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Title: Results of the January 28-31, 1992,
Particulate Emission Tests, South Pulp
Dryer- American Crystal Sugar
Company, Moorehead, Minnesota

Bay West, Inc.

Bay West, Inc.

March 1992

**RESULTS OF THE
JANUARY 28 - 31, 1992
PARTICULATE EMISSION TESTS
SOUTH PULP DRYER**

**AMERICAN CRYSTAL SUGAR COMPANY
MOORHEAD, MINNESOTA**

Submitted to:

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March 26, 1992

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1.0 INTRODUCTION

From January 21-24, 1992, Bay West, Inc. conducted engineering emission testing for particulate matter at the inlet and outlet of the South Pulp Dryer at American Crystal Sugar Company's facility in Moorhead, Minnesota.

The South Pulp Dryer is a rotary drum dryer for drying beet pulp. The dryer has a coal-fired furnace, rotary drum dryer, multiclone control system, and stack filter system. The rotary drum is heated by a coal-fired furnace. Emissions from the dryer are controlled by multiclone and stack filter systems. A portion of the exhaust gas from the multiclone can be returned to the rotary drums. Testing was conducted under various exhaust gas recycle rates.

On-site testing was performed by Dwayne Smith, Scott Bainville Dan Smith and Dennis Littfin of Bay West. Facility personnel present during testing included David Walden of American Crystal Sugar Company.

Evaluations were performed in accordance with EPA Methods 1 - 5, CFR Title 40, Part 60, Appendix A (revised July 1, 1991). Prior to and after each test series, air flowrate determinations were conducted for the source stack, recycle duct, and hopper aspirator duct locations. These flowrate determinations are included in Appendix 1.

The circular stack outlet had four sampling ports, the rectangular multiclone inlet had four sampling ports, and the dryer aspirator duct had one test port.

An ANDERSEN INSTRUMENTS sampling train was used to extract particulate samples by means of a glass-lined pitot assembly. This test determined the "front-half" and "back-half" portions of the total particulate catch. The "front-half" includes the residue from probe washings and particulate from the dry filter. The "back-half" catch includes the residue extracted from the impingers of the Method 5 train.

2.0 SUMMARY

The results of the January 21 - 24, 1992 inlet/outlet emission tests of the South Pulp Dryer are included in section 3.0 of this report. No difficulties occurred in the field or in the laboratory evaluation of the samples. Based on this fact and a review of all data, it is our opinion that the results reflect the actual emissions from this process at the time the testing was performed. Table 1 below lists the emission concentration determinations and collection efficiency for each test.

Table 1
Summary of Results

Test No.	Run No.	Inlet Concentration (gr/dscf)	Outlet Concentration (gr/dscf)	Collection Efficiency (%)
1	1	0.3533	0.0724	79.5
1	2	0.4167	0.0718	82.8
1	3	0.3414	0.0757	77.8
2	1	0.4139	0.1001	75.8
2	2	0.4206	0.0953	77.3
2	3	0.4494	0.1277	71.6
3	1	0.4774	0.0979	79.5
3	2	0.4937	0.1119	77.3
3	3	0.5692	0.1091	80.8
4	1	0.4687	0.1295	72.4
4	2	0.5411	0.1134	79.0
4	3	0.4783	0.1014	78.8

3.0 RESULTS

Tables 2 through 17 show the results of Method 5 testing for the inlet and outlet of the South Pulp Dryer. Field data, analytical data, testing procedures, calculations, calibration data, and process rates are included in Appendices 2 through 7, respectively.

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

BayWest

TEST NO. 1
SOURCE/SITE: SOUTH DRYER STACK

RESULTS OF PARTICULATE LOADING DETERMINATIONS - METHOD 5

	RUN 1	RUN 2	RUN 3
DATE OF RUN	21-Jan-92	21-Jan-92	21-Jan-92
RUN START TIME	1315	1600	1815
RUN END TIME	1519	1745	2013
STACK STATIC PRESSURE (in. H2O)	-0.84	-0.84	-0.84
CROSS SECTIONAL AREA (sq. ft.)	19.308	19.308	19.308
PITOT TUBE COEFFICIENT	0.840	0.840	0.840
SAMPLE GAS MOISTURE ANALYSES			
CONDENSER (ml.)	0.00	0.00	0.00
IMPINGER (ml.)	696.00	676.00	740.00
DESSICCANT (grams)	300.00	302.00	174.00
TOTAL (grams)	996.00	978.00	914.00
SAMPLE GAS MOISTURE CONTENT (%)	32.39	33.09	32.16
TOTAL PARTICULATE COLLECTED (g)	0.4594	0.4335	0.4454
DRY GAS METER COEFFICIENT	1.001	1.001	1.001
BAROMETRIC PRESSURE (in. Hg)	28.85	28.85	28.85
AVG. ORIFICE PRESSURE DROP (in. H2O)	3.65	3.32	3.16
AVG. GAS METER TEMP. (degrees F)	113.3	118.7	117.6
VOLUME THROUGH GAS METER			
AT METER CONDITIONS (cf)	109.20	104.93	102.16
STANDARD CONDITIONS (dscf)	97.93	93.16	90.82
TOTAL SAMPLING TIME (min.)	96	96	96
NOZZLE DIAMETER (in.)	0.312	0.312	0.312
AVG. STACK GAS TEMP. (degrees F)	233.3	232.8	228.8
AVG. STACK GAS VELOCITY (ft/sec)	58.99	59.33	58.89
VOLUMETRIC FLOWRATE			
ACTUAL (acfm)	68336	68733	68225
DRY STANDARD (dscfm)	33856	33725	34139
ISOKINETIC VARIATION (%)	109.64	104.70	100.84
PARTICULATE CONCENTRATION			
ACTUAL (gr/acf)	0.0359	0.0352	0.0379
DRY STANDARD (gr/dscf)	0.0724	0.0718	0.0757
PARTICLE MASS RATE (lb/hr)	20.985	20.736	22.121

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO. 2
SOURCE/SITE: SOUTH DRYER STACK

RESULTS OF PARTICULATE LOADING DETERMINATIONS - METHOD 5

	RUN 1	RUN 2	RUN 3
DATE OF RUN	22-Jan-92	22-Jan-92	22-Jan-92
RUN START TIME	1020	1250	1515
RUN END TIME	1212	1430	1652
STACK STATIC PRESSURE (in. H2O)	-0.43	-0.43	-0.43
CROSS SECTIONAL AREA (sq. ft.)	19.308	19.308	19.308
PITOT TUBE COEFFICIENT	0.840	0.840	0.840
SAMPLE GAS MOISTURE ANALYSES			
CONDENSER (ml.)	0.00	0.00	0.00
IMPINGER (ml.)	984.00	1074.00	1018.00
DESSICCANT (grams)	341.00	86.00	189.00
TOTAL (grams)	1325.00	1160.00	1207.00
SAMPLE GAS MOISTURE CONTENT (%)	42.65	42.44	44.09
TOTAL PARTICULATE COLLECTED (g)	0.5441	0.4578	0.5965
DRY GAS METER COEFFICIENT	1.001	1.001	1.001
BAROMETRIC PRESSURE (in. Hg)	28.70	28.70	28.70
AVG. ORIFICE PRESSURE DROP (in. H2O)	2.75	2.14	2.04
AVG. GAS METER TEMP. (degrees F)	122.4	123.5	128.6
VOLUME THROUGH GAS METER			
AT METER CONDITIONS (cf)	95.77	84.86	83.29
STANDARD CONDITIONS (dscf)	83.91	74.11	72.09
TOTAL SAMPLING TIME (min.)	96	96	96
NOZZLE DIAMETER (in.)	0.312	0.312	0.312
AVG. STACK GAS TEMP. (degrees F)	227.8	218.4	219.8
AVG. STACK GAS VELOCITY (ft/sec)	54.50	54.01	54.35
VOLUMETRIC FLOWRATE			
ACTUAL (acfm)	63134	62566	62962
DRY STANDARD (dscfm)	26632	26857	26199
ISOKINETIC VARIATION (%)	109.19	104.60	104.29
PARTICULATE CONCENTRATION			
ACTUAL (gr/acf)	0.0422	0.0409	0.0531
DRY STANDARD (gr/dscf)	0.1001	0.0953	0.1277
PARTICLE MASS RATE (lb/hr)	22.816	21.920	28.644

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO. 3
SOURCE/SITE: SOUTH DRYER STACK

RESULTS OF PARTICULATE LOADING DETERMINATIONS - METHOD 5

	RUN 1	RUN 2	RUN 3
DATE OF RUN	23-Jan-92	23-Jan-92	23-Jan-92
RUN START TIME	1005	1220	1445
RUN END TIME	1145	1355	1630
STACK STATIC PRESSURE (in. H2O)	-0.45	-0.45	-0.45
CROSS SECTIONAL AREA (sq. ft.)	19.308	19.308	19.308
PITOT TUBE COEFFICIENT	0.840	0.840	0.840
SAMPLE GAS MOISTURE ANALYSES			
CONDENSER (ml.)	0.00	0.00	0.00
IMPINGER (ml.)	1135.00	1135.00	1036.00
DESSICCANT (grams)	89.00	89.00	23.00
TOTAL (grams)	1224.00	1224.00	1059.00
SAMPLE GAS MOISTURE CONTENT (%)	46.02	46.74	43.70
TOTAL PARTICULATE COLLECTED (g)	0.4289	0.4762	0.4544
DRY GAS METER COEFFICIENT	1.001	1.001	1.001
BAROMETRIC PRESSURE (in. Hg)	28.68	28.68	28.68
AVG. ORIFICE PRESSURE DROP (in. H2O)	1.74	1.64	1.58
AVG. GAS METER TEMP. (degrees F)	107.5	107.8	109.7
VOLUME THROUGH GAS METER			
AT METER CONDITIONS (cf)	75.44	73.35	72.00
STANDARD CONDITIONS (dscf)	67.63	65.70	64.26
TOTAL SAMPLING TIME (min.)	96	96	96
NOZZLE DIAMETER (in.)	0.312	0.312	0.312
AVG. STACK GAS TEMP. (degrees F)	217.1	213.1	203.3
AVG. STACK GAS VELOCITY (ft/sec)	49.30	49.33	48.71
VOLUMETRIC FLOWRATE			
ACTUAL (acfm)	57117	57148	56430
DRY STANDARD (dscfm)	23021	22860	24213
ISOKINETIC VARIATION (%)	109.02	108.94	100.60
PARTICULATE CONCENTRATION			
ACTUAL (gr/acf)	0.0395	0.0448	0.0468
DRY STANDARD (gr/dscf)	0.0979	0.1119	0.1091
PARTICLE MASS RATE (lb/hr)	19.291	21.893	22.621

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO.

4

SOURCE/SITE:

SOUTH DRYER STACK

RESULTS OF PARTICULATE LOADING DETERMINATIONS - METHOD 5

	RUN 1	RUN 2	RUN 3
DATE OF RUN	24-Jan-92	24-Jan-92	24-Jan-92
RUN START TIME	1015	1245	1505
RUN END TIME	1210	1420	1655
STACK STATIC PRESSURE (in. H2O)	-0.55	-0.55	-0.55
CROSS SECTIONAL AREA (sq. ft.)	19.308	19.308	19.308
PITOT TUBE COEFFICIENT	0.840	0.840	0.840
SAMPLE GAS MOISTURE ANALYSES			
CONDENSER (ml.)	0.00	0.00	0.00
IMPINGER (ml.)	1109.00	1190.00	1242.00
DESSICCANT (grams)	122.00	24.00	15.00
TOTAL (grams)	1231.00	1214.00	1257.00
SAMPLE GAS MOISTURE CONTENT (%)	43.35	44.73	45.34
TOTAL PARTICULATE COLLECTED (g)	0.6358	0.5193	0.4688
DRY GAS METER COEFFICIENT	1.001	1.001	1.001
BAROMETRIC PRESSURE (in. Hg)	28.83	28.83	28.83
AVG. ORIFICE PRESSURE DROP (in. H2O)	2.17	1.90	1.98
AVG. GAS METER TEMP. (degrees F)	107.8	115.3	126.5
VOLUME THROUGH GAS METER			
AT METER CONDITIONS (cf)	84.02	79.47	81.83
STANDARD CONDITIONS (dscf)	75.75	70.66	71.38
TOTAL SAMPLING TIME (min.)	96	96	96
NOZZLE DIAMETER (in.)	0.312	0.312	0.312
AVG. STACK GAS TEMP. (degrees F)	209.5	201.5	190.8
AVG. STACK GAS VELOCITY (ft/sec)	50.80	50.17	50.24
VOLUMETRIC FLOWRATE			
ACTUAL (acfm)	58851	58123	58206
DRY STANDARD (dscfm)	25297	24675	24840
ISOKINETIC VARIATION (%)	108.32	108.55	108.92
PARTICULATE CONCENTRATION			
ACTUAL (gr/acf)	0.0557	0.0482	0.0433
DRY STANDARD (gr/dscf)	0.1295	0.1134	0.1014
PARTICLE MASS RATE (lb/hr)	28.053	23.961	21.555

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO.

1

SOURCE/SITE:

SOUTH DRYER MULTI-CLONE INLET

RESULTS OF PARTICULATE LOADING DETERMINATIONS - METHOD 5

	RUN 1	RUN 2	RUN 3
DATE OF RUN	21-Jan-92	21-Jan-92	21-Jan-92
RUN START TIME	1315	1600	1825
RUN END TIME	1500	1742	2002
STACK STATIC PRESSURE (in. H2O)	2.80	2.80	2.80
CROSS SECTIONAL AREA (sq. ft.)	53.472	53.472	53.472
PITOT TUBE COEFFICIENT	0.840	0.840	0.840
SAMPLE GAS MOISTURE ANALYSES			
CONDENSER (ml.)	374.00	342.00	0.00
IMPINGER (ml.)	0.00	0.00	0.00
DESSICCANT (grams)	34.00	46.00	34.00
TOTAL (grams)	408.00	388.00	34.00
SAMPLE GAS MOISTURE CONTENT (%)	31.09	31.76	31.18
TOTAL PARTICULATE COLLECTED (g)	0.9751	1.0606	0.8696
DRY GAS METER COEFFICIENT	1.000	1.000	1.000
BAROMETRIC PRESSURE (in. Hg)	28.85	28.85	28.85
AVG. ORIFICE PRESSURE DROP (in. H2O)	0.84	0.73	0.72
AVG. GAS METER TEMP. (degrees F)	127.0	124.5	126.6
VOLUME THROUGH GAS METER			
AT METER CONDITIONS (cf)	49.03	45.02	45.22
STANDARD CONDITIONS (dscf)	42.60	39.27	39.30
TOTAL SAMPLING TIME (min.)	96	96	96
NOZZLE DIAMETER (in.)	0.313	0.313	0.313
AVG. STACK GAS TEMP. (degrees F)	248.8	247.2	244.4
AVG. STACK GAS VELOCITY (ft/sec)	25.39	25.10	25.26
VOLUMETRIC FLOWRATE			
ACTUAL (acfm)	81456	80531	81030
DRY STANDARD (dscfm)	40605	39847	40596
ISOKINETIC VARIATION (%)	109.42	102.80	100.98
PARTICULATE CONCENTRATION			
ACTUAL (gr/acf)	0.1761	0.2062	0.2388
DRY STANDARD (gr/dscf)	0.3533	0.4167	0.3414
PARTICLE MASS RATE (lb/hr)	122.817	142.180	118.679

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO.

2

SOURCE/SITE:

SOUTH DRYER MULTI-CLONE INLET

RESULTS OF PARTICULATE LOADING DETERMINATIONS - METHOD 5

	RUN 1	RUN 2	RUN 3
DATE OF RUN	22-Jan-92	22-Jan-92	22-Jan-92
RUN START TIME	1020	1250	1515
RUN END TIME	1200	1430	1655
STACK STATIC PRESSURE (in. H2O)	2.80	2.80	2.80
CROSS SECTIONAL AREA (sq. ft.)	53.472	53.472	53.472
PITOT TUBE COEFFICIENT	0.840	0.840	0.840
SAMPLE GAS MOISTURE ANALYSES			
CONDENSER (ml.)	381.00	398.00	407.00
IMPINGER (ml.)	0.00	0.00	0.00
DESSICCANT (grams)	206.00	179.00	120.00
TOTAL (grams)	587.00	577.00	527.00
SAMPLE GAS MOISTURE CONTENT (%)	39.35	42.06	40.72
TOTAL PARTICULATE COLLECTED (g)	1.1431	1.0204	1.0523
DRY GAS METER COEFFICIENT	1.000	1.000	1.000
BAROMETRIC PRESSURE (in. Hg)	28.70	28.70	28.70
AVG. ORIFICE PRESSURE DROP (in. H2O)	0.85	0.66	0.62
AVG. GAS METER TEMP. (degrees F)	124.8	125.0	128.2
VOLUME THROUGH GAS METER			
AT METER CONDITIONS (cf)	49.12	43.19	41.92
STANDARD CONDITIONS (dscf)	42.62	37.44	36.14
TOTAL SAMPLING TIME (min.)	96	96	96
NOZZLE DIAMETER (in.)	0.313	0.313	0.313
AVG. STACK GAS TEMP. (degrees F)	243.0	242.8	242.8
AVG. STACK GAS VELOCITY (ft/sec)	27.56	27.31	27.09
VOLUMETRIC FLOWRATE			
ACTUAL (acfm)	88431	87614	86927
DRY STANDARD (dscfm)	38918	36846	37402
ISOKINETIC VARIATION (%)	105.87	105.98	100.77
PARTICULATE CONCENTRATION			
ACTUAL (gr/acf)	0.1822	0.1769	0.1934
DRY STANDARD (gr/dscf)	0.4139	0.4206	0.4494
PARTICLE MASS RATE (lb/hr)	137.931	132.691	143.911

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO.

3

SOURCE/SITE:

SOUTH DRYER MULTI-CLONE INLET

RESULTS OF PARTICULATE LOADING DETERMINATIONS - METHOD 5

	RUN 1	RUN 2	RUN 3
DATE OF RUN	23-Jan-92	23-Jan-92	23-Jan-92
RUN START TIME	945	1220	1450
RUN END TIME	1130	1400	1640
STACK STATIC PRESSURE (in. H2O)	2.60	2.60	2.60
CROSS SECTIONAL AREA (sq. ft.)	53.472	53.472	53.472
PITOT TUBE COEFFICIENT	0.840	0.840	0.840
SAMPLE GAS MOISTURE ANALYSES			
CONDENSER (ml.)	416.00	423.00	424.00
IMPINGER (ml.)	0.00	0.00	0.00
DESSICCANT (grams)	125.00	140.00	98.00
TOTAL (grams)	541.00	563.00	522.00
SAMPLE GAS MOISTURE CONTENT (%)	42.88	44.87	43.13
TOTAL PARTICULATE COLLECTED (g)	1.0501	1.0421	1.1957
DRY GAS METER COEFFICIENT	1.000	1.000	1.000
BAROMETRIC PRESSURE (in. Hg)	28.68	28.68	28.68
AVG. ORIFICE PRESSURE DROP (in. H2O)	0.53	0.50	0.49
AVG. GAS METER TEMP. (degrees F)	105.6	106.8	108.7
VOLUME THROUGH GAS METER			
AT METER CONDITIONS (cf)	37.90	36.45	36.40
STANDARD CONDITIONS (dscf)	33.94	32.58	32.42
TOTAL SAMPLING TIME (min.)	96	96	96
NOZZLE DIAMETER (in.)	0.313	0.313	0.313
AVG. STACK GAS TEMP. (degrees F)	243.6	243.3	244.0
AVG. STACK GAS VELOCITY (ft/sec)	25.16	25.05	25.26
VOLUMETRIC FLOWRATE			
ACTUAL (acfm)	80713	80381	81039
DRY STANDARD (dscfm)	33386	32101	33356
ISOKINETIC VARIATION (%)	106.05	105.85	101.38
PARTICULATE CONCENTRATION			
ACTUAL (gr/acf)	0.1975	0.1972	0.2343
DRY STANDARD (gr/dscf)	0.4774	0.4937	0.5692
PARTICLE MASS RATE (lb/hr)	136.465	135.681	162.548

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO.

4

SOURCE/SITE:

SOUTH DRYER MULTI-CLONE INLET

RESULTS OF PARTICULATE LOADING DETERMINATIONS - METHOD 5

	RUN 1	RUN 2	RUN 3
DATE OF RUN	24-Jan-92	24-Jan-92	24-Jan-92
RUN START TIME	1015	1245	1505
RUN END TIME	1200	1426	1645
STACK STATIC PRESSURE (in. H2O)	2.75	2.75	2.75
CROSS SECTIONAL AREA (sq. ft.)	53.472	53.472	53.472
PITOT TUBE COEFFICIENT	0.840	0.840	0.840
SAMPLE GAS MOISTURE ANALYSES			
CONDENSER (ml.)	413.00	571.00	563.00
IMPINGER (ml.)	0.00	0.00	0.00
DESSICCANT (grams)	223.00	22.00	30.00
TOTAL (grams)	636.00	593.00	593.00
SAMPLE GAS MOISTURE CONTENT (%)	42.35	43.45	43.48
TOTAL PARTICULATE COLLECTED (g)	1.2384	1.2746	1.1254
DRY GAS METER COEFFICIENT	1.000	1.000	1.000
BAROMETRIC PRESSURE (in. Hg)	28.83	28.83	28.83
AVG. ORIFICE PRESSURE DROP (in. H2O)	0.74	0.59	0.60
AVG. GAS METER TEMP. (degrees F)	116.9	118.7	124.1
VOLUME THROUGH GAS METER			
AT METER CONDITIONS (cf)	46.17	41.30	41.64
STANDARD CONDITIONS (dscf)	40.78	36.35	36.31
TOTAL SAMPLING TIME (min.)	96	96	96
NOZZLE DIAMETER (in.)	0.313	0.313	0.313
AVG. STACK GAS TEMP. (degrees F)	246.6	244.2	247.5
AVG. STACK GAS VELOCITY (ft/sec)	28.26	27.69	28.26
VOLUMETRIC FLOWRATE			
ACTUAL (acfm)	90671	88849	90663
DRY STANDARD (dscfm)	37901	36556	37106
ISOKINETIC VARIATION (%)	104.99	103.72	102.06
PARTICULATE CONCENTRATION			
ACTUAL (gr/acf)	0.1959	0.2227	0.1958
DRY STANDARD (gr/dscf)	0.4687	0.5411	0.4783
PARTICLE MASS RATE (lb/hr)	152.087	169.361	151.958

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO. 1
SOURCE/SITE: SOUTH DRYER STACK

RESULTS OF ORSAT & MOISTURE ANALYSES - METHODS 3 & 4 (%V/V)

	RUN 1	RUN 2	RUN 3
DATE OF TEST	21-Jan-92	21-Jan-92	21-Jan-92

DRY BASIS (ORSAT), %			
CARBON DIOXIDE	4.12	4.08	4.11
OXYGEN	16.00	15.50	15.25
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	79.88	80.42	80.64

WET BASIS (ORSAT), %			
CARBON DIOXIDE	2.79	2.73	2.79
OXYGEN	10.82	10.37	10.35
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	54.01	53.81	54.71
WATER VAPOR	32.39	33.09	32.16
DRY MOLECULAR WEIGHT	29.30	29.27	29.27
WET MOLECULAR WEIGHT	25.64	25.54	25.64

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO.

2

SOURCE/SITE:

SOUTH DRYER STACK

RESULTS OF ORSAT & MOISTURE ANALYSES - METHODS 3 & 4 (%V/V)

	RUN 1	RUN 2	RUN 3
DATE OF TEST	22-Jan-92	22-Jan-92	22-Jan-92
DRY BASIS (ORSAT), %			
CARBON DIOXIDE	5.50	6.00	5.20
OXYGEN	14.75	14.25	15.10
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	79.75	79.75	79.70
WET BASIS (ORSAT), %			
CARBON DIOXIDE	3.15	3.45	2.91
OXYGEN	8.46	8.20	8.44
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	45.73	45.91	44.55
WATER VAPOR	42.65	42.44	44.10
DRY MOLECULAR WEIGHT	29.47	29.53	29.44
WET MOLECULAR WEIGHT	24.58	24.64	24.39

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO. 3
SOURCE/SITE: SOUTH DRYER STACK

RESULTS OF ORSAT & MOISTURE ANALYSES - METHODS 3 & 4 (%V/V)

	RUN 1	RUN 2	RUN 3
DATE OF TEST	23-Jan-92	23-Jan-92	23-Jan-92

DRY BASIS (ORSAT), %			

CARBON DIOXIDE	5.02	5.79	4.85
OXYGEN	15.10	14.58	15.50
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	79.88	79.63	79.65
WET BASIS (ORSAT), %			

CARBON DIOXIDE	2.71	3.08	2.73
OXYGEN	8.15	7.76	8.72
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	43.12	42.41	44.83
WATER VAPOR	46.02	46.75	43.71
DRY MOLECULAR WEIGHT	29.41	29.51	29.40
WET MOLECULAR WEIGHT	24.16	24.13	24.41

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO.

4

SOURCE/SITE:

SOUTH DRYER STACK

RESULTS OF ORSAT & MOISTURE ANALYSES - METHODS 3 & 4 (%V/V)

	RUN 1	RUN 2	RUN 3
DATE OF TEST	24-Jan-92	24-Jan-92	24-Jan-92

DRY BASIS (ORSAT), %			
CARBON DIOXIDE	6.12	6.58	6.58
OXYGEN	14.00	13.65	13.88
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	79.88	79.77	79.54

WET BASIS (ORSAT), %			
CARBON DIOXIDE	3.47	3.64	3.60
OXYGEN	7.93	7.55	7.59
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	45.24	44.10	43.48
WATER VAPOR	43.37	44.71	45.34
DRY MOLECULAR WEIGHT	29.54	29.60	29.61
WET MOLECULAR WEIGHT	24.54	24.41	24.35

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO.

1

SOURCE/SITE:

SOUTH DRYER MULTI-CLONE INLET

RESULTS OF ORSAT & MOISTURE ANALYSES - METHODS 3 & 4 (%V/V)

	RUN 1	RUN 2	RUN 3
DATE OF TEST	21-Jan-92	21-Jan-92	21-Jan-92
DRY BASIS (ORSAT), %			
CARBON DIOXIDE	4.12	4.08	4.11
OXYGEN	16.00	15.50	15.25
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	79.88	80.42	80.64
WET BASIS (ORSAT), %			
CARBON DIOXIDE	2.84	2.79	2.83
OXYGEN	11.03	10.58	10.50
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	55.05	54.90	55.50
WATER VAPOR	31.09	31.74	31.18
DRY MOLECULAR WEIGHT	29.30	29.27	29.27
WET MOLECULAR WEIGHT	25.79	25.69	25.75

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO.

2

SOURCE/SITE:

SOUTH DRYER MULTI-CLONE INLET

RESULTS OF ORSAT & MOISTURE ANALYSES - METHODS 3 & 4 (%V/V)

	RUN 1	RUN 2	RUN 3
DATE OF TEST	22-Jan-92	22-Jan-92	22-Jan-92
DRY BASIS (ORSAT), %			
CARBON DIOXIDE	5.50	6.00	5.20
OXYGEN	14.75	14.25	15.10
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	79.75	79.75	79.70
WET BASIS (ORSAT), %			
CARBON DIOXIDE	3.34	3.48	3.08
OXYGEN	8.94	8.26	8.95
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	48.36	46.21	47.25
WATER VAPOR	39.36	42.06	40.72
DRY MOLECULAR WEIGHT	29.47	29.53	29.44
WET MOLECULAR WEIGHT	24.96	24.68	24.78

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO.

3

SOURCE/SITE:

SOUTH DRYER MULTI-CLONE INLET

RESULTS OF ORSAT & MOISTURE ANALYSES - METHODS 3 & 4 (%V/V)

	RUN 1	RUN 2	RUN 3
DATE OF TEST	23-Jan-92	23-Jan-92	23-Jan-92
DRY BASIS (ORSAT), %			
CARBON DIOXIDE	5.02	5.79	4.85
OXYGEN	15.10	14.58	15.50
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	79.88	79.63	79.65
WET BASIS (ORSAT), %			
CARBON DIOXIDE	2.87	3.19	2.76
OXYGEN	8.62	8.04	8.82
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	45.62	43.90	45.30
WATER VAPOR	42.89	44.88	43.13
DRY MOLECULAR WEIGHT	29.41	29.51	29.40
WET MOLECULAR WEIGHT	24.51	24.34	24.48

AMERICAN CRYSTAL SUGAR
MOORHEAD, MINNESOTA

TEST NO.

4

SOURCE/SITE:

SOUTH DRYER MULTI-CLONE INLET

RESULTS OF ORSAT & MOISTURE ANALYSES - METHODS 3 & 4 (%V/V)

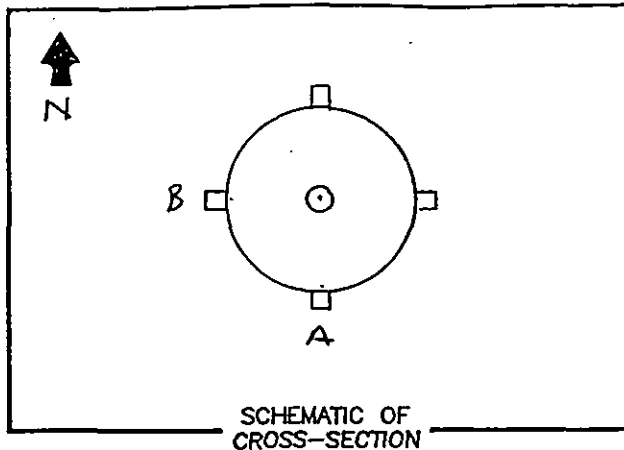
	RUN 1	RUN 2	RUN 3
DATE OF TEST	24-Jan-92	24-Jan-92	24-Jan-92
DRY BASIS (ORSAT), %			
CARBON DIOXIDE	6.12	6.58	6.12
OXYGEN	14.00	13.65	13.88
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	79.88	79.77	80.00
WET BASIS (ORSAT), %			
CARBON DIOXIDE	3.53	3.72	3.46
OXYGEN	8.07	7.72	7.85
CARBON MONOXIDE	0.00	0.00	0.00
NITROGEN	46.05	45.10	45.22
WATER VAPOR	42.35	43.46	43.47
DRY MOLECULAR WEIGHT	29.54	29.60	29.53
WET MOLECULAR WEIGHT	24.65	24.56	24.52

Appendix 1

Preliminary Flowrate Determination

EPA METHOD 2 FIELD DATA

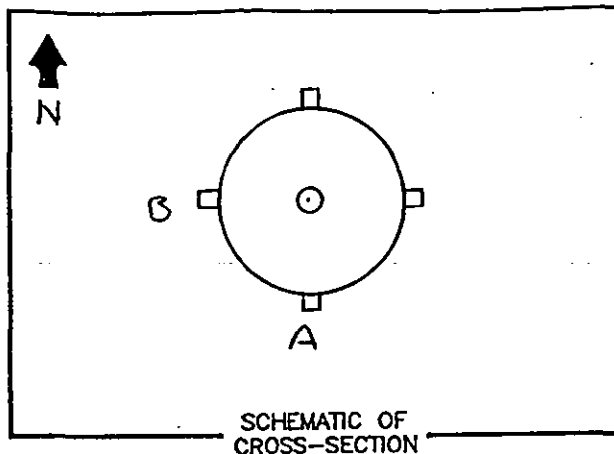
PROJECT NAME ACS / MOOREHEAD
PROJECT NUMBER 920014
SOURCE SOUTH PULP DRYER STACK
TEST 1 RUN 0 DATE 1-21-92
STACK DIA. 59.5 IN.
DRY BULB 24.2 °F WET BULB 15.8 °F
MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
BAROMETRIC PRESSURE 28.85 IN Hg
STATIC PRESSURE -.84 IN WC
OPERATORS S. BAINJULUE & D. LITFIN
PITOT NO. P1-6 Cp .840



TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH: 7.0	IN.	TIME START: 1115	HRS.
A 1	.044	2.62	9.62	.60	244
2	.146	8.69	15.69	.83	244
3	.296	17.61	24.61	.85	244
4	.704	41.89	48.89	.80	244
5	.854	50.81	57.81	.78	244
6	.956	56.88	63.88	.68	244
B 1				.61	244
2				.73	244
3				.83	244
4				.80	244
5				.80	244
6				.73	244
ACFM =		69.052			
DSACFM =		37.371			
FT/SEC =		59.60			
MC =		25 %			
O ₂ =		15 %			
TS =		244 °F			
TEMP. MEAS. TOOL & S/N: MERCURY THERMOMETER					
				TIME END: 1122	HRS.

EPA METHOD 2 FIELD DATA

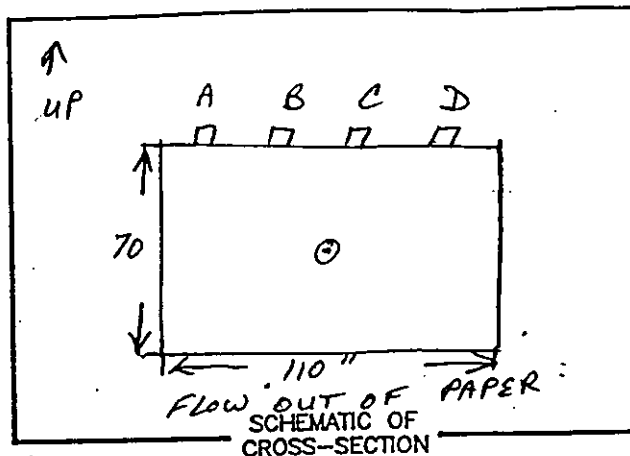
PROJECT NAME ACS / MOOREHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH PULP DRYER STACK
 TEST 1 RUN 0 DATE 1-21-92
 STACK DIA. 59.5 IN.
 DRY BULB 242 °F WET BULB 158 °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.85 IN Hg
 STATIC PRESSURE -.65 IN WC
 OPERATORS S. BAINVILLE ; D. LITFIN
 PITOT NO. 21-6 Cp .840



TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (°F)
		PORT LENGTH: 7.0	IN.	TIME START: 0800	HRS.
A 1	.044	2.62	9.62	.53	242
2	.146	8.69	15.69	.78	242
3	.296	17.61	24.61	.81	242
4	.704	41.89	48.89	.77	242
5	.854	50.81	57.81	.74	242
6	.956	56.88	63.88	.68	242
B 1				.54	242
2				.75	242
3				.77	242
4				.78	242
5				.78	242
6				.73	242
ACFM =		67.432			
DSCFM =		36.617			
FT/SEC =		58.20			
MC =		25%			
TS =		242°F			
O ₂ =		15%			
TEMP. MEAS. TOOL & S/N: <u>MERCURY THERMOMETER</u>				TIME END: 0822	HRS.

EPA METHOD 2 FIELD DATA

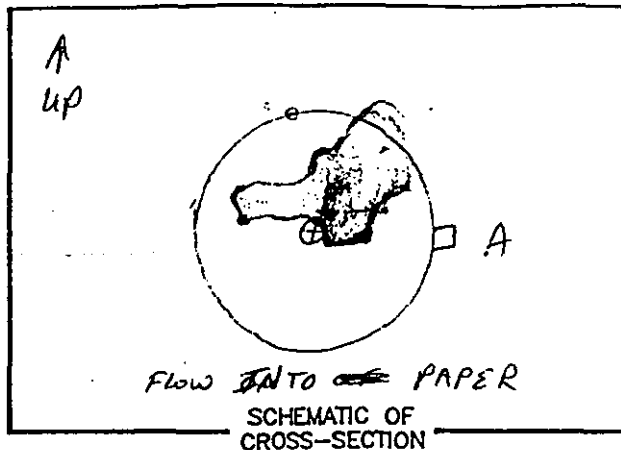
PROJECT NAME A.C.S. Moorhead
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER MULTI-CLONE INLET
 TEST 1 RUN 1 DATE 1-21-92
 STACK DIA. 110 x 70 IN.
 DRY BULB °F WET BULB °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.85 IN Hg
 STATIC PRESSURE +2.80 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. P1781 Cp .840



TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (°F)
		PORT LENGTH: <u>4</u> IN.	TIME START: <u>1215</u> HRS.		
A - 1		<u>5.83</u>	<u>9.83</u>	<u>0.45</u>	<u>242</u>
2		<u>17.50</u>	<u>21.50</u>	<u>0.23</u>	
3		<u>29.17</u>	<u>33.17</u>	<u>0.17</u>	
4		<u>40.84</u>	<u>44.84</u>	<u>0.15</u>	
5		<u>52.51</u>	<u>56.51</u>	<u>0.08</u>	
6		<u>64.18</u>	<u>68.18</u>	<u>0.05</u>	
B - 1				<u>0.50</u>	
2				<u>0.36</u>	
3				<u>0.28</u>	
4				<u>0.15</u>	
5				<u>0.10</u>	
6				<u>0.05</u>	
C - 1	FT/SEC =	<u>25.08</u>		<u>0.32</u>	
2	ACFM =	<u>80.469</u>		<u>0.18</u>	
3	DSCFM =	<u>44.082</u>		<u>0.08</u>	
4	MC =	<u>25%</u>		<u>0.06</u>	
5	O ₂ =	<u>15%</u>		<u>0.03</u>	
6	TS =	<u>242°F</u>		<u>0.02</u>	
D - 1				<u>0.25</u>	
2				<u>0.12</u>	
3				<u>0.08</u>	
4				<u>0.08</u>	
5				<u>0.04</u>	
6				<u>0.02</u>	
TEMP. MEAS. TOOL & S/N:				TIME END: <u>1230</u> HRS.	

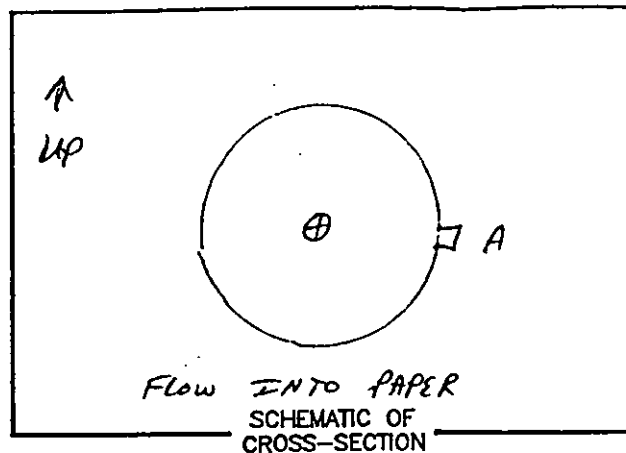
EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. / MOORHEAD
PROJECT NUMBER 920014
SOURCE SOUTH DRYER ASPIRATION DUCT
TEST 1 RUN 1 DATE 1-21-92
STACK DIA. 24.5 IN.
DRY BULB 242 °F WET BULB 158 °F
MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
BAROMETRIC PRESSURE 28.85 IN Hg
STATIC PRESSURE -0.50 IN WC
OPERATORS D. SMITH / A. NELSON
PITOT NO. PI-4 Cp .840



TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (°F)
		PORT LENGTH: 4	IN.	TIME START: 1100	HRS.
A - 1		0.51 → 1.00	5.00	0.08	242
2		1.64	5.64	0.25	242
3		2.89	6.89	0.26	243
4		4.34	8.34	0.31	243
5		6.13	10.13	0.31	242
6		8.72	12.72	0.38	242
7		15.78	19.78	0.89	241
8		18.38	22.38	1.15	241
9		20.16	24.16	1.30	241
10		21.61	25.61	1.80	242
11		22.86	26.86	2.00	242
12		23.99 → 23.50	27.50	1.80	243
FT/SEC =		58.79			
ACFM =		11,547			
DSCFM =		6,273			
MC % =		25%			
°FTS =		242			
O ₂ % =		15%			
TEMP. MEAS. TOOL & S/N:					
				TIME END: 1115	HRS.

PROJECT NAME A.C.S. MOORHEAD
PROJECT NUMBER 920014
SOURCE SOUTH DRYER ASPIRATION DUCT
TEST 1 RUN 1 DATE 1-21-92
STACK DIA. 24.5 IN.
DRY BULB _____ °F WET BULB _____ °F
MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
BAROMETRIC PRESSURE 28.85 IN Hg
STATIC PRESSURE -0.47 IN WC
OPERATORS D. SMITH / A. NELSON
PITOT NO. PI-4 Cp .840

AIR-2

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD

PROJECT NUMBER

SOURCE SWATH DRIVER ASPIRATION DUST

TEST 1 ^{POST}RUN 3 DATE 1-21-92

STACK DIA. 24.5 IN.

DRY BULB _____ °F WET BULB _____ °F

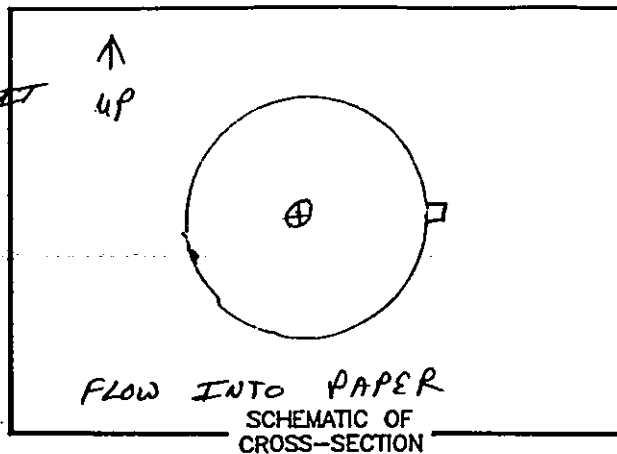
MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.

BAROMETRIC PRESSURE 28.85 IN Hg

STATIC PRESSURE -0.55 IN WC

OPERATORS D. SMITH / A. NELSON

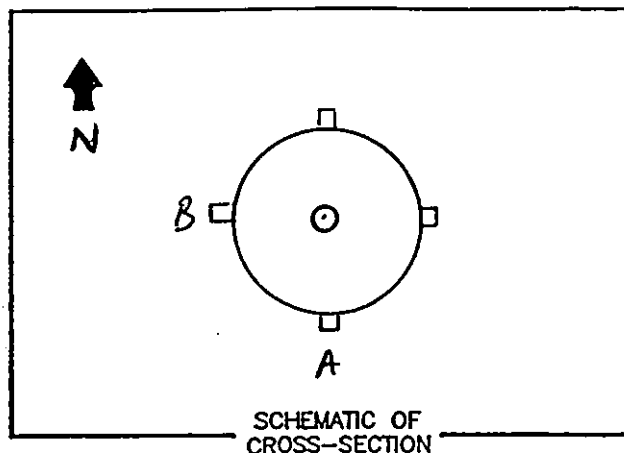
PITOT NO. P1-4 Cp 840



TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH:	4	IN.	TIME START: 2010 HRS.
A - 1				0.10	244
2				0.13	
3				0.18	
4				0.18	
5				0.21	
6				0.20	
7				0.53	
8				0.78	
9				1.10	
10				1.25	
11				1.30	
12				1.40	
	FT/SEC. =	49.53			
	ACFM =	9.729			
	DSCFM =	4.848			
	M.C. =	31%			
	O2 =	15%			
	T.S. =	244 °F			
TEMP. MEAS. TOOL & S/N:				TIME END: 2025 HRS.	

EPA METHOD 2 FIELD DATA

PROJECT NAME ACS / MOOREHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH PULD DRYING STACK
 TEST 2 RUN 0 DATE 1-22-92
 STACK DIA. 59.5 IN.
 DRY BULB 220 °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.70 IN Hg
 STATIC PRESSURE -.43 IN WC
 OPERATORS S. BAINBRIDGE / D. LITFIN
 PITOT NO. P1-6 Cp .840



TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (°F)
		PORT LENGTH: <u>7.0</u>	IN.	TIME START: <u>0817</u>	HRS.
A 1	.044	2.62	9.62	.47	220
2	.146	8.69	15.69	.68	220
3	.296	17.61	24.61	.70	220
4	.704	41.89	48.89	.68	220
5	.854	50.81	57.81	.65	220
6	.956	56.88	63.88	.60	220
B 1				.50	220
2				.65	220
3				.68	220
4				.67	220
5				.66	220
6				.60	220
ACFM =		62,880			
DSCFM =		32,748			
MC =		30			
TS =		270			
O ₂ =		14			
FT/SAC =		54.28			
TEMP. MEAS. TOOL & S/N: <u>MERCURY THERMOMETER</u>				TIME END: <u>0825</u>	HRS.

EPA METHOD 2 FIELD DATA

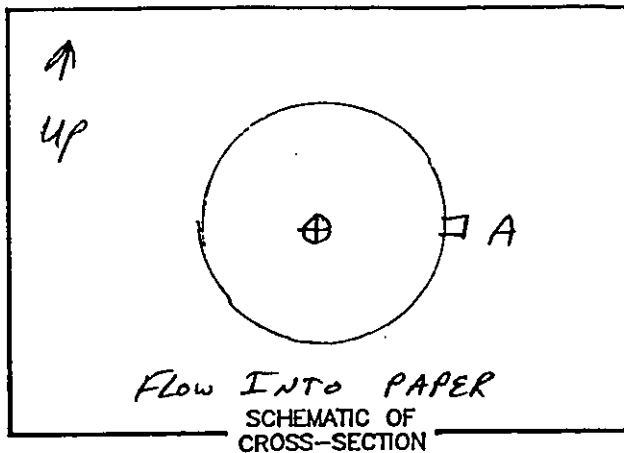
PROJECT NAME A.C.S. MOORHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER MULTI-CLONE INLET
 TEST 2 RUN 1 DATE 1-22-92
 STACK DIA. 70 x 110 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE _____ IN Hg
 STATIC PRESSURE + 2.80 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. P1-8 Cp .840

SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH:	<u>4</u> IN.	TIME START: <u>0815</u> HRS.	
A - 1				<u>0.48</u>	
2				<u>0.29</u>	
3				<u>0.14</u>	
4				<u>0.10</u>	
5				<u>0.06</u>	
6				<u>0.05</u>	
B - 1				<u>0.51</u>	
2				<u>0.42</u>	
3				<u>0.28</u>	
4				<u>0.15</u>	
5				<u>0.07</u>	
6				<u>0.04</u>	
C - 1				<u>0.38</u>	
2				<u>0.20</u>	
3				<u>0.15</u>	
4				<u>0.07</u>	
5				<u>0.05</u>	
6				<u>0.02</u>	
D - 1				<u>0.32</u>	
2				<u>0.16</u>	
3				<u>0.11</u>	
4				<u>0.10</u>	
5				<u>0.10</u>	
6				<u>0.08</u>	
TEMP. MEAS. TOOL. & S/N:				TIME END: <u>0835</u> HRS.	

EPA METHOD 2 FIELD DATA

PROJECT NAME ACS MOORHEAD
PROJECT NUMBER 920014
SOURCE SOUTH DRYER ASPIRATION
TEST 2 RUN 1 DATE 1-22-92
STACK DIA. 24.5 IN.
DRY BULB _____ °F WET BULB _____ °F
MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
BAROMETRIC PRESSURE _____ IN Hg
STATIC PRESSURE -0.52 IN WC
OPERATORS D. SMITH / A. NELSON
PITOT NO. P1-4 Cp 840

[illegible]

EPA METHOD 2 FIELD DATA

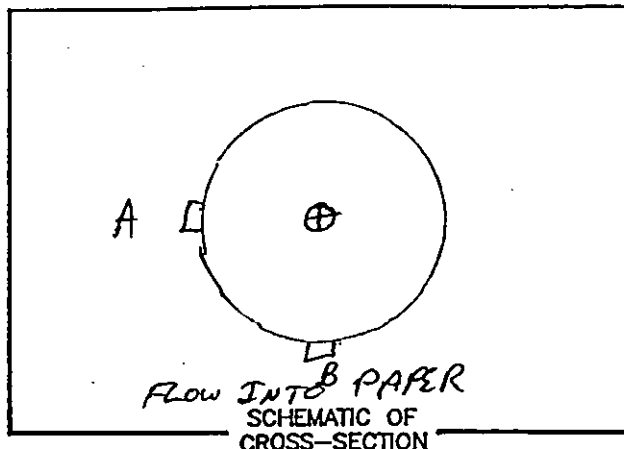
PROJECT NAME ACS MOORHEAD
PROJECT NUMBER 920014
SOURCE SOUTH DRYER ASPIRATION
TEST 2 RUN 3 DATE 1-22-92
STACK DIA. 24.5 IN.
DRY BULB _____ °F WET BULB _____ °F
MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
BAROMETRIC PRESSURE 28.70 IN Hg
STATIC PRESSURE -.50 IN WC
OPERATORS D. SMITH / A. NELSON
PITOT NO. P1-4 Cp .840

**SCHEMATIC OF
CROSS-SECTION**

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH:	4.0 IN.	TIME START:	1710 HRS.
A - 1				0.10	243
2				0.12	
3				0.15	
4				0.16	
5				0.18	
6				0.19	
7				0.44	
8				0.75	
9				0.89	
10				1.10	
11				1.20	
12				1.20	
	FT/SEC =	47.69			
	ACFM =	9367			
	DSCFM =	4044			
	M.C. =	40 %			
	O ₂ =	16 %			
	T.S. =	243 °F			
TEMP. MEAS. TOOL & S/N:				TIME END:	1725 HRS.

EPA METHOD 2 FIELD DATA

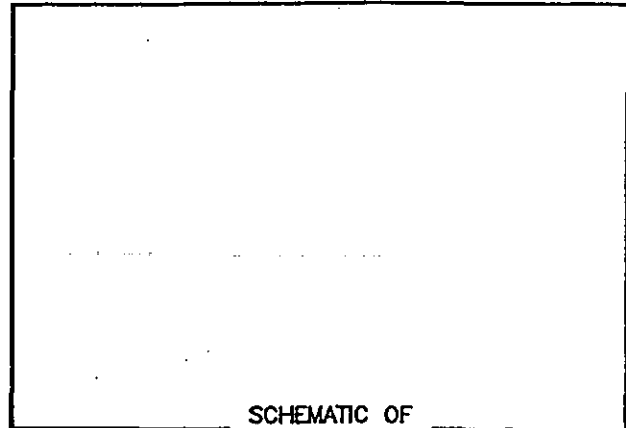
PROJECT NAME A.C.S. / MOORHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER RECYCLE
 TEST 2 RUN 1 DATE 1-22-92
 STACK DIA. 25.5 IN.
 DRY BULB °F WET BULB °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.70 IN Hg
 STATIC PRESSURE -0.58 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. P1-4 Cp .840



TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH: <u>3.5</u> IN.		TIME START: <u>0905</u> HRS.	
A - 1		1.00	<u>4.50</u>	0.19	236
2		2.68	6.18	0.27	
3		4.95	8.45	0.29	
4		8.24	11.74	0.28	
5		17.26	20.76	0.27	
6		20.55	24.05	0.28	
7		22.82	26.32	0.29	
8		24.50	28.00	0.29	
B - 1				0.30	
2				0.32	
3				0.34	
4				0.31	
5				0.22	
6				0.20	
7				0.20	
8				0.20	
	FT./SEC. =	35.63			
	ACFM =	75.81			
	DSCFM =	3,856			
	M.C. =	30 %			
	O ₂ =	16 %			
	Ts =	236 °F			
TEMP. MEAS. TOOL & S/N:				TIME END: <u>0920</u> HRS.	

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER RECYCLE
 TEST 2 RUN 3 DATE 1-22-92
 STACK DIA. 25.5 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.70 IN Hg
 STATIC PRESSURE -0.49 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. P1-4 Cp .840

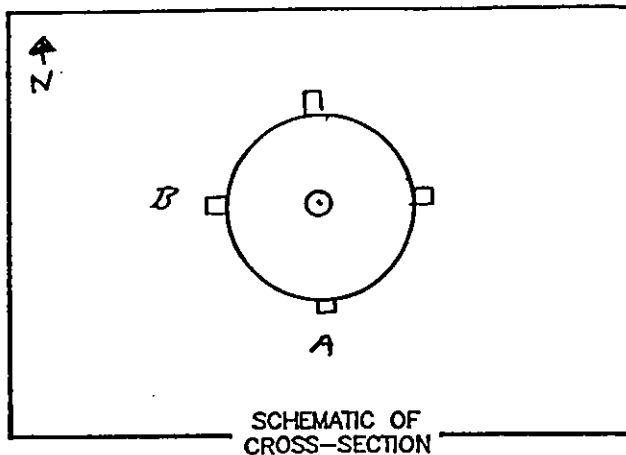


SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH: <u>3.5</u>	IN.	TIME START: <u>1730</u>	HRS.
A - 1				<u>0.21</u>	<u>243</u>
2				<u>0.25</u>	
3				<u>0.26</u>	
4				<u>0.26</u>	
5				<u>0.20</u>	
6				<u>0.19</u>	
7				<u>0.22</u>	
8				<u>0.24</u>	
B - 1				<u>0.27</u>	
2				<u>0.31</u>	
3				<u>0.32</u>	
4				<u>0.29</u>	
5				<u>0.20</u>	
6				<u>0.16</u>	
7				<u>0.17</u>	
8				<u>0.16</u>	
FT./SEC. =		<u>34.15</u>			
ACFM =		<u>7267</u>			
DSCFM =		<u>3137</u>			
M.C. =		<u>40 %</u>			
O ₂ =		<u>16 %</u>			
T _S =		<u>243 °F</u>			
TEMP. MEAS. TOOL & S/N:				TIME END: <u>1745</u>	HRS.

EPA METHOD 2 FIELD DATA

PROJECT NAME ACS / POWERHEAD
PROJECT NUMBER 920014
SOURCE SOUTH PULP DRYER STACK
TEST 3 RUN 0 DATE 1-23-72
STACK DIA. 59.5 IN.
DRY BULB 230 °F WET BULB _____ °F
MANOMETER: ☐ REG. ☐ EXP. ☐ ELEC.
BAROMETRIC PRESSURE 29.68 IN Hg
STATIC PRESSURE -.45 IN WC
OPERATORS S. BAINWILLG + D. L. GIFFIN
PITOT NO. P1-6 Cp .840



TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH:	7.00 IN.	TIME START: 0953	HRS.
A 1	.044			.32	220
2	.146			.49	232
3	.296			.53	230
4	.704			.55	231
5	.854			.53	231
6	.956			.47	231
B 1				.42	231
2				.53	221
3				.55	221
4				.57	229
5				.53	230
6				.45	230
	ACFM =	57,466			
	DSCFM =	25,262			
	FT/SEC =	49.60			
	TS =	230			
	MC =	40			
	O ₂ =	15			
TEMP. MEAS. TOOL & S/N: Mercury thermometer				TIME END: 0905	HRS.

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER M.C. INLET
 TEST 3 RUN 1 DATE 1-23-92
 STACK DIA. 70 X 110 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.68 IN Hg
 STATIC PRESSURE +2.60 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. P1-8 Cp .840

SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH:	<u>4</u> IN.	TIME START:	<u>0830</u> HRS.
A - 1				<u>0.35</u>	<u>242</u>
2				<u>0.25</u>	
3				<u>0.11</u>	
4				<u>0.08</u>	
5				<u>0.06</u>	
6				<u>0.03</u>	
B - 1				<u>0.47</u>	
2				<u>0.38</u>	
3				<u>0.28</u>	
4				<u>0.17</u>	
5				<u>0.08</u>	
6				<u>0.03</u>	
C - 1				<u>0.35</u>	
2				<u>0.18</u>	
3				<u>0.11</u>	
4				<u>0.08</u>	
5	1			<u>0.05</u>	
6				<u>0.03</u>	
D - 1				<u>0.25</u>	
2				<u>0.13</u>	
3				<u>0.08</u>	
4				<u>0.07</u>	
5				<u>0.03</u>	
6				<u>0.02</u>	
TEMP. MEAS. TOOL & S/N:				TIME END:	<u>0845</u> HRS.

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. Moorhead
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER ASPIRATION
 TEST 3 RUN 1 DATE 1-23-92
 STACK DIA. 24.5 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.68 IN Hg
 STATIC PRESSURE -0.41 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. P1-4 Cp .840

SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (°F)
		PORT LENGTH:	<u>4</u> IN.	TIME START:	<u>0815</u> HRS.
A- 1				<u>0.07</u>	<u>242</u>
2				<u>0.08</u>	
3				<u>0.10</u>	
4				<u>0.12</u>	
5				<u>0.12</u>	
6				<u>0.13</u>	
7				<u>0.38</u>	
8				<u>0.55</u>	
9				<u>0.73</u>	
10				<u>0.85</u>	
11				<u>0.93</u>	
12				<u>0.93</u>	
FT/SEC =		<u>41.47</u>			
ACFM =		<u>8146</u>			
DSCFM =		<u>3,520</u>			
ML =		<u>40 %</u>			
O ₂ =		<u>16 %</u>			
TS =		<u>242 °F</u>			
TEMP. MEAS. TOOL & S/N:				TIME END: <u>0830</u> HRS.	

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD
PROJECT NUMBER 920014
SOURCE SOUTH DRYER ASPIRATION
TEST 3 RUN 3 DATE 1-23-92
STACK DIA. 24.5 IN.
DRY BULB _____ °F WET BULB _____ °F
MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
BAROMETRIC PRESSURE 28.88 IN Hg
STATIC PRESSURE -0.46 IN WC
OPERATORS D. SMITH / A. NELSON
PITOT NO. P1-18 Cp .840

**SCHEMATIC OF
CROSS-SECTION**

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH:	4	IN.	TIME START: 1645 HRS.
A - 1				0.07	243
2				0.08	
3				0.10	
4				0.11	
5				0.12	
6				0.15	
7				0.40	
8				0.66	
9				0.81	
10				0.95	
11				1.08	
12				1.10	
	FT./SEC. =	43.93			
	ACFM =	8629			
	DSCFM =	3537			
	M.C. =	4.3 %			
	O ₂ =	16 %			
	TS =	243 °F			
TEMP. MEAS. TOOL & S/N:			TIME END: 1700 HRS.		

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER RECYCLE
 TEST 3 RUN 1 DATE 1-23-92
 STACK DIA. 25.5 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.68 IN Hg
 STATIC PRESSURE -2.00 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. P1-4 Cp .840

SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH:	<u>3.5</u> IN.	TIME START: <u>0800</u> HRS.	
A - 1				<u>0.65</u>	<u>242</u>
2				<u>0.76</u>	
3				<u>0.77</u>	
4				<u>0.70</u>	
5				<u>0.82</u>	
6				<u>0.83</u>	
7				<u>0.85</u>	
8				<u>0.90</u>	
B - 1				<u>0.91</u>	
2				<u>1.10</u>	
3				<u>1.10</u>	
4				<u>1.02</u>	
5				<u>0.74</u>	
6				<u>0.77</u>	
7				<u>0.77</u>	
8				<u>0.78</u>	
FT/SEC. =		<u>65.37</u>			
ACFM =		<u>13,910</u>			
DSCFM =		<u>5,986</u>			
M.C. =		<u>40 %</u>			
O ₂ =		<u>16 %</u>			
TS =		<u>242 °F</u>			
TEMP. MEAS. TOOL & S/N:				TIME END: <u>0815</u> HRS.	

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER RECYCLE
 TEST 3 RUN 3 DATE 1-23-92
 STACK DIA. 25.5 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.68 IN Hg
 STATIC PRESSURE -1.90 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. P1-4 Cp .840

SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (°F)
		PORT LENGTH:	3.5 IN.	TIME START:	1700 HRS.
A - 1			0.77	1.65	243
2			0.83	1.70	
3			0.80	1.75	
4			0.80	1.80	
5			0.87	1.85	
6			0.95	1.80	
7			1.00	1.75	
8			1.03	1.85	
B - 1				0.90	
2				1.15	
3				1.15	
4				1.10	
5				0.82	
6				0.82	
7				0.87	
8				0.90	
FT./SEC. =		68.99			
ACFM =		14,680			
DSCFM =		5,995			
M.C. =		43%			
O ₂ =		16%			
T.S. =		243°F			
TEMP. MEAS. TOOL & S/N:				TIME END:	1715 HRS.

EPA METHOD 2 FIELD DATA

PROJECT NAME ACS/MOOREHEAD
PROJECT NUMBER 920014
SOURCE SOUTH DRYER STACK
TEST 4 RUN 0 DATE 1-24-52
STACK DIA. 54.5 IN.
DRY BULB 22.6 °F WET BULB _____ °F
MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
BAROMETRIC PRESSURE 29.82 IN Hg
STATIC PRESSURE -.55 IN WC
OPERATORS S. BAINBRIDGE + D. LITFIN
PITOT NO. P1-6 Cp 840

SCHEMATIC OF CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH: 7.0	IN.	TIME START: 0725	HRS.
A 1				.54	226
2				.63	226
3				.66	226
4				.64	226
5				.60	226
6				.54	226
B 1				.43	226
2				.58	226
3				.65	226
4				.66	226
5				.64	226
6				.58	226
	ACFM	62.695			
	DSCFM	27.849			
	FT/SEC	59.11			
	TS	226			
	O2	15%			
	MC	40%			
TEMP. MEAS. TOOL & S/N: MRCOMM THERMISTOR				TIME END:	HRS.

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MacKHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER M.C. INLET
 TEST 4 RUN 1 DATE 1-24-92
 STACK DIA. 70 X 110 IN.
 DRY BULB °F WET BULB °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.83 IN Hg
 STATIC PRESSURE +2.75 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. PI-8 Cp .840

SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH:	<u>4</u> IN.	TIME START:	<u>0730</u> HRS.
A - 1				<u>0.40</u>	<u>265</u>
2				<u>0.30</u>	
3				<u>0.15</u>	
4				<u>0.12</u>	
5				<u>0.09</u>	
6				<u>0.06</u>	
B - 1				<u>0.47</u>	
2				<u>0.40</u>	
3				<u>0.30</u>	
4				<u>0.16</u>	
5				<u>0.11</u>	
6				<u>0.05</u>	
C - 1				<u>0.48</u>	
2				<u>0.24</u>	
3				<u>0.15</u>	
4				<u>0.10</u>	
5				<u>0.07</u>	
6				<u>0.04</u>	
D - 1				<u>0.26</u>	
2				<u>0.20</u>	
3				<u>0.11</u>	
4				<u>0.10</u>	
5				<u>0.09</u>	
6				<u>0.07</u>	
TEMP. MEAS. TOOL & S/N:				TIME END:	<u>0745</u> HRS.

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER ASPIRATION
 TEST 4 RUN 1 DATE 1-24-92
 STACK DIA. 24.5 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.83 IN Hg
 STATIC PRESSURE -0.52 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. PI-4 Cp .840

SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH:	<u>4</u> IN.	TIME START: <u>0715</u> HRS.	
A - 1				<u>0.14</u>	<u>265</u>
2				<u>0.15</u>	
3				<u>0.19</u>	
4				<u>0.20</u>	
5				<u>0.22</u>	
6				<u>0.25</u>	
7				<u>0.60</u>	
8				<u>0.90</u>	
9				<u>1.10</u>	
10				<u>1.40</u>	
11				<u>1.50</u>	
12				<u>1.60</u>	
FT./SEC. =		<u>53.94</u>			
ACFM =		<u>10,596</u>			
DSCFM =		<u>4,827</u>			
M.C. =		<u>35 %</u>			
O ₂ =		<u>16 %</u>			
TS =		<u>265</u>			
TEMP. MEAS. TOOL & S/N:					
TIME END: <u>0730</u> HRS.					

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD
PROJECT NUMBER 920014
SOURCE SOUTH DRYER ASPIRATION
TEST 4 RUN 3 DATE 1-24-92
STACK DIA. 24.5 IN.
DRY BULB _____ °F WET BULB _____ °F
MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
BAROMETRIC PRESSURE 28.83 IN Hg
STATIC PRESSURE -0.55 IN WC
OPERATORS D. SMITH / A. NELSON
PITOT NO. P1-4 Cp 840

**SCHEMATIC OF
CROSS-SECTION**

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH: 4.5 IN.		TIME START: 1700 HRS.	
A - 1				0.10	245
2				0.12	
3				0.13	
4				0.15	
5				0.17	
6				0.20	
7				0.51	
8				0.69	
9				0.96	
10				1.10	
11				1.20	
12				1.25	
	PT/SEC. =	48.19			
	ACFM =	9,466			
	DSCFM =	3888			
	M.C. =	43 %			
	O ₂ =	16 %			
	TS =	245 °F			
TEMP. MEAS. TOOL & S/N:				TIME END: 1715 HRS.	

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER RECYCLE
 TEST 4 RUN 1 DATE 1-24-92
 STACK DIA. 25.5 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.83 IN Hg
 STATIC PRESSURE -0.72 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITCH NO. P1-4 Cp 840

SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
PORT LENGTH: <u>3.5</u> IN.				TIME START: <u>0700</u> HRS.	
A - 1				<u>0.26</u>	<u>265</u>
2				<u>0.31</u>	
3				<u>0.31</u>	
4				<u>0.32</u>	
5				<u>0.25</u>	
6				<u>0.27</u>	
7				<u>0.30</u>	
8				<u>0.32</u>	
B - 1				<u>0.33</u>	
2				<u>0.39</u>	
3				<u>0.40</u>	
4				<u>0.38</u>	
5				<u>0.25</u>	
6				<u>0.24</u>	
7				<u>0.25</u>	
8				<u>0.25</u>	
FT/SEC =		<u>39.13</u>			
ACFM =		<u>8,327</u>			
DSCFM =		<u>3,791</u>			
M.C. =		<u>35%</u>			
O ₂ =		<u>16%</u>			
T.S. =		<u>265</u>			
TEMP. MEAS. TOOL & S/N:				TIME END: <u>0715</u> HRS.	

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER RECYCLE
 TEST 4 RUN 1 DATE 1-24-92
 STACK DIA. 25.5 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.83 IN Hg
 STATIC PRESSURE -0.89 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. PI-4 Cp 840

SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH: <u>3.5</u>	IN.	TIME START: <u>0915</u>	HRS.
A - 1				<u>0.33</u>	<u>240</u>
2				<u>0.37</u>	
3				<u>0.38</u>	
4				<u>0.38</u>	
5				<u>0.33</u>	
6				<u>0.34</u>	
7				<u>0.37</u>	
8				<u>0.42</u>	
B - 9				<u>0.35</u>	
10				<u>0.47</u>	
11				<u>0.50</u>	
12				<u>0.47</u>	
13				<u>0.32</u>	
14				<u>0.28</u>	
15				<u>0.29</u>	
16				<u>0.28</u>	
FT/SEC. = <u>42.42</u>					
ACFM = <u>9027</u>					
DSCFM = <u>4255</u>					
M.L. = <u>35%</u>					
O ₂ = <u>16%</u>					
TS = <u>240°F</u>					
TEMP. MEAS. TOOL & S/N:				TIME END: <u>0930</u>	HRS.

EPA METHOD 2 FIELD DATA

PROJECT NAME ACS MOORHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER RECYCLE
 TEST 4 RUN 1 DATE 1-24-92
 STACK DIA. 25.5 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.83 IN Hg
 STATIC PRESSURE -1.10 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. P1-4 Cp .840

SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH:	3.5 IN.	TIME START:	0945 HRS.
A - 1				0.39	240
2				0.45	
3				0.44	
4				0.46	
5				0.42	
6				0.43	
7				0.47	
8				0.48	
B - 1				0.50	
2				0.57	
3				0.59	
4				0.55	
5				0.39	
6				0.39	
7				0.42	
8				0.43	
FT./SEC. =		47.62			
ACFM =		10,134			
DSCFM =		4774			
MC =		35%			
O ₂ =		16%			
TEMP. MEAS. TOOL & S/N:				TIME END: 0955 HRS.	

EPA METHOD 2 FIELD DATA

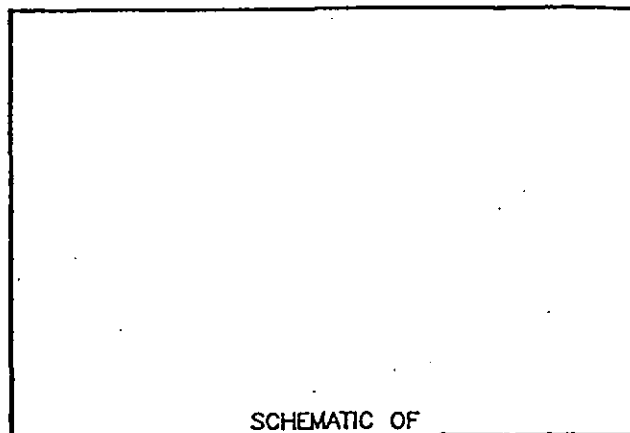
PROJECT NAME A.C.S. MOORHEAD
 PROJECT NUMBER 920014
 SOURCE SOUTH DRYER RECYCLE
 TEST 4 RUN 1 DATE 1-24-92
 STACK DIA. 25.5 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.83 IN Hg
 STATIC PRESSURE -1.17 IN WC
 OPERATORS D. SMITH
 PITOT NO. P1-4 Cp .840

SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH: <u>3.5</u> IN.	TIME START: <u>0955</u> HRS.		
A - 1				<u>0.43</u>	<u>240</u>
2				<u>0.46</u>	
3				<u>0.50</u>	
4				<u>0.46</u>	
5				<u>0.43</u>	
6				<u>0.48</u>	
7				<u>0.51</u>	
8				<u>0.53</u>	
B - 1				<u>0.56</u>	
2				<u>0.62</u>	
3				<u>0.65</u>	
4				<u>0.63</u>	
5				<u>0.43</u>	
6				<u>0.42</u>	
7				<u>0.42</u>	
8				<u>0.35</u>	
FT/SEC =		<u>49.71</u>			
ACFM =		<u>10,577</u>			
DSCFM =		<u>4599</u>			
MC =		<u>40%</u>			
O ₂ =		<u>16%</u>			
TEMP. MEAS. TOOL & S/N:				TIME END: <u>1010</u> HRS.	

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. Moorhead
 PROJECT NUMBER 950014
 SOURCE SOUTH DRYER RECYCLE
 TEST 4 RUN 3 DATE 1-24-92
 STACK DIA. 25.5 IN.
 DRY BULB _____ °F WET BULB _____ °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.83 IN Hg
 STATIC PRESSURE -1.20 IN WC
 OPERATORS D. SMITH / A. NELSON
 PITOT NO. P1-4 Cp .840

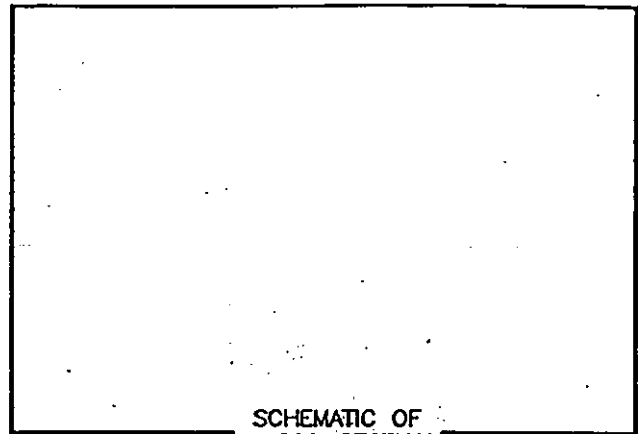


SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH: <u>3.5</u>	IN.	TIME START: <u>1715</u>	HRS.
A - 1				<u>0.43</u>	<u>242</u>
2				<u>0.47</u>	
3				<u>0.48</u>	
4				<u>0.49</u>	
5				<u>0.47</u>	
6				<u>0.48</u>	
7				<u>0.50</u>	
8				<u>0.55</u>	
B - 1				<u>0.54</u>	
2				<u>0.61</u>	
3				<u>0.65</u>	
4				<u>0.62</u>	
5				<u>0.45</u>	
6				<u>0.41</u>	
7				<u>0.43</u>	
8				<u>0.43</u>	
FT./SEC = <u>50.59</u>					
ACFM = <u>10,766</u>					
DSCFM = <u>4,434</u>					
MC = <u>43 %</u>					
O2 = <u>16 %</u>					
T.S. = <u>242 °F</u>					
TEMP. MEAS. TOOL & S/N:				TIME END: <u>1730</u>	HRS.

EPA METHOD 2 FIELD DATA

PROJECT NAME A.C.S. MoorHEAD
 PROJECT NUMBER 920014
 SOURCE NORTH DRYER STACK
 TEST 15 RUN 1 DATE 1-24-92
 STACK DIA. 59.5 IN.
 DRY BULB °F WET BULB °F
 MANOMETER: ☒ REG. ☐ EXP. ☐ ELEC.
 BAROMETRIC PRESSURE 28.83 IN Hg
 STATIC PRESSURE -1.5 IN WC
 OPERATORS S. BAINVILLE / D. LITVIN
 PITOT NO. P1-6 Cp 840



SCHEMATIC OF
CROSS-SECTION

TRAVERSE POINT NO.	FRACTION OF DIAMETER	DISTANCE FROM STACK WALL (IN.)	DISTANCE FROM END OF PORT (IN.)	VELOCITY PRESSURE (IN WC)	TEMPERATURE OF GAS (° F)
		PORT LENGTH:	4 IN.	TIME START:	1719 HRS.
A - 1				2.10	200
2				2.25	
3				2.10	
4				2.10	
5				1.40	
6				2.10	
B - 1				1.80	
2				2.00	
3				2.00	
4				1.40	
5				1.40	
6				1.80	
ACFM =		111,500			
DSCFM =		51,506			
FT/SEC =		96.24			
M.C. =		40 %			
O2 =		16 %			
TS =		200 °F			
TEMP. MEAS. TOOL & S/N:					
				TIME END:	HRS.

Appendix 2

Field Data Sheets

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME ACS / MOOREHEAD METHOD 1-5
 PROJECT NUMBER 920019 FILTER HOLDER GLASS
 SOURCE SOUTH PULP DRYER STACK NO. OF TRAVERSE POINTS 12
 DATE 1-21-92 TEST 1 RUN 1 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒
 POSTTEST: (0.00 CFM AT 25 IN. Hg (vac)) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED: 1120 RECOVERY SOLVENT(S):
☒ ACETONE
☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: S.B. + D.L.

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2	896	700	696
IMPINGER NO. 3			
CONDENSER			
DESICCANT	1424	1275	149
	1459	1308	151
TOTAL			996

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 1
 BAG MATERIAL: TEDLAR SIZE: 44L
 PRETEST LEAK CHECK: 00 cc/MIN AT 15 IN. Hg
 TIME START: 1315 (HRS) TIME END: 1519 (HRS)
 SAMPLING RATE: 100 cc/MIN OPERATOR: S.B.
 S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123828

PITOT NO. P1-6 Cp .840
 BAR. PRESS. 28.85 IN Hg H₂O 25 %
 NOZZLE NO. N1-4 NOZZLE DIA. .312 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME ACS / MOORHEAD SOURCE SOUTH PULP PAPER STACK OPERATORS S.B. / D.L.
 PROJECT NUMBER 920014 DATE 1-21-92 TEST 1 RUN 1 METER BOX NO. 1 ΔH 1.75 IN WC
 GASMETER COEFF. 1.001

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)						OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN	GAS/OUT		
	(1315)	(774.17)												
0	4	778.30	.72	3.28	8.53	8	240	245	251	40	109	78		15.7
6	8	782.70	.72	3.42	2.68	10	240	246	250	40	117	80		15.7
5	12	787.28	.78	3.77	7.26	12	233	246	251	41	123	83		15.7
5	16	791.85	.78	3.80	1.89	14	233	246	251	41	125	84		15.7
4	20	796.50	.80	3.91	6.57	17	233	247	252	42	129	87		15.2
4	24	801.20	.80	3.93	1.29	17	233	247	252	43	130	90		15.2
3	28	806.00	.81	3.99	6.05	18	234	247	253	43	132	91		15.2
3	32	810.75	.81	4.00	0.82	19	234	247	253	43	132	92		15.2
2	36	815.44	.75	3.72	5.43	20	232	247	254	44	133	94		14.5
2	40	820.00	.75	3.74	0.06	20	230	247	253	44	135	96		14.5
1	44	823.92	.53	2.66	3.97	15	230	246	250	42	136	97		15.0
1	48	827.90	.55	2.76	7.96	15	230	246	251	42	135	98		15.0
A	52	832.37	.67	3.36	2.36	16	230	248	250	43	129	97		15.0
6	56	836.70	.68	3.38	8.74	17	230	249	252	42	133	98		15.0
5	60	841.32	.73	3.66	1.33	18	230	250	253	42	137	99		15.2
5	64	845.90	.74	3.72	5.96	20	230	251	253	42	140	100		15.2
4	68	850.61	.77	3.88	0.69	20	230	251	253	42	139	99		16.2
4	72	855.32	.76	3.79	5.37	20	236	252	253	41	139	101		16.0
3	76	860.23	.83	4.14	0.27	21	237	252	253	41	134	101		16.0
3	80	865.10	.83	4.14	5.16	22	237	251	252	41	138	101		16.0
2	84	870.00	.83	4.06	0.00	22	237	251	252	41	137	101		15.0
2	88	874.80	.81	4.06	4.83	22	233	252	253	40	132	100		15.5
1	92	879.10	.63	3.16	9.11	18	233	252	255	40	137	100		15.5
1	96	883.37	.63	3.16	3.39	18	234	252	255	40	132	100		15.5
	(1519)													
	$\theta = 96$	$V_m = 104.20$		$\Delta H = 365$							AVG. =	113		

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME ACS/MOORHEAD METHOD 1-5
PROJECT NUMBER 92001A FILTER HOLDER GLASS
SOURCE SOUTH PULP DRYER STACK NO. OF TRAVERSE POINTS 12
DATE 1-21-92 TEST 1 RUN 2 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒POSTTEST: (0.00 CFM AT _____ IN. Hg (vac)) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED:

1170

RECOVERY SOLVENT(S):



ACETONE



OTHER(S)

NO. OF PROBE WASH BOTTLES: 1SAMPLE RECOVERED BY: S.B. & D.L.

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2	876	200	676
IMPINGER NO. 3			
CONDENSER			
DESICCANT	1493	1331	162
	1460	1320	140
TOTAL			778

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 2
BAG MATERIAL: TEDLAR SIZE: 44 Lr
PRETEST LEAK CHECK: 00 cc/MIN AT 15 IN. Hg
TIME START: 1600 (HRS) TIME END: _____ (HRS)
SAMPLING RATE: 100 cc/MIN OPERATOR: S.B.
S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123828

PITOT NO. P1-6 Cp .840BAR. PRESS. 28.85 IN Hg H₂O 30 %NOZZLE NO. N1-4 NOZZLE DIA. 3/2 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME ACS / mod. head SOURCE SOOTH PULP DRYER STACK OPERATORS S.B. + D.L.
 PROJECT NUMBER 920014 DATE 1-21-92 TEST 1 RUN 2 METER BOX NO. 1 $\Delta H = 1.35''$ IN WC
 GASMETER COEFF. 1.001

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
	(1600)	(883.87)											
A 6	4	888.10	.68	3.01	8.02	8	233	257	262	40	108	89	15.5
6	8	892.00	.67	2.89	7.04	7	234	252	262	40	123	90	15.5
5	12	896.36	.76	3.25	6.32	9	249	252	262	40	129	90	15.5
5	16	900.66	.75	3.29	0.65	10	235	253	262	40	136	94	15.5
4	20	905.08	.78	3.45	5.09	11	236	252	264	40	139	96	15.5
4	24	909.50	.77	3.42	9.53	11	236	252	262	40	140	97	15.5
3	28	914.15	.85	3.78	4.10	14	235	252	261	41	142	99	15.5
3	32	918.82	.84	3.75	8.86	15	235	252	261	41	142	100	15.5
2	36	923.41	.81	3.62	3.44	12	235	252	261	41	143	98	15.5
2	40	928.10	.80	3.60	8.00	12	230	252	261	41	143	101	15.5
1	44	932.06	.61	2.76	2.01	10	230	252	261	41	143	100	15.5
1	48	936.01	.63	2.85	6.08	11	230	252	261	41	143	100	15.5
B 6	52	940.32	.68	3.07	0.30	12	230	252	261	41	128	100	15.5
6	56	944.56	.70	3.12	4.53	13	230	252	260	42	136	100	15.5
5	60	949.00	.80	3.58	9.07	15	230	252	260	42	141	101	15.5
5	64	953.58	.80	3.60	3.64	17	231	252	260	42	142	101	15.5
4	68	958.20	.82	3.69	8.26	18	231	252	260	42	143	102	15.5
4	72	962.80	.82	3.69	2.89	19	231	252	260	41	143	102	16.0
3	76	967.21	.76	3.42	7.35	20	232	252	261	40	144	102	16.0
3	80	971.73	.78	3.57	1.87	20	232	252	260	40	143	103	16.0
2	84	976.34	.78	3.52	6.40	20	231	252	260	41	143	103	16.0
2	88	980.81	.76	3.43	0.86	20	231	252	261	41	143	103	16.0
1	92	984.86	.60	2.71	4.84	12	230	251	261	42	142	103	15.7
1	96	988.40	.60	2.71	9.41	13	230	251	261	42	141	103	15.7
	(1745)												
	θ = 96	Vm = 104.43		ΔH = 332							AVG = 119		

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME ACS/MOOR HEAD METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER CICASS
 SOURCE SOUTH PULP DRYER STACK NO. OF TRAVERSE POINTS 12
 DATE 1-21-92 TEST 1 RUN 3 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒POSTTEST: 0.00 CFM AT 25 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO.S OF FILTERS USED:

1172

RECOVERY SOLVENT(S):

☒ ACETONE☐ OTHER(S)NO. OF PROBE WASH BOTTLES: 1SAMPLE RECOVERED BY: S.B. + D.L.

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2	<u>940</u>	<u>200</u>	<u>740</u>
IMPINGER NO. 3			
CONDENSER			
DESICCANT	<u>1434</u>	<u>1345</u>	<u>89</u>
	<u>1408</u>	<u>1323</u>	<u>85</u>
TOTAL			<u>914</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 3BAG MATERIAL: TETLAR SIZE: 4/4 LPRETEST LEAK CHECK: DD cc/MIN AT 15 IN. HgTIME START: 1825 (HRS) TIME END: 2013 (HRS)SAMPLING RATE: 100 cc/MIN OPERATOR: SLBS/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123828PITOT NO. P1-6 Cp .890BAR. PRESS. 28.85 IN Hg H₂O 33 %NOZZLE NO. N1-4 NOZZLE DIA. .321 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME ACS / MODERHEAD SOURCE SOUTH RIVER DRYER STACK OPERATORS S.B. F.D.C.
 PROJECT NUMBER 920014 DATE 1-21-92 TEST 1 RUN 3 METER BOX NO. 1 ΔH 0.75 IN WC
 GASMETER COEFF. 1.001

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL. (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
	(1815)	(989.34)											
B 6	4	993.20	.68	2.78	3.26	6	230	261	260	38	116	88	15.0
6	8	997.23	.67	2.78	7.21	6	230	261	260	38	118	88	15.0
5	12	1001.51	.79	3.29	1.52	8	228	260	260	38	141	90	15.0
5	16	1005.81	.78	3.31	5.84	8	231	260	260	38	134	92	15.5
4	20	1010.23	.79	3.34	0.25	9	230	260	260	37	136	94	15.5
4	24	1014.69	.80	3.39	4.66	11	231	260	260	37	138	95	15.5
3	28	1019.21	.83	3.54	9.17	11	229	260	260	37	141	97	15.5
3	32	1023.86	.88	3.76	3.83	12	229	260	260	37	141	98	15.5
2	36	1028.15	.75	3.21	8.14	12	229	254	260	36	142	100	16.0
2	40	1032.48	.76	3.26	2.45	12	230	259	260	36	142	100	16.0
1	44	1036.26	.55	2.36	6.00	12	230	259	260	36	141	100	16.0
1	48	1039.87	.54	2.32	9.87	10	230	259	260	36	141	101	16.0
A 6	52	1043.93	.67	2.88	3.95	12	230	259	260	36	127	100	15.5
6	56	1047.86	.64	2.21	7.80	12	230	259	260	36	135	100	15.5
5	60	1052.13	.73	3.14	2.15	14	225	258	260	36	138	101	15.5
5	64	1056.50	.76	3.28	6.50	14	225	258	260	36	141	101	15.5
4	68	1061.00	.92	3.54	1.03	17	225	258	259	36	141	101	16.0
4	72	1065.46	.80	3.46	5.51	18	225	258	259	36	141	102	16.0
3	76	1070.01	.84	3.61	0.08	20	229	258	259	36	141	102	16.0
3	80	1074.60	.85	3.65	4.68	20	229	257	259	36	140	102	15.5
2	84	1079.20	.83	3.56	9.23	21	229	257	259	37	140	101	15.5
2	88	1083.78	.82	3.52	3.74	21	229	257	259	37	139	101	15.5
1	92	1087.63	.60	2.58	7.61	20	229	257	259	38	138	101	15.5
1	96	1091.50	.61	2.62	1.51	18	229	256	259	38	138	101	15.5
	(2013)												
	$\theta = 96$	$V_m = 102.16$		$\Delta H = 3/10$							AVG. =	118	

AIR 7

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME ACS/MOOREHEAD METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH PULP DRYER STACK NO. OF TRAVERSE POINTS 12
 DATE 1-22-92 TEST 2 RUN 1 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac) ☒
 POSTTEST: 0.00 CFM AT 25 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED: 1165 RECOVERY SOLVENT(S):
☒ ACETONE
☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1
 SAMPLE RECOVERED BY: SB + DL

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1		} 200	
IMPINGER NO. 2	1184		984
IMPINGER NO. 3			
CONDENSER			
DESICCANT	1655	1341	341
TOTAL			1325

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 1
 BAG MATERIAL: TFDLAR SIZE: 44L
 PRETEST LEAK CHECK: 00 cc/MIN AT 15 IN. Hg
 TIME START: 1020 (HRS) TIME END: 1212 (HRS)
 SAMPLING RATE: 100 cc/MIN OPERATOR: SLB
 S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123828

PITOT NO. P1-6 Cp 840
 BAR. PRESS. 28.70 IN Hg H₂O 30 %
 NOZZLE NO. N1-4 NOZZLE DIA. 3/2 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME ACS / MOOREHEAD SOURCE SOUTH PULP DRYER STACK OPERATORS S. BARNWELL & D. C. HARRIS
 PROJECT NUMBER 920014 DATE 1-22-92 TEST 2 RUN 1 METER BOX NO. 1 $\Delta H = 1.35$ IN WC
 GASMETER COEFF. 1.001

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)						OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN	GAS/OUT		
	(1020)	(1092.13)												
B 6	4	1095.68	.58	2.45	5.78	5	225	247	255	42	84	85		16.0
6	8	1099.41	.58	2.97	9.46	6	226	248	255	42	124	88		16.0
5	12	1103.40	.64	2.83	3.47	8	227	248	255	42	133	91		16.0
5	16	1107.42	.64	2.85	7.51	8	229	248	255	42	138	92		16.0
4	20	1111.62	.68	3.04	1.70	11	230	248	255	42	144	95		16.0
4	24	1115.86	.68	3.06	5.92	11	231	245	254	47	145	98		15.5
3	28	1120.10	.67	3.02	0.12	12	231	245	254	47	142	98		15.5
3	32	1124.30	.67	3.03	4.32	12	231	245	254	47	146	100		15.5
2	36	1128.30	.61	2.76	8.35	13	231	245	254	47	147	102		15.5
2	40	1132.40	.63	2.87	2.45	12	227	245	254	46	148	103		15.0
1	44	1136.00	.47	2.15	6.01	10	227	245	255	47	148	104		15.0
1	48	1139.44	.44	2.02	9.46	10	227	245	255	47	148	105		15.0
A 6	52	1143.30	.56	2.55	3.34	13	230	245	255	47	145	106		14.7
6	56	1147.30	.57	2.61	7.26	14	227	245	254	47	143	106		15.0
5	60	1151.20	.59	2.69	1.24	15	227	245	254	47	145	106		15.0
5	64	1155.30	.64	2.93	5.77	20	225	245	254	47	146	106		14.5
4	68	1159.53	.66	3.03	9.61	20	225	245	254	47	148	107		14.0
4	72	1163.75	.65	2.98	3.80	20	226	245	255	46	150	108		14.5
3	76	1168.68	.68	3.12	8.10	21	228	244	255	46	150	108		14.8
3	80	1172.32	.68	3.13	2.40	21	225	244	255	46	150	109		14.5
2	84	1176.60	.66	3.03	6.44	20	228	246	255	46	150	109		14.0
2	88	1180.49	.67	3.08	0.90	20	228	246	256	46	150	109		15.5
1	92	1184.39	.45	2.07	4.41	20	228	246	256	45	150	109		15.5
1	96	1187.90	.46	2.12	2.95	19	228	246	255	45	150	109		15.5
	(1212)													
	$\theta = 96$	$V_m = 95.77$			$\Delta H = 2.75$						AVG. =	123		

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME ACS/MOD. HARP METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLAS
 SOURCE SOUTH PULP DRAPE STACK NO. OF TRAVERSE POINTS 12
 DATE 1-22-92 TEST 2 RUN 2 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒POSTTEST: 0.40 CFM AT 25 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED:

1158

RECOVERY SOLVENT(S):

☒ ACETONE☐ OTHER(S)NO. OF PROBE WASH BOTTLES: 1SAMPLE RECOVERED BY: S.L.B. + D.L.

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2	<u>1274</u>	<u>200</u>	<u>1074</u>
IMPINGER NO. 3			
CONDENSER			
DESICCANT			
	<u>1444</u>	<u>1363</u>	<u>86</u>
TOTAL			<u>1160</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 2BAG MATERIAL: TFDLAR SIZE: 44LTPRETEST LEAK CHECK: 00 cc/MIN AT 15 IN. HgTIME START: 1250 (HRS) TIME END: 1430 (HRS)SAMPLING RATE: 100 cc/MIN OPERATOR: SLBS/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123828PITOT NO. P1-6 Cp 840BAR. PRESS. 28.70 IN Hg H₂O 40 %NOZZLE NO. N1:4 NOZZLE DIA. .312 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME ACS / MOOREHEAD SOURCE SOUTH BOLD PLYMOUTH STAKE OPERATORS S. B. AND J. D. LITTON

PROJECT NUMBER 920014 DATE 1-22-92 TEST 2 RUN 2 METER BOX NO. () ΔH 1.75 IN WC

GAS METER COEFF. 1.00

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL. (cf)	VAC IN Hg	TEMPERATURE (° F)						OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN	GAS/OUT		
	(1250)	(1188.44)												
A 6	4	1191.64	.56	1.86	1.65	6	225	250	260	42	104	97		15.7
6	8	1194.94	.58	1.96	4.48	6	225	250	260	42	138	100		15.7
5	12	1198.58	.64	2.23	8.59	8	225	250	260	40	142	101		15.2
5	16	1202.10	.62	2.17	2.15	8	225	250	260	40	142	101		15.5
4	20	1205.73	.65	2.28	5.80	9	225	250	260	40	144	102		15.5
4	24	1209.40	.65	2.29	9.06	9	224	250	260	40	146	104		15.5
3	28	1213.22	.70	2.48	3.28	10	222	250	260	40	147	104		15.5
3	32	1217.00	.69	2.45	7.08	10	220	250	260	40	148	106		15.5
2	36	1220.70	.65	2.32	0.78	11	220	250	260	41	148	106		15.0
2	40	1224.43	.65	2.32	4.48	11	220	251	260	41	149	106		15.0
1	44	1227.65	.68	1.71	7.66	11	220	257	260	41	147	107		15.0
1	48	1230.80	.67	1.68	0.92	11	218	252	261	41	143	107		15.0
B 6	52	1234.17	.54	1.93	4.18	11	218	252	260	40	140	106		15.0
6	56	1237.56	.54	1.93	7.55	13	215	252	261	40	142	106		15.5
5	60	1241.15	.62	2.21	1.05	13	215	252	261	40	142	105		15.5
5	64	1244.75	.62	2.21	4.76	14	215	252	261	40	142	105		15.5
4	68	1248.40	.66	2.35	8.47	15	215	252	260	40	142	105		15.5
4	72	1252.15	.65	2.32	2.16	16	215	252	260	41	145	105		15.5
3	76	1255.88	.66	2.36	5.89	16	215	252	261	41	145	105		15.2
3	80	1259.60	.66	2.32	9.62	16	213	252	261	40	145	105		15.2
2	84	1263.25	.64	2.30	3.30	17	213	252	260	40	145	105		15.2
2	88	1266.50	.64	2.30	6.47	18	213	252	255	34	145	105		15.5
1	92	1270.10	.47	1.69	0.13	17	213	252	255	79	145	105		15.5
1	96	1273.30	.48	1.72	3.32	17	213	252	255	39	145	105		15.3
	(1430)													
	$\theta = 96$	$V_m = 84.86$		$\Delta H = 2.14$							AVG. =	127		

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME ACS/MOOREHEAD METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH PULP DRYER SPACE NO. OF TRAVERSE POINTS 12
 DATE 1-22-92 TEST 2 RUN 3 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒

POSTTEST: 0.00 CFM AT 25 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED:

RECOVERY SOLVENT(S):

1171

☒ ACETONE

☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: SB & PL

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2	<u>1218</u>	<u>200</u>	<u>1018</u>
IMPINGER NO. 3			
CONDENSER			
DESICCANT	<u>1519</u>	<u>1330</u>	<u>189</u>
TOTAL			<u>1207</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 3

BAG MATERIAL: TEDLAR SIZE: 4/6/CT

PRETEST LEAK CHECK: 00 cc/MIN AT 15 IN. Hg

TIME START: 1515 (HRS) TIME END: 1652 (HRS)

SAMPLING RATE: 100 cc/MIN OPERATOR: SCB

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123828

PITOT NO. P1-6 Cp 840

BAR. PRESS. 28.70 IN Hg H₂O 42 %

NOZZLE NO. N1-4 NOZZLE DIA. 3/32 IN.

PROJECT NAME ACS/MOORHEAD

PROJECT NAME ACS/MODR HEAD

SOURCE SOUTH POL? DRYER STACK

OPERATORS

OPERATORS S. B. WICKS + P. L. PFIN

PROJECT NUMBER 120014

PROJECT NUMBER 120014

DATE 1-22-92 TEST 2 RUN 3

METER BOX

METER BOX NO. 1 AHO 6.35- IN WC

GASMETER COEFF. 1.001

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL. (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
	(15/15)	1275.15											
B C	4	1278.40	.54	1.81	8.41	5	220	251	260	39	112	103	14.5
	8	1281.50	.54	1.76	1.58	5	220	252	260	39	139	104	14.5
	12	1285.10	.64	2.15	5.12	7	215	252	260	39	143	105	14.0
	16	1288.62	.64	2.16	8.64	8	215	252	260	39	143	105	14.0
	20	1292.28	.66	2.22	2.30	8	215	252	260	39	149	107	15.0
	24	1295.90	.66	2.21	8.91	9	225	252	260	39	149	107	15.0
	28	1299.54	.67	2.29	9.55	10	226	252	261	39	150	109	14.5
	32	1303.22	.67	2.25	3.20	10	222	252	260	39	152	109	14.7
	36	1306.96	.62	2.08	6.72	11	224	252	260	40	152	109	14.7
	40	1310.20	.62	2.09	0.75	11	222	252	260	40	152	110	14.7
	44	1313.35	.48	1.63	3.36	11	220	252	260	40	151	111	15.0
	48	1316.50	.48	1.63	6.47	10	220	252	260	40	151	111	15.0
A 6	52	1319.81	.55	1.86	9.80	10	220	252	260	40	151	110	15.0
	56	1323.15	.57	1.93	3.19	12	220	252	260	40	147	111	15.0
	60	1326.70	.62	2.09	6.71	17	220	252	260	40	148	111	15.0
	64	1330.28	.65	2.19	3.32	14	220	252	260	40	150	112	14.5
	68	1333.99	.66	2.23	3.96	15	220	252	260	40	150	111	14.5
	72	1337.66	.68	2.28	7.64	15	225	252	261	40	150	111	14.5
	76	1341.310	.70	2.32	1.39	18	220	251	261	41	151	112	14.0
	80	1345.10	.70	2.32	5.15	17	220	251	261	41	151	112	14.0
	84	1348.80	.67	2.27	8.82	18	220	251	261	41	151	112	14.0
	88	1352.52	.62	2.29	2.51	20	215	251	261	41	151	111	14.0
	92	1355.50	.43	1.47	5.47	18	215	251	260	40	151	112	14.5
	96	1359.44	.43	1.47	8.43	18	215	251	260	40	152	112	14.5
	(1652)												
	θ = 96	Vm = 83.29		ΔH = 201							AVG =	129	

AIR

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME ACS/MOORMEAD METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH PUMP DRYER STACK NO. OF TRAVERSE POINTS 12
 DATE _____ TEST _____ RUN _____ FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒

POSTTEST: 0.00 CFM AT 25 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED:

1175

RECOVERY SOLVENT(S):

☒ ACETONE _____

☐ OTHER(S) _____

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: SLB + D.L.

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2	<u>1335</u>	} <u>200</u>	<u>1175</u>
IMPINGER NO. 3			
CONDENSER			
DESICCANT	<u>1119</u>	<u>1330</u>	<u>89</u>
TOTAL			<u>1224</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 1

BAG MATERIAL: TEDLAR SIZE: 54 LT

PRETEST LEAK CHECK: 0.0 cc/MIN AT 15 IN. Hg

TIME START: 1005 (HRS) TIME END: 1145 (HRS)

SAMPLING RATE: 100 cc/MIN OPERATOR: SLB

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123828

PITOT NO. PI-6 Cp .840

BAR. PRESS. 28.68 IN Hg H₂O 40 %

NOZZLE NO. NI-4 NOZZLE DIA. 212 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME ACS / MOOREHEAD SOURCE SOUTH POLO DAYAN STAGE OPERATORS S. BARNUM & D. LITTON
 PROJECT NUMBER 926614 DATE 1-23-92 TEST 3 RUN (METER BOX NO. (ΔH 1.75 IN WC
 GAS METER COEFF. 1.001

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL. (cf)	VAC IN Hg	TEMPERATURE (° F)						OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN	GAS/OUT		
	(100s)	1359.56												
A 6	4	1362.44	.47	1.53	2.43	6	220	262	260	36	98	72	15.5	
	8	1365.35	.47	1.52	5.36	6	220	260	260	36	120	73	15.5	
5	12	1368.52	.54	1.83	8.56	8	220	251	255	38	120	78	15.5	
5	16	1371.71	.54	1.83	1.77	8	220	251	255	38	123	80	15.5	
4	20	1375.00	.56	1.91	5.06	10	220	250	255	38	125	90	15.5	
4	24	1378.38	.56	1.91	8.35	11	220	250	255	38	127	83	15.0	
3	28	1381.59	.53	1.82	1.57	12	220	250	255	38	128	85	15.0	
3	32	1384.72	.52	1.79	4.77	12	220	249	256	38	128	86	15.0	
2	26	1387.96	.50	1.73	7.91	12	218	248	256	38	129	87	15.0	
2	40	1391.10	.51	1.76	1.09	12	218	248	256	38	129	87	15.0	
1	44	1394.39	.33	1.83	4.33	12	218	248	256	38	129	90	15.0	
1	48	1396.52	.33	1.15	6.90	10	218	248	256	38	130	91	15.5	
B 6	52	1399.91	.45	1.57	9.90	12	215	250	256	38	130	91	15.5	
6	56	1402.42	.48	1.57	2.92	11	215	250	256	38	130	91	15.5	
5	60	1406.21	.53	1.85	6.18	11	215	250	256	38	130	91	15.5	
5	64	1409.46	.54	1.89	9.47	15	215	250	256	38	131	91	15.5	
4	68	1412.26	.54	1.89	2.77	15	215	250	264	38	130	92	15.5	
4	72	1416.17	.57	1.45	6.15	16	215	250	263	37	130	92	15.5	
3	76	1419.46	.55	1.92	9.48	16	215	250	263	37	132	93	15.5	
3	80	1422.88	.55	1.93	2.81	16	215	250	263	37	132	93	15.5	
2	84	1426.10	.53	1.86	6.08	16	215	250	261	77	132	93	15.0	
2	88	1429.38	.53	1.86	9.36	15	215	250	260	36	132	93	15.5	
1	92	1432.26	.40	1.41	2.21	14	214	251	260	36	133	93	15.5	
1	96	1435.00	.40	1.41	5.06	17	214	251	260	36	133	93	15.5	
	(114s)													
	$\Theta = 96$	$V_m = 75.44$		$\Delta H = 1.74$							AVG. = 107			
														AIR 7

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME ACS/MOONHEAD METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH PULP DRYER STACK NO. OF TRAVERSE POINTS 12
 DATE 1-23-92 TEST 3 RUN 2 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒

POSTTEST: 0.00 CFM AT 25 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED:

1176

RECOVERY SOLVENT(S):

☒ ACETONE

☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: SLB + DL.

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2	<u>1335</u>	<u>200</u>	<u>1135</u>
IMPINGER NO. 3			
CONDENSER			
DESICCANT	<u>1419</u>	<u>1330</u>	<u>89</u>
TOTAL			<u>1224</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 2

BAG MATERIAL: TEDLAR SIZE: 40 L

PRETEST LEAK CHECK: 00 cc/MIN AT 15 IN. Hg

TIME START: 1220 (HRS) TIME END: 1355 (HRS)

SAMPLING RATE: 100 cc/MIN OPERATOR: SLB

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123828

PITOT NO. P1-6 Cp 840

BAR. PRESS. 28.68 IN Hg H₂O 42 %

NOZZLE NO. N1-4 NOZZLE DIA. 3/16 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME ACS/MODEHEAD SOURCE SOUTH PULP DRYER STACK OPERATORS S. BAINBRIDGE & D. C. ITTIN
 PROJECT NUMBER 92004 DATE 1-23-92 TEST 3 RUN 2 METER BOX NO. 1 $\Delta H = 1.75$ IN WC
 GASMETER COEFF. 1.001

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL VOL (cf)	VAC IN Hg	TEMPERATURE (° F)				OXYGEN				
							STACK	PROBE	OVEN	IMPG.	GAS/IN	GAS/OUT	(% v/v)	(% v/v)	
	(1220)	(1435.60)													
B 6	4	1438.56	.47	1.55	8.58	6	210	241	250	38	100	83	15.5		
6	8	1441.46	.47	1.51	1.08	6	210	241	250	38	106	83	15.5		
5	12	1444.62	.54	1.74	4.60	8	210	241	250	38	115	83	15.5		
5	16	1447.77	.54	1.76	7.04	8	210	242	249	38	121	83	15.0		
4	20	1451.00	.58	1.80	1.02	9	210	242	249	39	123	85	15.0		
4	24	1454.30	.69	1.94	4.34	10	210	242	249	38	123	85	15.0		
3	28	1457.53	.55	1.80	7.54	10	210	241	249	38	125	84	15.5		
3	32	1460.72	.55	1.81	0.75	10	210	241	249	38	125	82	15.5		
2	36	1463.96	.53	1.75	3.91	10	210	241	249	38	127	87	14.7		
2	40	1467.10	.53	1.74	7.06	10	215	241	249	38	129	89	14.2		
1	44	1469.88	.42	1.38	9.87	12	215	242	250	38	130	90	14.7		
1	48	1472.66	.42	1.38	2.69	12	215	242	251	39	130	90	14.7		
A 6	52	1475.20	.48	1.58	5.71	12	215	243	251	39	130	91	15.0		
6	56	1478.73	.48	1.58	1.72	12	215	243	251	38	131	92	15.0		
5	60	1481.99	.54	1.78	1.93	13	215	244	250	39	131	91	15.0		
5	64	1485.10	.54	1.78	5.13	12	215	244	250	38	132	93	15.0		
4	68	1488.42	.56	1.85	8.40	11	215	244	250	39	135	93	15.0		
4	72	1491.70	.56	1.86	1.67	11	215	245	252	39	135	93	15.0		
3	76	1494.93	.53	1.76	4.86	16	215	245	252	38	131	94	15.0		
3	80	1498.10	.53	1.75	9.04	17	215	245	252	38	131	94	15.5		
2	84	1500.99	.45	1.49	0.97	17	215	246	252	38	132	94	15.5		
2	88	1503.92	.45	1.49	3.91	16	215	246	252	38	129	94	15.5		
1	92	1506.38	.32	1.06	6.38	15	215	246	252	32	129	94	15.5		
1	96	1508.95	.34	1.12	8.93	15	215	246	252	37	130	94	15.5		
	(1355)														
	$\theta = 96$	$V_m = 73.35$		$\Delta H = 1.64$							AVG. = 108				

AIR 7

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME ACS/MOGR HEAD METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH PULP DRYER STACK NO. OF TRAVERSE POINTS 12
 DATE 1-23-92 TEST 3 RUN 3 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒
 POSTTEST: 0.00 CFM AT 25 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED: 1179 RECOVERY SOLVENT(S):
☒ ACETONE
☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1
 SAMPLE RECOVERED BY: SLB + D.L.

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2	1236	200	1036
IMPINGER NO. 3			
CONDENSER			
DESICCANT	1327	1304	23
TOTAL			1059

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 3
 BAG MATERIAL: TEDLAR SIZE: 44 Lt
 PRETEST LEAK CHECK: 00 cc/MIN AT 15 IN. Hg
 TIME START: 1445 (HRS) TIME END: 1630 (HRS)
 SAMPLING RATE: 100 cc/MIN OPERATOR: SLB
 S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123828

PITOT NO. P1-6 Cp .840
 BAR. PRESS. 28.68 IN Hg H₂O 44 %
 NOZZLE NO. N1-4 NOZZLE DIA. .312 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A-35 (MOORHEAD) SOURCE SOUTH RIVER DAYTON STATION OPERATORS S. BARNETT & D. LITFEN
 PROJECT NUMBER 920014 DATE 1-23-92 TEST 3 RUN 3 METER BOX NO. 1 ΔH 0.75 IN WC
 GASMETER COEFF. 1.001

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
	(1445)	(509.40)											
A 6	4	1512.30	.48	1.49	2.32	6	210	249	250	38	99	81	15.5
6	8	1515.15	.48	1.45	5.16	9	210	249	250	38	99	81	15.5
5	12	1518.22	.55	1.68	8.21	8	200	250	255	38	109	89	15.5
5	16	1521.34	.55	1.71	1.31	10	200	250	255	38	113	88	15.5
4	20	1524.49	.56	1.74	4.45	10	200	250	255	40	115	90	15.5
4	24	1527.64	.56	1.75	7.61	10	200	250	255	40	121	92	15.0
3	28	1530.68	.53	1.67	0.69	10	200	250	255	40	130	92	15.0
3	32	1533.81	.53	1.68	3.81	10	205	251	255	40	134	93	15.0
2	36	1536.88	.52	1.65	6.84	11	205	251	255	40	134	93	15.0
2	40	1539.96	.52	1.65	9.99	12	205	251	255	41	134	93	15.0
1	44	1542.42	.32	1.01	2.40	10	205	251	255	41	134	94	15.5
1	48	1544.78	.31	.98	4.34	10	205	251	255	41	133	94	15.5
B 6	52	1547.70	.45	1.44	7.67	12	200	251	256	41	133	95	15.5
6	56	1550.62	.46	1.47	0.54	12	200	251	256	39	137	95	15.5
5	60	1553.80	.53	1.69	3.21	12	200	251	256	39	133	96	15.5
5	64	1556.88	.53	1.69	6.85	13	200	251	256	39	133	96	15.5
4	68	1560.10	.57	1.82	0.09	13	200	251	256	40	133	96	15.0
4	72	1563.22	.58	1.84	3.35	13	205	251	256	40	133	96	15.0
3	76	1566.52	.55	1.70	6.53	13	205	251	256	40	133	96	15.0
3	80	1569.78	.55	1.74	9.71	13	205	251	256	40	132	95	15.5
2	84	1572.73	.52	1.65	2.29	13	205	250	254	40	132	94	15.5
2	88	1575.14	.52	1.64	5.87	15	205	250	254	40	132	94	15.5
1	92	1578.76	.41	1.30	8.72	15	205	246	254	40	131	94	15.5
1	96	1581.40	.41	1.30	1.35	14	205	249	254	40	131	94	15.5
	(1630)												
	$\theta = 96$	$V_m = 72.00$		$\Delta H = 67$							AVG. =	110	

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME ACS/MOONHEAD METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH RIVER PLANT STAKE NO. OF TRAVERSE POINTS 12
 DATE 1-24-92 TEST 4 RUN 1 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒

POSTTEST: (0.00 CFM AT 25 IN. Hg (vac)) ☒

PARTICULATE CATCH DATA:

NO.S OF FILTERS USED:

1181

RECOVERY SOLVENT(S):

☒ ACETONE
☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: SLB & D.L.

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2	<u>1309</u>	<u>200</u>	<u>1109</u>
IMPINGER NO. 3			
CONDENSER			
DESICCANT	<u>1504</u>	<u>1382</u>	<u>122</u>
TOTAL			<u>1231</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 1

BAG MATERIAL: TEDLAR SIZE: 44 L

PRETEST LEAK CHECK: 00 cc/MIN AT 15 IN. Hg

TIME START: 1015 (HRS) TIME END: 1210 (HRS)

SAMPLING RATE: 100 cc/MIN OPERATOR: SLB

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123829

PITOT NO. 91-6 Cp 0.40

BAR. PRESS. 28.92 IN Hg H₂O 40 %

NOZZLE NO. PI-4 NOZZLE DIA. .312 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME ACS/maonHAP SOURCE South Pump Dayton Spill OPERATORS S. BAINBRIDGE J.D. LUTHER
 PROJECT NUMBER 920014 DATE 1-24-92 TEST 4 RUN 1 METER BOX NO. 1 ΔH 1.75 IN WC
 GASMETER COEFF. 1.001

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
	(1015)	(581.68)											
1A 6	4	584.90	.50	1.89	4.87	5	212	250	260	40	71	69	12.5
6	8	587.99	.47	1.78	7.94	6	203	250	260	40	82	71	12.5
5	12	591.30	.56	2.10	1.31	7	216	250	260	41	93	73	12.0
5	16	594.65	.54	2.07	4.67	9	210	250	260	41	102	74	11.0
4	20	598.19	.58	2.28	8.20	9	201	250	260	41	111	78	11.5
4	24	601.80	.59	2.35	1.81	11	199	251	260	41	115	80	11.5
2	28	605.45	.61	2.38	5.46	9	215	251	260	41	122	92	11.5
3	32	609.08	.61	2.37	9.11	14	225	251	260	41	124	85	12.5
2	36	612.60	.58	2.26	2.69	14	225	251	260	41	127	87	12.7
2	40	616.17	.56	2.19	6.22	14	225	252	260	40	131	88	12.5
1	44	619.18	.38	1.52	9.16	11	217	252	260	40	134	90	12.7
1	48	622.14	.39	1.54	2.44	11	228	252	261	40	135	91	12.7
B 6	52	625.58	.54	2.13	5.63	12	224	252	260	40	132	93	12.7
6	56	629.17	.53	2.17	9.16	13	203	252	261	40	134	95	13.0
5	60	632.99	.60	2.73	2.80	13	210	252	261	40	134	95	13.0
5	64	636.66	.59	2.39	6.61	13	210	252	261	40	133	95	13.0
4	68	640.30	.59	2.41	0.33	16	205	252	260	40	140	97	12.0
4	72	644.17	.61	2.53	4.16	16	199	252	260	41	141	48	12.0
3	76	648.00	.62	2.56	8.02	16	203	252	261	41	142	99	12.0
3	80	651.80	.62	2.58	1.89	16	199	252	261	41	142	100	12.0
2	84	655.53	.57	2.32	5.61	17	199	252	260	40	144	102	12.5
2	88	659.36	.58	2.43	9.38	17	198	252	260	40	144	103	12.5
1	92	662.50	.41	1.72	2.55	15	199	252	260	40	144	103	12.5
1	96	665.70	.41	1.72	5.22	15	199	251	260	40	144	103	12.5
	(1210)												
	$\theta = 96$	$V_m = 84.02$		$\Delta H = 2.17$							AVG. = 108		

AIR 7

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME AL5 (MOUNTAIN) METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH PLANTATION STAIR NO. OF TRAVERSE POINTS 12
 DATE 1-24-92 TEST 4 RUN 2 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒
 POSTTEST: (0.02 CFM AT 25 IN. Hg (vac)) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED: 1159 RECOVERY SOLVENT(S):
☒ ACETONE _____
☐ OTHER(S) _____

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: S.L.R. + D.L.

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2	<u>1390</u>	<u>200</u>	<u>1190</u>
IMPINGER NO. 3			
CONDENSER			
DESICCANT	<u>1380</u>	<u>1356</u>	<u>24</u>
TOTAL			<u>1214</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 2
 BAG MATERIAL: TEDLAR SIZE: 4A16
 PRETEST LEAK CHECK: 00 cc/MIN AT 15 IN. Hg
 TIME START: 1245 (HRS) TIME END: 1420 (HRS)
 SAMPLING RATE: 100 cc/MIN OPERATOR: SRB
 S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123828

PITOT NO. P1-6 Cp .840
 BAR. PRESS. 28.83 IN Hg H₂O 40 %
 NOZZLE NO. N1-4 NOZZLE DIA. .312 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME ACS/moan/ea2 SOURCE SDPH Pump Dwyer Stack OPERATORS S. BAINVILLE & D. SMITH
 PROJECT NUMBER 920014 DATE 1-24-92 TEST 4 RUN 2 METER BOX NO. 1 ΔH 1.75 IN WC
 GASMETER COEFF. 1.20

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
	(1245)	(666.03)											
B 6	4	664.22	.50	1.77	9.21	6	189	250	260	40	89	91	11.5
6	9	672.40	.54	1.85	2.42	7	194	251	261	39	90	93	11.5
5	12	675.80	.61	2.09	5.83	8	200	251	261	38	100	93	11.5
5	16	679.30	.60	2.04	9.24	8	200	251	261	38	106	95	11.5
4	20	682.73	.60	2.09	2.68	9	200	251	261	38	110	97	11.5
4	24	686.15	.60	2.10	6.12	10	200	252	261	37	112	97	11.0
3	28	689.60	.61	2.12	9.59	10	205	252	261	37	119	97	11.0
3	32	693.17	.62	2.19	3.13	11	194	252	261	37	120	94	11.0
2	36	696.60	.58	2.06	6.57	12	199	252	261	37	129	95	11.0
2	40	700.00	.58	2.07	0.02	12	194	252	261	37	132	96	11.0
1	44	702.46	.41	1.42	2.93	10	200	252	260	37	136	96	11.5
1	48	705.90	.41	1.47	5.86	11	200	251	260	37	140	97	12.0
A 6	52	709.20	.52	1.87	9.16	11	200	251	260	37	145	100	12.0
0	56	712.36	.48	1.73	2.35	12	205	251	260	37	145	100	12.0
5	60	715.88	.56	2.01	5.79	12	205	251	260	37	147	105	12.0
5	64	719.21	.55	1.99	4.22	12	205	251	260	37	147	106	11.5
4	68	722.79	.57	2.04	2.71	13	205	250	261	36	147	108	11.5
4	72	726.33	.60	2.18	6.30	13	205	250	261	36	147	108	11.5
3	76	729.88	.59	2.14	5.86	14	205	250	262	36	145	107	11.5
3	80	733.42	.58	2.10	3.38	15	205	250	262	36	145	107	11.5
2	84	736.88	.56	2.04	6.85	15	200	250	260	36	145	107	12.0
2	88	739.72	.77	1.35	9.68	15	200	250	259	36	145	107	12.0
1	92	742.62	.40	1.46	2.62	15	200	250	259	36	144	107	12.0
1	96	745.50	.38	1.39	5.48	14	200	250	259	36	144	107	12.0
	(1420)												
	θ = 96	Vm = 85.47		ΔH = 1.40							AVG = 115		

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME ACS/MOORHEAD METHOD 1-5
 PROJECT NUMBER 920064 FILTER HOLDER GLASS
 SOURCE SOUTH PUMP DRYER STACK NO. OF TRAVERSE POINTS 12
 DATE 1-24-92 TEST 4 RUN 2 FILTER TYPE GLASS FIDR2

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒

POSTTEST: 0.00 CFM AT 25 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO.S OF FILTERS USED:

1160

RECOVERY SOLVENT(S):

☒ ACETONE
☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: SLB + DS

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2	<u>1442</u>	<u>200</u>	<u>1242</u>
IMPINGER NO. 3			
CONDENSER			
DESICCANT	<u>1399</u>	<u>1384</u>	<u>15</u>
TOTAL			<u>1257</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. BP-1 BOX NO. BB-1 BAG NO. 3

BAG MATERIAL: TEDLAR SIZE: 44 L+

PRETEST LEAK CHECK: 00 cc/MIN AT 15 IN. Hg

TIME START: 1505 (HRS) TIME END: 1658 (HRS)

SAMPLING RATE: 100 cc/MIN OPERATOR: SLB

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: 123828

PITOT NO. P1-6 Cp .840

BAR. PRESS. 28.83 IN Hg H₂O 41 %

NOZZLE NO. N1-01 NOZZLE DIA. 3/2 IN.

OPERATORS S. BAINBRIDGE + D. LINDEN
METER BOX NO. 1 ΔH 1.75 IN WC
GAS METER COEFF. 1.00

PROJECT NAME ACS/MONOTHEAD SOURCE SOUTH PULP DRYER STACK
PROJECT NUMBER 920014 DATE 1-24-92 TEST 4 RUN 3

[illegible]

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD METHOD 1-5
PROJECT NUMBER 920014 FILTER HOLDER GLASS
SOURCE SOUTH DRYER MULTI-CLONE INLET NO. OF TRAVERSE POINTS 24
DATE 1-21-92 TEST 1 RUN 1 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒POSTTEST: 0.00 CFM AT 10 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO.S OF FILTERS USED:

RECOVERY SOLVENT(S):

1111☒ ACETONE☐ OTHER(S)NO. OF PROBE WASH BOTTLES: 1SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	<u>474</u>	<u>100</u>	<u>374</u>
DESICCANT	<u>1322</u>	<u>1288</u>	<u>34</u>
TOTAL			<u>408</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____

BAG MATERIAL: _____ SIZE: _____

PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg

TIME START: _____ (HRS) TIME END: _____ (HRS)

SAMPLING RATE: _____ cc/MIN OPERATOR: _____

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____PITOT NO. P1-8 Cp .840BAR. PRESS. 28.85 IN Hg H₂O 25 %NOZZLE NO. N2-5 NOZZLE DIA. .313 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A.C.S. Moorhead SOURCE S. DRIVER M.C. INLET OPERATORS D. SMITH / A. NELSON
 PROJECT NUMBER 920014 DATE 1-21-92 TEST 1 RUN 1 METER BOX NO. 2 ΔH 1.79 IN WC
 GASMETER COEFF. 1.0000

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL. (cf)	VAC IN Hg	TEMPERATURE (° F)				OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.		GAS/IN
(1315)												
A - 6	4	147.24	0.05	0.25	7.24	1	250	250	250	N/A	108	103
5	8	148.74	0.08	0.40	8.74	1	249				120	104
4	12	150.74	0.14	0.71	0.74	1	249	250	250		127	104
3	16	153.05	0.18	0.93	3.03	1	247				137	106
2	20	155.64	0.23	1.20	5.65	2	246	252	250		142	108
1	24	159.35	0.45	2.35	9.32	3	246				146	109
B - 6	28	160.55	0.05	0.26	0.55	1	248	250	250		139	112
5	32	162.37	0.11	0.58	2.37	1	248				139	112
4	36	164.52	0.15	0.78	4.50	1	249	249	250		143	112
3	40	167.28	0.26	1.36	7.30	2	249				148	113
2	44	170.66	0.37	1.95	0.66	3	248	250	251		154	114
1	48	174.57	0.50	2.64	4.58	4	247				158	115
C - 6	52	175.95	0.02	0.11	5.05	1	247	251	250		150	115
5	56	180.07	0.04	0.21	7.07	1	249				143	114
4	60	178.42	0.06	0.32	8.42	1	249	250	250		138	115
3	64	179.97	0.08	0.42	9.97	1	250				138	116
2	68	182.42	0.20	1.04	2.43	2	251	250	250		152	116
1	72	185.46	0.30	1.58	5.46	3	251				156	116
D - 6	76	186.25	0.02	0.11	6.25	1	252	250	249		130	115
5	80	187.34	0.04	0.21	7.34	1	253				136	114
4	84	188.99	0.09	0.47	8.99	1	251	251	249		146	114
3	88	190.55	0.08	0.42	0.55	1	249				146	114
2	92	192.47	0.12	0.63	2.47	2	248	251	250		152	115
1	96	195.08	0.22	1.17	5.08	3	246			V	158	116
(1500)												
θ = 96		Vm = 490.3	ΔH = 0.86								AVG. = 127.0	
AIR 7												

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD METHOD 1-5
PROJECT NUMBER 920014 FILTER HOLDER GLASS
SOURCE SOUTH DRYER MULTI-CLONE INLET NO. OF TRAVERSE POINTS 24
DATE 1-21-92 TEST 1 RUN 2 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒POSTTEST: (0.00 CFM AT 10 IN. Hg (vac)) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED:

RECOVERY SOLVENT(S):

1117☒ ACETONE☐ OTHER(S)NO. OF PROBE WASH BOTTLES: 1SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	<u>442</u>	<u>100</u>	<u>342</u>
DESICCANT	<u>1346</u>	<u>1300</u>	<u>46</u>
TOTAL			<u>388</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____

BAG MATERIAL: _____ SIZE: _____

PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg

TIME START: _____ (HRS) TIME END: _____ (HRS)

SAMPLING RATE: _____ cc/MIN OPERATOR: _____

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____PITOT NO. P1-8 Cp .840BAR. PRESS. 28.85 IN Hg H₂O 30 %NOZZLE NO. N2-5 NOZZLE DIA. .313 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A.C.S. Moorhead SOURCE SOUTH DRYER MULTI-CLONE INLET OPERATORS D. SMITH / A. NELSON
 PROJECT NUMBER 920014 DATE 1-21-92 TEST 1 RUN 2 METER BOX NO. 2 ΔH 1.79 IN WC
 GAS METER COEFF. 1.0000

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
	1600	195.25											
A - 6	4	196.42	0.05	0.23	6.41	1	250	248	249	N/A	104	103	
5	3	197.82	0.08	0.36	7.82	1	251				112	103	
4	12	199.77	0.15	0.68	9.76	1	250	250	251		121	103	
3	16	202.02	0.20	0.91	2.02	1	251				131	104	
2	20	204.41	0.22	1.01	4.41	1	249	251	250		139	106	
1	24	207.83	0.45	2.08	7.86	2	248				143	108	
B - 6	28	209.02	0.05	0.23	9.02	1	246	250	250		140	109	
5	32	210.65	0.10	0.47	0.66	1	247				134	110	
4	36	212.65	0.15	0.69	2.65	1	248	249	251		141	111	
3	40	215.24	0.25	1.17	5.24	2	247				150	112	
2	44	218.23	0.33	1.55	8.24	3	246	249	250		153	112	
1	48	221.98	0.51	2.40	1.98	4	246				158	115	
C - 6	52	222.72	0.02	0.10	2.72	1	246	250	250		125	114	
5	56	223.63	0.03	0.14	3.62	1	246				129	115	
4	60	224.88	0.06	0.28	4.88	1	246	250	250		136	114	
3	64	226.37	0.08	0.37	6.35	1	245				139	114	
2	68	228.55	0.10	0.84	8.55	2	245	251	250		147	114	
1	72	231.51	0.32	1.50	1.51	3	246				157	115	
D - 6	76	232.25	0.02	0.09	2.25	1	246	251	249		132	115	
5	80	233.41	0.05	0.23	3.41	1	246				138	115	
4	84	234.79	0.07	0.33	4.79	1	247	250	250		140	115	
3	88	236.26	0.09	0.37	6.26	1	248				142	115	
2	92	237.82	0.09	0.42	7.82	1	246	250	250		144	115	
1	96	240.27	0.23	1.06	0.27	2	245			✓	150	115	
	1742												
Σ = 96		V _m = 45.02		ΔH = 0.73							AVG. =	123.9	

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD METHOD 1-5
PROJECT NUMBER 920014 FILTER HOLDER GLASS
SOURCE SOUTH DRYER MULTI-CLONE INLET NO. OF TRAVERSE POINTS 24
DATE 1-21-92 TEST 1 RUN 3 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒
POSTTEST: 0.00 CFM AT 10 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED: # 1116 RECOVERY SOLVENT(S):
☒ ACETONE
☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	<u>444</u>	<u>100</u>	<u>344</u>
DESICCANT	<u>1358</u>	<u>1324</u>	<u>34</u>
TOTAL			<u>378</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____

BAG MATERIAL: _____ SIZE: _____

PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg

TIME START: _____ (HRS) TIME END: _____ (HRS)

SAMPLING RATE: _____ cc/MIN OPERATOR: _____

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____

PITOT NO. P1-8 Cp 840

BAR. PRESS. 28.85 IN Hg H₂O 31 %

NOZZLE NO. N2-5 NOZZLE DIA. 313 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A.C.S. McCRITCHEAD SOURCE SOUTH DRYER MULTI-CLONE INLET OPERATORS D. SMITH / A. NELSON
PROJECT NUMBER 920014 DATE 1-21-92 TEST 1 RUN 3 METER BOX NO. 2 ΔH₀ 1.79 IN WC
GASMETER COEFF. 1.0000

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)						OXYGEN (% v/v)
							STACK	PROBE	OVEN	IMPG.	GAS-IN	GAS-OUT	
A - 6	(1825) 4	241.59	0.05	0.23	1.59	1	250	247	248	N/A	118	105	
5	8	243.09	0.09	0.40	3.09	1	248				130	105	
4	12	244.97	0.14	0.63	4.98	1	246	249	250		136	107	
3	16	247.26	0.20	0.90	7.26	2	246				143	108	
2	20	249.80	0.25	1.14	9.82	2	246	250	251		148	109	
1	24	253.14	0.43	1.97	3.14	3	245				153	111	
B - 6	28	254.35	0.05	0.23	4.35	1	243	250	250		139	112	
5	32	255.96	0.10	0.46	5.97	1	244				138	112	
4	36	257.96	0.15	0.69	7.96	1	243	251	250		143	112	
3	40	260.55	0.25	1.15	0.54	2	243				150	113	
2	44	263.60	0.35	1.61	3.60	3	243	252	251		154	113	
1	48	267.14	0.48	2.21	7.14	4	245				160	115	
C - 6	52	267.93	0.02	0.09	7.93	1	245	251	250		135	115	
5	56	268.95	0.04	0.18	8.95	1	244				131	115	
4	60	270.10	0.05	0.23	0.10	1	244	250	250		134	114	
3	64	271.65	0.09	0.41	1.64	1	242				137	114	
2	68	273.88	0.19	0.87	3.88	2	243	250	249		145	114	
1	72	276.75	0.31	1.42	6.75	3	244				153	114	
D - 6	76	277.48	0.02	0.09	7.48	1	243	250	250		135	114	
5	80	278.63	0.05	0.23	8.63	1	242				132	114	
4	84	280.10	0.08	0.36	0.08	1	243	250	250		137	114	
3	88	281.63	0.09	0.41	1.62	1	244				141	114	
2	92	283.25	0.10	0.46	3.25	1	245	250	251		143	114	
1	96	285.67	0.22	1.01	5.67	2	244			V	150	114	
	(1802)									I			
	Ø = %	Vm= 45.22		ΔH= 0.72							AVG.=	126.6	

AJR 7

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. MoorHEAD METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH DRYER M.-C. INLET NO. OF TRAVERSE POINTS 24
 DATE 1-22-92 TEST 2 RUN 1 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒

POSTTEST: (0.00 CFM AT 10 IN. Hg (vac)) ☒

PARTICULATE CATCH DATA:

NO.S OF FILTERS USED:

RECOVERY SOLVENT(S):

1126

☒ ACETONE
☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	<u>481</u>	<u>100</u>	<u>381</u>
DESICCANT	<u>1525</u>	<u>1319</u>	<u>206</u>
TOTAL			<u>587</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____

BAG MATERIAL: _____ SIZE: _____

PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg

TIME START: _____ (HRS) TIME END: _____ (HRS)

SAMPLING RATE: _____ cc/MIN OPERATOR: _____

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____

PITOT NO. P1-8 Cp .840

BAR. PRESS. 28.70 IN Hg H₂O 30 %

NOZZLE NO. N2-5 NOZZLE DIA. .313 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A.C.S. MacRHEAD SOURCE SOUTH DRYER MULTI-GLASS INLET OPERATORS D. SMITH / A. NELSON
 PROJECT NUMBER 920014 DATE 1-22-92 TEST 2 RUN 1 METER BOX NO. 2 ΔH 1.79 IN WC
 GAS METER COEFF. 1.0000

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)				GAS/OUT	OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.			
	(1020)	(285.80)											
A - 6	4	286.91	0.05	0.22	6.92	1	244	250	251	N/A	104	98	
	8	288.24	0.07	0.32	8.24	1	244				109	98	
	12	289.91	0.11	0.50	9.91	1	244	250	250		115	99	
	16	291.80	0.14	0.64	1.80	1	245				123	100	
	20	294.58	0.30	1.37	4.58	2	245	251	250		136	101	
	24	298.13	0.48	2.22	8.13	3	245				142	103	
B - 6	28	299.19	0.04	0.19	9.17	1	245	252	250		135	105	
	32	300.44	0.06	0.28	0.44	1	245				132	107	
	36	302.44	0.15	0.70	2.44	1	243	251	249		134	107	
	40	305.25	0.30	1.40	5.27	2	243				148	108	
	44	308.58	0.40	1.88	8.58	3	243	251	249		155	110	
	48	312.30	0.50	2.37	2.30	4	243				159	112	
C - 6	52	313.05	0.02	0.10	3.05	1	244	250	250		140	114	
	56	314.22	0.05	0.24	4.22	1	242				134	114	
	60	315.50	0.06	0.28	5.50	1	242	250	250		139	114	
	64	317.53	0.15	0.71	7.53	1	242				143	114	
	68	319.94	0.21	1.00	9.94	1	242	250	250		153	114	
	72	323.19	0.38	1.81	3.19	2	241				159	116	
D - 6	76	324.70	0.08	0.39	4.70	1	241	250	251		145	116	
	80	326.28	0.09	0.43	6.29	1	241				146	116	
	84	327.95	0.10	0.48	7.95	1	243	249	257		148	117	
	88	329.79	0.12	0.57	9.79	1	243				150	117	
	92	331.84	0.15	0.72	1.84	1	241	250	250		151	117	
	96	334.92	0.34	1.62	4.92	3	241			V	155	117	
	(1200)												
	θ = 96	Vm = 49.12		ΔH = 0.85							AVG. = 124.8		

AIR 7

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. MOOREHEAD METHOD 1-5
PROJECT NUMBER 920014 FILTER HOLDER GLASS
SOURCE SOUTH DRYER MC. INLET NO. OF TRAVERSE POINTS 24
DATE 1-22-92 TEST 2 RUN 2 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒
POSTTEST: (0.00 CFM AT 10 IN. Hg (vac)) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED: #1100 RECOVERY SOLVENT(S):
☒ ACETONE
☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	<u>498</u>	<u>100</u>	<u>398</u>
DESICCANT	<u>1513</u>	<u>1334</u>	<u>179</u>
TOTAL			<u>577</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____

BAG MATERIAL: _____ SIZE: _____

PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg

TIME START: _____ (HRS) TIME END: _____ (HRS)

SAMPLING RATE: _____ cc/MIN OPERATOR: _____

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____

PITOT NO. P1-8 Cp .840

BAR. PRESS. 28.70 IN Hg H₂O 39 %

NOZZLE NO. A2-5 NOZZLE DIA. .313 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD SOURCE SOUTH DRYER M.C. INLET OPERATORS D. SMITH / A. NELSON
 PROJECT NUMBER 920014 DATE 1-22-92 TEST 2 RUN 2 METER BOX NO. 2 ΔH 1.79 IN WC
 GASMETER COEFF. 1.0000

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL. (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
	(1250)	(335.10)											
A - 6	4	336.14	0.05	0.19	6.14	1	243	247	249	N/A	111	109	
5	8	337.33	0.07	0.25	7.33	1	244				125	108	
4	12	338.78	0.10	0.37	8.78	1	242	249	251		132	109	
3	16	340.56	0.15	0.55	0.56	1	243				139	109	
2	20	343.10	0.30	1.11	3.10	2	244	250	250		147	110	
1	24	346.30	0.48	1.79	6.32	3	242				153	110	
B - 6	28	347.14	0.03	0.11	7.14	1	243	250	250		132	112	
5	32	348.17	0.05	0.19	8.17	1	241				120	111	
4	36	350.00	0.16	0.59	0.01	2	243	250	250		142	111	
3	40	352.47	0.28	1.04	2.47	3	243				151	111	
2	44	355.47	0.41	1.54	5.47	4	242	251	250		155	112	
1	48	358.75	0.49	1.85	8.75	4	242				157	113	
C - 6	52	359.42	0.02	0.08	9.42	1	243	251	250		130	112	
5	56	360.35	0.04	0.15	0.35	1	244				130	112	
4	60	366.47	0.06	0.22	1.47	1	244	250	249		135	112	
3	64	363.27	0.15	0.56	3.27	2	244				142	111	
2	68	365.49	0.23	0.86	5.49	3	243	250	250		148	111	
1	72	368.25	0.35	1.31	8.25	4	244				152	111	
D - 6	76	369.40	0.06	0.23	9.40	1	244	250	250		135	112	
5	80	370.71	0.08	0.30	0.71	1	244				133	112	
4	84	372.17	0.10	0.37	2.17	1	243	250	250		135	111	
3	88	373.78	0.12	0.45	3.78	1	241				138	110	
2	92	375.58	0.15	0.56	5.58	2	241	250	250		142	110	
1	96	378.29	0.34	1.27	8.29	3	239			V	149	110	
	(1430)												
	θ = 96	Vm = 43.19		ΔH = 0.66							AVG. =	125.0	

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. Moorhead METHOD 1-5
PROJECT NUMBER 920014 FILTER HOLDER GLASS
SOURCE SOUTH DRYER M.C. INLET NO. OF TRAVERSE POINTS 24
DATE 1-22-92 TEST 2 RUN 3 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒
POSTTEST: (0.00 CFM AT 10 IN. Hg (vac)) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED: # 1169 RECOVERY SOLVENT(S):
☒ ACETONE
☐ OTHER(S)
NO. OF PROBE WASH BOTTLES: 1
SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	507	100	407
DESICCANT	1460	1340	120
TOTAL			527

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____
BAG MATERIAL: _____ SIZE: _____
PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg
TIME START: _____ (HRS) TIME END: _____ (HRS)
SAMPLING RATE: _____ cc/MIN OPERATOR: _____
S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____

PITOT NO. P1-8 Cp .840
BAR. PRESS. 28.70 IN Hg H₂O 41 %
NOZZLE NO. N2-5 NOZZLE DIA. .313 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A.C.S. Moorhead SOURCE SMITH DRYER M.C. INLET OPERATORS D. Smith / A. Nelson
 PROJECT NUMBER 920014 DATE 1-22-92 TEST 2 RUN 3 METER BOX NO. 2 ΔH 1.79 IN WC
 GAS METER COEFF. 1.0000

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
	(1515)	(378.50)											
A - 6	4	379.40	0.04	0.14	9.40	1	247	247	246	N/A	107	105	
5	8	380.47	0.06	0.20	0.47	1	246				113	105	
4	12	381.98	0.12	0.41	1.98	1	246	249	250		122	106	
3	16	383.64	0.15	0.51	3.64	1	246				131	106	
2	20	386.05	0.28	0.97	6.05	2	245	250	250		141	110	
1	24	389.05	0.45	1.58	9.07	3	242				154	111	
B - 6	28	389.86	0.03	0.11	9.86	1	243	251	250		132	113	
5	32	390.87	0.05	0.17	0.87	1	244				133	115	
4	36	392.42	0.12	0.42	2.42	1	243	250	251		145	115	
3	40	394.90	0.30	1.06	4.91	2	243				153	116	
2	44	397.73	0.38	1.35	7.73	3	243	250	250		159	117	
1	48	401.01	0.51	1.82	1.01	4	243				163	119	
C - 6	52	401.82	0.03	0.11	1.82	1	243	250	250		134	120	
5	56	402.83	0.05	0.18	2.83	1	242				137	120	
4	60	403.94	0.06	0.21	3.94	1	242	251	250		141	121	
3	64	405.59	0.13	0.46	5.59	2	240				144	120	
2	68	407.63	0.20	0.71	7.63	2	240	251	250		149	120	
1	72	410.34	0.35	1.25	0.34	3	240				156	120	
D - 6	76	411.57	0.07	0.25	1.57	1	240	250	250		143	119	
5	80	412.94	0.09	0.32	2.94	1	241				141	119	
4	84	414.45	0.11	0.39	4.44	1	243	250	250		143	118	
3	88	416.02	0.12	0.43	6.02	2	242				143	117	
2	92	417.84	0.16	0.57	7.84	2	241	250	250		147	117	
1	96	420.42	0.32	1.14	0.42	3	242			V	153	117	
	(1655)												
	θ = 96	Vm = 41.92		ΔH =							AVG. =		

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. Moorhead METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH DRYER M.C. INLET NO. OF TRAVERSE POINTS 24
 DATE 1-23-92 TEST 3 RUN 1 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac) ☒
 POSTTEST: (0.00 CFM AT 10 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO.S OF FILTERS USED: # 1174 RECOVERY SOLVENT(S):
☒ ACETONE
☐ OTHER(S) 1

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	<u>516</u>	<u>100</u>	<u>416</u>
DESICCANT	<u>1465</u>	<u>1340</u>	<u>125</u>
TOTAL			<u>541</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____

BAG MATERIAL: _____ SIZE: _____

PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg

TIME START: _____ (HRS) TIME END: _____ (HRS)

SAMPLING RATE: _____ cc/MIN OPERATOR: _____

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____

PITOT NO. P1-8 Cp .840

BAR. PRESS. 28.68 IN Hg H₂O 40 %

NOZZLE NO. N2-5 NOZZLE DIA. .313 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A.C.S. MACHHEAD SOURCE SOUTH DRYER M.C. INLET OPERATORS D-SMITH/A. NELSON
 PROJECT NUMBER 920014 DATE 1-23-92 TEST 3 RUN 1 METER BOX NO. 2 ΔH 1.79 IN WC
 GASMETER COEFF. 1.0000

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
	(0945)	(420.50)											
A - 6	4	421.24	0.03	0.10	1.24	1	249	250	250	N/A	84	83	
5	8	422.18	0.05	0.17	2.18	1	248				90	84	
4	12	423.37	0.08	0.27	3.39	1	246	250	250		98	84	
3	16	424.75	0.10	0.34	4.75	1	245				106	85	
2	20	426.96	0.26	0.89	6.96	2	247	250	250		116	87	
1	24	429.55	0.35	1.21	9.55	3	245				124	89	
B - 6	28	430.25	0.03	0.10	0.25	1	245	250	250		110	90	
5	32	431.32	0.06	0.21	1.32	1	244				117	92	
4	36	433.30	0.20	0.70	3.30	2	243	251	250		126	92	
3	40	435.55	0.26	0.91	5.56	2	244				129	93	
2	44	438.20	0.35	1.23	8.20	3	243	251	249		132	95	
1	48	441.57	0.48	1.84	1.57	4	243				136	95	
C - 6	52	442.35	0.03	0.11	2.35	1	243	250	248		114	97	
5	56	443.43	0.06	0.21	3.43	1	242				118	97	
4	60	444.69	0.08	0.28	4.69	1	241	250	249		120	97	
3	64	446.23	0.12	0.42	6.23	1	242				123	97	
2	68	448.02	0.16	0.56	8.02	1	242	250	250		129	97	
1	72	450.62	0.34	1.20	0.62	3	244				135	97	
D - 6	76	451.26	0.02	0.07	1.26	1	240	250	250		115	98	
5	80	452.15	0.04	0.14	2.15	1	240				112	98	
4	84	453.32	0.07	0.25	3.32	1	241	249	250		118	97	
3	88	454.58	0.08	0.28	4.58	1	241				122	97	
2	92	456.12	0.12	0.42	6.12	1	243	250	250		126	97	
1	96	458.40	0.26	0.91	8.40	2	245			V	135	98	
	(1130)												
	θ = 96	V _m = 3790		ΔH = 0.53							AVG. =	105.6	

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. Moorhead METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH DRYER M-C. INLET NO. OF TRAVERSE POINTS 24
 DATE 1-23-92 TEST 3 RUN 2 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒
 POSTTEST: (0.00 CFM AT 10 IN. Hg (vac)) ☒

PARTICULATE CATCH DATA:

NO.S OF FILTERS USED: # 1168 RECOVERY SOLVENT(S):
☒ ACETONE _____
☐ OTHER(S) 1 _____
 NO. OF PROBE WASH BOTTLES: _____
 SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	<u>523</u>	<u>100</u>	<u>423</u>
DESICCANT	<u>1474</u>	<u>1334</u>	<u>140</u>
TOTAL			<u>563</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____
 BAG MATERIAL: _____ SIZE: _____
 PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg
 TIME START: _____ (HRS) TIME END: _____ (HRS)
 SAMPLING RATE: _____ cc/MIN OPERATOR: _____
 S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____

PITOT NO. P1-8 Cp .840
 BAR. PRESS. 28.68 IN Hg H₂O 42 %
 NOZZLE NO. N2-5 NOZZLE DIA. .313 IN.

OPERATORS D. SMITH / A. NELSON
METER BOX NO. 2 ΔH 1.79 IN WC
GASMETER COEFF. 1.0000

PROJECT NAME A.C.S. MOORHEAD SOURCE SOUTH DRIVER M.C. INLET
PROJECT NUMBER 920014 DATE 1-23-92 TEST 3 RUN 2

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)				OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.		GAS/IN
	(1220)	(458.60)										
A - 6	4	459.34	0.03	0.10	9.84	1	244	250	N/A	90	86	
	8	460.28	0.05	0.16	0.28	1	244			94	86	
4	12	461.53	0.09	0.29	1.53	1	244	250		102	86	
3	16	462.92	0.11	0.35	2.92	1	246			110	87	
2	20	465.00	0.24	0.78	5.00	2	245	250		118	88	
1	24	467.56	0.36	1.18	7.56	3	243			126	90	
B - 6	28	468.31	0.03	0.10	8.31	1	241	250		110	92	
5	32	469.66	0.10	0.33	9.66	1	242			116	93	
4	36	471.32	0.15	0.49	1.32	1	243	250		119	93	
3	40	473.47	0.25	0.83	3.47	2	241			128	94	
2	44	476.05	0.36	1.20	6.07	3	242	250		135	95	
1	48	479.09	0.48	1.61	9.09	4	242			138	96	
C - 6	52	479.70	0.02	0.07	9.71	1	242	250		112	98	
5	56	480.67	0.05	0.16	0.67	1	242			115	98	
4	60	481.96	0.09	0.30	1.96	1	242	250		123	98	
3	64	483.33	0.10	0.33	3.33	1	241			125	98	
2	68	485.18	0.18	0.60	5.18	2	242	250		132	98	
1	72	487.75	0.35	1.17	7.75	3	244			137	99	
D - 6	76	488.38	0.02	0.07	8.38	1	246	250		112	100	
5	80	489.12	0.03	0.10	9.12	1	245			113	100	
4	84	490.08	0.05	0.16	0.08	1	244	250		116	100	
3	88	491.38	0.09	0.30	1.38	1	244			120	99	
2	92	492.87	0.12	0.40	2.87	1	245	250		128	99	
1	96	495.05	0.25	0.83	5.05	3	245		V	135	99	
	(1400)											
	θ=96	Vm= 36.45		ΔH=0.50						AVG=	106.8	

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH DRYER M.C. INLET NO. OF TRAVERSE POINTS 24
 DATE 1-23-92 TEST 3 RUN 3 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒

POSTTEST: 0.00 CFM AT 10 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO.S OF FILTERS USED:

RECOVERY SOLVENT(S):

1161

☒ ACETONE
☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	<u>524</u>	<u>100</u>	<u>424</u>
DESICCANT	<u>1439</u>	<u>1341</u>	<u>98</u>
TOTAL			<u>522</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____

BAG MATERIAL: _____ SIZE: _____

PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg

TIME START: _____ (HRS) TIME END: _____ (HRS)

SAMPLING RATE: _____ cc/MIN OPERATOR: _____

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____

PITOT NO. P1-8 Cp 840

BAR. PRESS. 28.68 IN Hg H₂O 43 %

NOZZLE NO. N2-5 NOZZLE DIA. 313 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD SOURCE SOUTH DRYER M.C. FINEST OPERATORS D. SMITH / A. NELSON
 PROJECT NUMBER 920014 DATE 1-23-92 TEST 3 RUN 3 METER BOX NO. 2 ΔH 1.79 IN WC
 GAS METER COEFF. 1.0000

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL. (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
	(1450)	(495.20)											
A - 6	4	495.80	0.02	0.06	5.80	1	243	250	250	N/A	90	88	
5	8	496.81	0.06	0.19	6.81	1	242				95	88	
4	12	497.98	0.08	0.25	7.98	1	242	250	250		103	88	
3	16	499.36	0.01	0.35	9.36	1	243				112	89	
2	20	501.41	0.24	0.76	1.41	2	244	250	250		121	89	
1	24	503.83	0.33	1.05	3.83	3	245				127	90	
B - 6	28	504.57	0.03	0.10	4.57	1	245	250	250		112	92	
5	32	505.75	0.08	0.25	5.75	1	245				116	93	
4	36	507.39	0.15	0.48	7.39	1	245	250	250		126	96	
3	40	509.64	0.28	0.90	9.64	2	245				134	97	
2	44	512.25	0.37	1.20	2.25	3	245	250	250		137	98	
1	48	515.17	0.46	1.49	5.17	4	248				140	99	
C - 6	52	515.92	0.03	0.10	5.92	1	246	250	250		114	100	
5	56	516.96	0.06	0.19	6.96	1	244				119	100	
4	60	518.24	0.09	0.29	8.24	1	243	250	250		124	100	
3	64	519.65	0.11	0.35	9.65	1	246				128	101	
2	68	521.58	0.20	0.65	1.58	2	243	250	250		132	101	
1	72	524.09	0.34	1.11	4.09	3	242				139	101	
D - 6	76	524.84	0.03	0.10	4.84	1	243	250	250		115	102	
5	80	525.69	0.04	0.13	5.69	1	244				117	101	
4	84	526.73	0.06	0.19	6.73	1	244	250	250		120	101	
3	88	528.02	0.09	0.29	8.02	1	242				123	101	
2	92	529.50	0.12	0.39	9.50	1	243	250	250		126	101	
1	96	531.60	0.24	0.78	1.60	2	243			✓	132	101	
	(1640)												
	θ = 96	Vm = 36.40		ΔH = 0.48							AVG. =	108.7	

$\Delta H = 0.48$

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD METHOD 1-5
PROJECT NUMBER 920014 FILTER HOLDER GLASS
SOURCE SOUTH DRYER M.C. INLET NO. OF TRAVERSE POINTS 24
DATE 1-24-92 TEST 4 RUN 1 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒POSTTEST: (0.00 CFM AT 10 IN. Hg (vac)) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED:

1162

RECOVERY SOLVENT(S):

☒ ACETONE☐ OTHER(S)NO. OF PROBE WASH BOTTLES: 1SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	<u>513</u>	<u>100</u>	<u>413</u>
DESICCANT	<u>1593</u>	<u>1370</u>	<u>223</u>
TOTAL			<u>636</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____

BAG MATERIAL: _____ SIZE: _____

PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg

TIME START: _____ (HRS) TIME END: _____ (HRS)

SAMPLING RATE: _____ cc/MIN OPERATOR: _____

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____PITOT NO. P1-8 Cp .840BAR. PRESS. 28.83 IN Hg H₂O 35 %NOZZLE NO. N2- NOZZLE DIA. .313 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD SOURCE SOUTH DRYER M.C. INLET OPERATORS D. SMITH / A. NELSON
 PROJECT NUMBER 920014 DATE 1-24-92 TEST 4 RUN 1 METER BOX NO. 2 ΔH 1.79 IN WC
 GAS METER COEFF. 1.0000

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL. (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL. (cf)	VAC IN Hg	TEMPERATURE (° F)				OXYGEN		
							STACK	PROBE	OVEN	IMPG.	GAS/IN	GAS/OUT	(% v/v)
(1015)													
A - 6	4	532.89	0.06	0.24	2.89	1	245	250	N/A	96	91		
5	8	534.27	0.09	0.35	4.27	1	245			104	91		
4	12	535.80	0.11	0.43	5.81	1	246	250		113	92		
3	16	537.63	0.15	0.59	7.63	1	247			121	93		
2	20	540.13	0.28	1.12	0.13	2	247	250		129	95		
1	24	543.13	0.40	1.61	3.13	3	247			137	97		
B - 6	28	544.21	0.05	0.20	4.21	1	249	250		115	100		
5	32	545.62	0.09	0.36	5.62	1	249			127	101		
4	36	547.41	0.14	0.56	7.41	1	249	250		132	101		
3	40	550.04	0.30	1.22	0.04	2	247			141	103		
2	44	553.10	0.40	1.64	3.10	3	247	250		145	104		
1	48	556.35	0.45	1.85	6.35	4	247			148	105		
C - 6	52	557.33	0.04	0.17	2.33	1	247	250		123	106		
5	56	558.50	0.06	0.24	8.50	1	248			130	106		
4	60	560.03	0.10	0.41	0.03	1	248	250		134	106		
3	64	561.90	0.15	0.61	1.90	1	246			138	106		
2	68	564.18	0.22	0.90	4.18	2	245	250		143	106		
1	72	567.47	0.46	1.89	7.47	4	245			149	107		
D - 6	76	568.77	0.07	0.29	8.77	1	246	250		125	107		
5	80	570.21	0.09	0.37	0.21	1	246			135	108		
4	84	571.75	0.10	0.41	1.75	1	246	250		138	108		
3	88	573.36	0.11	0.45	3.36	1	246			140	108		
2	92	575.48	0.19	0.78	5.48	2	245	250		144	108		
1	96	577.42	0.25	1.03	7.42	3	245		✓	147	108		
(1200)													
	θ = 96	Vm = 46.17		ΔH = 0.74						AVG. = 116.9			
AIR 7													

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. Moorhead METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH DRYER M.C. INLET NO. OF TRAVERSE POINTS 24
 DATE 1-24-92 TEST 4 RUN 2 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒

POSTTEST: 0.00 CFM AT 10 IN. Hg (vac) ☒

PARTICULATE CATCH DATA:

NO. OF FILTERS USED:

1167

RECOVERY SOLVENT(S):

☒ ACETONE

☐ OTHER(S)

NO. OF PROBE WASH BOTTLES: 1

SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	<u>671</u>	<u>100</u>	<u>571</u>
DESICCANT	<u>1384</u>	<u>1362</u>	<u>22</u>
TOTAL			<u>593</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____

BAG MATERIAL: _____ SIZE: _____

PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg

TIME START: _____ (HRS) TIME END: _____ (HRS)

SAMPLING RATE: _____ cc/MIN OPERATOR: _____

S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____

PITOT NO. P1-8 Cp .840

BAR. PRESS. 28.83 IN. Hg H₂O 42 %

NOZZLE NO. N2-5 NOZZLE DIA. .313 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A.C.S. MEERHEAD SOURCE SOUTH DRYER M.C. INLET OPERATORS D. SMITH / A. NELSON
 PROJECT NUMBER 920014 DATE 1-24-92 TEST 4 RUN 2 METER BOX NO. 2 ΔH 1.79 IN WC
 GAS METER COEFF. 1.0000

TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (° F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
A - 6	(1245)	(578.10)											
	4	578.97	0.04	0.13	8.97	1	246	250	250	N/A	101	98	
	5	580.17	0.08	0.26	0.17	1	245				108	98	
	4	581.52	0.10	0.33	1.52	1	246	250	250		118	98	
	3	583.13	0.14	0.46	3.13	1	246				124	99	
B - 6	2	585.41	0.28	0.93	5.41	2	243	250	250		132	100	
	1	588.24	0.42	1.41	8.24	3	242				135	101	
	28	589.22	0.05	0.17	9.22	1	243	250	250		129	102	
	32	590.59	0.10	0.33	0.59	1	242				125	102	
	4	592.10	0.12	0.40	2.10	1	243	250	250		129	103	
C - 6	3	594.36	0.27	0.91	4.36	2	243				136	105	
	2	597.07	0.38	1.28	7.07	3	242	250	250		144	107	
	1	600.01	0.44	1.50	0.01	4	243				149	109	
	52	600.78	0.03	0.10	0.78	1	244	250	250		125	108	
	5	601.93	0.07	0.23	1.93	1	245				122	110	
	4	603.32	0.10	0.34	3.32	1	245	250	250		135	110	
	3	605.03	0.15	0.51	5.03	1	243				139	110	
	2	607.06	0.21	0.71	7.06	2	244	250	250		143	110	
	1	610.03	0.45	1.53	0.03	4	243				148	111	
	D - 6	76	611.13	0.06	0.21	1.13	1	243	250	250		130	111
	5	612.37	0.08	0.27	2.37	1	245				133	111	
	4	613.83	0.11	0.37	3.83	1	245	250	250		136	111	
	3	615.30	0.11	0.37	5.30	1	246				140	111	
	2	617.23	0.19	0.64	7.23	2	247	250	250		144	111	
	1	619.40	0.24	0.82	9.40	3	246			4	148	112	
(1426)													
θ = 96		Vm = 41.30		ΔH = 0.59							AVG = 119.2		

EPA METHOD 3/4/5 FIELD DATA

PROJECT NAME A.C.S. MOORHEAD METHOD 1-5
 PROJECT NUMBER 920014 FILTER HOLDER GLASS
 SOURCE SOUTH DRYER NO. OF TRAVERSE POINTS 24
 DATE 1-24-92 TEST 4 RUN 3 FILTER TYPE GLASS FIBER

SAMPLE TRAIN LEAK CHECK:

PRETEST: (≤ 0.02 CFM AT 15 IN. Hg (vac)) ☒
 POSTTEST: (0.00 CFM AT 10 IN. Hg (vac)) ☒

PARTICULATE CATCH DATA:

NO.S OF FILTERS USED: #1164 RECOVERY SOLVENT(S):
☒ ACETONE _____
☐ OTHER(S) _____
 NO. OF PROBE WASH BOTTLES: 1
 SAMPLE RECOVERED BY: D. SMITH

CONDENSATE DATA:

ITEM	WEIGHT (g)		
	FINAL	TARE	DIFFERENCE
IMPINGER NO. 1			
IMPINGER NO. 2			
IMPINGER NO. 3			
CONDENSER	<u>663</u>	<u>100</u>	<u>563</u>
DESICCANT	<u>1382</u>	<u>1352</u>	<u>30</u>
TOTAL			<u>593</u>

INTEGRATED GAS SAMPLING DATA:

BAG PUMP NO. _____ BOX NO. _____ BAG NO. _____
 BAG MATERIAL: _____ SIZE: _____
 PRETEST LEAK CHECK: _____ cc/MIN AT _____ IN. Hg
 TIME START: _____ (HRS) TIME END: _____ (HRS)
 SAMPLING RATE: _____ cc/MIN OPERATOR: _____
 S/N OF O₂ ANALYZER USED TO MONITOR TRAIN OUTLET: _____

PITOT NO. P1-8 Cp 840
 BAR. PRESS. 28.83 IN Hg H₂O 43 %
 NOZZLE NO. N2-5 NOZZLE DIA. 3/32 IN.

EPA METHOD 5 FIELD DATA

PROJECT NAME A-C-S MORTHEAD SOURCE SOUTH DRYER M.C. INLET OPERATORS D-SMITH/A. NELSON
 PROJECT NUMBER 920014 DATE 1-24-92 TEST 4 RUN 3 METER BOX NO. 2 ΔH 1.79 IN WC
 GAS METER COEFF. 1.0000

GASMETER COEFF. 1.0000													
TRAVERSE POINT NO.	SAMPLING TIME (MIN.)	SAMPLE VOL (cf)	VELOCITY HEAD (IN WC)	ORIFICE METER (IN WC)	DES. VOL (cf)	VAC IN Hg	TEMPERATURE (°F)					OXYGEN (% v/v)	
							STACK	PROBE	OVEN	IMPG.	GAS/IN		GAS/OUT
A - 6	(1505)	619.55											
5	4	620.51	0.05	0.16	0.51	1	249	250	250	N/A	106	101	
4	8	621.70	0.08	0.25	1.70	1	250				113	101	
3	12	623.10	0.11	0.35	3.10	1	247	250	250		121	102	
2	16	624.75	0.15	0.48	4.75	1	246				129	103	
1	20	626.93	0.26	0.84	6.93	2	246	250	250		137	104	
B - 6	24	629.63	0.39	1.27	9.63	3	246				143	106	
5	28	630.50	0.04	0.13	0.50	1	248	250	250		130	107	
4	32	631.79	0.09	0.29	1.79	1	248				134	108	
3	36	633.58	0.17	0.56	3.58	1	244	250	250		139	109	
2	40	636.00	0.31	0.02	6.00	2	244				146	110	
1	44	638.69	0.38	1.26	8.69	3	246	250	250		150	111	
C - 6	48	641.63	0.45	1.49	1.63	4	247				154	111	
5	52	642.52	0.04	0.13	2.52	1	247	250	250		130	112	
4	56	643.66	0.07	0.23	3.66	1	245				134	114	
3	60	645.04	0.10	0.33	5.04	1	247	250	250		139	114	
2	64	646.67	0.14	0.46	6.67	1	250				142	114	
1	68	648.72	0.22	0.73	8.72	2	248	250	250		149	114	
D - 6	72	651.75	0.48	1.59	1.75	4	250				155	114	
5	76	652.92	0.07	0.23	2.92	1	250	250	250		135	114	
4	80	654.15	0.08	0.26	4.15	1	250				139	115	
3	84	655.46	0.09	0.30	5.46	1	248	250	250		141	115	
2	88	656.98	0.12	0.40	6.98	1	248				144	115	
1	92	658.99	0.21	0.69	8.99	2	249	250	250	↓	149	115	
	96	661.19	0.25	0.83	1.19	3	249				154	115	
	(1645)												
θ = 96		Vm = 41.64		ΔH = 0.60							AVG. =	124.1	

BAY WEST STACK SAMPLING
E.P.A. METHOD 3 ANALYSIS

JOB# 920014 DATE OF ANALYSIS 1-21-92
 SOURCE SOUTH PULP DRYER LEAK CHECK PERFORMED YFS
 SITE STACK / MULTI COMPONENT TECHNICIAN SLB
 CITY/STATE ROCKFORD, MN TYPE OF FUEL COAL

TEST/ RUN	READING NO.	BURET READING			CONCENTRATION (%v/v, dry)		F ₀
		ZERO POINT	AFTER CO 2	AFTER O 2	CO ₂	O ₂	
AMBIENT AIR		0.00	0.00	20.90	0.00	20.90	1.1565
1	1	0.00	4.12	20.12	4.12	16.00	1.19
	2	0.00	4.12	20.12	4.12	16.00	1.19
	3	0.00	4.12	20.12	4.12	16.00	1.19
2	1	0.00	4.08	19.58	4.08	15.50	1.13
	2	0.00	4.08	19.58	4.08	15.50	1.13
	3	0.00	4.08	19.58	4.08	15.50	1.13
3	1	0.00	4.11	19.36	4.11	15.25	1.16
	2	0.00	4.11	19.36	4.11	15.25	1.16
	3	0.00	4.11	19.36	4.11	15.25	1.16

CO₂

AVERAGE RUN 1 4.12

AVERAGE RUN 2 4.08

AVERAGE RUN 3 4.11

O₂

AVERAGE RUN 1 16.00

AVERAGE RUN 2 15.50

AVERAGE RUN 3 15.25

F₀

AVERAGE RUN 1 1.19

AVERAGE RUN 2 1.13

AVERAGE RUN 3 1.16

BAY WEST STACK SAMPLING
E.P.A. METHOD 3 ANALYSIS

JOB# 920014 DATE OF ANALYSIS 1-22-92
 SOURCE SOUTHERN PULP & PAPER LEAK CHECK PERFORMED YES
 SITE STACK / MULTIPLE CONFINEMENT TECHNICIAN SCB
 CITY/STATE MOOREHEAD, MS TYPE OF FUEL COAL

TEST/ RUN	READING NO.	BURET READING			CONCENTRATION (%v/v, dry)		F _o
		ZERO POINT	AFTER CO 2	AFTER O2	CO ₂	O ₂	
AMBIENT AIR		0.00	0.00	20.90	0.00	20.90	11565
2 1	1	0.00	5.50	20.25	5.50	14.75	1.12
	2	0.00	5.50	20.25	5.50	14.75	1.12
	3	0.00	5.50	20.25	5.50	14.75	1.12
2 2	1	0.00	6.00	20.25	6.00	14.25	1.11
	2	0.00	6.00	20.25	6.00	14.25	1.11
	3	0.00	6.00	20.25	6.00	14.25	1.11
2 3	1	0.00	5.20	20.30	5.20	15.10	1.12
	2	0.00	5.20	20.30	5.20	15.10	1.12
	3	0.00	5.20	20.30	5.20	15.10	1.12

CO₂

O₂

F_o

AVERAGE RUN 1 5.50

AVERAGE RUN 1 14.75

AVERAGE RUN 1 1.12

AVERAGE RUN 2 6.00

AVERAGE RUN 2 14.25

AVERAGE RUN 2 1.11

AVERAGE RUN 3 5.20

AVERAGE RUN 3 15.10

AVERAGE RUN 3 1.12

BAY WEST STACK SAMPLING
E.P.A. METHOD 3 ANALYSIS

JOB# 920014 DATE OF ANALYSIS 1-23-97
SOURCE SOUTH PUMP DRYER LEAK CHECK PERFORMED YES
SITE STACK / MULTI-COMER INLET TECHNICIAN SCB
CITY/STATE BRANDENBURG, MS TYPE OF FUEL COAL

TEST/ RUN	READING NO.	BURET READING			CONCENTRATION (%v/v,dry)		F ₀
		ZERO POINT	AFTER CO ₂	AFTER O ₂	CO ₂	O ₂	
AMBIENT AIR		0.00	0.00	20.90	0.00	20.90	1.1565
3 1	1	0.00	5.02	20.13	5.02	15.10	1.16
	2	0.00	5.02	20.12	5.02	15.10	1.16
	3	0.00	5.02	20.12	5.02	15.10	1.16
3 2	1	0.00	5.79	20.64	5.79	14.85	1.09
	2	0.00	5.79	20.64	5.79	14.85	1.09
	3	0.00	5.79	20.64	5.79	14.85	1.09
3 3	1	0.00	4.85	20.35	4.85	15.50	1.11
	2	0.00	4.85	20.35	4.85	15.50	1.11
	3	0.00	4.85	20.35	4.85	15.50	1.11

CO₂

O₂

F_O

AVERAGE RUN 1 5.02

AVERAGE RUN 1 15.10

AVERAGE RUN 1 1.16

AVERAGE RUN 2 5.79

AVERAGE RUN 2 14.85

AVERAGE RUN 2 1.09

AVERAGE RUN 3 4.85

AVERAGE RUN 3 15.50

AVERAGE RUN 3 1.11

BAY WEST STACK SAMPLING
E.P.A. METHOD 3 ANALYSIS

JOB# 92014 DATE OF ANALYSIS 1-24-92
SOURCE SOUTH PULP DRYER LEAK CHECK PERFORMED YES
SITE STARK / MURKIN COAST INDUST TECHNICIAN SCB
CITY/STATE MOOREHEAD, MS TYPE OF FUEL COAL

TEST/ RUN	READING NO.	BURET READING			CONCENTRATION (%v/v,dry)		F ₀
		ZERO POINT	AFTER CO 2	AFTER O2	CO ₂	O ₂	
AMBIENT AIR		0.00	0.00	20.90	0.00	20.90	1.1565
4 1	1	0.00	6.12	20.12	6.12	14.00	1.13
	2	0.00	6.12	20.12	6.12	14.00	1.13
	3	0.00	6.12	20.12	6.12	14.00	1.13
4 2	1	0.00	6.58	20.23	6.58	13.65	1.10
	2	0.00	6.58	20.23	6.58	13.65	1.10
	3	0.00	6.58	20.23	6.58	13.65	1.10
4 3	1	0.00	6.12	20.00	6.12	13.88	1.15
	2	0.00	6.12	20.00	6.12	13.88	1.15
	3	0.00	6.12	20.00	6.12	13.88	1.15

CO₂

O₂

F_O

AVERAGE RUN 1 6.12

AVERAGE RUN 1 14.00

AVERAGE RUN 1 1.13

AVERAGE RUN 2 6.58

AVERAGE RUN 2 13.65

AVERAGE RUN 2 1.10

AVERAGE RUN 3 6.12

AVERAGE RUN 3 13.88

AVERAGE RUN 3 1.15

Appendix 3

Bay West Analytical Data

LAB NO: 2034
 SOURCE: stock
 SITE: _____
 LOCATION: _____

 TEST NO: 1
 RUN NO.'S 1, 2, 3
 DATE: 2.13.92
 ANALYST: R. Hessler

SUMMARY OF PARTICULATE ANALYSES

Lab No.	Run No.	Total Corrected Wt. (g)
18908, '942, '973	<u>1</u>	<u>0.4594</u>
18910, '943, '974	<u>2</u>	<u>0.4335</u>
18912, '944, '975	<u>3</u>	<u>0.4454</u>
_____	_____	_____

BLANK VALUE ANALYSES

ACETONE

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)(residue)
<u>18954</u>	<u>21.2536</u>	- <u>21.2525</u>	= <u>0.0011</u>

Residue(g)	Volume(l)	g/l
<u>0.0011</u>	/ <u>0.135</u>	= <u>0.0081</u>

CONDENSIBLE ORGANICS

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)(residue)
<u>18941</u>	<u>140.7325</u>	- <u>140.7303</u>	= <u>0.0022</u>

Residue(g)	Volume(l)	g/l
<u>0.0022</u>	/ <u>0.200</u>	= <u>0.011</u>

NOTE: (l)=Liter
 (g)=Gram
 (g/l)=gram per liter

LAB NO: 2034
SOURCE: steck
SITE: _____
LOCATION: _____TEST NO: 1
RUN NO: 1
DATE: 2-13-92
ANALYST: R. Hessel**FILTERS**

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18973</u>	<u>0.9356</u>	<u>- 0.6204</u>	<u>= 0.3152</u>
			TOTAL <u>0.3152</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18942</u>	<u>21.4289</u>	<u>- 21.3372</u>	<u>= 0.0917</u>
BLANK <u>0.092</u> (1) * <u>0.0081</u> (g/l) = <u>0.0007</u> (g)			
			CORRECTED TOTAL <u>0.0910</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18908</u>	<u>141.7641</u>	<u>- 141.7008</u>	<u>= 0.0633</u>
BLANK <u>0.915</u> (1) * <u>0.011</u> (g/l) = <u>0.0101</u>			
			CORRECTED TOTAL <u>0.0532</u>

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>1</u>	<u>0.3152</u>	<u>+ 0.0910</u>	<u>+ 0.0532</u>	<u>= 0.4594</u>

LAB NO: 2034
 SOURCE: Stock
 SITE: _____
 LOCATION: _____

 TEST NO: 1
 RUN NO: 2
 DATE: 2.13.92
 ANALYST: R. Hessler
FILTERS

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18974</u>	<u>0.9284</u>	<u>- 0.6217</u>	<u>= 0.3067</u>
			TOTAL <u>0.3067</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18943</u>	<u>21.4370</u>	<u>- 21.3611</u>	<u>= 0.0759</u>
BLANK <u>0.095</u> (1) * <u>0.0081</u> (g/l) = <u>- 0.0008</u> (g)			
			CORRECTED TOTAL <u>0.0751</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18910</u>	<u>137.3848</u>	<u>- 137.3233</u>	<u>= 0.0615</u>
BLANK <u>0.890</u> (1) * <u>0.011</u> (g/l) = <u>- 0.0098</u>			
			CORRECTED TOTAL <u>0.0517</u>

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>2</u>	<u>0.3067</u>	<u>+ 0.0751</u>	<u>+ 0.0517</u>	<u>= 0.4335</u>

LAB NO: 2034
 SOURCE: stock
 SITE: _____
 LOCATION: _____

 TEST NO: 1
 RUN NO: 3
 DATE: 2.13.92
 ANALYST: R. Hessler
FILTERS

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18975</u>	<u>0.9156</u>	<u>- 0.6261</u>	<u>= 0.2895</u>
			TOTAL <u>0.2895</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18944</u>	<u>21.3925</u>	<u>- 21.3138</u>	<u>= 0.0787</u>
BLANK <u>0.066</u> (1) * <u>0.0081</u> (g/l) = <u>- 0.005</u> (g)			
			CORRECTED TOTAL <u>0.0782</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18912</u>	<u>135.2443</u>	<u>- 135.1561</u>	<u>= 0.0882</u>
BLANK <u>0.955</u> (1) * <u>0.011</u> (g/l) = <u>- 0.0105</u>			
			CORRECTED TOTAL <u>0.0777</u>

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>3</u>	<u>0.2895</u>	<u>+ 0.0782</u>	<u>+ 0.0777</u>	<u>= 0.4454</u>

LAB NO: 2034
 SOURCE: stock
 SITE: _____
 LOCATION: _____

 TEST NO: 2
 RUN NO.'S 1, 2, 3
 DATE: 2.13.92
 ANALYST: R. Hessler
SUMMARY OF PARTICULATE ANALYSES

Lab No.	Run No.	Total Corrected Wt. (g)
18914, '945, '976	<u>1</u>	<u>0.5441</u>
18917, '946, '977	<u>2</u>	<u>0.4578</u>
18920, '947, '978	<u>3</u>	<u>0.5965</u>
_____	_____	_____

BLANK VALUE ANALYSES
ACETONE

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)(residue)
<u>18954</u>	<u>21.2536</u>	<u>- 21.2525</u>	<u>= 0.0011</u>

Residue(g)	Volume(l)	g/l
<u>0.0011</u>	<u>/ 0.135</u>	<u>= 0.0081</u>

CONDENSIBLE ORGANICS

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)(residue)
<u>18941</u>	<u>140.7325</u>	<u>- 140.7303</u>	<u>= 0.0022</u>

Residue(g)	Volume(l)	g/l
<u>0.0022</u>	<u>/ 0.200</u>	<u>= 0.011</u>

 NOTE: (l)=Liter
 (g)=Gram
 (g/l)=gram per liter

LAB NO: 2034
 SOURCE: stock
 SITE: _____
 LOCATION: _____

 TEST NO: 2
 RUN NO: 1
 DATE: 2.13.92
 ANALYST: R. Hessler
FILTERS

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18976</u>	<u>1.0054</u>	<u>- 0.6219</u>	<u>= 0.3835</u>
			TOTAL <u>0.3835</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18945</u>	<u>21.3288</u>	<u>- 21.2513</u>	<u>= 0.0775</u>
BLANK <u>0.087</u> (l) * <u>0.008</u> (g/l) = <u>-0.0007</u> (g)			
			CORRECTED TOTAL <u>0.0768</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18914</u>	<u>136.8943</u>	<u>- 136.7975</u>	<u>= 0.0968</u>
BLANK <u>1.180</u> (l) * <u>0.011</u> (g/l) = <u>-0.0130</u>			
			CORRECTED TOTAL <u>0.0838</u>

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>1</u>	<u>0.3835</u>	<u>+ 0.0768</u>	<u>+ 0.0838</u>	<u>= 0.5441</u>

LAB NO: 2034
 SOURCE: Stock
 SITE: _____
 LOCATION: _____

 TEST NO: 2
 RUN NO: 2
 DATE: 2.13.92
 ANALYST: R. Hessley
FILTERS

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g)
<u>18977</u>	<u>0.9627</u>	<u>0.6341</u>	<u>0.3286</u>
TOTAL <u>0.3286</u>			

Probe & Front Half Wash

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g)
<u>18946</u>	<u>21.4229</u>	<u>21.3557</u>	<u>0.0672</u>
BLANK <u>0.064</u> (1) * <u>0.0081</u> (g/l) = <u>0.0005</u> (g)			
CORRECTED TOTAL <u>0.0667</u>			

IMPINGER CATCH

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g)
<u>18917</u>	<u>138.2972</u>	<u>138.2205</u>	<u>0.0767</u>
BLANK <u>1.295</u> (1) * <u>0.011</u> (g/l) = <u>0.0142</u>			
CORRECTED TOTAL <u>0.0625</u>			

SUMMARY OF CORRECTED TOTALS (g)

RUN NO.	FILTER	PROBE WASH	IMP. CATCH	TOTAL
<u>2</u>	<u>0.3286</u>	<u>0.0667</u>	<u>0.0625</u>	<u>0.4578</u>

LAB NO: 2034
SOURCE: stack
SITE: _____
LOCATION: _____

TEST NO: 2
RUN NO: 3
DATE: 2.13.92
ANALYST: R. Hessler

FILTERS

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18978</u>	<u>0.9565</u>	<u>- 0.6244</u>	<u>= 0.3321</u>

TOTAL 0.3321

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18947</u>	<u>21.4479</u>	<u>- 21.3038</u>	<u>= 0.1441</u>

BLANK 0.090 (1) * 0.0081 (g/l) = - 0.0007 (g)

CORRECTED TOTAL 0.1434

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18920</u>	<u>137.8898</u>	<u>- 137.7530</u>	<u>= 0.1368</u>

BLANK 1.440 (1) * 0.011 (g/l) = - 0.0158

CORRECTED TOTAL 0.1210

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>3</u>	<u>0.3321</u>	<u>+ 0.1434</u>	<u>+ 0.1210</u>	<u>= 0.5965</u>

LAB NO: 2034
SOURCE: stock
SITE: _____
LOCATION: _____

TEST NO: 3
RUN NO.'S 1, 2, 3
DATE: 2.13.92
ANALYST: R. Hessler

SUMMARY OF PARTICULATE ANALYSES

Lab No.	Run No.	Total Corrected Wt. (g)
18423, '948, '979	1	0.4289
18426, '949, '980	2	0.4762
18429, '950, '981	3	0.4544
_____	_____	_____

BLANK VALUE ANALYSES

ACETONE

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g) (residue)
18454	21.2536	21.2525	0.0011

Residue (g)	Volume (l)	g/l
0.0011	1	0.135

CONDENSIBLE ORGANICS

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g) (residue)
18441	140.7325	140.7303	0.0022

Residue (g)	Volume (l)	g/l
0.0022	1	0.200

NOTE: (l)=Liter
(g)=Gram
(g/l)=gram per liter

LAB NO: 2034
 SOURCE: stack
 SITE: _____
 LOCATION: _____

 TEST NO: 3
 RUN NO: 1
 DATE: 2.13.92
 ANALYST: R. Hess
FILTERS

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18979</u>	<u>0.8987</u>	<u>- 0.6095</u>	<u>= 0.2892</u>
			TOTAL <u>0.2892</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18948</u>	<u>21.4469</u>	<u>- 21.3712</u>	<u>= 0.0757</u>
BLANK <u>0.060</u> (1) * <u>0.0081</u> (g/l) = <u>- 0.0005</u> (g)			
			CORRECTED TOTAL <u>0.0752</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18923</u>	<u>137.5262</u>	<u>- 137.4492</u>	<u>= 0.0770</u>
BLANK <u>1.140</u> (1) * <u>0.011</u> (g/l) = <u>- 0.0125</u>			
			CORRECTED TOTAL <u>0.0645</u>

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>1</u>	<u>0.2892</u>	<u>+ 0.0752</u>	<u>+ 0.0645</u>	<u>= 0.4289</u>

LAB NO: 2034
 SOURCE: Stack
 SITE: _____
 LOCATION: _____

 TEST NO: 3
 RUN NO: 2
 DATE: 11/3/92
 ANALYST: R. Hessler
FILTERS

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18980</u>	<u>0.9048</u>	<u>0.6144</u>	<u>0.2904</u>
			TOTAL <u>0.2904</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18949</u>	<u>21.5347</u>	<u>21.3994</u>	<u>0.1353</u>
BLANK <u>0.077</u> (1) * <u>0.0051</u> (g/l) = <u>0.0006</u> (g)			
			CORRECTED TOTAL <u>0.1347</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18926</u>	<u>135.4499</u>	<u>135.3837</u>	<u>0.0662</u>
BLANK <u>1.370</u> (1) * <u>0.011</u> (g/l) = <u>0.0151</u>			
			CORRECTED TOTAL <u>0.0511</u>

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>2</u>	<u>0.2904</u>	<u>+ 0.1347</u>	<u>+ 0.0511</u>	<u>= 0.4762</u>

LAB NO: 2034
 SOURCE: stock
 SITE: _____
 LOCATION: _____

 TEST NO: 3
 RUN NO: 3
 DATE: 2.13.92
 ANALYST: R. Hesk
FILTERS

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18981</u>	<u>0.7079</u>	<u>- 0.6148</u>	<u>= 0.0931</u>
			TOTAL <u>0.2931</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18950</u>	<u>21.5119</u>	<u>- 21.3617</u>	<u>= 0.1502</u>
BLANK <u>0.075</u> (1) * <u>0.0081</u> (g/l) = <u>- 0.006</u> (g)			
			CORRECTED TOTAL <u>0.1496</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18929</u>	<u>136.6045</u>	<u>- 136.5283</u>	<u>= 0.0762</u>
BLANK <u>1.245</u> (1) * <u>0.011</u> (g/l) = <u>- 0.037</u>			
			CORRECTED TOTAL <u>0.0117</u>

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>3</u>	<u>0.2931</u>	<u>+ 0.1496</u>	<u>+ 0.0117</u>	<u>= 0.4544</u>

LAB NO: 2034
SOURCE: Stock
SITE: _____
LOCATION: _____

TEST NO: 41
RUN NO.'S 1, 2, 3
DATE: 2/13/92
ANALYST: R. Hessler

SUMMARY OF PARTICULATE ANALYSES

Lab No.	Run No.	Total Corrected Wt. (g)
18432, 951, 952	1	0.6358
18435, 952, 983	2	0.5193
18438, 953, 954	3	0.4688

BLANK VALUE ANALYSES

ACETONE

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g) (residue)
18954	21.2536	21.2525	0.0011

Residue (g)	Volume (l)	g/l
0.0011	0.135	0.0081

CONDENSIBLE ORGANICS

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g) (residue)
18941	140.7325	140.7303	0.0022

Residue (g)	Volume (l)	g/l
0.0022	0.200	0.011

NOTE: (l)=Liter
(g)=Gram
(g/l)=gram per liter

LAB NO: 2034
SOURCE: Stack
SITE: _____
LOCATION: _____

TEST NO: 4
RUN NO: 1
DATE: 2.13.92
ANALYST: R. Hessler

FILTERS

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18982</u>	<u>0.9505</u>	<u>- 0.6222</u>	<u>= 0.3283</u>
			TOTAL <u>0.3283</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18951</u>	<u>21.6776</u>	<u>- 21.4506</u>	<u>= 0.2270</u>
BLANK <u>0.076</u> (1) * <u>0.0081</u> (g/l) = <u>- 0.0006</u> (g)			
			CORRECTED TOTAL <u>0.2264</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18932</u>	<u>139.6786</u>	<u>- 139.5835</u>	<u>= 0.0951</u>
BLANK <u>1.275</u> (1) * <u>0.011</u> (g/l) = <u>- 0.0140</u>			
			CORRECTED TOTAL <u>0.0811</u>

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>1</u>	<u>0.3283</u>	<u>+ 0.2264</u>	<u>+ 0.0811</u>	<u>= 0.6358</u>

LAB NO: 2034
SOURCE: Stack
SITE: _____
LOCATION: _____

TEST NO: 4
RUN NO: 2
DATE: 2.13.92
ANALYST: R. Hesser

FILTERS

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18983</u>	<u>0.9165</u>	<u>- 0.6289</u>	<u>= 0.2876</u>
			TOTAL <u>0.2876</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18952</u>	<u>21.4627</u>	<u>- 21.3043</u>	<u>= 0.1584</u>
BLANK <u>0.076</u> (1) * <u>0.0081</u> (g/l) = <u>- 0.0006</u> (g)			
			CORRECTED TOTAL <u>0.1578</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18435</u>	<u>139.1562</u>	<u>- 139.0667</u>	<u>= 0.0895</u>
BLANK <u>1.415</u> (1) * <u>0.011</u> (g/l) = <u>- 0.0156</u>			
			CORRECTED TOTAL <u>0.0739</u>

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>2</u>	<u>0.2876</u>	<u>+ 0.1578</u>	<u>+ 0.0739</u>	<u>= 0.5193</u>

LAB NO: 2034
SOURCE: Stack
SITE: _____
LOCATION: _____

TEST NO: 4
RUN NO: 3
DATE: 2.13.92
ANALYST: R. Hessler

FILTERS

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18984</u>	<u>0.9261</u>	<u>- 0.6357</u>	<u>= 0.2904</u>

TOTAL 0.2904

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18953</u>	<u>21.3424</u>	<u>- 21.2453</u>	<u>= 0.0971</u>

BLANK 0.062 (1) * 0.0081 (g/l) = -0.0005 (g)

CORRECTED TOTAL 0.0966

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18938</u>	<u>139.9249</u>	<u>- 139.8271</u>	<u>= 0.0978</u>

BLANK 1.455 (1) * 0.011 (g/l) = -0.0160

CORRECTED TOTAL 0.0818

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>3</u>	<u>0.2904</u>	<u>+ 0.0966</u>	<u>+ 0.0818</u>	<u>= 0.4688</u>

LAB NO: 2034
SOURCE: Inlet
SITE: _____
LOCATION: _____

TEST NO: 1
RUN NO.'S 1, 2, 3
DATE: 2.17.92
ANALYST: R. Hessler

SUMMARY OF PARTICULATE ANALYSES

Lab No.	Run No.	Total Corrected Wt. (g)
<u>18955/18961</u>	<u>1</u>	<u>0.9751</u>
<u>18956/18964</u>	<u>3</u>	<u>1.0606</u>
<u>18957/18963</u>	<u>3</u>	<u>0.8696</u>
_____	_____	_____

BLANK VALUE ANALYSES

ACETONE

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)(residue)
<u>18954</u>	<u>21.2536</u>	<u>- 21.2525</u>	<u>= 0.0011</u>

Residue(g)	Volume(l)	g/l
<u>0.0011</u>	<u>/ 0.135</u>	<u>= 0.0081</u>

CONDENSIBLE ORGANICS

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)(residue)
_____	_____	<u>-</u>	<u>=</u>

Residue(g)	Volume(l)	g/l
_____	<u>/</u>	<u>=</u>

NOTE: (l)=Liter
(g)=Gram
(g/l)=gram per liter

LAB NO: 2034
 SOURCE: Tollet
 SITE: _____
 LOCATION: _____

 TEST NO: 1
 RUN NO: 1
 DATE: 2-17-92
 ANALYST: R. Hessler
FILTERS

<u>Lab No.</u>	<u>Final Wt. (g)</u>	-	<u>Tare Wt. (g)</u>	=	<u>Gain (g)</u>
<u>18961</u>	<u>1.6590</u>	-	<u>0.6330</u>	=	<u>0.4260</u>
<u>215H</u>	<u>1.3946</u>	-	<u>1.0040</u>	=	<u>0.3906</u>
TOTAL					<u>0.8166</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt. (g)</u>	-	<u>Tare Wt. (g)</u>	=	<u>Gain (g)</u>
<u>18455</u>	<u>21.5163</u>	-	<u>21.3571</u>	=	<u>0.1592</u>
BLANK <u>0.082</u> (l) * <u>0.0081</u> (g/l) = <u>0.0007</u> (g)					
CORRECTED TOTAL					<u>0.1585</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt. (g)</u>	-	<u>Tare Wt. (g)</u>	=	<u>Gain (g)</u>
_____	_____	-	_____	=	_____
_____	_____	-	_____	=	_____
BLANK _____ (l) * _____ (g/l) = _____					
CORRECTED TOTAL					_____

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>1</u>	<u>0.8166</u>	<u>+</u> <u>0.1585</u>	<u>+</u> _____	<u>= 0.9751</u>

LAB NO: 2034
SOURCE: Ink+
SITE: _____
LOCATION: _____

TEST NO: 1
RUN NO: 2
DATE: 2.17.92
ANALYST: R. Hassler

FILTERS

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18964</u>	<u>1.0654</u>	<u>- 0.6219</u>	<u>= 0.4435</u>
<u>dich</u>	<u>1.3830</u>	<u>- 1.0082</u>	<u>= 0.3748</u>
TOTAL			<u>0.8183</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18456</u>	<u>21.5572</u>	<u>- 21.3142</u>	<u>= 0.2430</u>
BLANK <u>0.092</u> (1) * <u>0.0081</u> (g/l) = <u>0.007</u> (g)			
CORRECTED TOTAL			<u>0.2423</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
_____	_____	<u>-</u>	<u>=</u>
_____	_____	<u>-</u>	<u>=</u>
BLANK _____ (1) * _____ (g/l) = _____			
CORRECTED TOTAL			_____

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>2</u>	<u>0.8183</u>	<u>+</u> <u>0.2423</u>	<u>+</u> _____	<u>= 1.0606</u>

LAB NO: 2034
 SOURCE: Ink+
 SITE: _____
 LOCATION: _____

 TEST NO: 1
 RUN NO: 3
 DATE: 2.17.92
 ANALYST: R. Hessler
FILTERS

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)
<u>18463</u>	<u>0.9445</u>	<u>0.6241</u>	<u>0.3204</u>
<u>dish</u>	<u>1.3585</u>	<u>1.0060</u>	<u>0.3525</u>

 TOTAL 0.6729
Probe & Front Half Wash

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)
<u>18957</u>	<u>21.6047</u>	<u>21.4075</u>	<u>0.1972</u>

 BLANK 0.060 (1) * 0.0061 (g/l) = 0.0005 (g)

 CORRECTED TOTAL 0.1967
IMPINGER CATCH

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)
_____	_____	_____	_____
_____	_____	_____	_____

BLANK _____ (1) * _____ (g/l) = _____

CORRECTED TOTAL _____

SUMMARY OF CORRECTED TOTALS (g)

RUN NO.	FILTER	PROBE WASH	IMP. CATCH	TOTAL
<u>3</u>	<u>0.6729</u>	<u>0.1967</u>	<u>_____</u>	<u>0.8696</u>

LAB NO: 2034
SOURCE: Inlet
SITE: _____
LOCATION: _____

TEST NO: 2
RUN NO.'S 1, 2, 3
DATE: 2-17-92
ANALYST: R. Hessler

SUMMARY OF PARTICULATE ANALYSES

Lab No.	Run No.	Total Corrected Wt. (g)
<u>18964/18985</u>	<u>1</u>	<u>1.1431</u>
<u>18965/18986</u>	<u>2</u>	<u>1.0204</u>
<u>18966/18987</u>	<u>3</u>	<u>1.0523</u>
_____	_____	_____

BLANK VALUE ANALYSES

ACETONE

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)(residue)
<u>18954</u>	<u>21.2536</u>	<u>21.2525</u>	<u>= 0.0011</u>

Residue(g)	Volume(l)	g/l
<u>0.0011</u>	<u>/ 0.135</u>	<u>= 0.0081</u>

CONDENSIBLE ORGANICS

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)(residue)
_____	_____	_____	<u>= _____</u>

Residue(g)	Volume(l)	g/l
_____	<u>/ _____</u>	<u>= _____</u>

NOTE: (l)=Liter
(g)=Gram
(g/l)=gram per liter

LAB NO: 2034
 SOURCE: Inlet
 SITE: _____
 LOCATION: _____

 TEST NO: 2
 RUN NO: 1
 DATE: 2.17.92
 ANALYST: R. Hessler
FILTERS

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)
<u>18964</u>	<u>1.1149</u>	<u>0.6210</u>	<u>0.4939</u>
<u>dish</u>	<u>1.3801</u>	<u>1.0043</u>	<u>0.3758</u>
			TOTAL <u>0.8697</u>

Probe & Front Half Wash

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)
<u>18985</u>	<u>21.5465</u>	<u>21.2722</u>	<u>0.2743</u>
BLANK <u>0.113</u> (1) * <u>0.0081</u> (g/l) = <u>0.0009</u> (g)			
			CORRECTED TOTAL <u>0.2734</u>

IMPINGER CATCH

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)
_____	_____	_____	_____
_____	_____	_____	_____
BLANK _____ (1) * _____ (g/l) = _____			
			CORRECTED TOTAL _____

SUMMARY OF CORRECTED TOTALS (g)

RUN NO.	FILTER	PROBE WASH	IMP. CATCH	TOTAL
<u>1</u>	<u>0.8697</u>	<u>0.2734</u>	<u>+</u>	<u>1.1431</u>

LAB NO: 2034
SOURCE: Inlet
SITE: _____
LOCATION: _____

TEST NO: 2
RUN NO: 2
DATE: 2.17.92
ANALYST: R. Hessbr

FILTERS

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18965</u>	<u>1.6471</u>	<u>- 0.6160</u>	<u>= 0.4311</u>
<u>dish</u>	<u>1.3520</u>	<u>- 1.0040</u>	<u>= 0.3480</u>
TOTAL			<u>0.7791</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18986</u>	<u>21.5417</u>	<u>- 21.2995</u>	<u>= 0.2422</u>
BLANK <u>0.113</u> (l) * <u>0.0081</u> (g/l) = <u>0.0009</u> (g)			
CORRECTED TOTAL			<u>0.2413</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
_____	_____	<u>-</u>	<u>=</u>
_____	_____	_____	_____
BLANK _____ (l) * _____ (g/l) = _____			
CORRECTED TOTAL			_____

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>2</u>	<u>0.7791</u>	<u>+</u> <u>0.2413</u>	<u>+</u> _____	<u>= 1.0204</u>

LAB NO: 2034
 SOURCE: Inlet
 SITE: _____
 LOCATION: _____

 TEST NO: 2
 RUN NO: 3
 DATE: 2-17-92
 ANALYST: R. Hesser
FILTERS

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18966</u>	<u>1.0780</u>	<u>- 0.6284</u>	<u>= 0.4496</u>
<u>dish</u>	<u>1.3934</u>	<u>- 1.0083</u>	<u>= 0.3851</u>
TOTAL			<u>0.8347</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18487</u>	<u>21.5781</u>	<u>- 21.3601</u>	<u>= 0.2180</u>
BLANK <u>0.055</u> (l) * <u>0.0081</u> (g/l) = <u>0.0004</u> (g)			
CORRECTED TOTAL			<u>0.2176</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
_____	_____	<u>-</u> _____	<u>=</u> _____
_____	_____	<u>-</u> _____	<u>=</u> _____
BLANK _____ (l) * _____ (g/l) = _____			
CORRECTED TOTAL			_____

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>3</u>	<u>0.8347</u>	<u>+</u> <u>0.2176</u>	<u>+</u> _____	<u>= 1.0523</u>

LAB NO: 2034
SOURCE: Inlet
SITE: _____
LOCATION: _____

TEST NO: 3
RUN NO.'S 1
DATE: 2-17-92
ANALYST: R. Hassler

SUMMARY OF PARTICULATE ANALYSES

Lab No.	Run No.	Total Corrected Wt. (g)
18967/18968	1	1.0501
18965/18989	2	1.0421
18969/18990	3	1.1957
_____	_____	_____

BLANK VALUE ANALYSES

ACETONE

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g) (residue)
18954	21.2536	21.2525	0.0011

Residue (g)	Volume (l)	g/l
0.0011	0.135	0.0081

CONDENSIBLE ORGANICS

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g) (residue)
_____	_____	_____	_____

Residue (g)	Volume (l)	g/l
_____	_____	_____

NOTE: (l)=Liter
(g)=Gram
(g/l)=gram per liter

LAB NO: 2034
 SOURCE: Inlet
 SITE: _____
 LOCATION: _____

 TEST NO: 3
 RUN NO: 1
 DATE: 2.17.92
 ANALYST: R. Hessler
FILTERS

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)
<u>18467</u>	<u>1.0674</u>	<u>0.6245</u>	<u>0.4429</u>
<u>dish</u>	<u>1.3499</u>	<u>1.6012</u>	<u>0.3487</u>
TOTAL			<u>0.7916</u>

Probe & Front Half Wash

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)
<u>18485</u>	<u>21.5450</u>	<u>21.2857</u>	<u>0.2593</u>
BLANK <u>0.101</u> (l) * <u>0.0081</u> (g/l) = <u>0.0008</u> (g)			
CORRECTED TOTAL			<u>0.2585</u>

IMPINGER CATCH

Lab No.	Final Wt.(g)	Tare Wt.(g)	Gain (g)
_____	_____	_____	_____
BLANK _____ (l) * _____ (g/l) = _____			
CORRECTED TOTAL			_____

SUMMARY OF CORRECTED TOTALS (g)

RUN NO.	FILTER	PROBE WASH	IMP. CATCH	TOTAL
<u>1</u>	<u>0.7916</u>	<u>0.2585</u>	<u>_____</u>	<u>1.0501</u>

LAB NO: 2034
SOURCE: Ink
SITE: _____
LOCATION: _____

TEST NO: 3
RUN NO: 2
DATE: 2.17.92
ANALYST: R. Hessler

FILTERS

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18968</u>	<u>1.0163</u>	<u>0.6279</u>	<u>0.3884</u>
<u>dish</u>	<u>1.2660</u>	<u>0.9996</u>	<u>0.2664</u>
TOTAL			<u>0.6548</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18989</u>	<u>21.5773</u>	<u>21.1889</u>	<u>0.3884</u>
BLANK <u>0.131</u> (l) * <u>0.0081</u> (g/l) = <u>0.0011</u> (g)			
CORRECTED TOTAL			<u>0.3873</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
_____	_____	_____	_____
BLANK _____ (l) * _____ (g/l) = _____			
CORRECTED TOTAL			_____

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>2</u>	<u>0.6548</u>	<u>0.3873</u>	<u>_____</u>	<u>1.0421</u>

LAB NO: 2034
SOURCE: Inlet
SITE: _____
LOCATION: _____

TEST NO: 3
RUN NO: 3
DATE: 2-17-92
ANALYST: R. Hessler

FILTERS

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18969</u>	<u>1.0162</u>	<u>0.6323</u>	<u>0.3839</u>
<u>Dish</u>	<u>1.4663</u>	<u>0.9960</u>	<u>0.4703</u>

TOTAL 0.8542

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18990</u>	<u>21.6158</u>	<u>21.2733</u>	<u>0.3425</u>

BLANK 0.124 (1) * 0.0081 (g/l) = 0.0010 (g)

CORRECTED TOTAL 0.3415

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
_____	_____	_____	_____

BLANK _____ (1) * _____ (g/l) = _____

CORRECTED TOTAL _____

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>3</u>	<u>0.8542</u>	<u>0.3415</u>	<u>_____</u>	<u>1.1957</u>

LAB NO: 2034
SOURCE: Inlet
SITE: _____
LOCATION: _____

TEST NO: 4
RUN NO.'S 1, 2, 3
DATE: 2.17.92
ANALYST: R. H. S. G. L.

SUMMARY OF PARTICULATE ANALYSES

Lab No.	Run No.	Total Corrected Wt. (g)
<u>18958/18970</u>	<u>1</u>	<u>1.2384</u>
<u>18959/18971</u>	<u>2</u>	<u>1.2746</u>
<u>18960/18972</u>	<u>3</u>	<u>1.1254</u>
_____	_____	_____

BLANK VALUE ANALYSES

ACETONE

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g) (residue)
<u>18954</u>	<u>21.2536</u>	<u>21.2525</u>	<u>= 0.0011</u>

Residue (g)	Volume (l)	g/l
<u>0.0011</u>	<u>/ 0.135</u>	<u>= 0.0081</u>

CONDENSIBLE ORGANICS

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g) (residue)
_____	_____	_____	<u>= _____</u>

Residue (g)	Volume (l)	g/l
_____	<u>/ _____</u>	<u>= _____</u>

NOTE: (l)=Liter
(g)=Gram
(g/l)=gram per liter

LAB NO: 2034
SOURCE: Ink
SITE: _____
LOCATION: _____

TEST NO: 4
RUN NO: 1
DATE: 2.17.92
ANALYST: R. Hessler

FILTERS

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18470</u>	<u>1.0837</u>	<u>0.6256</u>	<u>0.4581</u>
<u>dish</u>	<u>1.5995</u>	<u>1.0015</u>	<u>0.5980</u>
TOTAL			<u>1.0561</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
<u>18458</u>	<u>21.5365</u>	<u>21.3525</u>	<u>0.1830</u>
BLANK <u>0.091</u> (1) * <u>0.0081</u> (g/l) = <u>0.0067</u> (g)			
CORRECTED TOTAL			<u>0.1823</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt. (g)</u>	<u>Tare Wt. (g)</u>	<u>Gain (g)</u>
_____	_____	_____	_____
BLANK _____ (1) * _____ (g/l) = _____			
CORRECTED TOTAL			_____

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>1</u>	<u>1.0561</u>	<u>+ 0.1823</u>	<u>+</u>	<u>= 1.2384</u>

LAB NO: 2034
SOURCE: Inlet
SITE: _____
LOCATION: _____

TEST NO: 4
RUN NO: 2
DATE: 2.17.92
ANALYST: R. Hassler

FILTERS

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18471</u>	<u>1.0476</u>	<u>- 0.6285</u>	<u>= 0.4191</u>
<u>dish</u>	<u>1.5830</u>	<u>- 1.0003</u>	<u>= 0.5827</u>
TOTAL			<u>1.0018</u>

Probe & Front Half Wash

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
<u>18959</u>	<u>21.5487</u>	<u>- 21.2751</u>	<u>= 0.2736</u>
BLANK <u>0.098</u> (1) * <u>0.0081</u> (g/l) = <u>0.0008</u> (g)			
CORRECTED TOTAL			<u>0.2728</u>

IMPINGER CATCH

<u>Lab No.</u>	<u>Final Wt.(g)</u>	<u>Tare Wt.(g)</u>	<u>Gain (g)</u>
_____	_____	<u>-</u>	<u>=</u>
_____	_____	<u>-</u>	<u>=</u>
BLANK _____ (1) * _____ (g/l) = _____			
CORRECTED TOTAL			_____

SUMMARY OF CORRECTED TOTALS (g)

<u>RUN NO.</u>	<u>FILTER</u>	<u>PROBE WASH</u>	<u>IMP. CATCH</u>	<u>TOTAL</u>
<u>2</u>	<u>1.0018</u>	<u>+ 0.2728</u>	<u>+</u>	<u>= 1.2746</u>

LAB NO: 2034
SOURCE: Inlet
SITE: _____
LOCATION: _____

TEST NO: 4
RUN NO: 3
DATE: 2.17.92
ANALYST: R. Hessler

FILTERS

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g)
<u>18472</u>	<u>1.0649</u>	<u>- 0.6230</u>	<u>= 0.4419</u>
<u>dish</u>	<u>1.3648</u>	<u>- 1.0010</u>	<u>= 0.3638</u>
TOTAL			<u>0.8057</u>

Probe & Front Half Wash

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g)
<u>18960</u>	<u>21.6891</u>	<u>- 21.3688</u>	<u>= 0.3203</u>
BLANK <u>0.077</u> (1) * <u>0.0081</u> (g/l) = <u>-0.0006</u> (g)			
CORRECTED TOTAL			<u>0.3197</u>

IMPINGER CATCH

Lab No.	Final Wt. (g)	Tare Wt. (g)	Gain (g)
_____	_____	_____	_____
BLANK _____ (1) * _____ (g/l) = _____			
CORRECTED TOTAL			_____

SUMMARY OF CORRECTED TOTALS (g)

RUN NO.	FILTER	PROBE WASH	IMP. CATCH	TOTAL
<u>3</u>	<u>0.8057</u>	<u>+ 0.3197</u>	<u>+</u>	<u>= 1.1254</u>

Appendix 4

Procedures

SAMPLING EQUIPMENT AND PROCEDURES

The particulate sampling equipment, referred to as the "Particulate Sampling Train", was designed and constructed by Andersen Instruments, Atlanta, Georgia. This sampling train meets or exceeds all EPA guidelines as directed by CFR Title 40, Part 60. The particulate emission rates are determined by EPA Methods 1-5, CFR Title 40, Part 60, Appendix A (revised July 1, 1988). A preliminary velocity profile of the gases is conducted by a velocity and temperature traverse in order to select an appropriate nozzle to allow isokinetic sampling.

The particulate sampling train is made up of a heated glass-lined sampling probe, Type S pitot, and a thermocouple. The probe is attached to an enclosure which houses an all-glass filter holder in a heated chamber maintained to 250 degrees F. Attached to the enclosure is an ice bath which holds the impingers and dessicant-filled drying column. The particulate sampling train is attached to the control unit by an umbilical cord (vacuum line). The control unit is made up of a dry gas meter, calibrated orifice, a leakless pump, two inclined manometers, and the appropriate valves needed for operation of the particulate sampling train.

The particulate matter is collected by drawing the stack gas through the sampling probe isokinetically and passing it through an 11.0 cm diameter Whatman Type 934-AH glass microfibre filter. The sample gas is then passed through three glass impingers and a dessicant drying column to remove any remaining moisture. The impingers and the drying column are packed in crushed ice and water to maintain ≤ 68 degrees F. The stack gas is then transferred to the control unit via an umbilical cord where it travels through the vacuum pump and into a calibrated dry gas meter. The calibrated gas meter provides real time flow rate data throughout the entire test.

The particulate matter sample is acquired by drawing a gas sample for equal time periods at each of the centroids of the required number of equal area sampling points. The sampling rate is adjusted throughout the test in order to maintain isokinetic sampling. A Tandy PC-6 hand held computer is used for determination of the sampling rates.

After sampling is completed, the filter is removed with a set of teflon-coated tweezers and placed in a glass petri dish and sealed. The nozzle and the inlet side of the filter holder are washed with acetone and brushed to remove any deposits. The sampling probe is rinsed with acetone, brushed with a probe brush, and rinsed again. The acetone rinse/washing, called "probe wash", is taken to the laboratory along with the filter to be logged in. A chain of custody accompanies the samples during transport to the laboratory

The volume of the probe wash is recorded to determine if any acetone was lost in transport and then evaporated to near dryness by heating to 62 degrees C. Then it is quantitatively transferred to a tared 40 ml glass evaporation vial. This sample is evaporated to dryness by heating to 62 degrees C. The acetone-free sample is then dried at 105 degrees C for 30 minutes, cooled in a dessicator, and weighed to the nearest 0.1 mg. The filter is transferred to a 150 mm diameter glass petri dish and dried at 105 degrees C for two hours. It is then cooled in a dessicator and weighed to the nearest 0.1 mg. All sample weighings are done in a balance room where the relative humidity is maintained at less than 50%. The dessicant weight is recorded in the field and added to the collected condensate to give the total amount of water collected.

Modified Method 5 Test Method For Condensible Particulate

Purpose

To describe a test method for particulate which includes the condensible particulate captured in the impingers of the United States Environmental Protection Agency Method 5 (EPA Method 5) as stated in Title 40, Code of Federal Regulations, Part 60, Appendix A or any other test method approved by the Department.

The test method shall be applied to all sources. The Department may grant exemptions to New Source Performance Standard sources, sources to which Best Available Control Technology is applied, and other sources on a case-by-case basis.

Sampling Equipment

The sampling train and sample recovery equipment are the same as listed in par. 2 of EPA Method 5.

Reagents

The reagents are the same as listed in par. 3 of EPA Method 5 with the addition of methylene chloride-reagent grade. At the discretion of the tester, any of the following reagent grade solvents may also be used: chloroform, ethyl ether, 1,1,1-trichloroethane, trichlorotrifluoroethane (freon 113) and any other solvent exhibiting similar properties as the solvents listed.

Procedure

The sampling procedure is the same as listed in par. 4.1 of EPA Method 5. All parts of the sample collection portion of the train (nozzle, probe, cyclone and flask, filter holder, impinger glassware) shall be clean before sample collection. All sample collection portions of the train shall be made free of organic solvent residue before sample collection by rinsing them two or more times with distilled water.

The sample recovery procedure is the same as listed in par. 4.2 of EPA Method 5 with the addition of the following:

1. The filter is placed in Container #1.
2. The probe wash consisting of the probe rinse, the cyclone and flask rinse, the connecting glassware rinse, and the front half of the filter holder rinse is placed in Container #2.
3. The spent silica gel is placed in Container #3.

4. In order not to contaminate the impinger sample during sample recovery, the tester shall wipe off stopcock grease used on any glassware joint, that might come in contact with the impinger catch contained in the first 3 impingers, before recovering the sample.
5. Measure the volume of the impinger catch with a graduated cylinder or by weighing on a balance. The impinger catch is placed in Container #4.
6. Rinse the graduated cylinder, the back half of the filter holder, the first 3 impingers, and the glassware connectors with distilled water and add it to Container #4.
7. Repeat the rinse with acetone, being careful not to contaminate the acetone rinse with stopcock grease, and place it in Container #5.

The sample analysis shall be as follows:

1. The determination of weight gain on the filter in Container #1 is the same as described for Container #1 in par. 4.3 of EPA Method 5 except for the following items.
 - a. Desiccate the filter for at least 24 hours and no more than 48 hours in a desiccator and weight to a constant weight. Report the results to the nearest 0.1 mg. For the purposes of this handbook procedure, the term constant weight means a difference of no more than 0.5 mg between 2 consecutive weighings with at least 2 hours of desiccation between weighings.
 - b. At the discretion of the tester, the alternate oven drying procedure for the filter, listed in par. 4.3 of EPA Method 5, may be used provided that the tester provides for 2 hours of desiccation between weighings. After the procedure is performed, the initial weight determined may be used as the final weight.
2. The analysis of the probe wash in Container #2 is the same as described for Container #2 in par. 4.3 of EPA Method 5. With appropriate caution, the alternate drying procedure at an elevated temperature, listed in par. 4.3 of EPA Method 5, may be used. The desiccating and weighing procedure listed for the filter in par. 1.a. of this handbook procedure shall be used.
3. The spent silica gel in Container #3 is weighed in the same manner as Container #3 in par. 4.3 of EPA Method 5.
4. The analysis of the impinger catch in Container #4 is performed by transferring the sample to a separatory funnel. Rinse Container #4 with distilled water and add the rinse to the funnel. Repeat the rinse with acetone and add it to Container #5. Add 50 milliliters (ml) of methylene chloride to the funnel and shake for 1 minute. Allow the phases to separate and drain the solvent phase into a tared beaker. Perform the extraction 2 more times and drain the solvent phase into the same beaker.

Drain the remaining liquid in the funnel into another tared beaker. The solvent extract residue beaker is analyzed in the same way as Container #2 in par. 4.3 of EPA Method 5 except that evaporation of the sample to dryness shall be at ambient temperature and pressure. The desiccating and weighing procedure listed for the filter in par. 1.a. of this handbook procedure shall be used.

Only 3 solvent extractions are necessary regardless of the size of the sample. If the size of the sample exceeds the size of the available separatory funnel, the sample may be split and the 2 halves analyzed separately.

5. The liquid residue beaker is analyzed in the same way as Container #2 in par. 4.3 of EPA Method 5 except that evaporation of the sample to dryness may be performed at $220^{\circ}\text{F} \pm 10^{\circ}\text{F}$. As an alternate drying procedure, a 100 ml aliquot of the liquid residue may be evaporated to dryness at $220^{\circ}\text{F} \pm 10^{\circ}\text{F}$. Following the drying procedure, the desiccating and weighing procedure listed for the filter in par. 1.a. of this handbook procedure shall be used. If an aliquot was used, the weight of the sample shall be corrected to reflect the entire sample volume of the liquid residue. For some sources, the exhaust gases being sampled may chemically react with the impinger water to produce artifacts. These artifacts would show up as particulate in the liquid residue. If a source can demonstrate that all or part of the liquid residue particulate is due to artifacts, the source may subtract the weight of the artifacts from the total particulate weight.

A common artifact found during the testing of sources that emit SO_2 is sulfates. The tester may perform a U.S. EPA Method 8 barium perchlorate titration for H_2SO_4 on the sample and subtract the results.

6. The analysis of the impinger acetone rinse in Container #5 is the same as described for Container #2 in par. 4.3 of EPA Method 5 except that evaporation of the sample to dryness shall be at ambient temperature and pressure. The desiccating and weighing procedure listed for the filter in par. 1.a. of this handbook procedure shall be used.
7. Perform blank weight determinations on the distilled water, the acetone, and the solvent used in the extraction. Solvents, acetone, and distilled water with blank values greater than 0.01 mg/ml should not be used.
8. The filterable particulate weight or front half catch is determined by adding the weight gain of the filter and the probe wash weight and subtracting out the acetone blank weight.
9. The condensible particulate weight or back half catch is determined by summing the weights of the solvent extract residue, the liquid residue, and the impinger acetone rinse and subtracting out the appropriate blank weights. The organic fraction of the back half is equal to the solvent extract weight plus the impinger acetone rinse weight minus the appropriate blank weights. The inorganic fraction of the back half is equal to the liquid residue weight minus the water blank and any artifact correction.

10. The total particulate weight is the sum of the filterable particulate weight and the condensible particulate weight.

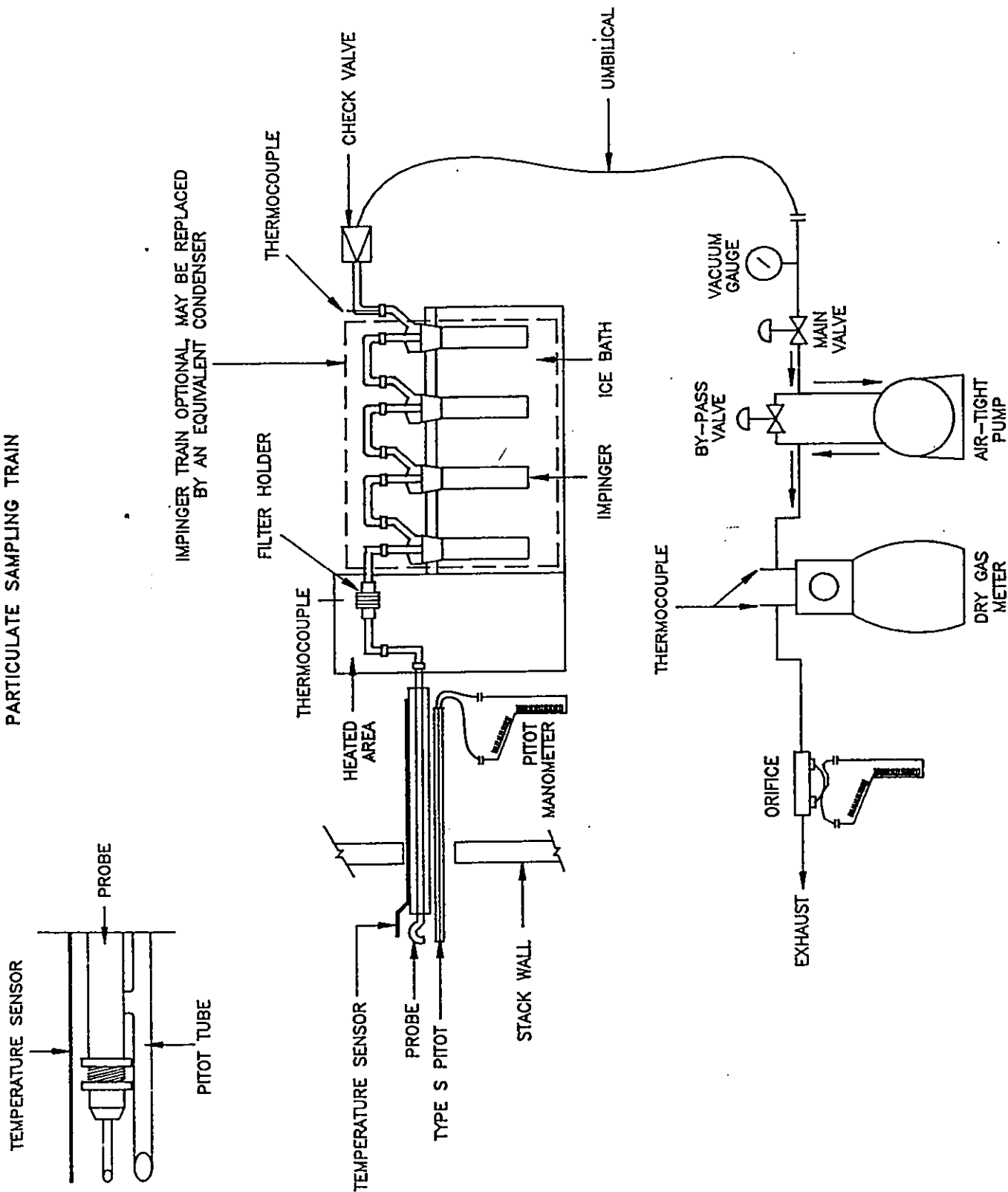
Calibrations

The calibrations that need to be performed on the sampling equipment are the same as listed in par. 5 of EPA Method 5.

Calculations

The calculation of results and the criteria for acceptable results is the same as described in par. 6 of EPA Method 5. The total particulate weight shall be used to determine compliance.

PARTICULATE SAMPLING TRAIN



Appendix 5

Calculations and Abbreviations

Symbols

A	Stack Cross Sectional Area, ft^2
A_n	Nozzle Cross Sectional Area, ft^2
B_{ws}	Moisture Content of Stack Gas, Proportion by Volume
C_{actual}	Concentration of Particulate Matter in Stack Gas, gr/acf
C_p	Pitot Tube Coefficient, dimensionless
C_s	Concentration of Particulate Matter in Stack Gas, Dry Basis, Corrected to Standard Conditions, gr/dscf
ΔH	Average Orifice Meter Pressure Drop, in. H_2O
I	Isokinetic Ratio, %
m_n	Mass of Particulate Collected, g
m_r	Mass Loading Rate, $\#/\text{hour}$
M_s	Wet Molecular Weight of Stack Gas, $\text{g}/\text{g-mole}$
t	Total Sampling Time, min.
Δp	Velocity Head of Stack Gas, in. H_2O
P_b	Absolute Barometric Pressure, in. Hg
P_s	Absolute Stack Pressure, in. Hg
P_{std}	Standard Absolute Stack Pressure, 29.92 in. Hg
Q_{sd}	Dry Volumetric Stack Flow Rate, scfm
$T_{m(\text{avg})}$	Average Absolute Dry Gas Meter Temperature, $^{\circ}\text{R}$
$T_{s,\text{avg}}$	Average Absolute Stack Gas Temperature, $^{\circ}\text{R}$
T_{std}	Standard Absolute Temperature, 528 $^{\circ}\text{R}$
$V_{s,\text{avg}}$	Average Stack Gas Velocity, ft/sec
$V_{w(\text{std})}$	Standard Volume of Water Collected from Stack Gas, ml
$V_{m(\text{std})}$	Standard Volume of Gas Measured by the Dry Gas Meter, dscf
V_m	Volume of Gas Measured by the Dry Gas Meter, cf
W_f	Weight of Water Collected in Silica Gel, g
Y	Dry Gas Meter Calibration Factor, dimensionless

ABBREVIATIONS

acfm	actual cubic feet per minute
cc	cubic centimeters
cf.	cubic feet
degrees C	degrees Centigrade
degrees F	degrees Fahrenheit
diam	diameter
dscf	dry standard cubic feet
ft/sec	feet per second
g	gram
gr/acf	grains per actual cubic foot
gr/dscf	grains per dry standard cubic foot
hrs	hours
in	inches
in Hg	inches of mercury
in wc	inches of water column
lb/hr	pounds per hour
lb/dscf	pounds per dry standard cubic foot
mg	milligrams
min	minutes
ml	milliliters
standard conditions	20° C and 29.92 inches of mercury
sq ft	square feet
v/v	percent by volume
w/w	percent by weight

Equations Used in this Report

Method 2

$$V_{s(avg)} = 85.48 C_p (\sqrt{\Delta P})_{avg} \sqrt{\frac{T_{s(avg)}}{P_s M_s}}$$

$$Q_{sd} = 60 (1 - B_{ws}) V_{s(avg)} A \frac{T_{std} P_s}{T_{s(avg)} P_{std}}$$

Method 3

$$M_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO)$$

$$M_s = M_d (1 - B_{ws}) + 0.18(\%B_{ws})$$

Method 4

$$B_{ws} = \frac{V_{w(std)}}{V_{w(std)} + V_{m(std)}}$$

$$V_{w(std)} = 0.04707 (W_f)$$

Method 5

$$V_{m(std)} = 17.65 V_m Y \frac{P_b + \Delta H/13.6}{T_{m(avg)}}$$

$$I = 0.0945 \frac{T_{s(avg)} V_{m(std)}}{P_s V_{s(avg)} A_n \theta (1 - B_{ws})}$$

$$C_s = \frac{15.43 m_n}{V_{m(std)}}$$

$$C_{actual} = \frac{272.3 m_n P_s}{T_{s(avg)} (V_{w(std)} + V_{m(std)})}$$

$$m_r = 0.008714 C_s Q_{sd}$$

$$m_i = C F \left(\frac{20.9}{20.9 - \%O_2} \right)$$

Appendix 6

Sampling Equipment Calibration Data

NOZZLE CALIBRATION DATA SHEET

NOZZLE IDENTIFICATION NUMBER:N1-4

FIELD TECHNICIAN:SCOTT BAINVILLE

DATE OF CALIBRATION:1-21-92

<u>POSITION</u>	<u>DIAMETER (INCHES)</u>
1	.312 IN.
2	.311 IN.
3	.312 IN.
<u>AVERAGE:</u>	<u>.312 IN.</u>

NOTE:Nozzle is rotated by 60 degree increments and diameter measured to the nearest 0.001 inch.

NOZZLE CALIBRATION DATA SHEET

NOZZLE IDENTIFICATION NUMBER:N2-5

FIELD TECHNICIAN:DWAYNE SMITH

DATE OF CALIBRATION:1-21-92

<u>POSITION</u>	<u>DIAMETER (INCHES)</u>
1	.313 IN.
2	.312 IN.
3	.313 IN.
<u>AVERAGE:</u>	<u>.313 IN.</u>

NOTE:Nozzle is rotated by 60 degree increments and diameter measured to the nearest 0.001 inch.

S-TYPE PITOT TUBE INSPECTION SHEET

PITOT NUMBER: P1-4

DATE OF INSPECTION: 9-9-91

TECHNICIAN: SCOTT BAINVILLE

PITOT TUBE DIMENSIONS:

External tubing diameter (D_t)	.315	IN.
Base to Side A opening plane (P_A)	.450	IN.
Base to Side B opening plane (P_B)	.453	IN.

ALIGNMENT:

a_1	<	10°	0	degrees
a_2	<	10°	0	degrees

B_1	<	5°	0	degrees
B_2	<	5°	0	degrees

Z	<	.125"	.021	IN.
W	<	.0625"	.034	IN.

DISTANCE FROM PITOT TO PROBE COMPONENTS:

Pitot to 0.500" nozzle	.745	IN.
Pitot to probe sheath	4.4567	IN.
Pitot to thermocouple (parallel to probe)	.9668	IN.
Pitot to thermocouple (perpendicular to probe)	3.525	IN.

S-TYPE PITOT TUBE INSPECTION SHEET

PITOT NUMBER: P1-6

DATE OF INSPECTION: 9-9-91

TECHNICIAN: SCOTT BAINVILLE

PITOT TUBE DIMENSIONS:

External tubing diameter (D_t)	.316	IN.
Base to Side A opening plane (P_A)	.450	IN.
Base to Side B opening plane (P_B)	.453	IN.

ALIGNMENT:

a_1	<	10°	0	degrees
a_2	<	10°	0	degrees

B_1	<	5°	0	degrees
B_2	<	5°	0	degrees

Z	<	.125"	.015	IN.
W	<	.0625"	.019	IN.

DISTANCE FROM PITOT TO PROBE COMPONENTS:

Pitot to 0.500" nozzle	.755	IN.
Pitot to probe sheath	4.3298	IN.
Pitot to thermocouple (parallel to probe)	.9328	IN.
Pitot to thermocouple (perpendicular to probe)	3.525	IN.

S-TYPE PITOT TUBE INSPECTION SHEET

PITOT NUMBER:P1-8

DATE OF INSPECTION:9-9-91

TECHNICIAN:SCOTT BAINVILLE

PITOT TUBE DIMENSIONS:

External tubing diameter (D_t)	.315	IN.
Base to Side A opening plane (P_A)	.450	IN.
Base to Side B opening plane (P_B)	.453	IN.

ALIGNMENT:

a_1	<	10°	2	degrees
a_2	<	10°	3	degrees

B_1	<	5°	3	degrees
B_2	<	5°	0	degrees

Z	<	.125"	.051	IN.
W	<	.0625"	.033	IN.

DISTANCE FROM PITOT TO PROBE COMPONENTS:

Pitot to 0.500" nozzle	.745	IN.
Pitot to probe sheath	4.4567	IN.
Pitot to thermocouple (parallel to probe)	.9668	IN.
Pitot to thermocouple (perpendicular to probe)	3.525	IN.

**TEMPERATURE MEASUREMENT DEVICE
CALIBRATION DATA**

DATE OF CALIBRATION: 10-14-91
MAKE: OMEGA T/C SOURCE CALIBRATOR
MODEL: CL-300-K-2100F
SERIAL NUMBER: 105
RANGE: 0F-2100F
THERMOCOUPLE TYPE: K
TECHNICIAN: DAS
UNIT WAS: IN TOLERANCE

DESIRED TEMP	TEMPURATURE OF SIMULATOR	RESPONSE	DEVIATION	
			(t)	(%)
0	0	-0.6	0.6	0.13
100	100	100.8	0.8	0.14
200	200	202.5	2.5	0.37
300	300	302.1	2.1	0.27
400	400	401.4	1.4	0.16
500	500	503.5	3.5	0.36
600	600	605.1	5.1	0.48
700	700	704.6	4.6	0.39
800	800	806.7	6.7	0.53
900	900	905.9	5.9	0.43
1000	1000	1007	7	0.47
1100	1100	1107	7	0.44
1200	1200	1206	6	0.36
1300	1300	1308	8	0.45
1400	1400	1409	9	0.48
1500	1500	1510	10	0.51
1600	1600	1611	11	0.53
1700	1700	1711	11	0.50
1800	1800	1813	13	0.57
1900	1900	1912	12	0.50
2000	2000	2015	15	0.60
2100	2100	2114	14	0.54
AVERAGES:			7.1	0.41

% DEVIATION = $(t \bullet 100) / (t + 460)$
% DEVIATION MUST BE < 1.5

#2

ANDERSEN Samplers INC.

4801 FULTON IND. BLVD., ATLANTA, GA 30336

CONTROL UNIT CALIBRATION

Date 1-2-92

Unit Number 1291-604

Barometric pressure, $P_b = 29.99$ in Hg.

Model Number 90-800

Orifice manometer setting, ΔH in. H ₂ O	Gas volume, wet test meter V_w , ft ³	Gas volume, dry gas meter V_d , ft ³	Temperature				Time θ , min	γ	ΔH_q
			Wet test Meter t_w , °R	Dry gas meter					
				Inlet t_{di} , °R	Outlet t_{do} , °R	Average t_d , °R			
1.0	5	5.342	75.2/535.2	133.9	93.7/553.7	113.80/573.80	8.76	1.00	1.71
2.0	5	5.362	74.0/539.0	139.5	94.9/559.4	116.95/576.25	6.39	1.00	1.81
4.0	5	5.397	74.8/539.8	142.7	95.8/555.8	119.25/579.25	4.56	.99	1.84
								1.00	1.79

Calculations

ΔH	$\frac{\Delta H}{13.6}$	γ	ΔH_q
		$\frac{V_w P_b (t_d)}{V_d (P_b + \frac{\Delta H}{13.6}) (t_w)}$	$\frac{0.0317 \Delta H}{P_b (t_{do})} \left[\frac{(t_w) \theta}{V_w} \right]^2$
1.0	0.0735		
2.0	0.147		
4.0	0.294		

γ = Ratio of accuracy of wet test meter to dry test meter. Tolerance : ± 0.01

ΔH_q = Orifice pressure differential that gives 0.75 cfm of air at 70°F and 29.92 inches of mercury, in. H₂O. Tolerance : ± 0.15

Calibrated by: MDC

ANDERSEN Samplers INC.

4801 FULTON IND. BLVD., ATLANTA, GA 30336

CONTROL UNIT CALIBRATION

Date 10-25-91

Unit Number 191-519

Barometric pressure, $P_b = 29.72$ in Hg.

Model Number 90-800

Orifice manometer setting, ΔH in. H ₂ O	Gas volume, wet test meter V_w , ft ³	Gas volume, dry gas meter V_d , ft ³	Temperature				Time θ , min	γ	ΔH_q
			Wet test Meter t_w , °R	Dry gas meter					
				Inlet t_{di} , °R	Outlet t_{do} , °R	Average t_d , °R			
1.0	5	5.279	78.2	122.1	89.5	109.3	8.4	.9976	1.25
2.0	5	5.281	78.4	135.1	90.2	112.6	6.3	1.002	1.74
4.0	5	5.289	77.0	139.6	92.2	115.9	4.5	1.003	1.76
								1.001	1.75

Calculations

ΔH	$\frac{\Delta H}{13.6}$	γ	ΔH_q
		$\frac{V_w P_b (t_d)}{V_d \left(P_b + \frac{\Delta H}{13.6} \right) \left(t_w \right)}$	$\frac{0.0317 \Delta H}{P_b (t_{do})} \left[\frac{(t_w) \theta}{V_w} \right]^2$
1.0	0.0735		
2.0	0.147		
4.0	0.294		

γ = Ratio of accuracy of wet test meter to dry test meter. Tolerance : ± 0.01

ΔH_q = Orifice pressure differential that gives 0.75 cfm of air at 70°F and 29.92 inches of mercury, in. H₂O. Tolerance : ± 0.15

Appendix 7

Process Rates

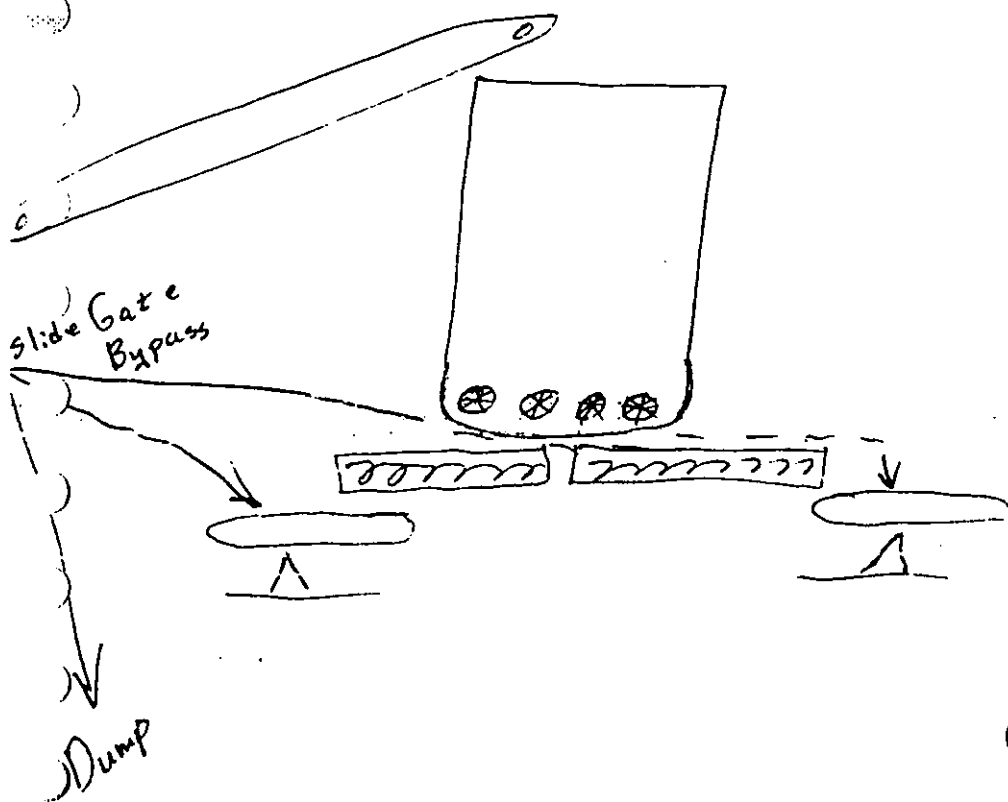
1/24/92

Jim Fater

Stack 62,695
 Recycle $\frac{8,327}{71,022}$ $> 11.72\%$ Rec. Asp. 10,596 before
~~turn down~~

0715 → 0730

Scralls having problems with "sticky" pulp -
 had to go back to slide gates. — Implications
 For Surge Bin — Need bypass to individual belts
 if plugs!



"Bypass For Scale
 Calibration"!!!

$$0.47 AP = 8,327 \quad \sqrt{= 0.686}$$

$$\text{need } 10,653$$

$$\sqrt{= 0.878}$$

$$\Delta = 0.77$$

1/24/92

SOUTH DRYER FD Air Flow

South Duct

Time	DraFt %	Instrument
1051	35.8	10.40
1054	35.5	11.22
1057	36.0	11.15
1105	33.0	7.82

North Duct

1109	33.3	6.82
1112	35.5	11.35
1116	38.7	13.39
1119	41.6	20.32
1124	41.4	20.26

North Duct

1335	40.9	20.90
1338	38.4	13.68
1341	39.6	18.43

South Duct

1344	39.8	16.20
1348	39.8	19.55

South Duct

1530	39.1	16.29
1532	37.7	14.76
1534	37.3	14.27

North Duct

1536	39.0	17.48
1538	39.7	17.51
1540	44.2	21.21
1542	47.1	23.30

Need FD
Duct Diameters
1/4 Sample Duct Locations
Cake Pan for
sampling bottom ash

FORCED DRAFT AIR FLOW

Unit F.O Location South

Static Pressure, in-H₂O 1.41

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u>1.29</u>	<u>1.1</u>	<u>125</u>
2	<u>1.28</u>	<u>1.1</u>	<u>124</u>
3	<u>1.19</u>	<u>1.1</u>	<u>123</u>
4	<u>1.19</u>	<u>1.1</u>	<u>122</u>
5	<u>1.14</u>	<u>1.1</u>	<u>121</u>
6	<u>1.01</u>	<u>1.0</u>	<u>120</u>
Average			+ 460 = T_s

Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$

$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s / 870.25})$

$v_s = \text{Feet/second}$

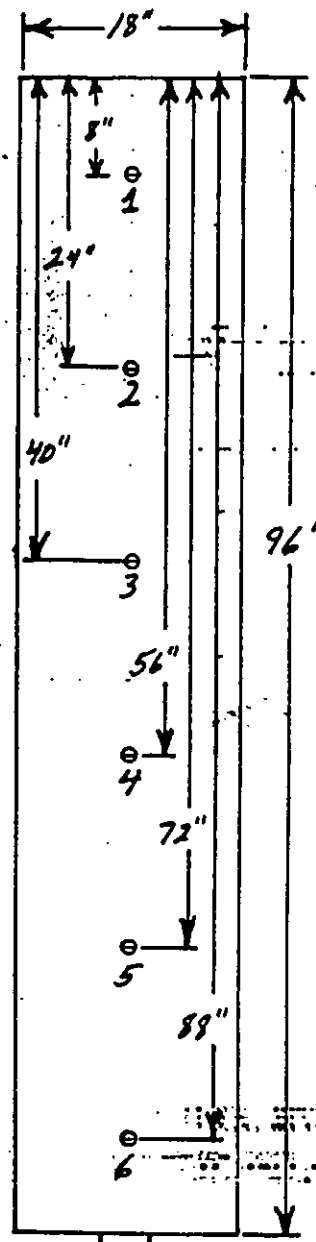
Air Flow, $V_f = v_s (A) (60 \text{ sec/min})$

$A = 12 \text{ ft}^2$

$V_f = 720 (v_s) = \text{acfm}$

FD Air Rate, $Q_F = 2381 (V_f) / (T_s)$

$Q_F = 2381 (V_f) / (T_s) = \text{lb/hr.}$



Time 11 AM

Date 1-25-92

Name

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit SOUTH Location NORTH SIDE

Static Pressure, in-H₂O -51

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u>0.11</u>	_____	<u>124</u>
2	<u>0.13</u>	_____	<u>124</u>
3	<u>0.36</u>	_____	<u>125</u>
4	<u>0.38</u>	_____	<u>126</u>
5	<u>0.58</u>	_____	<u>128</u>
6	<u>0.59</u>	_____	<u>127</u>
Average	_____	_____	<u>+ 460 = T_s</u>

Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$
 $v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s}) / 870.25$
 $v_s = \text{_____} \text{ Feet/second}$

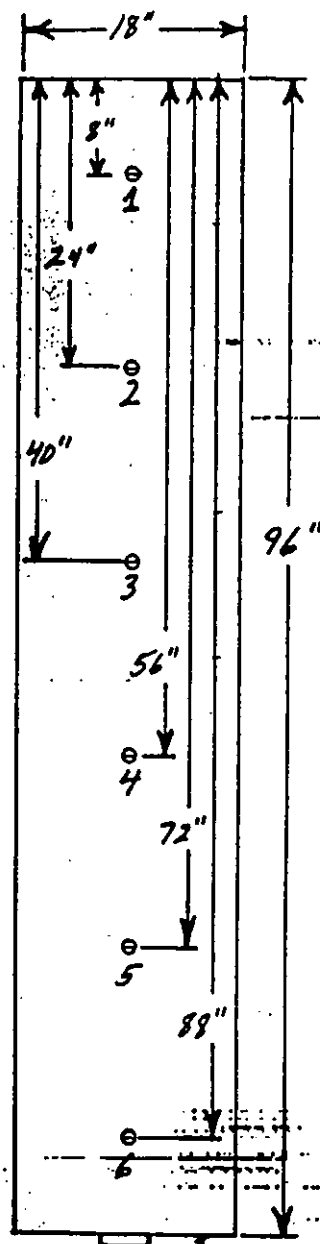
Air Flow, $V_f = v_s (A) (60 \text{ sec/min})$

$A = 12 \text{ Ft}^2$

$V_f = 720 (v_s) = \text{_____} \text{ acfm}$

FD Air Rate, $Q_F = 2381 (V_f) / (T_s)$

$Q_F = 2381 (V_f) / (T_s) = \text{_____} \text{ lb/hr.}$



Time 11:15

Date 1-25-92

Name _____

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit S. Driller Location N. Duct

Static Pressure, in-H₂O

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u>.08</u>	<u> </u>	<u>127.0</u>
2	<u>.10</u>	<u> </u>	<u>125.0</u>
3	<u>.10</u>	<u> </u>	<u>125.0</u>
4	<u>.14</u>	<u> </u>	<u>127.0</u>
5	<u>.34</u>	<u> </u>	<u>128.0</u>
6	<u>.41</u>	<u> </u>	<u>129.0</u>

Average + 460 = T_s

$$\text{Average Velocity, } v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$$

$$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s / 870.25})$$

$$v_s = \text{ } \text{ Feet/second}$$

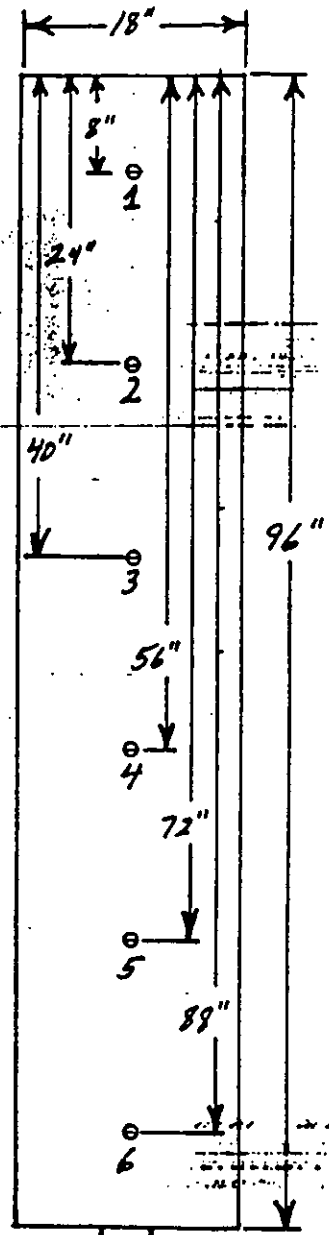
$$\text{Air Flow, } V_f = v_s (A) (60 \text{ sec/min})$$

$$A = 12 \text{ Ft}^2$$

$$V_f = 720 (v_s) = \text{ } \text{ acfm}$$

$$\text{FD Air Rate, } Q_f = 2381 (V_f) / (T_s)$$

$$Q_f = 2381 (V_f) / (T_s) = \text{ } \text{ lb/hr.}$$



Time 1:35 PM

Date 1/24/92

Name

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit S-1 Location 3

Static Pressure, in-H₂O 1.4

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
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1	<u>1.25</u>	<u> </u>	<u>125.0</u>
---	-------------	-------------------	--------------

2	<u>1.25</u>	<u> </u>	<u>127.2</u>
---	-------------	-------------------	--------------

3	<u>1.1</u>	<u> </u>	<u>125.0</u>
---	------------	-------------------	--------------

4	<u>1.04</u>	<u> </u>	<u>125.0</u>
---	-------------	-------------------	--------------

5	<u>0</u>	<u> </u>	<u>124.6</u>
---	----------	-------------------	--------------

6	<u>1.05</u>	<u> </u>	<u>124.6</u>
---	-------------	-------------------	--------------

Average + 460 = T_s

Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$

$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s}) / 870.25$

$v_s =$ Feet/second

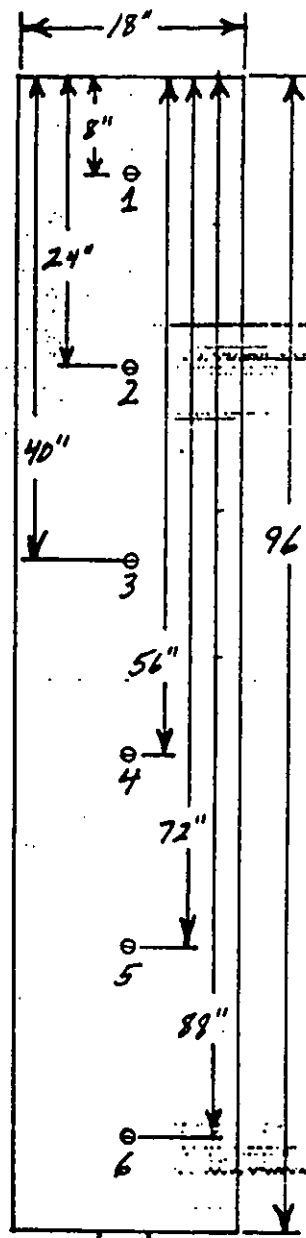
Air Flow, $V_f = v_s (A) (60 \text{ sec/min})$

$A = 12 \text{ Ft}^2$

$V_f = 720 (v_s) =$ acfm

FD Air Rate, $Q_F = 2381 (V_f) / (T_s)$

$Q_F = 2381 (V_f) / (T_s) =$ lb/hr.



Time 1:41.5 PM

Date 1/24/72

Name

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit S. Drier Location 5 D.

Static Pressure, in-H₂O 0.1

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
------------	--	-------------------	-----------------

1	0.21		125.0
---	------	--	-------

2	0.21		125.0
---	------	--	-------

3	0.21		125.0
---	------	--	-------

4	0.21		125.0
---	------	--	-------

5	0		125.0
---	---	--	-------

6	-0.05		125.0
---	-------	--	-------

Average 0.1 0.316 460 = T_s

Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$

$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s}) / 870.25$

$v_s =$ 0.316 Feet/second

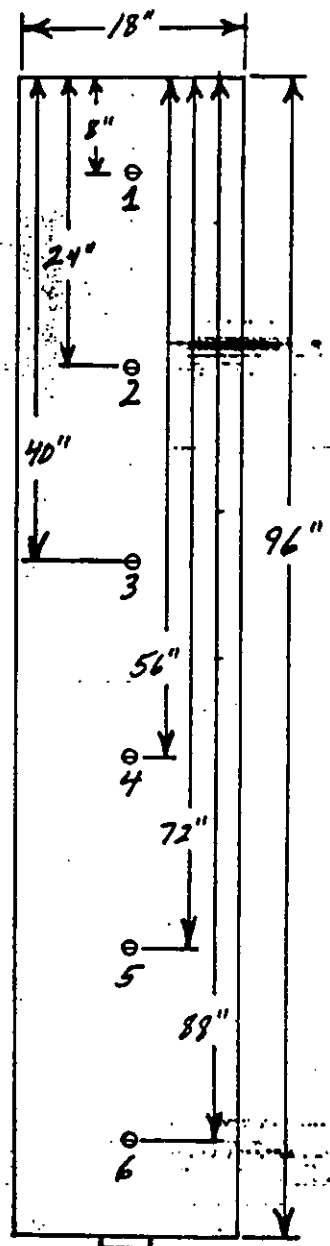
Air Flow, $V_F = v_s (A) (60 \text{ sec/min})$

$A = 12 \text{ Ft}^2$

$V_F = 720 (v_s) =$ 0.316 acfm

FD Air Rate, $Q_F = 2381 (V_F) / (T_s)$

$Q_F = 2381 (V_F) / (T_s) =$ 0.316 lb/hr.



Time 3:30 PM

Date 1/2/60

Name

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit Strip Location 101

Static Pressure, in-H₂O .52

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u> </u>	<u> </u>	<u> </u>
2	<u> </u>	<u> </u>	<u>120.2</u>
3	<u>.15</u>	<u> </u>	<u>120.2</u>
4	<u>.15</u>	<u> </u>	<u> </u>
5	<u>.57</u>	<u> </u>	<u>120.2</u>
6	<u>.46</u>	<u> </u>	<u>124.2</u>
Average	<u> </u>	<u> </u>	<u>+ 460 = T_s</u>

$$\text{Average Velocity, } v_s = 70.95 (\sqrt{\Delta P_{\text{avg}}}) (\sqrt{T_s / 870.25})$$

$$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s}) / 870.25$$

$$v_s = \text{ } \text{ Feet/second}$$

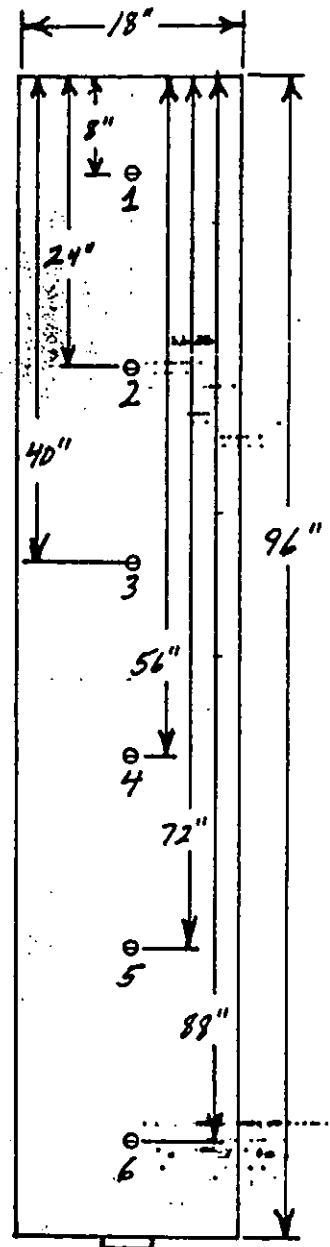
$$\text{Air Flow, } V_f = v_s (A) (60 \text{ sec/min})$$

$$A = 12 \text{ Ft}^2$$

$$V_f = 720 (v_s) = \text{ } \text{ acfm}$$

$$\text{FD Air Rate, } Q_F = 2381 (V_f) / (T_s)$$

$$Q_F = 2381 (V_f) / (T_s) = \text{ } \text{ lb/hr.}$$



Time

Date

Name

Moorhead Factory

1/24/92 Eof Day

South Stack 58⁴13
58205
58876

Rec 10,766

~~Asp~~ Asp 9,466

NORTH Stack 111,500 ACFM
200°F

15.54% Recycle

13.67% Aspiration

If 60% feed to South Unit = 34 Tph,
40% to North Unit = 23 Tph (60% Turndown = 13.8 Tph)

$$\text{Maximum} = 23 \text{ Tph-pulp} \times 0.15 = 3.45 \text{ Tph-coal}$$

$$\textcircled{a} 45\% \text{ xs-air} = 1.45 (3.45) (2000) (6.9124) = 69,159 \text{ lb-air/hr}$$

$$\textcircled{a} 131^\circ\text{F} = 17,166 \text{ acfm}$$

to get 50 fpm, need Rd Duct $\approx 5.722 \text{ ft}^2$

$$\text{ID} \approx 2.70 \text{ feet}$$

$$\text{in 30-inch Duct, } A = 4.909 \text{ ft}^2$$

$$\textcircled{a} \text{ max, } v_a = 59.28 \text{ fpm}$$

$$\text{Minimum} = 13.8 \text{ Tph-pulp} \times .15 = 2.07 \text{ Tph-coal}$$

$$\textcircled{a} 45\% \text{ xs-air} = 1.45 (2.07) (2000) (6.9124) = 41,495 \text{ lb-air/hr}$$

$$\textcircled{a} 131^\circ\text{F} = 10,300 \text{ acfm}$$

$$\text{in 30-inch Duct, } v_a = 34.97 \text{ fpm}$$

Recommend 30-inch ID Duct on North Unit

Maximum Coal Feed Rate = 4.69 Tph on 1/24/92 (1335-1349)

@ 0.15 T-coal/T-pulp $\approx$, equiv. pulp = 31.27 Tph

@ 34 Tph pulp, need 5.10 Tph-coal

$$10,200 \text{ lb-coal/hr} \div 60 = 170 \text{ lb/min}$$

$$\begin{aligned} \text{@ } 45\% \text{ x s-air, } 1.45(170) 6.7124 &= 1,704 \text{ lb-air/min} \\ &= 102,234 \text{ lb-air/hr} \\ &= 25,376 \text{ acfm} \end{aligned}$$

@ 131°F

To get 50 fpm, need $25,376 / 60(50) = 8.459 \text{ ft}^2$

Round Duct $\approx D = 3.28 \text{ ft}$

Minimum Coal Feed Rate = 3.79 Tph on 1/21/92 (1715-1730)

@ 0.15 T-coal/T-pulp, equiv. pulp = 25.27 Tph

$$60\% \text{ turndown} = 0.60 \times 34 = 20.4 \text{ Tph}$$

Use 20 Tph

$$\text{Coal} = 3 \text{ Tph} = 6,000 \text{ lb/hr}$$

$$\begin{aligned} \text{@ } 45\% \text{ x s-air, } 1.45(6,000) 6.7124 &= 60,553 \text{ lb-air/hr} \\ &= 15,030 \text{ acfm} \end{aligned}$$

in 3.28 ft duct, $v_a = 29.61 \text{ fpm}$

In 3-ft duct, $v_a \text{ max.} = 59.83 \text{ fpm}$
 $A = 7.069 \text{ ft}^2$ $\text{min.} = 35.44 \text{ fpm}$

Recommend 3-foot ID duct on South Unit

1/22/92

FORCED DRAFT AIR FLOW

Unit 30111 Location 2nd DuctStatic Pressure, in-H₂O .27

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
------------	--	-------------------	-----------------

1	<u>-.03</u>	<u>0</u>	<u>120.1</u>
---	-------------	----------	--------------

2	<u>-.01</u>	<u>0</u>	<u>120.8</u>
---	-------------	----------	--------------

3	<u>.03</u>	<u>0.173</u>	<u>121.2</u>
---	------------	--------------	--------------

4	<u>.12</u>	<u>0.346</u>	<u>122.8</u>
---	------------	--------------	--------------

5	<u>.27</u>	<u>0.520</u>	<u>125</u>
---	------------	--------------	------------

6	<u>.28</u>	<u>0.529</u>	<u>124.6</u>
---	------------	--------------	--------------

Average		<u>0.261</u>	<u>122.6 + 460 = T_s</u>
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$$\text{Average Velocity, } v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})^{582.6}$$

$$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s / 870.25})$$

$$v_s = \underline{15.15} \text{ Feet/second}$$

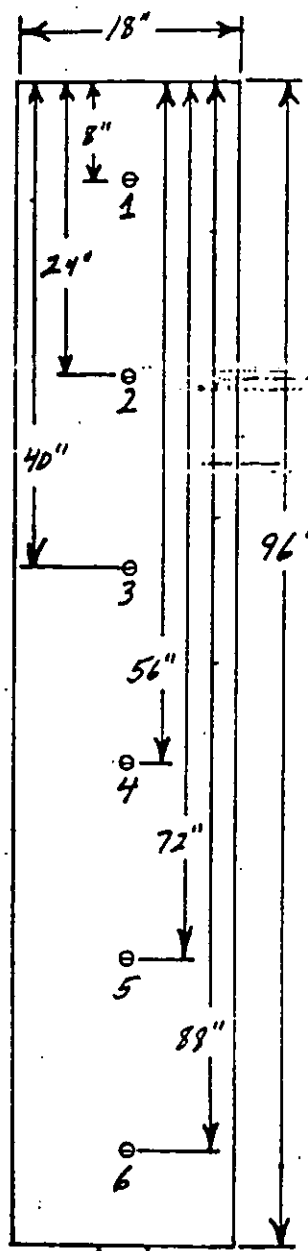
$$\text{Air Flow, } V_f = v_s (A) (60 \text{ sec/min})$$

$$A = 12 \text{ Ft}^2$$

$$V_f = 720 (v_s) = \underline{10,909} \text{ acfm}$$

$$\text{FD Air Rate, } Q_f = 2381 (V_f) / (T_s)$$

$$Q_f = 2381 (V_f) / (T_s) = \underline{\hspace{2cm}} \text{ lb/hr.}$$

Time 3:35 PMDate Name

Moorhead Factory

1/22/52

FORCED DRAFT AIR FLOW
 Unit North Drier Location North E. 2

Static Pressure, in-H₂O .25

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u> </u>	<u> </u>	<u>157.6</u>
2	<u>.03</u>	<u> </u>	<u>158.2</u>
3	<u>.07</u>	<u> </u>	<u>158.8</u>
4	<u>.08</u>	<u> </u>	<u>158.0</u>
5	<u>.07</u>	<u> </u>	<u>158.4</u>
6	<u>.08</u>	<u> </u>	<u>155.8</u>
Average	<u> </u>	<u> </u>	<u> </u> + 460 = T_s

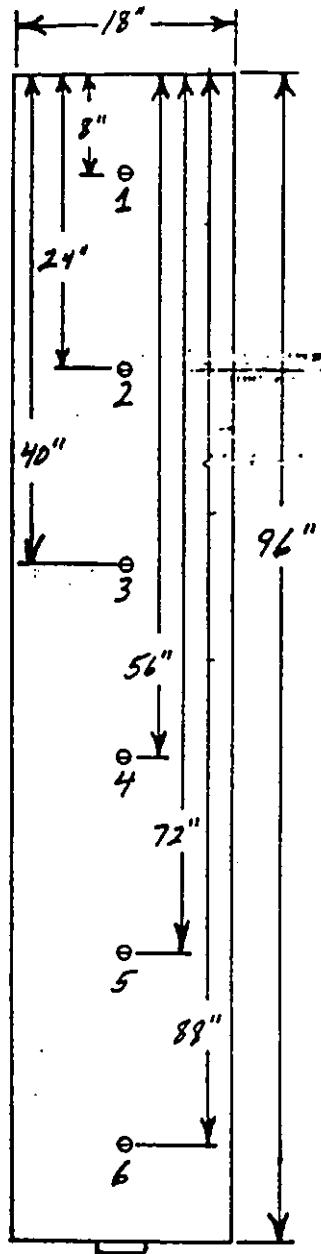
Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$
 $v_s = 70.95 (\sqrt{\Delta P} \text{ ———— }) (\sqrt{T_s \text{ ———— } / 870.25})$
 $v_s = \text{————— Feet/second}$

Air Flow, $V_f = v_s (A) (60 \text{ sec/min})$
 $A = 12 \text{ Ft}^2$

$V_f = 720 (v_s \text{ ———— }) = \text{————— acfm}$

FD Air Rate, $Q_F = 2381 (V_f) / (T_s)$

$Q_F = 2381 (V_f \text{ ———— }) / (T_s \text{ ———— }) = \text{————— lb/hr.}$



Time 3:47 PM ?
 Date
 Name

Moorhead Factory

COAL FEED RATE CHECK

Date 1/22/92

Name _____

UNIT SOUTH

Grate Speed Controller, 51.2/50.7 %, Time 1530

Elapsed Time, 8" grate section 186 seconds

Grate Speed Controller, _____ %, Time _____

Measured Grate Speed = $2,400 / (\text{elapsed time, sec}) = \underline{24.60}$ Feet/hr.

Coal Bed Depth, 5.55 inches

$$\begin{aligned}\text{Coal Feed Rate} &= \frac{4 (\text{Grate Speed } \underline{\hspace{2cm}}) (\text{Thickness } \underline{\hspace{2cm}}) (W \underline{\hspace{2cm}})^*}{2000} \\ &= \underline{4.26} \text{ Tph}\end{aligned}$$

UNIT SOUTH

Grate Speed Controller, _____ %, Time _____

Elapsed Time, 8" grate section _____ seconds

Grate Speed Controller, _____ %, Time _____

Measured Grate Speed = $2,400 / (\text{elapsed time, sec}) = \underline{\hspace{2cm}}$ Feet/hr.

Coal Bed Depth, _____ inches

$$\begin{aligned}\text{Coal Feed Rate} &= \frac{4 (\text{Grate Speed } \underline{\hspace{2cm}}) (\text{Thickness } \underline{\hspace{2cm}}) (W \underline{\hspace{2cm}})^*}{2000} \\ &= \underline{\hspace{2cm}} \text{ Tph}\end{aligned}$$

* W = Bed Width, Moorhead: NORTH = 12 Ft; SOUTH = 16 Ft.

1/22/92

end of day
1/21/92

67,835

69,280

68,753

9,729 ASP

ASP 8308

start 1/22/92

Stack 62,880

Rec 7581

70,461

1/22/92

62,008

62,933

63,313

62,751

7,267

70,018

Rec. 7,267

ASP 9,367

13.38% ASP

10.38% Recycle

End of day 1/22/92

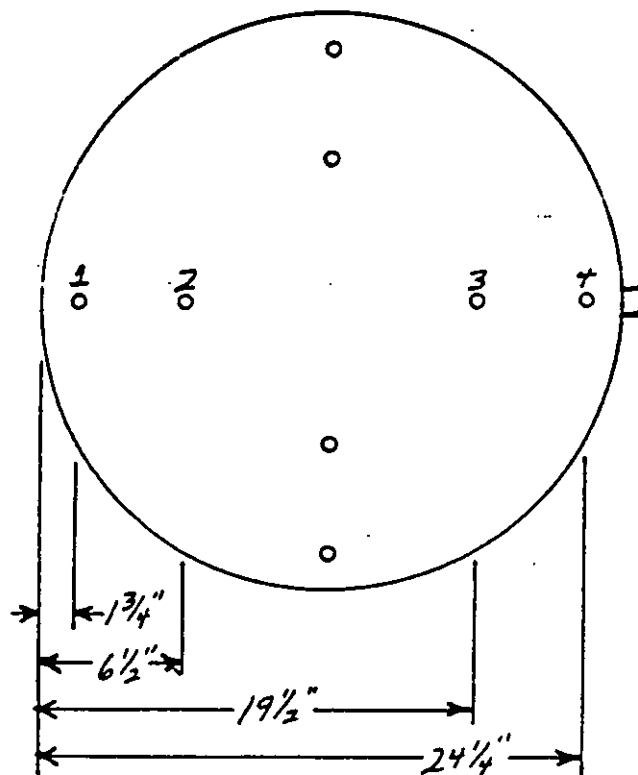
RECYCLE GAS FLOW

Unit 500 - Drier

Static Pressure, in-H₂O 4"

Diameter = 26 inches

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u>1.1</u>	<u>1.05</u>	<u>232</u>
2	<u>1.0</u>	<u>1.00</u>	<u>237</u>
3	<u>.75</u>	<u>0.866</u>	<u>238</u>
4	<u>.8</u>	<u>0.894</u>	<u>234</u>
Average	<u>0.952</u>		<u>236.8 + 460</u> <u>= T_s 696.75</u>



Average Velocity, $v_a = 70.95(\sqrt{\Delta P_{avg}})(\sqrt{T_s/761.46}) = 70.95(\sqrt{\Delta P_{0.952}})(\sqrt{T_s/761.46})$
 $v_a = \underline{64.61}$ Feet/second.

Gas Flow, $V_p = v_a (A)(60 \text{ sec/min})$ $A = 3.687 \text{ Ft}^2$
 $V_p = 221.22(v_a) = \underline{14,293}$ acfm

Time 6:30 PM

Date _____

Name _____

11/27/92
Moorhead Factory

1/20/92

Moorhead

34 Tph, ~~no~~ pulp flow

7.18 Tph Dry pulp. —

73.7% H_2O PP H_2O

Read Pulp Feeder Rpm

↑ feeders are identical, so ratios should show split of measured inlet pulp feed.

14% Asp/

1/21/92 MHD

South Unit FD flow

<u>Mgmt</u>	<u>Time</u>	<u>Draft Control</u>
So Side AP	1629	11.2
	1631	22.2
	1633	
	1635	18.5
No Side AP	1639	13.5
	1641	14.3
	1643	16.5
	1645 1647	21.0
	1649	21.6
	1651	23.5

North Duct
29, 216 lb/hr

South Viter Pulp moisture

8:00 - 3.4	8:30 3.7
9:00 5.5	9:30 10.3
10:00 7.3	10:30 9.9
11:00 - 7.6	11:00 - 8.0
11:30 - 4.8	1:00 - 6.1
12:30 7.8	1:30 6.3
2:00 - 9.1	3:00 - 7.4
2:30 - 3.1	3:30 6.8
4:00 - 8.4	4:30 - 8.6

1/24/92

dried pulp
moisture

14463
1-23-92

Press pulp Moisture

8:50	76.41
9:10	76.68
9:30	76.30
9:50	76.56
10:10	78.06
10:30	76.96
10:50	76.83
11:10	76.44
11:30	77.03
11:50	78.17
12:10	78.09
12:30	78.13
12:50	78.06
1:10	76.95
1:30	76.42
1:50	76.11
2:10	79.49
2:30	72.61
2:50	77.10
3:10	78.12
3:30	77.42
3:50	77.83
4:10	

1-24-72

8:40	78.85
8:50	78.76
8:50	78.49
9:10	78.08
9:30	77.55
9:50	77.29
10:10	77.82
10:30	76.04
10:50	78.02
11:10	79.77
11:30	78.22
11:50	78.59
12:10	79.28
12:30	77.42
12:50	78.62
1:10	78.26
1:30	79.19
1:50	78.56
2:10	78.44
2:30	78.32
2:50	76.95
3:10	78.21
3:30	77.46
3:50	77.89
4:10	76.88
4:30	78.57

Pulp Dryer Data Sheets

Date 11/24/92

Name _____

	1 Time of Day	2 Day	3 0730	4	5 0800	6 0930	7 1000	8	9 1030	1100
1	Slice Rate, Tph		210			213	208	1	192	195
2	Total Pulp Flow, Tph		42.5			45.4 45.4	55.1		60.0	56.4
3										
4	NORTH Unit									
5	Grate Speed, %						43.7		34.8	
6	ID Damper, %						94.0		94.0	
7	ID Fan, rpm						699.7		699.7	
8	Pulp Feed Gate, % open						21.46 44.5 rpm		35.63 44.5 rpm	
9	Draft Control, %						37.3		6.8	
10	FD Air Flow, MPPH						3.45		51.40	
11	BH Temp. In, °C						113		116	
12	Out, °C						108		110	
13	BH AP						6.28		6.23	
14	Multiclane, AP						3.82		3.76	
15	Dryer Throat, °C						621		586	
16	Dryer Exit, °C						131		135	
17	Furnace Pressure						-0.119		-0.64	
18	Exit Pressure						-1.48		-2.49	
19	Dryer AP						0.68		0.92	
20	Aspiration Flow, acfm						5.5		4.9	
21	Drum, amps						17.5		18.0	
22	ID Fan, amps						149		150	
23										
24										
25										
26	SOUTH Unit									
27	Grate Speed, %		27.9			60.7	58.0		52.4	46.8
28	ID Damper, %		97.0			97.0	97.0		97.0	97.0
29	ID Fan, rpm		578.1			583.5	586.1		585.4	584.6
30	Pulp Feed Gate, % open		61.8 rpm			62.7	62.2		62.2	62.2
31	Draft Control, %		-1.5			48.5	43.7		38.4	33.9
32	FD Air Flow, MPPH		0.00			24.78	21.81		16.29	8.87
33	BH Temp. In, °C		116			114	115		116	116
34	Out, °C		112			112	112		113	113
35	BH AP		2.67			2.16	2.16		2.18	2.23
36	Multiclane, AP		2.52			2.36	2.31		2.36	2.37
37	Dryer Throat, °C		696			916	865		862	808
38	Dryer Exit, °C		131			127	129		130	130
39	Furnace Pressure		-0.50			-0.13	-0.12		-0.18	-0.20
40	Exit Pressure		-1.08			-1.00	-1.00		-1.03	-1.03
41	Dryer AP		0.50.75			0.49	0.53		0.46	0.49
42	Aspiration Flow, acfm		7.8			7.8	7.7		7.7	8.0
43	Drum, amps		16.0			20.0	18.5		18.0	18.0
44	ID Fan, amps		166			166	164		164	164
45										
46										
47										
48										
49										
50										

cycled BH cleaning, left min, pulse every 3-minutes

Food Scroll Plugging (exposed in "stick" pulp), with BH overruns, resulting in "stick" pulp)

Went to Slide Gates
Back on scrolls 0910

SC 1015

35.0/35.0
8" in 492

62.7/40.0
8" in 81

wheel sage
5 1/2 5.6
same as
previous data

Pulp Dryer Data Sheets

Date 1/24/92

Name _____

	Time of Day	³ 1130	⁴ 1200	⁵ 1230	⁶	⁷ 1300	⁸ 1330	⁹ 1400	1430
1	Slice Rate, Tph	223		202		231	212	203	198
2	Total Pulp Flow, Tph	47.0		53.7		55.5	47.4	56.6	42.7
3									
4	NORTH Unit								
5	Grate Speed, %	25.0		31.0		39.9		25.0	
6	ID Damper, %	94.0		94.0		94.0		94.0	
7	ID Fan, rpm	699.7		699.7		699.7		706.6	
8	Pulp Feed Gate, % open	27.0 ^{45.7} 38.3 rpm		32.2 ^{45.1} 45.1 rpm		41.0 ^{45.1} 45.1 rpm		32.2 ^{45.1} 45.1 rpm	
9	Draft Control, %	-0.2		20.0		28.8		-0.5	
10	FD Air Flow, MPPH	—		-1.05		1.20		—	
11	BH Temp. In, °C	116		111		108		114	
12	Out, °C	111		109		105		111	
13	BH ΔP	6.29		6.29		6.31		6.26	
14	Multiclone, AP	3.75		3.90		3.91		3.77	
15	Dryer Throat, °C	503		523		530		510	
16	Dryer Exit, °C	134		124		125		125	
17	Furnace Pressure	-0.52		-0.49		-0.38		-0.71	
18	Exit Pressure	-1.80		-1.76		-1.75		-1.88	
19	Dryer ΔP	0.42		0.72		0.68		0.64	
20	Aspiration Flow, acfm	5.1		5.4		5.7		5.2	
21	Drum, amps	16.5		16.5		16.5		16.5	
22	ID Fan, amps	150		149		149		149	
23		25.0/25.0							
24		8" in 55s							
25		2.95 in wheel							
26	SOUTH Unit								
27	Grate Speed, %	57.3	56.5	47.0		50.1	57.1	53.3	46.5
28	ID Damper, %	97.0	97.0	97.0		97.0	97.0	97.0	97.0
29	ID Fan, rpm	587.2	583.8	586.9		586.7	584.3	588.2	588.2
30	Pulp Feed Gate, % open	62.2	62.2 rpm	62.2		62.2	62.2	62.2	62.2
31	Draft Control, %	41.2	41.0	31.7		35.1	43.1	38.3	32.2
32	FD Air Flow, MPPH	19.72	20.12	3.07		9.81	22.59	17.23	5.89
33	BH Temp. In, °C	115	115	116		116	115	115	116
34	Out, °C	113	113	114		114	112	113	114
35	BH ΔP	2.23	2.26	2.24		2.34	2.33	2.24	2.30
36	Multiclone, AP	2.46	2.38	2.34		2.29	2.25	2.25	2.31
37	Dryer Throat, °C	822	818	818		770	809	823	796
38	Dryer Exit, °C	130	129	131		128	128	130	130
39	Furnace Pressure	-0.15	-0.18	-0.25		-0.26	-0.15	-0.21	-0.27
40	Exit Pressure	-1.01	-1.02	-1.09		-1.09	-1.06	-1.04	-1.13
41	Dryer ΔP	0.17	0.46	0.47		0.45	0.46	0.47	0.43
42	Aspiration Flow, acfm	7.8	7.8	7.9		7.8	7.7	7.7	7.8
43	Drum, amps	20.0	20.0	18.5		18.5	20.0	17.5	18.5
44	ID Fan, amps	167	163	164		166	163	164	165
45									
46							56.0/53.9		50.6/53.4
47							8" in 90s		8" in 95s
48							↑		
49							?		
50							0		

SOT 1245

Pulp Dryer Data Sheets

Date 1/24/92

Name _____

	Time of Day	1500	1530	1600	1630	1700	
1	Slice Rate, Tph	204		204	203	212	
2	Total Pulp Flow, Tph	58.3		50.3	47.4	53.8	
3							
4	<u>NORTH Unit</u>						
5	Grate Speed, %	34.9		49.3			
6	ID Damper, %	94.0		94.0			
7	ID Fan, rpm	711.0		699.7			
8	Pulp Feed Gate, % open	75.0		75.0			
9	Draft Control, %	-3.3		29.0			
10	FD Air Flow, MPPH	—		10.41			
11	BH Temp. In, °C	115		109			
12	Out, °C	108		107			
13	BH ΔP	6.22		6.33			
14	Multiclone, AP	3.80		3.86			
15	Dryer Throat, °C	53.1		50.3			
16	Dryer Exit, °C	134		123			
17	Furnace Pressure	-0.73		-0.14			
18	Exit Pressure	-1.84		-1.63			
19	Dryer ΔP	0.60		0.73			
20	Aspiration Flow, acfm	5.7		5.3			
21	Drum, amps	16.5		16.5			
22	ID Fan, amps	14.9		14.9			
23							
24		W/hall = 23/4" 29.0/29.0					
25		measured = 2 5/8" 8" in SE					
26	<u>SOUTH Unit</u>						
27	Grate Speed, %	51.7		51.6	54.6	46.6	56.6
28	ID Damper, %	97.0		97.0	97.0	97.0	97.0
29	ID Fan, rpm	599.0		590.1	591.9	592.9	590.6
30	Pulp Feed Gate, % open	62.3		62.3 rpm	62.3 rpm	do	do
31	Draft Control, %	38.5		38.1	39.5	30.9	41.4
32	FD Air Flow, MPPH	17.32		13.31	19.24	0.00	20.07
33	BH Temp. In, °C	115		115	115	117	115
34	Out, °C	113		113	113	114	114
35	BH ΔP	2.29		2.28	2.26	2.33	2.35
36	Multiclone, AP	2.33		2.21	2.27	2.29	2.28
37	Dryer Throat, °C	77.6		82.2	83.7	81.2	78.0
38	Dryer Exit, °C	129		130	131	130	127
39	Furnace Pressure	-0.23		-0.20	-0.18	-0.26	-0.19
40	Exit Pressure	-1.09		-1.05	-1.07	-1.13	-1.06
41	Dryer ΔP	0.46		0.48	0.51	0.49	0.47
42	Aspiration Flow, acfm	7.9		7.6	7.7	7.6	7.4
43	Drum, amps	18.0		18.0	17.5	17.5	17.6
44	ID Fan, amps	16.4		16.5	16.5	16.6	16.6
45							
46		50.4/47.9		50.1/48.1			
47		8" in 99 sec		8" in 100 sec			
48		Wheel same					
49							
50							

24 HOUR

MISSIVE TEL LOG SHEET

Synth Drier, 15% Recycle, 214% Aspiration

ATE: 1/24/92

PULP DRYER:

[illegible]

TIME

SLICE (TPH)

PULP FLOWS (TPH)

DESSED

Page 1

DRYER FEED

FEEDER RPM

PRESSED

MOISTURES (%)

DRIED

GRATE SPEED

THROAT TEMP. (°C)

EXIT TEMP. (°C)

PURIN

I.C.A.P.

BAGHOUSE AP

ASP AIRFLOW

RECYCLE AIRFLOW (CFM)

1/21/92 cont'd

<u>Time</u>		<u>Draft Control</u> ✓
1915	50 Side ΔP	14.2%
1917		12.3%
1919		11.0%
1921		13.4%
1925	No Side ΔP	20.1%
1928		24.3%
1930		23.6%

Check on pulp feed

5³00 Tph slice 5% More 60% South

221 Tph slice 11.04 Tph dry solids = 52.58 Tph wet
 @ 79% H₂O ... Pulp
 60% = 31.55 Tph

50 = 26 0.52 Tph/rpm
 31.55 = 62 rpm

22-141 30 SHEETS
22-142 100 SHEETS
22-144 200 SHEETS



TIME	% SOUTH
11:00	3.5
11:30	3.2
12:00	4.1
12:30	6.1
1:00	3.3
1:30	3.7
2:00	5.2
2:30	5.7
3:00	3.1
3:30	5.7
4:00	4.4
4:30	4.4
5:00	6.1
5:30	5.7
6:00	4.3
6:30	6.2
7:00	6.3
7:30	
8:00	

WET PULP

11/21/92

TIME

10:30
10:50
11:10
11:30
11:50
12:10
12:30

Press Drip Moisture 1/21/92

Sartorius MA30 Moisture Analyzer

1/21/92

Time % Moisture

8:45	78.01
9:40	79.15
10:30	78.44
10:50	79.15
11:10	78.50
11:30	78.54
11:50	78.37
12:10	78.21
12:30	78.65
12:50	78.50
1:10	77.76
1:30	78.26
1:50	76.88
2:10	78.31
2:30	77.30
2:50	78.46
3:10	78.49
3:30	79.02
3:50	78.26
4:10	78.59
4:30	79.42
4:50	79.44
5:10	79.95
5:30	79.85
5:50	78.18
6:10	78.45
6:30	77.98
6:50	78.56
7:10	79.94
7:30	78.67
7:50	79.50

1/22/92-8:30

8:50	78.60
9:10	78.34
9:30	79.00
9:50	77.91
10:10	78.50
10:30	77.42
10:50	78.93
11:10	78.09
11:30	79.64
11:50	79.10
12:10	78.81
12:30	78.44
12:50	78.82
1:10	78.90
1:30	78.07
1:50	76.71
2:10	78.79
2:30	78.45
2:50	79.02
3:10	78.68
3:30	79.04
3:50	78.50
4:05	78.00
4:30	78.73
4:50	78.67

Pulp Dryer Data Sheets Constant pulp feed @ 51 rpm

No Recycle / $\approx 14\%$ Aspiration

Date 1/21/92

Name S.S.

	Time of Day	3 1045	4	5 1100	6	7 1315	8 1330	9
1	Slice Rate, Tph	190						
2	Total Pulp Flow, Tph	$\approx$						
3								
4	NORTH Unit							
5	Grate Speed, %	41.7						
6	ID Damper, %							
7	ID Fan, rpm							
8	Pulp Feed Gate, % open							
9	Draft Control, %							
10	FD Air Flow, MPPH							
11	BH Temp. In, °C							
12	Out, °C							
13	BH ΔP							
14	Multiclane, AP							
15	Dryer Throat, °C							
16	Dryer Exit, °C							
17	Furnace Pressure							
18	Exit Pressure							
19	Dryer ΔP							
20	Aspiration Flow, acfm							
21	Drum, amps							
22	ID Fan, amps							
23								
24								
25								
26	SOUTH Unit							
27	Grate Speed, %	76.1 / 75.8 / 42.1	37.2			38.4 / 46.0	45.7 / 49.5	
28	ID Damper, %	96.0	96.0			96.0	96.0	
29	ID Fan, rpm	588.2	589.8			590.8	589.0	
30	Pulp Feed Gate, % open	51 rpm	51			51 rpm	do	
31	Draft Control, %	28.6	6.4			8.7	25.4 / 32.9	33.7 / 34.2 / 34.5
32	FD Air Flow, MPPH	?				0.00	0.00	
33	BH Temp. In, °C	120	120			117	117	
34	Out, °C	117	118			116	115	
35	BH ΔP	2.66	2.53			2.17	2.19	
36	Multiclane, AP	2.14	2.13			2.07	2.12	
37	Dryer Throat, °C	789	785			718	737	
38	Dryer Exit, °C	133	135			130	129	
39	Furnace Pressure	-0.39	-0.47			-0.44	-0.40	
40	Exit Pressure	-1.14	-1.26			-1.29	-1.21	
41	Dryer ΔP	6.34	6.34			6.43	6.41	
42	Aspiration Flow, acfm	10.5	10.5			8.3	8.4	
43	Drum, amps	17.0	14.5			18.0	18.5	
44	ID Fan, amps	16.2	16.2			16.3	16.4	
45								
46								
47	Bed Depth Wheel	5 1/2" 5 1/2"				5 1/2" 5 1/2"	Right 7 3/4"	
48	Bed Depth Measured					5.5" 5.6"		
49								
50	Timed Grate, s/in	110 sec.				113	101	

last main pulp wheel to dryer

Test #1
Start of Testflow
desired
approx 7.0
 ≈ 11.0

Pulp Dryer Data Sheets

Date 11/21/92Name SJS

	Time of Day	1400	1430	1500	1530	1600	1630
1	Slice Rate, Tph	178	199	198	195	192	199
2	Total Pulp Flow, Tph	58.0	55.9	55.6	41.5	53.7	357.7
3							
4	NORTH Unit						
5	Grate Speed, %	38.3	34.1		28.0		
6	ID Damper, %	95.2	95.2		95.5		
7	ID Fan, rpm	552.5	552.2		552.5		
8	Pulp Feed Gate, % Open	40.0 ^{53mm}	36.6 ^{49mm}		37.8 ^{50mm}		
9	Draft Control, %	45.6	32.9		47.5		
10	FD Air Flow, MPPH	7.4	2.3		-1.4		
11	BH Temp. In, °C	115	116		117		
12	Out, °C	111	111		113		
13	BH ΔP	6.18	6.17		6.17		
14	Multiclane, AP	3.83	3.92		3.86		
15	Dryer Throat, °C	60.8	59.5		59.0		
16	Dryer Exit, °C	128	134		131		
17	Furnace Pressure	-0.32	-0.40		-0.54		
18	Exit Pressure	-1.62	-1.58		-1.75		
19	Dryer ΔP	0.96	0.72		0.67		
20	Aspiration Flow, acfm	6.1	6.1		5.6		
21	Drum, amps	16.5	16.5		17.0		
22	ID Fan, amps	148	148		148		
23							
24							
25							
26	SOUTH Unit						
27	Grate Speed, %	42.4	26.7	44.5	44.5	38.0	46.2
28	ID Damper, %	96.0	96.0	96.0	96.0	96.0	96.0
29	ID Fan, rpm	589.9	589.9	589.9	589.6	589.1	589.3
30	Pulp Feed Gate, % Open	37.1 ^{50mm}	do	do	do ^{50mm}	do	do
31	Draft Control, %	19.7	-3.3	24.3	26.0	11.0	21.2
32	FD Air Flow, MPPH	0.60	0.00	0.00	0.00	0.00	0.00
33	BH Temp. In, °C	117	119	116	116	117	116
34	Out, °C	115	116	114	114	114	115
35	BH ΔP	2.12	2.41	2.48	2.54	2.64	2.73
36	Multiclane, AP	2.04	2.06	2.10	2.10		
37	Dryer Throat, °C	76.7	71.5	72.0	75.5	73.8	70.6
38	Dryer Exit, °C	130	130	128	129	131	128
39	Furnace Pressure	-0.43	-0.50	-0.40	-0.39	-0.43	-0.39
40	Exit Pressure	-1.24	-1.29	-1.25	-1.23	-1.16	-1.24
41	Dryer ΔP	0.38	0.39	0.40	0.40	0.34	0.42
42	Aspiration Flow, acfm	8.5	8.3	8.5	8.4	8.3	8.0
43	Drum, amps	18.5	18.0	18.0	18.5	18.5	18.0
44	ID Fan, amps	162	164	164	164	164	166
45							
46							
47							
48							
49							
50							

Dryer cleaning was turned off condition days.

EOT ≈ 1515

SOT ≈ 1110

% Grate Spd
 44.2 - 46.9 42.5 - 43.5
 8" in 108mm 8" in 110.4

Pulp Dryer Data Sheets

Date 1/21/92

Name _____

	Time of Day	1700	1730		1800		1830	1900	1930
1	Slice Rate, Tph	194	197		200		191	181	
2	Total Pulp Flow, Tph	59.3	54.7		59.1		63.4	61.6	
3									
4	<u>NORTH Unit</u>								
5	Grate Speed, %		39.9					37.8	
6	ID Damper, %		96.0					96.0	
7	ID Fan, rpm		716.1					716.1	
8	Pulp Feed Gate, % open		41.0					36.4	
9	Draft Control, %		36.3					52.4	
10	FD Air Flow, MPPH		3.04					27.4	
11	BH Temp. In, °C		115					0.22	
12	Out, °C		110					11.4	
13	BH ΔP		6.28					6.24	
14	Multiclane, ΔP		3.72					3.94	
15	Dryer Throat, °C		626					625	
16	Dryer Exit, °C		132					131	
17	Furnace Pressure		-0.39					-0.48	
18	Exit Pressure		-1.61					-1.62	
19	Dryer ΔP		0.84					0.72	
20	Aspiration Flow, acfm		6.2					6.0	
21	Drum, amps		17.5					17.2	
22	ID Fan, amps		149					149	
23									
24									
25									
26	<u>SOUTH Unit</u>								
27	Grate Speed, %	46.4	39.9		40.8		39.9	45.0	41.2
28	ID Damper, %	97.0	97.0		97.0		97.0	97.0	97.0
29	ID Fan, rpm	594.2	593.4		593.4		593.3	592.9	593.4
30	Pulp Feed Gate, % open	same	do		do		do	do	do
31	Draft Control, %	30.4	10.9		12.9		13.2	26.7	21.6
32	FD Air Flow, MPPH	0	0		6		0	0	0
33	BH Temp. In, °C	115	116		115		115	114	114
34	Out, °C	114	114		113		113	112	112
35	BH ΔP	2.84	2.91		3.00		3.07	3.14	3.25
36	Multiclane, ΔP	—	—		2.09		2.03	2.04	2.04
37	Dryer Throat, °C	754	755		720		723	727	737
38	Dryer Exit, °C	129	128		127		128	126	127
39	Furnace Pressure	-0.36	-0.39		-0.61		-0.59	—	-0.64
40	Exit Pressure	-1.15	-1.27		-1.25		-1.21	-1.20	-1.22
41	Dryer ΔP	0.92	0.35		0.39		0.41	0.40	0.40
42	Aspiration Flow, acfm	8.1	8.1		8.2		8.1	8.1	8.1
43	Drum, amps	19.0	18.0		17.5		19.0	19.0	19.0
44	ID Fan, amps	168	168		168		168	168	168
45									
46									
47									
48									
49									

checked
unplugged, read -0.4" above grate zone side sight port, 1/2"
get almost -1.0" at furnace pressure gauge

EOT ≈ 1740

SOT ≈ 1825

Dust % 46.9 / 46.5

Grate % 45.6 / 44.6

8" in 1052

9" in 1092

setting on wheel = 5 1/2"

Pulp Dryer Data Sheets

Date 1/21/92

Name _____

	1 Time of Day	2 2000	3 2030	4	5	6	7	8	9
1	Slice Rate, Tph	177	186						
2	Total Pulp Flow, Tph	51.3	39.7						
3									
4	<u>NORTH Unit</u>								
5	Grate Speed, %	28.0							
6	ID Damper, %	96.0							
7	ID Fan, rpm	715.4							
8	Pulp Feed Gate, % open	2 496 FC							
9	Draft Control, %	18.5							
10	FD Air Flow, MPPH	0							
11	BH Temp. In, °C	113							
12	Out, °C	109							
13	BH ΔP	6.21							
14	Multiclone, AP	63.25							
15	Dryer Throat, °C	606							
16	Dryer Exit, °C	127							
17	Furnace Pressure	-0.54							
18	Exit Pressure	-1.67							
19	Dryer ΔP	0.73							
20	Aspiration Flow, acfm	5.7							
21	Drum, amps								
22	ID Fan, amps								
23									
24	Coal fed 3 1/4" on wheel								
25									
26	<u>SOUTH Unit</u>								
27	Grate Speed, %	39.8	43.2						
28	ID Damper, %	97.0	97.0						
29	ID Fan, rpm	593.4	592.4						
30	Pulp Feed Gate, % open	50 rpm	50.0 rpm						
31	Draft Control, %	10.9	22.4						
32	FD Air Flow, MPPH	0	0						
33	BH Temp. In, °C	115	114						
34	Out, °C	112	112						
35	BH ΔP	3.32	3.38						
36	Multiclone, AP	2.15	2.18						
37	Dryer Throat, °C	743	735						
38	Dryer Exit, °C	128	128						
39	Furnace Pressure	-0.71	-0.64						
40	Exit Pressure	-1.20	-1.17						
41	Dryer ΔP	0.42	0.40						
42	Aspiration Flow, acfm	8.1	8.1						
43	Drum, amps	17.0	17.0						
44	ID Fan, amps	167	167						
45									
46									
47									
48									
49									

EOT ≈ 2030
 Opened Recycle Damper - Front Only

COAL FEED THROUR ISS TE LOG FEET PRECIPITATED ATE: 1/21/92
 No Recycle, 14% Aspiration, 34 Tph Pulp PULP DRYER: SOUTH

TIME	1400	1430	1500	1530	1600	1630	1700	1730	1800	1830	1900	1930	2000	2030	
Slice (TPH)	196	200	207	197	195	207	1	197	195	196	186	181	185	175	
PULP FLOWS (TPH)	PRESSED		57.5	55.2	53.6	56.2	54.2	58.3	61.7	58.0	60.7	51.4	57.6	53.4	
	DRYER FEED		51	29.1	24.9	27.1	27.5	28.4	30.0	27.8	30.4	27.4	27.4	26.4	
FEEDER RPM	51		51	51	51	51	51	51	51	51	51	51	51	51	
	51		51	51	51	51	51	51	51	51	51	51	51	51	
PULP MOISTURES (%)	PRESSED														
	DRIED														
GRATE SPEED	43.3	33.9	45.3	45.3	40.4	39.6		38.8	40.0	39.5	45.0	42.6	40.0	41.9	
THROAT TEMP. (°C)	778	723	713	745	740	711		759	725	723	727	735	746	737	
EXIT TEMP. (°C)	130	131	127	129	130	129		129	128	128	127	128	128	128	
AP DRUM	0.40	0.38	0.42	0.43	0.37	0.38		0.42	0.36	0.41	0.39	0.41	0.41	0.41	
I.D. FAN RPH	589.9	589.8	589.8	590.6	590.6	590.6		593.4	593.4	593.4	593.4	592.8	593.4	592.7	
M.C. ΔP	2.11	2.12	2.12	2.08	--	--		--	2.15	2.15	2.15	2.13	2.1	2.11	
BAGHOUSE ΔP	2.16	2.10	2.14	2.52	2.63	2.73		2.91	3.00	3.08	3.13	3.22	3.30	3.38	
ASP. AIRFLOW	8.4	8.3	8.4	8.2	8.1	8.2		8.5	8.3	8.1	8.1	8.1	8.1	7.9	
RECYCLE AIRFLOW (CFM)	0	0	0	0	0	0		0	0	0	0	0	0	0	

FORCED DRAFT AIR FLOW

Unit S. Drier Location Wor. Duct

Static Pressure, in-H₂O -.37

Test Point	Differential, AP, in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
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1			115
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2	.03		113
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3	.05		114
---	-----	--	-----

4	.09		117.6
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5	.13		120.6
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83 1/2" 6	.13		122.2
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Average + 460 = T_s

Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$

$v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$

$v_s = \text{ }$ Feet/second

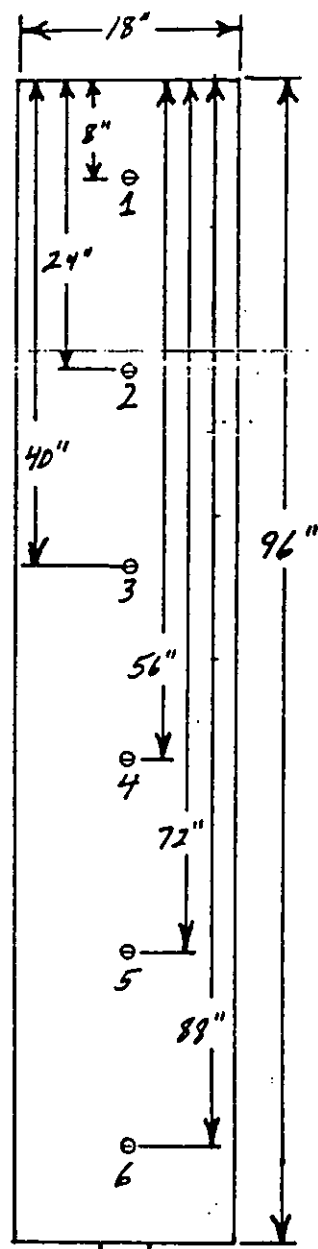
Air Flow, $V_f = v_s (A) (60 \text{ sec/min})$

$A = 12 \text{ Ft}^2$

$V_f = 720 (v_s \text{ }) = \text{ }$ acfm

FD Air Rate, $Q_F = 2381 (V_f) / (T_s)$

$Q_F = 2381 (V_f \text{ }) / (T_s \text{ }) = \text{ }$ lb/hr.



Time 10:55 PM

Date 1/21/92

Name

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit S. Drive Location South Rec

Static Pressure, in-H₂O .02

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
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1	<u>.1</u>	<u>.0.316</u>	<u>127.5</u>
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2	<u>.1</u>	<u>0.316</u>	<u>128.8</u>
---	-----------	--------------	--------------

3	<u>.06</u>	<u>0.245</u>	<u>126.6</u>
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4	<u>0</u>	<u>-</u>	<u>124.2</u>
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5	<u>0</u>	<u>-</u>	<u>123.5</u>
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3 1/2 6	<u>-.03</u>	<u>-</u>	<u>124.</u>
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Average $\sqrt{\Delta P} = \frac{0.146}{0.292}$ $T_s = 124.2 + 460 = T_s = 584.2$

Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$

$v_s = 70.95 (\sqrt{\Delta P} \frac{0.146}{0.292}) (\sqrt{T_s \frac{584.2}{870.25}})$

$v_s = \frac{17.00 \times 8.50}{17.00} \text{ Feet/second}$

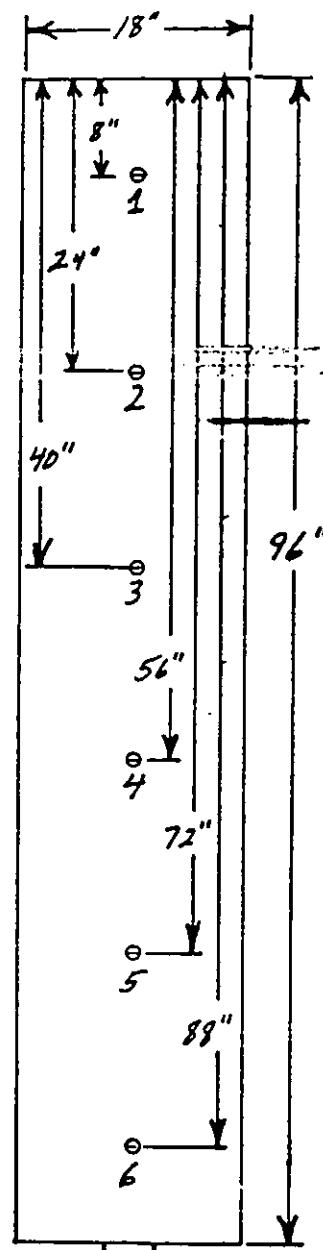
Air Flow, $V_f = v_s (A) (60 \text{ sec/min})$

$A = 12 \text{ Ft}^2$

$V_f = 720 (v_s \frac{8.50}{17.00}) = \frac{6,121}{17.00} \text{ acfm}$

FD Air Rate, $Q_f = 2381 (V_f) / (T_s)$

$Q_f = 2381 (V_f \frac{8.50}{17.00}) / (T_s \frac{584.2}{870.25}) = \frac{24,863}{49,726} \text{ lb/hr.}$



Time 1:25 P.M.

Date 1/21/92

Name _____

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit SPrier Location 1st Duct

Static Pressure, in-H₂O .06

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u>-.05</u>	<u>—</u>	<u>123.6</u>
2	<u>-.01</u>	<u>—</u>	<u>122.6</u>
3	<u>.02</u>	<u>0.141</u>	<u>122.8</u>
4	<u>.10</u>	<u>0.316</u>	<u>124.4</u>
5	<u>.27</u>	<u>0.520</u>	<u>125.6</u>
6	<u>.34</u>	<u>0.583</u>	<u>125.8</u>
Average	<u>0.260</u>	<u>0.510</u>	<u>124.1 + 460 = T_s</u>

$$\text{Average Velocity, } v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.35})$$

$$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s / 870.35})$$

$$v_s = \underline{15.11} \text{ Feet/second}$$

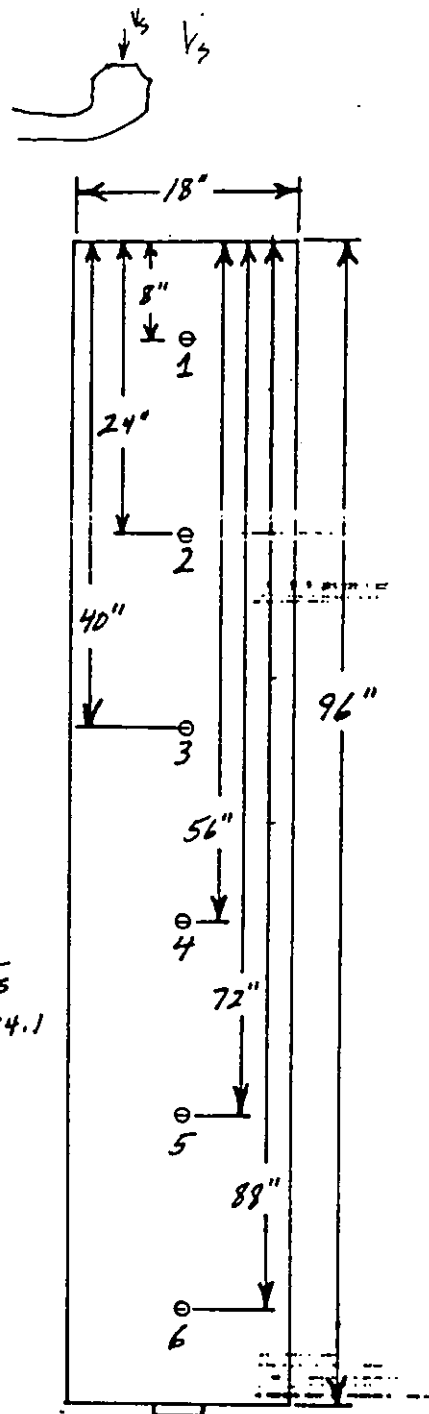
$$\text{Air Flow, } V_f = v_s (A) (60 \text{ sec/min})$$

$$A = 12 \text{ Ft}^2$$

$$V_f = 720 (v_s) = \underline{10,882} \text{ acfm}$$

$$\text{FD Air Rate, } Q_f = 2381 (V_f) / (T_s)$$

$$Q_f = 2381 (V_f) / (T_s) = \underline{44,357} \text{ lb/hr}$$



Time 1:35

Date 1/21/92

Name

Moorhead Factory

Total = 69,220 lb/hr

FORCED DRAFT AIR FLOW

Unit SDrier Location Nor Duct

Static Pressure, in-H₂O -.07

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
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1	<u>-.02</u>	<u>0</u>	<u>127.2</u>
---	-------------	----------	--------------

2	<u>-.01</u>	<u>0</u>	<u>126.4</u>
---	-------------	----------	--------------

3	<u>0</u>	<u>0</u>	<u>129.2</u>
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4	<u>.06</u>	<u>0.245</u>	<u>131.2</u>
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5	<u>.13</u>	<u>0.361</u>	<u>131.2</u>
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83 1/2 6	<u>.18</u>	<u>0.424</u>	<u>131.8</u>
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Average 0.172 129.2 + 460 = T_s
589.2

Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$

$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s / 870.25})$

$v_s = \underline{10.04}$ Feet/second

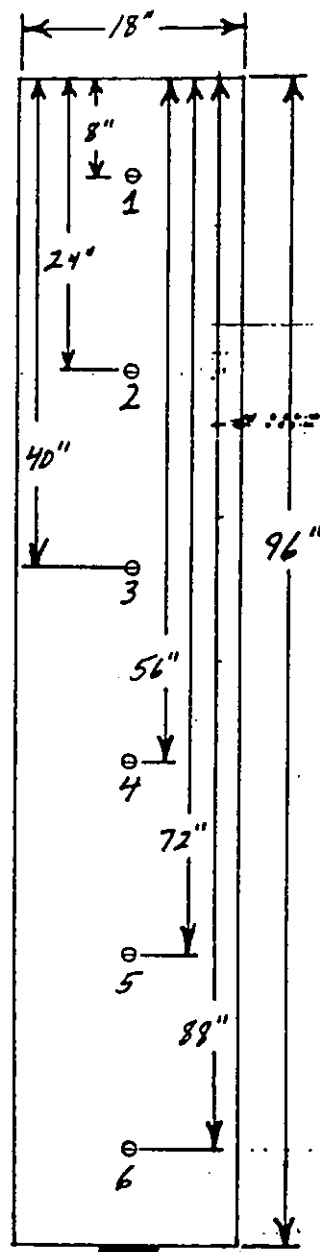
Air Flow, $V_f = v_s (A) (60 \text{ sec/min})$

$A = 12 \text{ Ft}^2$

$V_f = 720 (v_s) = \underline{7,230}$ acfm

FD Air Rate, $Q_f = 2381 (V_f) / (T_s)$

$Q_f = 2381 (V_f) / (T_s) = \underline{29,216}$ lb/hr.



Time 4:25 PM

Date 1/21/92

Name _____

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit S. Drier Location S. Line

Static Pressure, in-H₂O -.06

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u>.07</u>	<u>0.300</u>	<u>125.6</u>
2	<u>.09</u>	<u>0.300</u>	<u>125.5</u>
3	<u>.06</u>	<u>0.245</u>	<u>123.0</u>
4	<u>.02</u>	<u>0.141</u>	<u>121.4</u>
5	<u>.0</u>	<u>0</u>	<u>120.4</u>
6	<u>-.02</u>	<u>0</u>	<u>120.8</u>
Average		<u>0.164</u>	<u>122.8 + 460 = T_s</u> <u>582.8</u>

$$\text{Average Velocity, } v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$$

$$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s / 870.25})$$

$$v_s = \underline{9.52} \text{ Feet/second}$$

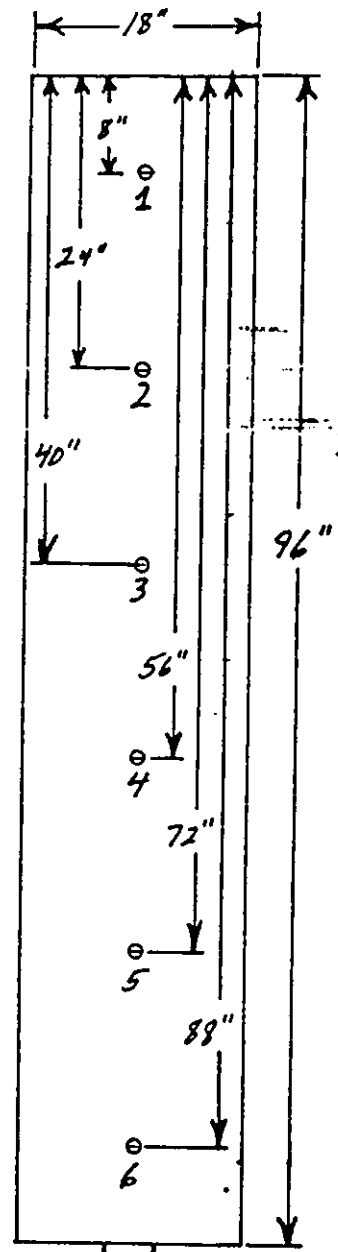
$$\text{Air Flow, } V_f = v_s (A) (60 \text{ sec/min})$$

$$A = 12 \text{ Ft}^2$$

$$V_f = 720 (v_s) = \underline{6,856} \text{ acFm}$$

$$\text{FD Air Rate, } Q_f = 2381 (V_f) / (T_s)$$

$$Q_f = 2381 (V_f) / (T_s) = \underline{28,009} \text{ lb/hr.}$$



Time 7:45

Date 1/21/92

Name _____

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit S-1111 Location S Duct

Static Pressure, in-H₂O -19

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
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1	.08		125.2
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2	.07		124.2
---	-----	--	-------

3	.04		122
---	-----	--	-----

4	0		119.2
---	---	--	-------

5	-.01		119.8
---	------	--	-------

8 3/4" 6	-.01		120
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Average _____ + 460 = T_s

Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$

$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s}) / 870.25$

$v_s =$ _____ Feet/second

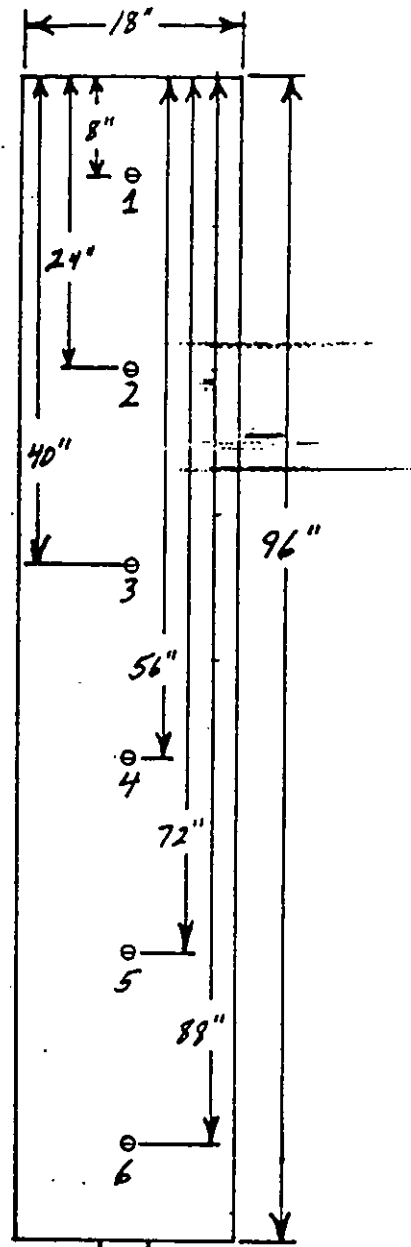
Air Flow, $V_f = v_s (A) (60 \text{ sec/min})$

$A = 12 \text{ Ft}^2$

$V_f = 720 (v_s) =$ _____ acfm

FD Air Rate, $Q_F = 2381 (V_f) / (T_s)$

$Q_F = 2381 (V_f) / (T_s) =$ _____ lb/hr.



Time 7:15

Date 1/21/92

Name _____

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit S-121 Location No. 1

Static Pressure, in-H₂O -1.13

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
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1	<u>0.02</u>	<u> </u>	<u>122.6</u>
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2	<u>0</u>	<u> </u>	<u>122.6</u>
---	----------	-----------------	--------------

3	<u>0</u>	<u> </u>	<u>122.6</u>
---	----------	-----------------	--------------

4	<u>.04</u>	<u> </u>	<u>125.8</u>
---	------------	-----------------	--------------

5	<u>.11</u>	<u> </u>	<u>127.4</u>
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83' = 6	<u>.16</u>	<u> </u>	<u>128.2</u>
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Average + 460 = T_s

$$\text{Average Velocity, } v_s = 70.95 (\sqrt{\Delta P_{\text{avg}}}) \left(\sqrt{T_s / 870.25} \right)$$

$$v_s = 70.95 (\sqrt{\Delta P_{\text{avg}}}) \left(\sqrt{T_s / 870.25} \right)$$

$$v_s = \text{ } \text{ Feet/second}$$

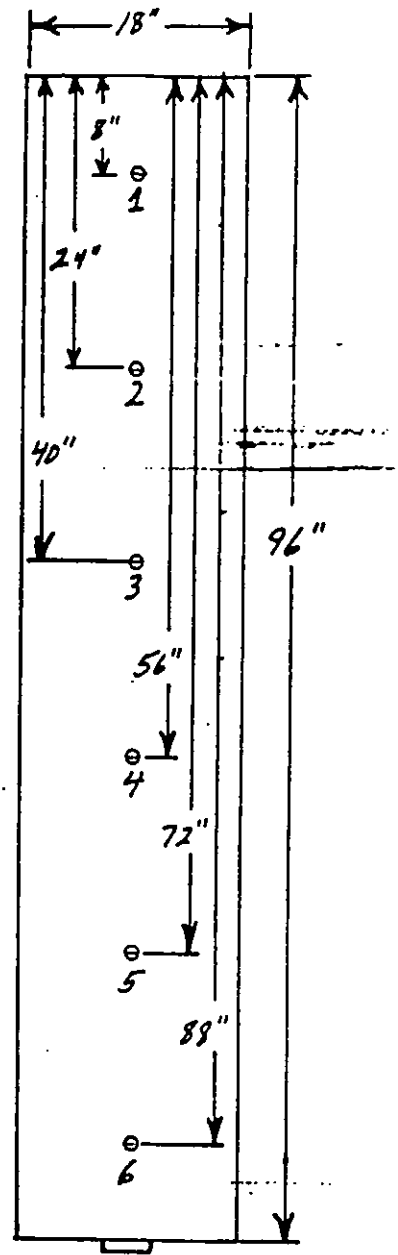
$$\text{Air Flow, } V_f = v_s (A) (60 \text{ sec/min})$$

$$A = 12 \text{ Ft}^2$$

$$V_f = 720 (v_s \text{ }) = \text{ } \text{ acfm}$$

$$\text{FD Air Rate, } Q_F = 2381 (V_f) / (T_s)$$

$$Q_F = 2381 (V_f \text{ }) / (T_s \text{ }) = \text{ } \text{ lb/hr.}$$



Time 7:25

Date 11/21/92

Name

Moorhead Factory

1/21/92

end of day
1/21/92

67,835

69,280

68,753

9,729 ASP

ASP 8308

start 1/22/92

Stack 62,880

Rec 7581

70,461

final

1/22/92

62,008

62,933

63,313

62,751

7,267

70,018

End of day 1/22/92

Rec. 7,267

ASP 8,367

13.38% ASP

10.38% Recycle

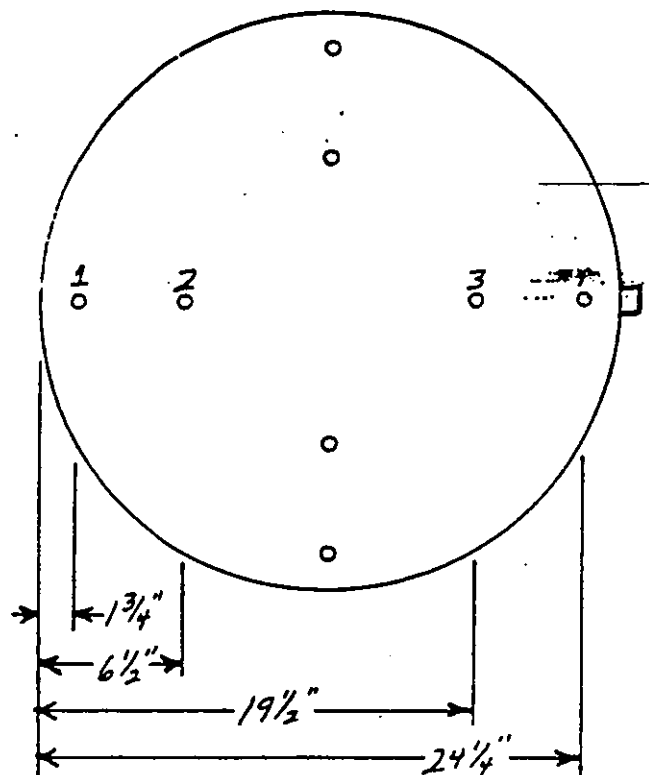
RECYCLE GAS FLOW

Unit S. D. 11

Static Pressure, in-H₂O .06

Diameter = 26 inches

Test Point	Differential, AP, in-H ₂ O	$\sqrt{AP}$	Temperature, °F
1	<u>.06</u>	<u>0.245</u>	<u>163</u>
2	<u>.06</u>	<u>0.245</u>	<u>165</u>
3	<u>.05</u>	<u>0.224</u>	<u>162</u>
4	<u>.04</u>	<u>0.2</u>	<u>162</u>
Average	<u>0.229</u>		<u>+460</u> <u>= T_s</u>



Average Velocity, $v_a = 70.95(\sqrt{AP_{avg}})(\sqrt{T_s/761.46}) = 70.95(\sqrt{AP})\left(\sqrt{\frac{T_s}{761.46}}\right)$
 $v_a = \underline{\hspace{2cm}}$ Feet/second.

Gas Flow, $V_f = v_a (A)(60 \text{ sec/min})$ $A = 3.687 \text{ Ft}^2$
 $V_f = 221.22(v_a) = \underline{\hspace{2cm}}$ acfm

Time 9:20 pm

Date 1/21/92

Name

Moorhead Factory

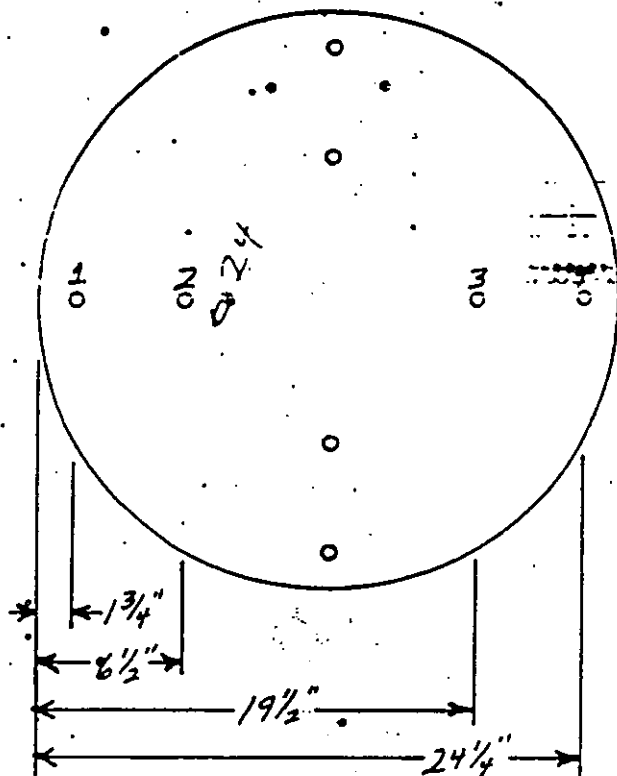
RECYCLE GAS FLOW

Unit S. L. 2

Static Pressure, in-H₂O _____

Diameter = 26 inches

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	.85	.724	161
2	.04	0.2	161
3	.04	0.2	161
4	.03	.173	160
Average			161.5 +460 = T_s 621.5



Average Velocity, $v_a = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 761.46}) = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s / 761.46})$
 $v_a = \frac{12.76}{31.19}$ Feet/second

Gas Flow, $V_f = v_a (A) (60 \text{ sec/min})$ $A = 3.687 \text{ ft}^2$

$V_f = 221.22 (v_a) = 2822 \text{ acfm}$

Time 9:00 PM

Date 1/21/92

Name _____

Moorhead Factory

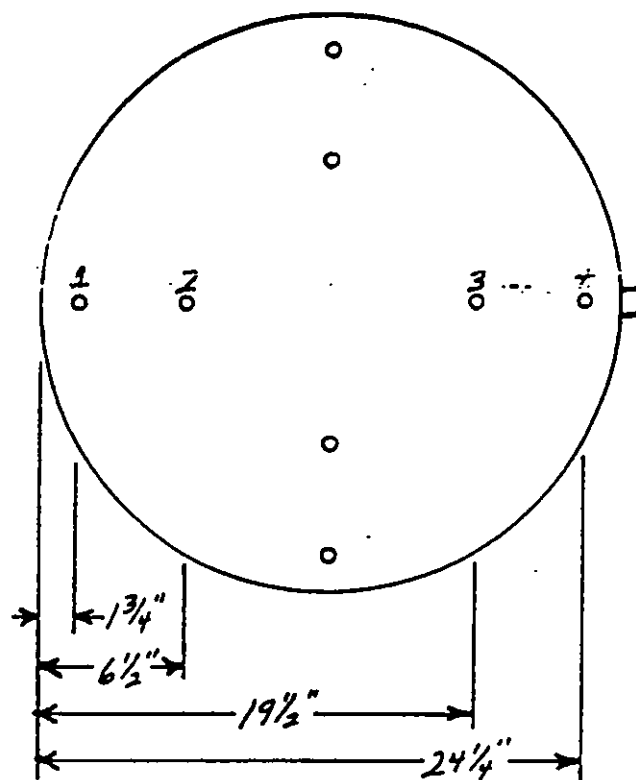
RECYCLE GAS FLOW

Unit S. Drier

Static Pressure, in-H₂O 5.2

Diameter = 26 inches

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u>.24</u>	_____	<u>164</u>
2	<u>.24</u>	_____	<u>167</u>
3	<u>.24</u>	_____	<u>167</u>
4	<u>.22</u>	_____	<u>167.8</u>
Average	_____	_____	<u>+460</u> <u>= T_s</u>



Average Velocity, $v_a = 70.95(\sqrt{\Delta P_{avg}})(\sqrt{T_s/761.46}) = 70.95(\sqrt{\Delta P})\sqrt{\frac{T_s}{761.46}}$
 $v_a =$ _____ Feet/second.

Gas Flow, $V_F = v_a (A)(60 \text{ sec/min})$ $A = 3.687 \text{ Ft}^2$
 $V_F = 221.22(v_a)$ = _____ acfm

Time 10:15

Date _____

Name _____

Moorhead Factory

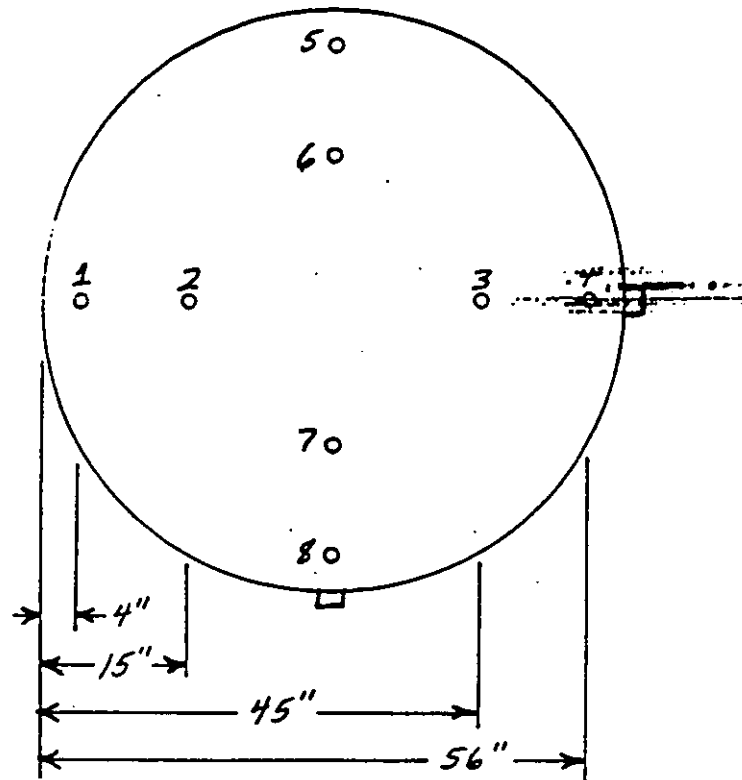
SOUTH PULP DRYER STACK

Diameter = 60 inches

Static Pressure, in-H₂O _____

Test Point	Differential, AP, in-H ₂ O	$\sqrt{AP}$	Temperature, °F
1	0.75	0.866	260
2	0.79	0.889	_____
3	0.73	0.854	_____
4	_____	_____	_____
5	_____	_____	_____
6	_____	_____	_____
7	_____	_____	_____
8	_____	_____	_____

Average $\sqrt{AP} = 0.8697$ $T_s = +460$
 $= T_s 720$



Average Velocity, $v_a = 70.95(\sqrt{AP_{avg}})(\sqrt{T_s/761.46}) = 70.95(\sqrt{AP})\sqrt{\frac{T_s}{761.46}}$
 $v_a = 60.00$ Feet/second.

Gas Flow, $V_p = v_a (A)(60 \text{ sec/min})$ $A = 19.635 \text{ ft}^2$
 $V_p = 6,178.1 (v_a) = 70,685 \text{ acfm}$

1) Fan
 88.2 rpm
 96.0% on "V"
 16 amps
 Moorhead Factory

86,000
 71,000
 15
 7,500
 71,000
 78,500

Time 10:00 PM

Date 1/20/92

Name _____

14% = 10,990

1/23/92

SOUTH DRYER FD Flow

	<u>Time</u>	<u>Damper</u>	<u>Flow Device</u>
SO Duct	{ 1013	34.9	11.27
	{ 1015	37.6	13.59
	{ 1017	37.8	14.28
NO DUCT	1020	39.0	16.25
	1022	38.5	15.18
	1024	38.3	18.81
NO Duct	{ 1315	42.7	21.65
	{ 1318	42.9	21.38
SO Duct	1323	43.6	21.53
	1326	42.3	21.15

NORTH DRYER PD Flow

1348	34.9	3.73
1350	35.6	3.53
1352	32.4	3.57
1354	32.3	2.48

SOUTH DRYER FD Flow

1530	37.8	12.92
1532	36.0	12.64
1543	39.0	15.57
1546	39.9	16.30

800 - 7.6	830 - 6.2
900 - 6.5	930 - 8.2
10 - 6.4	1030 - 6.9
110 - 6.5	1130 - 6.8
120 - 7.8	1230 - 7.1
130 - 9.1	
130 - 9.2	230 - 6.4
300 - 7.4	
330 - 8.9	400 - 6.6
400 - 8.5	

1/23/92
 Product Pulp
 Moisture
 South Dryer
 MHD

Pulp Dryer Data Sheets

Date 1/23/92

Name _____

	1 Time of Day	2 Day	3 0938	4	5 1000	6 1030	7 1100	8 1130	9 1200	
1	Slice Rate, Tph		20.2		205	186	195	193	208	
2	Total Pulp Flow, Tph		53.1		40.1	48.0	54.3	51.2	59.9	
3										
4	NORTH Unit									
5	Grate Speed, %				42.2		34.5		37.0	
6	ID Damper, %				94.0		94.0		94.0	
7	ID Fan, rpm				658.9		644.2		648.5	
8	Pulp Feed Gate, % open				30.3 ^{40 rpm}		26.7 ^{44 rpm}		26.4 ^{42 rpm}	
9	Drate Control, %				27.9		-3.3		5.2	
10	FD Air Flow, MPPH				1.28		-		-	
11	BH Temp In, °C				108		108		107	
12	Out, °C				104		104		103	
13	BH AP				6.36		6.38		6.34	
14	Multiclane, AP				3.90		3.81		3.70	
15	Dryer Throat, °C				537		549		550	
16	Dryer Exit, °C				126		125		124	
17	Furnace Pressure				-0.53		-0.82		-0.81	
18	Exit Pressure				-1.67		-2.13		-1.80	
19	Dryer AP				0.70		0.96		0.64	
20	Aspiration Flow, acfm				5.3		5.5		5.3	
21	Drum, amps				16.5		16.5		16.5	
22	ID Fan, amps				151		149		149	
23										
24										
25										
26	SOUTH Unit									
27	Grate Speed, %		50.4		52.3	50.2	50.4	53.0	55.3	
28	ID Damper, %		97.0		97.0	97.0	97.0	97.0	97.0	
29	ID Fan, rpm		583.8		582.8	584.6	583.9	582.8	579.9	
30	Pulp Feed Gate, % open		50.5 ^{42 rpm}		62.3 ^{40 rpm}	62.5	62.4	62.4	62.3	
31	Drate Control, %		36.2		38.4	36.7	36.7	40.6	39.7	
32	FD Air Flow, MPPH		13.13		14.14	12.53	14.30	18.99	18.27	
33	BH Temp In, °C		114		114	114	114	113	113	
34	Out, °C		112		112	112	112	112	111	
35	BH AP		3.09		3.15	3.29	3.31	3.41	3.48	
36	Multiclane, AP		2.46		2.57	2.46	2.44	2.56	2.56	
37	Dryer Throat, °C		762		757	765	773	782	761	
38	Dryer Exit, °C		128		127	128	128	127	127	
39	Furnace Pressure		-0.39		-0.36	-0.37	-0.37	-0.13	-0.16	
40	Exit Pressure		-0.91		-0.95	-0.90	-0.96	-1.03	-1.04	
41	Dryer AP		0.40		0.40	0.36	0.43	-0.53	-0.52	
42	Aspiration Flow, acfm		7.6		7.7	7.8	7.2	7.2	7.6	
43	Drum, amps		19.0		17.5	17.0	17.5	18.5	17.5	
44	ID Fan, amps		16.3		164	163	164	162	162	
45										
46	Wheel		5.5" SC			grate spd.	54.3/54.5			
47			5.6" NO				8" in 92 sec.			
48										
49										
50										

above grate pressure -0.15 in.

90T = 0945

flow check = 19.5% King

57.466 acfm @ 13.910 acfm @ 10.10

50T #2 = 1220

make sure you have good flow

Name _____

[illegible]

1/22/92

^{Dryer} SOUTH FD Flow	Time	Draft %	Flow Device
South Side	1055	39.1	15.55
	1058	37.9	18.19
North Side	1104	37.9	14.63
	1106	39.6	12.49

South Dryer

North Side	1319	40.5	19.91
	1321	39.8	19.73
	1323	40.4 39.8	17.27
South Side	1328	37.2 36.6	18.60
	1330	36.8	14.34
	1332	39.2	16.32

1436 - Coal to No Unit = 8" in 52 sec

46.15 ft/hr 3.1975 in - thick
3.53 Tph

Air required = $6.92 \text{ lb/lb coal} \times 1.4 \times 3.53 \times 2000 \text{ lb} = 68406 \text{ lb}$

= 16,003 AcFm = 267 acfa

for 50 fpm, need 5.33 ft^2

D = 2.606 feet.

11.1 ft²

1/22/92

SOUTH DRYER FD Flow

	<u>Time</u>	<u>Dryer %</u>	<u>Flow Device</u>
South Side	1528	35.6	11.29
North Side	1535	36.8	12.70
	1538	36.8	14.00

NORTH DRYER FD Flow

1606	5.0	?
1648	29.7	-0.37
1650	28.9	1.06
1652	29.5	1.24

adjust from 10% to $\approx$ 20% Recycle

	Pre <u>Adjust</u>	<u>Post</u>
MC AP	2.16	2.20
Throat °C	838	809
Exit °C	126	129
Furnace	-0.40	-0.31
Ex 1	-1.02	-0.99
AP Drum	0.46	0.47

~~0.47~~
-0.15" above grate

Pine Dulp Moisture 1/21/92

Sartorius MA30

Moisture Analyzer

1/21/92

Time % Moisture

8:45	78.01
9:40	79.15
10:30	78.44
10:50	79.15
11:10	78.50
11:30	78.54
11:50	78.37
12:10	78.21
12:30	78.65
12:50	78.50
1:10	77.76
1:30	78.26
1:50	76.88
2:10	78.31
2:30	77.30
2:50	78.46
3:10	78.49
3:30	79.02
3:50	78.26
4:10	78.54
4:30	79.42
4:50	79.44
5:10	79.25
5:30	78.85
5:50	78.18
6:10	78.45
6:30	77.98
6:50	78.56
7:10	79.94
7:30	78.67
7:50	79.50

1/22/92-8:30 78.27

8:50 78.60

9:10 78.34

9:30 79.00

9:50 77.91

10:10 78.50

10:30 77.42

10:50 78.93

11:10 78.09

11:30 79.64

11:50 79.10

12:10 78.81

12:30 78.44

12:50 78.82

1:10 78.90

1:30 78.07

1:50 76.71

2:10 78.79

2:30 78.45

2:50 79.02

3:10 78.68

3:30 79.04

3:50 78.50

4:05 78.00

4:30 78.73

4:50 78.67

8:30 - 11.2 - 800 - 9.3
 9:30 - 8.3 - 900 - 6.3
 10:30 - 8.9 - 10 - 98

1-22-91

South
 Pulp

Drier

11:30 - 8.9
 12:30 - 8.8
 1:30 - 8.3
 2:30 - 7.9
 3:30 - 9.3
 4:30 - 11.4

11:00 - 7.7
 1200 - 9.3
 200 - 9.9
 300 - 9.1
 4:00 7.9
 5:00 9.74

Dry Pulp Moisture

10% Recycle Rate

*David
 Watson*

Pulp Dryer Data Sheets

Date 1/22/92

Name _____

	Time of Day	³ 0830	⁴ 0900	⁵ 0930	⁶	⁷ 1000	⁸ 1030	⁹ 1100	1130
1	Slice Rate, Tph	198	187	195			192	200	192
2	Total Pulp Flow, Tph	56.5	45.6	56.8			53.2		48.3
3									
4	NORTH Unit								8" in 49 sec
5	Grate Speed, %	19.8		42.9			25.8		41.9/43.0
6	ID Damper, %	96.0		94.0			94.0		94.0
7	ID Fan, rpm	710.1		698.9			699.2		699.2
8	Pulp Feed Gate, % Open	27.20 ^{25.50} rpm		25.60 ^{28.1} rpm			22.1 ^{25.5} rpm		25.6 ^{24.38} rpm
9	Drain Control, %	-0.8		55.7			12.5		56.1
10	FD Air Flow, MPPH	—		8.46			-1.40		10.15
11	BH Temp. In, °C	119		112			118		113
12	Out, °C	113		107			112		111
13	BH ΔP	6.30		6.31	AP = 4.84		6.22		6.22
14	Multiclone, AP	3.74		3.75			3.58		3.83
15	Dryer Throat, °C	494		519			501		520
16	Dryer Exit, °C	135		126			133		123
17	Furnace Pressure	-0.82		-0.38			-0.88		-0.39
18	Exit Pressure	-1.95		-1.49			-1.80		-1.69
19	Dryer ΔP	0.65		0.70			0.57		0.75
20	Aspiration Flow, acfm	5.9		8.1			7.9		7.7
21	Drum, amps	16.0		16.5			14.5		17.0
22	ID Fan, amps	149		149			149		150
23		changed		Impact			changed		
24		cool tank		scale 3625			wheel back		
25		what from		12.5 amp			to 3 1/4		
26		3 1/4 - 5.3"							
27	SOUTH Unit								
28	Grate Speed, %	55.3	49.7	54.1			53.0	53.1	57.1
29	ID Damper, %	97.0	97.0	97.0			97.0	97.0	97.0
30	ID Fan, rpm	593.4	593.4	593.4			593.4	594.2	593.4
31	Pulp Feed Gate, % Open	50.0 ^{50.0} rpm	do	do			do	22	do
32	Drain Control, %	39.3	33.1	37.7			37.9	39.1	40.4
33	FD Air Flow, MPPH	17.93	7.24	15.32			13.72	15.37	19.24
34	BH Temp. In, °C	114	115	114			114	114	114
35	Out, °C	111	112	112			112	112	112
36	BH ΔP	4.78	4.79	5.71			2.32	2.42	2.51
37	Multiclone, AP	2.25	2.11	2.20			2.22	2.15	2.17
38	Dryer Throat, °C	783	824	822			831	798	813
39	Dryer Exit, °C	127	128	127			127	128	127
40	Furnace Pressure	-0.48	-0.47	-0.44			-0.72	-0.44	—
41	Exit Pressure	-1.15	-1.16	-1.02			-1.02	-1.11	-1.06
42	Dryer ΔP	0.50	0.47	0.47			0.48	0.44	0.48
43	Aspiration Flow, acfm	7.3	6.7	7.9			8.2	7.9	8.1
44	Drum, amps	18.0	18.0	18.5			18.0	20.0	19.0
45	ID Fan, amps	166	167	166			166	168	166
46							grt. 1/2" = 53.0/	51.9/52.7	
47							53.2		
48							5.5 5.6		
49							9" in 93 sec, 8" in 96 sec.		

changed Asp. air from 7.0 to 8.0
 North Dryer Pulp Control on Manual Operator Speed Control

BH Cleanout dropped BHA P
 from 5.75 to 5.5
 50T 1020

Pulp Dryer Data Sheets

Date 1/22/92

Name _____

	1	2	3	4	5	6	7	8	9	10
	Time of Day			1200	1230		1300	1330	1400	1430
1	Slice Rate, Tph			195	198		192	197	200	199
2	Total Pulp Flow, Tph			61.0	50.9		48.9	61.1	54.5	55.4
3										
4	NORTH Unit									
5	Grate Speed, %				30.8		30.8		32.2	
6	ID Damper, %				94.0		94.0		94.0	
7	ID Fan, rpm				698.9		699.7		699.2	
8	Pulp Feed Gate, % open				19.5% $\pm$ 32.3 rpm		23.5% $\pm$ 36.3 rpm		21.3% $\pm$ 31.5 rpm	
9	Draught Control, %				2.0		-0.9		15.0	
10	FD Air Flow, MPPH				—		—		-1.70	
11	BH Temp. In, °C				116		120		117	
12	Out, °C				111		115		113	
13	BH AP				6.24		6.17		6.24	
14	Multiclone, AP				3.62		3.68		3.61	
15	Dryer Throat, °C				540		558		561	
16	Dryer Exit, °C				132		134		129	
17	Furnace Pressure				-0.90		-0.87		-0.70	
18	Exit Pressure				-1.80		-1.96		-1.76	
19	Dryer AP				0.57		0.65		0.62	
20	Aspiration Flow, acfm				7.3		6.3		6.8	
21	Drum, amps				16.5		16.5		16.5	
22	ID Fan, amps				149		149		149	
23	med 3 1/16"				Gate 30.8		lowered coal gate		3" on wheel 3 3/16" measured thick	
24	wheel 3.33"				8" in 54 sec				32.2/32.2	
25									8" in 52 sec	
26	SOUTH Unit									
27	Grate Speed, %				51.6	55.1	57.0	52.7	48.0	57.1
28	ID Damper, %				97.0	97.0	97.0	97.0	97.0	97.0
29	ID Fan, rpm				593.4	592.9	595.0	593.4	594.5	596.0
30	Pulp Feed Gate, % open				50.5% $\pm$ 32.3 rpm	50.5% $\pm$ 32.3 rpm	62.3 rpm	62.4 rpm	62.4	62.2
31	Draught Control, %				35.6	38.3	39.0	38.0	31.0	40.5
32	FD Air Flow, MPPH				11.50	17.64	18.21	15.50	4.94	20.96
33	BH Temp. In, °C				114	114	114	114	114	113
34	Out, °C				112	112	112	112	112	111
35	BH AP				2.63	2.68	2.79	2.86	2.97	2.98
36	Multiclone, AP				2.19	2.12	2.20	2.21	2.14	2.24
37	Dryer Throat, °C				832	848	831	838	833	842
38	Dryer Exit, °C				128	128	128	129	127	128
39	Furnace Pressure				-0.43	-0.46	-0.44	-0.44	-0.46	-0.42
40	Exit Pressure				-1.01	-1.03	-1.04	-1.02	-1.04	-0.98
41	Dryer AP				0.43	0.45	0.43	0.43	0.47	0.45
42	Aspiration Flow, acfm				8.2	8.2	8.0	8.0	7.8	7.9
43	Drum, amps				19.5	18.0	18.5	18.5	20.0	18.0
44	ID Fan, amps				165	165	166	164	166	165
45										
46	med 50 5 1/2" No 5 1/2"									
47	wheel 5 1/2"				54"	56.0			54.9/57.1	
48					cont'd 52.6/52.1	56.0			8" in 91 sec	
49					8" in 93 sec	8" in 91 sec				

Pulp Dryer Data Sheets

Date 11/22/92

Name _____

	Time of Day	1500	1500	1530	1600	1630	1700	1730
1	Slice Rate, Tph	219		195	199	194	202	205
2	Total Pulp Flow, Tph	54.3		49.4	45.5	52.7	53.9	50.6
3								
4	NORTH Unit							
5	Grate Speed, %	43.0			24.7		42.7	57.0
6	ID Damper, %	94.0			94.0		94.0	94.0
7	ID Fan, rpm	677			700		698.9	698.9
8	Pulp Feed Gate, % open	25.4			32.0		33.4	30.0
9	Draft Control, %	43.1			4.8		31.6	48.6
10	FD Air Flow, MPPH	5.11					2.02	7.60
11	BH Temp, In, °C	114			120		107	108
12	Out, °C	112			115		107	104
13	BH ΔP	3.12			6.12		6.24	6.23
14	Multiclone, AP	2.13			3.53		3.80	3.73
15	Dryer Throat, °C	832			544		561	578
16	Dryer Exit, °C	127			133		114	125
17	Furnace Pressure	-0.50			-0.93		-0.57	-0.38
18	Exit Pressure	-1.06			-2.00		-1.74	-1.59
19	Dryer AP	0.46			0.59		0.79	0.74
20	Aspiration Flow, acfm	7.8			6.1		5.9	5.7
21	Drum, amps	20.0			16.5		17.5	17.0
22	ID Fan, amps	16.6			149		149	149
23								
24								47.1/45.7
25								8" in 45 sec
26	SOUTH Unit							
27	Grate Speed, %	50.8		52.3	52.5	56.6	56.6	50.8
28	ID Damper, %	97.0		97.0	97.0	97.0	97.0	97.0
29	ID Fan, rpm	596.3		597.9	597.9	593.4	596.3	598.5
30	Pulp Feed Gate, % open	62.4		67.2	62.2	same	same	same
31	Draft Control, %	37.0		37.6	34.5	41.1	39.6	35.9
32	FD Air Flow, MPPH	11.65		12.73	13.50	21.3	18.4	10.20
33	BH Temp, In, °C	114		114	114	113	114	115
34	Out, °C	112		112	112	112	112	112
35	BH ΔP	3.12		3.19	3.23	3.29	3.35	3.42
36	Multiclone, AP	2.16		2.17	2.11	2.14	2.14	2.16
37	Dryer Throat, °C	830		809	834	845	872	886
38	Dryer Exit, °C	128		127	127	125	129	128
39	Furnace Pressure	-0.49		-0.48	-0.45	-0.43	-0.42	-0.43
40	Exit Pressure	-1.08		-1.12	-1.09	-1.01	-1.05	-1.05
41	Dryer AP	0.43		0.46	0.46	0.47	0.47	0.45
42	Aspiration Flow, acfm	7.9		28	7.7	7.7	7.7	7.5
43	Drum, amps	18.0		20.0	19.0	20.0	20.5	20.5
44	ID Fan, amps	167		167	166	166	166	164
45								
46				51.2/50.7		62.7/58.3		50.4/52.1
47				8" in 141 sec		8" in 85 sec		9" in 95 sec
48								
49								

PULP DRYER: South

PULP DRYER: South																
TIME	0830	0900	0930	1000	1030	1100	1130	1200	1230	1300	1330	1400	1430	1500	1530	1600
SLICE (TPH)	191	100	202	192	189	169	196	206	204	195	197	208	183	210	233	203
PRESSED	49.6	49.3	52.7	53.1	50.5	60.2	56.3	53.7	50.2	48.8	48.9	48.8	50.2	58.3	45.7	54.5
DRYER FEED	34.3	32.4	35.5	33.6	35.9	37.1	32.5	33.1	32.3	33.3	36.2	32.1	34.6	35.8	37.3	31.9
FEEDER RPM	62.0	62.4	62.2	62.2	62.4	62.1	62.2	62.3	62.2	62.5	62.4	62.2	62.4	62.4	62.3	62.2
PRESSED																
DRIED																
PULP MOISTURES (%)																
GRATE SPEED	58.3	49.4	55.9	53.0	52.3	52.7	57.1	52.7	56.7	56.3	54.4	49.9	57.0	52.2	52.3	55.0
THROAT TEMP. (°C)	778	829	816	828	831	801	798	831	830	827	831	834	834	831	811	828
EXIT TEMP. (°C)	126	128	126	127	128	127	126	128	127	127	128	129	128	127	127	127
ΔP DRUM	0.48	0.49	0.49	0.49	0.44	0.45	0.45	0.45	0.46	0.51	0.49	0.49	0.49	0.49	0.49	0.49
I.D. FAN RPM	593.4	594.2	592.4	593.4	593.4	594.5	593.4	594.5	592.9	594.5	593.7	594.5	594.3	596.0	597.9	597.1
M.C. ΔP	2.25	2.22	2.20	2.16	2.20	2.15	2.11	2.17	2.15	2.17	2.14	2.12	2.21	2.21	2.22	2.14
BAGHOUSE ΔP	4.74	4.48	5.70		2.31	2.42	2.51	2.63	2.68	2.80	2.85	2.17	2.99	3.12	3.19	3.23
ASP. AIRFLOW	1.0	6.9	8.1	!	8.0	8.0	8.0	8.2	8.0	8.2	7.9	8.2	7.9	7.9	9.0	7.1
RECYCLE AIRFLOW (CFM)	n/a	n/a	n/a	!	n/a	n/a	n/a	n/a	n/a	n/a	w/z	n/a	n/a	n/a	n/a	n/a

1331 90, 31, 551,

ATE: /

COAL FEED ~~~~~ TYPHOID

PULP DRYER:

PULP DRYER:									
TIME	1630	1700	1730						
SLICE (TPH)	219	203	203						
PULP FLOWS (TPH)									
PRESSED	47.8	52.3	56.0						
DRYER FEED	31.8	32.0	39.5						
FEEDER RPM	62.2	62.2	62.2						
PULP MOISTURES (%)									
PRESSED									
DRIED									
GRATE SPEED	57.5	55.3	50.8						
THROAT TEMP. (°C)	86.3	96.4	98.5						
EXIT TEMP. (°C)	127	122	129						
AP DRUM	0.44	0.47	0.49						
I.D. FAN RPM	593.4	546.0	595.5						
M.C. ΔP	2.15	2.15	2.12						
BAGHOUSE ΔP	3.30	3.36	3.39						
ASP. AIRFLOW	7.4	7.8	7.6						
RECYCLE AIRFLOW (CFM)	n/a	n/a	n/a						

Unit S. Brier Location So Duc

<u>Test</u>	<u>Differential,</u>	<u>Temperature,</u>
<u>Point</u>	<u>ΔP, in-H_2O</u>	<u>$\sqrt{\Delta P}$</u>
		<u>$^{\circ}F$</u>

1 Average _____ + 460 = T_s

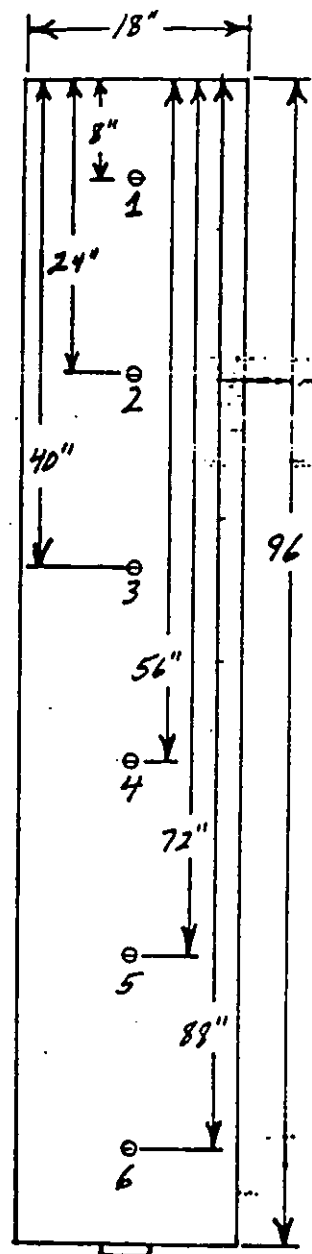
Air Flow, $V_f = v_s(A)(60 \text{ sec/min})$

$$A = 12 \text{ Ft}^2$$

$$V_f = 720(v_a \underline{\hspace{2cm}}) = \underline{\hspace{2cm}} \text{ acFm}$$

FD Air Rate, $Q_F = 2381 (V_F) / (T_s)$

$$Q_F = 2381 (V_p \underline{\hspace{1cm}}) / (T_s \underline{\hspace{1cm}}) = \underline{\hspace{1cm}} \text{ lb/hr.}$$



Time 10:50

Date 1/22/92

Name _____

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit 5511 Location IV₂ Duct

Static Pressure, in-H₂O .24

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
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1	<u>-.07</u>	<u> </u>	<u>115.0</u>
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2	<u>0</u>	<u> </u>	<u>115.8</u>
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3	<u>0</u>	<u> </u>	<u>116.4</u>
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4	<u>.12</u>	<u> </u>	<u>118.2</u>
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5	<u>.23</u>	<u> </u>	<u>119.8</u>
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6	<u>.34</u>	<u> </u>	<u>120.2</u>
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Average + 460 = T_s

Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$

$v_s = 70.95 (\sqrt{\Delta P} \text{ ———— }) (\sqrt{T_s \text{ ———— } / 870.25})$

$v_s = \text{————— Feet/second}$

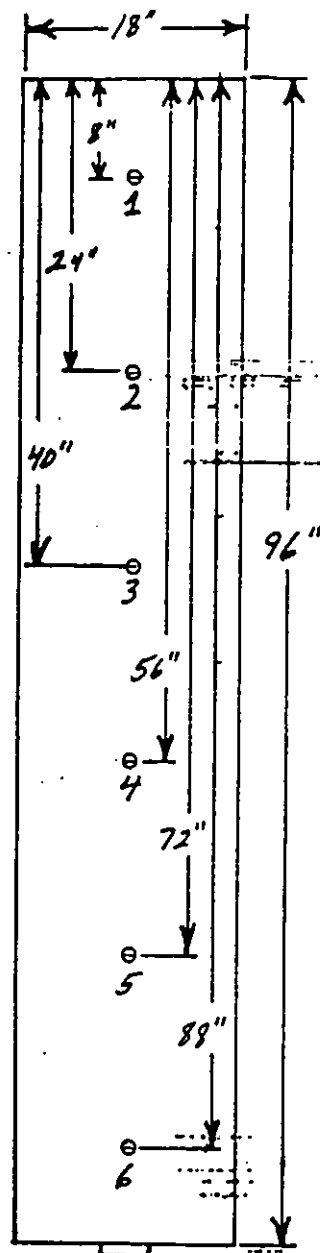
Air Flow, $V_F = v_s (A) (60 \text{ sec/min})$

$A = 12 \text{ Ft}^2$

$V_F = 720 (v_s \text{ ———— }) = \text{————— acfm}$

FD Air Rate, $Q_F = 2381 (V_F) / (T_s)$

$Q_F = 2381 (V_F \text{ ———— }) / (T_s \text{ ———— }) = \text{————— lb/hr.}$



Time 11:00

Date 11/22/92

Name

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit 535 Location N.O. Duct

Static Pressure, in-H₂O .32

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u>.04</u>	<u> </u>	<u>114.4</u>
2	<u>.02</u>	<u> </u>	<u>113.8</u>
3	<u>.04</u>	<u> </u>	<u>113.8</u>
4	<u>.14</u>	<u> </u>	<u>115.6</u>
5	<u>.35</u>	<u> </u>	<u>116.8</u>
6	<u>.41</u>	<u> </u>	<u>117.2</u>

Average + 460 = T_s

$$\text{Average Velocity, } v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$$

$$v_s = 70.95 (\sqrt{\Delta P} \text{ }) (\sqrt{T_s \text{ } } / 870.25)$$

$$v_s = \text{ } \text{ Feet/second}$$

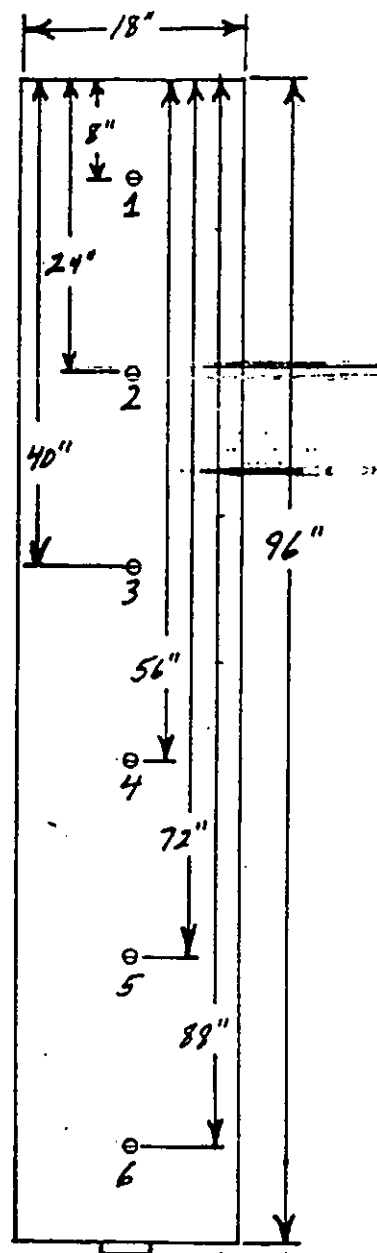
$$\text{Air Flow, } V_f = v_s (A) (60 \text{ sec/min})$$

$$A = 12 \text{ Ft}^2$$

$$V_f = 720 (v_s \text{ }) = \text{ } \text{ acfm}$$

$$\text{FD Air Rate, } Q_F = 2381 (V_f) / (T_s)$$

$$Q_F = 2381 (V_f \text{ }) / (T_s \text{ }) = \text{ } \text{ lb/hr.}$$



Time 1:20 PM

Date 1/22/92

Name

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit S Dryer Location S Duct

Static Pressure, in-H₂O .36

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
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1	.20		114.2
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2	.21		116.2
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3	.14		114.8
---	-----	--	-------

4	.04		114.0
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5	0		113.2
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6	-.02		113.0
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Average _____ + 460 = T_s

$$\text{Average Velocity, } v_s = 70.95 (\sqrt{\Delta P_{\text{avg}}}) (\sqrt{T_s / 870.25})$$

$$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s / 870.25})$$

$$v_s = \text{_____ Feet/second}$$

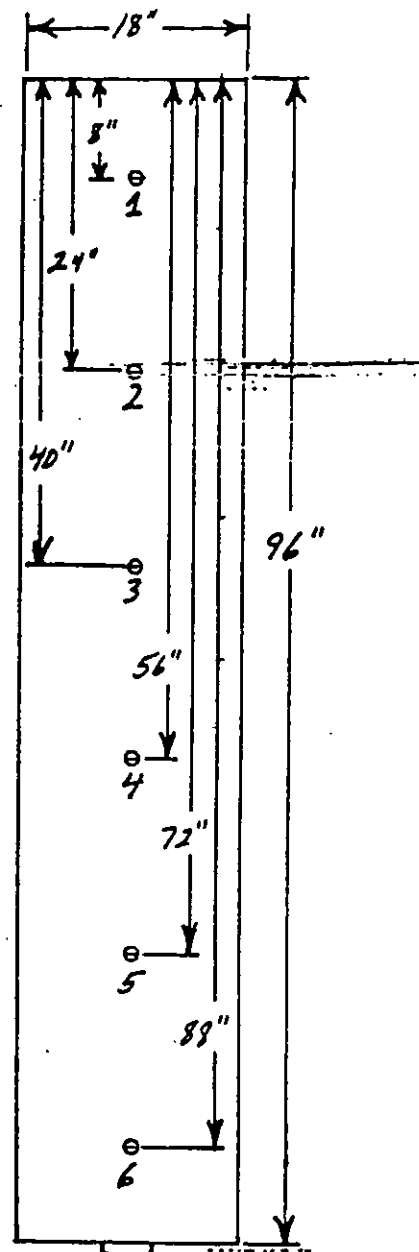
$$\text{Air Flow, } V_f = v_s (A) (60 \text{ sec/min})$$

$$A = 12 \text{ Ft}^2$$

$$V_f = 720 (v_s) = \text{_____ acfm}$$

$$\text{FD Air Rate, } Q_F = 2381 (V_f) / (T_s)$$

$$Q_F = 2381 (V_f) / (T_s) = \text{_____ lb/hr.}$$



Time 1:25 PM

Date 11/22/92

Name _____

Moorhead Factory

FORCED DRAFT AIR FLOW

1/22/92

Unit S Prier Location S. Duc +

Static Pressure, in-H₂O .22

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	.15	0.424	124.4
2	.2	0.447	124
3	.11	0.332	122.2
4	.04	0.200	121.0
5	0	0	120.6
6	-.02	0	121.0
Average		0.234	122.2 + 460 = T _s

$$\text{Average Velocity, } v_s = 70.95(\sqrt{\Delta P_{avg}})(\sqrt{T_s/870.25})$$

$$v_s = 70.95(\sqrt{\Delta P})(\sqrt{T_s/870.25})$$

$$v_s = 13.58 \text{ Feet/second}$$

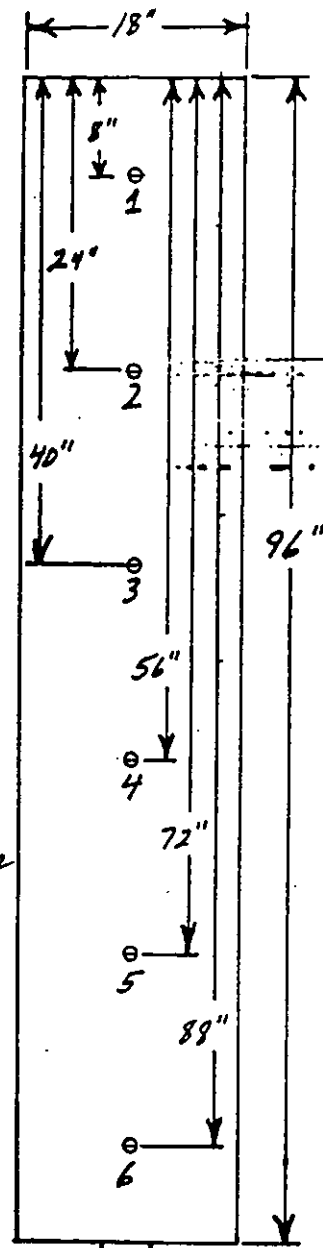
$$\text{Air Flow, } V_f = v_s(A)(60 \text{ sec/min})$$

$$A = 12 \text{ ft}^2$$

$$V_f = 720(v_s) = 9.777 \text{ acfm}$$

$$\text{FD Air Rate, } Q_f = 2381(V_f)/(T_s)$$

$$Q_f = 2381(V_f \frac{20,686}{84,600})/(T_s \frac{582.2}{84,600}) = 16/\text{hr.}$$



Moorhead Factory

$$A/f = 143.65$$

Time 3:27 PM

Date _____

Name _____

Pulp Dryer Data Sheets

Date 1/23/92

Name _____

1	Time of Day	1430	1700	5	6	7	8	9
1	Slice Rate, Tph	193	206					
2	Total Pulp Flow, Tph	62.8	54.2					
3								
4	<u>NORTH Unit</u>							
5	Grate Speed, %	45.1	32.3					
6	ID Damper, %	94.0	94.0					
7	ID Fan, rpm	698.9	698.6					
8	Pulp Feed Gate, % open	47.54 rpm	26.5 rpm					
9	Draft Control, %	16.1	5.5					
10	FD Air Flow, MPPH	-1.40	-1.40					
11	BH Temp. In, °C	108	108					
12	Out, °C	103	102					
13	BH ΔP	6.40	6.44					
14	Multiclone, ΔP	3.87	3.66					
15	Dryer Throat, °C	610	623					
16	Dryer Exit, °C	125	132					
17	Furnace Pressure	-0.46	-0.74					
18	Exit Pressure	-1.66	-1.76					
19	Dryer ΔP	0.70	0.61					
20	Aspiration Flow, acfm	5.1	5.3					
21	Drum, amps	16.5	16.5					
22	ID Fan, amps	149	149					
23								
24								
25								
26	<u>SOUTH Unit</u>							
27	Grate Speed, %	50.2	52.0					
28	ID Damper, %	97.0	97.0					
29	ID Fan, rpm	580.2	581.2					
30	Pulp Feed Gate, % open	53.2 rpm	62.2 rpm					
31	Draft Control, %	36.2	38.7					
32	FD Air Flow, MPPH	13.47	15.21					
33	BH Temp. In, °C	114	114					
34	Out, °C	111	111					
35	BH ΔP	4.14	4.28					
36	Multiclone, ΔP	2.44	2.46					
37	Dryer Throat, °C	787	770					
38	Dryer Exit, °C	129	127					
39	Furnace Pressure	-0.16	-0.16					
40	Exit Pressure	-0.89	-1.01					
41	Dryer ΔP	0.40	0.77					
42	Aspiration Flow, acfm	7.4	7.7					
43	Drum, amps	17.5	18.0					
44	ID Fan, amps	163	164					
45								
46								
47								
48								
49								

FORCED DRAFT AIR FLOW

Unit S. Drier Location So Duct

Static Pressure, in-H₂O .34

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u>.19</u>	<u> </u>	<u>122.0</u>
2	<u>.12</u>	<u> </u>	<u>121.6</u>
3	<u>.12</u>	<u> </u>	<u>120.0</u>
4	<u>.03</u>	<u> </u>	<u>118.4</u>
5	<u>0</u>	<u> </u>	<u>118.2</u>
6	<u>0</u>	<u> </u>	<u>118.2</u>
Average	<u> </u>	<u> </u>	<u> </u> + 460 = T_s

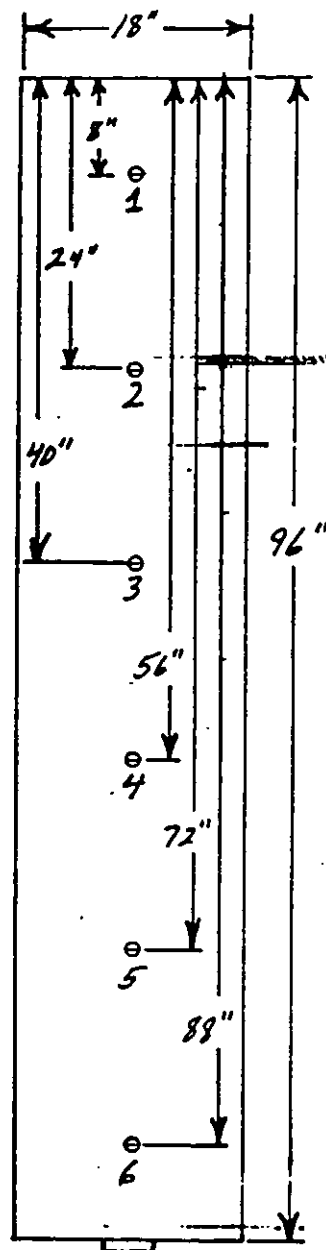
Average Velocity, $v_s = 70.95(\sqrt{\Delta P_{avg}})(\sqrt{T_s/870.25})$
 $v_s = 70.95(\sqrt{\Delta P})(\sqrt{T_s/870.25})$
 $v_s = \text{ }$ Feet/second

Air Flow, $V_f = v_s (A) (60 \text{ sec/min})$
 $A = 12 \text{ ft}^2$

$V_f = 720(v_s \text{ }) = \text{ }$ acfm

FD Air Rate, $Q_F = 2381(V_f)/(T_s)$

$Q_F = 2381(V_f \text{ })/(T_s \text{ }) = \text{ }$ lb/hr.



Moorhead Factory



Time 10:15 AM

Date 1/23/92

Name Bill Bergin

FORCED DRAFT AIR FLOW

Unit S Drier Location North Duct

Static Pressure, in-H₂O .35

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
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1	<u>-.01</u>	<u> </u>	<u>119.0</u>
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2	<u>-.01</u>	<u> </u>	<u>118.3</u>
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3	<u>.02</u>	<u> </u>	<u>119.0</u>
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4	<u>.12</u>	<u> </u>	<u>121.6</u>
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5	<u>.3</u>	<u> </u>	<u>122.8</u>
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83 1/2 6	<u>.37</u>	<u> </u>	<u>123.2</u>
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Average + 460 = T_s

Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$

$v_s = 70.95 (\sqrt{\Delta P} \text{ ———— }) (\sqrt{T_s \text{ ———— } / 870.25})$

$v_s = \text{————— Feet/second}$

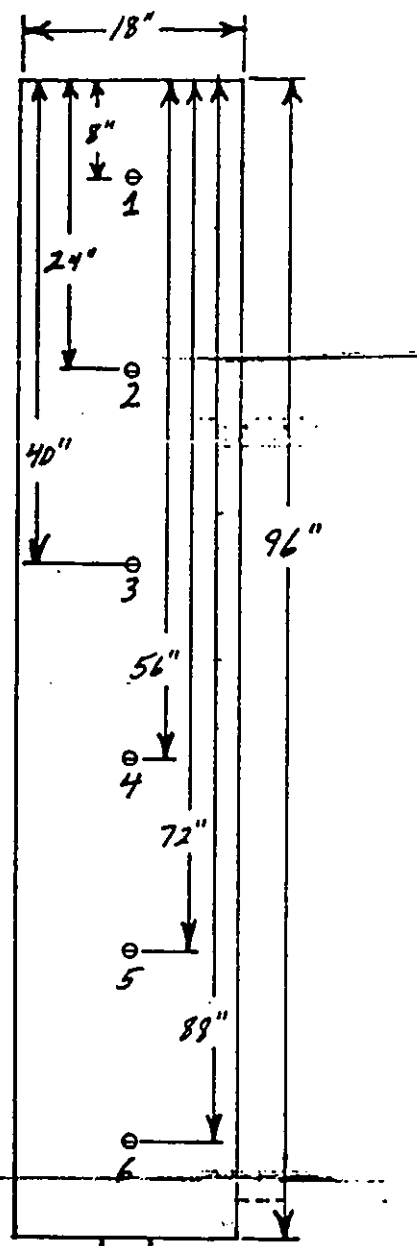
Air Flow, $V_f = v_s (A) (60 \text{ sec/min})$

$A = 12 \text{ Ft}^2$

$V_f = 720 (v_s \text{ ———— }) = \text{————— acfm}$

FD Air Rate, $Q_f = 2381 (V_f) / (T_s)$

$Q_f = 2381 (V_f \text{ ———— }) / (T_s \text{ ———— }) = \text{————— lb/hr.}$



Time 10:20 AM

Date 1/23/92

Name

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit S Drier Location No. 1 Drier

Static Pressure, in-H₂O .52

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
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1	<u>-.11</u>	<u> </u>	<u>121.4</u>
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2	<u>.02</u>	<u> </u>	<u>12.1</u>
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3	<u>.04</u>	<u> </u>	<u>120.8</u>
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4	<u>.18</u>	<u> </u>	<u>122.8</u>
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5	<u>.36</u>	<u> </u>	<u>124.0</u>
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83 1/2 6	<u>.45</u>	<u> </u>	<u>124.4</u>
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Average + 460 = T_s

Average Velocity, $v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$

$v_s = 70.95 (\sqrt{\Delta P} \text{ ———— }) (\sqrt{T_s \text{ ———— } / 870.25})$

$v_s = \text{————— Feet/second}$

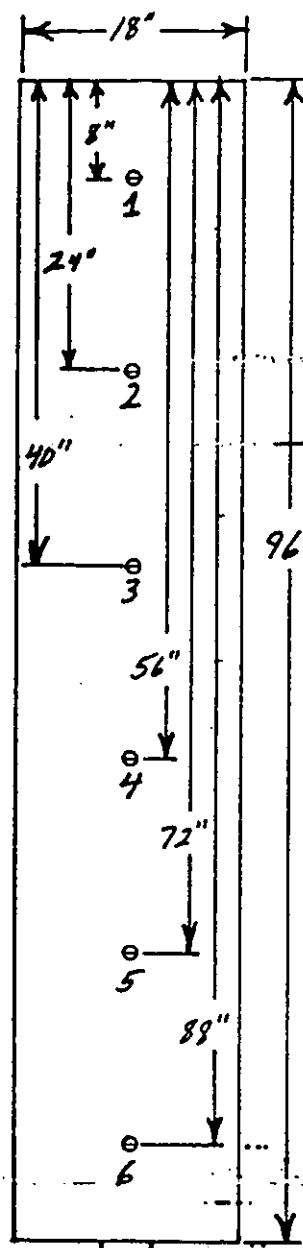
Air Flow, $V_f = v_s (A) (60 \text{ sec/min})$

$A = 12 \text{ Ft}^2$

$V_f = 720 (v_s \text{ ———— }) = \text{————— acfm}$

FD Air Rate, $Q_f = 2381 (V_f) / (T_s)$

$Q_f = 2381 (V_f \text{ ———— }) / (T_s \text{ ———— }) = \text{————— lb/hr.}$



Time 1:15 PM

Date 1/23/92

Name

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit Santa Clara Location S. B.

Static Pressure, in-H₂O .54

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u>.231</u>	_____	<u>122.8</u>
2	<u>.78</u>	_____	<u>122.4</u>
3	<u>.16</u>	_____	<u>121.2</u>
4	<u>.05</u>	_____	<u>120</u>
5	<u>0</u>	_____	<u>120</u>
6	<u>-.06</u>	_____	<u>120.2</u>
Average	_____	_____	_____ + 460 = T_s

$$\text{Average Velocity, } v_s = 70.95 (\sqrt{\Delta P_{avg}}) (\sqrt{T_s / 870.25})$$

$$v_s = 70.95 (\sqrt{\Delta P}) (\sqrt{T_s / 870.25})$$

$$v_s = \text{_____ Feet/second}$$

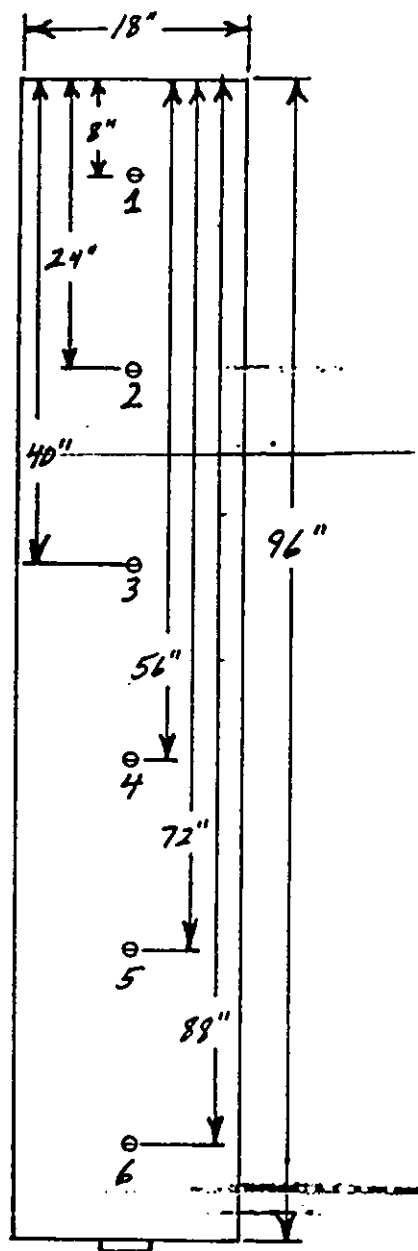
$$\text{Air Flow, } V_F = v_s (A) (60 \text{ sec/min})$$

$$A = 12 \text{ Ft}^2$$

$$V_F = 720 (v_s) = \text{_____ acfm}$$

$$\text{FD Air Rate, } Q_F = 2381 (V_F) / (T_s)$$

$$Q_F = 2381 (V_F) / (T_s) = \text{_____ lb/hr.}$$



Time 1:23 PM

Date 1/23/92

Name _____

Moorhead Factory

FORCED DRAFT AIR FLOW

Unit No. 1 Location No. 1

Static Pressure, in-H₂O .49

Test Point	Differential, ΔP , in-H ₂ O	$\sqrt{\Delta P}$	Temperature, °F
1	<u>.0</u>	<u> </u>	<u>124.6</u>
2	<u>.05</u>	<u> </u>	<u>125.8</u>
3	<u>.11</u>	<u> </u>	<u>126.4</u>
4	<u>.15</u>	<u> </u>	<u>126.6</u>
5	<u>.15</u>	<u> </u>	<u>126.4</u>
6	<u>.14</u>	<u> </u>	<u>126.6</u>

Average + 460 = T_s

$$\text{Average Velocity, } v_s = 70.95 (\sqrt{\Delta P_{\text{avg}}}) (\sqrt{T_s / 870.25})$$

$$v_s = 70.95 (\sqrt{\Delta P} \text{ }) (\sqrt{T_s \text{ } } / 870.25)$$

$$v_s = \text{ } \text{ Feet/second}$$

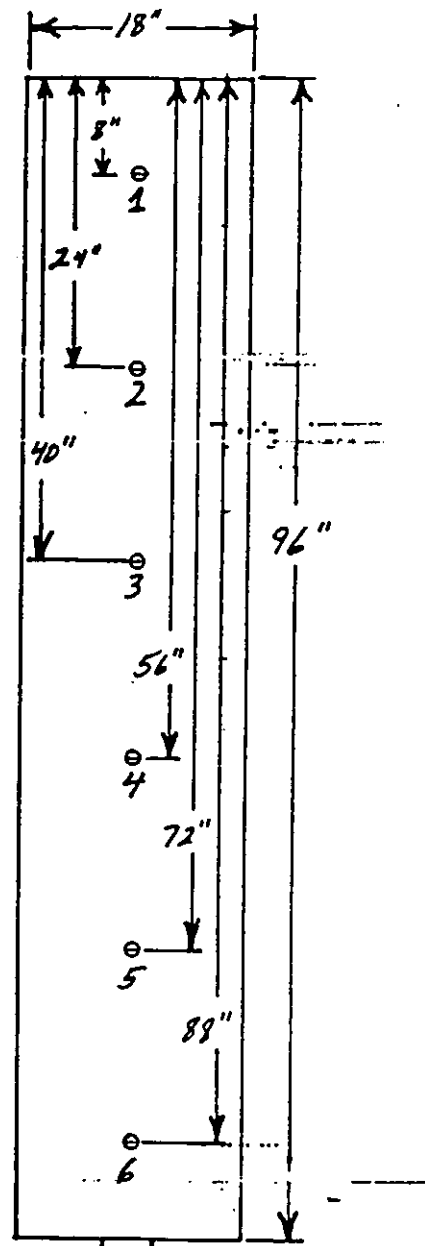
$$\text{Air Flow, } V_F = v_s (A) (60 \text{ sec/min})$$

$$A = 12 \text{ Ft}^2$$

$$V_F = 720 (v_s \text{ }) = \text{ } \text{ acfm}$$

$$\text{FD Air Rate, } Q_F = 2381 (V_F) / (T_s)$$

$$Q_F = 2381 (V_F \text{ }) / (T_s \text{ }) = \text{ } \text{ lb/hr.}$$



Time 1:52 PM

Date 1/23/92

Name

Moorhead Factory

ROOF DRAFT AIR FLOW

Unit 5-1-1 Location Pl. Duct

Static Pressure in-H₂O .19

Test Point	Differential, DP, in-H ₂ O	$\sqrt{DP}$	Temperature, °F
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1	.06		122.6
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2	.02		122.0
---	-----	--	-------

3	.02		122.6
---	-----	--	-------

4	.1		125.2
---	----	--	-------

5	.21		127.2
---	-----	--	-------

6	.25		127.6
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Average + 460 = T_s

Average Velocity, $V_s = 70.95(\sqrt{DP_{avg}})(\sqrt{T_s/870.35})$

$V_s = 70.95(\sqrt{DP}) \sqrt{(T_s)/870.35}$

$V_s =$ Feet/second

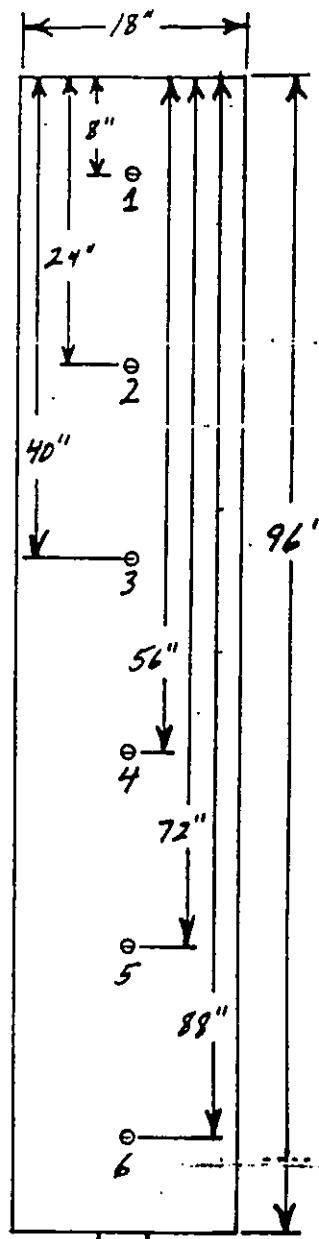
Air Flow, $Q_s (ft^3/min)$ (60 sec/min)

$A = 12 ft^2$

$Q_s = 720(V_s)$ = acfm

FD, $Q_F = 2381(V_F)/(T_s)$

$Q_F = 2381(V_F)$ = lb/hr.



Time 3:35 PM

Date 1-3-92

Name

Mac Factory

FORCED DRAFT AIR FLOW

Unit South Drier Location 5. Dec

Static Pressure in-H₂O 30

Point	ΔP, in-H ₂ O	√ΔP	Temperature, °F
1	.22		125
2	.22		124.4
3	.13		122.8
4	.04		121.6
5	0		121.2
6	.04		120.8
Average			+460 = T _s

$$\text{Average } v_s = 70.95 (\Delta P_{\text{avg}})^{1/2} (\sqrt{T_s / 870.35})$$

$$v_s = 70.95 (\Delta P)^{1/2} (\sqrt{T_s / 870.35})$$

$$v_s = \text{Feet/second}$$

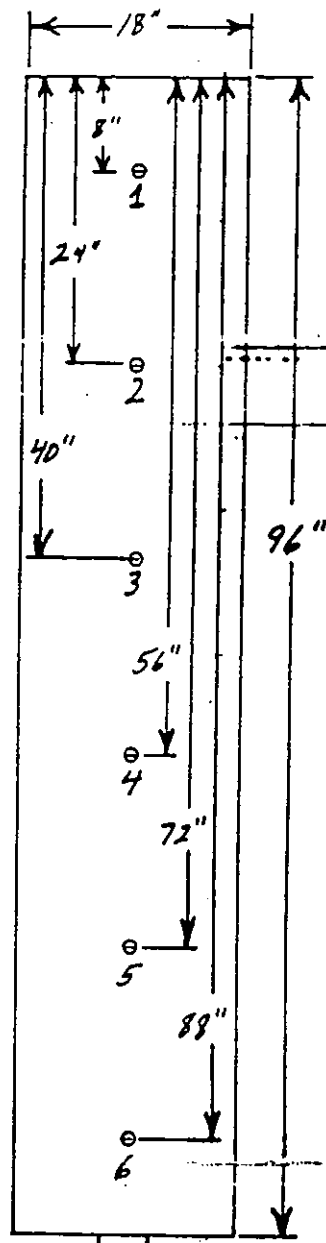
$$\text{Air Flow } Q_F = 25 (A) (60 \text{ sec/min})$$

$$A = 12 \text{ Ft}^2$$

$$Q_F = 720 (v_s) = \text{acfm}$$

$$\text{FD Air Flow } Q_F = 2381 (V_F) / (T_s)$$

$$Q_F = 2381 (V_F) / (T_s) = \text{lb/hr.}$$



Time 3:42 P.M.

Date 12-2-55

Name

Moisture 4.0

11/23/92

End of Day

Stack	57,409	Rec	14,680
	57,155		
	57,023	Asp	8,629
	57,196		

20.42% Rec.

12.01 Asp