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Note: This is a reference cited in AP 42, *Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at [www.epa.gov/ttn/chief/ap42/](http://www.epa.gov/ttn/chief/ap42/)

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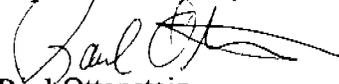
**Can and Bottle Filler Vent  
Volatile Organic Compound Test  
for  
Coors Brewing Company**

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## Introduction

Air Pollution Testing, Inc. was contracted by Coors Brewing Company to conduct a series of source emissions tests on the can filler line and bottle filler line vents. Testing at each location was conducted to determine mass flow rates of volatile organic compounds. The testing was conducted on October 14, 1992.

## Summary of Procedures

At each location, testing was conducted in accordance with EPA methods 1 through 4 and 25A as detailed in Code of Federal Regulations, Title 40, Part 60, Appendix A. Methods 1 through 4 were used to determine the volumetric air flows in the two ducts and method 25A was used to determine the concentrations of volatile organic compounds (VOCs). The data from all of the methods was then combined to calculate mass flow rates of VOCs at each location. Additionally, data was collected on the total volume of beer processed at each location during the testing, and the data was used to calculate the lbs of VOCs per barrel of beer at each location.

Each one hour method 25A sampling period consisted of extracting a gas sample from the duct through a heated sample line and running it directly into the inlet port of a Model 3-100 Flame Ionization Analyzer manufactured by JUM. The organic concentration was displayed in real-time on the analyzer front panel and recorded on a strip chart. Before and after the sampling program, the analyzer was calibrated with a high level propane calibration gas and zero gas, and then challenged with a mid level propane calibration gas to verify linearity of response. Before and after each one hour sampling period, the analyzer was challenged with the mid level calibration gas and zero gas to quantify any analyzer span and zero drift for the previous period. Additionally, the analyzer was re-calibrated at this point as necessary. To ensure accurate data collection, all calibration gases were prepared and certified in accordance with EPA Protocol 1, and were introduced to the analyzer at the sampling probe tip at ambient pressure. Additionally, at both locations, a traverse of the duct was conducted with the analyzer sampling probe to ensure that no VOC concentration gradient existed which would bias the data as a function of probe placement within the duct. In both cases, no gradient was indicated by the data, and sampling was conducted at the approximate area centers of the ducts. The recorded data from each sampling period was averaged using 40 equally spaced points per one hour sampling period, with all data corrected for analyzer span and zero drift.

Concurrent with each VOC sampling period, a differential pressure and temperature traverse of the duct was conducted in accordance with method 2 at a grid of sampling points selected in accordance with method 1. Additionally, a gas sample was extracted from the duct and pulled through a series of chilled glass impingers and through a calibrated dry gas meter to determine the duct gas moisture content in accordance with method 4. The effluent gas from the method 4 sampling train was collected in a Tedlar gas bag and analyzed for oxygen and carbon dioxide using Orsat analysis in accordance with method 3. This data was combined to determine the volumetric flow rate in each of the ducts sampled.

### **Additional Notes**

Because flame ionization analyzers do not respond perfectly to all organic species, it may be necessary to calibrate the analyzer with the specific organic compound or compounds present, if they are known. In this testing program, it was assumed that the dominant organic compound present was ethanol. In a previous VOC testing program conducted at Coors Brewing Company, a similar VOC analyzer was calibrated with ethanol and propane to determine an empirical constant for conversion of propane-calibrated VOC data to true ethanol values. The constant determined in this earlier program is assumed to be valid for analyzers employing similar detection technology, and is used in the current program. Consequently, where noted, the VOC data presented in this report have been corrected to ethanol using these two assumptions.

## Results

The results of the testing are presented in the following tables. Any testing variables not presented here may be found in *Appendix 1 Testing Parameters / Sample Calculations*.

run #	1	2	averages
start time	11:32	13:30	
stop time	12:32	14:30	
stack temp. (°F)	72	72	72
stack moisture (vol. %)	1.24	1.98	1.61
gas velocity (ft/sec)	21.4	21.0	21.2
gas flow (acfm)	12352	12096	12224
gas flow (dscfm)	9970	9691	9830
volume beer (bbls)	519	605	562
VOC (ppm wet as propane)	42.2	52.1	47.2
VOC (lb/hr as propane)	2.93	3.62	3.27
VOC (lb/hr as ethanol)*	6.90	8.53	7.72
VOC (lb/bbl as ethanol)*	0.013	0.014	0.014

Table 1 - Bottle Filler Vent  
VOC Testing Results  
10-14-92

\* - An empirical constant of 2.36 demonstrated in an earlier testing program was used to convert propane-calibrated analyzer data to ethanol. See Additional Notes (page 3) for more details.

Results (continued)

run #	1	2	averages
start time	15:30	17:00	
stop time	16:30	18:00	
stack temp. (°F)	75	75	75
stack moisture (vol. %)	1.11	1.29	1.20
gas velocity (ft/sec)	44.5	43.8	44.1
gas flow (acfm)	32306	31777	32041
gas flow (dscfm)	25932	25461	25697
volume beer (bbls)	1245	1108	1177
VOC (ppm wet as propane)	31.5	33.3	32.4
VOC (lb/hr as propane)	5.67	6.07	5.87
VOC (lb/hr as ethanol)*	13.38	14.33	13.86
VOC (lb/bbl as ethanol)*	0.011	0.013	0.012

Table 2 - Can Filler Vent  
VOC Testing Results  
10-14-92

\* - An empirical constant of 2.36 demonstrated in an earlier testing program was used to convert propane-calibrated analyzer data to ethanol. See Additional Notes (page 3) for more details.

**Appendix 1**  
**Testing Parameters**  
**Sample Calculations**

Coors Brewing Company

Bottle Filler Vent

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EPA Methods 1-4 : Determination of Volumetric Flow Rate and Molecular Weight

<u>Field Data</u>	Run #1	Run #2	Averages
sample volume (ft3)	35.120	36.797	35.959
sampling time (minutes)	30	30	30
stack temp. (oF) (pre-test)	72	72	72
stack temp. (oF) (post-test)	72	72	72
meter temp. (oF)	77	94	86
barometric pressure (mbar)	834	834	834
barometric pressure (" Hg)	24.633	24.633	24.633
static press. (in. water) (pre-test)	0.03	0.04	0.04
static press. (in. water) (post-test)	0.03	0.04	0.04
moisture (grams)	8.0	13.0	10.5
oxygen (%)	20.9	20.9	20.9
carbon dioxide (%)	0.0	0.0	0.0
delta H	4.00	4.00	4.00
(delta p) <sup>1/2</sup> (pre-test)	0.3435	0.3359	0.3397
(delta p) <sup>1/2</sup> (post-test)	0.3435	0.3359	0.3397
meter box Y	1.0389	1.0389	1.0389
delta H@	1.683	1.683	1.683
pitot tube constant	0.84	0.84	0.84
stack diameter (inches)	42	42	42
port length (inches)	1.75	1.75	1.75
<u>Calculations</u>			
sample volume (dscf)	29.880	30.346	30.113
moisture volume (scf)	0.377	0.612	0.494
moisture content (%/100)	0.0124	0.0198	0.0161
molecular weight (dry)	28.836	28.836	28.836
molecular weight (actual)	28.701	28.622	28.661
gas velocity (ft/sec)	21.40	20.95	21.17
gas flow (acfm)	12352	12096	12224
gas flow (dscfm)	9970	9691	9830

**Coors Brewing Company**

**Can Filler Vent**

10-14-92

**EPA Methods 1-4 : Determination of Volumetric Flow Rate and Molecular Weight**

<u>Field Data</u>	Run #1	Run #2	Averages
sample volume (ft3)	35.012	34.517	34.764
sampling time (minutes)	30	30	30
stack temp. (oF) (pre-test)	75	75	75
stack temp. (oF) (post-test)	75	75	75
meter temp. (oF)	85	87	86
barometric pressure (mbar)	833	833	833
barometric pressure (" Hg)	24.604	24.604	24.604
static press. (in. water) (pre-test)	0.03	0.03	0.03
static press. (in. water) (post-test)	0.03	0.03	0.03
moisture (grams)	7.0	8.0	7.5
oxygen (%)	20.9	20.9	20.9
carbon dioxide (%)	0.0	0.0	0.0
delta H	4.00	4.00	4.00
(delta p) <sup>1/2</sup> (pre-test)	0.7121	0.7002	0.7062
(delta p) <sup>1/2</sup> (post-test)	0.7121	0.7002	0.7062
meter box Y	1.0389	1.0389	1.0389
delta H@	1.683	1.683	1.683
pitot tube constant	0.84	0.84	0.84
stack diameter (inches)*	47.1	47.1	47
port length (inches)	1.25	1.25	1.25
<u>Calculations</u>			
sample volume (dscf)	29.316	28.796	29.056
moisture volume (scf)	0.329	0.377	0.353
moisture content (%/100)	0.0111	0.0129	0.0120
molecular weight (dry)	28.836	28.836	28.836
molecular weight (actual)	28.716	28.696	28.706
gas velocity (ft/sec)	44.49	43.77	44.13
gas flow (acfm)	32306	31777	32041
gas flow (dscfm)	25932	25461	25697

\* - diameter of a round stack with area equal to duct cross-section area.

## EPA Methods 1 - 4 : Determination of Volumetric Flow Rate and Molecular Weight

### Sample Calculations

sample volume (dscf)

$$\begin{aligned} &= [17.64 (\text{°R/in Hg})]V_m Y [P_{\text{bar}} + (\Delta H/13.6)]/T_m \\ &= (17.64 \text{ °R/in Hg})(35.120 \text{ ft}^3)(1.0389)[24.633+(4.00/13.6) \text{ inches Hg}]/(77+460 \text{ °R}) \\ &= 29.880 \text{ dscf} \end{aligned}$$

moisture volume (scf)

$$\begin{aligned} &= (0.04707 \text{ ft}^3/\text{ml})V_{\text{lc}} \\ &= (0.04707 \text{ ft}^3/\text{ml})(8.0) \\ &= 0.377 \text{ scf} \end{aligned}$$

moisture content (%/100)

$$\begin{aligned} &= V_{\text{w(std)}}/(V_{\text{m(std)}} + V_{\text{w(std)}}) \\ &= (0.377 \text{ scf})/(29.880 \text{ dscf} + 0.377 \text{ scf}) \\ &= 0.0124 \end{aligned}$$

molecular weight dry (grams/mole)

$$\begin{aligned} &= 0.440(\% \text{CO}_2) + 0.320(\% \text{O}_2) + 0.280(\% \text{N}_2 + \% \text{CO}) \\ &= 0.440(0.0 \% \text{CO}_2) + (0.320)(20.9 \% \text{O}_2) + (0.280)(79.1 \% \text{N}_2) \\ &= 28.836 \text{ grams/mole} \end{aligned}$$

molecular weight actual (grams/mole)

$$\begin{aligned} &= M_d(1 - B_{\text{ws}}) + 18.0(B_{\text{ws}}) \\ &= (28.836 \text{ grams/mole})(1 - 0.0124) + (18.0)(0.0124) \\ &= 28.701 \text{ grams/mole} \end{aligned}$$

gas velocity (ft/sec)

$$\begin{aligned} &= \{85.49 \text{ ft/sec} [(1\text{b}/\text{lb-mole})(\text{in. Hg})/(\text{°R})(\text{in. H}_2\text{O})]^{1/2}\} C_p (\Delta p^{1/2})_{\text{avg}} (T_{\text{s(avg)}}/P_{\text{s}} M_{\text{s}})^{1/2} \\ &= (85.49)(0.84)(0.3435) \{ (72+460)/[(24.633+0.03/13.6)(28.701)] \}^{1/2} \\ &= 21.40 \text{ ft/sec} \end{aligned}$$

gas flow (acfm)

$$\begin{aligned} &= A_{\text{vs}}(60 \text{ seconds/minute}) \\ &= (\pi)(42/12 \text{ ft})^2(21.40 \text{ ft/sec})(60)/4 \\ &= 12352 \text{ acfm} \end{aligned}$$

gas flow (dscfm)

$$\begin{aligned} &= (60 \text{ seconds/minute})(1 - B_{\text{ws}})v_{\text{s}} A T_{\text{std}} P_{\text{s}} / (T_{\text{s(avg)}} P_{\text{std}}) \\ &= (60)(1-0.0124)(21.40)(\pi)(42/12 \text{ ft})^2(528)(24.633+0.03/13.6)/[(72+460)(29.92)(4)] \\ &= 9970 \text{ dscfm} \end{aligned}$$

## EPA Methods 1 - 4 : Determination of Volumetric Flow Rate and Molecular Weight

### Variables

A = Stack cross-sectional area (ft<sup>2</sup>)

B<sub>ws</sub> = Water vapor in the gas stream, proportion by volume

C<sub>p</sub> = Pitot coefficient (0.84 dimensionless)

ΔH = Average pressure differential across the orifice meter (in. H<sub>2</sub>O)

Δp = Velocity head of stack gas (in. H<sub>2</sub>O)

M<sub>d</sub> = Molecular weight of dry stack gas (lb/lb mole)

M<sub>s</sub> = Molecular weight of wet stack gas (lb/lb mole)

P<sub>bar</sub> = Barometric pressure (in. Hg)

P<sub>g</sub> = Sack pressure relative to ambient (in. H<sub>2</sub>O)

P<sub>s</sub> = Absolute stack pressure (in. Hg)

P<sub>std</sub> = Standard atmospheric pressure (29.92 in. Hg)

Q<sub>a</sub> = Actual volumetric air flow out of stack (acfm)

Q<sub>std</sub> = Volumetric air flow out of stack corrected to standard conditions (dscfm)

T<sub>m</sub> = Average meter temperature (°F + 460 = °R)

T<sub>s(avg)</sub> = Average stack temperature (°F + 460 = °R)

T<sub>std</sub> = Standard temperature (528 °R)

V<sub>lc</sub> = volume of moisture collected from gas sample (ml)

v<sub>s</sub> = Stack gas velocity (ft/sec)

V<sub>m</sub> = Volume of gas through dry gas meter (ft<sup>3</sup>)

V<sub>m(std)</sub> = Volume of gas through dry gas meter corrected to standard conditions (dscf)

V<sub>w(std)</sub> = Volume of water vapor in gas sample at standard conditions (scf)

Y = Dry gas meter calibration factor (dimensionless)

Q = Total sampling time (minutes)

**Coors Brewing Company**  
**Bottle Filler Vent**  
**10-14-92**  
**VOC Mass Emission Rates**

**Field Data**

run #	1	2	Averages
start time	11:32	13:30	
stop time	12:32	14:30	
VOC conc. (ppm wet)	42.2	52.1	47.2
% H <sub>2</sub> O*	1.24	1.98	1.61
volumetric flow rate (dscfm)*	9970	9691	9831
bbls beer**	519	605	562

**Calculations**

VOC emissions (lb/hr as propane)	2.93	3.62	3.27
VOC emissions (lb/hr as ethanol)***	6.90	8.53	7.72
VOC emissions (lb/bbl as ethanol)	0.013	0.014	0.014

\* - flow data was obtained from concurrent methods 1 - 4 traverses.

\*\* - operating data was collected concurrently with sampling by Coors Brewing Company personnel.

\*\*\* - propane to ethanol conversion uses 2.36 empirical conversion factor obtained previously.

**Coors Brewing Company**  
**Can Filler Vent**  
**10-14-92**  
**VOC Mass Emission Rates**

**Field Data**

run #	1	2	Averages
start time	15:30	17:00	
stop time	16:30	18:00	
VOC conc. (ppm wet)	31.5	33.3	32.4
% H <sub>2</sub> O*	1.11	1.29	1.20
volumetric flow rate (dscfm)*	25932	25461	25697
bbls beer**	1245	1108	1177

**Calculations**

VOC emissions (lb/hr as propane)	5.67	6.07	5.87
VOC emissions (lb/hr as ethanol)***	13.38	14.33	13.86
VOC emissions (lb/bbl as ethanol)	0.011	0.013	0.012

\* - flow data was obtained from concurrent methods 1 - 4 traverses.

\*\* - operating data was collected concurrently with sampling by Coors Brewing Company personnel.

\*\*\* - propane to ethanol conversion uses 2.36 empirical conversion factor obtained previously.

Coors Brewing Company

Bottle Filler Vent

10-14-92

Method 25A : Measurement of Total Organic Concentration Using a Flame

Ionization Analyzer

Strip Chart Data

Run #1

		Zero (%FS)	Span (%FS)	Actual Span (ppm)
Start	11:32	0.0	38.5	40.1
Stop	12:32	-1.5	38.0	

point #	%FS VOC	ppm VOC	point #	%FS VOC	ppm VOC
1	49.0	51.2	21	39.0	40.9
2	48.0	50.1	22	42.0	44.0
3	47.0	49.1	23	39.0	40.9
4	50.0	52.2	24	37.0	38.8
5	40.0	41.9	25	40.0	41.9
6	35.0	36.8	26	44.0	46.0
7	36.0	37.8	27	44.0	46.0
8	35.0	36.8	28	48.0	50.1
9	35.0	36.8	29	38.0	39.8
10	35.0	36.8	30	40.0	41.9
11	34.0	35.7	31	47.0	49.1
12	37.0	38.8	32	43.0	45.0
13	34.0	35.7	33	46.0	48.1
14	31.0	32.6	34	41.0	42.9
15	30.0	31.6	35	39.0	40.9
16	22.0	23.4	36	45.0	47.0
17	18.0	19.3	37	46.0	48.1
18	40.0	41.9	38	48.0	50.1
19	48.0	50.1	39	48.0	50.1
20	47.0	49.1	40	48.0	50.1
averages:	37.5	39.4		43.1	45.1

Drift Cal. Avg. VOC (ppm as propane)

**Coors Brewing Company**

**Bottle Filler Vent**

**10-14-92**

**Method 25A : Measurement of Total Organic Concentration Using a Flame**

**Ionization Analyzer**

**Strip Chart Data**

Run #2

		Zero (%FS)	Span (%FS)	Actual Span (ppm)
Start	13:30	0.0	40.0	40.1
Stop	14:30	-0.8	39.0	

point #	%FS VOC	ppm VOC	point #	%FS VOC	ppm VOC
1	51.0	51.7	21	53.0	53.7
2	52.0	52.7	22	53.0	53.7
3	52.0	52.7	23	52.0	52.7
4	47.0	47.6	24	52.0	52.7
5	47.0	47.6	25	52.0	52.7
6	50.0	50.7	26	53.0	53.7
7	47.0	47.6	27	53.0	53.7
8	49.0	49.6	28	55.0	55.7
9	48.0	48.6	29	55.0	55.7
10	47.0	47.6	30	53.0	53.7
11	46.0	46.6	31	55.0	55.7
12	51.0	51.7	32	53.0	53.7
13	50.0	50.7	33	53.0	53.7
14	53.0	53.7	34	51.0	51.7
15	54.0	54.7	35	50.0	50.7
16	53.0	53.7	36	49.0	49.6
17	52.0	52.7	37	49.0	49.6
18	53.0	53.7	38	52.0	52.7
19	53.0	53.7	39	53.0	53.7
20	54.0	54.7	40	51.0	51.7
averages:	50.5	51.1		52.4	53.0

Drift Cal. Avg. VOC (ppm as propane)

Coors Brewing Company

Can Filler Vent

10-14-92

Method 25A : Measurement of Total Organic Concentration Using a Flame Ionization Analyzer

Strip Chart Data

Run #3

		Zero (%FS)	Span (%FS)	Actual Span (ppm)
Start	15:30	0.0	40.0	40.1
Stop	16:30	0.0	39.0	

point #	%FS VOC	ppm VOC	point #	%FS VOC	ppm VOC
1	33.0	33.5	21	28.0	28.4
2	35.0	35.5	22	25.0	25.4
3	34.0	34.5	23	27.0	27.4
4	34.0	34.5	24	25.0	25.4
5	32.0	32.5	25	23.0	23.3
6	36.0	36.5	26	28.0	28.4
7	34.0	34.5	27	30.0	30.5
8	35.0	35.5	28	29.0	29.4
9	35.0	35.5	29	30.0	30.5
10	35.0	35.5	30	30.0	30.5
11	32.0	32.5	31	30.0	30.5
12	35.0	35.5	32	28.0	28.4
13	34.0	34.5	33	26.0	26.4
14	35.0	35.5	34	28.0	28.4
15	34.0	34.5	35	29.0	29.4
16	28.0	28.4	36	27.0	27.4
17	32.0	32.5	37	28.0	28.4
18	33.0	33.5	38	32.0	32.5
19	34.0	34.5	39	34.0	34.5
20	34.0	34.5	40	32.0	32.5
averages:	33.7	34.2		28.4	28.9

Drift Cal. Avg. VOC (ppm as propane)

Coors Brewing Company

Can Filler Vent

10-14-92

Method 25A : Measurement of Total Organic Concentration Using a Flame Ionization Analyzer

Strip Chart Data

Run #4

		Zero (%FS)	Span (%FS)	Actual Span (ppm)
Start	17:00	0.0	40.0	40.1
Stop	18:00	0.0	39.5	

point #	%FS VOC	ppm VOC	point #	%FS VOC	ppm VOC
1	33.0	33.3	21	34.0	34.3
2	34.0	34.3	22	29.0	29.3
3	33.0	33.3	23	33.0	33.3
4	34.0	34.3	24	34.0	34.3
5	35.0	35.3	25	33.0	33.3
6	34.0	34.3	26	33.0	33.3
7	34.0	34.3	27	34.0	34.3
8	34.0	34.3	28	33.0	33.3
9	34.0	34.3	29	34.0	34.3
10	32.0	32.3	30	34.0	34.3
11	35.0	35.3	31	33.0	33.3
12	30.0	30.3	32	30.0	30.3
13	34.0	34.3	33	31.0	31.3
14	34.0	34.3	34	28.0	28.2
15	34.0	34.3	35	33.0	33.3
16	32.0	32.3	36	31.0	31.3
17	32.0	32.3	37	33.0	33.3
18	32.0	32.3	38	34.0	34.3
19	33.0	33.3	39	34.0	34.3
20	34.0	34.3	40	34.0	34.3
averages:	33.4	33.6		32.6	32.9

Drift Cal. Avg. VOC (ppm as propane)

## EPA Method 25A : Measurement of Total Organic Concentration Using a Flame Ionization Analyzer

### Sample Calculations

drift cal. ppm as propane

$$= \frac{[(\%FS \text{ analyzer stack value}) - (\%FS \text{ analyzer average 0 value})](\text{span gas value ppm})}{[(\%FS \text{ analyzer average span value}) - (\%FS \text{ analyzer average 0 value})]}$$

$$= \frac{(40.3 \%FS) - [(0.0 \%FS - 1.5 \%FS) / 2](40.1 \text{ ppm})}{[(38.5 \%FS + 38.0 \%FS) / 2] - [(0.0 \%FS - 1.5 \%FS) / 2]}$$

$$= 42.2 \text{ ppm VOC as propane}$$

VOC emissions (lb/hr as propane)

$$= \frac{[\text{avg. VOC conc. (ppm)}][\text{stack flow (dscfm)}](60 \text{ min/hr})(28.317 \text{ liter/ft}^3)(44.09 \text{ g/mole})(2.205 \text{ lb/kg})}{(24.055 \text{ liters/mole @ STP})(1000 \text{ g/kg})(1 \times 10^6)(1 - \%H_2O/100)}$$

$$= \frac{(42.2 \text{ ppm})(9970 \text{ dscfm})(60)(28.317)((44.09)(2.205))}{(24.055)(1000)(1 \times 10^6)(1 - 0.0124)}$$

$$= 2.93 \text{ lb/hr VOC}$$

VOC emissions (lb/hr as ethanol)

$$= [\text{VOC emissions (lb/hr as propane)}](2.36 \text{ empirical constant})$$

$$= (2.93 \text{ lb/hr})(2.36)$$

$$= 6.90$$

VOC emissions (lb/bbl as ethanol)

$$= [\text{VOC emissions (lb/hr as ethanol)}] / \{ [\text{beer volume (bbl)}] / [\text{sampling time (hours)}] \}$$

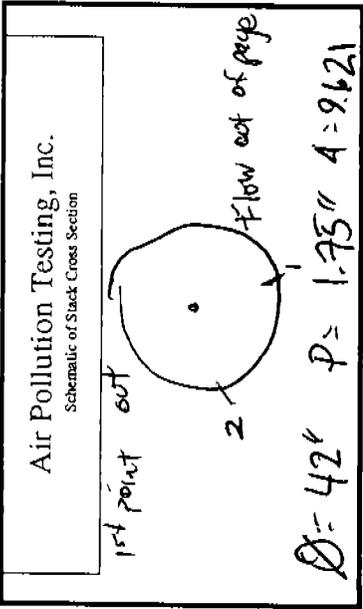
$$= (6.90 \text{ lb/hr}) / (519/1)$$

$$= 0.013 \text{ lb/bbl as ethanol}$$

**Appendix 2**  
**Field Data**

measured 24.633 kg

Plant: Coors Brewing Co  
 Location: Golden, Co  
 Operator: RB/MM  
 Run Number: 1683  
 Sample Box ID#: /  
 Meter ΔH@: 1.683  
 Pilot Tube Coefficient: 84  
 Meter Box ID#: /  
 C Factor: /  
 Pre-Test Pilot Leak Check:   
 Post-Test Pilot Leak Check:   
 Pre-Test Pump Leak Check:   
 Post-Test Pump Leak Check:



CO2 (%) 0.0  
 Assumed Moisture (%) 1  
 Ambient Temperature (oF) 75  
 Probe Length (ft) 4'  
 Probe Temperature (oF) /  
 Nozzle Diameter (in) /  
 Static Pressure (in H2O) 7.03  
 Filter ID# /  
 O2 (%) 20.8  
 Barometric Pressure (inbar) 834  
 Probe Material 55  
 Filter Temperature (oF) /  
 Moisture (grams) 8.0  
 Start Time /  
 Stop Time /  
 Method 1-4

Traverse Point Number	Sampling Time (minutes)	Vacuum (in Hg)	Velocity Head (in H2O)	Pressure Differential (in H2O)	Gas Volume (ft <sup>3</sup> ) Initial Volume	Stack Temp. (oF)	Probe Temp. (oF)	Pilot Temp. (oF)	Gas Temp. Inlet (oF)	Gas Temp. Outlet (oF)	Condenser Temp. (oF)	Notes
1-1	10	2	.11	4.0	337.387	76			68	69		10:58 → 11:28 Majlwe R1
2	20	2	.11	4.0	360.80	74			85	73		7.0 g + 1.0 ml
3	30	2	.12	4.0	372.507	73			90	76		discuss 9554
4			.12			73						Bwo = .012
5			.13		35.120	72						Vs = 21.4
6			.12			72						ACFM = 12352
7			.12			72						DSCFM = 9964
8			.11			74						Bottle Vent R1
2-1			.12			73						
2			.13			72						
3			.13			72						
4			.13			72						
5			.11			72						
6			.11			72						
7			.12			73						
8			.12			72						

(3435)

(77)

(72)

Measured

Plant: Coors Brewing Co Date: 10-14-92

Location: Golden, CO

Operator: PO/MAM

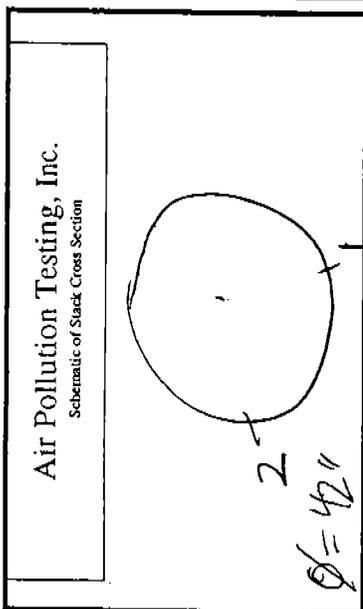
Run Number: 2 Pilot Tube Coefficient: .84

Sample Box ID#: 1.683 Meter Box ID#: 1.683

Meter ΔH@: 1.683 C Factor: 1.683

Pre-Test Pilot Leak Check:  Post-Test Pilot Leak Check:

Pre-Test Pump Leak Check:  Post-Test Pump Leak Check:



CO<sub>2</sub> (%): 0.0 O<sub>2</sub> (%): 20.8

Assumed Moisture (%): 75 Barometric Pressure (inbar): 834

Ambient Temperature (oF): 4 Probe Material: SS

Probe Length (ft): 4 Filter Temperature (oF): 13.0

Probe Temperature (oF): 13.0 Moisture (grams): 13.0

Nozzle Diameter (in): 1.04 Start Time: 13:21

Static Pressure (in H<sub>2</sub>O): 1.04 Stop Time: 13:21

Filter ID#: 1-4 Method: 1-4

Traverse Point	Sampling Time (minutes)	Velocity (in Hr)	Velocity Head (in H <sub>2</sub> O)	Pressure Differential (in H <sub>2</sub> O)	Gas Volume (ft <sup>3</sup> ) Initial Volume	Stack Temp. (oF)	Probe Temp. (oF)	Filter Temp. (oF)	Inlet Gas Temp. (oF)	Outlet Gas Temp. (oF)	Condenser Temp. (oF)	Notes
H-1	10	3	.10	4.0	372.707	75	75		90	89		Bottle Vent R2
2	20	2	.10	4.0	397.80	72	72		101	89		Floor 2 1/2
3	30	2	.10	4.0	409.504	71	71		104	91		Moisture R2 start 13:21
4			.11		36.797	71	71					4.0g 9.0ml
5			.11			71	71					
6			.11			71	71					
7			.11			71	71					
8			.11			72	72					
2-1			.10			73	73					
2			.12			72	72					
3			.14			72	72					
4			.13			72	72					
5			.11			72	72					
6			.11			72	72					
7			.12			71	71					
8			.13			71	71					

(3359)

(72)

(94)

24,603 HQ

Plant: Coors Brewing Co Date: 10-14-92

Location: Golden, CO

Operator: PO/MM

Run Number: 3

Pilot Tube Coefficient: .84

Sample Box ID#: /

Meter Box ID#: /

Meter ΔH@: 1.683

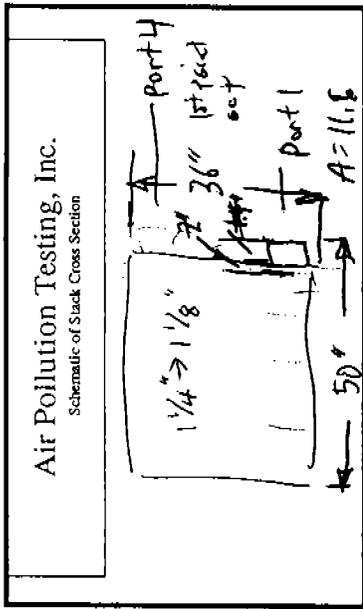
C Factor: /

Pre-Test Pilot Leak Check:

Post-Test Pilot Leak Check:

Pre-Test Pump Leak Check:

Post-Test Pump Leak Check:



CO2 (%) 0.0 O2 (%) 20.9

Assumed Moisture (%) 1 Barometric Pressure (mbar) 833

Ambient Temperature (oF) 75 Probe Material 55

Probe Length (ft) 4 Filter Temperature (oF) /

Probe Temperature (oF) / Moisture (grams) 7.0

Nozzle Diameter (in) / Start Time /

Static Pressure (in H2O) .03 Stop Time /

Filter ID# / Method 1-4

Traverse Point Number	Sampling Time (minutes)	Vacuum (in Hg)	Velocity Head (in H2O)	Pressure Differential (in H2O)	Gas Volume (ft3) Initial Volume	Stack Temp. (oF)	Probe Temp. (oF)	Filter Temp. (oF)	Inlet Gas Temp. (oF)	Outlet Gas Temp. (oF)	Condenser Temp. (oF)	Notes
1-1	10	2	.22	4.0	409.503	75			78	78		48 x 34.8"
2	20	2	.47	4.0		74			88	82		Moisture KI 351 → 4:21
3	30	2	.42	4.0	444.515	75			97	85		πd² = 1.1W
4			.37			75						7 deg = 48.1
2-1			.44			75						
2			.57			75						48.75 x 35.75
3			.58			75						47.1 = deg
4			.77			75						Can Vent R1
3-1			.40			75						
2			.61			75						
3			.59			75						
4			.81			75						
4-1			.22			75						
2			.44			75						
3			.59		35.012	75						
4			.89			75						
			.7121			75						

24.603 Hg

Plant CORR5 Date 10-14-92

Location GOLDEN

Operator MSJH

Run Number 4 Pilot Tube Coefficient .84

Sample Box ID# 1.683 Meter Box ID# 1.84

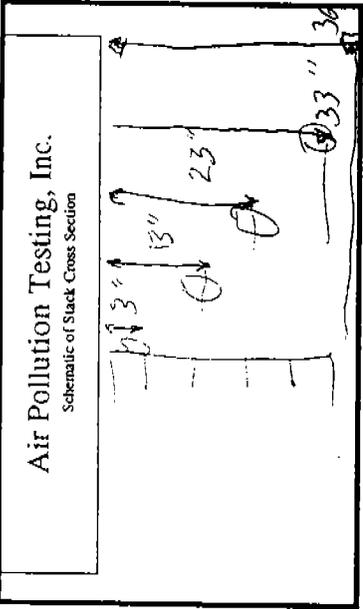
Meter ΔH@ 1.683 C Factor 1

Pre-Test Pilot Leak Check

Pre-Test Pump Leak Check

Post-Test Pilot Leak Check

Post-Test Pump Leak Check



CO<sub>2</sub> (%) 0.0 O<sub>2</sub> (%) 20.9

Assumed Moisture (%) 1 Barometric Pressure (inbar) 833

Ambient Temperature (oF) 75 Probe Material SS

Probe Length (ft) 4 Filter Temperature (oF) 1

Probe Temperature (oF) 1 Moisture (grams) 8.0

Nozzle Diameter (in) 1 Start Time 1:03

Static Pressure (in H<sub>2</sub>O) 0.3 Stop Time 1:04

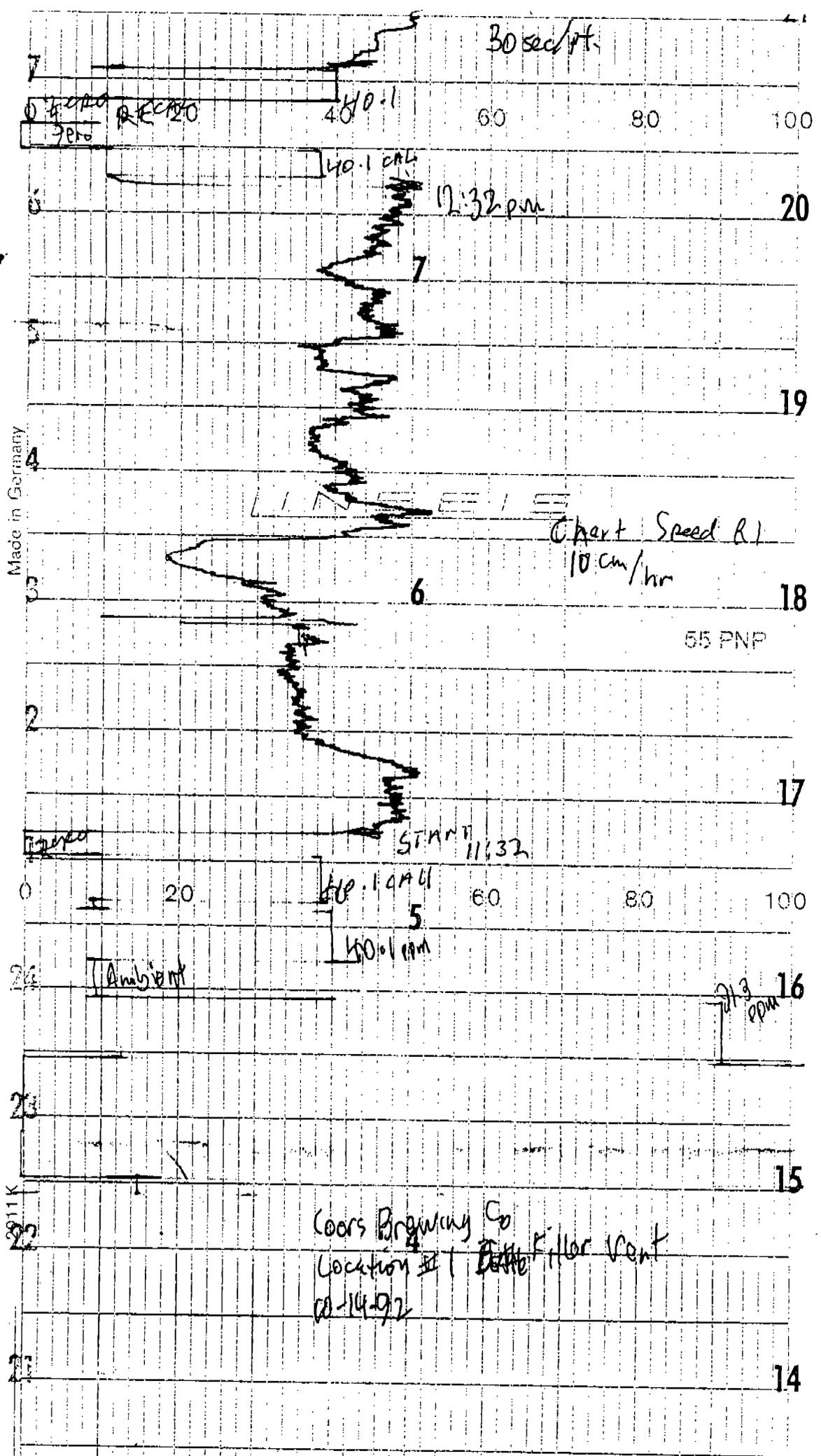
Filter ID# 1-4

Traverse Point	Sampling Time (minutes)	Vacuum (in Hg)	Velocity Head (in H <sub>2</sub> O)	Pressure Differential (in H <sub>2</sub> O)	Gas Volume (ft <sup>3</sup> ) Initial Volume	Stack Temp. (oF)	Probe Temp. (oF)	Filter Temp. (oF)	Inlet (oF) Gas Temp.	Outlet (oF) Gas Temp.	Condenser Temp. (oF)	Notes
1-1	10	3	.23		<del>444</del> 515	74			81	81		no. 1274 < 1 ml. + 7g Can Vent R2
1-2	20	2	.38		467.035	75			89	84		
1-3	30	2	.33		474.032	75			99	86		
1-4			.36		(34.517)	75						
2-1			.78			75						
2-2			.62			75						
2-3			.64			75						
2-4			.72			75						
3-1			.37			75						
3-2			.63			75						
3-3			.76			75						
3-4			.79			75						
4-1			.17			75						
4-2			.27			75						
4-3			.56			75						
4-4			.82			75						
												(87)

(7002)

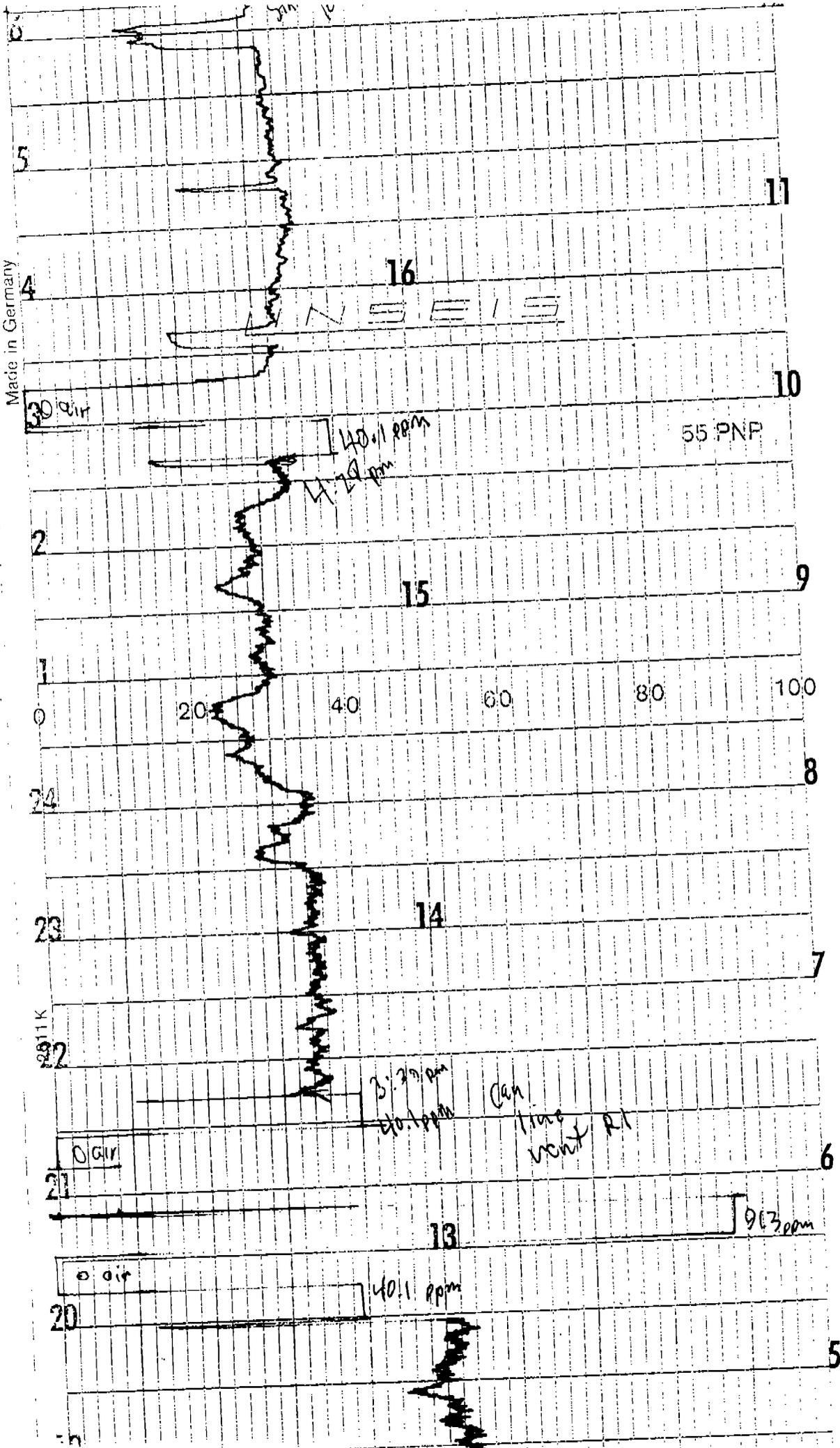
75







Made in Germany

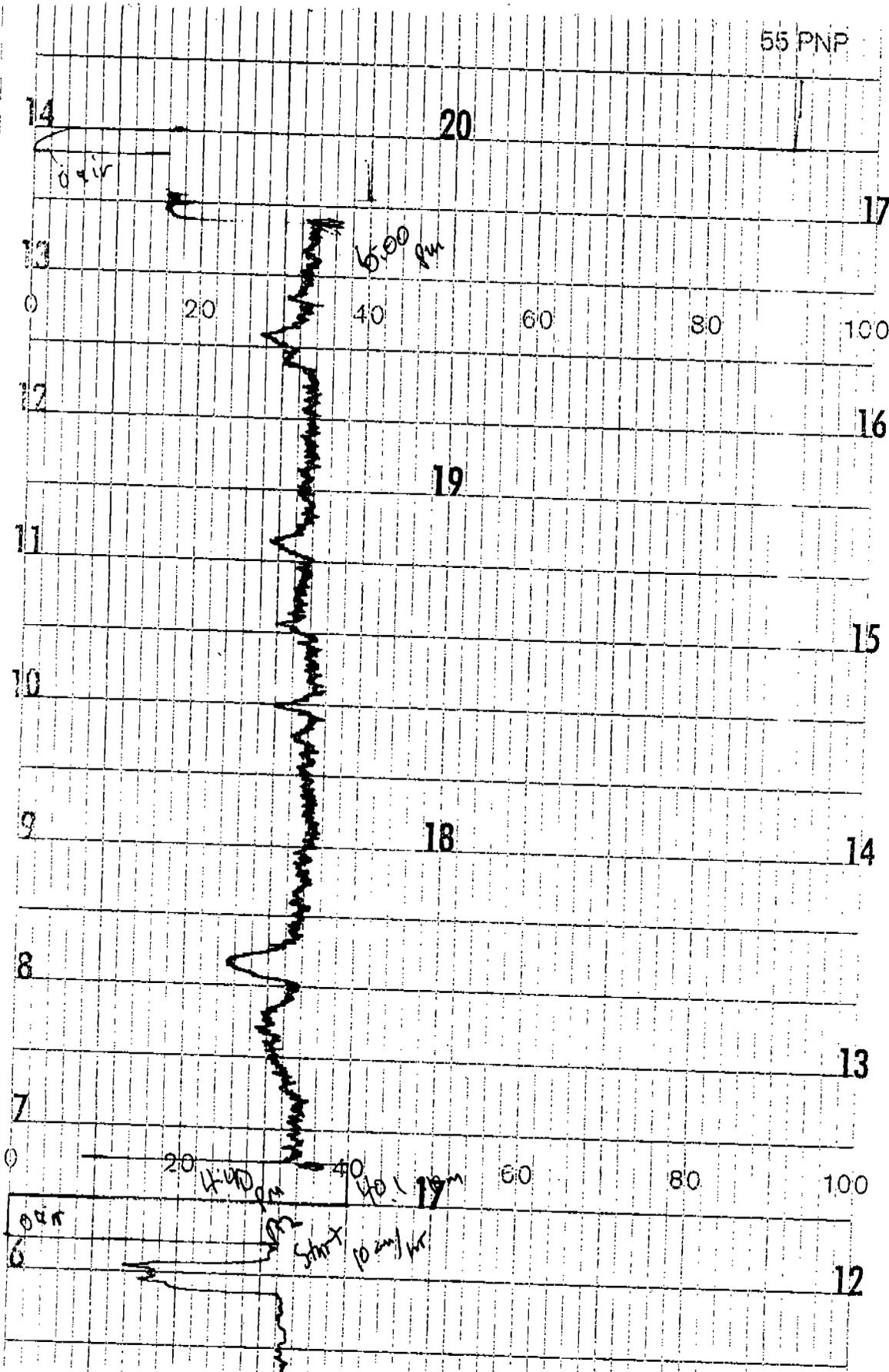


35  
30  
25  
20  
15  
10  
5  
0

0  
20  
40  
60  
80  
100

16  
INSEIS  
10  
30 air  
40.1 ppm  
11.2 ppm  
55 PNP  
2  
15  
9  
1  
7  
8  
23  
14  
7  
22  
6  
21  
0 air  
Can  
Time  
Vent  
R1  
913 ppm  
20  
40.1 ppm  
5

55 PNP



**Appendix 3**  
**Calibration Certificates**



# Scott Specialty Gases, Inc.

## E. P. A. PROTOCOL CERTIFICATE OF ANALYSIS

Shipped from:  
 Scott Specialty Gases  
 Route 611  
 Plumsteadville, PA 18949  
 Purchase order :  
 91047

Shipped to:  
 AIR POLLUTION TESTING INC  
 ATTN: PO#91047  
 4535 W 68TH AVE  
 WESTMINSTER, CO 80030

Project No 0134629

Certified per E.P.A. Protocol # 1 Procedure #G1 Section # 3.0.4  
 Certified accuracy +/- 1 % NIST Traceable

Cylinder number	ALM019712	Cylinder pressure	Date of assay:	1/23/92
		2000 psig.		
Component		Certified concentration	Expiration date:	7/23/93
PROPANE		91.3 ppm		
NITROGEN		Balance		

Standard Type	GMIS	Analyzer Make	: VARIAN
Concentration	98.21 ppm	Model	: VA3300
Cylinder #	CAL4282	Serial number	: 7945
		Analytical principle	: FID
		Date of calibration	: 1/23/92

Raw data units:	AREA	:	:	Concentration	:
		:	:	of Customer	:
		:	:	Cylinder	:
Analysis	1/23/92	:	:		:
		:	:		:
Z1=0.00	R1=432474	T1=402119	:	91.3 ppm	:
R2=432431	Z2=0.00	T2=402018	:	91.3 ppm	:
Z3=0.00	T3=402149	R3=432116	:	91.4 ppm	:
			:		:
			:		:
			:		:
			:		:
			:		:
			:		:

Analyst Paul White

Approved by Mark S. Sirinides/Ted Neeme  
 Mark S. Sirinides/Ted Neeme



# Scott Specialty Gases, Inc.

## E. P. A. PROTOCOL CERTIFICATE OF ANALYSIS

Shipped from:  
 Scott Specialty Gases  
 Route 611  
 Plumsteadville, PA 18949  
 Purchase order :  
 91047

Shipped to:  
 AIR POLLUTION TESTING INC  
 ATTN: PO#91047  
 4535 W 68TH AVE  
 WESTMINSTER, CO 80030

Project No 0134629

Certified per E.P.A. Protocol # 1 Procedure #G1 Section # 3.0.4  
 Certified accuracy +/- 1 % NIST Traceable

Cylinder number	ALM016822	Cylinder pressure	Date of assay:	1/23/92
		2000 psig.		
Component		Certified concentration	Expiration date:	7/23/93
PROPANE		40.1 ppm		
NITROGEN		Balance		

Standard		Analyzer	
Type	GMIS	Make	: VARIAN
Concentration	98.21 ppm	Model	: VA3300
Cylinder #	CAL4282	Serial number	: 7945
		Analytical principle	: FID
		Date of calibration	: 1/23/92

Raw data units:	AREA	:	:	Concentration	:
		:	:	of Customer	:
		:	:	Cylinder	:
Analysis	1/23/92	:	:		:
		:	:		:
Z1=0.00	R1=433693	T1=176863	:	40.1	ppm
R2=432885	Z2=0.00	T2=177019	:	40.2	ppm
Z3=0.00	T3=176482	R3=432460	:	40.1	ppm
			:		
			:		
			:		
			:		
			:		

Analyst Paul White Approved by Mark S. Sirinides/Ted Neeme  
 Mark S. Sirinides/Ted Neeme

**Appendix 4  
Diagrams**

## Diagrams

The following diagrams detail the duct dimensions and sampling points.

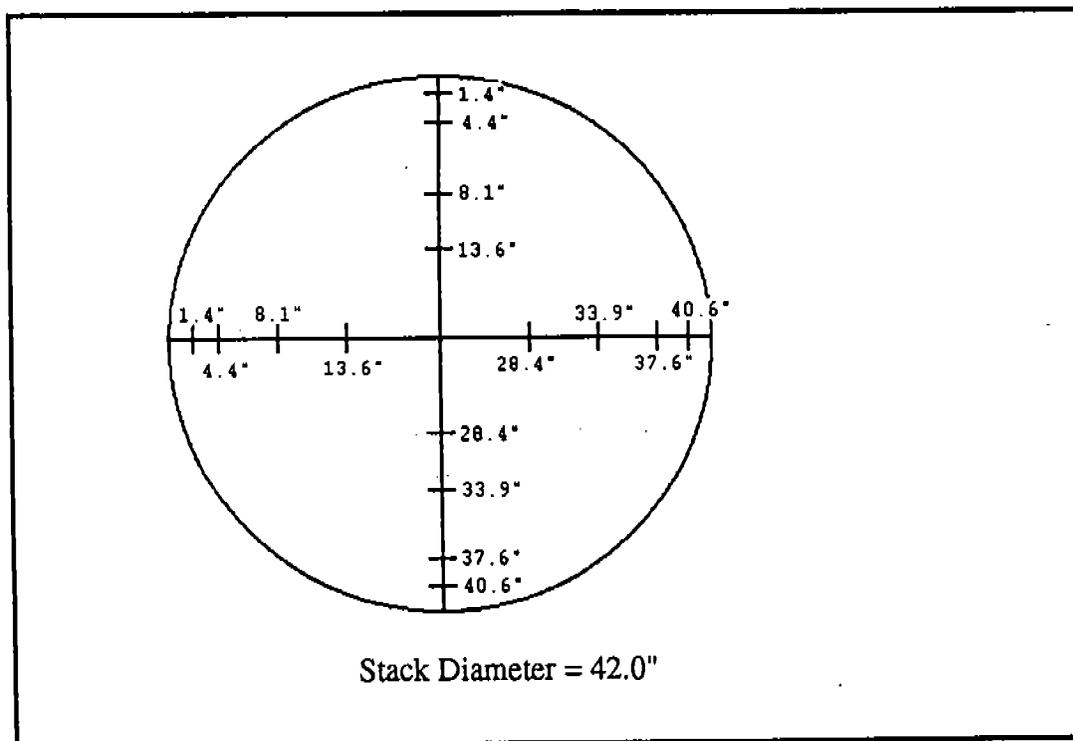


Diagram 1 - Bottle Filler Vent Cross-Section and Sampling Points

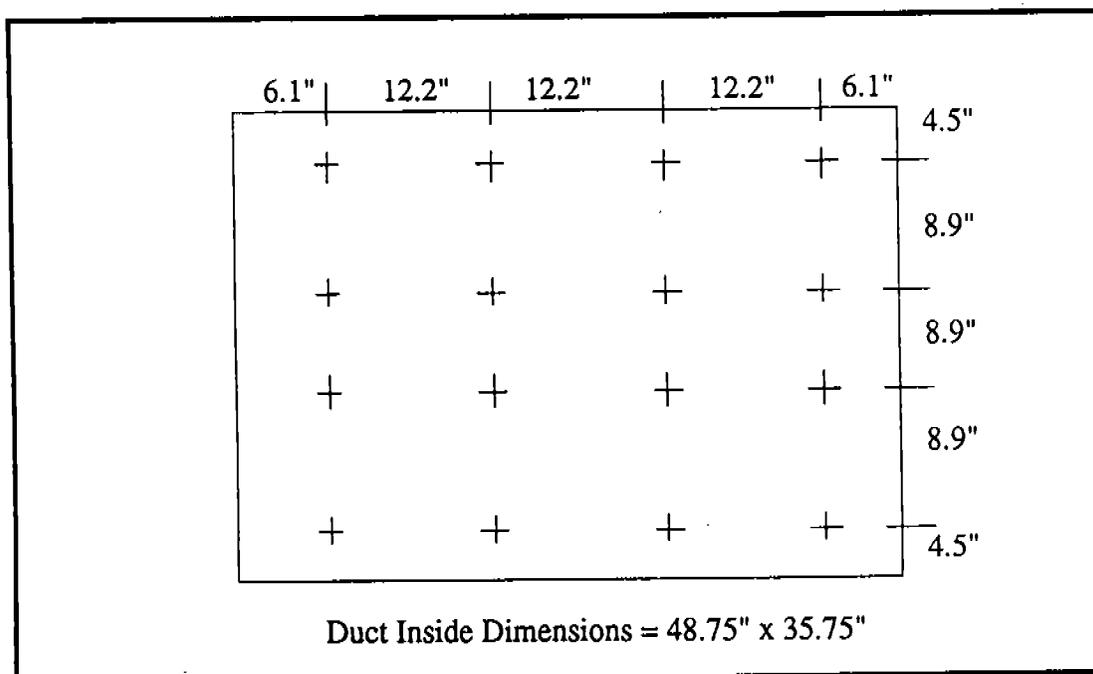


Diagram 2 - Can Filler Vent Cross-Section and Sampling Points

**Appendix 5**  
**Process Data**

## M E M O R A N D U M

OCTOBER 15, 1992

TO: TOM BUZZ

FROM: MIKE MURPHY

SUBJECT: BARRELAGES DURING PACKAGING STACK TESTING

The following is a listing of the number of cases/barrels produced during the air emissions stack re-testing on October 14, 1992:

## BOTTLE FILLER ROOM VENTS

11:30-12:30	-	5150 cs. (12 oz.) 1500 cs. (32 oz.)	=>	519 bbls.
13:30-14:30	-	4200 cs. (12 oz.) 1600 cs. (32 oz.)	=>	605 bbls.
Total cs/bbls.	-	11350 cs. (12 oz.) 3100 cs. (32 oz.)	=>	1124 bbls.
Average	-	5675 cs. (12 oz.) 1550 cs. (32 oz.)	=>	562 bbls.

## CAN FILLER ROOM VENTS

15:30-16:30	-	14150 cs. (12 oz.) 2250 cs. (16 oz.)	=>	1245 bbls.
17:00-18:00	-	13570 cs. (12 oz.) 2300 cs. (16 oz.)	=>	1108 bbls.
Total cs/bbls.	-	27720 cs. (12 oz.) 4550 cs. (16 oz.)	=>	2353 bbls.
Average	-	13860 cs. (12 oz.) 2275 cs. (16 oz.)	=>	1177 bbls.

NOTE: All barrelage figures represent the total for both package types produced during the times listed.

Conversion factors for cases to barrels are:

12 oz. (cans or btls.)	-	(# cs. * .07258)
16 oz. cans	-	(# cs. * .09677)
32 oz. btls.	-	(# cs. * .09677)