ 25.64  
03 -.0007 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00240 -.00310  
07 -.00310 -.00140

Tue - 08/20/96 DAY= 233 15:50:02

01 -.81230 - .95710  
02 28.07 ✓ 27.34  
03 .0000 -.0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00240  
07 -.00170 -.00310

Tue - 08/20/96 DAY= 233 15:51:02

01 -.81230 - .81230  
02 23.45 ✓ 28.07  
03 .0004 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00110  
07 -.00240 -.00170

Tue - 08/20/96 DAY= 233 15:52:02

01 -.91380 - .81230  
02 20.15 ✓ 23.45

Page = 25.67

03 -.0017 .0024  
04 .00000 .00000  
05 .00000 .00000  
06 -.00340 -.00070  
07 -.00210 -.00240

Tue - 08/20/96 DAY= 233 15:53:02

01 -.01230 -.91300  
02 3.551 / 22.15  
03 -.0038 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00240 -.00340  
07 -.00310 -.00210

Tue - 08/20/96 DAY= 233 15:54:02

01 -.03540 -.01230  
02 3.947 / 3.551  
03 -.0037 -.0038  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00240  
07 -.00410 -.00310

Tue - 08/20/96 DAY= 233 15:55:02

01 -.07990 -.03540  
02 4.047 / 3.947  
03 -.0041 -.0037  
04 .00000 .00000  
05 .00000 .00000  
06 -.00340 -.00170  
07 -.00210 -.00410

Tue - 08/20/96 DAY= 233 15:56:02

01 -.06000 -.07990  
02 4.001 / 4.047  
03 -.0051 -.0041  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00340  
07 -.00170 -.00210

Tue - 08/20/96 DAY= 233 15:57:02

01 -.06000 -.06000  
02 3.364 / 4.001  
03 -.0034 -.0051  
04 .00000 .00000  
05 .00000 .00000  
06 -.00310 -.00170  
07 -.00440 -.00170

Tue - 08/20/96 DAY= 233 15:58:03

01 .00000 / .06000  
02 4.335 / 3.364  
03 -.0038 -.0034  
04 .00000 .00000  
05 .00000 .00000  
06 -.00210 -.00310  
07 -.00300 -.00440

Pg Avg= 3.908

Tue - 03/20/96 DAY= 233 15:59:02

01 -.96880 -.97990  
02 4.099 ✓ 4.035  
03 -.0041 -.0038  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 .00000  
07 -.00170 -.00300

Tue - 03/20/96 DAY= 233 16:00:03

01 -.84610 -.85880  
02 4.151 ✓ 4.099  
03 -.0038 -.0041  
04 .00000 .00000  
05 .00000 .00000  
06 -.00310 -.00240  
07 -.00280 -.00170

Tue - 03/20/96 DAY= 233 16:01:02

01 -.74460 -.94610  
02 3.998 ✓ 4.151  
03 -.0028 -.0038  
04 .00000 .00000  
05 .00000 .00000  
06 -.00000 -.00310  
07 -.00070 -.00280

Tue - 03/20/96 DAY= 233 16:02:02

PA5 = 4.047

Run 1

DATE:

21-Aug-96

CLIENT REP:

Rechelle Kruse

PLANT:

IBP

WITNESSED?:

yes

DOC TYPE

BURNER TYPE:

N/A

OPERATOR:

SM, DW

GENERATOR TYPE:

N/A

TEST LOCATION:

Hydrolizer

O2 GENERATOR TYPE:

N/A

## CALIBRATION GASES

| O2  | CO2 | CO  | SO2 | NOx | THC outlet |
|-----|-----|-----|-----|-----|------------|
| 0   | 0   | 0   | 0   | 0   | 0          |
| N/A | N/A | N/A | N/A |     | 29.68      |
| N/A | N/A | N/A | N/A |     | 49.42      |
|     |     |     |     |     | 83.47      |

| END TIME | SAMPLE POINT | O2 wet | CO2 ppm | SO2 ppm | THC Outlet ppm | CO ppm | NOx ppm | COMMENTS |
|----------|--------------|--------|---------|---------|----------------|--------|---------|----------|
| 11:16    | 1            |        |         |         | 23.99          |        |         |          |
|          |              |        |         |         |                |        |         |          |
|          |              |        |         |         |                |        |         |          |
|          | AVERAGES     | ERR    | ERR     | ERR     | 23.99          | ERR    | ERR     |          |

Barometric Pres:

29.5

## EFFLUENT GAS CONCENTRATION, WET BASIS, PPM

|           | O2  | CO2 | SO2 | THC Outlet | CO  | NOx |
|-----------|-----|-----|-----|------------|-----|-----|
| PRE ZERO  | 0   |     | 0   | 0          | 0   | 0   |
| POST ZERO | 0   |     | 0   | 4          |     | 0   |
| ACT SPAN  | N/A | N/A | N/A | 49.42      | N/A | N/A |
| PRE SPAN  | 0   |     | 0   | 49.3       |     | 0   |
| POST SPAN | 0   |     | 0   | 51         |     | 0   |

|          |     |     |     |       |     |     |
|----------|-----|-----|-----|-------|-----|-----|
| GAS CONC | ERR | ERR | ERR | 22.57 | ERR | ERR |
|----------|-----|-----|-----|-------|-----|-----|

## EFFLUENT GAS CONC CALCULATION

$$\text{GAS CONC.} = (\text{Avg Stk Conc} - \text{Avg Zero Cal}) * (\text{Span Conc} / (\text{Avg Span Cal} - \text{Avg Zero Cal}))$$

### Calculations

|                                 |              |
|---------------------------------|--------------|
| Analyte                         | C3H8         |
| FWhc lbs/lb-mole                | 44           |
| Stack Flowrate, dry scf/hr      | 49,629       |
| Moisture, %                     | 31.0         |
| Cppmv                           | 22.57        |
| Cppmv minus CH4                 | 17.38        |
| <hr/>                           |              |
| Hydrocarbons Emissions (lbs/hr) | <b>0.983</b> |

$$\text{Lbs/Hr} = \text{Cppmv minus CH4} * \text{FWhc} * (\text{Stack Flowrate(dscf/hr)} / 60) * (1.554 * 10^4)$$

# WET BULB / DRY BULB MOISTURE DETERMINATION

Client IBP Logansport  
Date 8/21/96  
Project Number 20974-0000-00000  
Plant Logansport, IN  
Sampling Location vent stack  
Source Hydrolizer  
Run Number 1

Barometric Pressure 29.5  
Static Pressure 0.89

Temperature ( Dry ) 212  
Temperature ( Wet ) 160

S. V. P. ( at Twet ) 4.8  
(Water Saturation Vapor Pressure (PSI))

PST 0.0654  
PS 29.5654

Vapor Pressure 9.1626  
%Moisture 30.9909  
Md 0.6901

# WET BULB / DRY BULB MOISTURE DETERMINATION

Client IBP Logansport  
Date 8/21/96  
Project Number 20974-0000-00000  
Plant Logansport, IN  
Sampling Location vent stack  
Source Hydrolizer  
Run Number 2

Barometric Pressure 29.5  
Static Pressure 0.9

Temperature ( Dry ) 212  
Temperature ( Wet ) 160

S. V. P. ( at Twet ) 4.8  
(Water Saturation Vapor Pressure (PSI))

PST 0.0662  
PS 29.5662

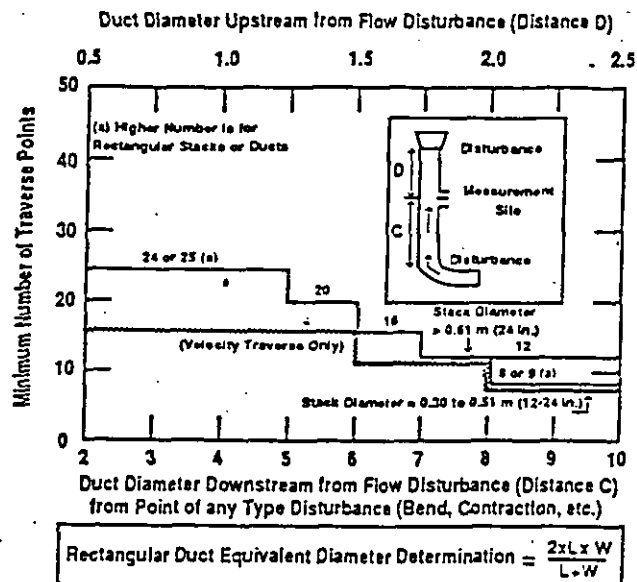
Vapor Pressure 9.1626  
%Moisture 30.9901  
Md 0.6901

# Traverse Point Location for Circular and Rectangular Ducts

Project No.: 20974-0000-00000  
 Client: IBP LOGANSFORD IND  
 Date: 8-20-96  
 Sampling Location: HYDROLIZER  
 Internal Stack Diameter: 8"  
 Nipple Length: 0  
 Total Stack Diameter: 8"  
 Nearest Upstream Disturbance (C): 71" 8575 DD  
 Nearest Downstream Disturbance (D): 100" 125 DD  
 Calculator: SM

GROUND level INSIDE  
 TS=212° STEAM 100% SATURATION  
 \* PT1 = .5  
 PT6 = 7.5

| Traverse Point Number | Fraction of Stack ID<br>( $\frac{1}{100}$ ) | Stack ID | Traverse Point<br>(1 + 2 = Point) | Nipple Length | Traverse Point<br>Inside of Far Wall to Outside<br>of Port Nipple<br>(3 + 4 = Point) |
|-----------------------|---------------------------------------------|----------|-----------------------------------|---------------|--------------------------------------------------------------------------------------|
| 1                     | .044                                        | 8"       | .352                              | 0             | N/A                                                                                  |
| 2                     | .146                                        |          | 1.17                              |               |                                                                                      |
| 3                     | .296                                        |          | 2.37                              |               |                                                                                      |
| 4                     | .704                                        |          | 5.63                              |               |                                                                                      |
| 5                     | .854                                        |          | 6.83                              |               |                                                                                      |
| 6                     | .956                                        |          | 7.65                              |               |                                                                                      |
| 7                     |                                             |          |                                   |               |                                                                                      |
| 8                     |                                             |          |                                   |               |                                                                                      |
| 9                     |                                             |          |                                   |               |                                                                                      |
| 10                    |                                             |          |                                   |               |                                                                                      |
| 11                    |                                             |          |                                   |               |                                                                                      |
| 12                    |                                             |          |                                   |               |                                                                                      |
| 13                    |                                             |          |                                   |               |                                                                                      |
| 14                    |                                             |          |                                   |               |                                                                                      |
| 15                    |                                             |          |                                   |               |                                                                                      |
| 16                    |                                             |          |                                   |               |                                                                                      |
| 17                    |                                             |          |                                   |               |                                                                                      |
| 18                    |                                             |          |                                   |               |                                                                                      |
| 19                    |                                             |          |                                   |               |                                                                                      |
| 20                    |                                             |          |                                   |               |                                                                                      |
| 21                    |                                             |          |                                   |               |                                                                                      |
| 22                    |                                             |          |                                   |               |                                                                                      |
| 23                    |                                             |          |                                   |               |                                                                                      |
| 24                    |                                             |          |                                   |               |                                                                                      |



Location of Traverse Points in Circular Stacks

|    | 4    | 6    | 8    | 10   | 12   | 14   | 16   | 18   | 20   | 22   | 24  |
|----|------|------|------|------|------|------|------|------|------|------|-----|
| 1  | 5.7  | 4.4  | 3.2  | 2.6  | 2.1  | 1.3  | 1.5  | 1.4  | 1.3  | 1.1  | 1.1 |
| 2  | 25.0 | 14.6 | 10.5 | 8.2  | 6.7  | 5.7  | 4.9  | 4.4  | 3.9  | 3.5  | 3.2 |
| 3  | 75.0 | 29.6 | 19.4 | 14.6 | 11.8 | 9.9  | 8.5  | 7.5  | 6.7  | 6.0  | 5.5 |
| 4  | 93.3 | 70.4 | 32.3 | 22.6 | 17.7 | 14.6 | 12.5 | 10.9 | 9.7  | 8.7  | 7.9 |
| 5  | 85.4 | 67.7 | 34.2 | 25.0 | 20.1 | 16.9 | 14.6 | 12.9 | 11.6 | 10.5 |     |
| 6  | 95.6 | 80.6 | 65.8 | 35.6 | 26.9 | 22.0 | 18.8 | 16.5 | 14.6 | 13.2 |     |
| 7  |      | 89.5 | 77.4 | 64.4 | 36.6 | 28.3 | 23.6 | 20.4 | 18.0 | 16.1 |     |
| 8  |      | 96.8 | 85.4 | 75.0 | 63.4 | 37.5 | 29.6 | 25.0 | 21.8 | 19.4 |     |
| 9  |      |      | 91.8 | 82.3 | 73.1 | 62.5 | 38.2 | 30.6 | 26.2 | 23.0 |     |
| 10 |      |      | 97.4 | 88.2 | 79.9 | 71.7 | 61.8 | 38.8 | 31.5 | 27.2 |     |
| 11 |      |      |      | 93.3 | 85.4 | 78.0 | 70.4 | 61.2 | 39.3 | 32.3 |     |
| 12 |      |      |      | 97.9 | 90.1 | 83.1 | 76.4 | 69.4 | 60.7 | 39.8 |     |
| 13 |      |      |      |      | 94.3 | 87.5 | 81.2 | 75.0 | 68.5 | 60.2 |     |
| 14 |      |      |      |      | 98.2 | 91.5 | 85.4 | 79.6 | 73.8 | 67.7 |     |
| 15 |      |      |      |      |      | 95.1 | 89.1 | 83.5 | 78.2 | 72.8 |     |
| 16 |      |      |      |      |      | 98.4 | 92.5 | 87.1 | 82.0 | 77.0 |     |
| 17 |      |      |      |      |      |      | 95.6 | 90.3 | 85.4 | 80.6 |     |
| 18 |      |      |      |      |      |      | 98.6 | 93.3 | 88.4 | 83.9 |     |
| 19 |      |      |      |      |      |      |      | 96.1 | 91.3 | 86.8 |     |
| 20 |      |      |      |      |      |      |      | 98.7 | 94.0 | 89.5 |     |
| 21 |      |      |      |      |      |      |      |      | 96.5 | 92.1 |     |
| 22 |      |      |      |      |      |      |      |      | 98.9 | 94.5 |     |
| 23 |      |      |      |      |      |      |      |      |      | 96.8 |     |
| 24 |      |      |      |      |      |      |      |      |      | 98.9 |     |

Location of Traverse Points in Rectangular Stacks

|    | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    | 10   | 11   | 12   |
|----|------|------|------|------|------|------|------|------|------|------|------|
| 1  | 25.0 | 16.7 | 12.5 | 10.0 | 8.3  | 7.1  | 6.3  | 5.6  | 5.0  | 4.5  | 4.2  |
| 2  | 75.0 | 50.0 | 37.5 | 30.0 | 25.0 | 21.4 | 18.8 | 15.7 | 15.0 | 13.6 | 12.5 |
| 3  |      | 83.3 | 62.5 | 50.0 | 41.7 | 35.7 | 31.3 | 27.8 | 25.0 | 22.7 | 20.8 |
| 4  |      |      | 87.5 | 70.0 | 58.3 | 50.0 | 43.8 | 38.9 | 35.0 | 31.8 | 29.2 |
| 5  |      |      |      | 90.0 | 75.0 | 64.3 | 56.3 | 50.0 | 45.0 | 40.9 | 37.5 |
| 6  |      |      |      |      | 91.7 | 78.6 | 68.8 | 61.1 | 55.0 | 50.0 | 45.8 |
| 7  |      |      |      |      |      | 92.9 | 81.3 | 72.2 | 65.0 | 59.1 | 54.2 |
| 8  |      |      |      |      |      |      | 93.8 | 83.3 | 75.0 | 68.2 | 62.5 |
| 9  |      |      |      |      |      |      |      | 94.4 | 85.0 | 77.3 | 70.8 |
| 10 |      |      |      |      |      |      |      |      | 95.0 | 85.4 | 79.2 |
| 11 |      |      |      |      |      |      |      |      |      | 95.5 | 87.5 |
| 12 |      |      |      |      |      |      |      |      |      |      | 95.8 |

## VELOCITY TRAVERSE

|                                                                                  |                                                                         |
|----------------------------------------------------------------------------------|-------------------------------------------------------------------------|
| Plant: <u>IBP LOGANSPORT</u>                                                     | Date: <u>8-21-96</u>                                                    |
| Unit Number: <u>HYDROLYZER</u>                                                   | Stack Diameter (in.): <u>8"</u>                                         |
| Load Condition: <u>Normal / Peak</u>                                             | Stack Gauge Pressure ("H <sub>2</sub> O): <u>8" <del>mm</del> + .89</u> |
| Run No.: <u>1</u>                                                                | Operators: <u>SM/DW</u>                                                 |
| Project No.: <u>20974</u>                                                        |                                                                         |
| Barometric Pressure at Ground Level ("Hg): <u>29.50</u>                          |                                                                         |
| Pitot Tube ID:                                                                   |                                                                         |
| Pitot Tube Coefficient: <u>.84</u>                                               | Port: Change Pitot<br>Leak Check                                        |
| Estimated Stack CO <sub>2</sub> %: <u>   </u> 0 %: <u>   </u> 11.0 %: <u>   </u> | <u>Pass</u> <u>Fail</u>                                                 |
| Platform Elevation (feet): <u>15'</u>                                            | Port #1 <u>   </u> <u>   </u>                                           |
| Schematic of Stack Cross Section:                                                | Port #2 <u>   </u> <u>   </u>                                           |
|                                                                                  | Port #3 <u>   </u> <u>   </u>                                           |
|                                                                                  | Port #4 <u>   </u> <u>   </u>                                           |
|                                                                                  | $\sqrt{X_{avg}} = 1.0992$                                               |
|                                                                                  | CO <sub>2</sub> -                                                       |
|                                                                                  | O <sub>2</sub> -                                                        |

| Traverse<br>Point<br>Number | Velocity<br>Head<br>(In H <sub>2</sub> O) | Stack<br>Temp.<br>(F) |
|-----------------------------|-------------------------------------------|-----------------------|
| 1A                          | .89                                       |                       |
| 2                           | 1.1                                       |                       |
| 3                           | 1.2                                       |                       |
| 4                           | 1.2                                       |                       |
| 5                           | 1.3                                       |                       |
| 6                           | 1.1                                       |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
| Average:                    |                                           |                       |

| Traverse<br>Point<br>Number | Velocity<br>Head<br>(In H <sub>2</sub> O) | Stack<br>Temp.<br>(F) |
|-----------------------------|-------------------------------------------|-----------------------|
| 1B                          | 1.3                                       |                       |
| 2                           | 1.3                                       |                       |
| 3                           | 1.25                                      |                       |
| 4                           | 1.3                                       |                       |
| 5                           | 1.3                                       |                       |
| 6                           | 1.3                                       |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
|                             |                                           |                       |
| Average:                    |                                           |                       |

VELOCITY TRAVERSE

|                                                                       |                                                                                                         |
|-----------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------|
| Plant: <u>IBP LOGANSPOET</u>                                          | Date: <u>8-21-96</u>                                                                                    |
| Unit Number: <u>HYDROLYZER</u>                                        | Stack Diameter (in.): <u>8"</u>                                                                         |
| Load Condition: <u>Normal/Peak</u>                                    | Stack Gauge Pressure (in. H <sub>2</sub> O): <u>+ .90</u>                                               |
| Run No.: <u>2</u>                                                     | Operators: _____                                                                                        |
| Project No.: <u>20974</u>                                             | _____                                                                                                   |
| Barometric Pressure at Ground Level (in. Hg): <u>29.50</u>            | _____                                                                                                   |
| Pitot Tube ID: _____                                                  | _____                                                                                                   |
| Pitot Tube Coefficient: <u>.84</u>                                    | Port Change Pitot Leak Check <u>Pass</u> <u>Fail</u>                                                    |
| Estimated Stack CO <sub>2</sub> %: <u>0</u> %: <u>0</u> %: <u>0</u> % | Port #1 <u>—</u> <u>—</u>                                                                               |
| Platform Elevation (feet): <u>15'</u>                                 | Port #2 <u>—</u> <u>—</u>                                                                               |
| Schematic of Stack Cross Section:<br><br><u>See Run #1</u>            | Port #3 <u>—</u> <u>—</u>                                                                               |
|                                                                       | Port #4 <u>—</u> <u>—</u>                                                                               |
| Wet Bulb = <u>160°F</u><br>Dry Bulb = <u>212</u>                      | <u><math>\sqrt{\Delta P_{avg}} = 1.1221</math></u><br><u>CO<sub>2</sub> -</u><br><u>O<sub>2</sub> -</u> |

| Traverse Point Number | Velocity Head (in H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1A                    | 1.05                                |                 |
| 2                     | 1.1                                 |                 |
| 3                     | 1.15                                |                 |
| 4                     | 1.3                                 |                 |
| 5                     | 1.3                                 |                 |
| 6                     | 1.1                                 |                 |
| 7                     |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              |                                     |                 |

| Traverse Point Number | Velocity Head (in H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1B                    | 1.35                                |                 |
| 2                     | 1.4                                 |                 |
| 3                     | 1.35                                |                 |
| 4                     | 1.4                                 |                 |
| 5                     | 1.45                                |                 |
| 6                     | 1.2                                 |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              |                                     |                 |

# Orsat Analysis

Project No. 20974-0  
 Plant IBP  
 Facility LOGANSFORD, IN  
 Source HYDROLIZER  
 Sample Location EXHAUST STACK  
 GC Checkoff - Pretest \_\_\_\_\_

Date 8/21/96  
 Run 1-  
 Operator DW, SM  
 Comments: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

Orsat Leak Checked (Yes) No

Expiration Date of Reagents \_\_\_\_\_

Purge System with Sample Gas YES

Ambient Air Check CO<sub>2</sub> 0.0 O<sub>2</sub> 20.9

Audit Gas Check (measured/actual): CO<sub>2</sub> 1 O<sub>2</sub> 1 CO 1

| Sample Point | Time         | CO <sub>2</sub> Reading 1 | (CO <sub>2</sub> ) Reading 2 |     | (CO) Reading 3 |     | F <sub>C</sub> |
|--------------|--------------|---------------------------|------------------------------|-----|----------------|-----|----------------|
|              |              |                           | Actual                       | Net | Actual         | Net |                |
| <u>R1</u>    | <u>10:00</u> |                           |                              |     |                |     |                |
|              |              |                           |                              |     |                |     |                |
|              |              |                           |                              |     |                |     |                |
|              |              |                           |                              |     |                |     |                |
|              |              |                           |                              |     |                |     |                |

Net CO<sub>2</sub> reading = Reading 2 - Reading 1 (Actual)

Net CO reading = Reading 3 - Reading 2 (Actual)

## GC Validation

Calculate F<sub>C</sub>

$$F_C = \frac{20.9 - \%O_2}{\%CO_2}$$

Fuel \_\_\_\_\_

Reported F<sub>C</sub> \_\_\_\_\_

## Expected F<sub>C</sub> Ranges

|                    |               |
|--------------------|---------------|
| Anthracite/Lignite | 1.015 - 1.100 |
| Bituminous         | 1.083 - 1.200 |
| Distillate Oil     | 1.250 - 1.413 |
| Residual Oil       | 1.210 - 1.370 |
| Natural Gas        | 1.500 - 1.535 |
| Wood Bark          | 1.000 - 1.100 |
| Municipal Garbage  | 1.045 - 1.177 |

Other \_\_\_\_\_

**TRC**

01 - .67060  
 02 - .5901-  
 03 99.68+ .0000-  
 04 .00000 .00000  
 05 .00000 .00  
 01 -.82280 -.80200  
 02 16.30 / 1.418  
 03 -.0024 -.0044  
 04 .00000 .00000  
 05 .00000 .00000  
 06 -.00210 -.00210  
 07 -.00140 -.00310

Wed - 08/21/96 DAY= 234 08:18:02 - START RUN# 1 Hydrolizer  
 8-21-96

01 -.93540 -.92250  
 02 17.14 / 16.30  
 03 .0024 -.0024  
 04 .00000 .00000  
 05 .00000 .00000  
 06 -.00240 -.00210  
 07 -.00170 -.00140

Wed - 08/21/96 DAY= 234 08:19:02

01 -.93540  
 02 17.14 / 16.30  
 03 -.0014 .0004  
 04 .00000 .00000  
 05 .00000 .00000  
 06 -.00170 -.00240  
 07 -.00110 -.00170

Wed - 08/21/96 DAY= 234 08:20:02

01 -.74460 -.91350  
 02 15.12 / 15.50  
 03 .0004 -.0014  
 04 .00000 .00000  
 05 .00000 .00000  
 06 .00040 -.00170  
 07 -.00240 -.00110

Wed - 08/21/96 DAY= 234 08:21:02

01 -.97790 -.74460  
 02 14.88 / 15.12  
 03 -.0014 .0004  
 04 .00000 .00000  
 05 .00000 .00000  
 06 .00110 .00040  
 07 .00240

Wed - 08/21/96 DAY= 234 08:22:02

01 -.74460 -.97790  
 02 13.93 / 14.88  
 03 -.0000 -.0014

Pg avg = 15.48

05 -.00000 -.00000  
06 -.00070 -.00110  
07 -.00140 -.00340

Wed - 08/21/96 DAY= 234 08:23:02

01 -0.1230 -0.74460  
02 15.17 ✓ 15.93  
03 -.0004 -.0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00070  
07 -.00210 -.00140

Wed - 08/21/96 DAY= 234 08:24:02

01 -.37990 -.31230  
02 18.49 ✓ 18.17  
03 -.0008 -.0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00220 -.00070  
07 -.00440 -.00240

01 -.00000 -.00000  
02 -.00000 -.00000  
03 -.00000 -.00000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00240 -.00070  
07 -.00140 -.00040

Wed - 08/21/96 DAY= 234 08:27:06

01 -0.0000 -0.77540  
02 19.99 ✓ 19.64  
03 -.0017 -.0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00210 -.00240  
07 -.00340 -.00140

Wed - 08/21/96 DAY= 234 08:28:02

01 -.31230 -.30000  
02 34.01 ✓ 17.99  
03 -.0004 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00210  
07 -.00110 -.00340

Wed - 08/21/96 DAY= 234 08:29:02

01 -.77340 -.31230  
02 23.77 ✓ 34.01  
03 .0004 -.0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00040  
07 -.00140 -.00110

Wed - 08/21/96 DAY= 234 08:30:02

01 -.30000 -.77340  
02 19.52 ✓ 23.77  
03 -.0007 .0004

P3 Avg = 21.23

05 -.00000 -.00000  
06 -.00210 -.00070  
07 -.00240 -.00140

Wed - 08/21/96 DAY= 234 08:31:02

01 -.00340 -.00000  
02 .0006 ✓ 17.52  
03 -.0014 -.0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00240 -.00210  
07 -.00210 -.00240

Wed - 08/21/96 DAY= 234 08:32:02

01 -.00000 -.77040  
02 16.60 ✓ 17.36  
03 -.0011 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00240  
07 -.00170 -.00210

Wed - 08/21/96 DAY= 234 08:33:02

01 -.07990 -.00000  
02 15.28 ✓ 16.63  
03 -.0014 -.0011  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00170  
07 .00000 -.00170

Wed - 08/21/96 DAY= 234 08:34:02

01 -.04610 -.07990  
02 13.71 ✓ 15.29  
03 -.0020 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00140  
07 -.00170 -.00200

Wed - 08/21/96 DAY= 234 08:35:02

01 -.00200 -.04610  
02 13.61 ✓ 13.71  
03 -.0017 -.0020  
04 .00000 .00000  
05 .00000 .00000  
06 -.00240 -.00110  
07 -.00270 -.00170

Wed - 08/21/96 DAY= 234 08:36:03

01 -.04610 -.00200  
02 .0001 ✓ 13.61  
03 .0001 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00240  
07 -.00110 -.00270

Wed - 08/21/96 DAY= 234 08:37:02

Pg Avg = 15.33

01 -.34610 -.34610  
02 15.02 ✓ 15.41  
03 -.0017 -.0021  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00140  
07 .00110 -.00110

Wed - 08/21/96 DAY= 234 08:38:02

01 -.77340 -.84610  
02 16.07 ✓ 16.02  
03 -.0017 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00110  
07 .00040 -.00210

Wed - 08/21/96 DAY= 234 08:39:02

01 -.84610 -.77340  
02 16.03 ✓ 16.07  
03 -.0007 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00240 -.00070  
07 -.00170 .00040

Wed - 08/21/96 DAY= 234 08:40:02

01 -.81230 -.84610  
02 16.06 ✓ 16.03  
03 .0007 -.0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00240  
07 -.00240 -.00170

Wed - 08/21/96 DAY= 234 08:41:02

01 -.74460 -.81230  
02 16.07 ✓ 16.06  
03 -.0004 -.0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00070  
07 -.00210 -.00240

Wed - 08/21/96 DAY= 234 08:42:02

01 -.83540 -.74460  
02 16.16 ✓ 16.07  
03 -.0014 -.0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00220 -.00040  
07 -.00240 -.00210

Wed - 08/21/96 DAY= 234 08:43:03

01 -.81230 -.83540  
02 16.32 ✓ 16.16  
03 -.0011 -.0014  
04 .00000 .00000  
05 .00000 .00000

Pg Avg = 16.10

26 -.00240 -.00000  
27 -.00250 .00240

Wed - 08/21/96 DAY= 234 08:44:03

01 -.77940 -.81230  
02 15.75 ✓ 16.32  
03 .00000 -.0011  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00040  
07 -.00140 -.00250

Wed - 08/21/96 DAY= 234 08:45:02

01 -.84610 -.77940  
02 16.28 ✓ 16.75  
03 -.0024 -.0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00210 -.00140  
07 -.00240 -.00140

Wed - 08/21/96 DAY= 234 08:46:02

01 -.97990 -.84610  
02 14.86 ✓ 16.28  
03 -.0014 -.0024  
04 .00000 .00000  
05 .00000 .00000  
06 -.00210 -.00210  
07 -.00230 -.00240

Wed - 08/21/96 DAY= 234 08:47:02

01 -.97990 -.97990  
02 13.67 ✓ 14.86  
03 -.0031 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00210  
07 -.00210 -.00230

Wed - 08/21/96 DAY= 234 08:48:02

01 -.75860 -.97990  
02 13.28 ✓ 13.67  
03 -.0007 -.0031  
04 .00000 .00000  
05 .00000 .00000  
06 -.00210 -.00140  
07 -.00000 -.00210

Wed - 08/21/96 DAY= 234 08:49:03

01 -.71380 -.75860  
02 13.42 ✓ 13.28  
03 -.0011 -.0007  
04 .00000 .00000  
05 .00000 .00000  
06 .00140 -.00210  
07 -.00140 -.00000

Wed - 08/21/96 DAY= 234 08:50:02

01 -.81230 -.71380

Pg Avg = 14.70

02 14.34 13.42  
03 -.0021 -.0011  
04 .00000 .00000  
05 .00000 .00000  
06 -.00280 .00140  
07 -.00140 -.00140

Wed - 08/21/96 DAY= 234 08:51:22

01 -.78600 -.81270  
02 49.56+ 14.34  
03 -.0008 -.0021  
04 .00000 .00000  
05 .00000 .00000  
06 -.00160 -.00280  
07 -.00240 -.00140

Wed - 09/21/96 DAY= 234 08:52:02

01 -.82280 -.78800  
02 41.67 49.56+  
03 .0004 -.0008  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00160  
07 -.00210 -.00240

Wed - 06/21/96 DAY= 234 08:53:02

01 -.84610 -.92280  
02 22.35 41.67  
03 -.0004 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00140  
07 -.00010 -.00210

Wed - 08/21/96 DAY= 234 08:54:03

01 -.84610 -.84610  
02 19.73 22.35  
03 -.0011 -.0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00140  
07 -.00410 -.00040

Wed - 08/21/96 DAY= 234 08:55:03

01 -.84610 -.84610  
02 19.75 19.73  
03 -.0014 -.0011  
04 .00000 .00000  
05 .00000 .00000  
06 -.00210 -.00110  
07 -.00340 -.00410

Wed - 03/21/96 DAY= 234 08:56:02

01 -.84610 -.84610  
02 19.42 19.75  
03 -.0024 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00210  
07 -.00170 -.00140

Pg Avg = 26.69.

Wed - 03/21/96 DAY= 234 08:57:02

01 -.81230 -.84610  
02 18.03✓ 19.42  
03 -.0004 -.0024  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00140  
07 -.00110 -.00170

Wed - 03/21/96 DAY= 234 08:58:02

01 -.80000 -.81230  
02 16.59✓ 18.03  
03 -.0014 -.0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00040  
07 -.00210 -.00110

Wed - 03/21/96 DAY= 234 08:59:02

01 -.84510 -.80000  
02 16.59✓ 16.59  
03 -.0017 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00170  
07 -.00240 -.00210

Wed - 03/21/96 DAY= 234 09:00:02

01 .00000 -.84510  
02 16.16✓ 16.59  
03 -.0017 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00200 -.00040  
07 -.00200 -.00240

Wed - 03/21/96 DAY= 234 09:01:02

01 -.84510 -.80000  
02 16.91✓ 16.16  
03 -.0030 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00200  
07 -.00310 -.00200

Wed - 03/21/96 DAY= 234 09:02:02

01 -.74450 -.84510  
02 17.02✓ 16.91  
03 -.0000 -.0030  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00170  
07 -.00110 -.00310

Wed - 03/21/96 DAY= 234 09:03:02

01 -.80000 -.74450  
02 16.39✓ 17.02  
03 .00000 .00000

Pz ang = 16.66

01 -.84410 -.81270  
02 15.39 ✓ 15.58  
03 -.0014 -.0024  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00070  
07 .00070 -.00070

Wed - 05/21/96 DAY= 234 09:11:02

01 -.84610 -.84610  
02 15.39 ✓ 15.39  
03 -.0017 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00070  
07 -.00310 -.00170

Wed - 05/21/96 DAY= 234 09:12:02

01 -.74460 -.84610  
02 15.59 ✓ 15.39  
03 -.0011 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00110  
07 -.00240 -.00310

Wed - 05/21/96 DAY= 234 09:13:02

01 -.77360 -.74460  
02 15.59 ✓ 15.59  
03 -.0004 -.0011  
04 .00000 .00000  
05 .00000 .00000  
06 -.00310 -.00070  
07 -.00310 -.00240

Wed - 05/21/96 DAY= 234 09:14:02

01 -.76960 -.77360  
02 4.913 ✓ 15.93  
03 -.0031 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00310  
07 -.00110 -.00310

Wed - 05/21/96 DAY= 234 09:15:02

01 -.77340 -.76960  
02 2.314 ✓ 4.913  
03 -.0041 -.0031  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00110  
07 .00110 -.00110

Wed - 05/21/96 DAY= 234 09:16:02

01 -.66380 -.77340  
02 2.786 ✓ 2.314  
03 -.0041 -.0041  
04 .00000 .00000

Pg Avg= 10.30

04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00140  
07 -.00010 -.00110

Wed - 08/21/96 DAY= 234 09:04:02

01 .00000 .00000  
02 15.99 ✓ 15.39  
03 -.0021 -.0031  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00240  
07 -.00140 -.00210

Wed - 08/21/96 DAY= 234 09:05:02

01 -.67690 -.91300  
02 15.89 ✓ 15.99  
03 -.0000 -.0021  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00070  
07 -.00070 -.00140

Wed - 08/21/96 DAY= 234 09:06:02

01 -.84610 -.67690  
02 15.80 ✓ 15.99  
03 -.0031 -.0000  
04 .00000 .00000  
05 .00000 .00000  
06 .00040 -.00140  
07 -.00010 -.00070

Wed - 08/21/96 DAY= 234 09:07:02

01 -.84610 -.84610  
02 15.67 ✓ 15.80  
03 -.0024 -.0031  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00340  
07 -.00000 -.00010

Wed - 08/21/96 DAY= 234 09:08:02

01 -.84600 -.84610  
02 15.55 ✓ 15.67  
03 -.0027 -.0024  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00070  
07 -.00010 -.00020

Wed - 08/21/96 DAY= 234 09:09:02

01 .00000 .00000  
02 15.55 ✓ 15.55  
03 -.0024 -.0027  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00070  
07 -.00070 -.00010

pg Avg = 15.73

01 - .76660 - .80000  
02 - .33370 - .30210  
03 - .20270 - .20210

Wed - 08/21/96 DAY= 234 09:17:02

01 - .30000 - .94920  
02 - .63 - 2.706  
03 - .44 - .3041  
04 - .20000 - .00000  
05 - .30000 - .30000  
06 - .20110 - .00370  
07 - .20210 - .00270

Wed - 08/21/96 DAY= 234 09:18:02

01 - .76660 - .80000  
02 - 2.907 - 2.753  
03 - .0044 - .0044  
04 - .30000 - .00000  
05 - .00200 - .00020  
06 - .00110 - .00110  
07 - .00140 - .00210

Wed - 08/21/96 DAY= 234 09:19:02

— End Run #1 Hydrolyzer

01 - .80000 - .76660  
02 - 13.44 - 2.907  
03 - .3034 - .2044  
04 - .00000 - .00000  
05 - .00020 - .00000  
06 - .00340 - .00110  
07 - .00510 - .00140

Pg Avg = 2.835

Wed - 08/21/96 DAY= 234 09:20:02

01 - .71000 - .30000  
02 - 12.42 - 13.44  
03 - .2024 - .0004  
04 - .20000 - .00000  
05 - .00000 - .00000  
06 - .20000 - .00340  
07 - .00310 - .00510

Wed - 08/21/96 DAY= 234 09:21:02

01 - .73520 - .71000  
02 - 3.097 - 12.42  
03 - .2031 - .0024  
04 - .00000 - .00000  
05 - .20000 - .00000  
06 - .00270 - .00000  
07 - .00170 - .00310

Wed - 08/21/96 DAY= 234 09:22:02

01 -.93550 - .73520  
 02 2.306 3.097  
 03 -.0061 - .0031  
 04 .00000 .00000  
 05 .00000 .00  
 01 -.90230 - .84610  
 02 1.566 ✓ 1.314  
 03 -.0044 - .0058  
 04 .00000 .00000  
 05 .00000 .00000  
 06 -.00240 - .00170  
 07 -.00240 - .00240

Wed - 08/21/96 DAY= 234 09:36:02 - Start Run #2 Hydrolyze

01 -.81230 - .90230  
 02 2.264 ✓ 1.566  
 03 -.0041 - .0044  
 04 .00000 .00000  
 05 .00000 .00000  
 06 -.00040 - .00240  
 07 -.00110 - .00240

\* only a 40 min Run -  
 unit having problems  
 causing PSI problems on  
 analyzer. (Snd)

Wed - 08/21/96 DAY= 234 09:37:02

01 -.85890 - .91230  
 02 2.426 ✓ 2.264  
 03 -.0014 - .0041  
 04 .00000 .00000  
 05 .00000 .00000  
 06 -.00140 - .00240  
 07 -.00140 - .00110

Wed - 08/21/96 DAY= 234 09:38:02

01 -.85040 - .86990  
 02 14.83+ ✓ 2.426  
 03 -.0029 - .0014  
 04 .00000 .00000  
 05 .00200 .00000  
 06 -.00140 - .00140  
 07 -.00070 - .00140

Wed - 08/21/96 DAY= 234 09:39:02

01 -.81530 - .86940  
 02 55.60+ ✓ 14.83+  
 03 -.0000 - .0029  
 04 .00000 .00000  
 05 .00000 .00000  
 06 -.00040 - .00110  
 07 -.00040 - .00070

Wed - 08/21/96 DAY= 234 09:40:02

01 -.75430 - .81530  
 02 77.77 55.60+

PJ avg 15.34

23 .0004 -.0000  
24 .0000 .0000  
25 .0000 .0000  
26 -.0007 -.0000  
27 .0004 -.0000

Wed - 08/21/96 DAY= 234 09:41:02

21 -.50960 -.73430  
22 59.60+ 37.73 ✓  
23 .0004 .0004  
24 .0000 .0000  
25 .0000 .0000  
26 -.00110 -.00070  
27 -.00110 .00040

Wed - 08/21/96 DAY= 234 09:42:02

21 -.00000 -.00000  
22 40.72 ✓ 59.60+  
23 .0000 .0004  
24 .0000 .0000  
25 .0000 .0000  
26 -.00170 -.00110  
27 -.00070 -.00110

Wed - 08/21/96 DAY= 234 09:43:02

21 -.02290 -.00000  
22 59.61 ✓ 40.72  
23 .0004 .0000  
24 .0000 .0000  
25 .0000 .0000  
26 -.00040 -.00170  
27 -.00000 -.00070

Wed - 08/21/96 DAY= 234 09:44:02

21 -.09190 -.02290  
22 37.18 ✓ 59.61  
23 .0004 .0004  
24 .0000 .0000  
25 .0000 .0000  
26 -.00040 -.00040  
27 -.00000 -.00000

Wed - 08/21/96 DAY= 234 09:45:02

21 -.05710 -.09190  
22 29.18 ✓ 37.18+  
23 -.0007 .0004  
24 .0000 .0000  
25 .0000 .0000  
26 -.00070 -.00040  
27 -.00000 -.00000

Wed - 08/21/96 DAY= 234 09:46:02

21 .0000 -.05710  
22 29.57 ✓ 29.18+  
23 -.0021 -.0007  
24 .0000 .0000  
25 .0000 .0000  
26 -.00000 -.00070  
27 -.00040 -.00000

Pg Avg = 48.85

Wed - 08/21/96 DAY= 234 09:47:02

01 -.7886D -.8462D  
02 54.75 ✓ 29.67  
03 .0011 -.0021  
04 .0000D .0000D  
05 .0000D .0000D  
06 .0000D -.0028D  
07 .0004D -.0041D

Wed - 08/21/96 DAY= 234 09:48:02

01 -.8624D -.7886D  
02 72.47 ✓ 54.75  
03 .0024 .0011  
04 .0000D .0000D  
05 .0000D .0000D  
06 .0000D .0007D  
07 .0004D .0004D

Wed - 08/21/96 DAY= 234 09:49:02

01 -.8914D -.8624D  
02 49.93 ✓ 72.47  
03 -.0011 .0004  
04 .0000D .0000D  
05 .0000D .0000D  
06 -.0011D .0000D  
07 -.0014D .0004D

Wed - 08/21/96 DAY= 234 09:50:02

01 .0000D -.8914D  
02 49.93 ✓ 49.93  
03 -.0021 -.0011  
04 .0000D .0000D  
05 .0000D .0000D  
06 -.0027D -.0011D  
07 -.0021D -.0014D

Wed - 08/21/96 DAY= 234 09:51:03

01 -.8461D -.8624D  
02 13.32 ✓ 12.93  
03 -.0011 -.0021  
04 .0000D .0000D  
05 .0000D .0000D  
06 -.0017D -.0027D  
07 -.0014D -.0021D

Wed - 08/21/96 DAY= 234 09:52:02

01 -.8461D -.8461D  
02 8.524 ✓ 13.82  
03 -.0004 -.0011  
04 .0000D .0000D  
05 .0000D .0000D  
06 .0000D -.0017D  
07 .0017D -.0014D

Wed - 08/21/96 DAY= 234 09:53:02

01 -.8600D ✓ -.8461D  
02 48.11 ✓ 8.524  
03 -.0008 -.0004

Pg Avg = 37.22

35 .00001 .00000  
36 -.00000 -.00070  
37 -.00100 -.00170

Wed - 08/21/96 DAY= 234 09:54:02

01 .00000 .00000  
02 .00000 48.11+  
03 .00000 -.00000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00100 -.00000  
07 -.00000 -.00100

Wed - 08/21/96 DAY= 234 09:55:02

01 -.94000 -.95710  
02 36.46+ 39.99  
03 -.00000 .00000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00100 -.00100  
07 -.00100 -.00070

Wed - 08/21/96 DAY= 234 09:56:02

01 -.95710 -.94000  
02 46.44+ 36.46+  
03 .00000 -.00000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00100 -.00100  
07 .00000 -.00100

Wed - 08/21/96 DAY= 234 09:57:02

01 -.95520 -.95710  
02 25.76+ 46.44+  
03 .00000 .00000  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00100  
07 -.00000 -.00100

Wed - 08/21/96 DAY= 234 09:58:02

01 -.95520 -.95520  
02 31.93+ 25.76+  
03 -.00000 .00000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00000 .00000  
07 -.00100 -.00000

Wed - 08/21/96 DAY= 234 09:59:02

01 -.95510 -.95520  
02 .00000 31.93+  
03 .00000 -.00000  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00000  
07 .00000 -.00100

Wed - 08/21/96 DAY= 234 10:00:02

pg Avg = 44.98

01 -.77440 -.93510  
02 46.32+ 29.42+  
03 .0004 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 .00000  
07 .00000 .00000

Wed - 08/21/96 DAY= 234 10:01:02

01 -.91510 -.77440  
02 35.73+ 46.32+  
03 -.0000 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 .00000  
07 -.00040 -.00040

Wed - 08/21/96 DAY= 234 10:02:02

01 -.52050 -.91510  
02 60.01+ 35.73+  
03 .0004 -.0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00110  
07 .00000 -.00040

Wed - 08/21/96 DAY= 234 10:03:02

01 -.61230 -.92050  
02 60.01+ 60.01+  
03 .0004 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 .00040 -.00040  
07 -.00110 .00000

Wed - 08/21/96 DAY= 234 10:04:02

01 -.69240 -.61230  
02 55.09+ 22.72  
03 .0004 -.0011  
04 .00000 .00000  
05 .00000 .00000  
06 -.00000 .00040  
07 -.00000 -.00110

Wed - 08/21/96 DAY= 234 10:05:02

01 -.84610 -.69240  
02 27.97 55.09+  
03 -.0011 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00000  
07 .00000 -.00000

Wed - 08/21/96 DAY= 234 10:06:02

01 -.66000 -.84610  
02 56.63+ 27.97  
03 -.0004 -.0011  
04 .00000 .00000  
05 .00000 .00000

Pg Avg 43.49

25 -.80040 -.80110  
27 -.80110 -.80210

Wed - 08/21/96 DAY= 234 10:07:03

01 -.84460 -.88000  
02 50.03 ✓ 56.63+  
03 0.0000 -.0004  
04 0.0000 .00000  
05 .00000 .00000  
06 .00240 -.00040  
07 -.00000 -.00110

Wed - 08/21/96 DAY= 234 10:08:02

01 -.80960 -.84460  
02 55.72 ✓ 50.03+  
03 -.0004 -.0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 .00040  
07 -.00110 -.00000

Wed - 08/21/96 DAY= 234 10:09:03

01 -.77950 -.80960  
02 40.87 ✓ 55.72+  
03 .0004 -.0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00000 -.00040  
07 -.00000 -.00110

Wed - 08/21/96 DAY= 234 10:10:02

01 -.77950 -.77950  
02 12.37 ✓ 40.87  
03 -.0000 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00000  
07 -.00000 -.00000

Wed - 08/21/96 DAY= 234 10:11:02

01 -.81130 -.84460  
02 11.47 ✓ 12.37  
03 -.0004 -.0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00040  
07 -.00110 -.00000

Wed - 08/21/96 DAY= 234 10:12:02

01 -.86640 -.81130  
02 51.33 ✓ 11.47  
03 0.0000 -.0004  
04 0.0000 .00000  
05 .00000 .00000  
06 .00000 -.00110  
07 .00000 -.00110

Wed - 08/21/96 DAY= 234 10:13:03

Pg Avg = 41.84

22 42.00 ✓ 51.30-  
23 .0000 .0000  
24 .0000 .0000  
25 .0000 .0000  
26 -.0011 .0000  
27 -.0014 .0000

4 25/21/96 DAY= 234 10:14:00

21 -.0410 -.0414  
22 1.955 ✓ 12.15  
23 -.0004 .0100  
24 .0000 .0000  
25 .0000 .0000  
26 -.0010 -.0010  
27 -.0014 -.0014

Wed - 22/21/96 DAY= 234 10:15:02 - Stop R-2 195

Aug = 21.00

21 -.0400 -.0400  
22 -.0002- 1.955  
23 -.0007 -.0004  
24 .0000 .0000  
25 .0000 .0000  
26 -.0010 -.0010  
27 -.0020 -.0014

Wed - 22/21/96 DAY= 234 10:16:02

21 -.0400 -.0400  
22 -.0409- -.0400-  
23 .0024 -.0027  
24 .0000 .0000  
25 .0000 .0000  
26 -.0020 -.0010  
27 -.0020 -.0020

Wed - 22/21/96 DAY= 234 10:17:02

21 -.0414 -.0400  
22 41.92 -.0409-  
23 -.0024 -.0024  
24 .0000 .0000  
25 .0000 .0000  
26 -.0007 -.0020  
27 -.0014 -.0020

Wed - 25/21/96 DAY= 234 10:18:02

Run 1

DATE:

22-Aug-96

CLIENT REP:

Rechelle Kruse

PLANT:

IBP

WITNESSED?:

yes

DOC TYPE

BURNER TYPE:

N/A

OPERATOR:

SM, DW

GENERATOR TYPE:

N/A

TEST LOCATION:

Melt Tank

O2 GENERATOR TYPE:

N/A

## CALIBRATION GASES

| O2  | CO2 | CO  | SO2 | NOx | THC outlet |
|-----|-----|-----|-----|-----|------------|
| 0   | 0   | 0   | 0   | 0   | 0          |
| N/A | N/A | N/A | N/A |     | 29.68      |
| N/A | N/A | N/A | N/A |     | 49.42      |
|     |     |     |     |     | 83.47      |

| END TIME | SAMPLE POINT | O2 wet | CO2 ppm | SO2 ppm | THC Outlet ppm | CO ppm | NOx ppm | COMMENTS |
|----------|--------------|--------|---------|---------|----------------|--------|---------|----------|
| 10:03    | 1            |        |         |         | 76.49          |        |         |          |
|          |              |        |         |         |                |        |         |          |
|          |              |        |         |         |                |        |         |          |
|          | AVERAGES     | ERR    | ERR     | ERR     | 76.49          | ERR    | ERR     |          |

Barometric Pres:

29.5

## EFFLUENT GAS CONCENTRATION, WET BASIS, PPM

|           | O2  | CO2 | SO2 | THC Outlet | CO  | NOx |
|-----------|-----|-----|-----|------------|-----|-----|
| PRE ZERO  | 0   |     | 0   | 0          | 0   | 0   |
| POST ZERO | 0   |     | 0   | 1          |     | 0   |
| ACT SPAN  | N/A | N/A | N/A | 83.47      | N/A | N/A |
| PRE SPAN  | 0   |     | 0   | 83.5       |     | 0   |
| POST SPAN | 0   |     | 0   | 83         |     | 0   |
| GAS CONC  | ERR | ERR | ERR | 76.65      | ERR | ERR |

### Calculations

|                            |       |      |
|----------------------------|-------|------|
| Analyte                    | C3H8  | C3H8 |
| FWhc lbs/lb-mole           | 44    | 44   |
| Stack Flowrate, dry scf/hr | n/a   | n/a  |
| Moisture, %                | n/a   | n/a  |
| Cppmv                      | 76.65 | 0    |
| Cppmv minus CH4            | 51.45 |      |

01 -.1760P -.7784D  
02 3.893P 1.848  
03 .022P -.0065  
04 .009P -.0004D  
05 .0005P -.00  
01 .0693D .0344D  
02 66.11 64.43  
03 .0101 .0100  
04 .0004D .0007D  
05 .0004D -.0004D  
06 -.0025D -.0007D  
07 -.0042D -.0059D

Thr - 08/22/96 DAY= 235 08:03:02 ~ Start Run#1 Melt Tank 0903

01 -.2059D .0693D  
02 67.34 66.11  
03 .0003 .0101  
04 .0007D .0004D  
05 .0000D .0004D  
06 -.0035D -.0025D  
07 -.0028D -.0042D

Thr - 08/22/96 DAY= 235 08:04:02

01 -.1391D -.2059D  
02 66.74 67.34  
03 .0000 .0003  
04 .0000 .0007D  
05 -.0000D .0000D  
06 .0021D -.0035D  
07 -.0011D -.0028D

Thr - 08/22/96 DAY= 235 08:05:02

01 -.1730D -.1391D  
02 85.09 96.74  
03 .0000 .0000  
04 .0104D .0000D  
05 .0014D -.0000D  
06 .0025D .0021D  
07 .0011D -.0011D

Thr - 08/22/96 DAY= 235 08:06:02

01 -.5352D .1730D  
02 76.61 85.07  
03 .0036 .0000  
04 .0103D .0104D  
05 .0010D .0014D  
06 -.0025D .0025D  
07 -.0033D .0011D

Thr - 08/22/96 DAY= 235 08:07:02

01 -.7295D -.5352D  
02 90.21 76.61  
03 .0025 .0036  
04 .0111D .0103D  
05 .0007D .0015D  
06 -.0032D -.0025D

Page Avg = 78.683

07 - .00320 - .00330

Thr - 08/22/96 DAY= 235 08:08:02

01 - .56320 - .72950  
02 89.14 ✓ 90.21  
03 .0022 .0025  
04 .0110 .01110  
05 .00040 .00070  
06 -.00110 -.00320  
07 -.00110 -.00320

Thr - 08/22/96 DAY= 235 08:09:02

01 - .62530 - .66320  
02 85.71 ✓ 89.14  
03 .0025 .0022  
04 .01210 .01200  
05 .00070 .00040  
06 -.00000 -.00110  
07 -.00100 -.00110

Thr - 08/22/96 DAY= 235 08:10:02

01 - .76420 - .62530  
02 75.69 ✓ 85.71  
03 .0018 .0025  
04 .00490 .01210  
05 -.00000 .00070  
06 -.00070 -.00000  
07 -.00250 -.00180

Thr - 08/22/96 DAY= 235 08:11:02

01 - .52530 - .76420  
02 66.82 ✓ 75.69  
03 .0035 .0018  
04 .00520 .00490  
05 -.00000 -.00000  
06 .00110 -.00070  
07 -.00040 -.00250

Thr - 08/22/96 DAY= 235 08:12:02

01 - .44570 - .62530  
02 82.70 ✓ 66.82  
03 .0045 .0035  
04 .00520 .00320  
05 -.00000 -.00000  
06 .00280 .00110  
07 .00210 -.00040

Thr - 08/22/96 DAY= 235 08:13:03

01 - .66000 - .44570  
02 69.51 ✓ 82.70  
03 .0021 .0045  
04 .00590 .00520  
05 .00070 -.00000  
06 .00110 .00280  
07 -.00100 .00210

Thr - 08/22/96 DAY= 235 08:14:02

01 - .75430 - .66000  
02 67.79 ✓ 69.51

page Avg = 76.766

03 .0014 .0021  
04 .00240 .00590  
05 .00110 .00070  
06 .00070 .00110  
07 -.00180 -.00180

Thr - 08/22/96 DAY= 235 08:15:02

01 .75420 .75430  
02 75.28 / 57.79  
03 .0014 .0014  
04 .00210 .00240  
05 .00070 .00110  
06 -.00200 .00070  
07 -.00040 -.00180

Thr - 08/22/96 DAY= 235 08:16:02

01 -.75850 -.75420  
02 64.25 / 75.28  
03 .0004 .0014  
04 .00140 .00210  
05 -.00310 .00070  
06 -.00070 -.00000  
07 -.00350 -.00040

Thr - 08/22/96 DAY= 235 08:17:02

01 -.69470 .73850  
02 60.71 / 64.25  
03 .0021 .0004  
04 .00520 .00140  
05 .75420 -.00310  
06 .00240 -.00070  
07 .00040 -.00350

Thr - 08/22/96 DAY= 235 08:18:02

01 -.58570 .67470  
02 59.66 / 60.71  
03 .0011 .0021  
04 .00110 .00520  
05 -.00250 .00420  
06 -.00210 -.00040  
07 -.00110 .00040

Thr - 08/22/96 DAY= 235 08:19:02

01 -.58290 -.68570  
02 61.73 / 59.66  
03 .0031 .0011  
04 .00450 .00110  
05 -.00080 -.00250  
06 -.00180 -.00210  
07 -.00250 -.11 13

Thr - 08/22/96 DAY= 235 08:20:03

01 .53290  
02 57.47 / 61.73  
03 .0013 .0031  
04 .00380 .00450  
05 -.00110 -.00080  
06 -.00210 -.00080  
07 -.00280 -.00250

Page Avg = 63.267

Thr - 08/22/96 DAY= 235 08:21:02

01 -.58290 -.59470  
02 53.38 ✓ 57.97  
03 .0031 .0018  
04 .00280 .00380  
05 -.00040 -.00110  
06 .0010 -.00210  
07 -.00350 -.00280

Thr - 08/22/96 DAY= 235 08:22:02

01 -.51430 -1  
02 ✓ 53.38  
03 .00000 .00000  
04 -.00040 -.00110  
05 -.00040 -.00140

Thr - 08/22/96 DAY= 235 08:40:44

01 -.85710 -.85710  
02 72.35 ✓ 63.29 ✓  
03 .0004 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00110  
07 -.00040 -.00140

Thr - 08/22/96 DAY= 235 08:40:46

01 -.85710 -.85710  
02 72.35 ✓ 63.29  
03 .0004 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00110  
07 -.00040 -.00140

Thr - 08/22/96 DAY= 235 08:40:48

01 -.85710 -.85710  
02 72.35 ✓ 63.29  
03 .0004 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00110  
07 -.00040 -.00140

Thr - 08/22/96 DAY= 235 08:40:50

01 -.85710 -.85710  
02 72.35 ✓ 63.29  
03 .0004 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00110  
07 -.00040 -.00140

Thr - 08/22/96 DAY= 235 08:40:52

01 -.85710 -.85710  
02 72.35 ✓ 63.29  
03 .0004 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00110

page Avg = 68.346

03 .0014 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 .00140 -.00040  
07 .00140 -.00040

Thr - 08/22/96 DAY= 235 08:41:07

01 .69480 -.85710  
02 73.85 ✓ 72.35  
03 .0014 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 .00140 -.00040  
07 .00140 -.00040

Thr - 08/22/96 DAY= 235 08:41:07

01 -.69480 -.85710  
02 73.85 ✓ 72.35  
03 .0014 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 .00140 -.00040  
07 .00140 -.00040

Thr - 08/22/96 DAY= 235 08:41:11

01 -.69480 -.85710  
02 73.85 ✓ 72.35  
03 .0014 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 .00140 -.00040  
07 .00140 -.00040

Thr - 08/22/96 DAY= 235 08:41:13

01 -.69480 -.85710  
02 73.85 ✓ 72.35  
03 .0014 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 .00140 -.00040  
07 .00140 -.00040

Thr - 08/22/96 DAY= 235 08:41:15

01 -.69480 -.85710  
02 73.85 ✓ 72.35  
03 .0014 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 .00140 -.00040  
07 .00140 -.00040

Thr - 08/22/96 DAY= 235 08:41:16

01 .69480 -.85710  
02 73.85 ✓ 72.35  
03 .0014 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 .00140 -.00040  
07 .00140 -.00040

Page Avg: 71.793

07 - .00040 - .00140

Thr - 08/22/96 DAY= 235 08:40:54

01 -.85710 -.85710  
02 72.35 ✓ 63.29  
03 .0004 .0004  
04 .0000 .0000  
05 .0000 .0000  
06 -.00040 -.00110  
07 -.00040 -.00140

Thr - 08/22/96 DAY= 235 08:40:56

01 -.85710 -.85710  
02 72.35 ✓ 63.29  
03 .0004 .0004  
04 .0000 .0000  
05 .0000 .0000  
06 -.00040 -.00110  
07 -.00040 -.00140

Thr - 08/22/96 DAY= 235 08:40:57

01 -.85710 -.85710  
02 72.35 ✓ 63.29  
03 .0004 .0004  
04 .0000 .0000  
05 .0000 .0000  
06 -.00040 -.00110  
07 -.00040 -.00140

Thr - 08/22/96 DAY= 235 08:40:59

01 -.85710 -.85710  
02 73.85 ✓ 72.35  
03 .0014 .0004  
04 .0000 .0000  
05 .0000 .0000  
06 .00140 -.00040  
07 .00140 -.00040

Thr - 08/22/96 DAY= 235 08:41:01

01 -.69460 -.85710  
02 73.85 ✓ 72.35  
03 .0014 .0004  
04 .0000 .0000  
05 .0000 .0000  
06 .00140 -.00040  
07 .00140 -.00040

Thr - 08/22/96 DAY= 235 08:41:03

01 -.69460 -.85710  
02 73.85 ✓ 72.35  
03 .0014 .0004  
04 .0000 .0000  
05 .0000 .0000  
06 .00140 -.00040  
07 .00140 -.00040

Thr - 08/22/96 DAY= 235 08:41:05

01 -.69460 -.85710  
02 73.85 ✓ 72.35

Page Aug = 73.207

Thr - 08/22/96 DAY= 235 08:42:02

01 -.89140 -.93370  
02 51.16 ✓ 61.51  
03 .0000 .0007  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 .00040  
07 -.00140 -.00000

Thr - 08/22/96 DAY= 235 08:43:02

01 -.89140 -.89140  
02 65.68 ✓ 51.16  
03 .0000 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00070  
07 .00000 -.00140

Thr - 08/22/96 DAY= 235 08:44:02

01 -.83370 -.89140  
02 72.34 ✓ 65.68  
03 .0000 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00040  
07 .00000 .00000

Thr - 08/22/96 DAY= 235 08:45:02

01 .00000 -.93370  
02 72.34 ✓ 72.34  
03 .0000 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00040  
07 .00000 .00000

Thr - 08/22/96 DAY= 235 08:46:02

01 -.89140 -.86340  
02 73.52 ✓ 72.37  
03 .0000 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00040  
07 -.00070 .00000

Thr - 08/22/96 DAY= 235 08:47:02

01 -.79890 -.89140  
02 73.39 ✓ 73.52  
03 .0007 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 .00040 -.00040  
07 .00000 -.00070

Thr - 08/22/96 DAY= 235 08:48:02

01 -.79890 -.79890  
02 73.60 ✓ 73.39  
03 .0007 .0007  
04 .00000 .00000

Page Avg = 70.294

35 .00000 .00000  
36 -.00000 .00040  
37 .00040 .00000

Thr - 08/22/96 DAY= 235 08:49:02

01 -.00140 -.79900  
02 73.60  
03 .0000 .0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00000  
07 -.00040 .00040

Thr - 08/22/96 DAY= 235 08:50:02

01 -.86840 -.89140  
02 81.95 74.73  
03 .0004 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00040  
07 .00040 -.00040

Thr - 08/22/96 DAY= 235 08:51:02

01 -.79890 -.86840  
02 88.32 91.95  
03 .0004 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 .00040 -.00040  
07 .00070 .00040

Thr - 08/22/96 DAY= 235 08:52:02

01 -.79890 -.79890  
02 85.28 88.32  
03 .0002 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 .00040  
07 .00000 -.00070

Thr - 08/22/96 DAY= 235 08:53:02

01 -.86840 -.90310  
02 82.25 85.28  
03 .0004 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 .00040 .00000  
07 -.00000 .00000

Thr - 08/22/96 DAY= 235 08:54:02

01 -.79890 -.86840  
02 88.32 92.25  
03 .0004 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 .00040 .00040  
07 -.00040 -.00000

Thr - 08/22/96 DAY= 235 08:55:02

page Avg = 82.418

01 -.86840 -.79890  
22 87.76 ✓ 81.93  
03 .0004 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00000 .00040  
07 .00040 -.00040

Thr - 08/22/96 DAY= 235 08:56:02

01 -.86800 -.86840  
02 88.73 ✓ 87.76  
03 .0000 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00000 -.00000  
07 -.00110 .00040

Thr - 08/22/96 DAY= 235 08:57:02

01 -.89190 -.88000  
02 98.57 ✓ 88.73+  
03 .0000 .0000  
04 .00020 .00000  
05 .00000 .00000  
06 -.00000 -.00000  
07 -.00110 -.00110

Thr - 08/22/96 DAY= 235 08:58:02

01 -.86340 -.89190  
02 93.56 ✓ 98.57+  
03 .0000 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00000  
07 .00000 -.00110

Thr - 08/22/96 DAY= 235 08:59:02

01 -.86340 -.86840  
02 87.70 ✓ 93.56  
03 .0002 .0000  
04 .00030 .00000  
05 .00030 .00000  
06 .00000 .00000  
07 -.00070 .00000

Thr - 08/22/96 DAY= 235 09:00:03

01 -.88020 -.86840  
02 84.43 ✓ 87.70  
03 .0000 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 .00000  
07 .00000 -.00070

Thr - 08/22/96 DAY= 235 09:01:02

01 -.83370 -.88000  
02 91.53 ✓ 84.43  
03 .0000 .0000  
04 .00000 .00000  
05 .00000 .00000

Page Avg = 90.326

05 .00000 .00000  
07 .00000 .00000

Thr - 08/22/96 DAY= 235 09:02:02

01 -.90310 -.93370  
02 92.08 ✓ 91.53  
03 .0000 .0000  
04 .0000 .0000  
05 .00000 .00000  
06 .00000 .00000  
07 .00000 .00000

Thr - 08/22/96 DAY= 235 09:03:02

01 -.90320 -.90310  
02 87.47 ✓ 92.00+  
03 .0000 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 .00000  
07 .00000 .00000

Thr - 08/22/96 DAY= 235 09:04:02 — End Run #1

page Avg = 89.775

01 -.84480 -.90320  
02 88.55 87.47  
03 .0000 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00040  
07 -.00040 .00000

Thr - 08/22/96 DAY= 235 09:05:02

01 -.90310 -.84480  
02 89.73 88.55  
03 .0000 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 .00000  
07 -.00110 -.00040

Thr - 08/22/96 DAY= 235 09:06:02

01 -.86040 -.90310  
02 97.31 ✓ 89.73  
03 .0000 .0000  
04 .0000 .0000  
05 .0000 .0000  
06 .00040 .00000  
07 -.00040 -.00040

Thr - 08/22/96 DAY= 235 09:09:19 - ~~START Run#2 Melt TANK 1019~~

01 -.82290 -.88000  
02 67.70 ✓ 94.84+  
03 .0007 .0000  
04 .0000  
01 -.77010 -.75440  
02 55.52+ 13.13+  
03 -.0000 -.0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00000 -.00210  
07 -.00040 -.00040

Thr - 08/22/96 DAY= 235 09:44:02 - Start Run#2 MELT TANK

01 .420 ✓ 77.010  
02 24.09+ 55.52+  
03 -.0022 -.0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00000 -.00000  
07 -.00220 -.00040

Thr - 08/22/96 DAY= 235 09:45:02

01 -.90240 -.90420  
02 7.501 ✓ 24.05+ x10  
03 -.0037 -.0022  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00000  
07 -.00070 -.00220

OFFSCALE 0-1000 ppm

Thr - 08/22/96 DAY= 235 09:46:03

01 -.00010 -.90240  
02 4.923 ✓ 7.501 x10  
03 -.0034 -.0037  
04 .00000 .00000  
05 .00000 .00000  
06 .110 -.00070  
07 -.00040 -.00070

Thr - 08/22/96 DAY= 235 09:47:02

01 -.86390 .88010  
02 3.253 ✓ 4.923 x10  
03 -.0014 -.0034

VOID

Page Avg = ~~57.575~~  
45.47

04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00110  
07 -.00070 -.00040

Thr - 08/22/96 DAY= 235 09:48:02

01 .00000 .00000  
02 .00000 3.255 X10  
03 -.0024 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00140  
07 .00000 -.00070

Thr - 08/22/96 DAY= 235 09:49:02

01 -.00240 -.00000  
02 3.057 3.011 X10  
03 -.0021 -.0024  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00110  
07 -.00170 .00000

Thr - 08/22/96 DAY= 235 09:50:02

01 -.00000 -.00240  
02 3.250 3.057 X10  
03 -.0021 -.0021  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 .00000  
07 .00000 -.00170

Thr - 08/22/96 DAY= 235 09:51:02

01 -.00000 -.00000  
02 3.078 3.250 X10  
03 -.0020 -.0021  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00110  
07 -.00070 -.00040

Thr - 08/22/96 DAY= 235 09:52:02

01 -.00000 -.00000  
02 2.003 3.078 X10  
03 -.0021 -.0023  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00170  
07 -.00170 -.00070

Thr - 08/22/96 DAY= 235 09:53:02

01 -.00000 -.00000  
02 .00000 2.003  
03 .00000 -.0021  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00170  
07 -.00110 -.00170

Thr - 08/22/96 DAY= 235 09:54:02

VOID  
Page 45 = 25.117

01 -.00010 -.00010  
02 23.17 ✓ 15.91  
03 -.0014 -.0011  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00070  
07 .00140 -.00110

Thr - 08/22/96 DAY= 235 09:55:02 - RESTART Run # 2 MELT TANK 1055

01 -.00000 -.00010  
02 21.36 ✓ 23.17  
03 -.0011 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00140  
07 -.00040 -.00140

Thr - 08/22/96 DAY= 235 09:56:02

01 -.00010 -.00000  
02 21.06 ✓ 21.36  
03 -.0004 -.0011  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00040  
07 -.00040 -.00040

Thr - 08/22/96 DAY= 235 09:57:02

01 -.77060 -.00010  
02 21.06 ✓ 21.06  
03 .0004 -.0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00140  
07 -.00000 -.00040

Thr - 08/22/96 DAY= 235 09:58:02

01 -.00010 -.77060  
02 19.12 ✓ 19.38  
03 -.0007 -.0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00040  
07 -.00140 -.00000

Thr - 08/22/96 DAY= 235 09:59:02

01 -.00010 -.00010  
02 19.25 ✓ 19.12  
03 .0000 -.0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00170  
07 .00140 -.00140

Thr - 08/22/96 DAY= 235 10:00:03

01 -.04630 -.00010  
02 18.00 ✓ 19.25  
03 -.0004 .0000  
04 .00000 .00000  
05 .00000 .00000

page avg = 20.191  
19.695

06 -.00070 -.00040  
07 -.00000 -.00140

Thr - 08/22/96 DAY= 235 10:01:02

01 -.01240 -.04630  
02 17.96 ✓ 13.00  
03 .0007 - .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00070  
07 .00040 -.00000

Thr - 08/22/96 DAY= 235 10:02:02

01 -.04620 -.01240  
02 17.37 ✓ 13.96  
03 .0004 - .0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00040  
07 -.00000 .00040

Thr - 08/22/96 DAY= 235 10:03:02

01 -.00010 -.04620  
02 16.38 ✓ 17.37  
03 -.0017 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00040  
07 -.00070 -.00000

Thr - 08/22/96 DAY= 235 10:04:02

01 -.04630 -.00010  
02 18.14 ✓ 15.38  
03 -.0011 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00140  
07 -.00070 -.00070

Thr - 08/22/96 DAY= 235 10:05:02

01 -.00010 -.04630  
02 20.79 ✓ 18.14  
03 -.0014 -.0011  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00110  
07 -.00070 -.00070

Thr - 08/22/96 DAY= 235 10:06:02

01 -.04630 -.00010  
02 18.39 ✓ 20.79  
03 .0007 - .0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00110 -.00070  
07 -.00110 -.00070

Thr - 08/22/96 DAY= 235 10:07:02

page Avg = 17.455

01 - .772145 / .041250  
02 15.74 / 16.09  
03 -.0214 -.0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00110  
07 -.00170 -.00110

Th - 08/22/96 DAY= 235 10:08:02

01 -.00010 -.90240  
02 18.35 / 16.74  
03 .0000 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 .00000 -.00070  
07 -.00240 -.00170

Th - 08/22/96 DAY= 235 10:09:02

01 -.04630 / .00010  
02 12.14 / 19.85  
03 -.0007 .0000  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 .00000  
07 -.00170 -.00040

Th - 08/22/96 DAY= 235 10:10:02

01 -.00010 -.04630  
02 13.95 / 12.14  
03 -.0017 -.0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00040  
07 -.00040 -.00170

Th - 08/22/96 DAY= 235 10:11:02

01 -.00010 -.00010  
02 15.74 / 13.95  
03 -.0017 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00140  
07 -.00110 -.00040

Th - 08/22/96 DAY= 235 10:12:02

01 -.03550 / .00010  
02 14.58 / 15.74  
03 -.0014 -.0017  
04 .00000 .00000  
05 .00000 .00000  
06 -.00070 -.00170  
07 .00240 -.00110

Th - 08/22/96 DAY= 235 10:13:03

01 -.01240 / .03550  
02 13.23 / 14.58  
03 -.0014 -.0014  
04 .00000 .00000  
05 .00000 .00000  
06 -.00170 -.00170

Page Avg = 15.0329

07 - .00070 - .00040

Th - 08/22/96 DAY= 235 10:14:02

01 - .80010 - .81240  
02 15.92 / 13.23  
03 - .0024 - .0014  
04 .0000 .0000  
05 .0000 .0000  
06 - .0010 - .00070  
07 - .00140 - .00070

Th - 08/22/96 DAY= 235 10:15:02

01 - .80010 - .80010  
02 17.68 / 15.92  
03 - .0011 - .0024  
04 .0000 .0000  
05 .0000 .0000  
06 - .00040 - .00110  
07 - .00140 - .00140

Th - 08/22/96 DAY= 235 10:16:02

01 - .80010 - .80010  
02 18.94 / 17.68  
03 - .0011 - .0011  
04 .0000 .0000  
05 .0000 .0000  
06 - .00170 - .00040  
07 - .00040 - .00140

Th - 08/22/96 DAY= 235 10:17:02

01 - .80010 - .80010  
02 13.60 / 18.94  
03 - .0021 - .0011  
04 .0000 .0000  
05 .0000 .0000  
06 - .0010 - .00170  
07 - .00210 - .00040

Th - 08/22/96 DAY= 235 10:18:02

01 - .80010 - .80010  
02 15.11 / 13.60  
03 - .0024 - .0021  
04 .0000 .0000  
05 .0000 .0000  
06 - .00040 - .0010  
07 - .00140 - .00210

Th - 08/22/96 DAY= 235 10:19:02

01 - .84630 - .80010  
02 13.51 / 15.11  
03 - .0007 - .0024  
04 .0000 .0000  
05 .0000 .0000  
06 - .00040 - .00040  
07 - .00140 - .00140

Th - 08/22/96 DAY= 235 10:20:02

01 - .76880 - .84630  
02 16.95 / 13.51

page avg = 15.959

02 -.0011 -.0007  
04 .00000 .00000  
05 .00000 .00000  
06 -.00040 -.00040  
07 .00040 -.00140

Thr - 08/22/96 DAY= 235 10:21:03

01 [REDACTED]630 -.76880  
02 18.97 / 16.95  
03 .0004 -.0011  
04 .00000 .00000  
05 .00000 .00000  
06 -.00140 -.00040  
07 -.00070 .00040

Thr - 08/22/96 DAY= 235 10:22:02

01 -.83010 -.84630  
02 17.85 / 18.97  
03 -.0004 .0004  
04 .00000 .00000  
05 .00000 .00000  
06 -.00340 -.00140  
07 -.00110 -.00070

Thr - 08/22/96 DAY= 235 10:23:02

01 -.84630 -.88010  
02 15.53 / 17.35  
03 -.0014 -.0004  
04 -.00040 .00000  
05 [REDACTED]040 .00000  
06 [REDACTED]40 -.00340  
07 -.00110 -.00110

Thr - 08/22/96 DAY= 235 10:24:02

01 -.84630 -.84630  
02 14.70 / 15.53  
03 -.0017 -.0014  
04 .00000 -.00040  
05 .00000 -.00040  
06 -.00110 -.00040  
07 -.00040 -.00110

Thr - 08/22/96 DAY= 235 10:25:02

01 -.88010 -.84630  
02 15.55 / 14.70  
03 -.0014 -.0017  
04 -.00110 .00000  
05 -.00110 .00000  
06 -.00110 -.00110  
07 -.00070 -.00040

Thr - 08/22/96 DAY= 235 10:26:02

01 [REDACTED]10 -.88010  
02 15.17 / 15.55  
03 -.0014 -.0014  
04 .00000 -.00110  
05 .00000 -.00110  
06 -.00170 -.00110  
07 -.00040 -.00070

Page Avg: 16.462

Thr - 08/22/96 DAY= 235 10:27:02

01 -.88010 -.88010  
02 16.30 / 15.17  
03 -.0011 -.0014  
04 -.00170 .00000  
05 -.00170 .00000  
06 .00170 -.00170  
07 -.00110 -.00040

Thr - 08/22/96 DAY= 235 10:28:02

01 -.93580 -.88010  
02 17.99 / 16.30  
03 -.0014 -.0011  
04 -.00040 -.00170  
05 -.00040 -.00170  
06 -.00110 -.00110  
07 -.00070 -.00110

Thr - 08/22/96 DAY= 235 10:29:02

01 -.84630 -.93580  
02 15.40 / 17.99  
03 -.0021 -.0014  
04 -.00110 -.00040  
05 -.00110 -.00040  
06 -.00210 -.00110  
07 -.00290 -.00070

Thr - 08/22/96 DAY= 235 10:30:02

01 .0050 -.84630  
02 15.43 / 15.40  
03 -.0021 -.0021  
04 -.00110 -.00110  
05 -.00110 -.00110  
06 -.00210 -.00210  
07 -.00040 -.00290

Thr - 08/22/96 DAY= 235 10:31:02

01 -.88010 -.81250  
02 14.06 / 15.43  
03 -.0014 -.0021  
04 -.00070 -.00110  
05 -.00110 -.00110  
06 -.00170 -.00210  
07 -.00110 -.00040

Thr - 08/22/96 DAY= 235 10:32:02

01 -.81250 -.88010  
02 14.66 / 14.06  
03 -.0004 -.0014  
04 -.00140 -.00070  
05 -.00170 -.00110  
06 .00140 -.00170  
07 .00110 -.00110

Thr - 08/22/96 DAY= 235 10:33:02

01 -.83560 -.81250  
02 18.09 / 14.66  
03 -.0000 -.0004  
04 .00110 .00110

page Avg = 15,990

05 -.00100 -.00170  
06 -.00140 -.00140  
07 -.00070 -.00110

Thr - 08/22/96 DAY= 235 10:34:02

01 .01630 -.03560  
02 .055 18.09  
03 -.0000 -.0000  
04 -.00750 -.00140  
05 -.00780 -.00100  
06 -.00110 -.00140  
07 -.00040 -.00070

Thr - 08/22/96 DAY= 235 10:35:02

01 -.00010 .04630  
02 17.15 15.55  
03 -.0007 -.0000  
04 -.00270 -.00750  
05 -.00270 -.00700  
06 -.00070 -.00110  
07 -.00070 -.00040

Thr - 08/22/96 DAY= 235 10:36:02

01 -.04630 -.00010  
02 17.49 17.15  
03 .0000 -.0007  
04 -.00410 -.00270  
05 -.00580 -.00270  
06 .00110 -.00070  
07 .0010 -.00070

Thr - 08/22/96 DAY= 235 10:37:02

01 -.05900 -.04630  
02 12.09 17.49  
03 -.0004 .0000  
04 -.01200 -.00410  
05 -.01340 -.00580  
06 -.00070 -.00110  
07 -.00070 -.00110

Thr - 08/22/96 DAY= 235 10:38:03

01 -.01240 -.05900  
02 12.35 12.09  
03 -.0007 -.0004  
04 -.00650 -.01200  
05 -.00710 -.01340  
06 -.00110 -.00070  
07 -.00110 -.00070

Thr - 08/22/96 DAY= 235 10:39:02

01 -.00010 -.01240  
02 .02 12.35  
03 .0017 -.0007  
04 -.00510 -.00650  
05 -.00540 -.00710  
06 -.00140 -.00110  
07 -.00110 -.00110

Thr - 08/22/96 DAY= 235 10:40:02

Page Avg = 15.108

01 -.81240 -.83010  
02 16.80 ✓ 15.22  
03 -.0004 -.0017  
04 -.00240 -.00510  
05 -.00240 -.00540  
06 -.00040 -.00140  
07 -.00070 -.00110

Thr - 03/22/96 DAY= 235 10:41:02

01 -.84630 -.81240  
02 14.69 16.80  
03 -.0014 -.0004  
04 -.00170 -.00240  
05 -.00110 -.00240  
06 -.00070 -.00040  
07 -.00070 -.00070

Thr - 08/22/96 DAY= 235 10:42:02

01 -.81250 -.84630  
02 15.95 ✓ 14.69  
03 -.0004 -.0014  
04 -.00440 -.00170  
05 -.00510 -.00110  
06 -.00070 -.00070  
07 -.00000 -.00070

Thr - 08/22/96 DAY= 235 10:43:02

01 -.84630 -.81250  
02 14.85 ✓ 15.95  
03 -.0004 -.0004  
04 -.00440 -.00440  
05 -.00540 -.00510  
06 -.00070 -.00070  
07 .00040 -.00000

Thr - 26/22/96 DAY= 235 10:44:02

01 -.80220 -.84630  
02 17.43 ✓ 16.35  
03 .0004 -.0004  
04 -.00470 -.00480  
05 -.00520 -.00540  
06 -.00000 -.00070  
07 -.00170 .00040

Thr - 03/22/96 DAY= 235 10:45:03

01 -.80010 -.80220  
02 15.92 ✓ 17.43  
03 -.0007 .0004  
04 -.00910 -.00470  
05 -.00550 -.00500  
06 -.00140 -.00000  
07 -.00140 -.00170

Thr - 08/22/96 DAY= 235 10:46:02

01 -.88010 / .88010  
02 14.55 ✓ 15.92  
03 -.0007 -.0007  
04 -.00380 -.00910  
05 -.00420 -.00550

Page avg = 16.027

05 -.00140 -.00140  
07 -.00040 -.00140

Thr - 06/22/96 DAY= 235 10:47:02

01 -.04630 -.00010  
02 16.61 ✓ 14.55  
03 .00074 -.0007  
04 .000550 -.00360  
05 -.00010 -.00490  
06 -.00140 -.00140  
07 -.00000 -.00040

Thr - 08/22/96 DAY= 235 10:48:02

01 -.00010 -.04630  
02 14.59 ✓ 16.61  
03 -.0011 -.0004  
04 -.00980 -.00650  
05 -.01120 -.00010  
06 -.00170 -.00140  
07 -.00040 -.00000

Thr - 09/22/96 DAY= 235 10:49:02

01 -.00010 -.00010  
02 14.55 ✓ 14.59  
03 -.0007 -.0011  
04 -.00700 -.00980  
05 -.00050 -.01120  
06 -.00110 -.00170  
07 -.00070 -.00040

Thr - 10/22/96 DAY= 235 10:50:02

01 -.00010 -.00010  
02 14.01 ✓ 14.55  
03 -.0017 -.0007  
04 -.00760 -.00780  
05 -.01020 -.00050  
06 -.00070 -.00110  
07 -.00070 -.00070

Thr - 08/22/96 DAY= 235 10:51:02

01 -.00210 -.00010  
02 14.56 ✓ 14.01  
03 .0007 -.0017  
04 -.01040 -.00780  
05 -.00970 -.01020  
06 .00070 -.00070  
07 -.00040 -.00070

Thr - 08/22/96 DAY= 235 10:52:02

01 -.00010 -.00210  
02 15.04 ✓ 14.56  
03 -.0017 .0007  
04 .00010 -.01040  
05 -.00000 -.00970  
06 -.00040 .00070  
07 .00000 -.00040

Thr - 08/22/96 DAY= 235 10:53:02

01 -.00010 -.00010

Page avg = 14.977

03 -.0007 -.0017  
04 -.00390 -.00710  
05 -.00410 -.00830  
06 -.00170 -.00040  
07 -.00040 .00000

Thr - 08/22/96 DAY= 235 10:54:02

01 -.01250 -.00010  
02 14.24 14.54  
03 -.0011 -.0007  
04 -.00710 -.00380  
05 -.00710 -.00410  
06 -.00070 -.00170  
07 -.00070 -.00040

Thr - 08/22/96 DAY= 235 10:55:02 - End Run #2

avg = 14.390

01 -.04630 -.01250  
02 15.04 14.24  
03 -.0004 -.0011  
04 -.00310 -.00710  
05 -.00310 -.00710  
06 -.00110 -.00070  
07 -.00110 -.00070

Thr - 08/22/96 DAY= 235 10:56:02

01 -.06900 -.04630  
02 15.05 15.04  
03 -.0004 -.0004  
04 -.00740 -.00310  
05 -.00040 -.00310  
06 -.00040 -.00110  
07 -.00070 -.00110

Thr - 08/22/96 DAY= 235 10:57:03

07 - .001-0 - .00000

Thr - 08/22/96 DAY= 235 11:39:02

01 -.54630 -.80010  
02 15.32 13.91  
03 -.0007 -.0014  
04 .00020 -.00000  
05 .00020 -.00000  
06 -.00070 -.00110  
07 .00040 -.00140

Thr - 08/22/96 DAY= 235 11:40:02

01 -.90240 -.84630  
02 12.23 15.32  
03 -.0017 -.0007  
04 -.00040 -.01020  
05 -.01040 -.01320  
06 -.00040 -.00070  
07 -.00110 .00040

Thr - 08/22/96 DAY= 235 11:41:02

01 -.80010 -.90240  
02 8.417 12.23  
03 -.0008 -.0017  
04 -.00000 -.00040  
05 -.00000 -.01040  
06 .00000 -.00040  
07 -.00140 -.00110

Thr - 08/22/96 DAY= 235 11:42:02

01 -.80000 -.80010  
02 8.937 8.417  
03 -.0017 -.0008  
04 -.01000 -.00000  
05 -.01320 -.00000  
06 .00000 .00000  
07 -.00110 -.00140

Thr - 08/22/96 DAY= 235 11:43:02

01 -.90230 -.80000  
02 9.032 8.937  
03 -.0011 -.0017  
04 -.00070 -.01000  
05 -.00770 -.01320  
06 -.00040 .00000  
07 -.00140 -.00110

Thr - 08/22/96 DAY= 235 11:44:02

01 - .91400  
02 - 24.56  
03 - .0004 - .0007  
04 - .00750 - .01050  
05 - .00090 - .00080  
06 - .00070 - .00070  
07 - .00140 - .00110

Thr - 08/22/96 DAY= 235 11:14:02

01 - .68010 - .39150  
02 26.28 42.32  
03 - .0004 - .0004  
04 - .00650 - .00760  
05 - .00950 - .00090  
06 - .00140 - .00070  
07 - .00070 - .00140

Thr - 08/22/96 DAY= 235 11:15:02

01 - .98010 - .00010  
02 21.50 26.28  
03 - .0004 - .0004  
04 - .00750 - .00650  
05 - .00910 - .00050  
06 - .00140 - .00140  
07 - .00070 - .00070

Thr - 08/22/96 DAY= 235 11:16:02

01 - .94630 - .00010  
02 19.78 21.50  
03 .0004 - .0004  
04 - .00750 - .00780  
05 - .01020 - .00910  
06 - .00030 - .00070  
07 - .00070 - .00070

Thr - 08/22/96 DAY= 235 11:17:02

01 - .77060 - .94630  
02 19.50 19.78  
03 .0004 .0004  
04 - .00750 - .00750  
05 - .01090 - .01020  
06 - .00110 - .00020  
07 - .00110 - .00070

Thr - 08/22/96 DAY= 235 11:18:02

01 - .84630 - .77060  
02 19.50 19.50  
03 - .0004 .0004  
04 - .00650 - .00780  
05 - .00790 - .01080  
06 - .00170 - .00110  
07 - .00110 - .00110

Thr - 08/22/96 DAY= 235 11:19:02

01 -.84630 -.84630  
02 9.157 12.73  
03 -.0324 -.0024  
04 -.00750 -.00650  
05 -.00540 -.00780  
06 -.00140 -.00170  
07 .00000 -.00110

Thr - 08/22/96 DAY= 235 11:20:02

01 -.90240 -.84630  
02 10.04 9.157  
03 -.0007 -.0024  
04 -.00270 -.00750  
05 -.00600 -.00540  
06 -.00210 -.00140  
07 -.00170 -.00000

Thr - 08/22/96 DAY= 235 11:21:02

01 -.80010 -.90240  
02 10.05 10.04  
03 -.0014 -.0007  
04 -.00340 -.00270  
05 -.00210 -.00600  
06 -.00140 -.00210  
07 -.00140 -.00170

Thr - 08/22/96 DAY= 235 11:22:02

01 -.86900 -.80010  
02 10.04 10.05  
03 .0007 -.0014  
04 -.00170 -.00340  
05 -.00440 -.00210  
06 -.00070 -.00140  
07 -.00040 -.00140

Thr - 08/22/96 DAY= 235 11:23:03

01 -.84630 -.86900  
02 10.17 10.34  
03 -.0004 -.0027  
04 -.00540 -.00170  
05 -.00440 -.00440  
06 -.00240 -.00070  
07 .00000 -.00040

Thr - 08/22/96 DAY= 235 11:24:02

01 -.86900 -.84630  
02 4.996 10.17  
03 -.0027 -.0004  
04 -.00370 -.00540  
05 -.00340 -.00440  
06 .00000 -.00040  
07 .00140 .00000

Thr - 08/22/96 DAY= 235 11:25:03

01 -.84630 -.86900  
02 .8612 4.996  
03 -.0024 -.0027  
04 -.00170 -.00370

01 -.33010 -.33010  
02 13.43 10.34  
03 -.0007 -.0007  
04 -.00310 -.00210  
05 -.00270 -.00140  
06 -.00040 -.00040  
07 -.00210 .00000

Th - 08/22/96 DAY= 235 11:33:02

01 -.03560 -.00010  
02 10.45 13.45  
03 .0004 -.0007  
04 -.00240 -.00310  
05 -.00340 -.00270  
06 .00040 -.00040  
07 -.00110 -.00210

Th - 08/22/96 DAY= 235 11:34:03

01 -.00010 -.03560  
02 8.479 10.45  
03 -.0011 .0004  
04 -.00340 -.00240  
05 -.00270 -.00340  
06 .00030 .00040  
07 .00400 -.00110

Th - 08/22/96 DAY= 235 11:35:02

01 -.04630 -.00010  
02 9.611 8.479  
03 .0007 -.0011  
04 .00030 -.00340  
05 -.00270 -.00270  
06 .00200 .00000  
07 -.00110 .00000

Th - 08/22/96 DAY= 235 11:36:02

01 -.06900 -.04630  
02 10.29 9.611  
03 .0000 -.0007  
04 -.00070 -.00400  
05 -.00400 -.00270  
06 .00040 .00000  
07 -.00040 -.00110

Th - 08/22/96 DAY= 235 11:37:02

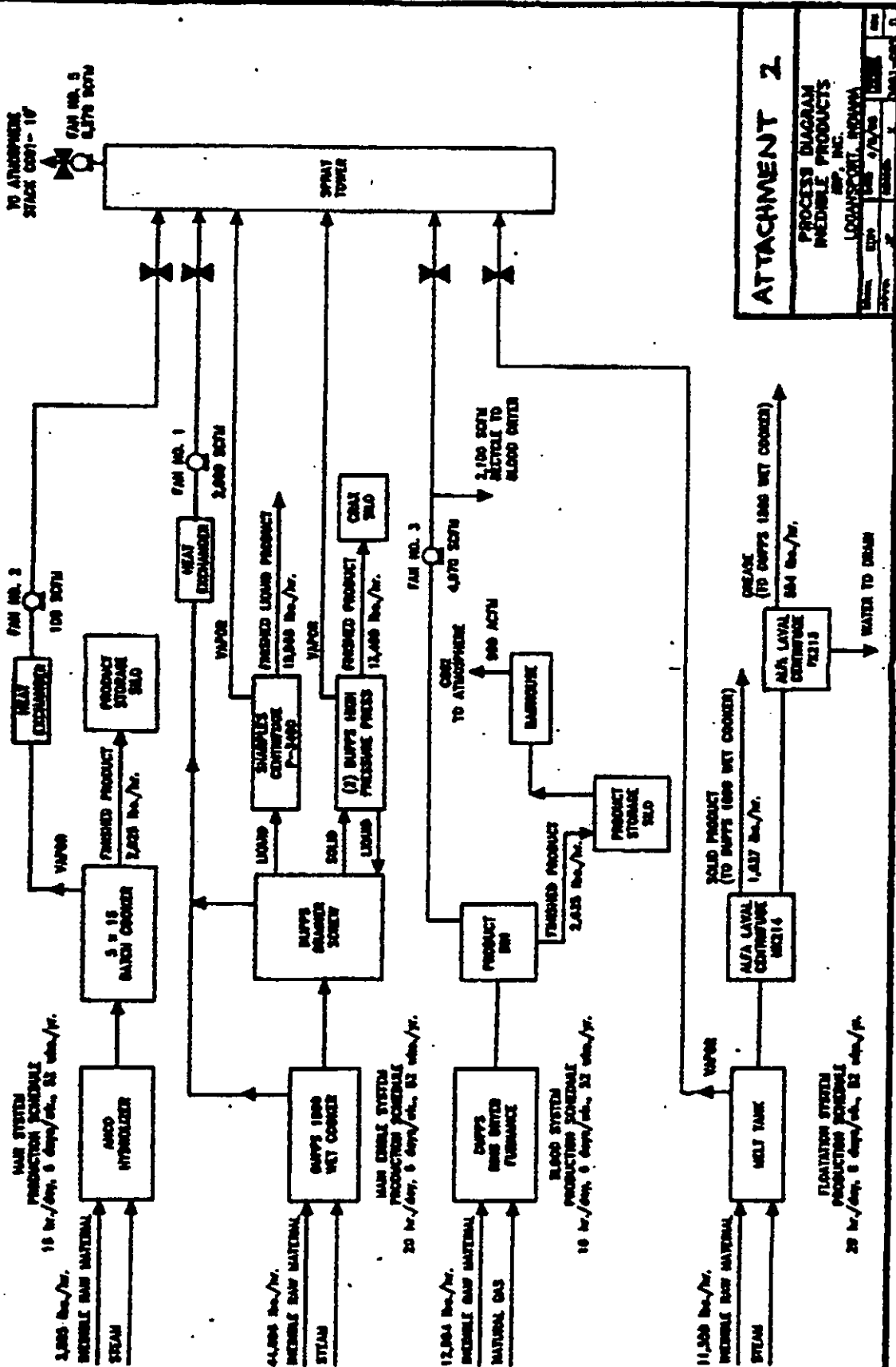
01 -.00010 -.06900  
02 12.56 10.29  
03 -.0011 .0000  
04 -.00400 -.00070  
05 -.00040 -.00400  
06 -.00040 -.00040  
07 .00200 -.00040

Th - 08/22/96 DAY= 235 11:38:02

01 -.00010 -.00010  
02 13.91 12.56  
03 -.0014 -.0011  
04 -.00060 -.00400  
05 -.01000 -.00540  
06 -.00110 -.00010

## **APPENDIX B**

### **PROCESS DATA**



X = Sampling Location

# DAILY KILL FLOOR REPORT

DATE: 8-19-96 PLANT: Loson SHIFT: A  
 CARD COUNT: 885 SET UP STD: 1.5  
 SET UP ACT: 3.5  
 TRAINERS HOURS: 99

## DAILY STATISTICS

| KILL GANG HOURS | KILL NET HOURS | ITD. CLEW HOURS | GROSS CHAIN SPEED | NET CHAIN SPEED | PERFECT HEAD KILL | ACTUAL HEAD KILL |
|-----------------|----------------|-----------------|-------------------|-----------------|-------------------|------------------|
| 1427            | 751            | 7000            | 6008              | 990             | 68                | 86%              |
| 53              | 4.34           | 6               | 10                | 87              |                   |                  |

HEAD PER MAN HOUR  
 HEAD INSPECTION  
 VICERA INSPECTION  
 FINAL INSPECTION

## DOWNTIME

| TECH | MID | PROD | COMMENTS/GENERAL/HOG QUALITY      |
|------|-----|------|-----------------------------------|
|      | 6   |      | Head inspection                   |
|      | 10  |      | Unusual find                      |
|      | 27  |      | Final kill - Horn, large piglets  |
|      | 4   |      | Hot water past 180° in drum, fire |
|      | 8   |      | P.C. stops at that water scale    |
|      | 13  |      | Hot water, water, water           |
|      |     |      | Bugs gun played up                |
|      |     |      | Stand up the drum                 |

SIGNATURE: P. Adams

| VARIANCE EXPLANATION HOURS          |  | 711/1 |     | 712/1 |     | 713/1 |     | 714/1 |     | 715/1 |     | 716/1 |     | 717/1 |     |
|-------------------------------------|--|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|
| CATEGORY                            |  | 911   | 912 | 913   | 914 | 915   | 916 | 917   | 918 | 919   | 920 | 921   | 922 | 923   | 924 |
| LEAD DUTY                           |  | 6     | 4   | 3     | 4   | 0     | 6   |       |     |       |     |       |     |       |     |
| TRAINING                            |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| REWORK                              |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCHEDULING                          |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| MECHANICAL                          |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| OVERSIGHT                           |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| EXTRA HOURS                         |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| H/A                                 |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SPECIAL LEAN AND PANCHAS PRODUCTION |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| TOTAL SPECIAL LEAN PRODUCED 7202    |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| TOTAL SPECIAL LEAN HOLLOW           |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| TOTAL PANCHAS PRODUCTION            |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| PERCENT OF CATTLE SAVED             |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| REASON                              |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 1 AVERAGE P/A                 |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 2 AVERAGE P/A                 |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 3 AVERAGE P/A                 |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 4 AVERAGE P/A                 |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 5 AVERAGE P/A                 |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 6 AVERAGE P/A                 |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 7 AVERAGE P/A                 |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 8 AVERAGE P/A                 |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 9 AVERAGE P/A                 |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 10 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 11 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 12 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 13 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 14 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 15 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 16 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 17 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 18 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 19 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 20 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 21 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 22 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 23 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 24 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 25 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 26 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 27 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 28 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 29 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 30 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 31 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 32 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 33 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 34 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 35 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 36 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 37 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 38 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 39 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 40 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 41 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 42 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 43 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 44 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 45 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 46 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 47 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 48 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 49 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 50 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 51 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 52 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 53 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 54 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 55 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 56 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 57 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 58 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 59 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 60 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 61 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 62 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 63 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 64 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 65 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 66 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 67 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 68 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 69 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 70 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 71 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 72 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 73 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 74 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 75 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 76 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 77 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 78 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 79 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 80 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 81 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 82 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 83 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 84 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 85 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 86 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 87 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 88 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 89 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 90 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 91 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 92 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 93 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 94 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 95 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 96 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 97 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 98 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 99 AVERAGE P/A                |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |
| SCALE 100 AVERAGE P/A               |  |       |     |       |     |       |     |       |     |       |     |       |     |       |     |



# DAILY KILL FLOOR REPORT

DATE: 8-22-96 PLANT: PAPA SHIFT: A  
CARD COUNT: 198 SET UP STD: 35  
ABSENTEEISM: 14 SET UP ACT: 35  
CALL INS: 17 TRAINERS/HOURS: 71 / 1585

[illegible]

| MECH | MID | PROD | COMMENTS/GENERAL/HOG QUALITY                    | DOWNTIME |
|------|-----|------|-------------------------------------------------|----------|
|      |     | 14   | Head inspect - Hair                             |          |
|      |     | 14   | Chin line - Left                                |          |
|      |     | 7    | Facial Hair - Hair                              |          |
|      |     | 6    | Blouse clean - up at head inspect               |          |
|      |     | 3    | Braided hair - rough - up in front              |          |
| 13   |     |      | 45 min down on 1.5 min. Sp<br>Back Sweater down |          |

| VARIANCE EXPLANATION HOURS           |      |      |      |      |      |      |      | 705                          |
|--------------------------------------|------|------|------|------|------|------|------|------------------------------|
| CATEGORY                             | 711/ | 712/ | 713/ | 714/ | 715/ | 716/ | 718/ |                              |
| LEAST DUTY                           | 6    | 4    | 2    | 2    | 0    | 0    | 6    |                              |
| TRAINING                             |      |      |      |      |      |      |      |                              |
| NETWORK                              |      |      |      |      |      |      |      |                              |
| SCHEDULING                           |      |      |      |      |      |      |      |                              |
| MECHANICAL                           |      |      |      |      |      |      |      |                              |
| OVER/UNDER                           |      |      |      |      |      |      |      |                              |
| ESTRADA MARRINO                      |      |      |      |      |      |      |      |                              |
|                                      |      |      |      |      |      |      |      |                              |
|                                      |      |      |      |      |      |      |      |                              |
|                                      |      |      |      |      |      |      |      |                              |
|                                      |      |      |      |      |      |      |      |                              |
| SPECIAL LEAN AND PANCEBAS PRODUCTION |      |      |      |      |      |      |      |                              |
| TOTAL SPECIAL LEAN PRODUCED 2/18 3   |      |      |      |      |      |      |      | A-SHIFT SPECIAL SENT TO CUT  |
| TOTAL SPECIAL LEAN HOLDOVER          |      |      |      |      |      |      |      | B-SHIFT SPECIAL SENT TO CUT  |
| TOTAL PANCEBAS PRODUCTION            |      |      |      |      |      |      |      | TOTAL SPEC. LEAN SENT TO CUT |
| PERCENT OF CHITS SAVED               |      |      |      |      |      |      |      | PERCENT OF CASINOS SAVED     |
| REASON                               |      |      |      |      |      |      |      | REASON                       |

| TRIM LOSS INFORMATION |                 |
|-----------------------|-----------------|
| SCALE 1 AVERAGE       | SCALE 3 AVERAGE |
| SCALE 2 AVERAGE       | SCALE 4 AVERAGE |
| TRIM LOSS             | TRIM LOSS       |

| HEADLOSS COUNTERS                     | VISCERA SET COUNTERS                  |
|---------------------------------------|---------------------------------------|
| AT 21-C-PATH LOSS 27-PATH--CONT. LOSS | AT 1-B-PATH LOSS 1-C-PATH--CONT. LOSS |
| (A) HEAD INSPECTOR 6.3                | (A) VISCERA TRIMMER 1                 |
| (B) VISCERA TRIMMER 61                | (B) DR. RAIL 2/12                     |
| (C) DR. RAIL 7/2                      | (C) SEPARATOR                         |
| HEADLOSS 6.37                         |                                       |

08X4-0A03-0278-0823-0861-0A65

then, vacuum plugged - up?

SIGNATURE: C. A. [Signature]



⊗ Shut Down 9:30p.m ⊗

LOGANSPOUT EQUACOOKER OPERATING LOGSHEET

| DESCRIPTION                               | TARGET | 2:00   | 3:00   | 4:00   | 5:00   | 6:00   | 7:00   | 8:00   | 9:00   | 10:00  | 11:00  | 12:00  |
|-------------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Raw Material Bin Level                    |        | 14     | 14     | 14     | 14     | 14     | 14     | 14     | 14     | 14     | 14     | 14     |
| Raw Feed #8 VFD Speed                     | 31.0   | 31.0   | 33.0   | 33.0   | 33.0   | 33.0   | 34.0   | 34.0   | 34.0   | 34.0   | 34.0   | 34.0   |
| Hogger Grinder Motor Load                 |        | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     |
| Cooker Steam P.S.I. (after Control Valve) |        | 210/22 | 210/22 | 210/22 | 210/22 | 210/22 | 210/22 | 210/22 | 210/22 | 210/22 | 210/22 | 210/22 |
| Equacooker Product Temperature            |        | 116    | 116    | 112    | 112    | 111    | 110    | 111    | 111    | 111    | 111    | 111    |
| Cooker Heat Exch Tailwater Temp           |        | 16     | 16     | 24     | 14     | 15     | 8      | 7      | 7      | 7      | 7      | 7      |
| Cooker Condensate Temp(after trap)        |        | 20.28  | 19.71  | 25.68  | 27.63  | 18.09  | 14.21  | 20.05  | 20.05  | 20.05  | 20.05  | 20.05  |
| Cooker Condensate PSI(after trap)         |        | 1/2    | 1/2    | 1/2    | 1/3    | 1/3    | 1/3    | 1/3    | 1/3    | 1/3    | 1/3    | 1/3    |
| Vapor Removal Rate/Bucket Test in sec.    |        | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   |
| Equacooker Level                          |        | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   |
| Control Wheel VFD Speed                   |        | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   |
| Drainor/Overpressor Screw VFD Speed       |        | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   | 20.6   |
| South Pressor Screw VFD Speed             |        | 50.0   | 38.0   | 38.0   | 41.0   | 41.0   | 41.0   | 41.0   | 41.0   | 41.0   | 41.0   | 41.0   |
| South Pressor Mainshaft Motor Load        |        | 45/55  | 45/55  | 45/55  | 45/55  | 45/55  | 45/55  | 45/55  | 45/55  | 45/55  | 45/55  | 45/55  |
| South Pressor Crax Quality                |        | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     |
| North Pressor Screw VFD Speed             |        |        |        |        |        |        |        |        |        |        |        |        |
| North Pressor Mainshaft Motor Load        |        |        |        |        |        |        |        |        |        |        |        |        |
| North Pressor Crax Quality                |        |        |        |        |        |        |        |        |        |        |        |        |
| Crax Surge Bin Level                      |        | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     |
| Crax Grinder Motor Load                   |        | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     | OK     |
| Sharples Centrifuge Motor Load            |        | 13     | 13     | 14     | 14     | 14     | 14     | 14     | 14     | 14     | 14     | 14     |
| East Grease Storage Tank Level            |        |        |        |        |        |        |        |        |        |        |        |        |
| West Grease Storage Tank Level            |        |        |        |        |        |        |        |        |        |        |        |        |

\*Record all mechanical downtime on the back of this form. Include equipment name, time down, time back operational, reason for downtime and end of shift status.

\*\*Report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.

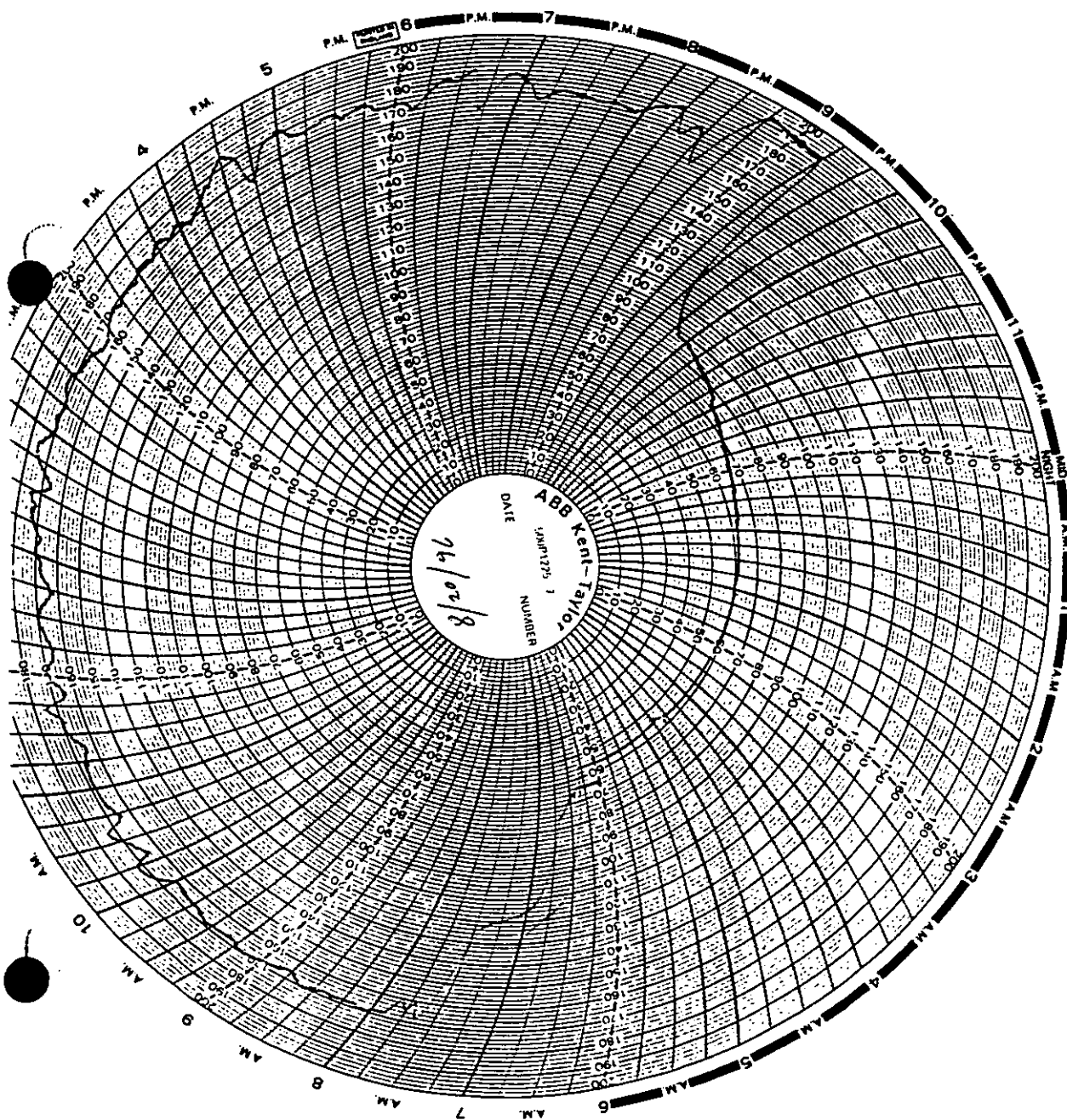
Department Condition: Shift Start (Good/Fair/Poor); Shift End (Good/Fair/Poor)

Time Electromagnet Checked 2:20pm

South Pressor Choke Pressure OK  
North Pressor Choke Pressure OK  
South Pressor Fines Pump Status OK  
North Pressor Fines Pump Status OK

Time Equacooker Jacket Steam was turned on 8:52  
Time Equacooker Jacket Steam was turned off 9:52

Temperature Recorder  
for Wet Cooker.





# LOGANSPORE EQUACOOKER OPERATING LOGSHEET

Operator Jim Moltz

Date and Shift 08-21-96 13:54-15:54

| DESCRIPTION                               | TARGET | 2:00  | 3:00  | 4:00  | 5:00  | 6:00  | 7:00  | 8:00  | 9:00  | 10:00 | REMARKS |
|-------------------------------------------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|
| Raw Material Bin Level                    |        | 1/3   | 1/2   | 1/4   | 1/4   | 1/4   | 1/4   | 1/4   | 1/4   | 1/4   |         |
| Raw Feed #8 VFD Speed                     |        | 33.0  | 33.0  | 33.0  | 33.0  | 33.0  | 33.0  | 33.0  | 33.0  | 33.0  |         |
| Hogger Grinder Motor Load                 |        | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |         |
| Cooker Steam P.S.I. (after Control Valve) |        |       |       |       |       |       |       |       |       |       |         |
| Equacooker Product Temperature            |        |       |       |       |       |       |       |       |       |       |         |
| Cooker Heat Exch Tailwater Temp           |        |       |       |       |       |       |       |       |       |       |         |
| Cooker Condensate Temp(after trap)        |        |       |       |       |       |       |       |       |       |       |         |
| Cooker Condensate PSI(after trap)         |        |       |       |       |       |       |       |       |       |       |         |
| Vapor Removal Rate/Bucket Test in sec     |        |       |       |       |       |       |       |       |       |       |         |
| Equacooker Level                          |        |       |       |       |       |       |       |       |       |       |         |
| Control Wheel VFD Speed                   |        | 22.0  | 22.0  | 22.0  | 22.0  | 21.5  | 24.5  | 22.5  | 22.5  | 21.5  |         |
| Drainor/Overpressor Screw VFD Speed       |        |       |       |       |       |       |       |       |       |       |         |
| South Pressor Screw VFD Speed             |        | 40.0  | 40.0  | 40.0  | 40.0  | 39.0  | 38.0  | 38.0  | 38.0  | 38.0  |         |
| South Pressor Mainshaft Motor Load        |        | 57.75 | 57.65 | 45/50 | 45/50 | 39/45 | 38/40 | 38/40 | 38/40 | 38/40 |         |
| South Pressor Crax Quality                |        | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |         |
| North Pressor Screw VFD Speed             |        |       |       |       |       |       |       |       |       |       |         |
| North Pressor Mainshaft Motor Load        |        |       |       |       |       |       |       |       |       |       |         |
| North Pressor Crax Quality                |        |       |       |       |       |       |       |       |       |       |         |
| Crax Surge Bin Level                      |        | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |         |
| Crax Grinder Motor Load                   |        | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |         |
| Sharples Centrifuge Motor Load            |        | 13    | 13    | 13    | 13    | 13    | 14    | 13    | 13    | 13    |         |
| East Grease Storage Tank Level            |        |       |       |       |       |       |       |       |       |       |         |
| West Grease Storage Tank Level            |        |       |       |       |       |       |       |       |       |       |         |

Shift Down 22:45 - 22:50

\*Record all mechanical downtime on the back of this form. Include equipment name, time down, time back operational, reason for downtime and end of shift status.

\*\*Report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.

Department Condition: Shift Start (Good) Fair Poor) Shift End (Good) Fair Poor)

Time Electromagnet Checked 12:30 PM

South Pressor Choke Pressure OK

North Pressor Choke Pressure OK

South Pressor Fines Pump Status OK

North Pressor Fines Pump Status OK

Time Equacooker Jacket Steam was turned on 12:30 PM

Time Equacooker Jacket Steam was turned off 22:30

Operator: *John R. Spence*  
 Date and Shift: *8/22/96* (A)

# LOGANSPOUT EQUACOOKER OPERATING LOGSHEET

| DESCRIPTION                               | T     | I     | M     | E     | REMARKS |
|-------------------------------------------|-------|-------|-------|-------|---------|
| Raw Material Bin Level                    | 9:00  | 11:00 | 12:00 | 1:00  | 2:00    |
| Raw Feed #8 VFD Speed                     | A     | A     | 1/3   | 1/3   |         |
| Hogger Grinder Motor Load                 | 3/48  | 3/48  | 3/48  | 3/48  |         |
|                                           | NA    | NA    | NA    | NA    |         |
| Cooker Steam P.S.I. (after Control Valve) | 273.7 | 271.5 | 268.5 | 265.5 |         |
| Equacooker Product Temperature            | 272.5 | 272.5 | 272.5 | 272.5 |         |
| Cooker Heat Exch Tailwater Temp           |       |       |       |       |         |
| Cooker Condensate Temp (after trap)       |       |       |       |       |         |
| Cooker Condensate PSI (after trap)        |       |       |       |       |         |
| Vapor Removal Rate/Bucket Test in sec.    |       |       |       |       |         |
| Equacooker Level                          | 1/4   | 1/4   | 1/2   | 1/3   |         |
| Control Wheel VFD Speed                   | 1631  | 1950  | 2070  | 2199  | 2210    |
| Drain/Overpressor Screw VFD Speed         |       |       |       |       |         |
| South Pressor Screw VFD Speed             | 2886  | 4210  | 4193  | 4194  |         |
| South Pressor Mainshaft Motor Load        | 70    | 60    | 60    | 65    |         |
| South Pressor Crax Quality                | Good  | Good  | Good  | Good  |         |
| North Pressor Screw VFD Speed             |       |       |       |       |         |
| North Pressor Mainshaft Motor Load        |       |       |       |       |         |
| North Pressor Crax Quality                |       |       |       |       |         |
| Crax Surge Bin Level                      | OK    | OK    | OK    | OK    |         |
| Crax Grinder Motor Load                   | NA    | NA    | NA    | NA    |         |
| Sharples Centrifuge Motor Load            | NA    | NA    | NA    | NA    |         |
| East Grease Storage Tank Level            | OK    | OK    | OK    | OK    |         |
| West Grease Storage Tank Level            | OK    | OK    | OK    | OK    |         |

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Department Condition: Shift Start (Good/Fair/Poor); Shift End (Good/Fair/Poor)

Time Electromagnet Checked

South Pressor Choke Pressure *630*  
 North Pressor Choke Pressure *630*  
 South Pressor Fines Pump Status *630*  
 North Pressor Fines Pump Status *—*

Time Equacooker Jacket Steam was turned on *630*  
 Time Equacooker Jacket Steam was turned off *630*

Start 630  
 Start 745

1040 AM  
 264.3  
 1050  
 263.9  
 1100  
 266.9

Operator Name Debra, Lynch  
 Date and Shift 8-20-96 A Shift

# LOGANSPORT BLOOD DRYING & TATING LOGSHEET

LOGS LOG.WK4

| DESCRIPTION                             | TARGET  | 06:00 | 07:00 | 08:00 | 09:00 | 10:00 | 11:00 | 12:00 | 01:00 | 02:00 | 03:00 | 04:00 | 05:00 |
|-----------------------------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Furnace Exhaust Temperature             | <700 F  |       |       |       |       | 200   | 200   | 190   | 191   | 190   |       |       |       |
| Ring Dryer Disch Temp Set-point         | 200 F   |       |       |       |       | 191   | 191   | 191   | 191   | 191   |       |       |       |
| Ring Dryer Disch Product Temperature    | actual  |       |       |       |       | 190   | 190   | 190   | 192   | 189   |       |       |       |
| Centrifuge Feed Pump Speed              | 18.5 Hz |       |       |       |       | 24.5  | 24.5  | 24.5  | 24.5  | 24.5  |       |       |       |
| Coagulator Temperature Setpoint         |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Coagulator Product Temperature          |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Centrifuge Motor Load Amperes           | <15 A   |       |       |       |       | 10    | 10    | 10    | 10    | 10    |       |       |       |
| South Raw Blood Surge Tank Level        | MIN     |       |       |       |       | 0     | 0     | 0     | 0     | 0     |       |       |       |
| North Raw Blood Surge Tank Level        | MIN     |       |       |       |       | 0     | 0     | 0     | 0     | 0     |       |       |       |
| Raw Blood Feed Tank Level               | 3/4     |       |       |       |       | 1/3   | 1/3   | 1/3   | 1/2   | 1/2   |       |       |       |
| Feed Tank Agitator                      | ON      |       |       |       |       | ON    | ON    | ON    | ON    | ON    |       |       |       |
| Main Steam Incoming Pressure            | 125psi  |       |       |       |       | 115   | 115   | 115   | 115   | 115   |       |       |       |
| After Regulator Steam Pressure          | 40psi   |       |       |       |       | 45    | 45    | 45    | 45    | 45    |       |       |       |
| Coagulator Main Steam Valve Pressure    | 30psi   |       |       |       |       | 25    | 25    | 25    | 25    | 25    |       |       |       |
| Pre-Coagulation Injection Water Rate    | 2gpm    |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Minutes Main Blood Valve Open           | actual  |       |       |       |       | 55    | 55    | 55    | 55    | 55    |       |       |       |
| Centrifuge Feed Pump Disch Pressure     | <20psi  |       |       |       |       | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 |       |       |       |
| Coagulator North Injector Valve Setting | 1-1/4   |       |       |       |       | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   |       |       |       |
| Coagulator South Injector Valve Setting | 3/4     |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Centrifuge Injection Water Rate         | 8gpm    |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Centrifuge Feed Temperature             |         |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| Centrifuge Stickwater Sample            |         |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| Centrifuged Blood Sample                |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Ring Dryer percent recycle              | MIN     |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| Air Lock and Cyclone status             | CLEAR   |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| Cyclone Outlet Pressure                 | 15"     |       |       |       |       | 17.5  | 17.5  | 17.5  | 17.5  | 17.5  |       |       |       |
| Dried Blood Moisture                    | 10%     |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Dried Blood Blower Discharge Pressure   |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |

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Department/Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)



Operator Name *JS Bush*

File and Shift *8-51-96 A - Shift*

# LOGANSPOUT BLOOD DRYING OPERATING LOGSHEET

LOBLOC.WK4

| DESCRIPTION                             | TARGET  | 06:00 | 07:00 | 08:00 | 09:00 | 10:00 | 11:00 | 12:00 | 01:00 | 02:00 | 03:00 | 04:00 | 05:00 |
|-----------------------------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Furnace Exhaust Temperature             | <700 F  |       |       |       |       | 195   | 195   | 190   | 195   | 195   |       |       |       |
| Ring Dryer Disch Temp Set-point         | 200 F   |       |       |       |       | 191   | 191   | 191   | 191   | 191   |       |       |       |
| Ring Dryer Disch Product Temperature    | actual  |       |       |       |       | 198   | 198   | 199   | 190   | 190   |       |       |       |
| Centrifuge Feed Pump Speed              | 18.5 Hz |       |       |       |       | 24.5  | 24.5  | 24.5  | 24.5  | 24.5  |       |       |       |
| Coagulator Temperature Setpoint         |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Coagulator Product Temperature          |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Centrifuge Motor Load Amperes           | <15 A   |       |       |       |       | 10    | 10    | 10    | 10    | 10    |       |       |       |
| South Raw Blood Surge Tank Level        | MIN     |       |       |       |       | 0     | 0     | 0     | 0     | 0     |       |       |       |
| North Raw Blood Surge Tank Level        | MIN     |       |       |       |       | 0     | 0     | 0     | 0     | 0     |       |       |       |
| Raw Blood Feed Tank Level               | 3/4     |       |       |       |       | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   |       |       |       |
| Feed Tank Agitator                      | ON      |       |       |       |       | ON    | ON    | ON    | ON    | ON    |       |       |       |
| Main Steam Incoming Pressure            | 125psi  |       |       |       |       | 115   | 115   | 115   | 115   | 115   |       |       |       |
| Steam Regulator Steam Pressure          | 40psi   |       |       |       |       | 45    | 45    | 45    | 45    | 45    |       |       |       |
| Coagulator Main Steam Valve Pressure    | 30psi   |       |       |       |       | 25    | 25    | 25    | 25    | 25    |       |       |       |
| Pre-Coagulation Injection Water Rate    | 2gpm    |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Minutes Main Blood Valve Open           | actual  |       |       |       |       | Start | 55    | 55    | 55    | 55    |       |       |       |
| Centrifuge Feed Pump Disch Pressure     | <20psi  |       |       |       |       | 10    | 10    | 10    | 10    | 10    |       |       |       |
| Coagulator North Injector Valve Setting | 1-1/4   |       |       |       |       | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 |       |       |       |
| Coagulator South Injector Valve Setting | 3/4     |       |       |       |       | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   |       |       |       |
| Centrifuge Injection Water Rate         | 8gpm    |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Centrifuge Feed Temperature             |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Centrifuge Stickwater Sample            |         |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| Centrifuged Blood Sample                |         |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| Ring Dryer percent recycle              | MIN     |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Ir Lock and Cyclone status              | CLEAR   |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| Cyclone Outlet Pressure                 | 15"     |       |       |       |       | 17.5  | 17.5  | 17.5  | 17.5  | 17.5  |       |       |       |
| Dried Blood Moisture                    | 10%     |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Dried Blood Blower Discharge Pressure   |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |

Record all mechanical downtime on the back of this form. Include equipment name, time down, time back operational, reason for downtime and end of shift status.  
Report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.  
Department-Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

Operator Name

Date and Shift 2-21-90

## LOGANSPOUT BLOOD DRYING ATING LOGSHEET

(08L00.WK4)

| DESCRIPTION                             | TARGET  | 06:00 | 07:00 | 08:00 | 09:00 | 10:00 | 11:00 | 12:00 | 01:00 | 02:00 | 03:00 | 04:00 | 05:00 |
|-----------------------------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Furnace Exhaust Temperature             | <700 F  | 190   | 190   | 190   | 190   | 190   | 190   | 190   |       |       |       |       |       |
| Ping Dryer Disch Temp Setpoint          | 200 F   | 191   | 191   | 191   | 191   | 191   | 191   | 191   |       |       |       |       |       |
| Fling Dryer Disch Product Temperature   | actual  | 191   | 191   | 191   | 191   | 191   | 191   | 191   |       |       |       |       |       |
| Centrifuge Feed Pump Speed              | 18.5 Hz | 24.5  | 24.5  | 24.5  | 24.5  | 24.5  | 24.5  | 24.5  |       |       |       |       |       |
| Coagulator Temperature Setpoint         |         |       |       |       |       |       |       |       |       |       |       |       |       |
| Coagulator Product Temperature          |         |       |       |       |       |       |       |       |       |       |       |       |       |
| Centrifuge Motor Load Amperes           | <15 A   | 20    | 10    | 10    | 10    | 10    | 10    | 10    |       |       |       |       |       |
| South Raw Blood Surge Tank Level        | MIN     |       |       |       |       |       |       |       |       |       |       |       |       |
| North Raw Blood Surge Tank Level        | MIN     |       |       |       |       |       |       |       |       |       |       |       |       |
| Raw Blood Feed Tank Level               | 3/4     | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   |       |       |       |       |       |
| Feed Tank Agitator                      | ON      | ON    | ON    | ON    | ON    | ON    | ON    | ON    |       |       |       |       |       |
| Main Steam Incoming Pressure            | 125psi  | 120   | 120   | 120   | 120   | 120   | 120   | 120   |       |       |       |       |       |
| After Regulator Steam Pressure          | 40psi   | 45    | 45    | 45    | 45    | 45    | 45    | 45    |       |       |       |       |       |
| Coagulator Main Steam Valve Pressure    | 30psi   | 47    | 47    | 47    | 47    | 47    | 47    | 47    |       |       |       |       |       |
| Pre-Coagulation Injection Water Rate    | 2gpm    |       |       |       |       |       |       |       |       |       |       |       |       |
| Minutiles Main Blood Valve Open         | actual  | 55    | 55    | 55    | 55    | 55    | 55    | 55    |       |       |       |       |       |
| Centrifuge Feed Pump Disch Pressure     | <20psi  | 12    | 12    | 12    | 12    | 12    | 12    | 12    |       |       |       |       |       |
| Coagulator North Injector Valve Setting | 1-1/4   | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 |       |       |       |       |       |
| Coagulator South Injector Valve Setting | 3/4     | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   |       |       |       |       |       |
| Centrifuge Injection Water Rate         | 8gpm    |       |       |       |       |       |       |       |       |       |       |       |       |
| Centrifuge Feed Temperature             |         |       |       |       |       |       |       |       |       |       |       |       |       |
| Centrifuge Stickwater Sample            |         | OK    | OK    | OK    | OK    | OK    | OK    | OK    |       |       |       |       |       |
| Centrifuged Blood Sample                |         | OK    | OK    | OK    | OK    | OK    | OK    | OK    |       |       |       |       |       |
| Ring Dryer percent recycle              | MIN     |       |       |       |       |       |       |       |       |       |       |       |       |
| Air Lock and Cyclone status             | CLEAR   | OK    | OK    | OK    | OK    | OK    | OK    | OK    |       |       |       |       |       |
| Cyclone Outlet Pressure                 | 15"     | 17.5  | 17.5  | 17.5  | 17.5  | 17.5  | 17.5  | 17.5  |       |       |       |       |       |
| Dried Blood Moisture                    | 10%     | 6.4   | 6.4   | 6.4   | 6.4   | 6.4   | 6.4   | 6.4   |       |       |       |       |       |
| Dried Blood Blower Discharge Pressure   |         |       |       |       |       |       |       |       |       |       |       |       |       |

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Report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.

Department Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

Operator Name

Date and Shift

J. J. Kunk  
8-22-98

## LOGANSPORT BLOOD DRYING OPERATING LOGSHEET

LOBBLOG.WK4

| DESCRIPTION                             | TARGET  | 06:00 | 07:00 | 08:00 | 09:00 | 10:00 | 11:00 | 12:00 | 01:00 | 02:00 | 03:00 | 04:00 | 05:00 |
|-----------------------------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Furnace Exhaust Temperature             | <700 F  |       |       |       |       | 190   | 190   | 190   |       |       |       |       |       |
| Ring Dryer Disch Temp Set-point         | 200 F   |       |       |       |       | 191   | 191   | 191   |       |       |       |       |       |
| Ring Dryer Disch Product Temperature    | actual  |       |       |       |       | 190   | 185   | 187   |       |       |       |       |       |
| Centrifuge Feed Pump Speed              | 18.5 Hz |       |       |       |       | 23.5  | 23.5  | 25.5  |       |       |       |       |       |
| Coagulator Temperature Setpoint         |         |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Coagulator Product Temperature          |         |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Centrifuge Motor Load Amperes           | <15 A   |       |       |       |       | 19    | 13    | 13    |       |       |       |       |       |
| South Raw Blood Surge Tank Level        | MIN     |       |       |       |       | NA    | 0     | 0     |       |       |       |       |       |
| North Raw Blood Surge Tank Level        | MIN     |       |       |       |       | 0     | 0     | 0     |       |       |       |       |       |
| Raw Blood Feed Tank Level               | 3/4     |       |       |       |       | 3/4   | 3/4   | 3/4   |       |       |       |       |       |
| Feed Tank Agitator                      | ON      |       |       |       |       | ON    | ON    | ON    |       |       |       |       |       |
| Main Steam Incoming Pressure            | 125psi  |       |       |       |       | 115   | 115   | 115   |       |       |       |       |       |
| After Regulator Steam Pressure          | 40psi   |       |       |       |       | 43    | 43    | 43    |       |       |       |       |       |
| Coagulator Main Steam Valve Pressure    | 30psi   |       |       |       |       | 25    | 25    | 25    |       |       |       |       |       |
| Pre-Coagulation Injection Water Rate    | 2gpm    |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Minutes Main Blood Valve Open           | actual  |       |       |       |       | Start | 55    | 55    |       |       |       |       |       |
| Centrifuge Feed Pump Disch Pressure     | <20psi  |       |       |       |       | 1-1/4 | 1-1/4 | 1-1/4 |       |       |       |       |       |
| Coagulator North Injector Valve Setting | 1-1/4   |       |       |       |       | 3/4   | 3/4   | 3/4   |       |       |       |       |       |
| Coagulator South Injector Valve Setting | 3/4     |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Centrifuge Injection Water Rate         | 8gpm    |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Centrifuge Feed Temperature             |         |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Centrifuge Stickwater Sample            |         |       |       |       |       | OK    | OK    | OK    |       |       |       |       |       |
| Centrifuged Blood Sample                |         |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Ring Dryer percent recycle              | MIN     |       |       |       |       | OK    | OK    | OK    |       |       |       |       |       |
| Drum Lock and Cyclone status            | CLEAR   |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Cyclone Outlet Pressure                 | 15"     |       |       |       |       | OK    | OK    | OK    |       |       |       |       |       |
| Dried Blood Moisture                    | 10%     |       |       |       |       | 17.5  | 17.5  | 17.5  |       |       |       |       |       |
| Dried Blood Blower Discharge Pressure   |         |       |       |       |       | NA    | 6.6   | NA    |       |       |       |       |       |

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 Department/Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

Date and Shift 10-76 A

| DESCRIPTION                             | TARGET | 8:00 | 9:00 | 10:00 | 11:00 | 12:00 | 1:00 | 2:00 | E | :00 | :00 | :00 | :00 | :00 |
|-----------------------------------------|--------|------|------|-------|-------|-------|------|------|---|-----|-----|-----|-----|-----|
| Bsmr Hair Collection Bin Status         |        | OK   | OK   | OK    | OK    | OK    | OK   | OK   |   |     |     |     |     |     |
| Hair Vacuum Blower Motor Load           |        | 18   | 18   | 18    | 18    | 18    | 18   | 18   |   |     |     |     |     |     |
| # of Minutes Feed Screw was Reversed    |        | 0    | 0    | 0     | 0     | 0     | 0    | 0    |   |     |     |     |     |     |
| Hydrolizer Reg. Internal Steam Pressure |        | 30   | 50   | 50    | 50    | 50    | 50   | 50   |   |     |     |     |     |     |
| Hydrolizer Reg. Jacket Steam Pressure   |        | 90   | 90   | 90    | 90    | 90    | 90   | 90   |   |     |     |     |     |     |
| Hydrolizer Feeder Screw Motor Load      |        | 12   | 8    | 8     | 8     | 8     | 8    | 8    |   |     |     |     |     |     |
| Hydrolizer Feed Temperature             |        | 108  | 111  | 154   | 112   | 113   | 150  | 114  |   |     |     |     |     |     |
| Hydrolizer Main Shaft Motor Load        |        | NA   | NA   | NA    | NA    | NA    | NA   | NA   |   |     |     |     |     |     |
| Hydrolizer Discharge Pressure           |        | 50   | 47   | 50    | 49    | 48    | 50   | 49   |   |     |     |     |     |     |
| Hydrolizer Condensate Temperature       |        | 225  | 215  | 215   | 215   | 215   | 215  | 215  |   |     |     |     |     |     |
| Hydrolized Hair Sample Quality          |        | Good | Good | Good  | Good  | Good  | Good | Good |   |     |     |     |     |     |
| Hair Cooker Jacket Reg. Steam Pressure  |        | 89   | 85   | 85    | 85    | 84    | 84   | 80   |   |     |     |     |     |     |
| Hair Cooker Condensate Temperature      |        | 190  | 190  | 198   | 198   | 198   | 198  | 198  |   |     |     |     |     |     |
| Hair Cooker Motor Load                  |        | NA   | NA   | NA    | NA    | NA    | NA   | NA   |   |     |     |     |     |     |
| Hair Cooker Discharge Time              |        | ✓    | ✓    | ✓     | ✓     | ✓     | ✓    | ✓    |   |     |     |     |     |     |
| East Flotation Cell Condition           |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| # of Minutes East Skimmer Arm Running   |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| East Recycle Pump Discharge Pressure    |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| East Air Injection Air Flow             |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| East Air Mix Tank Inlet Pressure        |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| East Air Mix Tank Outlet Pressure       |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| West Flotation Cell Condition           |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| # of Minutes West Skimmer Arm Running   |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| West Recycle Pump Discharge Pressure    |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| West Air Injection Air Flow             |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| West Air Mix Tank Inlet Pressure        |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| West Air Mix Tank Outlet Pressure       |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| Flotation Heat Tank Level               |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| Flotation Heat Tank Temperature         |        |      |      |       |       |       |      |      |   |     |     |     |     |     |
| Tank Discharge Pump Rate                |        |      |      |       |       |       |      |      |   |     |     |     |     |     |

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\*\*report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.

Department Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

Time Hair Vacuum System Started

# of Paddles Removed from Hydrolizer

# of Times Hydrolizer Plugged & Blown Down

Hair Silo Beginning Level

Time Hair Received from Kill Floor  
 Time Hair Finished from Kill Floor  
 Time Hydrolizer Feeder Shut Off  
 Final Time Hair Cooker Discharged  
 Hair Silo Ending Level

6:30  
 0  
 0  
 0  
 OK

Operator *David Richardson*  
Date and Shift *8-20-96 B-Shift*

LOGANSPOUT HAIR HYDROLIZER and FLOTATION CELL LOGSHEET

LOGAN LOG WMA

| DESCRIPTION                             | TARGET | 3:00  | 4:00  | 5:00  | 6:00 | M | E | :00 | :00 | :00 | :00 | DISPOSITION |
|-----------------------------------------|--------|-------|-------|-------|------|---|---|-----|-----|-----|-----|-------------|
| Bsmt Hair Collection Bin Status         |        | OK    | OK    | OK    |      |   |   |     |     |     |     |             |
| Hair Vacuum Blower Motor Load           |        | 180   | 18    | 18    |      |   |   |     |     |     |     |             |
| # of Minutes Feed Screw was Reversed    |        | 0     | 0     | 0     |      |   |   |     |     |     |     |             |
| Hydrolizer Reg. Internal Steam Pressure |        | 48.3  | 48.3  | 48.3  |      |   |   |     |     |     |     |             |
| Hydrolizer Reg. Jacket Steam Pressure   |        | 89.5  | 89.5  | 89.5  |      |   |   |     |     |     |     |             |
| Hydrolizer Feeder Screw Motor Load      |        | 5     | 5     | 5     |      |   |   |     |     |     |     |             |
| Hydrolizer Feed Temperature             |        | 110   | 125   | 140   |      |   |   |     |     |     |     |             |
| Hydrolizer Main Shaft Motor Load        |        | N/A   | N/A   | N/A   |      |   |   |     |     |     |     |             |
| Hydrolizer Discharge Pressure           |        | 48.6  | 48.6  | 48.6  |      |   |   |     |     |     |     |             |
| Hydrolizer Condensate Temperature       |        | 230.5 | 230.4 | 230.7 |      |   |   |     |     |     |     |             |
| Hydrolized Hair Sample Quality          |        | 0.400 | 0.400 | 0.400 |      |   |   |     |     |     |     |             |
| Hair Cooker Jacket Reg. Steam Pressure  |        | 158.5 | 158.5 | 158.5 |      |   |   |     |     |     |     |             |
| Hair Cooker Condensate Temperature      |        | 197.5 | 196.5 | 197   |      |   |   |     |     |     |     |             |
| Hair Cooker Motor Load                  |        | N/A   | N/A   | N/A   |      |   |   |     |     |     |     |             |
| Hair Cooker Discharge Time              |        |       |       |       |      |   |   |     |     |     |     |             |
| East Flotation Cell Condition           |        |       |       |       |      |   |   |     |     |     |     |             |
| # of Minutes East Skimmer Arm Running   |        |       |       |       |      |   |   |     |     |     |     |             |
| East Recycle Pump Discharge Pressure    |        |       |       |       |      |   |   |     |     |     |     |             |
| East Air Injection Air Flow             |        |       |       |       |      |   |   |     |     |     |     |             |
| East Air Mix Tank Inlet Pressure        |        |       |       |       |      |   |   |     |     |     |     |             |
| East Air Mix Tank Outlet Pressure       |        |       |       |       |      |   |   |     |     |     |     |             |
| West Flotation Cell Condition           |        |       |       |       |      |   |   |     |     |     |     |             |
| # of Minutes West Skimmer Arm Running   |        |       |       |       |      |   |   |     |     |     |     |             |
| West Recycle Pump Discharge Pressure    |        |       |       |       |      |   |   |     |     |     |     |             |
| West Air Injection Air Flow             |        |       |       |       |      |   |   |     |     |     |     |             |
| West Air Mix Tank Inlet Pressure        |        |       |       |       |      |   |   |     |     |     |     |             |
| West Air Mix Tank Outlet Pressure       |        |       |       |       |      |   |   |     |     |     |     |             |
| Flotation Heat Tank Level               |        |       |       |       |      |   |   |     |     |     |     |             |
| Flotation Heat Tank Temperature         |        |       |       |       |      |   |   |     |     |     |     |             |
| Tank Discharge Pump Rate                |        |       |       |       |      |   |   |     |     |     |     |             |

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\*\*report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.

Department Condition: Shift Start-(Good/Fair/Poor); Shift End-(Good/Fair/Poor)

Time Hair Vacuum System Started

# of Paddles Removed from Hydrolizer

# of Times Hydrolizer Plugged & Blown Down

Hair Silo Beginning Level

Time Hair Received from Kill Floor  
Time Hair Finished from Kill Floor  
Time Hydrolizer Feeder Shut Off  
Final Time Hair Cooker Discharged  
Hair Silo Ending Level

OK  
5:20  
5:15  
5:15  
OK

LOGANSPOUT HAIR HYDROLIZER FLOTATION CELL LOGSHEET

Operator: [Signature]  
Date and Shift: 11-1-95 A

| DESCRIPTION                             | TARGET | 8:00 | 9:00 | 10:00 | 11:00 | 12:00 | 1:00 | 2:00 | E | :00 | :00 | :00 |
|-----------------------------------------|--------|------|------|-------|-------|-------|------|------|---|-----|-----|-----|
| Bsmt Hair Collection Bin Status         |        | OK   | OK   | OK    | OK    | OK    | OK   | OK   |   |     |     |     |
| Hair Vacuum Blower Motor Load           |        | 20   | 0    | 0     | 0     | 0     | 0    | 0    |   |     |     |     |
| # of Minutes Feed Screw was Reversed    |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   |   |     |     |     |
| Hydrolizer Reg. Internal Steam Pressure |        | 90   | 90   | 90    | 90    | 90    | 90   | 90   |   |     |     |     |
| Hydrolizer Reg. Jacket Steam Pressure   |        | 10   | 8    | 10    | 8     | 10    | 10   | 10   |   |     |     |     |
| Hydrolizer Feeder Screw Motor Load      |        | 106  | 106  | 119   | 108   | 108   | 108  | 115  |   |     |     |     |
| Hydrolizer Feed Temperature             |        | NA   | NA   | NA    | NA    | NA    | NA   | NA   |   |     |     |     |
| Hydrolizer Main Shaft Motor Load        |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   |   |     |     |     |
| Hydrolizer Discharge Pressure           |        | 225  | 225  | 225   | 225   | 225   | 225  | 225  |   |     |     |     |
| Hydrolizer Condensate Temperature       |        | 600  | 600  | 600   | 600   | 600   | 600  | 600  |   |     |     |     |
| Hydrolized Hair Sample Quality          |        | 90   | 88   | 88    | 89    | 88    | 88   | 88   |   |     |     |     |
| Hair Cooker Jacket Reg. Steam Pressure  |        | 195  | 195  | 195   | 195   | 195   | 195  | 195  |   |     |     |     |
| Hair Cooker Condensate Temperature      |        | NA   | NA   | NA    | NA    | NA    | NA   | NA   |   |     |     |     |
| Hair Cooker Motor Load                  |        | NA   | NA   | NA    | NA    | NA    | NA   | NA   |   |     |     |     |
| Hair Cooker Discharge Time              |        | NA   | NA   | NA    | NA    | NA    | NA   | NA   |   |     |     |     |
| East Flotation Cell Condition           |        | OK   | Full | Full  | Full  | Full  | Full | Full |   |     |     |     |
| # of Minutes East Skimmer Arm Running   |        | 3:40 | 3:40 | 3:45  | 3:40  | 3:45  | 3:45 | 3:45 |   |     |     |     |
| East Recycle Pump Discharge Pressure    |        | 50   | 45   | 45    | 45    | 45    | 45   | 45   |   |     |     |     |
| East Air Injection Air Flow             |        | 45   | 45   | 45    | 45    | 45    | 45   | 45   |   |     |     |     |
| East Air Mix Tank Inlet Pressure        |        | 90   | 90   | 90    | 90    | 90    | 90   | 90   |   |     |     |     |
| East Air Mix Tank Outlet Pressure       |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   |   |     |     |     |
| West Flotation Cell Condition           |        | OK   | Full | Full  | Full  | Full  | Full | Full |   |     |     |     |
| # of Minutes West Skimmer Arm Running   |        | 3:40 | 3:40 | 3:45  | 3:40  | 3:45  | 3:45 | 3:45 |   |     |     |     |
| West Recycle Pump Discharge Pressure    |        | 50   | 45   | 45    | 45    | 45    | 45   | 45   |   |     |     |     |
| West Air Injection Air Flow             |        | 45   | 45   | 45    | 45    | 45    | 45   | 45   |   |     |     |     |
| West Air Mix Tank Inlet Pressure        |        | 90   | 90   | 90    | 90    | 90    | 90   | 90   |   |     |     |     |
| West Air Mix Tank Outlet Pressure       |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   |   |     |     |     |
| Flotation Heat Tank Level               |        | NA   | NA   | NA    | NA    | NA    | NA   | NA   |   |     |     |     |
| Flotation Heat Tank Temperature         |        | NA   | NA   | NA    | NA    | NA    | NA   | NA   |   |     |     |     |
| Tank Discharge Pump Rate                |        | NA   | NA   | NA    | NA    | NA    | NA   | NA   |   |     |     |     |

\*record all mechanical downtime on the back of this form. Include equipment name, time down, time back operational, reason for downtime and end of shift status.

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Department Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

Time Hair Vacuum System Started

# of Paddles Removed from Hydrolizer

# of Times Hydrolizer Plugged & Blown Down

Hair Silo Beginning Level

Time Hair Received from Kill Floor

Time Hair Finished from Kill Floor

Time Hydrolizer Feeder Shut Off

Final Time Hair Cooker Discharged

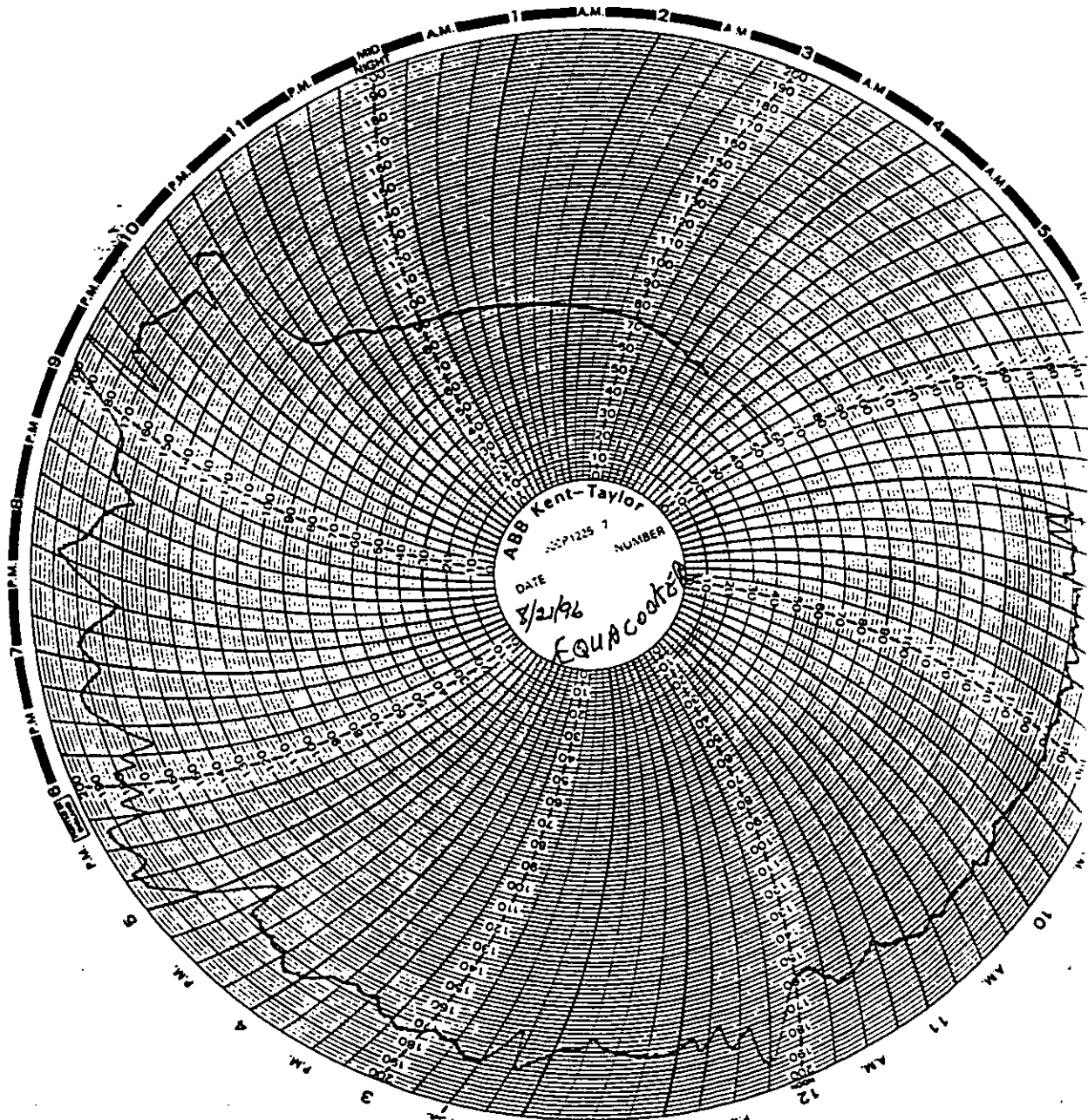
Hair Silo Ending Level

|      |
|------|
| 7:20 |
|      |
|      |
|      |

OK







Pork Inedible - Steam  
Logansport Inedible VOC Test

Tested August 22, 1996 at Logansport, IN on Dupps 1800 Cooker

|         |       |
|---------|-------|
| Test #1 | 1.300 |
| Test #2 | 0.900 |
| Test #3 | 2.200 |
|         | 1.467 |

|                            |       |
|----------------------------|-------|
| Head Kill                  | 6324  |
| Inedible Opeation Hours    | 14    |
| Inedible Crax Yield lbs/hd | 14.94 |

|                           |         |         |
|---------------------------|---------|---------|
|                           | lbs/hr  | tons/hr |
| Inedible Processed lbs/hr | 6748.61 | 3.37    |

|                        |       |
|------------------------|-------|
| Emission Rate (lb/ton) | 0.435 |
|------------------------|-------|

Pork Hair Hydrolizer - Steam  
Logansport Hair Hydrolizer VOC Test

Tested on September 21, 1996 at Logansport, IN on Anco Hydrolizer

Test #1 0.107

Test #2

Test #3

0.107

Head Kill 6121

Hydrolizer Opeation Hours 8

Hair Yield lbs/hd 0.7

|                       | lbs/hr | tons/hr |
|-----------------------|--------|---------|
| Hair Processed lbs/hr | 535.59 | 0.27    |

Emission Rate (lb/ton) 0.400

Pork Blood - Natural Gas  
Logansport Blood VOC Test

Tested August 20, 1996 at Logansport, IN on Dupps Ring Dryer

|         |       |
|---------|-------|
| Test #1 | 0.223 |
| Test #2 | 0.120 |
| Test #3 | 0.072 |
|         | 0.138 |

|                       |      |
|-----------------------|------|
| Head Kill             | 5968 |
| Blood Operation Hours | 10   |
| Blood Yield lbs/hd    | 1.33 |

|                        |        |         |
|------------------------|--------|---------|
|                        | lbs/hr | tons/hr |
| Blood Processed lbs/hr | 793.74 | 0.40    |

|                        |       |
|------------------------|-------|
| Emission Rate (lb/ton) | 0.328 |
|------------------------|-------|

|                         |          |
|-------------------------|----------|
| Heat Capacity MMBtu/hr  | 3        |
| Emission Factor VOC- NG | 2.78E-06 |

|                         |          |
|-------------------------|----------|
| VOC emission from Comb  | 0.00834  |
| VOC emission from blood | 0.129993 |

**APPENDIX B**

**PROCESS DATA**









Operator William R. Spiller  
 Date and Shift 8/20/96 (A)

# LOGANSPOUT EQUACOOKER OPERATING LOGSHEET

| DESCRIPTION                               | TARGET | 9:00  | 10:00 | 11:00 | 12:00 | 1:00  | 2:00  | 3:00  | 4:00  | 5:00  |
|-------------------------------------------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Raw Material Bin Level                    |        | A     | 5/50  | 3/51  | 1/3   | 1/4   | 1/4   | 1/4   | 1/4   | 1/4   |
| Raw Feed #8 VFD Speed                     |        | NA    | NA    | NA    | NA    | NA    | NA    | NA    | NA    | NA    |
| Hogger Grinder Motor Load                 |        | NA    | NA    | NA    | NA    | NA    | NA    | NA    | NA    | NA    |
| Cooker Steam P.S.I. (after Control Valve) | 267.4  | 267.4 | 267.4 | 267.4 | 267.4 | 267.4 | 267.4 | 267.4 | 267.4 | 267.4 |
| Equacooker Product Temperature            | 270.0  | 270.0 | 270.0 | 270.0 | 270.0 | 270.0 | 270.0 | 270.0 | 270.0 | 270.0 |
| Cooker Heat Exch Tailwater Temp           |        |       |       |       |       |       |       |       |       |       |
| Cooker Condensate Temp(after trap)        |        |       |       |       |       |       |       |       |       |       |
| Cooker Condensate PSI(after trap)         |        |       |       |       |       |       |       |       |       |       |
| Vapor Removal Rate/Bucket Test in sec.    |        |       |       |       |       |       |       |       |       |       |
| Equacooker Level                          |        | 1/3   | 1/3   | 1/2   | 1/2   | 1/2   | 1/2   | 1/2   | 1/2   | 1/2   |
| Control Wheel VFD Speed                   |        | 690   | 1790  | 1900  | 1946  | 2034  | 2043  | 2043  | 2043  | 2043  |
| Drainor/Overpressor Screw VFD Speed       |        |       |       |       |       |       |       |       |       |       |
| South Pressor Screw VFD Speed             |        | 70    | 75    | 75    | 76    | 60    | 60    | 50    | 50    | 50    |
| South Pressor Mainshaft Motor Load        |        | 3409  | 3394  | 3985  | 4977  | 4979  | 4979  | 4979  | 4979  | 4979  |
| South Pressor Crax Quality                |        | Good  | Good  | Good  | Good  | Good  | Good  | Good  | Good  | Good  |
| North Pressor Screw VFD Speed             |        |       |       |       |       |       |       |       |       |       |
| North Pressor Mainshaft Motor Load        |        |       |       |       |       |       |       |       |       |       |
| North Pressor Crax Quality                |        |       |       |       |       |       |       |       |       |       |
| Crax Surge Bin Level                      |        | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |
| Crax Grinder Motor Load                   |        | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |
| Sharples Centrifuge Motor Load            |        | NA    | NA    | NA    | NA    | NA    | NA    | NA    | NA    | NA    |
| East Grease Storage Tank Level            |        | NA    | NA    | NA    | NA    | NA    | NA    | NA    | NA    | NA    |
| West Grease Storage Tank Level            |        | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |

1250 AM  
 Down to  
 263.7 w.s.  
 1257 AM  
 up to 265.0  
 w.s.  
 10 min,  
 out  
 0+  
 Range

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\*\*report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.

Department Condition: Shift Start (Good Fair Poor); Shift End (Good Fair Poor)

Time Electromagnet Checked 6:30

South Pressor Choke Pressure 630

North Pressor Choke Pressure 630

South Pressor Fines Pump Status 630

North Pressor Fines Pump Status 630

Time Equacooker Jacket Steam was turned on 6:30

Time Equacooker Jacket Steam was turned off 6:30

⊗ Shut Down 9:30 p.m. ⊗

LOGANSPOUT EQUACOOKER OPERATING LOGSHEET

| DESCRIPTION                               | TIME  |       |       |       |       |       |       |       |       |       |       |       |
|-------------------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|                                           | 7:00  | 3:00  | 4:00  | 5:00  | 6:00  | 7:00  | 8:00  | 9:00  | 10:00 | 11:00 | 12:00 | 1:00  |
| Raw Material Bin Level                    | 14    | 14    | 14    | 14    | 14    | 14    | 14    | 14    | 14    | 14    | 14    | 14    |
| Raw Feed #B VFD Speed                     | 31.0  | 31.0  | 33.0  | 33.0  | 33.0  | 34.0  | 34.0  | 34.0  | 34.0  | 34.0  | 34.0  | 34.0  |
| Hogger Grinder Motor Load                 | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |
| Cooker Steam P.S.I. (after Control Valve) | 220   | 220   | 220   | 220   | 220   | 220   | 220   | 220   | 220   | 220   | 220   | 220   |
| Equacooker Product Temperature            | 116   | 116   | 112   | 112   | 111   | 110   | 111   | 111   | 110   | 110   | 110   | 110   |
| Cooker Heat Exch Tailwater Temp           | 16    | 14    | 26    | 14    | 15    | 8     | 7     | 7     | 8     | 7     | 7     | 7     |
| Cooker Condensate Temp(after trap)        | 20.28 | 19.71 | 25.68 | 27.63 | 18.63 | 18.21 | 20.05 | 20.05 | 18.21 | 20.05 | 20.05 | 20.05 |
| Cooker Condensate PSI(after trap)         | 1/2   | 1/2   | 1/2   | 1/3   | 1/3   | 1/3   | 1/3   | 1/3   | 1/3   | 1/3   | 1/3   | 1/3   |
| Vapor Removal Rate/Bucket Test in sec.    | 220   | 24.5  | 24.5  | 27.1  | 27.1  | 27.1  | 27.1  | 27.1  | 27.1  | 27.1  | 27.1  | 27.1  |
| Equacooker Level                          | 20.6  | 20.6  | 20.6  | 20.6  | 20.6  | 20.6  | 20.6  | 20.6  | 20.6  | 20.6  | 20.6  | 20.6  |
| Control Wheel VFD Speed                   | 50.0  | 38.0  | 38.0  | 41.0  | 41.0  | 41.0  | 41.0  | 41.0  | 41.0  | 41.0  | 41.0  | 41.0  |
| Drainor/Overpressor Screw VFD Speed       | 45/55 | 45/55 | 45/55 | 45/55 | 45/55 | 45/55 | 45/55 | 45/55 | 45/55 | 45/55 | 45/55 | 45/55 |
| South Pressor Screw VFD Speed             | SAIR  | SAIR  | SAIR  | SAIR  | SAIR  | SAIR  | SAIR  | SAIR  | SAIR  | SAIR  | SAIR  | SAIR  |
| South Pressor Mainshaft Motor Load        | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |
| South Pressor Crax Quality                | 13    | 13    | 14    | 14    | 14    | 14    | 14    | 14    | 14    | 14    | 14    | 14    |
| North Pressor Screw VFD Speed             | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |
| North Pressor Mainshaft Motor Load        | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |
| North Pressor Crax Quality                | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |
| Crax Surge Bin Level                      | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |
| Crax Grinder Motor Load                   | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |
| Sharples Centrifuge Motor Load            | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |
| East Grease Storage Tank Level            | 13    | 13    | 14    | 14    | 14    | 14    | 14    | 14    | 14    | 14    | 14    | 14    |
| West Grease Storage Tank Level            | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    | OK    |

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Department Condition: Shift Start (Good) Fair Poor); Shift End (Good Fair Poor)

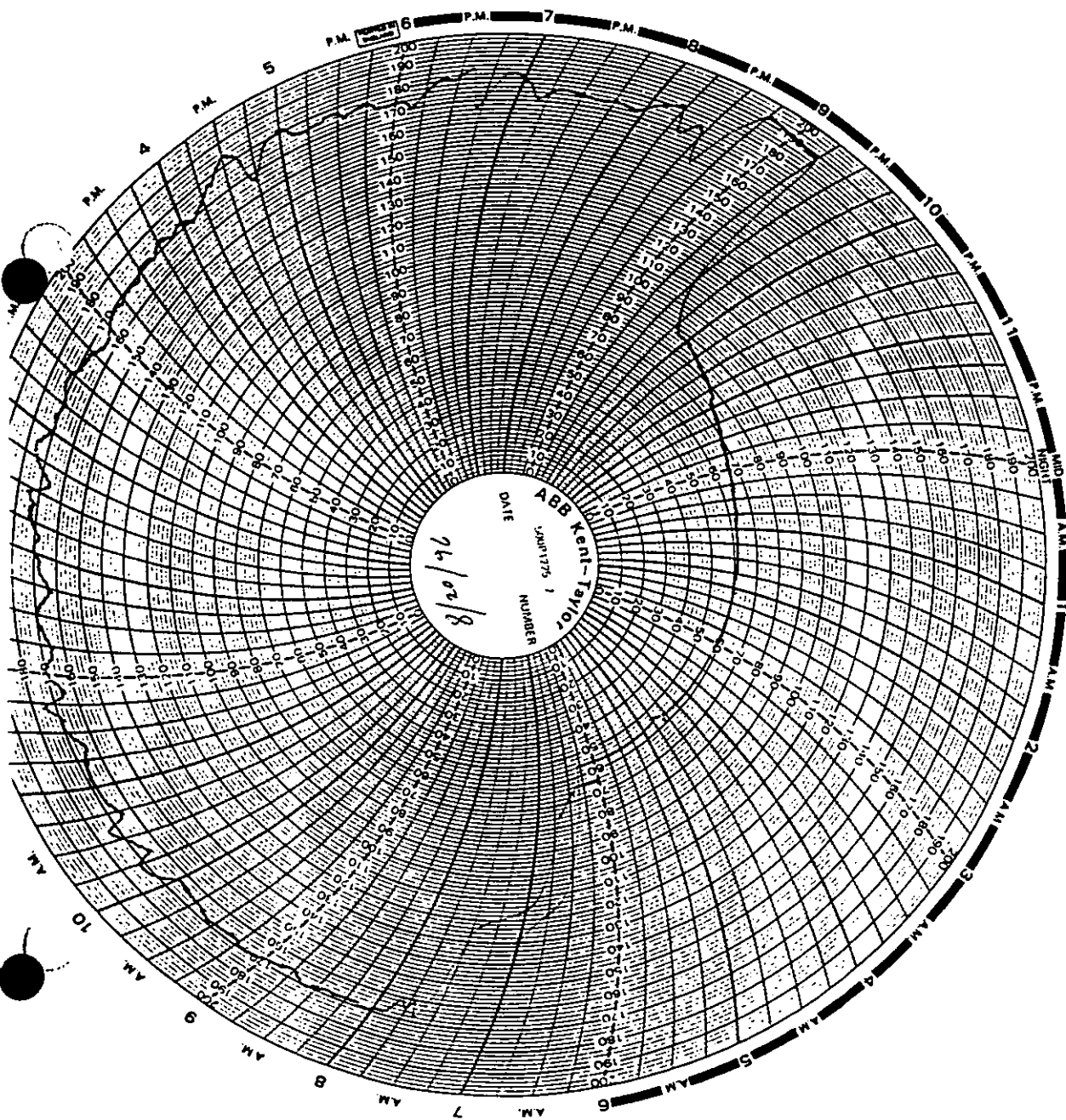
Time Electromagnet Checked 2:20 pm

Time Equacooker Jacket Steam was turned on

South Pressor Choke Pressure OK  
North Pressor Choke Pressure OK  
South Pressor Fines Pump Status OK  
North Pressor Fines Pump Status OK

Time Equacooker Jacket Steam was turned off 9:50

# Temperature Recorder for Wet Cooker.





# LOGANSPOUT EQUACOOKER OPERATING LOGSHEET

Operator Jim M012 / JMS  
 Date and Shift 08-21-96 13:54-34

| DESCRIPTION                               | TARGET | 2:00    | 3:00    | 4:00    | 5:00    | 6:00    | 7:00    | 8:00    | 9:00    | 10:00   |
|-------------------------------------------|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| Raw Material Bin Level                    |        | 1/3     | 1/2     | 1/4     | 1/4     | 1/4     | 1/4     | 1/4     | 1/4     | 1/4     |
| Raw Feed #8 VFD Speed                     |        | 33.0    | 33.0    | 33.0    | 33.0    | 33.0    | 33.0    | 33.0    | 33.0    | 33.0    |
| Hogger Grinder Motor Load                 |        | OK      | OK      | OK      | OK      | OK      | OK      | OK      | OK      | OK      |
| Cooker Steam P.S.I. (after Control Valve) |        |         |         |         |         |         |         |         |         |         |
| Equacooker Product Temperature            |        | 271/270 | 265/270 | 265/270 | 265/270 | 265/270 | 265/270 | 265/270 | 265/270 | 265/270 |
| Cooker Heat Exch Tailwater Temp           |        |         |         |         |         |         |         |         |         |         |
| Cooker Condensate Temp(after trap)        |        | 110     | 108     | 110     | 111     | 109     | 112     | 115     | 118     | 110     |
| Cooker Condensate PSI(after trap)         |        | 110     | 110     | 110     | 110     | 110     | 110     | 110     | 110     | 110     |
| Vapor Removal Rate/Bucket Test in sec     |        | 110     | 110     | 110     | 110     | 110     | 110     | 110     | 110     | 110     |
| Equacooker Level                          |        | 1/4     | 1/3     | 1/3     | 1/3     | 1/3     | 1/4     | 1/4     | 1/4     | 1/4     |
| Control Wheel VFD Speed                   |        | 22.0    | 22.0    | 22.0    | 22.0    | 21.5    | 24.5    | 22.5    | 22.5    | 21.5    |
| Drainor/Overpressor Screw VFD Speed       |        |         |         |         |         |         |         |         |         |         |
| South Pressor Screw VFD Speed             |        | 40.0    | 40.0    | 40.0    | 40.0    | 39.0    | 38.0    | 38.0    | 38.0    | 38.0    |
| South Pressor Mainshaft Motor Load        |        | 50/75   | 50/75   | 45/50   | 45/50   | 45/50   | 45/50   | 45/50   | 45/50   | 45/50   |
| South Pressor Crax Quality                |        | OK      | OK      | OK      | OK      | OK      | OK      | OK      | OK      | OK      |
| North Pressor Screw VFD Speed             |        |         |         |         |         |         |         |         |         |         |
| North Pressor Mainshaft Motor Load        |        |         |         |         |         |         |         |         |         |         |
| North Pressor Crax Quality                |        |         |         |         |         |         |         |         |         |         |
| Crax Surge Bin Level                      |        | OK      | OK      | OK      | OK      | OK      | OK      | OK      | OK      | OK      |
| Crax Grinder Motor Load                   |        | OK      | OK      | OK      | OK      | OK      | OK      | OK      | OK      | OK      |
| Sharples Centrifuge Motor Load            |        | 13      | 13      | 13      | 13      | 13      | 14      | 13      | 13      | 13      |
| East Grease Storage Tank Level            |        |         |         |         |         |         |         |         |         |         |
| West Grease Storage Tank Level            |        |         |         |         |         |         |         |         |         |         |

Shift down 22:45 mark

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Department Condition: Shift Start- (Good Fair Poor); Shift End- (Good Fair Poor)

Time Electromagnet Checked 2:20 PM  
 South Pressor Choke Pressure OK  
 North Pressor Choke Pressure OK  
 South Pressor Fines Pump Status OK  
 North Pressor Fines Pump Status OK

Time Equacooker Jacket Steam was turned on 2:22 PM  
 Time Equacooker Jacket Steam was turned off 2:22 PM

Operator: *Steve R. Spruick*  
 Date and Shift: *8/22/96* (A)

# LOGANSPOUT EQUACOOKER OPERATING LOGSHEET

Start 630  
 Start 745

1040 AM  
 264.3  
 1050  
 263.7  
 1100  
 266.9

| DESCRIPTION                               | TARGET | 8:00 | 9:00 | 10:00 | 11:00 | 12:00 | 1:00 | 2:00 | 3:00 | 4:00 | 5:00 | 6:00 | 7:00 | 8:00 |
|-------------------------------------------|--------|------|------|-------|-------|-------|------|------|------|------|------|------|------|------|
| Raw Material Bin Level                    |        | A    | A    | A     | 1/3   | 1/3   | 1/3  |      |      |      |      |      |      |      |
| Raw Feed #8 VFD Speed                     |        | 3148 | 3148 | 3148  | 3148  | 3148  | 3148 |      |      |      |      |      |      |      |
| Hogger Grinder Motor Load                 |        | NA   | NA   | NA    | NA    | NA    | NA   |      |      |      |      |      |      |      |
| Cooker Steam P.S.I. (after Control Valve) |        | 273  | 273  | 273   | 273   | 273   | 273  |      |      |      |      |      |      |      |
| Equacooker Product Temperature            |        | 272  | 272  | 272   | 272   | 272   | 272  |      |      |      |      |      |      |      |
| Cooker Heat Exch Tailwater Temp           |        |      |      |       |       |       |      |      |      |      |      |      |      |      |
| Cooker Condensate Temp(after trap)        |        |      |      |       |       |       |      |      |      |      |      |      |      |      |
| Cooker Condensate PSI(after trap)         |        |      |      |       |       |       |      |      |      |      |      |      |      |      |
| Vapor Removal Rate/Bucket Test in sec.    |        |      |      |       |       |       |      |      |      |      |      |      |      |      |
| Equacooker Level                          |        | 1/4  | 1/4  | 1/4   | 1/2   | 1/2   | 1/3  |      |      |      |      |      |      |      |
| Control Wheel VFD Speed                   |        | 1631 | 1631 | 1950  | 2070  | 2199  | 2260 |      |      |      |      |      |      |      |
| Drainor/Overpressor Screw VFD Speed       |        |      |      |       |       |       |      |      |      |      |      |      |      |      |
| South Pressor Screw VFD Speed             |        | 2886 | 2886 | 4210  | 4193  | 4193  | 4194 |      |      |      |      |      |      |      |
| South Pressor Mainshaft Motor Load        |        | 70   | 70   | 60    | 60    | 60    | 65   |      |      |      |      |      |      |      |
| South Pressor Crax Quality                |        | Good | Good | Good  | Good  | Good  | Good |      |      |      |      |      |      |      |
| North Pressor Screw VFD Speed             |        |      |      |       |       |       |      |      |      |      |      |      |      |      |
| North Pressor Mainshaft Motor Load        |        |      |      |       |       |       |      |      |      |      |      |      |      |      |
| North Pressor Crax Quality                |        |      |      |       |       |       |      |      |      |      |      |      |      |      |
| Crax Surge Bin Level                      |        | OK   | OK   | OK    | OK    | OK    | OK   |      |      |      |      |      |      |      |
| Crax Grinder Motor Load                   |        | NA   | NA   | NA    | NA    | NA    | NA   |      |      |      |      |      |      |      |
| Sharples Centrifuge Motor Load            |        | NA   | NA   | NA    | NA    | NA    | NA   |      |      |      |      |      |      |      |
| East Grease Storage Tank Level            |        | OK   | OK   | OK    | OK    | OK    | OK   |      |      |      |      |      |      |      |
| West Grease Storage Tank Level            |        | OK   | OK   | OK    | OK    | OK    | OK   |      |      |      |      |      |      |      |

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Department Condition: Shift Start (Good) Fair Poor; Shift End (Good) Fair Poor

Time Equacooker Jacket Steam was turned on 630  
 Time Equacooker Jacket Steam was turned off 745

Time Electromagnet Checked  
 South Pressor Choke Pressure  
 North Pressor Choke Pressure  
 South Pressor Fines Pump Status  
 North Pressor Fines Pump Status

Operator Name Deborah  
 Date and Shift 8-20-96 A Shift

# LOGANSPORT BLOOD DRYING UNIT OPERATING LOGSHEET

LOBLOG.WK4

| DESCRIPTION                             | TARGET  | 06:00 | 07:00 | 08:00 | 09:00 | 10:00 | 11:00 | 12:00 | 01:00 | 02:00 | 03:00 | 04:00 | 05:00 |
|-----------------------------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Furnace Exhaust Temperature             | <700 F  |       |       |       |       | 200   | 200   | 190   | 191   | 190   |       |       |       |
| Ring Dryer Disch Temp Set-point         | 200 F   |       |       |       |       | 191   | 191   | 191   | 191   | 191   |       |       |       |
| Ring Dryer Disch Product Temperature    | actual  |       |       |       |       | 190   | 190   | 190   | 192   | 189   |       |       |       |
| Centrifuge Feed Pump Speed              | 18.5 Hz |       |       |       |       | 24.5  | 24.5  | 24.5  | 24.5  | 24.5  |       |       |       |
| Coagulator Temperature Setpoint         |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Coagulator Product Temperature          |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Centrifuge Motor Load Amperes           | <15 A   |       |       |       |       | 10    | 10    | 10    | 10    | 10    |       |       |       |
| South Raw Blood Surge Tank Level        | MIN     |       |       |       |       | 0     | 0     | 0     | 0     | 0     |       |       |       |
| North Raw Blood Surge Tank Level        | MIN     |       |       |       |       | 0     | 0     | 0     | 0     | 0     |       |       |       |
| Raw Blood Feed Tank Level               | 3/4     |       |       |       |       | 1/3   | 1/3   | 1/3   | 1/2   | 1/2   |       |       |       |
| Feed Tank Agitator                      | ON      |       |       |       |       | ON    | ON    | ON    | ON    | ON    |       |       |       |
| Main Steam Incoming Pressure            | 125psi  |       |       |       |       | 115   | 115   | 115   | 115   | 115   |       |       |       |
| After Regulator Steam Pressure          | 40psi   |       |       |       |       | 45    | 45    | 45    | 45    | 45    |       |       |       |
| Coagulator Main Steam Valve Pressure    | 30psi   |       |       |       |       | 25    | 25    | 25    | 25    | 25    |       |       |       |
| Pre-Coagulation Injection Water Rate    | 2gpm    |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Minutes Main Blood Valve Open           | actual  |       |       |       |       | 55    | 55    | 55    | 55    | 55    |       |       |       |
| Centrifuge Feed Pump Disch Pressure     | <20psi  |       |       |       |       |       |       |       |       |       |       |       |       |
| Coagulator North Injector Valve Setting | 1-1/4   |       |       |       |       | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 |       |       |       |
| Coagulator South Injector Valve Setting | 3/4     |       |       |       |       | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   |       |       |       |
| Centrifuge Injection Water Rate         | 8gpm    |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Centrifuge Feed Temperature             |         |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| Centrifuge Stickwater Sample            |         |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| Centrifuged Blood Sample                |         |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| Ring Dryer percent recycle              | MIN     |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Air Lock and Cyclone status             | CLEAR   |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| Cyclone Outlet Pressure                 | 15"     |       |       |       |       | 17.5  | 17.5  | 17.5  | 17.5  | 17.5  |       |       |       |
| Dried Blood Moisture                    | 10%     |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| Dried Blood Blower Discharge Pressure   |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |

Record all mechanical downtimes on the back of this form. Include equipment name, time down, time back operational, reason for downtime and end of shift status.  
 Report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.  
 Department/Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

# LOGANSPORT BLOOD DRYING CO. DATING LOGSHEET

LOGSHEET WK4

Operator Name

Date and Shift

8-20-96 B-Shift 3:00 4:00 5:00 6:00 7:00 8:00 9:00

| DESCRIPTION                             | TARGET  | 06:00 | 07:00 | 08:00 | 09:00 | 10:00 | 11:00 | 12:00 | 01:00 | 02:00 | 03:00 | 04:00 | 05:00 |
|-----------------------------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Furnace Exhaust Temperature             | <700 F  | 140   | 190   | 195   | 193   | 193   |       |       |       |       |       |       |       |
| Ring Dryer Disch Temp Set-point         | 200 F   | 191   | 191   | 191   | 191   | 191   |       |       |       |       |       |       |       |
| Ring Dryer Disch Product Temperature    | actual  | 193   | 190   | 191   | 192   | 192   |       |       |       |       |       |       |       |
| entrifuge Feed Pump Speed               | 18.5 Hz | 24.5  | 24.5  | 24.5  | 24.5  | 24.5  |       |       |       |       |       |       |       |
| Coagulator Temperature Setpoint         |         | -     | -     | -     | -     | -     |       |       |       |       |       |       |       |
| Coagulator Product Temperature          |         | -     | -     | -     | -     | -     |       |       |       |       |       |       |       |
| entrifuge Motor Load Amperes            | <15 A   | 10    | 10    | 10    | 10    | 10    |       |       |       |       |       |       |       |
| South Raw Blood Surge Tank Level        | MIN     | -     | -     | -     | -     | -     |       |       |       |       |       |       |       |
| North Raw Blood Surge Tank Level        | MIN     | -     | -     | -     | -     | -     |       |       |       |       |       |       |       |
| Raw Blood Feed Tank Level               | 3/4     | 1/2   | 1/2   | 1/2   | 1/2   | 1/2   |       |       |       |       |       |       |       |
| Feed Tank Agitator                      | ON      | ON    | ON    | ON    | ON    | ON    |       |       |       |       |       |       |       |
| Main Steam Incoming Pressure            | 125psi  | 120   | 120   | 125   | 120   | 125   |       |       |       |       |       |       |       |
| Header Regulator Steam Pressure         | 40psi   | 45    | 45    | 45    | 45    | 45    |       |       |       |       |       |       |       |
| Coagulator Main Steam Valve Pressure    | 30psi   | 22    | 25    | 25    | 25    | 25    |       |       |       |       |       |       |       |
| Re-Coagulation Injection Water Rate     | 2gpm    | -     | -     | -     | -     | -     |       |       |       |       |       |       |       |
| Inlet Main Blood Valve Open             | actual  | 55    | 55    | 55    | 55    | 55    |       |       |       |       |       |       |       |
| entrifuge Feed Pump Disch Pressure      | <20psi  | 10    | 20    | 12    | 3     | 12    |       |       |       |       |       |       |       |
| Coagulator North Injector Valve Setting | 1-1/4   | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 |       |       |       |       |       |       |       |
| Coagulator South Injector Valve Setting | 3/4     | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   |       |       |       |       |       |       |       |
| entrifuge Injection Water Rate          | 8gpm    | -     | -     | -     | -     | -     |       |       |       |       |       |       |       |
| entrifuge Feed Temperature              |         | OK    | OK    | OK    | OK    | OK    |       |       |       |       |       |       |       |
| entrifuge Stickwater Sample             |         | OK    | OK    | OK    | OK    | OK    |       |       |       |       |       |       |       |
| entrifuge Blood Sample                  |         | OK    | OK    | OK    | OK    | OK    |       |       |       |       |       |       |       |
| Ring Dryer percent recycle              | MIN     | -     | -     | -     | -     | -     |       |       |       |       |       |       |       |
| Filter Lock and Cyclone status          | CLEAR   | OK    | OK    | OK    | OK    | OK    |       |       |       |       |       |       |       |
| Cyclone Outlet Pressure                 | 15"     | 12.5  | 12.5  | 12.5  | 12.5  | 12.5  |       |       |       |       |       |       |       |
| Feed Blood Moisture                     | 10%     | 6.8   | 7.3   | 6.9   | 8     | 6.9   |       |       |       |       |       |       |       |
| Feed Blood Blower Discharge Pressure    |         |       |       |       |       |       |       |       |       |       |       |       |       |

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Report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.

Department-Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

Operator Name: John Bush

Date and Shift: 8-21-96 A Shift

# LOGANSPORT BLOOD DRYING & AGITATING LOGSHEET

LOGSHEET WK4

| DESCRIPTION                           | TARGET  | 06:00 | 07:00 | 08:00 | 09:00 | 10:00 | 11:00 | 12:00 | 01:00 | 02:00 | 03:00 | 04:00 | 05:00 |
|---------------------------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| urnace Exhaust Temperature            | <700 F  |       |       |       |       | 195   | 195   | 190   | 195   | 195   |       |       |       |
| ring Dryer Disch Temp Set-point       | 200 F   |       |       |       |       | 191   | 191   | 191   | 191   | 191   |       |       |       |
| ring Dryer Disch Product Temperature  | actual  |       |       |       |       | 198   | 198   | 199   | 190   | 190   |       |       |       |
| entrifuge Feed Pump Speed             | 18.5 Hz |       |       |       |       | 24.5  | 24.5  | 24.5  | 24.5  | 24.5  |       |       |       |
| agulator Temperature Setpoint         |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| agulator Product Temperature          |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| entrifuge Motor Load Amperes          | <15 A   |       |       |       |       | 10    | 10    | 10    | 10    | 10    |       |       |       |
| outh Raw Blood Surge Tank Level       | MIN     |       |       |       |       | 0     | 0     | 0     | 0     | 0     |       |       |       |
| orth Raw Blood Surge Tank Level       | MIN     |       |       |       |       | 0     | 0     | 0     | 0     | 0     |       |       |       |
| aw Blood Feed Tank Level              | 3/4     |       |       |       |       | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   |       |       |       |
| eed Tank Agitator                     | ON      |       |       |       |       | ON    | ON    | ON    | ON    | ON    |       |       |       |
| ain Steam Incoming Pressure           | 125psi  |       |       |       |       | 115   | 115   | 115   | 115   | 115   |       |       |       |
| fter Regulator Steam Pressure         | 40psi   |       |       |       |       | 45    | 45    | 45    | 45    | 45    |       |       |       |
| agulator Main Steam Valve Pressure    | 30psi   |       |       |       |       | 25    | 25    | 25    | 25    | 25    |       |       |       |
| re-Coagulation Injection Water Rate   | 2gpm    |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| inules Main Blood Valve Open          | actual  |       |       |       |       | Start | 55    | 55    | 55    | 55    |       |       |       |
| entrifuge Feed Pump Disch Pressure    | <20psi  |       |       |       |       | 10    | 10    | 10    | 10    | 10    |       |       |       |
| agulator North Injector Valve Setting | 1-1/4   |       |       |       |       | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 |       |       |       |
| agulator South Injector Valve Setting | 3/4     |       |       |       |       | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   |       |       |       |
| entrifuge Injection Water Rate        | 8gpm    |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| entrifuge Feed Temperature            |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| entrifuge Stickwater Sample           |         |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| entrifuged Blood Sample               |         |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| ing Dryer percent recycle             | MIN     |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| ir Lock and Cyclone status            | CLEAR   |       |       |       |       | OK    | OK    | OK    | OK    | OK    |       |       |       |
| yclone Outlet Pressure                | 15"     |       |       |       |       | 17.5  | 17.5  | 17.5  | 17.5  | 17.5  |       |       |       |
| ried Blood Moisture                   | 10%     |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |
| ried Blood Blower Discharge Pressure  |         |       |       |       |       | NA    | NA    | NA    | NA    | NA    |       |       |       |

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Department Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

Operator Name

Date and Shift

LOGANSPOUT BLOOD DRYING LOGSHEET

LOG LOGSHEET

| DESCRIPTION                             | TARGET  | 06:00 | 07:00 | 08:00 | 09:00 | 10:00 | 11:00 | 12:00 | 01:00 | 02:00 | 03:00 | 04:00 | 05:00 |
|-----------------------------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Furnace Exhaust Temperature             | <700 F  | 190   | 190   | 190   | 190   | 190   | 190   | 190   |       |       |       |       |       |
| Flng Dryer Disch Temp Set-point         | 200 F   | 191   | 191   | 191   | 191   | 191   | 191   | 191   |       |       |       |       |       |
| Flng Dryer Disch Product Temperature    | actual  | 191   | 191   | 191   | 191   | 191   | 191   | 191   |       |       |       |       |       |
| Centrifuge Feed Pump Speed              | 18.5 Hz | 24.5  | 24.5  | 24.5  | 24.5  | 24.5  | 24.5  | 24.5  |       |       |       |       |       |
| Coagulator Temperature Setpoint         |         |       |       |       |       |       |       |       |       |       |       |       |       |
| Coagulator Product Temperature          |         |       |       |       |       |       |       |       |       |       |       |       |       |
| Centrifuge Motor Load Amperes           | <15 A   | 20    | 10    | 10    | 10    | 10    | 10    | 10    |       |       |       |       |       |
| South Raw Blood Surge Tank Level        | MIN     |       |       |       |       |       |       |       |       |       |       |       |       |
| North Raw Blood Surge Tank Level        | MIN     |       |       |       |       |       |       |       |       |       |       |       |       |
| Raw Blood Feed Tank Level               | 3/4     | 3/4   | Full  | Full  | Full  | Full  | Full  | Full  |       |       |       |       |       |
| Feed Tank Agitator                      | ON      | ON    | ON    | ON    | ON    | ON    | ON    | ON    |       |       |       |       |       |
| Main Steam Incoming Pressure            | 125psi  | 120   | 120   | 120   | 120   | 120   | 120   | 120   |       |       |       |       |       |
| After Regulator Steam Pressure          | 40psi   | 45    | 45    | 45    | 45    | 45    | 45    | 45    |       |       |       |       |       |
| Coagulator Main Steam Valve Pressure    | 30psi   | 27    | 27    | 27    | 27    | 27    | 27    | 27    |       |       |       |       |       |
| Pre-Coagulation Injection Water Rate    | 2gpm    |       |       |       |       |       |       |       |       |       |       |       |       |
| Minutes Main Blood Valve Open           | actual  | 55    | 55    | 55    | 55    | 55    | 55    | 55    |       |       |       |       |       |
| Centrifuge Feed Pump Disch Pressure     | <20psi  | 12    | 12    | 12    | 12    | 12    | 12    | 12    |       |       |       |       |       |
| Coagulator North Injector Valve Setting | 1-1/4   | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 | 1-1/4 |       |       |       |       |       |
| Coagulator South Injector Valve Setting | 3/4     | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   | 3/4   |       |       |       |       |       |
| Centrifuge Injection Water Rate         | 8gpm    |       |       |       |       |       |       |       |       |       |       |       |       |
| Centrifuge Feed Temperature             |         |       |       |       |       |       |       |       |       |       |       |       |       |
| Centrifuge Stickwater Sample            |         | OK    | OK    | OK    | OK    | OK    | OK    | OK    |       |       |       |       |       |
| Centrifuged Blood Sample                |         | OK    | OK    | OK    | OK    | OK    | OK    | OK    |       |       |       |       |       |
| Ring Dryer percent recycle              | MIN     |       |       |       |       |       |       |       |       |       |       |       |       |
| Air Lock and Cyclone status             | CLEAR   | OK    | OK    | OK    | OK    | OK    | OK    | OK    |       |       |       |       |       |
| Cyclone Outlet Pressure                 | 15"     | 17.5  | 17.5  | 17.5  | 17.5  | 17.5  | 17.5  | 17.5  |       |       |       |       |       |
| Dried Blood Moisture                    | 10%     | 10    | 10    | 10    | 10    | 10    | 10    | 10    |       |       |       |       |       |
| Dried Blood Blower Discharge Pressure   |         |       |       |       |       |       |       |       |       |       |       |       |       |

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Department-Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

Operator Name

Date and Shift

76000  
8-22-98

## LOGANSPORT BLOOD DRYING OPERATING LOGSHEET

LGBLLOC.WK4

| DESCRIPTION                             | TARGET  | 06:00 | 07:00 | 08:00 | 09:00 | 10:00 | 11:00 | 12:00 | 01:00 | 02:00 | 03:00 | 04:00 | 05:00 |
|-----------------------------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Furnace Exhaust Temperature             | <700 F  |       |       |       |       | 190   | 190   | 190   |       |       |       |       |       |
| Ring Dryer Disch Temp Set-point         | 200 F   |       |       |       |       | 191   | 191   | 191   |       |       |       |       |       |
| Ring Dryer Disch Product Temperature    | actual  |       |       |       |       | 190   | 185   | 187   |       |       |       |       |       |
| Centrifuge Feed Pump Speed              | 18.5 Hz |       |       |       |       | 23.5  | 25.5  | 25.5  |       |       |       |       |       |
| Coagulator Temperature Setpoint         |         |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Coagulator Product Temperature          |         |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Centrifuge Motor Load Amperes           | <15 A   |       |       |       |       | 19    | 15    | 15    |       |       |       |       |       |
| South Raw Blood Surge Tank Level        | MIN     |       |       |       |       | NA    | 0     | 0     |       |       |       |       |       |
| North Raw Blood Surge Tank Level        | MIN     |       |       |       |       | 0     | 0     | 0     |       |       |       |       |       |
| Raw Blood Feed Tank Level               | 3/4     |       |       |       |       | 3/4   | 3/4   | 3/4   |       |       |       |       |       |
| Feed Tank Agitator                      | ON      |       |       |       |       | ON    | ON    | ON    |       |       |       |       |       |
| Main Steam Incoming Pressure            | 125psi  |       |       |       |       | 115   | 115   | 115   |       |       |       |       |       |
| Steam Regulator Steam Pressure          | 40psi   |       |       |       |       | 45    | 45    | 45    |       |       |       |       |       |
| Coagulator Main Steam Valve Pressure    | 30psi   |       |       |       |       | 25    | 25    | 25    |       |       |       |       |       |
| Pre-Coagulation Injection Water Rate    | 2gpm    |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Minutes Main Blood Valve Open           | actual  |       |       |       |       | Start | 55    | 55    |       |       |       |       |       |
| Centrifuge Feed Pump Disch Pressure     | <20psi  |       |       |       |       | 1-1/4 | 1-1/4 | 1-1/4 |       |       |       |       |       |
| Coagulator North Injector Valve Setting | 1-1/4   |       |       |       |       | 3/4   | 3/4   | 3/4   |       |       |       |       |       |
| Coagulator South Injector Valve Setting | 3/4     |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Centrifuge Injection Water Rate         | 8gpm    |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Centrifuge Feed Temperature             |         |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Centrifuge Stickwater Sample            |         |       |       |       |       | OK    | OK    | OK    |       |       |       |       |       |
| Centrifuged Blood Sample                |         |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Ring Dryer percent recycle              | MIN     |       |       |       |       | OK    | OK    | OK    |       |       |       |       |       |
| Dr Lock and Cyclone status              | CLEAR   |       |       |       |       | NA    | NA    | NA    |       |       |       |       |       |
| Cyclone Outlet Pressure                 | 15"     |       |       |       |       | OK    | OK    | OK    |       |       |       |       |       |
| Feed Blood Moisture                     | 10%     |       |       |       |       | 17.5  | 17.5  | 17.5  |       |       |       |       |       |
| Feed Blood Blower Discharge Pressure    |         |       |       |       |       | NA    | 6.6   | NA    |       |       |       |       |       |

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Report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.  
apartment Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

10-16 A

| DESCRIPTION                             | TARGET | 8:00 | 9:00 | 10:00 | 11:00 | 12:00 | 1:00 | 2:00 | E | :00 | :00 | :00 | :00 | BP000000 |
|-----------------------------------------|--------|------|------|-------|-------|-------|------|------|---|-----|-----|-----|-----|----------|
| Bsmr Hair Collection Bin Status         |        | OK   | OK   | OK    | OK    | OK    | OK   | OK   |   |     |     |     |     |          |
| Hair Vacuum Blower Motor Load           |        | 18   | 18   | 18    | 20    | 20    | 20   | 20   |   |     |     |     |     |          |
| # of Minutes Feed Screw was Reversed    |        | 0    | 0    | 0     | 0     | 0     | 0    | 0    |   |     |     |     |     |          |
| Hydrolizer Reg. Internal Steam Pressure |        | 30   | 50   | 50    | 50    | 50    | 50   | 50   |   |     |     |     |     |          |
| Hydrolizer Reg. Jacket Steam Pressure   |        | 90   | 90   | 90    | 90    | 90    | 90   | 90   |   |     |     |     |     |          |
| Hydrolizer Feeder Screw Motor Load      |        | 12   | 8    | 8     | 8     | 8     | 8    | 8    |   |     |     |     |     |          |
| Hydrolizer Feed Temperature             |        | 108  | 111  | 154   | 110   | 113   | 150  | 114  |   |     |     |     |     |          |
| Hydrolizer Main Shaft Motor Load        |        | NA   | NA   | NA    | NA    | NA    | NA   | NA   |   |     |     |     |     |          |
| Hydrolizer Discharge Pressure           |        | 50   | 47   | 50    | 49    | 48    | 50   | 49   |   |     |     |     |     |          |
| Hydrolizer Condensate Temperature       |        | 225  | 215  | 215   | 215   | 225   | 225  | 225  |   |     |     |     |     |          |
| Hydrolized Hair Sample Quality          |        | Good | Good | Good  | Good  | Good  | Good | Good |   |     |     |     |     |          |
| Hair Cooker Jacket Reg. Steam Pressure  |        | 89   | 85   | 85    | 85    | 84    | 84   | 80   |   |     |     |     |     |          |
| Hair Cooker Condensate Temperature      |        | 190  | 198  | 198   | 198   | 198   | 198  | 198  |   |     |     |     |     |          |
| Hair Cooker Motor Load                  |        | NA   | NA   | NA    | NA    | NA    | NA   | NA   |   |     |     |     |     |          |
| Hair Cooker Discharge Time              |        | ✓    | ✓    | ✓     | ✓     | ✓     | ✓    | ✓    |   |     |     |     |     |          |
| East Flotation Cell Condition           |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| # of Minutes East Skimmer Arm Running   |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| East Recycle Pump Discharge Pressure    |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| East Air Injection Air Flow             |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| East Air Mix Tank Inlet Pressure        |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| East Air Mix Tank Outlet Pressure       |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| West Flotation Cell Condition           |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| # of Minutes West Skimmer Arm Running   |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| West Recycle Pump Discharge Pressure    |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| West Air Injection Air Flow             |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| West Air Mix Tank Inlet Pressure        |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| West Air Mix Tank Outlet Pressure       |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| Flotation Heat Tank Level               |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| Flotation-Heat Tank Temperature         |        |      |      |       |       |       |      |      |   |     |     |     |     |          |
| Tank Discharge Pump Rate                |        |      |      |       |       |       |      |      |   |     |     |     |     |          |

\*Record all mechanical downtime on the back of this form. Include equipment name, time down, time back operational, reason for downtime and end of shift status.

\*\*Report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.

Department Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

Time Hair Vacuum System Started  
# of Paddles Removed from Hydrolizer  
# of Times Hydrolizer Plugged & Blown Down

Time Hair Received from Kill Floor  
Time Hair Finished from Kill Floor  
Time Hydrolizer Feeder Shut Off  
Final Time Hair Cooker Discharged  
Hair Silo Ending Level

6:30  
OK

Operator *David Richardson*  
Date and Shift *8-20-96 B-Shift*

LOGANSPOUT HAIR HYDROLIZER AND FLOTATION CELL LOGSHEET LGR-RLCO-1W4

| DESCRIPTION                             | TARGET | T     | 6:00  | I | M | E | BP000000gm |
|-----------------------------------------|--------|-------|-------|---|---|---|------------|
| Bsmt Hair Collection Bin Status         | 3:00   | 4:00  | 5:00  |   |   |   |            |
| Hair Vacuum Blower Motor Load           | 75%    | 65%   | 0%    |   |   |   |            |
| # of Minutes Feed Screw was Reversed    | 180    | 18    | 0     |   |   |   |            |
| Hydrolizer Reg. Internal Steam Pressure | 0      | 48.4  | 48.4  |   |   |   |            |
| Hydrolizer Reg. Jacket Steam Pressure   | 48.3   | 48.4  | 48.4  |   |   |   |            |
| Hydrolizer Feeder Screw Motor Load      | 84.6   | 84.6  | 84.6  |   |   |   |            |
| Hydrolizer Feed Temperature             | 4      | 110   | 125   |   |   |   |            |
| Hydrolizer Main Shaft Motor Load        | 110    | 125   | 119   |   |   |   |            |
| Hydrolizer Discharge Pressure           | N/A    | N/A   | N/A   |   |   |   |            |
| Hydrolizer Condensate Temperature       | 48.4   | 48.4  | 48.4  |   |   |   |            |
| Hydrolized Hair Sample Quality          | 230.5  | 230.4 | 230.4 |   |   |   |            |
| Hair Cooker Jacket Reg. Steam Pressure  | 230.5  | 230.4 | 230.4 |   |   |   |            |
| Hair Cooker Condensate Temperature      | 15.5   | 15.4  | 15.4  |   |   |   |            |
| Hair Cooker Motor Load                  | 19.7   | 19.6  | 19.6  |   |   |   |            |
| Hair Cooker Discharge Time              | N/A    | N/A   | N/A   |   |   |   |            |
| East Flotation Cell Condition           | —      | —     | 5.15  |   |   |   |            |
| # of Minutes East Skimmer Arm Running   |        |       |       |   |   |   |            |
| East Recycle Pump Discharge Pressure    |        |       |       |   |   |   |            |
| East Air Injection Air Flow             |        |       |       |   |   |   |            |
| East Air Mix Tank Inlet Pressure        |        |       |       |   |   |   |            |
| East Air Mix Tank Outlet Pressure       |        |       |       |   |   |   |            |
| West Flotation Cell Condition           |        |       |       |   |   |   |            |
| # of Minutes West Skimmer Arm Running   |        |       |       |   |   |   |            |
| West Recycle Pump Discharge Pressure    |        |       |       |   |   |   |            |
| West Air Injection Air Flow             |        |       |       |   |   |   |            |
| West Air Mix Tank Inlet Pressure        |        |       |       |   |   |   |            |
| West Air Mix Tank Outlet Pressure       |        |       |       |   |   |   |            |
| Flotation Heat Tank Level               |        |       |       |   |   |   |            |
| Flotation Heat Tank Temperature         |        |       |       |   |   |   |            |
| Tank Discharge Pump Rate                |        |       |       |   |   |   |            |

\*record all mechanical downtime on the back of this form. Include equipment name, time down, time back operational, reason for downtime and end of shift status.

\*\*report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.

Department Condition: Shift Start-(Good/Fair/Poor); Shift End-(Good/Fair/Poor)

Time Hair Vacuum System Started  
# of Paddles Removed from Hydrolizer  
# of Times Hydrolizer Plugged & Blown Down

Time Hair Received from Kill Floor  
Time Hair Finished from Kill Floor  
Time Hydrolizer Feeder Shut Off  
Final Time Hair Cooker Discharged  
Hair Silo Ending Level

0.17  
5.10  
5.05  
5.15  
0.4

Hair Silo Beginning Level

# LOGANSPOUT HAIR HYDROLIZER FLOTATION CELL LOGSHEET

Operator: LOWAN SCHO  
Date and Shift: 3-21-95 A

| DESCRIPTION                             | TARGET | 8:00   | 9:00   | 10:00  | 11:00  | 12:00  | 1:00   | 2:00   | E | M | :00 | :00 | :00 | :00 |
|-----------------------------------------|--------|--------|--------|--------|--------|--------|--------|--------|---|---|-----|-----|-----|-----|
| Bsmt Hair Collection Bin Status         |        | OK     | OK     | OK     | OK     | OK     | OK     | OK     |   |   |     |     |     |     |
| Hair Vacuum Blower Motor Load           |        | 20     | 20     | 20     | 20     | 20     | 20     | 20     |   |   |     |     |     |     |
| # of Minutes Feed Screw was Reversed    |        | 0      | 0      | 0      | 0      | 0      | 0      | 0      |   |   |     |     |     |     |
| Hydrolizer Reg. Internal Steam Pressure |        | 50     | 50     | 50     | 50     | 50     | 50     | 50     |   |   |     |     |     |     |
| Hydrolizer Reg. Jacket Steam Pressure   |        | 90     | 90     | 90     | 90     | 90     | 90     | 90     |   |   |     |     |     |     |
| Hydrolizer Feeder Screw Motor Load      |        | 10     | 8      | 10     | 8      | 10     | 10     | 10     |   |   |     |     |     |     |
| Hydrolizer Feed Temperature             |        | 106    | 106    | 119    | 108    | 108    | 108    | 115    |   |   |     |     |     |     |
| Hydrolizer Main Shaft Motor Load        |        | NA     | NA     | NA     | NA     | NA     | NA     | NA     |   |   |     |     |     |     |
| Hydrolizer Discharge Pressure           |        | 50     | 50     | 50     | 50     | 50     | 50     | 50     |   |   |     |     |     |     |
| Hydrolizer Condensate Temperature       |        | 225    | 225    | 225    | 225    | 225    | 225    | 225    |   |   |     |     |     |     |
| Hydrolized Hair Sample Quality          |        | Good   | Good   | Good   | Good   | Good   | Good   | Good   |   |   |     |     |     |     |
| Hair Cooker Jacket Reg. Steam Pressure  |        | 90     | 88     | 88     | 89     | 88     | 88     | 88     |   |   |     |     |     |     |
| Hair Cooker Condensate Temperature      |        | 195    | 195    | 195    | 195    | 195    | 195    | 195    |   |   |     |     |     |     |
| Hair Cooker Motor Load                  |        | NA     | NA     | NA     | NA     | NA     | NA     | NA     |   |   |     |     |     |     |
| Hair Cooker Discharge Time              |        | NA     | NA     | NA     | NA     | NA     | NA     | NA     |   |   |     |     |     |     |
| East Flotation Cell Condition           |        | Full   | Full   | Full   | Full   | Full   | Full   | Full   |   |   |     |     |     |     |
| # of Minutes East Skimmer Arm Running   |        | 3:40.3 | 3:40.3 | 3:45.3 | 3:46.0 | 3:45.3 | 3:45.3 | 3:45.3 |   |   |     |     |     |     |
| East Recycle Pump Discharge Pressure    |        | 50     | 50     | 50     | 50     | 50     | 50     | 50     |   |   |     |     |     |     |
| East Air Injection Air Flow             |        | 45     | 45     | 45     | 45     | 45     | 45     | 45     |   |   |     |     |     |     |
| East Air Mix Tank Inlet Pressure        |        | 90     | 90     | 90     | 90     | 90     | 90     | 90     |   |   |     |     |     |     |
| East Air Mix Tank Outlet Pressure       |        | 50     | 50     | 50     | 50     | 50     | 50     | 50     |   |   |     |     |     |     |
| West Flotation Cell Condition           |        | Full   | Full   | Full   | Full   | Full   | Full   | Full   |   |   |     |     |     |     |
| # of Minutes West Skimmer Arm Running   |        | 3:40.3 | 3:40.3 | 3:45.3 | 3:46.0 | 3:45.3 | 3:45.3 | 3:45.3 |   |   |     |     |     |     |
| West Recycle Pump Discharge Pressure    |        | 50     | 50     | 50     | 50     | 50     | 50     | 50     |   |   |     |     |     |     |
| West Air Injection Air Flow             |        | 45     | 45     | 45     | 45     | 45     | 45     | 45     |   |   |     |     |     |     |
| West Air Mix Tank Inlet Pressure        |        | 90     | 90     | 90     | 90     | 90     | 90     | 90     |   |   |     |     |     |     |
| West Air Mix Tank Outlet Pressure       |        | 50     | 50     | 50     | 50     | 50     | 50     | 50     |   |   |     |     |     |     |
| Flotation Heat Tank Level               |        | NA     | NA     | NA     | NA     | NA     | NA     | NA     |   |   |     |     |     |     |
| Flotation Heat Tank Temperature         |        | NA     | NA     | NA     | NA     | NA     | NA     | NA     |   |   |     |     |     |     |
| Tank Discharge Pump Rate                |        | NA     | NA     | NA     | NA     | NA     | NA     | NA     |   |   |     |     |     |     |

\*record all mechanical downtime on the back of this form. Include equipment name, time down, time back operational, reason for downtime and end of shift status.

\*\*report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.

Department Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)

Time Hair Vacuum System Started

# of Paddles Removed from Hydrolizer

# of Times Hydrolizer Plugged & Blown Down

Time Hair Received from Kill Floor

Time Hair Finished from Kill Floor

Time Hydrolizer Feeder Shut Off

Final Time Hair Cooker Discharged

Hair Silo Ending Level

|      |
|------|
| 7:20 |
|      |
|      |
|      |

Hair Silo Beginning Level

OK



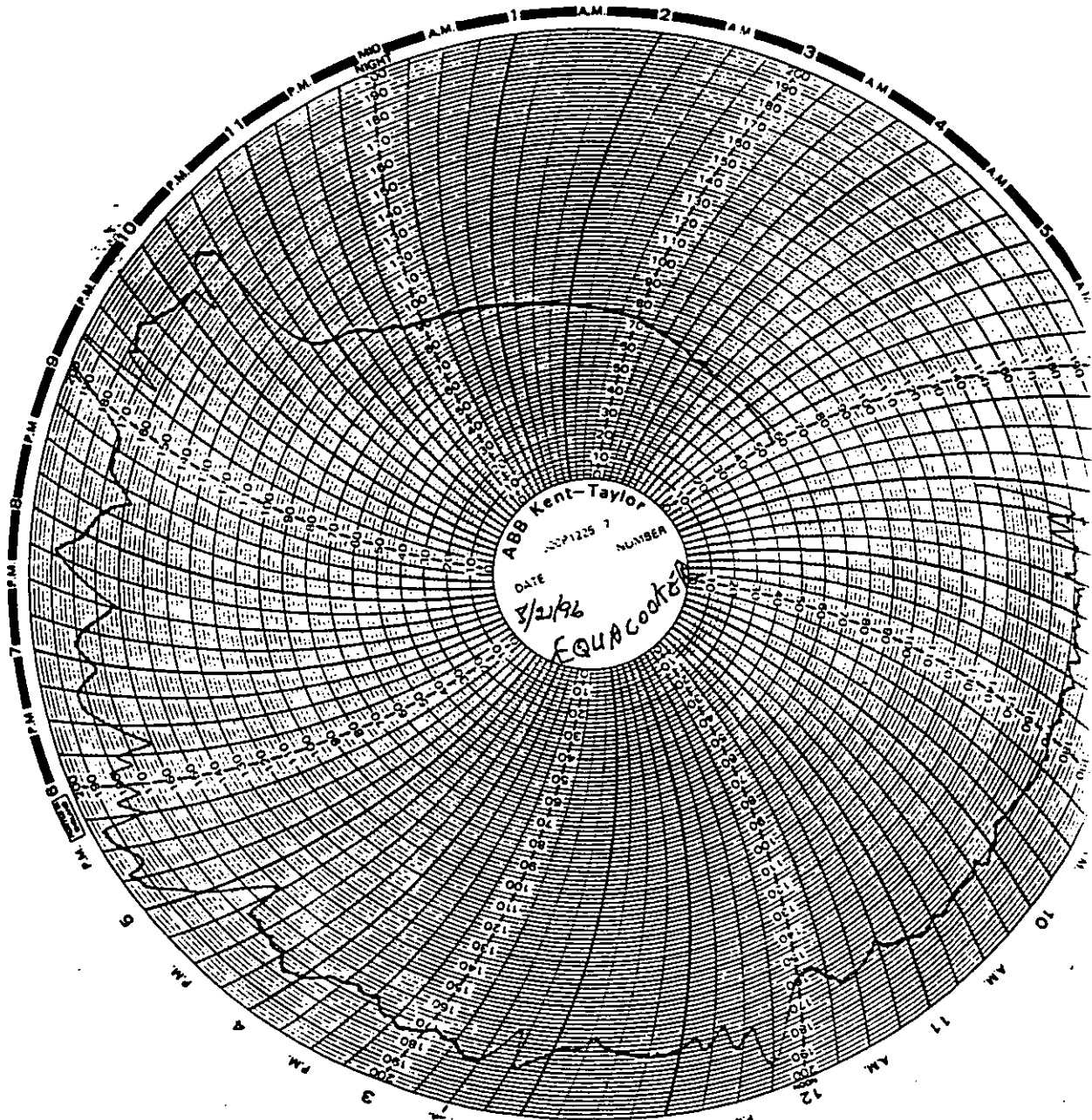
# LOGANSPOUT HAIR HYDROLIZER and FLOTATION CELL LOGSHEET LOG#100444

Operator *N. Towles*  
Date and Shift *8-22-96 A*

| DESCRIPTION                             | TARGET | 8:00 | 9:00 | 10:00 | 11:00 | 12:00 | 1:00 | 2:00 | 3:00 | 4:00 | 5:00 |
|-----------------------------------------|--------|------|------|-------|-------|-------|------|------|------|------|------|
| Bsmt Hair Collection Bin Status         |        | OK   | OK   | OK    | OK    | OK    | OK   | OK   | OK   | OK   | OK   |
| Hair Vacuum Blower Motor Load           |        | 13   | 18   | 18    | 13    | 18    | 19   | 19   | 19   | 19   | 19   |
| # of Minutes Feed Screw was Reversed    |        | 0    | 0    | 0     | 0     | 0     | 0    | 0    | 0    | 0    | 0    |
| Hydrolizer Reg. Internal Steam Pressure |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   | 50   | 50   | 50   |
| Hydrolizer Reg. Jacket Steam Pressure   |        | 90   | 90   | 90    | 90    | 90    | 90   | 90   | 90   | 90   | 90   |
| Hydrolizer Feeder Screw Motor Load      |        | B    | B    | B     | B     | B     | B    | B    | B    | B    | B    |
| Hydrolizer Feed Temperature             |        | 104  | 106  | 116   | 112   | 114   | 115  | 115  | 115  | 115  | 115  |
| Hydrolizer Main Shaft Motor Load        |        | N/A  | N/A  | N/A   | N/A   | N/A   | N/A  | N/A  | N/A  | N/A  | N/A  |
| Hydrolizer Discharge Pressure           |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   | 50   | 50   | 50   |
| Hydrolizer Condensate Temperature       |        | 225  | 225  | 225   | 225   | 225   | 225  | 225  | 225  | 225  | 225  |
| Hydrolized Hair Sample Quality          |        | Good | Good | Good  | Good  | Good  | Good | Good | Good | Good | Good |
| Hair Cooker Jacket Reg. Steam Pressure  |        | 88   | 90   | 87    | 89    | 89    | 88   | 88   | 88   | 88   | 88   |
| Hair Cooker Condensate Temperature      |        | 195  | 195  | 195   | 195   | 195   | 195  | 195  | 195  | 195  | 195  |
| Hair Cooker Motor Load                  |        | N/A  | N/A  | N/A   | N/A   | N/A   | N/A  | N/A  | N/A  | N/A  | N/A  |
| Hair Cooker Discharge Time              |        | ✓    | ✓    | ✓     | ✓     | ✓     | ✓    | ✓    | ✓    | ✓    | ✓    |
| East Flotation Cell Condition           | Active | Good | Good | Good  | Good  | Good  | Good | Good | Good | Good | Good |
| # of Minutes East Skimmer Arm Running   |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   | 50   | 50   | 50   |
| East Recycle Pump Discharge Pressure    |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   | 50   | 50   | 50   |
| East Air Injection Air Flow             |        | 90   | 90   | 90    | 90    | 90    | 90   | 90   | 90   | 90   | 90   |
| East Air Mix Tank Inlet Pressure        |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   | 50   | 50   | 50   |
| East Air Mix Tank Outlet Pressure       |        | 45   | 45   | 45    | 45    | 45    | 45   | 45   | 45   | 45   | 45   |
| West Flotation Cell Condition           |        | Good | Good | Good  | Good  | Good  | Good | Good | Good | Good | Good |
| # of Minutes West Skimmer Arm Running   |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   | 50   | 50   | 50   |
| West Recycle Pump Discharge Pressure    |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   | 50   | 50   | 50   |
| West Air Injection Air Flow             |        | 90   | 90   | 90    | 90    | 90    | 90   | 90   | 90   | 90   | 90   |
| West Air Mix Tank Inlet Pressure        |        | 50   | 50   | 50    | 50    | 50    | 50   | 50   | 50   | 50   | 50   |
| West Air Mix Tank Outlet Pressure       |        | 45   | 45   | 45    | 45    | 45    | 45   | 45   | 45   | 45   | 45   |
| Flotation Heat Tank Level               |        | N/A  | N/A  | N/A   | N/A   | N/A   | N/A  | N/A  | N/A  | N/A  | N/A  |
| Flotation Heat Tank Temperature         |        | N/A  | N/A  | N/A   | N/A   | N/A   | N/A  | N/A  | N/A  | N/A  | N/A  |
| Tank Discharge Pump Rate                |        | N/A  | N/A  | N/A   | N/A   | N/A   | N/A  | N/A  | N/A  | N/A  | N/A  |

Record all mechanical downtime on the back of this form. Include equipment name, time down, time back operational, reason for downtime and end of shift date.  
\*\*Report any and all mechanical problems to your supervisor immediately. Record all problems on the back of this form.

Department Condition: Shift Start-(Good Fair Poor); Shift End-(Good Fair Poor)  
Time Hair Vacuum System Started  
# of Paddles Removed from Hydrolizer  
# of Times Hydrolizer Plugged & Blown Down  
Hair Silo Beginning Level  
Time Hair Received from Kill Floor  
Time Hair Finished from Kill Floor  
Time Hydrolizer Feeder Shut Off  
Time Hair Coater Charged  
Time Silo Empty



Pork Inedible - Steam  
Logansport Inedible VOC Test

Tested August 22, 1996 at Logansport, IN on Dupps 1800 Cooker

|         |       |
|---------|-------|
| Test #1 | 1.300 |
| Test #2 | 0.900 |
| Test #3 | 2.200 |
|         | 1.467 |

|                            |       |
|----------------------------|-------|
| Head Kill                  | 6324  |
| Inedible Opeation Hours    | 14    |
| Inedible Crax Yield lbs/hd | 14.94 |

|                           |         |         |
|---------------------------|---------|---------|
|                           | lbs/hr  | tons/hr |
| Inedible Processed lbs/hr | 6748.61 | 3.37    |

|                        |       |
|------------------------|-------|
| Emission Rate (lb/ton) | 0.435 |
|------------------------|-------|

Pork Hair Hydrolizer - Steam  
Logansport Hair Hydrolizer VOC Test

Tested on September 21, 1996 at Logansport, IN on Anco Hydrolizer

Test #1 0.107  
Test #2  
Test #3

0.107

Head Kill 6121  
Hydrolizer Opeation Hours 8  
Hair Yield lbs/hd 0.7

|                       | lbs/hr | tons/hr |
|-----------------------|--------|---------|
| Hair Processed lbs/hr | 535.59 | 0.27    |

Emission Rate (lb/ton) 0.400

Pork Blood - Natural Gas  
Logansport Blood VOC Test

Tested August 20, 1996 at Logansport, IN on Dupps Ring Dryer

|         |       |
|---------|-------|
| Test #1 | 0.223 |
| Test #2 | 0.120 |
| Test #3 | 0.072 |
|         | 0.138 |

|                       |      |
|-----------------------|------|
| Head Kill             | 5968 |
| Blood Operation Hours | 10   |
| Blood Yield lbs/hd    | 1.33 |

|                        | lbs/hr | tons/hr |
|------------------------|--------|---------|
| Blood Processed lbs/hr | 793.74 | 0.40    |

|                        |       |
|------------------------|-------|
| Emission Rate (lb/ton) | 0.328 |
|------------------------|-------|

|                         |          |
|-------------------------|----------|
| Heat Capacity MMBtu/hr  | 3        |
| Emission Factor VOC- NG | 2.78E-06 |

|                         |          |
|-------------------------|----------|
| VOC emission from Comb  | 0.00834  |
| VOC emission from blood | 0.129993 |

**APPENDIX C**

**LABORATORY DATA**

TRC ENVIRONMENTAL CORPORATION, INC.  
5 WATERSIDE CROSSING, WINDSOR, CT 06095  
860-298-6326

Connecticut Certification No. PH-0426  
AIHA Laboratory Accreditation No. 259

\*\*\*LABORATORY REPORT\*\*\*

IBP LOGANSPOUT (NON-COMPLIANCE DATA)

| Sample Number            | Analyte | Result (ppm) |
|--------------------------|---------|--------------|
| Run #1 Blood Furnace     | Methane | 6.31         |
| Run #2 Blood Furnace     | Methane | 5.29         |
| Run #3 Blood Furnace     | Methane | 11.40        |
| Run 1&2 Hydrolyzer Stack | Methane | 15.57        |
| Run #1&3 Melt Tank       | Methane | 75.60        |

Analyst: Lance R. Cotton

Reviewed by: Margaret F. Flanagan or Lance R. Cotton  
Margaret F. Flanagan      Laboratory Supervisor  
Quality Control Manager

**Method 25  
Analytical Results**

prepared for

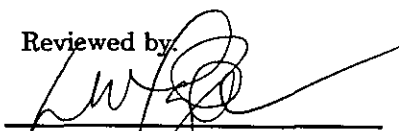
**TRC ENVIRONMENTAL CORPORATION**

1307 Butterfield Road, Suite 420  
Downers Grove, IL 60515

by

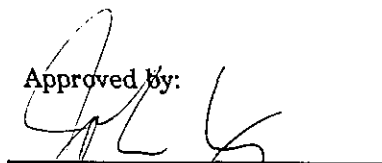
**Triangle Environmental Services, Inc.**

Reviewed by:



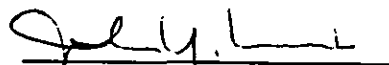
Larry W. Taylor  
Laboratory Analyst

Approved by:



John Venezia  
Laboratory Supervisor

Approved by:



John Y. Morimoto, Ph.D.  
QA Officer

Report

**97317**

December 24, 1997

**Triangle Environmental Services, Inc.**  
**METHOD 25 TABLE OF RESULTS**

Client: TRC Environmental Corporation

ID#97317 Analyzed: 12/18-22/97

Project ID: IBP (Madison, Nebraska)

|   | Sample<br>Description | Concentrations (ppmC) |     |      |                      |                   |       | Mass<br>Conc.<br>(mgC/cu.m) |
|---|-----------------------|-----------------------|-----|------|----------------------|-------------------|-------|-----------------------------|
|   |                       | CO                    | CH4 | CO2  | Noncon-<br>densibles | Conden-<br>sibles | TGNMO |                             |
| 1 | IBP Run #1            | 171                   | 38  | 2487 | 64                   | 14299             | 14362 | 7171                        |
| 2 | IBP Run #2            | 136                   | 32  | 2193 | 22                   | 1621              | 1644  | 821                         |
| 3 | IBP Run #3            | 91                    | 23  | 2210 | 7                    | 795               | 802   | 400                         |
| 4 | Blank                 | < 3                   | < 3 | 2679 | < 6                  | 75                | 75    | 37                          |

< # = Concentration Below Practical Quantitation Limit

\* Please refer to the "Comments on the Analyses" page of the report for additional information.

# Triangle Environmental Services, Inc.

## METHOD 25 PROCEDURES

### CALIBRATION

Initial calibrations and operational checks of the recovery and analytical systems are conducted at a frequency of no greater than one year between sets. The calibrations satisfy the requirements for Methods 25, 25-C, and 10-B.

Triplicate injections of a calibration gas mixture consisting of 199.7 ppm carbon monoxide, 49.85 ppm methane, 10000 ppm carbon dioxide, and 24.88 ppm propane are made immediately before and after each batch of samples. Daily response factors are calculated from the pre-batch integrated responses (average area count / concentration in ppmC) and must agree within 10% of the response factors of the initial calibrations. Further, the post-batch response factors must agree within 2% of the pre-batch response factors. Both criteria must be met before the analyses are considered valid.

### CONDENSATE RECOVERY

To flush the trap of CO<sub>2</sub>, hydrocarbon-free air is flushed through the trap maintained at -78 °C into the sample tank until less than 10 ppm CO<sub>2</sub> is detected in the flow stream (the concentration of CO<sub>2</sub> is monitored with an NDIR CO<sub>2</sub> detector and measured using a CO<sub>2</sub> analyzer). The sample tank is pressurized to about 1200 mm Hg for analysis and is replaced with an intermediate collection vessel (ICV).

To oxidize the organic material in the trap, hydrocarbon-free air is then passed through the trap heated to 250 °C and the recovery oxidation catalyst into the ICV until less than 10 ppm CO<sub>2</sub> is detected in the flow stream. The ICV is pressurized to about 1200 mm Hg for analysis.

### ANALYSIS

All samples, which include the daily calibration gas mixture, sample tanks, and ICVs, are analyzed in triplicate using a computer-interfaced gas chromatograph equipped with an automated gas sampling system and a flame ionization detector (FID). CO, CH<sub>4</sub>, and CO<sub>2</sub> are eluted from the Unibead 1S-Carbosieve G column and pass through the analytical oxidation and reduction catalysts to the FID. The column is then backflushed to elute the nonmethane organic (NMO) fraction, which passes through the analytical oxidation and reduction catalysts to the FID.

### CALCULATIONS

Calculations are done in accord with USEPA Method 25 procedures. A sample calculation for one of the samples is provided in the report. CO and CO<sub>2</sub> blanks are used to compensate for a background concentration of (1) "CO" due to the interference of O<sub>2</sub> resulting from the coelution of O<sub>2</sub> and CO and (2) CO<sub>2</sub> due to CO<sub>2</sub> and organic compounds in the recovery carrier gas. A concentration of noncondensibles or condensibles of less than the PQL is considered to be zero in computing the TGNMO.

### EQUIPMENT

Tanks and ICVs are twice evacuated and filled with ambient air filtered through charcoal and are then evacuated to below 10 mm Hg and monitored for at least an hour to check that the tanks do not leak more than 1 mm Hg/hour. They are then pressurized to greater than ambient pressure with helium, analyzed to ensure < 2 ppmC NMO, and stored for later use.

Traps are flushed at 300 °C for at least 30 minutes with compressed air. Each trap is then flushed at 300 °C for thirty minutes with hydrocarbon-free air. The effluent is then routed through an oxidation catalyst and a reduction catalyst for analysis by FID-GC to confirm less than 10 ppmC total C.

Sampling units are reconditioned by replacing filters and checking that all sections operate properly. The unit is heated (with a Teflon® line used in place of a trap) and is flushed with zero air for at least thirty minutes before an aliquot of this flow is injected into the analyzer. If the total carbon concentration is below 10 ppm, the unit is made ready for use and stored for shipment.

**Triangle Environmental Services, Inc.**  
**METHOD 25 SAMPLE CALCULATION**

Client: TRC Environmental Corporation

ID#97317 Analyzed: 12/18-22/97

Project ID: IBP (Madison, Nebraska)

Sample # 3 IBP Run #3

**D A T A**

Note: All pressure values have been converted when necessary to mm Hg and all temperature values to Kelvin.

Pressure, Temperature, Volume Data:

|              | Pressure<br>(mm Hg) | Temp.<br>(K) |                             |
|--------------|---------------------|--------------|-----------------------------|
| Presampling  | 2.8                 | 294.26       | Tank N294T:                 |
| Postsampling | 610.8               | 294.26       | Tank Volume = 0.004531 cu.m |
| Lab Receipt  | 636.0               | 296.15       |                             |
| Tank Final   | 1476.0              | 296.15       | Trap GGC →                  |
| CV Final     | 1676.0              | 298.15       | Collection Vessel 28:       |
|              |                     |              | CV Volume = 0.008383 cu.m   |

Response Factors (RF), Practical Quantitation Limits (PQL), and Area Counts:

|                 | RF<br>(area/ppmC) | PQL<br>(ppmC) | Area 1  | Area 2  | Area 3  |
|-----------------|-------------------|---------------|---------|---------|---------|
| CO              | 212.9             | 2             | 8,073   | 8,085   | 8,050   |
| CH4             | 221.6             | 2             | 2,183   | 2,165   | 2,128   |
| CO2             | 221.5             | 2             | 203,257 | 203,946 | 203,551 |
| Noncondensibles | 222.8             | 5             | 657     | 682     | 599     |
| Condensibles    | 221.5             | 5             | 35,593  | 35,668  | 35,677  |

CO Blank = 0 area counts    CO2 Blank = 3 ppm

**C A L C U L A T I O N S**

Measured Concentrations, corrected for blank (ppmC):

$$\begin{aligned}\text{Cm(CO)} &= [\text{Area(CO)} - \text{CO Blank}] / \text{RF(CO)} \\ &= [8073 - 0] / 212.9 = 37.9 \\ &= [8085 - 0] / 212.9 = 38.0 \\ &= [8050 - 0] / 212.9 = 37.8\end{aligned}$$

$$\begin{aligned}\text{Cm(CH}_4\text{)} &= \text{Area(CH}_4\text{)} / \text{RF(CH}_4\text{)} \\ &= 2183 / 221.6 = 9.9 \\ &= 2165 / 221.6 = 9.8 \\ &= 2128 / 221.6 = 9.6\end{aligned}$$

$$\begin{aligned}\text{Cm(CO}_2\text{)} &= \text{Area(CO}_2\text{)} / \text{RF(CO}_2\text{)} - \text{CO}_2 \text{ Blank} \\ &= 203257 / 221.5 - 3 = 914.6 \\ &= 203946 / 221.5 - 3 = 917.7 \\ &= 203551 / 221.5 - 3 = 916.0\end{aligned}$$

$$\begin{aligned}\text{Cm(Noncondensibles)} &= \text{Area(Noncondensibles)} / \text{RF(Noncondensibles)} \\ &= 657 / 222.8 = 2.9 \\ &= 682 / 222.8 = 3.1 \\ &= 599 / 222.8 = 2.7\end{aligned}$$

$$\begin{aligned}\text{Cm(Condensibles)} &= \text{Area(Condensibles)} / \text{RF(Condensibles)} - \text{CO}_2 \text{ Blank} \\ &= 35593 / 221.5 - 3 = 157.7 \\ &= 35668 / 221.5 - 3 = 158.0 \\ &= 35677 / 221.5 - 3 = 158.1\end{aligned}$$

Pressure-Temperature Ratio,  $Q(i) = P(i)/T(i)$  (mm Hg/K):

$$\begin{aligned}\text{Tank Presampling: } Q(2) &= 2.8 / 294.26 = 0.010 \\ \text{Tank Postsampling: } Q(1) &= 610.8 / 294.26 = 2.076 \\ \text{Tank Lab Receipt: } Q(5) &= 636.0 / 296.15 = 2.148 \\ \text{Tank Final: } Q(3) &= 1476.0 / 296.15 = 4.984 \\ \text{CV Final: } Q(4) &= 1676.0 / 298.15 = 5.621\end{aligned}$$

$$\begin{aligned}\text{Volume Sampled (dscm)} &= 0.3857 \times \text{Tank Volume} \times [Q(1) - Q(2)] \\ &= 0.3857 \times 0.004531 \times [2.076 - 0.010] \\ &= 0.003611\end{aligned}$$

Averages and % Relative Standard Deviations (%RSD) of Cm's are calculated.  
(%RSD of C=%RSD of Cm)

Calculated Concentrations (ppmC):

$$\begin{aligned}\text{C(CO)} &= Q(3) / [Q(1) - Q(2)] \times \text{Cm(CO)} \\ &= 4.984 / (2.076 - 0.010) \times 37.9 = 91.4\end{aligned}$$

$$\begin{aligned}\text{C(CH}_4\text{)} &= Q(3) / [Q(1) - Q(2)] \times \text{Cm(CH}_4\text{)} \\ &= 4.984 / (2.076 - 0.010) \times 9.7 = 23.5\end{aligned}$$

$$\begin{aligned}\text{C(CO}_2\text{)} &= Q(3) / [Q(1) - Q(2)] \times \text{Cm(CO}_2\text{)} \\ &= 4.984 / (2.076 - 0.010) \times 916.1 = 2209.8\end{aligned}$$

$$\begin{aligned}\text{C(Noncondensibles)} &= Q(3) / [Q(1) - Q(2)] \times \text{Cm(Noncondensibles)} \\ &= 4.984 / (2.076 - 0.010) \times 2.9 = 7.0\end{aligned}$$

$$\begin{aligned}\text{C(Condensibles)} &= \text{Volume(CV)} / \text{Volume(Tank)} \times Q(4) / [Q(1) - Q(2)] \times \text{Cm(Condensibles)} \\ &= 0.008383 / 0.004531 \times 5.621 / (2.076 - 0.010) \times 157.9 = 794.9\end{aligned}$$

$$\begin{aligned}\text{Total Gaseous Non-Methane Organics (TGNMO)} &= \text{C(Noncondensibles)} + \text{C(Condensibles)} \\ &= 7.0 + 794.9 \\ &= 801.9\end{aligned}$$

$$\begin{aligned}\text{Mass Concentration (mgC/cu.m)} &= 0.4993 \times \text{TGNMO} \\ &= 0.4993 \times 801.9 = 400.4\end{aligned}$$

# Triangle Environmental Services, Inc.

## METHOD 25 SAMPLE QA/QC DATA

### DAILY RECOVERY SYSTEM CHECKS

#### 4.3.1.1\* Condensate Recovery System Leak Check

Evacuate system to  $\leq 10$  mm Hg absolute pressure, isolate system, and monitor for ten minutes.

Requirement: Pressure Change  $\leq 3$  mm Hg

#### 4.3.1.2\* Condensate Recovery System Background Test

Analyze recovery system effluent for CO<sub>2</sub> concentrations.

Requirement: CO<sub>2</sub>  $\leq 10$  ppm

#### 4.3.1.3\* Condensate Oxidation Catalyst Efficiency Check

Analyze 1% methane standard through oxidation catalyst.

Requirement: CO<sub>2</sub> = CH<sub>4</sub> concentration  $\pm 2\%$

### DAILY ANALYZER CHECKS

#### 5.3\* Daily Calibration

##### Response Factor Checks

Requirement: Daily RF = Initial RF  $\pm 5\%$

|                 | Initial RF for<br>Analyzer A<br>2/25/97 | Initial RF for<br>Analyzer B<br>3/13/97 |
|-----------------|-----------------------------------------|-----------------------------------------|
| CO              | 249.70                                  | 224.96                                  |
| CH <sub>4</sub> | 242.40                                  | 216.84                                  |
| CO <sub>2</sub> | 244.04                                  | 215.46                                  |
| NMO             | 243.64                                  | 216.92                                  |

Triplicate injections of a mixture of CO, CH<sub>4</sub>, CO<sub>2</sub>, and C<sub>3</sub>H<sub>8</sub> are made before and after each batch of samples.

**INITIAL CONDENSATE RECOVERY SYSTEM TESTS****5.1.1\* Carrier and Auxiliary Gas Blank**Requirement:  $\text{CO} + \text{CH}_4 + \text{CO}_2 + \text{NMO} \leq 5 \text{ ppm}$ **5.1.3\* System Performance Check**

| Volume Injected  | Compound | Average % Recovery |     |      |       | % RSD    |       |       |       |
|------------------|----------|--------------------|-----|------|-------|----------|-------|-------|-------|
| 50 $\mu\text{L}$ | Hexane   | 101                | 102 | 98.8 | 104.6 | 0.058    | 0.101 | 1.68  | 0.229 |
| 50 $\mu\text{L}$ | Decane   | 97                 | 100 | 93.7 | 103.3 | 0.120    | 0.047 | 1.7   | 0.359 |
| 10 $\mu\text{L}$ | Hexane   | 104                | 107 | 92   | 90.0  | 0.118    | 0.145 | 1.206 | 0.135 |
| 10 $\mu\text{L}$ | Decane   | 98                 | 97  | 99.6 | 93.3  | 0.119    | 0.232 | 1.36  | 0.254 |
| Requirement:     |          | $100 \pm 10\%$     |     |      |       | $\leq 5$ |       |       |       |

**INITIAL NMO ANALYZER PERFORMANCE CHECKS****5.2.1\* Oxidation Catalyst Efficiency Check** Analyzer A, 2/25/97; Analyzer B, 3/13/97

FID response with reduction catalyst in bypass mode = 0, 0  
 Requirement:  $\leq 1\%$

**5.2.2\* Reduction Catalyst Efficiency Check** Analyzer A, 2/25/97; Analyzer B, 3/13/97

Response of  $\text{CH}_4$  with oxidation and reduction catalysts in series mode compared to response with both catalysts in bypass mode.  
 97.7%, 100.6% Requirement:  $> 95\%$

**5.2.3\* Analyzer Linearity Check+NMO Calibration** Analyzer A, 2/25/97; Analyzer B, 3/13/97

|                                                     |                             |              |               |
|-----------------------------------------------------|-----------------------------|--------------|---------------|
| RF Value $\text{CO}$ :                              | $\pm 1.18\%$ , $\pm 1.18\%$ | Requirement: | $\pm 2.5\%$   |
| RF Value $\text{CH}_4$ :                            | $\pm 1.56\%$ , $\pm 0.81\%$ |              | $\pm 2.5\%$   |
| RF Value $\text{CO}_2$ :                            | $\pm 1.47\%$ , $\pm 1.70\%$ |              | $\pm 2.5\%$   |
| RF Value NMO:                                       | $\pm 1.18\%$ , $\pm 1.90\%$ |              | $\pm 2.5\%$   |
| % RSD Values:                                       | 0.46%, 0.45%                |              | $\leq 2\%$    |
| $\frac{\text{RF (NMO)}}{\text{RF (CO}_2\text{)}} =$ | 1.00, 0.99                  |              | $1.0 \pm 0.1$ |

5.2.4\*      **System Performance Check**      Analyzer A, 2/25/97; Analyzer B, 3/13/97

|                | Measured Value | Expected Value | Requirement |
|----------------|----------------|----------------|-------------|
| Propane in Mix | 24.9, 25.3     | 25.0, 24.88    | ± 5%        |
| Hexane         | 50.2, 51.0     | 51.4, 51.4     | ± 5%        |
| Toluene        | 20.4, 19.5     | 19.97, 19.97   | ± 5%        |
| Methanol       | 102.6, 102.9   | 100.0, 100.0   | ± 5%        |

**EQUIPMENT CHECKS**4.1.1\*      **Clean Sampling Equipment Check**

|             |     |              |        |
|-------------|-----|--------------|--------|
| Sample Unit | <10 | ppmC total C | @ 100% |
| Trap        | <10 | ppmC total C | @ 100% |
| Tank        | < 2 | ppmC NMO     | @ 100% |

4.1.2\*      **Sample Tank Evacuation and Leak Check**

Tank evacuated to  $\leq 10$  mm Hg absolute pressure, monitored for  $\geq 1$  hour, and passed for use if no pressure change ( $< 1$  mm Hg/hr) is noted.

5.4\*      **Sample Tank and ICV Volumes**

Tank weighed empty, filled with deionized distilled water (temperature recorded), and weighed to the nearest 2 g. Volume calculated based on density of water at that temperature and results recorded in permanent file.

# Triangle Environmental Services, Inc.

## METHOD 25 DATA REPORT

Client: TRC Environmental Corporation

ID#97317 Analyzed: 12/18-22/97

Project ID: IBP (Madison, Nebraska)

Sample # 1 IBP Run #1

### Pressure, Temperature, Volume Data:

|              | Pressure<br>(mm Hg) | Temp.<br>(K) | P/T   |                                |
|--------------|---------------------|--------------|-------|--------------------------------|
| Presampling  | 3.0                 | 294.26       | 0.010 | Tank 6207T:                    |
| Postsampling | 591.8               | 294.26       | 2.011 | Tank Volume = 0.004125 cu.m    |
| Lab Receipt  | 600.0               | 296.15       | 2.026 | Volume Sampled = 0.003184 dscm |
| Tank Final   | 1276.0              | 296.15       | 4.309 | <u>Lab Receipt P/T</u>         |
| CV Final     | 1620.0              | 298.15       | 5.434 | Postsampling P/T = 1.007       |
|              |                     |              |       | Trap GGJ →                     |
|              |                     |              |       | Collection Vessel 23:          |
|              |                     |              |       | CV Volume = 0.008343 cu.m      |

### Response Factors (RF), Practical Quantitation Limits (PQL), and Area Counts:

|                 | RF<br>(area/ppmC) | PQL<br>(ppmC) | Area 1  | Area 2  | Area 3  |
|-----------------|-------------------|---------------|---------|---------|---------|
| CO              | 212.9             | 2             | 16,943  | 16,999  | 16,918  |
| CH4             | 221.6             | 2             | 3,885   | 3,849   | 3,890   |
| CO2             | 221.5             | 2             | 257,117 | 257,461 | 254,815 |
| Noncondensibles | 222.8             | 5             | 6,649   | 6,613   | 6,528   |
| Condensibles    | 221.5             | 5             | 579,754 | 576,354 | 575,891 |

Recovery Oxidation Catalyst Efficiency Check: CO2/CH4 = 99.9%

CO Blank = 0 area counts CO2 Blank = 3 ppm

### Concentrations:

| *corrected for Blank | ppmC   |   |    | %RSD |
|----------------------|--------|---|----|------|
|                      | Amount | ± | SD |      |
| CO*                  | 171    | ± | 0  | 0.2  |
| CH4                  | 38     | ± | 0  | 0.6  |
| CO2*                 | 2487   | ± | 14 | 0.6  |
| Noncondensibles      | 64     | ± | 1  | 0.9  |
| Condensibles*        | 14299  | ± | 52 | 0.4  |
| TGNMO                | 14362  |   |    |      |

Mass Concentration 7171 mgC/cu.m

# Triangle Environmental Services, Inc.

## METHOD 25 DATA REPORT

Client: TRC Environmental Corporation

ID#97317 Analyzed: 12/18-22/97

Project ID: IBP (Madison, Nebraska)

Sample # 2 IBP Run #2

### Pressure, Temperature, Volume Data:

|              | Pressure<br>(mm Hg) | Temp.<br>(K) | P/T   |                                |
|--------------|---------------------|--------------|-------|--------------------------------|
| Presampling  | 3.8                 | 294.26       | 0.013 | Tank 6210T:                    |
|              |                     |              |       | Tank Volume = 0.006075 cu.m    |
| Postsampling | 596.8               | 294.26       | 2.028 | Volume Sampled = 0.004722 dscm |
| Lab Receipt  | 608.0               | 296.15       | 2.053 | <u>Lab Receipt P/T</u> = 1.012 |
|              |                     |              |       | Postsampling P/T               |
| Tank Final   | 1168.0              | 296.15       | 3.944 | Trap GGB →                     |
| CV Final     | 1616.0              | 298.15       | 5.420 | Collection Vessel 26:          |
|              |                     |              |       | CV Volume = 0.008346 cu.m      |

### Response Factors (RF), Practical Quantitation Limits (PQL), and Area Counts:

|                 | RF<br>(area/ppmC) | PQL<br>(ppmC) | Area 1  | Area 2  | Area 3  |
|-----------------|-------------------|---------------|---------|---------|---------|
| CO              | 212.9             | 2             | 14,841  | 14,826  | 14,837  |
| CH4             | 221.6             | 2             | 3,609   | 3,643   | 3,704   |
| CO2             | 221.5             | 2             | 249,702 | 248,444 | 248,360 |
| Noncondensibles | 222.8             | 4             | 2,538   | 2,483   | 2,659   |
| Condensibles    | 221.5             | 3             | 97,724  | 97,555  | 98,217  |

Recovery Oxidation Catalyst Efficiency Check: CO2/CH4 = 99.5%

CO Blank = 0 area counts CO2 Blank = 3 ppm

### Concentrations:

|                       | ppmC   |      | %RSD |
|-----------------------|--------|------|------|
|                       | Amount | ± SD |      |
| *=corrected for Blank |        |      |      |
| CO*                   | 136    | ± 0  | 0.1  |
| CH4                   | 32     | ± 0  | 1.3  |
| CO2*                  | 2193   | ± 7  | 0.3  |
| Noncondensibles       | 22     | ± 1  | 3.5  |
| Condensibles*         | 1621   | ± 6  | 0.4  |
| TGNMO                 | 1644   |      |      |

Mass Concentration 821 mgC/cu.m

# Triangle Environmental Services, Inc.

## METHOD 25 DATA REPORT

Client: TRC Environmental Corporation

ID#97317 Analyzed: 12/18-22/97

Project ID: IBP (Madison, Nebraska)

Sample # 3 IBP Run #3

### Pressure, Temperature, Volume Data:

|              | Pressure<br>(mm Hg) | Temp.<br>(K) | P/T   |                                |
|--------------|---------------------|--------------|-------|--------------------------------|
| Presampling  | 2.8                 | 294.26       | 0.010 | Tank N294T:                    |
| Postsampling | 610.8               | 294.26       | 2.076 | Tank Volume = 0.004531 cu.m    |
| Lab Receipt  | 636.0               | 296.15       | 2.148 | Volume Sampled = 0.003611 dscm |
| Tank Final   | 1476.0              | 296.15       | 4.984 | <u>Lab Receipt P/T</u> = 1.035 |
| CV Final     | 1676.0              | 298.15       | 5.621 | Postsampling P/T               |
|              |                     |              |       | Trap GGC →                     |
|              |                     |              |       | Collection Vessel 28:          |
|              |                     |              |       | CV Volume = 0.008383 cu.m      |

### Response Factors (RF), Practical Quantitation Limits (PQL), and Area Counts:

|                 | RF<br>(area/ppmC) | PQL<br>(ppmC) | Area 1  | Area 2  | Area 3  |
|-----------------|-------------------|---------------|---------|---------|---------|
| CO              | 212.9             | 2             | 8,073   | 8,085   | 8,050   |
| CH4             | 221.6             | 2             | 2,183   | 2,165   | 2,128   |
| CO2             | 221.5             | 2             | 203,257 | 203,946 | 203,551 |
| Noncondensibles | 222.8             | 5             | 657     | 682     | 599     |
| Condensibles    | 221.5             | 5             | 35,593  | 35,668  | 35,677  |

Recovery Oxidation Catalyst Efficiency Check: CO2/CH4 = 98.9%

CO Blank = 0 area counts CO2 Blank = 3 ppm

### Concentrations:

|                       | ppmC   |   |    | %RSD |
|-----------------------|--------|---|----|------|
|                       | Amount | ± | SD |      |
| *=corrected for Blank |        |   |    |      |
| CO*                   | 91     | ± | 0  | 0.2  |
| CH4                   | 23     | ± | 0  | 1.3  |
| CO2*                  | 2210   | ± | 4  | 0.2  |
| Noncondensibles       | 7      | ± | 0  | 6.6  |
| Condensibles*         | 795    | ± | 1  | 0.1  |
| TGNMO                 | 802    |   |    |      |

Mass Concentration 400 mgC/cu.m

# Triangle Environmental Services, Inc.

## METHOD 25 DATA REPORT

Client: TRC Environmental Corporation

ID#97317 Analyzed: 12/18-22/97

Project ID: IBP (Madison, Nebraska)

Sample # 4 Blank

### Pressure, Temperature, Volume Data:

|              | Pressure<br>(mm Hg) | Temp.<br>(K) | P/T   |                                |
|--------------|---------------------|--------------|-------|--------------------------------|
| Presampling  | 3.2                 | 294.26       | 0.011 | Tank N295T:                    |
| Postsampling | 599.8               | 294.26       | 2.038 | Tank Volume = 0.004503 cu.m    |
| Lab Receipt  | 603.6               | 296.15       | 2.038 | Volume Sampled = 0.003521 dscm |
| Tank Final   | 1656.0              | 296.15       | 5.592 | <u>Lab Receipt P/T</u> = 1.000 |
| CV Final     | 1163.0              | 298.15       | 3.901 | Postsampling P/T               |
|              |                     |              |       | Trap DDV →                     |
|              |                     |              |       | Collection Vessel 33:          |
|              |                     |              |       | CV Volume = 0.008361 cu.m      |

### Response Factors (RF), Practical Quantitation Limits (PQL), and Area Counts:

|                 | RF<br>(area/ppmC) | PQL<br>(ppmC) | Area 1  | Area 2  | Area 3  |
|-----------------|-------------------|---------------|---------|---------|---------|
| CO              | 212.9             | 3             | 46      | 0       | 0       |
| CH4             | 221.6             | 3             | 0       | 0       | 0       |
| CO2             | 221.5             | 3             | 215,140 | 217,076 | 215,127 |
| Noncondensibles | 222.8             | 6             | 0       | 0       | 0       |
| Condensibles    | 221.5             | 3             | 5,184   | 5,373   | 5,299   |

Recovery Oxidation Catalyst Efficiency Check: CO2/CH4 = 99.4%  
CO Blank = 0 area counts CO2 Blank = 3 ppm

### Concentrations:

|                       | ppmC   |      | %RSD |
|-----------------------|--------|------|------|
|                       | Amount | ± SD |      |
| *=corrected for Blank |        |      |      |
| CO*                   | < 3    |      |      |
| CH4                   | < 3    |      |      |
| CO2*                  | 2679   | ± 14 | 0.5  |
| Noncondensibles       | < 6    |      |      |
| Condensibles*         | 75     | ± 2  | 2.1  |

Note: A concentration of noncondensibles or condensibles of less than the PQL is considered to be zero in computing the TGNMO value.

TGNMO 75

Mass Concentration 37 mgC/cu.m

< # = Concentration Below Practical Quantitation Limit

**APPENDIX D**

**EQUIPMENT CALIBRATION**

# Thermocouple Calibration Form

## Meter Box #2

| Thermocouple<br>Number | Temperature<br>Reading #1 | Reference<br>Temp #1 | Temperature<br>Reading #2 | Reference<br>Temp #2 | Temperature<br>Reading #3 | Reference<br>Temp #3 |
|------------------------|---------------------------|----------------------|---------------------------|----------------------|---------------------------|----------------------|
| 1                      | 74                        | 73                   | 185                       | 183                  | 286                       | 283                  |
| 2                      | 74                        | 73                   | 185                       | 183                  | 285                       | 283                  |
| 3                      | 73                        | 73                   | 185                       | 183                  | 285                       | 283                  |
| 4                      | 74                        | 73                   | 185                       | 183                  | 284                       | 283                  |
| 5                      | 73                        | 73                   | 185                       | 183                  | 284                       | 283                  |
| 6                      | 40                        | 39                   | 73                        | 73                   | 108                       | 108                  |
| 7                      | 39                        | 39                   | 74                        | 73                   | 108                       | 108                  |

Calibrated By: SRM  
Date: 4-8-96

Criteria: Absolute temp reading cant exceed 1.5% of Absolute reference temp



# Scott Specialty Gases, Inc.

1290 COMBERMERE STREET, TROY, MI 48083

(810) 589-2950 FAX:(810) 589-2134

## CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

**Customer**  
TRC ENVIRONMENTAL  
1307 BUTTERFIELD ROAD STE420  
ATTN CARIN O'BRIEN  
DOWNERS GROVE, IL 60515

**Assay Laboratory**  
Scott Specialty Gases, Inc  
1290 Combermere  
Troy, MI 48083

**Purchase Order :** L 27130  
**Scott Project # :** 583405

### ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay and Certification of Gaseous Calibration Standards; Procedure G1; September, 1993.

**Cylinder Number :** ALM038887  
**Cylinder Pressure + :** 1800 psig

**Certificate Date :** 7/18/95  
**Previous Certificate Date :** None

**Expiration Date :** 7/18/98

### ANALYZED CYLINDER

**Components**  
Propane

**Certified Concentration**  
27.88 ppm

**Analytical Uncertainty\***  
±1% NIST Directly Traceable

**Balance Gas:** Nitrogen

\*Do not use when cylinder pressure is below 150 psig.

\*Analytical accuracy is inclusive of usual known error sources which at least include precision of the measurement processes.

### REFERENCE STANDARD

**Type**  
SRM 2643A

**Expiration Date**  
3/28/98

**Cylinder Number**  
SX-20290

**Concentration**  
99.12 ppm Propane in Nitrogen

### INSTRUMENTATION

**Instrument/Model/Serial #**  
Propane : Beckman/400/1002059

**Last Date Calibrated**  
7/12/95

**Analytical Principle**  
Flame Ionization Detector

### ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

**Components**  
Propane

#### First Triad Analysis

Date: 7/18/95 Response Units: mv  
Z1=0.00 R1=99.10 T1=27.90  
R2=99.10 Z2=0.00 T2=27.90  
Z3=0.00 T3=27.90 R3=99.10  
Avg. Conc. of Cust. Cyl. 27.88 ppm

#### Second Triad Analysis

#### Calibration Curve

Concentration =  $A + Bx + Cx^2 + Dx^3 + Ex^4$   
r=1.00000 SRM 2643A  
Constants: A=-0.034421000  
B=1.000500000 C=0.000000000  
D=0.000000000 E=0.000000000

**Special Notes**

Cylinder

Analyst

# PYROMETER CALIBRATION SHEET

Date: 8/14/96  
 Initials: DW  
 Model #: \_\_\_\_\_  
 Serial #: \_\_\_\_\_  
 Part #: RIG #3

Roto scale: 0-130 cc/min  
 Roto used for: SAMPLING  
 Equip. attached to roto: RM25 RIG 3

| Setting<br>on Rotometer<br>(cc/min) | Volume<br>(mL) | Time<br>(sec) | Actual<br>Sampling Rate<br>(ml/min) |
|-------------------------------------|----------------|---------------|-------------------------------------|
| 30                                  | 50             | 95            | 31                                  |
| "                                   | 50             | 100           | 30                                  |
| "                                   | 50             | 97            | 31                                  |
| "                                   | 50             | 94            | 32                                  |
| "                                   | 50             | 98            | 30                                  |
| 40                                  | 50             | 72            | 41                                  |
| "                                   | 50             | 70            | 43                                  |
| "                                   | 50             | 73            | 41                                  |
| "                                   | 50             | 70            | 43                                  |
| "                                   | 50             | 70            | 43                                  |
| 50                                  | 50             | 59            | 51                                  |
| "                                   | 50             | 60            | 50                                  |
| "                                   | 50             | 60            | 50                                  |
| "                                   | 50             | 59            | 51                                  |
| "                                   | 100            | 1180          | 50                                  |
| 60                                  | 50             | 51            | 59                                  |
| "                                   | 50             | 50            | 58                                  |
| "                                   | 50             | 53            | 60                                  |
| "                                   | 100            | 106           | 60                                  |
| "                                   | 100            | 102           | 59                                  |
| 80                                  | 50             | 35            | 85                                  |
| "                                   | 50             | 36            | 82                                  |
| "                                   | 50             | 36            | 82                                  |
| "                                   | 100            | 73            | 82                                  |
| "                                   | 150            | 110           | 82                                  |
| 90                                  | 50             | 33            | 90                                  |
| "                                   | 50             | 34            | 88                                  |
| "                                   | 50             | 34            | 88                                  |
| "                                   | 100            | 70            | 86                                  |
| "                                   | 150            | 102           | 88                                  |
| 100                                 | 50             | 29            | 104                                 |
| "                                   | 50             | 29            | 104                                 |
| "                                   | 50             | 30            | 100                                 |
| "                                   | 100            | 60            | 100                                 |
| "                                   | 150            | 90            | 100                                 |

Comments:

Avg 31 ml/min

Avg 42

Avg 50.5

Avg 59

Avg 82.5

Avg 88

Avg 101.5

**TRC**

# ROTOMETER CALIBRATION SHEET

Date: 7/30/96  
 Initials: DW  
 Part #: RIG #2

Rotometer Scale: 0-120 cc/min  
 Rotometer Use: RM25 RIG SAMPLE  
 Calibrated Against: 5.001E METER

| Setting<br>on Rotometer<br>(cc/min) | Volume<br>(mL) | Time<br>(sec) | Actual<br>Sampling Rate<br>(cc/min) |              |
|-------------------------------------|----------------|---------------|-------------------------------------|--------------|
| <del>300</del>                      | 50             | 91            | 33                                  |              |
| <del>30</del>                       | 50             | 91            | 32                                  | <u>32.7</u>  |
|                                     | 50             | 94            | 33                                  |              |
| 40                                  | 50             | 71            | 42                                  |              |
|                                     | 50             | 74            | 40.5                                | <u>41.2</u>  |
|                                     | 50             | 73            | 41                                  |              |
| 50                                  | 50             | 57            | 52                                  |              |
|                                     | 100            | 115           | 52                                  | <u>52</u>    |
|                                     | 100            | 116           | 52                                  |              |
| 60                                  | 100            | 96            | 62                                  |              |
|                                     | 100            | 95            | 63                                  | <u>62</u>    |
|                                     | 50             | 49            | 61                                  |              |
| 70                                  | 100            | 84            | 71                                  |              |
|                                     | 100            | 82            | 73                                  | <u>72.3</u>  |
|                                     | 50             | 41            | 73                                  |              |
| 80                                  | 150            | 109           | 82                                  |              |
|                                     | 100            | 74            | 81                                  | <u>81.3</u>  |
|                                     | 50             | 37            | 81                                  |              |
| 90                                  | 100            | 64            | 93                                  |              |
|                                     | 100            | 64            | 93                                  | <u>93</u>    |
|                                     | 50             | 34            | 93                                  |              |
| 100                                 | 100            | 56            | 107                                 |              |
|                                     | 100            | 61            | 99                                  | <u>102.7</u> |
|                                     | 100            | 59            | 102                                 |              |

# ROTOMETER CALIBRATION SHEET

Date: 8/14/96  
 Initials: DW  
 Model #: \_\_\_\_\_  
 Serial #: \_\_\_\_\_  
 Part #: RIG #1

Roto scale: 0-130 cc/min  
 Roto used for: SAMPLING  
 Equip. attached to roto: Rm25 Rig #1

| Setting<br>on Rotometer<br>(cc/min) | Volume<br>(mL) | Time<br>(sec)    | Actual<br>Sampling Rate<br>(ml/min) |
|-------------------------------------|----------------|------------------|-------------------------------------|
| 30                                  | 50             | 98               | 31                                  |
|                                     | 50             | 85               | 35                                  |
|                                     | 50             | 84               | 35                                  |
|                                     | 50             | 85               | 35                                  |
|                                     | 100            | 176              | 34                                  |
| 40                                  | 50             | 63               | 48                                  |
|                                     | 50             | 66               | 45                                  |
|                                     | 50             | 64               | 47                                  |
|                                     | 100            | 130              | 46                                  |
|                                     | 100            | 130              | 46                                  |
| 50                                  | 50             | 53               | 56                                  |
|                                     | 50             | 58               | 52                                  |
|                                     | 100            | 107              | 56                                  |
|                                     | 100            | 106              | 56                                  |
|                                     | 100            | 105              | 57                                  |
| 60                                  | 50             | 45               | 66                                  |
|                                     | 50             | 43               | 69                                  |
|                                     | 50             | 46               | 66                                  |
|                                     | 100            | 97               | 62                                  |
|                                     | 150            | 133              | 66                                  |
| 80                                  | 50             | <del>58</del> 34 | 88                                  |
|                                     | 50             | 36               | 90                                  |
|                                     | 50             | 34               | 88                                  |
|                                     | 50             | 34               | 88                                  |
|                                     | 100            | 66               | 86                                  |
| 90                                  | 50             | 31               | 98                                  |
|                                     | 50             | 31               | 98                                  |
|                                     | 50             | 30               | 94                                  |
|                                     | 100            | 62               | 100                                 |
|                                     | 100            | 62               | 100                                 |
| 100                                 | 50             | 28               | 106                                 |
|                                     | 50             | 29               | 104                                 |
|                                     | 50             | 29               | 104                                 |
|                                     | 50             | 29               | 104                                 |
|                                     | 200            | 115              | 105                                 |

Comments:

AVG 34

AVG 46.5

AVG 55.5

AVG 66

AVG 88

AVG 98

AVG 104.5

**TRC**

# Type S Pitot Inspection Form

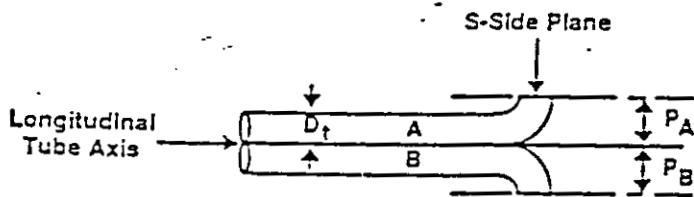
Pitot Tube No. 321

Tubing Diameter,  $D_t$  3/8 in.

$$\left(\frac{3}{16} < D_t < \frac{31}{16}\right)$$

Pitot Tube Assembly Level? Yes/No

Pitot Tube Opening Damaged? Yes/No



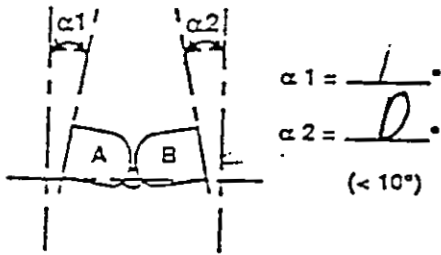
Note:

$$1.05 D_t < P < 1.50 D_t$$

$$P_A = P_B$$

$$P_A = \frac{7}{16} \text{ in.}$$

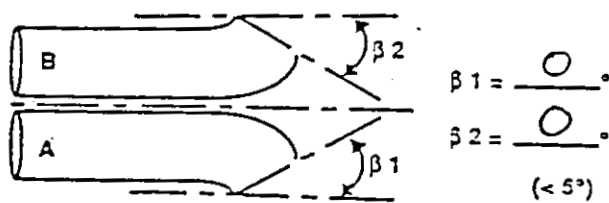
$$P_B = \frac{7}{16} \text{ in.}$$



$$\alpha 1 = \frac{1}{D}$$

$$\alpha 2 = \frac{D}{1}$$

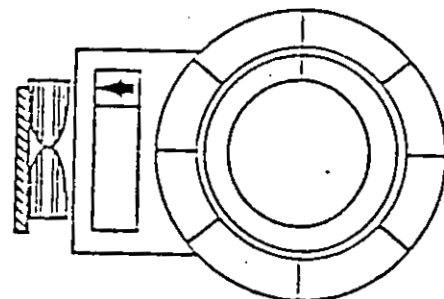
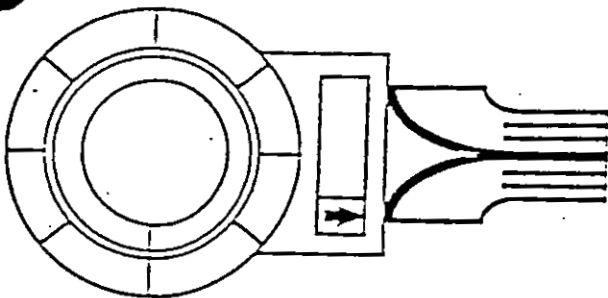
$$(< 10^\circ)$$



$$\beta 1 = \frac{0}{1}$$

$$\beta 2 = \frac{0}{1}$$

$$(< 5^\circ)$$



Level Position to find  $\gamma = \underline{0}$

$$Z = A' \sin \gamma \underline{0} \text{ in. } (< 1/8 \text{ in.})$$

Level Position to find  $\theta = \underline{0}$

$$W = A' \sin \theta \underline{0} \text{ in. } (< 1/32 \text{ in.})$$

Comments: \_\_\_\_\_

Checked by: DW

Date: 5/17/95

Calibration Required? NO

$D_t$  = External Tube Diameter

$A'$  = Distance Between Tips ( $P_A - P_B$ ) inches



## **APPENDIX E**

### **CALCULATION FORMULAS**

Facility \_\_\_\_\_ Job No. \_\_\_\_\_  
 Source \_\_\_\_\_ Date \_\_\_\_\_  
 Run \_\_\_\_\_ Calc/Review \_\_\_\_\_

# SAMPLE CALCULATIONS

## Particulate Isokinetic Sampling

### I. Calculations for stack volume and Isokinetic Ratio

| Time | Dry Gas<br>Meter ft <sup>3</sup> | Pitot<br>ΔP,<br>in. H <sub>2</sub> O | Orifice<br>ΔH,<br>in. H <sub>2</sub> O | Dry Gas<br>Temp °F<br>In Out | Stack<br>Static<br>Pressure<br>in. H <sub>2</sub> O | Stack<br>Temp °F |
|------|----------------------------------|--------------------------------------|----------------------------------------|------------------------------|-----------------------------------------------------|------------------|
| T    | VM                               | ΔP                                   | PM                                     | TMI TMO                      | PST                                                 | TS               |

- DN = Nozzle Diameter, inches \_\_\_\_\_ in.
- PB = Barometric Pressure, inches Hg \_\_\_\_\_ in. Hg
- TT = Net Sampling Time, minutes \_\_\_\_\_ min.
- VM = VM final - VM initial = Sample Gas Volume, ft<sup>3</sup> \_\_\_\_\_ ft<sup>3</sup>
- VML = Use only if any final or intermediate leak check rate is over 0.02 cfm  
 LI = Leak rate after any given sampling period, cfm  
 TLI = Total time of sampling period in which leak occurred, min.  
 VML = VM - [(L1 - 0.02) TLI + (L2 - 0.02) TL2 + (L3 - 0.02) TL3 + (L4 - 0.02) TL4]  
 = \_\_\_\_\_ ft<sup>3</sup>

- TM = Average Dry Gas Temperature at Meter, °F.

$$TM = \frac{\text{Avg. TMI} + \text{Avg. TMO}}{2} = \text{_____}^{\circ}\text{F}$$

- PM = Average Orifice Pressure Drop, inches H<sub>2</sub>O

$$PM = \text{Avg. } \Delta H = \text{_____} + 13.6 = \text{_____} \text{ in. Hg}$$

- Volume of dry gas sampled at standard conditions, dscf<sup>a</sup>

$$VMSTD = \frac{529(Y)(VM) \left( PB + \frac{PM}{13.6} \right)}{29.92(TM+460)}$$

Y = dry gas meter calibration factor  
 Y = \_\_\_\_\_ = \_\_\_\_\_ ft<sup>3</sup>

- VW = Total Water Collected = gm H<sub>2</sub>O Silica gel + mL Imp. H<sub>2</sub>O = \_\_\_\_\_ mL

- Volume of water vapor at standard conditions, scf<sup>b</sup>

$$VW_{\text{gas}} = 0.04715 \times VW = \text{_____} \text{ ft}^3$$

Run No. \_\_\_\_\_

Job No. \_\_\_\_\_

Date \_\_\_\_\_

10. Percent moisture in stack gas

$$\% M = \frac{100 \times VW_{\text{gas}}}{VMSTD + VW_{\text{gas}}} = \underline{\hspace{2cm}} \%$$

11. Mole fraction of dry gas (dimensionless)

$$MD = \frac{100 - \%M}{100} = \underline{\hspace{2cm}}$$

12. Molecular weight of dry stack gas

$$MWD = \left( \%CO_2 \times \frac{44}{100} \right) + \left( \%O_2 \times \frac{32}{100} \right) + \left[ (\%CO + \%N_2) \times \frac{28}{100} \right] = \underline{\hspace{2cm}} \text{ lb/lb mole dry}$$

- 12A. %EA = %Excess Air =

$$\frac{[(\%O_2) - 0.5(\%CO)] \times 100}{[(0.264)(\%N_2)] - (\%O_2) + 0.5(\%CO)} = \underline{\hspace{2cm}} \%$$

13. Molecular weight of wet stack gas

$$MW = MWD \times MD + 18 (1 - MD) = \underline{\hspace{2cm}} \text{ lb/lb mole wet}$$

14. AS = Stack Area, square inches

$$\text{Circular, } = \left( \frac{\text{stack diameter}}{2} \right)^2 \pi = \underline{\hspace{2cm}} \text{ sq. in.}$$

$$\text{Rectangular, } = \text{Length} \times \text{width} = \underline{\hspace{2cm}} \text{ sq. in.}$$

15. PS = Stack Pressure, absolute, inches Hg = PS ± AV PST

PST = Stack static pressure

$$\text{PST in. Hg} = \frac{\text{PST in. H}_2\text{O}}{13.6} = \underline{\hspace{2cm}} \text{ in. Hg}$$

$$PS = PS \pm \text{Avg. PST} = \underline{\hspace{2cm}} \text{ in. Hg}$$

16. TS
- <sub>AV</sub>
- = Average Stack Temperature

$$= \underline{\hspace{2cm}} ^\circ\text{F}$$

Run No. \_\_\_\_\_

Job No. \_\_\_\_\_

Date \_\_\_\_\_

17.  $SDE_{AV} = (\sqrt{\Delta P})_{AV} \times \sqrt{TS_{AV} + 460}$  = \_\_\_\_\_

18. Stack gas velocity at stack conditions, afpm

$$VS = 5130^c \times C_p \times SDE_{AV} \times \left[ \frac{1}{PS \times MW} \right]^{1/2} = \text{afpm}$$

$C_p$  = pitot tube coefficient

$C_p$  = \_\_\_\_\_ = \_\_\_\_\_ afpm

19. Stack gas volumetric flow rate at stack conditions, acfm<sup>d</sup>

$$Q_a = \frac{VS \times AS}{144} = \text{acfm}$$

20. Stack gas volumetric flow rate at standard conditions, dscfm<sup>e</sup>

$$Q_s = \frac{Q_a \times 528 \times MD \times PS}{(29.92)(TS_{AV} + 460)} = \text{dscfm}$$

21. Percent isokinetics

$$\% I = \frac{1,039^f \times (TS_{AV} + 460) \times VMSTD}{VS \times TT \times PS \times MD \times (DN)^2} = \text{\%}$$

<sup>a</sup>Dry standard cubic feet at 68°F (528R) and 29.92 in. Hg.

<sup>b</sup>Standard conditions at 68°F (528R) and 29.92 in. Hg.

$$^c 5130 = 85.5 \frac{\text{ft}}{\text{sec}} \left[ \frac{(\text{lb/lb mole})(\text{in. Hg})}{(^{\circ}\text{R})(\text{in. H}_2\text{O})} \right] \times 60 \text{ sec/min}$$

<sup>d</sup>Actual cubic feet per minute

<sup>e</sup>Dry standard cubic feet per minute at 68°F (528R) and 29.92 in. Hg.

$$^f 1039 = \frac{29.92 \text{ in Hg}}{528 \text{ Deg R}} \times \frac{144 \text{ in.}^2}{\text{ft}^2} \times \frac{4}{\pi} \times 100$$

## MOISTURE DETERMINATION WET BULB-DRY BULB TEMPERATURE TECHNIQUE

Client \_\_\_\_\_ Date \_\_\_\_\_  
 Project No. \_\_\_\_\_ Source \_\_\_\_\_  
 Plant \_\_\_\_\_ Calculated by: \_\_\_\_\_  
 Sampling Location \_\_\_\_\_ Checked by: \_\_\_\_\_

Barometric Pressure PB =  in Hg  $t_{dry} =$   °F

PST  $\frac{13.6}{13.6}$  in H<sub>2</sub>O =  in Hg  $t_{wet} =$   °F

PS = PB + PST =  in Hg

S.V.P. = water saturation vapor press =  in Hg  
 at  $t_{wet}$

$$V.P. = S.V.P. - \left[ 0.000367 (PS)(t_d - t_w) \left( 1 + \frac{t_w - 32}{1571} \right) \right]$$

$$V.P. = ( ) - \left[ 0.000367 ( ) ( - ) 1 + \left( \frac{( ) - 32}{1571} \right) \right]$$

$$= ( ) - \left[ 0.000367 ( ) ( ) ( ) \right]$$

V.P. =

$$\%M = \frac{V.P.}{PS} \times 100 = \frac{ }{ } \times 100 = \text{  }$$

$$Md = 1 - \frac{\%M}{100} = 1 - \frac{ }{100} = \text{  0. }$$

### **CALCULATION FORMULAS**

$\text{FLOW dscf/hr} = (\text{ACFM} * 528 * \text{Dry Mole Fraction} * \text{Stack Pressure}) / (29.92 * (\text{Stack Temp} + 460)) * 60$

$\text{Lbs/Hr} = \text{Cpmmv minus CH}_4 * \text{FWhc} * (\text{Stack Flowrate(dscf/hr)} / 60) * (1.554 * 10^4)$



October 16, 1998

Mr. Dave Meierhenry  
Air Quality Compliance Section  
Nebraska Department of Environmental Quality  
P. O. Box 98922  
Lincoln, NE 68509-8922

**RE:** IBP, inc., Dakota City, Nebraska  
Updated Summary Tables

Dear Mr. Meierhenry:

Please find enclosed a copy of the summary table for the SO<sub>x</sub>, NO<sub>x</sub>, and CO test data from testing conducted July 22, 1998, as well as the field data sheets. Also enclosed is a copy of the summary table showing flow data from testing conducted September 10, 1997, for which the flow data was used in the calculations to generate the final lbs/hr for the July 22, 1998 testing.

If you have any questions concerning the testing results or procedures used please contact me at 402-241-3647 or you may contact Mr. Scott Miller, TRC Project Manager, at 630-810-1122.

Sincerely,

*Rechelle Kruse by ml*

Rechelle Kruse  
Air Pollution Control Engineer

c: Tom Trosper (w/o test report)  
Angela Gogel (w/test report)  
Dallas Seifert (w/test report)

RK98-603/Stack Tests

IBP, inc. P.O. BOX 515, DAKOTA CITY, NEBRASKA 68731 TELEPHONE: 402-494-2061

IBP/DC Condenser Outlet prior to packed bed

Flow data from previous testing used to calculate Lb/Hr

| Run No.                                      | SC-4          | SC-5             | SC-6          |          |
|----------------------------------------------|---------------|------------------|---------------|----------|
| Date                                         | July 22, 1998 | July 22/23, 1998 | July 23, 1998 | AVERAGES |
| Start Time                                   | 2202          | 2335             | 102           |          |
| Stop Time                                    | 2302          | 35               | 202           |          |
| Barometric Pressure, in. Hg                  | 29.05         | 29.05            | 29.05         | 29.05    |
| Net Sampling Time, minutes                   | 30.0          | 30.0             | 30.0          | 30.0     |
| Volume Metered, cf                           | 15.415        | 15.415           | 15.415        | 15.415   |
| Avg. DGM Temp, F                             | 84.8          | 84.8             | 84.8          | 84.8     |
| AVG Delta H, in of H <sub>2</sub> O          | 2.00          | 2.00             | 2.00          | 2.00     |
| AVG Delta H, in of Hg                        | 0.1471        | 0.1471           | 0.1471        | 0.1471   |
| DGM Calibration Factor                       | 0.982         | 0.982            | 0.982         | 0.982    |
| Volume of Gas Collected, dscf                | 14.318        | 14.318           | 14.318        | 14.318   |
| Total Water Collected, mL                    | 8.7           | 8.7              | 8.7           | 8.7      |
| Volume of Water Vapor, scf                   | 0.410         | 0.410            | 0.410         | 0.410    |
| Moisture, %                                  | 2.79          | 2.79             | 2.79          | 2.79     |
| Dry Mole Fraction, 100-%M                    | 0.9721        | 0.9721           | 0.9721        | 0.9721   |
| CO <sub>2</sub> at Stack, % dry              | 5.1           | 4.9              | 2.6           | 4.2      |
| O <sub>2</sub> at Stack, % dry               | 19.0          | 19.2             | 19.8          | 19.3     |
| CO + N <sub>2</sub> , % dry                  | 75.9          | 75.9             | 77.6          | 76.5     |
| Dry Molecular Weight, lb/lb mole             | 29.57         | 29.55            | 29.21         | 29.45    |
| Wet Molecular Weight, lb/lb mole             | 29.25         | 29.23            | 28.90         | 29.13    |
| Stack Diameter, in                           | 6             | 6                | 6             | 6.00     |
| Stack Area, sq. in. (@ pitot meas. location) | 28.3          | 28.3             | 28.3          | 28.3     |
| Static Pressure, in. of H <sub>2</sub> O     | -10.40        | -10.40           | -10.40        | -10.40   |
| Stack Pressure, in. of Hg                    | 28.29         | 28.29            | 28.29         | 28.29    |
| Avg. Stack Temp., F                          | 73.8          | 73.8             | 73.8          | 73.8     |
| Avg. Sqroot of Delta P                       | 0.7346        | 0.7346           | 0.7346        | 0.7346   |
| SDE Average                                  | 16.972        | 16.972           | 16.972        | 16.972   |
| Pitot Coefficient                            | 0.84          | 0.84             | 0.84          | 0.84     |
| Stack Gas Velocity, afpm                     | 2542.7        | 2543.6           | 2558.1        | 2548.1   |
| Stack Flowrate, wet acfm                     | 499           | 499              | 502           | 500      |
| Stack Flowrate, dry scfm                     | 454           | 454              | 457           | 455      |
| Stack Flowrate, dry scf/hr                   | 27,231        | 27,240           | 27,396        | 27288.91 |
| Stack Flowrate, wet scf/hr                   | 2.8011E+04    | 2.8021E+04       | 2.8181E+04    | 28070.74 |
| NO <sub>x</sub> Lb/Hr                        | 0.0143        | 0.0055           | 0.0092        | 0.0097   |
| SO <sub>2</sub> Lb/Hr                        | 0.0562        | 0.0346           | 0.1098        | 0.0669   |
| CO Lb/Hr                                     | 0.0365        | 0.0358           | 0.0236        | 0.0320   |

IBP Dakota City Neb.

Inedible

Testing after the Heat Exchanger

| Run No.                                      | 1             | 2             | 3             |          |
|----------------------------------------------|---------------|---------------|---------------|----------|
| Date                                         | Sept 10, 1997 | Sept 10, 1997 | Sept 10, 1997 |          |
| Start Time                                   | 12:45         | 14:50         | 17:07         |          |
| Stop Time                                    | 13:45         | 15:50         | 17:57         | AVERAGES |
| Barometric Pressure, in. Hg                  | 29.26         | 29.26         | 29.26         | 29.26    |
| Net Sampling Time, minutes                   | 30.0          | 18.0          | 15.0          | 21.0     |
| Volume Metered, cf                           | 23.558        | 13.25         | 9.44          | 15.415   |
| Avg. DGM Temp, F                             | 79.0          | 86.70         | 88.80         | 84.8     |
| AVG Delta H, in of H2O                       | 2.00          | 1.70          | 1.40          | 1.70     |
| AVG Delta H, in of Hg                        | 0.1471        | 0.1250        | 0.1029        | 0.1250   |
| DGM Calibration Factor                       | 1.002         | 1.002         | 1.002         | 1.002    |
| Volume of Gas Collected, dscf                | 22.720        | 12.592        | 8.924         | 14.745   |
| Total Water Collected, mL                    | 188.0         | 664.0         | 528.0         | 460.0    |
| Volume of Water Vapor, scf                   | 8.864         | 31.308        | 24.895        | 21.689   |
| Moisture, % (%M is from Saturation Table)    | 2.8           | 2.8           | 2.8           | 2.8      |
| Dry Mole Fraction, 100-%M                    | 0.9717        | 0.9717        | 0.9717        | 0.9717   |
| CO2 at Stack, % dry                          | 0.0           | 0.0           | 0.0           | 0.0      |
| O2 at Stack, % dry                           | 20.9          | 20.9          | 20.9          | 20.9     |
| CO + N2, % dry                               | 79.1          | 79.1          | 79.1          | 79.1     |
| Dry Molecular Weight, lb/lb mole             | 28.84         | 28.84         | 28.84         | 28.84    |
| Wet Molecular Weight, lb/lb mole             | 28.53         | 28.53         | 28.53         | 28.53    |
| Stack Diameter, in                           | 6             | 6             | 6             |          |
| Stack Area, sq. in. (@ pitot meas. location) | 28.3          | 28.3          | 28.3          | 28.3     |
| Static Pressure, in. of H2O                  | -10.50        | -10.50        | -10.20        | -10.40   |
| Stack Pressure, in. of Hg                    | 28.49         | 28.49         | 28.51         | 28.50    |
| Avg. Stack Temp., F                          | 73.6          | 73.8          | 74.0          | 73.8     |
| Avg. Sqrroot of Delta P                      | 0.7740        | 0.7034        | 0.7263        | 0.7346   |
| SDE Average                                  | 17.879        | 16.251        | 16.784        | 16.971   |
| Pitot Coefficient                            | 0.84          | 0.84          | 0.84          | 0.84     |
| Stack Gas Velocity, afpm                     | 2702.5        | 2456.5        | 2535.9        | 2565.0   |
| Stack Flowrate, wet acfm                     | 531           | 482           | 498           | 504      |
| Stack Flowrate, dry scfm                     | 486           | 441           | 456           | 461      |
| Stack Flowrate, dry scf/hr                   | 29,147        | 26,484        | 27,351        | 27,661   |
| Stack Flowrate, wet scf/hr                   | 2.9996E+04    | 2.7255E+04    | 2.8148E+04    | 28,466   |

**TRC**













|                                                                               |                                                    |
|-------------------------------------------------------------------------------|----------------------------------------------------|
| Plant: IBP DAKOTA CITY, NE                                                    | Date: 9/10/97                                      |
| Unit Number: #2 COOKER INERT                                                  | Stack Diameter (in.): 6"                           |
| Load Condition: Norm                                                          | Stack Gauge Pressure (in. H <sub>2</sub> O): -10.2 |
| Run No.: 3                                                                    | Operators: DW, TL                                  |
| Project No.: 22214                                                            |                                                    |
| Barometric Pressure at Ground Level (in. Hg): 29.26                           |                                                    |
| Pitot Tube ID: 321                                                            |                                                    |
| Pitot Tube Coefficient: .84                                                   | Port Change Pitot Leak Check                       |
| Estimated Stack CO <sub>2</sub> : 0.2% <sup>20.9</sup> 11.0%: <u>Am Bient</u> | Pass                                               |
| Platform Elevation (feet): 8'                                                 | Fail                                               |
| Schematic of Stack Cross Section:                                             | Port #1                                            |
|                                                                               | Port #2                                            |
|                                                                               | Port #3                                            |
|                                                                               | Port #4                                            |
|                                                                               | $\sqrt{DP_{avg}} = .7263$                          |
|                                                                               | $T_{avg} = 74.0$                                   |

| Traverse Point Number | Velocity Head (in H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1                     | .22                                 | 74              |
| 2                     | .35                                 | 74              |
| 3                     | .40                                 | 75              |
| 4                     | .51                                 | 75              |
| 5                     | .49                                 | 75              |
| 6                     | .53                                 | 72              |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              |                                     |                 |

| Traverse Point Number | Velocity Head (in H <sub>2</sub> O) | Stack Temp. (F) |
|-----------------------|-------------------------------------|-----------------|
| 1                     | .22.51                              | 74              |
| 2                     | .30.55                              | 74              |
| 3                     | .51                                 | 74              |
| 4                     | .63                                 | 74              |
| 5                     | .85                                 | 73              |
| 6                     | .91                                 | 74              |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
|                       |                                     |                 |
| Average:              |                                     |                 |