

Note: This is a reference cited in *AP 42, Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at www.epa.gov/ttn/chief/ap42/

The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

AP-42 Section Number: 9.9.1

Reference Number: 20

**Title: Dust Control Systems Performance
Test**

Pollution Curbs, Inc.

July 1976



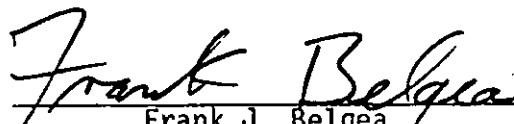
AP-42 Section 9.9.1
Reference 20
Report Sect. _____
Reference _____

Equipment Division
PCI Contract No. 508357
July 15, 1976

DUST CONTROL
SYSTEMS
PERFORMANCE TEST

Prepared For:
FARMERS UNION ELEVATOR ASSOCIATION
SARLES, NORTH DAKOTA

Prepared By:
POLLUTION CURBS, INC.
502 NORTH PRIOR AVENUE
ST. PAUL, MINNESOTA 55104


Frank J. Belgea
Vice President of Operations



PCI Contract No. 508357

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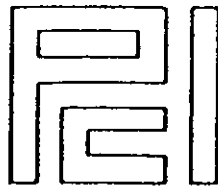
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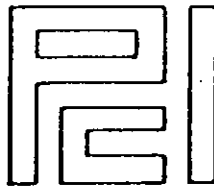
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1. SUMMARY

The average dust emission rate from each of the three dust control systems was as follows:

House System	-	0.71 lb/hr
Crippen System	-	0.37 lb/hr
Ideal System	-	0.25 lb/hr

The emissions from all three stacks were found to comply with the Air Pollution Control Regulations of the State of North Dakota.



2. INTRODUCTION

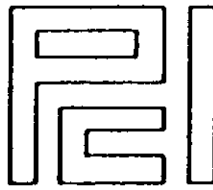
Jacobson and Sons Construction Company (Jacobson) had purchased from the Equipment Division of Pollution Curbs, Inc. (PCI) eight dust control systems to be installed in three grain elevators under construction at Niobe, Sarles, and Kramer, North Dakota. Plans and specifications for the eight dust control systems were submitted to the North Dakota State Health Department for review and approval. Construction permits for the three projects were subsequently issued.

By letter from Mr. Willis Van Heuvelen, dated February 5, 1976, PCI was apprised of North Dakota State Health Department policy requiring all suppliers of dust control equipment to the North Dakota market to provide performance test data on the supplier's initial installation. Because construction at the Sarles site was completed before Niobe or Kramer, and because the ductwork configuration at Sarles presented an opportunity to collect more representative data than did either Niobe or Kramer, Sarles was selected by PCI as the most appropriate installation at which to conduct the required performance tests.

On July 8 and 9, 1976 a field test crew representing PCI's Consulting Division occupied the Sarles site to collect samples and other pertinent data relative to evaluating the performance of the three dust control systems known as the House System, the Crippen System, and the Ideal System.

The following persons participated in the test:

<u>Name</u>	<u>Affiliation</u>
Howard Thompson	Farmers Union Elevator Association
Bud Hinkle	Jacobson & Sons Construction Company
Gerry Wentz	Jacobson & Sons Construction Company



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Name

Affiliation

Frank Belgea

Pollution Curbs, Inc.

Mark Oemichen

PCI - Field Services Section

Dean Franke

PCI - Air Engineering Section

Robert King

North Dakota State Health Department

Kevin Kiemele

North Dakota State Health Department



3. PROCEDURES

3.1 Emissions Measurements

The quantity of particulate matter passing each of the cyclone dust collectors was determined by sampling the respective exhaust stacks and extrapolating the data. Three representative isokinetic samples were obtained from the vertical ductwork serving as the clean air exhaust for the House Dust Control System and three such samples were obtained from a similar location in the Crippen Cleaner Dust Control System. Two samples were obtained from the Ideal Cleaner cyclone exhaust. A planned third sample run on the Ideal System was aborted due to a malfunction in the sampling equipment.

All of the above samples were collected by extracting exhaust gas from preselected points located on horizontal planes in the exhaust stacks. The dust was captured on tared fiberglass filters and the sample gas volume was metered. The velocity of exhaust gas was measured simultaneously with the sample extraction to ensure isokinetic conditions and to provide flow rates for subsequent extrapolation of the sampling data. For all sample runs, the sample site selections and traverse techniques, the gas velocity and volumetric flow rates, and the sample collection and recovery procedures all followed EPA Reference Methods 1, 2 and 5 and North Dakota Performance Test Guidelines. The equipment employed in sampling and data gathering met or exceeded EPA specifications. Copies of all field data sheets and all calculations were reproduced for inclusion in the Appendix of this report.

The opacity of the exhaust stream from each stack was determined employing the procedures in EPA Reference Method 9. Readings were made by Mr. Frank Belgea,



a certified smoke reader. A copy of Mr. Belgea's certification was reproduced for inclusion in the Appendix.

3.2 Process Weight Rate

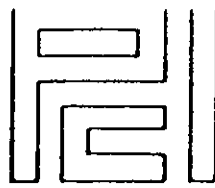
During the sampling periods for each dust control system, the pertinent elevator grain handling equipment or cleaners were operated at or near their maximum capacity.

Grain was either dumped by truck or continuously spouted into the front pit throughout testing of the house system. The process weight rate for the house system was calculated from the rated leg capacity, 5000 bushels per hour, which was operated at its maximum speed. Huge clouds of dust were observed in the pits, however, none escaped through the grate or hatches but was instead captured by the dust control system. Some dust was noticed puffing out between the floor and the scale deck. However, this occurred because the stripping to cover the opening had not yet been installed pending calibration of the scale by State inspectors.

The process weight rate for each of the cleaners was determined by timing the throughput of a measured volume of grain with the cleaner operating at maximum conditions.

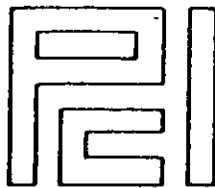
The cleaner fan dampers were appropriately set by Mr. Howard Thompson for the grain to be handled during testing. No dust could be found escaping the cleaners or the bell hood bleed-ins although billows of dust in the back pits showed the grain to be dirty.

As the elevator was new and not yet operating normally, a limited amount of



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grain was available for test purposes. Therefore, it was necessary to transfer grain from place to place within the facility to provide a constant flow at maximum operating conditions during testing of each dust control system. This was accomplished without interruption.



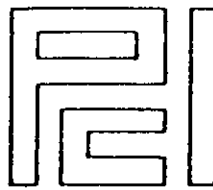
4. RESULTS

4.1 House Dust Control System

<u>Item</u>	<u>Run #1</u>	<u>Run #2</u>	<u>Run #3</u>	<u>Average</u>
Volumetric Flow Rate (sdcfm)	7440	7620	7480	7510
Temperature (°F)	85	85	85	85
Moisture Content (vol. %)	1.8	1.8	1.7	1.8
Dust Concentration (gr/sdcf)	0.015	0.012	0.007	0.011
Process Weight Rate (bu/hr)	5000	5000	5000	5000
Process Weight Rate (ton/hr) ¹	150	150	150	150
Dust Emission Rate (lb/hr)	0.96	0.78	0.45	0.71
Allowable Emission Rate (lb/hr) ²	55	55	55	55
Stack Opacity (%)	<5	<5	<5	<5

4.2 Crippen Cleaner Dust Control System

Volumetric Flow Rate (sdcfm)	4350	4360	4270	4330
Temperature (°F)	80	80	80	80
Moisture Content (vol. %)	1.5	1.7	1.8	1.7
Dust Concentration (gr/sdcf)	0.012	0.008	0.010	0.010
Process Weight Rate (bu/hr)	430	430	430	430
Process Weight Rate (ton/hr) ¹	13	13	13	13
Dust Emission Rate (lb/hr)	0.45	0.30	0.37	0.37
Allowable Emission Rate (lb/hr) ²	23	23	23	23
Stack Opacity (%)	<5	<5	<5	<5



4.3 Ideal Cleaner Dust Control System

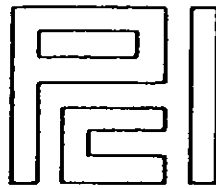
<u>Item</u>	<u>Run #1</u>	<u>Run #2</u>	<u>Average</u>
Volumetric Flow Rate (sdcfm)	2440	2400	2420
Temperature (°F)	80	80	80
Moisture Content (vol. %)	1.6	1.7	1.6
Dust Concentration (gr/sdcf)	0.012	0.012	0.012
Process Weight Rate (bu/hour)	900	900	900
Process Weight Rate (ton/hr) ¹	27	27	27
Dust Emission Rate (lb/hr)	0.25	0.25	0.25
Allowable Emission Rate (lb/hr) ²	37	37	37
Stack Opacity (%)	<5	<5	<5

4.4 Discussion

The reliability of the above tabulated results is evidenced by the close agreement among successive flow rate measurements for the respective systems, by the compatibility between low dust concentrations and respective low stack opacities, and by the degree of isokinesis achieved for each sample run. The progressive lessening of dust concentrations over successive runs for the House System is probably due to the test grain becoming cleaner as sampling proceeded.

Notes: 1. Calculated @ 60 lb/bu

2. From Table 3, Regulation 23-25-05

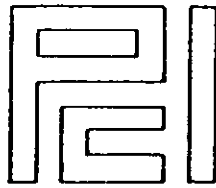


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5. CONCLUSIONS

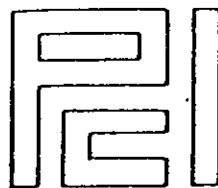
The results tabulated in Sections 4.1, 4.2, and 4.3 indicate that all three dust control systems perform up to the specifications of the North Dakota State Health Department as presented in Regulation 23-25. Particulate emissions were well below the maximum allowed by Table 3, Rule 23-25-05 and visible emissions were less than the 20% opacity limitation of Rule 23-25-03 for new sources.

Based on the excellent performance of the three dust control systems tested, as observed by previously named State officials and as reported herein, it is the Consulting Division's opinion that final approval and operating permits be granted to the Farmers Union Elevator Association of Sarles, North Dakota and to other in the state having similar design and operating characteristics.



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A P P E N D I X

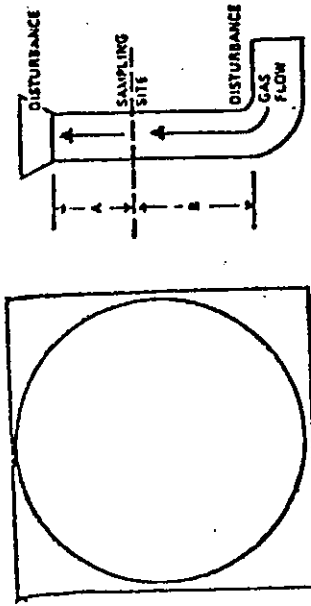


STANDARD SYMBOLS AND
ABBREVIATIONS

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1. acfm = Actual cubic feet per minute
2. BOD =
3. COD = Chemical oxygen demand
4. Btu = British thermal units
5. cfm = Cubic feet per minute
6. cps = Cycles per second
7. Δ = Delta, signifies a change
8. dB = Decibel
9. dBA = Decibel as measured on the A scale of a sound level meter
10. DO = Dissolved oxygen
11. E = Symbol for sum of
12. gpd = Gallons per day
13. gpm = Gallons per minute
14. g = Grams
15. gpcd = Gallons per capita day
16. $<$ = Less than
17. $>$ = Greater than
18. hp = Horsepower
19. Hz = Hertz
20. KHz = Kilo Hertz
21. l = Liter
22. lb = Pound
23. lpm = Liters per minute
24. mg = Milligram
25. mg/l = Milligrams per liter
26. mg/m³ = Milligrams per cubic meter
27. ml = Milliliter
28. M² = Square meter
29. M³ = Cubic meter
30. μ = Micron
31. μ m = Micrometer
32. μ g = Microgram
33. MPN = Most probable number
34. mgd = Million gallons per day
35. ou = Odor unit
36. ou/min = Odor unit per minute
37. ppm = Parts per million
38. SDI = Sludge density index
39. SS = Suspended solids
40. scf = Standard cubic feet
41. scfh = Standard cubic feet per hour
42. scfm = Standard cubic feet per minute
43. sdcfm = Standard dry cubic feet per minute
44. TWA = Time weighted average
45. rpm = Revolutions per minute
46. TOC = Total organic carbon
47. Vol % = Volume percent
48. Wt % = Weight percent
49. TS = Total solids
50. VS = Volatile solids

SCHEMATIC OF STICK



CROSS SECTION

1100
N. 2017

PLANT SARLES, N. 22
DATE 8 JULY 1976
LOCATION EUEL. HENHOUSE
OPERATOR F. J. B. D. C. F. M. A. O.
STACK NO. House System
RUN NO. ONE (1)
SAMPLE BOX NO. 2343-3
METER BOX NO. 2343-3

METER, H₂

C FACTOR

PROCESS WEIGHT RATE

WEIGHT OF PARTICULATE COLLECTED, mg

SAMPLE	FILTER	PROBE WASH
FINAL WEIGHT	0.7178	63.6385
TARE WEIGHT	0.6870	63.5977
WEIGHT GAIN	0.0308	0.0408
TOTAL		0.0716

[illegible]

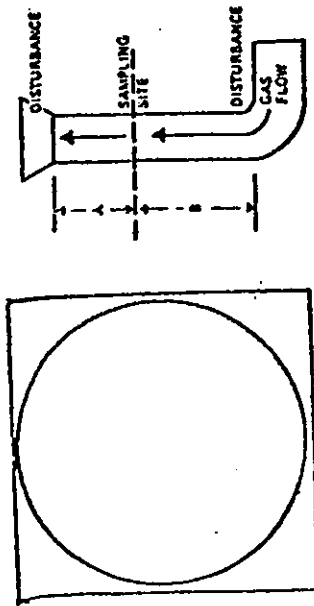
AVERAGE

VOLUME OF LIQUID WATER COLLECTED	JAPINGER VOLUME ml				SILICA GEL WEIGHT, g
	1	2	3	4	
FINAL					
INITIAL					
LIQUID COLLECTED					
					28.5

COMMENTS:

ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
1					
2					
3					
4					

SYNTHETIC OF STICK



N. port

METER IN; _____
C FACTOR 0.87

PROCESS WEIGHT RATE

WEIGHT OF PARTICULATE COLLECTED, mg

SAMPLE	FILTER	PROBE WASH
FINAL WEIGHT	0.7178	63.6385
TARE WEIGHT	0.6870	63.5977
WEIGHT GAIN	0.0308	0.0408
TOTAL		0.0716

TOTAL	0.0716
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[illegible]

AVERAGE

IMPINGER
VOL 116

VOLUME OF LIQUID
WATER COLLECTED

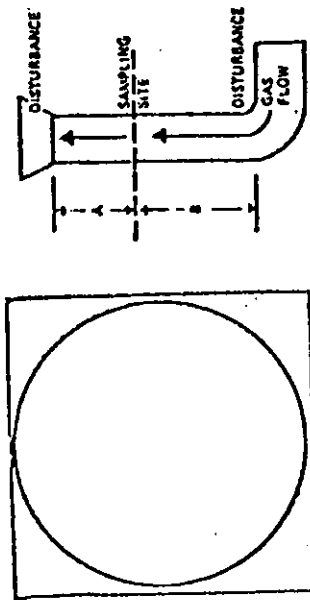
SILICA GEL
WEIGHT,

ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
1	00:00	15.0	18.0	0.0	67.0
2	00:05	14.5	18.5	0.0	67.0
3	00:10	14.0	19.0	0.0	67.0
4	00:15	13.5	19.5	0.0	67.0
5	00:20	13.0	20.0	0.0	67.0
6	00:25	12.5	20.5	0.0	67.0
7	00:30	12.0	21.0	0.0	67.0
8	00:35	11.5	21.5	0.0	67.0
9	00:40	11.0	22.0	0.0	67.0
10	00:45	10.5	22.5	0.0	67.0
11	00:50	10.0	23.0	0.0	67.0
12	00:55	9.5	23.5	0.0	67.0
13	01:00	9.0	24.0	0.0	67.0
14	01:05	8.5	24.5	0.0	67.0
15	01:10	8.0	25.0	0.0	67.0
16	01:15	7.5	25.5	0.0	67.0
17	01:20	7.0	26.0	0.0	67.0
18	01:25	6.5	26.5	0.0	67.0
19	01:30	6.0	27.0	0.0	67.0
20	01:35	5.5	27.5	0.0	67.0
21	01:40	5.0	28.0	0.0	67.0
22	01:45	4.5	28.5	0.0	67.0
23	01:50	4.0	29.0	0.0	67.0
24	01:55	3.5	29.5	0.0	67.0
25	02:00	3.0	30.0	0.0	67.0
26	02:05	2.5	30.5	0.0	67.0
27	02:10	2.0	31.0	0.0	67.0
28	02:15	1.5	31.5	0.0	67.0
29	02:20	1.0	32.0	0.0	67.0
30	02:25	0.5	32.5	0.0	67.0
31	02:30	0.0	33.0	0.0	67.0
32	02:35	0.0	33.5	0.0	66.5
33	02:40	0.0	34.0	0.0	66.0
34	02:45	0.0	34.5	0.0	65.5
35	02:50	0.0	35.0	0.0	65.0
36	02:55	0.0	35.5	0.0	64.5
37	03:00	0.0	36.0	0.0	64.0
38	03:05	0.0	36.5	0.0	63.5
39	03:10	0.0	37.0	0.0	63.0
40	03:15	0.0	37.5	0.0	62.5
41	03:20	0.0	38.0	0.0	62.0
42	03:25	0.0	38.5	0.0	61.5
43	03:30	0.0	39.0	0.0	61.0
44	03:35	0.0	39.5	0.0	60.5
45	03:40	0.0	40.0	0.0	60.0
46	03:45	0.0	40.5	0.0	59.5
47	03:50	0.0	41.0	0.0	59.0
48	03:55	0.0	41.5	0.0	58.5
49	04:00	0.0	42.0	0.0	58.0
50	04:05	0.0	42.5	0.0	57.5
51	04:10	0.0	43.0	0.0	57.0
52	04:15	0.0	43.5	0.0	56.5
53	04:20	0.0	44.0	0.0	56.0
54	04:25	0.0	44.5	0.0	55.5
55	04:30	0.0	45.0	0.0	55.0
56	04:35	0.0	45.5	0.0	54.5
57	04:40	0.0	46.0	0.0	54.0
58	04:45	0.0	46.5	0.0	53.5
59	04:50	0.0	47.0	0.0	53.0
60	04:55	0.0	47.5	0.0	52.5
61	05:00	0.0	48.0	0.0	52.0
62	05:05	0.0	48.5	0.0	51.5
63	05:10	0.0	49.0		

COMMENTS:

301. 311.4.4.1.2. 00000000 1761(3)

SYNTHETIC OF STICK



CROSS SECTION

met

METER A.H. _____
C FACTOR 0.84

PROCESS WEIGHT RATE

WEIGHT OF PARTICULATE COLLECTED, mg

SAMPLE		FILTER	PROBE WAS
FINAL WEIGHT	0.7178	63.638	
TARE WEIGHT	0.6870	63.597	
WEIGHT GAIN	0.0308	0.0403	
TOTAL		0.0716	

TOTAL 2.07%

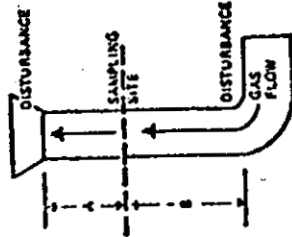
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AVERAGE

COMMENT:

VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml				SILICA GEL WEIGHT, g	ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
	1	2	3	4							
FINAL						1					
INITIAL						2					
LIQUID COLLECTED						3					

SCHEMATIC OF STACK



E. por

PROCESS WEIGHT RATE

WEIGHT OF PARTICULATE COLLECTED, mg		
SAMPLE	FILTER	PROBE WASH
FINAL WEIGHT	0.7178	63.6385
TARE WEIGHT	0.6870	63.5971
WEIGHT GAIN	0.0308	0.0408
TOTAL		0.0716

COMMENTS:

VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml				SILICA GEL WEIGHT, g	ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
	1	2	3	4							
FINAL						1					
INITIAL						2					
LIQUID COLLECTED						3					
						4					

HS-1

PARTICULATE EMISSION CALCULATION

Plant: *SARLES, NETH. DAKOTA* Orsat Analysis: (Dry Basis, % by Vol.), Average
 Location: *ELEVATOR HEADHOUSE* CO₂ *ZERO*
 Stack or Source: *HOUSE SYSTEM* O₂ *20.9*
 Date: *8 JULY 1976* CO *ZERO*
 Run No.: *ONE (1)* N₂ *79.1*
 Operator: *F.J.B., D.F.F., M.W.O.* Water Collected, GMS.: *28.5*
 Bar. Pr., In. Hg: *28.76 ABSOLUTE* Filter No.: *A*
 Nozzle Dia, In.: *0.25 (1/4)"* Particulate Collected, GMS.:
 Stack Dia., In.: *19" Ø* Filter *0.0308*
 Cp: *0.82* Probe Wash *0.0408*
 Total Time, Min.: *60 (1 HOUR)*
 Vol. Through Gas Meter, Cu. Ft.: FRONT END TOTAL *0.0716*
 Impinger Catch
 FRONT PLUS BACK END CATCH TOTAL

Standard Conditions: Dry Gas at *15.6°C* and 29.92 in. Hg.

C - 1 Calculate Average Meter Temperature

T_m = The average of both inlet and outlet temperatures
 obtained during sampling, *559.3* °R.

C - 2 Calculate Sample Volume at Standard Conditions

$$\begin{aligned}
 V_{mstd} &= \text{SCF (Dry) Through meter} \\
 &= 17.32 \frac{V_m}{T_m} \times P_m \\
 &= 17.32 \frac{83.29}{28.96} \\
 &= \underline{558.3} \\
 &= \underline{73.71} \text{ SCF (Dry)}
 \end{aligned}$$

Where: V_m = Dry gas measured by meter, cu.ft.

P_m = Abs. Pr. at meter (use barometric pressure, uncorrected for altitude), In. Hg

C - 3 Calculate Volume Fraction Water in Flue Gas

$$\begin{aligned}
 V_{wstd} &= \text{Water vapor in SCF} \\
 &= 0.0465 V_{lc} \\
 &= 0.0465 \cdot 28.5 \\
 &= \underline{1.33} \text{ SCF}
 \end{aligned}$$

$$\begin{aligned}
 B_{wo} &= \text{Water } \frac{V}{V} \\
 &= \frac{V_{wstd}}{(V_{wstd} + V_{mstd})} \\
 &= \frac{1.33}{1.33 + 73.71} = \underline{0.0178}
 \end{aligned}$$

Where V_{lc} = Weight of water collected in impingers plus that gained by drierite, GMS

C - 4 Calculate Dry and Wet Molecular Weight of Stack Gas

M_d = Dry Mol. Wt.

$$= 0.44 (\% \text{ CO}_2) + 0.32 (\% \text{ O}_2)$$

$$+ 0.28 (\% \text{ N}_2 + \text{CO})$$

$$= 0.44 \times \underline{\text{ZERO}} + 0.32 \times \underline{20.9 = 6.69} + 0.28 \times \underline{79.1 = 22.15}$$

$$= \underline{28.87}$$

M_s = Wet Mol. Wt.

$$= M_d (1 - B_{wo}) + 18 B_{wo}$$

$$= \underline{28.87} \times \underline{0.9822} + 18 \times \underline{0.0178}$$

$$= \underline{28.65} \quad \underline{0.320}$$

C - 5 Calculate The Average $\sqrt{\Delta P}$, ($\sqrt{\Delta P}$) Avg., Obtained during gas sample acquisition.

$$(\sqrt{\Delta P}) \text{ Avg.} = \underline{1.198}$$

C - 6 Calculate The Average Stack Gas Temperature, T_s , at time of Gas Sample Acquisition

$$T_s = \underline{595} \text{ } ^\circ\text{R}$$

C - 7 Calculate The Average Stack Gas Velocity

$$(V_s) \text{ Avg.} = 85.48 \times C_p \times (\sqrt{\Delta P}) \text{ Avg.}$$

$$= 85.48 \times \underline{0.87} \times \underline{1.198}$$

$$= \underline{70.57} \text{ ft./sec}$$

$$\sqrt{\frac{T_s}{P_s \times M_s}} = \sqrt{\frac{595}{28.50 \times 28.65}} = \underline{0.82}$$

Where:

C_p = Pitot Tube Coefficient

P_s = Absolute Stack Gas Press., In. Hg.

C - 8 Calculate Stack Cross Sectional Area at Sampling Site

$$A_s = \underline{1.97} \text{ Sq. Ft.}$$

C - 9 Calculate Stack Gas Average Volumetric Flow Rate

Q_s = Stack Gas Flow Rate, SCFM (Dry)

$$= 1043 \times (1 - B_{wO}) (V_s)_{\text{Avg.}} \times A_s \times \frac{P_s}{T_s}$$

$$= \underline{1043} \times \underline{0.9822} \times \underline{70.54} \times \underline{1.97} \times \underline{28.50}$$

$$= \underline{7,770} \text{ SCFM (Dry)} \quad \underline{545}$$

C - 10 Calculate Isokinetic Sampling Efficiency

$$I = \frac{0.00321 (V_{wstd} + V_{mstd}) \times T_s \times P_m}{\theta \times A_n \times (V_s)_{\text{Avg.}} \times P_s}$$

$$= 0.00321 \times \underline{77.74} \times \underline{545} \times \underline{28.96}$$

$$\underline{60} \times \underline{0.000341} \times \underline{70.54} \times \underline{28.50}$$

$$= \underline{90.5} \%$$

θ = Total Sampling Time, Min.

A_n = Nozzle Opening, Sq. Ft.

C - 11 Calculate Heat Input during testing period

Z = Total Heat Input Rate to Boiler, MEGA BTU/hr.

$$= W_1 \times H_1 =$$

$$+ W_2 \times H_2$$

$$+ W_3 \times H_3$$

= TOTAL

$$= \underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

TOTAL MEGA BTU/hr.

45-1

Where $W_1, W_2, & W_3$ = hourly fuel input of respective fuels and
 $H_1, H_2, & H_3$ = gross (as received) heating value of respective
 fuels in mega BTU per input unit (consistent with fuel input unit).

C - 12 Calculate Front End Particulate Grain Loading (with Front
 Half Washings Only)

$$C_s' = \text{Part. Grain Loading, gr/SCF (Dry)}$$

$$= 15.42 \times \frac{M_n}{V_{mstd}}$$

$$= 15.42 \times \frac{0.0716}{73.41}$$

$$= \frac{0.015}{\text{gr/SCF (Dry)}}$$

Where

M_n = Total Particulate Collected (Filter Plus Front Half
 Washings Only), GMS

C - 13 Calculate Front End Emission Factor

E_t = Hourly Mass Rate, lbs/hr.

$$= 0.00857 \times C_s' \times Q_s$$

$$= 0.00857 \times 0.015 \times 7,740$$

$$= 0.96 \text{ lbs/hr.}$$

E_h = Front End Emission Factor, lbs/MEGA BTU

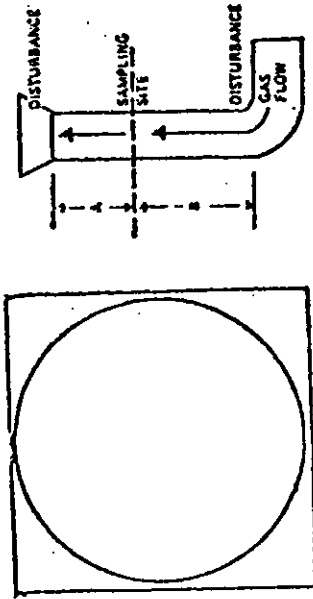
$$= \frac{E_t}{Z}$$

$$= \frac{\quad}{\quad}$$

$$= \frac{\quad}{\quad} \text{ lbs/MEGA BTU}$$

PARTICULATE FIELD DATA

SCHEMATIC OF STACK



CROSS SECTION

Al. port

PLANT SARLES, N. 2 AMBIENT TEMPERATURE 80 F
 DATE 8 JULY 1976 BAROMETRIC PRESSURE 28.86
 LOCATION ELEV. HENRICH HOUSE ASSUMED MOISTURE, % 2.03
 OPERATOR F.J.B., J.E.S., M.W.O. PROBE LENGTH, in. 36
 STACK NO. House System NOZZLE DIAMETER, in. 0.25
 RUN NO. Two (2) STACK DIAMETER, in. 19"
 SAMPLE BOX NO. 2383-3 PROBE HEATER SETTING None
 METER BOX NO. 2383-3 HEATER BOX SETTING None

WEIGHT OF PARTICULATE COLLECTED, mg			
SAMPLE	FILTER	PROBE WASH	
FINAL WEIGHT	0.6799	0.22075	
TARE WEIGHT	0.6538	0.11753	
WEIGHT GAIN	0.0261	0.10322	
TOTAL			0.0583

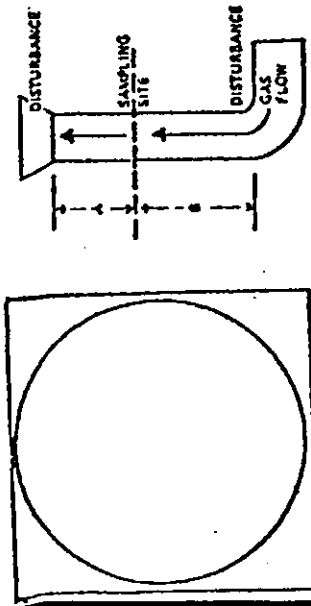
TRAVERSE POINT NUMBER	SAMPLING TIME (H), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY (AP _s) (√AP _s)	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (ΔH) in. H ₂ O	GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER		SAMPLE BOX TEMPERATURE °F	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER °F	PUMP VACUUM in. Hg gauge	VELOCITY f/s
							INLET (T _{m, in}), °F	OUTLET (T _{m, out}), °F				
1	1616	+0.6	85	1.5	6.6	414	106	97	85	85	102	
2	1618			1.5	6.6	417	108	98				
3	1622			1.5	6.6	420	111	98				
4	1625			1.5	6.6	424	114	99				
5	1628			1.5	6.6	428	118	100				
6	1631			1.6	7.1	432	119	100				
7	1634			1.6	7.1	437	120	99				
8	1637			1.6	7.1	441	123	100				
9	1640			1.6	7.1	450	123	100				
10	1643			1.6	7.1	453	124	100				
11												
12												
13												
14												
15												
TOTAL												
AVERAGE												

During this run, 20 TAPAC POINTS WERE SAMPLED INSTEAD OF 30, ENABLING THE USE OF 3 MIN. PER SAMPLE PERIODS

COMMENTS:

VOLUME OF LIQUID WATER COLLECTED		IMPINGER VOLUME ml		SILICA GEL WEIGHT, g		ORSAT MEASUREMENT				TIME			
1	2	3	4	1	2	CO ₂	O ₂	CO	N ₂	1	2	3	4
FINAL													
INITIAL													
LIQUID COLLECTED													

SYNOPSIS OF SYL



CROSS SECTION

Al. port

[illegible]

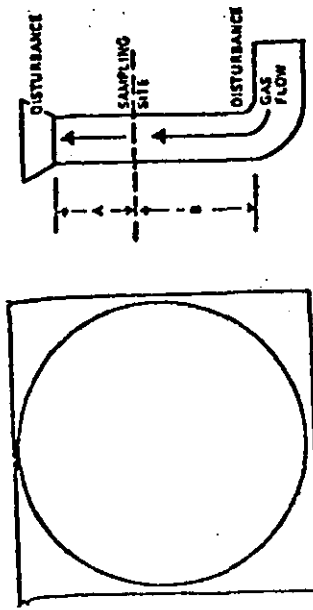
AVERAGE

VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml				SILICA GEL WEIGHT, g	ORSAT MEASUREMENT				
	1	2	3	4		TIME	CO ₂	O ₂	CO	N ₂
FINAL						1				
INITIAL						2				
LIQUID COLLECTED						3				
						4				

COMMENTS:

METER NO. 0-84
C FACTOR 0.84

SCHEMATIC OF STACK



CROSS SECTION

E. Port

PROCESS WEIGHT RATE

WEIGHT OF PARTICULATE COLLECTED, mg			
SAMPLE	FILTER	PROBE WASH	
FINAL WEIGHT	0.6799	22.2025	
TARE WEIGHT	0.6539	61.1753	
WEIGHT GAIN	20.261	0.0322	
TOTAL			0.0583

NOZZLE DIAMETER, in. 0.25
STACK DIAMETER, in. 19.4
PROBE HEATER SETTING None
HEATER BOX SETTING None

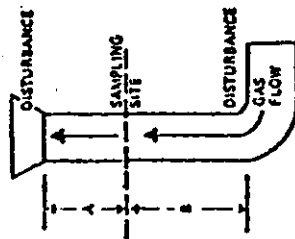
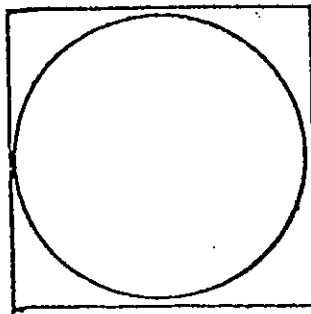
TRAVERSE POINT NUMBER	SAMPLING TIME (H), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD (AP ₃) (1/4" P)	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (ΔH) in. H ₂ O		GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER		SAMPLE BOX TEMPERATURE °F	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER °F	PUMP VACUUM in. Hg gauge	VELOCITY fps
					ACTUAL	DESIRED		INLET (T _{in}), °F	OUTLET (T _{out}), °F				
1	1651	40.6	85	1.5	6.6	6.6	457	117	61	85	85	170.2	
2	1654			1.5	6.6	6.6	461	118	62				
3	1657			1.4	6.2	6.2	465	120	62				
4	1700			1.4	6.2	6.2	469	120	61				
5	1703			1.4	6.2	6.2	473	120	62				
6	1706			1.4	6.2	6.2	477	120	62				
7	1709			1.4	6.2	6.2	481	120	60				
8	1712			1.6	7.1	7.1	485	120	60				
9	1715			1.6	7.1	7.1	489	120	100				
10	1718			1.6	7.1	7.1	494.216	120	100				
11	END												
12													
13													
14													
15													
TOTAL	60						494.216	236.1	2000	85	85	1.5	
AVERAGE	3	70.6	85					118.05	100				

CHERRY THIS RUN TO TOTAL POINTS WERE SAMPLED INSTEAD OF 40. ENABLING THE USE OF 5.3 MIN. PR. SAMPLING PERIODS.

VOLUME OF LIQUID WATER COLLECTED		IMPINGER VOLUME ml				SILICA GEL WEIGHT, g				ORSAT MEASUREMENT				TIME				CO ₂ O ₂ CO N ₂			
FINAL		1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4				
INITIAL																					
LIQUID COLLECTED																					

COMMENTS:

SCHEMATIC OF STACK



CROSS SECTION

2. 1000

METER IN; _____
C FACTOR 13.82

PROCESS WEIGHT RATE _____

WEIGHT OF PARTICULATE COLLECTED, mg

SAMPLE

FINAL WEIGHT

HEIGHT GAIN

TOTAL

PLANT Sares, N.D. AMBIENT TEMPERATURE 80°F
DATE 8 July 1976 BAROMETRIC PRESSURE 28.96
LOCATION Everl. Henon House ASSUMED MOISTURE, % 270.3
OPERATOR F.J.B., D.F.S., M.A.O. PROBE LENGTH, in. 36
STACK NO. House System NOZZLE DIAMETER, in. 0.25
RUN NO. Two (2) STACK DIAMETER, in. 19"
SAMPLE BOX NO. 2383-3 PROBE HEATER SETTING NONE
ETER BOX NO. 2383-3 HEATER BOX SETTING NONE

[illegible]

AVERAGE

VOLUME OF LIQUID	IMPINGER VOLUME ml
10	10
20	20
30	30
40	40
50	50
60	60
70	70
80	80
90	90
100	100

SILICA GEL
WEIGHT.

ORSAT MEASUREMENT

TIME | CO₂ | O₂ | CO | N₂

COMMENTS:

24/

H5-2

PARTICULATE EMISSION CALCULATION

Plant: *SARLES, NETH. DAKOTA* Orsat Analysis: (Dry Basis, % by Vol.), Average
 Location: *ELEVATOR HEADHOUSE* CO₂ *ZERO*
 Stack or Source: *HOUSE SYSTEM* O₂ *20.9*
 Date: *8 JULY 1976* CO *ZERO*
 Run No.: *TWO (2)* N₂ *79.1*
 Operator: *R.J.B., O.F.F., M.W.O.* Water Collected, GMS.: *30*
 Bar. Pr., In. Hg: *28.46 ABSOLUTE* Filter No.: *B*
 Nozzle Dia, In.: *0.25 (1/4)"* Particulate Collected, GMS.:
 Stack Dia., In.: *19" Ø* Filter *0.0261*
 Cp: *0.84* Probe Wash *0.0322*
 Total Time, Min.: *60 (1 HOUR)*
 Vol. Through Gas Meter, Cu. Ft.: FRONT END TOTAL *0.0583*

Impinger Catch

FRONT PLUS BACK END CATCH TOTAL

Standard Conditions: Dry Gas at 15.6°C and 29.92 in. Hg.

C - 1 Calculate Average Meter Temperature

T_m = The average of both inlet and outlet temperatures
 obtained during sampling, 569 °R.

C - 2 Calculate Sample Volume at Standard Conditions

$$V_{mstd} = \text{SCF (Dry) Through meter}$$

$$= 17.32 \frac{V_m}{T_m} \times P_m$$

$$= 17.32 \frac{81.63}{28.76}$$

$$= 569$$

$$= 75.91 \text{ SCF (Dry)}$$

Where: V_m = Dry gas measured by meter, cu.ft.

P_m = Abs. Pr. at meter (use barometric pressure, uncorrected for altitude), In. Hg

C - 3 Calculate Volume Fraction Water in Flue Gas

$$V_{wstd} = \text{Water vapor in SCF}$$

$$= 0.0465 V_{lc}$$

$$= 0.0465 \cdot 30$$

$$= 1.40 \text{ SCF}$$

$$B_{wo} = \text{Water } \frac{V}{V}$$

$$= \frac{V_{wstd}}{(V_{wstd} + V_{mstd})}$$

$$= \frac{1.40}{1.40 + 75.91}$$

$$= 0.0181$$

$$\frac{1.40}{(77.31)} + \frac{75.91}{77.31}$$

Where

V_{lc} = Weight of water collected in impingers plus that gained by drierite, GMS

21
H5-2

C - 4 Calculate Dry and Wet Molecular Weight of Stack Gas

$$M_d = \text{Dry Mol. Wt.}$$

$$= 0.44 (\% \text{ CO}_2) + 0.32 (\% \text{ O}_2)$$

$$+ 0.28 (\% \text{ N}_2 + \text{CO})$$

$$= 0.44 \times \underline{\text{ZERO}} + 0.32 \times \underline{20.9 \div 6.69} + 0.28 \times \underline{79.1 \div 22.15}$$

$$= \underline{28.84}$$

$$M_s = \text{Wet Mol. Wt.}$$

$$= M_d (1 - B_{wo}) + 18 B_{wo}$$

$$= \underline{28.84} \times \underline{0.9819} + 18 \times \underline{0.0181}$$

$$= \underline{28.64} \quad \underline{0.326}$$

C - 5 Calculate The Average $\sqrt{\Delta P}$, ($\sqrt{\Delta P}$) Avg., Obtained during gas sample acquisition

$$(\sqrt{\Delta P}) \text{ Avg.} = \underline{1.231}$$

C - 6 Calculate The Average Stack Gas Temperature, T_s , at time of Gas Sample Acquisition

$$T_s = \underline{595} \text{ } ^\circ\text{R}$$

C - 7 Calculate The Average Stack Gas Velocity

$$(V_s) \text{ Avg.} = 85.48 \times C_p \times (\sqrt{\Delta P}) \text{ Avg.}$$

$$= 85.48 \times \underline{0.84} \times \underline{1.231}$$

$$= \underline{72.21} \text{ ft./sec}$$

$$\sqrt{\frac{T_s}{P_s \times M_s}} = \sqrt{\frac{595}{28.50 \times 28.64}} = \underline{0.817}$$

Where:

C_p = Pitot Tube Coefficient

P_s = Absolute Stack Gas Press., In. Hg.

C - 8 Calculate Stack Cross Sectional Area at Sampling Site

$$A_s = \underline{1.97} \text{ Sq. Ft.}$$

C - 9 Calculate Stack Gas Average Volumetric Flow Rate

Q_s = Stack Gas Flow Rate, SCFM (Dry)

$$= 1043 \times (1 - B_{wO}) (V_s)_{\text{Avg.}} \times A_s \times \frac{P_s}{T_s}$$

$$= \underline{1043} \times \underline{0.9819} \times \underline{72.21} \times \underline{1.97} \times \underline{28.50}$$

$$= \underline{7,620} \text{ SCFM (Dry)} \quad \underline{545}$$

C - 10 Calculate Isokinetic Sampling Efficiency

$$I = \frac{0.0032 \{ (V_{wstd} + V_{mstd}) \times T_s \times P_m}{\theta \times A_n \times (V_s)_{\text{Avg.}} \times P_s}$$

$$= \frac{0.0032 \{ \times \underline{77.31} \times \underline{545} \times \underline{28.46}}{\underline{60} \times \underline{0.000341} \times \underline{72.21} \times \underline{28.50}}$$

$$= \underline{91.4} \%$$

θ = Total Sampling Time, Min.

A_n = Nozzle Opening, Sq. Ft.

C - 11 Calculate Heat Input during testing period

Z = Total Heat Input Rate to Boiler, MEGA BTU/hr.

$$= W_1 \times H_1 =$$

$$+ W_2 \times H_2$$

$$+ W_3 \times H_3$$

= TOTAL

$$= \underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

TOTAL MEGA BTU/hr.

Where W_1 , W_2 , & W_3 = hourly fuel input of respective fuels and
 H_1 , H_2 , & H_3 = gross (as received) heating value of respective
 fuels in mega BTU per input unit (consistent with fuel input unit).

C - 12 Calculate Front End Particulate Grain Loading (with Front
 Half Washings Only)

$$C_s' = \text{Part. Grain Loading, gr/SCF (Dry)}$$

$$= 15.42 \times \frac{M_n}{V_{mstd}}$$

$$= 15.42 \times \frac{0.0583}{75.91}$$

$$= \underline{0.012} \text{ gr/SCF (Dry)}$$

Where

M_n = Total Particulate Collected (Filter Plus Front Half
 Washings Only), GMS

C - 13 Calculate Front End Emission Factor

E_t = Hourly Mass Rate, lbs/hr.

$$= 0.00857 \times C_s' \times Q_s$$

$$= 0.00857 \times \underline{0.012} \times \underline{7,620}$$

$$= \underline{0.78} \text{ lbs/hr.}$$

E_h = Front End Emission Factor, lbs/MEGA BTU

$$= \frac{E_t}{Z}$$

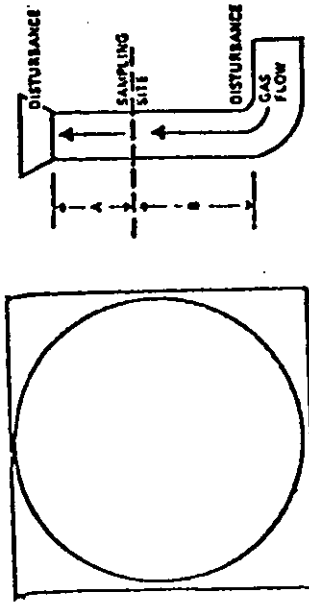
$$= \underline{\hspace{2cm}}$$

$$= \underline{\hspace{2cm}}$$

$$= \underline{\hspace{2cm}} \text{ lbs/MEGA BTU}$$

PARTICULATE FIELD DATA

SCHEMATIC OF STACK



CROSS SECTION

F. part

PLANT Sarges, W. M. AMBIENT TEMPERATURE 80
 DATE 8 July 1976 BAROMETRIC PRESSURE 28.96
 LOCATION East Henon House ASSUMED MOISTURE, % 2.203
 OPERATOR E. J. B. O. G. S. M. A. D. O. PROBE LENGTH, in. 36
 STACK NO. House System NOZZLE DIAMETER, in. 0.935
 RUN NO. Three (3) STACK DIAMETER, in. 19"
 SAMPLE BOX NO. 2383-3 PROBE HEATER SETTING None
 METER BOX NO. 2383-3 HEATER BOX SETTING None

WEIGHT OF PARTICULATE COLLECTED, mg			
SAMPLE	FILTER	PROBE WASH	
FINAL WEIGHT	0.6921	67.8019	
TARE WEIGHT	0.6783	67.8816	
WEIGHT GAIN	0.0138	0.0203	
TOTAL 0.0331			

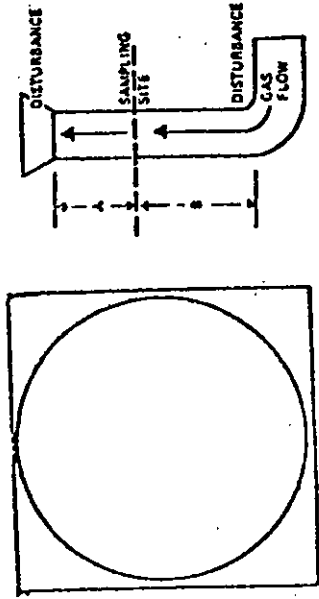
TRAVERSE POINT NUMBER	SAMPLING TIME (H), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD (AP ₃) (1/AP ₃)	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (ΔH) in. H ₂ O		GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER		TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER F	PUMP VACUUM in. Hg gauge	VELOCITY f/s
					ACTUAL	DESIRED		INLET (T _{m, in}), °F	OUTLET (T _{m, out}), °F			
1	1745	+0.6	85	1.6	7.1	7.1	485.303	95	95	85	1702	
2				1.6	7.1	7.1	497	97	97			
3	1748			1.6	7.1	7.1	499	97	97			
4				1.6	7.1	7.1	501	97	97			
5	1751			1.6	7.1	7.1	503	104	97			
6				1.6	7.1	7.1	506	104	97			
7	1754			1.6	7.1	7.1	509	104	97			
8				1.7	7.7	7.7	511	104	97			
9	1757			1.7	7.7	7.7	514	104	97			
10				1.7	7.7	7.7	516	104	97			
11	1800			1.7	7.7	7.7	518	104	97			
12				1.7	7.7	7.7	520	104	97			
13	1803			1.7	7.7	7.7	521	104	97			
14				1.7	7.7	7.7	524	104	97			
15	1806	V	V	1.7	7.7	7.7	526	104	97	V	V	
TOTAL												
AVERAGE												

COMMENTS:

VOLUME OF LIQUID WATER COLLECTED		IMPINGER VOLUME ml				SILICA GEL WEIGHT, g		ORSAT MEASUREMENT				TIME				CO ₂ O ₂ CO N ₂			
FINAL		1	2	3	4							1							
INITIAL												2							
LIQUID COLLECTED												3							
												4							

SYNTHETIC

CROSS SECTION



E. Port

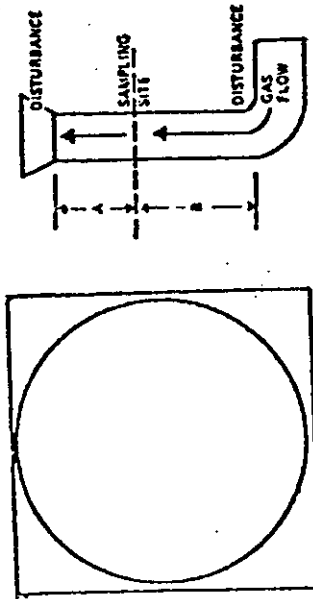
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AVERAGE

COMMENTS:

VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml				SILICA GEL WEIGHT, g	ORSAT MEASUREMENT				
	1	2	3	4		TIME	CO ₂	O ₂	CO	N ₂
FINAL						1				
INITIAL						2				
LIQUID COLLECTED						3				
						4				

SCHEMATIC OF STACK



CROSS SECTION

N. PORT

PLANT SANES, INC. AMBIENT TEMPERATURE 80
 DATE 8 JULY 1976 BAROMETRIC PRESSURE 28.96
 LOCATION ELEC. HOUSE ASSUMED MOISTURE, % 2.03
 OPERATOR E.T.B. D.C.G. M.A.O. PROBE LENGTH, in. 36
 STACK NO. HOUSE SYSTEM NOZZLE DIAMETER, in. 0.25
 RUN NO. THREE (3) STACK DIAMETER, in. 19"
 SAMPLE BOX NO. 2383-3 PROBE HEATER SETTING NONE
 METER BOX NO. 2383-3 HEATER BOX SETTING NONE

METER AM, 0.84
 C FACTOR 0.84

PROCESS WEIGHT RATE

WEIGHT OF PARTICULATE COLLECTED, mg

SAMPLE	FILTER	PROBE WASH
FINAL WEIGHT	0.6921	0.9019
TARE WEIGHT	0.6793	0.8816
WEIGHT GAIN	0.0128	0.0203
TOTAL		0.0331

TRAVERSE POINT NUMBER	SAMPLING TIME (H), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD (AP), (VAP) ²	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (ΔH) in. H ₂ O		GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER		SAMPLE BOX TEMPERATURE °F	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER F	PUMP VACUUM in. Hg gauge	VELOCITY fps
					ACTUAL	DESIRED		INLET (T _{min}), °F	OUTLET (T _{mount}), °F				
1	1818	+0.6	85	1.15	5.2	5.2	538	109	98	85	85	170.2	
2				1.15	5.2	5.2	541	109	98				
3	1821			1.15	5.2	5.2	542	109	98				
4				1.15	5.2	5.2	544	109	98				
5	1824			1.15	5.2	5.2	545	109	98				
6				1.15	5.2	5.2	548	109	98				
7	1827			1.15	5.2	5.2	550	109	98				
8				1.15	5.2	5.2	552	109	98				
9	1830			1.15	5.2	5.2	554	109	98				
10				1.15	5.2	5.2	556	109	98				
11	1833			1.15	5.2	5.2	558	109	98				
12				1.15	5.2	5.2	561	109	98				
13	1836			1.15	5.2	5.2	562	109	98				
14				1.15	5.2	5.2	564	109	98				
15	1839	V	V	1.15	5.2	5.2	565	109	98	V	V	V	
TOTAL													

AVERAGE

VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml				ORSAT MEASUREMENT				TIME				COMMENTS			
	1	2	3	4	CO ₂	O ₂	CO	N ₂	1	2	3	4	1	2	3	4
FINAL																
INITIAL																
LIQUID COLLECTED																

H5-3

PARTICULATE EMISSION CALCULATION

Plant: *SARLES, N. DAKOTA* Orsat Analysis: (Dry Basis, % by Vol.), Average

Location: *ELEVATOR HEADHOUSE* CO₂ *ZERO*

Stack or Source: *HOUSE SYSTEM* O₂ *20.9*

Date: *8 JULY 1976* CO *ZERO*

Run No.: *THREE (3)* N₂ *79.1*

Operator: *F.J.B., D.F.F., M.W.O.* Water Collected, GMS.: *28*

Bar. Pr., In. Hg: *28.96 ABSOLUTE* Filter No.: *C*

Nozzle Dia, In.: *0.25 (1/4)"* Particulate Collected, GMS.:

Stack Dia., In.: *19" Ø* Filter *0.0128*

Cp: *0.84* Probe Wash *0.0203*

Total Time, Min.: *60*

Vol. Through Gas Meter, Cu. Ft.: FRONT END TOTAL *0.0331*

Impinger Catch

FRONT PLUS BACK END CATCH TOTAL ~~~~~

Standard Conditions: Dry Gas at *15.6°C* and *29.92 in. Hg.*

C - 1 Calculate Average Meter Temperature

T_m = The average of both inlet and outlet temperatures obtained during sampling, *562* °R.

C - 2 Calculate Sample Volume at Standard Conditions

$$\begin{aligned}
 V_{mstd} &= \text{SCF (Dry) Through meter} \\
 &= 17.32 \frac{V_m}{T_m} \times P_m \\
 &= 17.32 \frac{87.93}{28.76} \\
 &= \underline{562} \\
 &= \underline{77.12} \text{ SCF (Dry)}
 \end{aligned}$$

Where: V_m = Dry gas measured by meter, cu.ft.

P_m = Abs. Pr. at meter (use barometric pressure, uncorrected for altitude), In. Hg

C - 3 Calculate Volume Fraction Water in Flue Gas

$$\begin{aligned}
 V_{wstd} &= \text{Water vapor in SCF} \\
 &= 0.0465 V_{lc} \\
 &= 0.0465 \cdot 28 \\
 &= \underline{1.30} \text{ SCF} \\
 B_{wo} &= \text{Water } \frac{V}{V} \\
 &= \frac{V_{wstd}}{(V_{wstd} + V_{mstd})} \\
 &= \frac{1.30}{1.30 + 77.12} = \underline{0.0166}
 \end{aligned}$$

Where

V_{lc} = Weight of water collected in impingers plus that gained by drierite, GMS

C - 4 Calculate Dry and Wet Molecular Weight of Stack Gas

$$M_d = \text{Dry Mol. Wt.}$$

$$= 0.44 (\% \text{ CO}_2) + 0.32 (\% \text{ O}_2)$$

$$+ 0.28 (\% \text{ N}_2 + \text{CO})$$

$$= 0.44 \times \underline{\text{ZERO}} + 0.32 \times \underline{20.9} = 6.69 + 0.28 \times \underline{79.1} = 22.15$$

$$= \underline{28.84}$$

$$M_s = \text{Wet Mol. Wt.}$$

$$= M_d (1 - B_{wo}) + 18 B_{wo}$$

$$= \underline{28.84} \times \underline{0.9834} + 18 \times \underline{0.0166}$$

$$= \underline{28.66} \quad \underline{0.30}$$

C - 5 Calculate The Average $\sqrt{\Delta P}$, ($\sqrt{\Delta P}$) Avg., Obtained during gas sample acquisition

$$(\sqrt{\Delta P}) \text{ Avg.} = \underline{1.207}$$

C - 6 Calculate The Average Stack Gas Temperature, T_s , at time of Gas Sample Acquisition

$$T_s = \underline{545} \text{ } ^\circ\text{R}$$

C - 7 Calculate The Average Stack Gas Velocity

$$(V_s) \text{ Avg.} = 85.48 \times C_p \times (\sqrt{\Delta P}) \text{ Avg.}$$

$$= 85.48 \times \underline{0.87} \times \underline{1.207}$$

$$= \underline{70.81} \text{ ft./sec}$$

$$\sqrt{\frac{T_s}{P_s \times M_s}} = \sqrt{\frac{545}{28.50 \times 28.66}} = \underline{0.817}$$

Where:

C_p = Pitot Tube Coefficient

P_s = Absolute Stack Gas Press., In. Hg.

HS-3
37

C - 8 Calculate Stack Cross Sectional Area at Sampling Site

$$A_s = \underline{1.97} \text{ Sq. Ft.}$$

C - 9 Calculate Stack Gas Average Volumetric Flow Rate

Q_s = Stack Gas Flow Rate, SCFM (Dry)

$$= 1043 \times (1 - B_{wO}) (V_s)_{\text{Avg.}} \times A_s \times \frac{P_s}{T_s}$$

$$= \underline{1043} \times \underline{0.9832} \times \underline{70.81} \times \underline{1.97} \times \underline{28.50}$$

$$= \underline{7,780} \text{ SCFM (Dry)} \quad \underline{545}$$

C - 10 Calculate Isokinetic Sampling Efficiency

$$I = \frac{0.00321 (V_{wstd} + V_{mstd}) \times T_s \times P_m}{\theta \times A_n \times (V_s)_{\text{Avg.}} \times P_s}$$

$$= 0.00321 \times \underline{78.92} \times \underline{545} \times \underline{28.46}$$

$$\underline{60} \times \underline{0.000341} \times \underline{70.81} \times \underline{28.50}$$

$$= \underline{97.6} \%$$

θ = Total Sampling Time, Min.

A_n = Nozzle Opening, Sq. Ft.

C - 11 Calculate Heat Input during testing period

Z = Total Heat Input Rate to Boiler, MEGA BTU/hr.

$$= W_1 \times H_1 =$$

$$+ W_2 \times H_2$$

$$+ W_3 \times H_3$$

= TOTAL

$$= \underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

TOTAL MEGA BTU/hr.

Where $W_1, W_2, \& W_3$ = hourly fuel input of respective fuels and
 $H_1, H_2, \& H_3$ = gross (as received) heating value of respective
fuels in mega BTU per input unit (consistent with fuel input unit).

C - 12 Calculate Front End Particulate Grain Loading (with Front
Half Washings Only)

C_s' = Part. Grain Loading, gr/SCF (Dry)

$$\begin{aligned} &= 15.42 \times \frac{M_n}{V_{mstd}} \\ &= 15.42 \times \frac{0.0331}{27.12} \\ &= \underline{0.007} \text{ gr/SCF (Dry)} \end{aligned}$$

Where

M_n = Total Particulate Collected (Filter Plus Front Half
Washings Only), GMS

C - 13 Calculate Front End Emission Factor

$$\begin{aligned} E_t &= \text{Hourly Mass Rate, lbs/hr.} \\ &= 0.00857 \times C_s' \times Q_s \\ &= 0.00857 \times \underline{0.007} \times \underline{7,480} \\ &= \underline{0.45} \text{ lbs/hr.} \end{aligned}$$

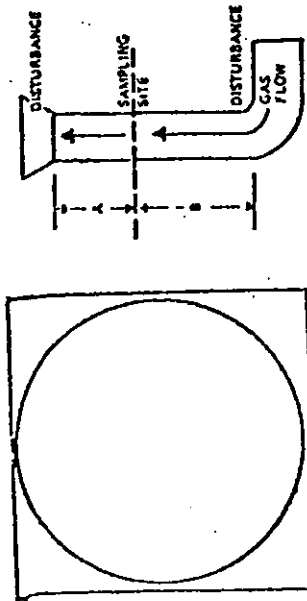
E_h = Front End Emission Factor, lbs/MEGA BTU

$$\begin{aligned} &= \frac{E_t}{Z} \\ &= \underline{\hspace{2cm}} \\ &= \underline{\hspace{2cm}} \\ &= \underline{\hspace{2cm}} \text{ lbs/MEGA BTU} \end{aligned}$$

SCHEMATIC OF STACK

METER NO. 0.872
C FACTOR 0.872

PLANT SARES, N. W. AMBIENT TEMPERATURE 80.5
DATE 9 July 1976 BAROMETRIC PRESSURE 28.69
LOCATION ECU. HENRIQUEZ ASSUMED MOISTURE, % 27.3
OPERATOR E. J. B. G. S. S. M. A. D. PROBE LENGTH, in. 36
STACK NO. CRIPAN CANNER NOZZLE DIAMETER, in. 0.25
RUN NO. ONE (1) STACK DIAMETER, in. 17.11
SAMPLE BOX NO. 2383-3 PROBE HEATER SETTING NONE
METER BOX NO. 2383-3 HEATER BOX SETTING NONE



CROSS SECTION

N. part

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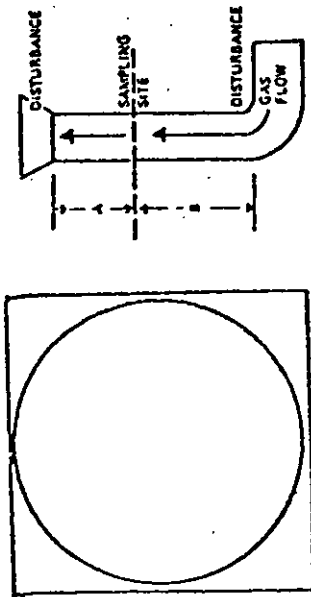
AVERAGE

VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml				SILICA GEL WEIGHT, g	ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
	1	2	3	4							
FINAL						1					
INITIAL						2					
LIQUID COLLECTED						3					
LIQUID COLLECTED					22.5	4					

COMMENTS:

39

SYNTHETIC OF SYACK



CROSS SECTION

N. post

PLANT SARLES, N. d. AMBIENT TEMPERATURE 24 F
DATE 9 JULY 1976 BAROMETRIC PRESSURE 28.62
LOCATION EVEN. HENHOUSE ASSUMED MOISTURE, % 27.3
OPERATOR E. J. B. D. S. S. M. A. O. PROBE LENGTH, in. 36
STACK NO. CRIPPER CEMENT NOZZLE DIAMETER, in. 0.25
RUN NO. ONE(1) STACK DIAMETER, in. 17"
SAMPLE BOX NO. 2373-3 PROBE HEATER SETTING NONE
METER BOX NO. 2373-3 HEATER BOX SETTING NONE

METER NO. _____
C FACTOR 0.84
PROCESS WEIGHT RATE _____

WEIGHT OF PARTICULATE COLLECTED, mg			
SAMPLE	FILTER	PROBE WASH	
FINAL WEIGHT	0.7691	61.7069	
TARE WEIGHT	0.6785	61.3238	
WEIGHT GAIN	0.0906	0.0231	
TOTAL		0.0537	

[illegible]

LYFRAGE

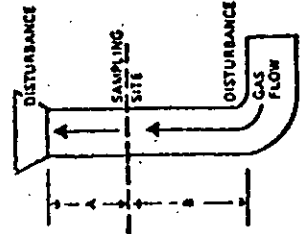
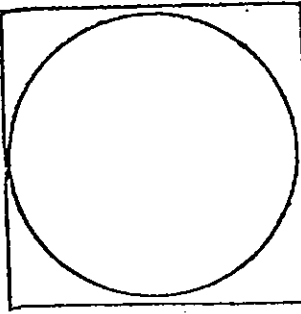
VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml	SILICA GEL WEIGHT, g
1	2	3
4	3	4

ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
1					
2					
3					
4					

COMMENTS:

Conclusion

40



20.25

PLANT SARLES, M. L. AMBIENT TEMPERATURE 20.1
DATE 9 JULY 1976 BAROMETRIC PRESSURE 28.69
LOCATION GREEN, HENDONHOUSE ASSUMED MOISTURE, % 270.3
OPERATOR F. J. B., D. S. S., M. W. O. PROBE LENGTH, in. 36
STACK NO. CRIPPER CEMEX NOZZLE DIAMETER, in. 0.25
RUN NO. ONE (1) STACK DIAMETER, in. 17"
SAMPLE BOX NO. 2393-3 PROBE HEATER SETTING NONE
METER BOX NO. 2393-3 HEATER BOX SETTING NONE

METER A.H. 0.82
CE FACTOR 0.82

PROCESS WEIGHT RATE

WEIGHT OF PARTICULATE COLLECTED, mg			
SAMPLE	FILTER	PROBE WASH	
FINAL WEIGHT	0.7091	61.4068	
TARE WEIGHT	0.6782	61.3438	
WEIGHT GAIN	0.0306	0.0631	
TOTAL			0.0537

[illegible]

COMMENTS:

VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml				SILICA GEL WEIGHT, g	ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
	1	2	3	4							
FINAL						1					
INITIAL						2					
LIQUID COLLECTED						3					
TOTAL VOLUME COLLECTED					23.5	4					

CR-1

PARTICULATE EMISSION CALCULATION

Plant: *SARLES, N. DAKOTA* Orsat Analysis: (Dry Basis, % by Vol.), Average

Location: *ELEVATOR HEADHOUSE* CO₂ *ZERO*

Stack or Source: *CRIPPEN CLEANER* O₂ *20.9*

Date: *9 JULY 1976* CO *ZERO*

Run No.: *ONE (1)* N₂ *79.1*

Operator: *F.J.B., D.F.R., M.W.O.* Water Collected, GMS.: *23.5*

Bar. Pr., In. Hg: *28.69 Absolute* Filter No.: *0*

Nozzle Dia, In.: *0.25 (1/4)"* Particulate Collected, GMS.: *0.0306*

Stack Dia., In.: *17" Ø* Filter *0.0306*

Cp: *0.82* Probe Wash *0.0231*

Total Time, Min.: *72*

Vol. Through Gas Meter, Cu. Ft.: FRONT END TOTAL *0.0537*

Impinger Catch

FRONT PLUS BACK END CATCH TOTAL

Standard Conditions: Dry Gas at 15.6°C and 29.92 in. Hg.

C - 1 Calculate Average Meter Temperature

T_m = The average of both inlet and outlet temperatures obtained during sampling, *545.9* °R.

C - 2 Calculate Sample Volume at Standard Conditions

$$\begin{aligned}
 V_{mstd} &= \text{SCF (Dry) Through meter} \\
 &= 17.32 \frac{V_m}{T_m} \times P_m \\
 &= 17.32 \frac{18.91}{28.69} \times 28.69 \\
 &= \underline{585.9} \\
 &= \underline{71.83} \text{ SCF (Dry)}
 \end{aligned}$$

Where: V_m = Dry gas measured by meter, cu.ft.

P_m = Abs. Pr. at meter (use barometric pressure, uncorrected for altitude), In. Hg

C - 3 Calculate Volume Fraction Water in Flue Gas

$$\begin{aligned}
 V_{wstd} &= \text{Water vapor in SCF} \\
 &= 0.0465 V_{lc} \\
 &= 0.0465 \cdot 23.5 \\
 &= \underline{1.09} \text{ SCF}
 \end{aligned}$$

$$\begin{aligned}
 B_{wo} &= \text{Water } \frac{V}{V} \\
 &= \frac{V_{wstd}}{(V_{wstd} + V_{mstd})} \\
 &= \frac{1.09}{1.09 + 71.83} = \underline{0.0149} \\
 &= \frac{1.09}{(72.92)}
 \end{aligned}$$

Where

V_{lc} = Weight of water collected in impingers plus that gained by drierite, GMS

C - 4 Calculate Dry and Wet Molecular Weight of Stack Gas

$$M_d = \text{Dry Mol. Wt.}$$

$$= 0.44 (\% \text{ CO}_2) + 0.32 (\% \text{ O}_2)$$

$$+ 0.28 (\% \text{ N}_2 + \text{CO})$$

$$= 0.44 \times \underline{\text{ZERO}} + 0.32 \times \underline{20.9 = 6.69} + 0.28 \times \underline{79.1 = 22.15}$$

$$= \underline{28.87}$$

$$M_s = \text{Wet Mol. Wt.}$$

$$= M_d (1 - B_{wo}) + 18 B_{wo}$$

$$= \underline{28.87} \times \underline{0.9851} + 18 \times \underline{0.0149}$$

$$= \underline{28.68} \quad \underline{0.268}$$

C - 5 Calculate The Average $\sqrt{\Delta P}$, ($\sqrt{\Delta P}$) Avg., Obtained during gas sample acquisition

$$(\sqrt{\Delta P}) \text{ Avg.} = \underline{0.867}$$

C - 6 Calculate The Average Stack Gas Temperature, T_s , at time of Gas Sample Acquisition

$$T_s = \underline{570} \text{ } ^\circ\text{R}$$

C - 7 Calculate The Average Stack Gas Velocity

$$(V_s) \text{ Avg.} = 85.48 \times C_p \times (\sqrt{\Delta P}) \text{ Avg.}$$

$$= 85.48 \times \underline{0.87} \times \underline{0.867}$$

$$= \underline{50.73} \text{ ft./sec}$$

$$\sqrt{\frac{T_s}{P_s \times M_s}} = \sqrt{\frac{570}{28.70 \times 28.68}} = \underline{0.81}$$

Where:

C_p = Pitot Tube Coefficient

P_s = Absolute Stack Gas Press., In. Hg.

46
CR-1

C - 8 Calculate Stack Cross Sectional Area at Sampling Site

$$A_s = \underline{1.58} \text{ Sq. Ft.}$$

C - 9 Calculate Stack Gas Average Volumetric Flow Rate

Q_s = Stack Gas Flow Rate, SCFM (Dry)

$$= 1043 \times (1 - B_{wO}) (V_s)_{\text{Avg.}} \times A_s \times \frac{P_s}{T_s}$$

$$= \underline{1043} \times \underline{0.9851} \times \underline{50.43} \times \underline{1.58} \times \underline{28.70}$$

$$= \underline{7,350} \text{ SCFM (Dry)} \quad \underline{540}$$

C - 10 Calculate Isokinetic Sampling Efficiency

$$I = \frac{0.0032 \{ (V_{wstd} + V_{mstd}) \times T_s \times P_m}{\theta \times A_n \times (V_s)_{\text{Avg.}} \times P_s}$$

$$= 0.0032 \times \underline{72.92} \times \underline{540} \times \underline{28.69}$$

$$\underline{72} \times \underline{0.000391} \times \underline{50.43} \times \underline{28.70}$$

$$= \underline{102.1} \%$$

θ = Total Sampling Time, Min.

A_n = Nozzle Opening, Sq. Ft.

C - 11 Calculate Heat Input during testing period

Z = Total Heat Input Rate to Boiler, MEGA BTU/hr.

$$= W_1 \times H_1 =$$

$$+ W_2 \times H_2$$

$$+ W_3 \times H_3$$

= TOTAL

$$= \underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

TOTAL MEGA BTU/hr.

CR-1
47

Where $W_1, W_2, & W_3$ = hourly fuel input of respective fuels and
 $H_1, H_2, & H_3$ = gross (as received) heating value of respective
fuels in mega BTU per input unit (consistent with fuel input unit).

C - 12 Calculate Front End Particulate Grain Loading (with Front
Half Washings Only)

C_s' = Part. Grain Loading, gr/SCF (Dry)

$$= 15.42 \times \frac{M_n}{V_{mstd}}$$

$$= 15.42 \times 0.0537$$

$$\underline{71.83}$$

$$= \underline{0.012} \text{ gr/SCF (Dry)}$$

Where

M_n = Total Particulate Collected (Filter Plus Front Half
Washings Only), GMS

C - 13 Calculate Front End Emission Factor

E_t = Hourly Mass Rate, lbs/hr.

$$= 0.00857 \times C_s' \times Q_s$$

$$= 0.00857 \times 0.012 \times 8,350$$

$$= \underline{0.75} \text{ lbs/hr.}$$

E_h = Front End Emission Factor, lbs/MEGA BTU

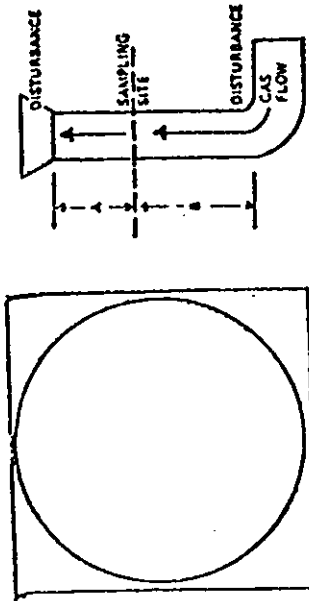
$$= \frac{E_t}{Z}$$

$$= \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}}$$

$$= \underline{\hspace{2cm}} \text{ lbs/MEGA BTU}$$

SCHEMATIC OF STACK



CROSS SECTION

N. PORT

PLANT SURVEY, N. PORT
 DATE 9 JULY 1976
 LOCATION FUEL HANDLING
 OPERATOR E. J. O. R. A. S. M. A. O.
 STACK NO. CRIPPER LUMBER
 RUN NO. TWO (2)
 SAMPLE BOX NO. 2383-3
 METER BOX NO. 2383-3

METER NO. 0.88
 C FACTOR 0.88
 PROCESS WEIGHT RATE
 WEIGHT OF PARTICULATE COLLECTED, mg
 SAMPLE FILTER PROBE WASH
 FINAL WEIGHT 0.1241 0.03331
 TARE WEIGHT 0.0513 0.03165
 WEIGHT GAIN 0.0189 0.0166
 TOTAL 0.0354

TRAVERSE POINT NUMBER	SAMPLING TIME (H), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD (AP ₁) (√AP ₁)	VELOCITY (ft/min)	DIFFERENTIAL PRESSURE ACROSS ORIFICE METER (ΔH, in. H ₂ O)	ACTUAL DESIRED (in. H ₂ O)	GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER INLET (T _m), °F	OUTLET (T _m), °F	SAMPLE BOX TEMPERATURE °F	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER °F	PUMP VACUUM in. Hg gauge	VELOCITY ft/min
1	1214	40.2	80	0.62	787	2.8	2.8	658.200	98	92	80	80	10.2	
2	1216			0.62	"	2.8	2.8	657	98	92				
3	1218			0.62	"	2.8	2.8	659	98	92				
4	1220			0.62	"	2.8	2.8	661	98	92				
5	1222			0.62	"	2.8	2.8	662	98	92				
6	1224			0.25	866	3.3	3.3	667	98	92				
7	1226			0.25	"	3.3	3.3	666	98	92				
8	1228			0.29	889	3.5	3.5	669	98	92				
9	1230			0.29	"	3.5	3.5	670	98	92				
10	1232			0.29	"	3.5	3.5	672	98	92				
11	1234			0.29	"	3.5	3.5	674	98	92				
12	1236			0.29	"	3.5	3.5	677	98	92				
13	1238			0.29	"	3.5	3.5	680	98	92				
14	1240			0.29	"	3.5	3.5	681	98	92				
15	1242			0.29	"	3.5	3.5	683	98	92				
TOTAL														

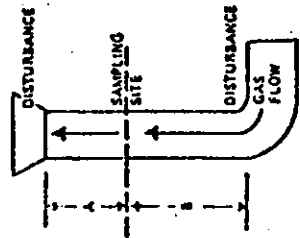
AVERAGE

VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml	SILICA GEL WEIGHT, g
FINAL		
INITIAL		
LIQUID COLLECTED		
TOTAL VOLUME COLLECTED		96

COMMENTS:

ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	H ₂
1					
2					
3					
4					

SCHEMATIC OF TRACK



N. B. 1345

METER NO. _____
C FACTOR _____ 0.24

PROCESS WEIGHT RAYE

WEIGHT OF PARTICULATE COLLECTED, mg			
SAMPLE	FILTER	PROBE WEA	
FINAL WEIGHT	0.6701	62.535	
TARE WEIGHT	0.6513	62.516	
WEIGHT GAIN	0.0188	0.019	
TOTAL			0.035

SAMPLE BOX NO.	2323-3	PROBE HEATER SETTING	NONE
HEATER BOX NO.	2323-3	HEATER BOX SETTING	NONE

AVERAGE

[illegible]

IMPINGER
VOLUME ml

ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
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COMMENTS:

49

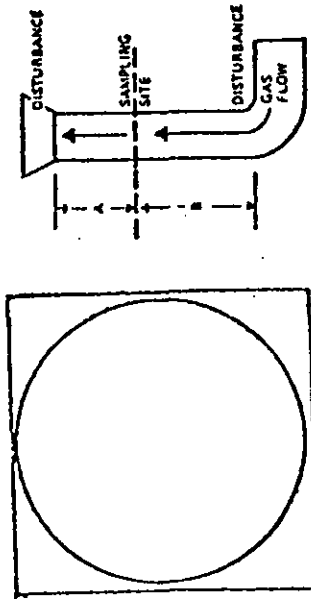
COPIES COLLECTED

FINAL	INITIAL
-------	---------

FINAL	INITIAL	LIQUID COLLECTED
-------	---------	------------------

METER NO. _____
 CEACTION _____

PLANT SARLES, N. D. AMBIENT TEMPERATURE 80 F
DATE 9 July 1976 BAROMETRIC PRESSURE 28.69
LOCATION Engl. Henhouse ASSUMED MOISTURE, % 27.03
OPERATOR F. J. B., D. C. S., M. A. O. PROBE LENGTH, in. 36
STACK NO. CERRAN CERRAR NOZZLE DIAMETER, in. 0.935
RUN NO. Two (2) STACK DIAMETER, in. 17"
SAMPLE BOX NO. 2383-3 PROBE HEATER SETTING NONE
HEATER BOX NO. 2383-3 HEATER BOX SETTING NONE



CROSS SECTION

F. 2011

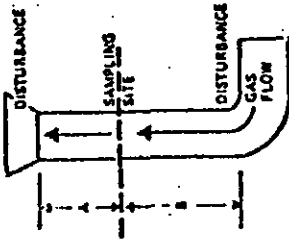
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AVERAGE

VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml				SILICA GEL WEIGHT, g	ORSAT MEASUREMENT				
	1	2	3	4		TIME	CO ₂	O ₂	CO	N ₂
FINAL						1				
INITIAL						2				
LIQUID COLLECTED						3				
					21	4				

СЛІДНОВ

SCHEMATIC OF STACK



Port

METER IN: _____
CFactor: 0.82

PROCESS WEIGHT RATE

WEIGHT OF PARTICULATE COLLECTED, mg

SAMPLE	FILTER	PROBE WASH
FINAL WEIGHT	2.5721	0.1533
TARE WEIGHT	2.5743	0.1565
WEIGHT GAIN	0.0188	0.0166
TOTAL		0.0354

TOTAL A. A359.

TRAVERSE POINT NUMBER	SAMPLING TIME (H), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD ($\Delta P_s / \rho V^2$)	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (in. H ₂ O)		GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER		SAMPLE BOX TEMPERATURE °F	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER F	PUMP VACUUM in. Hg gauge	VELOCITY f/s
					(ΔH) ACTUAL DESIRED	INLET (T _{MIn}), °F		OUTLET (T _{MOut}), °F					
16	1329	70.2	80	.71	3.2	3.2	723	111	98	80	80	70.2	
17	1326		V	.69	3.1	3.1	725	111	98	- V	V	V	
18	1328	V	V	.71	3.2	3.2	727	111	98	- V	V	V	
							END =						
							729.6						
TOTAL	72	70.2	80						3645	3367			
AVERAGE	2	70.2	80	X	31.362				101.25	93.53			1.5

COMMENTS:

VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml				SILICA GEL WEIGHT, g	ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
	1	2	3	4							
FINAL						1					
INITIAL						2					
						3					

51

4/1/76

52

CR-2

PARTICULATE EMISSION CALCULATION

Plant: *SARLES, N. DAKOTA* Orsat Analysis: (Dry Basis, % by Vol.), Average
 Location: *ELEVATOR HEADHOUSE* CO₂ *ZERO*
 Stack or Source: *CRIPPEN CLEANER* O₂ *20.9*
 Date: *9 JULY 1976* CO *ZERO*
 Run No.: *TWO (2)* N₂ *79.1*
 Operator: *F.J.B., D.F.R., M.W.O.* Water Collected, GMS.: *26*
 Bar. Pr., In. Hg: *28.69 ABSOLUTE* Filter No.: *E*
 Nozzle Dia, In.: *0.25 (1/4)"* Particulate Collected, GMS.:
 Stack Dia., In.: *17" Ø* Filter *0.0188*
 Cp: *0.84* Probe Wash *0.0166*
 Total Time, Min.: *72*
 Vol. Through Gas Meter, Cu. Ft.: FRONT END TOTAL *0.0354*
 Impinger Catch
 FRONT PLUS BACK END CATCH TOTAL ~~~~~

Standard Conditions: Dry Gas at *15.6°C* and *29.92 in. Hg.*

C - 1 Calculate Average Meter Temperature

T_m = The average of both inlet and outlet temperatures
 obtained during sampling, *557.7* °R.

C - 2 Calculate Sample Volume at Standard Conditions

$$\begin{aligned}
 V_{mstd} &= \text{SCF (Dry) Through meter} \\
 &= 17.32 \frac{V_m}{T_m} \times P_m \\
 &= 17.32 \frac{80.08}{28.69} \\
 &= \underline{557.2} \\
 &= \underline{71.39} \text{ SCF (Dry)}
 \end{aligned}$$

Where: V_m = Dry gas measured by meter, cu.ft.

P_m = Abs. Pr. at meter (use barometric pressure, uncorrected for altitude), In. Hg

C - 3 Calculate Volume Fraction Water in Flue Gas

V_{wstd} = Water vapor in SCF

$$= 0.0465 V_{lc}$$

$$= 0.0465 \cdot 26$$

$$= \underline{1.21} \text{ SCF}$$

B_{wo} = Water $\frac{V}{V}$

$$= \frac{V_{wstd}}{(V_{wstd} + V_{mstd})}$$

$$= \frac{1.21}{72.60}$$

$$= \underline{0.0167}$$

$$\frac{1.21}{72.60} + \frac{71.39}{72.60}$$

Where

V_{lc} = Weight of water collected in impingers plus that gained by drierite, GMS

C - 4 Calculate Dry and Wet Molecular Weight of Stack Gas

M_d = Dry Mol. Wt.

$$= 0.44 (\% \text{ CO}_2) + 0.32 (\% \text{ O}_2)$$

$$+ 0.28 (\% \text{ N}_2 + \text{CO})$$

$$= 0.44 \times \underline{ZERO} + 0.32 \times \underline{20.9=6.69} + 0.28 \times \underline{79.1=22.15}$$

$$= \underline{28.84}$$

M_s = Wet Mol. Wt.

$$= M_d (1 - B_{wo}) + 18 B_{wo}$$

$$= \underline{28.84} \times \underline{0.9833} + 18 \times \underline{0.0167}$$

$$= \underline{28.66} \quad \underline{0.301}$$

C - 5 Calculate The Average $\sqrt{\Delta P}$, ($\sqrt{\Delta P}$) Avg., Obtained during gas sample acquisition

$$(\sqrt{\Delta P}) \text{ Avg.} = \underline{0.870}$$

C - 6 Calculate The Average Stack Gas Temperature, T_s , at time of Gas Sample Acquisition

$$T_s = \underline{570} \text{ } ^\circ\text{R}$$

C - 7 Calculate The Average Stack Gas Velocity

$$(V_s) \text{ Avg.} = 85.48 \times C_p \times (\sqrt{\Delta P}) \text{ Avg.} \sqrt{\frac{T_s}{P_s \times M_s}}$$

$$= 85.48 \times \underline{0.84} \times \underline{0.870}$$

$$= \underline{50.6} \text{ ft./sec}$$

$$\sqrt{\frac{\underline{570}}{\underline{28.70} \times \underline{28.66}}} = \underline{0.810}$$

Where:

C_p = Pitot Tube Coefficient

P_s = Absolute Stack Gas Press., In. Hg.

CR-2
55

C - 8 Calculate Stack Cross Sectional Area at Sampling Site

$$A_s = \underline{1.58} \text{ Sq. Ft.}$$

C - 9 Calculate Stack Gas Average Volumetric Flow Rate

Q_s = Stack Gas Flow Rate, SCFM (Dry)

$$= 1043 \times (1 - B_{wo}) (V_s)_{\text{Avg.}} \times A_s \times \frac{P_s}{T_s}$$

$$= \underline{1043} \times \underline{0.9833} \times \underline{50.6} \times \underline{1.58} \times \underline{28.70}$$

$$= \underline{7,360} \text{ SCFM (Dry)} \quad \underline{540}$$

C - 10 Calculate Isokinetic Sampling Efficiency

$$I = \frac{0.00321 (V_{wstd} + V_{mstd}) \times T_s \times P_m}{\theta \times A_n \times (V_s)_{\text{Avg.}} \times P_s}$$

$$= 0.00321 \times \underline{72.60} \times \underline{540} \times \underline{28.69}$$

$$\underline{72} \times \underline{0.000371} \times \underline{50.6} \times \underline{28.70}$$

$$= \underline{101.3} \%$$

θ = Total Sampling Time, Min.

A_n = Nozzle Opening, Sq. Ft.

C - 11 Calculate Heat Input during testing period

Z = Total Heat Input Rate to Boiler, MEGA BTU/hr.

$$= W_1 \times H_1 =$$

$$+ W_2 \times H_2$$

$$+ W_3 \times H_3$$

= TOTAL

$$= \underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

TOTAL MEGA BTU/hr.

Where $W_1, W_2, \& W_3$ = hourly fuel input of respective fuels and
 $H_1, H_2, \& H_3$ = gross (as received) heating value of respective
 fuels in mega BTU per input unit (consistent with fuel input unit).

C - 12 Calculate Front End Particulate Grain Loading (with Front
 Half Washings Only)

$$C_s' = \text{Part. Grain Loading, gr/SCF (Dry)}$$

$$= 15.42 \times \frac{M_n}{V_{mstd}}$$

$$= 15.42 \times \frac{0.0358}{71.39}$$

$$= \underline{0.008} \text{ gr/SCF (Dry)}$$

Where

M_n = Total Particulate Collected (Filter Plus Front Half
 Washings Only), GMS

C - 13 Calculate Front End Emission Factor

E_t = Hourly Mass Rate, lbs/hr.

$$= 0.00857 \times C_s' \times Q_g$$

$$= 0.00857 \times \underline{0.008} \times \underline{7,360}$$

$$= \underline{0.30} \text{ lbs/hr.}$$

E_h = Front End Emission Factor, lbs/MEGA BTU

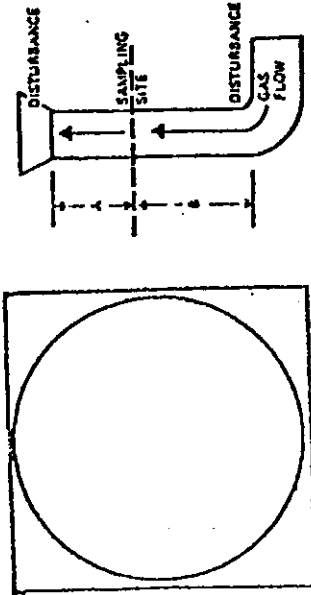
$$= \frac{E_t}{Z}$$

$$= \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}}$$

$$= \underline{\hspace{2cm}} \text{ lbs/MEGA BTU}$$

SCHEMATIC OF STACK



CROSS SECTION

N. PORT

PLANT SUNCOCK, N. 12 AMBIENT TEMPERATURE 50 F
 DATE 9 JULY 1976 BAROMETRIC PRESSURE 28.69
 LOCATION ELEV. HENHOUSE ASSUMED MOISTURE, % 27.03
 OPERATOR E.J. B. A.C.F. M.A.O. PROBE LENGTH, in. 36
 STACK NO. CRIPPER CLENNER NOZZLE DIAMETER, in. 0.23
 RUN NO. THREE (3) STACK DIAMETER, in. 17"
 SAMPLE BOX NO. 2383-3 PROBE HEATER SETTING NONE
 METER BOX NO. 2383-3 HEATER BOX SETTING NONE

PROCESS WEIGHT RATE

WEIGHT OF PARTICULATE COLLECTED, mg

SAMPLE	FILTER	PROBE WASH
FINAL WEIGHT	0.6785	61.9754
TARE WEIGHT	0.6453	61.9626
WEIGHT GAIN	0.0332	0.0128
TOTAL 0.0420		

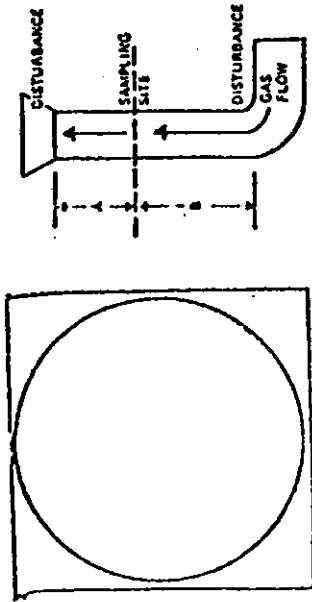
TRAVERSE POINT NUMBER	SAMPLING TIME (h), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD (AP ₃) (VAP ₃)	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (ΔH) in. H ₂ O	GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER		SAMPLE BOX TEMPERATURE °F	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER °F	PUMP VACUUM in. Hg gauge	VELOCITY f/s
							INLET (T _{min}), °F	OUTLET (T _{out}), °F				
1	1402	40.2	80	.55 .742	2.5 2.5	731	100	95	80	80	10.2	
2	1404			.56 .748	2.5 2.5	732	101	96				
3	1406			.55 .742	2.5 2.5	733	103	96				
4	1408			.62 .787	2.8 2.8	735	104	96				
5	1410			.62 "	2.8 2.8	736	105	97				
6	1412			.62 "	2.8 2.8	737	105	96				
7	1414			.67 .819	3.0 3.0	739	106	98				
8	1416			.66 .812	3.0 3.0	741	106	98				
9	1418			.79 .889	3.5 3.5	743	106	96				
10	1420			.80 .899	3.5 3.5	745	107	96				
11	1422			.79 .889	3.5 3.5	747	108	97				
12	1424			.79 .889	3.5 3.5	749	108	95				
13	1426			.76 .872	3.4 3.4	751	109	96				
14	1428			.75 .866	3.4 3.4	753	108	96				
15	1430	V	V	.76 .872	3.4 3.4	755	108	96	V	V	V	
TOTAL												

AVERAGE

COMMENTS:

VOLUME OF LIQUID WATER COLLECTED	IMPINGER VOLUME ml				SILICA GEL WEIGHT, g	ORSAT MEASUREMENT				TIME	CO ₂	O ₂	CO	N ₂
	1	2	3	4		1	2	3	4					
FINAL														
INITIAL														
LIQUID COLLECTED														
TOTAL VOLUME COLLECTED					25.5									

SYNTHETIC OF STICK



NO:1375 55682

7. 1000

PLANT SARLES, W. D. AMBIENT TEMPERATURE 80 F
DATE 9 JULY 1976 BAROMETRIC PRESSURE 28.69
LOCATION EVER. HENDHOUSE ASSUMED MOISTURE, % 27.3
OPERATOR F. J. B., D. S. S., M. D. 10. PROBE LENGTH, in. 36
STACK NO. CRIPPLED CLENNER NOZZLE DIAMETER, in. 0.25
RUN NO. THREE (3) STACK DIAMETER, in. 17.11
SAMPLE BOX NO. 2383-3 PROBE HEATER SETTING NONE
METER BOX NO. 2383-3 HEATER BOX SETTING NONE

METER IN: _____
C.Factor: 0.82

PROCESS WEIGHT & YIELD

WEIGHT OF PARTICULATE COLLECTED, mg			
SAMPLE	FILTER	PROBE WASH	
FINAL WEIGHT	0.6745	61.9754	
TARE WEIGHT	2.6023	61.9638	
WEIGHT GAIN	2.6023	2.0128	
TOTAL			2.0720

[illegible]

AVERAGE

VOLUME OF LIQUID	IMPINGER VOLUME ml	SILICA GEL
10	10	10
20	20	20
30	30	30
40	40	40
50	50	50
60	60	60
70	70	70
80	80	80
90	90	90
100	100	100

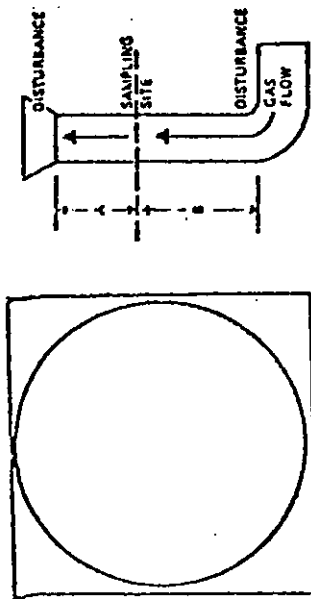
ORSAT MEASUREMENT		TIME	CO ₂	O ₂	CO	N ₂
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CROSS SECTION

E. PART

PLANT SARLES, N. D. AMBIENT TEMPERATURE 80 °C
DATE 9 JULY 1976 BAROMETRIC PRESSURE 28.69
LOCATION FEED HOUSE ASSUMED MOISTURE, % 27.03
OPERATOR F. J. B., A. C. S., M. M. O. PROBE LENGTH, in. 36
STACK NO. CRIPPEN CEMENT NOZZLE DIAMETER, in. 0.95
RUN NO. THREE (3) STACK DIAMETER, in. 17"
SAMPLE BOX NO. 2373-3 PROBE HEATER SETTING NONE
METER BOX NO. 2373-3 HEATER BOX SETTING NONE

МЕТЕРЪ ИМ:

301373

PROCESS WEIGHT: 3.47E

WEIGHT OF PARTICULATE COLLECTED, mg

SAMPLE	FILTER	PROBE WASH
FINAL WEIGHT	0.6745	61.9754
TARE WEIGHT	0.6953	61.9696
WEIGHT GAIN	0.0292	0.0058
TOTAL		0.0420

TRAVERSE POINT NUMBER	SAMPLING TIME (H), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD $(\Delta P_s) (\sqrt{\Delta P_s})$	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (in. H ₂ O)		GAS SAMPLE VOLUME (V _m), ft. ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER		SAMPLE BOX TEMPERATURE °F	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER °F	PUMP VACUUM in. Hg gauge	VELOCITY fps
					ACTUAL DESIRED	(ΔH)		INLET (T _{m,in}), °F	OUTLET (T _{m,out}), °F				
16	1512	70.2	80	.82	3.6	3.6	791	111	98	80	80	10.2	
17	1514			.78	3.5	3.5	793	111	97				
18	1516			.78	3.5	3.5	798.000 = 110	110	99				
							ENO						
TOTAL	72												
AVERAGE	2	70.2	80	X	3.6	3.6		38.6	34.74	80	80	10.2	
					0.852			102.39	102.02				

COMMENTS:

WATER COLLECTED	VOLUME IN				WEIGHT, g	ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
	1	2	3	4							
FINAL						1					
INITIAL						2					
LIQUID COLLECTED						3					
						4					

60

CR-3

PARTICULATE EMISSION CALCULATION

Plant: *SARLES, N. DAKOTA* Orsat Analysis: (Dry Basis, % Vol.), Average
 Location: *ELEVATOR HEADHOUSE* CO₂ *ZERO*
 Stack or Source: *CRIPPEN CLEANER* O₂ *20.9*
 Date: *9 JULY 1976* CO *ZERO*
 Run No.: *THREE (3)* N₂ *79.1*
 Operator: *F.J.B., D.F.F., M.W.O.* Water Collected, GMS.: *25.5*
 Bar. Pr., In. Hg: *28.69 ABSOLUTE* Filter No.: *L*
 Nozzle Dia, In.: *0.25 (1/4)"* Particulate Collected, GMS.:
 Stack Dia., In.: *17" Ø* Filter *0.0292*
 Cp: *0.82* Probe Wash *0.0128*
 Total Time, Min.: *72*
 Vol. Through Gas Meter, Cu. Ft.: FRONT END TOTAL *0.0920*
 Impinger Catch
 FRONT PLUS BACK END CATCH TOTAL *~~~~~*

Standard Conditions: Dry Gas at *15.6°C* and *29.92* in. Hg.

C - 1 Calculate Average Meter Temperature

T_m = The average of both inlet and outlet temperatures
 obtained during sampling, *102.0* °R.

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C - 2 Calculate Sample Volume at Standard Conditions

$$\begin{aligned}
 V_{\text{mstd}} &= \text{SCF (Dry) Through meter} \\
 &= 17.32 \frac{V_m}{T_m} \times P_m \\
 &= 17.32 \frac{12.11}{562} \times 28.69 \\
 &= \underline{63.76} \text{ SCF (Dry)}
 \end{aligned}$$

Where: V_m = Dry gas measured by meter, cu.ft.

P_m = Abs. Pr. at meter (use barometric pressure, uncorrected for altitude), In. Hg

C - 3 Calculate Volume Fraction Water in Flue Gas

$$\begin{aligned}
 V_{\text{wstd}} &= \text{Water vapor in SCF} \\
 &= 0.0465 V_{1c} \\
 &= 0.0465 \cdot 25.5 \\
 &= \underline{1.19} \text{ SCF} \\
 B_{\text{wo}} &= \text{Water } \frac{V}{V} \\
 &= \frac{V_{\text{wstd}}}{(V_{\text{wstd}} + V_{\text{mstd}})} \\
 &= \frac{1.19}{1.19 + 63.76} = \underline{0.0183}
 \end{aligned}$$

Where

V_{1c} = Weight of water collected in impingers plus that gained by drierite, GMS

C - 4 Calculate Dry and Wet Molecular Weight of Stack Gas

$$M_d = \text{Dry Mol. Wt.}$$

$$= 0.44 (\% \text{ CO}_2) + 0.32 (\% \text{ O}_2)$$

$$+ 0.28 (\% \text{ N}_2 + \text{CO})$$

$$= 0.44 \times \underline{\text{ZERO}} + 0.32 \times \underline{20.9} = 6.69 + 0.28 \times \underline{79.1} = 22.1$$

$$= \underline{28.87}$$

$$M_s = \text{Wet Mol. Wt.}$$

$$= M_d (1 - B_{wo}) + 18 B_{wo}$$

$$= \underline{28.87} \times \underline{0.9817} + 18 \times \underline{0.0183}$$

$$= \underline{28.67} \quad \underline{0.329}$$

C - 5 Calculate The Average $\sqrt{\Delta P}$, ($\sqrt{\Delta P}$) Avg., Obtained during gas sample acquisition

$$(\sqrt{\Delta P}) \text{ Avg.} = \underline{0.852}$$

C - 6 Calculate The Average Stack Gas Temperature, T_s , at time of Gas Sample Acquisition

$$T_s = \underline{540} \text{ } ^\circ\text{R}$$

C - 7 Calculate The Average Stack Gas Velocity

$$(V_s) \text{ Avg.} = 85.48 \times C_p \times (\sqrt{\Delta P}) \text{ Avg.}$$

$$= 85.48 \times \underline{0.87} \times \underline{0.852}$$

$$= \underline{79.61} \text{ ft./sec}$$

$$\sqrt{\frac{T_s}{P_s \times M_s}} = \sqrt{\frac{540}{28.70 \times 28.67}} = 0.811$$

Where:

C_p = Pitot Tube Coefficient

P_s = Absolute Stack Gas Press., In. Hg.

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C - 8 Calculate Stack Cross Sectional Area at Sampling Site

$$A_s = \underline{1.58} \text{ Sq. Ft.}$$

C - 9 Calculate Stack Gas Average Volumetric Flow Rate

Q_s = Stack Gas Flow Rate, SCFM (Dry)

$$= 1043 \times (1 - B_{wO}) (V_s)_{\text{Avg.}} \times A_s \times \frac{P_s}{T_s}$$

$$= 1043 \times 0.9817 \times 79.61 \times 1.58 \times 28.70$$

$$= \underline{4,270} \text{ SCFM (Dry)} \quad \underline{540}$$

C - 10 Calculate Isokinetic Sampling Efficiency

$$I = \frac{0.00321 (V_{wstd} + V_{mstd}) \times T_s \times P_m}{\theta \times A_n \times (V_s)_{\text{Avg.}} \times P_s}$$

$$= 0.00321 \times 64.95 \times 540 \times 28.69$$

$$\underline{72 \times 0.000371 \times 79.61 \times 28.70}$$

$$= \underline{92.7} \%$$

θ = Total Sampling Time, Min.

A_n = Nozzle Opening, Sq. Ft.

C - 11 Calculate Heat Input during testing period

Z = Total Heat Input Rate to Boiler, MEGA BTU/hr.

$$= W_1 \times H_1 =$$

$$+ W_2 \times H_2$$

$$+ W_3 \times H_3$$

= TOTAL

$$= \underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

TOTAL MEGA BTU/hr.

Where W_1 , W_2 , & W_3 = hourly fuel input of respective fuels and
 H_1 , H_2 , & H_3 = gross (as received) heating value of respective
fuels in mega BTU per input unit (consistent with fuel input unit).

C - 12 Calculate Front End Particulate Grain Loading (with Front
Half Washings Only)

C_s' = Part. Grain Loading, gr/SCF (Dry)

$$= 15.42 \times \frac{M_n}{V_{mstd}}$$

$$= 15.42 \times \frac{0.092}{63.76}$$

$$= \frac{0.01}{\text{gr/SCF (Dry)}}$$

Where

M_n = Total Particulate Collected (Filter Plus Front Half
Washings Only), GMS

C - 13 Calculate Front End Emission Factor

E_t = Hourly Mass Rate, lbs/hr.

$$= 0.00857 \times C_s' \times Q_s$$

$$= 0.00857 \times \frac{0.01}{\text{gr/SCF (Dry)}} \times 4,270$$

$$= \frac{0.37}{\text{lbs/hr.}}$$

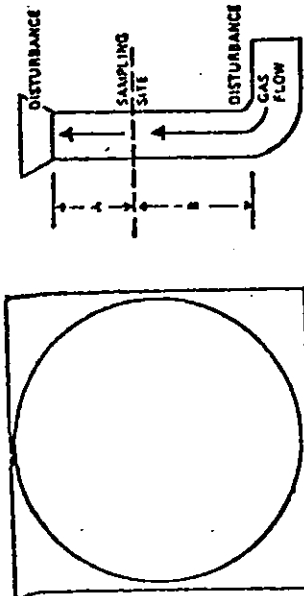
E_h = Front End Emission Factor, lbs/MEGA BTU

$$= \frac{E_t}{Z}$$

$$= \frac{\text{lbs/hr.}}{\text{SCF (Dry)}}$$

$$= \frac{\text{lbs/hr.}}{\text{SCF (Dry) \times 10^6 \text{ BTU}}} \text{ lbs/MEGA BTU}$$

SCHEMATIC OF STACK



CROSS SECTION

5. part

PLANT SARLES, N. H. AMBIENT TEMPERATURE 00
DATE 9 July 1976 BAROMETRIC PRESSURE 28.69
LOCATION ECOL. HENAROUSE ASSUMED MOISTURE, % 27.03
OPERATOR F. J. B. D. S. M. A. O. PROBE LENGTH, in. 36
STACK NO. Loone Creek NOZZLE DIAMETER, in. 0.25
RUN NO. ONE (1) STACK DIAMETER, in. 13"
SAMPLE BOX NO. 2343-3 PROBE HEATER SETTING NONE
METER BOX NO. 2343-3 HEATER BOX SETTING NONE

MEYER, H. J. _____
CEFACTOR 0.84 _____

PROCESS WEIGHT RATE

WEIGHT OF PARTICULATE COLLECTED, mg

SAMPLE	FILTER	PROBE WASH
FINAL WEIGHT	0.6690	0.2308
TARE WEIGHT	0.2851	0.2300
WEIGHT GAIN	0.0239	0.0008
TOTAL		0.0048

TRAVERSE POINT NUMBER	SAMPLING TIME (H), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD (AP _s) (√AP _s)	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER		GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER		SAMPLE BOX TEMPERATURE °F	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER F	PUMP VACUUM in. Hg gauge	VELOCITY f _{ps}
					ACTUAL DESIRED	(ΔH) in. H ₂ O		INLET (T _{m, in}), °F	OUTLET (T _{m, out}), °F				
1	1644	10.3	80	.70	.837	3.4	3.4	828	106	98	80	170.2	
2	1647			.70	.837	3.4	3.4	832	106	98			
3	1650			.68	.825	3.2	3.2	835	110	98			
4	1653			.70	.837	3.4	3.4	838	110	98			
5	1656			.70	.837	3.4	3.4	841	110	98			
6	1659			.70	.837	3.4	3.4	844	110	98			
7	1702			.70	.837	3.4	3.4	848	110	98			
8	1705			.70	.837	3.4	3.4	851	110	98			
9	1708			.65	.806	3.1	3.1	854	110	98			
10	1711		V	.65	.806	3.1	3.1	857	110	98	V	V	
								860.300 =					
								END					
TOTAL	60								20.86	1935			
AVERAGE	3	10.3	80	0.835					104.30	100.50	80		1.5

СЛЕНГОВЫЙ

	VOLUME IN				WEIGHT, g	ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
	1	2	3	4							
GASES WATER COLLECTED											
FINAL						1					
INITIAL						2					
Liquid Collected						3					
LIQUID COLLECTED						4					

1991 1992 1993 1994 1995 1996 1997 1998 1999 2000 2001 2002 2003 2004 2005 2006 2007 2008 2009 2010 2011 2012 2013 2014 2015 2016 2017 2018 2019 2020 2021 2022 2023 2024 2025 2026 2027 2028 2029 2030 2031 2032 2033 2034 2035 2036 2037 2038 2039 2040 2041 2042 2043 2044 2045 2046 2047 2048 2049 2050 2051 2052 2053 2054 2055 2056 2057 2058 2059 2060 2061 2062 2063 2064 2065 2066 2067 2068 2069 2070 2071 2072 2073 2074 2075 2076 2077 2078 2079 2080 2081 2082 2083 2084 2085 2086 2087 2088 2089 2090 2091 2092 2093 2094 2095 2096 2097 2098 2099 2100 2101 2102 2103 2104 2105 2106 2107 2108 2109 2110 2111 2112 2113 2114 2115 2116 2117 2118 2119 2120 2121 2122 2123 2124 2125 2126 2127 2128 2129 2130 2131 2132 2133 2134 2135 2136 2137 2138 2139 2140 2141 2142 2143 2144 2145 2146 2147 2148 2149 2150 2151 2152 2153 2154 2155 2156 2157 2158 2159 2160 2161 2162 2163 2164 2165 2166 2167 2168 2169 2170 2171 2172 2173 2174 2175 2176 2177 2178 2179 2180 2181 2182 2183 2184 2185 2186 2187 2188 2189 2190 2191 2192 2193 2194 2195 2196 2197 2198 2199 2200 2201 2202 2203 2204 2205 2206 2207 2208 2209 2210 2211 2212 2213 2214 2215 2216 2217 2218 2219 2220 2221 2222 2223 2224 2225 2226 2227 2228 2229 2230 2231 2232 2233 2234 2235 2236 2237 2238 2239 2240 2241 2242 2243 2244 2245 2246 2247 2248 2249 2250 2251 2252 2253 2254 2255 2256 2257 2258 2259 2260 2261 2262 2263 2264 2265 2266 2267 2268 2269 2270 2271 2272 2273 2274 2275 2276 2277 2278 2279 2280 2281 2282 2283 2284 2285 2286 2287 2288 2289 2290 2291 2292 2293 2294 2295 2296 2297 2298 2299 2300 2301 2302 2303 2304 2305 2306 2307 2308 2309 2310 2311 2312 2313 2314 2315 2316 2317 2318 2319 2320 2321 2322 2323 2324 2325 2326 2327 2328 2329 2330 2331 2332 2333 2334 2335 2336 2337 2338 2339 2340 2341 2342 2343 2344 2345 2346 2347 2348 2349 2350 2351 2352 2353 2354 2355 2356 2357 2358 2359 2360 2361 2362 2363 2364 2365 2366 2367 2368 2369 2370 2371 2372 2373 2374 2375 2376 2377 2378 2379 2380 2381 2382 2383 2384 2385 2386 2387 2388 2389 2390 2391 2392 2393 2394 2395 2396 2397 2398 2399 2400 2401 2402 2403 2404 2405 2406 2407 2408 2409 2410 2411 2412 2413 2414 2415 2416 2417 2418 2419 2420 2421 2422 2423 2424 2425 2426 2427 2428 2429 2430 2431 2432 2433 2434 2435 2436 2437 2438 2439 2440 2441 2442 2443 2444 2445 2446 2447 2448 2449 2450 2451 2452 2453 2454 2455 2456 2457 2458 2459 2460 2461 2462 2463 2464 2465 2466 2467 2468 2469 2470 2471 2472 2473 2474 2475 2476 2477 2478 2479 2480 2481 2482 2483 2484 2485 2486 2487 2488 2489 2490 2491 2492 2493 2494 2495 2496 2497 2498 2499 2500 2501 2502 2503 2504 2505 2506 2507 2508 2509 2510 2511 2512 2513 2514 2515 2516 2517 2518 2519 2520 2521 2522 2523 2524 2525 2526 2527 2528 2529 2530 2531 2532 2533 2534 2535 2536 2537 2538 2539 2540 2541 2542 2543 2544 2545 2546 2547 2548 2549 2550 2551 2552 2553 2554 2555 2556 2557 2558 2559 2560 2561 2562 2563 2564 2565 2566 2567 2568 2569 2570 2571 2572 2573 2574 2575 2576 2577 2578 2579 2580 2581 2582 2583 2584 2585 2586 2587 2588 2589 2590 2591 2592 2593 2594 2595 2596 2597 2598 2599 2600 2601 2602 2603 2604 2605 2606 2607 2608 2609 2610 2611 2612 2613 2614 2615 2616 2617 2618 2619 2620 2621 2622 2623 2624 2625 2626 2627 2628 2629 2630 2631 2632 2633 2634 2635 2636 2637 2638 2639 2640 2641 2642 2643 2644 2645 2646 2647 2648 2649 2650 2651 2652 2653 2654 2655 2656 2657 2658 2659 2660 2661 2662 2663 2664 2665 2666 2667 2668 2669 2670 2671 2672 2673 2674 2675 2676 2677 2678 2679 2680 2681 2682 2683 2684 2685 2686 2687 2688 2689 2690 2691 2692 2693 2694 2695 2696 2697 2698 2699 2700 2701 2702 2703 2704 2705 2706 2707 2708 2709 2710 2711 2712 2713 2714 2715 2716 2717 2718 2719 2720 2721 2722 2723 2724 2725 2726 2727 2728 2729 2730 2731 2732 2733 2734 2735 2736 2737 2738 2739 2740 2741 2742 2743 2744 2745 2746 2747 2748 2749 2750 2751 2752 2753 2754 2755 2756 2757 2758 2759 2760 2761 2762 2763 2764 2765 2766 2767 2768 2769 2770 2771 2772 2773 2774 2775 2776 2777 2778 2779 2780 2781 2782 2783 2784 2785 2786 2787 2788 2789 2790 2791 2792 2793 2794 2795 2796 2797 2798 2799 2800 2801 2802 2803 2804 2805 2806 2807 2808 2809

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10-1

PARTICULATE EMISSION CALCULATION

Plant: *SAPLES, N. DAKOTA* Orsat Analysis: (Dry Basis, % by Vol.), Average
 Location: *ELEVATOR HEADHOUSE* CO₂ *ZERO*
 Stack or Source: *IDENT. CLEANER* O₂ *20.9*
 Date: *9 JULY 1976* CO *ZERO*
 Run No.: *ONE (1)* N₂ *79.1*
 Operator: *F.J.B., D.F.F., M.W.O.* Water Collected, GMS.: *20.5*
 Bar. Pr., In. Hg: *28.69 ABSOLUTE* Filter No.: *6*
 Nozzle Dia, In.: *0.25 (1/4)"* Particulate Collected, GMS.:
 Stack Dia., In.: *13" Ø* Filter *0.0239*
 Cp: *0.84* Probe Wash *0.0209*
 Total Time, Min.: *60*
 Vol. Through Gas Meter, Cu. Ft.: FRONT END TOTAL *0.0778*
 Impinger Catch
 FRONT PLUS BACK END CATCH TOTAL *~~~~~*

Standard Conditions: Dry Gas at *15.6°C* and *29.92 in. Hg.*

C - 1 Calculate Average Meter Temperature

T_m = The average of both inlet and outlet temperatures
 obtained during sampling, *560.5 °R.*

C - 2 Calculate Sample Volume at Standard Conditions

$$\begin{aligned}
 V_{mstd} &= \text{SCF (Dry) Through meter} \\
 &= 17.32 \frac{V_m \times P_m}{T_m} \\
 &= 17.32 \frac{65.31 \times 28.69}{560.5} \\
 &= \underline{57.9} \text{ SCF (Dry)}
 \end{aligned}$$

Where: V_m = Dry gas measured by meter, cu.ft.

P_m = Abs. Pr. at meter (use barometric pressure, uncorrected for altitude), In. Hg

C - 3 Calculate Volume Fraction Water in Flue Gas

$$\begin{aligned}
 V_{wstd} &= \text{Water vapor in SCF} \\
 &= 0.0465 V_{lc} \\
 &= 0.0465 \cdot 20.5 \\
 &= \underline{0.95} \text{ SCF}
 \end{aligned}$$

$$\begin{aligned}
 B_{wo} &= \text{Water } \frac{V}{V} \\
 &= \frac{V_{wstd}}{(V_{wstd} + V_{mstd})} \\
 &= \frac{0.95}{0.95 + 57.9} = \underline{0.0161}
 \end{aligned}$$

Where

V_{lc} = Weight of water collected in impingers plus that gained by drierite, GMS

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C - 4 Calculate Dry and Wet Molecular Weight of Stack Gas

M_d = Dry Mol. Wt.

$$= 0.44 (\% \text{ CO}_2) + 0.32 (\% \text{ O}_2)$$

$$+ 0.28 (\% \text{ N}_2 + \text{CO})$$

$$= 0.44 \times \underline{\text{ZERO}} + 0.32 \times \underline{26.9 = 6.69} + 0.28 \times \underline{79.1 = 22.15}$$

$$= \underline{28.84}$$

M_s = Wet Mol. Wt.

$$= M_d (1 - B_{wo}) + 18 B_{wo}$$

$$= \underline{28.84} \times \underline{0.9839} + 18 \times \underline{0.0161}$$

$$= \underline{28.67} \quad \underline{0.290}$$

C - 5 Calculate The Average $\sqrt{\Delta P}$, ($\sqrt{\Delta P}$) Avg., Obtained during gas sample acquisition

$$(\sqrt{\Delta P}) \text{ Avg.} = \underline{0.835}$$

C - 6 Calculate The Average Stack Gas Temperature, T_s , at time of Gas Sample Acquisition

$$T_s = \underline{540} \text{ } ^\circ\text{R}$$

C - 7 Calculate The Average Stack Gas Velocity

$$(V_s) \text{ Avg.} = 85.48 \times C_p \times (\sqrt{\Delta P}) \text{ Avg.}$$

$$= 85.48 \times \underline{0.84} \times \underline{0.835}$$

$$= \underline{58.56} \text{ ft./sec}$$

$$\sqrt{\frac{T_s}{P_s \times M_s}}$$

$$\sqrt{\frac{540}{28.71 \times 28.67}} = \underline{0.810}$$

Where:

C_p = Pitot Tube Coefficient

P_s = Absolute Stack Gas Press., In. Hg.

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C - 8 Calculate Stack Cross Sectional Area at Sampling Site

$$A_s = \underline{0.92} \text{ Sq. Ft.}$$

C - 9 Calculate Stack Gas Average Volumetric Flow Rate

Q_s = Stack Gas Flow Rate, SCFM (Dry)

$$= 1043 \times (1 - B_{wo}) (V_s)_{\text{Avg.}} \times A_s \times \frac{P_s}{T_s}$$

$$= \underline{1043} \times \underline{0.9839} \times \underline{78.56} \times \underline{0.92} \times \underline{28.69}$$
$$= \underline{2,440} \text{ SCFM (Dry)} \quad \underline{540}$$

C - 10 Calculate Isokinetic Sampling Efficiency

$$I = \frac{0.00321 (V_{wstd} + V_{mstd}) \times T_s \times P_m}{\theta \times A_n \times (V_s)_{\text{Avg.}} \times P_s}$$

$$= \frac{0.00321 \times \underline{58.85} \times \underline{540} \times \underline{28.69}}{\underline{60} \times \underline{0.000371} \times \underline{78.56} \times \underline{28.71}}$$
$$= \underline{102.6} \%$$

θ = Total Sampling Time, Min.

A_n = Nozzle Opening, Sq. Ft.

C - 11 Calculate Heat Input during testing period

Z = Total Heat Input Rate to Boiler, MEGA BTU/hr.

$$= W_1 \times H_1 =$$

$$+ W_2 \times H_2$$

$$+ W_3 \times H_3$$

= TOTAL

$$= \underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$
$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$
$$\underline{\hspace{2cm}} \times \underline{\hspace{2cm}}$$

TOTAL MEGA BTU/hr.

Where W_1 , W_2 , & W_3 = hourly fuel input of respective fuels and
 H_1 , H_2 , & H_3 = gross (as received) heating value of respective
fuels in mega BTU per input unit (consistent with fuel input unit).

C - 12 Calculate Front End Particulate Grain Loading (with Front
Half Washings Only)

C_s' = Part. Grain Loading, gr/SCF (Dry)

$$\begin{aligned} &= 15.42 \times \frac{M_n}{V_{mstd}} \\ &= 15.42 \times \frac{0.0798}{57.9} \\ &= \underline{0.012} \text{ gr/SCF (Dry)} \end{aligned}$$

Where

M_n = Total Particulate Collected (Filter Plus Front Half
Washings Only), GMS

C - 13 Calculate Front End Emission Factor

E_t = Hourly Mass Rate, lbs/hr.

$$\begin{aligned} &= 0.00857 \times C_s' \times Q_s \\ &= 0.00857 \times 0.012 \times 2,770 \\ &= \underline{0.25} \text{ lbs/hr.} \end{aligned}$$

E_h = Front End Emission Factor, lbs/MEGA BTU

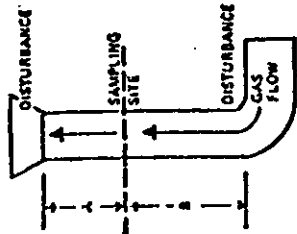
$$= \frac{E_t}{Z}$$

$$= \frac{\quad}{\quad}$$

$$= \underline{\quad} \text{ lbs/MEGA BTU}$$

DATE 9 July 1976 BAROMETRIC PRESSURE 28.69

METER NO. 0.84
C FACTOR 0.84



CROSS SECTION

LOCATION ELI, Henderson ASSUMED MOISTURE, % 270.3

OPERATOR E.J. G. P. S. M. A. O. PROBE LENGTH, in. 36

STACK NO. LDENG CEMENT NOZZLE DIAMETER, in. 0.25

RUN NO. 1200(2) STACK DIAMETER, in. 13"

SAMPLE BOX NO. 2343-3 PROBE HEATER SETTING NONE

METER BOX NO. 2343-3 HEATER BOX SETTING NONE

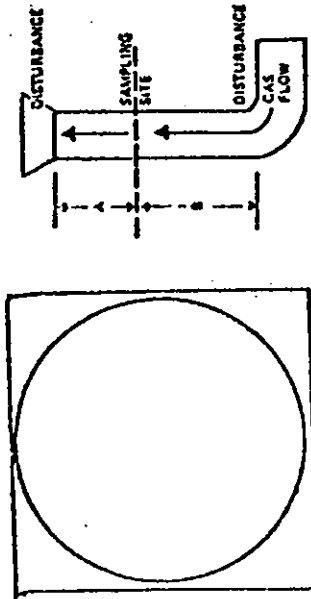
WEIGHT OF PARTICULATE COLLECTED, mg			
SAMPLE	FILTER	PROBE WASH	
FINAL WEIGHT	<u>0.6702</u>	<u>0.6702</u>	<u>0.0000</u>
TARE WEIGHT	<u>0.6512</u>	<u>0.6512</u>	<u>0.0000</u>
WEIGHT GAIN	<u>0.0190</u>	<u>0.0190</u>	<u>0.0000</u>
TOTAL <u>0.0190</u>			

TRAVERSE POINT NUMBER	SAMPLING TIME (h), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD (ΔP ₃) (in. H ₂ O)	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (Δh) (in. H ₂ O)		GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER		TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER F	PUMP VACUUM in. Hg gauge	VELOCITY fps
					ACTUAL	DESIRED		INLET (T _{inlet}), °F	OUTLET (T _{outlet}), °F			
1	1728	40.3	80	.55	2.5	2.5	863	100	96	80	170.2	
2	1731			.55	2.5	2.5	866	101	97			
3	1734			.70	3.4	3.4	869	102	96			
4	1737			.69	3.3	3.3	872	104	96			
5	1740			.71	3.4	3.4	875	103	96			
6	1743			.68	3.2	3.2	878	105	97			
7	1746			.68	3.2	3.2	881	106	98			
8	1749			.70	3.4	3.4	884	106	97			
9	1752			.72	3.4	3.4	887	107	98			
10	1755			.72	3.4	3.4	890	108	98			
TOTAL												
AVERAGE												

COMMENTS:

VOLUME OF LIQUID WATER COLLECTED		IMPINGER VOLUME ml				SILICA GEL WEIGHT, g				ORSAT MEASUREMENT				TIME				CO ₂ O ₂ CO N ₂			
FINAL		1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4
INITIAL																					
LIQUID COLLECTED																					
LIQUID COLLECTED																					

THE UNIVERSITY OF CHICAGO



5. 10127

PLANT SAPLES, M. A. AMBIENT TEMPERATURE 00
DATE 9 JULY 1976 BAROMETRIC PRESSURE 28.69
LOCATION ELEV. HENDHOUSE ASSUMED MOISTURE, % 27.3
OPERATOR E. J. B. & S. M. A. D. PROBE LENGTH, in. 36
STACK NO. Loene Coerner NOZZLE DIAMETER, in. 0.25
RUN NO. Two (2) STACK DIAMETER, in. 13"
SAMPLE BOX NO. 2373-3 PROBE HEATER SETTING None
METER BOX NO. 2373-3 HEATER BOX SETTING None

METER IN: _____
C FACTOR 0.84
PROCESS WEIGHT RATE _____

WEIGHT OF PARTICULATE COLLECTED, mg			
SAMPLE	FILTER	PROBE WASH	
FINAL WEIGHT	2.6278	62.1883	
TARE WEIGHT	2.6542	62.1652	
WEIGHT GAIN	7.0196	0.0231	
TOTAL			2.0927

TRAVERSE POINT NUMBER	SAMPLING TIME (H), min.	STATIC PRESSURE (in. H ₂ O)	STACK TEMPERATURE (T _s), °F	VELOCITY HEAD (AP ₃) (√AP ₃)	PRESSURE DIFFERENTIAL ACROSS ORIFICE METER (ΔH) in. H ₂ O	GAS SAMPLE VOLUME (V _m), ft ³	GAS SAMPLE TEMPERATURE AT DRY GAS METER INLET (T _{m,i}), °F	OUTLET (T _{m,out}), °F	SAMPLE BOX TEMPERATURE °F	TEMPERATURE OF GAS LEAVING CONDENSER OR LAST IMPINGER °F	PUMP VACUUM in. Hg gauge	VELOCITY f/s
1	1801	40.3	80	0.52, 0.72	2.3, 2.3	893	109	98	80	80	170.2	
2	1809			0.52, "	2.3, 2.3	896	109	98				
3	1807			0.55, 0.72	2.5, 2.5	899	108	98				
4	1810			0.55, "	2.5, 2.5	902	109	98				
5	1813			0.66, 0.82	3.0, 3.0	905	109	98				
6	1816			0.66, 0.82	3.0, 3.0	908	111	98				
7	1819			0.81, 0.90	3.9, 3.9	911	110	99				
8	1822			0.88, 0.93	4.3, 4.3	914	110	98				
9	1825			0.88, 0.93	4.3, 4.3	917	110	98				
10	1828	V	V	0.88, 0.93	4.3, 4.3	921.998	110	98	V	V	V	
						END						
TOTAL	60			16.844			2137	1950				
AVERAGE	3	40.3	80	0.822			106.85	97.50	80	80	1.5	

COMMENTS:

WATER COLLECTED	WEIGHT.				ORSAT MEASUREMENT	TIME	CO ₂	O ₂	CO	N ₂
	1	2	3	4						
FINAL					1					
INITIAL					2					
LIQUID COLLECTED					3					
WATER COLLECTED					4					

1951071 8:05 AM 5:10 PM 1:00C 195

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4/1/76 75

ID-2

PARTICULATE EMISSION CALCULATION

Plant: *SARLES, N. DAKOTA* Orsat Analysis: (Dry Basis, % by Vol.), Average
 Location: *ELEVATOR HEADHOUSE* CO₂ *ZERO*
 Stack or Source: *IDENC CLEANER* O₂ *20.9*
 Date: *9 JULY 1976* CO *ZERO*
 Run No.: *TWO (2)* N₂ *79.1*
 Operator: *L.J.B., D.F.F., M.W.O.* Water Collected, GMS.: *21*
 Bar. Pr., In. Hg: *28.69 ABSOLUTE* Filter No.: *H*
 Nozzle Dia, In.: *0.25 (1/4)"* Particulate Collected, GMS.:
 Stack Dia., In.: *13 "φ* Filter *0.0196*
 Cp: *0.84* Probe Wash *0.0231*
 Total Time, Min.: *60*
 Vol. Through Gas Meter, Cu. Ft.: FRONT END TOTAL *0.0427*
 Impinger Catch
 FRONT PLUS BACK END CATCH TOTAL

Standard Conditions: Dry Gas at *15.6°C* and 29.92 in. Hg.

C - 1 Calculate Average Meter Temperature

T_m = The average of both inlet and outlet temperatures
 obtained during sampling, *569.2* °R.

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10-2

C - 2 Calculate Sample Volume at Standard Conditions

$$V_{mstd} = \text{SCF (Dry) Through meter}$$

$$= 17.32 \frac{V_m}{T_m} \times P_m$$

$$= 17.32 \frac{14.52}{28.69} \times 28.69$$

$$= 569.2$$

$$= 570.3 \text{ SCF (Dry)}$$

Where: V_m = Dry gas measured by meter, cu.ft.

P_m = Abs. Pr. at meter (use barometric pressure, uncorrected for altitude), In. Hg

C - 3 Calculate Volume Fraction Water in Flue Gas

$$V_{wstd} = \text{Water vapor in SCF}$$

$$= 0.0465 V_{lc}$$

$$= 0.0465 \cdot 21$$

$$= 0.98 \text{ SCF}$$

$$B_{wo} = \text{Water } \frac{V}{V}$$

$$= \frac{V_{wstd}}{(V_{wstd} + V_{mstd})}$$

$$= \frac{0.98}{0.98 + 570.3}$$

$$= 0.0169$$

$$\frac{0.98}{(58.01)} + \frac{570.3}{58.01}$$

Where

V_{lc} = Weight of water collected in impingers plus that gained by drierite, GMS

C - 4 Calculate Dry and Wet Molecular Weight of Stack Gas

$$M_d = \text{Dry Mol. Wt.}$$

$$= 0.44 (\% \text{ CO}_2) + 0.32 (\% \text{ O}_2)$$

$$+ 0.28 (\% \text{ N}_2 + \text{CO}).$$

$$= 0.44 \times \underline{\text{ZERO}} + 0.32 \times \underline{26.9} = 6.69 + 0.28 \times \underline{79.1} = 22.1$$

$$= \underline{28.84}$$

$$M_s = \text{Wet Mol. Wt.}$$

$$= M_d (1 - B_{wo}) + 18 B_{wo}$$

$$= \underline{28.84} \times \underline{0.9831} + 18 \times \underline{0.0169}$$

$$= \underline{28.66} \quad \underline{0.304}$$

C - 5 Calculate The Average $\sqrt{\Delta P}$, ($\sqrt{\Delta P}$) Avg., Obtained during gas sample acquisition

$$(\sqrt{\Delta P}) \text{ Avg.} = \underline{0.822}$$

C - 6 Calculate The Average Stack Gas Temperature, T_s , at time of Gas Sample Acquisition

$$T_s = \underline{540} \text{ } ^\circ\text{R}$$

C - 7 Calculate The Average Stack Gas Velocity

$$(V_s) \text{ Avg.} = 85.48 \times C_p \times (\sqrt{\Delta P}) \text{ Avg.}$$

$$= 85.48 \times \underline{0.82} \times \underline{0.822}$$

$$= \underline{57.81} \text{ ft./sec}$$

$$\sqrt{\frac{T_s}{P_s \times M_s}} = \sqrt{\frac{540}{28.71 \times 28.66}} = \underline{0.810}$$

Where:

C_p = Pitot Tube Coefficient

P_s = Absolute Stack Gas Press., In. Hg.

C - 8 Calculate Stack Cross Sectional Area at Sampling Site

$$A_s = \underline{0.92} \text{ Sq. Ft.}$$

C - 9 Calculate Stack Gas Average Volumetric Flow Rate

$$\begin{aligned} Q_s &= \text{Stack Gas Flow Rate, SCFM (Dry)} \\ &= 1043 \times (1 - B_{wo}) (V_s)_{\text{Avg.}} \times A_s \times \frac{P_s}{T_s} \\ &= \underline{1043} \times \underline{0.9831} \times \underline{47.81} \times \underline{0.92} \times \underline{28.71} \\ &= \underline{2,700} \text{ SCFM (Dry)} \quad \underline{540} \end{aligned}$$

C - 10 Calculate Isokinetic Sampling Efficiency

$$\begin{aligned} I &= \frac{0.00321 (V_{wstd} + V_{mstd}) \times T_s \times P_m}{\theta \times A_n \times (V_s)_{\text{Avg.}} \times P_s} \\ &= 0.00321 \times \underline{58.01} \times \underline{540} \times \underline{28.69} \\ &\quad \underline{60 \times 0.000371 \times 47.81 \times 28.71} \\ &= \underline{102.7} \% \end{aligned}$$

θ = Total Sampling Time, Min.

A_n = Nozzle Opening, Sq. Ft.

C - 11 Calculate Heat Input during testing period

Z = Total Heat Input Rate to Boiler, MEGA BTU/hr.

$$\begin{aligned} &= W_1 \times H_1 = \\ &\quad + W_2 \times H_2 \\ &\quad + W_3 \times H_3 \\ &= \text{TOTAL} \\ &= \underline{\hspace{2cm}} \times \underline{\hspace{2cm}} \\ &\quad \underline{\hspace{2cm}} \times \underline{\hspace{2cm}} \\ &\quad \underline{\hspace{2cm}} \times \underline{\hspace{2cm}} \end{aligned}$$

TOTAL _____ MEGA BTU/hr.

Where $W_1, W_2, & W_3$ = hourly fuel input of respective fuels and
 $H_1, H_2, & H_3$ = gross (as received) heating value of respective
 fuels in mega BTU per input unit (consistent with fuel input unit).

C - 12 Calculate Front End Particulate Grain Loading (with Front
 Half Washings Only)

$$\begin{aligned} C_s' &= \text{Part. Grain Loading, gr/SCF (Dry)} \\ &= 15.42 \times \frac{M_n}{V_{\text{mstd}}} \\ &= 15.42 \times \frac{0.0827}{57.03} \\ &= \underline{0.012} \text{ gr/SCF (Dry)} \end{aligned}$$

Where

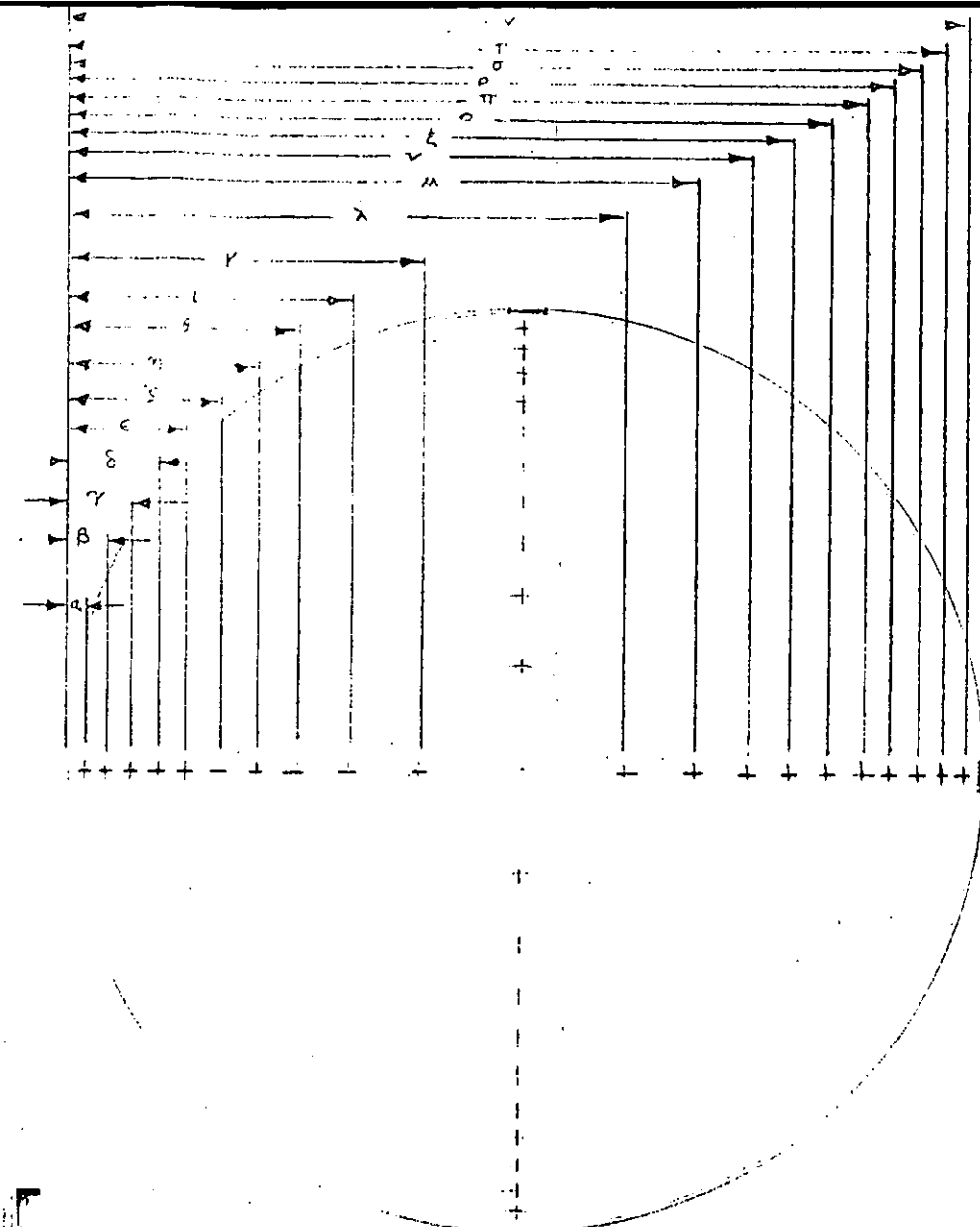
M_n = Total Particulate Collected (Filter Plus Front Half
 Washings Only), GMS

C - 13 Calculate Front End Emission Factor

$$\begin{aligned} E_t &= \text{Hourly Mass Rate, lbs/hr.} \\ &= 0.00857 \times C_s' \times Q_s \\ &= 0.00857 \times \underline{0.012} \times \underline{2,400} \\ &= \underline{0.025} \text{ lbs/hr.} \end{aligned}$$

E_h = Front End Emission Factor, lbs/MEGA BTU

$$\begin{aligned} &= \frac{E_t}{2} \\ &= \underline{\hspace{2cm}} \\ &= \underline{\hspace{2cm}} \text{ lbs/MEGA BTU} \end{aligned}$$

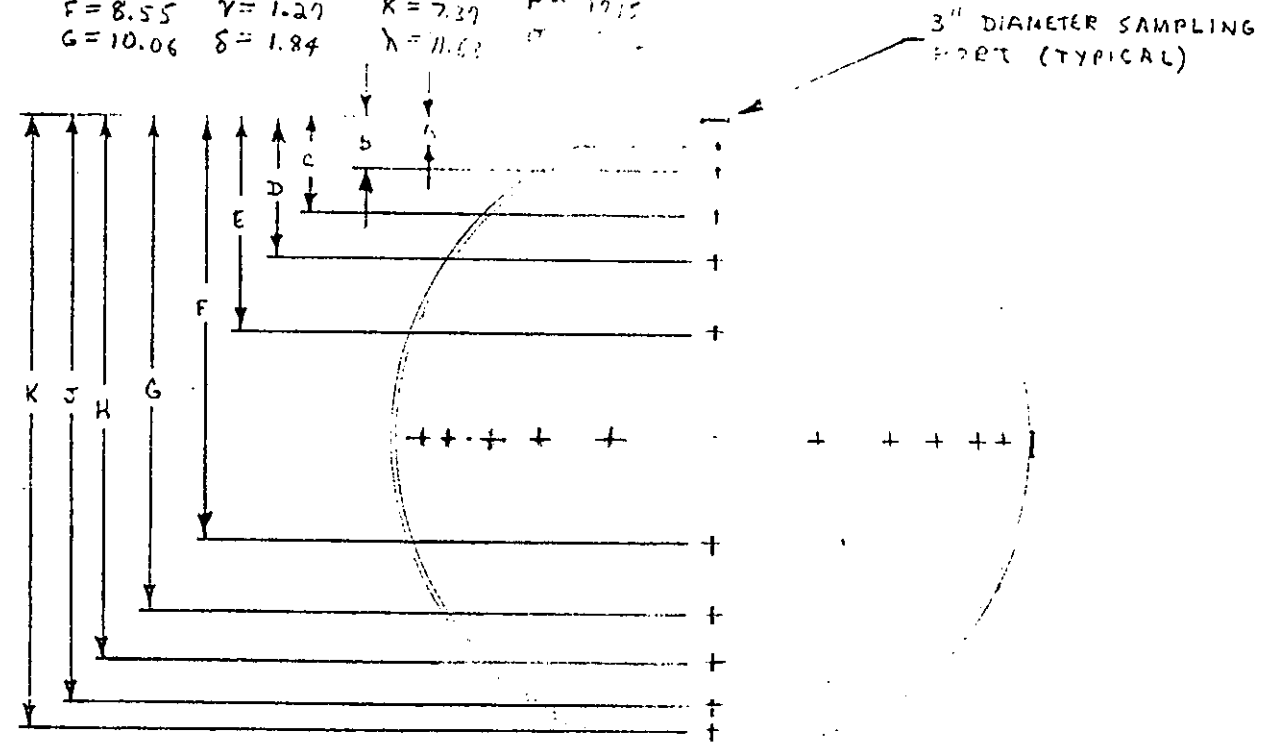


SECTION A-A
19" DIA. DUCT
SCALE: 3"=1'

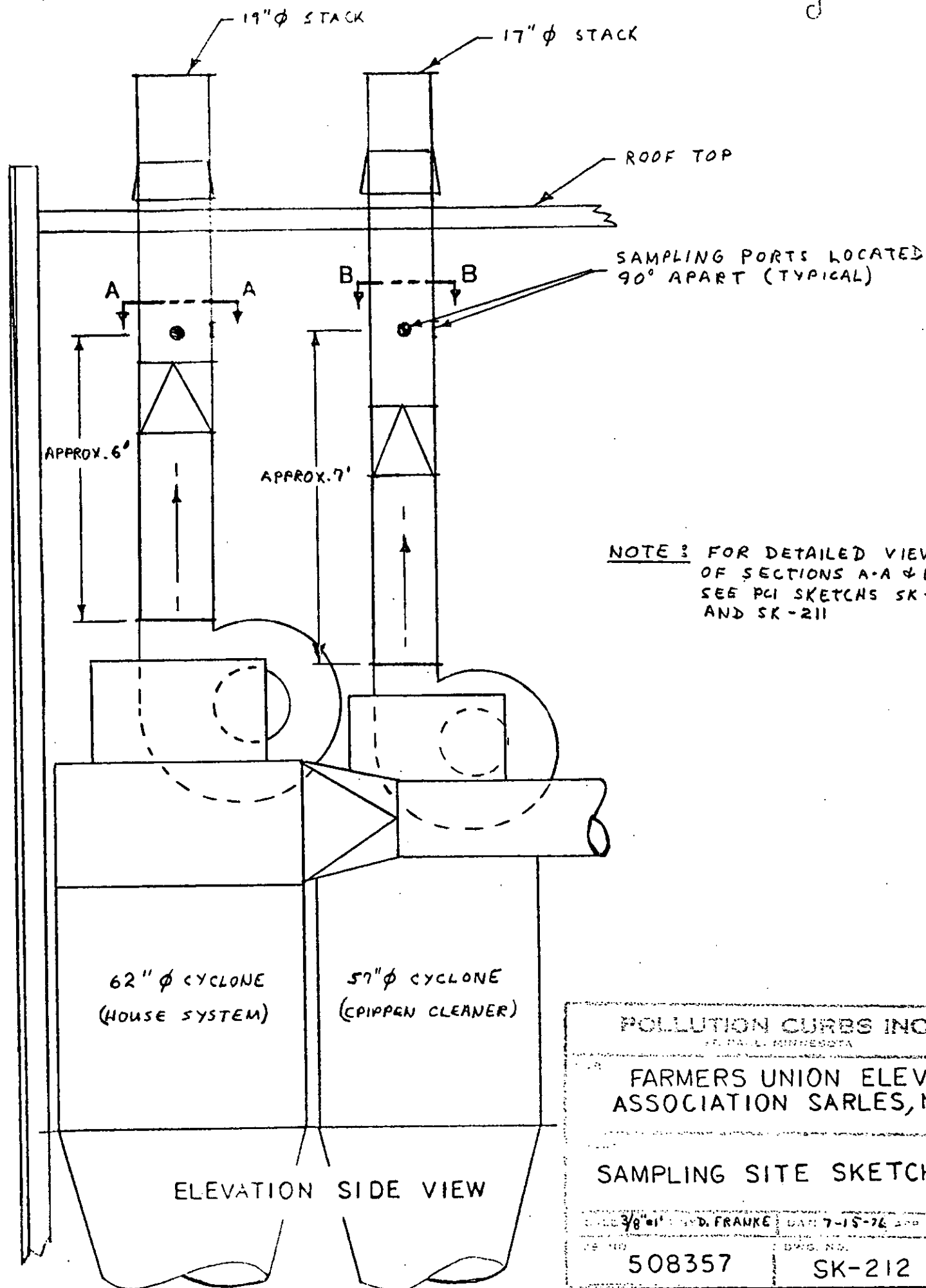
NOTES:

1. + INDICATES TRAVERSE POINTS AT WHICH AIR FLOW RATES AND SAMPLES WERE TAKEN.
2. DISTANCE FROM DUCT WALL TO TRAVERSE POINT, IN FEET AS LISTED BELOW

A = .33	H = 11.10	E = 2.45	M = 13.18	T = 12.01
B = 1.07	J = 11.93	S = 3.13	V = 14.25	W = 14.95
C = 1.90	K = 12.68	η = 3.87	Ξ = 15.12	
D = 2.94	α = .25	θ = 4.95	Ο = 15.86	
E = 4.45	β = .74	ι = 5.81	π = 16.55	
F = 8.55	γ = 1.27	κ = 7.37	ρ = 17.15	
G = 10.06	δ = 1.84	λ = 11.62	τ =	



SECTION C-C
13" DIA. DUCT
SCALE: 3"=1'



POLLUTION CURBS INC.

ST. PAUL, MINNESOTA

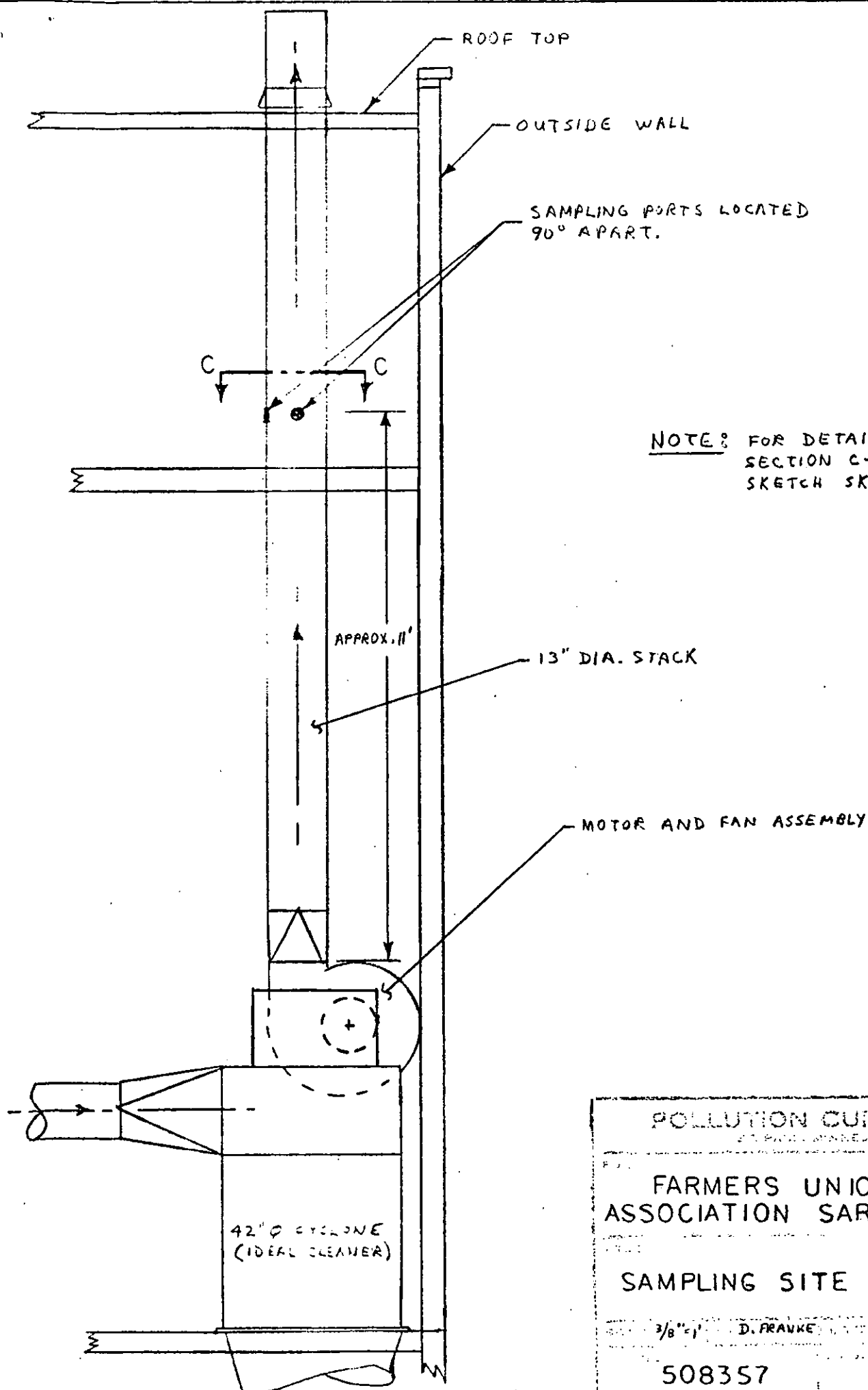
FARMERS UNION ELEV.
ASSOCIATION SARLES, N.D.

SAMPLING SITE SKETCH

SCALE 3/8" = 1' D. FRANKS DATE 7-15-76

508357 DWG. NO.

SK-212



POLLUTION CURBS INC.
2700 W. WISCONSIN AVE.
MINNEAPOLIS, MINN. 55416

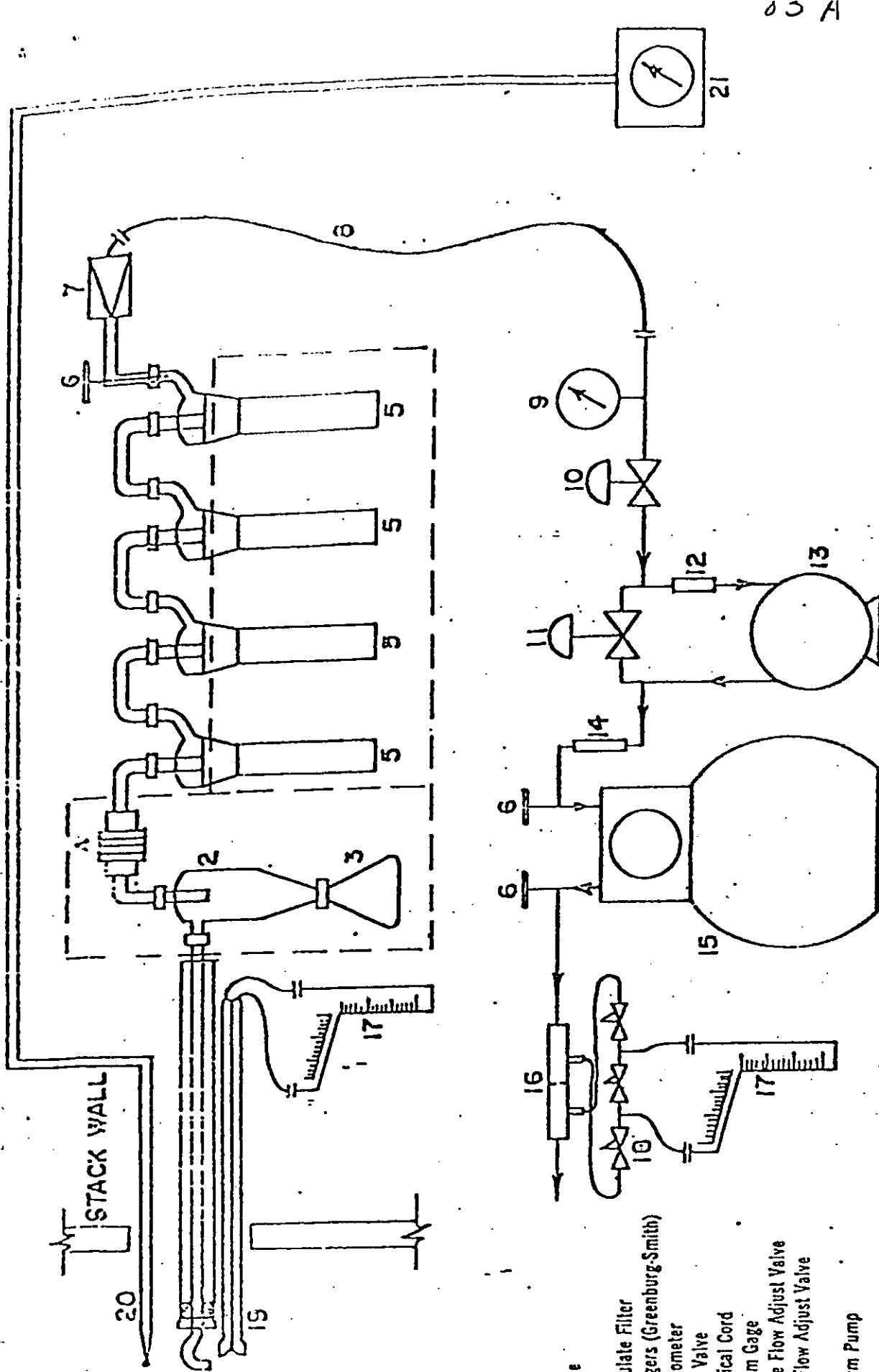
FARMERS UNION ELEV.
ASSOCIATION SARLES, N.D.

SAMPLING SITE SKETCH

3/8" = 1' D. FRANK 7-15-76

508357

SK-213



- 1) Probe
- 2) Cyclone
- 3) Flask
- 4) Particulate Filter
- 5) Impingers (Greenburg-Smith)
- 6) Thermometer
- 7) Check Valve
- 8) Umbilical Cord
- 9) Vacuum Gage
- 10) Coarse Flow Adjust Valve
- 11) Fine Flow Adjust Valve
- 12) Orificer
- 13) Vacuum Pump
- 14) Filler
- 15) Dry Gas Meter
- 16) Orifice Tube
- 17) Incline Manometer
- 18) Solenoid Valves
- 19) Pilot
- 20) Thermocouple
- 21) Pyrometer

FIGURE 10

PROPERTY OF RESEARCH APPLIANCE CO. GIBSONIA, PA.					
TOLERANCES		TITLE STACK SAMPLES FLOW SYSTEM			
DEC. ±		DWG. NO.	MATL.	SCALE	
FRAC. ±		1748			
NO. REQ'D		DRAWN BY	APPROV.	DATE	PART NO.
		R.C.		6-23-6	
FINISH					

MINNESOTA POLLUTION CONTROL AGENCY

1935 W. County Road 82, / Roseville, Minnesota 55113

612-296-7373

This is to certify that,

FRANK BELGEA

attended and fulfilled the requirements of the

VISIBLE EMISSION EVALUATION RE-CERTIFICATION COURSE

offered by

THE MINNESOTA POLLUTION CONTROL AGENCY

on

APRIL 1, 1976

During the course of the test an average deviation of less than 7.5% for a set of 25 white smoke and a set of 25 black smoke was maintained and none of the readings deviated by 20% or more.

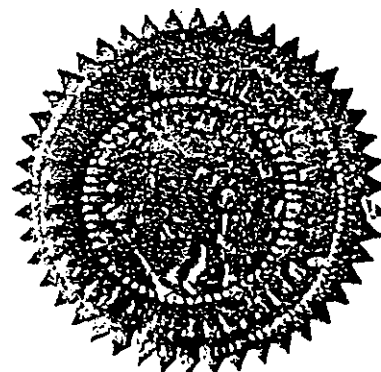
By achieving the above accuracy, certification as a "Smoke Reader" is granted for a period of six months from the date of the test.

James L. Kolar

JAMES L. KOLAR
Instructor
Pollution Control Specialist
MPCA, DAQ

Richard J. Sandberg

RICHARD J. SANDBERG
Instructor
Pollution Control Specialist
MPCA, DAQ



Environmental Health
and
Engineering Services

Division of
Environmental Engineering
GENE A. CHRISTIANSON, M.E.
DIRECTOR
(701) 224-2374

North Dakota State



W. VAN HEUVELEN, CHIEF

Department of Health

State Capitol
Bismarck, North Dakota 58505

February 5, 1976

Mr. Frank J. Belgea
Vice President of Operations
Pollution Curbs, Incorporated
502 North Prior Avenue
St. Paul, Minnesota 55104

Re: Niobe Farmers Co-op Elevator Company
PCI Project No. 508357

Dear Mr. Belgea:

In response to your letter of January 22, 1976, regarding the above referenced facility, we have received a copy of revisions to the dust control system design from Jacobson & Sons Construction Company. These revisions have been reviewed and are satisfactory to the Department.

Performance testing is required for your company's collection equipment as this is the Department's policy regarding initial installation of a line of collection equipment for which no performance tests, efficiency curves, etc. are available. Once performance tests of the control equipment have been submitted and are satisfactory to us, we will give approval for the use of your equipment throughout the State without further tests. However, if the design of your equipment should be modified, additional tests may be required.

Our records indicate that your firm will also be installing dust control systems for the Farmers Union Elevator Association at Sarles, North Dakota and the Kramer Equity Elevator Company at Kramer, North Dakota. As mentioned earlier, performance testing of your collection equipment would be required at only one of these locations (Niobe, Sarles, or Kramer). If the tests are satisfactory to us, we would approve the use of your equipment throughout the State without further testing. We request that the testing be conducted as soon as possible on the first of these three facilities to begin operation.

Mr. Frank J. Belgen

-2-

February 5, 1976

Please inform us of your decision as to which dust control system will be tested. Enclosed is a copy of the guidelines to be used in conducting performance testing in North Dakota.

If you have any questions, please feel free to contact us.

Yours truly,



W. Van Heuvelen, Chief
Environmental Control

CDR:1rr

Encl:

cc: Wesley Hennix - Niobe Farmers Elevator
Howard Thompson - Farmers Union Elev. Assoc., Sarles
Myron Brandt - Kramer Equity Elevator

DRY TEST METER CALIBRATION

Date: JUNE 1, 1976 Meter No. RAC 2343-3

Standard: "PRECISION" WET TEST METER - PRECISION SCIENTIFIC CO

DATA:

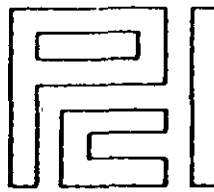
	<u>Standard</u>	<u>Test Meter</u>
Flow Rate	<u>1.0 CFM</u>	<u>1.0 CFM</u>
Test Volume	<u>65.40 CU.FT.</u>	<u>61.35</u>
Test Time	<u>65.4 MINS.</u>	<u>65.4 MINS.</u>
Gas Temperature	<u>77°F (25°C)</u>	<u>77°F (25°C)</u>
Gas Pressure	<u>760 mm Hg.</u>	<u>760 mm Hg.</u>
Correction Factor	<u>ZERO</u>	<u>0.938</u>

Date: _____ Meter No. _____

Standard: _____

DATA:

	<u>Standard</u>	<u>Test Meter</u>
Flow Rate	_____	_____
Test Volume	_____	_____
Test Time	_____	_____
Gas Temperature	_____	_____
Gas Pressure	_____	_____
Correction Factor	_____	_____

PITOT TUBE CALIBRATION - STAUSCHEIBE TYPE

Date: June 1, 1976

Pitot Tube: 3 foot RAC Stainless Steel Pitobe with 0.25" nozzle attached.

Standard: 12" Standard type pitot tube (Dwyer Instruments, Inc.) - Used for calibration purposes only.

Data:

Indicated Velocity Pressure (inches of water)		Calibration Factor	Coefficient
A. Standard	B. Stauscheibe		
1. 0.02	0.03	0.667	0.817
2. 0.05	0.07	0.714	0.845
3. 0.10	0.14	0.714	0.845
4. 0.18	0.24	0.750	0.866
5. 0.32	0.45	0.711	0.843
6. 0.49	0.68	0.721	0.849
7. 0.65	0.95	0.684	0.827
8. 0.90	1.28	0.708	0.839
9. 0.22	0.30	0.733	0.856
10. 0.07	0.10	0.700	0.837
<u>Average pitot tube coefficient:</u>			0.842

Client: Farmers Union Elevator Association, Sarles, North Dakota

Specifications of Calibration System:

6" inside diameter PVC pipe - Calibration orifice or access port is 18 duct diameters downstream and 11 diameters upstream from any outlet, bend, or obstruction - 1 hp Dayton Electric Motor (3450 rpm) - Dayton Blower with 10-5/8"Ø wheel - Bell housing inlet to calibration system.