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Background Report Reference

AP-42 Section Number: 9.9.1

Background Report Section: 2

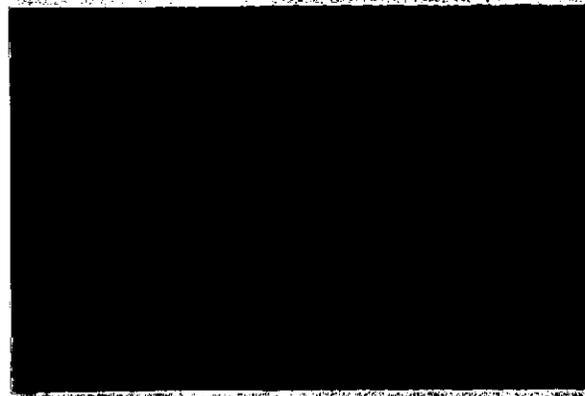
Reference Number: 37

**Title: Compliance Test Report for the
No. 15 Kiln Malt Dryer Exhaust**

Ladish Malting Company

December 1995

AP-42 Section 9.91
Reference
Report Sect. 2
Reference 37



AIR
SCIENCES &
ENGINEERING

**COMPLIANCE TEST REPORT FOR THE
NO. 15 KILN MALT DRYER EXHAUST**

LADISH MALTING COMPANY

**December 18, 1995
Project No. 95.502AQ**

**COMPLIANCE TEST REPORT FOR THE
DETERMINATION OF NONMETHANE
ORGANIC COMPOUND EMISSIONS FROM THE
NO. 15 KILN MALT DRYER EXHAUST**

Prepared for:

**LADISH MALTING COMPANY
N5355 East Junction Road
Jefferson Junction, WI 53549**

Prepared by:

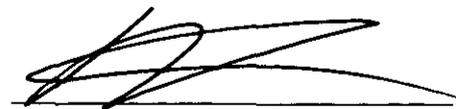
**Fluid Management, Inc.
Air Sciences & Engineering
Milwaukee, WI**

**December 1995
Project No. 95.502AQ**

Prepared by:


**Michael B. Weiner
Senior Scientist**

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Reviewed by:


**JoAnna M. Ferdzock
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1.0 INTRODUCTION

Fluid Management, Inc. ("FMI") was retained by Ladish Malting Company ("Ladish") to conduct compliance emissions testing at its facility located in Jefferson Junction, Wisconsin.

Methane and nonmethane organic compound ("NMOC") emission testing was performed on the No. 15 kiln while processing barley. The No. 15 kiln is one of Ladish's largest kilns. No. 15 kiln has two (2) floors and represents a "worst case" scenario for potential nonmethane hydrocarbon emissions. The kiln is heated by indirect natural gas-fired kiln propylene glycol heaters. During the test, approximately 7,000 bushels of barley were dried on each of two (2) floors. The upper floor malt goes from 45-48 percent moisture to 15-20 percent moisture, while the lower floor goes from 15-20 percent moisture to 3.5-4.3 percent moisture during the 24 hour cycle. The total amount of barley dried during the testing event was recorded by Ladish and used by FMI to determine the emission factor for NMOCs being emitted.

All testing was performed in accordance with the United States Environmental Protection Agency ("U.S. EPA") and Wisconsin Department of Natural Resources ("WDNR") source testing methodologies. Testing was conducted in accordance with a compliance test plan submitted to Mr. James Crawford of the WDNR on September 26, 1995. The only notable deviation from the methodologies described in the original compliance test plan was a change in sampling and analytical methodologies from U.S. EPA Reference Method 25A using a total hydrocarbon analyzer to U.S. EPA Reference Method 18 using an on-site gas chromatograph ("GC"). This change was determined to be necessary due to anticipated extremely low concentrations of NMOCs in the exhaust stack gas and was done with the approval of the WDNR. The instrumentation utilized for U.S. EPA Reference Method 18 testing has a reported lower level of detection of less than 0.10 parts per million by volume ("ppmv") total hydrocarbon. Testing was completed by Messrs. Michael Weiner and Jeffrey Anderson of FMI's Air Science and Engineering Group on November 14 and 15, 1995. Production coordination was conducted by Mr. Roger Ziegler and process data collection was conducted by Ms. Gail Smith of Ladish. All compliance testing was witnessed by Mr. James Crawford of the WDNR.



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APR 3 1996
LAKE MICH. DIST.

April 1, 1996

VIA CERTIFIED MAIL RETURN RECEIPT

Mr. James G. Crawford, P.E.
Wisconsin Department of Natural Resources
1125 N. Military Avenue
P.O. Box 10448
Green Bay, WI 54307-0448

**RE: LADISH MALTING COMPANY
COMPLIANCE TEST REPORT FOR THE DETERMINATION OF
NON-METHANE ORGANIC COMPOUND EMISSIONS FROM THE
NO. 15 KILN MALT DRYER EXHAUST
Project No. 95.502AQ**

Dear Mr. Crawford:

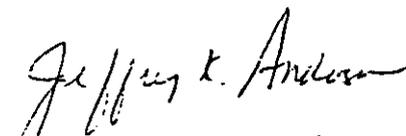
Please find enclosed a copy of two (2) gas chromatograms. The first chromatogram demonstrates the position of a standard propylene glycol peak. The second is a blank water sample used as a method blank. Both samples were run on an SPB-5 column identical to that used during the November testing.

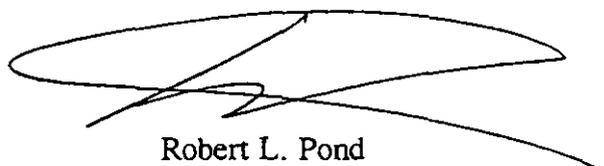
Also included is an example of one (1) of the testing event chromatograms with the relative position of a propylene glycol peak superimposed. Having reviewed the chromatograms included in the test report, and comparing them to the propylene glycol standard, it is evident that no measurable amounts of propylene glycol were contained within any of the sample bags. The sample corresponding to Run No. 2, Fan No. 2, indicates a peak in the general location of propylene glycol, but is most likely water, which also shows a peak in close proximity to propylene glycol. This peak shows concentrations just slightly over the detection limit, and does not show the characteristic sharpness of a standard propylene glycol peak.

We hope this additional information clears up any previous questions or concerns. If you have any further questions or require additional information, please contact us at (414) 549-6898.

Sincerely,

FLUID MANAGEMENT, INC.

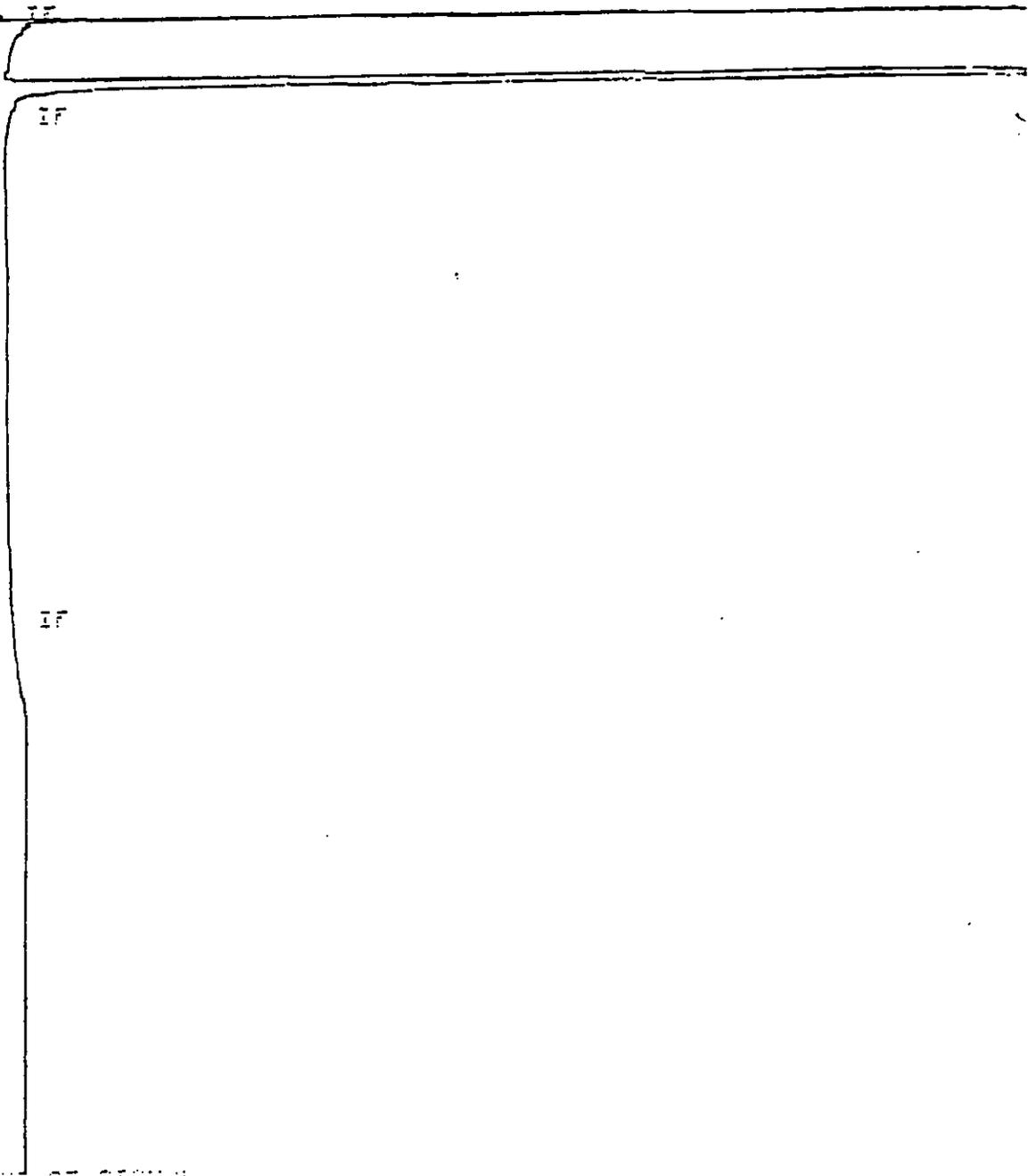

Jeffrey K. Anderson,
Project Chemical Engineer


Robert L. Pond
Principal Engineer

Enclosures

cc: Mr. George Groskopf, Ladish Malting Company
Mr. John Renz, Ladish Malting Company
Mr. Roger Ziegler, Ladish Malting Company

21001



Propylene Glycol.

END OF SIGNAL

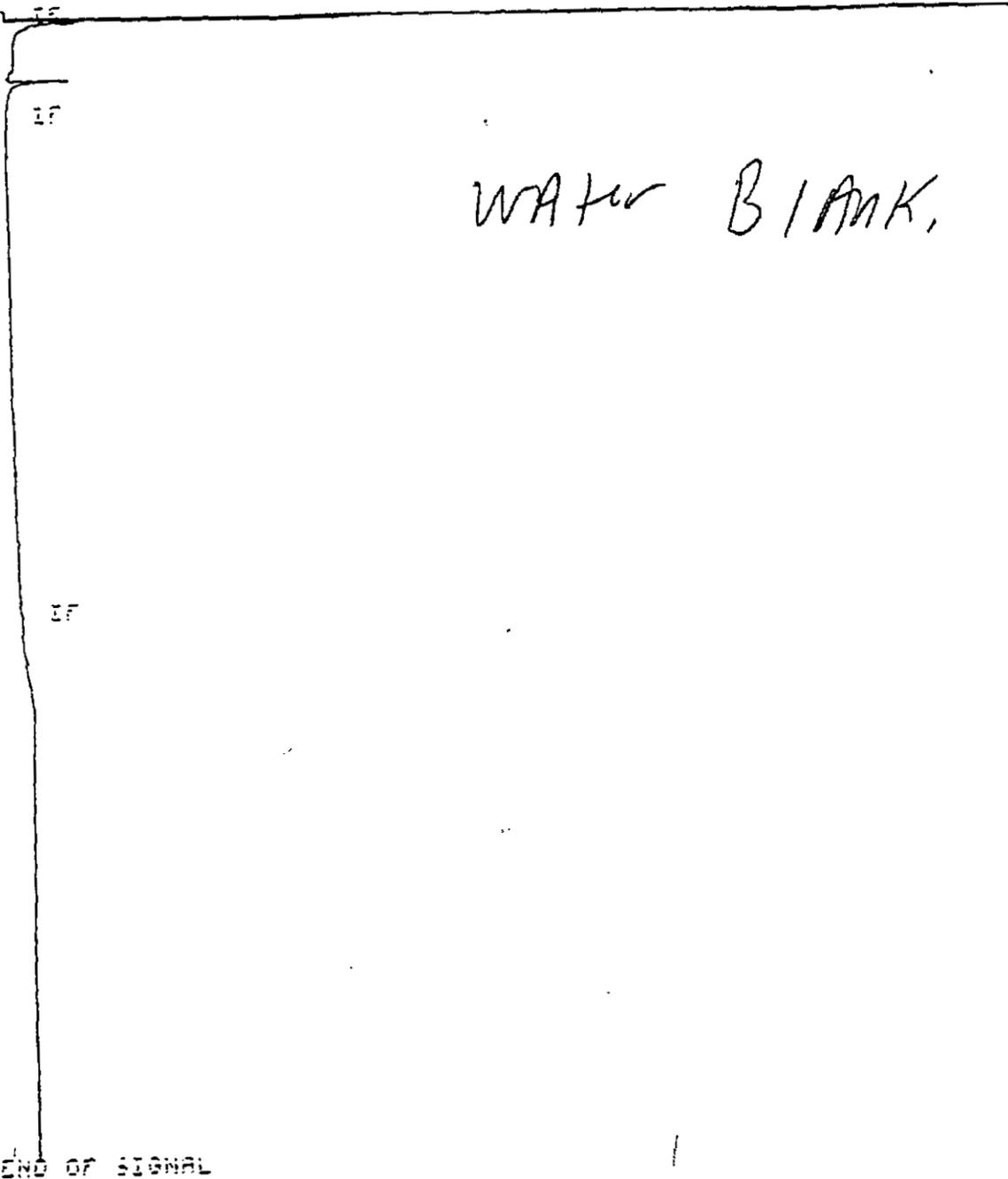
BUFFERED RUN# 573 MAR 26, 1998 14:27:23

SAMPLE NAME: 857 SAMPLE# 57
METHOD NAME: M-EXTB.MET
PROPYLENE GLYCOL

EXTRACTABLE HYDRO FROM ORANGE

NO RUN PEAKS STORED

START BUFFERED RUN# 572 MAR 26, 1996 15:42:37



WATER BLANK

END OF SIGNAL

BUFFERED RUN# 572 MAR 26, 1996 15:42:37

SAMPLE# 00

METHOD NAME: HPLC.MET
H2O

EXTRACTABLE HYDRO FRONT ORANGE

NO RUN PEAKS STORED

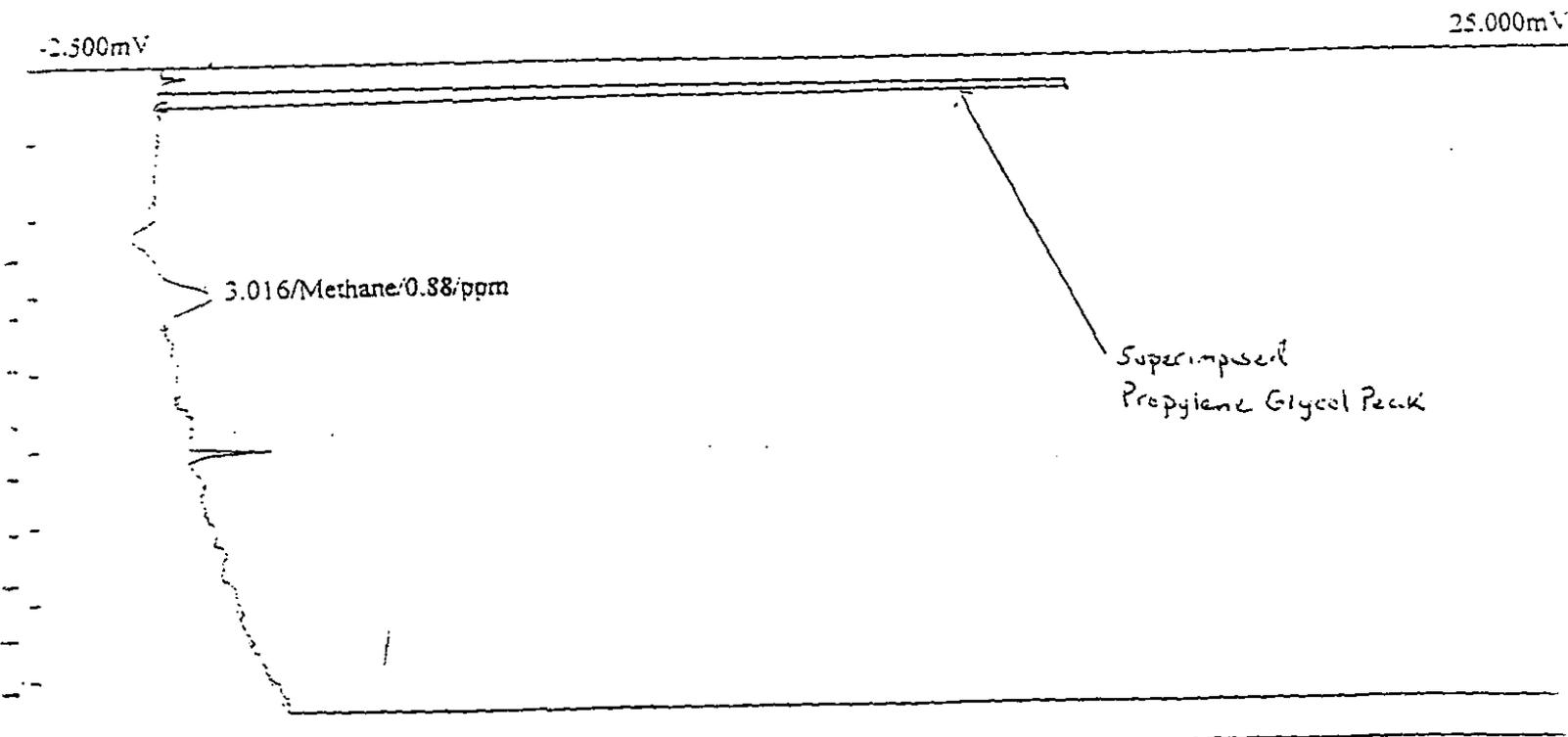
Job name: Fluid Management, Inc.
 Client: Ladish Malting Co.
 Client ID: 395.502AQ
 Collected: 11/14/95
 Analysis date: 11/15/1995 14:33:04
 Method: Mod. USEPA Method 18
 Description: Ch. 1 FMI-FID
 Column: 3' Silica Gel
 Carrier: N2 at 300 on dial
 Temp. prog: FMI.TEM
 Components: FMI.CPT
 Control file: DEFAULT.CON
 Data file: F1R62.CHR (c:\peakwin)
 Sample: Fan #1 Run #6
 Operator: Michael B. Weiner
 Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

Temp	Hold	Ramp	Final temp
	1.000	10.000	130

Components:

Peak Name	Start	End	Calibration	Int. Std	Units
Methane	2.850	3.150	CH4.CAL	0.000	ppm
Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
Methane	3.016	28.154	0.88	ppm
		28	1	

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December 19, 1995

VIA CERTIFIED MAIL RETURN RECEIPT

Mr. Jim Crawford
Wisconsin Department of Natural Resources
1125 North Military Avenue, Box 10448
Green Bay, WI 54307

**RE: LADISH MALTING COMPANY
COMPLIANCE TEST REPORT
Project No. 95.502AQ**

Dear Mr. Crawford:

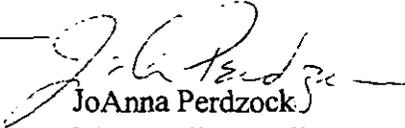
Enclosed please find three (3) copies of the compliance test report for the determination of non-methane organic compound emissions from the No. 15 kiln malt dryer exhaust at Ladish Malting Company.

If you have any questions, please contact us at (414) 291-8282.

Sincerely,

FLUID MANAGEMENT, INC.
Air Sciences & Engineering


Robert A. Schilling
Project Engineer


JoAnna Perdsock
Manager/Source Testing & Analysis

cc: Mr. John Renz, Ladish Malting Company
Mr. George Groskopf, Ladish Malting Company

250 East Wisconsin Avenue
Suite 1000
Milwaukee, Wisconsin 53202
Tel: (414) 291-8282
Fax: (414) 291-8299

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2.0 PROCESS DESCRIPTION

Ladish receives barley by rail. The malt is loaded out in an enclosed area. From the receiving area, barley is conveyed via a bucket elevator to the top of the elevator. The barley is then screened and separated to proper sizes. The barley that does not meet the size specification is conveyed to the palletizing area. The rest of the barley is conveyed to the steeping tanks. The barley is rinsed several times in the steeping tanks. Next, the barley is dumped into compartments, and is then moved by screw conveyor to one (1) of nine (9) kilns. The heat is provided to the kilns by six (6) indirect natural gas-fired kiln heaters, each with a maximum heat input rating of sixty (60) mmBtu/hr. The kilns are typically comprised of three (3) levels, and the barley spends a predetermined amount of time at each level of the kiln. The barley enters the kilns at approximately forty-five (45) percent moisture content, and leaves at approximately four (4) percent moisture content. While in the kiln, the barley is converted from barley to malted barley. The malted barley is then transported by a screw conveyor to a storage elevator until it is needed for shipping. Additional process steam requirements are met by a seventy-five (75) horsepower Cleaver-Brooks package boiler.

Testing was conducted on the No. 15 kiln. The No. 15 kiln was processing malt during the testing event. Typically, the malt will spend twenty-four (24) hours on each level of the kiln. The No. 15 kiln is heated by a Somerset Technologies, Inc., sixty (60) mmBtu/hr indirect natural gas-fired propylene glycol heater. Sulfur is burned below the kiln, in a stove exhausting directly into the kiln. The fan speed will be set on high for the start of the testing. Fan speed is changed (lowered) as the malt becomes dryer by continuously monitoring the relative humidity and relaying the signal to the PCL which controls the fan speed during the cycle. The following schedule was followed during the testing program:

- 7:00 am - 7:30 pm holding heats
- 7:30 pm- 8:30 pm first high heat
- 8:30 pm- 12:30 am second high heats
- 12:30 am- 1:00 am cool down
- 1:00 am kiln dumped
- 1:30 am- 3:00 am upper floor is empty
- 3:30 am- 5:00 am upper floor is being loaded

Ladish personnel were responsible for operating the process and monitoring the operation during the testing event. Appendix A presents calculations for volumetric flowrates from field data included in Appendix B of this report. Appendix C contains sample chromatograms from the six (6) runs performed on the five (5) fan malt dryer exhausts. Appendix D contains calibration and certification data for the testing program. Process data collected during the testing program is included in Appendix E of this report. Appendix F contains a listing of key personnel involved in the project.

3.0 SUMMARY OF RESULTS

Summaries of the nonmethane organic compound emission test results for each fan malt dryer exhaust are presented in Table Nos. 1 through 5. Included in these tables are the results for stack gas temperature (°F), stack gas velocity in feet per second (“ft/sec”), volumetric flowrate in actual cubic feet per minute (“acfm”), methane concentration in parts per million by volume (“ppmv”), and nonmethane organic compound concentration in parts per million by volume (as propane) (“ppmvp”).

Table No. 6 presents the overall summary of stack gas parameters for the five (5) fan malt dryer exhaust ducts of Kiln No. 15. The average stack gas temperature for the ducts over the entire drying cycle was determined to be 73.5 °F. Average stack gas velocity of the outlet ducts over the entire cycle was determined to be 157.28 ft/sec. The average volumetric flowrate of the outlet ducts over the entire drying cycle was determined to be 197,573 acfm. For the purposes of determining emission rates, the true volumetric flowrates were used for all exhaust stacks tested.

Table No. 7 presents the summary of methane concentrations (in terms of ppmv), nonmethane organic compound concentrations (in terms of ppmvp), and emission rates (in terms of pounds per hour as carbon) for the five fan malt dryer exhaust ducts of Kiln No. 15. The NMOC concentrations and emission rates were found to be:

- **Run No. 1 - < 0.35 ppmv (as propane), < 0.45 lb/hr (as carbon)**
- **Run No. 2 - < 0.35 ppmv (as propane), < 0.61 lb/hr (as carbon)**
- **Run No. 3 - < 0.35 ppmv (as propane), < 0.50 lb/hr (as carbon)**
- **Run No. 4 - < 0.35 ppmv (as propane), < 0.20 lb/hr (as carbon)**
- **Run No. 5 - < 0.35 ppmv (as propane), < 0.23 lb/hr (as carbon)**
- **Run No. 6 - < 0.35 ppmv (as propane), < 0.34 lb/hr (as carbon)**

The average NMOC concentration and emission rate of organic compounds from the five fan malt drying exhausts was determined to be < 0.35 ppmv (as propane) and < 0.39 lb/hr (as carbon).

4.0 SAMPLING AND ANALYTICAL PROCEDURES

The following sampling and analytical procedures were used during this testing program.

4.1 Exhaust Gas Parameters

Determination for velocity pressures, temperature, gas density, and moisture in the exhaust gas stream was performed in accordance with U.S. EPA Reference Methods 1 through 3.

4.1.1 Traverse and Sampling Points

The number of traverse points for the exhaust stacks was determined using U.S. EPA Reference Method 1, "*Sampling and Velocity Traverses for Stationary Sources.*" The No. 15 Kiln fan room has five (5) fans each with six (6) sampling locations located three (3) diameters upstream and two (2) diameters downstream from the flow disturbance. They are located on the floor above the two (2) separate barley drying floors. Figure No. 1 visually depicts a typical fan with these ducts along with the sample port locations. Based on the configuration of the stacks, thirty-six (36) sample points [six (6) per traverse] were used for each fan. These five (5) fan exhaust stacks were used for velocity determinations.

4.1.2 Velocity Traverse

A velocity traverse was performed for each fan during each of the tests in accordance with U.S. EPA Reference Method 2, "*Determination of Stack Gas Temperature and Velocity (Type S Pitot Tube).*" An "S" type pitot tube with an attached "K" type thermocouple was used in conjunction with an oil-filled manometer to conduct the velocity traverses.

4.1.3 Molecular Weight of Stack Gas

The determination of molecular weight of the stack gas was made in accordance with U.S. EPA Reference Method 3, "*Gas Analysis for the Determination of Dry Molecular Weight.*" An integrated gas sample will be collected during each test and analyzed for oxygen and carbon dioxide with a Fyrite analyzer. Nitrogen was determined by difference.

4.2 Nonmethane Organic Compound ("NMOC")

Nonmethane organic compound ("NMOC") emissions were determined in accordance with applicable sections of U.S. EPA Reference Method 18, Section 7.1, "*Determination of Gaseous Organic Compound Emissions Using a Gas Chromatograph (Flexible Bag Sampling Method)*". Six (6) discrete, one (1) hour continuously collected samples were taken from each of five (5) fans during the testing event. All samples were one (1) hour in duration. NMOC measurements were made in the malt dryer exhaust fan stacks on the top floor of the kiln, after the gas has been passed through the propylene glycol heat exchangers, and just before it is exhausted into the atmosphere.

The concentration of NMOCs in each gas stream were extracted and measured according to the requirements and procedures of U.S. EPA Reference Method 18. The method principle is that a gas sample is extracted from the emission source; transported to a mobile laboratory; and then an aliquot of the sample gas is then analyzed for NMOCs by gas chromatography ("GC") utilizing a GC column for compound separation and flame ionization detection ("FID").

The sample was injected onto the analytical column by compression of the Tedlar bag inserted into the sample inlet of a heated, electrically actuated, 10-port Valco valve. Separation of methane and nonmethane organic compound was accomplished by utilizing a SPB-5 3 feet x 0.53 millimeter silica gel column capable of back flush. Temperature ramping was utilized to aid in the elution of the compounds and decrease the sample run time on the GC. Separation of the compounds was accomplished in approximately ten (10) minutes. The GC used was a SRI Instruments, Inc. Model 8610A equipped with a FID, with output directed through a serial port to a notebook computer. Integration, interpretation, manipulation, and storage was performed by gas chromatograph software - PeakSimple for Windows ®, version 1.20. All chromatograms are maintained as a permanent record of each project.

The GC system was field calibrated for each compound using a mixed compound calibration gas generated in accordance with U.S. EPA Reference Method 18 protocol for the preparation of gaseous standards by dynamic dilution of cylinder gas with oxygen-free nitrogen. Before testing began, the GC was checked thoroughly for proper operation. A standard gas was injected several times to verify compound retention times and to check

peak area with previously obtained calibration curves. Calibration curves were prepared before each test began and verified periodically. Calibration points were constructed daily. Each gas concentration was injected at least three times to ensure instrument stability. The resulting calibration curves were produced from the mean response of three (3) injections of at least three (3) concentrations. Each calibration point is considered valid when the mean peak area of three successive injections does not differ by more than five (5) percent from the peak areas contributing to the mean.

Data reduction was accomplished by referral to calibration curves generated from the analysis of known concentrations. Calibration curves fit the general equation of $Y = mX + b$. Coefficients of this equation were determined using the PeakSimple for Windows software which was programmed with a linear regression least-squares program to give the best fit of the points. Correlation coefficients (R^2 values) are typically 0.98 or better.

The NMOC measurement system consisted of the following:

- a flexible Tedlar bag sampling system to collect exhaust gas from the centrally located ten (10) percent area of the stack cross-section;
- a heated, electrically-actuated 10-port sampling valve;
- a gas chromatograph equipped with a flame ionization detector;
- a silica gel column equipped with back-flush capabilities for component separation;
- a personal notebook computer equipped with a serial port for recording measurement data;
- high purity nitrogen with less than 0.25 percent of NMOCs;
- a series of calibration gases with a concentration equivalent to the applicable exhaust value; and
- gas chromatography software capable of generating calibration curves and storage of analytical data.

The GC was calibrated in accordance with the prescribed methodology. Calibrations were performed at the beginning and end of the testing. U.S. EPA Protocol 1 gases were used for all calibrations and preparation of dynamically diluted standards.

5.0 QUALITY ASSURANCE PROGRAM

5.1 QA/QC Procedures and Results

The objectives of a quality assurance/quality control ("QA/QC") program is to assure that the precision and accuracy of all environmental data generated by FMI are commensurate with data quality objectives ("DQOs"). DQOs are based on a common understanding of the intended end use(s) of the data, the measurement process, and the availability of resources. Once DQOs are established, formally or informally, QA/QC protocol can be defined for the measurements.

The DQOs in this project are to provide defensible data that can be used for determination of NMOC emission rates. The final data user will be Ladish and the WDNR.

The goal of a QA/QC program is that data generated and used for decision-making are scientifically sound, of known quality, and documented to be "in control." To accomplish this goal, standardized methods or procedures are used whenever possible. They must be validated for their intended use, rigorously followed, and data reported with quality indicators (precision, accuracy, completeness, etc.).

Two (2) basic concepts used in a QA/QC program are to:

1. Control errors; and
2. Verify that the entire Sampling and Analytical ("S&A") method is operating within acceptable performance limits.

Use of qualified personnel, reliable and well-maintained equipment, appropriate calibrations and standards, and close supervision of all operations are important components of the QA/QC system. QA/QC in this test program included the use and documentation of calibrated sampling and analytical instruments, use of U.S. EPA validated methods (U.S. EPA 40 CFR Part 60), adherence to established protocol, method blanks as a check against possible contamination, sample chain-of-custody documentation, and redundant data calculation with checking.

5.1.1 Equipment Quality Control

All of the equipment used was calibrated according to procedures outlined in the Quality Assurance Handbook for Air Pollution Measurement System, Volume III, EPA-600/4-77-027b. Actual calibration data sheets are provided in Appendix D.

5.1.2 Volumetric Flow

5.1.2.1 Barometer

Barometric pressure values for the testing period were recorded from a calibrated barometer on-site and verified by telephone from a local airport and were corrected for elevation to stack sample port level (0.01 inches Hg per 10 ft. elevation).

5.1.2.2 Pitot Tubes

Each pitot tube used in sampling meets the design specifications for type-S pitot tubes in U.S. EPA Method 2. Therefore, a maximum value baseline coefficient (“ C_p ”) of 0.84 is assigned to each pitot tube. Calibration at the manufacturer for pitot face-opening alignment included measuring the external tubing diameter (dimension “ D_t ”), the base-to-opening plane distance (dimensions “ P_a ” and “ P_b ”), and the face opening misalignment angles, with all terms as described in Figures 2-2 and 2-3 of U.S. EPA Method 2. Pitot tubes were visually inspected at the completion of the test to insure structural integrity.

5.1.2.3 Calibration Meter and Metering System

The secondary reference meter equipment arrangement for calibration is shown in Figure 5.7 of U.S. EPA Method 5. The prescribed procedures were followed. A wet test meter with a 1 cubic feet per revolution (“ ft^3/rev ”) capacity and ± 1 percent accuracy is used as the primary calibrant. The dry gas meter's pump is operated for a minimum of five (5) minutes at a flow rate of 0.35 cubic feet per minute (“ cfm ”) to condition the interior surface of the wet test meter. Leak checks are performed and if satisfactory, triplicate runs at each of no less than five (5) different flow rates are performed. A calibration curve is prepared and the meter is recalibrated after two hundred (200) hours of operation or annually, whichever comes first.

The calibration set-up for the dry gas metering system using the secondary reference meter in lieu of the wet test meter is given in Figure 5.5 of U.S. EPA Method 5. A leak check of the metering system before calibration was performed as shown in Figure 5.4 of U.S. EPA Method 5. The metering system's pump is operated for five (5) minutes at an orifice manometer setting of 0.5 inches H₂O to heat up the pump and system to stabilize the meter inlet and outlet temperatures. Values for the orifice setting ("ΔH"), wet test meter volume ("V_w"), corresponding dry test meter volume ("V_d"), dry test meter inlet and outlet gas temperatures ("t_{di}" and "t_{dn}"), and time are recorded for the initial calibration. The ratio of the wet test meter to the dry test meter ("gamma") and the orifice pressure differential that equates to 0.75 cubic feet per minute ("cfm") at standard conditions ("ΔH@") are then calculated.

5.1.2.4 Thermocouples and Digital Indicators

Thermocouples are calibrated by comparison to an American Standards for Testing and Materials ("ASTM") Method-3F mercury-in-glass thermometer at approximately 32° F (ice water), ambient temperature and approximately 100° F (hot oil). Each thermocouple is calibrated against temperature ranges to which it is typically exposed during test conditions, and they must agree within 1.5 percent (expressed in degrees Rankine ["°R"]) of the reference thermometer throughout the entire calibration range.

Digital indicators are checked by introducing a series of millivolt signal strengths to the input and comparing the indicator reading with the actual signal strength. Acceptable calibration error must not exceed 0.5 percent when temperatures are expressed in °R.

5.1.2.5 Analytical Balance

The analytical balance was calibrated by comparing its readings against National Institute of Standards and Technology ("NIST"), formerly known as the National Bureau of Standards ("NBS"), traceable Class-S1 standard weights, with acceptable agreement within 0.5 milligram ("mg").

5.1.2.6 Replicates and Precision

Replicate samples of NMOCs are not possible due to the nature of continuous emission sampling. In addition, no analytical precision estimate can be determined.

Precision and accuracy are quantitative measures that characterize the amount of variability and bias inherent in a given data set. Precision refers to the level of agreement among repeated measurements of the same parameter. Accuracy refers to the difference between an estimate based on the data and the true value of the parameter being estimated. The error due to measurement variability for sulfur dioxide concentration can be as much as ± 10.4 percent of concentration (intralab precision determined by U.S. EPA during collaborative method validation tests). Accuracy for NMOC concentration cannot be determined because no "true" concentration can be created to estimate accuracy. Instead, documentation of equipment calibration is used to establish traceability as a surrogate for accuracy of NMOC measurements.

5.1.3 Nonmethane Organic Compound

The GC used in this series of tests was calibrated according to the methodologies described in 40 CFR, Part 60, Appendix A, Method 18. Measurement system performance specifications followed during the testing program in accordance with U.S. EPA Method 18, included the following:

- analyzer calibration error of less than ± 2 percent of the span value for zero, mid, and high-range calibration gases;
- sampling system bias of less than ± 5 percent of the span value for zero, and mid- or high-range calibration gases;
- zero drift of less than ± 3 percent of the span value over the period of the run; and
- calibration drift of less than ± 3 percent of span value over the period of the run.

All calibration gases utilized during the testing program will be U.S. EPA Protocol 1 gases, certified in accordance with Method G1, "*Traceability Protocol for Establishing True Concentrations of Gases Used for Calibration and Audits of Continuous Source Emission Monitors (Protocol No. 1)*." Additionally, the certification of the cylinders provides a recommended shelf life for each calibration gas cylinder over which the concentration does not change more than ± 2 percent from the certified value. Cylinder gas certifications were available during the testing event.

6.0 REGULATORY REVIEW

Ladish was issued a Synthetic Minor Non-Part 70 operating permit (Permit No. 128002930.F01) on June 14, 1995. The operating permit does not specify specific emissions limitations for volatile organic compound emissions from the malt kilns (Process P28). However, the malt kilns are subject to the general permit conditions found in Part II of the operating permit. The general emissions limits for organic compounds as listed in Part II, section C, are as follows:

4. *No person may cause, allow or permit organic compound emissions into the ambient air which substantially contribute to the exceeding of an air standard or cause air pollution (s. NR 419.03, Wis. Adm. Code).*

Additionally, Chapter NR 424 of the Wisconsin Administrative Code regulates emissions of organic compounds from process lines. Pursuant to § NR 424.03(1)(a)4, Wis. Adm. Code, all process lines emitting less than 15 pounds of organic compounds in any day and 3.1 pounds of organic compounds in any hour are exempt from the requirements of Chapter NR 424.

The measured emission rates of organic compounds from the malt kilns are below the limitations specified in the operating permit and are exempt from the requirements of Chapter NR 424, Wisconsin Administrative Code.

TABLE NO. 1
Summary of Exhaust Gas Parameters for the
Fan No. 1 Malt Dryer Exhaust of Kiln No. 15 at
Ladish Malting Company

Source I.D.	Stack Gas Temperature (°F)	Stack Gas Velocity (ft/sec)	Stack Gas Flowrate (acfm)	Methane Concentration (ppmv)	NMOC Concentration (ppmvp)
Fan 1 Run 1	71.1	33.54	42,131	0.72	<0.07
Fan 1 Run 2	72.8	49.75	62,498	0.84	<0.07
Fan 1 Run 3	69.5	38.71	48,633	0.72	<0.07
Fan 1 Run 4	73.3	15.41	19,357	0.58	<0.07
Fan 1 Run 5	73.7	18.34	23,042	1.37	<0.07
Fan 1 Run 6	73.7	18.34	23,042	0.88	<0.07
Average	72.4	29.02	36,451	0.85	<0.07

NMOC: Nonmethane organic compound.
°F: Degrees Fahrenheit.
ft/sec: Feet per second.
acfm: Actual cubic feet per minute.
ppmv: Parts per million by volume, wet basis.
ppmvp: Parts per million by volume, wet basis, as propane.
<: Indicates a nondetectable concentration.

TABLE NO. 2
Summary of Exhaust Gas Parameters for the
Fan No. 2 Malt Dryer Exhaust of Kiln No. 15 at
Ladish Malting Company

Source I.D.	Stack Gas Temperature (°F)	Stack Gas Velocity (ft/sec)	Stack Gas Flowrate (acfm)	Methane Concentration (ppmv)	NMOC Concentration (ppmvp)
Fan 2 Run 1	72.7	37.18	46,710	0.73	<0.07
Fan 2 Run 2	71.9	48.64	61,100	0.73	<0.07
Fan 2 Run 3	71.2	38.90	48,865	0.64	<0.07
Fan 2 Run 4	72.4	15.07	18,926	1.15	<0.07
Fan 2 Run 5	74.0	17.14	21,529	0.54	<0.07
Fan 2 Run 6	77.7	25.25	31,720	1.54	<0.07
Average	73.3	30.36	38,141	0.89	<0.07

NMOC: Nonmethane organic compound.
°F: Degrees Fahrenheit.
ft/sec: Feet per second.
acfm: Actual cubic feet per minute.
ppmv: Parts per million by volume, wet basis.
ppmvp: Parts per million by volume, wet basis, as propane.
<: Indicates a nondetectable concentration.

TABLE NO. 3
Summary of Exhaust Gas Parameters for the
Fan No. 3 Malt Dryer Exhaust of Kiln No. 15 at
Ladish Malting Company

Source I.D.	Stack Gas Temperature (°F)	Stack Gas Velocity (ft/sec)	Stack Gas Flowrate (acfm)	Methane Concentration (ppmv)	NMOC Concentration (ppmvp)
Fan 3 Run 1	73.7	37.76	47,430	0.80	<0.07
Fan 3 Run 2	74.8	53.55	67,212	1.22	<0.07
Fan 3 Run 3	72.2	43.02	54,044	0.65	<0.07
Fan 3 Run 4	72.5	17.70	22,230	0.75	<0.07
Fan 3 Run 5	73.4	20.24	25,423	0.94	<0.07
Fan 3 Run 6	71.5	40.93	51,414	0.89	<0.07
Average	73.0	35.53	44,636	0.88	<0.07

NMOC: Nonmethane organic compound.
°F: Degrees Fahrenheit.
ft/sec: Feet per second.
acfm: Actual cubic feet per minute.
ppmv: Parts per million by volume, wet basis.
ppmvp: Parts per million by volume, wet basis, as propane.
<: Indicates a nondetectable concentration.

TABLE NO. 4
Summary of Exhaust Gas Parameters for the
Fan No. 4 Malt Dryer Exhaust of Kiln No. 15 at
Ladish Malting Company

Source I.D.	Stack Gas Temperature (°F)	Stack Gas Velocity (ft/sec)	Stack Gas Flowrate (acfm)	Methane Concentration (ppmv)	NMOC Concentration (ppmvp)
Fan 4 Run 1	75.8	39.17	49,206	0.90	<0.07
Fan 4 Run 2	74.3	52.11	65,461	0.72	<0.07
Fan 4 Run 3	72.1	43.42	54,542	1.08	<0.07
Fan 4 Run 4	74.3	17.13	21,525	0.80	<0.07
Fan 4 Run 5	75.1	20.35	25,560	1.14	<0.07
Fan 4 Run 6	77.5	29.62	37,206	0.93	<0.07
Average	74.9	33.63	42,250	0.93	<0.07

NMOC: Nonmethane organic compound.
 °F: Degrees Fahrenheit.
 ft/sec: Feet per second.
 acfm: Actual cubic feet per minute.
 ppmv: Parts per million by volume, wet basis.
 ppmvp: Parts per million by volume, wet basis, as propane.
 <: Indicates a nondetectable concentration.

TABLE NO. 5
Summary of Exhaust Gas Parameters for the
Fan No. 5 Malt Dryer Exhaust of Kiln No. 15 at
Ladish Malting Company

Source I.D.	Stack Gas Temperature (°F)	Stack Gas Velocity (ft/sec)	Stack Gas Flowrate (acfm)	Methane Concentration (ppmv)	NMOC Concentration (ppmvp)
Fan 5 Run 1	73.8	32.90	41,334	0.79	<0.07
Fan 5 Run 2	73.7	44.60	56,031	0.68	<0.07
Fan 5 Run 3	71.3	36.90	46,351	0.74	<0.07
Fan 5 Run 4	74.5	15.01	18,850	0.83	<0.07
Fan 5 Run 5	76.2	17.42	21,885	0.92	<0.07
Fan 5 Run 6	73.2	25.57	32,120	0.94	<0.07
Average	73.8	28.73	36,095	0.82	<0.07

NMOC: Nonmethane organic compound.
°F: Degrees Fahrenheit.
ft/sec: Feet per second.
acfm: Actual cubic feet per minute.
ppmv: Parts per million by volume, wet basis.
ppmvp: Parts per million by volume, wet basis, as propane.
<: Indicates a nondetectable concentration.

TABLE NO. 6
Overall Summary of the Five Fan
Malt Dryer Exhausts of Kiln No. 15 at
Ladish Malting Company

Source I.D.	Average Stack Gas Temperature (°F)	Total Stack Gas Velocity (ft/sec)	Total Stack Gas Flowrate (acfm)	Total Methane Concentration (ppmv)	Total NMOC Concentration (ppmvp)
Run 1	73.4	180.55	226,811	3.94	<0.35
Run 2	73.5	248.65	312,362	4.19	<0.35
Run 3	71.3	200.95	252,435	3.83	<0.35
Run 4	73.4	80.32	100,888	4.11	<0.35
Run 5	74.5	93.49	117,439	4.91	<0.35
Run 6	74.7	139.71	175,502	5.18	<0.35
Average	73.5	157.28	197,573	4.36	<0.35

NMOC: Nonmethane organic compound.
°F: Degrees Fahrenheit.
ft/sec: Feet per second.
acfm: Actual cubic feet per minute.
ppmv: Parts per million by volume, wet basis.
ppmvp: Parts per million by volume, wet basis, as propane.
<: Indicates a nondetectable concentration.

TABLE NO. 7
Summary of NMOC Emission Rates for the
Five Fan Malt Dryer Exhausts of Kiln No. 15 at
Ladish Malting Company

Source ID.	Total Methane Concentration (ppmv)	Total NMOC Concentration (ppmvp)	NMOC Emission Rate (lb/hr)
Run 1	3.94	<0.35	<0.45
Run 2	4.19	<0.35	<0.61
Run 3	3.83	<0.35	<0.50
Run 4	4.11	<0.35	<0.20
Run 5	4.91	<0.35	<0.23
Run 6	5.18	<0.35	<0.34
Average	4.36	<0.35	<0.39

NMOC: Nonmethane organic compound.
ppmv: Parts per million by volume, wet basis.
ppmvp: Parts per million by volume, wet basis, as propane.
lb/hr: Pounds per hour, as carbon.
<: Indicates a nondetectable concentration, lower level of detection used for emission rate calculation.

FIGURES

Heat Recovery Floor

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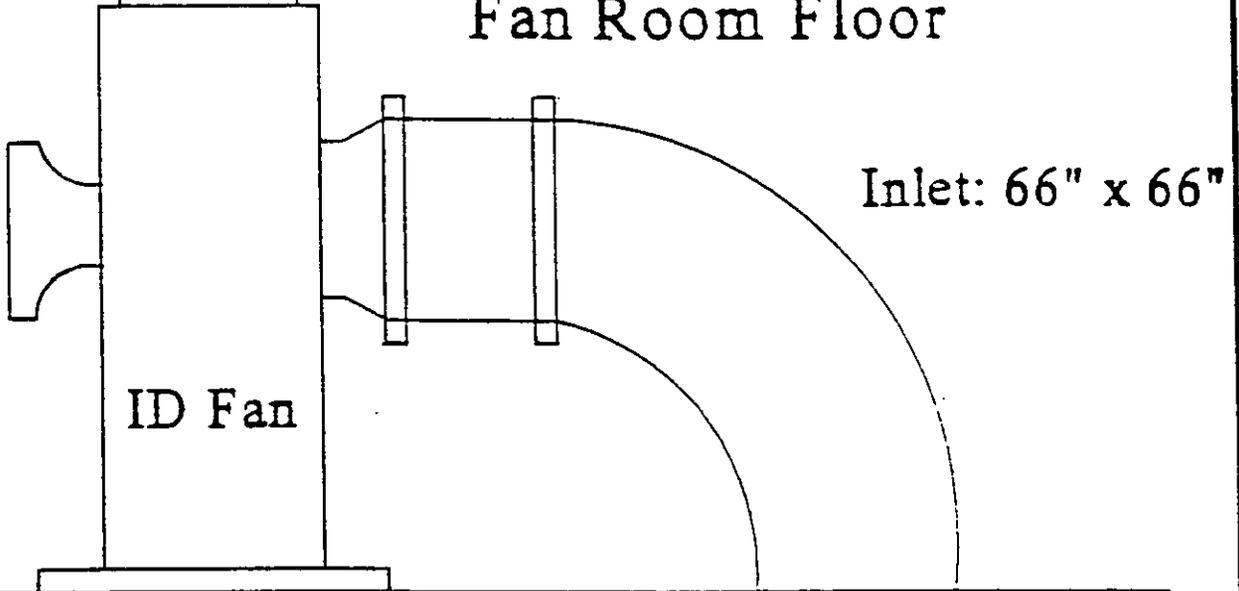
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Flow



Outlet: 67" x 45"

Fan Room Floor



Inlet: 66" x 66"

ID Fan

Kiln Floor

APPENDIX A

Results, Calculations, and Equations

NOMENCLATURE

A_s	Area of stack, square feet
ACFM	Actual cubic feet per minute
B_w	Moisture content of the sample gas
cm^3	Cubic centimeters
CO_2	Carbon dioxide
C_p	Pitot coefficient
DSCFM	Dry standard cubic feet per minute
ft^2	Square feet
ft^3	Cubic feet
hr	Hour
K_p	Pitot tube constant, 85.49 for English units (See Method 2, Equation 2-9)
lb	Pounds
lb-mole	Pound-mole
M_s	Molecular weight of stack gas, wet basis
M_w	Ratio of vapor pressure of water at stack conditions to stack pressure
MBtu	Million British thermal units
min	Minute
ml	Milliliters
O_2	Oxygen
Δp	Gas velocity pressure (in water)
P_s	Stack static pressure (inches mercury)
P_b	Barometric pressure (inches water)
P_a	Absolute stack pressure (barometric + static pressure in inches of H_2O)
P_w	Vapor pressure of water at stack conditions
P_{std}	Standard pressure, 29.92-inches mercury
ppm _v	Parts per million by volume
SCFM	Standard cubic feet per minute
T_s	Temperature of the stack
T_{std}	Standard temperature, 68° Fahrenheit (F)
V_w	Volume of sample gas measured by the dry gas meter
V_w	Volume of water collected in the impingers and silica gel
Y_s	Dry gas meter correction factor

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	1
Location	Jefferson Junction, WI	Start	10:00 AM
Stack ID	Fan #1 Outlet	Stop	10:15 AM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.05 in H2O		
Vlc	12.5 g	Ps	30.30 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0254
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.56 lb/lb-mole
Cp	0.84	Vs	33.54 ft/s
Tm	° F	Qs	42,131 acfm
(DP) ^{1/2}	0.5962	Qs	2,544,143 scfh
Ts	71.1 ° F	Qs(d)	41,327 dscfm
Vm	ft ³		
Dn	in	C3H8	0.029 lb/hr
As	20.94 ft ²	Carbon	0.024 lb/hr
Yd		Carbon	0.10 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	1
Location	Jefferson Junction, WI	Start	10:00 AM
Stack ID	Fan #1 Outlet	Stop	10:15 AM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.680	0.825	69.0
2	0.665	0.815	70.0
3	0.585	0.765	70.0
4	0.485	0.696	70.0
5	0.420	0.648	70.0
6	0.455	0.675	70.0
B-1	0.595	0.771	71.0
2	0.545	0.738	71.0
3	0.365	0.604	71.0
4	0.280	0.529	71.0
5	0.285	0.534	71.0
6	0.335	0.579	71.0
C-1	0.515	0.718	70.0
2	0.530	0.728	71.0
3	0.525	0.725	71.0
4	0.325	0.570	71.0
5	0.460	0.678	71.0
6	0.395	0.628	71.0
D-1	0.420	0.648	71.0
2	0.415	0.644	71.0
3	0.425	0.652	71.0
4	0.285	0.534	72.0
5	0.280	0.529	72.0
6	0.450	0.671	72.0
E-1	0.310	0.557	71.0
2	0.305	0.552	71.0
3	0.320	0.566	72.0
4	0.260	0.510	72.0
5	0.225	0.474	72.0
6	0.335	0.579	72.0
F-1	0.225	0.474	72.0
2	0.220	0.469	72.0
3	0.215	0.464	72.0
4	0.140	0.374	72.0
5	0.075	0.274	72.0
6	0.070	0.265	72.0
36	0.3728	0.5962	71.14

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	1
Location	Jefferson Junction, WI	Start	11:45 AM
Stack ID	Fan #2 Outlet	Stop	12:00 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.06 in H2O		
Vlc	12.5 g	Ps	30.30 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0267
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.55 lb/lb-mole
Cp	0.84	Vs	37.18 ft/s
Tm	° F	Qs	46,710 acfm
(DP) ^{1/2}	0.6598	Qs	2,812,443 scfh
Ts	72.7 ° F	Qs(d)	45,620 dscfm
Vm	ft ³		
Dn	in	C3H8	0.032 lb/hr
As	20.94 ft ²	Carbon	0.026 lb/hr
Yd		Carbon	0.11 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	1
Location	Jefferson Junction, WI	Start	11:45 AM
Stack ID	Fan #2 Outlet	Stop	12:00 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	1.050	1.025	73.0
2	1.100	1.049	73.0
3	1.150	1.072	73.0
4	1.100	1.049	73.0
5	0.730	0.854	73.0
6	0.815	0.903	73.0
B-1	0.930	0.964	73.0
2	0.985	0.992	73.0
3	0.975	0.987	73.0
4	1.050	1.025	73.0
5	1.150	1.072	73.0
6	0.640	0.800	73.0
C-1	0.470	0.686	73.0
2	0.645	0.803	73.0
3	0.890	0.943	73.0
4	1.050	1.025	73.0
5	0.865	0.930	73.0
6	0.620	0.787	73.0
D-1	0.260	0.510	71.0
2	0.380	0.616	71.0
3	0.430	0.656	73.0
4	0.495	0.704	73.0
5	0.465	0.682	73.0
6	0.370	0.608	73.0
E-1	0.100	0.316	71.0
2	0.130	0.361	72.0
3	0.165	0.406	73.0
4	0.175	0.418	73.0
5	0.145	0.381	72.0
6	0.085	0.292	73.0
F-1	0.020	0.141	71.0
2	0.030	0.173	73.0
3	0.025	0.158	72.0
4	0.020	0.141	73.0
5	0.015	0.122	73.0
6	0.010	0.100	73.0
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36	0.5426	0.6598	72.69

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	1
Location	Jefferson Junction, WI	Start	10:30 AM
Stack ID	Fan #3 Outlet	Stop	10:50 AM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.04 in H2O		
Vlc	12.5 g	Ps	30.30 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0277
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.54 lb/lb-mole
Cp	0.84	Vs	37.76 ft/s
Tm	° F	Qs	47,430 acfm
(DP) ^{1/2}	0.6692	Qs	2,850,185 scfh
Ts	73.7 ° F	Qs(d)	46,188 dscfm
Vm	ft ³		
Dn	in	C3H8	0.033 lb/hr
As	20.94 ft ²	Carbon	0.027 lb/hr
Yd		Carbon	0.12 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	1
Location	Jefferson Junction, WI	Start	10:30 AM
Stack ID	Fan #3 Outlet	Stop	10:50 AM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.900	0.949	73.0
2	0.890	0.943	73.0
3	0.820	0.906	73.0
4	0.560	0.748	73.0
5	0.400	0.632	73.0
6	0.500	0.707	73.0
B-1	0.850	0.922	73.0
2	0.860	0.927	73.0
3	0.840	0.917	74.0
4	0.420	0.648	74.0
5	0.425	0.652	73.0
6	0.575	0.758	74.0
C-1	0.785	0.886	74.0
2	0.775	0.880	74.0
3	0.760	0.872	74.0
4	0.380	0.616	74.0
5	0.240	0.490	74.0
6	0.610	0.781	74.0
D-1	0.675	0.822	74.0
2	0.670	0.819	74.0
3	0.595	0.771	74.0
4	0.445	0.667	74.0
5	0.155	0.394	74.0
6	0.320	0.566	74.0
E-1	0.380	0.616	74.0
2	0.405	0.636	74.0
3	0.375	0.612	74.0
4	0.385	0.620	74.0
5	0.135	0.367	74.0
6	0.205	0.453	74.0
F-1	0.225	0.474	74.0
2	0.220	0.469	74.0
3	0.215	0.464	74.0
4	0.135	0.367	73.0
5	0.095	0.308	74.0
6	0.185	0.430	74.0
36	0.4836	0.6692	73.72

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	1
Location	Jefferson Junction, WI	Start	11:20 AM
Stack ID	Fan #4 Outlet	Stop	11:40 AM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.02 in H2O		
Vlc	12.5 g	Ps	30.30 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0297
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.51 lb/lb-mole
Cp	0.84	Vs	39.17 ft/s
Tm	° F	Qs	49,206 acfm
(DP) ^{1/2}	0.6927	Qs	2,945,399 scfh
Ts	75.8 ° F	Qs(d)	47,633 dscfm
Vm	ft ³		
Dn	in	C3H8	0.034 lb/hr
As	20.94 ft ²	Carbon	0.028 lb/hr
Yd		Carbon	0.12 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	1
Location	Jefferson Junction, WI	Start	11:20 AM
Stack ID	Fan #4 Outlet	Stop	11:40 AM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.840	0.917	76.0
2	0.845	0.919	76.0
3	0.830	0.911	76.0
4	0.795	0.892	76.0
5	0.640	0.800	76.0
6	0.550	0.742	76.0
B-1	0.735	0.857	75.0
2	0.725	0.851	75.0
3	0.710	0.843	75.0
4	0.745	0.863	75.0
5	0.695	0.834	76.0
6	0.405	0.636	76.0
C-1	0.780	0.883	75.0
2	0.780	0.883	75.0
3	0.840	0.917	76.0
4	0.910	0.954	76.0
5	0.685	0.828	76.0
6	0.335	0.579	76.0
D-1	0.610	0.781	75.0
2	0.680	0.825	76.0
3	0.720	0.849	76.0
4	0.680	0.825	76.0
5	0.355	0.596	76.0
6	0.325	0.570	76.0
E-1	0.455	0.675	75.0
2	0.495	0.704	76.0
3	0.560	0.748	76.0
4	0.585	0.765	76.0
5	0.525	0.725	76.0
6	0.305	0.552	76.0
F-1	0.050	0.224	76.0
2	0.030	0.173	76.0
3	0.030	0.173	76.0
4	0.060	0.245	76.0
5	0.040	0.200	76.0
6	0.040	0.200	76.0
36	0.5386	0.6927	75.78

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	1
Location	Jefferson Junction, WI	Start	11:00 AM
Stack ID	Fan #5 Outlet	Stop	11:15 AM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.06 in H2O		
Vlc	12.5 g	Ps	30.30 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0277
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.54 lb/lb-mole
Cp	0.84	Vs	32.90 ft/s
Tm	° F	Qs	41,334 acfm
(DP) ^{1/2}	0.5832	Qs	2,483,826 scfh
Ts	73.8 ° F	Qs(d)	40,250 dscfm
Vm	ft ³		
Dn	in	C3H8	0.028 lb/hr
As	20.94 ft ²	Carbon	0.023 lb/hr
Yd		Carbon	0.10 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	1
Location	Jefferson Junction, WI	Start	11:00 AM
Stack ID	Fan #5 Outlet	Stop	11:15 AM

Flow Averages Calcs >>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.690	0.831	74.0
2	0.670	0.819	74.0
3	0.645	0.803	74.0
4	0.400	0.632	74.0
5	0.350	0.592	74.0
6	0.440	0.663	74.0
B-1	0.555	0.745	74.0
2	0.560	0.748	73.0
3	0.515	0.718	74.0
4	0.345	0.587	74.0
5	0.380	0.616	74.0
6	0.475	0.689	74.0
C-1	0.455	0.675	73.0
2	0.430	0.656	73.0
3	0.435	0.660	74.0
4	0.355	0.596	74.0
5	0.525	0.725	74.0
6	0.505	0.711	74.0
D-1	0.430	0.656	74.0
2	0.420	0.648	74.0
3	0.375	0.612	74.0
4	0.300	0.548	74.0
5	0.290	0.539	74.0
6	0.570	0.755	74.0
E-1	0.225	0.474	72.0
2	0.210	0.458	73.0
3	0.265	0.515	74.0
4	0.205	0.453	74.0
5	0.135	0.367	74.0
6	0.425	0.652	74.0
F-1	0.100	0.316	73.0
2	0.105	0.324	73.0
3	0.110	0.332	73.0
4	0.085	0.292	74.0
5	0.075	0.274	74.0
6	0.100	0.316	74.0
36	0.3654	0.5832	73.75

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	2
Location	Jefferson Junction, WI	Start	02:50 PM
Stack ID	Fan #1 Outlet	Stop	03:05 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.09 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0268
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.55 lb/lb-mole
Cp	0.84	Vs	49.75 ft/s
Tm	° F	Qs	62,498 acfm
(DP) ^{1/2}	0.8828	Qs	3,762,545 scfh
Ts	72.8 ° F	Qs(d)	61,026 dscfm
Vm	ft ³		
Dn	in	C3H8	0.043 lb/hr
As	20.94 ft ²	Carbon	0.035 lb/hr
Yd		Carbon	0.15 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	2
Location	Jefferson Junction, WI	Start	02:50 PM
Stack ID	Fan #1 Outlet	Stop	03:05 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	1.550	1.245	72.0
2	1.450	1.204	72.0
3	1.400	1.183	72.0
4	0.990	0.995	73.0
5	0.780	0.883	73.0
6	0.860	0.927	73.0
B-1	1.350	1.162	72.0
2	1.200	1.095	72.0
3	0.980	0.990	73.0
4	0.600	0.775	73.0
5	0.765	0.875	73.0
6	0.830	0.911	73.0
C-1	1.250	1.118	72.0
2	1.200	1.095	72.0
3	1.050	1.025	73.0
4	0.525	0.725	73.0
5	0.835	0.914	73.0
6	0.910	0.954	73.0
D-1	0.980	0.990	73.0
2	1.000	1.000	73.0
3	1.000	1.000	73.0
4	0.775	0.880	73.0
5	0.370	0.608	73.0
6	0.960	0.980	73.0
E-1	0.770	0.877	73.0
2	0.790	0.889	73.0
3	0.740	0.860	73.0
4	0.635	0.797	73.0
5	0.305	0.552	73.0
6	0.435	0.660	73.0
F-1	0.325	0.570	73.0
2	0.420	0.648	73.0
3	0.465	0.682	73.0
4	0.405	0.636	73.0
5	0.245	0.495	73.0
6	0.335	0.579	73.0
36	0.8189	0.8828	72.81

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	2
Location	Jefferson Junction, WI	Start	01:50 PM
Stack ID	Fan #2 Outlet	Stop	02:05 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.71 in H2O		
Vlc	12.5 g	Ps	30.35 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0260
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.55 lb/lb-mole
Cp	0.84	Vs	48.64 ft/s
Tm	° F	Qs	61,100 acfm
(DP) ^{1/2}	0.8645	Qs	3,689,879 scfh
Ts	71.9 ° F	Qs(d)	59,897 dscfm
Vm	ft ³		
Dn	in	C3H8	0.042 lb/hr
As	20.94 ft ²	Carbon	0.034 lb/hr
Yd		Carbon	0.15 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	2
Location	Jefferson Junction, WI	Start	01:50 PM
Stack ID	Fan #2 Outlet	Stop	02:05 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.011	0.105	71.0
2	0.020	0.141	71.0
3	0.010	0.100	71.0
4	0.005	0.071	71.0
5	0.010	0.100	71.0
6	0.015	0.122	71.0
B-1	0.070	0.265	70.0
2	0.060	0.245	71.0
3	0.065	0.255	71.0
4	0.230	0.480	71.0
5	0.560	0.748	71.0
6	0.465	0.682	71.0
C-1	0.665	0.815	71.0
2	0.865	0.930	71.0
3	1.100	1.049	72.0
4	1.300	1.140	72.0
5	1.150	1.072	72.0
6	0.825	0.908	72.0
D-1	1.700	1.304	72.0
2	1.850	1.360	72.0
3	1.000	1.000	72.0
4	1.150	1.072	73.0
5	1.850	1.360	73.0
6	1.700	1.304	73.0
E-1	1.150	1.072	72.0
2	1.200	1.095	73.0
3	1.750	1.323	73.0
4	1.850	1.360	73.0
5	1.050	1.025	73.0
6	1.850	1.360	73.0
F-1	1.500	1.225	72.0
2	1.600	1.265	73.0
3	1.650	1.285	73.0
4	1.450	1.204	73.0
5	1.200	1.095	73.0
6	1.400	1.183	73.0
36	0.9535	0.8645	71.94

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	2
Location	Jefferson Junction, WI	Start	02:35 PM
Stack ID	Fan #3 Outlet	Stop	02:50 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.43 in H2O		
Vlc	12.5 g	Ps	30.33 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0287
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.53 lb/lb-mole
Cp	0.84	Vs	53.55 ft/s
Tm	° F	Qs	67,272 acfm
(DP) ^{1/2}	0.9485	Qs	4,038,136 scfh
Ts	74.8 ° F	Qs(d)	65,371 dscfm
Vm	ft ³		
Dn	in	C3H8	0.046 lb/hr
As	20.94 ft ²	Carbon	0.038 lb/hr
Yd		Carbon	0.17 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	2
Location	Jefferson Junction, WI	Start	02:35 PM
Stack ID	Fan #3 Outlet	Stop	02:50 PM

Flow Averages Calcs >>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.950	0.975	74.0
2	0.850	0.922	74.0
3	0.750	0.866	75.0
4	1.100	1.049	75.0
5	0.910	0.954	75.0
6	1.150	1.072	75.0
B-1	1.850	1.360	74.0
2	1.900	1.378	74.0
3	1.400	1.183	75.0
4	0.755	0.869	75.0
5	0.810	0.900	75.0
6	1.350	1.162	75.0
C-1	0.850	0.922	75.0
2	0.800	0.894	75.0
3	1.550	1.245	75.0
4	0.905	0.951	75.0
5	0.515	0.718	75.0
6	1.300	1.140	75.0
D-1	1.550	1.245	74.0
2	1.500	1.225	74.0
3	1.300	1.140	74.0
4	1.250	1.118	75.0
5	0.955	0.977	75.0
6	0.830	0.911	75.0
E-1	0.965	0.982	75.0
2	1.050	1.025	75.0
3	0.990	0.995	75.0
4	0.600	0.775	75.0
5	0.310	0.557	75.0
6	0.580	0.762	75.0
F-1	0.490	0.700	75.0
2	0.525	0.725	75.0
3	0.415	0.644	75.0
4	0.310	0.557	75.0
5	0.300	0.548	75.0
6	0.490	0.700	75.0
36	0.9474	0.9485	74.81

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	2
Location	Jefferson Junction, WI	Start	02:05 PM
Stack ID	Fan #4 Outlet	Stop	02:20 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.09 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0283
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.53 lb/lb-mole
Cp	0.84	Vs	52.11 ft/s
Tm	° F	Qs	65,461 acfm
(DP) ^{1/2}	0.9230	Qs	3,929,671 scfh
Ts	74.3 ° F	Qs(d)	63,643 dscfm
Vm	ft ³		
Dn	in	C3H8	0.045 lb/hr
As	20.94 ft ²	Carbon	0.037 lb/hr
Yd		Carbon	0.16 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	2
Location	Jefferson Junction, WI	Start	02:05 PM
Stack ID	Fan #4 Outlet	Stop	02:20 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	1.300	1.140	74.0
2	1.350	1.162	74.0
3	1.150	1.072	74.0
4	1.100	1.049	74.0
5	1.000	1.000	74.0
6	1.000	1.000	74.0
B-1	1.150	1.072	74.0
2	1.100	1.049	74.0
3	1.150	1.072	74.0
4	1.100	1.049	74.0
5	0.950	0.975	74.0
6	0.750	0.866	74.0
C-1	1.600	1.265	74.0
2	1.700	1.304	74.0
3	1.600	1.265	74.0
4	1.500	1.225	74.0
5	1.400	1.183	74.0
6	1.300	1.140	74.0
D-1	1.300	1.140	74.0
2	1.400	1.183	75.0
3	1.450	1.204	75.0
4	1.400	1.183	75.0
5	0.960	0.980	75.0
6	0.510	0.714	75.0
E-1	0.810	0.900	75.0
2	0.910	0.954	75.0
3	0.940	0.970	75.0
4	0.905	0.951	75.0
5	0.775	0.880	75.0
6	0.460	0.678	75.0
F-1	0.010	0.100	74.0
2	0.010	0.100	74.0
3	0.015	0.122	74.0
4	0.080	0.283	74.0
5	0.280	0.529	74.0
6	0.220	0.469	75.0
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36	0.9621	0.9230	74.33

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	2
Location	Jefferson Junction, WI	Start	02:25 PM
Stack ID	Fan #5 Outlet	Stop	02:35 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.32 in H2O		
Vlc	12.5 g	Ps	30.32 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0276
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.54 lb/lb-mole
Cp	0.84	Vs	44.60 ft/s
Tm	° F	Qs	56,031 acfm
(DP) ^{1/2}	0.7909	Qs	3,369,515 scfh
Ts	73.7 ° F	Qs(d)	54,606 dscfm
Vm	ft ³		
Dn	in	C3H8	0.038 lb/hr
As	20.94 ft ²	Carbon	0.031 lb/hr
Yd		Carbon	0.14 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	2
Location	Jefferson Junction, WI	Start	02:25 PM
Stack ID	Fan #5 Outlet	Stop	02:35 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	1.300	1.140	73.0
2	1.150	1.072	73.0
3	1.050	1.025	73.0
4	0.675	0.822	73.0
5	0.690	0.831	73.0
6	0.880	0.938	73.0
B-1	1.100	1.049	73.0
2	1.050	1.025	73.0
3	0.915	0.957	73.0
4	0.560	0.748	73.0
5	0.855	0.925	73.0
6	0.940	0.970	73.0
C-1	0.890	0.943	73.0
2	0.900	0.949	73.0
3	0.810	0.900	74.0
4	0.620	0.787	74.0
5	0.670	0.819	74.0
6	1.050	1.025	74.0
D-1	0.790	0.889	74.0
2	0.810	0.900	74.0
3	0.820	0.906	74.0
4	0.630	0.794	74.0
5	0.335	0.579	74.0
6	0.825	0.908	74.0
E-1	0.485	0.696	74.0
2	0.440	0.663	75.0
3	0.475	0.689	75.0
4	0.480	0.693	75.0
5	0.230	0.480	75.0
6	0.520	0.721	75.0
F-1	0.220	0.469	73.0
2	0.185	0.430	73.0
3	0.190	0.436	74.0
4	0.155	0.394	74.0
5	0.150	0.387	74.0
6	0.265	0.515	74.0
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36	0.6697	0.7909	73.69

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	3
Location	Jefferson Junction, WI	Start	06:10 PM
Stack ID	Fan #1 Outlet	Stop	06:20 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.32 in H2O		
Vlc	12.5 g	Ps	30.32 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0239
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.58 lb/lb-mole
Cp	0.84	Vs	38.71 ft/s
Tm	° F	Qs	48,633 acfm
(DP) ^{1/2}	0.6897	Qs	2,947,911 scfh
Ts	69.5 ° F	Qs(d)	47,956 dscfm
Vm	ft ³		
Dn	in	C3H8	0.033 lb/hr
As	20.94 ft ²	Carbon	0.027 lb/hr
Yd		Carbon	0.12 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	3
Location	Jefferson Junction, WI	Start	06:10 PM
Stack ID	Fan #1 Outlet	Stop	06:20 PM

Flow Averages Calcs >>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
F-1	0.320	0.566	69.0
2	0.365	0.604	69.0
3	0.370	0.608	69.0
4	0.290	0.539	69.0
5	0.130	0.361	69.0
6	0.160	0.400	69.0
E-1	0.455	0.675	69.0
2	0.440	0.663	69.0
3	0.430	0.656	69.0
4	0.425	0.652	69.0
5	0.205	0.453	69.0
6	0.255	0.505	69.0
D-1	0.555	0.745	69.0
2	0.565	0.752	69.0
3	0.520	0.721	69.0
4	0.240	0.490	69.0
5	0.585	0.765	69.0
6	0.550	0.742	69.0
C-1	0.680	0.825	69.0
2	0.715	0.846	70.0
3	0.650	0.806	70.0
4	0.325	0.570	70.0
5	0.515	0.718	70.0
6	0.605	0.778	70.0
B-1	0.695	0.834	70.0
2	0.665	0.815	70.0
3	0.510	0.714	70.0
4	0.360	0.600	70.0
5	0.420	0.648	70.0
6	0.495	0.704	70.0
A-1	0.870	0.933	70.0
2	0.830	0.911	70.0
3	0.755	0.869	70.0
4	0.680	0.825	70.0
5	0.625	0.791	70.0
6	0.560	0.748	70.0
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36	0.4949	0.6897	69.47

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	3
Location	Jefferson Junction, WI	Start	07:05 PM
Stack ID	Fan #2 Outlet	Stop	07:15 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.34 in H2O		
Vlc	12.5 g	Ps	30.33 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0254
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.56 lb/lb-mole
Cp	0.84	Vs	38.90 ft/s
Tm	° F	Qs	48,865 acfm
(DP)½	0.6916	Qs	2,952,362 scfh
Ts	71.2 ° F	Qs(d)	47,955 dscfm
Vm	ft ³		
Dn	in	C3H8	0.034 lb/hr
As	20.94 ft ²	Carbon	0.027 lb/hr
Yd		Carbon	0.12 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	3
Location	Jefferson Junction, WI	Start	07:05 PM
Stack ID	Fan #2 Outlet	Stop	07:15 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	1.050	1.025	71.0
2	1.150	1.072	71.0
3	1.150	1.072	71.0
4	1.200	1.095	71.0
5	1.150	1.072	71.0
6	0.920	0.959	71.0
B-1	0.905	0.951	71.0
2	0.930	0.964	71.0
3	1.050	1.025	71.0
4	1.250	1.118	71.0
5	0.790	0.889	71.0
6	0.550	0.742	71.0
C-1	0.545	0.738	71.0
2	0.775	0.880	71.0
3	0.965	0.982	71.0
4	1.200	1.095	71.0
5	0.945	0.972	71.0
6	0.685	0.828	71.0
D-1	0.515	0.718	71.0
2	0.595	0.771	71.0
3	0.780	0.883	71.0
4	0.895	0.946	71.0
5	0.865	0.930	72.0
6	0.605	0.778	72.0
E-1	0.070	0.265	72.0
2	0.090	0.300	72.0
3	0.100	0.316	72.0
4	0.120	0.346	72.0
5	0.090	0.300	72.0
6	0.090	0.300	72.0
F-1	0.010	0.100	71.0
2	0.005	0.071	71.0
3	0.010	0.100	71.0
4	0.015	0.122	71.0
5	0.010	0.100	71.0
6	0.005	0.071	71.0
36	0.6133	0.6916	71.22

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	3
Location	Jefferson Junction, WI	Start	06:20 PM
Stack ID	Fan #3 Outlet	Stop	06:30 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.10 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0263
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.55 lb/lb-mole
Cp	0.84	Vs	43.02 ft/s
Tm	° F	Qs	54,044 acfm
(DP) _{1/2}	0.7639	Qs	3,257,369 scfh
Ts	72.2 ° F	Qs(d)	52,862 dscfm
Vm	ft ³		
Dn	in	C3H8	0.037 lb/hr
As	20.94 ft ²	Carbon	0.030 lb/hr
Yd		Carbon	0.13 tpy

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Client Ladish Malting Company
 Unit Kiln No. 15 Malt Dryer Exhaust
 Location Jefferson Junction, WI
 Stack ID Fan #3 Outlet

Date 11/15/95
 Run 3
 Start 06:20 PM
 Stop 06:30 PM

Flow Averages Cales >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	1.100	1.049	72.0
2	1.050	1.025	72.0
3	0.970	0.985	72.0
4	0.790	0.889	72.0
5	0.740	0.860	72.0
6	0.705	0.840	72.0
B-1	1.150	1.072	72.0
2	1.100	1.049	72.0
3	1.050	1.025	72.0
4	0.530	0.728	72.0
5	0.470	0.686	72.0
6	0.690	0.831	72.0
C-1	1.100	1.049	72.0
2	1.050	1.025	72.0
3	1.050	1.025	72.0
4	0.510	0.714	72.0
5	0.320	0.566	72.0
6	0.755	0.869	72.0
D-1	0.900	0.949	72.0
2	0.830	0.911	73.0
3	0.740	0.860	73.0
4	0.515	0.718	73.0
5	0.220	0.469	73.0
6	0.415	0.644	73.0
E-1	0.535	0.731	72.0
2	0.550	0.742	72.0
3	0.520	0.721	72.0
4	0.345	0.587	72.0
5	0.175	0.418	72.0
6	0.345	0.587	72.0
F-1	0.230	0.480	72.0
2	0.255	0.505	72.0
3	0.245	0.495	73.0
4	0.190	0.436	72.0
5	0.200	0.447	72.0
6	0.265	0.515	73.0
36	0.6279	0.7639	72.19

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	3
Location	Jefferson Junction, WI	Start	06:50 PM
Stack ID	Fan #4 Outlet	Stop	07:00 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.05 in H2O		
Vlc	12.5 g	Ps	30.30 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0262
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.55 lb/lb-mole
Cp	0.84	Vs	43.42 ft/s
Tm	° F	Qs	54,542 acfm
(DP) ^{1/2}	0.7710	Qs	3,287,716 scfh
Ts	72.1 ° F	Qs(d)	53,360 dscfm
Vm	ft ³		
Dn	in	C3H8	0.037 lb/hr
As	20.94 ft ²	Carbon	0.031 lb/hr
Yd		Carbon	0.13 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	3
Location	Jefferson Junction, WI	Start	06:50 PM
Stack ID	Fan #4 Outlet	Stop	07:00 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	1.050	1.025	72.0
2	1.100	1.049	72.0
3	1.050	1.025	72.0
4	1.000	1.000	72.0
5	0.890	0.943	72.0
6	0.685	0.828	72.0
B-1	0.990	0.995	72.0
2	1.050	1.025	72.0
3	1.150	1.072	72.0
4	1.050	1.025	72.0
5	0.795	0.892	72.0
6	0.530	0.728	72.0
C-1	1.150	1.072	72.0
2	1.100	1.049	72.0
3	1.100	1.049	72.0
4	1.100	1.049	72.0
5	0.825	0.908	72.0
6	0.545	0.738	72.0
D-1	0.815	0.903	72.0
2	0.855	0.925	72.0
3	0.930	0.964	72.0
4	0.920	0.959	72.0
5	0.710	0.843	73.0
6	0.395	0.628	73.0
E-1	0.520	0.721	72.0
2	0.565	0.752	72.0
3	0.570	0.755	72.0
4	0.585	0.765	72.0
5	0.540	0.735	72.0
6	0.360	0.600	73.0
F-1	0.010	0.100	72.0
2	0.005	0.071	72.0
3	0.010	0.100	72.0
4	0.015	0.122	72.0
5	0.020	0.141	72.0
6	0.040	0.200	72.0
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36	0.6951	0.7710	72.08

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	3
Location	Jefferson Junction, WI	Start	06:35 PM
Stack ID	Fan #5 Outlet	Stop	06:45 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.36 in H2O		
Vlc	12.5 g	Ps	30.33 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0254
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.56 lb/lb-mole
Cp	0.84	Vs	36.90 ft/s
Tm	° F	Qs	46,351 acfm
(DP)½	0.6560	Qs	2,800,451 scfh
Ts	71.3 ° F	Qs(d)	45,487 dscfm
Vm	ft ³		
Dn	in	C3H8	0.032 lb/hr
As	20.94 ft ²	Carbon	0.026 lb/hr
Yd		Carbon	0.11 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	3
Location	Jefferson Junction, WI	Start	06:35 PM
Stack ID	Fan #5 Outlet	Stop	06:45 PM

Flow Averages Calcs >>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.865	0.930	70.0
2	0.795	0.892	71.0
3	0.700	0.837	71.0
4	0.560	0.748	71.0
5	0.510	0.714	71.0
6	0.560	0.748	71.0
B-1	0.710	0.843	71.0
2	0.685	0.828	71.0
3	0.550	0.742	71.0
4	0.410	0.640	71.0
5	0.590	0.768	71.0
6	0.705	0.840	71.0
C-1	0.615	0.784	71.0
2	0.625	0.791	71.0
3	0.605	0.778	71.0
4	0.445	0.667	71.0
5	0.395	0.628	71.0
6	0.755	0.869	71.0
D-1	0.565	0.752	71.0
2	0.545	0.738	71.0
3	0.520	0.721	71.0
4	0.405	0.636	71.0
5	0.205	0.453	72.0
6	0.495	0.704	72.0
E-1	0.345	0.587	71.0
2	0.350	0.592	71.0
3	0.365	0.604	71.0
4	0.325	0.570	71.0
5	0.140	0.374	72.0
6	0.370	0.608	72.0
F-1	0.145	0.381	72.0
2	0.155	0.394	72.0
3	0.125	0.354	72.0
4	0.105	0.324	72.0
5	0.100	0.316	72.0
6	0.215	0.464	72.0
36	0.4599	0.6560	71.25

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	4
Location	Jefferson Junction, WI	Start	10:05 PM
Stack ID	Fan #1 Outlet	Stop	10:15 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.16 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0273
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.54 lb/lb-mole
Cp	0.84	Vs	15.41 ft/s
Tm	° F	Qs	19,357 acfm
(DP) ^{1/2}	0.2733	Qs	1,164,417 scfh
Ts	73.3 ° F	Qs(d)	18,877 dscfm
Vm	ft ³		
Dn	in	C3H8	0.013 lb/hr
As	20.94 ft ²	Carbon	0.011 lb/hr
Yd		Carbon	0.05 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	4
Location	Jefferson Junction, WI	Start	10:05 PM
Stack ID	Fan #1 Outlet	Stop	10:15 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.135	0.367	74.0
2	0.135	0.367	74.0
3	0.140	0.374	74.0
4	0.120	0.346	74.0
5	0.105	0.324	74.0
6	0.090	0.300	74.0
B-1	0.105	0.324	73.0
2	0.110	0.332	73.0
3	0.095	0.308	73.0
4	0.085	0.292	73.0
5	0.075	0.274	73.0
6	0.070	0.265	73.0
C-1	0.100	0.316	73.0
2	0.110	0.332	73.0
3	0.110	0.332	74.0
4	0.085	0.292	74.0
5	0.085	0.292	74.0
6	0.080	0.283	74.0
D-1	0.075	0.274	73.0
2	0.080	0.283	73.0
3	0.080	0.283	73.0
4	0.060	0.245	74.0
5	0.075	0.274	74.0
6	0.070	0.265	72.0
E-1	0.055	0.235	72.0
2	0.055	0.235	73.0
3	0.065	0.255	73.0
4	0.050	0.224	73.0
5	0.060	0.245	73.0
6	0.055	0.235	73.0
F-1	0.035	0.187	73.0
2	0.040	0.200	73.0
3	0.045	0.212	73.0
4	0.035	0.187	73.0
5	0.020	0.141	73.0
6	0.020	0.141	74.0
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36	0.0781	0.2733	73.31

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	4
Location	Jefferson Junction, WI	Start	09:05 PM
Stack ID	Fan #2 Outlet	Stop	09:15 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.20 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0264
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.55 lb/lb-mole
Cp	0.84	Vs	15.07 ft/s
Tm	° F	Qs	18,926 acfm
(DP) ^{1/2}	0.2675	Qs	1,140,677 scfh
Ts	72.4 ° F	Qs(d)	18,509 dscfm
Vm	ft ³		
Dn	in	C3H8	0.013 lb/hr
As	20.94 ft ²	Carbon	0.011 lb/hr
Yd		Carbon	0.05 tpy

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Client	Laotian Malt Company	Date	11/16/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	4
Location	Jefferson Junction, WI	Start	09:05 PM
Stack ID	Fan #2 Outlet	Stop	09:15 PM

Flow Averages Calcs >>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.005	0.071	72.0
2	0.010	0.100	72.0
3	0.010	0.100	72.0
4	0.005	0.071	72.0
5	0.010	0.100	72.0
6	0.015	0.122	72.0
B-1	0.005	0.071	71.0
2	0.005	0.071	71.0
3	0.010	0.100	72.0
4	0.015	0.122	72.0
5	0.020	0.141	72.0
6	0.005	0.071	72.0
C-1	0.020	0.141	70.0
2	0.025	0.158	71.0
3	0.025	0.158	71.0
4	0.050	0.224	72.0
5	0.060	0.245	72.0
6	0.050	0.224	73.0
D-1	0.150	0.387	73.0
2	0.160	0.400	73.0
3	0.165	0.406	73.0
4	0.180	0.424	73.0
5	0.155	0.394	73.0
6	0.125	0.354	73.0
E-1	0.165	0.406	73.0
2	0.180	0.424	73.0
3	0.200	0.447	73.0
4	0.195	0.442	73.0
5	0.130	0.361	73.0
6	0.115	0.339	73.0
F-1	0.165	0.406	73.0
2	0.185	0.430	73.0
3	0.200	0.447	73.0
4	0.185	0.430	73.0
5	0.180	0.424	73.0
6	0.175	0.418	73.0
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36	0.0932	0.2675	72.36

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	4
Location	Jefferson Junction, WI	Start	09:50 PM
Stack ID	Fan #3 Outlet	Stop	10:00 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.13 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0265
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.55 lb/lb-mole
Cp	0.84	Vs	17.70 ft/s
Tm	° F	Qs	22,230 acfm
(DP) ^{1/2}	0.3141	Qs	1,339,255 scfh
Ts	72.5 ° F	Qs(d)	21,729 dscfm
Vm	ft ³		
Dn	in	C3H8	0.015 lb/hr
As	20.94 ft ²	Carbon	0.012 lb/hr
Yd		Carbon	0.05 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	4
Location	Jefferson Junction, WI	Start	09:50 PM
Stack ID	Fan #3 Outlet	Stop	10:00 PM

Flow Averages Calcs >>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.165	0.406	72.0
2	0.175	0.418	72.0
3	0.165	0.406	73.0
4	0.145	0.381	73.0
5	0.120	0.346	73.0
6	0.115	0.339	73.0
B-1	0.160	0.400	71.0
2	0.165	0.406	72.0
3	0.170	0.412	73.0
4	0.105	0.324	73.0
5	0.095	0.308	73.0
6	0.110	0.332	73.0
C-1	0.145	0.381	72.0
2	0.155	0.394	72.0
3	0.150	0.387	73.0
4	0.115	0.339	73.0
5	0.080	0.283	73.0
6	0.105	0.324	73.0
D-1	0.110	0.332	72.0
2	0.115	0.339	72.0
3	0.115	0.339	73.0
4	0.100	0.316	73.0
5	0.050	0.224	73.0
6	0.090	0.300	73.0
E-1	0.065	0.255	69.0
2	0.070	0.265	70.0
3	0.085	0.292	71.0
4	0.090	0.300	72.0
5	0.045	0.212	73.0
6	0.055	0.235	73.0
F-1	0.065	0.255	73.0
2	0.060	0.245	73.0
3	0.060	0.245	73.0
4	0.050	0.224	73.0
5	0.035	0.187	73.0
6	0.025	0.158	73.0
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36	0.1035	0.3141	72.47

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	4
Location	Jefferson Junction, WI	Start	09:20 PM
Stack ID	Fan #4 Outlet	Stop	09:30 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.14 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0282
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.53 lb/lb-mole
Cp	0.84	Vs	17.13 ft/s
Tm	° F	Qs	21,525 acfm
(DP) ^{1/2}	0.3036	Qs	1,292,503 scfh
Ts	74.3 ° F	Qs(d)	20,935 dscfm
Vm	ft ³		
Dn	in	C3H8	0.015 lb/hr
As	20.94 ft ²	Carbon	0.012 lb/hr
Yd		Carbon	0.05 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	4
Location	Jefferson Junction, WI	Start	09:20 PM
Stack ID	Fan #4 Outlet	Stop	09:30 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
F-1	0.005	0.071	66.0
2	0.005	0.071	67.0
3	0.005	0.071	69.0
4	0.005	0.071	70.0
5	0.005	0.071	71.0
6	0.005	0.071	73.0
E-1	0.055	0.235	74.0
2	0.070	0.265	75.0
3	0.085	0.292	75.0
4	0.090	0.300	76.0
5	0.090	0.300	76.0
6	0.060	0.245	76.0
D-1	0.105	0.324	74.0
2	0.120	0.346	75.0
3	0.130	0.361	75.0
4	0.145	0.381	76.0
5	0.125	0.354	76.0
6	0.065	0.255	76.0
C-1	0.145	0.381	74.0
2	0.155	0.394	75.0
3	0.165	0.406	75.0
4	0.185	0.430	75.0
5	0.150	0.387	76.0
6	0.070	0.265	76.0
B-1	0.130	0.361	74.0
2	0.140	0.374	75.0
3	0.155	0.394	75.0
4	0.155	0.394	76.0
5	0.135	0.367	76.0
6	0.095	0.308	76.0
A-1	0.170	0.412	75.0
2	0.185	0.430	75.0
3	0.180	0.424	75.0
4	0.160	0.400	75.0
5	0.135	0.367	75.0
6	0.125	0.354	75.0
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36	0.1057	0.3036	74.25

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	4
Location	Jefferson Junction, WI	Start	09:35 PM
Stack ID	Fan #5 Outlet	Stop	09:45 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.16 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0284
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.53 lb/lb-mole
Cp	0.84	Vs	15.01 ft/s
Tm	° F	Qs	18,850 acfm
(DP) ^{1/2}	0.2658	Qs	1,131,509 scfh
Ts	74.5 ° F	Qs(d)	18,323 dscfm
Vm	ft ³		
Dn	in	C3H8	0.013 lb/hr
As	20.94 ft ²	Carbon	0.011 lb/hr
Yd		Carbon	0.05 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	4
Location	Jefferson Junction, WI	Start	09:35 PM
Stack ID	Fan #5 Outlet	Stop	09:45 PM

Flow Averages Calcs >>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
F-1	0.030	0.173	73.0
2	0.040	0.200	73.0
3	0.035	0.187	74.0
4	0.035	0.187	75.0
5	0.040	0.200	75.0
6	0.035	0.187	75.0
E-1	0.050	0.224	75.0
2	0.055	0.235	75.0
3	0.050	0.224	75.0
4	0.045	0.212	75.0
5	0.050	0.224	75.0
6	0.070	0.265	75.0
D-1	0.060	0.245	74.0
2	0.060	0.245	74.0
3	0.065	0.255	75.0
4	0.060	0.245	75.0
5	0.070	0.265	75.0
6	0.085	0.292	75.0
C-1	0.080	0.283	73.0
2	0.080	0.283	73.0
3	0.085	0.292	75.0
4	0.080	0.283	75.0
5	0.080	0.283	75.0
6	0.085	0.292	75.0
B-1	0.095	0.308	72.0
2	0.100	0.316	73.0
3	0.100	0.316	74.0
4	0.085	0.292	74.0
5	0.080	0.283	75.0
6	0.075	0.274	75.0
A-1	0.120	0.346	74.0
2	0.130	0.361	75.0
3	0.130	0.361	75.0
4	0.120	0.346	75.0
5	0.105	0.324	75.0
6	0.070	0.265	75.0
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36	0.0732	0.2658	74.47

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	5
Location	Jefferson Junction, WI	Start	11:05 PM
Stack ID	Fan #1 Outlet	Stop	11:15 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.18 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0276
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.54 lb/lb-mole
Cp	0.84	Vs	18.34 ft/s
Tm	° F	Qs	23,042 acfm
(DP) ^{1/2}	0.3252	Qs	1,385,253 scfh
Ts	73.7 ° F	Qs(d)	22,450 dscfm
Vm	ft ³		
Dn	in	C3H8	0.016 lb/hr
As	20.94 ft ²	Carbon	0.013 lb/hr
Yd		Carbon	0.06 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	5
Location	Jefferson Junction, WI	Start	11:05 PM
Stack ID	Fan #1 Outlet	Stop	11:15 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
F-1	0.060	0.245	74.0
2	0.065	0.255	74.0
3	0.070	0.265	74.0
4	0.055	0.235	74.0
5	0.050	0.224	74.0
6	0.035	0.187	74.0
E-1	0.075	0.274	73.0
2	0.080	0.283	73.0
3	0.085	0.292	73.0
4	0.095	0.308	73.0
5	0.075	0.274	74.0
6	0.055	0.235	74.0
D-1	0.110	0.332	73.0
2	0.115	0.339	73.0
3	0.120	0.346	73.0
4	0.080	0.283	73.0
5	0.105	0.324	74.0
6	0.125	0.354	74.0
C-1	0.135	0.367	73.0
2	0.145	0.381	73.0
3	0.140	0.374	74.0
4	0.115	0.339	74.0
5	0.120	0.346	74.0
6	0.115	0.339	74.0
B-1	0.155	0.394	73.0
2	0.160	0.400	74.0
3	0.140	0.374	74.0
4	0.115	0.339	74.0
5	0.105	0.324	74.0
6	0.095	0.308	74.0
A-1	0.195	0.442	73.0
2	0.190	0.436	74.0
3	0.175	0.418	74.0
4	0.150	0.387	74.0
5	0.125	0.354	74.0
6	0.110	0.332	74.0
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36	0.1094	0.3252	73.67

Client Ladish Malting Company
 Unit Kiln No. 15 Malt Dryer Exhaust
 Location Jefferson Junction, WI
 Stack ID Fan #2 Outlet

Date 11/15/95
 Run 5
 Start 11:55 PM
 Stop 12:05 AM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.19 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0280
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.53 lb/lb-mole
Cp	0.84	Vs	17.14 ft/s
Tm	° F	Qs	21,529 acfm
(DP) ^{1/2}	0.3037	Qs	1,293,445 scfh
Ts	74.0 ° F	Qs(d)	20,954 dscfm
Vm	ft ³		
Dn	in	C3H8	0.015 lb/hr
As	20.94 ft ²	Carbon	0.012 lb/hr
Yd		Carbon	0.05 tpy

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Client Ladish Malting Company
 Unit Kiln No. 15 Malt Dryer Exhaust
 Location Jefferson Junction, WI
 Stack ID Fan #2 Outlet

Date 11/15/95
 Run 5
 Start 11:55 PM
 Stop 12:05 AM

Flow Averages Calcs >>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
F-1	0.250	0.500	74.0
2	0.275	0.524	75.0
3	0.285	0.534	75.0
4	0.280	0.529	75.0
5	0.265	0.515	75.0
6	0.250	0.500	75.0
E-1	0.245	0.495	74.0
2	0.270	0.520	75.0
3	0.295	0.543	75.0
4	0.285	0.534	75.0
5	0.185	0.430	75.0
6	0.160	0.400	75.0
D-1	0.105	0.324	74.0
2	0.225	0.474	73.0
3	0.245	0.495	74.0
4	0.250	0.500	75.0
5	0.225	0.474	75.0
6	0.180	0.424	75.0
C-1	0.015	0.122	73.0
2	0.020	0.141	73.0
3	0.025	0.158	74.0
4	0.050	0.224	74.0
5	0.060	0.245	74.0
6	0.025	0.158	74.0
B-1	0.010	0.100	73.0
2	0.005	0.071	73.0
3	0.010	0.100	73.0
4	0.020	0.141	74.0
5	0.015	0.122	74.0
6	0.010	0.100	74.0
A-1	0.005	0.071	72.0
2	0.005	0.071	72.0
3	0.010	0.100	73.0
4	0.010	0.100	73.0
5	0.005	0.071	74.0
6	0.015	0.122	74.0
36	0.1275	0.3037	74.03

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	5
Location	Jefferson Junction, WI	Start	11:20 PM
Stack ID	Fan #3 Outlet	Stop	11:30 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.17 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0274
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.54 lb/lb-mole
Cp	0.84	Vs	20.24 ft/s
Tm	° F	Qs	25,423 acfm
(DP)½	0.3589	Qs	1,529,078 scfh
Ts	73.4 ° F	Qs(d)	24,786 dscfm
Vm	ft ³		
Dn	in	C3H8	0.017 lb/hr
As	20.94 ft ²	Carbon	0.014 lb/hr
Yd		Carbon	0.06 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	5
Location	Jefferson Junction, WI	Start	11:20 PM
Stack ID	Fan #3 Outlet	Stop	11:30 PM

Flow Averages Calcs >>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
F-1	0.065	0.255	69.0
2	0.085	0.292	72.0
3	0.085	0.292	72.0
4	0.060	0.245	73.0
5	0.045	0.212	73.0
6	0.035	0.187	73.0
E-1	0.070	0.265	70.0
2	0.095	0.308	72.0
3	0.105	0.324	73.0
4	0.105	0.324	73.0
5	0.050	0.224	74.0
6	0.080	0.283	74.0
D-1	0.165	0.406	74.0
2	0.170	0.412	74.0
3	0.140	0.374	74.0
4	0.045	0.212	74.0
5	0.060	0.245	74.0
6	0.115	0.339	74.0
C-1	0.195	0.442	73.0
2	0.205	0.453	74.0
3	0.200	0.447	74.0
4	0.155	0.394	74.0
5	0.105	0.324	74.0
6	0.160	0.400	74.0
B-1	0.210	0.458	74.0
2	0.220	0.469	74.0
3	0.215	0.464	74.0
4	0.145	0.381	74.0
5	0.125	0.354	74.0
6	0.165	0.406	74.0
A-1	0.235	0.485	74.0
2	0.240	0.490	74.0
3	0.225	0.474	74.0
4	0.205	0.453	74.0
5	0.195	0.442	74.0
6	0.150	0.387	74.0
36	0.1368	0.3589	73.42

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	5
Location	Jefferson Junction, WI	Start	11:45 PM
Stack ID	Fan #4 Outlet	Stop	11:55 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.19 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0290
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.52 lb/lb-mole
Cp	0.84	Vs	20.35 ft/s
Tm	° F	Qs	25,560 acfm
(DP) ^{1/2}	0.3602	Qs	1,532,574 scfh
Ts	75.1 ° F	Qs(d)	24,803 dscfm
Vm	ft ³		
Dn	in	C3H8	0.018 lb/hr
As	20.94 ft ²	Carbon	0.014 lb/hr
Yd		Carbon	0.06 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	5
Location	Jefferson Junction, WI	Start	11:45 PM
Stack ID	Fan #4 Outlet	Stop	11:55 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.225	0.474	76.0
2	0.230	0.480	76.0
3	0.240	0.490	76.0
4	0.235	0.485	76.0
5	0.195	0.442	76.0
6	0.180	0.424	76.0
B-1	0.210	0.458	75.0
2	0.220	0.469	76.0
3	0.230	0.480	76.0
4	0.240	0.490	76.0
5	0.180	0.424	76.0
6	0.125	0.354	76.0
C-1	0.215	0.464	76.0
2	0.235	0.485	76.0
3	0.240	0.490	76.0
4	0.260	0.510	76.0
5	0.205	0.453	76.0
6	0.105	0.324	76.0
D-1	0.145	0.381	75.0
2	0.165	0.406	76.0
3	0.195	0.442	76.0
4	0.200	0.447	76.0
5	0.160	0.400	76.0
6	0.085	0.292	76.0
E-1	0.075	0.274	74.0
2	0.095	0.308	74.0
3	0.115	0.339	75.0
4	0.125	0.354	76.0
5	0.120	0.346	76.0
6	0.090	0.300	76.0
F-1	0.005	0.071	69.0
2	0.010	0.100	70.0
3	0.005	0.071	71.0
4	0.005	0.071	73.0
5	0.005	0.071	73.0
6	0.010	0.100	74.0
36	0.1494	0.3602	75.08

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	5
Location	Jefferson Junction, WI	Start	11:35 PM
Stack ID	Fan #5 Outlet	Stop	11:45 PM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.18 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0301
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.51 lb/lb-mole
Cp	0.84	Vs	17.42 ft/s
Tm	° F	Qs	21,885 acfm
(DP) ^{1/2}	0.3080	Qs	1,309,593 scfh
Ts	76.2 ° F	Qs(d)	21,170 dscfm
Vm	ft ³		
Dn	in	C3H8	0.015 lb/hr
As	20.94 ft ²	Carbon	0.012 lb/hr
Yd		Carbon	0.05 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	5
Location	Jefferson Junction, WI	Start	11:35 PM
Stack ID	Fan #5 Outlet	Stop	11:45 PM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
F-1	0.065	0.255	74.0
2	0.050	0.224	75.0
3	0.050	0.224	75.0
4	0.045	0.212	76.0
5	0.050	0.224	76.0
6	0.040	0.200	76.0
E-1	0.065	0.255	75.0
2	0.070	0.265	75.0
3	0.060	0.245	76.0
4	0.060	0.245	76.0
5	0.060	0.245	76.0
6	0.085	0.292	76.0
D-1	0.085	0.292	75.0
2	0.085	0.292	75.0
3	0.080	0.283	76.0
4	0.080	0.283	76.0
5	0.085	0.292	77.0
6	0.120	0.346	77.0
C-1	0.115	0.339	76.0
2	0.110	0.332	77.0
3	0.115	0.339	77.0
4	0.105	0.324	77.0
5	0.110	0.332	77.0
6	0.120	0.346	77.0
B-1	0.135	0.367	75.0
2	0.145	0.381	76.0
3	0.135	0.367	76.0
4	0.110	0.332	76.0
5	0.100	0.316	77.0
6	0.110	0.332	77.0
A-1	0.175	0.418	77.0
2	0.170	0.412	77.0
3	0.165	0.406	77.0
4	0.145	0.381	77.0
5	0.125	0.354	77.0
6	0.115	0.339	77.0
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36	0.0983	0.3080	76.17

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	6
Location	Jefferson Junction, WI	Start	02:05 AM
Stack ID	Fan #1 Outlet	Stop	02:15 AM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.18 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0276
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.54 lb/lb-mole
Cp	0.84	Vs	18.34 ft/s
Tm	° F	Qs	23,042 acfm
(DP) ^{1/2}	0.3252	Qs	1,385,253 scfh
Ts	73.7 ° F	Qs(d)	22,450 dscfm
Vm	ft ³		
Dn	in	C3H8	0.016 lb/hr
As	20.94 ft ²	Carbon	0.013 lb/hr
Yd		Carbon	0.06 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	6
Location	Jefferson Junction, WI	Start	02:05 AM
Stack ID	Fan #1 Outlet	Stop	02:15 AM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
F-1	0.060	0.245	74.0
2	0.065	0.255	74.0
3	0.070	0.265	74.0
4	0.055	0.235	74.0
5	0.050	0.224	74.0
6	0.035	0.187	74.0
E-1	0.075	0.274	73.0
2	0.080	0.283	73.0
3	0.085	0.292	73.0
4	0.095	0.308	73.0
5	0.075	0.274	74.0
6	0.055	0.235	74.0
D-1	0.110	0.332	73.0
2	0.115	0.339	73.0
3	0.120	0.346	73.0
4	0.080	0.283	73.0
5	0.105	0.324	74.0
6	0.125	0.354	74.0
C-1	0.135	0.367	73.0
2	0.145	0.381	73.0
3	0.140	0.374	74.0
4	0.115	0.339	74.0
5	0.120	0.346	74.0
6	0.115	0.339	74.0
B-1	0.155	0.394	73.0
2	0.160	0.400	74.0
3	0.140	0.374	74.0
4	0.115	0.339	74.0
5	0.105	0.324	74.0
6	0.095	0.308	74.0
A-1	0.195	0.442	73.0
2	0.190	0.436	74.0
3	0.175	0.418	74.0
4	0.150	0.387	74.0
5	0.125	0.354	74.0
6	0.110	0.332	74.0
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36	0.1094	0.3252	73.67

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	6
Location	Jefferson Junction, WI	Start	01:10 AM
Stack ID	Fan #2 Outlet	Stop	01:20 AM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.32 in H2O		
Vlc	12.5 g	Ps	30.32 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0316
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.49 lb/lb-mole
Cp	0.84	Vs	25.25 ft/s
Tm	° F	Qs	31,720 acfm
(DP) ^{1/2}	0.4457	Qs	1,893,238 scfh
Ts	77.7 ° F	Qs(d)	30,555 dscfm
Vm	ft ³		
Dn	in	C3H8	0.022 lb/hr
As	20.94 ft ²	Carbon	0.018 lb/hr
Yd		Carbon	0.08 tpy

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Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	6
Location	Jefferson Junction, WI	Start	01:10 AM
Stack ID	Fan #2 Outlet	Stop	01:20 AM

Flow Averages Calcs >>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
F-1	0.005	0.071	77.0
2	0.005	0.071	78.0
3	0.005	0.071	78.0
4	0.005	0.071	78.0
5	0.005	0.071	78.0
6	0.005	0.071	78.0
E-1	0.010	0.100	78.0
2	0.005	0.071	78.0
3	0.015	0.122	78.0
4	0.020	0.141	78.0
5	0.020	0.141	78.0
6	0.005	0.071	78.0
D-1	0.115	0.339	78.0
2	0.145	0.381	78.0
3	0.175	0.418	78.0
4	0.195	0.442	78.0
5	0.185	0.430	78.0
6	0.075	0.274	78.0
C-1	0.350	0.592	77.0
2	0.485	0.696	78.0
3	0.535	0.731	78.0
4	0.575	0.758	78.0
5	0.475	0.689	78.0
6	0.370	0.608	78.0
B-1	0.530	0.728	78.0
2	0.585	0.765	78.0
3	0.620	0.787	78.0
4	0.580	0.762	78.0
5	0.405	0.636	78.0
6	0.315	0.561	78.0
A-1	0.435	0.660	76.0
2	0.545	0.738	76.0
3	0.595	0.771	77.0
4	0.585	0.765	77.0
5	0.545	0.738	77.0
6	0.495	0.704	77.0
36	0.2783	0.4457	77.72

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	6
Location	Jefferson Junction, WI	Start	01:45 AM
Stack ID	Fan #3 Outlet	Stop	01:55 AM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.10 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0257
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.56 lb/lb-mole
Cp	0.84	Vs	40.93 ft/s
Tm	° F	Qs	51,414 acfm
(DP)½	0.7273	Qs	3,102,774 scfh
Ts	71.5 ° F	Qs(d)	50,384 dscfm
Vm	ft ³		
Dn	in	C3H8	0.035 lb/hr
As	20.94 ft ²	Carbon	0.029 lb/hr
Yd		Carbon	0.13 tpy

g:\projects\95502aq\ladvmd6.wk3

27-Nov-95
07:38 AM

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	6
Location	Jefferson Junction, WI	Start	01:45 AM
Stack ID	Fan #3 Outlet	Stop	01:55 AM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.985	0.992	72.0
2	0.910	0.954	73.0
3	0.830	0.911	73.0
4	0.720	0.849	73.0
5	0.615	0.784	73.0
6	0.635	0.797	73.0
B-1	0.925	0.962	72.0
2	0.910	0.954	72.0
3	0.825	0.908	72.0
4	0.375	0.612	72.0
5	0.435	0.660	73.0
6	0.590	0.768	73.0
C-1	0.885	0.941	72.0
2	0.870	0.933	72.0
3	0.850	0.922	72.0
4	0.435	0.660	72.0
5	0.295	0.543	72.0
6	0.710	0.843	72.0
D-1	0.805	0.897	71.0
2	0.760	0.872	71.0
3	0.675	0.822	71.0
4	0.550	0.742	71.0
5	0.230	0.480	71.0
6	0.415	0.644	71.0
E-1	0.580	0.762	71.0
2	0.615	0.784	71.0
3	0.495	0.704	71.0
4	0.270	0.520	71.0
5	0.180	0.424	71.0
6	0.150	0.387	71.0
F-1	0.305	0.552	70.0
2	0.325	0.570	70.0
3	0.285	0.534	70.0
4	0.195	0.442	70.0
5	0.235	0.485	70.0
6	0.325	0.570	70.0
36	0.5610	0.7273	71.53

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	6
Location	Jefferson Junction, WI	Start	01:25 AM
Stack ID	Fan #4 Outlet	Stop	01:35 AM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.15 in H2O		
Vlc	12.5 g	Ps	30.31 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0315
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.50 lb/lb-mole
Cp	0.84	Vs	29.62 ft/s
Tm	° F	Qs	37,206 acfm
(DP) ^{1/2}	0.5228	Qs	2,220,533 scfh
Ts	77.5 ° F	Qs(d)	35,845 dscfm
Vm	ft ³		
Dn	in	C3H8	0.026 lb/hr
As	20.94 ft ²	Carbon	0.021 lb/hr
Yd		Carbon	0.09 tpy

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27-Nov-95
07:38 AM

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	6
Location	Jefferson Junction, WI	Start	01:25 AM
Stack ID	Fan #4 Outlet	Stop	01:35 AM

Flow Averages Calcs >>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
F-1	0.005	0.071	73.0
2	0.005	0.071	75.0
3	0.005	0.071	76.0
4	0.005	0.071	77.0
5	0.005	0.071	77.0
6	0.010	0.100	77.0
E-1	0.180	0.424	76.0
2	0.225	0.474	77.0
3	0.255	0.505	78.0
4	0.270	0.520	78.0
5	0.255	0.505	78.0
6	0.195	0.442	78.0
D-1	0.335	0.579	78.0
2	0.370	0.608	78.0
3	0.395	0.628	78.0
4	0.415	0.644	78.0
5	0.325	0.570	78.0
6	0.195	0.442	78.0
C-1	0.490	0.700	77.0
2	0.515	0.718	78.0
3	0.525	0.725	78.0
4	0.540	0.735	78.0
5	0.455	0.675	78.0
6	0.235	0.485	78.0
B-1	0.435	0.660	78.0
2	0.475	0.689	78.0
3	0.505	0.711	78.0
4	0.515	0.718	78.0
5	0.405	0.636	78.0
6	0.285	0.534	78.0
A-1	0.495	0.704	78.0
2	0.490	0.700	78.0
3	0.505	0.711	78.0
4	0.445	0.667	78.0
5	0.410	0.640	78.0
6	0.385	0.620	78.0
36	0.3211	0.5228	77.53

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	6
Location	Jefferson Junction, WI	Start	01:35 AM
Stack ID	Fan #5 Outlet	Stop	01:45 AM

Meter Box	N/A		
Pb	30.30 in Hg		
Static	0.21 in H2O		
Vlc	12.5 g	Ps	30.32 in Hg
VOC	0.1 ppmv	Vmstd	ft ³
Theta	60 min	Vwstd	0.59 ft ³
O2	20.9 %	Bwo	0.0272
CO2	0.0 %	Below Sat.	NO
N2	79.1 %	Md	28.84 lb/lb-mole
DH	in H2O	Ms	28.54 lb/lb-mole
Cp	0.84	Vs	25.57 ft/s
Tm	° F	Qs	32,120 acfm
(DP) ^{1/2}	0.4536	Qs	1,932,892 scfh
Ts	73.2 ° F	Qs(d)	31,339 dscfm
Vm	ft ³		
Dn	in	C3H8	0.022 lb/hr
As	20.94 ft ²	Carbon	0.018 lb/hr
Yd		Carbon	0.08 tpy

g:\projects\95502aql\advmd6.wk3

27-Nov-95
07:38 AM

Client	Ladish Malting Company	Date	11/15/95
Unit	Kiln No. 15 Malt Dryer Exhaust	Run	6
Location	Jefferson Junction, WI	Start	01:35 AM
Stack ID	Fan #5 Outlet	Stop	01:45 AM

Flow Averages Calcs >>>>>>>

	Delta p	Sqrt Delta p	Ts (°F)
A-1	0.425	0.652	75.0
2	0.385	0.620	75.0
3	0.365	0.604	75.0
4	0.295	0.543	75.0
5	0.280	0.529	75.0
6	0.195	0.442	75.0
B-1	0.345	0.587	74.0
2	0.340	0.583	74.0
3	0.280	0.529	74.0
4	0.225	0.474	74.0
5	0.230	0.480	74.0
6	0.290	0.539	74.0
C-1	0.265	0.515	72.0
2	0.270	0.520	72.0
3	0.255	0.505	73.0
4	0.205	0.453	73.0
5	0.275	0.524	73.0
6	0.345	0.587	73.0
D-1	0.225	0.474	73.0
2	0.215	0.464	73.0
3	0.195	0.442	73.0
4	0.180	0.424	73.0
5	0.175	0.418	73.0
6	0.310	0.557	74.0
E-1	0.145	0.381	72.0
2	0.135	0.367	72.0
3	0.145	0.381	72.0
4	0.120	0.346	72.0
5	0.090	0.300	73.0
6	0.270	0.520	73.0
F-1	0.065	0.255	72.0
2	0.075	0.274	72.0
3	0.070	0.265	72.0
4	0.065	0.255	72.0
5	0.065	0.255	72.0
6	0.070	0.265	72.0
36	0.2190	0.4536	73.19

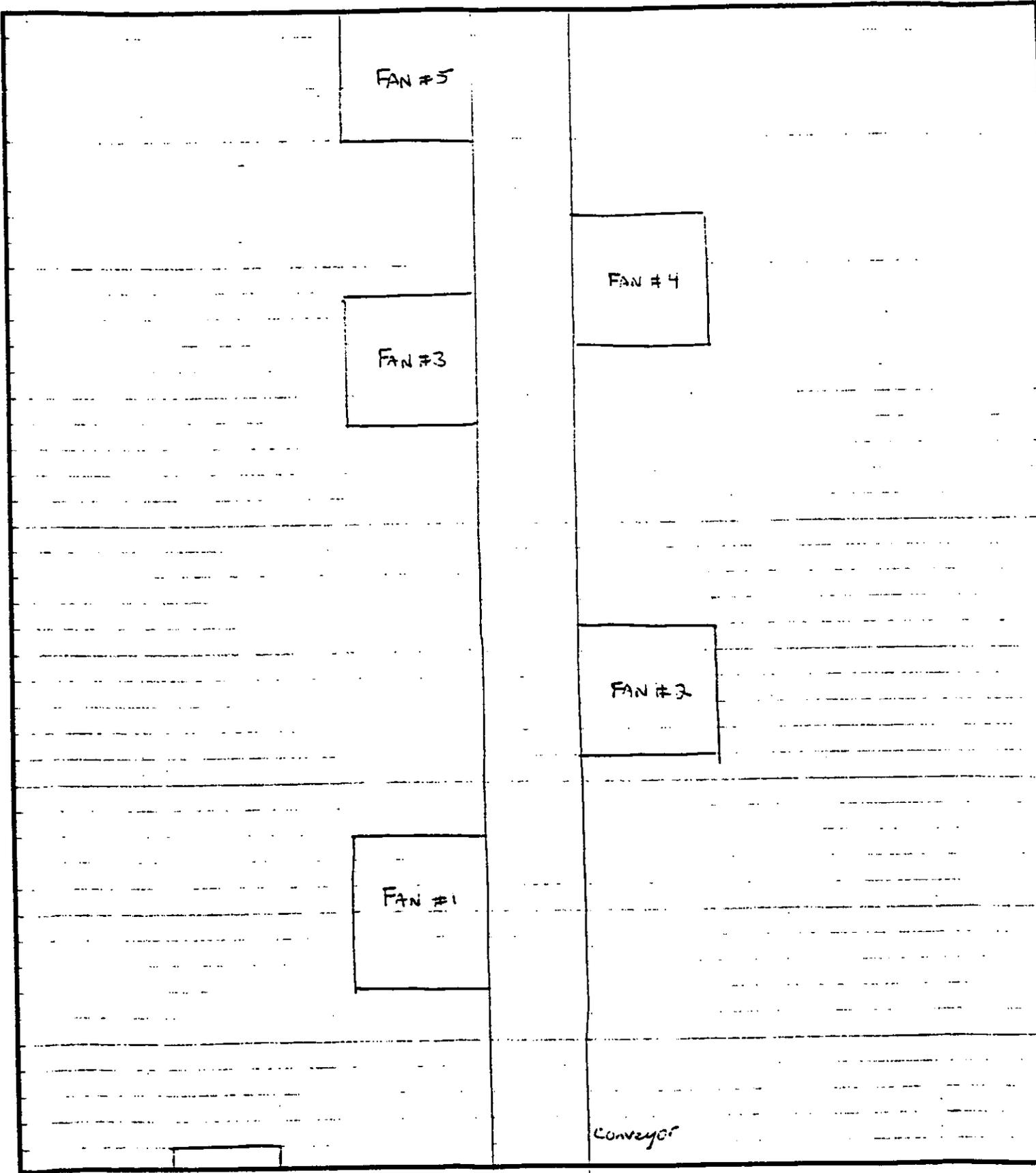
APPENDIX B

Field Data



PROJECT Liquid Molding
SHEET NO. VCC Testing
CALCULATED BY: _____
CHECKED BY: _____

NO. _____
OF Floor Layout
DATE 11-14-95
DATE _____



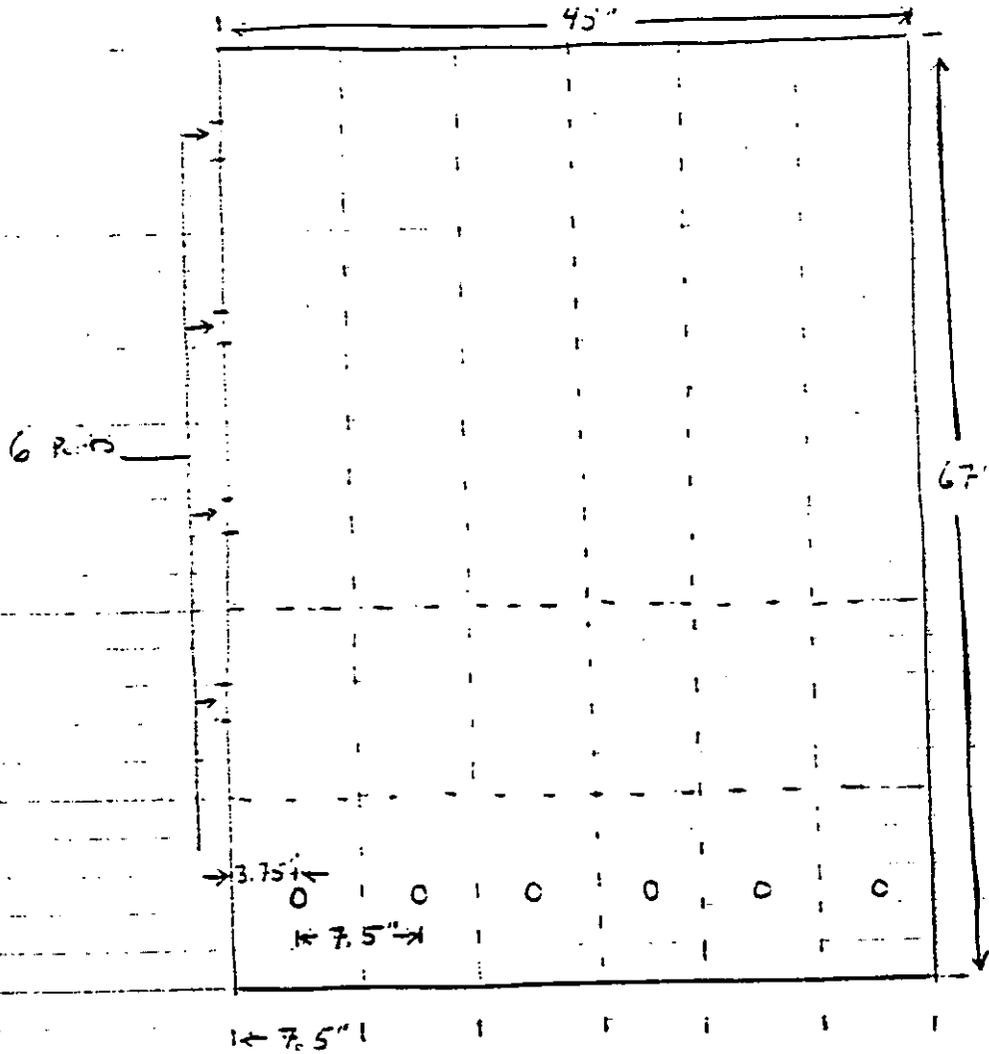
Door
Elev. Port



PROJECT Lacfish Maltng
 SHEET NO. vcc Testing
 CALCULATED BY: JKA
 CHECKED BY: _____

NO. _____
 OF Traverse Point Location
 DATE 11-15-95
 DATE _____

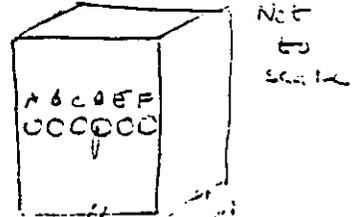
"Traverse Point Location"



Point #	Distance (inches)	(Five Ducts)
1	3.75	
2	11.25	
3	18.75	
4	26.25	
5	33.75	
6	41.25	


Fluid Management, Inc.
 Air Sciences & Engineering Group
 VELOCITY TRAVERSE DATA SHEET

CLIENT <i>Wish Mills</i>	DATE <i>11-17-95</i>	TEST NO. <i>1</i>
FMI Project # <i>12.502</i>		
FMI Personnel <i>JKA, MBW</i>		
Plant Location <i>2210</i>		
Stack ID <i>E15 K11</i>		
Stack Diameter (ft) <i>4.5" x 6.0"</i>		
Stack X-Area (ft ²) <i>140.94</i>		
Pitot ID # <i>6.1</i>	Pitot Cp <i>0.84</i>	
Pre-Pitot Leak Check <i>OK</i>	Post-Pitot Leak Check <i>OK</i>	
Bar Press (in Hg) <i>30.30</i>	Amb. Temp. <i>54°F</i>	
# of Traverse Points (n) <i>6 x 6</i>		
Differential Static Press (in H ₂ O) <i>10.05</i>		
Differential Static Press (in Hg)	Stack Press	
Start Time <i>10:00</i>	Stop Time <i>10:15</i>	Stack Port Drawing



TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE (°F)		SQRT DELTA P	COMMENTS
1A 1D	0.680	470	69	71	1st pt not exact due to infra-structure
2 2	0.665	415	70	71	
3 3	0.585	475	70	71	
4 4	0.485	285	70	72	
5 5	0.720	780	70	72	
6 6	0.555	450	70	72	
1B 1E	0.85	310	71	71	Bags on @ 10am
2 2	0.545	305	71	71	
3 3	0.365	320	71	72	
4 4	0.280	260	71	72	
5 5	0.285	325	71	72	
6 6	0.335	335	71	72	
1C 1E	0.55	225	70	72	Bags off @ 11:20 am
2 2	0.530	220	71	72	
3 3	0.575	215	71	72	
4 4	0.325	145	71	72	
5 5	0.460	075	71	72	
6 6	0.395	070	71	72	
AVERAGE					Fans @ 10:00 ~ 65%

CO ₂ (%)	Molecular Weight - Md
O ₂ (%)	Velocity - V _s (ft/min)
N ₂ (%)	Flow Rate - Q (scfm)

EQUATIONS:

$P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
 $\%N_2 = 100 - [(\% O_2) + (\% CO_2) - (\% CO)]$
 $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] - [0.23 * ((\% N_2) + (\% CO))]$
 $M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$
 $B_{wo} = V_{wl} / (V_m + V_{mc})$
 $V_m(\text{std}) = 17.467 * [(V_m * P_m) / T_m]$
 $V_s = 85.49 * (C_p) * (\text{AVG}(\text{SQRT } dP) * \text{SQRT}(T_s / (P_s * M_s)))$
 $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
 $C_p = 2.205 * 10^{-6} \text{ lb/mg} * (M_p / V_m(\text{std}))$
 $ER_p = Q_s * C_p$
 $\% ISO = 100 * (0.09457 * (T_s - 460) * V_m(\text{std}) / ((P_s) * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100)))$


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 VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Ladish Main</u>	DATE <u>11/14/95</u>	TEST NO. <u>1</u>
FMI Project # <u>95-505</u>	SIME AS FAVE/	
FMI Personnel <u>J&A/maw</u>		
Plant Location <u>J&A/maw</u>		
Stack ID <u>R15K1a FIVE 2</u>		
Stack Diameter (ft) <u>4.5" x 6.3"</u>		
Stack X-Area (ft ²) <u>20.44</u>		
Pitot ID # <u>6 Effective</u>	Pitot Cp <u>0.84</u>	
Pre-Pitot Leak Check <u>OK</u>	Post-Pitot Leak Check	
Bar Press (in Hg) <u>30.30</u>	Amb. Temp.	
# of Traverse Points (n) <u>6 x 6</u>		
Differential Static Press (in H2O) <u>TC.06</u>		
Differential Static Press (in Hg)	Stack Press	
Start Time <u>11:35</u>	Stop Time <u>12:00</u>	Stack / Port Drawing

TRAVERSE		DELTA P		STACK TEMPERATURE		SQRT DELTA P	COMMENTS
Point #		(in H2O)		(°F)	(°R)		
1A	1D	1.05	73	260	71		
2	2	1.10	73	260	71		
3	3	1.15	73	260	73		
4	4	1.10	73	260	72		
5	5	1.30	73	265	73		
6	6	1.15	73	270	73		
1B	1E	1.30	73	100	71		
2	2	1.85	73	130	73		
3	3	1.75	73	165	73		
4	4	1.05	73	165	72		
5	5	1.15	73	165	72		
6	6	1.40	73	185	73		
1C	1F	1.70	73	100	71		
2	2	1.65	73	100	73		
3	3	1.70	73	125	72		
4	4	1.65	73	120	73		
5	5	1.85	73	115	73		
6	6	1.20	73	110	73		

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- Ps = Pbar - Pstatic / (13.6 in. H2O/in. Hg)
- %N2 = 100 - ((% O2) + (% CO2) - (% CO))
- Md = [0.44 * (% CO2)] - [0.32 * (% O2)] - [0.23 * ((% N2) + (% CO))]
- Ms = Md * (1 - Bwo) + 18 * Bwo
- Bwo = Vw / (Vm + Vwc)
- Vm(std) = 17.467 * [(Vm * Pm) / Tm]
- Vs = 85.49 * (Cp) * (AVG(SQRT dP)) * SQRT[(Ts / (Ps * Ms))]
- Qs = 63.529 * Vs * As * (1 - Bwo) * (Ps / Ts)
- Cp = 2.205^-6 lb/mg * (Mpw / Vm(std))
- ERp = Qs * Cp
- % ISO = 100 * (0.09457 * (Ts + 460) * Vm(std) / ((Ps) * vs * ((0.5 * Dn)^2 * 3.141716 / 144) * theta * (1 - Bwo / 100)))

MSWVELOCITY.WGI

Ladish Fan ID #'s opposite of FMI's
 (i.e. 1 → 5 Ladish)
 5 → 1 FMI



Fluid Management, Inc.

Air Sciences & Engineering Group

VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Kulish Malaysia</u>	DATE <u>11-17-95</u>	TEST NO. <u>1</u>
FMI Project # <u>95-502</u>		
FMI Personnel <u>JKA/MBW</u>		<u>SAME AS FAN #1</u>
Plant Location <u>Johore</u>		
Stack ID <u>#15 K-10 Fan #3</u>		
Stack Diameter (ft) <u>45" x 6.3"</u>		
Stack X-Area (ft ²) <u>20.94</u>		
Pitot ID # <u>6 effective</u>	Pitot Cp <u>0.84</u>	
Pre-Pitot Leak Check <u>OR</u>	Post-Pitot Leak Check	
Bar Press (in Hg) <u>30.30</u>	Amb. Temp. <u>69</u>	
# of Traverse Points (n) <u>6 x 5</u>		
Differential Static Press (in H2O) <u>+0.04</u>		
Differential Static Press (in Hg)	Stack Press	
Start Time <u>1030</u>	Stop Time <u>1050</u>	Stack / Port Drawing

TRAVERSE Point #	DELTA P (in H2O)	STACK TEMPERATURE (°F)	SQRT DELTA P (°R)	COMMENTS
1 1	900	73	1.675	1st pt not exact due to infra-structure
2 2	890	73	1.670	
3 3	870	73	1.595	
4 4	860	73	1.465	
5 5	400	73	1.55	
6 6	500	73	1.320	
1B 1B	850	73	1.380	
2 2	860	73	1.405	
3 3	840	74	1.375	
4 4	420	74	1.385	
5 5	1475	73	1.35	
6 6	575	74	1.205	
1C 1C	785	74	1.225	
2 2	775	74	1.220	
3 3	760	74	1.15	
4 4	1380	74	1.35	
5 5	140	74	1.075	
6 6	610	74	1.185	

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - (\% O_2) - (\% CO_2) - (\% CO)$
- $M_d = [0.44 * (\% CO_2)] - [0.32 * (\% O_2)] - [0.23 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$
- $B_{wo} = V_{wl} / (V_m - V_{mc})$
- $V_m(\text{std}) = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(\text{SQRT } dP)) * \text{SQRT}[T_s / (P_s * M_s)]$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205^{-6} \text{ lb/mg} * (M_p / V_m(\text{std}))$
- $ER_p = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_m(\text{std}) / ((P_s) * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \text{thera} * (1 - B_{wo} / 100)))$



Air Sciences & Engineering Group

VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Luich Mch...</u>	DATE <u>11-14-95</u>	TEST NO. <u> </u>
FMI Project # <u>25-22</u>		SAME AS FAN # 1
FMI Personnel <u>JR & LINDA</u>		
Plant Location <u>TITL...</u>		
Stack ID <u>F15</u>		
Stack Diameter (ft) <u>4.5</u>		
Stack X-Area (ft ²) <u>20.24</u>		
Pitot ID # <u>6</u>	Pitot Co. <u>10.24</u>	
Pre-Pitot Leak Check <u>OK</u>	Post-Pitot Leak Check	
Bar Press (in Hg) <u>30.30</u>	Amb. Temp. <u>64</u>	
# of Traverse Points (n) <u>6 x 6</u>		
Differential Static Press (in H ₂ O) <u>10.02</u>		
Differential Static Press (in Hg)	Stack Press	
Start Time <u>1120</u>	Stop Time <u>1140</u>	Stack Port Drawing

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE (°F)	SQRT DELTA P	COMMENTS
1 A 1 D	810 76	610 75		Sulfur on @ 10-15-20
2 2	825 76	630 76		
3 3	830 76	620 76		
4 4	825 76	620 76		
5 5	810 76	620 76		
6 6	850 76	675 76		
1 B 1 E	735 76	455 76		
2 2	725 75	495 76		
3 3	710 75	560 76		
4 4	705 75	535 76		
5 5	695 76	525 76		
6 6	465 76	305 76		
1 C 1 F	780 75	650 76		
2 2	785 75	630 76		
3 3	800 76	630 76		
4 4	710 76	660 76		
5 5	685 76	605 76		
6 6	335 76	2040 76		

AVERAGE

CO ₂ (%)	Molecular Weight - Md
O ₂ (%)	Velocity - V _s (ft/min)
N ₂ (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - [(\% O_2) + (\% CO_2) + (\% CO)]$
- $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] + [0.28 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$
- $B_{wo} = V_{wv} / (V_m - V_{mc})$
- $V_{m(std)} = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT(T_s / (P_s * M_s))$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205 * 10^{-6} \text{ lb/mg} * (M_p / V_{m(std)})$
- $ER_p = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_{m(std)} / ((P_s) * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100)))$


Fluid Management, Inc.
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 VELOCITY TRAVERSE DATA SHEET

CLIENT <i>Livingston</i>	DATE <i>11-14-95</i>	TEST NO.
FMI Project # <i>275502</i>		Same as FAN # 1
FMI Personnel <i>JKA/mi36</i>		
Plant Location <i>Te Anau</i>		
Stack ID <i>#15 1/2 in Fan #5</i>		
Stack Diameter (ft) <i>4.5" x 2.2"</i>		
Stack X-Area (ft ²) <i>20.70</i>		
Pitot ID # <i>1.0</i>	Pitot Cp <i>0.84</i>	
Pre-Pitot Leak Check <i>OK</i>	Post-Pitot Leak Check	
Bar Press (in Hg) <i>30.30</i>	Amb. Temp. <i>64</i>	
# of Traverse Points (n) <i>2 x 6</i>		
Differential Static Press (in H ₂ O) <i>+0.06</i>		
Differential Static Press (in Hg)	Stack Press <i>1115</i>	Stack Port Drawing
Start Time <i>1100</i>	Stop Time	

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE (°F)	SQRT DELTA P	COMMENTS
1A 1D	640 74	450 74		
2 2	670 74	470 74		
3 3	695 74	375 74		
4 4	600 74	300 74		
5 5	350 74	290 74		
6 6	440 74	510 74		
1B 1E	555 74	225 72		
2 2	560 73	210 72		
3 3	55 74	265 72		
4 4	305 74	215 74		
5 5	380 74	135 74		
6 6	475 74	425 74		
1C 1E	405 73	100 73		
2 2	400 73	100 73		
3 3	115 74	110 73		
4 4	135 74	085 74		
5 5	525 74	075 74		
6 6	505 74	100 74		

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

$P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
 $\%N_2 = 100 - ((\% O_2) + (\% CO_2) + (\% CO))$
 $M_d = (0.44 * (\% CO_2)) + (0.52 * (\% O_2)) + (0.28 * ((\% N_2) + (\% CO)))$
 $M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$
 $B_{wo} = V_{wl} / (V_m - V_{mc})$
 $V_{m(std)} = 17.467 * ((V_m * P_m) / T_m)$
 $V_s = 85.49 * (C_p) * (AVG(SQRT \Delta P)) * SQRT(T_s / (P_s * M_s))$
 $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
 $C_p = 2.205 * 6 \text{ lb/mg} * (M_p / V_{m(std)})$
 $ER_p = Q_s * C_p$
 $\% ISO = 100 * (0.09457 * (T_s - 460) * V_{m(std)} / ((P_s) * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \text{thick} * (1 - B_{wo} / 100)))$

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VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Lady's Machine Co</u>	DATE <u>10/14/80</u>	TEST NO. <u>2</u>
FMI Project # <u>745-5-7</u>		
FMI Personnel <u>JCA/P/min</u>		
Plant Location <u>Johnson</u>		
Stack ID <u>Part # (let #5)</u>		
Stack Diameter (ft) <u>45" x (6")</u>		
Stack X-Area (ft ²) <u>29.44</u>		
Pitot ID # <u>6 effective</u>	Pitot Cp <u>0.84</u>	
Pre-Pitot Leak Check <u>ok</u>	Post-Pitot Leak Check <u>ok</u>	
Bar Press (in Hg) <u>30.30</u>	Amb. Temp. <u>64</u>	
# of Traverse Points (n) <u>6x6</u>		
Differential Static Press (in H ₂ O) <u>+0.085</u>		
Differential Static Press (in Hg)	Stack Press	
Start Time <u>1450</u>	Stop Time <u>1505</u>	Stack / Port Drawing

TRAVERSE	Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
			(°F)	(°R)		
1 A	1 D	1.55	72	780	1.25	
2	2	.45	72	780	.73	
3	3	.40	72	780	.73	
4	4	1.00	73	785	.73	
5	5	.75	73	790	.73	
6	6	.80	73	790	.73	
1 B	1 E	1.55	72	780	1.25	
2	2	1.20	72	780	.73	
3	3	.90	73	790	.73	
4	4	1.00	73	790	.73	
5	5	.75	73	790	.73	
6	6	.80	73	790	.73	
1 C	1 F	1.75	72	785	1.25	
2	2	1.70	72	785	.73	
3	3	1.05	73	795	.73	
4	4	1.25	73	795	.73	
5	5	.85	73	795	.73	
6	6	.90	73	795	.73	

AVERAGE

CO ₂ (%)	Molecular Weight - Md
O ₂ (%)	Velocity - V _s (ft/min)
N ₂ (%)	Flow Rate - Q (scfm)

EQUATIONS:

$P_s = P_{bar} - P_{static} (13.6 \text{ in. H}_2\text{O/in. Hg})$
 $\%N_2 = 100 - [(\% O_2) + (\% CO_2) + (\% CO)]$
 $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] + [0.28 * ((\% N_2) + (\% CO))]$
 $M_s = M_d * (1 - B_{wo}) - 18 * B_{wo}$
 $B_{wo} = V_{wl} / (V_m - V_{mc})$
 $V_m(\text{std}) = (7.467 * [(V_m * P_m) / T_m])$
 $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT(T_s / (P_s * M_s))$
 $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
 $C_p = 2.205 * 6 \text{ lb/mg} * (M_p / V_m(\text{std}))$
 $ERP = Q_s * C_p$
 $\% ISO = 100 * (0.09457 * (T_s - 460) * V_m(\text{std}) / ((P_s * V_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100)))$


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 VELOCITY TRAVERSE DATA SHEET

CLIENT <i>Ladish Mfg</i>	DATE <i>11-14-95</i>	TEST NO. <i>2</i>
FMI Project # <i>195-302</i>		
FMI Personnel <i>JKA (MFA)</i>		
Plant Location <i>Jefferson</i>		
Stack ID <i>Far #1 (Ladish Env #1)</i>		
Stack Diameter (ft) <i>45 x 65</i>		
Stack X-Area (ft ²) <i>20.90</i>		
Pitot ID # <i>6 effective</i>	Pitot Cp <i>0.84</i>	
Pre-Pitot Leak Check <i>OK</i>	Post-Pitot Leak Check <i>OK</i>	
Bar Press (in Hg) <i>30.50</i>	Amb. Temp. <i>64</i>	
# of Traverse Points (n) <i>6 x 6</i>		
Differential Static Press (in H2O) <i>+ .71</i>		
Differential Static Press (in Hg)	Stack Press	
Start Time <i>1350</i>	Stop Time <i>1405</i>	Stack Port Drawing

TRAVERSE		DELTA P		STACK TEMPERATURE		SQRT DELTA P	COMMENTS
Point #	ID	(in H2O)		(°F)			
1A	1D	.011	71	170	72		Bags on @ 1350
2	2	.026	71	155	72		
3	3	.010	71	2.0	72		
4	4	.005	71	2.15	73		
5	5	.010	71	1.85	73		
6	6	.015	71	1.70	73		
1B	1E	.070	71	2.15	72		Bags off @ 1450
2	2	.060	71	2.20	73		
3	3	.065	71	2.75	73		
4	4	.230	71	2.85	73		
5	5	.150	71	2.05	73		
6	6	.065	71	1.85	73		
1c	1F	.022	71	2.50	72		
2	2	.865	71	3.60	73		
3	3	1.10	72	2.65	73		
4	4	1.30	72	2.45	73		
5	5	1.15	72	2.30	73		
6	6	.825	72	2.40	73		

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - ((\% O_2) + (\% CO_2) - (\% CO))$
- $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] - [0.28 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$
- $B_{wo} = V_{wl} / (V_m - V_{mc})$
- $V_m(\text{std}) = 17.467 * ((V_m * P_m) / T_m)$
- $V_s = 85.49 * (C_p) * (AVG(\text{SQRT } dP)) * \text{SQRT}[(T_s / (P_s * M_s))]$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205 * 6 \text{ lb/mg} * (M_p / V_m(\text{std}))$
- $ER_p = Q_s * C_p$
- $\% \text{ ISO} = 100 * (0.09457 * (T_s - 460) * V_m(\text{std}) / ((P_s) * v_s * ((0.5 * D_u)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100)))$


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 VELOCITY TRAVERSE DATA SHEET

CLIENT <i>Ladakh, Michigan</i>	DATE <i>11-4-85</i>	TEST NO. <i>2</i>
FMI Project # <i>45-507</i>		
FMI Personnel <i>JCA/mgw</i>		
Plant Location <i>Tellus</i>		
Stack ID <i>Line 3 (Unit 3)</i>		
Stack Diameter (ft) <i>45" x 27"</i>		
Stack X-Area (ft ²) <i>20.70</i>		
Pitot ID # <i>6 effective</i>	Pitot Cp <i>0.84</i>	
Pre-Pitot Leak Check <i>ok</i>	Post-Pitot Leak Check <i>ok</i>	
Bar Press (in Hg) <i>30.30</i>	Amb. Temp. <i>64</i>	
# of Traverse Points (n) <i>6 x 6</i>		
Differential Static Press (in H2O) <i>+0.425</i>		
Differential Static Press (in Hg)	Stack Press	
Start Time <i>1425</i>	Stop Time <i>1450</i>	Stack Port Drawing

TRAVERSE Point #	DELTA P (in H2O)	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
		(°F)	(°R)		
1 A 1 D	0.95	74	135	74	
2 2	0.85	74	130	74	
3 3	0.75	75	130	74	
4 4	0.70	75	125	75	
5 5	0.70	75	125	75	
6 6	1.15	75	130	75	
1 B 1 E	0.55	74	125	75	
2 2	0.90	74	125	75	
3 3	1.40	75	120	75	
4 4	0.75	75	120	75	
5 5	0.810	75	130	75	
6 6	1.35	75	120	75	
1 C 1 F	0.85	75	120	75	
2 2	0.30	75	125	75	
3 3	1.55	75	115	75	
4 4	0.05	75	110	75	
5 5	0.15	75	120	75	
6 6	1.30	75	120	75	

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} + P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - [(\% O_2) + (\% CO_2) + (\% CO)]$
- $Md = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] + [0.23 * ((\% N_2) + (\% CO))]$
- $M_s = Md * (1 - Bwo) + 18 * Bwo$
- $Bwo = V_{wl} / (V_m + V_{mc})$
- $V_m(std) = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT[T_s / (P_s * M_s)]$
- $Q_s = 63.529 * V_s * A_s * (1 - Bwo) * (P_s / T_s)$
- $C_p = 2.205^{-6} \text{ lb/mg} * (M_p / V_m(std))$
- $ER_p = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_m(std) / ((P_s) * v_s * ((0.5 * D_m)^2 * 3.141716 / 144) * \theta * (1 - Bwo / 100)))$


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 VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Laksh</u>	DATE <u>11-14-95</u>	TEST NO. <u>2</u>
FMI Project # <u>J95.202</u>		
FMI Personnel <u>TKJ/mpr</u>		
Plant Location <u>Tekkenon</u>		
Stack ID <u>Fan 4 (Laksh #?)</u>		
Stack Diameter (ft) <u>4.5 x 6.711</u>		
Stack X-Area (ft ²) <u>20.99</u>		
Pitot ID # <u>6 effective</u>	Pitot Cp <u>0.89</u>	
Pre-Pitot Leak Check <u>ok</u>	Post-Pitot Leak Check <u>ok</u>	
Bar Press (in Hg) <u>30.30</u>	Amb. Temp. <u>64</u>	
# of Traverse Points (n) <u>6 x 6</u>		
Differential Static Press (in H ₂ O) <u>70.09</u>		
Differential Static Press (in Hg)	Stack Press	
Start Time <u>1405</u>	Stop Time <u>1420</u>	Stack Port Drawing

TRAVERSE		DELTA P	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
Point #		(in H ₂ O)	(°F)	(°R)		
1A	1D	1.30	74	1.30	1.14	
2	2	1.35	74	1.40	1.15	
3	3	1.15	74	1.45	1.13	
4	4	1.10	74	1.40	1.13	
5	5	1.00	74	0.90	1.13	
6	6	1.00	74	1.50	1.13	
1B	1E	1.15	74	1.10	1.14	
2	2	1.10	74	1.10	1.14	
3	3	1.15	74	1.40	1.14	
4	4	1.10	74	1.05	1.15	
5	5	0.75	74	1.75	1.15	
6	6	0.75	74	1.60	1.15	
1C	1F	1.60	74	1.10	1.14	
2	2	1.70	74	1.10	1.14	
3	3	1.60	74	1.15	1.14	
4	4	1.50	74	1.80	1.14	
5	5	1.40	74	2.50	1.14	
6	6	1.30	74	2.20	1.15	

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

$$P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$$

$$\%N_2 = 100 - ((\% O_2) + (\% CO_2) + (\% CO))$$

$$M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] + [0.28 * ((\% N_2) + (\% CO))]$$

$$M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$$

$$B_{wo} = V_{wv} / (V_m - V_{mc})$$

$$V_m(\text{std}) = 17.467 * [(V_m * P_m) / T_m]$$

$$V_s = 85.49 * (C_p) * (AVG(\text{SQRT } \Delta P)) * \text{SQRT}[T_s / (P_s * M_s)]$$

$$Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$$

$$C_p = 2.205 * 10^{-6} \text{ lb/mg} * (M_p / V_m(\text{std}))$$

$$ER_p = Q_s * C_p$$

$$\% \text{ ISO} = 100 * (0.09457 * (T_s - 460) * V_m(\text{std}) / ((P_s) * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100)))$$



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VELOCITY TRAVERSE DATA SHEET

CLIENT <i>Sadash Machine</i>	DATE <i>11-14-85</i>	TEST NO. <i>2</i>
FMI Project # <i>795-502</i>		
FMI Personnel <i>JR/Mou</i>		
Plant Location <i>Jefferson</i>		
Stack ID <i>Fan 5 (Line 2)</i>		
Stack Diameter (ft) <i>4.5</i>		
Stack X-Area (ft ²) <i>20.70</i>		
Pitot ID # <i>6 effective</i>	Pitot Cp <i>0.84</i>	
Pre-Pitot Leak Check <i>OK</i>	Post-Pitot Leak Check	
Bar Press (in Hg) <i>30.30</i>	Amb. Temp. <i>64</i>	
# of Traverse Points (n) <i>6x6</i>		
Differential Static Press (in H ₂ O) <i>10.520</i>		
Differential Static Press (in Hg)	Stack Press	
Start Time <i>1425</i>	Stop Time <i>1435</i>	Stack / Port Drawing

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
		(°F)	(°R)		
1A 1	1.50	73	790	74	
2 2	1.15	73	810	74	
3 3	1.05	73	820	74	
4 4	1.675	73	1630	74	
5 5	1.90	73	335	74	
6 6	1.80	73	825	74	
1B 1 E	1.10	73	105	74	
2 2	1.05	73	110	75	
3 3	1.15	73	115	75	
4 4	1.10	73	100	75	
5 5	1.85	73	730	75	
6 6	1.90	73	520	75	
1C 1 E	1.80	73	220	73	
2 2	1.70	73	185	73	
3 3	1.80	74	190	74	
4 4	1.60	74	155	74	
5 5	1.70	74	150	74	
6 6	1.05	74	265	74	

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - (\%O_2) - (\%CO_2) - (\%CO)$
- $M_d = [0.44 * (\%CO_2)] + [0.32 * (\%O_2)] + [0.28 * ((\%N_2) + (\%CO))]$
- $M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$
- $B_{wo} = V_{wl} / (V_m + V_{mc})$
- $V_m(Std) = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT \Delta P)) * SQRT(T_s / (P_s * M_s))$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205^{-6} \text{ lb/mg} * (M_p / V_m(Std))$
- $ER_p = Q_s * C_p$
- $\%ISO = 100 * (0.09457 * (T_s - 460) * V_m(Std) / ((P_s * V_s * ((0.5 * D_p)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100)))$


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 VELOCITY TRAVERSE DATA SHEET

CLIENT <i>Ludlow Milling</i>	DATE <i>1-4</i>	TEST NO. <i>5</i>
FMI Project # <i>295502</i>		
FMI Personnel <i>JRT/WSCW</i>		
Plant Location <i>Tray #1 (Lead = 5) 5</i>		
Stack ID <i>Johnson #</i>		
Stack Diameter (ft) <i>10.5" x 6"</i>		
Stack X-Area (ft ²) <i>20.74</i>		
Pitot ID # <i>1 effect</i>	Pitot Cp <i>0.84</i>	
Pre-Pitot Leak Check <i>OK</i>	Post-Pitot Leak Check <i>OK</i>	
Bar Press (in Hg) <i>30.50</i>	Amb. Temp. <i>64</i>	
# of Traverse Points (n) <i>6 x 6</i>		
Differential Static Press (in H ₂ O) <i>T-0.920</i>		
Differential Static Press (in Hg)	Stack Press	
Start Time <i>1810</i>	Stop Time <i>1820</i>	Stack Port Drawing

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
		(°F)	(°C)		
1A	3.11	67	6.21	70	Bags on @ 1810
2	3.25	67	7.15	70	
3	3.0	67	6.50	70	
4	2.90	67	3.75	70	
5	1.30	67	5.5	70	
6	1.60	67	6.25	70	
1B	4.55	67	6.25	70	Bags off @ 1910
2	4.40	67	6.65	70	
3	4.20	67	5.10	70	
4	4.25	67	3.80	70	
5	2.05	67	4.70	70	
6	2.55	67	4.25	70	
1D	5.55	67	8.70	70	
2	5.65	70	8.30	70	
3	5.20	70	7.55	70	
4	2.40	70	6.80	70	
5	5.85	70	6.75	70	
6	5.50	70	5.60	70	

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - (\% O_2) - (\% CO_2) - (\% CO)$
- $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] + [0.28 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) - 18 * B_{wo}$
- $B_{wo} = V_{wu} / (V_m - V_{mc})$
- $V_{m(std)} = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT(T_s / (P_s * M_s))$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205 * 6 \text{ lb/mg} * (M_p / V_{m(std)})$
- $ER_p = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_{m(std)} / ((P_s * V_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100)))$


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 VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Cadash Petroleum</u>	DATE <u>11-14-75</u>	TEST NO. <u>3</u>
FMI Project # <u>T95-507</u>		
FMI Personnel <u>JR+MPLW</u>		
Plant Location <u>Unit 2, Leasing</u>		
Stack ID <u>Jackson</u>		
Stack Diameter (ft) <u>45" x 1.7"</u>		
Stack X-Area (ft ²) <u>1.20</u>		
Pitot ID # <u>6" Jetflow</u>	Pitot Co. <u>0-54</u>	
Pre-Pitot Leak Check <u>ok</u>	Post-Pitot Leak Check <u>ok</u>	
Bar Press (in Hg) <u>30.50</u>	Amb. Temp. <u>64</u>	
# of Traverse Points (n) <u>18</u>		
Differential Static Press (in H ₂ O) <u>+0.340</u>		
Differential Static Press (in Hg)	Stack Press	
Start Time <u>1905</u>	Stop Time <u>1915</u>	Stack Port Drawing

TRAVERSE	Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
			(°F)	(°R)		
1A	1D	1.05	71	515	1.11	
2	2	1.15	71	515	1.11	
3	3	1.15	71	515	1.11	
4	4	1.20	71	515	1.11	
5	5	1.15	71	515	1.11	
6	6	1.20	71	515	1.11	
1B	1E	1.05	71	515	1.11	
2	2	1.20	71	515	1.11	
3	3	1.05	71	515	1.11	
4	4	1.25	71	515	1.11	
5	5	1.20	71	515	1.11	
6	6	1.30	71	515	1.11	
1C	1F	1.55	71	515	1.11	
2	2	1.75	71	515	1.11	
3	3	1.65	71	515	1.11	
4	4	1.20	71	515	1.11	
5	5	1.45	71	515	1.11	
6	6	1.65	71	515	1.11	

AVERAGE

CO ₂ (%)	Molecular Weight - Md
O ₂ (%)	Velocity - V _s (ft/min)
N ₂ (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - [(\% O_2) + (\% CO_2) + (\% CO)]$
- $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] + [0.28 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$
- $B_{wo} = V_{wU} / (V_m + V_{mc})$
- $V_m(\text{std}) = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(\text{SQRT } dP)) * \text{SQRT}[T_s / (P_s * M_s)]$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205^{-6} \text{ lb/mg} * (M_p / V_m(\text{std}))$
- $ER_p = Q_s * C_p$
- $\% \text{ ISO} = 100 * (0.09457 * (T_s - 460) * V_m(\text{std}) / ((P_s) * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \text{theta} * (1 - B_{wo} / 100)))$

Fluid Management, Inc.

Air Sciences & Engineering Group

VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Lalorin Muttung</u>	DATE <u>11-14-95</u>	TEST NO. <u>3</u>
FMI Project # <u>JOS. 507</u>		
FMI Personnel <u>TG + MPTL</u>		
Plant Location <u>Telfer</u>		
Stack ID <u>Tru 3 Mod # 2</u>		
Stack Diameter (ft) <u>45" x 6"</u>		
Stack X-Area (ft ²) <u>1701.36</u>		
Pitot ID # <u>6 effective</u>	Pitot Cp <u>0.84</u>	
Pre-Pitot Leak Check <u>ok</u>	Post-Pitot Leak Check <u>ok</u>	
Bar Press (in Hg) <u>30.30</u>	Amb. Temp. <u>64</u>	
# of Traverse Points (n) <u>6 x 6</u>		
Differential Static Press (in H ₂ O) <u>+0.095</u>		
Differential Static Press (in Hg)	Stack Press	
Start Time <u>1820</u>	Stop Time <u>1830</u>	Stack Port Drawing

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
		(°F)	(°R)		
1 A 1 D	1.10	72	780	72	
2 2	1.05	72	830	73	
3 3	970	72	740	73	
4 4	790	72	59	72	
5 5	740	72	720	73	
6 6	1.05	72	415	72	
1 B 1 E	1.15	72	535	72	
2 2	1.10	72	550	72	
3 3	1.05	72	570	72	
4 4	1.30	72	305	72	
5 5	470	72	175	72	
6 6	690	72	345	72	
1 C 1 F	1.15	72	230	72	
2 2	1.05	72	255	72	
3 3	1.05	72	265	73	
4 4	510	72	140	72	
5 5	370	72	260	72	
6 6	755	72	265	73	

AVERAGE

CO ₂ (%)	Molecular Weight - Md
O ₂ (%)	Velocity - V _s (ft/min)
N ₂ (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - [(\% O_2) + (\% CO_2) + (\% CO)]$
- $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] - [0.23 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$
- $B_{wo} = V_{wu} / (V_m - V_{mc})$
- $V_m(Std) = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT[(T_s) / (P_s * M_s)]$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205 * 10^{-6} \text{ lb/mg} * (M_p / V_m(Std))$
- $ER_p = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_m(Std) / ((P_s) * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * theca * (1 - B_{wo} / 100)))$

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VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Walden</u>	DATE <u>11-14-85</u>	TEST NO. <u>5</u>
FMI Project # <u>T-5-501</u>	FMI Personnel <u>JKA/mgw</u>	
Plant Location <u>T-5-501</u>	Stack ID <u>Fan #4 (12" x 2')</u>	
Stack Diameter (ft) <u>4.5" x 2'</u>	Stack X-Area (ft ²) <u>2.25</u>	
Pitot ID # <u>6 effective</u>	Pitot Cp <u>0.84</u>	Pre-Pitot Leak Check <u>OK</u>
Bar Press (in Hg) <u>30.50</u>	Post-Pitot Leak Check <u>OK</u>	Amb. Temp. <u>67</u>
# of Traverse Points (n) <u>0 x 6</u>	Differential Static Press (in H ₂ O) <u>+0.005</u>	Stack Press
Differential Static Press (in Hg)	Start Time <u>1850</u>	Stop Time <u>1900</u>
Stack Press	Stack Port Drawing	

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE (°F)	SQRT DELTA P	COMMENTS
1 A 1	1.05	72	.81	
2 2	1.10	72	.83	
3 3	1.05	72	.81	
4 4	1.00	72	.78	
5 5	.890	72	.70	
6 6	.685	72	.52	
1 B 1	1.00	72	.78	
2 2	1.05	72	.81	
3 3	1.15	72	.87	
4 4	1.05	72	.81	
5 5	.795	72	.69	
6 6	.530	72	.42	
1 C 1	1.15	72	.87	
2 2	1.10	72	.83	
3 3	1.10	72	.83	
4 4	1.10	72	.83	
5 5	.825	72	.65	
6 6	.545	72	.42	
AVERAGE				

CO ₂ (%)	Molecular Weight - Md
O ₂ (%)	Velocity - V _s (ft/min)
N ₂ (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - (\% O_2) - (\% CO_2) - (\% CO)$
- $M_d = [0.44 * (\% CO_2)] - [0.32 * (\% O_2)] - [0.23 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) - 18 * B_{wo}$
- $B_{wo} = V_{wl} / (V_m - V_{mc})$
- $V_m(\text{std}) = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT(T_s / (P_s * M_s))$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205 * 10^{-6} \text{ lb/mg} * (M_p / V_m(\text{std}))$
- $ER_p = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_m(\text{std}) / ((P_s) * v_s * ((0.5 * D_m)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100)))$



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VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Larkspur</u>	DATE <u>11-14-95</u>	TEST NO. <u>3</u>
FMI Project # <u>595507</u>		
FMI Personnel <u>JKL/MOW</u>		
Plant Location <u>Jackson</u>		
Stack ID <u>Furn #5 (let #1)</u>		
Stack Diameter (ft) <u>45" (13.7)</u>		
Stack X-Area (ft ²) <u>200.94</u>		
Pitot ID # <u>6-010010</u>	Pitot Cp <u>0.34</u>	
Pre-Pitot Leak Check <u>ok</u>	Post-Pitot Leak Check <u>ok</u>	
Bar Press (in Hg) <u>30.30</u>	Amb. Temp. <u>64</u>	
# of Traverse Points (n) <u>6 x 6</u>		
Differential Static Press (in H ₂ O) <u>+0.205</u>		
Differential Static Press (in Hg)	Stack Press	Stack Port Drawing
Start Time <u>1935</u>	Stop Time <u>1845</u>	

TRAVERSE	Point #	DELTA P		STACK TEMPERATURE		SQRT DELTA P	COMMENTS
		(in H ₂ O)	(in Hg)	(°F)	(°R)		
1 A	1 D	865	71	565	71		
2	2	795	71	505	71		
3	3	760	71	520	71		
4	4	660	71	485	71		
5	5	510	71	485	72		
6	6	560	71	405	72		
1 B	1 E	710	71	305	71		
2	2	685	71	350	71		
3	3	550	71	365	71		
4	4	410	71	385	71		
5	5	540	71	400	72		
6	6	705	71	370	72		
1 C	1 F	665	71	445	72		
2	2	625	71	455	72		
3	3	605	71	475	72		
4	4	445	71	485	72		
5	5	395	71	480	72		
6	6	755	71	415	72		

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} + P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - (\%O_2) - (\%CO_2) - (\%CO)$
- $M_d = [0.44 * (\%CO_2)] - [0.32 * (\%O_2)] - [0.28 * ((\%N_2) + (\%CO))]$
- $M_s = M_d * (1 - B_{wo}) - 18 * B_{wo}$
- $B_{wo} = V_{wl} / (V_m + V_{mc})$
- $V_m(\text{std}) = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT \Delta P)) * SQRT[(P_s / T_s) * M_s]$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205 * 10^{-6} \text{ lb/mg} * (M_p / V_m(\text{std}))$
- $ER_p = Q_s * C_p$
- $\%ISO = 100 * (0.09457 * (T_s - 460) * V_m(\text{std}) / ((P_s) * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \text{thca} * (1 - B_{wo} / 100)))$



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VELOCITY TRAVERSE DATA SHEET

CLIENT <i>Wendy Heston</i>	DATE <i>11-14-95</i>	TEST NO. <i>4</i>
FMI Project # <i>1955025-1</i>		
FMI Personnel <i>JR/ALB</i>		
Plant Location <i>Tennessee</i>		
Stack ID <i>Fan #1 (Lad #3)</i>		
Stack Diameter (ft) <i>45" x 1.7</i>		
Stack X-Area (ft ²) <i>20.44</i>		
Pitot ID # <i>6 effective</i>	Pitot Cp <i>0.84</i>	
Pre-Pitot Leak Check <i>OK</i>	Post-Pitot Leak Check <i>OK</i>	
Bar Press (in Hg) <i>30.30</i>	Amb. Temp. <i>67</i>	
# of Traverse Points (n) <i>6 x 6</i>		
Differential Static Press (in H ₂ O) <i>TC 1.55</i>		
Differential Static Press (in Hg)	Stack Press	
Start Time <i>2205</i>	Stop Time <i>2215</i>	Stack Port Drawing

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE (°F)		SQRT DELTA P	COMMENTS
		(°F)	(°R)		
1 A 1 0	.125	74	.075	75	
2 A 2 0	.125	74	.080	73	
3 A 3 0	.107	74	.080	73	
4 A 4 0	.170	74	.060	70	
5 A 5 0	.125	74	.075	74	
6 A 6 0	.097	74	.070	70	
1 B 1 E	.105	73	.055	72	
2 B 2 E	.111	73	.055	72	
3 B 3 E	.075	73	.065	73	
4 B 4 E	.085	73	.050	72	
5 B 5 E	.075	73	.060	73	
6 B 6 E	.070	73	.055	73	
1 C 1 F	.106	73	.055	73	
2 C 2 F	.110	73	.045	73	
3 C 3 F	.110	74	.045	73	
4 C 4 F	.085	74	.055	73	
5 C 5 F	.085	74	.070	73	
6 C 6 F	.080	74	.070	73	

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - [(\% O_2) + (\% CO_2) + (\% CO)]$
- $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] + [0.28 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) - 18 * B_{wo}$
- $B_{wo} = V_{wi} / (V_m + V_{mc})$
- $V_{m(std)} = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 35.49 * (C_p) * (AVG(SQRT dP)) * SQRT[T_s / (P_s * M_s)]$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205 * 10^{-6} \text{ lb/mg} * (M_p / V_{m(std)})$
- $ER_p = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_{m(std)} / ((P_s * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * theca * (1 - B_{wo} / 100)))$



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VELOCITY TRAVERSE DATA SHEET

CLIENT Ludlow Manufacturing DATE 11-14-95 TEST NO. 4

FMI Project # 95-502

FMI Personnel JCS + MBSW

Plant Location T Jefferson

Stack ID Can # 2 (Can # 4)

Stack Diameter (ft) 47" x 12"

Stack X-Area (ft²) 26.75

Pitot ID = 6" effective Pitot Cp 0.84

Pre-Pitot Leak Check OK Post-Pitot Leak Check OK

Bar Press (in Hg) 30.30 Amb. Temp. 64

of Traverse Points (n) 6 x 6

Differential Static Press (in H₂O) +0.23

Differential Static Press (in Hg)

Stack Press 2.15

Start Time 2105 Stop Time

Stack Port Drawing

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE (°F)	SQRT DELTA P	COMMENTS
1 A	0.005	72	0.150	Bags on @ 2105
2	0.010	72	0.160	
3	0.010	72	0.165	
4	0.005	72	0.180	
5	0.000	72	0.155	
6	0.015	72	0.125	
1 B	0.005	71	0.160	Bags off @ 2205
2	0.005	71	0.180	
3	0.010	72	0.200	
4	0.015	72	0.145	
5	0.020	72	0.130	
6	0.005	72	0.115	
1 C	0.020	70	0.165	
2	0.025	71	0.185	
3	0.025	71	0.200	
4	0.050	72	0.195	
5	0.060	72	0.180	
6	0.050	73	0.175	

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - ((\% O_2) - (\% CO_2) - (\% CO))$
- $M_d = [0.44 * (\% CO_2)] - [0.32 * (\% O_2)] - [0.23 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) - 18 * B_{wo}$
- $B_{wo} = V_{wU} / (V_m + V_{mc})$
- $V_{m(std)} = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT[T_s / (P_s * M_s)]$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205 * 10^{-6} \text{ lb/mg} * (M_p / V_{m(std)})$
- $ER_p = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_{m(std)} / ((P_s) * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \text{theta} * (1 - B_{wo} / 100)))$



Air Sciences & Engineering Group

VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Adair Machinery</u>	DATE <u>1-14-95</u>	TEST NO. <u>4</u>
FMI Project # <u>195-502</u>		
FMI Personnel <u>JKT/mplw</u>		
Plant Location <u>Jefferson</u>		
Stack ID <u>tan & 3 (tan & 3)</u>		
Stack Diameter (ft) <u>45" x 61"</u>		
Stack X-Area (ft ²) <u>24.90</u>		
Pitot ID # <u>6 electronic</u>	Pitot Cp <u>0.84</u>	
Pre-Pitot Leak Check <u>ok</u>	Post-Pitot Leak Check <u>ok</u>	
Bar Press (in Hg) <u>30.50</u>	Amb. Temp. <u>67</u>	
# of Traverse Points (n) <u>6x6</u>		
Differential Static Press (in H ₂ O) <u>10.125</u>		
Differential Static Press (in Hg)	Stack Press	
Start Time <u>2150</u>	Stop Time <u>2200</u>	Stack Port Drawing

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE (°F)	SQRT DELTA P	COMMENTS
1A	165	72	110	72
2	175	72	115	72
3	165	73	115	73
4	145	73	100	73
5	120	73	105	73
6	115	73	090	73
1B	160	71	105	69
2	162	72	107	70
3	170	73	108	71
4	105	73	090	72
5	095	73	095	73
6	110	73	095	73
1C	105	72	085	73
2	155	72	100	73
3	150	73	100	73
4	115	73	090	73
5	080	73	085	73
6	105	73	095	73

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - [(\% O_2) + (\% CO_2) + (\% CO)]$
- $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] + [0.28 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$
- $B_{wo} = V_{wi} / (V_{wi} - V_{mci})$
- $V_{m(Std)} = 17.467 * [(V_{mi} * P_{mi}) / T_{mi}]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT(T_s / (P_s * M_s))$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205 * 10^{-6} \text{ lb/mg} * (M_p / V_{m(Std)})$
- $ERP = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_{m(Std)}) / ((P_s)^{-1} * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100))$



Air Sciences & Engineering Group

VELOCITY TRAVERSE DATA SHEET

CLIENT Ladakh Malt DATE 11-14-95 TEST NO. 4

FMI Project # 195.507

FMI Personnel JK + MCB

Plant Location Jefferson

Stack ID Can #4 (Lat # 2)

Stack Diameter (ft) 45" x 21"

Stack X-Area (ft²) 210.74

Pitot ID # 6 efflow Pitot Cp 0.84

Pre-Pitot Leak Check ok Post-Pitot Leak Check ok

Bar Press (in Hg) 30.50 Amb. Temp. 64

of Traverse Points (n) 6 x 6

Differential Static Press (in H₂O) 70.55

Differential Static Press (in Hg) _____ Stack Press _____

Start Time 2120 Stop Time 2130 Stack Port Drawing _____

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
		(°F)	(°R)		
1 F	.005	66	146	74	
2	.005	67	155	75	
3	.005	69	165	75	
4	.005	70	185	75	
5	.005	71	150	76	
6	.005	73	170	76	
1 B	.055	75	130	74	
2	.070	75	140	75	
3	.085	75	155	75	
4	.090	76	155	76	
5	.090	76	135	76	
6	.060	76	105	76	
1 D	.105	74	170	75	
2	.120	75	185	75	
3	.130	75	180	75	
4	.145	76	160	75	
5	.125	76	135	75	
6	.065	76	125	75	

AVERAGE

CO ₂ (%)	Molecular Weight - Md
O ₂ (%)	Velocity - V _s (ft/min)
N ₂ (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} + P_{static} (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - [(\% O_2) - (\% CO_2) - (\% CO)]$
- $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] - [0.23 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) - 18 * B_{wo}$
- $B_{wo} = V_{wu} / (V_m - V_{mc})$
- $V_m(Std) = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT[T_s / (P_s * M_s)]$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205^{-6} \text{ lb/mg} * (M_p / V_m(Std))$
- $ER_p = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_m(Std) / ((P_s)^3 * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \text{thera} * (1 - B_{wo} / 100)))$


Fluid Management, Inc.
 Air Sciences & Engineering Group
 VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Radco Maching</u>	DATE <u>11-14-85</u>	TEST NO. <u>11</u>
FMI Project # <u>395-502</u>		
FMI Personnel <u>TICA / MIB</u>		
Plant Location <u>Jefferson</u>		
Stack ID <u>Flue 5 (Lair E 1)</u>		
Stack Diameter (ft) <u>45" x 67"</u>		
Stack X-Area (ft ²) <u>20.90</u>		
Pitot ID # <u>6 effective</u>	Pitot Cp <u>0.84</u>	
Pre-Pitot Leak Check <u>ok</u>	Post-Pitot Leak Check <u>ok</u>	
Bar Press (in Hg) <u>30.50</u>	Amb. Temp. <u>64</u>	
# of Traverse Points (n) <u>6 x 6</u>		
Differential Static Press (in H ₂ O) <u>TC.160</u>		
Differential Static Press (in Hg)	Stack Press	
Start Time <u>2155</u>	Stop Time <u>2145</u>	Stack Port Drawing

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
		(°F)	(°R)		
1 C	.030	73	580	175	
2 C	.040	73	580	173	
3 C	.035	74	585	175	
4 C	.035	73	580	175	
5 C	.040	75	580	175	
6 C	.035	75	585	175	
1 B	.050	75	585	172	
2 B	.055	75	590	173	
3 B	.050	75	590	174	
4 B	.045	75	585	174	
5 B	.050	75	580	175	
6 B	.050	75	575	175	
1 A	.060	74	570	174	
2 A	.060	74	570	175	
3 A	.065	75	570	175	
4 A	.060	75	570	175	
5 A	.070	75	565	175	
6 A	.085	75	570	175	

AVERAGE

CO ₂ (%)	Molecular Weight - Md
O ₂ (%)	Velocity - V _s (ft/min)
N ₂ (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - (\% O_2) - (\% CO_2) - (\% CO)$
- $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] + [0.23 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) - 18 * B_{wo}$
- $B_{wo} = V_{wu} / (V_m - V_{mc})$
- $V_m(\text{std}) = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT(T_s / (P_s * M_s))$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205 * 10^{-6} \text{ lb/mg} * (M_p / V_m(\text{std}))$
- $ER_p = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_m(\text{std}) / ((P_s * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100)))$


Fluid Management, Inc.
 Air Sciences & Engineering Group
 VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Ladish Welding</u>	DATE <u>11-14-85</u>	TEST NO. <u>5</u>
FMI Project # <u>JES-502</u>		
FMI Personnel <u>JR+MBW</u>		
Plant Location <u>Jefferson</u>		
Stack ID <u>Can #1 (last)</u>		
Stack Diameter (ft) <u>45" x 61"</u>		
Stack X-Area (ft ²) <u>20.90</u>		
Pitot ID # <u>6 effective</u>	Pitot Cp <u>0.54</u>	
Pre-Pitot Leak Check <u>OK</u>	Post-Pitot Leak Check <u>OK</u>	
Bar Press (in Hg) <u>20.30</u>	Amb. Temp. <u>64</u>	
# of Traverse Points (n) <u>6 x 6</u>		
Differential Static Press (in H ₂ O) <u>-0.15</u>		
Differential Static Press (in Hg)	Stack Press <u>2315</u>	
Start Time <u>2305</u>	Stop Time <u>2315</u>	Stack Port Drawing

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
		(°F)	(°R)		
1 F	0.161	74	135	63	Bags on @ 11:05
2 F	0.165	74	135	73	
3 F	.170	74	140	71	
4 F	.055	74	115	70	
5 F	.052	74	122	74	
6 F	.055	74	115	74	
1 B	.075	73	135	73	
2 B	.081	73	130	71	
3 B	.085	73	140	70	
4 B	.075	73	115	70	
5 B	.075	70	115	70	
6 B	.055	70	105	70	
1 A	.110	73	135	73	
2 A	.115	73	140	71	
3 A	.170	73	135	70	
4 A	.080	73	130	70	
5 A	.165	74	125	70	
6 A	.175	70	110	70	

AVERAGE

CO ₂ (%)	Molecular Weight - Md
O ₂ (%)	Velocity - V _s (ft/min)
N ₂ (%)	Flow Rate - Q (scfm)

EQUATIONS:

$P_s = P_{bar} - P_{static} (13.6 \text{ in. H}_2\text{O/in. Hg})$
 $\%N_2 = 100 - (\%O_2) - (\%CO_2) - (\%CO)$
 $M_d = [0.44 * (\%CO_2)] - [0.32 * (\%O_2)] - [0.28 * ((\%N_2) + (\%CO))]$
 $M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$
 $B_{wo} = V_{wi} / (V_m + V_{mc})$
 $V_{m(std)} = 17.467 * [(V_m * P_m / T_m)]$
 $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT(T_s / (P_s * M_s))$
 $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
 $C_p = 2.205^{-6} \text{ lb/mg} * (M_p / V_{m(std)})$
 $ER_p = Q_s * C_p$
 $\%ISO = 100 * (0.09457 * (T_s - 460) * V_{m(std)} / ((P_s * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100)))$



Air Sciences & Engineering Group

VELOCITY TRAVERSE DATA SHEET

CLIENT Ladish Industries DATE 11-14-95 TEST NO. 5

FMI Project # 95-302

FMI Personnel RA/MFW

Plant Location Johnson #1

Stack ID Fun #1 (man #1)

Stack Diameter (ft) 45.26

Stack X-Area (ft²) 20.40

Pitot ID # 60012104 Pitot Cp 0.84

Pre-Pitot Leak Check OK Post-Pitot Leak Check OK

Bar Press (in Hg) 30.30 Amb. Temp. 64

of Traverse Points (n) 6 x 6

Differential Static Press (in H₂O) +0.185

Differential Static Press (in Hg) _____ Stack Press 0005

Start Time 2:55 Stop Time _____ Stack / Port Drawing _____

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
		(°F)	(°R)		
1 E 1 C	.250	75	0.085	73	
2 2	.215	75	.070	73	
3 3	.255	75	.025	74	
4 4	.780	75	.050	74	
5 5	.465	75	.060	74	
6 6	.750	75	.025	74	
1 E 2 B	.245	74	.060	73	
2 2	.270	75	.085	73	
3 3	.255	75	.010	73	
4 4	.255	75	.020	74	
5 5	.185	75	.015	74	
6 6	.160	75	.010	74	
1 D 1 A	.185	74	.005	72	
2 2	.225	75	.005	72	
3 3	.280	74	.010	73	
4 4	.750	75	.010	73	
5 5	.725	75	.005	74	
6 6	.180	75	.005	74	

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - (\%O_2) - (\%CO_2) - (\%CO)$
- $M_d = [0.44 * (\%CO_2)] + [0.32 * (\%O_2)] + [0.28 * ((\%N_2) + (\%CO))]$
- $M_s = M_d * (1 - B_{wo}) + 18 * B_{wo}$
- $B_{wo} = V_{wv} / (V_m - V_{mc})$
- $V_{m(std)} = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT[(T_s / (P_s * M_s))]$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.295 * 10^{-6} \text{ lb/mg} * (M_p / V_{m(std)})$
- $ER_p = Q_s * C_p$
- $\%ISO = 100 * (0.09457 * (T_s - 460) * V_{m(std)} / ((P_s * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \theta_{ex} * (1 - B_{wo} / 100)))$

VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Calgon Industries</u>	DATE <u>11-14-95</u>	TEST NO. <u>5</u>
FMI Project # <u>195502</u>		
FMI Personnel <u>JR + MRS</u>		
Plant Location <u>Jefferson</u>		
Stack ID <u>Fan 3 (Lan 2)</u>		
Stack Diameter (ft) <u>45" x 6"</u>		
Stack X-Area (ft ²) <u>20.70</u>		
Pitot ID # <u>6227</u>	Pitot Cp <u>0.84</u>	
Pre-Pitot Leak Check <u>OK</u>	Post-Pitot Leak Check <u>OK</u>	
Bar Press (in Hg) <u>30.30</u>	Amb. Temp. <u>64</u>	
# of Traverse Points (n) <u>6 x 6</u>		
Differential Static Press (in H ₂ O) <u>+0.165</u>		
Differential Static Press (in Hg)	Stack Press	
Start Time <u>2320</u>	Stop Time <u>2330</u>	Stack Port Drawing

TRAVERSE Point.#	DELTA P (in H ₂ O)	STACK TEMPERATURE (°F)	SQRT DELTA P	COMMENTS
1 E	.065	73	1.5	
2	.085	72	2.05	
3	.085	72	2.05	
4	.060	73	1.5	
5	.105	73	2.15	
6	.035	73	1.60	
1 E	.070	70	2.10	
2	.095	72	2.20	
3	.105	72	2.15	
4	.105	73	2.15	
5	.050	74	1.25	
6	.080	74	1.15	
1 D	.165	74	2.35	
2	.170	74	2.40	
3	.140	74	2.25	
4	.095	74	1.05	
5	.060	74	1.95	
6	.115	74	1.50	

AVERAGE

CO2 (%)	Molecular Weight - Md
O2 (%)	Velocity - Vs (ft/min)
N2 (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - ((\% O_2) - (\% CO_2) - (\% CO))$
- $M_d = [0.44 * (\% CO_2)] - [0.32 * (\% O_2)] - [0.23 * ((\% N_2) + (\% CO))]$
- $M_s = M_d * (1 - B_{wo}) - 18 * B_{wo}$
- $B_{wo} = V_{wv} / (V_m + V_{mc})$
- $V_m(\text{std}) = 17.467 * [(V_m * P_{atm} / T_m)]$
- $V_s = 85.49 * (C_p) * (AVG(\text{SQRT } dP)) * \text{SQRT}[T_s / (P_s * M_s)]$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205^{-6} \text{ lb/mg} * (M_p / V_m(\text{std}))$
- $ERP = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_m(\text{std}) / ((P_s) * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \text{theta} * (1 - B_{wo} / 100)))$

Fluid Management, Inc.

Air Sciences & Engineering Group

VELOCITY TRAVERSE DATA SHEET

CLIENT <u>Ladish Machine</u>	DATE <u>11-4-95</u>	TEST NO. <u>5</u>
FMI Project # <u>193-501</u>		
FMI Personnel <u>JCA/UM/SL</u>		
Plant Location <u>Jackson MS</u>		
Stack ID <u>Unit 4/12/16</u>		
Stack Diameter (ft) <u>45.86</u>		
Stack X-Area (ft ²) <u>179.90</u>		
Pitot ID # <u>6-0-0-0-0-0</u>	Pitot Cp <u>0.84</u>	
Pre-Pitot Leak Check <u>OK</u>	Post-Pitot Leak Check <u>OK</u>	
Bar Press (in Hg) <u>30.50</u>	Amb. Temp. <u>69</u>	
# of Traverse Points (n) <u>18</u>		
Differential Static Press (in H ₂ O) <u>+0.185</u>	Stack Press <u>23.55</u>	
Differential Static Press (in Hg) <u>-0.185</u>	Stop Time <u>2355</u>	
Start Time <u>2345</u>		Stack Port Drawing

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE		SQRT DELTA P	COMMENTS
		(°S)	(°R)		
1 A 1 D	.775	76	1105	15	
2 2	.730	76	1165	18	
3 3	.700	76	1145	17	
4 4	.735	76	1200	17	
5 5	.745	76	1160	17	
6 6	.780	76	1185	17	
1 B 1 E	.710	75	1175	17	
2 2	.722	76	1195	17	
3 3	.730	76	115	15	
4 4	.740	76	125	16	
5 5	.750	76	120	16	
6 6	.75	76	120	16	
1 C 1 F	.715	75	1185	17	
2 2	.735	76	1110	17	
3 3	.740	76	1005	17	
4 4	.760	76	1005	13	
5 5	.765	76	1005	13	
6 6	.765	76	1010	14	

AVERAGE

CO ₂ (%)	Molecular Weight - Md
O ₂ (%)	Velocity - Vs (ft/min)
N ₂ (%)	Flow Rate - Q (scfm)

EQUATIONS:

- $P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
- $\%N_2 = 100 - [(\% O_2) + (\% CO_2) + (\% CO)]$
- $M_d = (0.44 * (\% CO_2)) + (0.32 * (\% O_2)) + (0.28 * ((\% N_2) + (\% CO)))$
- $M_s = M_d * (1 - B_{wo}) - 18 * B_{wo}$
- $B_{wo} = V_{wl} / (V_m - V_{mc})$
- $V_m(\text{std}) = 17.467 * [(V_m * P_m) / T_m]$
- $V_s = 85.49 * (C_p) * (AVG(\text{SQRT } \Delta P)) * \text{SQRT}[T_s / (P_s * M_s)]$
- $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
- $C_p = 2.205 * 6 \text{ lb/mg} * (M_p / V_m(\text{std}))$
- $ER_p = Q_s * C_p$
- $\% ISO = 100 * (0.09457 * (T_s - 460) * V_m(\text{std}) / ((P_s) * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \text{thick} * (1 - B_{wo} / 100)))$



Fluid Management, Inc.

Air Sciences & Engineering Group

VELOCITY TRAVERSE DATA SHEET

CLIENT <i>Ladco Industries</i>	DATE <i>11-14-95</i>	TEST NO. <i>5</i>
FMI Project # <i>75-502</i>		
FMI Personnel <i>1127 MURKIN</i>		
Plant Location <i>Jefferson</i>		
Stack ID <i>Low 5 1127</i>		
Stack Diameter (ft) <i>45" x 61"</i>		
Stack X-Area (ft ²) <i>2094</i>		
Pitot ID # <i>6 effective</i>	Pitot Cp <i>0.84</i>	
Pre-Pitot Leak Check <i>OK</i>	Post-Pitot Leak Check <i>OK</i>	
Bar Press (in Hg) <i>30.30</i>	Amb. Temp. <i>64</i>	
# of Traverse Points (n) <i>6, 6, 6</i>		
Differential Static Press (in H ₂ O) <i>+0.170</i>		
Differential Static Press (in Hg)	Stack Press <i>2345</i>	Stack Port Drawing
Start Time <i>2335</i>	Stop Time	

TRAVERSE Point #	DELTA P (in H ₂ O)	STACK TEMPERATURE (°F)	SQRT DELTA P	COMMENTS
1 F 1 C	.065	74	.115	16
2 2	.050	75	.110	17
3 3	.050	75	.115	17
4 4	.065	76	.105	17
5 5	.050	76	.110	17
6 6	.040	76	.170	17
1 E 1 B	.065	75	.155	16
2 2	.070	75	.145	16
3 3	.060	76	.135	16
4 4	.060	76	.110	16
5 5	.060	76	.100	17
6 6	.085	76	.110	17
1 D 1 A	.085	75	.175	17
2 2	.085	75	.170	17
3 3	.080	76	.165	17
4 4	.080	76	.145	17
5 5	.085	77	.125	17
6 6	.170	77	.115	17

AVERAGE

CO ₂ (%)	Molecular Weight - Md
O ₂ (%)	Velocity - Vs (ft/min)
N ₂ (%)	Flow Rate - Q (scfm)

EQUATIONS:

$P_s = P_{bar} - P_{static} / (13.6 \text{ in. H}_2\text{O/in. Hg})$
 $\%N_2 = 100 - [(\% O_2) + (\% CO_2) + (\% CO)]$
 $M_d = [0.44 * (\% CO_2)] + [0.32 * (\% O_2)] + [0.29 * ((\% N_2) + (\% CO))]$
 $M_s = M_d * (1 - B_{wo}) - 18 * B_{wo}$
 $B_{wo} = V_{wt} / (V_m - V_{mc})$
 $V_{m(std)} = 17.467 * [(V_m * P_m) / T_m]$
 $V_s = 85.49 * (C_p) * (AVG(SQRT dP)) * SQRT[T_s / (P_s * M_s)]$
 $Q_s = 63.529 * V_s * A_s * (1 - B_{wo}) * (P_s / T_s)$
 $C_p = 2.205 * 10^{-6} \text{ lb/mg} * (M_p / V_{m(std)})$
 $ER_p = Q_s * C_p$
 $\% ISO = 100 * (0.09457 * (T_s - 460) * V_{m(std)} / ((P_s * v_s * ((0.5 * D_n)^2 * 3.141716 / 144) * \theta * (1 - B_{wo} / 100)))$



Date: _____
Client: Jefferson
Site Location: Farm (Cads)
Port Location: Rumb
Port Direction: _____
Project No.: _____
Test Crew: _____
Run No.: _____
Control Box No.: _____
Delta H(@): _____
Meter Correction (Yr): _____

Start Time: 0205
Stop Time: 0216
Sample Box No.: 11-159
Probe No.: _____
Filter No.: _____
Filter Type: _____
Stack Diameter: 4.5 x 6.74
Unobstructed Length: _____
Stack Area: ft²: 20.74
Nozzle Dia: _____
Pitot Correction: 0.84

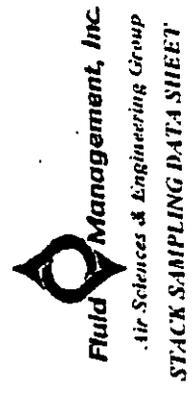
Barometric Press: 30.30 Assumed Moisture:
Static Press, Ps: +0.175 Calculator Multiplier:
Ambient Temp: _____ or "K" Factor: _____

Point	Time	Meter Reading (dry) (ft)	Velocity Head Delta P (in. H2O)	Square Root Delta P	Orifice (in. H2O) Required	Delta H (in. H2O) Actual	Meter Vacuum (in. Hg)	Stack Temp. (°F)	Probe Temp. (°F)	Oven Temp. (°F)		Imp. Temp. (°F)		Meter Temp. (°F)		Comments	
										To	From	To	From	To	From		To
F-E	1-2	0.40	74	0.35	73	73											
F-E	1-3	0.65	74	0.46	74	74											
F-E	1-4	0.70	74	0.55	74	74											
F-E	1-5	0.55	74	0.48	74	74											
F-E	1-6	0.35	74	0.35	73	73											
F-E	1-7	0.75	74	0.55	74	74											
F-E	1-8	0.85	74	0.60	74	74											
F-E	1-9	0.95	74	0.65	74	74											
F-E	1-10	0.75	74	0.55	74	74											
F-E	1-11	0.55	74	0.45	74	74											
F-E	1-12	0.10	74	0.25	74	74											
F-E	1-13	0.95	74	0.75	74	74											
F-E	1-14	1.20	74	0.95	74	74											
F-E	1-15	0.50	74	0.40	74	74											
F-E	1-16	1.05	74	0.80	74	74											
F-E	1-17	1.25	74	1.10	74	74											

Gas Analysis				Moisture Analysis			
Impinger No.	Grams Final	Grams Initial	Difference	Impinger No.	Grams Final	Grams Initial	Difference
1				1			
2				2			
3				3			
4				4			
Average:				Total:			

Sample Train Leak Check		Pitot Leak Check	
Before	After	Red X	Black X

Sample Train Leak Check	
in Hg	Rate



Start Time: 0110
 Stop Time: 0120
 Sample Box No.: 1175-95
 Probe No.:
 Filter No.:
 Filter Type:
 Stack Diameter: 45" x 67"
 Unobstructed Length:
 Stack Area: ft²: 20.71
 Nozzle Dia:
 Pilot Correction: 0.81

Assumed Moisture:
 Calculator Multiplier:
 or "K" Factor:

Date:
 Client:
 Site Location: Fan 2 Cell #4
 Port Location: Rumb
 Port Direction:
 Project No.:
 Test Crew:
 Run No.:
 Control Box No.:
 Delta H₂O:
 Meter Correction (Vd):

Barometric Press: 30.30
 Static Press, Ps: 10.320
 Ambient Temp: 69

Point	Time	Meter Reading (dry) Δ HP	Velocity Head Delta P (in. H ₂ O)	Square Root Delta P	Orifice (in. H ₂ O) Δ HP	Delta H (in. H ₂ O) Actual	Meter Vacuum (in. Hg)	Stack Temp. T _s (°F)	Probe Temp. T _p (°F)	Oven Temp. To (°F)	Imp. Temp.		Meter Temp.		Comments
											To (°F)	Out (°F)	To (°F)	Out (°F)	
1	C	1.005	77.8	3.85	77.8	77.8									Bag
2	C	1.005	77.8	3.85	77.8	77.8									Bag
3	C	1.005	77.8	3.85	77.8	77.8									0100
4	C	1.005	77.8	3.85	77.8	77.8									Bag
5	C	1.005	77.8	3.85	77.8	77.8									Bag
6	C	1.005	77.8	3.85	77.8	77.8									0100
7	C	1.005	77.8	3.85	77.8	77.8									Bag
8	C	1.005	77.8	3.85	77.8	77.8									Bag
9	C	1.005	77.8	3.85	77.8	77.8									0100
10	C	1.005	77.8	3.85	77.8	77.8									Bag
11	C	1.005	77.8	3.85	77.8	77.8									Bag
12	C	1.005	77.8	3.85	77.8	77.8									0100

Sample Train Leak Check			Pilot Leak Check			Gas Analysis			Moisture Analysis			Difference	
Before	After	in Hg	Rate	Red X	Black X	1	2	3	Average	Impinger No.	Grams Final	Grams Initial	Total
				X	X					1			
				X	X					2			
										3			
										4			



STACK SAMPLING DATA SHEET

Start Time: 0748
 Stop Time: 0155
 Sample Box No.: 1112
 Probe No.:
 Filter No.:
 Filter Type:
 Stack Diameter: 45" x 67"
 Umbilical Length:
 Stack Area: ft²: 20.94
 Nozzle Dia:
 Pilot Correction: 0.88

Assumed Moisture:
 Calculator Multiplier,
 or "K" Factor:

Barometric Press: 30.30
 Static Press, Ps: 70.095
 Ambient Temp: 69

Meter Correction (Vol):

Date:
 Client:
 Site Location:
 Port Location:
 Port Direction: Fan 3 (ad 3)
 Project No.:
 Test Crew: Rumb
 Run No.:
 Control Box No.:
 Delta H@:
 Meter Correction (Vol):

Point	Time	Meter Reading (dry)	Velocity Head Delta P (in. H ₂ O)	Square Root Delta P	Orifice (in. H ₂ O) Required	Delta H (in. H ₂ O) Actual	Meter Vacuum (in. Hg)	Stack Temp. T _s (°F)	Probe Temp. T _p (°F)	Oven Temp. T _o (°F)	Imp. Temp.		Comments
											To (°F)	Out (°F)	
A	1:30	9.85	73	8.05	71	71							
B	1:35	9.10	73	7.60	71	71							
C	1:40	8.35	73	6.75	71	71							
D	1:45	7.60	73	5.50	71	71							
E	1:50	6.85	72	4.15	71	71							
F	1:55	6.10	72	3.80	71	71							
G	2:00	5.35	72	2.95	71	71							
H	2:05	4.60	73	2.10	71	71							
I	2:10	3.85	73	1.50	70	70							
J	2:15	3.10	72	1.25	70	70							
K	2:20	2.35	72	0.85	70	70							
L	2:25	1.60	72	0.35	70	70							

Gas Analysis				Moisture Analysis			
Impinger No.	Gas	Final	Initial	Impinger No.	Gas	Final	Initial
1	O ₂			1			
2	CO ₂			2			
3	CO			3			
4	N ₂			4			
Average				Total			

Sample Train Leak Check		Pilot Leak Check	
Before	After	Red X	Black X

Rate



Start Time: 0125
 Stop Time: 0135
 Sample Ilos No.: 11-1575
 Probe No.:
 Filter No.:
 Filter Type:
 Stack Diameter: 45" x 67"
 Unfitted Length: 20 ft
 Stack Area: ft²:
 Nozzle Dia:
 Pitot Correction: 0.84

Assumed Moisture:
 Calculator Multiplier:
 or "K" Factor:

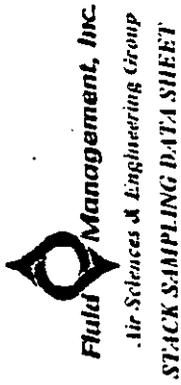
Date:
 Client:
 Site Location: Fan 4 (ad 2)
 Port Location: Rumb
 Port Direction:
 Project No.:
 Test Crew:
 Run No.:
 Control Box No.:
 Delta II@:
 Meter Correction (Yul):

Barometric Press: 30.30
 Static Press, P_s: 10.145
 Ambient Temp: 64

Point	Time	Meter Reading (dry)	Velocity Head Delta P (in. H ₂ O)	Square Root Delta P	Orifice (in. H ₂ O) Required	Delta II (in. H ₂ O) Actual	Meter Vacuum (in. Hg)	Stack Temp. T _s (°F)	Probe Temp. T _p (°F)	Oven Temp. T _o (°F)	Imp. Temp.		Meter Temp.		Comments
											To (°F)	From (°F)	To (°F)	From (°F)	
F	0	0.00	77	0.90	78	78									
C		0.005	77	0.915	78	78									
E		0.005	77	0.915	78	78									
B		0.005	77	0.915	78	78									
A		0.010	77	0.93	78	78									
		0.015	77	0.945	78	78									
		0.020	77	0.96	78	78									
		0.025	77	0.975	78	78									
		0.030	77	0.99	78	78									
		0.035	77	1.005	78	78									
		0.040	77	1.02	78	78									
		0.045	77	1.035	78	78									
		0.050	77	1.05	78	78									
		0.055	77	1.065	78	78									
		0.060	77	1.08	78	78									
		0.065	77	1.095	78	78									
		0.070	77	1.11	78	78									
		0.075	77	1.125	78	78									
		0.080	77	1.14	78	78									
		0.085	77	1.155	78	78									
		0.090	77	1.17	78	78									
		0.095	77	1.185	78	78									
		0.100	77	1.20	78	78									
		0.105	77	1.215	78	78									
		0.110	77	1.23	78	78									
		0.115	77	1.245	78	78									
		0.120	77	1.26	78	78									
		0.125	77	1.275	78	78									
		0.130	77	1.29	78	78									
		0.135	77	1.305	78	78									
		0.140	77	1.32	78	78									
		0.145	77	1.335	78	78									
		0.150	77	1.35	78	78									
		0.155	77	1.365	78	78									
		0.160	77	1.38	78	78									
		0.165	77	1.395	78	78									
		0.170	77	1.41	78	78									
		0.175	77	1.425	78	78									
		0.180	77	1.44	78	78									
		0.185	77	1.455	78	78									
		0.190	77	1.47	78	78									
		0.195	77	1.485	78	78									
		0.200	77	1.50	78	78									
		0.205	77	1.515	78	78									
		0.210	77	1.53	78	78									
		0.215	77	1.545	78	78									
		0.220	77	1.56	78	78									
		0.225	77	1.575	78	78									
		0.230	77	1.59	78	78									
		0.235	77	1.605	78	78									
		0.240	77	1.62	78	78									
		0.245	77	1.635	78	78									
		0.250	77	1.65	78	78									
		0.255	77	1.665	78	78									
		0.260	77	1.68	78	78									
		0.265	77	1.695	78	78									
		0.270	77	1.71	78	78									
		0.275	77	1.725	78	78									
		0.280	77	1.74	78	78									
		0.285	77	1.755	78	78									
		0.290	77	1.77	78	78									
		0.295	77	1.785	78	78									
		0.300	77	1.80	78	78									
		0.305	77	1.815	78	78									
		0.310	77	1.83	78	78									
		0.315	77	1.845	78	78									
		0.320	77	1.86	78	78									
		0.325	77	1.875	78	78									
		0.330	77	1.89	78	78									
		0.335	77	1.905	78	78									
		0.340	77	1.92	78	78									
		0.345	77	1.935	78	78									
		0.350	77	1.95	78	78									
		0.355	77	1.965	78	78									
		0.360	77	1.98	78	78									
		0.365	77	1.995	78	78									
		0.370	77	2.01	78	78									
		0.375	77	2.025	78	78									
		0.380	77	2.04	78	78									
		0.385	77	2.055	78	78									
		0.390	77	2.07	78	78									
		0.395	77	2.085	78	78									
		0.400	77	2.10	78	78									
		0.405	77	2.115	78	78									
		0.410	77	2.13	78	78									
		0.415	77	2.145	78	78									
		0.420	77	2.16	78	78									
		0.425	77	2.175	78	78									
		0.430	77	2.19	78	78									
		0.435	77	2.205	78	78									
		0.440	77	2.22	78	78									
		0.445	77	2.235	78	78									
		0.450	77	2.25	78	78									
		0.455	77	2.265	78	78									
		0.460	77	2.28	78	78									
		0.465	77	2.295	78	78									
		0.470	77	2.31	78	78									
		0.475	77	2.325	78	78									
		0.480	77	2.34	78	78									
		0.485	77	2.355	78	78									
		0.490	77	2.37	78	78									
		0.495	77	2.385	78	78									
		0.500	77	2.40	78	78									

Gas Analysis		Moisture Analysis			
Impinger No.	Grams Final	Grams Initial	Grams Initial	Grams Initial	Difference
1					
2					
3					
4					
Average					

Sample Train Leak Check		Pilot Leak Check	
Before	In Hg	Red X	Black X
	</		



Fluid Management, Inc.
Air Sciences & Engineering Group
STACK SAMPLING DATA SHEET

Date: 01/35
Client: 0175
Site Location: 11-15
Port Location:
Port Direction:
Project No.: Fau 5 (cell 1)
Test Crew: Rumb
Run No.:
Control Box No.:
Delta H₂O:
Meter Correction (Vol):

Barometric Press: 30.30 Assumed Moisture:
Static Press, Ps: 70.70 Calculator Multiplier:
Ambient Temp: or "K" Factor:

Start Time: 01:35
Stop Time:
Sample Box No.:
Probe No.:
Filter No.:
Filter Type:
Stack Diameter: 45" x 67"
Unobstructed Length:
Stack Area, ft²: 20.94
Nozzle Dia:
Pilot Correction: 0.84

Point	Time	Meter Reading (dry)	Velocity Head Delta P (in. H ₂ O)	Square Root Delta P	Orifice (in. H ₂ O) Required	Delta H (in. H ₂ O) Actual	Meter Vacuum (in. Hg)	Stack Temp. T _s (°F)	Probe Temp. T _p (°F)	Oven Temp. To (°F)	Imp. Temp. (°F)		Meter Temp. (°F)		Comments	
											To	Out	In	Out		In
A	0	0.00	0.00	0.00	73	73										
B	1	0.05	0.05	0.05	73	73										
C	2	0.05	0.05	0.05	73	73										
D	3	0.05	0.05	0.05	73	73										
E	4	0.05	0.05	0.05	73	73										
F	5	0.05	0.05	0.05	73	73										
G	6	0.05	0.05	0.05	73	73										
H	7	0.05	0.05	0.05	73	73										
I	8	0.05	0.05	0.05	73	73										
J	9	0.05	0.05	0.05	73	73										
K	10	0.05	0.05	0.05	73	73										

Gas Analysis				Moisture Analysis			
Impinger No.	Grams Final	Grams Initial	Difference	Impinger No.	Grams Final	Grams Initial	Difference
1				1			
2				2			
3				3			
4				4			
Average:				Total:			

Sample Train Leak Check		Pilot Leak Check	
Before	After	Red X	Black X

Rate	Rate

APPENDIX C

Sample Chromatograms

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 00:16:19

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F4R12.CHR (c:\peakwin)

Sample: Fan #4 Run #1

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

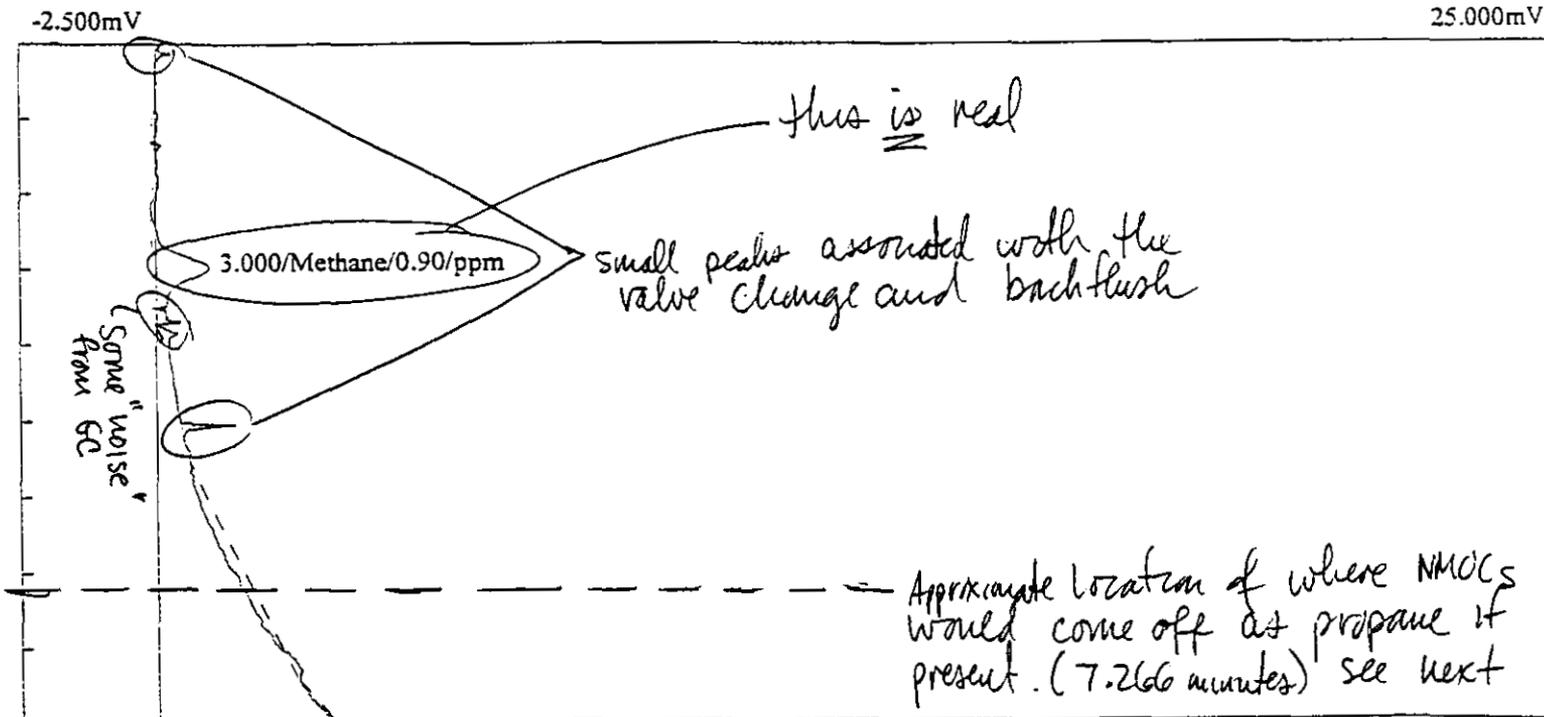
DRAFT

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
Methane	3.000	28.826	0.90	ppm
		29	1	

page

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 17:57:20

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: C3H83.CHR (c:\peakwin)

Sample: C3H8 std

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

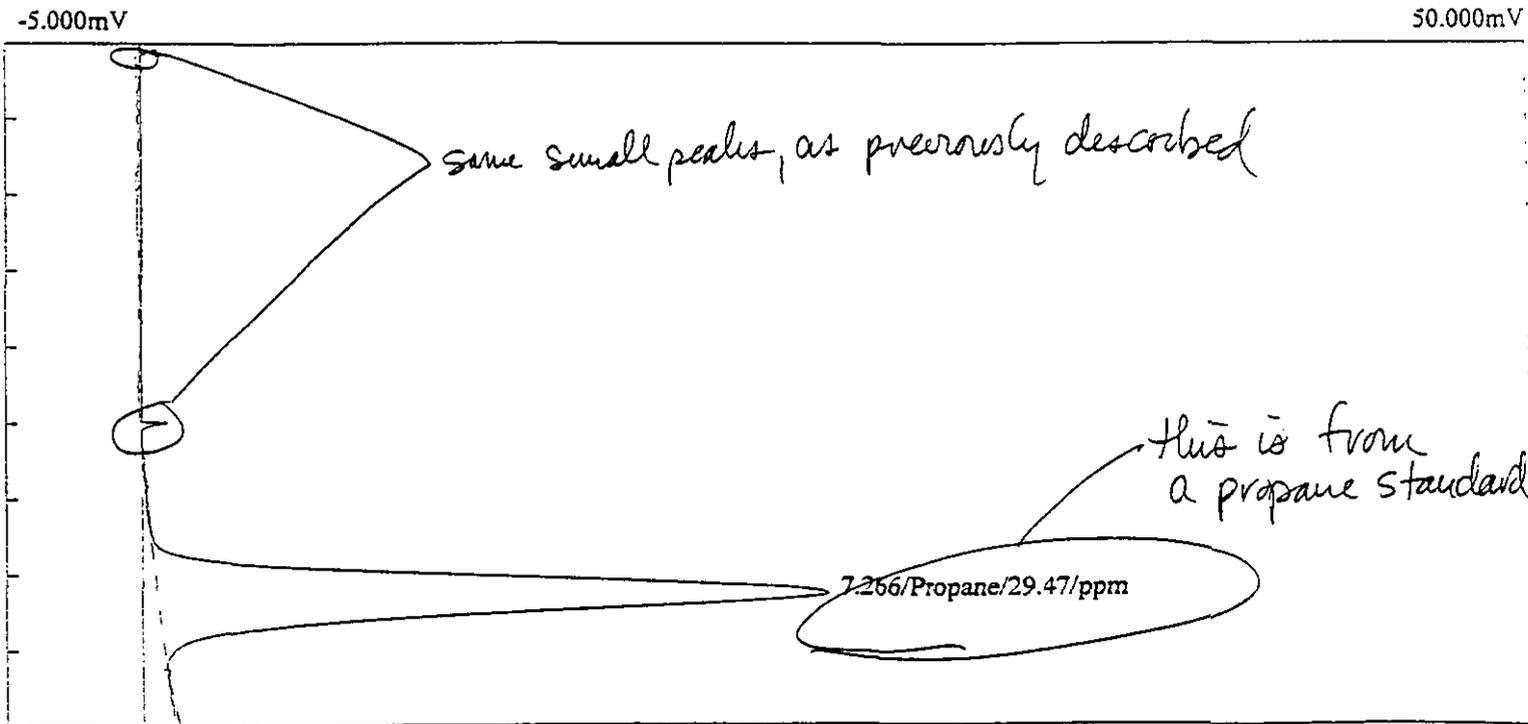
DRAFT

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
Propane	7.266	774.786	29.47	ppm
		775	29	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 16:12:50

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F1R25.CHR (c:\peakwin)

Sample: Fan #1 Run 2

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

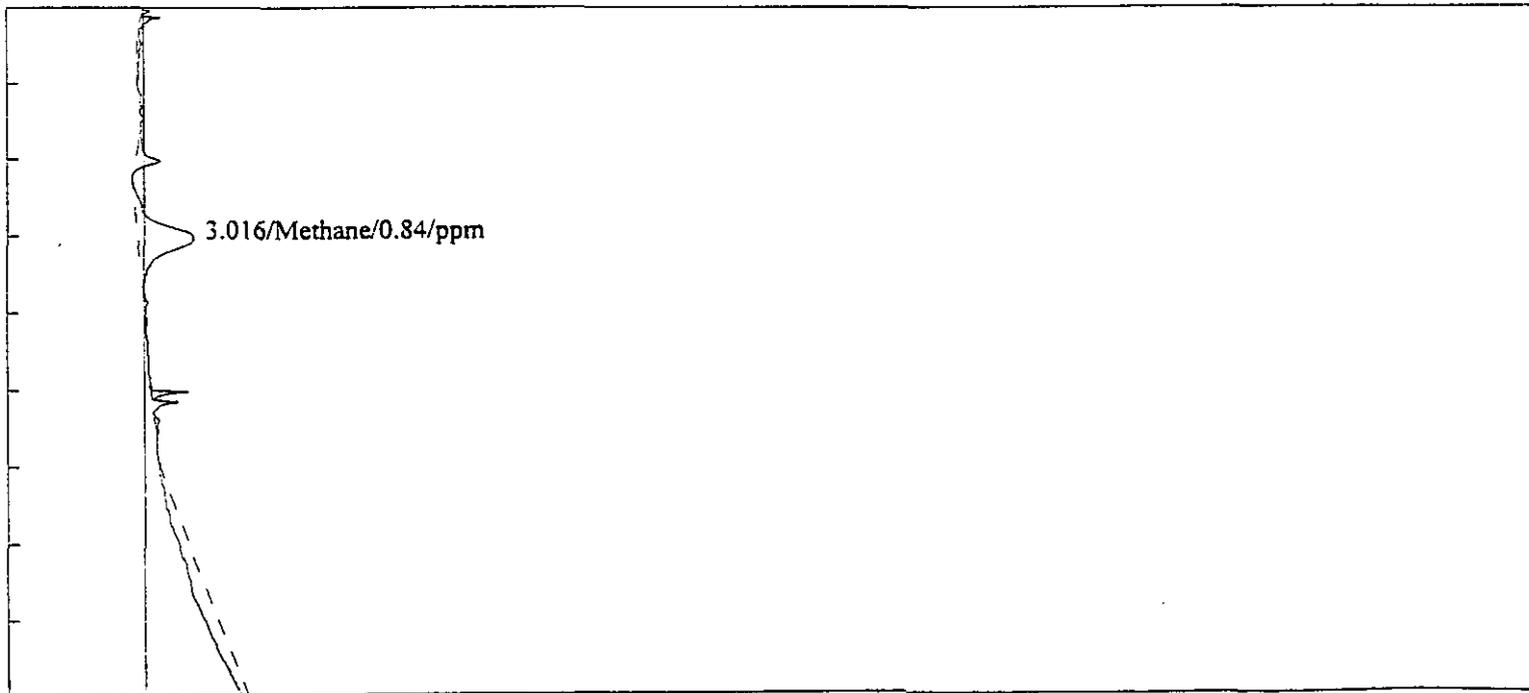
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.016	26.644	0.84	ppm

27 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 20:44:04

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F1R32.CHR (c:\peakwin)

Sample: Fan #1 Run #3

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

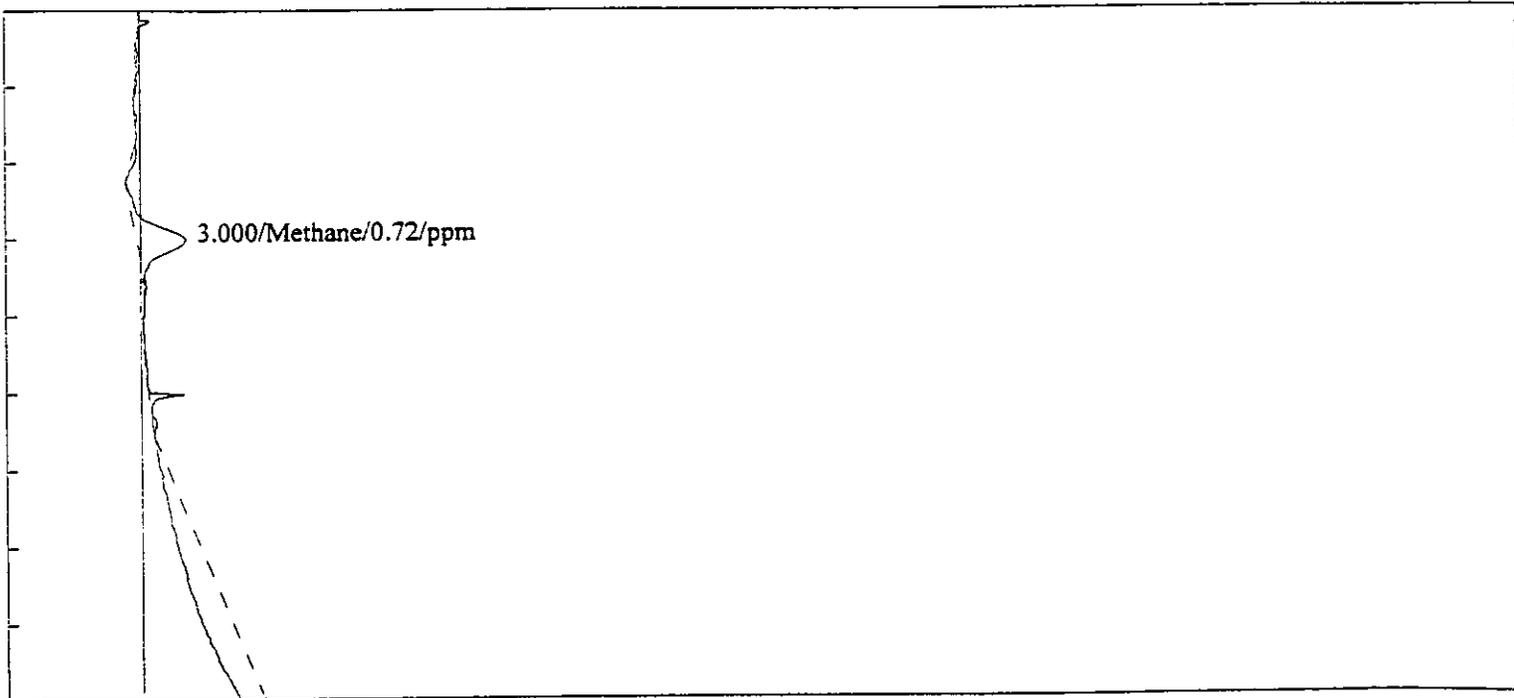
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.000	22.854	0.72	ppm
		23	1	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 00:43:46

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F1R42.CHR (c:\peakwin)

Sample: Fan #1 Run #4

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

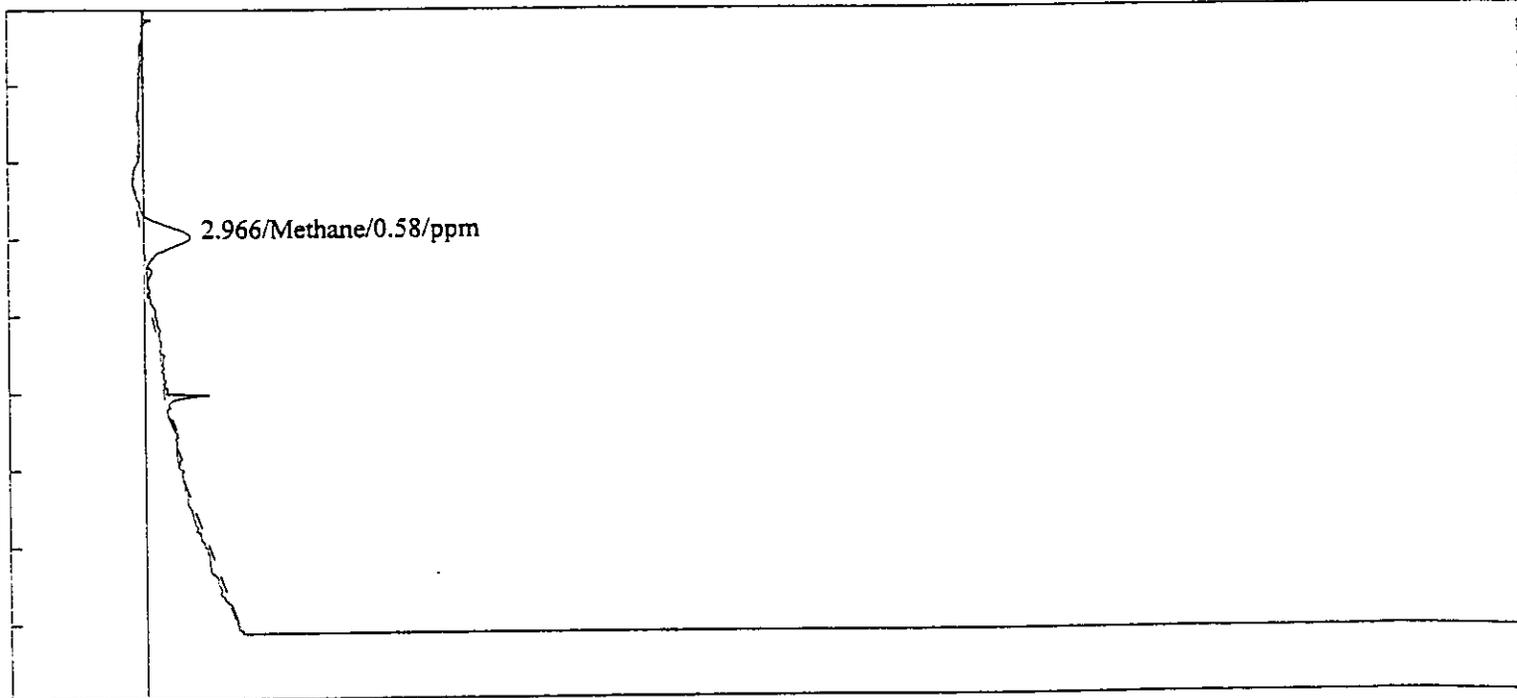
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	2.966	18.500	0.58	ppm

18 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 05:39:35

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F1R52.CHR (c:\peakwin)

Sample: Fan #1 Run #5

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

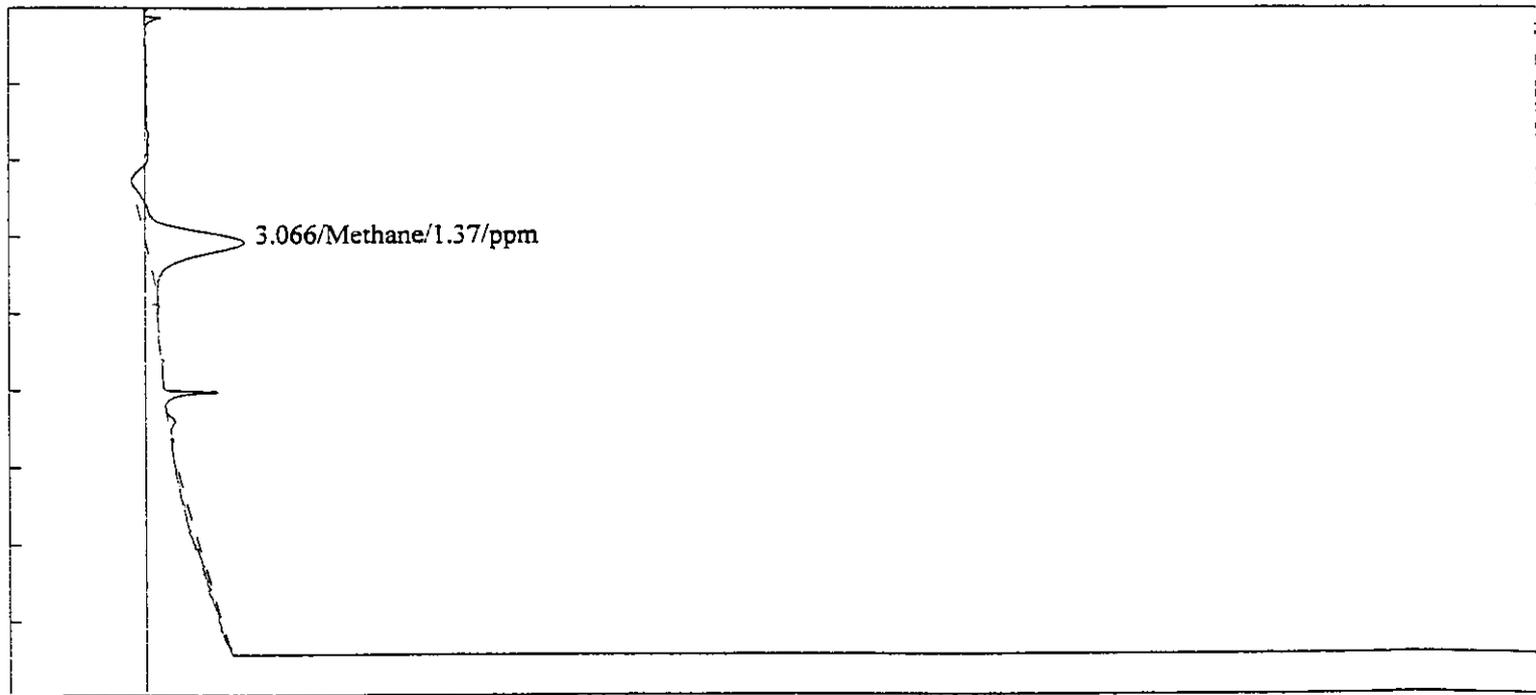
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.066	43.735	1.37	ppm

44 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 14:33:04

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F1R62.CHR (c:\peakwin)

Sample: Fan #1 Run #6

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

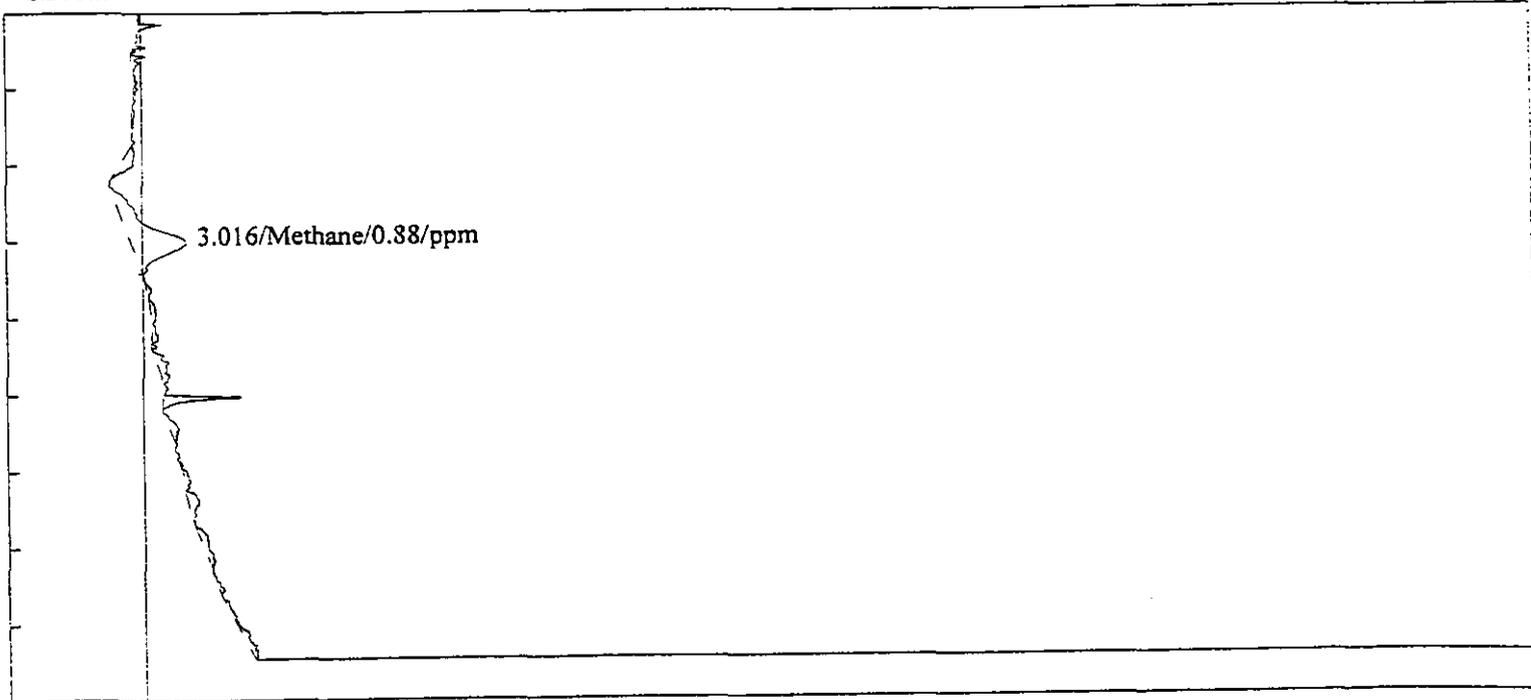
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.016	28.154	0.88	ppm

28 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 20:07:05

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F2R12.CHR (c:\peakwin)

Sample: Fan #2 Run #1

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

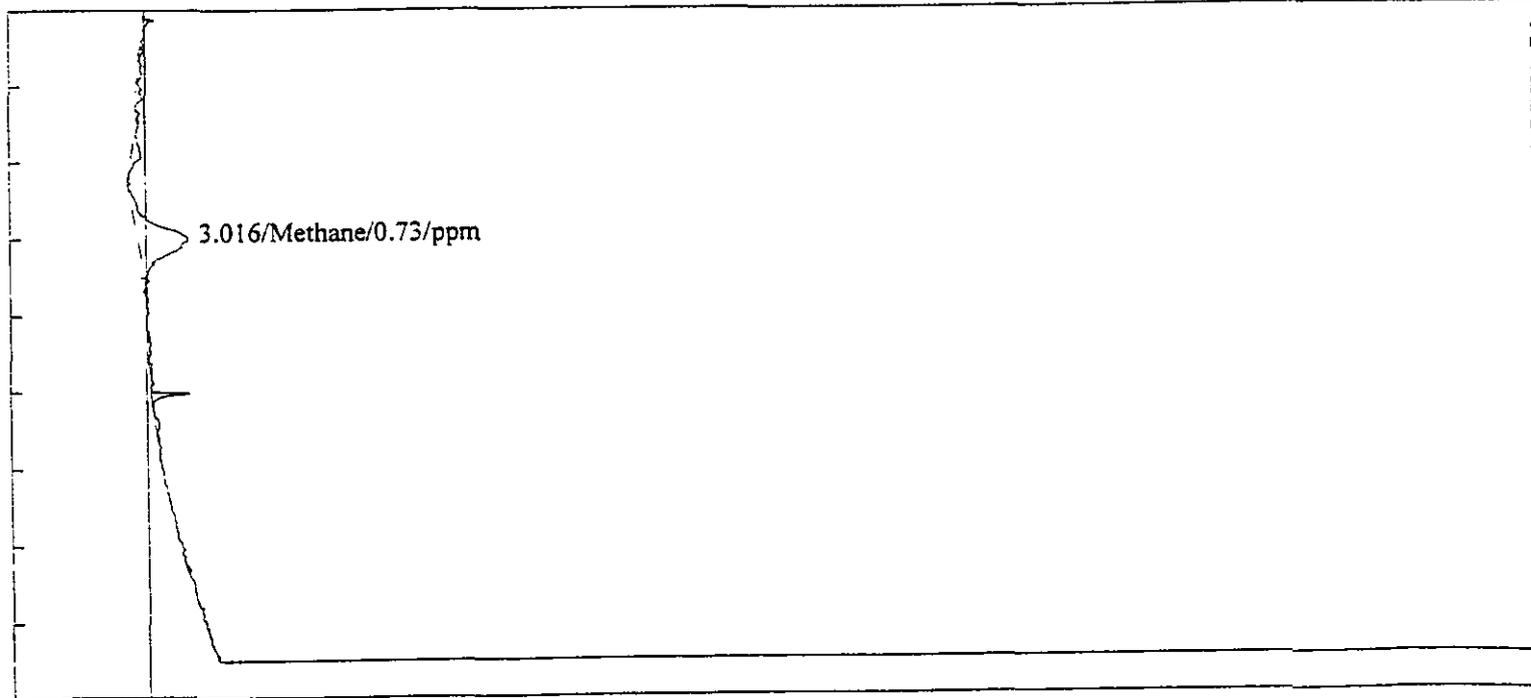
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.016	23.274	0.73	ppm

23 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 16:29:05

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F2R22.CHR (c:\peakwin)

Sample: Fan #2 Run 2

Operator: Michael B. Weiner

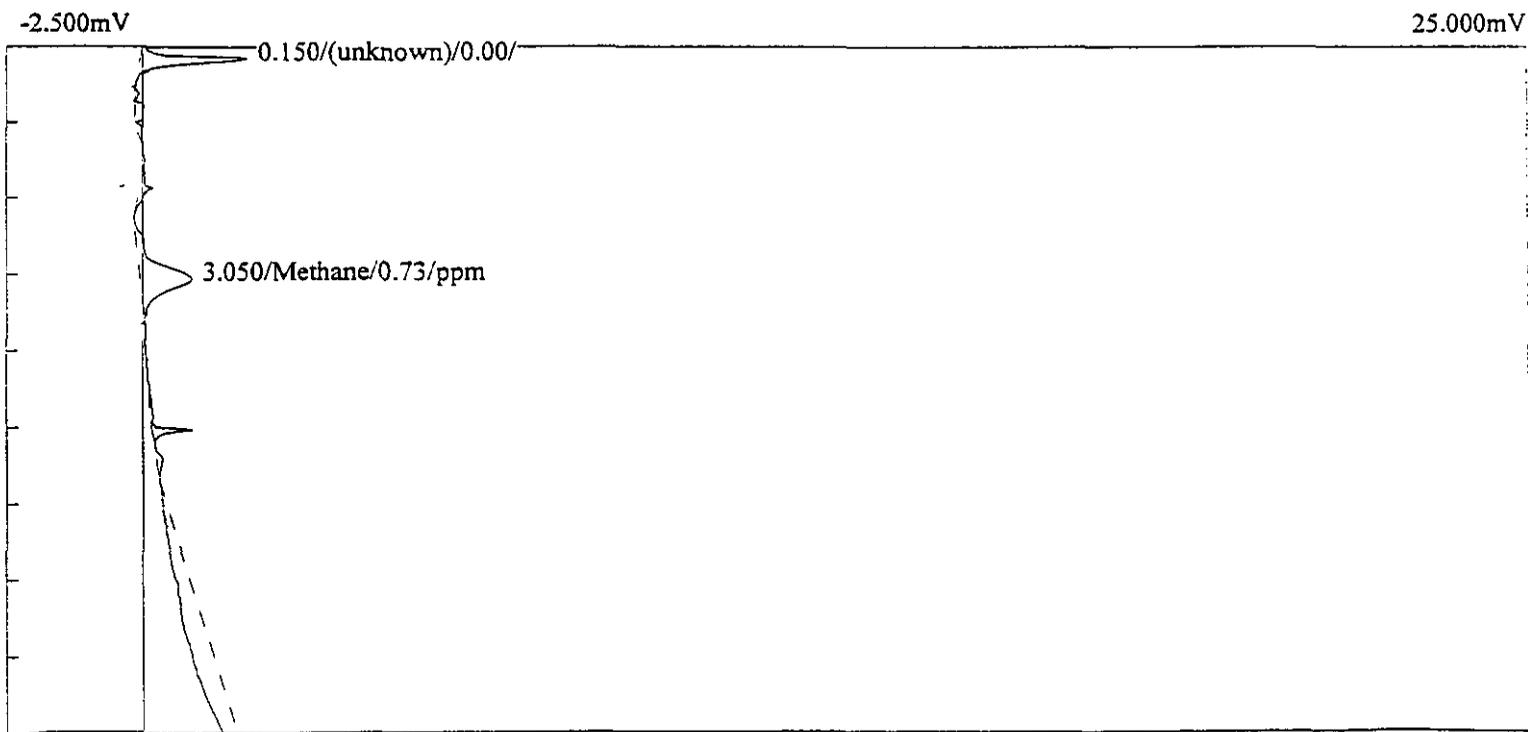
Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
(unknown)	0.150	14.076	0.00	
Methane	3.050	23.392	0.73	ppm

37 0

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 22:21:44

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F2R32.CHR (c:\peakwin)

Sample: Fan #2 Run #3

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

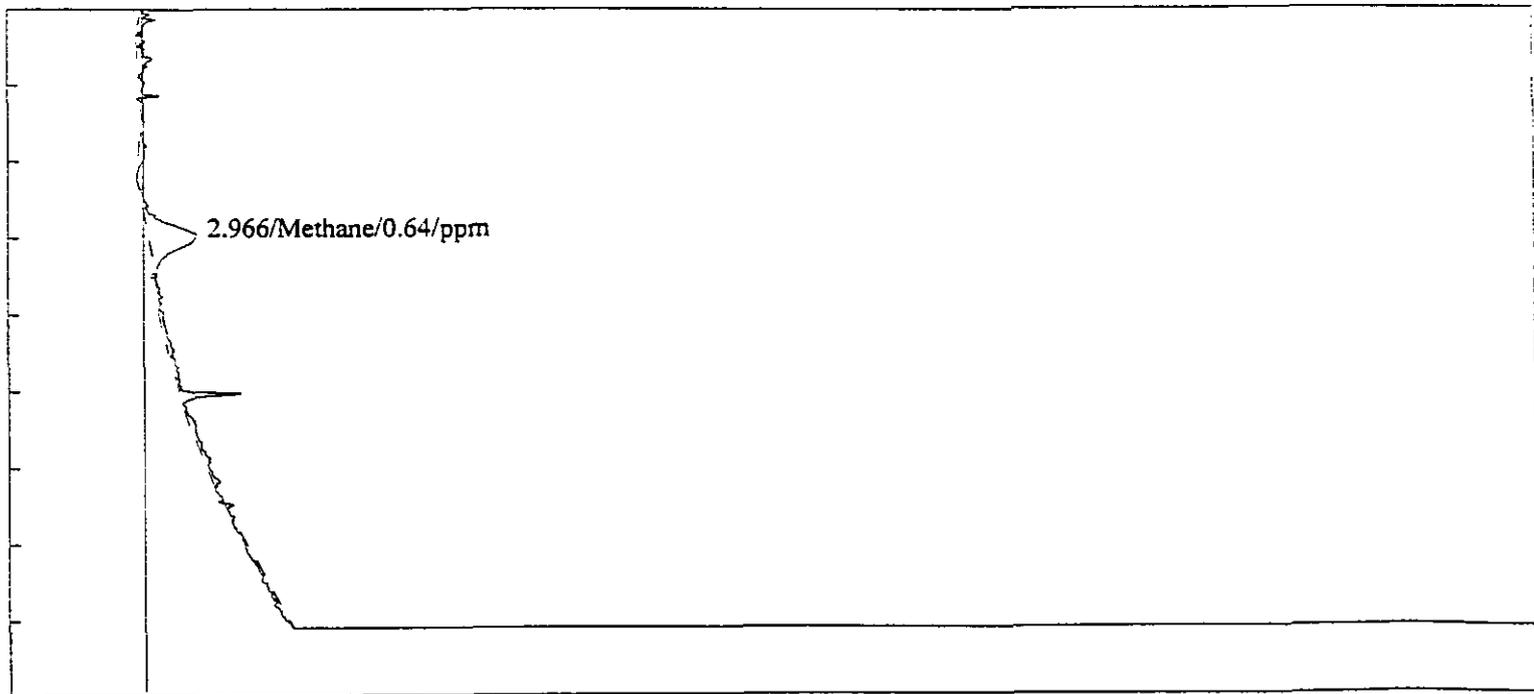
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention Area	External	Units
Methane	2.966	20.532	0.64 ppm

21 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 14:37:42

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F2R44.CHR (c:\peakwin)

Sample: Fan #2 Run #4

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

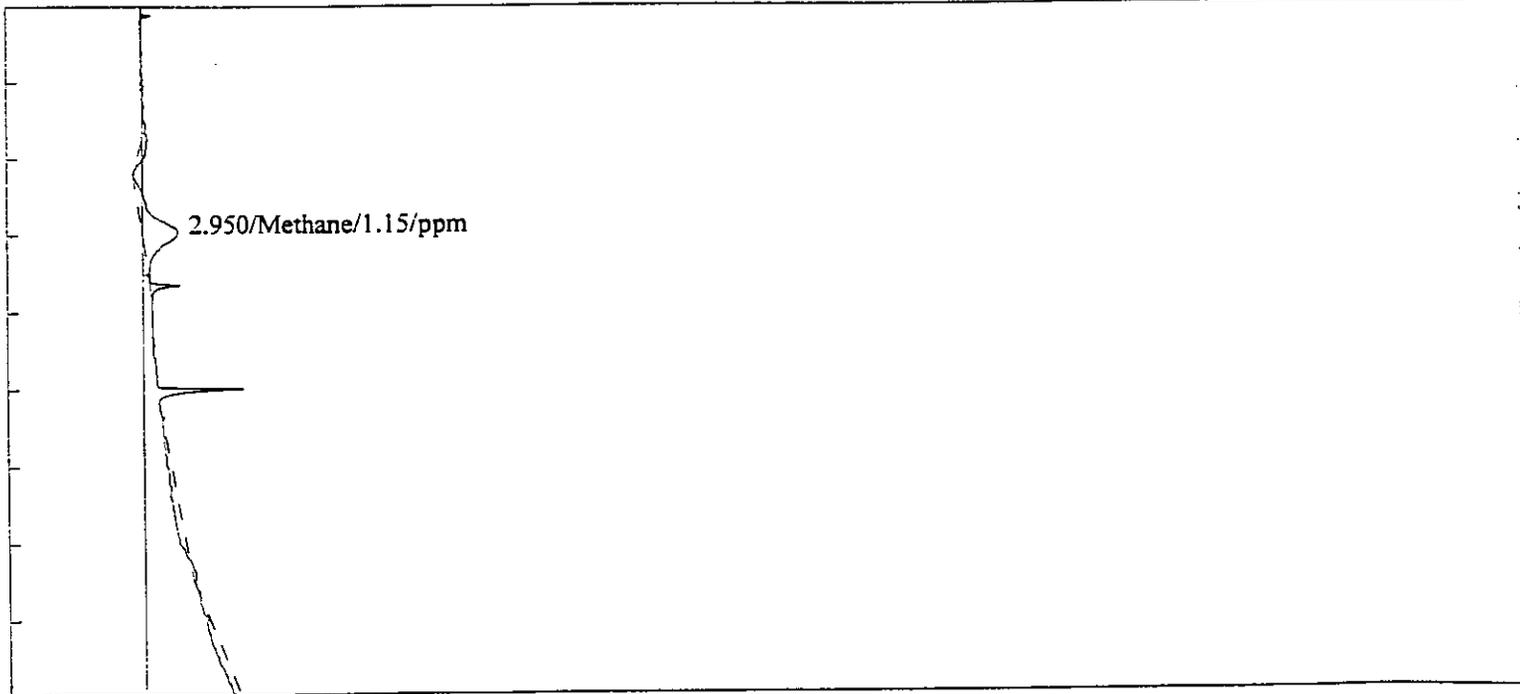
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Methane	2.950	36.797	1.15	ppm

37 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 05:51:33

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F2R52.CHR (c:\peakwin)

Sample: Fan #2 Run #5

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

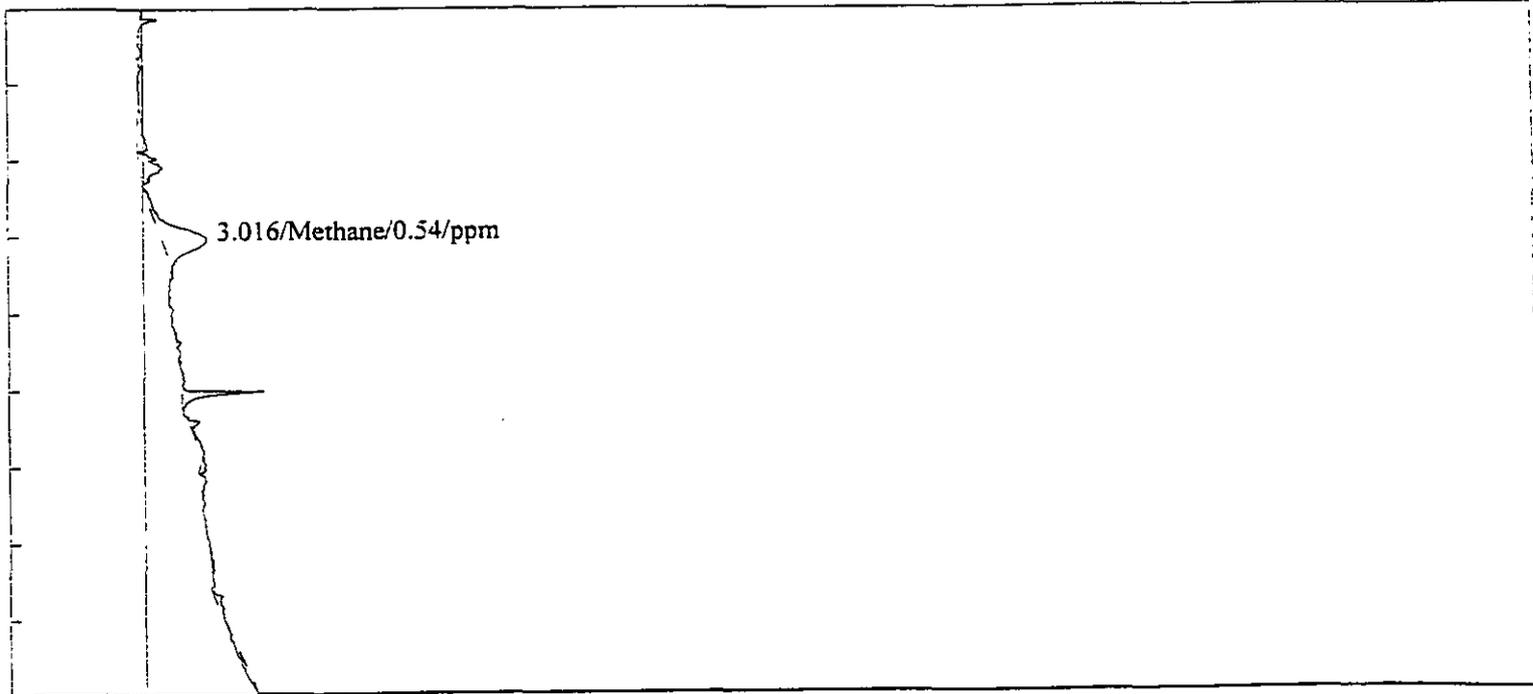
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.016	17.364	0.54	ppm

17 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 14:47:14

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F2R62.CHR (c:\peakwin)

Sample: Fan #2 Run #6

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

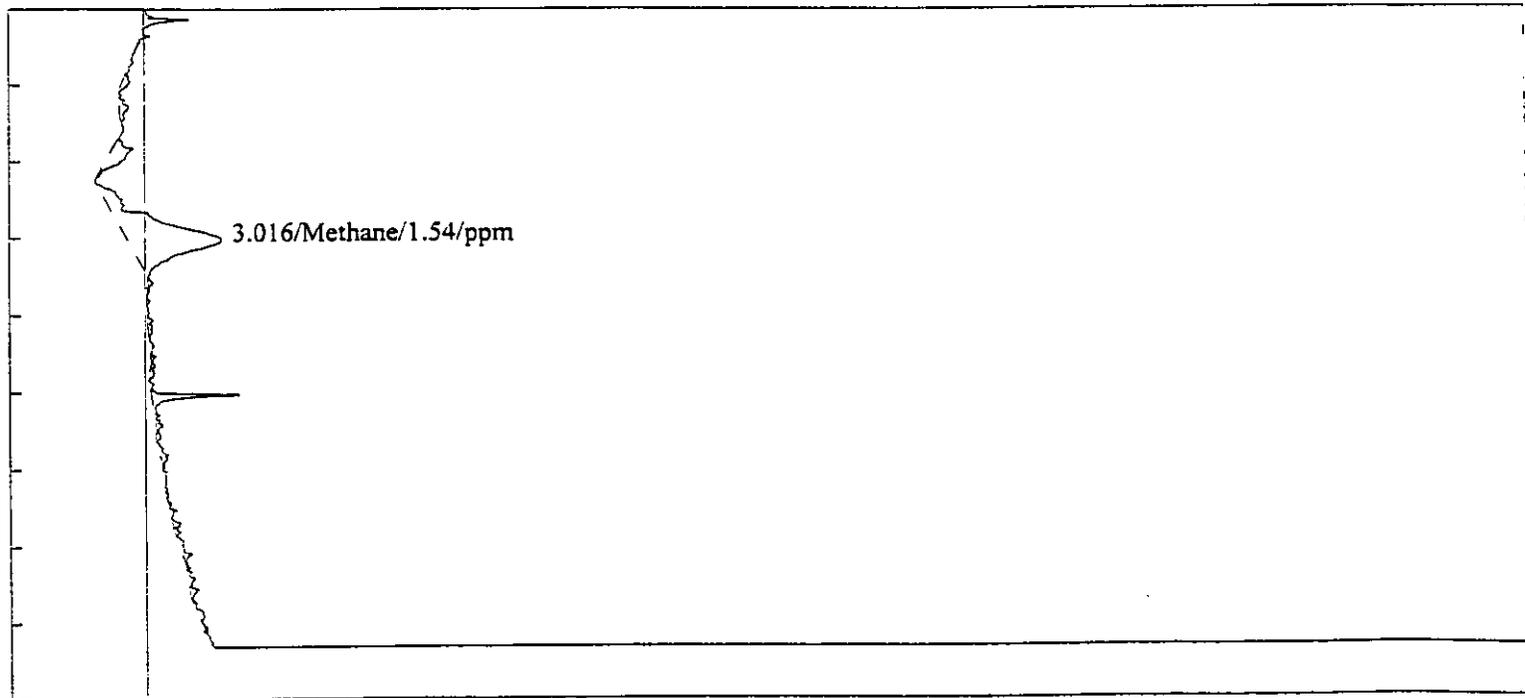
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.016	49.176	1.54	ppm

49 2

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 20:19:38

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F3R12.CHR (c:\peakwin)

Sample: Fan #3 Run #1

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

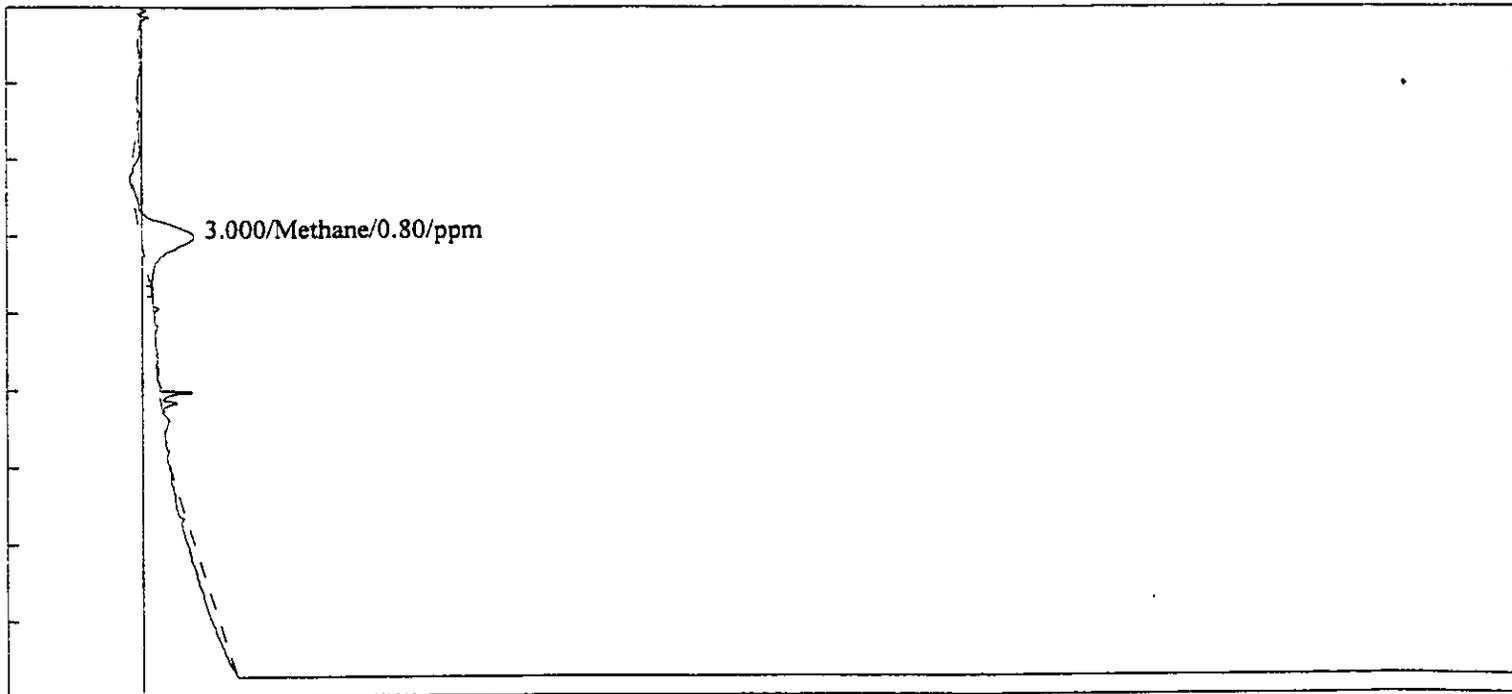
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.000	25.345	0.80	ppm
		25	1	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 13:13:10

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F3R24.CHR (c:\peakwin)

Sample: Fan #3 Run 2

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

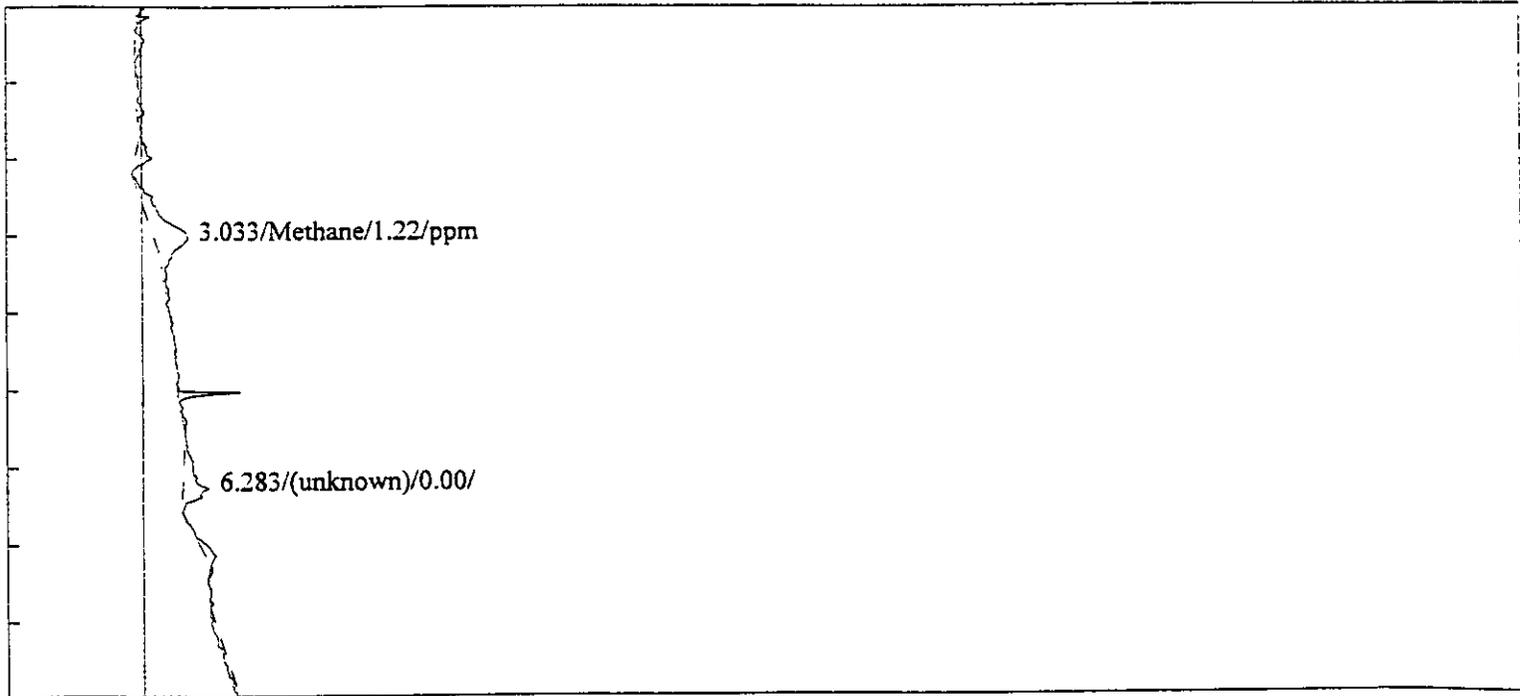
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Methane	3.033	38.880	1.22	ppm
(unknown)	6.283	19.394	0.00	

58 0

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 22:33:09

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F3R32.CHR (c:\peakwin)

Sample: Fan #3 Run #3

Operator: Michael B. Weiner

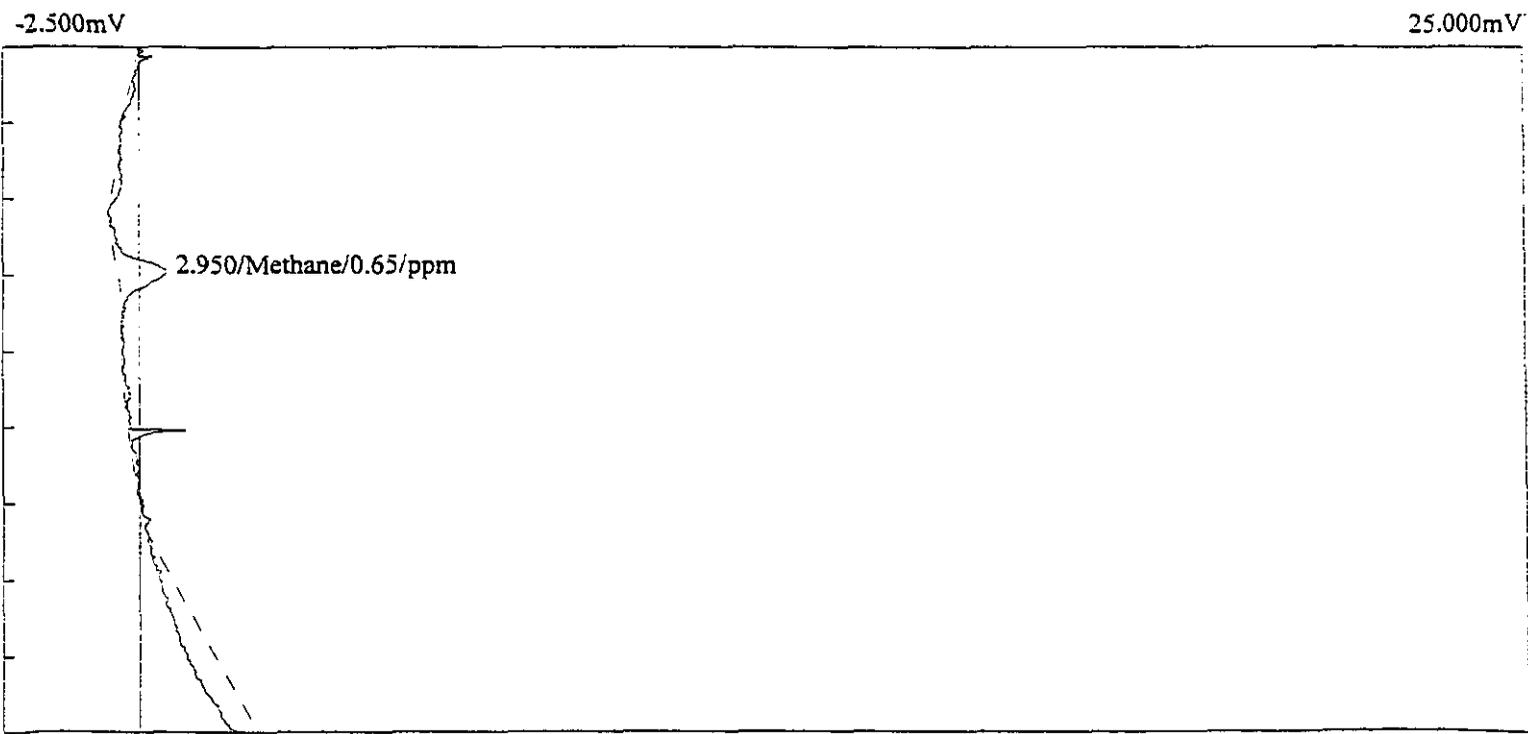
Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
Methane	2.950	20.760	0.65	ppm
		21	1	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 04:25:36

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F3R42.CHR (c:\peakwin)

Sample: Fan #3 Run #4

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

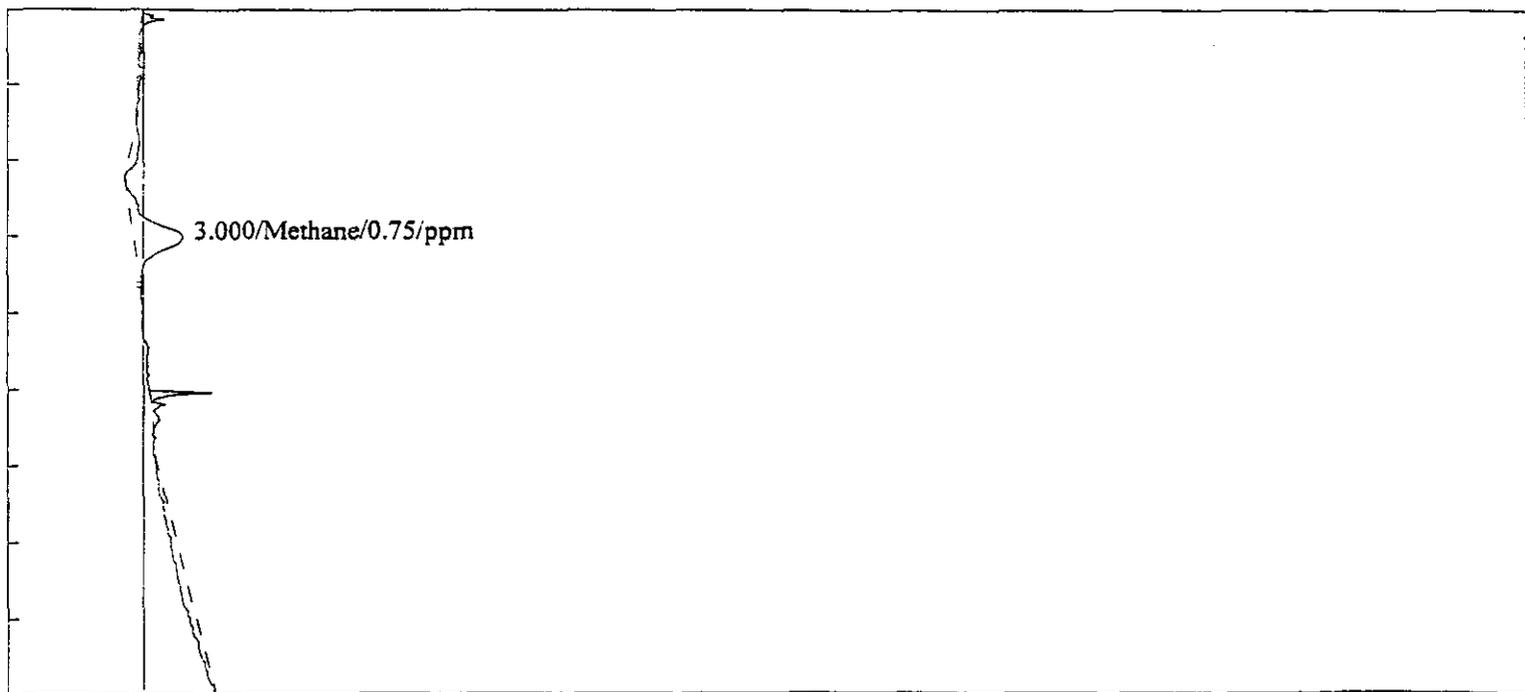
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.000	23.862	0.75	ppm

24 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 13:35:45

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F3R53.CHR (c:\peakwin)

Sample: Fan #3 Run #5

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

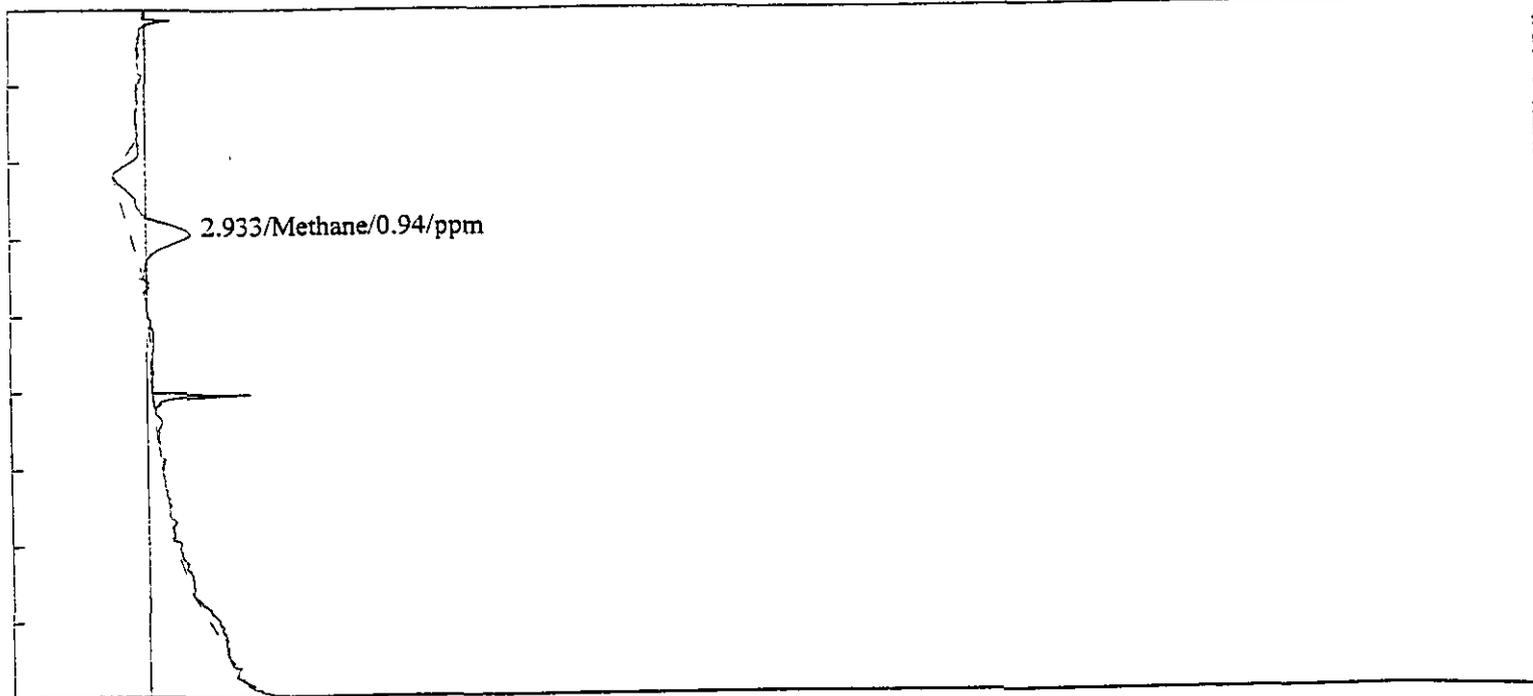
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	2.933	30.066	0.94	ppm
		30	1	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 14:59:09

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F3R62.CHR (c:\peakwin)

Sample: Fan #3 Run #6

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

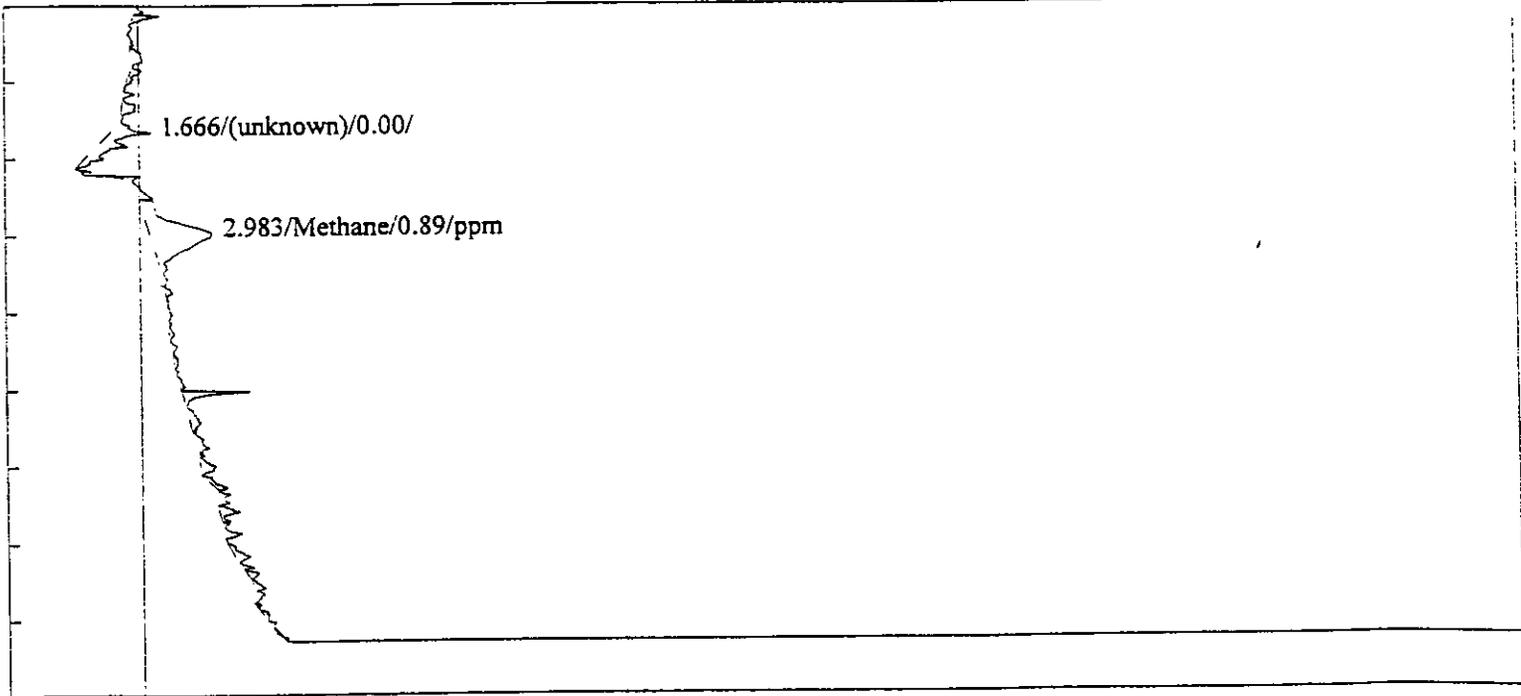
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
(unknown)	1.666	10.576	0.00	
Methane	2.983	28.473	0.89	ppm
		39	0	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 00:16:19

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F4R12.CHR (c:\peakwin)

Sample: Fan #4 Run #1

Operator: Michael B. Weiner

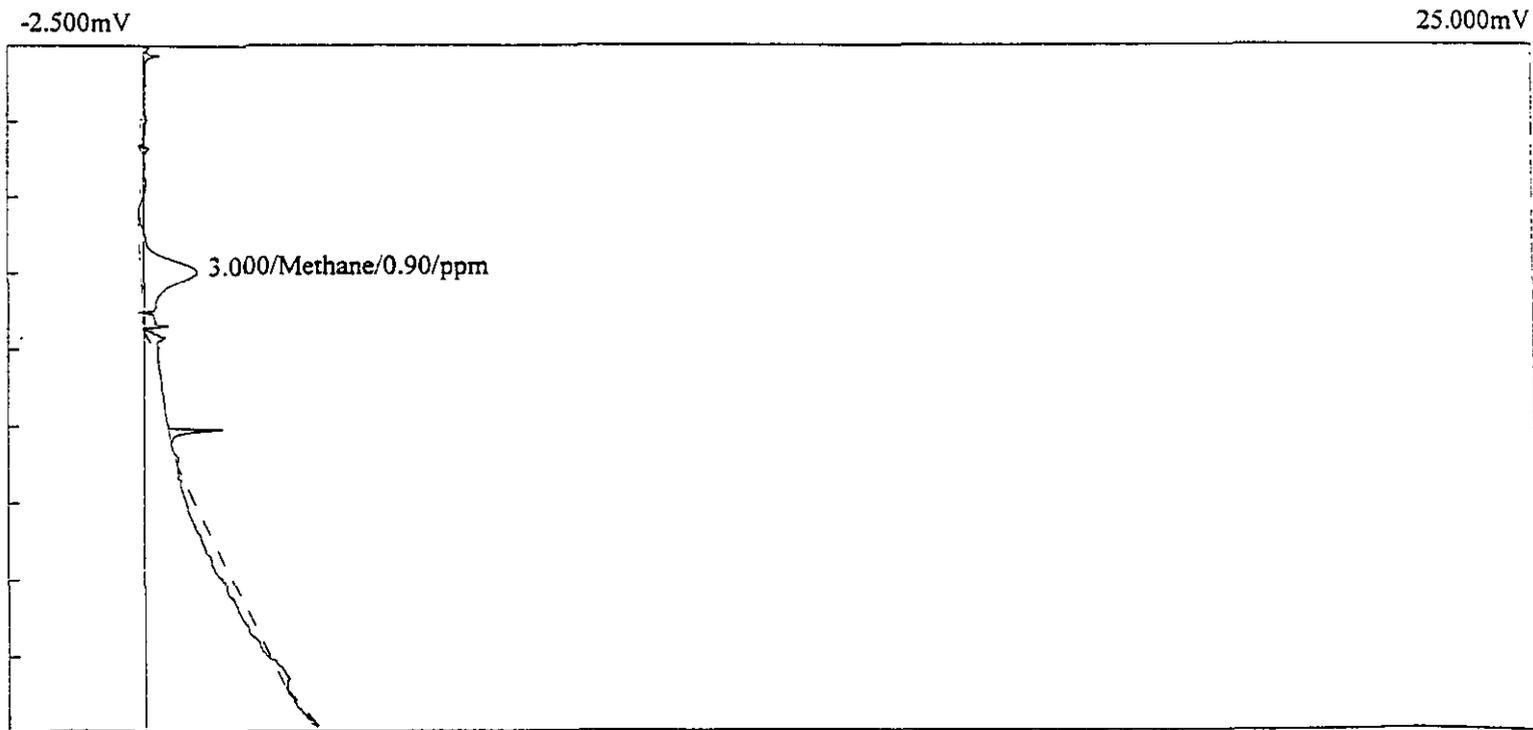
Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
Methane	3.000	28.826	0.90	ppm

29 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 19:40:05

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F4R22.CHR (c:\peakwin)

Sample: Fan #4 Run #2

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

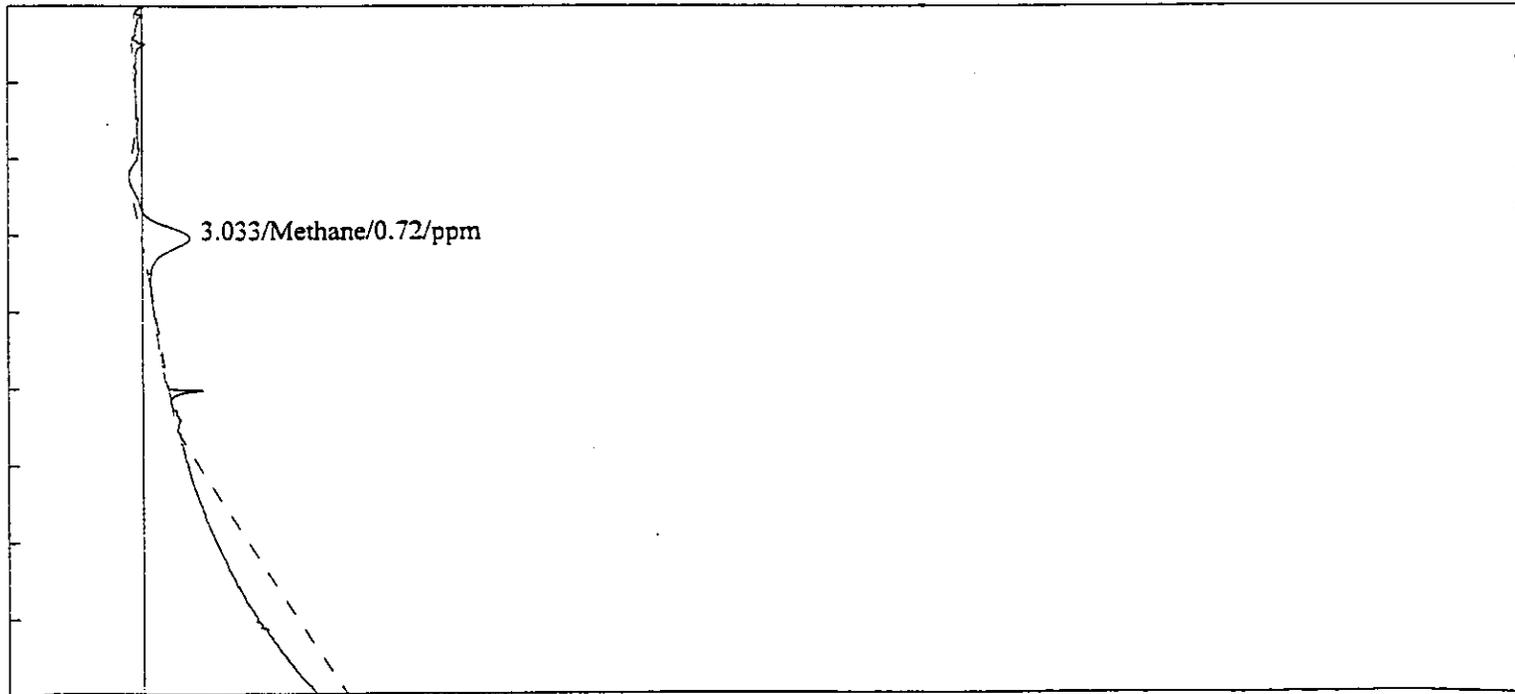
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	150

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.033	23.068	0.72	ppm

23 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 13:32:33

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F4R33.CHR (c:\peakwin)

Sample: Fan #4 Run #3

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

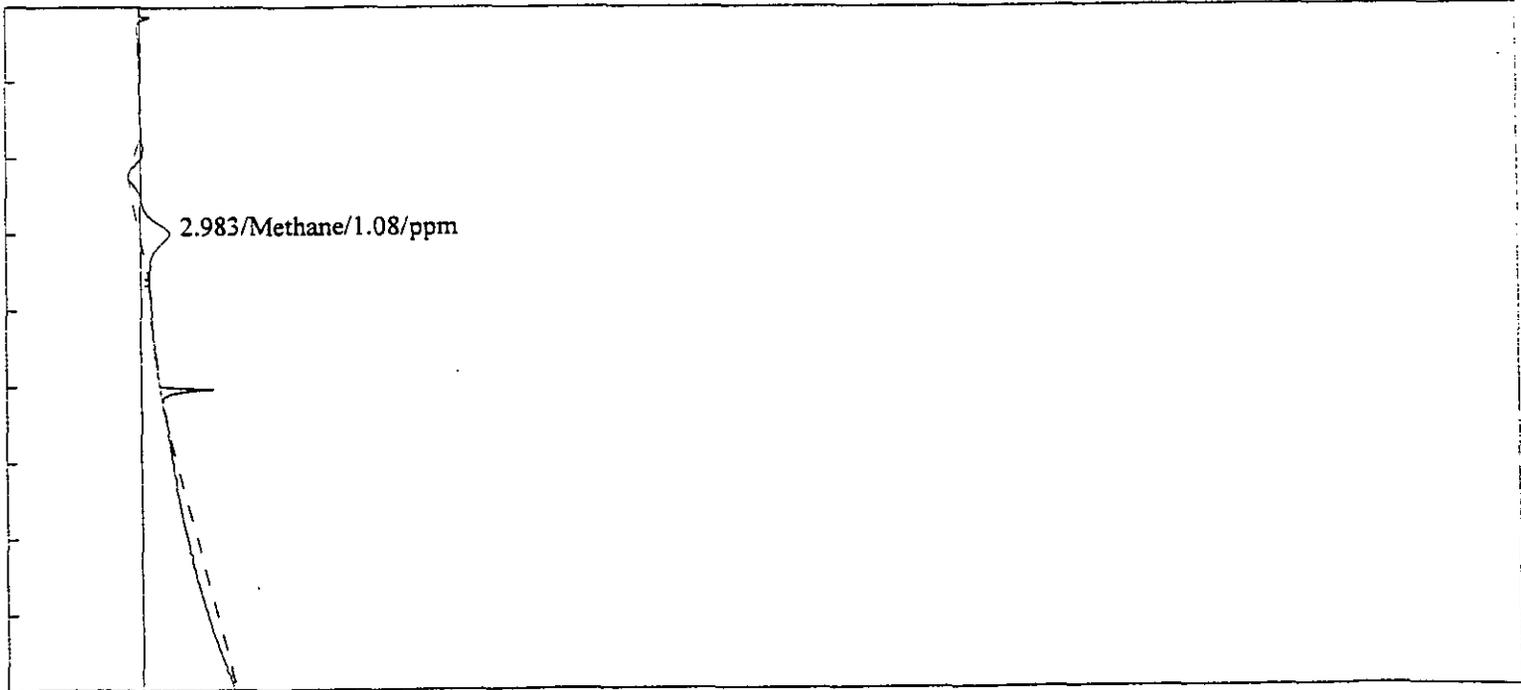
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Methane	2.983	34.558	1.08	ppm
		35	1	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 05:12:15

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F4R42.CHR (c:\peakwin)

Sample: Fan #4 Run #4

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

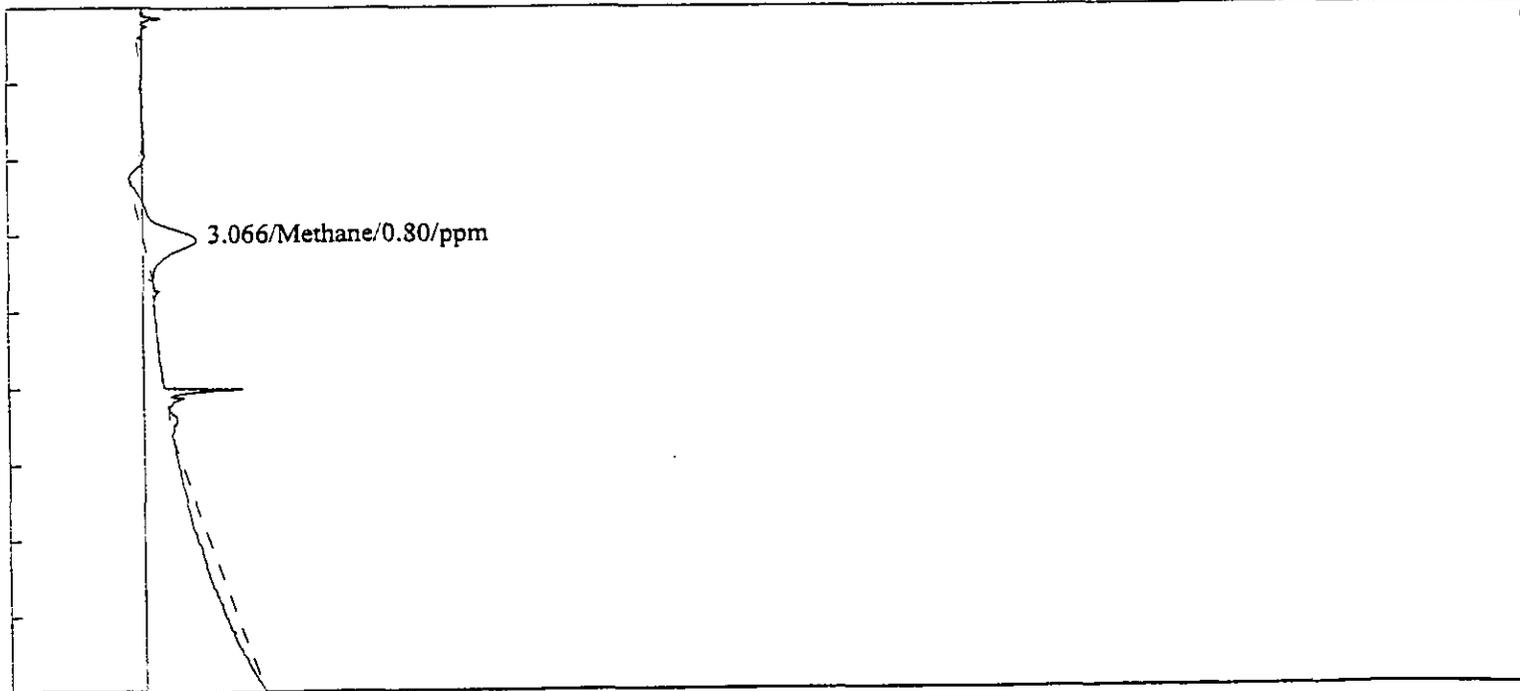
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.066	25.471	0.80	ppm

25 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 14:00:54

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F4R52.CHR (c:\peakwin)

Sample: Fan #4 Run #5

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

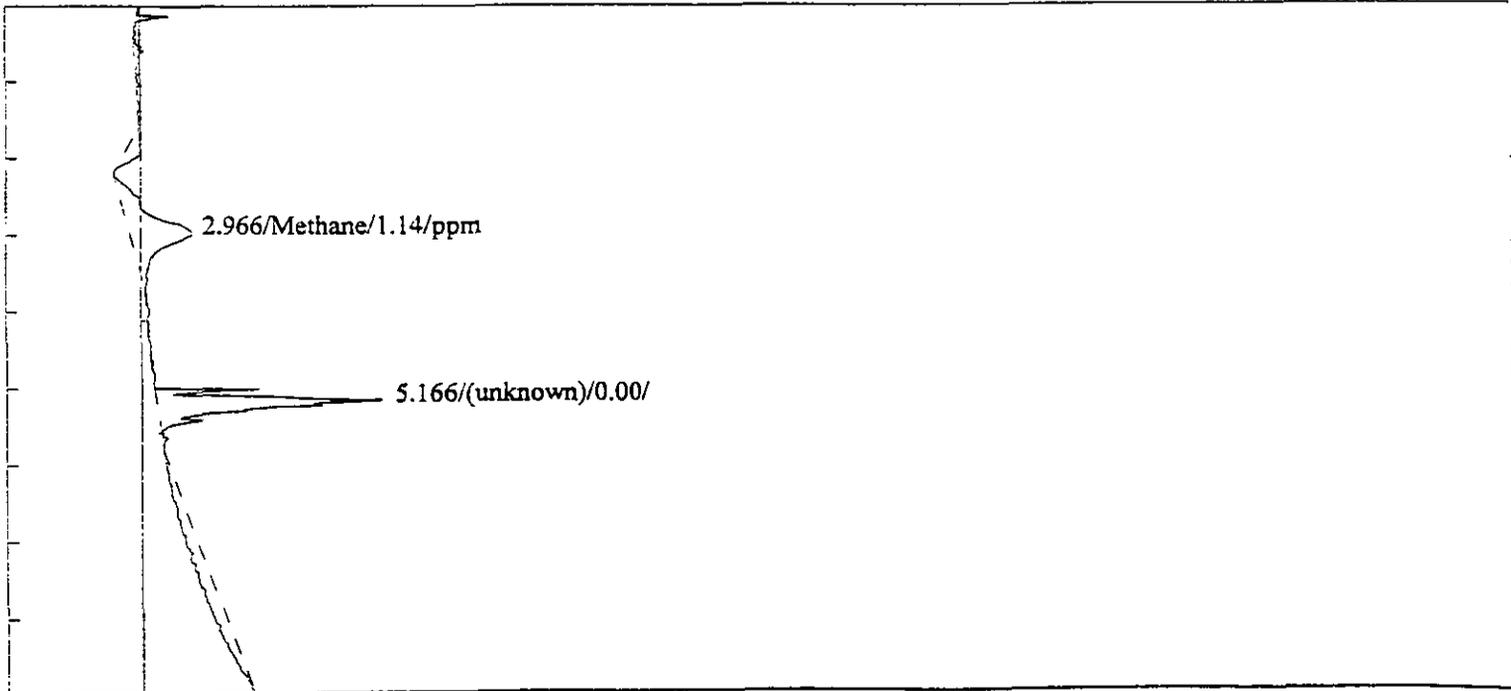
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	2.966	36.424	1.14	ppm
(unknown)	5.166	44.460	0.00	

81 0

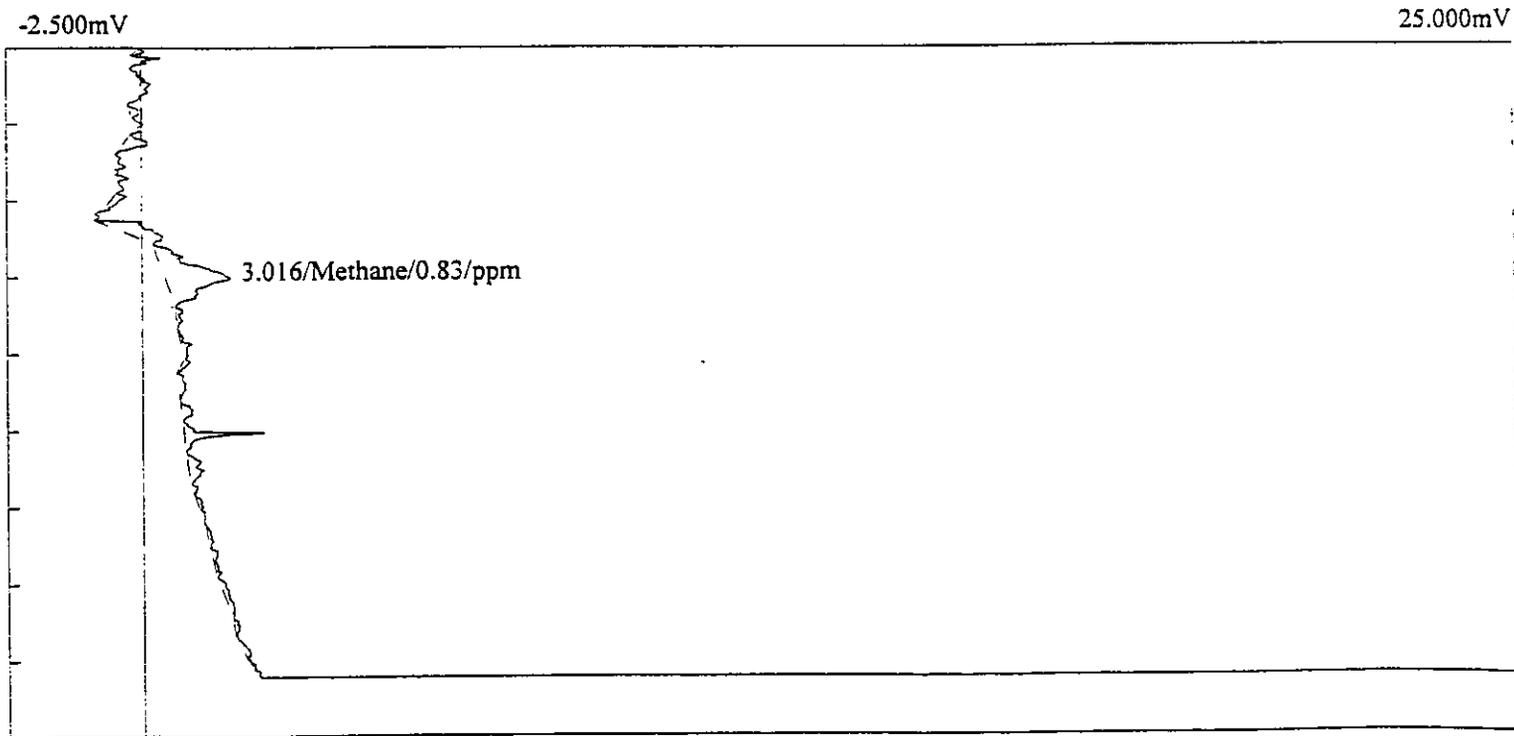
Lab name: Fluid Management, Inc.
 Client: Ladish Malting Co.
 Client ID: J95.502AQ
 Collected: 11/14/95
 Analysis date: 11/15/1995 15:11:47
 Method: Mod. USEPA Method 18
 Description: Ch. 1 FMI-FID
 Column: 3' Silica Gel
 Carrier: N2 at 300 on dial
 Temp. prog: FMI.TEM
 Components: FMI.CPT
 Control file: DEFAULT.CON
 Data file: F4R62.CHR (c:\peakwin)
 Sample: Fan #4 Run #6
 Operator: Michael B. Weiner
 Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	150

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
Methane	3.016	26.404	0.83	ppm
		26	1	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 20:31:53

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F5R12.CHR (c:\peakwin)

Sample: Fan #5 Run #1

Operator: Michael B. Weiner

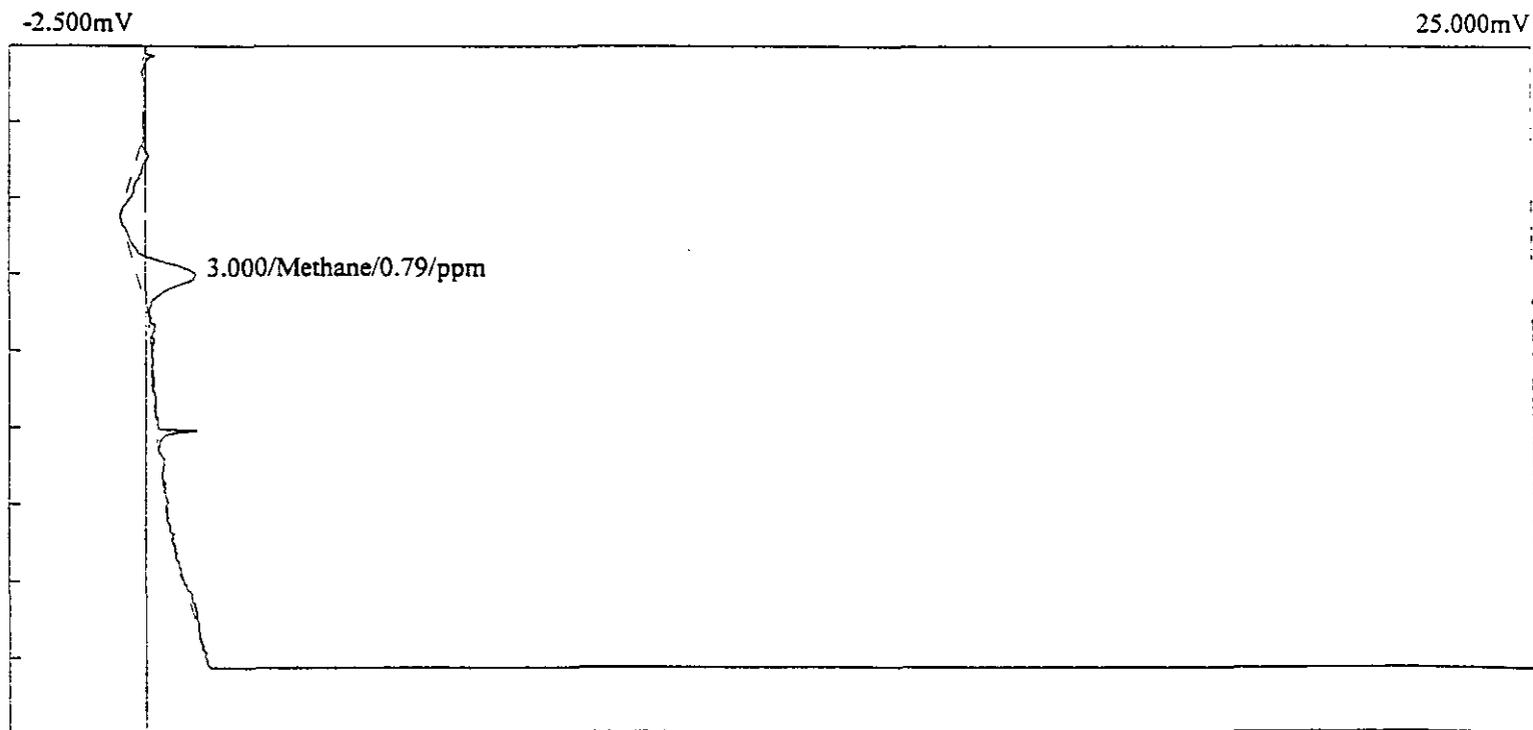
Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
Methane	3.000	25.140	0.79	ppm
		25	1	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 19:54:54

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F5R22.CHR (c:\peakwin)

Sample: Fan #5 Run #2

Operator: Michael B. Weiner

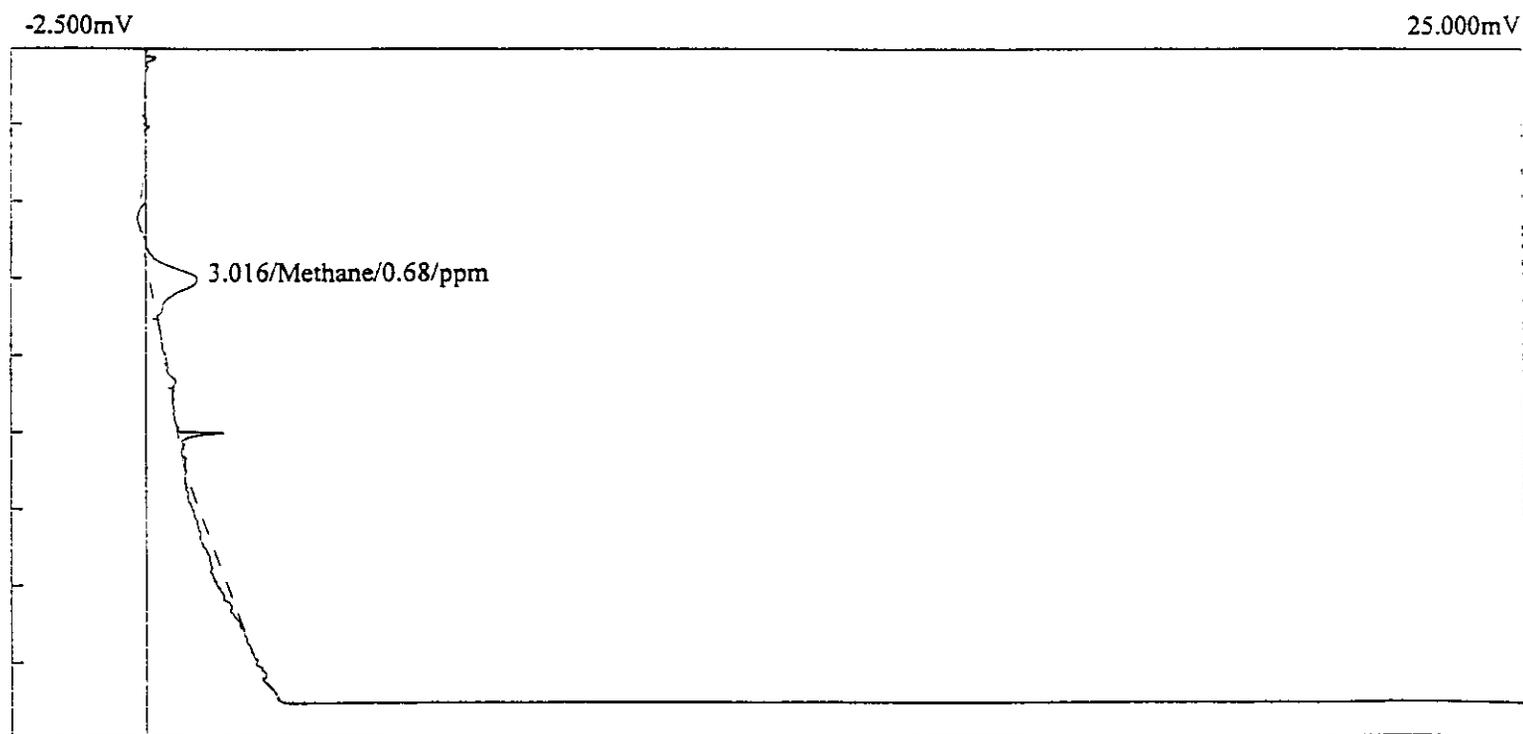
Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
Methane	3.016	21.808	0.68	ppm

22 1

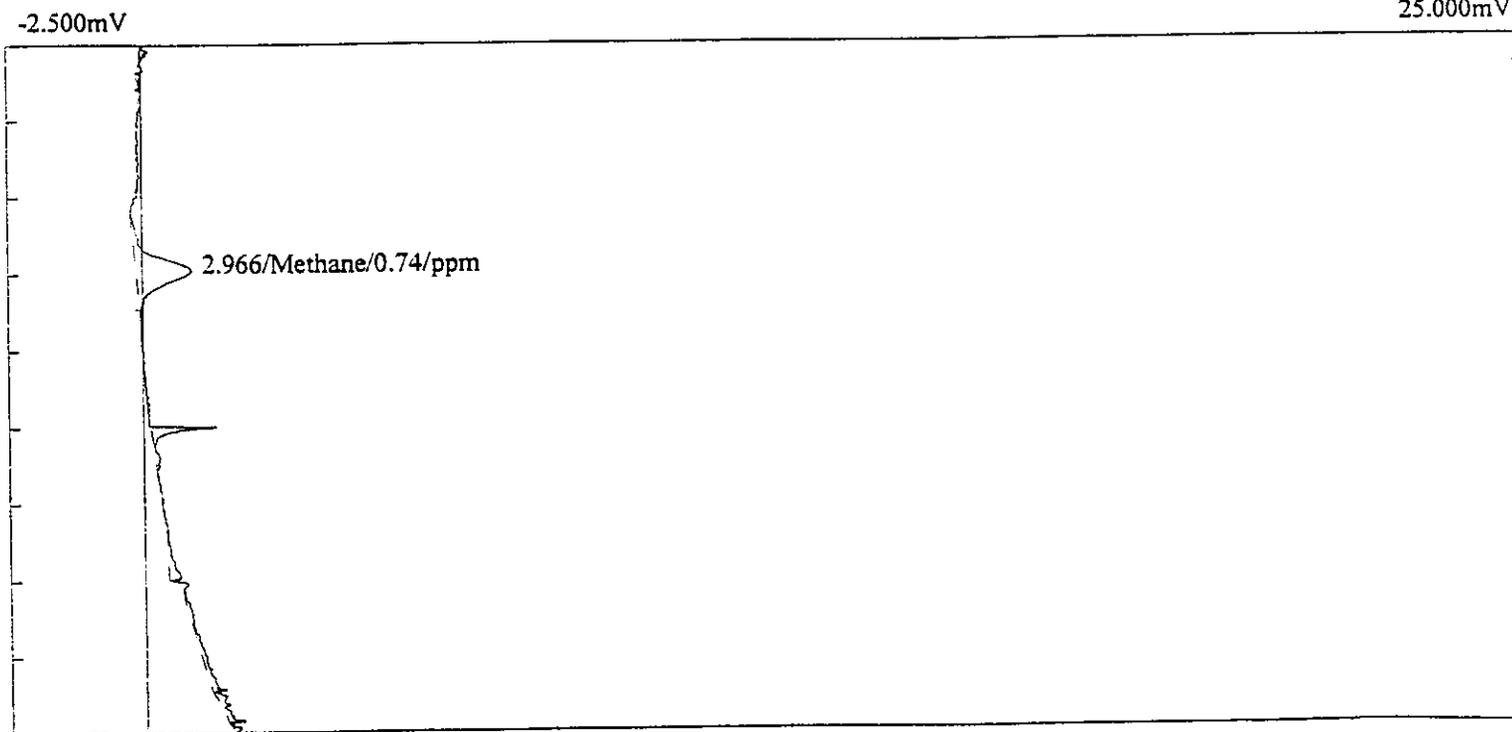
Lab name: Fluid Management, Inc.
 Client: Ladish Malting Co.
 Client ID: J95.502AQ
 Collected: 11/14/95
 Analysis date: 11/15/1995 00:30:04
 Method: Mod. USEPA Method 18
 Description: Ch. 1 FMI-FID
 Column: 3' Silica Gel
 Carrier: N2 at 300 on dial
 Temp. prog: FMI.TEM
 Components: FMI.CPT
 Control file: DEFAULT.CON
 Data file: F5R32.CHR (c:\peakwin)
 Sample: Fan #5 Run #3
 Operator: Michael B. Weiner
 Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
Methane	2.966	23.722	0.74	ppm
		24	1	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 05:24:44

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F5R42.CHR (c:\peakwin)

Sample: Fan #5 Run #4

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

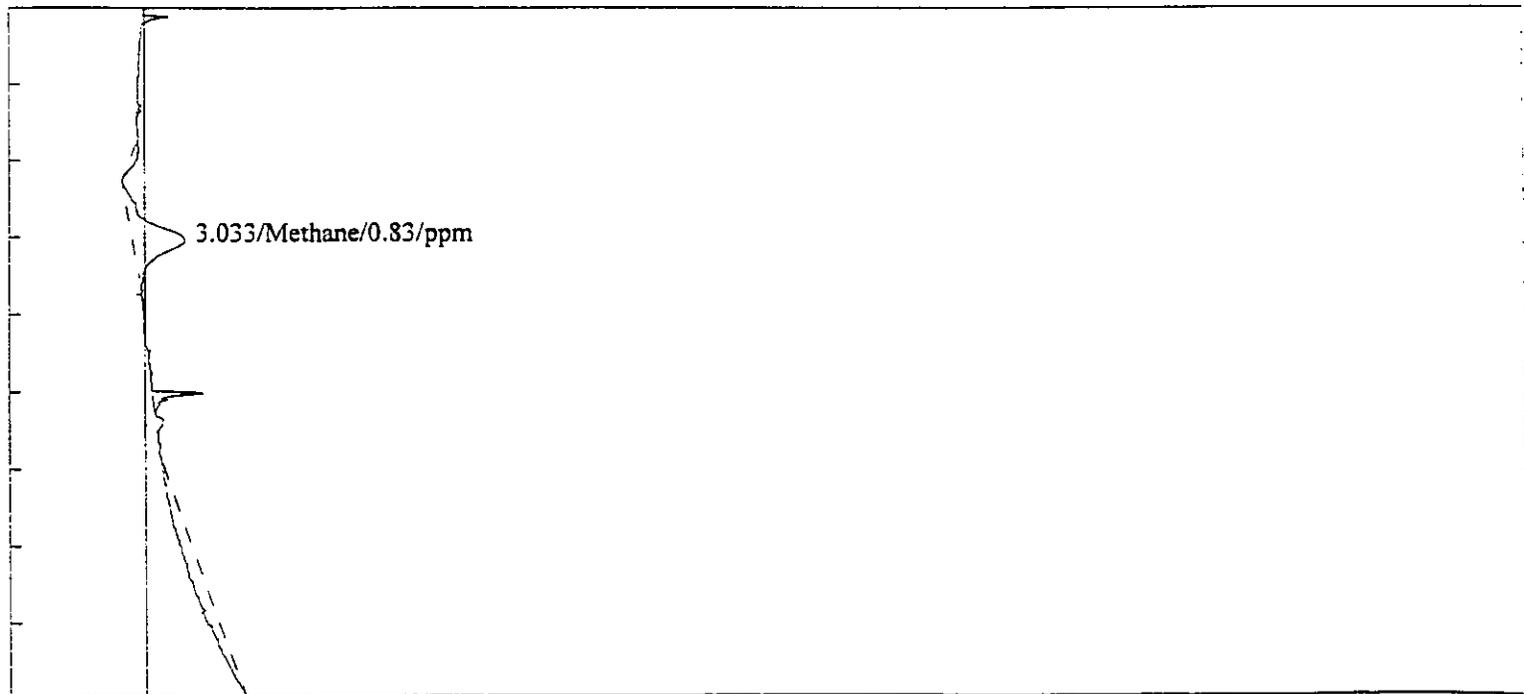
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.033	26.576	0.83	ppm

27 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 14:20:15

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F5R52.CHR (c:\peakwin)

Sample: Fan #5 Run #5

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

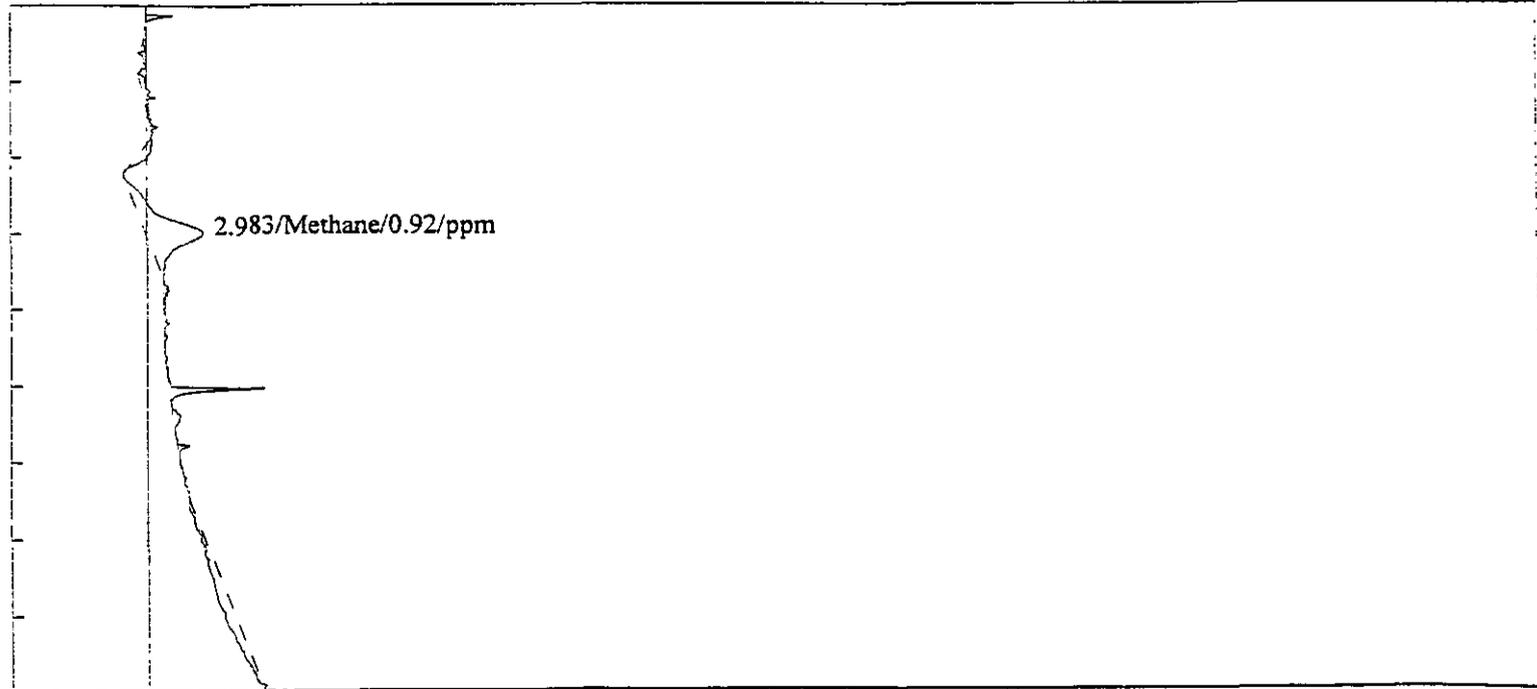
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	2.983	29.272	0.92	ppm

29 1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/15/1995 15:23:46

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: F5R62.CHR (c:\peakwin)

Sample: Fan #5 Run #6

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

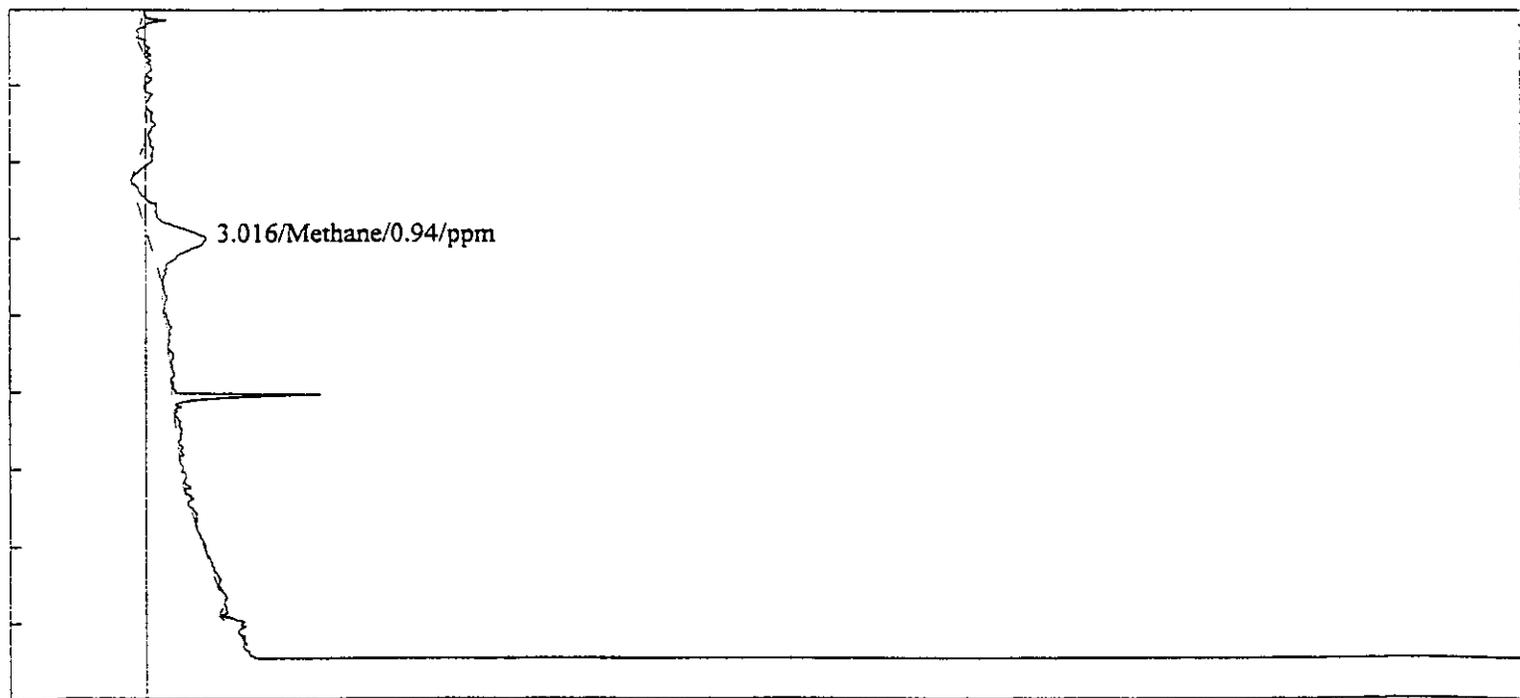
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-2.500mV

25.000mV



Component	Retention	Area	External	Units
Methane	3.016	30.044	0.94	ppm

30 1

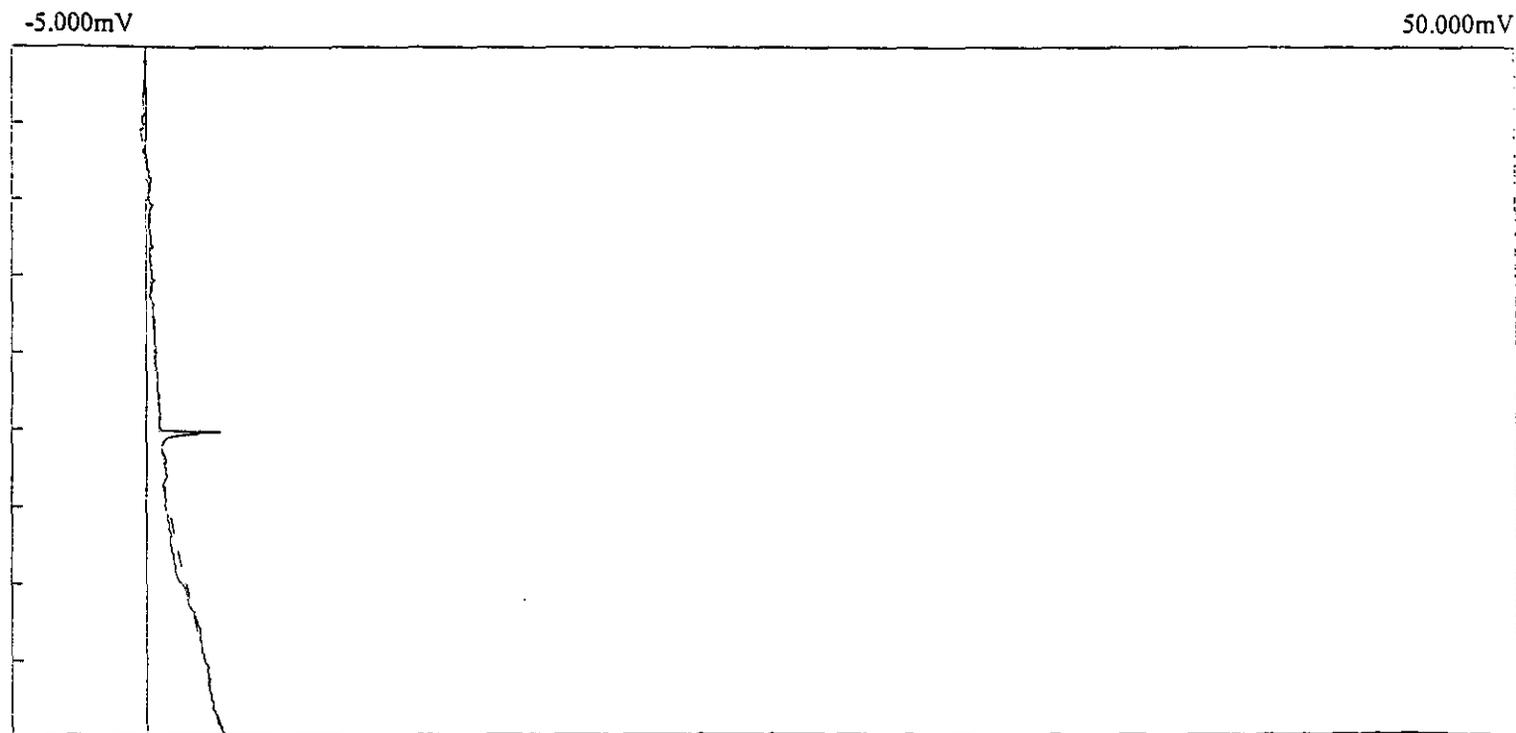
Client: Ladish Malting Co.
Client ID: J95.502AQ
Collected: 11/14/95
Analysis date: 11/17/1995 09:42:07
Method: Mod. USEPA Method 18
Description: Ch. 1 FMI-FID
Column: 3' Silica Gel
Carrier: N2 at 300 on dial
Temp. prog: FMI2.TEM
Components: FMI.CPT
Control file: DEFAULT.CON
Data file: N2BLNK2.CHR (c:\peakwin)
Sample: N2 Blank Run
Operator: Michael B. Weiner
Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention Area	External	Units
	0	0	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 09:59:17

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI2.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: N2BLNK3.CHR (c:\peakwin)

Sample: N2 Blank Run

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

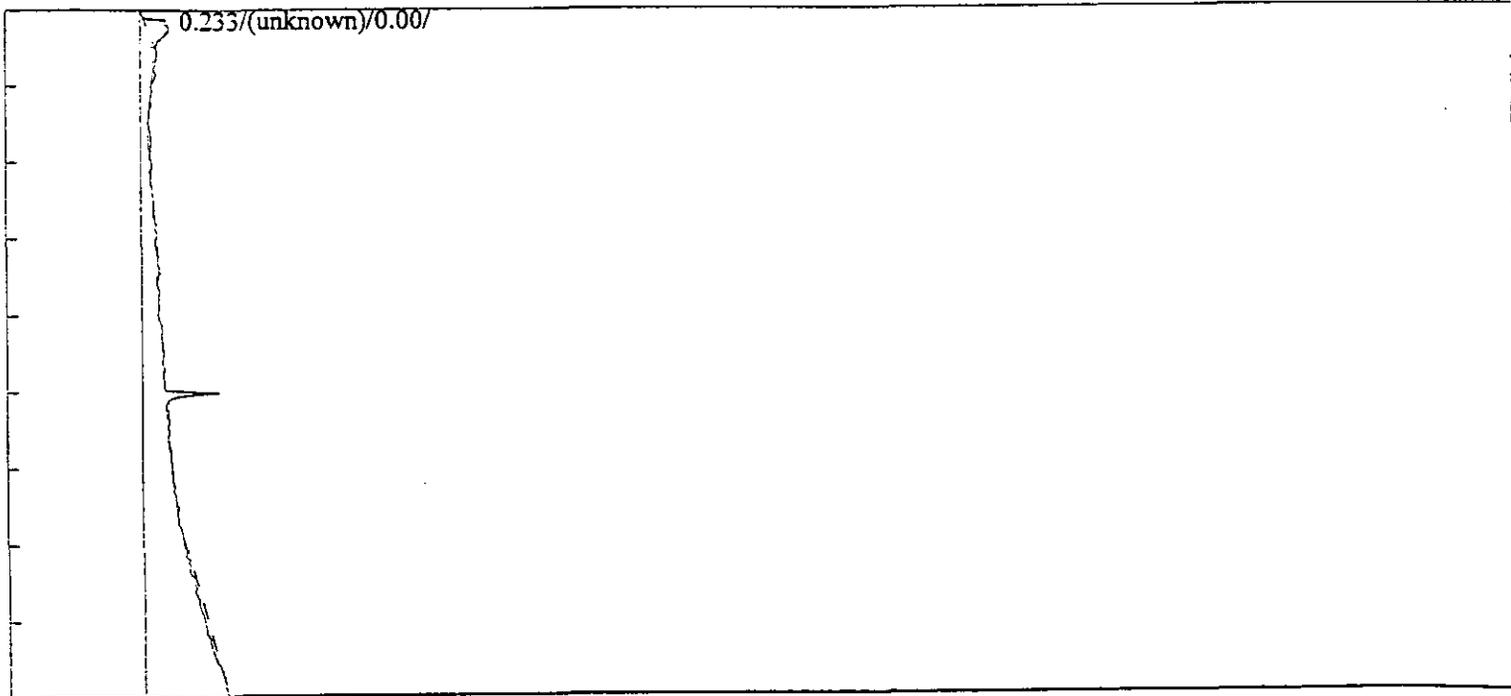
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
(unknown)	0.233	10.802	0.00	

11 -1

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 14:53:45

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: PROGLY2.CHR (c:\peakwin)

Sample: Propylene glycol

Operator: Michael B. Weiner

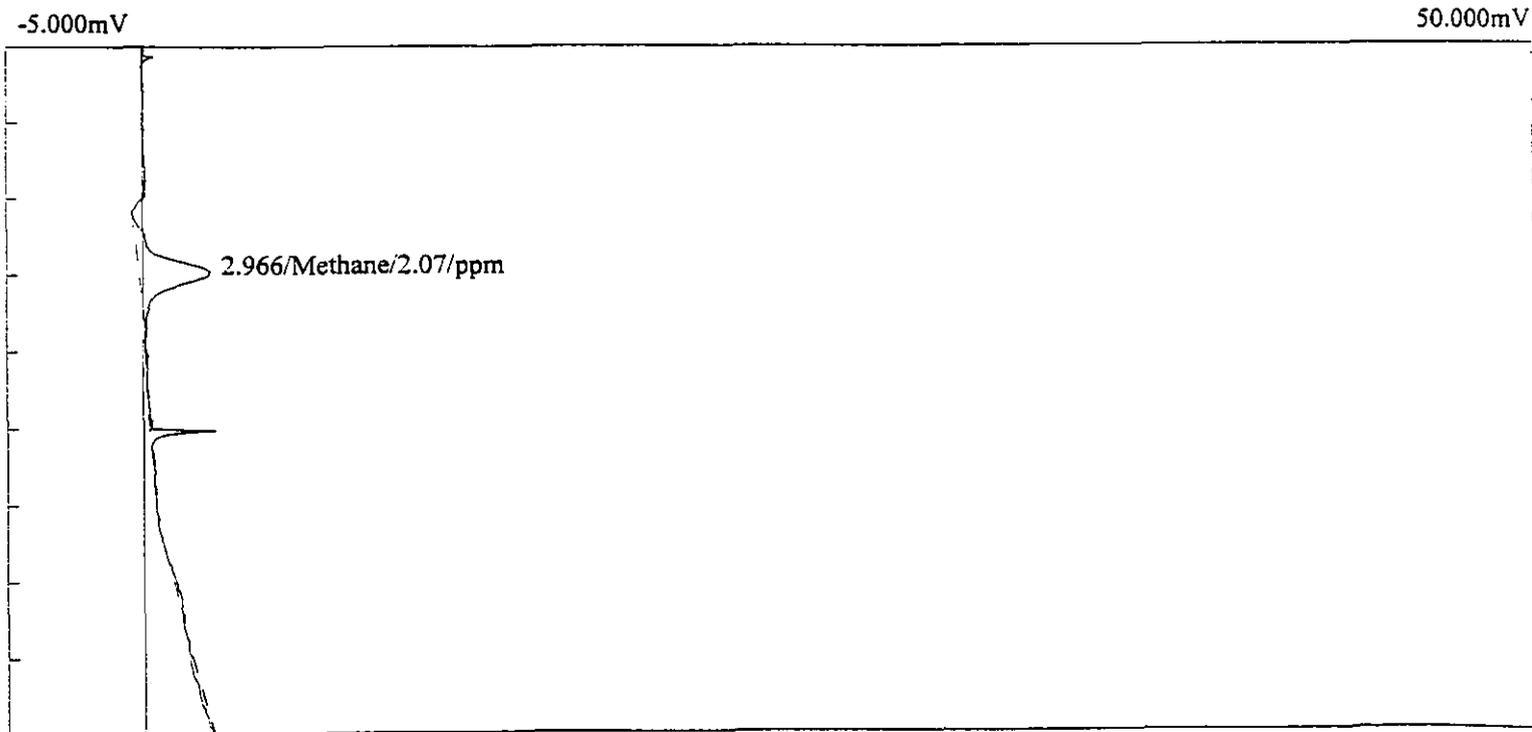
Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
Methane	2.966	66.124	2.07	ppm
		66	2	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 15:08:24

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: PROGLY3.CHR (c:\peakwin)

Sample: Propylene glycol

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

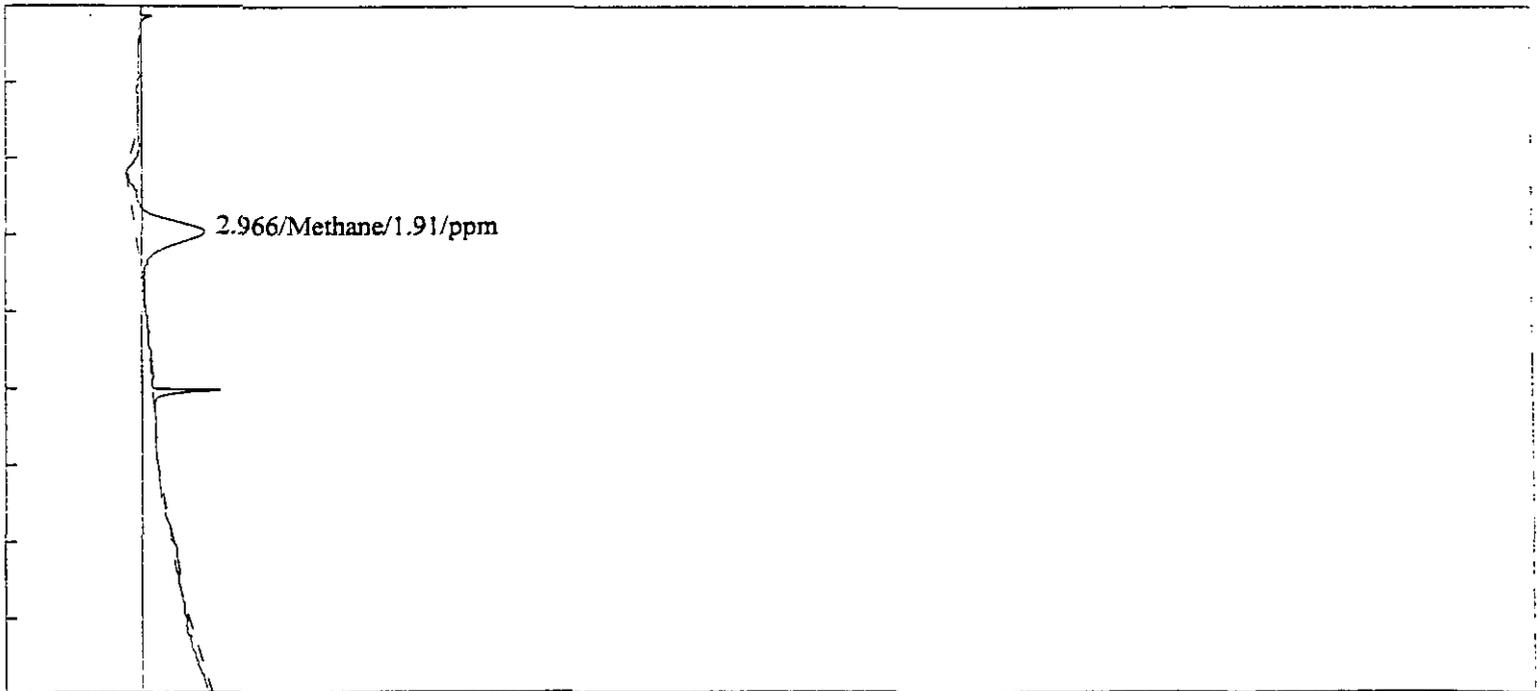
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Methane	2.966	61.022	1.91	ppm
		61	2	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 12:45:54

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI2.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: SULF2.CHR (c:\peakwin)

Sample: Burnt raw sulfur

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

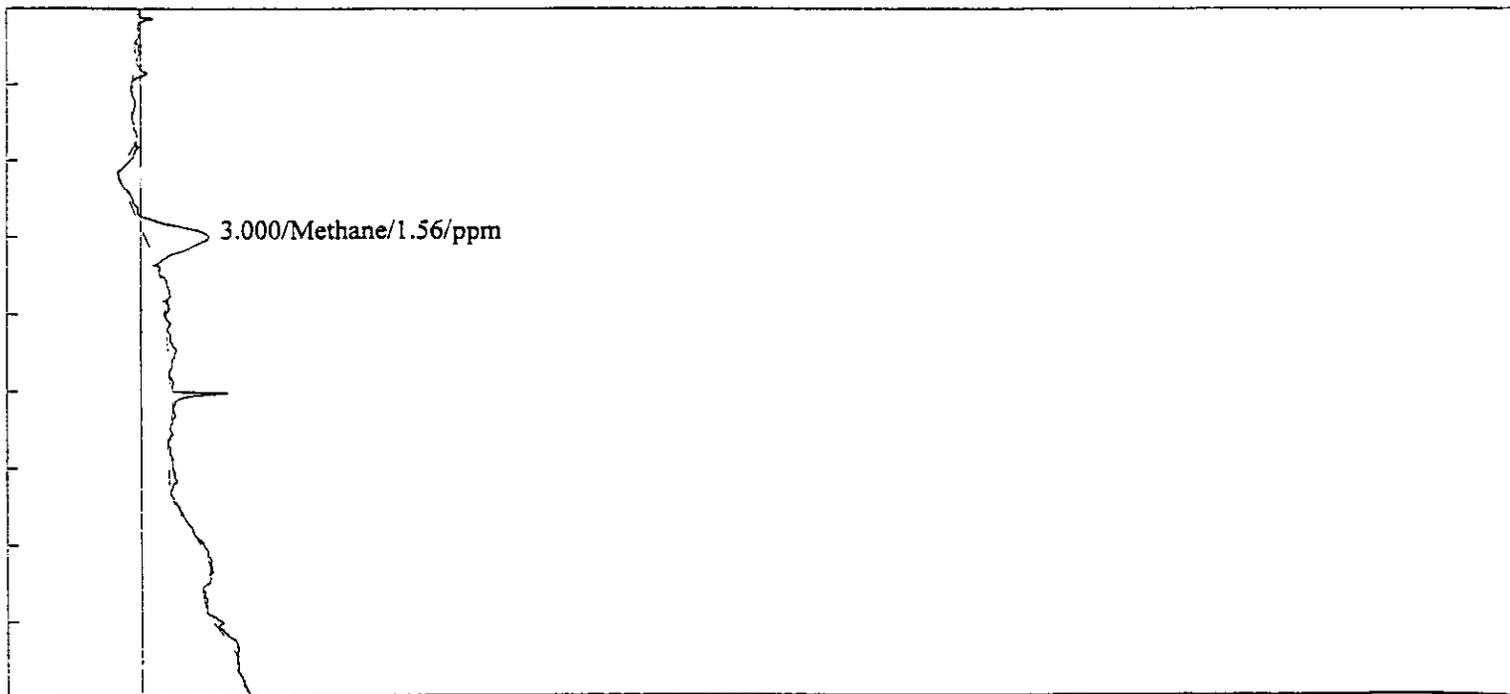
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Methane	3.000	49.832	1.56	ppm

50 2

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 12:59:06

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI2.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: SULF3.CHR (c:\peakwin)

Sample: Burnt raw sulfur

Operator: Michael B. Weiner

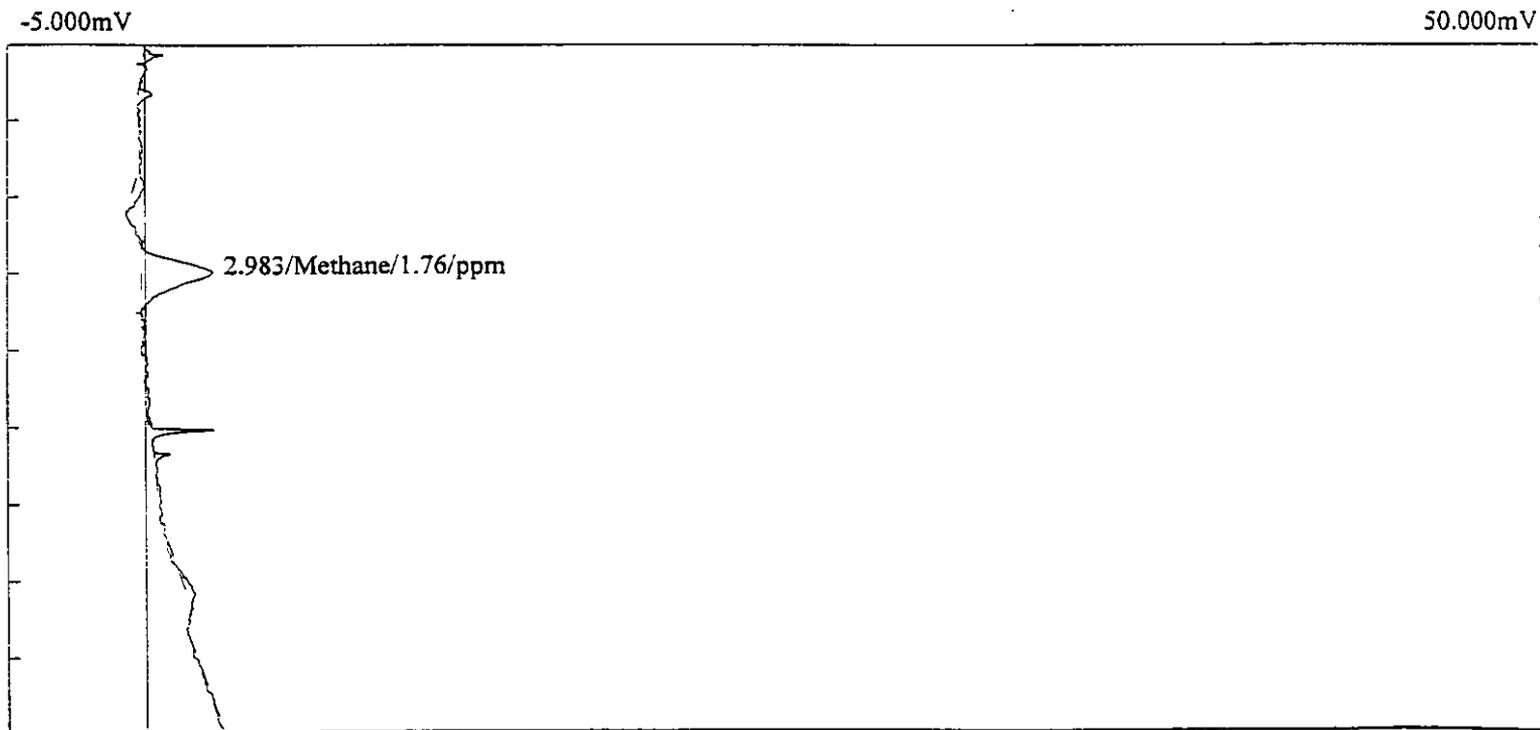
Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm



Component	Retention	Area	External	Units
Methane	2.983	56.250	1.76	ppm
		56	2	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 11:50:01

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI2.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: STD22.CHR (c:\peakwin)

Sample: Std 2 - 2.98ppm

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

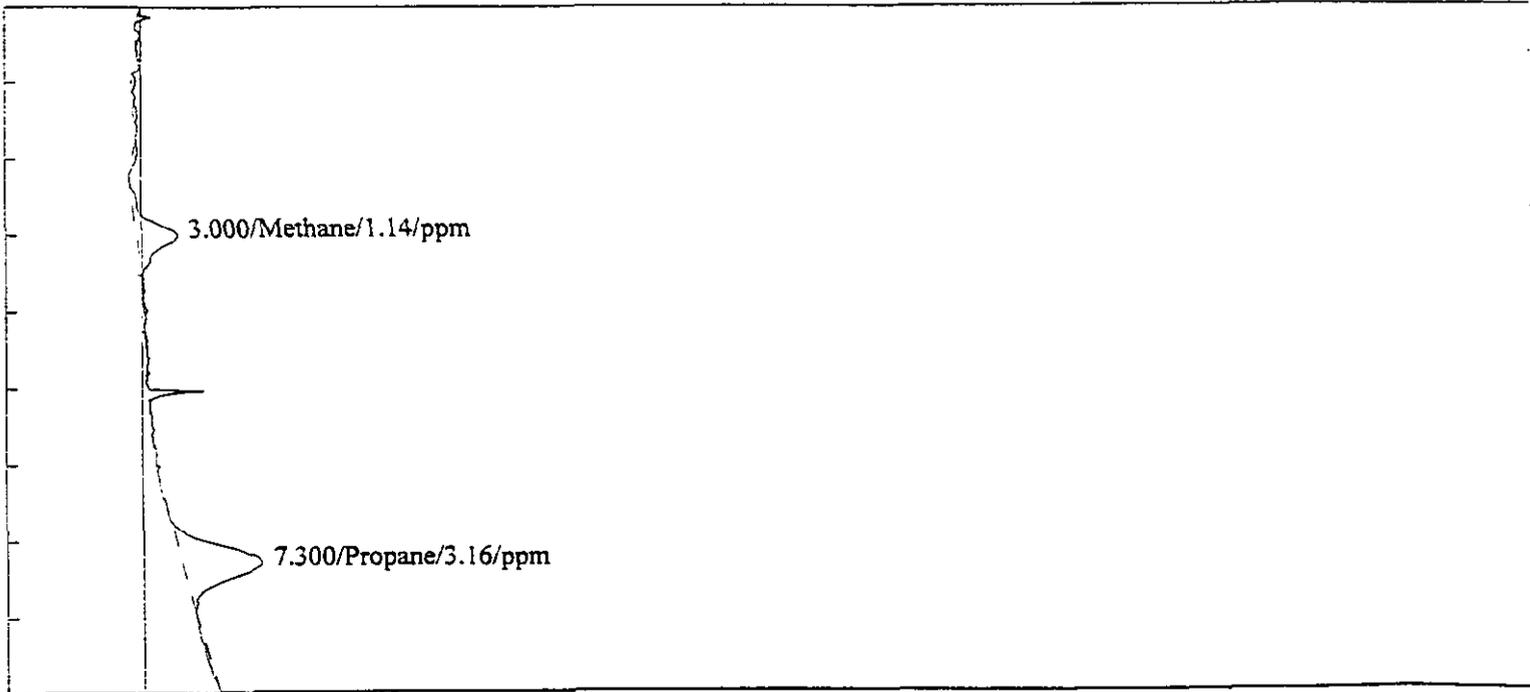
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Methane	3.000	36.491	1.14	ppm
Propane	7.300	83.112	3.16	ppm

120 4

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 12:03:23

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI2.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: STD23.CHR (c:\peakwin)

Sample: Std 2 - 2.98ppm

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

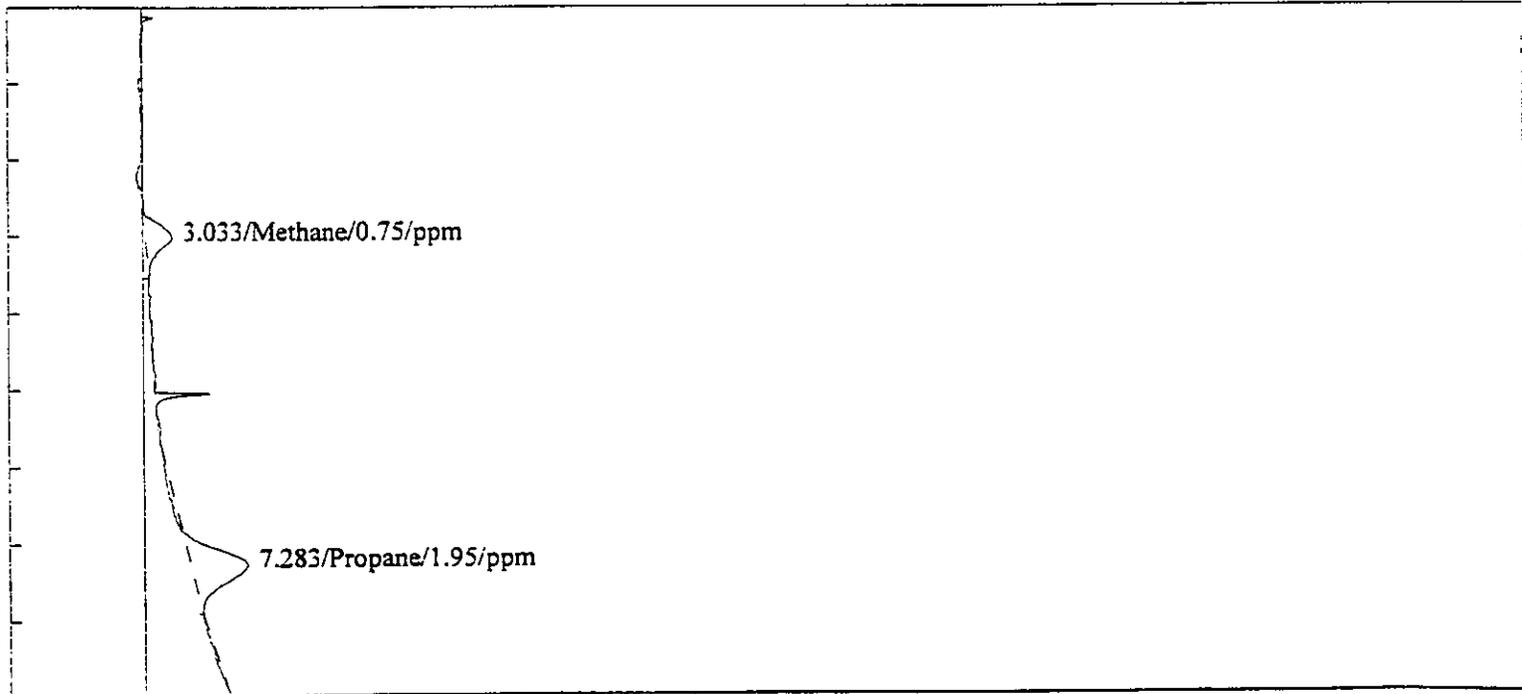
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Methane	3.033	23.822	0.75	ppm
Propane	7.283	51.289	1.95	ppm

75 3

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 12:16:38

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI2.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: STD24.CHR (c:\peakwin)

Sample: Std 2 - 2.98ppm

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

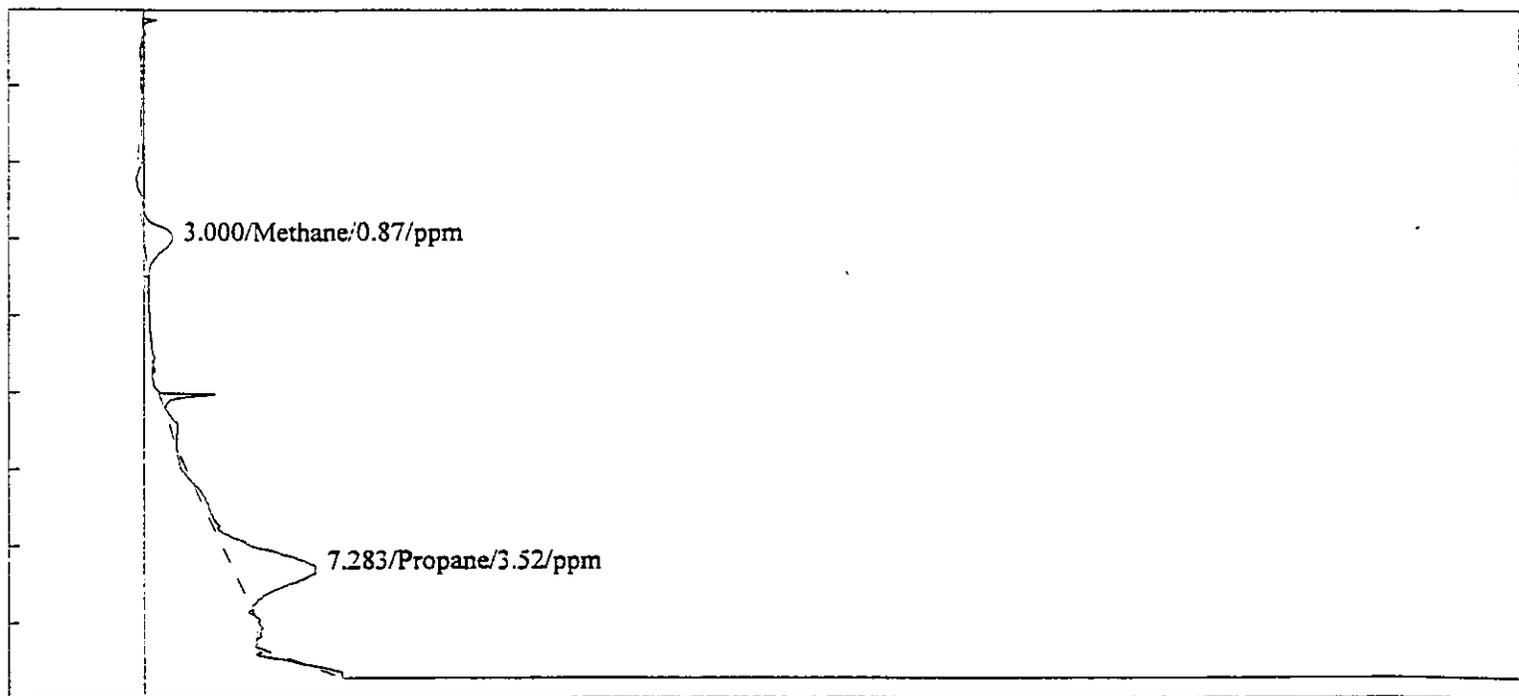
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Methane	3.000	27.614	0.87	ppm
Propane	7.283	92.669	3.52	ppm

120 4

Lab Name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 12:32:35

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI2.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: STD25.CHR (c:\peakwin)

Sample: Std 2 - 2.98ppm

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

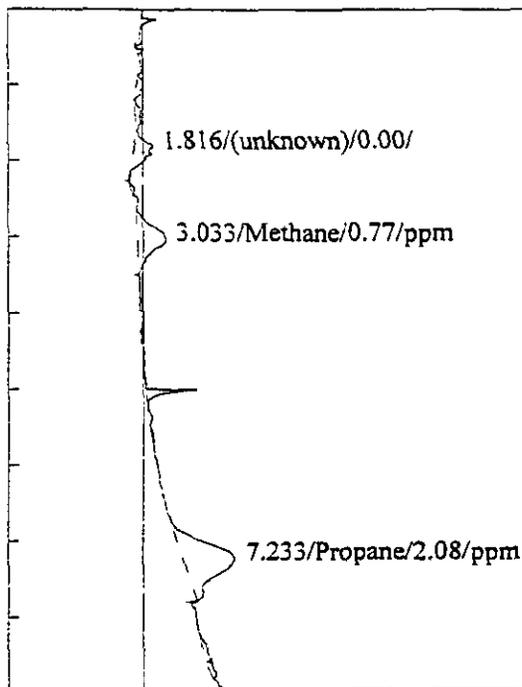
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
(unknown)	1.816	12.008	0.00	
Methane	3.033	24.493	0.77	ppm
Propane	7.233	54.809	2.08	ppm

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 10:41:47

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI2.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: STD13.CHR (c:\peakwin)

Sample: Std 1 - 5.91 ppm

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

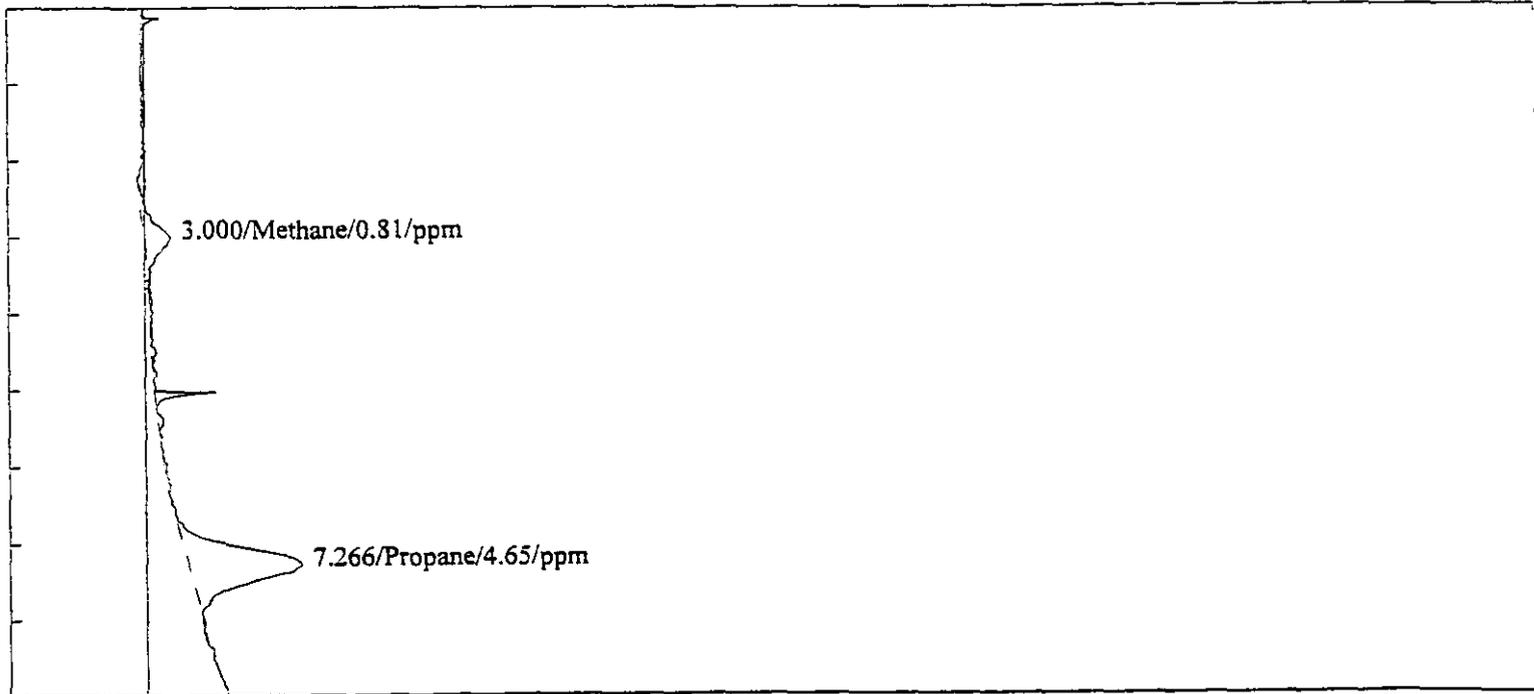
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
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Methane	3.000	25.921	0.81	ppm
Propane	7.266	122.220	4.65	ppm

148 5

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 10:54:46

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI2.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: STD14.CHR (c:\peakwin)

Sample: Std 1 - 5.91ppm

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

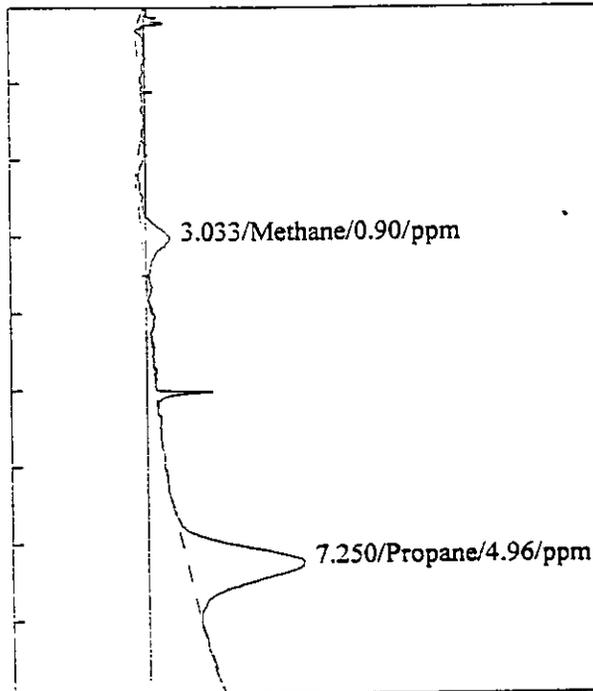
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Methane	3.033	28.789	0.90	ppm
Propane	7.250	130.344	4.96	ppm

159 6

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 11:09:15

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI2.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: STD15.CHR (c:\peakwin)

Sample: Std 1 - 5.91 ppm

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

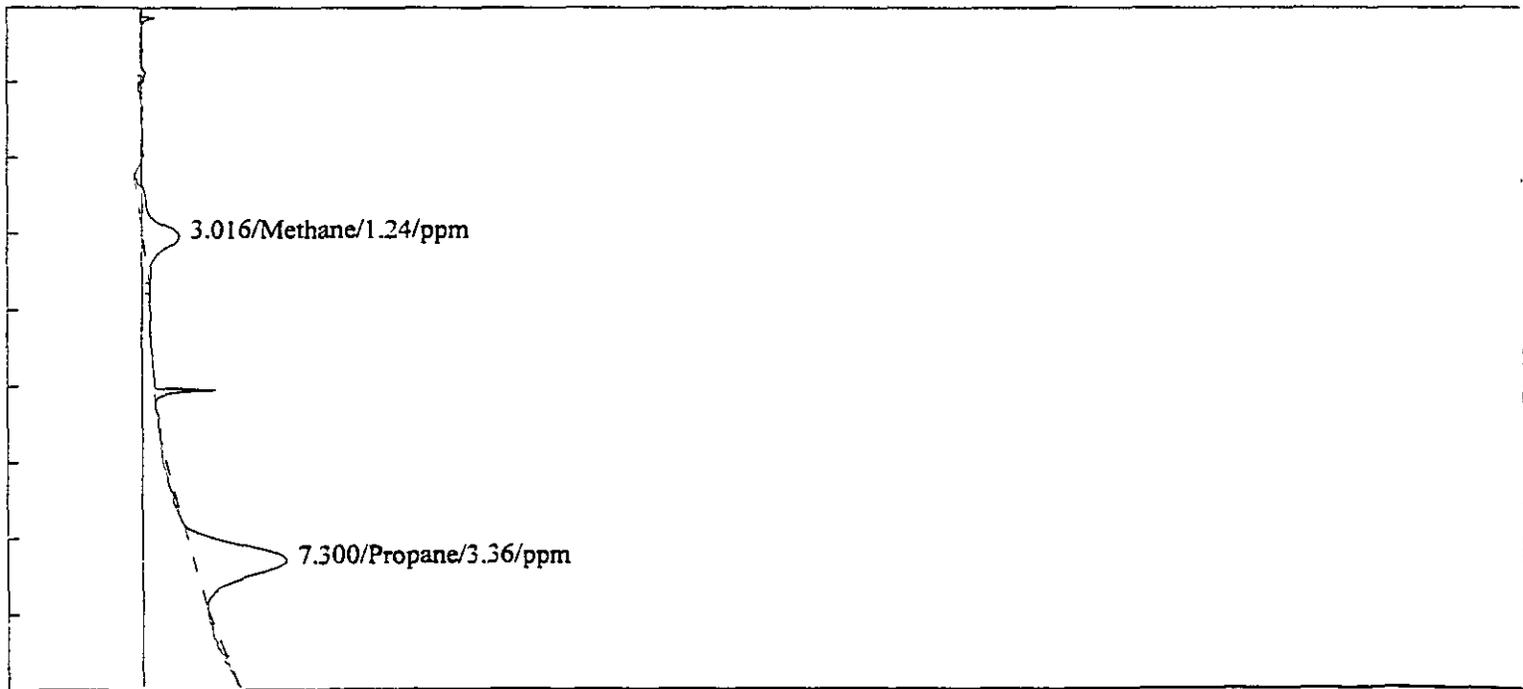
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Methane	3.016	39.430	1.24	ppm
Propane	7.300	88.446	3.36	ppm

128 5

Client: Laidish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/17/1995 11:23:20

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI2.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: STD16.CHR (c:\peakwin)

Sample: Std 1 - 5.91ppm

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

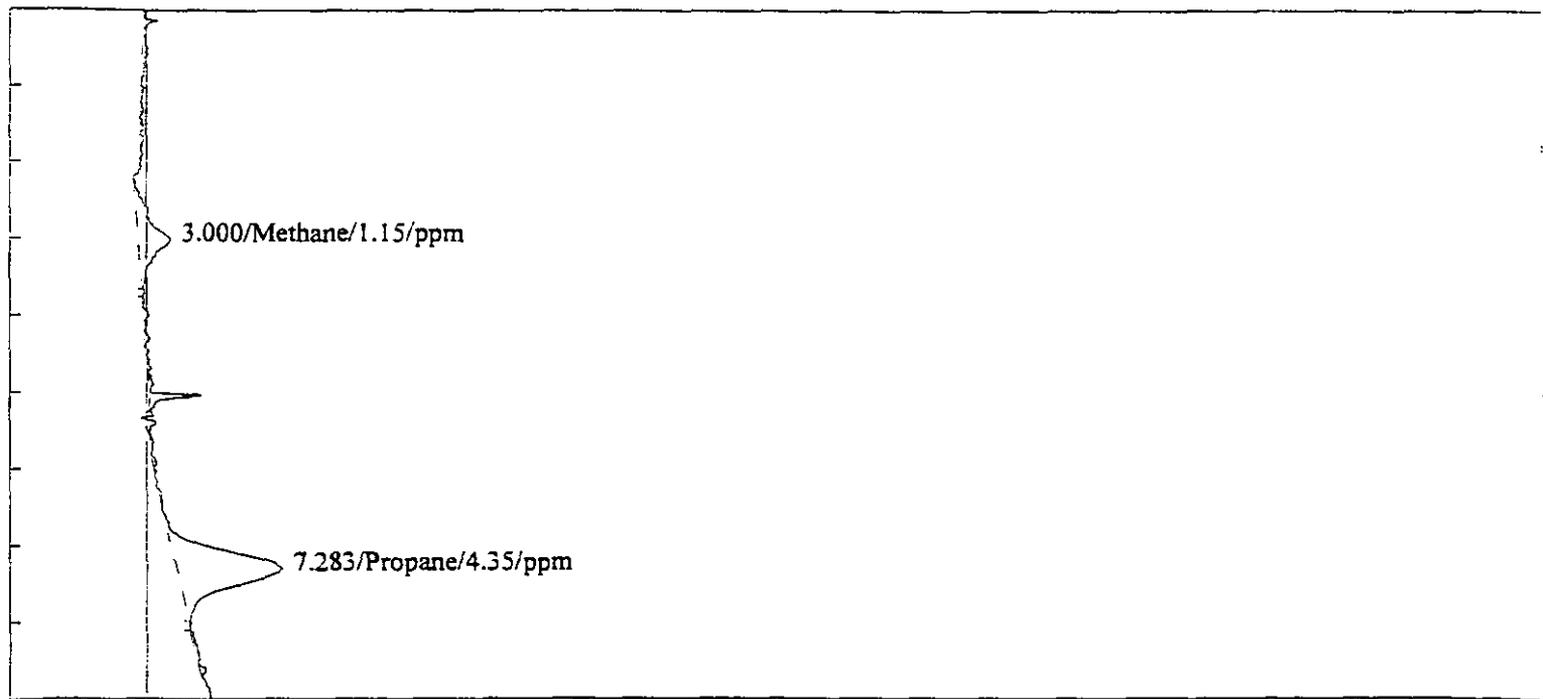
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Methane	3.000	36.698	1.15	ppm
Propane	7.283	114.420	4.35	ppm

151 6

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 17:45:00

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: C3H82.CHR (c:\peakwin)

Sample: C3H8 std

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

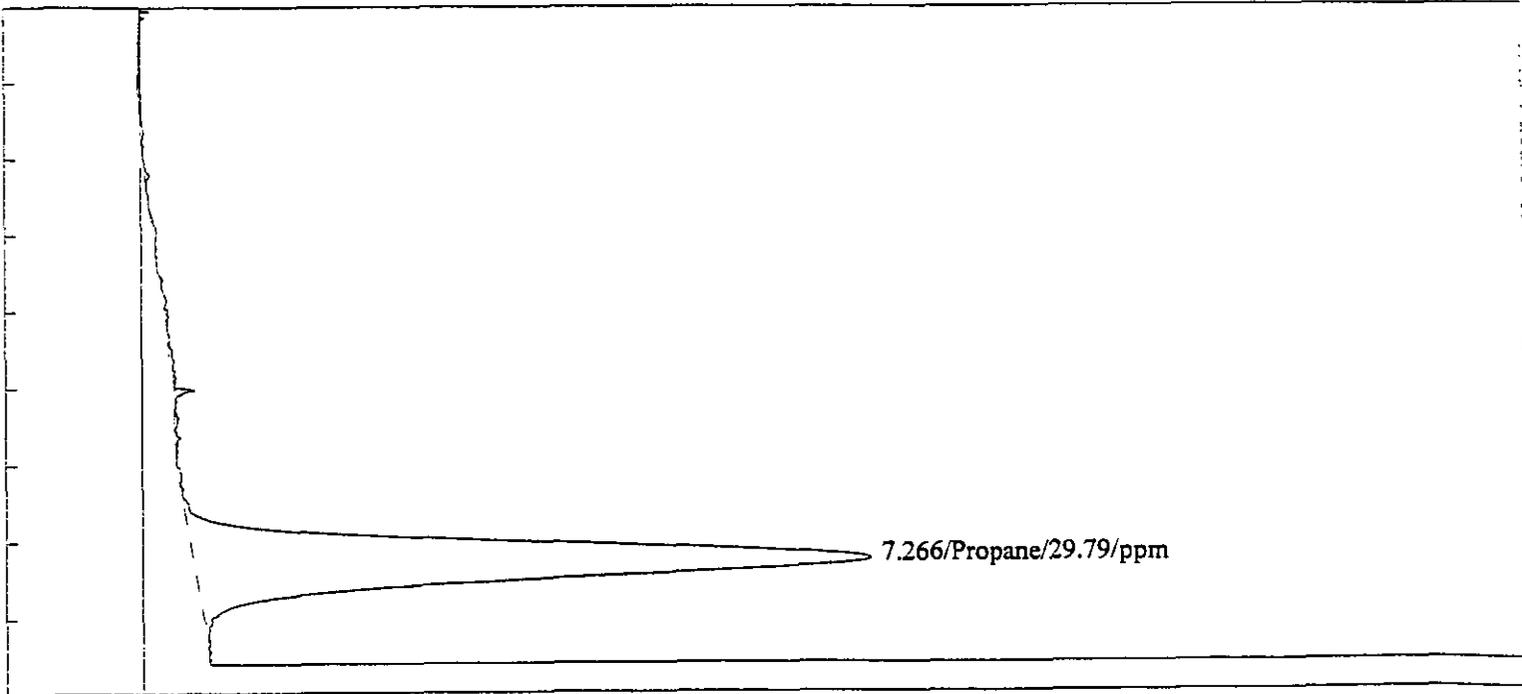
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Propane	7.266	783.254	29.79	ppm
		783	30	

Lab name: Fluid Management, Inc.

Client: Ladish Malting Co.

Client ID: J95.502AQ

Collected: 11/14/95

Analysis date: 11/14/1995 17:57:20

Method: Mod. USEPA Method 18

Description: Ch. 1 FMI-FID

Column: 3' Silica Gel

Carrier: N2 at 300 on dial

Temp. prog: FMI.TEM

Components: FMI.CPT

Control file: DEFAULT.CON

Data file: C3H83.CHR (c:\peakwin)

Sample: C3H8 std

Operator: Michael B. Weiner

Comments: 10-port Valco valve with 1.0 ml loop and backflush

Temperature program:

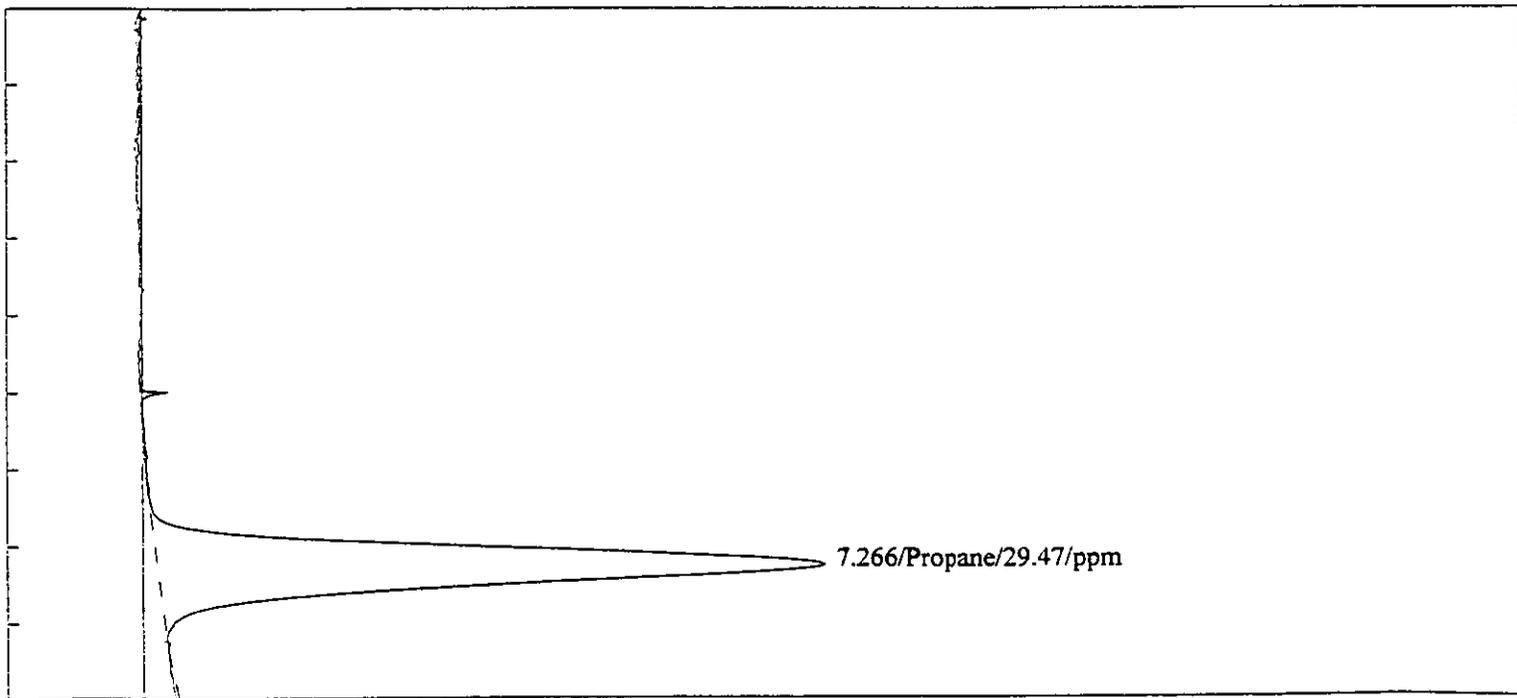
Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Components:

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

-5.000mV

50.000mV



Component	Retention	Area	External	Units
Propane	7.266	774.786	29.47	ppm
		775	29	

APPENDIX D

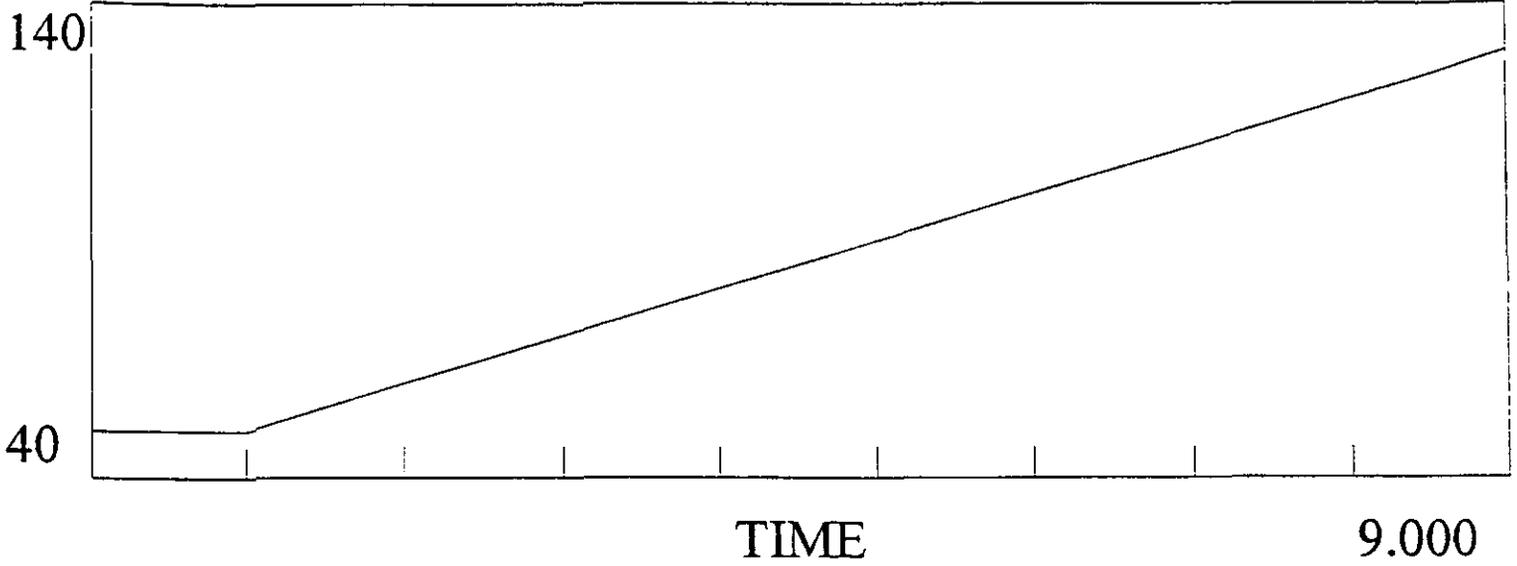
Calibration Data

Event file: FMI.EVT

Time	Event
0.000	ZERO
0.100	G ON (Load to Inject)
0.150	G OFF (Load to Inject)
5.000	H ON (Inject to Load)
5.100	H OFF (Inject to Load)
5.150	INTEG BASED

Temperature control file: FMI.TEM

TEMPERATURE

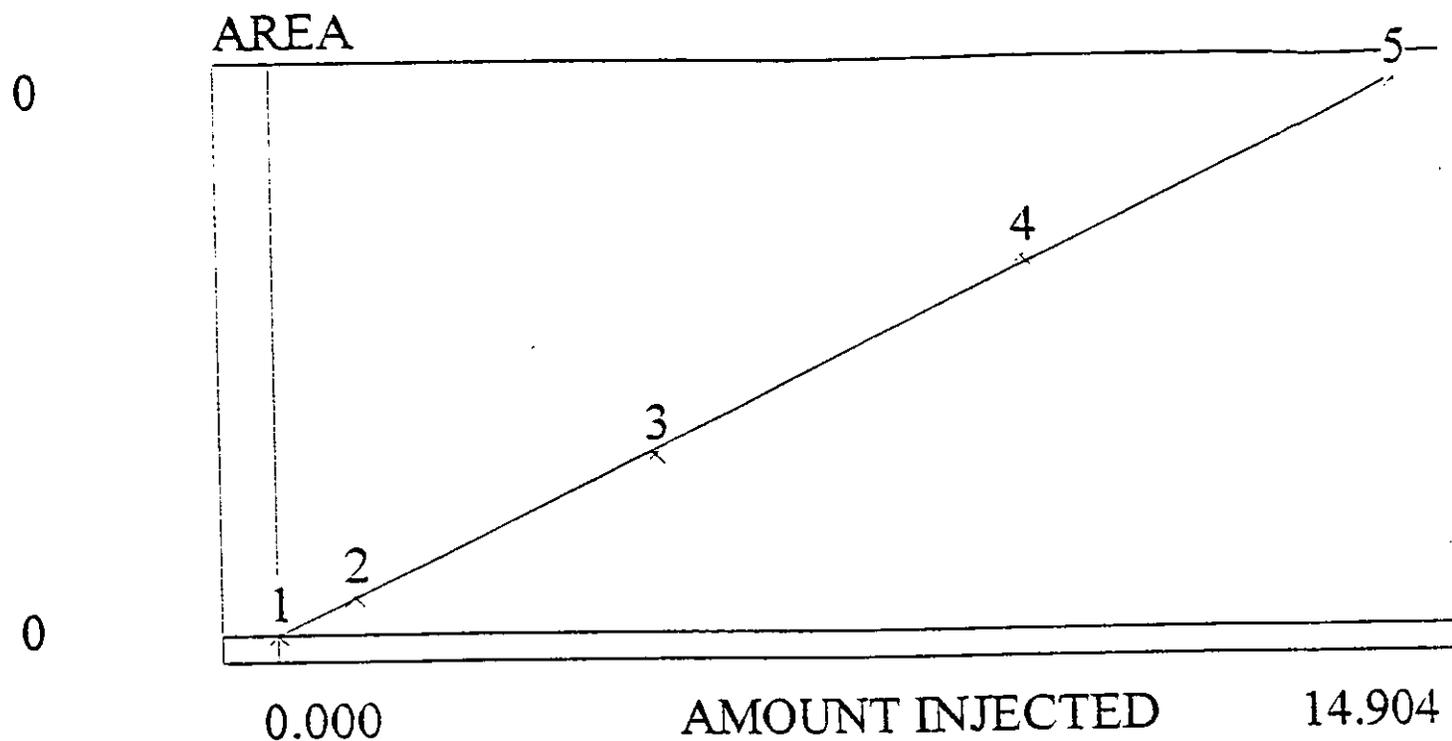


Init temp	Hold	Ramp	Final temp
50	1.000	10.000	130

Component file: FMI.CPT

PeakName	Start	End	Calibration	Int.Std	Units
1 Methane	2.850	3.150	CH4.CAL	0.000	ppm
2 Propane	7.150	7.450	C3H8.CAL	0.000	ppm

Calibration file: CH4.CAL



Avg slope of curve: 31.87

Y-axis intercept: 0.00

Linearity: 1.00

Number of levels: 5

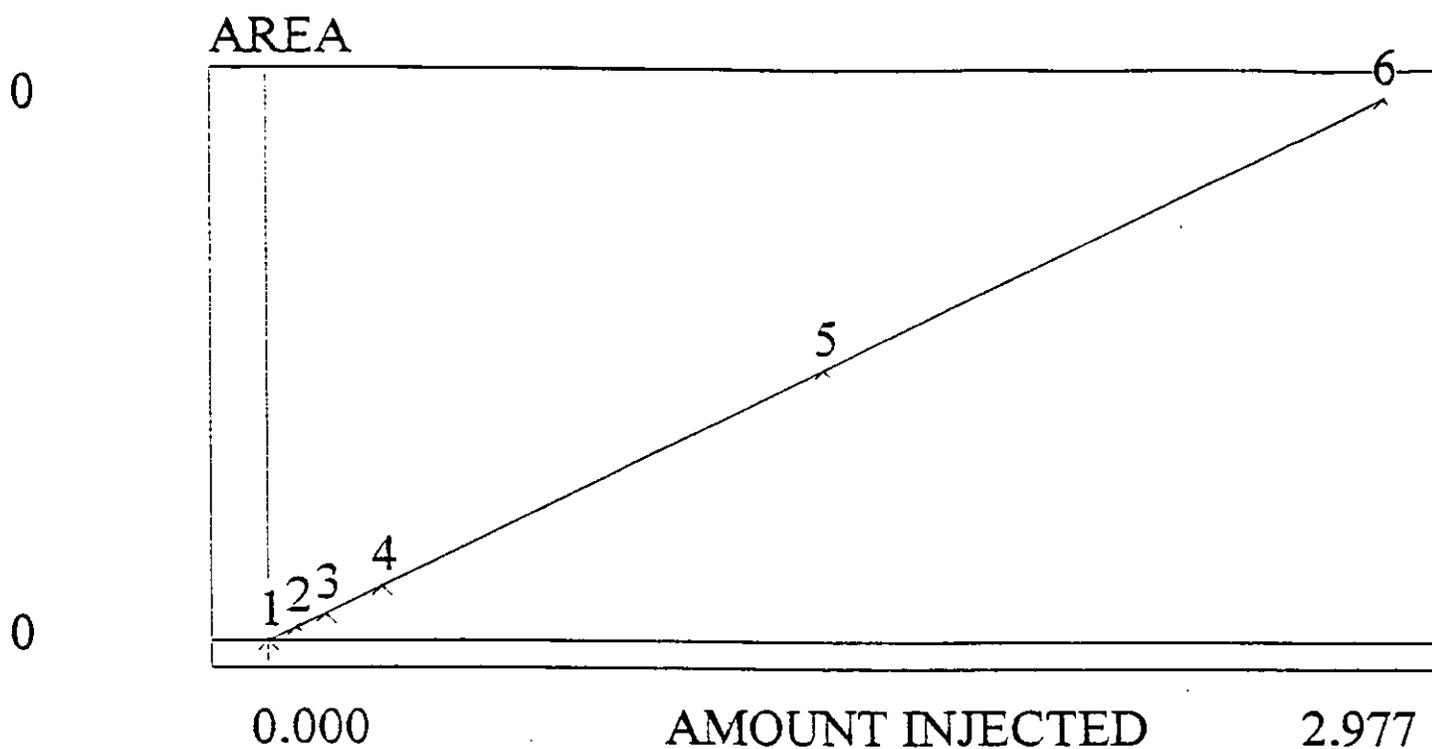
SD/rel SD of CF's: 14.3/56.0

$Y=0.0314X$

$r^2: 0.9996$

Lvl.	Area/ht.	Amount	CF
1	0.000	0.000	0.000
2	33.000	1.000	33.000
3	155.000	5.000	31.000
4	325.000	10.000	32.500
5	475.000	15.000	31.667

Calibration file: C3H8.CAL



Avg slope of curve: 26.29

Y-axis intercept: 0.00

Linearity: 1.00

Number of levels: 6

SD/rel SD of CF's: 10.8/49.0

$Y=0.0380X$

$r^2: 1.0000$

Lvl	Area/ht.	Amount	CF
1	0.000	0.000	0.000
2	1.975	0.074	26.689
3	3.920	0.149	26.309
4	7.825	0.298	26.258
5	39.160	1.489	26.300
6	78.250	2.978	26.276

APPENDIX E

Process Data

FAX Transmission

From: Gail A. Smith Ladish Malting Co.
Questions? Call 414-674-3730 N5355 Junction Road
Fax 414-674-6158 Jefferson, WI 53549
To: Michael Weiner
Company: Fluid Management, Inc.
Address: 250 E. Wisconsin, Ave.
Milwaukee, WI 53202

Date: November 16, 1995
Time: 4:32 PM Pages: 2 (including this one)

Message: Here is the data on average coil temperature and fan output for the period of time when you were measuring. If there is any other data you need to complete this project, please call.

MD

TEMPERATURES & FAN SPEEDS FOR 15 KILN

NOVEMBER 14 & 15, 1995 FROM 7 AM TO 7 AM

<u>TIME</u>	<u>AVG COIL TEMP.</u>	<u>% FAN OUTPUT</u>	<u>TIME</u>	<u>AVG COIL TEMP.</u>	<u>% FAN OUTPUT</u>
07:00 AM	134	60	19:30	134	70
07:30	134	60	20:00	160	30
08:00	120	100	20:30	170	30
08:30	125	100	21:00	185	30
09:00	125	100	21:30	188	30
09:30	110	65	22:00	188	30
10:00	139	65	22:30	188	30
10:30	133	65	23:00	187	35
11:00	134	65	23:30	189	35
11:30	134	65	00:00	188	35
12:00 PM	133	70	00:30	162	35
12:30	110	70	01:00 AM	92	50
13:00	120	75	01:30	91	50
13:30	134	75	02:00	85	65
14:00	134	85	02:30	130	65
14:30	134	85	03:00	132	65
15:00	133	90	03:30	133	65
15:30	133	95	04:00	133	65
16:00	133	100	04:30	133	65
16:30	132	100	05:00	133	65
17:00	132	100	05:30	133	65
17:30	111	100	06:00	133	65
18:00	120	80	06:30	106	65
18:30	137	70	07:00	98	65
19:00	134	70			

DRY CYCLE FOR 15 KILN 11/14-11/15

7000 BUSHEL ON EACH FLOOR-TWO FLOORS

UPPER FLOOR MALT GOES FROM 45-48 % MOISTURE TO 15-20 % DURING 24 HOURS

LOWER FLOOR MALT GOES FROM 15-20 % MOISTURE TO 3.5-4.3 % DURING 24 HOURS

7 AM TO 7:30 PM Holding heats

7:30-8:30 PM First high heat

8:30 PM to 12:30 AM Second high heats

12:30 AM to 1:00 AM Cool down

1:00 AM Kiln dumped

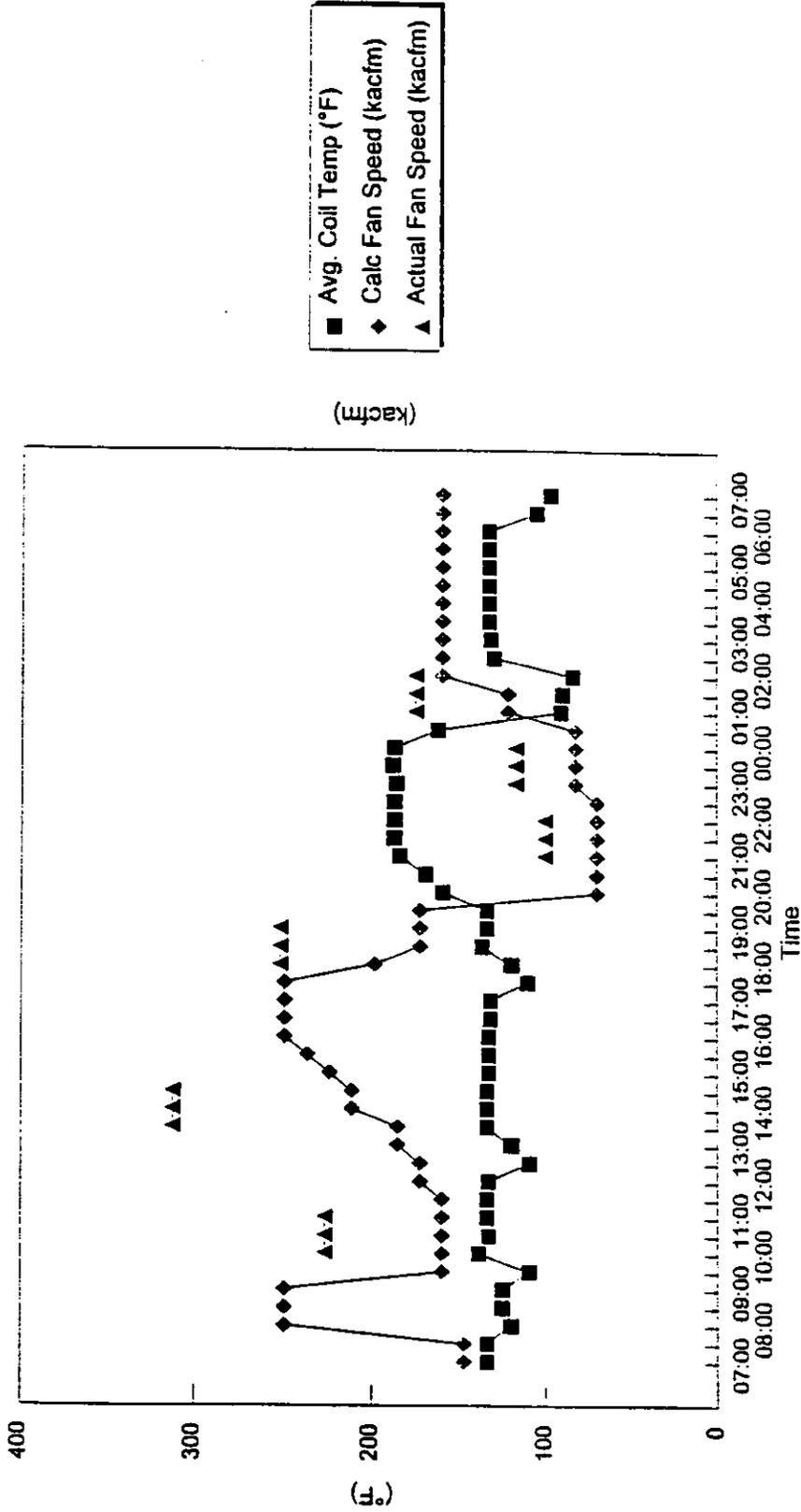
1:30-3:00 AM Upper floor is empty

3:30-5:00 AM Upper floor is being loaded

Note: At 1:00 AM the fans may have been off for 10-15 min. while the kiln floors were dumped

Ladish Malting Company

Temperatures and Fan Speeds for 15 Kiln



% Fan Output	Calculated acfm
100	250,000
90	226,000
80	197,000
70	174,000
60	146,000
50	123,000
40	96,200
30	70,543
20	44,886
10	19,229
0	0

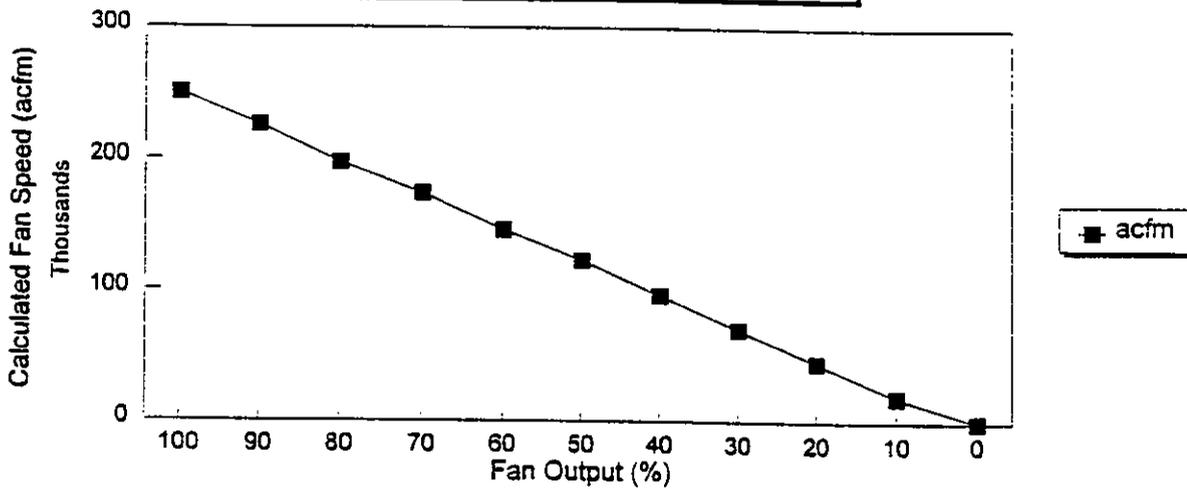
Regression Output:

Constant	-6428.57
Std Err of Y Est	1576.615
R Squared	0.999138
No. of Observations	6
Degrees of Freedom	4

X Coefficient(s)	2565.714
Std Err of Coef.	37.6883

$y = mx + b$

Ladish Malting Company
Fan Speed Calculation



APPENDIX F

Key Personnel

List of Personnel

Source Testing Personnel

Michael B. Weiner (FMI)

Jeffrey K. Anderson (FMI)

Plant Personnel

Roger Ziegler (Ladish Malting Company)

Gail Smith (Ladish Malting Company)

Regulatory Personnel

James Crawford (WDNR)