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Background Report Reference

AP-42 Section Number: 9.9.1

Background Report Section: 4

Reference Number: 59

**Title: Bay Area Area Quality Management
District, Summary of Source Test
Results**

Willowbrook Feeds, Petaluma, CA.

October 1995



BAY AREA AIR QUALITY MANAGEMENT DISTRICT

AP-42 Section 9.9.1
Reference
Report Sect. 4
Reference 59

December 19, 1995

Glenn Bach, Plant Manager
Willowbrook Feeds
40 N. Ely Road
P. O. Box 750818
Petaluma, California 94975-0818

Dear Mr. Bach:

Enclosed are the results of the source tests that this District conducted on your *Feed Pellet Cooler* on *October 26, 1995*.

These data are considered to be representative of the emissions from this source for the operating parameters described during the test times and are forwarded as a courtesy for your information.

Your cooperation with our Source Test personnel is appreciated. Please contact Ken Kunaniec, Air Quality Engineering Manager, if you have any questions regarding these data.

Sincerely,

Ellen J. Garvey
Director, Technical Services Division

EJG:KK:cm

Enclosure

DISTRIBUTION:

Firm
Permit Services
Enforcement
Technical Services
Planning
Requester
DAPCO

BAY AREA
AIR QUALITY MANAGEMENT DISTRICT
939 Ellis Street
San Francisco, California 94109
(415) 771-6000

Report No. 96069Test Date: 10/26/95

Test Times:

Run A: 1948 - 2102 (27 min)Run B: 2120 - 2213 (50 min)Run C: 2221 - 2301 (37 min)

SUMMARY OF SOURCE TEST RESULTS

SOURCE INFORMATION		BAAQMD REPRESENTATIVES
Firm Name and Address WILLOWBROOK FEEDS 40 N. Ely Road P. O. Box 750818 Petaluma, CA 94975-0818	Firm Representative and Title Glenn Bach, Plant Manager Phone No. (707) 792-9585	Source Test Engineers T. Underwood/H. Doi
Permit Conditions To be determined. A grain loading limit of 0.01 gr/SDCF has been proposed.	Source: Feed Pellet Cooler Abated by 3 Parallel Cyclones Plant No. 10292 Permit No. 14920 Operates On Demand between 7pm to 9am Batch	Permit Services Division / Enforcement Division Test Requested by: D. Singh, (Request)

Operating Parameters:

Plant produces chicken feed (pellets) between 22 to 27 tph. Different feed products were produced in batch sizes ranging from 4 to 27 tons. Products produced during these tests are identified in the supporting documentation to this report.

Applicable Regulations: Developmental Data

VN Recommended: NO

Source Test Results and Comments:

METHOD:	TEST	RUN A	RUN B	RUN C	AVERAGE	LIMIT
ST-17	Volume Flowrate, SDCFM	10,500	8,810	7,840	9,050	
	Stack Temperature, °F	108	128	134	124	
ST-23	Water Content, Volume %	8.2	13.4	17.0	12.8	
EPA-5	Particulate, gr/SDCF	0.004	0.004	0.005	0.004	0.010**
	Particulate, lb/hr	0.32	0.33	0.35	0.33	
	Isokinetic Ratio, act/theo	106%	52%*	103%		

Stack gas composition is the same as ambient air.

* Note: Plant operating conditions did not fully stabilize until Run C.

** Proposed grain loading emission limit.

NO COMMERCIAL USE OF THESE RESULTS IS AUTHORIZED

Air Quality Engineer II <i>T. Underwood</i> Date <u>11/15/95</u>	Supervising Air Quality Engineer <i>C. McClure</i> Date <u>11/15/95</u> C. McClure	Approved by Air Quality Engineering Manager <i>K. Kunaniec</i> Date <u>11/15/95</u> K. Kunaniec
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BAY AREA AIR QUALITY MANAGEMENT DISTRICT

939 Ellis Street San Francisco, California 94109

(415) 771-1000

Test Number: assign
Test Date: October 26, 1995

096069

DISTRIBUTION
Firm
Permit Services
Enforcement
Technical Services
Source Inventory
Requestor
D.A.P.C.O.Test Times:
Run A: 1948 to 2102 27 min
Run B: 2120 to 2213 50 min
Run C: 2221 to 2301 37 min

SUMMARY OF SOURCE TEST RESULTS

SOURCE INFORMATION

BAAQMD Representatives

Firm Name and Address	Representative and Title	Source Test Engineers
Willowbrook Feeds	Glenn Bach	Tim Underwood
40 N. Ely Rd.: POB 750818	plt mgr	Hiroshi Doi
Petaluma, CA 94975-0818	Phone No (707) 792-9585	
Plant No. 10292	Permit Services:	
Feed pellet cooler abated by 3 parallel cyclones		
Permit Conditions	Permit N 14920	Enforcement Division:
To be determined. A grainloading limit of 0.01 gr/SDCF has been proposed.		
Operating Parameters:	Operates: On demand between 7pm to 9am.	
Plant produces chicken feed (pellets) between 22 to 27 tph.	Batch	Test Requested By:
Different feed products were produced in batch sizes ranging from 4 to 27 tons.		D. Singh, (Request)
We tried to sample only during periods when actual product was in the pellet cooler.		
Products produced during these tests are identified in the supporting documentation to this report.		
Applicable Regulations: Developmental Data		VN Recommended? No

Test Results and Comments:

METHOD	TEST	RUN A	RUN B	RUN C	AVERAGE	LIMIT
ST-17	Volume Flowrate, SDCFM	10,500	8,810	7,840	9,050	
	Stack Temperature, F	108	128	134	124	
ST-23	Water Content, volume %	8.2	13.4	17.0	12.8	
EPA-5	Particulate, gr/SDCF	0.004	0.004	0.005	0.004	0.010**
	Particulate, lb/hr	0.32	0.33	0.35	0.33	
	Isokinetic Ratio, act/theo	106%	52% *	103%		

PLANT Stack gas composition is the same as ambient air.

* Note: ~~Operating conditions did not fully stabilize until run C. During the test there was much confusion which resulted in a 'sub-iso' sample for run B. The effect of sub-isokinetic sampling would be an apparent increase in mass rate emissions. The relative insensitivity to isokinetic conditions actually observed supports the view that the particulate is primarily submicron in size.~~

** Proposed grainloading emission limit.

NO COMMERCIAL USE OF THESE RESULTS IS AUTHORIZED

Source Test Team Leader
Tim Underwood
C McClure

Date

11/6/95

Approved-Chief of Source Test
Ken Kunaniec

CMB

Fixed Gases Results

Traverse	Run A	Run B	Run C
Oxygen, %	21.0	21.0	21.0
CO2, %	0.1	0.1	0.1
CO, ppmv	41	41	41
N2, %	79.0	79.0	79.0

Willowbrook Feeds

plt 10292

October 26, 1995

Source numbers not assigned yet

Run Data

Traverse	Run A	Run B	Run C
Ym	1.002	1.002	1.002
Cp, pitot constant	0.835	0.835	0.835
Dn, mm:Nozzle	6.21667	6.21667	4.45
An, ft^2:Nozzle	3.27E-04	3.27E-04	1.67E-04
Dstack, inches	29.5	29.5	29.5
Astack, ft^2	4.75	4.75	4.75
Pstd, in Hg	29.92	29.92	29.92
Pbar, in Hg	30.1	30.1	30.1
Pstatic, in H2O	0.5	0.5	0.5
Pstack, in Hg	30.14	30.14	30.14
del H, in H2O, mtr press cor	1.97	1.47	0.30
Pvacimp, in Hg	5.79	2.06	1.65
(del p)^.5avg	0.65	0.65	0.61
{(del p)^.5*cos(x)}avg	0.65	0.65	0.61
Tstd, R	530	530	530
Tstk, F	129.4	128.1	134.4
Tstk, R	567.8	587.7	594.0
Tm, R	533.3	533.5	534.0
Tsat, F: Impinger	43.6	41.1	40.1
Vm, meter vol CF	20.6	15.7	10.5
Vstd, SCF	20.731	15.758	10.496
Wsg, Saturated Imp H2O, gms	5.2	3.1	2.0
Vw, CF H2O, condensed and on dessicant	1.93	2.44	2.15
Bws, [lH2O], (trav uses run A)	0.082	0.134	0.170
1-Bws, [Dry gas]	0.918	0.866	0.830
Mwdry, g/g-mol	28.846	28.85	28.85
Mwwet, g/g-mol	27.436	27.39	27.01
Vs, wet, ft/sec actual	40.0	39.3	36.9
(Vs, wet*k), ft/sec actual ex vect	40.0	39.3	36.9
t, min: test time	27	50	37
Qstd, SDCFM	8990.248	10491	7840
Isokinetic Ratio, overall	106.3%	52.0%	102.6%

See sample calculation using Run A values, EQ1

See sample calculation using Run A values, EQ 2

See sample calculation using Run A values, EQ 3

See sample calculation using Run A values, EQ's 4,5,6,7

See sample calculation using Run A values, EQ 8

See sample calculation using Run A values, EQ 9

See sample calculation using Run A values, EQ 10

See sample calculation using Run A values, EQ11

See sample calculation using Run A values, EQ 12

See sample calculation using Run A values, EQ 13

Vs*k may differ from Vs if some points were traversed with a secondary pitot or there was cy

See sample calculation using Run A values, EQ 14

See sample calculation using Run A values, EQ 15

LAB RESULTS

Run A	Run B	Run C
Basis, (sample vlm)	20.731	15.758
Prorata del wt, gms	0	0
Prorated wt, gms	0.0000	0.0000
P&N&F weight, gms	0.0048	0.0044
Total wt gain, gms	0.0048	0.0044
G, gr/SDCF	0.0036	0.0043
M, lb/hr	0.32	0.33
Wc, Condenser Imp H2O, gms	35.5	48.3

See sample calculation using Run A values, EQ 16

See sample calculation using Run A values, EQ 17

Sample Calculations Using Run A Data

Willowbrook Feeds
plt 10292

October 26, 1995

Source numbers not assigned yet

EQ 1

Absolute Stack Pressure Equation

$$P_{stack} = P_{bar} + P_{static} / 13.6$$

$$P_{stack} = 30.10 + 0.5 / 13.6$$

$$P_{stack} = 30.14 \text{ in Hg}$$

EQ 2

Fundamental physical law, Conversion to absolute temperature, R (Rankine)

$$T, \text{ deg R} = T, \text{ deg F} + 459.6$$

$$T_{stk}, R = T_{stk}, F + 459.6$$

$$T_{stk}, R = 108.2 + 459.6$$

$$T_{stk}, R = 567.8$$

EQ 3

EPA Method 5, Eqtn 5-1, Dry gas volume corrected to standard conditions:

$$V_{std} = V_m * Y * (T_{std} / T_m) * (P_{bar} + (\Delta H) / 13.6) / P_{std}$$

$$V_{std} = 20.593 * 1.002 * (530 / 533.3) * [(30.10 + 1.97 / 13.6) / 29.92]$$

$$V_{std} = 20.731$$

Parametric Equation for Ppw calculates partial Pressure of H2O passing final knockout impinger at T_{sat}. Application of Henry's Law to determine Vwsg, water vapor volume, that is scrubbed out by silica gel just before meter quantifies dry gas volume. Constant from BAAQMD ST-23, Eqtn 9.2 converts gaseous H2O to grams, Wsg, and vice versa. Full equation cited in Bws calculation.

EQ 4

Parametric Eqtn

$$P_{pw} = (T_{sat} / 79.48)^3 - (T_{sat} / 115.34)^2 + (T_{sat} / 164.42) - (1 / 364)$$

$$P_{pw} = (43.6 / 79.48)^3 - (43.6 / 115.34)^2 + (43.6 / 164.42) - (1 / 364)$$

$$P_{pw} = 0.2842 \text{ in Hg}$$

EQ 5

Ppdry, partial pressure of dry gas in T_{sat} impinger is also calculated:

$$P_{pdry} = P_{bar} - P_{vacimp} - P_{pw}$$

$$P_{pdry} = 30.10 - 5.79 - 0.28$$

$$P_{pdry} = 24.022 \text{ in Hg}$$

One term from BAAQMD ST-23, Eqtn 9.2 and Henry's Law

EQ 6

$$V_{wsg} = V_{std} * (P_{pw} / P_{pdry})$$

$$V_{wsg} = 20.731 * (0.28 / 24.02)$$

$$V_{wsg} = 0.24527$$

One term from BAAQMD ST-23, Eqtn 9.2 and Henry's Law

EQ 7

$$W_{sg} = V_{wsg} / 0.0474$$

$$W_{sg} = 0.25 / 0.0474$$

$$W_{sg} = 5.17447 \text{ grams H}_2\text{O}$$

Constant from BAAQMD ST-23, Eqtn 9.2

EQ 8

$$V_w = 0.0474 * (W_c + W_{sg})$$

$$V_w = 0.0474 * (35.5 + 5.2)$$

$$V_w = 1.93 \text{ CF}$$

Constant from BAAQMD ST-23, Eqtn 9.2

EQ 9

EPA Method 4, Eqtn 4-4 or BAAQMD ST-23, Eqtn 9.2: Stack gas Moisture Content

$$Bws = (V_w + V_{wsg}) / (V_w + V_{wsg} + V_{std}) = V_w / (V_w + V_{std})$$

EPA 4-4

$$\% \text{H}_2\text{O} = 100\% * Bws = \frac{\{0.0474 * W_c + V_{std} * P_{pw} / (P_{bar} - P_{vacimp} - P_{pw})\}}{\{0.0474 * W_c + V_{std} * P_{pw} / (P_{bar} - P_{vacimp} - P_{pw})\} + V_{std}} = (V_w + V_{wsg}) / (V_w + V_{wsg} + V_{std})$$

$$\% \text{H}_2\text{O} = 100\% * Bws = \frac{\{0.0474 * W_c + V_{std} * P_{pw} / (P_{bar} - P_{vacimp} - P_{pw})\}}{\{0.0474 * W_c + V_{std} * P_{pw} / (P_{bar} - P_{vacimp} - P_{pw})\} + V_{std}} = (V_w + V_{wsg}) / (V_w + V_{wsg} + V_{std})$$

BAAQMD S-23, Eqtn 9.2

Sample Calculations Using Run A Data--Page 2

Both equations are presented here so that one can see their equivalence. Previously calculated intermediate values makes the use of EPA 4-4 more convenient and easier to follow.

$$\begin{aligned} Bws &= Vw / (Vw + Vstd) \\ Bws &= 1.93 / (1.93 + 20.73) \\ Bws &= 0.08509 = 8.2\% \end{aligned}$$

EQ 10

EPA Method 3, Eqn 3-2, Dry Molecular weight

$$\begin{aligned} Mwdry &= .44 * \%CO_2 + .32 * \%O_2 + .28 * (\%N_2 + \%CO) \\ Mwdry &= .44 * 0.1 + .32 * 21.0 + .28 * (79.0 + 0.0) \\ Mwdry &= 28.85 \text{ g/g-mol} \end{aligned}$$

EQ 11

EPA Method 2 Eqn 2-5, Wet molecular weight determination

$$\begin{aligned} Mwwet &= (1 - Bws) * Mwdry + 18 * Bws \\ Mwwet &= 0.918 * 28.85 + 18 * 0.082 \\ Mwwet &= 27.96 \text{ g/g-mol} \end{aligned}$$

EQ 12

BAAQMD ST-17, Eqn 8.2 and EPA Method 2, Eqn 2-9: Stack gas velocity

$$\begin{aligned} Vs, wet &= 85.49 * Cp * [(del p)^.5 \text{ avg}] * (Tstk / (Pstk * Mww))^{.5} \\ Vs, wet &= 85.49 * 0.84 * 0.729 * (567.8 / (30.14 * 27.96))^{.5} \\ Vs, wet &= 42.7 \text{ ft/sec} \end{aligned}$$

EQ 13

For Cyclonic flow exhaust calculations, del p root avg must be corrected by cosine of exhaust angle

$$\begin{aligned} Vs, wet * k &= 85.49 * Cp * [(del p)^.5 * \cos(x)] \text{ avg} * (Tstk / (Pstk * Mww))^{.5} \\ Vs, wet * k &= 85.49 * 0.84 * 0.729 * (567.8 / (30.14 * 27.96))^{.5} \\ Vs, wet * k &= 42.7 \text{ ft/sec} \end{aligned}$$

EQ 14

EPA Method 2, Eqn 2-10 and BAAQMD ST-17 Eqn 8.3: Stack Volume Flowrate, SDCFM

$$\begin{aligned} Qstd &= 60 * (1 - Bws) * (Vs, wet * k) * Astack * (Tstd / Tstk) * (Pstack / Pstd) \\ Qstd &= 60 * 0.918 * 42.7 * 4.75 * (530 / 568 * (30.14 / 29.92)) \\ Qstd &= 10491 \text{ SDCFM} \end{aligned}$$

EQ 15

EPA Equation 5-8 for overall Isokinetic rate determination:

$$\begin{aligned} I &= (Tstack * Vstd * Pstd * 100) / (Tstd * Vs, wet * \text{sample time} * An * Pstack * 60 * (1 - Bws)) \\ \text{Example from run A:} \\ I &= (567.8 * 20.731 * 29.92 * 100) / (530 * 42.7 * 27 * 3.27E-4 * 30.14 * 60 * 0.92) \\ I &= 106.3\% \end{aligned}$$

EQ 16

BAAQMD ST-15, Eqn 10.6, Grain Loading, gr/SDCF

$$\begin{aligned} G &= 15.43 * (\text{Weight Gain, gms}) / (Vstd) \\ G &= 15.43 * 0.0048 / 20.731 \\ G &= 0.004 \text{ gr/SDCF} \end{aligned}$$

Miscellaneous Emissions:

$$\begin{aligned} Mx &= 156E-6 * Mwx * Q * [X] \\ x &= [\text{species}] \\ Mwx &= [\text{molecular weight of } x, \text{ amu}] \\ [X] &= \text{concentration of } X, \text{ dry ppmv} \end{aligned}$$

EQ 17

BAAQMD ST-15, Eqn 10.7, Particulate Mass Emission Rate, lb/hr

$$\begin{aligned} M &= G * Qstd / 116.67 \\ M &= 0.004 * 10491 / 116.67 \\ M &= 0.32 \text{ lb/hr} \end{aligned}$$

Table of Nomenclature

Variable or constant	Units	Description
An	[=] ft^2	Nozzle Area
As or Astack	[=] ft^2	Stack Area
Bws	[=] CF H ₂ O/CF Gas	Water vapor fraction
Cp	[=] unitless	Pitot tube constant
Dn	[=] mm	Nozzle diameter
Ds or Dstack	[=] in	Stack diameter
G	[=] grain/SDCF	grain loading (per cubic foot)
del H or ΔH	[=] inches H ₂ O	Back pressure on the meter
I	[=] dimensionless or %	Ratio of actual to theoretical sample volumes
M	[=] lb/hr	Mass rate emissions
Mwdry	[=] amu	Molecular weight of dry stack gas
Mwwet	[=] amu	Molecular weight of wet stack gas
Pbar	[=] inches Hg	Barometric pressure
Ppdry	[=] inches Hg	Partial pressure of dry gas in final impinger
Ppw	[=] inches Hg	Partial pressure of water gas in final impinger
Ps or Pstack	[=] inches Hg	Absolute stack pressure
Pstd	[=] inches Hg	Average Ambient Air Pressure, defined at 29.92
Pstatic	[=] inches H ₂ O	Static gauge pressure of stack
Pvacimp	[=] inches Hg	Gauge vacuum at the saturated gas impinger, knockout before dessicant
del p or Δp	[=] inches H ₂ O	Velocity head as measured by pitot tube
Qstd	[=] SDCFM	Volumetric flow rate corrected to Pstd and Tstd
Tsat	[=] F or R	Temperature of gas saturated with water vapor
Tm	[=] F or R	Meter temperature
Tstk	[=] F or R	Stack Temperature
Tstd	[=] F or R	Standard temperature defined at 70 F or 530 R
t or At	[=] minutes	time between sample points or time of entire sample
Vm	[=] CF	meter reading or cumulative sample volume according to dry gas meter
Vstd	[=] SCF	sample volume corrected to standard temperature and pressure
Vw	[=] SCF	Water condensed and dessicated at Tstd and Pstd in the gaseous state
Vwc	[=] SCF	Water condensed at Tstd and Pstd in the gaseous state
Vwsg	[=] SCF	Water dessicated at standard temperature and pressure in the gaseous state
Vswet	[=] ft/sec	actual stack velocity
Vswet*k	[=] ft/sec	k vector component of actual stack velocity
Wc	[=] grams H ₂ O	Condensed water weight in the first two knockout impingers
Wsg	[=] grams H ₂ O	Scrubbed water weight on the silica gel or other dessicant
Ym	[=] dimensionless	meter calibration coefficient
13.6	[=] dimensionless	Ratio of liquid densities, Hg to H ₂ O: EQ's 1 and 3
.0474	[=] CF-H ₂ O/g-H ₂ O	Conversion factor at Tstd and Pstd: EQ's 7, 8 and 9
.44	[=] amu/%-CO ₂	Molecular Weight: EQ 10
.32	[=] amu/%-O ₂	Molecular Weight: EQ 10
.28	[=] amu/%-N ₂	Molecular Weight: EQ 10
.28	[=] amu/%-CO	Molecular Weight: EQ 10
18	[=] amu/H ₂ O	Molecular Weight: EQ 11
85.49	[=] $\text{ft/s}[\text{in Hg} \cdot \text{amu}]^{.5}$ [in H ₂ O * R]^{.5}	Pitot tube constant: EQ 12 and 13
60	[=] sec/min	Conversion factor: EQ 14 and 15
15.43	[=] gr/g	Conversion factor: EQ 16
116.67	[=] gr-hr/lb-min	Conversion factors 7000 gr/lb * 1hr/60-min: EQ 17

Notes for the particulate Spread sheet

- Note 1: The initial estimate of water content is the one parameter that most affects the final isokinetic ratio. The upper bound on stack $[H_2O]$ is the vapor pressure at T_{stk} . Additionally, the water in a stack is often a result of fuel combustion. $[H_2O]$ at T_{sat} is calculated according to the following parametric equation:

$$[H_2O] = (\exp(18.3036 - 3816.44 / (T_{sat} - 46.13))) / 7.6; \quad T [=] ^\circ R; \text{ atm}$$
 Stoichiometry of methane and air combustion was used to develop $[H_2O]$ based on $[CO_2]$:

$$[H_2O] = 2 / (.02 + 1 / [CO_2])$$
 Other methods for estimating water content may be available. An on-site evaluation is made to select the best guess. Final water content is calculated from the equation in BAAQMD ST-23-9.2:

$$B_{ws} = .0474 * W / (V_{std} + .0474 * W) * 100\%$$
 B_{ws} is the water vapor percentage, wet basis. W is the weight in grams of water condensed during sampling and that which is adsorbed in the desiccant after passing through the final knockout impinger.
- Note 2: These pre-test calculations of gas velocity at the nozzle help ensure that the selected nozzle will cover the entire range of stack gas velocities. EPA equations 2-9 and 2-10 calculate stack gas velocity and volumetric flow rate. For stacks with cyclonic flow, it is necessary to include the factor $\cos(\text{angle of egress})$ for the exhaust vector component. Calculation of the nozzle velocity can not include this cosine factor. Instead, the sample time at each traverse point is adjusted by this cosine factor in order to maintain representative sampling criteria at each traverse point.

$$v_{s,wet} = 85.49 c_p (\Delta p)^{.5} (T_s / (P_s M_{wwet}))^{.5} \cos(x); \text{ ft/sec}$$

$$Q_{std} = 60 A_s V_s (1 - B_{ws}) (P_s / P_{std}) (T_{std} / T_s); \text{ SDCFM; referenced to } P_{std} \text{ and } T_{std}$$
 Additionally, the relationship between wet and dry gas velocity or volumetric flow is given by:

$$v_{s,dry} = (1 - B_{ws}) v_{s,wet}; \quad Q_{s,dry} = (1 - B_{ws}) Q_{s,wet}$$

$$\Delta t_i = \cos(x_i) * \text{basic time interval}$$
- Note 3: Method ST-18-3.2 specifies the number of traverse points and their location. Stacks less than 12 inches in diameter require 4 traverse points per diameter; up to 20 Inch $D \Rightarrow 6$ pts
 < 30 in $D \Rightarrow 8$ pts; < 48 in $D \Rightarrow 10$ pts; > 48 in $D \Rightarrow 12$ pts
 The radial location of traverse point "i" in duct of radius "R" with a total of "2a" points per diameter is:

$$r_i = R((i - .5) / a)^{.5}$$

PLANT DATA Willowbrook Feeds
 Address 40 N. Ely Rd.: POB 750818
 City, Zip Petaluma, CA 94975-0818
 Date: October 26, 1995
 Permit No 14920
 Request by? D. Singh
 CDS,NSR,NESHAPS? Request
 Test Engineer Tim Underwood
 Technician Hiroshi Doi

Contact: Glenn Bach
 Title plt mgr
 Phone (707) 792-9585
 Plant no. 10292
 Test No. assign
 Source: Source numbers not assigned yet
 (source de Feed pellet cooler abated by 3 parallel cyclones)

Willowbrook Feeds
 plt 10292
 October 26, 1995
 Source numbers not assigned yet

Operates: On demand between 7pm to 9am.
 Batch

Common Regulation references:

Reg 2-1-307 Failure to Meet Permit Con
 Reg 2-2-x NSR permit conditions
 Reg 6-310 Particulate grainloading
 Reg 6-311 Particulate mass rate

Applicable Regulations

ton/hr

cap Reg 6 cap, lb/hr

40 37.31 = 4.1*(ton processed/hr)^0.67 = 4.1*27.0^0.67

Permit Conditions:

To be determined

xxxxxxx 35minutes of broiler grower # M7

xxxxxxx 1.5 hr of range starter # M 6430N

xxxxxxx 1 hr of range grower # M6442DC

Plant produces chicken feed (pellets) between 22 to 27 tph.

Different feed products were produced in batch sizes ranging from

We tried to sample only during periods when actual product was in

Products produced during these tests are identified in the supporting documentation to this

Used: T=traverse, S=sample

Calibration Date

6/27/95

0.86

0.00

0.00

0.84

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

Meter Y value

Imp Code: S

Initial Filter

368

Calibrated: February 1, 1998

Have @.5 CFM 1.867

Traverse

0.855

Run A

30.1

0.5

30.14

0.5

30.14

0.5

30.14

0.5

30.14

0.5

Sample

0.835

Run B

30.1

0.5

30.14

0.5

30.14

0.5

30.14

0.5

30.14

0.5

30.14

0.5

30.14

Stack id [in]

29.50

Run C

Stack Area [ft2]

4.75

Run D

Stack Area [ft2]

4.75

Run E

Stack Area [ft2]

4.75

Run F

Stack Area [ft2]

4.75

Run G

Stack Area [ft2]

Willowbush Feeds

plit 10292
 October 26, 1995
 Source numbers not assigned yet
 Filter ID 369
 Impingers S3 and S4
 Temperat Digttemp No 1
 Pressure Digital Manometer
 Train=Probe>Filter>Imp S3>Imp S4>pump box #80631

not

simpld

Van but 1120

lmp	l2	lmp	trav	EQ 3	imp
-----	----	-----	------	------	-----

Temp	Vac	Vac	del p	sdef	gram
10	0.000	0.000	0.000	0.000	0.000
20	0.000	0.000	0.000	0.000	0.000
30	0.000	0.000	0.000	0.000	0.000
40	0.000	0.000	0.000	0.000	0.000
50	0.000	0.000	0.000	0.000	0.000
60	0.000	0.000	0.000	0.000	0.000
70	0.000	0.000	0.000	0.000	0.000
80	0.000	0.000	0.000	0.000	0.000
90	0.000	0.000	0.000	0.000	0.000
100	0.000	0.000	0.000	0.000	0.000

40	5.0	2.6	1.158	0.2
40	5.0	2.6	1.158	0.2

41	5.0	2.5	1.135	0.2

41	5.5	2.4	1.126	0.2
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Case	Time (h)	Time (min)	Time (s)
1	41	4.0	2.3
2	41	4.0	2.3
3	41	4.0	2.3
4	41	4.0	2.3
5	41	4.0	2.3
6	41	4.0	2.3
7	41	4.0	2.3
8	41	4.0	2.3
9	41	4.0	2.3
10	41	4.0	2.3
11	41	4.0	2.3
12	41	4.0	2.3
13	41	4.0	2.3
14	41	4.0	2.3
15	41	4.0	2.3
16	41	4.0	2.3
17	41	4.0	2.3
18	41	4.0	2.3
19	41	4.0	2.3
20	41	4.0	2.3
21	41	4.0	2.3
22	41	4.0	2.3
23	41	4.0	2.3
24	41	4.0	2.3
25	41	4.0	2.3
26	41	4.0	2.3
27	41	4.0	2.3
28	41	4.0	2.3
29	41	4.0	2.3
30	41	4.0	2.3
31	41	4.0	2.3
32	41	4.0	2.3
33	41	4.0	2.3
34	41	4.0	2.3
35	41	4.0	2.3
36	41	4.0	2.3
37	41	4.0	2.3
38	41	4.0	2.3
39	41	4.0	2.3
40	41	4.0	2.3
41	41	4.0	2.3
42	41	4.0	2.3
43	41	4.0	2.3
44	41	4.0	2.3
45	41	4.0	2.3
46	41	4.0	2.3
47	41	4.0	2.3
48	41	4.0	2.3
49	41	4.0	2.3
50	41	4.0	2.3
51	41	4.0	2.3
52	41	4.0	2.3
53	41	4.0	2.3
54	41	4.0	2.3
55	41	4.0	2.3
56	41	4.0	2.3
57	41	4.0	2.3
58	41	4.0	2.3
59	41	4.0	2.3
60	41	4.0	2.3
61	41	4.0	2.3
62	41	4.0	2.3
63	41	4.0	2.3
64	41	4.0	2.3
65	41	4.0	2.3
66	41	4.0	2.3
67	41	4.0	2.3
68	41	4.0	2.3
69	41	4.0	2.3
70	41	4.0	2.3
71	41	4.0	2.3
72	41	4.0	2.3
73	41	4.0	2.3
74	41	4.0	2.3
75	41	4.0	2.3
76	41	4.0	2.3
77	41	4.0	2.3
78	41	4.0	2.3
79	41	4.0	2.3
80	41	4.0	2.3
81	41	4.0	2.3
82	41	4.0	2.3
83	41	4.0	2.3
84	41	4.0	2.3
85	41	4.0	2.3
86	41	4.0	2.3
87	41	4.0	2.3
88	41	4.0	2.3
89	41	4.0	2.3
90	41	4.0	2.3
91	41	4.0	2.3
92	41	4.0	2.3
93	41	4.0	2.3
94	41	4.0	2.3
95	41	4.0	2.3
96	41	4.0	2.3
97	41	4.0	2.3
98	41	4.0	2.3
99	41	4.0	

41	4.0	2.0	0.952	0.2
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41	4.0	2.0	0.936	0.2
41	4.0	2.0	0.957	0.2

Case	Time	Time	Time
1	4.0	2.0	0.95
2	4.0	2.0	0.95
3	4.0	2.0	0.95
4	4.0	2.0	0.95
5	4.0	2.0	0.95
6	4.0	2.0	0.95
7	4.0	2.0	0.95
8	4.0	2.0	0.95
9	4.0	2.0	0.95
10	4.0	2.0	0.95
11	4.0	2.0	0.95
12	4.0	2.0	0.95
13	4.0	2.0	0.95
14	4.0	2.0	0.95
15	4.0	2.0	0.95
16	4.0	2.0	0.95
17	4.0	2.0	0.95
18	4.0	2.0	0.95
19	4.0	2.0	0.95
20	4.0	2.0	0.95
21	4.0	2.0	0.95
22	4.0	2.0	0.95
23	4.0	2.0	0.95
24	4.0	2.0	0.95
25	4.0	2.0	0.95
26	4.0	2.0	0.95
27	4.0	2.0	0.95
28	4.0	2.0	0.95
29	4.0	2.0	0.95
30	4.0	2.0	0.95
31	4.0	2.0	0.95
32	4.0	2.0	0.95
33	4.0	2.0	0.95
34	4.0	2.0	0.95
35	4.0	2.0	0.95
36	4.0	2.0	0.95
37	4.0	2.0	0.95
38	4.0	2.0	0.95
39	4.0	2.0	0.95
40	4.0	2.0	0.95
41	4.0	2.0	0.95
42	4.0	2.0	0.95
43	4.0	2.0	0.95
44	4.0	2.0	0.95
45	4.0	2.0	0.95
46	4.0	2.0	0.95
47	4.0	2.0	0.95
48	4.0	2.0	0.95
49	4.0	2.0	0.95
50	4.0	2.0	0.95
51	4.0	2.0	0.95
52	4.0	2.0	0.95
53	4.0	2.0	0.95
54	4.0	2.0	0.95
55	4.0	2.0	0.95
56	4.0	2.0	0.95
57	4.0	2.0	0.95
58	4.0	2.0	0.95
59	4.0	2.0	0.95
60	4.0	2.0	0.95
61	4.0	2.0	0.95
62	4.0	2.0	0.95
63	4.0	2.0	0.95
64	4.0	2.0	0.95
65	4.0	2.0	0.95
66	4.0	2.0	0.95
67	4.0	2.0	0.95
68	4.0	2.0	0.95
69	4.0	2.0	0.95
70	4.0	2.0	0.95
71	4.0	2.0	0.95
72	4.0	2.0	0.95
73	4.0	2.0	0.95
74	4.0	2.0	0.95
75	4.0	2.0	0.95
76	4.0	2.0	0.95
77	4.0	2.0	0.95
78	4.0	2.0	0.95
79	4.0	2.0	0.95
80	4.0	2.0	0.95
81	4.0	2.0	0.95
82	4.0	2.0	0.95
83	4.0	2.0	0.95
84	4.0	2.0	0.95
85	4.0	2.0	0.95
86	4.0	2.0	0.95
87	4.0	2.0	0.95
88	4.0	2.0	0.95
89	4.0	2.0	0.95
90	4.0	2.0	0.95
91	4.0	2.0	0.95
92	4.0	2.0	0.95
93	4.0	2.0	0.95
94	4.0	2.0	0.95
95			

41	4.0	2.0	0.925	0.2
41	4.0	2.0	0.925	0.2

[illegible][illegible][illegible]

Time (min)	Flow rate (L/min)	Pressure (bar)
40	3.0	0.000
40	3.0	0.923
40	3.0	0.0

Case	Age	Sex	Duration	Site	Pathologic	Response	Survival
1	41	F	4.0	2.0	0.984	0.2	0.2
2	41	F	4.0	2.0	0.984	0.2	0.2

Case	Age	Sex	Duration	Site	Pathologic	Response	Survival
1	41	M	3.5	2.0	0.925	0.2	0.2

42	3.5	2.0	0.960	0.2
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41	3.5	1.8	0.949	0.2
----	-----	-----	-------	-----

41	3.5	1.8	0.948	0.2
----	-----	-----	-------	-----

42	3.5	2.0	0.924	0.2
----	-----	-----	-------	-----

42	3.5	2.0	0.951	0.2
----	-----	-----	-------	-----

Country	Percentage (%)
Argentina	85
Brazil	75
Chile	65
Colombia	60
Costa Rica	55
Ecuador	50
El Salvador	45
Guatemala	40
Honduras	35
Mexico	30
Nicaragua	25
Panama	20
Paraguay	15
Peru	10
Uruguay	10
Venezuela	80

Age group	Number of cases
0-14	0.000
15-24	0.000
25-34	0.000
35-44	0.000
45-54	0.000
55-64	0.000
65-74	0.000
75-84	0.000
85-94	0.000
95-104	0.000

Age Group	Percentage of Respondents
18-29	0.75
30-49	0.85
50-69	0.90
70+	0.95

Age Group	Percentage of Respondents
18-29	75.0
30-49	85.0
50-69	90.0
70+	95.0

Case	Age	Sex	Duration (yr)	Onset (yr)	Family history	Pathologic findings	Response to treatment	Outcome
1	41	F	2.06	15.758	3.1			

Sample Form - Run C

Cal gases
Oxygen, %
CO₂, %
CO, ppmv
Nitrogen, %
Initial H₂O guess
H₂O from KO imps
H₂O from T_{sat} imp
H₂O vapor volume
EPA method 4 H₂O
Run C Int'l Lk Chk at 28.5"Hg 368.315-322/.5=014 CFM
Run C Final L Chk at 28.5"Hg 379.105-115=.010 CFM

Span Strip Chart
Response
Span Response
20.95 84 84
15 59.5 0.2
1190 58 2
15.0
43.3
2.0
2.1
17.0
Run C max H₂O vap pres
H₂O--run C, %
Mwdry
Mwvel

Order and Direction of Traverse:
W then S ports ----- in to out
W then S ports end time 2301
in to out end time 2301

W then S ports start ti 2221
in to out start time
Basic time interval, minut 2.50
Cp= 0.835

Initialization	Tpt	Cyclo	Ang	Time	del p	T _{sat}	M	E	T	V _{lm}	R	Imp	Imp	not	H ₂ O	sat	iso	Probe	Filt
1	0	0	0	2.50	0.38	118	74	0.281	368.432	0.32	39	3.5	1.8	0.729	0.1	0.24	102.07%	249	227
2	0	0	0	5.00	0.40	125	74	0.287	369.160	0.33	39	3.5	1.8	0.743	0.1	0.24	102.08%	252	242
3	0	0	0	7.50	0.37	134	74	0.274	370.610	0.30	40	3.5	1.8	0.709	0.1	0.25	102.07%	243	245
4	0	0	0	10.00	0.39	134	74	0.281	371.338	0.32	40	3.5	1.8	0.728	0.1	0.25	102.07%	247	246
5	0	0	0	12.50	0.40	135	74	0.284	372.074	0.33	40	3.5	1.8	0.737	0.1	0.25	102.07%	253	245
6	0	0	0	15.00	0.39	136	74	0.280	372.800	0.32	39	3.5	1.8	0.727	0.1	0.24	102.07%	246	245
7	0	0	0	17.50	0.35	136	74	0.266	373.488	0.29	39	3.0	1.5	0.689	0.1	0.24	102.06%	253	242
8	0	0	0	20.00	0.35	137	74	0.265	374.175	0.28	40	3.0	1.5	0.688	0.1	0.25	102.06%	255	246
0	0	0	0	20.00				0.000	374.175	0.00			0.0	0.000	0.0	0.00	0.00%		
0	0	0	0	20.00				0.000	374.175	0.00			0.0	0.000	0.0	0.00	0.00%		
0	0	0	0	20.00				0.000	374.175	0.00			0.0	0.000	0.0	0.00	0.00%		
0	0	0	0	20.00				0.000	374.175	0.00			0.0	0.000	0.0	0.00	0.00%		
1	0	0	0	22.50	0.38	136	74	0.277	374.892	0.31	40	3.5	1.8	0.718	0.1	0.25	102.07%	247	240
2	0	0	0	25.00	0.38	137	74	0.277	375.608	0.31	40	3.5	1.8	0.717	0.1	0.25	102.07%	242	246
3	0	0	0	27.50	0.40	136	74	0.284	376.343	0.33	41	3.5	1.8	0.736	0.1	0.26	102.07%	254	244
4	0	0	0	30.00	0.36	135	74	0.270	377.041	0.29	41	3.5	1.8	0.699	0.1	0.26	102.07%	247	245
5	0	0	0	32.50	0.33	135	74	0.258	377.710	0.27	41	3.5	1.8	0.669	0.1	0.26	102.06%	255	244
6	0	0	0	35.00	0.33	136	74	0.258	378.378	0.27	41	3.5	1.8	0.669	0.1	0.26	102.06%	250	243
7	0	0	0	37.00	0.33	140	74	0.257	378.910	0.27	41	3.5	1.8	0.533	0.1	0.26	102.06%	250	243
8	0	0	0	37.00	0.33	140	74	0.257	378.915	0.27	41			0.005	0.0	0.26	#DIV/0!		
0	0	0	0	37.00				0.000	378.915	0.00			0.0	0.000	0.0	0.00	0.00%		
0	0	0	0	37.00				0.000	378.915	0.00			0.0	0.000	0.0	0.00	0.00%		
0	0	0	0	37.00				0.000	378.915	0.00			0.0	0.000	0.0	0.00	0.00%		
0	0	0	0	37.00				0.000	378.915	0.00			0.0	0.000	0.0	0.00	0.00%		
Averages				37	0.366	134	74		10.483	0.30	40		1.65	10.496	2.0	0.00	102.59%		

Willowbrook Feeds
plt 10292
October 26, 1995
Source numbers not assigned yet
Filter ID 370
Impingers S5 and S6
Temperat Digitemp No 1
Pressure Digital Manometer
Train=Probe>Filter>Imp S5>Imp S6>pump box #80631

SOURCE TEST LAB DATA SHEET

PLANT: WILLOWBROOK FEED COMPANY

PAGE: 1 OF 1

SOURCE OPERATION: CYCLONEINITIAL: CM

SOURCE TEST NO.: _____

TEST DATE: 10/26/95

FILTER MEDIA: GLASS FIBER, 90 MM

FILTER DATA								
RUN #	FILTER #	TARE WEIGHT(g)			FINAL WEIGHT(g)			TOTAL(g)
A	368	0.4795	0.4795	0.4795	0.4807	0.4809	0.4809	0.0013
B	369	0.4912	0.4911	0.4912	0.4918	0.4918	0.4919	0.0007
C	370	0.4896	0.4895	0.4896	0.4900	0.4901	0.4901	0.0005
DATE/TIME		9/21/95P	9/22/95A	9/22/95P	10/31/95P	11/1/95A	11/1/95P	
Room Relative Humidity, %		73	70	71	62	67	69	
Room Temperature		65	68	66	70	67	65	
Dessicator Relative Humidity, %		20-38	20-39	24-50	29-32	23-27	30-36	
PROBE & NOZZLE RINSE DATA								
RUN #	JAR #	TARE WEIGHT(g)			FINAL WEIGHT(g)			TOTAL(g)
A	17	54.5168	54.5169	54.5171	54.5204	54.5202	54.5205	0.0034
B	18	58.0725	58.0727	58.0728	58.0766	58.0762	58.0764	0.0037
C	19	55.6723	55.6725	55.6725	55.6753	55.6753	55.6755	0.0030
DATE/TIME		9/28/95P	9/29/95P	10/2/95A	10/31/95P	11/1/95A	11/1/95P	
Room Relative Humidity, %		73	71	71	62	67	69	
Room Temperature		62	64	68	70	67	65	
Dessicator Relative Humidity, %		29-40	15-27	11-25	29-32	23-27	30-36	
TOTAL WEIGHTS								
RUN #	FILTER FINAL WT(g)		P & N FINAL WT(g)		TOTAL(g)			
A	0.0013		0.0034		0.0048			
B	0.0007		0.0037		0.0044			
C	0.0005		0.0030		0.0035			

P+N+C

Source Test Lab Data Sheet

Impinger Data

Plant:	WILLOWBROOK FEED COMPANY		
Source operation:	CYCLONE	Page:	1 of 1
Source test no.:		Initial:	CM
Impinger solution:	Distilled H2O	Test date:	10/26/95

DATA			
Impinger #	A Tare weight(g)	B Filled weight(g)	C Final weight(g)
S-1	533.5	633.8	666.4
S-2	514.3	614.8	617.7
S-3	485.3	585.8	633.3
S-4	514.3	614.7	615.5
S-5	512.5	612.9	655.5
S-6	501.6	602.1	602.8

Impinger #	C - A Sample weight (g)	C - B Condensate wt.(g)	Total weight (g)
S-1	132.9	32.6	Run A
S-2	103.4	2.9	35.5
S-3	148.0	47.5	Run B
S-4	101.2	0.8	48.3
S-5	143.0	42.6	Run C
S-6	101.2	0.7	43.3

SOURCE TEST LAB DATA SHEET

PLANT: BLANKS

PAGE: 1 OF 1

SOURCE OPERATION: 100ML ACETONE & H2OINITIAL: CM

SOURCE TEST NO.: _____

TEST DATE: 8/14/95

FILTER MEDIA: _____

FILTER DATA								
RUN #	FILTER #	TARE WEIGHT(g)			FINAL WEIGHT(g)			TOTAL(g)
DATE/TIME								
Room Relative Humidity, %								
Room Temperature								
Dessicator Relative Humidity, %								
PROBE & NOZZLE RINSE DATA								
RUN #	JAR #	TARE WEIGHT(g)			FINAL WEIGHT(g)			TOTAL(g)
A	12H2O	64.9946	64.9943	64.9943	64.9944	64.9947	64.9949	0.0003
B	23ACETONE	70.3122	70.3118	70.3118	70.3122	70.3123	70.3127	0.0005
DATE/TIME		8/14/95A	8/14/95P	8/15/95A	8/21/95A	8/21/95P	8/24/95A	
Room Relative Humidity, %		75	73	74	77	76	73	
Room Temperature		61	60	62	63	64	64	
Dessicator Relative Humidity, %		30-40	27-37	15-30	23-25	31-32	25-27	
TOTAL WEIGHTS								
RUN #	FILTER FINAL WT(g)	P & N FINAL WT(g)			TOTAL(g)			
A		0.0003			0.0003			
B		0.0005			0.0005			

JACK HILLIKER
JBH EQUIPMENT SALES

TEL 209-521-2191

FAX 209-521-5032

CPH ROSKAM CHAMPION SILVER-WEIBULL ABEL MICRO-SYSTEMS MAC EQUIPMENT WEM AUTOMATION

TO: GLENN BACH

DATE: 02/16/93

PAGES: 4

REF: MAC EQUIPMENT

Just to confirm our conversation of Tuesday, MAC has agreed to sell to you the four 96AVS16 Style II Filters as quoted on 12-30-92, at \$2,465 each, plus the fans as specified at \$648 each, all assembled, and shipped FOB Sabetha Kansas. THANKS!

We need more information to properly size the bin vent filters. I have enclosed the information I am working from, which may be more than you ever wanted to know about sizing filters, but on the other hand, will help you in your justification of the sizing to the Air Quality folks when they ask.

I need your best guess as to the following:

1. effective length of the spout in feet

Here we mean how far from the last "break" i.e. the spout from the turn-head, the transition from the screw or super-flo, or the spout from the elevator discharge.

2. spout area in feet

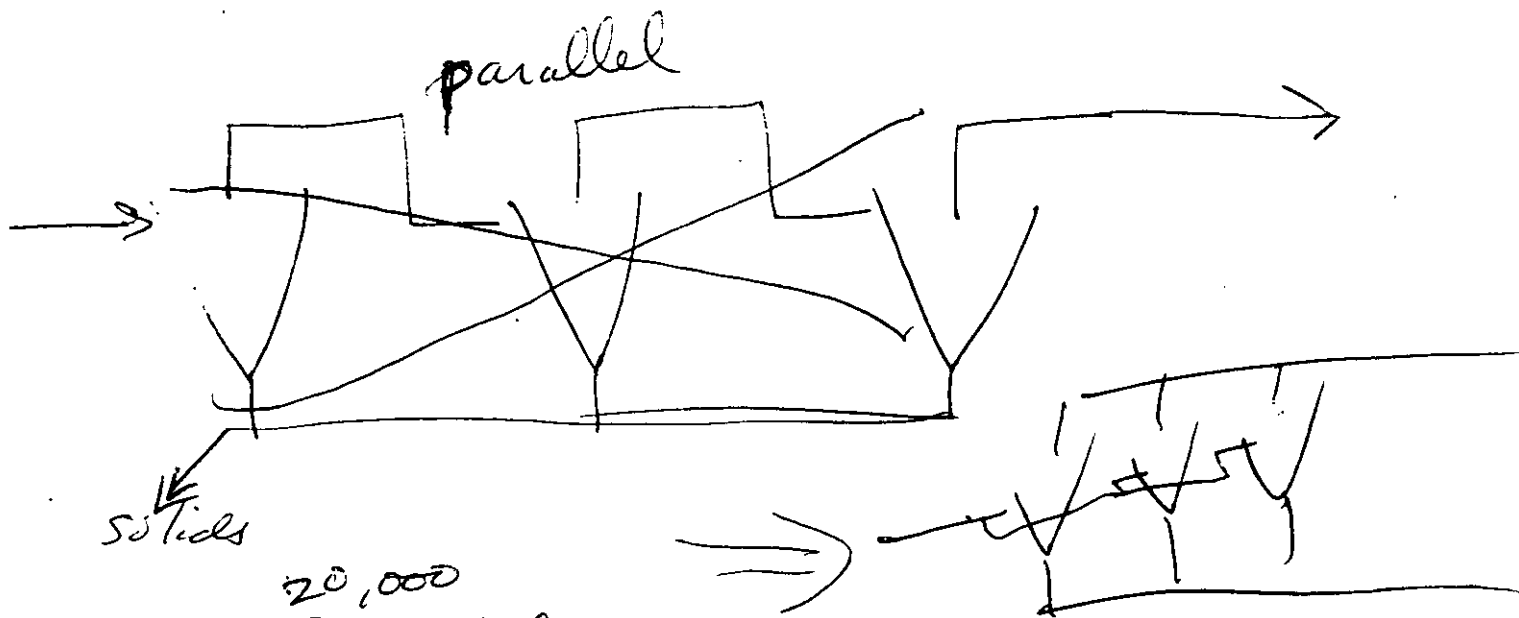
width times width, or area of the circle

3. particle size of the product in inches - a range of the smallest (like soyabean meal), to the largest, (like corn).

As I will be traveling on Wednesday and Thursday, you are welcome to call Curt Strahn at 800-442-0622 (MAC) to get quick answers to any questions you have in generating this information. Curt is up to speed on this project, and can be of immeasurable help. He may be on the road also, but you can imagine how long it will take if you call me, I call him, he calls me back, I call you back, etc.

You also need to be thinking how you could inter-connect the bins with ducts of 6" to 8" diameter. Cross-contamination needs to be a consideration. For example, connecting the bins in series of three, meaning three filters instead of nine, cuts the cost by 50%. I can't remember how your bins are arranged so I can't make that decision for you.

MAC innovated with cartridge filters some time ago and the industry quickly followed suit. The cartridge filter is close in capital cost to the bag filter, but is ten times more efficient! For example, the cartridge emits .002 grains per scfm, while the bag emits .02 grains per scfm. On a 600 cfm system, the bags would emit 12 grains/minute while the cartridges emit 1.2 grains. Your next question is "what the Hell is a grain?" There are 7000 grains in a pound.



20,000
SDCFM / 5000 Total

Cyclone 1 ID	<u>8 inches</u>	Cut pt	_____	Recover rate	_____
Cyc 2 ID	_____	Cut pt	_____	Recover rate	_____
Cyc 3 ID	_____	Cut pt	_____	Recover rate	_____
Ambient?		Temp?	Sat @	85-176	
Feed Wet?				130°	
PS Dist Data	90% cut @ 10 μ				

Baghouse data

16oz bag (uff)

Number
SDCFM
No. of bags
Bag type

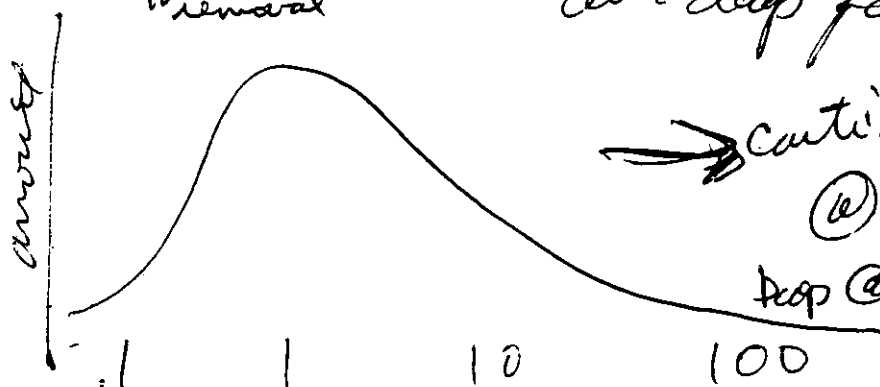
1
4x4 = 16 unit (4)
52 (1)

4 5

mini variable speed

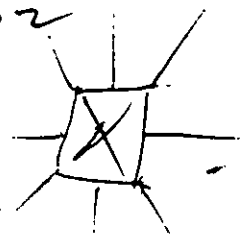
either deep form on low speed?

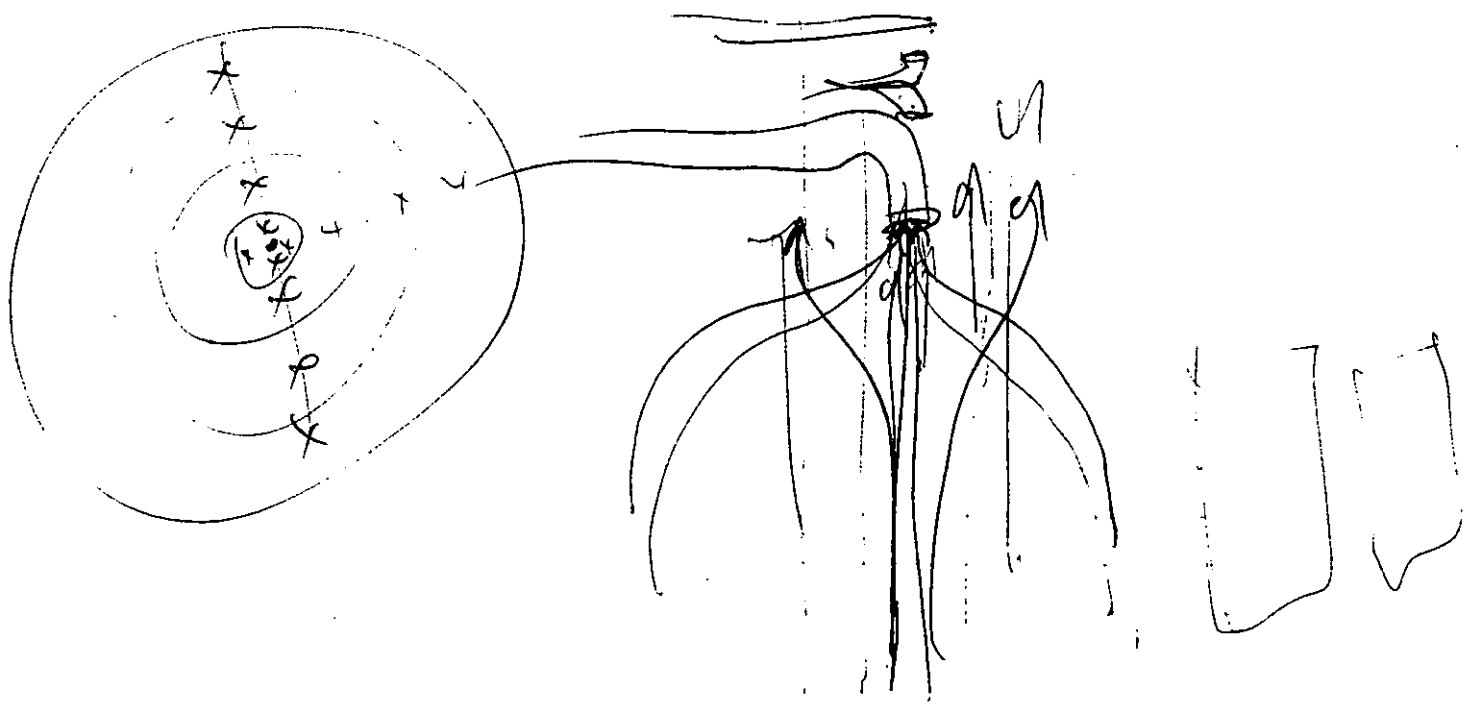
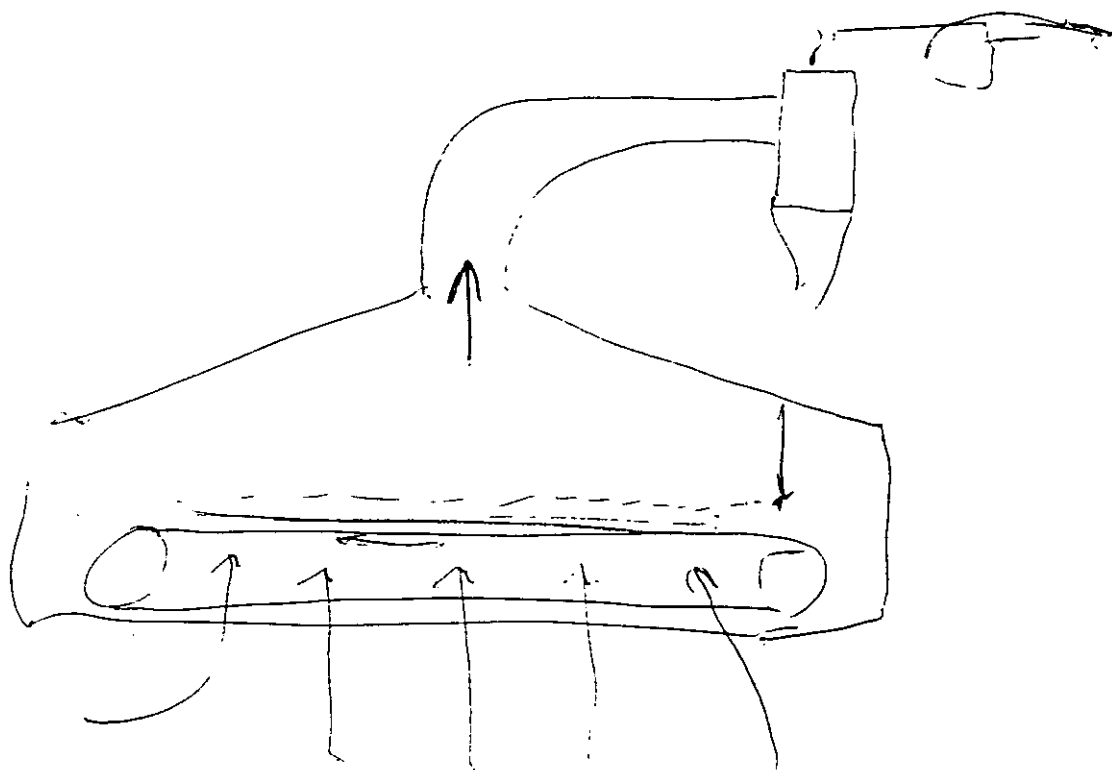
Rated eff & size removal



→ cartidge .002 gr/SDCFM
@ 600 CFM = 1.2 gr/min

drop @ .02





list condition COMMANDS >> c

list condition NUMBER >> 12948

COND# 12948 -----

PERMIT CONDITIONS

S-1 through S-18:

1. The animal feed raw material throughput shall not exceed the following limits per consecutive 12 month period.

S-1 : 88,000 tons
S-2 : 88,000 tons
S-3 : 14,000 tons
S-4 : 14,000 tons
S-5 : 14,000 tons
S-6 : 14,000 tons
S-7 : 54,000 tons
S-8 : 18,000 tons
S-9 : 18,000 tons
S-10: 18,000 tons
S-11: 42,000 tons
S-12: 42,000 tons
S-13: 54,000 tons
S-14: 7,000 tons
S-15: 54,000 tons
S-16: 36,000 tons
S-17: 54,000 tons
S-18: 61,000 tons

2. The grain loading of the exhaust from A-1, A-2, A-3, A-4, A-5, and A-8 shall not exceed 0.01 gr/dscf.
3. In order to demonstrate compliance with condition #1, the owner/operator of the sources, S-1 through S-18, shall keep dated records of material throughput in a District approved logbook. The records shall be kept for at least two years from the date of data entry, and shall be made available to the District staff for inspection.
4. Visible dust emissions from any source/operation at this facility shall not exceed Ringelmann 0.5 or result in fallout on adjacent property in such quantities as to cause a public nuisance per Regulation 1-301.
5. All roadways associated with the facility shall be maintained in a clean or wetted condition, as necessary, to minimize visible emissions.

list condition NUMBER >>

SOURCE TEST REQUEST

SOURCE TEST ACTION
Date Rec'd: 10-2-95
Sr. Engineer Assigned: CM
Test Number: 96069
Date Tested: 10/26/95
Date Completed:

SOURCE DATA

Firm Name: Willowbrook Feeds Telephone No.: (707) 1-792-4585
Address: 401 Ely Road PCB 750818 City: Petaluma Zip: 94975
Representative to Contact: Mr. Glenn Bach Title: Plant Manager
Source Operation: S-1 thru S-12 Permit No.: P/A # 14920 Plant No.: 10292
Permit Conditions: None CON# 12948

SAMPLE DATA

Points to be Tested: Exhaust of all abatement devices (5 baghouses, 3 cyclones)

(List each Source No.):

Type of Tests: Grain loading (gr/dscf) and emission rates (lb/hr)

Special Instructions:

1-CYCLONE
1-BAGHOUSE
1-CYLOS
DO 1 OF EACH
REPRESENTATIVE
TIME
PRIORITY B
CHECK 10/4/95

REQUEST DATA

Reason for Request: To estimate emissions and compliance with Reg 6, Part 120

☒ Compliance with Regulation 6 Rule Section(s)

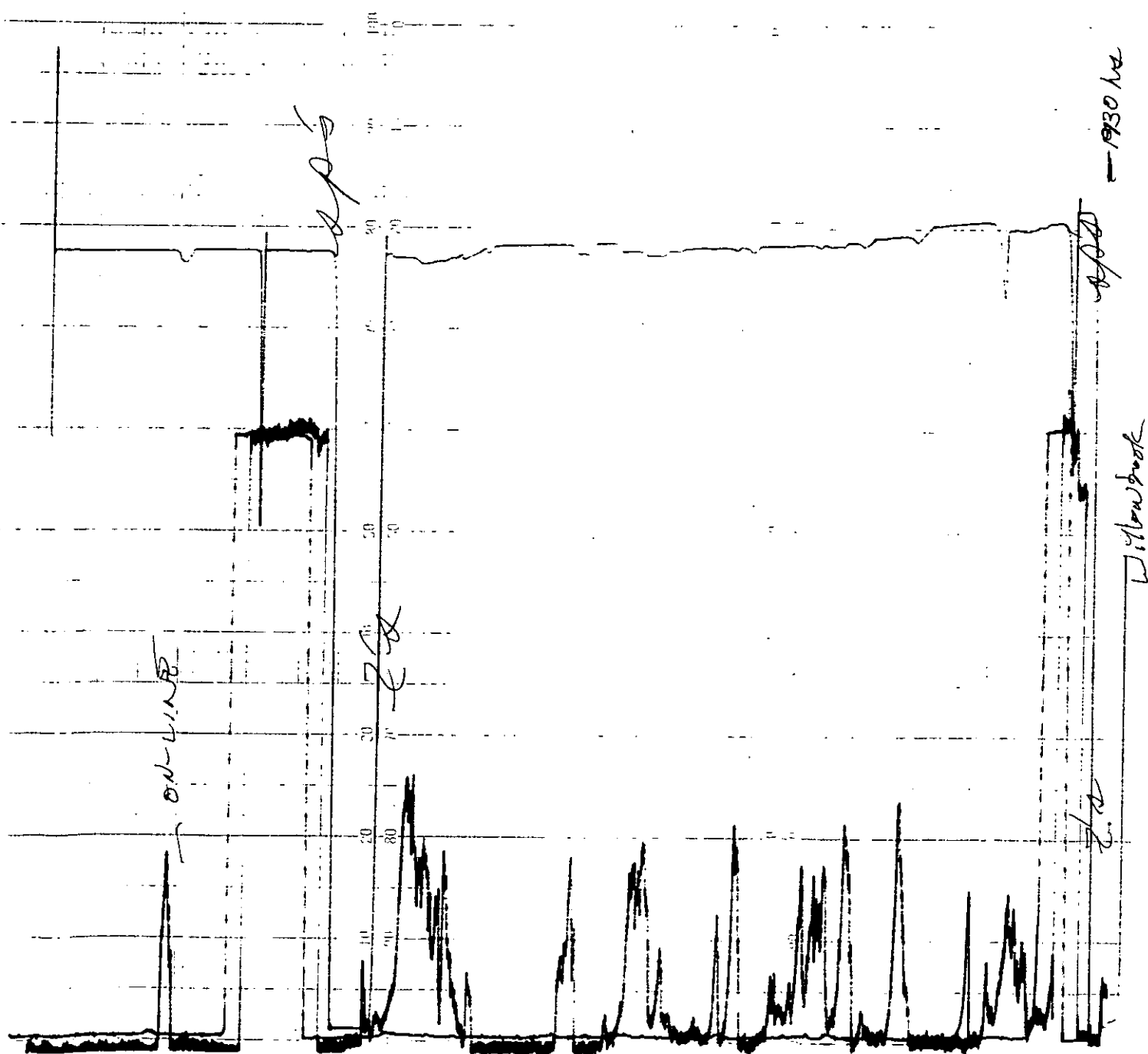
☐ Developmental Data ☐ Hearing Board ☒ Permit

☐ Other

Date Results Requested by: [Signature] ASAP (10/6/95) Type of Request: ☒ Announced ☒ Unannounced

Request Initiated by: [Signature] Section: NSR

Requester to be Present During Test? No Approved by: [Signature] 9/29/95
(Date)



MR I
401 Harrison Oaks Blvd #350
Cary, NC 27513-2412

Thomas Lapp