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Title: Results of a Source Emission
Compliance Test At Southern
Minnesota Beet Sugar Cooperative,
Renville, Minnesota

MMT Environmental, Inc.

MMT Environmental, Inc.

January 1988

MMT Environmental, Inc.
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RESULTS OF A SOURCE
EMISSION COMPLIANCE TEST AT
SOUTHERN MINNESOTA BEET SUGAR
COOPERATIVE
RENVILLE, MINNESOTA 56284

January 21, 1988

Submitted to:

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RESULTS OF A SOURCE
EMISSION COMPLIANCE TEST
AT SOUTHERN MINNESOTA BEET SUGAR
COOPERATIVE
RENVILLE, MINNESOTA 56284

Report Number 8675
Project Number 8014

1 INTRODUCTION

On January 21, 1988, MMT Environmental, Inc. performed a source emission compliance test on one of the four cyclones used to remove the particulates from the exhaust gas of drum dryer "A". The cyclone tested is designated "A2", it is the only cyclone of the four that has straightening vanes in the discharge. Testing of the other cyclones, without flow straightening vanes, would be invalid due to turbulence and cyclonic flow patterns. The tests were performed at the request of Mr. W.D. DeBelly.

The MMT sampling team consisted of Clifford E. Mohs and Robert A. Laska.

MPCA officials were notified of the compliance test but elected not to observe the on-site testing.

2 TEST RESULTS

The significant results generated by the test program are presented in this section.

2.1 Particulate Emissions

Table 2.1 presents the results of the particulate emission tests. Particulate emissions of the three runs averaged 0.105 gr/SCF.

2.2 Visible Emissions

Attempts were made to make visible emissions observation during all three of the test runs but because of the high moisture content of the gas and the close proximity of the other stacks, it was impossible to make V.E. reading.

2.3 Cyclone A2 Particulate Removal

Table 2.3.1 presents the result of the pulp material collected at the bottom of the cyclone A2. Collected material averaged 263.2 lb/hr.

Table 2.3.2 presents the cyclone removal efficiency. The average efficiency was determined as 94.8%.

2.4. Comments

Flow measurements were made in two cyclones B1 and B2 of drum dryer "B", to determine if the flow patterns would be acceptable under EPA regulations to perform a US-EPA method 5 to determine the emissions. Both stacks showed significant cyclonic flow patterns and testing would not be acceptable unless straightening vanes or other mechanical method was used to provide a better flow pattern.

TABLE 2.1 SUMMARY OF PARTICULATE EMISSION TEST RESULTS

PROJECT NUMBER: 8214 COMPANY: SOUTHERN MN. BEET SUGAR
TEST NUMBER: 1 SOURCE: CYCLONE "A-2"

TEST PARAMETER	RUN 1	RUN 2	RUN 3
TEST DATE	1/21/88	1/21/88	1/21/88
TIME OF TEST, HR:			
START	1123	1243	1432
FINISH	1231	1352	1533
EFFLUENT TEMPERATURE, DEGREES F	268	292	292
EFFLUENT MOISTURE CONTENT, % W/W	37.8	36.4	41.7
EFFLUENT COMPOSITION, % W/W DRY:			
CARBON DIOXIDE	5.5	4.6	6.2
OXYGEN	14.2	15.6	13.1
CARBON MONOXIDE	0.0	0.0	0.0
EFFLUENT VOLUMETRIC FLOW RATE:			
ACTUAL CONDITIONS, ACFM	22532	22593	24128
STANDARD CONDITIONS, SCFM	15367	15535	16566
DRY STANDARD CONDITIONS, DSCFM	9678	9874	9662
ISOKINETIC VARIATION, %	118.2	120.3	112.0
EFFLUENT PARTICULATE CONCENTRATION:			
ACTUAL CONDITIONS, GR/ACF	3.0744	3.0755	3.2665
STANDARD CONDITIONS, GR/SCF	3.1277	3.1112	3.0768
DRY STANDARD CONDITIONS, GR/DSCF	3.1733	3.1750	3.1663
SOURCE PARTICULATE EMISSION RATE:			
CLASSICAL METHOD, LB/HR	14.38	14.82	13.76
RATIO OF AREAS METHOD, LB/HR	15.85	15.18	15.42

PARTICULATE CONCENTRATION AND EMISSION RATES BASED ON ANALYSIS OF THE SAMPLING TRAIN FRONT AND BACK CATCHES.

STANDARD CONDITIONS: 68 DEGREES FAHRENHEIT, 29.92 INCHES OF MERCURY.

Rated @ 23,000 ACFM
23,078 100.3% of capacity
9738
105.17

0.1714

14.32
15.47

CYCLONE BOTTOM COLLECTION

Table 2.3.1

Start: 11:45 End 3:45 4 Hours

Wheelbarrow Tare Weight	44 lbs	46 lbs
Wheelbarrow & Pulp	73	78
Weight	74	78
	74	79
	76	80
	78	80
	81	82
	82	90
	89	90
	97	97
	78	84
	96	88
	98	90
	94	88
	<u>73</u>	<u> </u>
	1163	1104
- (14 x 44)	<u> </u>	- (13 x 46)
	546 lbs	506 lbs

Total 546 lbs + 506 lbs = 1053/4hours = 263.2 lbs/hr

CYCLONE "A2" REMOVAL EFFICIENCY

Table 2.3.2

	lb/hr	lb/hr	Efficiency
Run #1	14.38	277.4	94.8
Run #2	14.82	277.8	94.7
Run #3	13.76	276.8	95.0
Average	14.32	277.3	94.8

$$E = 100 - \left(\frac{\text{Emissions (lb/hr)}}{\text{Bottom Collection (lb/hr) + Emission (lb/hr)}} \times 100 \right)$$

3 EMISSION TEST PROCEDURES

3.1 General

In order to determine the pollutant emission rate from stationary sources, the Environmental Protection Agency (EPA) has established a series of reference methods which specify the manner in which tests must be performed. These reference methods are found in the Code of Federal Regulations under Title 40 - Protection of Environment; Chapter 1 - Environmental Protection Agency; Subchapter C - Air Programs; Part 60 - Standards of Performance for New Stationary Sources; Appendix A - Reference Methods. Unless otherwise noted, the tests presented in this report were performed according to the EPA Reference Methods as revised on July 1, 1983. A brief description of the test procedures used follows.

3.2 Sampling Points

The sampling required for EPA Methods 2 and 5 was performed at numerous points across the duct cross-section. The number of sampling points and their locations within the duct were determined according to EPA Method 1 (Figures 3.1 and 3.2). The number of points required is based on the distance of undisturbed flow both up and downstream of the sampling location.

3.3 Effluent Flow Rate

The effluent volumetric flow rate was determined per EPA Method 2. The effluent velocity pressure and temperature were measured at numerous points across the duct cross-section using an S-type pitot tube and a chromel-alumel thermocouple. The flow rate measurements were made simultaneously with each particulate concentration test run.

Figure 3.1 Description of Sampling Location

Duct cross-sectional dimensions at the sampling location: 47.5

Equivalent diameter (rectangular duct only): _____

Distance from sampling ports to the nearest flow disturbance;

Before sampling ports: 5.6 = _____ duct diameters

After sampling ports: 2.0 = _____ duct diameters

Number of sampling points;

Required by EPA Method 1: 26

Actually used: Only used 20 because straightening vanes were installed

Number of ports: 2

Points per port: 10

Sketch of sampling location:

Not to Scale

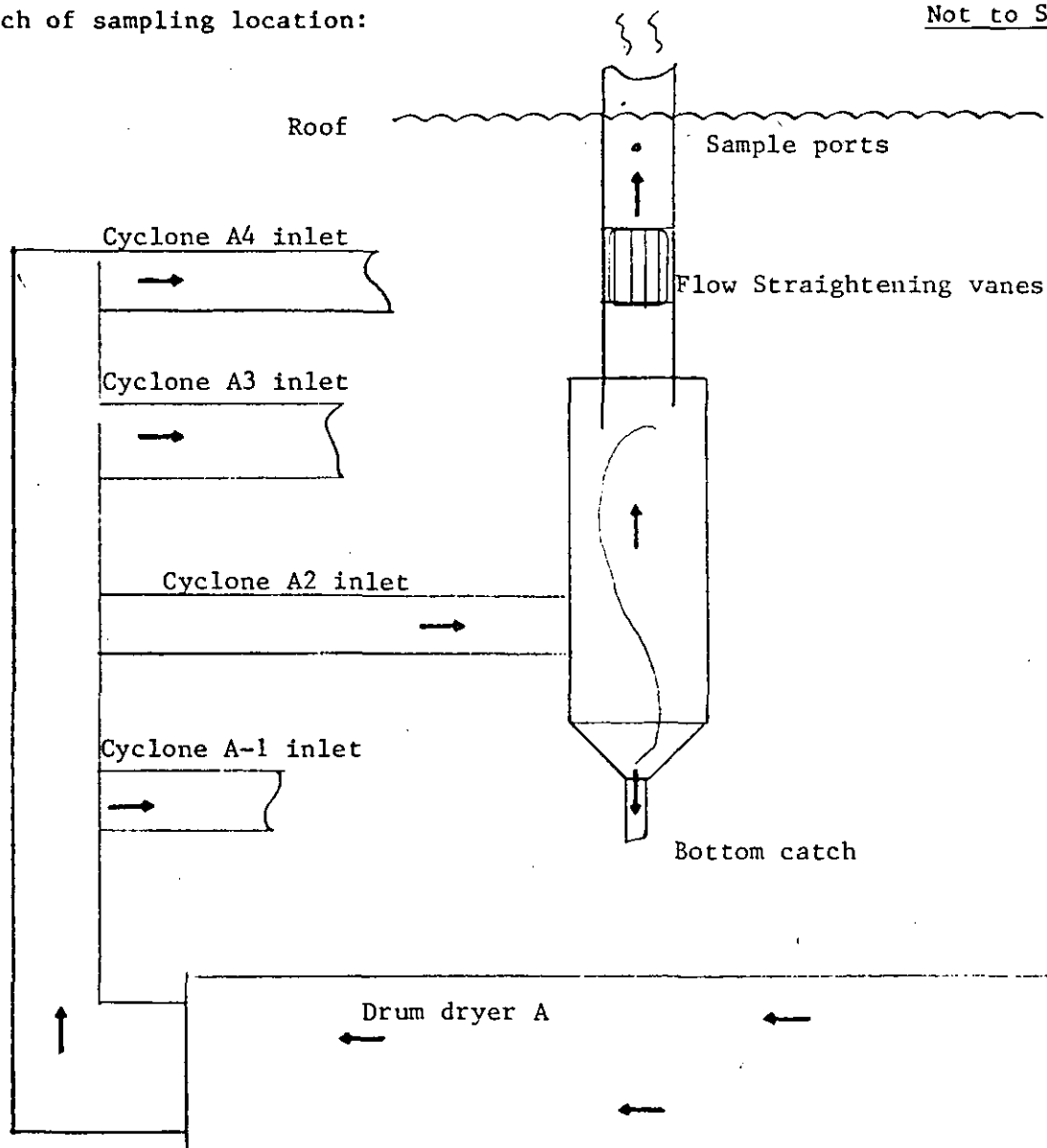
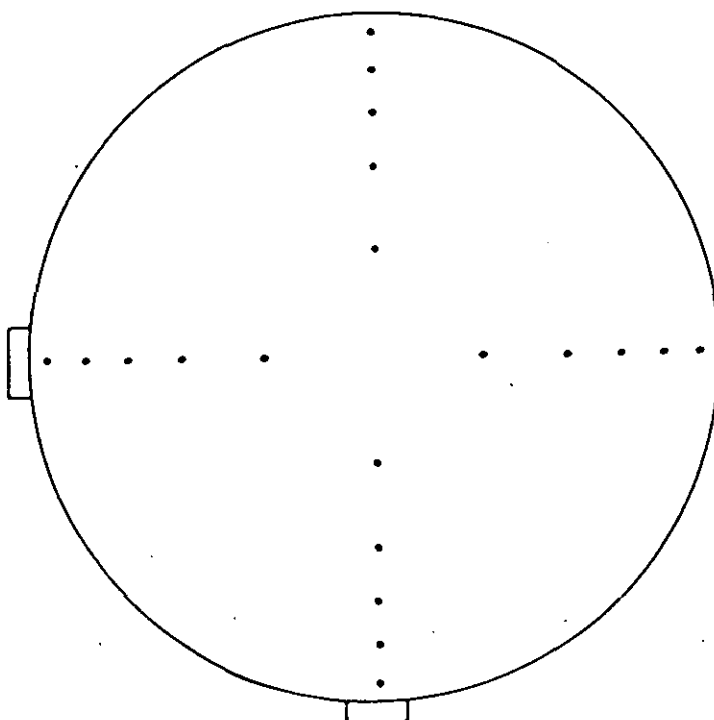


Figure 3.2 Sampling Point Locations Within the Duct

Sketch:

Not to Scale



Location of sampling points within each port:

Point Number	Distance From Duct Inside Wall (by Port) to the Sampling Point	
	% of Duct Diameter	Inches
1	2.53	1.2
2	8.21	3.9
3	14.5	6.9
4	22.5	10.7
5	34.1	16.2
6	65.9	31.3
7	77.5	36.8
8	85.5	40.6
9	91.8	43.6
10	97.5	46.3
11		
12		

Point Number	Distance From Duct Inside Wall (by Port) to the Sampling Point	
	% of Duct Diameter	Inches
13		
14		
15		
16		
17		
18		
19		
20		
21		
22		
23		
24		

3.4 Effluent Composition (CO_2 , O_2)

The carbon dioxide and oxygen content of the effluent was determined per EPA Method 3. One (1) multi-point integrated sample was collected simultaneously with each particulate test run. Analysis of the sample was performed with a standard Orsat analyzer using commercially prepared solutions.

3.5 Effluent Moisture Content

The effluent moisture content during each test run was determined simultaneously with the particulate concentration determination as per EPA Method 5. The moisture content was calculated from the volume and/or mass of condensed water collected in the cold box impingers and the volume of gas sampled.

3.6 Effluent Particulate Concentration

The effluent particulate concentration was determined per EPA Method 5. In this procedure, particulate matter is isokinetically withdrawn from the source and collected on a glass-fiber filter. Organic vapors and other condensibles which pass through the filter are collected in an ice-cooled impinger trap. The particulate mass, which includes any material which condenses at the filtration temperature, is determined gravimetrically after removal of any uncombined water.

The sampling train (Figure 3.3) consists of a heated sampling probe with attached thermocouple and S-type pitot tube. The probe attaches to the front sample case (hot box) which has an all-glass in-line filter holder in a temperature controlled environment. The back sample case (cold box) houses a series of impingers and a desiccant column in an ice bath. The sample case is connected via an umbilical cord to the control unit which contains the vacuum pump, pressure indicator and all operating controls. The thermocouple is connected to a separately housed temperature readout.

Figure 3.3 Particulate Sampling Train

Sampling train;

Manufacturer: RAC (Research Appliance Company)

Model: Stak Sampler

Hot box set-up;

Cyclone: NA

Filter media: Type A/E glass fiber
100 mm effective diameter

Filtration temperature, °F: +250°F

Cold box set-up;

Impinger Number	Type*	Contents
1	M	Deionized - Distilled H ₂ O
2	S	Deionized - Distilled H ₂ O
3	M	Empty
4	M	Silica Gel
5		

* S: Standard Greenburg-Smith design

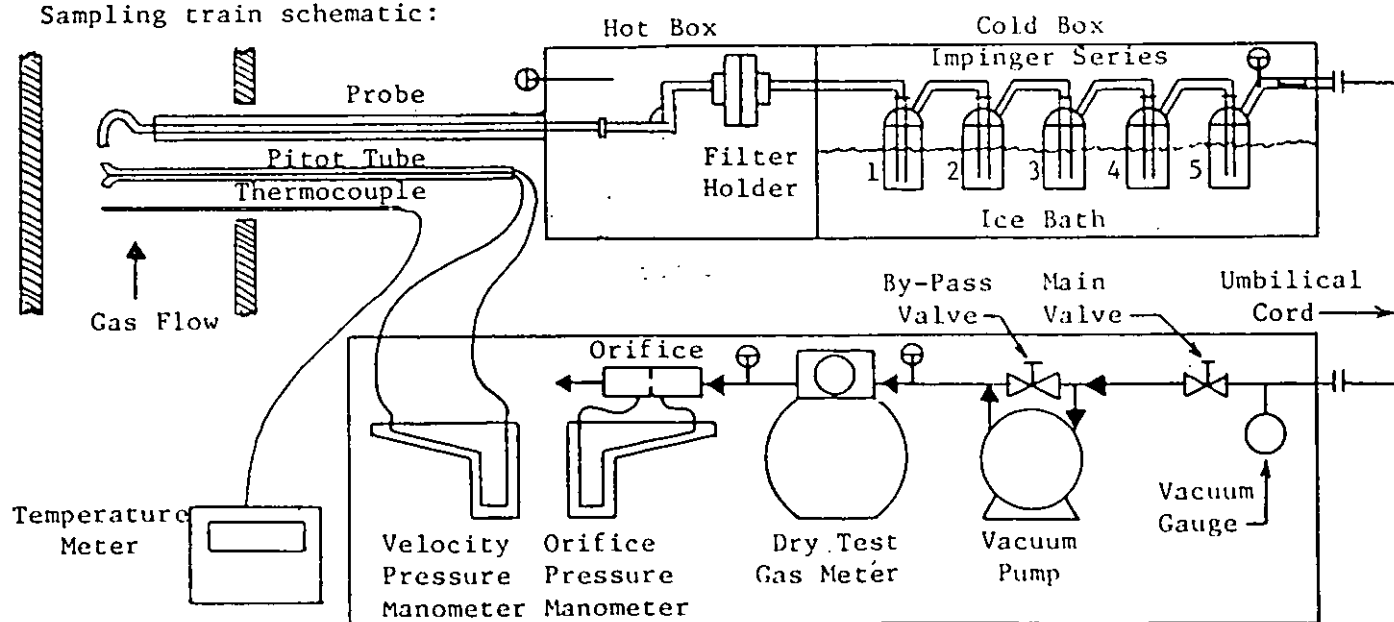
M: Modified Greenburg-Smith design (straight tip)

Probe: 5 foot with stainless steel liner.

Nozzle: stainless steel, .375 inch nominal diameter

Sampling time: 60 minutes per point; 5 minutes per test run.

Sampling train schematic:



⊕ Indicates
Thermometer

Control Unit

A representative particulate sample was acquired by sampling for equal periods of time at the center of a number of equal area regions in the duct. At each sampling point the gas velocity head and temperature were measured and the sampling rate rapidly adjusted to isokinetic conditions with the aid of a nomograph. Sample gas drawn into the nozzle flowed through the probe to the glass fiber filter where the particulates were collected. The gases then passed through the ice-cooled condenser (impingers and desiccant column) which quantitatively sorbed all moisture from the gas stream. The gas then passed through the vacuum pump, the drytest meter and the calibrated orifice.

Leak checks to detect any dilution air being pulled into the sampling line were performed at the beginning and end of each test run and also when and if any sample line connections were broken.

After completion of each test run, the sampling train was removed to the clean-up area for sample recovery. The filter was removed from the filter holder and placed in Container #1. Particulate matter collected in the nozzle, probe, cyclone and all connecting glassware in front of the filter was quantitatively transferred to Container #2 by means of a distilled water wash followed by an acetone wash. A stiff brush was used in the probe cleaning step to help dislodge deposits. The water collected in each of the impingers (desiccant column excluded) was measured and transferred to Container #3. All sample exposed surfaces between the filter and the desiccant column were then rinsed with distilled water and the rinsings added to Container #3. These same surfaces were then rinsed with acetone and the rinsings placed in Container #4. The desiccant column was then weighed and its contents transferred to a waste desiccant container.

Sample analysis was performed at MMT's laboratory. The filter was dried in a 105°C oven for 3 hours and then desiccated to constant weight. The contents of Containers #2 and #4 were each transferred to a tared beaker, evaporated to near dryness, and

desiccated to a constant weight. Organic particulate matter was extracted (separatory funnel) from the impinger solution in Container #3 with three (3) 25 ml portions of chloroform followed by three (3) 25 ml portions of ethyl ether. The ether and chloroform extracts were combined in a tared dish, evaporated to near dryness, and then desiccated to constant weight. The total mass of particulate matter collected during each test run is the sum of the front catch, filler catch and back catch.

3.7 Source Plume Opacity

The opacity of emissions from the stationary source was determined visually by a certified observer per EPA Method 9.

The observer positioned himself at a distance sufficient to provide a clear view of the emissions with the sun oriented in the 140° sector to his back. Consistent with the requirement, the observer's line of site was, as much as possible, perpendicular to the plume's direction.

Opacity observations were made at the point of greatest opacity in that portion of the plume where condensed water vapor was not present. Observations were made at 15-second intervals and recorded to the nearest 5 percent opacity. (Refer section 2.2, page 2)

4 CYCLONE DISCHARGE PROCEDURE

Two preweighed wheelbarrows were alternately placed under the cyclone A2 bottom discharge pipe. Approximately every 10 minutes the wheelbarrow under the discharge pipe would be replaced with the other wheelbarrow and then weighed. This was done continuously during the test period, including the change over time between each of the runs.

APPENDIX A
CALCULATIONS

DEFINITION OF VARIABLES

An CROSS-SECTIONAL AREA OF NOZZLE, SF
 As CROSS-SECTIONAL AREA OF STACK, SF
 Bwp EFFLUENT MOISTURE CONTENT, PERCENT BY VOLUME
 Bws EFFLUENT MOISTURE CONTENT, PROPORTION BY VOLUME
 Ca* EFFLUENT PARTICULATE CONCENTRATION AT ACTUAL
 CONDITIONS, GR/ACF; *=f,b,t; Caf: FRONT CATCH ONLY;
 Cab: BACK CATCH ONLY; Cat: TOTAL CATCH
 Cd EFFLUENT CARBON DIOXIDE CONCENTRATION, % V/V DRY
 Cm EFFLUENT CARBON MONOXIDE CONCENTRATION, % V/V DRY
 Cp PITOT TUBE COEFFICIENT, DIMENSIONLESS
 Cs* EFFLUENT PARTICULATE CONCENTRATION AT DRY STANDARD
 CONDITIONS, GR/DSCF; *=f,b,t; Csf: FRONT CATCH ONLY;
 Csb: BACK CATCH ONLY; Cst: TOTAL CATCH
 Cu* EFFLUENT PARTICULATE CONCENTRATION AT STANDARD
 CONDITIONS, GR/SCF; *=f,b,t; Cuf: FRONT CATCH ONLY;
 Cub: BACK CATCH ONLY; Cwt: TOTAL CATCH
 Dn NOZZLE DIAMETER, IN
 I ISOKINETIC VARIATION, %
 Md EFFLUENT MOLECULAR WEIGHT, LB/LB-MOLE, DRY BASIS
 Ms EFFLUENT MOLECULAR WEIGHT, LB/LB-MOLE, WET BASIS
 Ni EFFLUENT NITROGEN CONCENTRATION, % V/V DRY
 OX EFFLUENT OXYGEN CONCENTRATION, % V/V DRY
 Pb BAROMETRIC PRESSURE, IN HG
 Pg STACK STATIC PRESSURE, IN WC
 Pd AVERAGE PRESSURE DROP ACROSS THE METERING
 ORIFICE, IN WC
 Ps STACK ABSOLUTE PRESSURE, IN HG
 Pv AVERAGE SQUARE-ROOT VELOCITY PRESSURE, IN WC
 Qa EFFLUENT FLOW RATE AT ACTUAL CONDITIONS, ACFM
 Qs EFFLUENT FLOW RATE AT STANDARD CONDITIONS, SCFM
 Qsd ... EFFLUENT FLOW RATE AT STANDARD CONDITIONS,
 DRY BASIS, DSCFM
 Rc* SOURCE PARTICULATE EMISSION RATE, CLASSICAL
 METHOD, LB/HR; *=f,b,t; Rcf: FRONT CATCH ONLY;
 Rcb: BACK CATCH ONLY; Rct: TOTAL CATCH
 Rr* SOURCE PARTICULATE EMISSION RATE, RATIO OF
 AREAS METHOD, LB/HR; *=f,b,t; Rrf: FRONT CATCH ONLY;
 Rrb: BACK CATCH ONLY; Rrt: TOTAL CATCH
 S1 STACK DIAMETER OR LENGTH, IN
 Sw STACK WIDTH, IN
 T1 TOTAL SAMPLING TIME, MIN
 Tm AVERAGE DRY GAS METER TEMPERATURE, DEG F
 Te AVERAGE EFFLUENT TEMPERATURE, DEG F
 V1 VOLUME OF LIQUID COLLECTED, ML
 Vm VOLUME OF GAS SAMPLED AT METER CONDITIONS, DCF
 Vms ... VOLUME OF GAS SAMPLED AT STANDARD CONDITIONS, DSCF
 Vs AVERAGE EFFLUENT VELOCITY, FPS
 Vw VOLUME OF WATER VAPOR COLLECTED AT STANDARD
 CONDITIONS, SCF
 Wb MASS OF PARTICULATE MATTER COLLECTED IN THE
 BACK (WET) CATCH, G
 Wf MASS OF PARTICULATE MATTER COLLECTED IN THE
 FRONT (DRY) CATCH, G
 Wt TOTAL MASS OF PARTICULATE MATTER COLLECTED, G
 Y DRY GAS METER COEFFICIENT, DIMENSIONLESS

EQUATIONS USED TO CALCULATE PARTICULATE EMISSIONS

$$A_n = 0.005454154 \cdot D_n \cdot D_n$$

$$A_s = 0.005454154 \cdot S_1 \cdot S_1 \quad (\text{FOR ROUND STACKS})$$

$$A_s = S_1 \cdot S_w / 144.0 \quad (\text{FOR RECTANGULAR STACKS})$$

$$P_s = P_b + P_g/13.6$$

$$NI = 100.0 - CD - OX - CM$$

$$W_t = W_f + W_b$$

$$V_{ms} = (528/29.92) \cdot V_m \cdot Y \cdot (P_b + P_g/13.6) / (T_m + 460.0)$$

$$V_w = 0.04707 \cdot V_1$$

$$B_{ws} = V_w / (V_w + V_{ms})$$

$$B_{wp} = 100.0 \cdot B_{ws}$$

$$M_d = 0.440 \cdot CD + 0.320 \cdot OX + 0.280 \cdot (NI + CM)$$

$$M_s = M_d \cdot (1.0 - B_{ws}) + 18.0 \cdot B_{ws}$$

$$V_s = 85.49 \cdot C_p \cdot P_v \cdot \text{SQRT}((T_s + 460.0)/(M_s \cdot P_s))$$

$$Q_a = 60.0 \cdot V_s \cdot A_s$$

$$Q_s = Q_a \cdot (528/29.92) \cdot P_s / (T_s + 460.0)$$

$$Q_{sd} = Q_s \cdot (1.0 - B_{ws})$$

$$I = 0.09450 \cdot (T_s + 460.0) \cdot V_{ms} / (P_s \cdot V_s \cdot A_n \cdot T_i \cdot (1.0 - B_{ws}))$$

$$C_{sf} = 15.42 \cdot W_f / V_{ws}$$

$$C_{sb} = 15.42 \cdot W_b / V_{ws}$$

$$C_{st} = 15.42 \cdot W_t / V_{ws}$$

$$C_{wf} = C_{sf} / (1.0 - B_{ws})$$

$$C_{wb} = C_{sb} / (1.0 - B_{ws})$$

$$C_{wt} = C_{st} / (1.0 - B_{ws})$$

$$C_{af} = C_{wf} \cdot (29.92/528.0) \cdot (T_s + 460.0) / P_s$$

$$C_{ab} = C_{wb} \cdot (29.92/528.0) \cdot (T_s + 460.0) / P_s$$

$$C_{at} = C_{wt} \cdot (29.92/528.0) \cdot (T_s + 460.0) / P_s$$

$$R_{cf} = 0.008578 \cdot C_{sf} \cdot Q_{sd}$$

$$R_{cb} = 0.008578 \cdot C_{sb} \cdot Q_{sd}$$

$$R_{ct} = 0.008578 \cdot C_{st} \cdot Q_{sd}$$

$$R_{rf} = 0.008578 \cdot C_{sf} \cdot (V_{ms}/T_i) \cdot (A_s/A_n)$$

$$R_{rb} = 0.008578 \cdot C_{sb} \cdot (V_{ms}/T_i) \cdot (A_s/A_n)$$

$$R_{rt} = 0.008578 \cdot C_{st} \cdot (V_{ms}/T_i) \cdot (A_s/A_n)$$

DEFINITION OF UNIT ABBREVIATIONS

ACFM ACTUAL CUBIC FEET PER MINUTE
DEG F DEGREES FAHRENHEIT
DCF DRY CUBIC FEET
DSCF DRY STANDARD CUBIC FEET
DSCFM DRY STANDARD CUBIC FEET PER MINUTE
FPS FEET PER SECOND
G GRAMS
GR/ACF GRAINS PER ACTUAL CUBIC FOOT
GR/DSCF GRAINS PER DRY STANDARD CUBIC FOOT
GR/SCF GRAINS PER STANDARD CUBIC FOOT
IN INCHES
IN HG INCHES OF MERCURY
IN WC INCHES OF WATER
LB/HR POUNDS PER HOUR
LB/LB-MOLE .. POUND PER POUND-MOLE
MIN MINUTES
ML MILLILITERS
SCF STANDARD CUBIC FEET
SCFM STANDARD CUBIC FEET PER MINUTE
SF SQUARE FEET
% V/V DRY ... PERCENT BY VOLUME, DRY BASIS

DEFINITION OF STANDARD CONDITIONS

STANDARD TEMPERATURE 68 DEGREES FAHRENHEIT
STANDARD PRESSURE 29.92 INCHES OF MERCURY

PARTICULATE EMISSION TEST CALCULATIONS

PROJECT NUMBER: 8014	COMPANY: SOUTHERN MN. BEET SUGAR
TEST NUMBER: 1	SOURCE: CYCLONE "A-2"
RUN NUMBER: 1	TIME: 1/21/88 1128-1231

TEST DATA

GAS METER COEFFICIENT	1.0035 Y	VOLUME OF LIQUID COLLECTED, ML	515.5 V1
PITOT TUBE COEFFICIENT	0.840 Cp	GAS COMPOSITION, % V/V DRY:	
NOZZLE DIMENSIONS:		CARBON DIOXIDE	5.50 CD
DIAMETER, IN	0.375 Dn	OXYGEN	14.20 OX
AREA, SF	0.000767 An	CARBON MONOXIDE	0.00 CM
		NITROGEN (BY DIFFERENCE)	80.30 NI
STACK DIMENSIONS:		AVE. TRAVERSE POINT DATA:	
DIAMETER/LENGTH, IN	47.50 S1	STACK TEMP., DEG F	288 Ts
WIDTH, IN	0.00 Sw	METER TEMP., DEG F	60 Tm
AREA, SF	12.306 As	ORIFICE PRESSURE, IN WC	1.450 Po
BAROMETRIC PRESSURE, IN HG	29.30 Pb	SQRT VELOCITY P., IN WC	0.421 Pv
STACK PRESSURES:		MASS OF PARTICULATE MATTER COLLECTED, G:	
STATIC, IN WC	0.00 Pg	FRONT CATCH (94.8%)	0.4246 Wf
ABSOLUTE, IN HG	29.30 Ps	BACK CATCH (5.2%)	0.0234 Wb
SAMPLING TIME, MIN	60.00 Ti	TOTAL CATCH	0.4480 Wt
VOLUME OF GAS SAMPLED AT METER, DCF	40.427 Vm		

CALCULATED RESULTS

VOLUME OF GAS SAMPLED AT METER, DSCF	39.872 Vms	GAS MOLECULAR WEIGHT:	
		DRY BASIS, LB/LB-MOLE	29.45 Mg
		WET BASIS, LB/LB-MOLE	25.12 Ms
EQUIVALENT VOLUME OF WATER VAPOR COLLECTED, SCF	24.265 Vw	AVERAGE GAS VELOCITY, FPS	30.52 Vs
GAS MOISTURE CONTENT:		GAS VOLUMETRIC FLOW RATE:	
VOLUME FRACTION	0.3783 Zws	ACTUAL, ACFM	22532 Qa
PERCENT BY VOLUME	37.83 Zwp	STANDARD, SCFM	15567 Qs
		DRY STANDARD, DSCFM	9678 Qsd
		ISOKINETIC VARIATION, %	110.24 I

PARTICULATE EMISSION PARAMETER	FRONT CATCH	BACK CATCH	TOTAL CATCH
PARTICULATE CONCENTRATION			
ACTUAL, GR/ACF	0.0705 Caf	0.0039 Cab	0.2744 Cat
STANDARD, GR/SCF	0.1021 Cwf	0.0056 Cwb	0.1077 Cwt
DRY STANDARD, GR/DSCF	0.1642 Csf	0.0090 Csd	0.1733 Cst
PARTICULATE EMISSION RATE, LB/HR			
CLASSICAL METHOD	13.63 Rcf	0.75 Rcb	14.38 Rct
RATIO OF AREAS METHOD	15.02 Rrf	0.63 Rrb	15.65 Rrt

STANDARD CONDITIONS: 68 DEG F, 29.92 IN HG

* NON-APPLICABLE DATA

PARTICULATE EMISSION TEST CALCULATIONS

PROJECT NUMBER: 8014	COMPANY: SOUTHERN MN. BEET SUGAR
TEST NUMBER: 1	SOURCE: CYCLONE "A-2"
RUN NUMBER: 2	TIME: 1/21/88 1248-1352

TEST DATA

GAS METER COEFFICIENT	1.0035 Y	VOLUME OF LIQUID COLLECTED, ML	460.0 VI
PITOT TUBE COEFFICIENT	0.840 Cp	GAS COMPOSITION, % V/V DRY;	
NOZZLE DIMENSIONS;		CARBON DIOXIDE	4.60 CD
DIAMETER, IN	0.375 Dn	OXYGEN	15.60 OX
AREA, SF	0.200767 An	CARBON MONOXIDE	0.00 CM
		NITROGEN (BY DIFFERENCE)	79.80 NI
STACK DIMENSIONS;		AVE. TRAVERSE POINT DATA;	
DIAMETER/LENGTH, IN	47.50 S1	STACK TEMP., DEG F	292 Ts
WIDTH, IN	0.20 Sw	METER TEMP., DEG F	68 Tm
AREA, SF	12.306 As	ORIFICE PRESSURE, IN WC	1.385 Po
BAROMETRIC PRESSURE, IN HG	29.30 Pb	SQRT VELOCITY P., IN WC	2.422 Pv
STACK PRESSURES;		MASS OF PARTICULATE MATTER	
STATIC, IN WC	2.00 Pg	COLLECTED, G;	
ABSOLUTE, IN HG	29.30 Ps	FRONT CATCH (96.0%)	0.4116 Wf
		BACK CATCH (4.0%)	0.0170 Wb
SAMPLING TIME, MIN	60.00 T:	TOTAL CATCH	0.4286 Wt
VOLUME OF GAS SAMPLED			
AT METER, DCF	38.299 Vm		

CALCULATED RESULTS

VOLUME OF GAS SAMPLED		GAS MOLECULAR WEIGHT;	
AT METER, DSCF	37.767 Vms	DRY BASIS, LB/LB-MOLE	29.36 Md
		WET BASIS, LB/LB-MOLE	25.22 Ms
EQUIVALENT VOLUME OF WATER		AVERAGE GAS VELOCITY, FPS	30.60 Vs
VAPOR COLLECTED, SCF	21.652 Vw		
GAS MOISTURE CONTENT;		GAS VOLUMETRIC FLOW RATE;	
VOLUME FRACTION	0.3644 Bws	ACTUAL, ACFM	22593 Qa
PERCENT BY VOLUME	36.44 Bwp	STANDARD, SCFM	15535 Qs
		DRY STANDARD, DSCFM	9974 Qsc
		ISOKINETIC VARIATION, %	102.34 I

PARTICULATE EMISSION PARAMETER	FRONT CATCH	BACK CATCH	TOTAL CATCH
PARTICULATE CONCENTRATION:			
ACTUAL, GR/ACF	0.0734 Caf	0.0030 Cab	0.0765 Cat
STANDARD, GR/SCF	0.1068 Cwf	0.0244 Cwb	0.1112 Cwt
DRY STANDARD, GR/DSCF	0.1681 Csf	0.0069 Csb	0.1750 Cst
PARTICULATE EMISSION RATE, LB/HR			
CLASSICAL METHOD	14.23 Rcf	0.59 Rcb	14.82 Rct
RATIO OF AREAS METHOD	14.56 Rrf	0.60 Rrb	15.16 Rrt

STANDARD CONDITIONS: 68 DEG F, 29.92 IN HG

* NON-APPLICABLE DATA

PARTICULATE EMISSION TEST CALCULATIONS

PROJECT NUMBER: 8014 COMPANY: SOUTHERN MN. BEET SUGAR
 TEST NUMBER: 1 SOURCE: CYCLONE "A-2"
 RUN NUMBER: 3 TIME: 1/21/88 1430-1533

TEST DATA

GAS METER COEFFICIENT	1.0035 Y	VOLUME OF LIQUID COLLECTED, ML	614.1 V1
PITOT TUBE COEFFICIENT	0.840 Cp	GAS COMPOSITION, % V/V DRY:	
NOZZLE DIMENSIONS:		CARBON DIOXIDE	6.00 CD
DIAMETER, IN	0.375 Dn	OXYGEN	13.10 OX
AREA, SF	0.000767 An	CARBON MONOXIDE	0.20 CM
		NITROGEN (BY DIFFERENCE)	80.90 NI
STACK DIMENSIONS:		AVE. TRAVERSE POINT DATA:	
DIAMETER/LENGTH, IN	47.50 S1	STACK TEMP., DEG F	292 Ts
WIDTH, IN	0.02 Sw	METER TEMP., DEG F	68 Tm
AREA, SF	12.306 As	ORIFICE PRESSURE, IN WC	1.555 Po
BAROMETRIC PRESSURE, IN HG	29.30 Pb	SQRT VELOCITY P., IN WC	0.446 Pv
STACK PRESSURES:		MASS OF PARTICULATE MATTER	
STATIC, IN WC	0.20 Pg	COLLECTED, G:	
ABSOLUTE, IN HG	29.30 Ps	FRONT CATCH (95.8%)	0.4170 Wf
		BACK CATCH (4.2%)	0.0184 Wb
SAMPLING TIME, MIN	60.00 Ti	TOTAL CATCH	0.4354 Wt
VOLUME OF GAS SAMPLED AT METER, DCF	41.000 Vm		

CALCULATED RESULTS

VOLUME OF GAS SAMPLED AT METER, DSCF	42.448 Vms	GAS MOLECULAR WEIGHT:	
		DRY BASIS, LB/LB-MOLE	29.46 Md
		WET BASIS, LB/LB-MOLE	24.70 Ms
EQUIVALENT VOLUME OF WATER VAPOR COLLECTED, SCF	28.906 Vw	AVERAGE GAS VELOCITY, FPS	32.65 Vs
GAS MOISTURE CONTENT:		GAS VOLUMETRIC FLOW RATE:	
VOLUME FRACTION	0.4168 Bws	ACTUAL, ACFM	24108 Qa
PERCENT BY VOLUME	41.68 Bwp	STANDARD, SCFM	16566 Qs
		DRY STANDARD, DSCFM	9662 Qsd
		ISOKINETIC VARIATION, %	112.02 I

PARTICULATE EMISSION PARAMETER	FRONT CATCH	BACK CATCH	TOTAL CATCH
PARTICULATE CONCENTRATION			
ACTUAL, GR/ACF	0.0637 Caf	0.0328 Cab	0.0665 Cat
STANDARD, GR/SCF	0.0927 Cwf	0.0041 Cwb	0.0968 Cwt
DRY STANDARD, GR/DSCF	0.1590 Csf	0.0070 Csb	0.1660 Cst
PARTICULATE EMISSION RATE, LB/HR			
CLASSICAL METHOD	13.18 Rcf	0.58 Rcb	13.76 Rct
RATIO OF AREAS METHOD	14.75 Rrf	0.65 Rrb	15.42 Rrt

STANDARD CONDITIONS: 68 DEG F, 29.92 IN HG * NON-APPLICABLE DATA

TRAVERSE POINT DATA SUMMARY AND VELOCITY PROFILE

PROJECT NUMBER: 8014 COMPANY: SOUTHERN MN. BEET SUGAR
 TEST NUMBER: 1 SOURCE: CYCLONE "A-2"
 RUN NUMBER: 1 TIME: 1/21/88 1128-1231

		TRAVERSE POINT DATA					VELOCITY PROFILE	
SAMPLING LOCATION	PORT POINT	VELOCITY PRESSURE IN WC	ORIFICE PRESSURE IN WC	TEMPERATURE, DEG.F STACK GAS	METER INLET	METER OUTLET	SQRT VELOCITY PRESSURE	GAS VELOCITY FT/SEC
A	1	0.160	1.300	290	68	68	0.400	29.00
A	2	0.160	1.300	288	68	68	0.400	28.96
A	3	0.170	1.300	285	68	68	0.412	29.79
A	4	0.190	1.400	284	68	68	0.436	31.47
A	5	0.220	1.600	291	68	68	0.469	34.03
A	6	0.210	1.900	293	68	68	0.458	33.29
A	7	0.220	1.700	294	68	68	0.469	34.09
A	8	0.210	1.800	295	68	68	0.458	33.33
A	9	0.210	1.700	296	68	68	0.458	33.35
A	10	0.160	1.700	291	68	68	0.400	29.02
B	1	0.160	1.300	287	68	68	0.400	28.94
B	2	0.160	1.300	285	68	68	0.400	28.90
B	3	0.160	1.300	289	68	68	0.400	28.98
B	4	0.190	1.600	291	68	68	0.436	31.62
B	5	0.200	1.600	290	68	68	0.447	32.42
B	6	0.190	1.600	290	68	68	0.436	31.60
B	7	0.170	1.400	286	68	68	0.412	29.81
B	9	0.140	1.100	282	68	68	0.374	26.98
B	9	0.140	1.100	282	68	68	0.374	26.98
B	10	2.150	1.100	279	68	68	0.387	27.87
AVERAGE		0.179	1.450	288	68	68	0.421	30.52

TRAVERSE POINT DATA SUMMARY AND VELOCITY PROFILE

PROJECT NUMBER: 8814 COMPANY: SOUTHERN MN. BEET SUGAR
 TEST NUMBER: 1 SOURCE: "CYCLONE "A-2"
 RUN NUMBER: 2 TIME: 1/21/88 1248-1352

		TRAVERSE POINT DATA					VELOCITY PROFILE	
SAMPLING LOCATION PORT	POINT	VELOCITY PRESSURE	ORIFICE PRESSURE	TEMPERATURE, DEG. F.			SORT VELOCITY	GAS VELOCITY
		IN WC	IN WC	GAS	INLET	METER OUTLET	PRESSURE	FT/SEC
A	1	0.180	1.400	293	68	68	0.424	30.76
A	2	0.190	1.500	294	68	68	0.436	31.62
A	3	0.190	1.500	295	68	68	0.436	31.64
A	4	0.192	1.500	295	68	68	0.436	31.64
A	5	0.200	1.500	298	68	68	0.447	32.53
A	6	0.200	1.500	300	68	68	0.447	32.57
A	7	0.180	1.400	295	68	68	0.424	30.80
A	8	0.160	1.200	287	68	68	0.400	28.88
A	9	0.130	1.000	288	68	68	0.361	26.05
A	10	0.130	1.000	286	68	68	0.361	26.02
B	1	0.170	1.300	287	68	68	0.412	29.77
B	2	0.190	1.500	292	68	68	0.436	31.58
B	3	0.130	1.000	291	68	68	0.361	26.10
B	4	0.210	1.600	292	68	68	0.458	33.20
B	5	0.230	1.800	294	68	68	0.480	34.79
B	6	0.210	1.600	294	68	68	0.458	33.24
B	7	0.190	1.500	293	68	68	0.436	31.60
B	8	0.190	1.500	292	68	68	0.436	31.58
B	9	0.170	1.300	286	68	68	0.412	29.75
B	10	0.150	1.100	288	68	68	0.387	27.98
AVERAGE		0.180	1.365	292	68	68	0.422	30.60

TRAVERSE POINT DATA SUMMARY AND VELOCITY PROFILE

PROJECT NUMBER: 8314 COMPANY: SOUTHERN MN. BEET SUGAR
 TEST NUMBER: 1 SOURCE: CYCLONE "A-2"
 RUN NUMBER: 3 TIME: 1/21/88 1430-1533

		TRAVERSE POINT DATA					VELOCITY PROFILE	
SAMPLING LOCATION PORT	POINT	VELOCITY	ORIFICE	TEMPERATURE, DEG.F			SQRT	GAS
		PRESSURE IN WC	PRESSURE IN WC	STACK GAS	METER INLET	METER OUTLET	VELOCITY PRESSURE	VELOCITY FT/SEC
A	1	0.190	1.500	292	68	68	0.435	31.91
A	2	0.230	1.800	294	68	68	0.480	35.15
A	3	0.220	1.750	296	68	68	0.469	34.43
A	4	0.220	1.750	294	68	68	0.469	34.38
A	5	0.220	1.500	295	68	68	0.469	34.40
A	6	0.190	1.400	293	68	68	0.436	31.93
A	7	0.180	1.300	292	68	68	0.424	31.06
A	8	0.170	1.300	290	68	68	0.412	30.14
A	9	0.160	1.300	289	68	68	0.400	29.22
A	10	0.160	1.300	287	68	68	0.400	29.18
B	1	0.180	1.400	298	68	68	0.424	31.18
B	2	0.190	1.500	292	68	68	0.436	31.91
B	3	0.190	1.500	293	68	68	0.436	31.93
B	4	0.200	1.600	293	68	68	0.447	32.76
B	5	0.210	1.700	294	68	68	0.458	33.59
B	6	0.220	1.750	293	68	68	0.469	34.36
B	7	0.240	1.900	294	68	68	0.490	35.91
B	8	0.230	1.800	292	68	68	0.480	35.11
B	9	0.210	1.650	290	68	68	0.458	33.50
B	10	0.180	1.400	288	68	68	0.424	30.98
AVERAGE		0.200	1.555	292	68	68	0.446	32.65

APPENDIX B

FIELD DATA FORMS

**SOURCE EMISSION TEST
FIELD DATA SHEET**

TEST: / RUN: /
Page / of /

TEST IDENTIFICATION		EQUIPMENT IDENTIFICATION		NOMOGRAPH PARAMETERS
MMT Job Number:	8015	Control Unit No.:	1	$\Delta H @ 1.95$
Date:	1/21/88	Gas Meter Coefficient:	1 0.9985	TM 1.10
Company:	Southern Mn Sugar	Sample Box No.:	#1	MC 35
Source:	Cyclone A-2	Probe No.:	5ft Length: 5ft	PS/PM 1.00
Source Dimensions:	47.5	Pitot No.:	5-1 Coefficient: .84	C
Test Team:	CM/RL	Nozzle No.:	5 Diameter: 0.375	TS 300290
Test Procedure:	M-5	Filter No.:	8093	R
Ambient Temp., °F:		Barometric Pressure, in.Hg: 29.30		Static Pressure, in.WC: 0.00

CLOCK TIME hours	TRAVERSE POINT NUMBER	SAMPLE TIME min.	SAMPLE VOLUME cu.ft.	VELOCITY HEAD in.WC	ORIFICE ΔH , in.WC		PUMP VAC. in.Hg	TEMPERATURE, DEG F					LAST IMP.
					REQ.	ACT.		STACK GAS	GAS METER IN	GAS METER OUT	OVEN	PROBE	
11:28	A-1	0	380.598	0.16	1.3	1.3	2	290	74	74	255	Max	30
31	A-2	3	82.3	0.16	1.3	1.3	2	288	72	72			
34	A-3	6	84.4	0.16	1.3	1.3	2	285	68	68	260		34
37	A-4	9	86.4	0.17	1.4	1.4	2	284	68	68			
40	A-5	12	88.3	0.19	1.6	1.6	3	291	68	68			
43	A-6	15	90.5	0.22	1.8	1.8	4	293	68	68	260		36
46	A-7	18	92.7	0.21	1.7	1.7	4	294	68	68			
49	A-8	21	94.8	0.22	1.8	1.8	4	295	68	68	265		39
52	A-9	24	97.1	0.21	1.7	1.7	5	296	68	68			
55	A-10	27	99.5	0.21	1.7	1.7	5	291	68	68			
11:58	END A	30	401.9										
12:01	B-1	0	1.9	0.16	1.3	1.3	2	287	68	68	265	Max	40
4	B-2	3	3.8	0.16	1.3	1.3	2	285	68	68			
7	B-3	6	5.7	0.16	1.3	1.3	3	289	68	68			
10	B-4	9	7.3	0.19	1.6	1.6	4	291	68	68			
13	B-5	12	9.2	0.20	1.6	1.6	4	290	68	68	265		44
16	B-6	15	12.0	0.19	1.6	1.6	4	290	68	68			
19	B-7	18	14.2	0.17	1.4	1.4	3	286	68	68			
22	B-8	21	16.2	0.14	1.1	1.1	2	282	68	68	260		49
25	B-9	24	18.1	0.14	1.1	1.1	2	282	68	68			
28	B-10	27	19.6	0.15	1.1	1.1	2	279	68	68			
12:31	END B	30	421.025										

MOISTURE DETERMINATION					
IMPINGER	1	2	3	4	5
Final	391.9	258.6	42.4	718.2	
Initial	100.0	100.0	0	695.6	
Difference	291.9	158.6	42.4	22.6	
Total Moisture Collected: 515.5					

SYSTEM LEAK CHECKS		
Time	Rate (cfm)	Vac. (in.Hg)
11:16	27" Hg	0.002 cfm
12:33	0.002	15" Hg

Impinger Catch Description: light yellow in color

DETERMINATION OF GAS COMPOSITION BY ORSAT ANALYSIS								
Sample Id:	Replicate 1		Replicate 2		Replicate 3		Average	
	Buret Reading	Percent Volume	Buret Reading	Percent Volume	Buret Reading	Percent Volume	Compound	Percent Volume
# 2								
Initial Reading								
Carbon Dioxide	94.4	5.6	94.5	5.5	94.3	5.5	CO2	5.5
Oxygen	80.2	14.2	80.2	14.3	80.3	14.2	O2	14.2
Carbon Monoxide							CO	

Total Sampling Time, min.: 60
Volume of Gas Sampled: DCF: 40.4270

SOURCE EMISSION TEST
FIELD DATA SHEET

TEST: 2 RUN: 1
Page 1 of 1

TEST IDENTIFICATION		EQUIPMENT IDENTIFICATION		NOMOGRAPH PARAMETERS
MMT Job Number:	8014	Control Unit No.:	1 10035	$\Delta H@$ 1.45
Date:	1-21-88	Gas Meter Coefficient:	0.4445	TM 68
Company:	S. MN Sugar Coop	Sample Box No.:	#2	MC 35
Source:	A-2 Cyclone	Probe No.:	5-1 Length: 5'	PS/PM 1.00
Source Dimensions:	47.5	Pitot No.:	5-1 Coefficient: 0.84	C
Test Team:	CM RL	Nozzle No.:	5 Diameter: 0.375	TS 290
Test Procedure:	EPA 5	Filter No.:	8094	R
Ambient Temp., °F:		Barometric Pressure, in.Hg: 29.30 Static Pressure, in.WC: 200		

CLOCK TIME hours	TRAVERSE POINT NUMBER	SAMPLE TIME min.	SAMPLE VOLUME cu.ft.	VELOCITY HEAD in.WC	ORIFICE ΔH , in.WC		PUMP VAC. in.Hg	TEMPERATURE, DEG F					LAST IMP.
					REQ.	ACT.		STACK GAS	GAS METER IN	GAS METER OUT	OVEN	PROBE	
1248	B-1	0	422.280	0.18	1.4	1.4	4	293	68	68	265	Max	38
51	2	3	24.2	0.19	1.5	1.5	5	294	68	68			
54	3	6	26.2	0.19	1.5	1.5	5	295	68	68			
57	4	9	28.2	0.19	1.5	1.5	5	295	68	68	260		40
1300	5	12	30.1	0.20	1.5	1.5	5	298	68	68			
3	6	15	32.1	0.20	1.5	1.5	5	300	68	68			
6	7	18	34.1	0.18	1.4	1.4	5	295	68	68			
9	8	21	36.0	0.16	1.2	1.2	4	287	68	68	265		39
12	9	24	37.8	0.13	1.0	1.0	2	288	68	68			
15	10	27	39.6	0.13	1.0	1.0	2	286	68	68			
1218	end B	30	41.2										
1322	A-1	0	41.2	0.17	1.3	1.3	4	287	68	68	265	Max	43
25	2	3	43.1	0.19	1.5	1.5	6	292	68	68			
28	3	6	45.0	0.13	1.0	1.0	3	291	68	68			
31	4	9	46.6	0.21	1.6	1.6	7	292	68	68	265		46
34	5	12	48.7	0.23	1.8	1.8	9	294	68	68			
37	6	15	50.8	0.21	1.6	1.6	7	294	68	68			
40	7	18	52.9	0.19	1.5	1.5	6	293	68	68			
43	8	21	55.0	0.19	1.5	1.5	6	292	68	68	265		48
46	9	24	58.9	0.17	1.3	1.3	5	286	68	68			
49	10	27	58.8	0.15	1.1	1.1	3	288	68	68			
1352	end A	30	460.599										

MOISTURE DETERMINATION					
IMPINGER	1	2	3	4	5
Final	266.4	279.6	74.3	7750	
Initial	100	100	0	730.0	
Difference	166.4	179.6	74.3	45.0	
Total Moisture Collected:				460.0	

SYSTEM LEAK CHECKS		
Time	Rate (cfm)	Vac. (in.Hg)
1240	0.001	16"
1353	0.002	19"

Impinger Catch Description: Light Yellow Color

DETERMINATION OF GAS COMPOSITION BY ORSAT ANALYSIS								
Sample Id:	Replicate 1		Replicate 2		Replicate 3		Average	
	Buret Reading	Percent Volume	Buret Reading	Percent Volume	Buret Reading	Percent Volume	Compound	Percent Volume
# 4								
Initial Reading								
Carbon Dioxide	95.4	4.6	95.4	4.5	95.4	4.6	CO2	4.6
Oxygen	79.8	15.6	79.8	15.7	80.0	15.4	O2	15.6
Carbon Monoxide							CO	

Total Sampling Time, min.: 60
Volume of Gas Sampled, DCF: 38.299

SOURCE EMISSION TEST
FIELD DATA SHEET

Page 1 of 1 RUN: 5

TEST IDENTIFICATION		EQUIPMENT IDENTIFICATION		NOMOGRAPH PARAMETERS	
MMT Job Number:	8014	Control Unit No.:	1.0035	ΔH _C	1.95
Date:	1-21-88	Gas Meter Coefficient:	0.995	TM	68
Company:	S. MD Sugar Coop	Sample Box No.:	1	MC	34
Source:	A2 cyclone	Probe No.:	5-1	Length:	5'
Source Dimensions:	47.5"	Pitot No.:	5-1	Coefficient:	0.84
Test Team:	RL CM	Nozzle No.:	5	Diameter:	3/8 (0.375)
Test Procedure:	EPA 5	Filter No.:	8095	TS	290
Ambient Temp., °F:		Barometric Pressure, in.Hg:	29.32	Static Pressure, in.WC:	0.00

CLOCK TIME hours	TRAVERSE POINT NUMBER	SAMPLE TIME min.	SAMPLE VOLUME cu.ft.	VELOCITY HEAD in.WC	ORIFICE ΔH, in.WC		PUMP VAC. in.Hg	TEMPERATURE, DEG F					LAST IMP.
					REQ.	ACT.		STACK GAS	GAS METER IN	GAS METER OUT	OVEN	PROBE	
1430	A-1	0	463.90	0.19	1.5	1.5	2	292	68	68	260	Max	38
33	2	3	65.4	0.23	1.8	1.8	2	294	68	68			
36	3	6	67.6	0.22	1.75	1.75	2	296	68	68			
39	4	9	69.8	0.22	1.75	1.75	3	294	68	68			
42	5	12	71.9	0.22	1.75	1.75	3	295	68	68	260		42
45	6	15	74.1	0.19	1.5	1.5	3	293	68	68			
48	7	18	76.1	0.18	1.4	1.4	2	292	68	68			
51	8	21	78.1	0.17	1.3	1.3	2	290	68	68			
54	9	24	79.9	0.16	1.3	1.3	2	289	68	68	260		44
57	10	27	81.8	0.16	1.3	1.3	2	287	68	68			
1500	end A	30	83.6										
1503	B-1	0	83.6	0.18	1.4	1.4	3	298	68	68		Max	
6	2	3	85.5	0.19	1.5	1.5	3	292	68	68	260		42
9	3	6	87.5	0.19	1.5	1.5	3	293	68	68			
12	4	9	89.5	0.20	1.6	1.6	4	293	68	68			
15	5	12	91.6	0.21	1.7	1.7	4	294	68	68	260		45
18	6	15	93.7	0.22	1.75	1.75	4	293	68	68			
21	7	18	95.9	0.24	1.9	1.9	5	294	68	68			
24	8	21	98.1	0.23	1.8	1.8	5	292	68	68	265		49
27	9	24	100.2	0.21	1.65	1.65	4	290	68	68			
30	10	27	102.4	0.18	1.4	1.4	4	288	68	68			
1533	end B	30	104.390										

MOISTURE DETERMINATION					
IMPINGER	1	2	3	4	5
Final	382.7	331.6	83.7	76.1	
Initial	100	100	0	745.0	
Difference	282.7	231.6	83.7	16.1	
Total Moisture Collected: 614.1					

SYSTEM LEAK CHECKS		
Time	Rate (cfm)	Vac. (in.Hg)
1426	0.003	18" Hg
1534	0.002	15"

Impinger Catch Description: Light Yellow Color

DETERMINATION OF GAS COMPOSITION BY ORSAT ANALYSIS								
Sample Id:	Replicate 1		Replicate 2		Replicate 3		Average	
	Buret Reading	Percent Volume	Buret Reading	Percent Volume	Buret Reading	Percent Volume	Compound	Percent Volume
#6								
Initial Reading								
Carbon Dioxide	94	6	94	6	94.1	5.9	CO2	6.0
Oxygen	80.9	13.1	80.5	12.7	80.7	13.4	O2	13.1
Carbon Monoxide							CO	

Total Sampling Time, min.: 60
Volume of Gas Sampled, bcf: 41.000

VISIBLE EMISSIONS OBSERVATION FORM

Job No.: 8014 Date: 1/21/88 Observer (print): Clifford E. Mohs

Company: Southern Ma Beet Sugar Coop

Address: _____

Source: Cyclone A-2 discharge

Source Dimensions: Height: _____ Diameter: _____

Observer's position from source: _____

Plume Description: large moisture plume

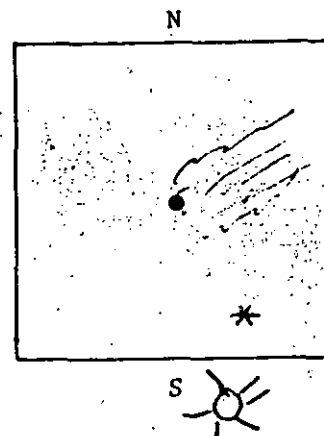
Background Description: Clear sky

Wind Direction: S-10 Speed: SW

Ambient Temperature, °F: 50

Comments (use back of form if necessary):

OBSERVERS (X) POSITION
RELATIVE TO SOURCE (●),
PLUME (≡) AND SUN (☼)



Because the stack was too close to the other stacks and from all the other emission sources it is impossible to take any V.E. Readings. The Plumes are all combining together and there is one large moisture plume heading across the field

VISUAL OBSERVATIONS OF PLUME OPACITY

Observations are to be made at fifteen second intervals and recorded to the nearest five percent opacity

No Reading

To much moisture and Time: Start 11:45 Finish _____
Interferences from other sources

SEC MIN	0	15	30	45
0				
1				
2				
3				
4				
5				
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				
18				
19				

SEC MIN	0	15	30	45
20				
21				
22				
23				
24				
25				
26				
27				
28				
29				
30				
31				
32				
33				
34				
35				
36				
37				
38				
39				

SEC MIN	0	15	30	45
40				
41				
42				
43				
44				
45				
46				
47				
48				
49				
50				
51				
52				
53				
54				
55				
56				
57				
58				
59				

SEC MIN	0	15	30	45
60				
61				
62				
63				
64				
65				
66				
67				
68				
69				
70				
71				
72				
73				
74				
75				
76				
77				
78				
79				

Last Re-Certification Date: 10/21/87 Observers Signature: Clifford E. Mohs

APPENDIX C

LABORATORY REPORT

SUMMARY OF PARTICULATE EMISSION TEST LABORATORY DATA

PROJECT NUMBER: 8014
TEST NUMBER: 1

COMPANY: SOUTHERN MN. BEET SUGAR
SOURCE: CYCLONE "A-2"

MASS OF PARTICULATE MATTER COLLECTED: GRAMS								
RUN NUMBER	FRONT CATCH				BACK CATCH			TOTAL PARTICULATE MASS COLLECTED
	FRONT WASH	CYCLONE CATCH	FILTER CATCH	FRONT TOTAL	IMPINGER CATCH **	IMPINGER WASH	BACK TOTAL	
1	0.1630	0.0000	0.2616	0.4246	0.0112	0.0122	0.0234	0.4480
2	0.1760	0.0000	0.2356	0.4116	0.0087	0.0083	0.0170	0.4286
3	0.1611	0.0000	0.2559	0.4170	0.0122	0.0062	0.0184	0.4354
* NOT APPLICABLE					** CHLOROFORM/ETHYL ETHER EXTRACTION			

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Page 1

Date of Weightings, Filter Weights

ID #	Tare wt Date	1 st wt	2 nd wt	3 rd wt	Usage
1 ms					
8083	12-17-87	1/18/88			
8084	" " "	1/18/88			
8085	" " "	1/18/88			
8086	" " "	1/18/88			
8087	" " "	1/18/88			
8088	12-18-87	1/18/88			
8089					
8090	12-17-87				
8091	12-18-87				
8092	1/20-88	1/25/88	1/26/88		
8093	1/20-88	1/25/88	1/26/88		
8094	1/20-88	1/25/88	1/26/88		
8095	1/20-88	1/25/88	1/26/88		
8096	1/20-88				
8097					
8098					
8099					
1 ms					
8100					
8101					
8102					
8103					
8104					
8105					
8106					
8107					
8108					
8109					

Filter Wts

Page 2

15

ID	TARE WT	1ST WT	2 nd WT	3 rd WT	WT Gain	Test Run
1mg						
8083	.7734	.9202			.1468	S 3-2
8084	.7771	.9587			.1816	N 3-3
8085	.7606	.8753			.1147	S 3-3
8086	.7581	.9707			.2126	S 4-1
8087	.7692	.9194			.1502	N 4-1
8088	.7712	.9708			.1996	N 4-3
8089	.7666	.7665			.0001	Blank
1mg	1.0003				.0003	
8090	.7615					
8091	.7543					
8092	.7675	.7656	.7677	.0001	.2616	Blank
8093	.7694	1.0313	1.314		1.2356	SmBS T-1 R-1
8094	.7570	.9924	.9927		.2356	SmBS T-1 R2
8095	.7630	1.0189	1.0187		.2559	SmBST-1 R3.
8096	.7761					Spare
8097						
8098						
8099						
1mg						
8100						
8101						
8102						
8103						
8104						
8105						
8106						
8107						
8108						
8109						

Probe Rinse, emp. extran, acetone 2 mp. Rinse

Wt's

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Date of Wt's	Sample	TARE	1 st	2 nd	wt gain	
TARE	Final	TARE	WT	WT		
1/22/88		8149	2.4756			SD-1-123 wt
"		8150	2.5009			SD-2-123 wt
"		8151	2.4660			SD-3-123 wt
"		8152	2.4843			SD-4-123 wt
1/22/88		8153	2.4593			Blank
1/25/88	Y27	8154	2.4683	2.4809	2.4800	0.0122 SmnSD T1-R1 xtract
"	"	8155	2.4928	2.5019	2.5005	0.0083 SmnSD T1-R2 ytract
"	"	8156	2.4838	2.5004	2.4998	0.0062 SmnSD T1-R3 ytract
"	"	8157	2.4815	2.6440	2.6430	0.1630 SmnSD T1-R1 Active RP
"	"	8158	2.4982	2.6743	2.6740	0.1760 SmnSD T1-R2 Probe
"	"	8159	2.4742	2.6353	2.6358	0.1611 SmnSD T1-R3 Probe
"	"	OC	1.0001			
"	"	8160	2.4716	2.4833	2.4823	0.0112 SmnSD T1-R3 Acet. Imp
"	"	8161	2.4747	2.4834	2.4833	0.0087 SmnSD T1-R3 Acet. Imp
"	"	8162	2.4629	2.4748	2.4854	0.0122 SmnSD T1-R3 Acet. Imp
"	"	8163	2.4821	2.4825	2.4824	0.0003 Acetone blank
1/25/88	Y27	8164	2.4671	2.4672	2.4673	0.0001 CHCl ₃ + Ether Blank
		8165				
		8166				
		8167				
		8168				
		8169				
		8170				
		8171				
		8172				
		8173				
		8174				
		8175				
		8176				

APPENDIX D

CALIBRATION DATA.

CALIBRATION
DRY TEST METER/ORIFICE METER

Page: SSQA-1-55

Date: 1/11/88 Barometric Pressure, in. Hg. (Pb): 29.12

EQUIPMENT IDENTIFICATION			
Control Unit	Dry Test Meter	Wet Test Meter	Calibration Type
Mfg: <u>RAC</u>	Mfg: <u>Rockwell</u>	Mfg: <u>BCA</u>	General: <u>X</u>
Model: <u>STAKSampler</u>	Model: <u>R-200 TC</u>	Model: <u>63123</u>	Post-test:
SN: <u>2452</u>	SN: <u>3041326</u>	SN: <u>11-AH12</u>	

EQUIPMENT CALIBRATION											
Orifice Pressure Drop in. WC H	Pump Vac. in. Hg	Wet Test Meter			Dry Test Meter						Elapsed Time, min. Q
		Volume, CF		Temp. OF Tw	Volume, CF		Temperature, OF				
		Initial Vwi	Final Vwf		Initial Vdi	Final Vdf	Inlet		Outlet		
							Initial Tii	Final Tif	Initial Toi	Final Tof	
0.5	0	0.00	4.730	56	10.662	15.482	68	68	68	68	12
1.1		4.730	10.500	56.5	15.482	21.358	68	68	68	68	10
2.0		10.500	18.180	56.5	21.358	27.137	68	68	68	68	10
4.0		18.180	26.410	56.5	27.137	32.682	68	68	68	68	8

COMPUTER PRINTOUT							
H	Vw	Tw	Vd	Td	Q	C	Hg
0.5	4.730	56	4.620	68.0	12.0	1.0029	1.7666
1.1	5.770	57	5.875	65.0	10.2	1.0010	1.8173
2.0	7.680	57	7.775	68.0	10.0	1.0056	1.8624
4.0	8.460	57	8.545	68.0	8.0	1.0220	1.9673
AVERAGE CORRECTION FACTOR: C = 1.0029							
AVERAGE ORIFICE CONSTANT: Hg = 1.0534							
EQUATIONS:							
$V_w = V_{wf} - V_{wi}$							
$V_d = V_{df} - V_{di}$							
$T_d = (T_{ii} + T_{if} + T_{oi} + T_{of}) / 4$							
$C = V_w * P_b * (T_d + 460) / (V_d * (P_s * H / 13.6) * (T_w + 460))$							
$H_g = 0.0317 * H * ((T_w + 460) * Q / V_w)^{1/2} / (P_s * (T_d + 460))$							

Calibration Performed by:

(Print) Clifford E. Mohs

(Signature) Clifford E. Mohs

CALIBRATION
DRY TEST METER/ORIFICE METER

Page: SSQA-1- 56

Date: 1/27/88 Barometric Pressure, in. Hg. (Pb): 29.57

EQUIPMENT IDENTIFICATION			
Control Unit	Dry Test Meter	Wet Test Meter	Calibration Type
Mfg: <u>RAC</u>	Mfg: <u>Rockwell</u>	Mfg: <u>GCA</u>	General:
Model: <u>STAK Sampler</u>	Model: <u>R-200 -TC</u>	Model: <u>63123</u>	Post-test: <u>X</u>
SN: <u>2452</u>	SN: <u>3041326</u>	SN: <u>11-AH12</u>	

EQUIPMENT CALIBRATION											
Orifice Pressure Drop in. WC H	Pump Vac. in. Hg	Wet Test Meter			Dry Test Meter						Elapsed Time, min. Q
		Volume, CF		Temp. °F Tw	Volume, CF		Temperature, °F				
		Initial Vwi	Final Vwf		Initial Vdi	Final Vdf	Inlet		Outlet		
							Initial Tii	Final Tif	Initial Toi	Final Tof	
.5	0	0.00	7.057	64.5	510.763	517.853	68	68	68	68	18.0
1.0	0	7.057	14.136	65.0	517.853	524.892	68	68	68	68	13.0
2.0	0	14.136	22.441	65.0	524.892	533.169	68	68	68	68	11.0
3.0	0	22.441	31.518	65.0	533.169	542.214	68	68	68	68	10.0

COMPUTER PRINTOUT							
H	Vw	Tw	Vd	Td	Q	C	HQ
0.5	7.057	65	7.290	68.0	18.0	1.2037	1.6169
1.0	7.079	65	7.039	68.0	13.0	1.0029	1.8873
2.0	9.325	65	8.277	68.0	11.0	1.2041	1.9635
3.0	9.077	65	9.045	68.0	10.0	1.2018	2.0376
AVERAGE CORRECTION FACTOR: C = 1.2039							
AVERAGE ORIFICE CONSTANT: HQ = 1.9267							
EQUATIONS:							
Vw = Vwf - Vwi							
Vd = Vdf - Vdi							
Td = (Tii + Tif + Toi + Tof) / 4							
C = Vw * Pb * (Td+460) / (Vd * (Pb+H/13.6) * (Tw+460))							
HQ = 8.0317 * H * ((Tw+460)*Q/Vw)^2 / (Pb * (Td+460))							

Calibration Performed by:

(Print) Clifford E. Mohs

(Signature) Clifford E. Mohs

CALIBRATION S-TYPE PITOT TUBE

Date: 1/20/88 S-Type Pitot Tube ID No.: 5
 Ambient Temperature, °F: 78 Standard Pitot Tube ID No.: STD-5
 Barometric Pressure, in. Hg.: 29.6 Standard Pitot Tube Coefficient: .995

PITOT TUBE EXAMINATION		
Alignment Check	Pitot Tube Dimensions	Pitot Assembly Intercomponent Spacings
$\checkmark$ $\alpha_1 < 10^\circ$ $\checkmark$ $\alpha_2 < 10^\circ$ $\checkmark$ $\beta_1 < 5^\circ$ $\checkmark$ $\beta_2 < 5^\circ$ $\checkmark$ $Q < 1/8$ in. $\checkmark$ $R < 1/32$ in.	External tubing diameter (D_t): <u>$3/8$"</u> Base to Side A opening plane (P_A): <u>6"</u> Base to Side B opening plane (P_B): <u>6"</u>	Pitot to <u>$1/2$"</u> nozzle (X): <u>$.5$"</u> Pitot to probe sheath (Y): <u>3.2"</u> Pitot to thermocouple, along probe (W): <u>2.3"</u> Pitot to thermocouple, perpen- dicular to probe (Z): <u>$.28$"</u>

DESIRED CALIBRATION POINT		SIDE A CALIBRATION		SIDE B CALIBRATION	
Velocity ft/sec	P_{std} in. WC	P_{std} in. WC	P_s in. WC	P_{std} in. WC	P_s in. WC
20	0.09	.09	.121	.09	.12
40	0.37	.37	.52	.37	.51
60	0.82	.82	1.16	.82	1.16
80	1.45	1.45	1.90	1.45	2.00
100	2.30				

COMPUTER PRINTOUT							
SIDE A CALIBRATION				SIDE B CALIBRATION			
P_{std}	P_s	C_p	$C_p - C_p(A)$	P_{std}	P_s	C_p	$C_p - C_p(B)$
0.090	0.121	0.858	0.007	0.090	0.120	0.862	0.013
0.370	0.520	0.839	-0.011	0.370	0.510	0.847	-0.001
0.820	1.160	0.837	-0.014	0.820	1.160	0.837	-0.012
1.450	1.900	0.869	0.018	1.450	2.000	0.847	-0.001
$C_p(A) = 0.851$				$C_p(B) = 0.848$			

Calibration Performed by:

(Print) Clifford Mohs

(Signature) Clifford P Mohs

APPENDIX E

PROCESS DATA



CHICAGO TUBE & IRON

2940 EAGANDALE BLVD. ST. PAUL, MN 55121
612/454-6800

wt of fuel barrel →

4.4 lb 11:45 AM 46 lb ← *wt of wheel barrel*

1	73	Jan 21-88	78
2	74		78
3	74		79
4	76		80
5	78		80
6	81		82
7	82		90 1053
8	89		90
9	97		97
10	78		84
11	96		88
12	98		90
13	94	3:45	13 88
14	73	5:47	1104 - 598 = 506

1163

everything in tubing • pipe • valves • fittings
IN MINNESOTA—800/382-2015 • OUTSIDE MINNESOTA—800/328-0151

$$\frac{547 + 506}{4 \text{ hrs}} = 263 \text{ lbs/hr}$$



RECEIVED JAN 22 1988

KOCH REFINING COMPANY

January 21, 1988

Mr. Dean DeBelley
Southern Minnesota Beet Sugar Coop.
Post Office Box 500
Renville, Minnesota 56248

Dear Dean:

Confirming our telephone conversation, listed below is current analysis of Koch Refining Company's Industrial Fuel Oil (Clarified Oil).

API Gravity	-4.0
Viscosity, ssu 100°F	1400
Flash Point	150°
Pour Point	55°
Sulfur, wt. %	1.55
BTU Content	155,500 per gallon

If I can be of any further assistance please give me a call.

Sincerely,

KOCH REFINING COMPANY

Don Howe
Sales Representative

**SOUTHERN MINNESOTA SUGAR CO-OP
DRYER REPORT**

JAN 26 1966

DAY ENDING 1-22-68 8 A.M.

9.1 hour
1000 pounds
85%
145% Brix

OPERATOR Wesley
SHIFT 1 Wesley
SHIFT 2 Wesley
SHIFT 3 Wesley

FEED RATE %		9	10	11	12	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8
NORTH	45	45	45	45	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	45
	45	45	45	45	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	45
FURNACE TEMP.																									
NORTH	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050	1050
	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200
EXIT TEMP.																									
NORTH	320	320	320	320	315	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310
	325	325	325	325	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310	310
MOISTURES																									
NORTH	76.2	76.4	75.8	76.0	73.6	75.6	73.4	72.6	72.8	72.8	71.5	72.8	71.8	71.8	71.8	71.8	71.8	71.8	71.8	71.8	71.8	71.8	71.8	71.8	71.8
	4.8	9.4	4.2	9.6	8.4	10.2	9.2	10.0	11.5	8.0	9.2	9.6	8.8	8.6	8.4	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2
FUEL OIL USED																									
NORTH METER	8 A.M.																								
	8 A.M. 04-305.2																								
STORAGE BIN																									
PYROMETER	NORTH	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200
	SOUTH	1400	1350	1000	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350	1350
FIRE VISIBLE																									
EXIT END	NORTH	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y
	SOUTH	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y
CHEMICALS TO WATER TANK																									

REASON FOR PULP TO FLOOR: FD Dinger 500lb Recycle 35lb combustion air 90%

* COMMENTS:

* NOTE TIMES FOR INSTALLATION OF NEW DIES AND ROLLERS.



(4) JAN 26 1988

DIFFUSER REPORT

DAY ENDING 8 A.M. 1-21-88

SIGNATURES

OPER.

BEET END 4MAN

SHIFT 1 David L. [Signature]SHIFT 2 David [Signature]SHIFT 3 Julia Stewart

	A.M.								P.M.								A.M.							
	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8
BEETS SLICED TONS	2.2	2.0	2.0	2.0	2.2	2.0	2.0	2.2	0	2.0	2.0	2.0	2.0	2.0	2.0	2.2	2.0	3.0	3.0	2.0	2.0	2.2	2.2	2.2
COSSETTE SCALE	8 A.M. 21945								4 P.M. 24316								12 Mid. 26431							
SLICERS IN SERVICE	4	4	3	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4
CONDITION OF COSSETTES	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd	gd
TEMPS:																								
SCALDING TEMP. ENT. DIFF. °F	96	83	79	84	81	83	89	↑	76	84	85	82	82	83	84	84	84	82	83	80	76	76	75	
RAW JUICE LVG. DIFF.	51	61	56	56	61	68	10	65	65	62	64	60	61	62	63	63	66	64	65	64	62	61	57	
DIFFUSER SUPPLY	61	67	67	68	67	68	68	67	69	67	67	67	66	67	67	68	68	68	68	68	69	69	69	
RAW JUICE TO CARBS.	80	78	-	79	82	86	85		84	84	83	82	82	82	83	84	85	85	85	85	85	83	-	
Cossette	55	55	50	50	56	64	57		58	57	59	53	55	56	58	58	60	58	58	58	59	57	48	
WATER FLOW TO DIFF. (TON/HRI)	1.5	1.5	1.5	1.5	2.75	2.15	3.75		2.75	2.75	2.75	2.75	2.75	2.75	2.75	2.75	2.75	2.75	2.75	2.75	2.75	2.75	2.75	
DIFF. SCREENS CLEANED																				X	X			
RAW JUICE FLOW %	66	66	66	70	70	70	70	V	66	66	70	70	70	70	70	66	70	70	66	66	66	66	66	
DELAY TO SLICE (BELOW 250 TON/HRI)																								

FORMALDEHYDE GALS.

SHIFT 1

12:45pm - 7:00am

SHIFT 2

SHIFT 3

8:00am - 5:00am

FOAM OIL GALS.

SHIFT 1

7:00 - 7:05

SHIFT 2

7:05 - 7:06

SHIFT 3

7:06 - 7:05

DIFFUSER TEMP.

CELL 2	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71
CELL 9	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71
CELL 13	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71
CELL 17	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71
CELL 22	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71
CELL 25	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71

REASON FOR DELAY:

SHUTTING @ 3:30 P.M. LIME KILN @ 5:00 P.M.

COMMENTS: Flushed Flume @ 10:20 A.M. Flushed Flume @ 5:15 P.M.

ICFROZE "B" SLICER - SLICING AGAIN 11:50 -

B-SLICER MOTOR SHUT OFF 3 TIMES - SUMMER TIME