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AP-42 Section Number: 9.10.2.1

Reference Number: 11

Title: Emission Testing on Two Baghouses
at Harris Woolf California Almonds

Steiner Environmental, Inc.

Steiner Environmental, Inc.

October 1992

**EMISSION TESTING ON ONE BAGHOUSE
AT HARRIS WOOLF CALIFORNIA ALMONDS**

September 14, 1992

Prepared for:

**Harris Woolf California Almonds
Route 1, Box 470
Coalinga, California 93210**

October 1992

Prepared by:

**Steiner Environmental, Inc.
4930 Boylan Street
Bakersfield, California 93308**

Report PS-92-2909/Project 7242-92

SECTION 1

INTRODUCTION

At the request of Harris Woolf California Almonds, Steiner Environmental, Inc. conducted a series of emission tests on the effluent of a baghouse located at their almond processing plant located near Coalinga, California. These tests were conducted on September 14, 1992. The purpose of these tests was to determine compliance with Fresno County APCD Rules and Regulations.

Almonds are hauled to the plant by trucks and are bottom dumped into a pit with a conveyor. The emissions from this almond receiving/pre-cleaning facility (Permit to Operate No. 1140140101R) are controlled by a Saunco baghouse (Model No. RA12-252-5040) containing 252 polyester dacron bags each six inches in diameter and 144 inches long. The total surface area is 5040 ft² and the air-to-cloth ratio is 6.94 to 1.0 at an air flow of 35,000 acfm.

Almonds are hulled and shelled in another part of the plant and the emissions from these processes are also controlled by a baghouse (Permit to Operate No. 1140140102R). A Saunco baghouse (Model RA12-312-6240) with one compartment containing 312 polyester dacron bags each six inches in diameter and 144 inches long with a rated air flow of 77,500 acfm and an airleg recycle with a rated air flow of 23,000 acfm. The

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SECTION 1

INTRODUCTION

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total bag surface area is 6,240 ft² for an air-to-cloth ratio of 12.4 to 1.0.

Triplicate particulate tests were performed using EPA Method 5 on the outlet duct from the receiving/pre-cleaner baghouse prior to the fan. No PM₁₀ tests were conducted. Fresno County has agreed that if the baghouses passed the particulate tests, then they would also pass the PM₁₀ tests, since PM₁₀ is a fraction of the total particulate emitted from the baghouses.

Section 2 of the report presents the test matrix for this program.

SECTION 2
TEST PROGRAM

Table 2-1 presents the test matrix for this program. The baghouse was in continuous operation during the test program.

Section 3 of the report summarizes the test results.

TABLE 2-1. RECEIVING/PRE-CLEANING BAGHOUSE TEST MATRIX

<u>Date</u>	<u>Test No.</u>	<u>Test Parameter</u>	<u>Test Time</u>
9/14/92	1	Particulates	7:47 am - 9:55 am
	2	Particulates	10:30 am - 12:37 pm
	3	Particulates	1:12 pm - 3:19 pm

SECTION 3

TEST RESULTS

Table 3-1 summarizes the test results for the receiving/pre-cleaning baghouse.

3.1 RECEIVING/PRE-CLEANING BAGHOUSE

The permit limits particulate (and PM_{10}) emissions to 0.004 gr/scf, 1.20 lb/hr or 28.8 lb/day based on a 24-hour operating day. The measured emissions were 0.0032 gr/scf, 0.87 lb/hr or 20.88 lb/day. This baghouse was in compliance with the permit limits.

TABLE 3-1. SUMMARY OF SOURCE EMISSION TEST DATA (60 dF)

Unit Tested : HARRIS WOOLF
PRECLEANER BAGHOUSE

Date : SEPT 14, 1992

Test Number	1	2	3	Average
Test Condition				
Barometric Pressure (in. Hg)	29.46	29.52	29.48	29.49
Stack Pressure (in. Hg)	28.61	28.71	28.69	28.67
Stack Area (ft ²)	10.08	10.08	10.08	10.08
Elapsed Sampling Time (min.)	120.0	120.0	120.0	120.00
Volume Gas Sampled (dscf)	105.253	94.912	102.526	100.897
F-Factor				
MMBtu/Bbl				
GAS DATA				
Average Gas Velocity (fps)	54.78	53.41	55.93	54.70
Average Gas Temperature (dF)	77.13	91.38	97.46	88.66
Gas Flowrate (dscfm)	30,439	28,961	29,964	29,788
Gas Analysis (Volume %)				
Carbon Dioxide, dry	0.00	0.00	0.00	0.00
Oxygen, dry	20.90	20.90	20.90	20.90
Water	0.78	0.98	0.99	0.92
EMISSION CONCENTRATION				
Filterable Particulate (gr/dscf)	0.0040	0.0023	0.0032	0.0032
Total Particulate (gr/dscf)	0.0042	0.0025	0.0035	0.0034
EMISSION RATE - lb/hr				
Filterable Particulate	1.05	0.58	0.83	0.82
Total Particulate	1.09	0.63	0.90	0.87
EMISSION FACTOR - lb/day				
Filterable Particulate	25.20	13.92	19.92	19.68
Total Particulate	26.16	15.12	21.60	20.88

SECTION 4

SAMPLING EQUIPMENT AND PROCEDURES

This section of the report describes the equipment and procedures used to conduct the particulate tests on this program.

4.1 PRELIMINARY MEASUREMENTS

Before conducting the stack tests a series of preliminary measurements were made to determine:

- The location of the sampling site and the number and location of the sampling points to be used (EPA Method 1)
- The velocity, temperature and pressure of the gases in the stack (EPA Method 2)
- The composition of the stack gases (EPA Method 3)
- The moisture content of the stack gases (EPA Method 4)

Using the results of these preliminary measurements and the calibration constants for the sampling train, a series of calculations were made to determine the value of K, a constant, and N_d , ideal nozzle diameter, required to run an isokinetic test according to the equation:

$$\Delta H = \left[\frac{60^2 \pi^2 (K_p)^2 (C_p)^2 (1 - B_{wo})^2 P_s MW_d}{576^2 (K_o)^2 MW_s P_n} \right] (N_d)^4 \left(\frac{T_n}{T_s} \right) (\Delta P)$$

where

$$K = \left[\frac{60^2 \pi^2 (K_p)^2 (C_p)^2 (1 - B_{wo})^2 P_s MW_d}{576^2 (K_o)^2 MW_s P_s} \right]$$

An actual nozzle, whose diameter was as close as possible to the ideal nozzle diameter, was selected for the test. Isokinetic sampling rates for each sampling point in the stack were computed using the equation:

$$\Delta H = (K) (N_d)^4 \left(\frac{T_m}{T_s} \right) (\Delta P)$$

Since K and N_d were known, and remain constant during a test, the only variables were the meter temperatures, the stack gas temperature and the velocity pressure for each sampling point.

4.2 PREPARATION OF THE PARTICULATE SAMPLING TRAIN

All sampling train components were cleaned in the laboratory (soap and water, tap water rinse, distilled water rinse, and IPA rinse) to eliminate previous contamination. The sampling train components were sealed and transported to the sampling site in a mobile lab. The EPA Method 5 equipment used to measure particulates (filterable and total) consisted of:

- A calibrated 316 stainless steel nozzle for isokinetic sampling
- A heated Pyrex glass sampling probe (4 feet long) equipped with an S-type pitot tube and a thermocouple to measure stack velocity, pressure and temperature

- A heated Pyrex glass filter holder containing a weighed 100-mm Whatman 934 AH glass fiber filter
- A Pyrex glass impinger train in an icebath (impingers 1 and 2 contained 100-ml distilled water; bubbler 3 was dry; bubbler 4 contained a weighed amount of silica gel)
- An umbilical to connect the probe and sample box to the control module
- A control module containing a vacuum pump, a calibrated dry gas meter and a calibrated orifice meter to measure the pressure, temperature and flowrate throughout the train.

The sampling train was charged in the mobile lab using freshly prepared reagents. Each impinger and its contents was weighed to the nearest 0.1 gm on a calibrated electronic balance. Blanks of all filters and reagents were retained for subsequent analysis. The sampling point locations were marked on the probe using a high-temperature marker. The sampling train was completely assembled and lifted to the sampling site.

4.3 SAMPLING PROCEDURES FOR PARTICULATE SAMPLING TRAIN

Prior to a test, the sampling train was heated and leak-checked at 15-inches Mercury to insure leakage was less than 0.02 cfm or 4% of the average sampling rate. The S-type pitot tube was also leak-checked. The sampling train was installed on the untrail and the probe was inserted into the stack at the farthest point. An isokinetic sampling rate was calculated using an HP-41CV calculator for each sampling point on the traverse (12 points per traverse, 2 traverses at 90°). Each point was sampled for an equal period of time (5.0 minutes) and all pertinent data were recorded on the data sheet for each point. The probe and sample box

were maintained at 250°F throughout the traverse. The gases leaving the impinger train were maintained at <68°F. At the end of a traverse, the probe was withdrawn from the stack and the entire sampling train was transferred intact to the next sampling port. The other traverse of the stack was completed and the sampling train was withdrawn for the final leak-check. This leak-check was performed at 15-inches Mercury or at the highest vacuum achieved during the test. The S-type pitot tube was also checked at this time. The probe, nozzle, filter holder and impinger train were sealed with aluminum foil and lowered to the mobile lab for sample recovery.

4.4 SAMPLE RECOVERY PROCEDURES FOR PARTICULATE SAMPLING TRAIN

Sample recovery for the nozzle and probe occurred on the stack. The nozzle and probe were brushed and rinsed three times using ACS reagent grade acetone into a polyethylene sample bottle. Sample recovery for the filter holder and impinger train occurred in the mobile lab. The 100-mm filter was removed from the 4-inch filter holder and sealed in its petri dish. The front half of the 4-inch glass filter holder was brushed and rinsed with acetone. Each impinger was removed from the icebath, wiped dry and weighed to the nearest 0.1 gm. The contents of impinger 1 were transferred to a polyethylene sample bottle. The back half of the 4-inch glass filter holder, the glass connectors, impingers 1, 2 and 3 were rinsed with distilled water and the rinsings were transferred to this same bottle. All sample bottles and petri dishes were marked and labeled. A chain-of-custody log was completed and the field data sheet was also labeled with the sample ID numbers. The sampling train was then recharged in preparation for the next test.

SECTION 5

ANALYTICAL PROCEDURES

This section of the report describes the procedures used to analyze the samples collected during the test program. All analyses were performed in the Steiner Environmental, Inc. climate-controlled laboratory located in Bakersfield, California.

5.1 ANALYSIS OF PARTICULATE SAMPLES

5.1.1 Nozzle. Probe. Filter Holder Wash

The volume of the acetone washings was measured and the washings were transferred to clean, tared, aluminum weighing dishes. The dishes were placed on temperature-controlled water bath under a fume hood and gently heated to dryness (100°F). The dishes with the dry residue were desiccated and weighed repeatedly at 6-hour intervals until a constant weight was achieved (to the nearest 0.01 mg with a tolerance of <0.1 mg between weighings). The ACS reagent grade acetone blank was treated in the same manner.

5.1.2 Filter

The 100-mm filter was removed from its petri dish and transferred to an oven where it was heated for 2 hours at 105°C. The filter was then desiccated and weighed repeatedly at 6-hour intervals until a constant weight was achieved (to nearest 0.01 mg with a tolerance of <0.1 mg

between weighings). An unused, tared blank filter was treated in the same manner.

5.1.3 Condensible Particulate

The volume of sample was measured and the entire volume was transferred to a clean, tared glass evaporating dish. The dish was placed on a temperature-controlled hot plate under a fume hood and gently heated to dryness (150°F). The dish with the dry residue was desiccated and weighed repeatedly at 6-hour intervals until a constant weight was achieved (to nearest 0.01 mg with a tolerance of <0.1 mg between weighings). A blank of the distilled water was treated in the same manner.

SECTION 6

QUALITY ASSURANCE

This section of the report describes the QA/QC procedures employed on the test program.

6.1 PARTICULATE SAMPLING EQUIPMENT

A detailed record of repair and maintenance to each sampling train is kept. Preventative maintenance to each system is performed periodically to avoid complete component breakdown during a field test.

A detailed record of sampling system calibrations is also kept. Calibration data for the sampling nozzles, pitot tubes, dry gas meters and orifice meters are available for review. Results of the EPA Quality Assurance Branch bi-annual audits of the dry gas meter and orifice meter combinations are also logged and verify our in-house calibration data. The calibration data for the equipment used on this program can be found in the Appendix of this report.

6.2 LAB ANALYSIS

All field samples are assigned a label and an ID number. This ID is also affixed to a chain-of-custody log and to the field data sheet to eliminate any chance of sample mixup.

Prior to analysis, all glassware is thoroughly cleaned (soap and water, tap water rinse, distilled water rinse, IPA rinse) to eliminate

***** STEPS error listing 04/14/94 15:40:35 *****

Please report to Pacific Environmental Services, Inc.
PO Box 12077
Research Triangle Park, NC 27709

(919) 941-0333

FAX (919) 941-0234

Error number: 12

Error message: Variable 'NRE_EST_EM' not found.

Line number of error: 346

Program where error occurred: _QP40W1PHK

Number of FILES specified in CONFIG.SYS = 109

Remaining free space on disk drive = 13272 Kilobytes

Available conventional memory = 125760 bytes

Total memory available to FoxPro = 285920 bytes

Memory used by variables, files, etc. = 96320 bytes

***** Program trace-back information *****

C:\MODIFY\STEPS.APP

ON...

FILE_POP.FXP

ON...

FRTS.FXP

ON...

FRTS_RPT.SPX

PROCEDURE _QP40W1PHK FRTS_RPT.SPX

ON...

ERR_TRAP.FXP

***** System memory contents *****

MBELL	Pub	C	" "
MSTR_KEY	Pub	C	" "
MMSTR_DBF	Pub	C	" "
MSG	Pub	L	.F.
MMODE	Pub	C	" "
MAP_YN	Pub	C	"Y"
SUPER_OK	Pub	L	.F.
CE_EDIT_OK	Pub	L	.F.
E_EDIT_OK	Pub	L	.F.
C_EDIT_OK	Pub	L	.F.
VIEW_OK	Pub	L	.F.
MONITOR	Pub	C	"color"
VERSION	Pub	C	"Version 2.1b"
PASSINIT	Pub	C	"DWH"
UPDTINIT	Pub	C	" "
SUPEROK	Pub	L	.T.
CE_EDITOK	Pub	L	.T.
E_EDITOK	Pub	L	.T.
C_EDITOK	Pub	L	.T.
VIEWOK	Pub	L	.T.
NORMAL	Pub	C	"w+/b"

GET	Pub	C	"gr+/r"			
SAY	Pub	C	"n/gr"			
HIGH	Pub	C	"g/b"			
ERROR	Pub	C	"w+*/b"			
HNORMAL	Pub	C	"n/gr"			
HHIGH	Pub	C	"w+/b"			
HBDR	Pub	C	"gr+/gr"			
WNORMAL	Pub	C	"w/gr"			
WHIGH	Pub	C	"w/gr"			
F1	Pub	C	"w/gr"			
F2	Pub	C	"w/gr"			
F3	Pub	C	"gr+/gr"			
F4	Pub	C	"b/w"			
F5	Pub	C	"r/gr"			
COLOR	Pub	L	.F.			
PASSWORD	Pub	C	"SECRET"			
MSCRN	Pub	L	.F.			
MMENU	Pub	L	.F.			
IDX_LEN	Pub	N		0	(	0.00000000)
MMSTR_KEY	Pub	C	" "			
MICONPG	Pub	L	.F.			
OLDICON	Pub	C	" "			
SATELLITE	Priv	L	.F.			STEPS
HQ_SAT	Priv	L	.F.			STEPS
PROJ_VER	Priv	C	"DE"			STEPS
DATFILE	Priv	C	"datapath.dat"			STEPS
DAT_HANDLE	Priv	N		7	(	7.00000000)
DATAPATH	Priv	C	"c:\modify\satdata"			STEPS
OLD_RSRC	Priv	C	"FOXUSER"			STEPS
BATCH_EDIT	Priv	L	.F.			STEPS
STARTIME	Priv	C	"15:37:46"			STEPS
STARTDATE	Priv	D	04/14/94			STEPS
ICONDIS	Priv	L	.F.			STEPS
MENU_LP	Priv	L	.T.			STEPS
TALKSTAT	Priv	C	"OFF"			FRTS_RPT
COMPSTAT	Priv	C	"OFF"			FRTS_RPT
RPTTORUN	Priv	C	"voc_rpt"			FRTS_RPT
DEVICE	Priv	C	"Screen"			FRTS_RPT
RPT_SEL	Priv	N		3	(	3.00000000)
OUT_SEL	Priv	N		1	(	1.00000000)
OK_SEL	Priv	N		1	(	1.00000000)
TMP_QUERY1	Priv	C	"65747141.DBF"			_QP40W1PHK
TEMPFILE	Priv	C	"65752414.txt"			_QP40W1PHK
ERR_NUM	Priv	N		12	(	12.00000000)
ERR_MESS	Priv	C	"Variable 'NRE_EST_EM' not found."			ERR_TRAP
ERR_MESS1	Priv	C	"Variable 'NRE_EST_EM' not found."			ERR_TRAP
ERR_LINENU	Priv	N		346	(	346.00000000)
ERR_PROGNA	Priv	C	"_QP40W1PHK"			ERR_TRAP
I	Priv	N		11	(	11.00000000)

70 variables defined, 545 bytes used
186 variables available

Print System Memory Variables

_ALIGNMENT	Pub	C	"LEFT"			
_BOX	Pub	L	.T.			
_CALCMEM	Pub	N		0.00	(	0.00000000)
_CALCVALUE	Pub	N		0.00	(	0.00000000)
_CUROBJ	Pub	N		-1	(	-1.00000000)
_DBLCLICK	Pub	N		0.49	(	0.49432944)

_DIARYDATE	Pub	D	04/14/94		
_FOXDOC	Pub	C	" "		
_FOXGRAPH	Pub	C	" "		
_GENGRAPH	Pub	C	" "		
_GENMENU	Pub	C	" "		
_GENPD	Pub	C	"stepspd.app"		
_GENSCRN	Pub	C	" "		
_GENXTAB	Pub	C	" "		
_INDENT	Pub	N	0	(	0.00000000)
_LMARGIN	Pub	N	0	(	0.00000000)
_MLINE	Pub	N	0	(	0.00000000)
_PADVANCE	Pub	C	"FORMFEED"		
_PAGENO	Pub	N	3	(	3.00000000)
_PBPAGE	Pub	N	1	(	1.00000000)
_PCOLNO	Pub	N	55	(	55.00000000)
_PCOPIES	Pub	N	1	(	1.00000000)
_PDRIVER	Pub	C	" "		
_PDSETUP	Pub	C	" "		
_PECODE	Pub	C	" "		
_PEJECT	Pub	C	"BEFORE"		
_PEPAGE	Pub	N	32767	(	32767.00000000)
_PLENGTH	Pub	N	66	(	66.00000000)
_PLINENO	Pub	N	31	(	31.00000000)
_PLOFFSET	Pub	N	0	(	0.00000000)
_PPITCH	Pub	C	"DEFAULT"		
_PQUALITY	Pub	L	.F.		
_PRETEXT	Pub	C	" "		
_PSCODE	Pub	C	" "		
_PSPACING	Pub	N	1	(	1.00000000)
_PWAIT	Pub	L	.F.		
_RMARGIN	Pub	N	80	(	80.00000000)
_STARTUP	Pub	C	" "		
_TABS	Pub	C	" "		
_TALLY	Pub	N	249	(	249.00000000)
_TEXT	Pub	N	-1	(	-1.00000000)
_THROTTLE	Pub	N	0.00	(	0.00000000)
_WRAP	Pub	L	.F.		

45 System Variables Defined

Menu and Pad Definitions

Menu name

STEPS 227 bytes

Pad name

MAP	60 bytes
REPT	60 bytes
FILE	60 bytes
UTIL	60 bytes
QUIT	60 bytes
FILL	60 bytes

1 Menu Defined

Popup Definitions

FRTS_POP	527 bytes
UTIL_POP	1067 bytes
LKUP_POP	287 bytes
FILE_POP	767 bytes

REPORT_POP 527 bytes
MAP_AIR 407 bytes
MAP_1 467 bytes

7 Popups Defined

Window Definitions

Name	From	To	Size	
HELP	1,46	10,76	468 bytes	
CALC	1,44	21,76	1188 bytes	
CALCHELP	1,44	21,76	1188 bytes	
ICON_WIN	0,0	50,79	8164 bytes	
_QP40W10P4	3,9	20,69	1892 bytes	
_ERROR	8,10	16,69	820 bytes	
ERR_WIND	0,0	24,79	3588 bytes	ACTIVE

7 Windows Defined

***** System status *****

Processor is INTEL 80486

Select area: 1, Database in Use: C:\MODIFY\SATDATA\SYS.DBF Alias: SYS
Lock(s): Exclusive USE

Select area: 2, Database in Use: C:\MODIFY\SATDATA\PLANT.DBF Alias: PLANT
Structural CDX file: C:\MODIFY\SATDATA\PLANT.CDX
Index tag: PLANT_NAME Key: NAME
Index tag: PLANT_ID Key: STATE_CODE+CNTY_CODE+PLANT_ID
Index tag: CITY_NAME Key: STATE_CODE+CITY_NAME
Memo file: C:\MODIFY\SATDATA\PLANT.FPT
Lock(s): Exclusive USE

Select area: 3, Database in Use: C:\MODIFY\GEO.DBF Alias: GEO
Structural CDX file: C:\MODIFY\GEO.CDX
Index tag: FIPSTATE Key: FIPS_STATE
Index tag: FIPSCNTY Key: FIPS_STATE+FIPS_CNTY
Index tag: COUNTY Key: STATE+COUNTY
Index tag: STATE Key: STATE Unique
Index tag: NCCNTY Key: FIPS_STATE+FIPS_CNTY For: FIPS_STATE="37
Index tag: ABBREV2 Key: ABBREV2+STATE Unique
Lock(s): Exclusive USE

Select area: 4, Database in Use: C:\MODIFY\SATDATA\PLNTPOLL.DBF Alias: PLNTP
Structural CDX file: C:\MODIFY\SATDATA\PLNTPOLL.CDX
Index tag: POLLUTANT Key: STATE_CODE+CNTY_CODE+PLANT_ID+POLLUTANT
Index tag: PLANT Key: STATE_CODE+CNTY_CODE+PLANT_ID Unique For:
Memo file: C:\MODIFY\SATDATA\PLNTPOLL.FPT
Lock(s): Exclusive USE

Currently Selected Database:

Select area: 5, Database in Use: C:\MODIFY\65747141.DBF Alias: TMP_QUERY1
Lock(s): Exclusive USE

File search path: C:\MODIFY\SATDATA
Default disk drive: C:
Print file/device: PRN:
Work area = 5

Margin = 0
Decimals = 2
Memowidth = 50
Typeahead = 20
Blocksize = 64
Reprocess = Automatic
Refresh = 0 SECONDS
No EMS

Date format: American
Macro Hot Key = SHIFT+F10
UDF parameters are passed by: VALUE

ON KEY LABEL hot keys:

F1 null = .t.
F2 null = .t.
F3 null = .t.
F4 null = .t.
F5 null = .t.
F6 null = .t.
F7 null = .t.
F8 null = .t.
F9 null = .t.
F10 null = .t.
F11 null = .t.
F12 null = .t.
CTRL+N null = .t.
CTRL+P null = .t.
CTRL+B null = .t.
CTRL+T null = .t.
CTRL+END null = .t.

Textmerge Options

Delimiters: Left = << Right = >>
Show

Alternate	- off	Console	- off	Fixed	- off	Safety	- off
ANSI	- off	Cursor	- on	Heading	- off	Space	- on
Bell	- off	Debug	- on	Help	- on	Status	- off
Blink	- on	Deleted	- on	Intensity	- on	Sticky	- on
Brstatus	- off	Device	- scrn	Lock	- off	Sysmenus	- on
Carry	- off	Echo	- off	Logerrors	- on	Talk	- off
Century	- off	EMS	- on	Mouse	- on	Textmerge	- off
Clear	- on	Escape	- off	Multilocks	- off	Title	- off
Color	- on	Exact	- off	Near	- off	Unique	- off
Compatible	- off	Exclusive	- off	Optimize	- on		
Confirm	- on	Fields	- off	Print	- on		

Modules loaded: CURSON CURSOFF

***** End of error listing *****

any contamination. The evaporating dishes used to evaporate the washings are treated the same as a sample (dried in an oven, desiccated and weighed repeatedly at 6-hour intervals until a constant weight is achieved). The glassware used to measure volumes and make transfers and dilutions are all NBS Class A to insure accurate measurements. All weighings are carried out on a Sartorius Research Model R160P electronic semi-micro balance supported by a marble table in a separate room from the main analytical laboratory. The balance is calibrated regularly against an NBS Class S-1 weight.

All reagents used in the field and in the laboratory are ACS reagent grade and blanks of these reagents are evaluated for every set of tests. Blanks are taken in the field from the squeeze bottles and not the original container. Records are kept on these blanks to insure consistent quality of the reagents.

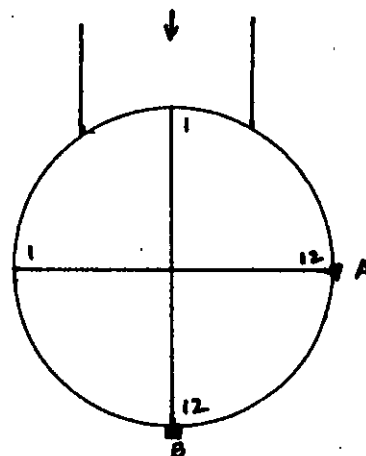
APPENDIX A
STEINER ENVIRONMENTAL RAW DATA

Steiner Environmental, Inc.

SAMPLING POINT LOCATION DATA SHEET



Plant Harris Woolf
 Date 9/14/92
 Test Location Precleaning Baghouse
 Upstream Dist./Dia. 41" / 1.0 ft
 Downstream Dist./Dia. 328" / 2.6 ft
 No. of Sampling Points 24
 Stack Dimension 43
 Coupling Length 3.75



2, 3 -inch MPT/FPT/Flange

*has hooks
 plant supplies ladder
 50' power
 no rope*

*flow goes down
 high - 20 pressure; go in but running
 bring stack tube man*

XEQ PNT

earplugs

Sample Point	Dist	Sample Point	Dist	Sample Point	Dist	Sample Point	Dist
1	4.7						
2	6.6						
3	8.8						
4	11.4						
5	14.5						
6	19.0						
7	31.5						
8	36.0						
9	39.1						
10	41.7						
11	43.9						
12	45.8						

SAMPLING POINT RELOCATION: #1 → 4.75 #2 → 45.75

PLANT Harris Woolf

Run No. /

[illegible]

TEST TYPE MS FIELD TEST DATA SHEET (Page 1 of 2)

TEST TYPE HS FIELD TEST DATA SHEET (Page 1 of 2)

[IMPINGER	VOLUMES/WEIGHTS	]	[	GAS COMPOSITION
1	100/0			100% CO ₂
2	100/0			100% CO ₂
3	100/0			100% CO ₂
4	100/0			100% CO ₂
5	100/0			100% CO ₂
6	100/0			100% CO ₂
7	100/0			100% CO ₂
8	100/0			100% CO ₂
9	100/0			100% CO ₂
10	100/0			100% CO ₂
11	100/0			100% CO ₂
12	100/0			100% CO ₂
13	100/0			100% CO ₂
14	100/0			100% CO ₂
15	100/0			100% CO ₂
16	100/0			100% CO ₂
17	100/0			100% CO ₂
18	100/0			100% CO ₂
19	100/0			100% CO ₂
20	100/0			100% CO ₂
21	100/0			100% CO ₂
22	100/0			100% CO ₂
23	100/0			100% CO ₂
24	100/0			100% CO ₂
25	100/0			100% CO ₂
26	100/0			100% CO ₂
27	100/0			100% CO ₂
28	100/0			100% CO ₂
29	100/0			100% CO ₂
30	100/0			100% CO ₂
31	100/0			100% CO ₂
32	100/0			100% CO ₂
33	100/0			100% CO ₂
34	100/0			100% CO ₂
35	100/0			100% CO ₂
36	100/0			100% CO ₂
37	100/0			100% CO ₂
38	100/0			100% CO ₂
39	100/0			100% CO ₂
40	100/0			100% CO ₂
41	100/0			100% CO ₂
42	100/0			100% CO ₂
43	100/0			100% CO ₂
44	100/0			100% CO ₂
45	100/0			100% CO ₂
46	100/0			100% CO ₂
47	100/0			100% CO ₂
48	100/0			100% CO ₂
49	100/0			100% CO ₂
50	100/0			100% CO ₂
51	100/0			100% CO ₂
52	100/0			100% CO ₂
53	100/0			100% CO ₂
54	100/0			100% CO ₂
55	100/0			100% CO ₂
56	100/0			100% CO ₂
57	100/0			100% CO ₂
58	100/0			100% CO ₂
59	100/0			100% CO ₂
60	100/0			100% CO ₂
61	100/0			100% CO ₂
62	100/0			100% CO ₂
63	100/0			100% CO ₂
64	100/0			100% CO ₂
65	100/0			100% CO ₂
66	100/0			100% CO ₂
67	100/0			100% CO ₂
68	100/0			100% CO ₂
69	100/0			100% CO ₂
70	100/0			100% CO ₂
71	100/0			100% CO ₂
72	100/0			100% CO ₂
73	100/0			100% CO ₂
74	100/0			100% CO ₂
75	100/0			100% CO ₂
76	100/0			100% CO ₂
77				

3.1. GAS COMPOSITION

IMPINGER VOLUMES/WEIGHTS

I

Filter No. 902 Nozzle No./Size 1450 / .2943

		TOTAL	20.2	Final	0.007	6.5
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TEMPERATURE . . .

Year	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	2100
1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	2100	

Steiner Environmental, Inc.

PLANT Harris Woolf TEST TYPE MS FIELD TEST DATA SHEET (Page 2 of 2)
 DATE 9/14/92 RUN NO. 3
 TEST LOCATION Becleaner OPERATOR gt

Sample Point	Time	AP in wg	AH in wg	Gas Meter Volume Fc ³	TEMPERATURE °F							Pump Vacuum in. Hg	ΔP	Comments
					Stack	Probe	Oven	Imp.	Gas Meter					
									In	Out				
B 1	0	0.82	2.33	351.081	100	243	243	90	111	109	3.0	0.906		
2		0.92	2.61	355.525	99	249	254	75	109	107	3.0	0.959		
3	10	0.92	2.61	360.174	98	255	255	70	108	107	3.0	0.959		
4		0.94	2.67	364.940	98	252	260	66	108	105	3.0	0.920		
5	20	0.94	2.67	369.600	98	252	249	66	108	105	3.0	0.970		
6		0.92	2.61	374.393	98	256	253	66	108	105	3.0	0.959		
7	30	0.91	2.57	379.110	99	255	256	67	107	104	3.0	0.954		
8		0.91	2.57	383.774	99	251	257	67	108	104	3.0	0.954		
9	40	0.92	2.60	388.530	99	255	254	67	108	104	3.0	0.959		
10		0.89	2.51	393.137	99	250	251	67	108	103	3.0	0.943		
11	50	0.87	2.46	397.715	99	255	244	67	107	103	3.0	0.933		
12		0.83	2.34	402.265	99	253	252	68	107	103	3.0	0.911	pitotok	
	60			406.689										
													31963	
													31964	
													31965	
	120		2.57	112.399	97.46					ND-23		0.919		

Steiner Environmental, Inc.

Date: 9/15/92

Test Location: Precleaner Baghouse

SAMPLE HANDLING/LOG-IN

NO	SAMPLE TYPE	VOLUME	COMMENTS
1	31954 <u>5</u> <u>FWW</u> <u>1</u> Meth Sample Test		
2	31955 <u>5</u> <u>MF</u> <u>1</u> Meth Sample Test		
3	31956 <u>5</u> <u>BNW</u> <u>1</u> Meth Sample Test		
4	31957 <u>5</u> <u>FWW</u> <u>2</u> Meth Sample Test		
5	31958 <u>5</u> <u>MF</u> <u>2</u> Meth Sample Test		
6	31959 <u>5</u> <u>BNW</u> <u>2</u> Meth Sample Test		
7	31960 <u>5</u> <u>FWW</u> <u>3</u> Meth Sample Test		
8	31961 <u>5</u> <u>MF</u> <u>3</u> Meth Sample Test		
9	31962 <u>5</u> <u>BNW</u> <u>3</u> Meth Sample Test		
10	31963 <u>5</u> <u>FWW</u> <u>BL</u> Meth Sample Test		
11	31964 <u>5</u> <u>MF</u> <u>BL</u> Meth Sample Test		
12	31965 <u>5</u> <u>BNW</u> <u>BL</u> Meth Sample Test		

CHAIN-OF-CUSTODY

Signature

Date/Time

Signature

Date/Time

Jim Steiner

9/15/92 0:50am

Wayne A. Brown

9/15/92 0930

ANALYTICAL REPORT

SAMPLE TYPE : FHW ANALYSIS (g) TEST DATE : 09/14/92
 SAMPLING METHOD : M5 ANALYSIS DATE : 09/17/92
 SAMPLE COMPONENT : ACETONE ANALYST : MC, WB
 REQUESTED BY : HARRIS WOOLF
 ANALYTICAL METHOD : GRAVIMETRIC

Sample ID #	Test No.	Sample Volume (ml)	Analytical Result (total sample)	
			Uncorrected	Blank Corr. (g)
31954	1	170	0.02621	0.02592
31957	2	150	0.01125	0.01099
31960	3	180	0.02051	0.02020
31963	Bk	100	0.00017	

ANALYTICAL REPORT

SAMPLE TYPE : FILTERABLE PARTICULATE TEST DATE :09/14/92
 SAMPLING METHOD : M5 ANALYSIS DATE :09/17/92
 SAMPLE COMPONENT : 100 mm FILTER ANALYST :MC, WB
 REQUESTED BY : HARRIS WOOLF
 ANALYTICAL METHOD : GRAVIMETRIC

Sample ID #	Test No.	Filter No.	Analytical Result (total sample)	
			Uncorrected	Blank Corr. (g)
31955	1	982	0.00165	0.00164
31958	2	981	0.00344	0.00343
31961	3	983	0.00135	0.00134
31964	Bk	984	0.00001	

ANALYTICAL REPORT

SAMPLE TYPE : CONDENSIBLE PARTICULATE TEST DATE :09/14/92
 SAMPLING METHOD : M5 ANALYSIS DATE:09/17/92
 SAMPLE COMPONENT : DIH2O ANALYST :MC, WB
 REQUESTED BY : HARRIS WOOLF
 ANALYTICAL METHOD : GRAVIMETRIC

Sample ID #	Test No.	Sample Volume	Analytical Result (total sample) grams	
			Uncorrected	Blank Corrected
31956	1	390	0.00183	0.00089
31959	2	370	0.00205	0.00116
31962	3	370	0.00275	0.00186
31965	Bk	100	0.00024	

SOURCE TEST CALCULATIONS

PLANT : HARRIS WOOLF
PRECLEANER BAGHOUSE

RUN NO.: 1
DATE : SEPT 14, 1992

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	71.88 DEG. F		STATIC PRESS.	=	-11.60 in. H2O
STACK TEMP.	=	77.13 DEG. F		Cp	=	0.840
SQ. RT. dP	=	0.9439 in. H2O		STACK I.D.	=	43.00 inch
METER ORIFICE	=	2.47 in. H2O		DUCT LENGTH	=	inch
METER VOLUME	=	107.614 Cu.Ft.		DUCT WIDTH	=	inch
METER Y	=	1.0098		STACK AREA	=	10.085 Sq.Ft.
BAR. PRESSURE	=	29.46 in.Hg		TEST TIME	=	120.00 min.
COND. (Vlc)	=	17.9 ml		NOZZLE DIA.	=	0.2343 inch

GAS ANALYSIS	=	20.90 % O2		0.00 % CO
		0.00 % CO2		79.10 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times (Pb + (dH / 13.6)) / (Tm + 460) \dots\dots = 105.253 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vlc = 0.830 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots\dots\dots = 0.008$ | Lower
| Bws
Bws @ Saturated Conditions = Vapor Press. of H2O | value
@ Dew Point Temp. / (Ps, in.Hg.) | used.

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)] = 28.84$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots\dots\dots = 28.75$

$P(stack) = Pbar + [Pstatic / 13.6] \dots\dots\dots = 28.61 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots\dots\dots = 54.78 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots\dots\dots = 33,144 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots\dots\dots = 30,439 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 97.05 \%$

SOURCE TEST CALCULATIONS

PLANT : HARRIS WOOLF
PRECLEANER BAGHOUSE

RUN NO.: 2
DATE : SEPT 14, 1992

STANDARD TEMP.: 60 DEG. F

METER TEMP.	=	109.9 DEG. F	STATIC PRESS.	=	-11.00 in. H2O
STACK TEMP.	=	91.38 DEG. F	Cp	=	0.840
SQ. RT. dP	=	0.9097 in. H2O	STACK I.D.	=	43.00 inch
METER ORIFICE	=	2.39 in. H2O	DUCT LENGTH	=	inch
METER VOLUME	=	103.788 Cu.Ft.	DUCT WIDTH	=	inch
METER Y	=	1.0098	STACK AREA	=	10.085 Sq.Ft.
BAR. PRESSURE	=	29.52 in. Hg	TEST TIME	=	120.00 min.
COND. (Vlc)	=	20.2 ml	NOZZLE DIA.	=	0.2343 inch

GAS ANALYSIS	:	20.90 % O2	0.00 % CO
		0.00 % CO2	79.10 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times (Pb + (dH / 13.6)) / (Tm + 460) \dots = 94.912 \text{ dscf}$

$Vw(std) = (8.9148 \times 10e-5) \times (Tstd + 460) \times Vlc = 0.936 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots = 0.010 \text{ | Lower}$

Bws @ Saturated Conditions = Vapor Press. of H2O
@ Dew Point Temp. / (Ps, in. Hg.) $\dots = 0.051 \text{ | value used.}$

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)] = 28.84$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots = 28.73$

$P(stack) = Pbar + [Pstatic / 13.6] \dots = 28.71 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq. Rt. dP) \times [Sq. Rt. (Ts + 460) / (Ms \times Ps)] \dots = 53.41 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots = 32,318 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots = 28,961 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 91.98 \%$

SOURCE TEST CALCULATIONS

PLANT : HARRIS WOOLF
PRECLEANER BAGHOUSE

RUN NO.: 3
DATE : SEPT. 14, 1992

STANDARD TEMP.: 60 DEG. F

METER TEMP.	= 110.83 DEG. F	STATIC PRESS.	= -10.80 in. H2O
STACK TEMP.	= 97.46 DEG. F	Cp	= 0.840
SQ. RT. dP	= 0.9469 in. H2O	STACK I.D.	= 43.00 inch
METER ORIFICE	= 2.57 in. H2O	DUCT LENGTH	= inch
METER VOLUME	= 112.399 Cu.Ft.	DUCT WIDTH	= inch
METER Y	= 1.0098	STACK AREA	= 10.085 Sq.Ft.
BAR. PRESSURE	= 29.48 in.Hg	TEST TIME	= 120.00 min.
COND. (Vlc)	= 22.1 ml	NOZZLE DIA.	= 0.2343 inch

GAS ANALYSIS	:	20.90 % O2	0.00 % CO
		0.00 % CO2	79.10 % N2

$Vm(std) = [T(std) + 460 / 29.92] \times Vm \times Y \times (Pb + (dH / 13.6)) / (Tm + 460) \dots = 102.526 \text{ dscf}$

$Vw(std) = (8.9148 \times 10^{-5}) \times (Tstd + 460) \times Vlc = 1.024 \text{ scf}$

$Bws = Vw(std) / (Vm(std) + Vw(std)) \dots = 0.010$ | Lower Bws

Bws @ Saturated Conditions = Vapor Press. of H2O | value
@ Dew Point Temp. / (Ps, in.Hg.) | used.

$\%EA = (\%O2 - 0.5\%CO) / (0.264\%N2 - (\%O2 - 0.5\%CO)) \times 100 = \text{*****}$

$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)] = 28.84$

$Ms = (Md \times (1 - Bws)) + (18.0 \times Bws) \dots = 28.73$

$P(stack) = Pbar + [Pstatic / 13.6] \dots = 28.69 \text{ in. Hg}$

$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts + 460) / (Ms \times Ps)] \dots = 55.93 \text{ ft/sec}$

$Qs = vs \times As \times 60 \dots = 33,840 \text{ acf/min}$

$Qs(std) = Qs \times (1 - Bws) \times ((Tstd + 460) / (Ts + 460)) \times (Ps / 29.92) \dots = 29,964 \text{ dscf/min}$

$I = (Ts + 460) \times [(0.002669 \times Vlc) + (Vm(std) / (Tstd + 460) / 29.92)] \times 100 / (Time \times Ps \times An \times vs \times 60) = 96.04 \%$

EMISSION RATE CALCULATIONS

PLANT : HARRIS WOOLF
PRECLEANER BAGHOUSE

RUN NO.: 1
DATE : SEPT 14, 1992
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.02592 grams | Vm(std) 105.253 ft3
Mass Filter (MF)           0.00164 grams | Vw(std)  0.830 ft3
Back Half Wash (BHW)       0.00089 grams | Qs(std) 30,439 dscfm
Front Half Sulfate (FHS)    mg H2SO4 | Bws      0.008
Back Half Sulfate (BHS)     mg H2SO4 | CO2       0.00 %
H2O2 Catch (SO2)           mg H2SO4 | O2        20.90 %
*****
```

F-FACTOR

$10E6 \times [3.64(\%H) + 1.53(\%C) + 0.57(\%S) + 0.14(\%N) - 0.46(\%O_2)] / (Btu/lb) \times [(Tstd + 460)/528]$ dscf/MMBtu

FILTERABLE PARTICULATE

$15.432 \times (FHW + MF) / [Vm(std) + Vw(std)]$ 0.0040 gr/scf
 $15.432 \times (FHW + MF) / Vm(std)$ 0.0040 gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 1.05 lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL PARTICULATE

$15.432 \times (FHW + MF + BHW) / [(Vm(std) + Vw(std))]$... 0.0041 gr/scf
 $15.432 \times (FHW + MF + BHW) / Vm(std)$ 0.0042 gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 1.09 lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL SULFATE

$0.015432 \times (FHS + BHS) / [Vm(std) + Vw(std)]$ gr/scf
 $0.015432 \times (FHS + BHS) / Vm(std)$ gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ lb/hr
 $F-Fac \times 1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

SULFUR DIOXIDE (SO2)

$1.60982 \times [T(std) + 460] \times (mg H_2SO_4) / [98.076 \times Vm(std)]$ ppm
 ppm x [(20.9 - Oxygen Corr.) / (20.9 - %O2)] @ O2 corr.
 ppm x (1 - Bws) ppm (wet)
 $8.223E-5 \times Qs(std) \times 64.062 \times ppm / [T(std) + 460]$.. lb/hr
 $F-Factor \times 64.062 \times [1.3711E-6 / [T(std) + 460]] \times [20.9 / (20.9 - \%O_2)] \times ppm$ lb/MMBtu
 lb/hr / (dscfm x 60 min/hr) lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 lb/MMBtu
 (lb/MMBtu Total Sulfate) x (32 / 98.076) lb/MMBtu
 Total Sulfur lb/MMBtu

EMISSION RATE CALCULATIONS

PLANT : HARRIS WOOLF
PRECLEANER BAGHOUSE

RUN NO.: 2
DATE : SEPT 14, 1992
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.01099 grams | Vm(std)  94.912 ft3
Mass Filter (MF)           0.00343 grams | Vw(std)   0.936 ft3
Back Half Wash (BHW)       0.00116 grams | Qs(std) 28,961 dscfm
Front Half Sulfate (FHS)    mg H2SO4 | Bws      0.010
Back Half Sulfate (BHS)    mg H2SO4 | CO2       0.00 %
H2O2 Catch (SO2)          mg H2SO4 | O2        20.90 %
*****
```

F-FACTOR

$10E6 \times [3.64(\%H) + 1.53(\%C) + 0.57(\%S) + 0.14(\%N) - 0.46(\%O_2)] / (Btu/lb) \times [(T_{std} + 460)/528]$ dscf/MMBtu

FILTERABLE PARTICULATE

$15.432 \times (FHW + MF) / [Vm(std) + Vw(std)]$ 0.0023 gr/scf
 $15.432 \times (FHW + MF) / Vm(std)$ 0.0023 gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 0.58 lb/hr
 F-Fac x $1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL PARTICULATE

$15.432 \times (FHW + MF + BHW) / [(Vm(std) + Vw(std))]$... 0.0025 gr/scf
 $15.432 \times (FHW + MF + BHW) / Vm(std)$ 0.0025 gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 0.63 lb/hr
 F-Fac x $1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL SULFATE

$0.015432 \times (FHS + BHS) / [Vm(std) + Vw(std)]$ gr/scf
 $0.015432 \times (FHS + BHS) / Vm(std)$ gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ lb/hr
 F-Fac x $1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

SULFUR DIOXIDE (SO2)

$1.60982 \times [T(std) + 460] \times (mg H_2SO_4) / [98.076 \times Vm(std)]$ ppm
 ppm x $[(20.9 - \text{Oxygen Corr.}) / (20.9 - \%O_2)]$ @ O2 corr.
 ppm x (1 - Bws) ppm (wet)
 $8.223E-5 \times Qs(std) \times 64.062 \times ppm / [T(std) + 460]$.. lb/hr
 F-Factor x $64.062 \times [1.3711E-6 / [T(std) + 460]] \times [20.9 / (20.9 - \%O_2)] \times ppm$ lb/MMBtu
 lb/hr / (dscfm x 60 min/hr) lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 lb/MMBtu
 (lb/MMBtu Total Sulfate) x (32 / 98.076) lb/MMBtu
 Total Sulfur lb/MMBtu

EMISSION RATE CALCULATIONS

PLANT : HARRIS WOOLF
PRECLEANER BAGHOUSE

RUN NO.: 3
DATE : SEPT 14, 1992
O2 CORR.: 3.0 %

STANDARD TEMP. : 60 DEG. F

```
*****
Front Half Wash (FHW)      0.02020 grams | Vm(std) 102.526 ft3
Mass Filter (MF)           0.00134 grams | Vw(std)  1.024 ft3
Back Half Wash (BHW)       0.00186 grams | Qs(std) 29,964 dscfm
Front Half Sulfate (FHS)    mg H2SO4 | Bws      0.010
Back Half Sulfate (BHS)     mg H2SO4 | CO2       0.00 %
H2O2 Catch (SO2)           mg H2SO4 | O2        20.90 %
*****
```

F-FACTOR

$10E6 \times [3.64(\%H) + 1.53(\%C) + 0.57(\%S) + 0.14(\%N) - 0.46(\%O_2)] / (Btu/lb) \times [(T_{std} + 460)/528]$ dscf/MMBtu

FILTERABLE PARTICULATE

$15.432 \times (FHW + MF) / [Vm(std) + Vw(std)]$ 0.0032 gr/scf
 $15.432 \times (FHW + MF) / Vm(std)$ 0.0032 gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 0.83 lb/hr
 F-Fac x $1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL PARTICULATE

$15.432 \times (FHW + MF + BHW) / [(Vm(std) + Vw(std))]$... 0.0035 gr/scf
 $15.432 \times (FHW + MF + BHW) / Vm(std)$ 0.0035 gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ 0.90 lb/hr
 F-Fac x $1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

TOTAL SULFATE

$0.015432 \times (FHS + BHS) / [Vm(std) + Vw(std)]$ gr/scf
 $0.015432 \times (FHS + BHS) / Vm(std)$ gr/dscf
 gr/dscf x (12 / %CO2) @ 12% CO2
 $0.00857 \times Qs(std) \times gr/dscf$ lb/hr
 F-Fac x $1.4286E-4 \times [20.9 / (20.9 - \%O_2)] \times gr/dscf$.. lb/MMBtu

SULFUR DIOXIDE (SO2)

$1.60982 \times [T(std) + 460] \times (mg H_2SO_4) / [98.076 \times Vm(std)]$ ppm
 ppm x $[(20.9 - \text{Oxygen Corr.}) / (20.9 - \%O_2)]$ @ O2 corr.
 ppm x (1 - Bws) ppm (wet)
 $8.223E-5 \times Qs(std) \times 64.062 \times ppm / [T(std) + 460]$.. lb/hr
 F-Factor x $64.062 \times [1.3711E-6 / [T(std) + 460]] \times [20.9 / (20.9 - \%O_2)] \times ppm$ lb/MMBtu
 lb/hr / (dscfm x 60 min/hr) lb/dscf

SULFUR (S)

(lb/MMBtu SO2) / 2 lb/MMBtu
 (lb/MMBtu Total Sulfate) x (32 / 98.076) lb/MMBtu
 Total Sulfur lb/MMBtu

DRY GAS METER / ORIFICE METER CALIBRATION DATA

DateJULY 20 1992
 Bar. Press. in.Hg 29.88
 Meter Box No. ... 21313

Dry Gas Meter No. ... 103707
 Standard Test Meter # 69279
 Operator AB

STANDARD TEST METER			DRY TEST METER				Time t (min)
Press. dHs (in. H2O)	Temp. Ts (dF)	Volume Vs (ft3)	Press. dH (in. H2O)	Temp. Tdi (dF)	Temp. Tdo (dF)	Volume Vd (ft3)	
-1.4	68.0	391.523	0.5	83	82	1020.297	54.0
	67.0	368.346		82	81	996.854	
Avg/Net :	67.5	23.177			82	23.443	
-2.3	68.0	367.739	1.0	81	80	996.234	40.0
	67.0	344.170		80	79	972.482	
Avg/Net :	67.5	23.569			80	23.752	
-2.5	67.0	265.627	1.5	80	79	894.385	38.0
	67.0	237.624		78	79	866.307	
Avg/Net :	67.0	28.003			79	28.078	
-3.8	67.0	299.374	2.0	79	80	928.127	42.0
	68.0	266.025		78	79	894.793	
Avg/Net :	67.5	33.349			79	33.334	
-5.4	67.0	343.531	3.0	80	79	971.849	42.0
	66.0	301.895		78	78	930.627	
Avg/Net :	66.5	41.636			79	41.222	

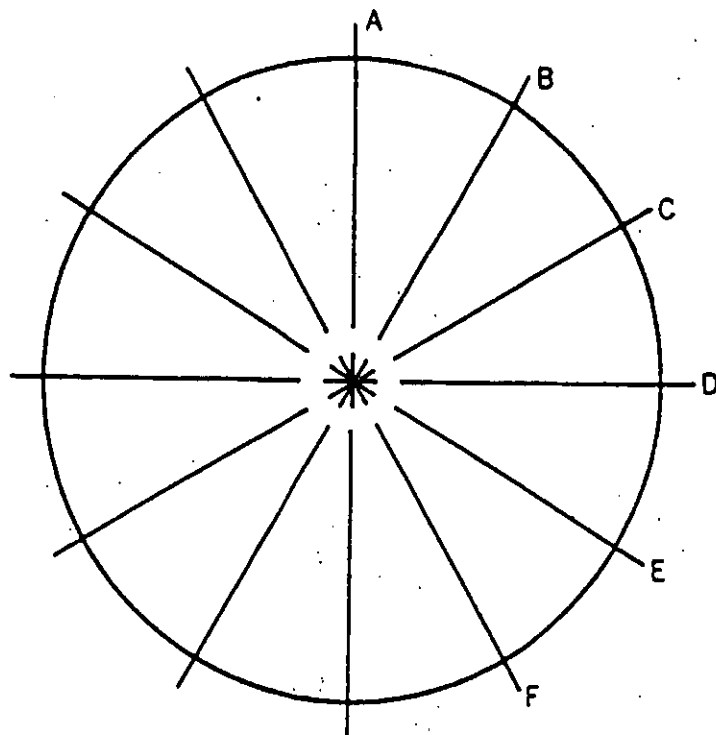
$$y = V_s \times (P_{bar} + (dH_s / 13.6)) \times (Avg. T_d + 460) / [V_d \times (P_{bar} + (dH / 13.6)) \times (T_s + 460)]$$

$$K_o = [(V_s/t) \times [(T_{do} + 460) / (T_s + 460)] \times [(P_{bar} + (dH_s/13.6)) / (P_{bar} + (dH/13.6))] / [((T_{do} + 460) \times dH) / (P_{bar} + (dH/13.6)) \times (Mm)]^{0.5}$$

dH :	0.5	1.0	1.5	2.0	3.0	Avg.	Std.Dev.
y :	1.0111	1.0076	1.0100	1.0077	1.0123	1.0098	0.0019
Ko :	0.7845	0.7580	0.7735	0.7187	0.7295	0.7528	0.0252
y :	0.18 % Relative Std. Dev.						
Ko :	3.34 % Relative Std. Dev.						

 Steiner Environmental, Inc.

NOZZLE CALIBRATION



DIAMETER (in.)

A 0.234

B 0.234

C 0.235

D 0.234

E _____

F _____

AVG. 0.2343

DATE 3-25-92

NOZZLE NO. 1458

OPERATOR SW

APPENDIX B
HARRIS WOOLF OPERATING DATA



HARRIS WOOLF

CALIFORNIA ALMONDS



Route 1, Box 470 • Coalinga, CA 93210 • Tel: 209-884-2147 Fax: 209-884-2746

To Stinner Environmental
From Hortencia

Date 9/1/92

- ☐ Reply and send me copy
- ☐ Take appropriate action
- ☐ For your signature
- ☒ For your information
- ☐ For your comments
- ☐ See me about this

- ☐ Note and file
- ☐ Note and return
- ☐ For your approval
- ☐ Please reply promptly
- ☐ As you requested
- ☐ Report on this

Comments: product done during
test, total lbs 353,560 lbs.

Thank you
Hortencia Solari

Selectform, Inc., Box 3045, Freeport, NY 11520

Form 60 - Printed in U.S.A.

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HARRIS - WOOLF
CALIFORNIA ALMONDS

PRECLEANER LOG

DATE: 9-14-92

ME TART ↑↑	TIME STOP	ISCALETICKET NUMBER	CHOWER	FIELD	TANK NUMBER	INCOMING FIELD RUN LEB	COMMENTS
6:35	18:30	2681	ATP	2B-2	* 3	52,250	TEST RUN 1 13.8 TPH
8:35	210:24	2682	ATP	2B-2	* 6	54,740	
9:34	312:20	2680	ATP	2B-2	* 5	48,710	
12:25	42:10	2685	ATP	2B-1	* 1	57,650	TEST RUN 2 13.8 TPH TEST RUN 3 15.6 TPH
2:20	54:00	2691	ATP	2B-1	* 5	51,570	
4:49	66:24	2694	DOUBLE	INE-24	* 6	46,190	
7:27	77:53	2697	DOUBLE	INE-24	* 1	46,290	alot of grass & leaves. Leaves not available. 135 minutes - Diet & grass
8:24	810:20	2693	DOUBLE	INE-24	* 7	48,370	Diet & dust
9:28	912:00	2656	Woolf	BIK-4	* 6	60,000	Diet & twigs
10:00	1012:25	2638	Woolf	BIK-1	* 1	65,310	Diet & alot of twigs
11							alot of diet & twigs
12							
13							
14							
15							
16							

TOTAL 507,240
TODAY

* END OF TEST

TOTAL LBS FANNED 353,560

OPERATOR: Math Espinoza

-Day- Roque Ayala