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AP-42 Section Number: 9.10.2.1

Reference Number: 10

Title: Emission Testing on Two Baghouses
at Harris Woolf California Almonds

Steiner Environmental, Inc.

Steiner Environmental, Inc.

October 1991

AP-42 Section 9.10.2
Reference 10
Report Sect. _____
Reference _____

**EMISSION TESTING ON TWO BAGHOUSES
AT HARRIS WOOLF CALIFORNIA ALMONDS**

September 23 and 27, 1991

Prepared for:

Harris Woolf California Almonds
Route 1, Box 470
Coalinga, California 93210

October 1991

Prepared by:

Steiner Environmental, Inc.
4930 Boylan Street
Bakersfield, California 93308

Report PS-91-2572/Project 7082-91

SECTION 1
INTRODUCTION

At the request of Harris Woolf California Almonds, Steiner Environmental, Inc. conducted a series of emission tests on the effluent of two baghouses located at their almond processing plant located near Coalinga, California. These tests were conducted on September 23 and September 27, 1991. The purpose of these tests was to determine compliance with Fresno County APCD Rules and Regulations.

Almonds are hauled to the plant by trucks and are bottom dumped into a pit with a conveyor. The emissions from this almond receiving/pre-cleaning facility (Permit to Operate No. 1140140101R) are controlled by a Saunco baghouse (Model No. RA12-252-5040) containing 252 polyester dacron bags each six inches in diameter and 144 inches long. The total surface area is 5040 ft² and the air-to-cloth ratio is 6.94 to 1.0 at an air flow of 35,000 acfm.

Almonds are hulled and shelled in another part of the plant and the emissions from these processes are also controlled by a baghouse (Permit to Operate No. 1140140102R). A Saunco baghouse (Model RA12-312-6240) with one compartment containing 312 polyester dacron bags each six inches in diameter and 144 inches long with a rated air flow of 77,500 acfm and an airleg recycle with a rated air flow of 23,000 acfm. The

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SECTION 1
INTRODUCTION

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total bag surface area is 6,240 ft² for an air-to-cloth ratio of 12.4 to 1.0.

Triplicate particulate tests were performed using EPA Method 5 on each outlet duct from each baghouse prior to the fan. The almond receiving/pre-cleaning baghouse has one stack. The almond hulling and shelling baghouse has two stacks, both of which were tested simultaneously. No PM₁₀ tests were conducted. Fresno County has agreed that if the baghouses passed the particulate tests, then they would also pass the PM₁₀ tests, since PM₁₀ is a fraction of the total particulate emitted from the baghouses.

Section 2 of the report presents the test matrix for this program.

SECTION 2

TEST PROGRAM

Table 2-1 presents the test matrix for this program. Both baghouses were in continuous operation during the test program. The pre-cleaning baghouse went down momentarily during Test #3, but came back on line six minutes later.

Section 3 of the report summarizes the test results.

TABLE 2-1. TEST MATRIX FOR HARRIS WOOLF CALIFORNIA ALMONDS

Date	Test Location	Test No.	Test Parameter	Test Condition (ton/hr)	Test Time
09/23/91	Receiving/Pre-Cleaning Baghouse	1	Particulates	16.6 to 18.7	11:48 am - 1:54 pm
09/23/91	Receiving/Pre-Cleaning Baghouse	2	Particulates	15.9 to 18.1	2:14 pm - 4:20 pm
09/23/91	Receiving/Pre-Cleaning Baghouse	3	Particulates	16.1	4:30 pm - 6:45 pm
09/27/91	Hulling/Shelling Baghouse - Stack A	1	Particulates	18.6	8:20 am - 10:30 am
09/27/91	Hulling/Shelling Baghouse - Stack A	2	Particulates	14.6	11:20 am - 1:25 pm
09/27/91	Hulling/Shelling Baghouse - Stack A	3	Particulates	21.4	2:15 pm - 4:20 pm
09/27/91	Hulling/Shelling Baghouse - Stack B	1	Particulates	18.6	8:30 am - 10:35 am
09/27/91	Hulling/Shelling Baghouse - Stack B	2	Particulates	14.6	11:20 am - 1:25 pm
09/27/91	Hulling/Shelling Baghouse - Stack B	3	Particulates	21.4	2:15 pm - 4:20 pm

SECTION 3

TEST RESULTS

Table 3-1 summarizes the test results for the receiving/pre-cleaning baghouse. Tables 3-2 and 3-3 summarize the results from the two stacks serving the hulling and shelling baghouse.

3.1 RECEIVING/PRE-CLEANING BAGHOUSE

The permit limits particulate (and PM_{10}) emissions to 0.004 gr/scf, 1.20 lb/hr or 28.8 lb/day based on a 24-hour operating day. The measured emissions were 0.0069 gr/scf, 1.68 lb/hr or 40.32 lb/day. This baghouse was just over the permit limits.

3.2 HULLING AND SHELLING BAGHOUSE

The permit limits particulate (and PM_{10}) emissions to 0.0032 gr/scf, 1.50 lb/hr or 35.9 lb/day based on a 24-hour operating day. The measured emissions were 0.0020 gr/scf, 1.17 lb/hr or 28.1 lb/day. This baghouse is in compliance with the permit limits.

TABLE 3-1. SUMMARY OF SOURCE EMISSION TEST DATA (60°F)

Unit Tested: Harris Woolf
California Almonds
Receiving/Pre-Cleaning
Baghouse

Date: September 23, 1991

Test Number	1	2	3	Average
Test Condition (tph)	16.6/18.1	15.9/18.1	16.1	
Barometric Pressure (in. Hg)	29.15	29.58	29.52	29.42
Stack Pressure (in. Hg)	28.75	29.18	29.12	29.02
Stack Area (ft ²)	10.08	10.08	10.08	10.08
Elapsed Sampling Time (min.)	120.00	120.00	120.00	120.00
Volume Gas Sampled (dscf)	99.715	97.196	94.826	97.246

GAS DATA

Average Gas Velocity (fps)	54.74	53.39	50.04	52.72
Average Gas Temperature (°F)	93.29	100.17	101.08	98.18
Gas Flowrate (dscfm)	29,563	29,000	27,084	28,549
Gas Analysis (Volume %)				
Carbon Dioxide, dry	0.00	0.00	0.00	0.00
Oxygen, dry	20.90	20.90	20.90	20.90
Water	1.15	0.85	0.83	0.95

EMISSION CONCENTRATION - gr/dscf

Filterable Particulate	0.0048	0.0076	0.0076	0.0067
Total Particulate	0.0051	0.0078	0.0079	0.0069

EMISSION RATE - lb/hr

Filterable Particulate	1.22	1.89	1.77	1.63
Total Particulate	1.28	1.94	1.82	1.68

EMISSION FACTOR - lb/day

Filterable Particulate	29.28	45.36	42.48	39.04
Total Particulate	30.72	46.56	43.68	40.32 ✓

TABLE 3-2. SUMMARY OF SOURCE EMISSION TEST DATA (60°F)

Unit Tested: Harris Woolf
California Almonds
Hulling/Shelling
Baghouse - Stack A

Date: September 27, 1991

Test Number	1	2	3	Average
Test Condition (tph)	18.6	14.6	21.4	
Barometric Pressure (in. Hg)	29.83	29.68	29.54	29.68
Stack Pressure (in. Hg)	29.29	29.14	29.00	29.14
Stack Area (ft ²)	19.63	19.63	19.63	19.63
Elapsed Sampling Time (min.)	120.00	120.00	120.00	120.00
Volume Gas Sampled (dscf)	155.406	139.543	134.130	143.026

GAS DATA

Average Gas Velocity (fps)	53.53	50.43	49.16	51.04
Average Gas Temperature (°F)	77.21	92.46	99.46	89.71
Gas Flowrate (dscfm)	59,072	53,811	51,721	54,868
Gas Analysis (Volume %)				
Carbon Dioxide, dry	0.00	0.00	0.00	0.00
Oxygen, dry	20.90	20.90	20.90	20.90
Water	1.13	1.19	0.88	1.07

EMISSION CONCENTRATION - gr/dscf

Filterable Particulate	0.0018	0.0014	0.0012	0.0015
Total Particulate	0.0020	0.0016	0.0021	0.0019

EMISSION RATE - lb/hr

Filterable Particulate	0.90	0.65	0.54	0.70
Total Particulate	1.00	0.76	0.93	0.90

EMISSION FACTOR - lb/day

Filterable Particulate	21.60	15.60	12.96	16.80
Total Particulate	24.00	18.24	22.32	21.60

TABLE 3-3. SUMMARY OF SOURCE EMISSION TEST DATA (60°F)

Unit Tested: Harris Woolf
California Almonds
Hulling/Shelling
Baghouse - Stack B

Date: September 27, 1991

Test Number	1	2	3	Average
Test Condition (tph)	18.6	14.6	21.4	
Barometric Pressure (in. Hg)	29.83	29.68	29.54	29.68
Stack Pressure (in. Hg)	29.32	29.20	29.13	29.22
Stack Area (ft ²)	6.31	6.31	6.31	6.31
Elapsed Sampling Time (min.)	120.00	120.00	120.00	120.00
Volume Gas Sampled (dscf)	104.218	100.036	93.630	99.295

GAS DATA

Average Gas Velocity (fps)	41.10	42.74	41.60	41.81
Average Gas Temperature (°F)	79.46	94.04	101.46	91.65
Gas Flowrate (dscfm)	14,500	14,661	14,039	14,400
Gas Analysis (Volume %)				
Carbon Dioxide, dry	0.00	0.00	0.00	0.00
Oxygen, dry	20.90	20.90	20.90	20.90
Water	1.28	1.02	1.05	1.12

EMISSION CONCENTRATION - gr/dscf

Filterable Particulate	0.0020	0.0015	0.0017	0.0017
Total Particulate	0.0023	0.0022	0.0021	0.0022

EMISSION RATE - lb/hr

Filterable Particulate	0.25	0.19	0.21	0.22
Total Particulate	0.29	0.28	0.25	0.27

EMISSION FACTOR - lb/day

Filterable Particulate	6.00	4.56	5.04	5.28
Total Particulate	6.96	6.72	6.00	6.48

SECTION 4

SAMPLING EQUIPMENT AND PROCEDURES

This section of the report describes the equipment and procedures used to conduct the particulate tests on this program.

4.1 PRELIMINARY MEASUREMENTS

Before conducting the stack tests a series of preliminary measurements were made to determine:

- The location of the sampling site and the number and location of the sampling points to be used (EPA Method 1)
- The velocity, temperature and pressure of the gases in the stack (EPA Method 2)
- The composition of the stack gases (EPA Method 3)
- The moisture content of the stack gases (EPA Method 4)

Using the results of these preliminary measurements and the calibration constants for the sampling train, a series of calculations were made to determine the value of K, a constant, and N_d , ideal nozzle diameter, required to run an isokinetic test according to the equation:

$$\Delta H = \left[\frac{60^2 \pi^2 (K_p)^2 (C_p)^2 (1 - B_{vo})^2 P_s MW_d}{576^2 (K_o)^2 MW_s P_m} \right] (N_d)^4 \left(\frac{T_m}{T_s} \right) (\Delta P)$$

where

$$K = \left[\frac{60^2 \pi^2 (K_p)^2 (C_p)^2 (1 - B_{no})^2 P_s MW_d}{576^2 (K_o)^2 MW_s P_s} \right]$$

An actual nozzle, whose diameter was as close as possible to the ideal nozzle diameter, was selected for the test. Isokinetic sampling rates for each sampling point in the stack were computed using the equation:

$$\Delta H = (K) (N_d)^4 \left(\frac{T_s}{T_a} \right) (\Delta P)$$

Since K and N_d were known, and remain constant during a test, the only variables were the meter temperatures, the stack gas temperature and the velocity pressure for each sampling point.

4.2 PREPARATION OF THE PARTICULATE SAMPLING TRAIN

All sampling train components were cleaned in the laboratory (soap and water, tap water rinse, distilled water rinse, and IPA rinse) to eliminate previous contamination. The sampling train components were sealed and transported to the sampling site in a mobile lab. The EPA Method 5 equipment used to measure particulates (filterable and total) consisted of:

- A calibrated 316 stainless steel nozzle for isokinetic sampling
- A heated Pyrex glass sampling probe (6 feet long) equipped with an S-type pitot tube and a thermocouple to measure stack velocity, pressure and temperature

- A heated Pyrex glass filter holder containing a weighed 100-mm Whatman 934 AH glass fiber filter
- A Pyrex glass impinger train in an icebath (impingers 1 and 2 contained 100-ml distilled water; bubbler 3 was dry; bubbler 4 contained a weighed amount of silica gel)
- An umbilical to connect the probe and sample box to the control module
- A control module containing a vacuum pump, a calibrated dry gas meter and a calibrated orifice meter to measure the pressure, temperature and flowrate throughout the train.

The sampling train was charged in the mobile lab using freshly prepared reagents. Each impinger and its contents was weighed to the nearest 0.1 gm on a calibrated electronic balance. Blanks of all filters and reagents were retained for subsequent analysis. The sampling point locations were marked on the probe using a high-temperature marker. The sampling train was completely assembled and lifted to the sampling site.

4.3 SAMPLING PROCEDURES FOR PARTICULATE SAMPLING TRAIN

Prior to a test, the sampling train was heated and leak-checked at 15-inches Mercury to insure leakage was less than 0.02 cfm or 4% of the average sampling rate. The S-type pitot tube was also leak-checked. The sampling train was installed on the untrail and the probe was inserted into the stack at the farthest point. An isokinetic sampling rate was calculated using an HP-41CV calculator for each sampling point on the traverse (12 points per traverse, 2 traverses at 90°). Each point was sampled for an equal period of time (5.0 minutes) and all pertinent data were recorded on the data sheet for each point. The probe and sample box

were maintained at 250°F throughout the traverse. The gases leaving the impinger train were maintained at <68°F. At the end of a traverse, the probe was withdrawn from the stack and the entire sampling train was transferred intact to the next sampling port. The other traverse of the stack was completed and the sampling train was withdrawn for the final leak check. This leak check was performed at 15-inches Mercury or at the highest vacuum achieved during the test. The S-type pitot tube was also checked at this time. The probe, nozzle, filter holder and impinger train were sealed with aluminum foil and lowered to the mobile lab for sample recovery.

4.4 SAMPLE RECOVERY PROCEDURES FOR PARTICULATE SAMPLING TRAIN

Sample recovery for the nozzle and probe occurred on the stack. The nozzle and probe were brushed and rinsed three times using ACS reagent grade acetone into a polyethylene sample bottle. Sample recovery for the filter holder and impinger train occurred in the mobile lab. The 100-mm filter was removed from the 4-inch filter holder and sealed in its petri dish. The front half of the 4-inch glass filter holder was brushed and rinsed with acetone. Each impinger was removed from the icebath, wiped dry and weighed to the nearest 0.1 gm. The contents of impinger 1 were transferred to a polyethylene sample bottle. The back half of the 4-inch glass filter holder, the glass connectors, impingers 1, 2 and 3 were rinsed with distilled water and the rinsings were transferred to this same bottle. All sample bottles and petri dishes were marked and labeled. A chain-of-custody log was completed and the field data sheet was also labeled with the sample ID numbers. The sampling train was then recharged in preparation for the next test.

SECTION 5

ANALYTICAL PROCEDURES

This section of the report describes the procedures used to analyze the samples collected during the test program. All analyses were performed in the Steiner Environmental, Inc. climate-controlled laboratory located in Bakersfield, California.

5.1 ANALYSIS OF PARTICULATE SAMPLES

5.1.1 Nozzle, Probe, Filter Holder Wash

The volume of the acetone washings was measured and the washings were transferred to clean, tared, aluminum weighing dishes. The dishes were placed on temperature-controlled water bath under a fume hood and gently heated to dryness (100°F). The dishes with the dry residue were desiccated and weighed repeatedly at 6-hour intervals until a constant weight was achieved (to the nearest 0.01 mg with a tolerance of <0.1 mg between weighings). The ACS reagent grade acetone blank was treated in the same manner.

5.1.2 Filter

The 100-mm filter was removed from its petri dish and transferred to an oven where it was heated for 2 hours at 105°C. The filter was then desiccated and weighed repeatedly at 6-hour intervals until a constant weight was achieved (to nearest 0.01 mg with a tolerance of <0.1 mg

between weighings). An unused, tared blank filter was treated in the same manner.

5.1.3 Condensible Particulate

The volume of sample was measured and the entire volume was transferred to a clean, tared glass evaporating dish. The dish was placed on a temperature-controlled hot plate under a fume hood and gently heated to dryness (150°F). The dish with the dry residue was desiccated and weighed repeatedly at 6-hour intervals until a constant weight was achieved (to nearest 0.01 mg with a tolerance of <0.1 mg between weighings). A blank of the distilled water was treated in the same manner.

SECTION 6

QUALITY ASSURANCE

This section of the report describes the QA/QC procedures employed on the test program.

6.1 PARTICULATE SAMPLING EQUIPMENT

A detailed record of repair and maintenance to each sampling train is kept. Preventative maintenance to each system is performed periodically to avoid complete component breakdown during a field test.

A detailed record of sampling system calibrations is also kept. Calibration data for the sampling nozzles, pitot tubes, dry gas meters and orifice meters are available for review. Results of the EPA Quality Assurance Branch bi-annual audits of the dry gas meter and orifice meter combinations are also logged and verify our in-house calibration data. The calibration data for the equipment used on this program can be found in the Appendix of this report.

6.2 LAB ANALYSIS

All field samples are assigned a label and an ID number. This ID is also affixed to a chain-of-custody log and to the field data sheet to eliminate any chance of sample mixup.

Prior to analysis, all glassware is thoroughly cleaned (soap and water, tap water rinse, distilled water rinse, IPA rinse) to eliminate

any contamination. The evaporating dishes used to evaporate the washings are treated the same as a sample (dried in an oven, desiccated and weighed repeatedly at 6-hour intervals until a constant weight is achieved). The glassware used to measure volumes and make transfers and dilutions are all NBS Class A to insure accurate measurements. All weighings are carried out on a Sartorius Research Model R160P electronic semi-micro balance supported by a marble table in a separate room from the main analytical laboratory. The balance is calibrated regularly against an NBS Class S-1 weight.

All reagents used in the field and in the laboratory are ACS reagent grade and blanks of these reagents are evaluated for every set of tests. Blanks are taken in the field from the squeeze bottles and not the original container. Records are kept on these blanks to insure consistent quality of the reagents.

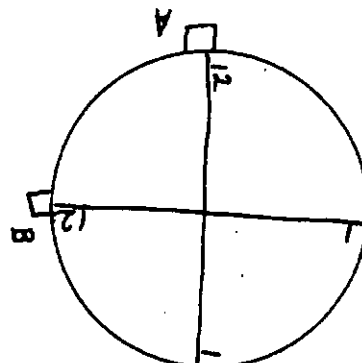
APPENDIX A
STEINER ENVIRONMENTAL RAW DATA

Steiner Environmental, Inc.

N
E
S
W

SAMPLING POINT LOCATION DATA SHEET

Plant Harris-Woolf
 Date 9-23-91
 Test Location Pre-Cleaning Bag House
 Upstream Dist./Dia. 41.0" / 1.0 Ø
 Downstream Dist./Dia. 328.0" / 2.6 Ø
 No. of Sampling Points 24
 Stack Dimension 43.0"
 Coupling Length 4.0"
2, 3-inch MPT/FPT/Flange



setup CM on ground no rope
 100' power; high -ve static, bring stack tube
 step ladder from plant to reach ports

XEQ PNT

Sample Point	Dist	Sample Point	Dist	Sample Point	Dist	Sample Point	Dist
B- 1	4.9						
2	6.9						
3	9.1						
4	11.6						
5	14.8						
6	19.3						
7	31.7						
8	36.3						
9	39.4						
10	41.9						
11	44.1						
12	46.1						

SAMPLING POINT RELOCATION: NONE

PORT B 16.0" lower than East Port

Steiner Environmental, Inc.

SAMPLING POINT LOCATION DATA SHEET

Plant HARRIS- WOLF

Date 9-24-91

Test Location SHELLING BAGHOUSE ^{OUT} A

Upstream Dist./Dia. 144.0" / 2.4 ϕ

Downstream Dist./Dia. 108.0" / 1.8 ϕ

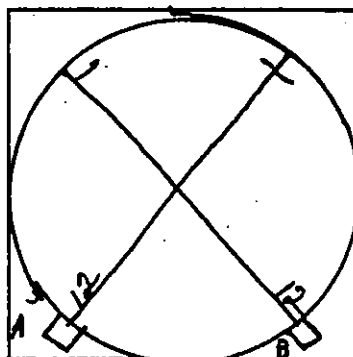
No. of Sampling Points 24

Stack Dimension 60.0"

Coupling Length 3.5"

2-3 -inch MPT/FPT/Flang high - ve static (bring stack tube)

HAS HOOKS, SET UP ON ROOF; 50' rope
100' POWER CORD; need ladder from plant or lift.



XEQ PNT

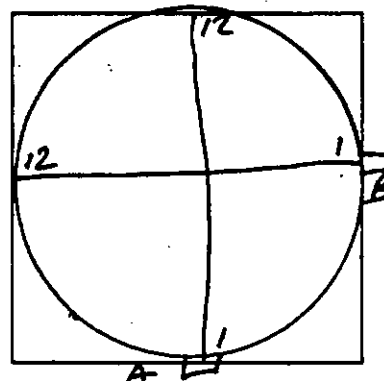
Sample Point	Dist	Sample Point	Dist	Sample Point	Dist	Sample Point	Dist
1	4.8						
2	7.5						
3	10.6						
4	14.1						
5	18.5						
6	24.8						
7	42.2						
8	48.5						
9	52.9						
10	56.4						
11	59.5						
12	62.2						

SAMPLING POINT RELOCATION: NONE

Steiner Environmental, Inc.

SAMPLING POINT LOCATION DATA SHEET

Plant HARRIS WOLF
 Date 9-24-91
 Test Location SHELLING BAGHOUSE - DUCT B
 Upstream Dist./Dia. 58" / 1.70
 Downstream Dist./Dia. 367.5" / 10.80
 No. of Sampling Points 24
 Stack Dimension 34"
 Coupling Length 3.5"
2-3 -inch MPT/FPT/Flang



NEED 12' LADDER OR MANLIFT
 HAS HOOKS - 100' POWER CORD FOR STATIC
 HIGH NEGATIVE FLOW - NEED SLACK MANOMETER

XEQ PNT

Sample Point	Dist	Sample Point	Dist	Sample Point	Dist	Sample Point	Dist
1	4.2						
2	5.8						
3	7.5						
4	9.5						
5	12.0						
6	15.6						
7	25.4						
8	29.0						
9	31.5						
10	33.5						
11	35.2						
12	36.8						

SAMPLING POINT RELOCATION: NONE

Date 9-23-91 Barometric Pressure 29.15
PRE-CLEANING
 Test Location BAGHOUSE Static In. wg. -5.50
 Run Number 1 Probe Type/Length 66'-6"
 Stack Diameter 43.0" Pitot Coefficient 0.84
 Operator SC/SW Meter Box No. 1779/10081
 Filter No. 457 Nozzle No./Size #158/0.2333

IMPINGER		VOLUME/WEIGHTS		GAS COMPOSITION				
Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO	
OI	539.0	553.7	-14.7		0.0	20.9		
OI	581.5	567.5	14.0					
DRY	468.1	463.8	4.3					
				Leakrate	cfm		"Hg	
S.G.	654.8	633.3	21.5	Initial	0.017	15		
		TOTAL	25.1	Final	2.003	5"		

[illegible]

Forms: Fieldat. frm

PLANT Harris-Woolf TEST TYPE M-5 FIELD TEST DATA SHEET (Page 2 of 2)
 DATE 5-23-91 RUN NO. 1
 TEST LOCATION Doc Cleaning Bag House OPERATOR SC/SW

Sample Point	Time	AP in wg	ΔH in wg	Gas Meter Volume Ft ³	TEMPERATURE °F							Pump Vacuum in. Hg	ΔAP	Comments
					Stack	Probe	Oven	Imp.	Gas Meter					
									In	Out				
A-1	12:54	0.72	2.49	802.697	91	262	251	64	124	112	2.0	0.849		
2	5	0.85	2.91	806.951	95	257	255	62	120	112	2.0	0.922		
3	10	0.91	3.12	811.582	96	260	250	63	124	113	2.0	0.954		
4	15	0.87	2.99	816.373	96	259	256	61	125	113	2.0	0.933		
5	20	0.88	3.03	821.045	96	253	249	63	126	114	2.0	0.938		
6	25	0.85	2.93	825.732	96	257	252	64	127	116	2.0	0.922		
7	30	0.87	3.04	830.327	96	259	258	66	127	116	2.0	0.938		
8	35	0.84	2.91	835.028	96	255	252	63	129	117	2.0	0.917		
9	40	0.67	2.32	839.644	95	257	252	63	129	118	2.0	0.819		
10	45	0.77	2.66	843.781	97	253	251	63	129	118	2.0	0.877		
11	50	1.30	4.52	848.138	93	250	253	62	129	118	2.0	1.140		
12	55	1.10	3.84	853.574	92	257	254	66	130	118	2.0	1.049		
	1:00			858.130										
T/A	12:00 ^{PM}		2.99	111.3760	93.29				114.75			2.0	0.9310	Phot. ✓ OK

Date 9-23-91 Barometric Pressure 29.58
 Test Location PRO-CHEMICAL Static in.wg. -5.43
BAGHOUSE
 Run Number 2 Probe Type/Length 6C-6'
 S/Stack Diameter 43.0" Pitot Coefficient 0.84
 Operator SW Meter Box No./Y 779/10081
 Filter No. 484 Nozzle No./Size 1458/2.333

IMPINGER			VOLUMES/WEIGHTS			GAS COMPOSITION				
Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO			
O I	531.9	548.2	-16.3							
O I	525.8	518.2	7.6							
O R Y	464.2	461.4	2.8							
				Leakrate	cfm		"Hg			
S.O.	690.4	666.5	23.9	Initial		0.013	15"			
		TOTAL	18.0	Final		0.007	8"			

[illegible]

i-Steps Sales Analysis

Jan 30, 1993

COMPANY	RATING	NO.	LAST CONTACT	ACTION
ALCOA	A	5	28-Jan	MEET PLANTS
ARCO CHEMICAL	A	5	21-Jan	MEET GROUP
B.P. OIL	A	10	27-Jan	RFP
BABCOCK ULTR PWR	A	1	7-Dec	QUOTE
CHAMPION INT.PAPR	A	4	14-Dec	MEET CORP
DuPONT	A	25	21-Jan	PILOT INSTALL'T'N
JAMES RIVER	A	8	14-Dec	FEB 9 CORP MTG
MAINE RUBBER	A	1	7-Jan	FEB INSTALL
PSE & G	A	3	7-Dec	AUTOCAD INSTALL
R.J. REYNOLDS	A	7	21-Jan	INSTALL
RHONE POULAC	A	6	19-Dec	CORP MEET
SUN OIL	A	7	21-Jan	RFP FOLLOW UP
U S STEEL	A	8	25-Jan	RFP
UNION CARBIDE	A	8	6-Oct	CORP FOLLOW UP
BETHLEHEM STEEL	B	4	28-Jan	CORP RFP
BIO ENERGY	B	1	6-Oct	RFP
CHRYSLER	B	12	23-Nov	CORP FOLLOW UP
CORN PRODUCTS	B	5	7-Dec	CHICAGO MEETING
ELF ATOCHEM	B	25	5-Jan	RFP FOLLOW UP
EMERY CHEMICAL	B	7	15-Nov	CORP PRESENTATION
GEON COMPANY	B	1	27-Jan	RFP
GETTY PETROLEUM	B	4	12-Oct	CORP MEETING
HARBISON-WALKER	B	1	7-Jan	QUOTE
LINCOLN PULP & PR	B	2	12-Oct	CORP MEETING
MAINE ENERGY	B	1	13-Oct	RFP FOLLOW UP
MALLINCKRODT	B	3	14-Jan	CORP MEETING
NABISCO	B	1	21-Jan	QUOTE
PSN H	B	5	14-Dec	CORP PRESENTATON
PHILIP MORRIS	B	12	14-Dec	CORP PRESENTATION
ROHM & HAAS	B	7	14-Dec	WEST VA VISIT
SHISEIDO AMERICA	B	3	14-Dec	CORP PRESENTAION
STAR ENTERPRISES	B	5	16-Oct	CORP PRESENTATION
WESTINGHOUSE	B	16	7-Jan	RFP FOLLOW UP
WEYERHAEUSER	B	5	8-Jan	CORP PRESENTATION
WHITEFIELD PWR	B	1	17-Oct	RFP FOLLOW UP
ALCAN	C	6	15-Dec	CORP MEETING
BATESVILLE	C	2	16-Dec	CORP MEETING
EASTERN FINE PAPR	C	1	17-Oct	RFP
FORD	C	12	16-Nov	CORP MEETING
FREUDENBERG NOK	C	3	14-Dec	RFP
GENERAL MOTORS	C	12	21-Nov	CORP MEETING
JOHNSON MATTHEY	C	1	15-Dec	RFP
KRAFT FOODS	C	2	7-Dec	QUOTE
MAGRUDER CLR	C	1	13-Dec	RFP
PFISTER CHEM	C	1	8-Dec	RFP
PPG INTERNATIONAL	C	8	7-Jan	CORP MEETING
S. D. WARREN	C	2	16-Oct	RFP
WAUSAU PAPER	C	2	13-Oct	RFP
"A" POTENTIAL	98	TOTAL	\$931,000	
"B" POTENTIAL	121	TOTAL	\$1,149,500	
"C" POTENTIAL	54	TOTAL	\$513,000	

PLANT Harri's - Woolf TEST TYPE M-5 FIELD TEST DATA SHEET (Form 2 of 2)
 DATE 9-23-91 RUN NO. 2
 TEST LOCATION Pac-Cleaning Bag House OPERATOR SW

Sample Point	Time	ΔP in wg	ΔH in wg	Gas Meter Volume Ft ³	TEMPERATURE °F						Pump Vacuum in. Hg	ΔP	Comments
					Stack	Probe	Oven	Imp.	Gas Meter				
									In	Out			
A-1	15:10	0.72	2.45	913.662	97	257	262	62	113	114	7.5	0.849	
2	5	0.80	2.72	917.961	100	259	257	64	120	116	8.0	0.874	
3	10	0.88	2.99	922.327	100	253	249	63	121	114	8.0	0.938	
4	15	0.82	2.79	926.935	101	243	256	63	122	115	8.0	0.906	
5	20	0.85	2.88	931.405	103	247	252	62	122	115	8.5	0.922	
6	25	0.84	2.84	935.898	104	252	257	64	123	115	8.5	0.917	
7	30	0.82	2.78	940.407	104	256	255	62	123	116	8.5	0.906	
8	35	0.87	2.95	944.908	103	263	245	65	124	115	8.5	0.933	
9	40	0.79	2.68	949.409	103	262	242	68	124	116	8.5	0.889	
10	45	0.69	2.35	953.878	102	251	247	66	124	116	7.5	0.831	
11	50	0.83	2.83	958.018	102	253	248	66	125	116	7.5	0.911	
12	55	0.72	2.47	962.150	98	249	256	69	125	116	7.5	0.849	
	60			966.312									
T/A	120 ^{min}		2.83	107.662	100.17				118.10			0.908	Plot OK

1 of 2,

Filter No. 490 Nozzle No./Size 1458/.2333

INPINGER		VOLUMES/WEIGHTS			GAS COMPOSITION				
Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO		
	523.9	537.8	-13.9						
	544.3	552.0	7.3						
	448.5	405.4	3.1						
				Leakrate	cfm		Wg		
S.G.	643.6	622.9	20.7	Initial		0.013	15"		
		TOTAL	17.2	Final		0.004	6"		

[illegible]

Forms: Fieldac. Form

PLANT HORRIS - WOLF TEST TYPE M-5 FIELD TEST DATA SHEET (Page 2 of 2)
 DATE 9-23-91 RUN NO. 3
 TEST LOCATION Pac. Cleaning Bag House OPERATOR SW

Sample Point	Time	AP in wg	AH in wg	Gas Meter Volume Ft ³	TEMPERATURE °F							Pump Vacuum in. Hg	ΔP	Comments
					Stack	Probe	Oven	Imp.	Gas Meter					
									In	Out				
A-1	12:45	0.79	2.69	021.015	96	249	260	65	114	112	5.0	0.889		
2	5	0.77	2.61	025.998	102	251	269	65	122	113	5.0	0.877		
3	10	0.80	2.72	029.721	102	263	266	65	123	114	5.0	0.894		
4	15	0.83	2.82	034.145	101	258	263	65	125	114	5.0	0.911		
5	20	0.81	2.76	038.648	102	247	257	64	125	114	5.0	0.900		
6	25	0.83	2.83	043.088	101	252	248	63	125	114	5.25	0.911		
7	30	0.78	2.66	047.594	101	248	254	65	125	114	5.5	0.883		
8	35	0.84	2.87	051.967	100	248	249	66	125	114	5.5	0.917		
9	40	0.81	2.76	056.448	101	251	257	67	125	115	5.5	0.900		
10	45	0.72	2.46	060.724	100	253	249	67	124	115	5.0	0.849		
11	50	0.32	1.10	065.205	97	257	251	67	125	115	3.0	0.566		
12	55	0.03	0.10	068.200	96	259	247	68	122	114	1.0	0.123		
	60			072.004										
T/A	120"		2.55	105.539	101.08				119.29				0.8511 Pitot ✓ OK	

PLANT HARRIS - WOLF TEST TYPE METHOD 5 FIELD TEST DATA SHEET (Page 1 of 2)

Date 9-27-91 Barometric Pressure 29.83
 Test Location HOLING 2 Static In. wg. -7.4
 Run Number 1-A Probe Type/Length GL/8'
 Stack Diameter 60" Pitot Coefficient 0.84
 Operator SW Meter Box No./Size 644/0.9812
 Filter No. 485 Nozzle No./Size #1555/0.2792

TEMPERATURE			VOLUMES/WEIGHTS			GAS COMPOSITION		
Contents	Final	Initial	Net	Time	CO	O ₂	CO	
DI	520.0	547.9	27.9					
DI	588.7	567.5	21.2					
DI	425.3	413.3	12.0					
s.c.	653.4	620.3	33.1					
		TOTAL	38.4					
				Leakrate	cfm			
				Initial				
				Final				

Sample Point	Time	ΔP in wg	ΔH in wg	Gas Meter Volume Ft. ³	TEMPERATURE °F							Pump Vacuum in. Hg	ΔP	Comments
					Stack	Probe	Oven	Imp.	Gas Meter					
									In	Out				
A-1	0	0.73	4.61	668.734	72	241	259	47	70	71	6.75	0.854	Pitot OK.	
2	5	0.68	4.35	674.742	73	253	251	49	81	76	6.75	0.825		
3	10	0.69	4.43	680.746	74	250	256	49	84	79	6.75	0.831	30596	
4	15	0.73	4.71	686.814	75	258	258	49	87	82	7.0	0.854	30595	
5	20	0.74	4.79	693.049	75	256	260	50	89	84	7.0	0.860	30595	
6	25	0.78	5.06	699.365	75	258	259	49	90	86	8.0	0.883		
7	30	0.94	6.10	705.853	76	257	255	48	91	87	9.0	0.910	30594	
8	35	0.96	6.25	713.145	76	257	258	49	92	89	9.0	0.980		
9	40	1.15	7.49	720.237	76	257	255	51	93	89	11.0	1.072		
10	45	0.86	5.62	728.129	75	259	258	50	93	90	8.5	0.927		
11	50	0.88	5.75	735.058	75	261	263	51	93	91	8.5	0.938		
12	55	1.45	9.60	742.115	69	258	260	51	94	91	12.0	1.204		

PLANT Harris-Woolf TEST TYPE M-5 FIELD TEST DATA SHEET (Page 2 of 2)
 DATE 9-27-91 RUN NO. 1-A
 TEST LOCATION Shelling-Shelling B.H OPERATOR SW

Sample Point	Time	AP in wg	ΔH in wg	Gas Meter Volume Ft ³	TEMPERATURE °F							Pump Vacuum in. Hg	ΔP	Comments
					Stack	Probe	Oven	Imp.	Gas Meter					
									In	Out				
B-1	09:30	0.79	5.12	751.809	78	249	260	48	91	90	7.5	0.889		
2	65	0.78	5.07	758.204	78	252	260	46	93	91	7.5	0.883		
3	70	0.80	5.21	764.645	79	259	253	48	95	92	8.0	0.894		
4	75	0.79	5.14	771.248	80	253	252	49	96	93	8.0	0.889		
5	80	0.81	5.28	777.867	80	251	254	50	97	94	8.0	0.900		
6	85	0.82	5.35	784.462	80	253	258	53	97	94	8.0	0.906		
7	90	0.96	6.27	791.146	80	255	253	53	98	95	9.5	0.980		
8	95	0.95	6.21	798.420	80	255	250	54	99	95	9.5	0.975		
9	100	0.96	6.28	805.771	80	255	250	54	99	96	9.5	0.980		
10	105	0.93	6.07	813.055	82	256	253	56	100	97	9.0	0.964		
11	110	0.94	6.14	820.281	82	257	252	56	100	97	9.0	0.970		
12	115	0.91	5.93	827.525	83	258	258	58	100	97	8.5	0.954	Pitot/OK	
	120			834.734										
T/A	120		5.70	166.000	77.21				91.00			0.9326		

PLANT

Harris - WolffTEST TYPE METHOD 5 FIELD TEST DATA SHEET (Form 1 of 2)

Date 9-27-91 Barometric Pressure 29.68
 Test Location SHEDS Static In. wg. -7.4
 Run Number 2-A Probe Type/Length GL/8'
 Stack Diameter 60.0" Pitot Coefficient 0.84
 Operator SW Meter Box No. 17 644/0.9812
 Filter No. 490 Nozzle No./Size 1555/0.2792

IMPUISER			VOLUMES/WEIGHTS			GAS COMPOSITION			
Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO		
DI	531.8	539.3	-7.5						
DI	539.3	525.9	13.4						
dry	463.5	460.3	3.2						
s.s.	711.6	684.6	27					Leakrate	cfm
								Initial	0.002
								Final	0.005
			TOTAL	36.1					4"

Sample Point	Time	AP in wg	AH in wg	Gas Meter Volume Ft ³	TEMPERATURE °F							Pump Vacuum in. Hg	ΔP	Comments
					Stack	Probe	Oven	Imp.	Gas Meter					
									In	Out				
A-1	11:20	0.61	3.93	835.367	87	246	245	69	95	98	3.25	0.781	Pitot OK.	
2	5	0.63	4.06	840.995	89	257	251	63	100	96	3.25	0.794	30590	
3	10	0.64	4.14	846.876	89	247	248	66	103	98	3.25	0.800	30590	
4	15	0.62	4.01	852.788	90	260	257	60	104	99	3.0	0.787	30589	
5	20	0.65	4.20	858.629	91	253	250	60	104	100	3.25	0.806	30589	
6	25	0.75	4.87	864.635	91	260	250	60	106	102	3.50	0.866	30588	
7	30	0.83	5.38	871.083	92	251	252	60	106	102	3.50	0.911	30588	
8	35	0.82	5.32	877.747	92	253	253	62	107	102	3.50	0.906		
9	40	0.81	5.26	884.518	92	252	256	62	107	104	3.50	0.900		
10	45	0.80	5.22	891.197	90	255	253	63	108	104	3.50	0.894		
11	50	0.78	5.09	897.872	90	254	251	63	108	104	3.50	0.883		
12	55	0.91	5.98	904.455	86	241	254	64	108	104	4.0	0.954		

Forms: Field Data Form

PLANT Harris-Woolf TEST TYPE M-S FIELD TEST DATA SHEET (Page 2 of 2)
 DATE 9-27-91 RUN NO. 2-A
 TEST LOCATION Shelling Bag House OPERATOR SW

Sample Point	Time	AP in wg	AH in wg	Gas Meter Volume Fc3	TEMPERATURE °F							Pump Vacuum in. Hg	fAP	Comments
					Stack	Probe	Oven	Imp.	Gas Meter					
									In	Out				
B-1	12:25	0.72	4.66	911.622	93	249	251	64	105	105	3.25	0.849		
2	65	0.69	4.48	917.928	94	249	255	59	109	105	3.25	0.831		
3	70	0.68	4.42	924.150	94	244	262	57	110	106	3.25	0.825		
4	75	0.66	4.29	930.272	94	244	264	58	110	107	3.25	0.812		
5	80	0.65	4.22	936.413	95	245	257	59	111	107	3.25	0.806		
6	85	0.80	5.20	942.421	95	242	257	61	111	107	3.25	0.894		
7	90	0.83	5.40	948.458	95	244	263	59	111	108	3.50	0.911		
8	95	0.79	5.14	955.479	95	247	261	60	111	108	3.25	0.889		
9	100	0.78	5.06	962.153	96	246	254	62	111	108	3.25	0.883		
10	105	0.82	5.32	968.848	96	248	260	60	111	108	3.50	0.906		
11	110	0.85	5.52	975.608	96	250	251	59	111	108	3.50	0.922		
12	115	0.86	5.58	982.513	97	248	254	61	112	108	3.50	0.927		
	120			989.497									Plot/ok.	
T/A	120"		4.86	154.130	92.46				105.77			0.864		

PLANT HARRIS - WOLF TEST TYPE METHOD S FIELD TEST DATA SHEET (Page 1 of 2)

Date 9-27-91 Barometric Pressure 29.54
 Test Location SHEDS BASHOUSE Static In.wg. -7.3
 Run Number 3-A Probe Type/Length GL/8'
 Stack Diameter 60.0" Pitot Coefficient 0.84
 Operator SW Meter Box No./Size 644/0.9812
 Filter No. S13 Nozzle No./Size 1555/2792

IMPIRGER	VOLUMES/WEIGHTS				GAS COMPOSITION			
	Contents	Final	Initial	Net	Time	O ₂	CO	
	DI	526.2	538.5	-12.3				
	DI	567.8	561.9	6.4				
	ORV	456.6	432.3	4.3				
					Leakrate	cfm		mg
	s.e.	728.3	701.0	27.3	Initial	.007	15"	
			TOTAL	25.7	Final	.004	9"	

Sample Point	Time	AP in wg	AH in wg	Gas Meter Volume Ft ³	TEMPERATURE °F							Pump Vacuum in.Hg	fap	Comments
					Stack	Probe	Oven	Imp.	Gas Meter					
									In	Out				
A-1	14:15	0.57	3.64	991.382	100	241	257	65	104	105	7.0	0.755	Plot OK.	
2	5	0.58	3.74	996.825	99	259	255	63	110	108	6.0	0.762		
3	10	0.63	4.07	1001.337	99	249	249	61	111	108	6.75	0.794	30584 AHW 3-A	
4	15	0.60	3.88	1008.458	99	248	257	61	112	108	6.25	0.775		
5	20	0.67	4.33	1014.263	100	246	260	62	113	110	7.0	0.819	30583 AHW 3-A	
6	25	0.62	4.02	1020.345	100	252	252	61	114	111	6.5	0.787		
7	30	0.81	5.25	1026.281	100	249	249	61	114	111	7.0	0.900	30582 AHW 3-A	
8	35	0.80	5.19	1032.995	100	243	259	60	115	112	7.0	0.894		
9	40	0.81	5.30	1039.676	96	249	258	63	115	112	7.0	0.900		
10	45	0.75	4.89	1046.444	98	240	258	61	116	112	7.0	0.866		
11	50	0.64	4.17	1052.958	98	242	251	61	115	112	6.5	0.800		
12	55	0.35	2.28	1058.995	98	244	257	62	116	112	5.0	0.592		

Steiner Environmental, Inc.

PLANT Harris-Woolf TEST TYPE M-5 FIELD TEST DATA SHEET (Page 2 of 2)
 DATE 9-27-91 RUN NO. 3-A
 TEST LOCATION Shelling Bag House OPERATOR SW

Sample Point	Time	AP in wg	AH in wg	Gas Meter Volume Ft ³	TEMPERATURE °F							Pump Vacuum in. Hg	ΔP	Comments
					Stack	Probe	Oven	Imp.	Gas Meter					
									In	Out				
B-1	15:20	0.62	4.03	1064.111	98	256	252	63	113	111	6.5	0.787		
2	65	0.66	4.29	1070.008	100	258	260	62	116	112	6.75	0.812		
3	70	0.63	4.09	1076.084	101	254	256	60	117	112	6.5	0.794		
4	75	0.62	4.03	1082.047	101	251	253	61	117	113	6.5	0.787		
5	80	0.70	4.56	1087.964	101	251	261	63	118	114	7.0	0.837		
6	85	0.68	4.43	1094.222	100	257	257	62	118	114	7.0	0.825		
7	90	0.85	5.53	1100.409	101	255	250	62	118	114	8.0	0.922		
8	95	0.82	5.35	1107.267	100	255	250	63	118	115	8.0	0.906		
9	100	0.88	5.73	1114.068	100	255	259	62	117	114	9.0	0.938		
10	105	0.84	5.48	1121.105	99	255	257	63	117	114	8.75	0.917		
11	110	0.87	5.66	1128.012	100	258	257	63	116	114	9.0	0.933		
12	115	0.91	5.93	1135.018	99	25	252	64	116	114	9.0	0.954		
	120			1142.209									Plat/OK.	
T/A	120 ^{min}		4.58	150.927	99.46				113.	29		0.835		

Date 9-27-91 Barometric Pressure 29.83
 Test Location SHELLING Static in. wg. -6.9
 Run Number 1-B Probe Type/Length GC-6'
 Stack Diameter 34" Pitot Coefficient 0.84
 Operator SL Meter Box No. 17 279/1.0081
 Filter No. 518 Nozzle No./Size 208/0.2637

IMPUING			VOLUMES/WEIGHTS			GAS COMPOSITION		
Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO	
OI	549.2	552.3	-3.1		0	20.9		
OI	583.5	573.0	10.5					
OI	465.8	463.4	2.4					
s.c.	618.4	599.0	19.4					
		TOTAL	29.2					
				Leakrate	cfm			
				Initial		0.14	15	
				Final		0.08	4	

Sample Point	Time	AP in wg	AH in wg	Gas Meter Volume Ft ³	TEMPERATURE °F						Pump Vacuum in. Hg	fap	Comments
					Stack	Probe	Oven	Imp.	Gas Meter				
									In	Out			
A-1	0	0.34	1.83	265.837	74	250	251	63	74	75	2.0	0.583	PITOT OK
2	5	0.37	2.03	269.635	75	253	247	63	92	79	2.0	0.608	
3	10	0.36	1.98	273.652	75	256	249	63	95	81	2.5	0.600	30593 344-1.8
4	15	0.47	2.60	277.666	76	253	250	64	97	89	3.0	0.686	30592 344-1.8
5	20	0.44	2.44	282.168	76	251	258	63	100	89	2.5	0.663	
6	25	0.41	2.27	286.534	78	257	260	64	102	87	2.5	0.640	
7	30	0.87	4.82	290.828	77	248	265	64	101	88	4.0	0.933	30591 344-1.8
8	35	0.54	3.01	296.682	77	247	261	64	103	90	3.0	0.735	
9	40	0.43	2.40	301.503	78	249	258	63	104	92	3.0	0.656	
10	45	0.37	2.06	305.823	77	249	252	64	102	92	2.5	0.608	
11	50	0.38	2.11	309.840	79	251	256	64	104	92	3.0	0.616	
12	55	0.36	2.00	313.982	79	262	251	65	104	93	2.5	0.600	
	60			317.980									

Steiner Environmental, Inc.

PLANT HARRIS-WOOLF TEST TYPE METHOD-5 FIELD TEST DATA SHEET (Page 2 of 2)
 DATE 9-27-91 RUN NO. 1-8
 TEST LOCATION SHELLING BAGHOUSE OPERATOR SC
DUCT - B

Sample Point	Time	AP in wg	AH in wg	Gas Meter Volume Ft ³	TEMPERATURE °F							Pump Vacuum in. Hg	ΔP	Comments
					Stack	Probe	Oven	Imp.	Gas Meter					
									In	Out				
B-1	0935	0.50	2.76	317.980	79	261	257	64	95	92	3.0	0.707		
2	65	0.50	2.77	322.464	80	265	259	64	102	93	3.0	0.707		
3	70	0.57	3.16	326.865	81	262	260	65	103	93	3.0	0.755		
4	75	0.65	3.60	331.470	81	261	258	65	104	93	3.0	0.886		
5	80	0.50	2.77	336.272	82	259	260	65	106	93	3.0	0.707		
6	85	0.90	4.99	340.660	82	261	259	66	106	94	4.0	0.949		
7	90	0.77	4.29	346.375	82	264	248	66	108	96	3.5	0.877		
8	95	0.50	2.78	351.675	83	258	250	67	109	97	3.0	0.707		
9	100	0.45	2.51	356.168	83	258	248	66	109	98	3.0	0.671		
10	105	0.40	2.23	360.432	83	253	251	66	109	98	2.5	0.632		
11	110	0.70	3.89	364.546	85	247	250	65	110	99	3.5	0.837		
12	115	0.76	4.24	370.197	85	250	252	66	111	100	4.0	0.872	Pilot OK	
1035	120			375.472										
T/A			2.90	109.635	79.46				96.73			0.718		

PLANT HARRIS WOOD

Date 9-27-91 Barometric Pressure 29.68
 Test Location SMELTING Static In. wg. -6.5
 Run Number A-B-DUT Probe Type/Length 6C-6'
 Stack Diameter 34" Pitot Coefficient 0.84
 Operator SC Meter Box No./Y 779/1.0081
 Filter No. 519 Nozzle No./Size 208/0.2637

IMPROVER		VOLUMES/WEIGHTS			GAS COMPOSITION		
Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO
OI	533.9	541.4	-7.50		0	10.9	
OI	527.6	519.7	7.90				
DEV	463.0	461.4	1.6				
				Leakrate	cfm		mg
s.g.	650.1	629.8	20.3	Initial	.012	15	
		TOTAL	22.3	Final	-0.10	12	

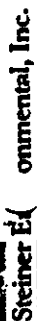
Sample Point	Time	ΔP in wg	ΔH in wg	Gas Meter Volume Ft ³	TEMPERATURE °F							Pump Vacuum in. Hg	Δap	Comments
					Stack	Probe	Oven	Imp.	Gas Meter					
									In	Out				
A-1	0	0.33	1.78	376.875	89	249	257	63	93	92	7.0	0.574	0.101 OK	
2	5	0.40	2.16	380.568	89	251	260	63	95	90	7.0	0.632		
3	10	0.45	2.43	384.600	90	253	255	63	99	91	8.0	0.671	30587 2442.8	
4	15	0.45	2.46	388.832	90	252	252	64	104	94	8.5	0.671		
5	20	0.49	2.66	393.098	93	248	251	64	105	95	9.0	0.700	30586 2442.8	
6	25	0.42	2.30	397.542	92	254	249	64	108	97	8.0	0.698		
7	30	0.93	5.10	401.734	92	250	251	64	110	98	12.0	0.768	30585 2442.8	
8	35	0.65	3.56	407.125	93	255	248	64	108	101	10.0	0.806		
9	40	0.50	2.74	412.330	93	255	256	64	108	104	8.5	0.707		
10	45	0.45	2.48	416.795	93	248	254	64	112	103	8.5	0.671		
11	50	0.39	2.15	420.999	94	248	256	65	113	104	7.5	0.624		
12	55	0.40	2.20	424.965	95	250	257	65	114	105	7.0	0.632		
	60			428.865										



Steiner Environmental, Inc.

PUMP	HARRIS - WOODCF	TEST TYPE	METHOD S	FIELD TEST DATA SHEET (P-000)	2 of 2
DATE	9-27-91		RUN NO.	2-B	
TEST LOCATION	SHELUNG - BIGHOUSE		OPERATOR	SC	
	DUCT-B				

[illegible]



HARRIS - WOLF

Date 9-27-91 Barometric Pressure 29.54
 Test Location SWELLING Static In. wg. - 5.6
 2nd. APTS
 Run Number 3-B Probe Type/Length 6C-6'
 Stack Diameter 34" Pitot Coefficient 0.84
 Operator SC Meter Box No./Y 779/1.0081
 Filter No. 520 Nozzle No./Size 208/0.2637

IMPIINGER		VOLUMES/WEIGHTS			GAS COMPOSITION				
Contents	Final	Initial	Net	Time	CO ₂	O ₂	CO		
DI	535.7	547.2	11.5						
DI	545.2	536.7	8.5						
DI	447.9	445.4	2.5						
				Leakrate	cfm		mg		
S.G.	647.4	627.4	22.0	Initial	.009		15		
		TOTAL	21.5	Final	.009		12		

[illegible]

Forms: Fieldat. Form

PUMP NAME HARRIS - WATER TEST TYPE METHOD 5 FIELD TEST DATA SHEET (Page 2 of 2)
DATE 9-27-91 RUN NO. 3-B DUCT
TEST LOCATION BAGHOUSE DUCT OPERATOR SC
DUCT - B

[illegible]

Steiner Environmental, Inc.

Date: 9-27-91

Test Location: SHELLING BARNHOUSE
HARRIS - WOLF

SAMPLE HANDLING/LOG-IN

NO	SAMPLE TYPE	VOLUME	COMMENTS
1	30596 <u>S</u> <u>BHW</u> <u>1</u> Meth Sample Test		
2	30595 <u>S</u> <u>FHW</u> <u>1</u> Meth Sample Test		
3	30594 <u>S</u> <u>MF</u> <u>1</u> Meth Sample Test		
4	30593 <u>S</u> <u>BHW</u> <u>1</u> Meth Sample Test		
5	30592 <u>S</u> <u>FHW</u> <u>1</u> Meth Sample Test		
6	30591 <u>S</u> <u>MF</u> <u>1</u> Meth Sample Test		
7	30590 <u>S</u> <u>BHW</u> <u>2</u> Meth Sample Test		
8	30589 <u>S</u> <u>FHW</u> <u>2</u> Meth Sample Test		
9	30588 <u>S</u> <u>MF</u> <u>2</u> Meth Sample Test		
10	30587 <u>S</u> <u>BHW</u> <u>2</u> Meth Sample Test		
11	30586 <u>S</u> <u>FHW</u> <u>2</u> Meth Sample Test		
12	30585 <u>S</u> <u>MF</u> <u>2</u> Meth Sample Test		

CHAIN-OF-CUSTODY

Signature	Date/Time	Signature	Date/Time
<u>S. Coughlin</u>	<u>2240/9-27-91</u>		
<u>M. Cameron</u>	<u>10-3-91</u>		

Steiner Environmental, Inc.

Date: 9-27-91

Test Location: SHELLING BAGHOUSE
HARRIS-WOLFF

SAMPLE HANDLING/LOG-IN

NO	SAMPLE TYPE	VOLUME	COMMENTS
1	30584 <u>5</u> <u>BHW</u> <u>3</u> Meth Sample Test		
2	30583 <u>5</u> <u>FHW</u> <u>3</u> Meth Sample Test		
3	30582 <u>5</u> <u>MF</u> <u>3</u> Meth Sample Test		
4	30581 <u>5</u> <u>BHW</u> <u>3</u> Meth Sample Test		
5	30580 <u>5</u> <u>FHW</u> <u>3</u> Meth Sample Test		
6	30579 <u>5</u> <u>MF</u> <u>3</u> Meth Sample Test		
7			
8			
9			
10			
11			
12			

CHAIN-OF-CUSTODY

Signature	Date/Time	Signature	Date/Time
<u>S. Wofham</u>	<u>2235 / 9-27-91</u>		
<u>M. Patnasco</u>	<u>10-3-91</u>		

Steiner Environmental, Inc.

Date: 9-23-91

Test Location: HARRIS-400CF

SAMPLE HANDLING/LOG-IN

NO	SAMPLE TYPE	VOLUME	COMMENTS
1	30608 <u>S</u> <u>BLK</u> <u>AK</u> Meth Sample Test		
2	30607 <u>S</u> <u>BLK</u> <u>AK</u> Meth Sample Test		
3	30606 <u>S</u> <u>BLK</u> <u>AK</u> Meth Sample Test		
4	30605 <u>S</u> <u>BHW</u> <u>1</u> Meth Sample Test		
5	30604 <u>S</u> <u>FHW</u> <u>1</u> Meth Sample Test		
6	30603 <u>S</u> <u>MF</u> <u>1</u> Meth Sample Test		
7	30602 <u>S</u> <u>BHW</u> <u>2</u> Meth Sample Test		
8	30601 <u>S</u> <u>FHW</u> <u>2</u> Meth Sample Test		
9	30600 <u>S</u> <u>MF</u> <u>2</u> Meth Sample Test		
10	30599 <u>S</u> <u>BHW</u> <u>3</u> Meth Sample Test		
11	30598 <u>S</u> <u>FHW</u> <u>3</u> Meth Sample Test		
12	30597 <u>S</u> <u>MF</u> <u>3</u> Meth Sample Test		

CHAIN-OF-CUSTODY

Signature	Date/Time	Signature	Date/Time
<u>S. Coughlin</u>	<u>9-23-91 1540</u>		
<u>M. Canan</u>	<u>10-3-91</u>		

ANALYTICAL REPORT

SAMPLE TYPE : FHW ANALYSIS (g) DATE : 09-24-91
 SAMPLING METHOD : M5
 SAMPLE COMPONENT : Acetone ANALYST : MC & KG
 REQUESTED BY : Harris-Woolf, Pre-cleaning Baghouse,
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Sample Volume (ml)	Analytical Result (total sample)	
		Uncorrected	Blank Corr. (g)
1	105	0.02507	0.02498
2	150	0.04336	0.04322
3	160	0.04175	0.04161
Blank	100	0.00009	

ANALYTICAL REPORT

SAMPLE TYPE : FILTERABLE PARTICULATE DATE : 09-24-91
 SAMPLING METHOD : M5
 SAMPLE COMPONENT : 100 mm FILTER ANALYST : MC & KG
 REQUESTED BY : Harris-Woolf, Pre-cleaning Baghouse,
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Filter No.	Analytical Result (total sample)	
		Uncorrected	Blank Corr. (g)
1	457	0.00632	0.00618
2	484	0.00481	0.00467
3	490	0.00548	0.00534
Blank		0.00014	

ANALYTICAL REPORT

SAMPLE TYPE :CONDENSIBLE PARTICULATE DATE : 09-24-91
 SAMPLING METHOD :M5
 SAMPLE COMPONENT :DiH2O ANALYST : MC & KG
 REQUESTED BY :Harris-Woolf, Pre-cleaning Baghouse,
 ANALYTICAL METHOD :GRAVIMETRIC

Test No.	Sample Volume	Analytical Result (total sample) grams	
		Uncorrected	Blank Corrected
1	325	0.00183	0.00154
2	365	0.00172	0.00139
3	395	0.00166	0.00130
Blank	100	0.00009	

ANALYTICAL REPORT

SAMPLE TYPE : FHW ANALYSIS (g) DATE : 09-27-91
 SAMPLING METHOD : M5
 SAMPLE COMPONENT : Acetone ANALYST : MC & KG
 REQUESTED BY : Harris-Woolf, Shelling Baghouse Duct A,
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Sample Volume (ml)	Analytical Result (total sample)	
		Uncorrected	Blank Corr. (g)
1	95	0.01757	0.01748
2	100	0.01198	0.01189
3	105	0.01070	0.01061
Blank	100	0.00009	

ANALYTICAL REPORT

SAMPLE TYPE : FILTERABLE PARTICULATE DATE : 09-27-91
 SAMPLING METHOD : M5
 SAMPLE COMPONENT : 100 mm FILTER ANALYST : MC & KG
 REQUESTED BY : Harris-Woolf, Shelling Baghouse Duct A,
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Filter No.	Analytical Result (total sample)	
		Uncorrected	Blank Corr. (g)
1	485	0.00053	0.00039
2	492	0.00106	0.00092
3	513	0.00014	0.00000
Blank		0.00014	

ANALYTICAL REPORT

SAMPLE TYPE : CONDENSIBLE PARTICULATE DATE : 09-27-91
 SAMPLING METHOD : M5
 SAMPLE COMPONENT : DiH2O ANALYST : MC & KG
 REQUESTED BY : Harris-Woolf, Shelling Baghouse Duct A,
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Sample Volume	Analytical Result (total sample) grams	
		Uncorrected	Blank Corrected
1	330	0.00242	0.00212
2	345	0.00233	0.00202
3	330	0.00788	0.00758
Blank	100	0.00009	

ANALYTICAL REPORT

SAMPLE TYPE : FHW ANALYSIS (g) DATE : 09-27-91
 SAMPLING METHOD : M5
 SAMPLE COMPONENT : Acetone ANALYST : MC & KG
 REQUESTED BY : Harris-Woolf, Shelling Baghouse Duct B,
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Sample Volume (ml)	Analytical Result (total sample)	
		Uncorrected	Blank Corr. (g)
1	110	0.01230	0.01220
2	130	0.00991	0.00979
3	120	0.01052	0.01041
Blank	100	0.00009	

ANALYTICAL REPORT

SAMPLE TYPE : FILTERABLE PARTICULATE DATE : 09-27-91
 SAMPLING METHOD : M5
 SAMPLE COMPONENT : 100 mm FILTER ANALYST : MC & KG
 REQUESTED BY : Harris-Woolf, Shelling Baghouse Duct B,
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Filter No.	Analytical Result (total sample)	
		Uncorrected	Blank Corr. (g)
1	518	0.00145	0.00131
2	519	0.00020	0.00006
3	520	-0.00089	-0.00103
Blank		0.00014	

ANALYTICAL REPORT

SAMPLE TYPE : CONDENSIBLE PARTICULATE DATE : 09-27-91
 SAMPLING METHOD : M5
 SAMPLE COMPONENT : DiH2O ANALYST : MC & KG
 REQUESTED BY : Harris-Woolf, Shelling Baghouse Duct B,
 ANALYTICAL METHOD : GRAVIMETRIC

Test No.	Sample Volume	Analytical Result (total sample) grams	
		Uncorrected	Blank Corrected
1	350	0.00229	0.00198
2	390	0.00475	0.00440
3	340	0.00241	0.00210
Blank	100	0.00009	

SOURCE TEST CALCULATIONS

PLANT : HARRIS WOOLF
PRE-CLEANING BAGHOUSE

RUN NO.: 1
DATE : SEPT 23, 1991

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	114.75 DEG. F	STATIC PRESS.	=	-5.50 in. H2O
STACK TEMP.	=	93.29 DEG. F	Cp	=	0.840
SQ.RT. dP	=	0.9310 in. H2O	STACK I.D.	=	43.00 inch
METER ORIFICE	=	2.99 in. H2O	DUCT LENGTH	=	inch
METER VOLUME	=	111.376 Cu.Ft.	DUCT WIDTH	=	inch
METER Y	=	1.0081	STACK AREA	=	10.085 Sq.Ft.
BAR. PRESSURE	=	29.15 in.Hg	TEST TIME	=	120.00 min.
COND. (Vlc)	=	25.1 ml	NOZZLE DIA.	=	0.2333 inch

GAS ANALYSIS	=	20.90 % O2	0.00 % CO
		0.00 % CO2	79.10 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times$
 $(Pb + (dH / 13.6)) / (Tm + 460) \dots\dots = 99.715 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic = 1.164 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots = 0.012$ | Lower
| Bws

Bws @ Saturated Conditions = Vapor Press. of H2O
@ Dew Point Temp. / (Ps, in.Hg.) $\dots\dots\dots = 0.054$ | value
| used.

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)] = 28.84$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots\dots\dots = 28.71$

$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots = 28.75 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots\dots\dots = 54.74 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots\dots\dots = 33,123 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots\dots\dots = 29,563 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 95.49 \%$

SOURCE TEST CALCULATIONS

PLANT : HARRIS WOOLF
PRE-CLEANING BAGHOUSE

RUN NO.: 2
DATE : SEPT 23, 1991

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	118.1 DEG. F	STATIC PRESS.	=	-5.43 in. H2O
STACK TEMP.	=	100.17 DEG. F	Cp	=	0.840
SQ. RT. dP	=	0.9098 in. H2O	STACK I.D.	=	43.00 inch
METER ORIFICE	=	2.83 in. H2O	DUCT LENGTH	=	inch
METER VOLUME	=	107.662 Cu.Ft.	DUCT WIDTH	=	inch
METER Y	=	1.0081	STACK AREA	=	10.085 Sq.Ft.
BAR. PRESSURE	=	29.58 in.Hg	TEST TIME	=	120.00 min.
COND. (Vlc)	=	18.0 ml	NOZZLE DIA.	=	0.2333 inch

GAS ANALYSIS	:	20.90 % O2	0.00 % CO
		0.00 % CO2	79.10 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times$
 $(Pb + (dH / 13.6)) / (Tm + 460) \dots\dots = 97.196 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vlc = 0.834 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots = 0.009 \text{ Lower}$

$Bws @ \text{ Saturated Conditions} = \text{Vapor Press. of H2O}$
 $@ \text{ Dew Point Temp.} / (Ps, \text{ in.Hg.}) \dots\dots\dots = 0.066 \text{ value used.}$

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)] = 28.84$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots\dots\dots = 28.74$

$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots = 29.18 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460)$
 $/ (Ms \times Ps)] \dots\dots\dots = 53.39 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots\dots\dots = 32,307 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460))$
 $\times (Ps / 29.92) \dots\dots\dots = 29,000 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 94.88 \%$

SOURCE TEST CALCULATIONS

PLANT : HARRIS WOOLF
PRE-CLEANING BAGHOUSE

RUN NO.: 3
DATE : SEPT 23,1991

STANDARD TEMP.: 60 DEG. F

METER TEMP.	= 119.29 DEG. F	STATIC PRESS.	= -5.40 in. H2O
STACK TEMP.	= 101.08 DEG. F	Cp	= 0.840
SQ.RT. dP	= 0.8511 in. H2O	STACK I.D.	= 43.00 inch
METER ORIFICE	= 2.55 in. H2O	DUCT LENGTH	= inch
METER VOLUME	= 105.539 Cu.Ft.	DUCT WIDTH	= inch
METER Y	= 1.0081	STACK AREA	= 10.085 Sq.Ft.
BAR. PRESSURE	= 29.52 in.Hg	TEST TIME	= 120.00 min.
COND. (Vlc)	= 17.2 ml	NOZZLE DIA.	= 0.2333 inch

GAS ANALYSIS	:	20.90 % O2	0.00 % CO
		0.00 % CO2	79.10 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times$
 $(Pb + (dH / 13.6)) / (Tm + 460) \dots\dots = 94.826 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic = 0.797 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots = 0.008$ | Lower
| Bws

Bws @ Saturated Conditions = Vapor Press. of H2O | value
@ Dew Point Temp. / (Ps, in.Hg.) | used.

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)] = 28.84$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots\dots\dots = 28.75$

$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots = 29.12 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots\dots\dots = 50.04 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots\dots\dots = 30,276 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots\dots\dots = 27,084 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 99.12 \%$

SOURCE TEST CALCULATIONS

PLANT : HARRIS MOOLF
HULL/SHELL-A

RUN NO.: 1
DATE : SEPT 27, 1991

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	91 DEG. F	STATIC PRESS.	=	-7.40 in. H2O
STACK TEMP.	=	77.21 DEG. F	Cp	=	0.840
SQ. RT. dP	=	0.9326 in. H2O	STACK I.D.	=	60.00 inch
METER ORIFICE	=	5.70 in. H2O	DUCT LENGTH	=	inch
METER VOLUME	=	166.000 Cu.Ft.	DUCT WIDTH	=	inch
METER Y	=	0.9812	STACK AREA	=	19.635 Sq.Ft.
BAR. PRESSURE	=	29.83 in.Hg	TEST TIME	=	120.00 min.
COND. (Vlc)	=	38.4 ml	NOZZLE DIA.	=	0.2792 inch
GAS ANALYSIS	=	20.90 % O2	0.00 % CO		
		0.00 % CO2	79.10 % N2		

$$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times (Pb + (dH / 13.6)) / (Tm + 460) \dots\dots = 155.406 \text{ dscf}$$

$$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic = 1.780 \text{ scf}$$

$$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots = 0.011 \text{ Lower Bws value}$$

$$Bws @ \text{ Saturated Conditions} = \text{ Vapor Press. of H2O @ Dew Point Temp. / (Ps, in.Hg.) } \dots\dots\dots = 0.032 \text{ used.}$$

$$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$$

$$Md = (.44 \times \%CO2) + (.32 \times \%O2) + (.28 \times (\%N2 + \%CO)) = 28.84$$

$$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots\dots\dots = 28.71$$

$$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots = 29.29 \text{ in. Hg}$$

$$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots\dots\dots = 53.53 \text{ ft/sec}$$

$$Qs = vs \times As \times 60 \dots\dots\dots = 63,063 \text{ acf/min}$$

$$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots\dots\dots = 59,072 \text{ dscf/min}$$

$$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 101.25 \%$$

SOURCE TEST CALCULATIONS

PLANT : HARRIS MOOLF
HULL/SHELL-A

RUN NO.: 2
DATE : SEPT 27, 1991

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	105.77 DEG. F	STATIC PRESS.	=	-7.40 in. H2O
STACK TEMP.	=	92.46 DEG. F	Cp	=	0.840
SQ. RT. dP	=	0.8641 in. H2O	STACK I.D.	=	60.00 inch
METER ORIFICE	=	4.86 in. H2O	DUCT LENGTH	=	inch
METER VOLUME	=	154.130 Cu.Ft.	DUCT WIDTH	=	inch
METER Y	=	0.9812	STACK AREA	=	19.635 Sq.Ft.
BAR. PRESSURE	=	29.68 in.Hg	TEST TIME	=	120.00 min.
COND. (Vlc)	=	36.1 ml	NOZZLE DIA.	=	0.2792 inch

GAS ANALYSIS	:	20.90 % O2	0.00 % CO
		0.00 % CO2	79.10 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times$
 $(Pb + (dH / 13.6)) / (Tm + 460) \dots\dots = 139.543 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic = 1.673 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots = 0.012$ | Lower
| Bws

Bws @ Saturated Conditions = Vapor Press. of H2O | value
@ Dew Point Temp. / (Ps, in.Hg.) | used.

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + (.28 \times (\%N2 + \%CO)) = 28.84$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots\dots\dots = 28.71$

$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots = 29.14 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots\dots\dots = 50.43 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots\dots\dots = 59,412 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots\dots\dots = 53,811 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92] \times 100 / (Time \times Ps \times An \times vs \times 60) = 99.80 \%$

SOURCE TEST CALCULATIONS

PLANT : HARRIS MOOLF
HULL/SHELL-A

RUN NO.: 3
DATE : SEPT 27, 1991

STANDARD TEMP.: 60 DEG. F

METER TEMP.	= 113.29 DEG. F	STATIC PRESS.	= -7.30 in. H2O
STACK TEMP.	= 99.46 DEG. F	Cp	= 0.840
SQ. RT. dP	= 0.8356 in. H2O	STACK I.D.	= 60.00 inch
METER ORIFICE	= 4.58 in. H2O	DUCT LENGTH	= inch
METER VOLUME	= 150.927 Cu.Ft.	DUCT WIDTH	= inch
METER Y	= 0.9812	STACK AREA	= 19.635 Sq.Ft.
BAR. PRESSURE	= 29.54 in.Hg	TEST TIME	= 120.00 min.
COND. (Vlc)	= 25.7 ml	NOZZLE DIA.	= 0.2792 inch

GAS ANALYSIS	:	20.90 % O2	0.00 % CO
		0.00 % CO2	79.10 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times (Pb + (dH / 13.6)) / (Tm + 460) \dots = 134.130 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic = 1.191 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots = 0.009 \text{ | Lower Bws}$

Bws @ Saturated Conditions = Vapor Press. of H2O
@ Dew Point Temp. / (Ps, in.Hg.) $\dots = 0.065 \text{ | value used.}$

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + (.28 \times (\%N2 + \%CO)) = 28.84$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots = 28.74$

$P(stack) = Pbar + [Pstatic / 13.6] \dots = 29.00 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots = 49.16 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots = 57,915 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots = 51,721 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 99.80 \%$

SOURCE TEST CALCULATIONS

PLANT : HARRIS WOOLF
HULL/SHELL-B

RUN NO.: 1
DATE : SEPT 27, 1991

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	93.73 DEG. F	STATIC PRESS.	=	-6.90 in. H2O
STACK TEMP.	=	79.46 DEG. F	Cp	=	0.840
SQ. RT. dP	=	0.7148 in. H2O	STACK I.D.	=	34.00 inch
METER ORIFICE	=	2.90 in. H2O	DUCT LENGTH	=	inch
METER VOLUME	=	109.635 Cu.Ft.	DUCT WIDTH	=	inch
METER Y	=	1.0081	STACK AREA	=	6.305 Sq.Ft.
BAR. PRESSURE	=	29.83 in.Hg	TEST TIME	=	120.00 min.
COND. (Vlc)	=	29.2 ml	NOZZLE DIA.	=	0.2637 inch

GAS ANALYSIS	=	20.90 % O2	0.00 % CO
		0.00 % CO2	79.10 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times (Pb + (dH / 13.6)) / (Tm + 460) \dots\dots = 104.218 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic = 1.354 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots = 0.013 \text{ Lower Bws}$

Bws @ Saturated Conditions = Vapor Press. of H2O @ Dew Point Temp. / (Ps, in.Hg.) $\dots\dots\dots = 0.034 \text{ value used.}$

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + (.28 \times (\%N2 + \%CO)) = 28.84$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots\dots\dots = 28.70$

$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots = 29.32 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots\dots\dots = 41.10 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots\dots\dots = 15,548 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots\dots\dots = 14,500 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 99.57 \%$

SOURCE TEST CALCULATIONS

PLANT : HARRIS WOOLF
HULL/SHELL-B

RUN NO.: 2
DATE : SEPT 27, 1991

STANDARD TEMP.: 60 DEG. F

METER TEMP.	= 105.97 DEG. F	STATIC PRESS.	= -6.50 in. H2O
STACK TEMP.	= 94.04 DEG. F	Cp	= 0.840
SQ. RT. dP	= 0.7324 in. H2O	STACK I.D.	= 34.00 inch
METER ORIFICE	= 3.01 in. H2O	DUCT LENGTH	= inch
METER VOLUME	= 108.072 Cu.Ft.	DUCT WIDTH	= inch
METER Y	= 1.0081	STACK AREA	= 6.305 Sq.Ft.
BAR. PRESSURE	= 29.68 in.Hg	TEST TIME	= 120.00 min.
COND. (Vlc)	= 22.3 ml	NOZZLE DIA.	= 0.2637 inch

GAS ANALYSIS	:	20.90 % O2	0.00 % CO
		0.00 % CO2	79.10 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times (Pb + (dH / 13.6)) / (Tm + 460) \dots\dots = 100.036 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic = 1.034 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots = 0.010 \text{ Lower Bws value used.}$

Bws @ Saturated Conditions = Vapor Press. of H2O @ Dew Point Temp. / (Ps, in.Hg.) $\dots\dots\dots = 0.055$

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + (.28 \times (\%N2 + \%CO)) = 28.84$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots\dots\dots = 28.73$

$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots = 29.20 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots\dots\dots = 42.74 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots\dots\dots = 16,170 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots\dots\dots = 14,661 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 94.53 \%$

SOURCE TEST CALCULATIONS

PLANT : HARRIS WOOLF
HULL/SHELL-B

RUN NO.: 3
DATE : SEPT 27, 1991

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	115.25 DEG. F	STATIC PRESS.	=	-5.60 in. H2O
STACK TEMP.	=	101.46 DEG. F	Cp	=	0.840
SQ. RT. dP	=	0.7071 in. H2O	STACK I.D.	=	34.00 inch
METER ORIFICE	=	2.80 in. H2O	DUCT LENGTH	=	inch
METER VOLUME	=	103.347 Cu.Ft.	DUCT WIDTH	=	inch
METER Y	=	1.0081	STACK AREA	=	6.305 Sq.Ft.
BAR. PRESSURE	=	29.54 in.Hg	TEST TIME	=	120.00 min.
COND. (Vlc)	=	21.5 ml	NOZZLE DIA.	=	0.2637 inch

GAS ANALYSIS	:	20.90 % O2	0.00 % CO
		0.00 % CO2	79.10 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times$
 $(Pb + (dH / 13.6)) / (Tm + 460) \dots\dots = 93.630 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vic = 0.997 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots = 0.011 \text{ Lower}$

$Bws @ \text{ Saturated Conditions} = \text{Vapor Press. of H2O}$
 $@ \text{ Dew Point Temp.} / (Ps, \text{ in.Hg.}) \dots\dots\dots = 0.068 \text{ Bws value used.}$

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)] = 28.84$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots\dots\dots = 28.72$

$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots = 29.13 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq. Rt. dP) \times [Sq. Rt. (Ts + 460) / (Ms \times Ps)] \dots\dots\dots = 41.60 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots\dots\dots = 15,736 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots\dots\dots = 14,039 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 92.39 \%$

EMISSION RATE CALCULATIONS

PLANT : HARRIS WOOLF
PRE-CLEANING BAGHOUSE

RUN NO.: 1
DATE : SEPT 23, 1991
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.02498 grams | Vm(std)  99.715 ft3
Mass Filter (MF)           0.00618 grams | Vw(std)  -1.164 ft3
Back Half Wash (BHW)       0.00154 grams | Qs(std)  29,563 dscfm
Front Half Sulfate (FHS)    0.00 mg H2SO4 | Bws      -0.012
Back Half Sulfate (BHS)     0.00 mg H2SO4 | CO2       0.00 %
H2O2 Catch (SO2)           0.00 mg H2SO4 | O2        20.90 %
*****
```

F-FACTOR

$10E6 \times [3.64(\%H) + 1.53(\%C) + 0.57(\%S) + 0.14(\%N) - 0.46(\%O_2)] / (Btu/lb) \times [(Tstd + 460)/528] \dots\dots\dots$ dscf/MMBtu

FILTERABLE PARTICULATE

$15.432 \times (FHW + MF) / [Vm(std) + Vw(std)] \dots\dots\dots$ 0.0048 gr/scf
 $15.432 \times (FHW + MF) / Vm(std) \dots\dots\dots$ 0.0048 gr/dscf
 gr/dscf $\times (12 / \%CO_2) \dots\dots\dots$ @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf \dots\dots\dots$ 1.22 lb/hr
 F-Fac $\times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf \dots\dots\dots$ lb/MMBtu

TOTAL PARTICULATE

$15.432 \times (FHW + MF + BHW) / [(Vm(std) + Vw(std))] \dots\dots\dots$ 0.0050 gr/scf
 $15.432 \times (FHW + MF + BHW) / Vm(std) \dots\dots\dots$ 0.0051 gr/dscf
 gr/dscf $\times (12 / \%CO_2) \dots\dots\dots$ @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf \dots\dots\dots$ 1.28 lb/hr
 F-Fac $\times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf \dots\dots\dots$ lb/MMBtu

TOTAL SULFATE

$0.015432 \times (FHS + BHS) / [Vm(std) + Vw(std)] \dots\dots\dots$ gr/scf
 $0.015432 \times (FHS + BHS) / Vm(std) \dots\dots\dots$ gr/dscf
 gr/dscf $\times (12 / \%CO_2) \dots\dots\dots$ @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf \dots\dots\dots$ lb/hr
 F-Fac $\times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf \dots\dots\dots$ lb/MMBtu

SULFUR DIOXIDE (SO2)

$1.60982 \times [T(std) + 460] \times (mg H_2SO_4) / [98.076 \times Vm(std)] \dots\dots\dots$ ppm
 ppm $\times [(20.9 - \text{Oxygen Corr.}) / (20.9 - \%O_2)] \dots\dots\dots$ @ O2 corr.
 ppm $\times (1 - Bws) \dots\dots\dots$ ppm (wet)
 $8.223E-5 \times Qs(std) \times 64.062 \times ppm / [T(std) + 460] \dots\dots\dots$ lb/hr
 F-Factor $\times 64.062 \times [1.3711E-6 / [T(std) + 460]] \times [20.9 / (20.9 - \%O_2)] \times ppm \dots\dots\dots$ lb/MMBtu
 lb/hr / (dscfm $\times 60$ min/hr) $\dots\dots\dots$ lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 $\dots\dots\dots$ lb/MMBtu
 (lb/MMBtu Total Sulfate) $\times (32 / 98.076) \dots\dots\dots$ lb/MMBtu
 Total Sulfur $\dots\dots\dots$ lb/MMBtu

EMISSION RATE CALCULATIONS

PLANT : HARRIS WOOLF
PRE-CLEANING BAGHOUSE

RUN NO.: 2
DATE : SEPT 23, 1991
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.04322 grams   | Vm(std)  97.196 ft3
Mass Filter (MF)           0.00467 grams   | Vw(std)  -0.834 ft3
Back Half Wash (BHW)       0.00139 grams   | Qs(std)  29,000 dscfm
Front Half Sulfate (FHS)    0.00 mg H2SO4 | Bws      -0.009
Back Half Sulfate (BHS)     0.00 mg H2SO4 | CO2      0.00 %
H2O2 Catch (SO2)           0.00 mg H2SO4 | O2       20.90 %
*****
```

F-FACTOR

10E6 x [3.64(%H) + 1.53(%C) + 0.57(%S) + 0.14(%N) -
0.46(%O2)] / (Btu/lb) x [(Tstd + 460)/528] dscf/MMBtu

FILTERABLE PARTICULATE

15.432 x (FHW + MF) / [Vm(std) + Vw(std)] 0.0075 gr/scf
15.432 x (FHW + MF) / Vm(std) 0.0076 gr/dscf
gr/dscf x (12 / %CO2) @ 12% CO2
0.00857 x Qs(std) x gr/dscf 1.89 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. lb/MMBtu

TOTAL PARTICULATE

15.432 x (FHW + MF + BHW) / [(Vm(std) + Vw(std))] ... 0.0078 gr/scf
15.432 x (FHW + MF + BHW) / (Vm(std) 0.0078 gr/dscf
gr/dscf x (12 / %CO2) @ 12% CO2
0.00857 x Qs(std) x gr/dscf 1.94 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. lb/MMBtu

TOTAL SULFATE

0.015432 x (FHS + BHS) / [Vm(std) + Vw(std)] gr/scf
0.015432 x (FHS + BHS) / Vm(std) gr/dscf
gr/dscf x (12 / %CO2) @ 12% CO2
0.00857 x Qs(std) x gr/dscf lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. lb/MMBtu

SULFUR DIOXIDE (SO2)

1.60982 x [T(std) + 460] x (mg H2SO4) / [98.076 x
Vm(std)] ppm
ppm x [(20.9 - Oxygen Corr.) / (20.9 - %O2)] @ O2 corr.
ppm x (1 - Bws) ppm (wet)
8.223E-5 x Qs(std) x 64.062 x ppm / [T(std) + 460].. lb/hr
F-Factor x 64.062 x [1.3711E-6 / [T(std) + 460]] x
[20.9 / (20.9 - %O2)] x ppm lb/MMBtu
lb/hr / (dscfm x 60 min/hr) lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 lb/MMBtu
(lb/MMBtu Total Sulfate) x (32 / 98.076) lb/MMBtu
Total Sulfur lb/MMBtu

EMISSION RATE CALCULATIONS

PLANT : HARRIS WOOLF
PRE-CLEANING BAGHOUSE

RUN NO.: 3
DATE : SEPT 23, 1991
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.04161 grams | Vm(std)  94.826 ft3
Mass Filter (MF)           0.00534 grams | Vw(std)  -0.797 ft3
Back Half Wash (BHW)       0.00130 grams | Qs(std)  27,084 dscfm
Front Half Sulfate (FHS)    0.00 mg H2SO4 | Bws      -0.008
Back Half Sulfate (BHS)     0.00 mg H2SO4 | CO2       0.00 %
H2O2 Catch (SO2)           0.00 mg H2SO4 | O2        20.90 %
*****
```

F-FACTOR

$10E6 \times [3.64(\%H) + 1.53(\%C) + 0.57(\%S) + 0.14(\%N) - 0.46(\%O_2)] / (Btu/lb) \times [(T_{std} + 460)/528]$ dscf/MMBtu

FILTERABLE PARTICULATE

$15.432 \times (FHW + MF) / [Vm(std) + Vw(std)]$ 0.0076 gr/scf
 $15.432 \times (FHW + MF) / Vm(std)$ 0.0076 gr/dscf
 gr/dscf x (12 / %CO₂) @ 12% CO₂
 $0.00857 \times Qs(std) \times gr/dscf$ 1.77 lb/hr
 F-Fac x $1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL PARTICULATE

$15.432 \times (FHW + MF + BHW) / [(Vm(std) + Vw(std))]$... 0.0078 gr/scf
 $15.432 \times (FHW + MF + BHW) / (Vm(std))$ 0.0079 gr/dscf
 gr/dscf x (12 / %CO₂) @ 12% CO₂
 $0.00857 \times Qs(std) \times gr/dscf$ 1.82 lb/hr
 F-Fac x $1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL SULFATE

$0.015432 \times (FHS + BHS) / [Vm(std) + Vw(std)]$ gr/scf
 $0.015432 \times (FHS + BHS) / Vm(std)$ gr/dscf
 gr/dscf x (12 / %CO₂) @ 12% CO₂
 $0.00857 \times Qs(std) \times gr/dscf$ lb/hr
 F-Fac x $1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

SULFUR DIOXIDE (SO₂)

$1.60982 \times [T(std) + 460] \times (mg H_2SO_4) / [98.076 \times Vm(std)]$ ppm
 ppm x $[(20.9 - O_2 \text{ Corr.}) / (20.9 - \%O_2)]$ @ O₂ corr.
 ppm x (1 - Bws) ppm (wet)
 $8.223E-5 \times Qs(std) \times 64.062 \times ppm / [T(std) + 460]$.. lb/hr
 F-Factor x $64.062 \times [1.3711E-6 / [T(std) + 460]] \times [20.9 / (20.9 - \%O_2)] \times ppm$ lb/MMBtu
 lb/hr / (dscfm x 60 min/hr) lb/dscf

SULFUR (S)

(lb/MMBtu SO₂) / 2 lb/MMBtu
 (lb/MMBtu Total Sulfate) x (32 / 98.076) lb/MMBtu
 Total Sulfur lb/MMBtu

EMISSION RATE CALCULATIONS

PLANT : HARRIS MOOLF
HULL/SHELL-A

RUN NO.: 1
DATE : SEPT 27, 1991
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.01748 grams | Vm(std) 155.406 ft3
Mass Filter (MF)           0.00039 grams | Vw(std)  1.780 ft3
Back Half Wash (BHW)       0.00212 grams | Qs(std) 59.072 dscfm
Front Half Sulfate (FHS)    0.00 mg H2SO4 | Bws     0.011
Back Half Sulfate (BHS)     0.00 mg H2SO4 | CO2      0.00 %
H2O2 Catch (SO2)           0.00 mg H2SO4 | O2       20.90 %
*****
```

F-FACTOR

$10E6 \times [3.64(\%H) + 1.53(\%C) + 0.57(\%S) + 0.14(\%N) - 0.46(\%O_2)] / (Btu/lb) \times [(T_{std} + 460)/528]$ dscf/MMBtu

FILTERABLE PARTICULATE

$15.432 \times (FHW + MF) / [Vm(std) + Vw(std)]$ 0.0018 gr/scf
 $15.432 \times (FHW + MF) / Vm(std)$ 0.0018 gr/dscf
 gr/dscf $\times (12 / \%CO_2)$ @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 0.90 lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL PARTICULATE

$15.432 \times (FHW + MF + BHW) / [(Vm(std) + Vw(std))]$... 0.0020 gr/scf
 $15.432 \times (FHW + MF + BHW) / (Vm(std))$ 0.0020 gr/dscf
 gr/dscf $\times (12 / \%CO_2)$ @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 1.00 lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL SULFATE

$0.015432 \times (FHS + BHS) / [Vm(std) + Vw(std)]$ gr/scf
 $0.015432 \times (FHS + BHS) / Vm(std)$ gr/dscf
 gr/dscf $\times (12 / \%CO_2)$ @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

SULFUR DIOXIDE (SO2)

$1.60982 \times [T(std) + 460] \times (mg H_2SO_4) / [98.076 \times Vm(std)]$ ppm
 ppm $\times [(20.9 - O_2 \text{ Corr.}) / (20.9 - \%O_2)]$ @ O2 corr.
 ppm $\times (1 - Bws)$ ppm (wet)
 $8.223E-5 \times Qs(std) \times 64.062 \times ppm / [T(std) + 460]$.. lb/hr
 $F-Factor \times 64.062 \times [1.3711E-6 / [T(std) + 460]] \times [20.9 / (20.9 - \%O_2)] \times ppm$ lb/MMBtu
 lb/hr / (dscfm $\times 60 \text{ min/hr}$) lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 lb/MMBtu
 (lb/MMBtu Total Sulfate) $\times (32 / 98.076)$ lb/MMBtu
 Total Sulfur lb/MMBtu

EMISSION RATE CALCULATIONS

PLANT : HARRIS MOOLF
HULL/SHELL-A

RUN NO.: 2
DATE : SEPT 27, 1991
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.01189 grams | Vm(std) 139.543 ft3
Mass Filter (MF)           0.00092 grams | Vw(std)  1.673 ft3
Back Half Wash (BHW)       0.00202 grams | Qs(std) 53.811 dscfm
Front Half Sulfate (FHS)    0.00 mg H2SO4 | Bws      0.012
Back Half Sulfate (BHS)     0.00 mg H2SO4 | CO2       0.00 %
H2O2 Catch (SO2)           0.00 mg H2SO4 | O2        20.90 %
*****
```

F-FACTOR

$10E6 \times [3.64(\%H) + 1.53(\%C) + 0.57(\%S) + 0.14(\%N) - 0.46(\%O2)] / (Btu/lb) \times [(Tstd + 460)/528]$ dscf/MMBtu

FILTERABLE PARTICULATE

$15.432 \times (FHW + MF) / [Vm(std) + Vw(std)]$ 0.0014 gr/scf
 $15.432 \times (FHW + MF) / Vm(std)$ 0.0014 gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 0.65 lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O2)] \times gr/dscf$.. lb/MMBtu

TOTAL PARTICULATE

$15.432 \times (FHW + MF + BHW) / [(Vm(std) + Vw(std))]$... 0.0016 gr/scf
 $15.432 \times (FHW + MF + BHW) / Vm(std)$ 0.0016 gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 0.76 lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O2)] \times gr/dscf$.. lb/MMBtu

TOTAL SULFATE

$0.015432 \times (FHS + BHS) / [Vm(std) + Vw(std)]$ gr/scf
 $0.015432 \times (FHS + BHS) / Vm(std)$ gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O2)] \times gr/dscf$.. lb/MMBtu

SULFUR DIOXIDE (SO2)

$1.60982 \times [T(std) + 460] \times (mg H2SO4) / [98.076 \times Vm(std)]$ ppm
 ppm x [(20.9 - Oxygen Corr.) / (20.9 - %O2)] @ O2 corr.
 ppm x (1 - Bws) ppm (wet)
 $8.223E-5 \times Qs(std) \times 64.062 \times ppm / [T(std) + 460]$.. lb/hr
 $F-Factor \times 64.062 \times [1.3711E-6 / [T(std) + 460]] \times [20.9 / (20.9 - \%O2)] \times ppm$ lb/MMBtu
 lb/hr / (dscfm x 60 min/hr) lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 lb/MMBtu
 (lb/MMBtu Total Sulfate) x (32 / 98.076) lb/MMBtu
 Total Sulfur lb/MMBtu

EMISSION RATE CALCULATIONS

PLANT : HARRIS MOOLF
HULL/SHELL-A

RUN NO.: 3
DATE : SEPT 27, 1991
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.01061 grams | Vm(std) 134.130 ft3
Mass Filter (MF)           0.00000 grams | Vw(std)  1.191 ft3
Back Half Wash (BHW)       0.00758 grams | Qs(std) 51,721 dscfm
Front Half Sulfate (FHS)    0.00 mg H2SO4 | Bws      0.009
Back Half Sulfate (BHS)     0.00 mg H2SO4 | CO2       0.00 %
H2O2 Catch (SO2)           0.00 mg H2SO4 | O2        20.90 %
*****
```

F-FACTOR

10E6 x [3.64(%H) + 1.53(%C) + 0.57(%S) + 0.14(%N) -
0.46(%O2)] / (Btu/lb) x [(Tstd + 460)/528] dscf/MMBtu

FILTERABLE PARTICULATE

15.432 x (FHW + MF) / [Vm(std) + Vw(std)] 0.0012 gr/scf
15.432 x (FHW + MF) / Vm(std) 0.0012 gr/dscf
gr/dscf x (12 / %CO2) @ 12% CO2
0.00857 x Qs(std) x gr/dscf 0.54 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. lb/MMBtu

TOTAL PARTICULATE

15.432 x (FHW + MF + BHW) / [(Vm(std) + Vw(std)] ... 0.0021 gr/scf
15.432 x (FHW + MF + BHW) / (Vm(std) 0.0021 gr/dscf
gr/dscf x (12 / %CO2) @ 12% CO2
0.00857 x Qs(std) x gr/dscf 0.93 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. lb/MMBtu

TOTAL SULFATE

0.015432 x (FHS + BHS) / [Vm(std) + Vw(std)] gr/scf
0.015432 x (FHS + BHS) / Vm(std) gr/dscf
gr/dscf x (12 / %CO2) @ 12% CO2
0.00857 x Qs(std) x gr/dscf lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. lb/MMBtu

SULFUR DIOXIDE (SO2)

1.60982 x [T(std) + 460] x (mg H2SO4) / [98.076 x
Vm(std)] ppm
ppm x [(20.9 - Oxygen Corr.) / (20.9 - %O2)] @ O2 corr.
ppm x (1 - Bws) ppm (wet)
8.223E-5 x Qs(std) x 64.062 x ppm / [T(std) + 460].. lb/hr
F-Factor x 64.062 x [1.3711E-6 / [T(std) + 460]] x
[20.9 / (20.9 - %O2)] x ppm lb/MMBtu
lb/hr / (dscfm x 60 min/hr) lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 lb/MMBtu
(lb/MMBtu Total Sulfate) x (32 / 98.076) lb/MMBtu
Total Sulfur lb/MMBtu

EMISSION RATE CALCULATIONS

PLANT : HARRIS WOOLF
HULL/SHELL-B

RUN NO.: 1
DATE : SEPT 27, 1991
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.01220 grams   | Vm(std) 104.218 ft3
Mass Filter (MF)           0.00131 grams   | Vw(std)  1.354 ft3
Back Half Wash (BHW)       0.00198 grams   | Qs(std) 14,500 dscfm
Front Half Sulfate (FHS)    0.00 mg H2SO4  | Bws      0.013
Back Half Sulfate (BHS)    0.00 mg H2SO4  | CO2      0.00 %
H2O2 Catch (SO2)          0.00 mg H2SO4  | O2       20.90 %
*****
```

F-FACTOR

10E6 x [3.64(%H) + 1.53(%C) + 0.57(%S) + 0.14(%N) -
0.46(%O2)] / (Btu/lb) x [(Tstd + 460)/528] dscf/MMBtu

FILTERABLE PARTICULATE

15.432 x (FHW + MF) / [Vm(std) + Vw(std)] 0.0020 gr/scf
15.432 x (FHW + MF) / Vm(std) 0.0020 gr/dscf
gr/dscf x (12 / %CO2) @ 12% CO2
0.00857 x Qs(std) x gr/dscf 0.25 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. lb/MMBtu

TOTAL PARTICULATE

15.432 x (FHW + MF + BHW) / [(Vm(std) + Vw(std))] 0.0023 gr/scf
15.432 x (FHW + MF + BHW) / Vm(std) 0.0023 gr/dscf
gr/dscf x (12 / %CO2) @ 12% CO2
0.00857 x Qs(std) x gr/dscf 0.29 lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. lb/MMBtu

TOTAL SULFATE

0.015432 x (FHS + BHS) / [Vm(std) + Vw(std)] gr/scf
0.015432 x (FHS + BHS) / Vm(std) gr/dscf
gr/dscf x (12 / %CO2) @ 12% CO2
0.00857 x Qs(std) x gr/dscf lb/hr
F-Fac x 1.4286E-4 x [20.9 / (20.9-%O2)] x gr/dscf .. lb/MMBtu

SULFUR DIOXIDE (SO2)

1.60982 x [T(std) + 460] x (mg H2SO4) / [98.076 x
Vm(std)] ppm
ppm x [(20.9 - Oxygen Corr.) / (20.9 - %O2)] @ O2 corr.
ppm x (1 - Bws) ppm (wet)
8.223E-5 x Qs(std) x 64.062 x ppm / [T(std) + 460].. lb/hr
F-Factor x 64.062 x [1.3711E-6 / [T(std) + 460]] x
[20.9 / (20.9 - %O2)] x ppm lb/MMBtu
lb/hr / (dscfm x 60 min/hr) lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 lb/MMBtu
(lb/MMBtu Total Sulfate) x (32 / 98.076) lb/MMBtu
Total Sulfur lb/MMBtu

EMISSION RATE CALCULATIONS

PLANT : HARRIS WOOLF
HULL/SHELL-B

RUN NO.: 2
DATE : SEPT 27, 1991
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.00979 grams   | Vm(std) 100.036 ft3
Mass Filter (MF)           0.00006 grams   | Vw(std)  1.034 ft3
Back Half Wash (BHW)       0.00440 grams   | Qs(std) 14,661 dscfm
Front Half Sulfate (FHS)    0.00 mg H2SO4  | Bws      0.010
Back Half Sulfate (BHS)     0.00 mg H2SO4  | CO2      0.00 %
H2O2 Catch (SO2)           0.00 mg H2SO4  | O2       20.90 %
*****
```

F-FACTOR

$10E6 \times [3.64(\%H) + 1.53(\%C) + 0.57(\%S) + 0.14(\%N) - 0.46(\%O_2)] / (Btu/lb) \times [(Tstd + 460)/528]$ dscf/MMBtu

FILTERABLE PARTICULATE

$15.432 \times (FHW + MF) / [Vm(std) + Vw(std)]$ 0.0015 gr/scf
 $15.432 \times (FHW + MF) / Vm(std)$ 0.0015 gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 0.19 lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL PARTICULATE

$15.432 \times (FHW + MF + BHW) / [(Vm(std) + Vw(std))]$... 0.0022 gr/scf
 $15.432 \times (FHW + MF + BHW) / (Vm(std))$ 0.0022 gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 0.28 lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL SULFATE

$0.015432 \times (FHS + BHS) / [Vm(std) + Vw(std)]$ gr/scf
 $0.015432 \times (FHS + BHS) / Vm(std)$ gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

SULFUR DIOXIDE (SO2)

$1.60982 \times [T(std) + 460] \times (mg H_2SO_4) / [98.076 \times Vm(std)]$ ppm
 ppm x [(20.9 - Oxygen Corr.) / (20.9 - %O2)] @ O2 corr.
 ppm x (1 - Bws) ppm (wet)
 $8.223E-5 \times Qs(std) \times 64.062 \times ppm / [T(std) + 460]$.. lb/hr
 $F-Factor \times 64.062 \times [1.3711E-6 / [T(std) + 460]] \times [20.9 / (20.9 - \%O_2)] \times ppm$ lb/MMBtu
 lb/hr / (dscfm x 60 min/hr) lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 lb/MMBtu
 (lb/MMBtu Total Sulfate) x (32 / 98.076) lb/MMBtu
 Total Sulfur lb/MMBtu

EMISSION RATE CALCULATIONS

PLANT : HARRIS WOOLF
HULL/SHELL-B

RUN NO.: 3
DATE : SEPT 27, 1991
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.01041 grams   | Vm(std)  93.630 ft3
Mass Filter (MF)           0.00000 grams   | Vw(std)  _0.997 ft3
Back Half Wash (BHW)       0.00210 grams   | Qs(std)  14,039 dscfm
Front Half Sulfate (FHS)    0.00 mg H2SO4 | Bws      _0.011
Back Half Sulfate (BHS)     0.00 mg H2SO4 | CO2      _0.00 %
H2O2 Catch (SO2)           0.00 mg H2SO4 | O2       20.90 %
*****
```

F-FACTOR

$10E6 \times [3.64(\%H) + 1.53(\%C) + 0.57(\%S) + 0.14(\%N) - 0.46(\%O_2)] / (Btu/lb) \times [(Tstd + 460)/528] \dots\dots\dots$ dscf/MMBtu

FILTERABLE PARTICULATE

$15.432 \times (FHW + MF) / [Vm(std) + Vw(std)] \dots\dots\dots$ 0.0017 gr/scf
 $15.432 \times (FHW + MF) / Vm(std) \dots\dots\dots$ 0.0017 gr/dscf
 gr/dscf $\times (12 / \%CO_2) \dots\dots\dots$ @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf \dots\dots\dots$ 0.21 lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf \dots$ lb/MMBtu

TOTAL PARTICULATE

$15.432 \times (FHW + MF + BHW) / [(Vm(std) + Vw(std))] \dots$ 0.0020 gr/scf
 $15.432 \times (FHW + MF + BHW) / Vm(std) \dots\dots\dots$ 0.0021 gr/dscf
 gr/dscf $\times (12 / \%CO_2) \dots\dots\dots$ @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf \dots\dots\dots$ 0.25 lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf \dots$ lb/MMBtu

TOTAL SULFATE

$0.015432 \times (FHS + BHS) / [Vm(std) + Vw(std)] \dots\dots\dots$ gr/scf
 $0.015432 \times (FHS + BHS) / Vm(std) \dots\dots\dots$ gr/dscf
 gr/dscf $\times (12 / \%CO_2) \dots\dots\dots$ @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf \dots\dots\dots$ lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf \dots$ lb/MMBtu

SULFUR DIOXIDE (SO2)

$1.60982 \times [T(std) + 460] \times (mg H_2SO_4) / [98.076 \times Vm(std)] \dots\dots\dots$ ppm
 ppm $\times [(20.9 - \text{Oxygen Corr.}) / (20.9 - \%O_2)] \dots\dots\dots$ @ O2 corr.
 ppm $\times (1 - Bws) \dots\dots\dots$ ppm (wet)
 $8.223E-5 \times Qs(std) \times 64.062 \times ppm / [T(std) + 460] \dots$ lb/hr
 $F-Factor \times 64.062 \times [1.3711E-6 / [T(std) + 460]] \times$
 $[20.9 / (20.9 - \%O_2)] \times ppm \dots\dots\dots$ lb/MMBtu
 lb/hr / (dscfm $\times 60$ min/hr) $\dots\dots\dots$ lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 $\dots\dots\dots$ lb/MMBtu
 (lb/MMBtu Total Sulfate) $\times (32 / 98.076) \dots\dots\dots$ lb/MMBtu
 Total Sulfur $\dots\dots\dots$ lb/MMBtu

DRY GAS METER / ORIFICE METER CALIBRATION DATA

Date07/22/91
 Bar. Press, in.Hg 29.72
 Meter Box No. 779

Dry Gas Meter No. ... 658977
 Standard Test Meter # 69279
 Operator DM

STANDARD TEST METER			DRY TEST METER				Time t (min)
Press. dHs (in. H2O)	Temp. Ts (dF)	Volume Vs (ft3)	Press. dH (in. H2O)	Temp. Tdi (dF)	Temp. Tdo (dF)	Volume Vd (ft3)	
	70.0	279.390		96	93	207.738	
-1.0	69.0	260.522	0.5	94	89	187.938	49.0
Avg/Net :	69.5	18.868			93	19.800	
	72.0	341.427		109	98	271.362	
-1.5	71.0	321.939	1.0	100	95	251.184	36.0
Avg/Net :	71.5	19.488			101	20.178	
	68.0	259.770		100	88	187.152	
-1.8	68.0	239.616	1.5	76	77	166.532	31.0
Avg/Net :	68.0	20.154			85	20.620	
	71.0	321.256		103	95	250.486	
-2.3	70.0	300.894	2.0	100	95	229.639	27.0
Avg/Net :	70.5	20.362			98	20.847	
	70.0	300.258		105	95	228.980	
-3.0	70.0	280.112	3.0	97	93	208.485	22.0
Avg/Net :	70.0	20.146			98	20.495	

$$Y = V_s \times (P_{bar} + (dH_s / 13.6)) \times (Avg. T_d + 460) / [V_d \times (P_{bar} + (dH / 13.6)) \times (T_s + 460)]$$

$$K_o = [(V_s/t) \times [(T_{do} + 460) / (T_s + 460)] \times [(P_{bar} + (dH_s/13.6)) / (P_{bar} + (dH/13.6))] / [((T_{do} + 460) \times dH) / (P_{bar} + (dH/13.6))] \times (M_m)]^{0.5}$$

dH :	0.5	1.0	1.5	2.0	3.0	Avg.	Std.Dev.
Y :	0.9915	1.0122	1.0011	1.0169	1.0187	1.0081	0.0103
Ko :	0.706	0.7014	0.6827	0.6891	0.6812	0.6921	0.0100
Y :	1.02 % Relative Std. Dev.						
Ko :	1.44 % Relative Std. Dev.						

DRY GAS METER / ORIFICE METER CALIBRATION DATA

DateSEPT 21,1991
 Bar. Press, in.Hg 29.57
 Meter Box No. 644

Dry Gas Meter No. ... 1008455
 Standard Test Meter # 69279
 Operator JS

STANDARD TEST METER			DRY TEST METER				
Press. dHs (in. H2O)	Temp. Ts (dF)	Volume Vs (ft3)	Press. dH (in. H2O)	Temp. Tdi (dF)	Temp. Tdo (dF)	Volume Vd (ft3)	Time t (min)
	80.0	717.379		108	106	571.366	
-1.0	75.0	697.129	0.5	97	92	550.107	50.0
Avg/Net :	77.5	20.250			101	21.259	
	82.0	740.078		113	110	595.624	
-1.6	80.0	719.864	1.0	110	107	574.012	36.0
Avg/Net :	81.0	20.214			110	21.612	
	83.0	762.838		116	113	620.017	
-2.0	82.0	742.021	1.5	114	110	597.714	31.0
Avg/Net :	82.5	20.817			113	22.303	
	84.0	784.980		117	114	643.633	
-2.5	83.0	765.340	2.0	116	113	622.711	25.0
Avg/Net :	83.5	19.640			115	20.922	
	85.0	808.084		120	117	668.286	
-3.5	85.0	787.858	3.0	118	114	646.712	21.0
Avg/Net :	85.0	20.226			117	21.574	

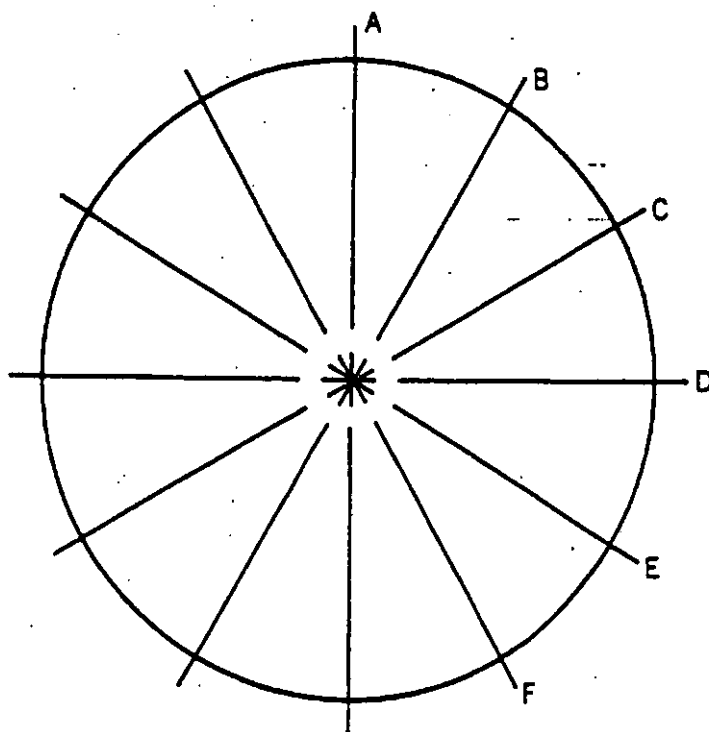
$$y = V_s \times (P_{bar} + (dH_s / 13.6)) \times (Avg. T_d + 460) / [V_d \times (P_{bar} + (dH / 13.6)) \times (T_s + 460)]$$

$$K_o = [(V_s/t) \times [(T_{do} + 460) / (T_s + 460)] \times [(P_{bar} + (dH_s/13.6)) / (P_{bar} + (dH/13.6))] / [((T_{do} + 460) \times dH) / (P_{bar} + (dH/13.6))] \times (Mm)]^{0.5}$$

dH :	0.5	1.0	1.5	2.0	3.0	Avg.	Std.Dev.
y :	0.9902	0.9791	0.9777	0.9821	0.9771	0.9812	0.0048
Ko :	0.7351	0.7204	0.7022	0.7101	0.7074	0.7150	0.0116
y :	0.49 % Relative Std. Dev.						
Ko :	1.63 % Relative Std. Dev.						

 Steiner Environmental, Inc.

NOZZLE CALIBRATION



DIAMETER (in.)

A 0.2332

B 0.2342

C 0.2325

D 0.2331

E _____

F _____

AVG. 0.2333

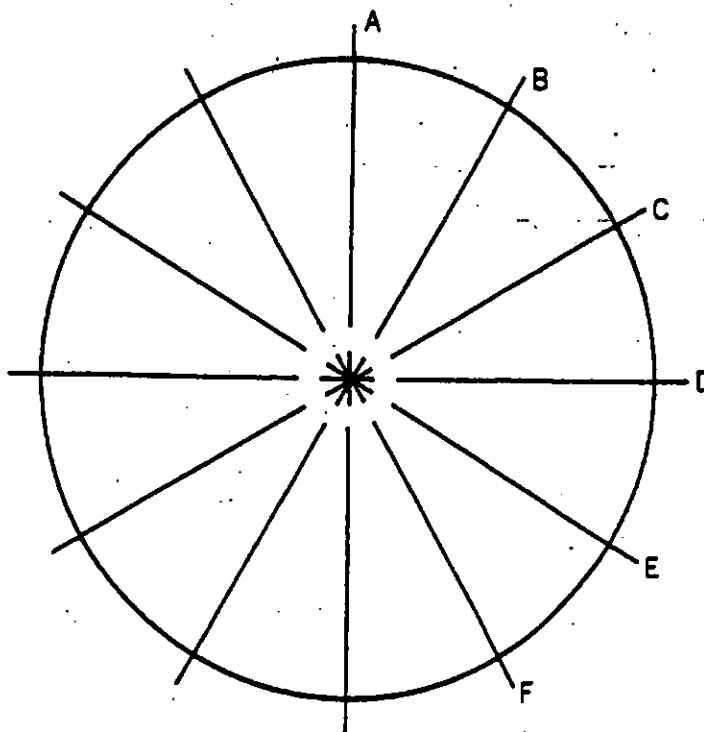
DATE 7-18-91

NOZZLE NO. 1458

OPERATOR SW

 Steiner Environmental, Inc.

NOZZLE CALIBRATION



DIAMETER (in.)

A .2781

B .2815

C .2790

D .2782

E _____

F _____

AVG. .2792

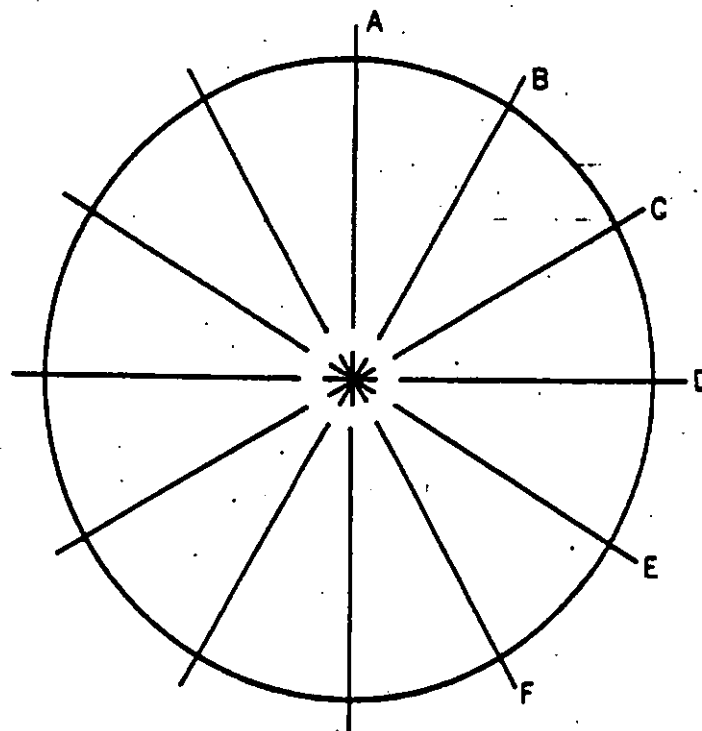
DATE 7-18-91

NOZZLE NO. 1555

OPERATOR Sw

 Steiner Environmental, Inc.

NOZZLE CALIBRATION



DIAMETER (in.)

A 0.2619

B 0.2625

C 0.2645

D 0.2660

E _____

F _____

AVG. 0.2637

DATE 7-18-91

NOZZLE NO. 208

OPERATOR SW

APPENDIX B
HARRIS WOOLF OPERATING DATA

000542

HARRIS - WOOLF
CALIFORNIA ALMONDS

RECEIVED

OCT - 8 1991

Ans'd.....

HULLER LOG

DATE 9-27-91

TIME	ISCALE	TICKET	GROWER	FIELD	TANK	INCOMING FIELD RUN	Comments
	NUMBER				NUMBER	LBS	
Pm 17:35	1916	CVLC	SEC 8	5	54.560		
Pm 29:20	1943	CVLC	Block 4	3	16.490		Test 1
Pm 310:40	1941	Harris	SEC 8	2	4.3440		
Pm 412:45	1944	Harris	Block 4	1	43.820		Test 2
Pm 52:35	1947	Harris	16-15-11	3	24.330		
Pm 63:35	1946	Harris	NW 14	5	18.660		Test 3
Pm 74:35	1949	Harris	NW 14	2	42.790		Total Field Run
8 Stop	600 am						2002,650
9	Shear	Rollers					
10	Air	Brigs					3 Age house Test
11	Pum.	one	Friday	By			
12							
13							
14							
15							
16							

TOTAL 1XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX11XXXXXXXXXXXXXXXXXXXX11
 TODAY 1XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX11XXXXXXXXXXXXXXXXXXXX11

OPERATOR.....

HULLER LOG

HARRIS - WOLF
CALIFORNIA ALMONDS

PRECLEANER LOG

DATE 23-9-91

TIME START	TIME STOP	I SCALETICKET# NUMBER	GROWER	FIELD	TANK	INCOMING FIELDRUN LBS	COMMENTS
9:40	10:55	1886 ✓	Sayer America	SW 7	5	48,220 ✓	
11:00	12:40	1903 ✓	CULC	S-8 BKI	2	62,440 ✓	} Test 1
1245	32:15	1904 ✓	MATTS	KW 14	5	49,800 ✓	
2:20	3:35	1905 ✓	Aufelore	HAY 48	7	45,280 ✓	} Test 2
3:35	5:10	1906 ✓	BARTIS	NUGY	2	50,230 ✓	
6:25	6:	1907 ✓	Fanning	26-1	5	50,900 ✓	} Test 3
8:00	7:	1909 ✓	Bartis	NUGY, H-H	2	48,870 ✓	
11:38	:	1890 ✓	OVLG	Sec 8 BK I	2	52,010	
1'45	9:	1892 ✓	CVLC	Sec 8 BK I	5	54,850 ✓	
3:20	10:	1871 ✓	CVLL	Sec 8 BK I	2	53,770 ✓	
4:20	11:	" "	" "	" "	" "	" "	
630	12:	" "	" "	" "	" "	" "	New stuff
13:							
14:			Pre Cleaner	Field runny log			Eat
15:			Test on #3	1991			
16:							
		TOTAL TODAY	XXXXXXXXXXXXX XXXXXXXXXXXXX XXXXXXXXXXXXX XXXXXXXXXXXXX			514,170	XXXXXXXXXXXXX XXXXXXXXXXXXX XXXXXXXXXXXXXXXXXX

OPERATOR