

Note: This is a reference cited in AP 42, *Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at [www.epa.gov/ttn/chief/ap42/](http://www.epa.gov/ttn/chief/ap42/)

The file name refers to the reference number, the AP42 chapter and section. The file name "ref02\_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

## **Background Report Reference**

**AP-42 Section Number:** 9.13.2

**Background Chapter:** 4

**Reference Number:** 3

**Title:** Stack Sampling Report for General  
Foods Corporation, Maxwell House  
Division, Hoboken, NJ, on Rotoclone  
Inlet and Outlet

Recon Systems, Inc.

Recon Systems, Inc.

September 1987

# RECON SYSTEMS, INC.

Route 202 North, P.O. Box 460  
Three Bridges, N.J. 08887  
201-782-5900

New England 617-752-4217      Pennsylvania 215-433-5511

AP-42 Section 9.13.2  
Reference         
Report Sect. 4  
Reference 3

## STACK SAMPLING REPORT FOR

General Foods Corporation  
Maxwell House Division  
Hoboken, New Jersey  
on Rotoclone Inlet and Outlet

### INTRODUCTION

The above referenced stacks were sampled for total particulate emissions and percent efficiency on September 9, 1987. This report contains the following information.

|                                      | <u>PAGE</u> |
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ENGINEERING, CONSULTING, LABORATORY,  
PILOT PLANT, PLANT TEST SERVICES

POLLUTION CONTROL, WASTE DISPOSAL  
RESOURCE RECOVERY, CHEMICAL PROCESS SYSTEMS

SUMMARY

The following results were obtained:

INLET

|         |           |           |           |
|---------|-----------|-----------|-----------|
| Run No. | 1         | 2         | 3         |
| Date    | 9/9/87    | 9/9/87    | 9/9/87    |
| Time    | 1116-1229 | 1346-1503 | 1541-1700 |

EMISSIONS DATA

|                     |        |        |        |
|---------------------|--------|--------|--------|
| <u>Particulates</u> |        |        |        |
| Pounds/hour         | 0.35 ✓ | 0.11 ✓ | 0.24 ✓ |
| Grains/dscf         | 0.0123 | 0.0038 | 0.0077 |
| Grains/scf          | 0.0119 | 0.0037 | 0.0075 |

OUTLET

|         |           |           |           |
|---------|-----------|-----------|-----------|
| Run No. | 1         | 2         | 3         |
| Date    | 9/9/87    | 9/9/87    | 9/9/87    |
| Time    | 1115-1230 | 1345-1459 | 1540-1704 |

EMISSIONS DATA

|                     |         |         |         |
|---------------------|---------|---------|---------|
| <u>Particulates</u> |         |         |         |
| Pounds/hour         | 0.017 ✓ | 0.014 ✓ | 0.014 ✓ |
| Grains/dscf         | 0.0006  | 0.0005  | 0.0005  |
| Grains/scf          | 0.0006  | 0.0005  | 0.0005  |

UNIT EFFICIENCY, %

95

87

94

Samples from this project will be retained for sixty days from the date of this report unless otherwise directed.

PERSONNEL AND CERTIFICATIONS

Field sampling on this project was performed by:

|                |              |
|----------------|--------------|
| P. F. Marshall | T. F. Mattei |
| C. D. Ruff     | J. D. Kirby  |

Laboratory work on this project was performed by:

P. F. Marshall

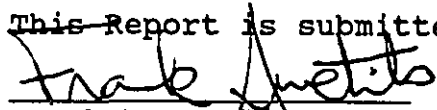
Calculations and report preparation were by:

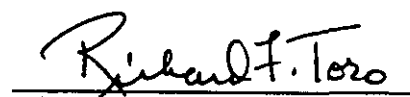
P. F. Marshall

The testing was observed by:

|               |               |
|---------------|---------------|
| Tom Brown     | NJDEP         |
| Beth Rossi    | NJDEP         |
| Ernie Lasalle | General Foods |

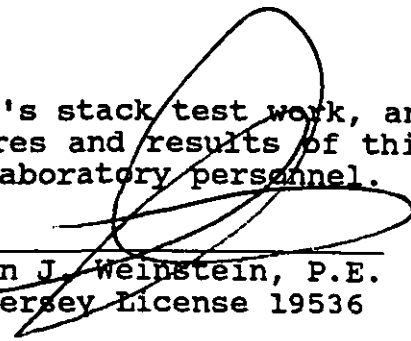
This Report is submitted by:

  
Frank W. Swettis  
Manager, Air Testing

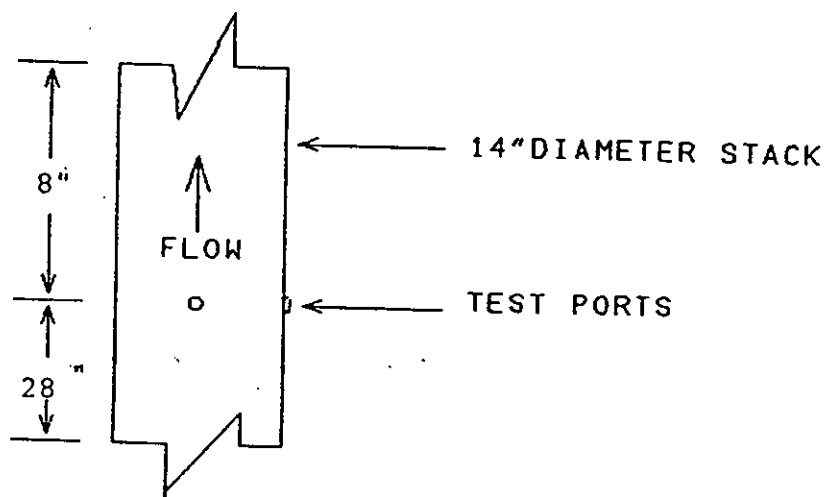
  
Richard F. Toro, M.Ch.E.  
Executive Vice President

Professional Engineer Certification

I am in responsible charge of RECON's stack test work, and have discussed and reviewed the procedures and results of this set of tests with the relevant field and laboratory personnel.

  
Norman J. Weinstein, P.E.  
New Jersey License 19536

# GENERAL FOODS ROTOCLONE OUTLET



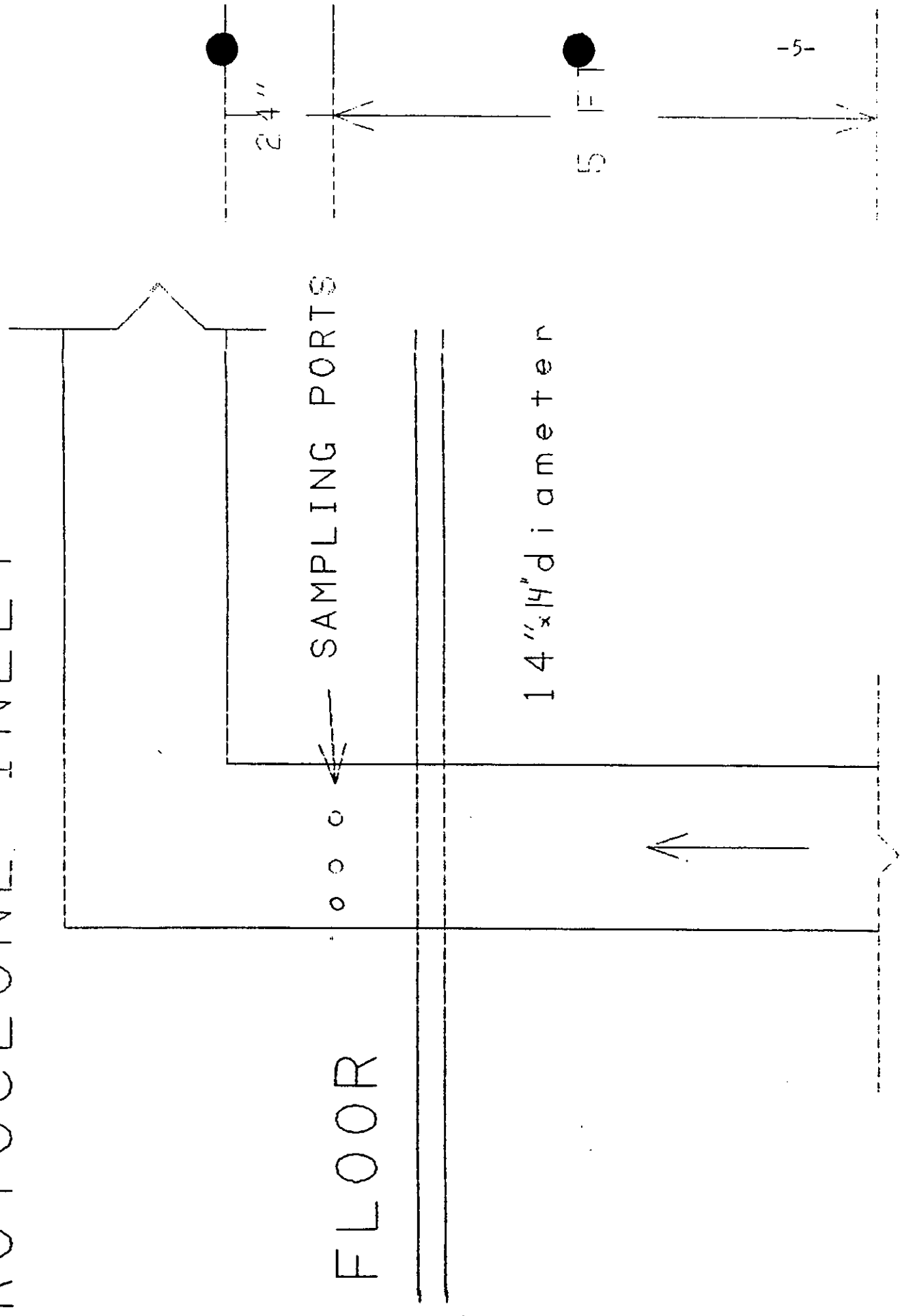
## EPA DISTANCES

DISTANCE "A" = 2

DISTANCE "B" = 0.57

# GENERAL FOODS

## ROTOCLONE INLET



VELOCITY AND FLOW RATE DATA - Inlet

|                                            |              |           |           |
|--------------------------------------------|--------------|-----------|-----------|
| Sample No.                                 | 1            | 2         | 3         |
| Date                                       | 9/9/87 ----- |           |           |
| Time                                       | 1116-1229    | 1346-1503 | 1551-1700 |
| Stack Diameter (in)                        | 14 -----     |           |           |
| Stack Cross<br>Section (sq ft)             | 1.07 -----   |           |           |
| Barometric Pressure<br>("Hg)               | 29.90 -----  |           |           |
| Average Stack<br>Temperature (°F)          | 81           | 81        | 83        |
| Stack Pressure<br>("H <sub>2</sub> O-gage) | -2.1         | -2.0      | -2.0      |
| Moisture (% vol)                           | 2.4          | 2.4       | 3.2       |
| Average Velocity<br>(ft/sec)               | 53.86        | 55.17     | 59.24     |
| Actual Flow Rate<br>(acfm)                 | 3460         | 3540      | 3800      |
| Standard Flow Rate<br>(scfm)               | 3370         | 3440      | 3690      |
| Dry Standard Flow<br>Rate (dscfm)          | 3290         | 3350      | 3570      |

Standard Conditions are 70°F, 29.92 "Hg.

VELOCITY AND FLOW RATE DATA - Outlet

|                                            |              |           |           |
|--------------------------------------------|--------------|-----------|-----------|
| Sample No.                                 | 1            | 2         | 3         |
| Date                                       | 9/9/87 ----- |           |           |
| Time                                       | 1115-1239    | 1345-1459 | 1540-1704 |
| Stack Diameter (in)                        | 14 -----     |           |           |
| Stack Cross<br>Section (sq ft)             | 1.07 -----   |           |           |
| Barometric Pressure<br>("Hg)               | 29.90 -----  |           |           |
| Average Stack<br>Temperature (°F)          | 80           | 80        | 81        |
| Stack Pressure<br>("H <sub>2</sub> O-gage) | 1.4          | 1.3       | 1.3       |
| Moisture (% vol)                           | 2.9          | 2.8       | 3.0       |
| Average Velocity<br>(ft/sec)               | 55.93        | 57.23     | 56.81     |
| Actual Flow Rate<br>(acfm)                 | 3590         | 3670      | 3650      |
| Standard Flow Rate<br>(scfm)               | 3540         | 3610      | 3580      |
| Dry Standard Flow<br>Rate (dscfm)          | 3430         | 3510      | 3470      |

Standard Conditions are 70°F, 29.92 "Hg.

CYCLONIC FLOW CHECK

| <u>INLET</u> |              |                           |
|--------------|--------------|---------------------------|
| <u>Port</u>  | <u>Point</u> | <u>Angle</u> <sup>o</sup> |
| A            | 1            | 6                         |
|              | 2            | 8                         |
|              | 3            | 8                         |
|              | 4            | 7                         |
|              | 5            | 4                         |
|              | 6            | 5                         |
|              | 7            | 9                         |
|              | 8            | 12                        |
| B            | 1            | 8                         |
|              | 2            | 10                        |
|              | 3            | 12                        |
|              | 4            | 12                        |
|              | 5            | 9                         |
|              | 6            | 8                         |
|              | 7            | 8                         |
|              | 8            | 10                        |
| C            | 1            | 10                        |
|              | 2            | 12                        |
|              | 3            | 11                        |
|              | 4            | 11                        |
|              | 5            | 9                         |
|              | 6            | 9                         |
|              | 7            | 8                         |
|              | 8            | <u>10</u>                 |

Avg 9.0<sup>o</sup>

| <u>OUTLET</u> |              |                           |
|---------------|--------------|---------------------------|
| <u>Port</u>   | <u>Point</u> | <u>Angle</u> <sup>o</sup> |
| A             | 1            | 14                        |
|               | 2            | 13                        |
|               | 3            | 13                        |
|               | 4            | 10                        |
|               | 5            | 0                         |
|               | 6            | 2                         |
|               | 7            | 8                         |
|               | 8            | 4                         |
|               | 9            | 1                         |
|               | 10           | 6                         |
|               | 11           | 0                         |
|               | 12           | 1                         |
| B             | 1            | 18                        |
|               | 2            | 15                        |
|               | 3            | 13                        |
|               | 4            | 14                        |
|               | 5            | 13                        |
|               | 6            | 3                         |
|               | 7            | 10                        |
|               | 8            | 5                         |
|               | 9            | 4                         |
|               | 10           | 1                         |
|               | 11           | 5                         |
|               | 12           | <u>8</u>                  |

Avg. 7.5<sup>o</sup>

STACK GAS COMPOSITION - Inlet

|            |              |           |           |
|------------|--------------|-----------|-----------|
| Sample No. | 1            | 2         | 3         |
| Date       | 9/9/87 ----- |           |           |
| Time       | 1116-1229    | 1346-1503 | 1551-1700 |

% By Volume  
(Dry Basis)

ONSITE FYRITE

|                                |    |    |    |
|--------------------------------|----|----|----|
| CO <sub>2</sub>                | 0  | 0  | 0  |
| O <sub>2</sub>                 | 21 | 21 | 21 |
| N <sub>2</sub> (By Difference) | 79 | 79 | 79 |

LAB ORSAT

|                                |    |    |    |
|--------------------------------|----|----|----|
| CO <sub>2</sub>                | 0  | 0  | 0  |
| O <sub>2</sub>                 | 21 | 21 | 21 |
| N <sub>2</sub> (By Difference) | 79 | 79 | 79 |

STACK GAS COMPOSITION - Outlet

|            |              |           |           |
|------------|--------------|-----------|-----------|
| Sample No. | 1            | 2         | 3         |
| Date       | 9/9/87 ----- |           |           |
| Time       | 1115-1230    | 1345-1459 | 1540-1704 |

|                                |    |                            |    |
|--------------------------------|----|----------------------------|----|
|                                |    | % By Volume<br>(Dry Basis) |    |
| <u>ONSITE FYRITE</u>           |    |                            |    |
| CO <sub>2</sub>                | 0  | 0                          | 0  |
| O <sub>2</sub>                 | 21 | 21                         | 21 |
| N <sub>2</sub> (By Difference) | 79 | 79                         | 79 |

LAB ORSAT

|                                |    |    |    |
|--------------------------------|----|----|----|
| CO <sub>2</sub>                | 0  | 0  | 0  |
| O <sub>2</sub>                 | 21 | 21 | 21 |
| N <sub>2</sub> (By Difference) | 79 | 79 | 79 |

PARTICULATE EMISSIONS - Inlet

|            |           |           |           |
|------------|-----------|-----------|-----------|
| Sample No. | 1         | 2         | 3         |
| Date       | 9/9/87    | -----     | -----     |
| Time       | 1116-1229 | 1346-1503 | 1551-1700 |

Sampling Data

|                             |       |       |       |
|-----------------------------|-------|-------|-------|
| Nominal<br>Nozzle Size (in) | 3/16  | ----- | ----- |
| No. of Sampling<br>Points   | 24    | ----- | ----- |
| Sampling Time (min)         | 72    | ----- | ----- |
| Sample Volume (dscf)        | 41.97 | 42.40 | 45.27 |
| % Isokinetic                | 92    | 91    | 91    |

Emissions DataParticulates

|             |        |        |        |
|-------------|--------|--------|--------|
| Grains/dscf | 0.0123 | 0.0038 | 0.0077 |
| Grains/scf  | 0.0119 | 0.0037 | 0.0075 |
| Pounds/hour | 0.35   | 0.11   | 0.24   |

PARTICULATE EMISSIONS - Outlet

|            |              |           |           |
|------------|--------------|-----------|-----------|
| Sample No. | 1            | 2         | 3         |
| Date       | 9/9/87 ----- |           |           |
| Time       | 1115-1230    | 1345-1459 | 1540-1704 |

Sampling Data

|                             |            |       |       |
|-----------------------------|------------|-------|-------|
| Nominal<br>Nozzle Size (in) | 3/16 ----- |       |       |
| No. of Sampling<br>Points   | 24 -----   |       |       |
| Sampling Time (min)         | 72 -----   |       |       |
| Sample Volume (dscf)        | 43.46      | 44.98 | 44.47 |
| % Isokinetic                | 94         | 95    | 94    |

Emissions Data

|                                    |        |        |        |
|------------------------------------|--------|--------|--------|
| <u>Particulates</u><br>Grains/dscf | 0.0006 | 0.0005 | 0.0005 |
| Grains/scf                         | 0.0006 | 0.0005 | 0.0005 |
| Pounds/hour                        | 0.017  | 0.014  | 0.014  |
| <u>Unit Efficiency, %</u>          | 95     | 87     | 94     |

PROCESS INFORMATION

Process information was not supplied to RECON.

ALLOWABLE EMISSIONS

The following allowable emissions are based on our understanding of the applicable regulatory rules and regulations. Since we are not always privy to the situation, these should not be accepted without confirmation from relevant sources.

| <u>Particulate</u>                       | <u>Reference</u> | <u>Allowable</u> |
|------------------------------------------|------------------|------------------|
| Federal Regulations                      | _____            | _____            |
| State Regulations                        | _____            | _____            |
| State Permit                             | _____            | _____            |
| <u>Sulfur Dioxide</u>                    |                  |                  |
| Federal Regulations                      | _____            | _____            |
| State Regulations                        | _____            | _____            |
| State Permit                             | _____            | _____            |
| <u>Sulfur Trioxide and Sulfuric Acid</u> |                  |                  |
| Federal Regulations                      | _____            | _____            |
| State Regulations                        | _____            | _____            |
| State Permit                             | _____            | _____            |
| <u>Nitrogen Oxides</u>                   |                  |                  |
| Federal Regulations                      | _____            | _____            |
| State Regulations                        | _____            | _____            |
| State Permit                             | _____            | _____            |
| <u>Hydrocarbon (VOS, VOC)</u>            |                  |                  |
| Federal Regulations                      | _____            | _____            |
| State Regulations                        | _____            | _____            |
| State Permit                             | _____            | _____            |
| <u>Other:</u> _____                      |                  |                  |
| Federal Regulations                      | _____            | _____            |
| State Regulations                        | _____            | _____            |
| State Permit                             | _____            | _____            |

  X   We do not have sufficient information to determine allowable emissions.

# RECON SYSTEMS, INC.

-15-

Route 202 North, P.O. Box 460  
Three Bridges, N.J. 08887  
201-782-5900

New England 617-752-4217      Pennsylvania 215-433-5511

## STACK TEST PROTOCOL SUBMITTAL

NEW JERSEY DEPARTMENT OF  
ENVIRONMENTAL PROTECTION  
Technical Services Section  
380 Scotch Road  
W. Trenton, NJ 08628

RE: General Foods Corporation  
Maxwell House Division  
1125 Hudson Street  
Hoboken, NJ 07030

ATTN: Edward Choromanski

Contact: Ernie LaSalle  
Phone No. 201-420-3731  
RECON Project No. 0554

This protocol is submitted for stack testing planned by RECON SYSTEMS, INC. for the above referenced client.

Source to be tested      Rotoclone Outlet, Rotoclone Inlet  
ID No.      059

Applicable permit and/or  
certificate numbers      078004

Approximate Date of Testing      September 9, 1987

### For Isokinetic Testing or Velocity Measurements, if any Rotoclone Outlet

Stack diameter or dimensions      14"  
Nearest upstream disturbances      20"  
Nearest downstream disturbances      14"  
EPA Distance "A" 1.42      EPA Distance "B"      1.00  
Proposed number of sampling points 24  
Proposed time per sampling point      3 minutes  
Proposed total stack gas sample size -34.00 dry standard ft<sup>3</sup>

### Rotoclone Inlet

Stack diameter or dimensions      14" x 14"  
Nearest upstream disturbances      5'  
Nearest downstream disturbances      24"  
EPA Distance "A" 1.7      EPA Distance "B"      4.3  
Proposed number of sampling points 24  
Proposed time per sampling point      3 minutes  
Proposed total stack gas sample size -34.00 dry standard ft<sup>3</sup>

All measurements to field verified

ENGINEERING, CONSULTING, LABORATORY,  
PILOT PLANT, PLANT TEST SERVICES

POLLUTION CONTROL, WASTE DISPOSAL  
RESOURCE RECOVERY, CHEMICAL PROCESS SYSTEMS

### Source Operation Record Keeping

Responsibility of   A   Owner   B   RECON

  A   Production rate  
  A   Fuel usage  
       Incineration feed rate  
       Steam production  
  A   Operating parameters (temperatures, pressures, flows, etc.)  
       Other

### Sampling Program

Three (3) compliance tests will be run for total particulates, flow rate, temperature, O<sub>2</sub>, CO<sub>2</sub> and N<sub>2</sub> (by difference) utilizing New Jersey Method No. 1. Temperatures of the stack probe, filter inlet, filter box, and filter outlet will be recorded. Impingers Nos. 1 and 2 will have 100 mls each of distilled water. Impinger no. 3 will be empty. Impinger no. 4 will contain 200 gms silica gel.

### Analytical Program

The sample filter is dried at 105°C, cooled in a dessicator, and weighed to a constant weight. The probe wash is evaporated in a pretared beaker, dessicated and weighed to a constant weight. The impingers are weighed to determine moisture gain.

The following are attached if available:

1. Test procedures proposed
2. Stack diagram
3. Permits or applications
4. Process description

This protocol submitted by

*Richard F. Toro*  
Richard F. Toro  
Executive Vice President  
*Peter F. Marshall*  
Per Peter F. Marshall  
Environmental Engineer  
August 5, 1987

STACK TESTING PROCEDURES CHECKLIST

## Particulate

Emissions: ☐ US EPA 5  
☐ US EPA 17  
☒ N.J. Method 1  
☐ N.J. Method 4 (draft)  
☐ Plus impinger catch  
☐ Plus aqueous and organic impinger catch  
☐ Other \_\_\_\_\_  
 Probe Material Pyrex Glass

Velocity: ☐ Standard pitot tube and manometer  
☒ "S" pitot tube and manometer  
☐ Other: \_\_\_\_\_  
☒ Cyclonic Flow Check ☒ Yes ☐ No

Temperature: ☒ Thermocouple  
☐ Temperature gage  
☐ Process indicator

## Gas

Composition: ☒ Onsite fyrite  
☐ Grab sample and lab orsat  
☐ Integrated sample and lab orsat  
☒ Integrated and traversed sample and lab orsat  
☐ Oxygen by Infrared Industries 2200 Electrochemical Analyzer

## Particle

Sizing: ☐ Instack cascade impactor  
☐ Heated out of stack cascade impactor  
☐ Plus impinger catch  
☐ Plus aqueous and organic impinger catch

## Sulfur Oxide

Emissions: ☐ US EPA 6  
☐ US EPA 8  
☐ Sulfite Corrections Made  
☐ Controlled condensation for SO<sub>2</sub>  
☐ US EPA 6 ☐ or 8 ☐ combined with  
☐ US EPA 5 ☐ or 17 ☐ or particle sizing ☐

## Nitrogen Oxide

Emissions: ☐ US EPA 7 ☐ A, ☐ B, ☐ C, ☐ D, ☐ E  
☐ Chemiluminescent monitor  
☐ US EPA 20 (Chemiluminescent Monitor)

## Hydrogen Chloride (HCl)

Emissions: ☐ API 767-54  
☐ Cl<sup>-</sup> analysis of particulate test wet catch  
☐ Other \_\_\_\_\_

## Hydrocarbon

Emissions: ☐ N.J. Method 3  
☐ RECON Method 2  
☐ Integrated gas bag direct and lab GC  
☐ Grab sample gas bag direct and lab GC  
☐ Onsite GC direct ☐ detector  
☐ Onsite Continuous Monitor (FID)

Metal Emissions ☐ AA determination on filter and probe wash  
☐ AA determination on impinger catch

## Carbon Monoxide

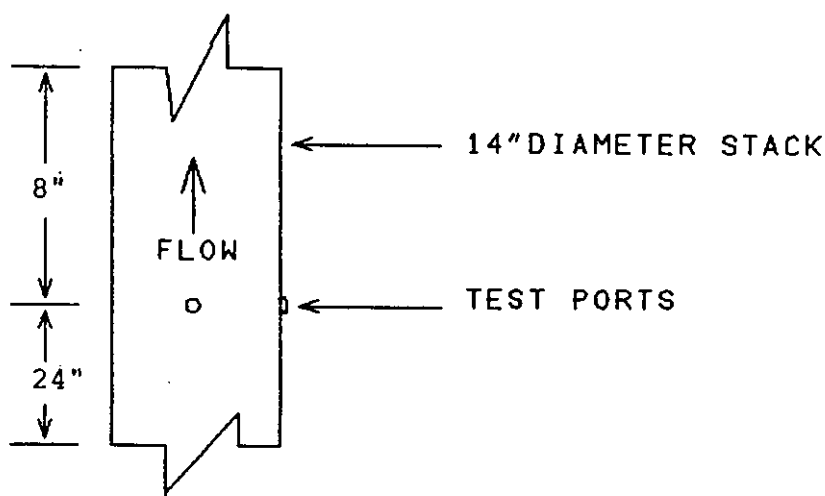
Emissions: ☐ Thermal Conductivity analysis of "Gas Composition" sample(s)  
☐ Onsite Continuous Monitor

Opacity: ☐ N.J. Method 2  
☐ U.S. EPA Method 9

Calibrations: Dry gas meters and orifice, pitot tubes, thermocouples and nozzle calibrations will be supplied with the test report unless test is unofficial.

Comments:

# GENERAL FOODS ROTOCLONE OUTLET



## EPA DISTANCES

DISTANCE "A" = 2

DISTANCE "B" = 0.57

## CYCLONIC FLOW CHECK

### PORT A

1 = 5 °  
2 = 8 °  
3 = 7 °  
4 = 6 °  
5 = 1 °  
6 = 10 °

AVG. = 6.2 °

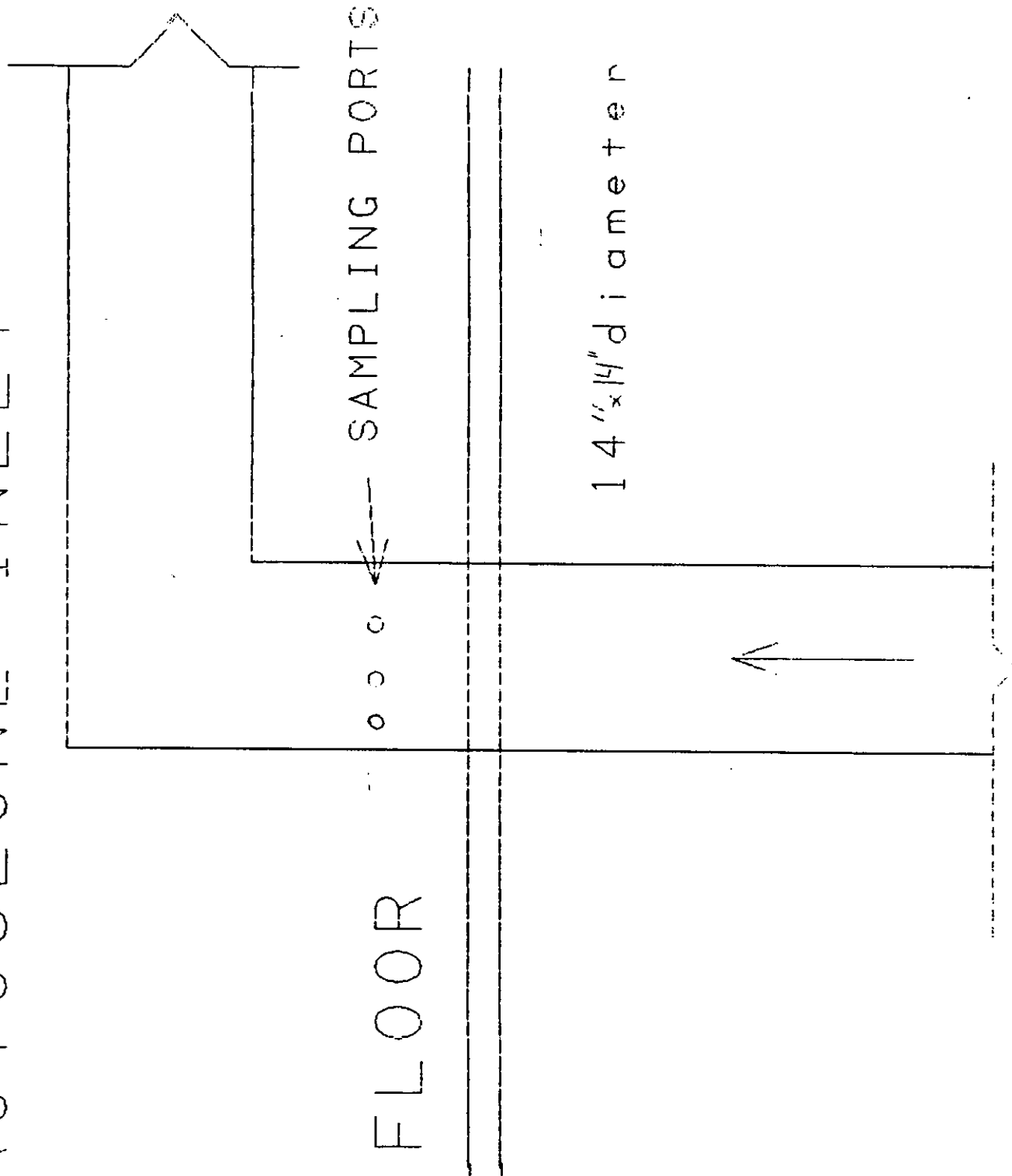
### PORT B

1 = 6 °  
2 = 5 °  
3 = 3 °  
4 = 2 °  
5 = 0 °  
6 = 7 °

AVG. = 3.8 °

# GENERAL FOODS

## ROTOCLONE INLET



FLOOR

SAMPLING PORTS

14" x 14" diameter

5 FT

24"

-19-

DIVISION OF ENVIRONMENTAL QUALITY  
AIR POLLUTION CONTROL PROGRAM  
BUREAU OF NEW SOURCE REVIEW

All Correspondence must indicate your APC PLANT ID NUMBER

Permit/Certificate Number 078004

LOG NUMBER 853866A

APC PLANT ID 10082

(Mailing Address)

GENERAL FOODS CORP.  
1125 HUDSON STREET  
HUDSON NJ 07030

(Plant Location)

MAXWELL HOUSE DIVISION  
1125 HUDSON STREET  
HUDSON

Applicant's Designation of Equipment BLDG.#10- ROTOCLONE

NJ. Stack No. 057

No. of Stacks 001

No. of Sources 01

Original Approval 03/30/87

Effective 03/30/87

Expiration 06/27/87

PERMIT TO CONSTRUCT, INSTALL OR ALTER CONTROL APPARATUS OR EQUIPMENT  
AND  
TEMPORARY CERTIFICATE TO OPERATE CONTROL APPARATUS OR EQUIPMENT

\* CONDITIONAL \*

THIS PERMIT AND TEMPORARY CERTIFICATE IS BEING ISSUED UNDER THE AUTHORITY OF CHAPTER 106, P.L. 1967 (N.J.S.A.26:26-9.2). THE TEMPORARY CERTIFICATE WILL ALLOW FOR INSPECTION AND EVALUATION TO ASSURE CONFORMANCE WITH ALL PROVISIONS OF THE NEW JERSEY ADMINISTRATIVE CODE, TITLE 7, CHAPTER 27. BASED ON THIS EVALUATION, STACK TESTS MAY BE REQUIRED IN ACCORDANCE WITH N.J.A.C. 7:27-8.4(C).

IF THE DEPARTMENT IS SOLELY RESPONSIBLE FOR BEING UNABLE TO INSPECT THIS EQUIPMENT IN OPERATION AS PERMITTED DURING THIS 90-DAY PERIOD, THIS TEMPORARY CERTIFICATE WILL BE EXTENDED AUTOMATICALLY. HOWEVER, IF YOU ARE RESPONSIBLE FOR THE DEPARTMENT'S BEING UNABLE TO INSPECT, E.G., NOT NOTIFYING THE DEPARTMENT WHEN THIS EQUIPMENT OR PROCESS IS IN OPERATION, THIS CERTIFICATE MAY NOT BE EXTENDED AND YOU WILL BE NOTIFIED BY THE DEPARTMENT THAT YOU MUST APPLY FOR AND OBTAIN AN EXTENSION AUTHORIZING YOU TO CONTINUE TO OPERATE THE EQUIPMENT. THE DEPARTMENT RESERVES THE RIGHT TO WITHHOLD ANY EXTENSION OF THIS TEMPORARY CERTIFICATE, IN WHICH EVENT YOU WILL BE NOTIFIED THAT YOU MUST APPLY FOR AND OBTAIN AN EXTENSION AUTHORIZING YOU TO CONTINUE TO OPERATE AFTER THE EXPIRATION DATE OF THIS CERTIFICATE.

IN ACCORDANCE WITH N.J.A.C. 7:27-6.3(D), THIS PERMIT AND CERTIFICATE MUST BE READILY AVAILABLE FOR INSPECTION ON THE OPERATING PREMISES.

## THE FOLLOWING CONDITION(S) APPLY TO THIS PERMIT AND CERTIFICATE:

1. THE OWNER OR OPERATOR SHALL NOT CONSTRUCT, INSTALL, USE OR CAUSE TO BE USED THIS EQUIPMENT IN A MANNER WHICH WILL RESULT IN ODORS BEING DETECTABLE BY SENSE OF SMELL IN ANY AREA, EXCEPT FOR THOSE AREAS OVER WHICH THE OWNER OR OPERATOR HAS EXCLUSIVE USE OR OCCUPANCY.
2. STACK TEST REQUIRED (SEE ATTACHED).

N.J. Department of Environmental Protection  
Division of Environmental Quality  
CN-027, 401 East State Street  
Trenton, New Jersey 08625

Approved by

Chief

Bureau of New Source Review

YOU MUST CONDUCT A STACK TESTS IN ACCORDANCE WITH N.J.A.C. 7:27-8.4(c) WITHIN 90 DAYS OF START-UP OF THIS EQUIPMENT.

STACK TEST FOR: PARTICULATES & % CONTROL

- A. SUBMIT FOR REVIEW AND APPROVAL, AT LEAST 30 DAYS PRIOR TO TESTING, A DETAILED DESCRIPTION OF SAMPLING LOCATIONS, SAMPLING EQUIPMENT, AND ANALYTICAL PROCEDURES FOR SUCH TESTS TO SUPERVISOR, TECHNICAL REVIEW, BUREAU OF TECHNICAL SERVICES, CN 411, 380 SCOTCH RD. TRENTON, N.J. 08618. PHONE 609-530-4041
- B. NOTIFY THE METROPOLITAN REGIONAL OFFICE AT 201-669-3935 AT LEAST 7 DAYS PRIOR TO THE ACTUAL TESTING.
- C. SUBMIT TWO (2) COPIES OF THE TEST RESULTS TO THE TECHNICAL SERVICES SECTION WITHIN 30 DAYS OF THE COMPLETION OF THE STACK TEST. THE TEST RESULTS MUST BE CERTIFIED BY A NEW JERSEY LICENSED PROFESSIONAL ENGINEER OR BY A CERTIFIED INDUSTRIAL HYGIENIST.



88 AUG 1

**State of New Jersey**  
**DEPARTMENT OF ENVIRONMENTAL PROTECTION**  
**DIVISION OF ENVIRONMENTAL QUALITY**  
 CN 027, TRENTON, N.J. 08625

JORGE H. BERKOWITZ, Ph.D.  
 DIRECTOR

(609) 292-5383

August 12, 1987

Mr. Peter F. Marshall  
 Senior Environmental Specialist  
 Recon Systems, Inc.  
 P.O. Box 460  
 Three Bridges, New Jersey 08887

Dear Mr. Marshall:

We have received the sampling and analytical protocol your company has submitted for the proposed emission tests at General Foods Corporation, Maxwell House Division located in Hoboken, New Jersey. These tests are to be conducted on the Building No. 10 - Rotoclone (NJ Stack No. 059).

Our review of the proposed procedures indicates that the outlet sampling location does not meet the minimum requirements for stacks less than 24 inches in diameter, as prescribed by USEPA Reference Method One. Unless the sampling location can be changed by incorporating temporary and/or permanent stack extensions or other similar alternatives, we will not approve the proposed protocol.

You will be required to submit details describing the changes necessary to insure the outlet sampling location will be acceptable.

A proposed sample date of September 9, 1987, was mentioned in your letter. We cannot schedule any test date until an approve protocol has been submitted.

If you have any questions, please feel free to call me at (609) 530-4041.

Sincerely,

Edward M. Choromanski  
 Supervisor/Technical Review  
 Bureau of Technical Services

# RECON SYSTEMS, INC.

-23-

Route 202 North, P.O. Box 460  
Three Bridges, N.J. 08887  
201-782-5900

New England 617-752-4217      Pennsylvania 215-433-5511

August 18, 1987

Mr. Edward M. Choromanski  
Supervisor/Technical Review  
Bureau of Technical Services  
State of New Jersey  
Department of Environmental Protection  
CN 027  
Trenton, NJ 08825

Re: General Foods Corporation  
Maxwell House Division  
NJ Stack No. 059  
Hoboken, NJ  
RECON Project No. 0554

Dear Mr. Choromanski:

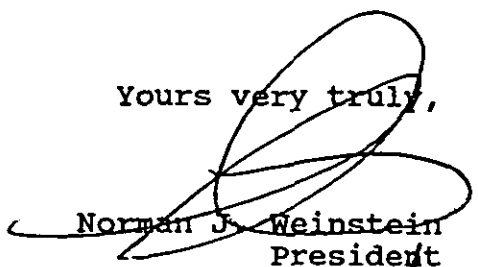
This letter is in response to your letter dated August 12, 1987 for the above mentioned project.

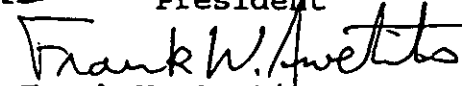
Enclosed please find revised sample location drawing for the outlet of the Rotoclone.

We would still like to keep the test scheduled for September 9, 1987.

If you have any questions, please call.

Yours very truly,

  
Norman J. Weinstein  
President

  
Frank W. Swetits  
Manager, Field Testing

FWS/cp

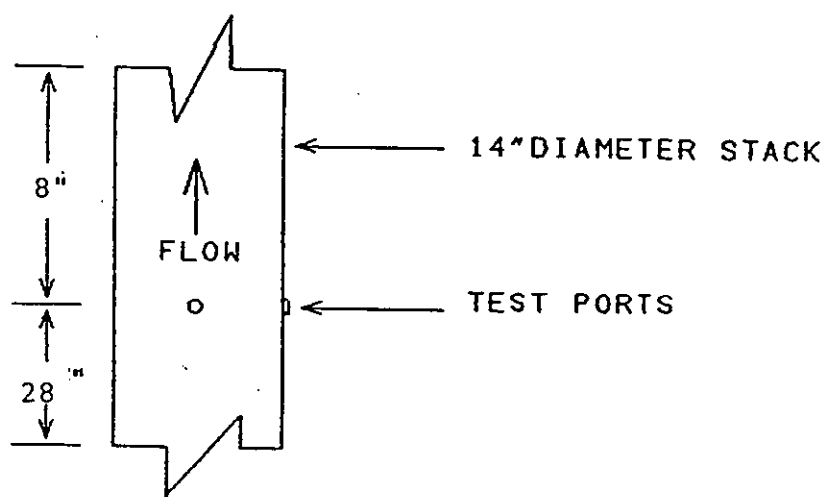
Enclosure

cc: E. LaSalle, General Foods

ENGINEERING, CONSULTING, LABORATORY.  
PILOT PLANT, PLANT TEST SERVICES

POLLUTION CONTROL, WASTE DISPOSAL  
RESOURCE RECOVERY, CHEMICAL PROCESS SYSTEMS

# GENERAL FOODS ROTOCLONE OUTLET



## EPA DISTANCES

DISTANCE "A" = 2

DISTANCE "B" = 0.57

## CYCLONIC FLOW CHECK

### PORT A

1 = 5 °  
2 = 8 °  
3 = 7 °  
4 = 6 °  
5 = 1 °  
6 = 10 °

AVG. = 6.2 °

### PORT B

1 = 6 °  
2 = 5 °  
3 = 3 °  
4 = 2 °  
5 = 0 °  
6 = 7 °

AVG. = 3.8 °

# SELECTED NOMENCLATURE

-25-

|                                |                                                                                                                       |
|--------------------------------|-----------------------------------------------------------------------------------------------------------------------|
| Time                           | = military time                                                                                                       |
| min                            | = minutes                                                                                                             |
| °F                             | = degrees Fahrenheit                                                                                                  |
| °C                             | = degrees Centigrade                                                                                                  |
| "H <sub>2</sub> O              | = inches water (pressure or vacuum)                                                                                   |
| "Hg                            | = inches mercury (pressure or vacuum)                                                                                 |
| mm Hg                          | = millimeters of mercury (pressure or vacuum)                                                                         |
| psig                           | = pounds of pressure per square inch-gage                                                                             |
| sq ft                          | = square feet                                                                                                         |
| in                             | = inches                                                                                                              |
| micron                         | = 10 <sup>-6</sup> meters                                                                                             |
| ft/sec                         | = feet per second                                                                                                     |
| ft/min                         | = feet per minute                                                                                                     |
| acfm                           | = cubic feet per minute of total gas flow at flowing conditions                                                       |
| scfm                           | = cubic feet per minute of total gas flow at 70°F, 29.92"Hg                                                           |
| dscfm                          | = dry cubic feet per minute of dry gas flow at 70°F, 29.92"Hg                                                         |
| pounds/hour                    | = pounds per hour                                                                                                     |
| pounds/hour                    | = pounds per hour                                                                                                     |
| BTU/hr                         | = British thermal units per hour                                                                                      |
| %                              | = volume per cent when referred to gases and water vapor                                                              |
|                                | = weight percent for solids, liquids                                                                                  |
| % vol                          | = volume per cent                                                                                                     |
| % wgt                          | = weight percent                                                                                                      |
| ppmv                           | = volumes of gaseous contaminants per million volumes of total gas                                                    |
| grains                         | = grams x 15.4                                                                                                        |
| ug                             | = micrograms = 10 <sup>-6</sup> grams                                                                                 |
| mg                             | = milligrams = 10 <sup>-3</sup> grams                                                                                 |
| grains/dscf                    | = grains of pollutants per cubic foot of dry stack gas at 70°F, 29.92 "Hg                                             |
| gr/dscf                        | = grains/dscf                                                                                                         |
| ug/m <sup>3</sup>              | = micrograms of pollutants per cubic meter of total stack gas at 25°C, 760 mm Hg                                      |
| mg/l                           | = milligrams/liter of liquid = ppm by weight if specific gravity of liquid = 1.0                                      |
| C                              | = elemental carbon                                                                                                    |
| CO <sub>2</sub>                | = carbon dioxide                                                                                                      |
| H                              | = elemental hydrogen                                                                                                  |
| H <sub>2</sub>                 | = molecular hydrogen                                                                                                  |
| H <sub>2</sub> O               | = water                                                                                                               |
| N                              | = elemental nitrogen                                                                                                  |
| N <sub>2</sub>                 | = molecular nitrogen                                                                                                  |
| NO <sub>x</sub>                | = NO + NO <sub>2</sub> = nitrogen oxides = nitric oxide plus nitrogen dioxide reported as equivalent nitrogen dioxide |
| S                              | = elemental sulfur                                                                                                    |
| SO <sub>2</sub>                | = sulfur dioxide                                                                                                      |
| SO <sub>3</sub>                | = sulfur trioxide                                                                                                     |
| SO <sub>4</sub>                | = sulfate                                                                                                             |
| H <sub>2</sub> SO <sub>4</sub> | = sulfuric acid                                                                                                       |
| H <sub>2</sub> S               | = hydrogen sulfide                                                                                                    |
| Cl                             | = elemental chlorine or chloride                                                                                      |
| Cl <sub>2</sub>                | = molecular chlorine                                                                                                  |
| HCl                            | = hydrogen chloride                                                                                                   |
| F                              | = elemental fluorine or fluoride                                                                                      |
| CH <sub>4</sub>                | = methane                                                                                                             |
| O                              | = elemental oxygen                                                                                                    |
| O <sub>2</sub>                 | = molecular oxygen                                                                                                    |
| A                              | = argon                                                                                                               |
| <                              | = less than; represents the minimum detectability limits                                                              |
| ≤                              | = equal to or less than                                                                                               |
| ND                             | = none detected                                                                                                       |

Front half (dry catch particulate) = particulate matter collected in/on nozzle, probe, cyclone, flask heated hose, and filter of EPA sampling train

Back Half (wet catch particulate) = material collected in impingers after filter of EPA sampling train

Organic wet catch = residue after low temperature (70°F) evaporation of ether/chloroform used to extract soluble materials from the wet catch

Aqueous wet catch = residue after high temperature (220°F) evaporation of water left after ether/chloroform extraction

Combustibles = volatiles = loss on heating @ 550°C after drying @ 100°C

Ash = residue after heating @550°C

CALIBRATION DATA

Test Equipment Calibration

Data Sheets Follow

# PITOT TUBE CALIBRATION

Pitot tube calibration number 7 Date JUNE 11, 87

Calibrated by PEM & CORNH

EFFECTIVE LENGTH 3'

## A Side Calibration

| Run No.               | $\Delta p_{std}$<br>cm H <sub>2</sub> O<br>(in. H <sub>2</sub> O) | $\Delta p_s$<br>cm H <sub>2</sub> O<br>(in. H <sub>2</sub> O) | $C_{p(s)}$ | Deviation<br>$C_{p(s)} - \bar{C}_{p(A)}$ |
|-----------------------|-------------------------------------------------------------------|---------------------------------------------------------------|------------|------------------------------------------|
| 1                     | 0.74                                                              | 1.00                                                          | 0.85       | +0.02                                    |
| 2                     | 0.29                                                              | 0.41                                                          | 0.83       | 0.00                                     |
| 3                     | 0.17                                                              | 0.25                                                          | 0.82       | -0.01                                    |
| $\bar{C}_{p(side A)}$ |                                                                   |                                                               | 0.83       | $\delta = 0.010 *$                       |

## B Side Calibration

| Run No.               | $\Delta p_{std}$<br>cm H <sub>2</sub> O<br>(in. H <sub>2</sub> O) | $\Delta p_s$<br>cm H <sub>2</sub> O<br>(in. H <sub>2</sub> O) | $C_{p(s)}$ | Deviation<br>$C_{p(s)} - \bar{C}_{p(B)}$ |
|-----------------------|-------------------------------------------------------------------|---------------------------------------------------------------|------------|------------------------------------------|
| 1                     | 0.74                                                              | 1.00                                                          | 0.85       | +0.02                                    |
| 2                     | 0.29                                                              | 0.41                                                          | 0.83       | 0.00                                     |
| 3                     | 0.17                                                              | 0.25                                                          | 0.82       | -0.01                                    |
| $\bar{C}_{p(side B)}$ |                                                                   |                                                               | 0.83       | $\delta = 0.010 *$                       |

$$C_p(A) - C_p(B) = 0.00 *$$

Figure 4-10. Pitot tube calibration data.

\* VALUE MUST BE  $\leq \pm 0.01$

FORM: L-26 (REV. JUNE 10, 87)

**RECON SYSTEMS, INC.**  
Route 202 North P.O. Box 460  
THREE BRIDGES, NEW JERSEY 08887  
(201) 782-5900

CALIBRATION OF PITOT TUBE

-28-

Time \_\_\_\_\_  
Date 6/30/86  
Location RECUM  
Operator JD K

Type S Tube No.: 217  
Standard Tube No.: 167 WIGGET  
Comments: \_\_\_\_\_

SIDE A DOWNSTREAM

| Run No. | Fan Setting | Flue Temp °F | Vel. From $\Delta P_{STD}$ f/s | $CP_{STD}$ | $\Delta P_{STD}$ | $\Delta P_{TEST}$ | $CP_{TEST}$ | Average $CP_{TEST}$       |
|---------|-------------|--------------|--------------------------------|------------|------------------|-------------------|-------------|---------------------------|
| 1       | H           | FULL<br>72   |                                | 0.99       | 0.680            | 0.960             | 0.833       | 0.831<br>$\sigma = 0.008$ |
| 2       | H           | FULL<br>72   |                                | 0.99       | 0.475            | 0.675             | 0.830       |                           |
| 3       | L           | FULL<br>72   |                                | 0.99       | 0.315            | 0.460             | 0.819       |                           |
| 4       | L           | FULL<br>72   |                                | 0.99       | 0.170            | 0.235             | 0.842       |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |

SIDE B DOWNSTREAM

| Run No. | Fan Setting | Flue Temp °F | Vel. From $\Delta P_{STD}$ f/s | $CP_{STD}$ | $\Delta P_{STD}$ | $\Delta P_{TEST}$ | $CP_{TEST}$ | Average $CP_{TEST}$       |
|---------|-------------|--------------|--------------------------------|------------|------------------|-------------------|-------------|---------------------------|
| 1       | H           | FULL<br>72   |                                | 0.99       | 0.680            | 0.910             | 0.856       | 0.855<br>$\sigma = 0.007$ |
| 2       | H           | FULL<br>72   |                                | 0.99       | 0.475            | 0.655             | 0.843       |                           |
| 3       | L           | FULL<br>72   |                                | 0.99       | 0.315            | 0.415             | 0.862       |                           |
| 4       | L           | FULL<br>72   |                                | 0.99       | 0.170            | 0.225             | 0.860       |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |
|         |             |              |                                |            |                  |                   |             |                           |

$$CP_{TEST} = CP_{STD} \sqrt{\frac{\Delta P_{STD}}{\Delta P_{TEST}}}$$

- WHERE:  $CP_{TEST}$  - Pitot tube coefficient of Type S pitot tube.  
 $CP_{STD}$  - Pitot tube coefficient of standard type pitot tube (if unknown, use 0.99).  
 $\Delta P_{STD}$  - Velocity head measured by standard type pitot tube.  
 $\Delta P_{TEST}$  - Velocity head measured by Type S pitot tube.

BY: 7/27/87

METER BOX I.D.T. #4 METER NO. 578 DATE INSTALLED 7/27/87

BARO. PRESS. - 30.26

| ΔH<br>OFFICE<br>SETTING | METER TEMP. |     | METER<br>READING | A<br>CUBIC<br>FEET | TIME @<br>SEC. | ΔH @<br>FEET | DIFFERENCE<br>FROM AVG. ΔH @ |
|-------------------------|-------------|-----|------------------|--------------------|----------------|--------------|------------------------------|
|                         | IN          | OUT | READING          |                    |                |              |                              |
| .5                      | 90          | 80  | 545              | 1581.979           | 120            | 2.04         | + 0.04                       |
| 1.0                     | 88          | 80  | 544              | 1581.201           | 120            | 1.94         | - 0.06                       |
| 1.5                     | 87          | 80  | 544              | 1582.540           | 120            | 2.06         | + 0.06                       |
| 2.0                     | 91          | 81  | 546              | 1579.519           | 120            | 1.98         | - 0.02                       |
| 2.5                     | 90          | 82  | 546              | 1591.684           | 120            | 2.02         | + 0.02                       |
| 3.0                     | 89          | 81  | 545              | 1593.283           | 120            | 1.97         | - 0.03                       |
|                         |             |     |                  |                    |                | AVG = 2.00   |                              |

CALCULATION:

$$\Delta H @ = \frac{0.317(\Delta H)}{29.84(T+460)} \left[ \frac{T+460(120)}{A(60)} \right]^2$$

AVG. ΔH @ = 2.00  
NOTE: DIFF. NOT TO EXCEED  
± .15 FROM AVG. ΔH @

PROOF AND DIFFERENTIAL TEST RECORD

Meter Size 1304190 Date Received 8/6/86 Inspector Rich Gatto  
 Date Tested 8/7/86 New      Repaired ✓ Manufacturer Singmaster & Rockwell  
 Prover No. 1264 Temperatures: Room Air 77 F.       
 Total Meters this Page 3 Oil 77 F.  
 Prover Air 77 F.

Temp. Comp. Meters:  $\frac{\text{Abs. Base Temp.}}{\text{Abs. Prover Temp.}} \times \text{Uncorr. \% Proof} = \text{Corr. \% Proof}$

| Meter No. | Repair Class    | Percent Proof |       | Differential Maximum | Remarks                                              |
|-----------|-----------------|---------------|-------|----------------------|------------------------------------------------------|
|           |                 | Check         | Open  |                      |                                                      |
| 59295     | Intest          | 101.5         | 102.5 | 38                   | Uncorr. as<br>% Proof found<br>Corr.<br>% Proof      |
| 578753    | Intest          | 99.5          | 98.7  | 27                   | Uncorr. as<br>% Proof found<br>Corr.<br>% Proof      |
| 625432    | Intest          | 103.0         | 102.5 | 32                   | Uncorr. as<br>% Proof found<br>Corr.<br>% Proof      |
|           |                 |               |       |                      | Uncorr.<br>% Proof<br>Corr.<br>% Proof               |
| 59295     | Value<br>adjust | 100.0         | 100.0 | 25                   | Uncorr. as<br>% Proof calibrated<br>Corr.<br>% Proof |
| 578753    | adjust          | 100.0         | 100.0 | 26                   | Uncorr. as<br>% Proof calibrated<br>Corr.<br>% Proof |
| 625432    | Value<br>adjust | 100.0         | 100.0 | 28                   | Uncorr. as<br>% Proof calibrated<br>Corr.<br>% Proof |

| METER BOX I.D. - #3 METER NO. - 59333 DATE INSTALLED - AUG. 20, 87 BY: Tom M.                 |     | METER TEMP. |        | METER<br>READING | A<br>CYCLES | TIME<br>SEC. | $\Delta H$<br>C | DIFFERENCE<br>FROM AVG. $\Delta H$ |
|-----------------------------------------------------------------------------------------------|-----|-------------|--------|------------------|-------------|--------------|-----------------|------------------------------------|
| $\Delta H$<br>OFFICE<br>SETTING                                                               | IN  | OUT         | AVG. T |                  |             |              |                 |                                    |
| .5                                                                                            | 101 | 95          | 98     | 558              | 744.814     | 767          | 1.98            | -0.10                              |
| 1.0                                                                                           | 101 | 95          | 98     | 558              | 744.077     | 767          | 1.98            | -0.10                              |
| 1.5                                                                                           | 103 | 95          | 99     | 559              | 746.343     | 767          | 1.99            | -0.09                              |
| 2.0                                                                                           | 106 | 96          | 101    | 561              | 745.221     | 767          | 2.05            | -0.03                              |
| 2.5                                                                                           | 108 | 96          | 102    | 562              | 747.918     | 767          | 2.02            | -0.06                              |
| 3.0                                                                                           | 105 | 93          | 98     | 559              | 746.612     | 767          | 2.23            | +0.15                              |
|                                                                                               |     |             |        |                  | 749.958     | 767          | 2.21            | +0.13                              |
|                                                                                               |     |             |        |                  | 748.436     | 767          | 2.08            |                                    |
|                                                                                               |     |             |        |                  | 752.235     | 767          | 2.08            |                                    |
|                                                                                               |     |             |        |                  | 750.615     | 767          | 2.08            |                                    |
|                                                                                               |     |             |        |                  | 765.021     | 767          | 2.08            |                                    |
|                                                                                               |     |             |        |                  | 763.243     | 767          | 2.08            |                                    |
|                                                                                               |     |             |        |                  |             | AVG = 767    |                 |                                    |
| CALCULATION:                                                                                  |     |             |        |                  |             |              |                 |                                    |
| $\Delta H_c = \frac{0.317(\Delta H)}{29.84(T+460)} \left[ \frac{T+460(120)}{A(60)} \right]^2$ |     |             |        |                  |             |              |                 |                                    |
| $\Delta H_c = \frac{0.317(1.98)}{29.84(98+460)} \left[ \frac{98+460(120)}{767(60)} \right]^2$ |     |             |        |                  |             |              |                 |                                    |
| $\Delta H_c = 1.15 \text{ FROM AVG. } \Delta H_c$                                             |     |             |        |                  |             |              |                 |                                    |
| NOTE: DIFF. NOT TO EXCEED $\pm 0.15$ FROM AVG. $\Delta H_c$                                   |     |             |        |                  |             |              |                 |                                    |

## PROOF AND DIFFERENTIAL TEST RECORD

-32-

2-1905

Meter Size 1-130 Date Received 4-13-87 Inspector Joe SopranoDate Tested 4-20-87 New      Repaired ✓ Manufacturer Rockwell + Amer.Prover No. 1264 Temperatures: Room Air 78 F.Total Meters this Page 3 Oil 78 F.Prover Air 78 F.Temp. Comp. Meters:  $\frac{\text{Abs. Base Temp.}}{\text{Abs. Prover Temp.}} \times \text{Uncorr. \% Proof} = \text{Corr. \% Proof}$ 

| Meter No. | Repair Class | Percent Proof |       | Differential Maximum | Remarks                          |
|-----------|--------------|---------------|-------|----------------------|----------------------------------|
|           |              | Check         | Open  |                      |                                  |
| 59295     | INTEST       | 101.0         | 101.9 | 24                   | Uncorr. AS<br>% Proof - FOUND    |
|           |              |               |       |                      | Corr.<br>% Proof -               |
| 59333     | INTEST       | 101.6         | 102.0 | 28                   | Uncorr. AS<br>% Proof FOUND      |
|           |              |               |       |                      | Corr.<br>% Proof                 |
| L250998   | INTEST       | 100.9         | 101.9 | 31                   | Uncorr. AS<br>% Proof FOUND      |
|           |              |               |       |                      | Corr.<br>% Proof                 |
|           |              |               |       |                      | Uncorr.<br>% Proof               |
|           |              |               |       |                      | Corr.<br>% Proof                 |
| 59295     | VALVE        | 100.0         | 100.5 | 20                   | Uncorr. AS<br>% Proof CALIBRATED |
|           |              |               |       |                      | Corr.<br>% Proof                 |
| 59333     | ADJUST       | 99.5          | 99.9  | 28                   | Uncorr. AS<br>% Proof CALIBRATED |
|           |              |               |       |                      | Corr.<br>% Proof                 |
| L250998   | ADJUST       | 100.1         | 100.0 | 31                   | Uncorr. AS<br>% Proof CALIBRATED |
|           |              |               |       |                      | Corr.<br>% Proof                 |

Date

1/6/87

Calibrated by

T. Matf.

| Nozzle identification number (CSA) <sup>d</sup> | Nozzle Diameter <sup>a</sup> |                     |                     | $\Delta D$ , <sup>b</sup><br>mm (in.) | $D_{avg}$ <sup>c</sup> |
|-------------------------------------------------|------------------------------|---------------------|---------------------|---------------------------------------|------------------------|
|                                                 | $D_1$ ,<br>mm (in.)          | $D_2$ ,<br>mm (in.) | $D_3$ ,<br>mm (in.) |                                       |                        |
| # 23                                            | .179                         | .178                | .180                | .002                                  | .179                   |
| # 24                                            | .250                         | .250                | .250                | .000                                  | .250                   |
| # 33                                            | .368                         | .368                | .368                | .000                                  | .368                   |
| Nozzle used<br>43 runs<br>- n outlet → # 34     | .374                         | .374                | .374                | .000                                  | .374                   |
| # 4                                             | .250                         | .251                | .251                | .001                                  | .251                   |
| # 35                                            | .153                         | .152                | .153                | .001                                  | .153                   |
| # 36                                            | .174                         | .176                | .175                | .002                                  | .175                   |
| # 37                                            | .490                         | .488                | .488                | .002                                  | .489                   |
| # 38                                            | .500                         | .500                | .500                | .501                                  | .500                   |

where:

<sup>a</sup> $D_{1,2,3}$  = three different nozzle diameters, mm (in.); each diameter must be within (0.025 mm) 0.001 in.

<sup>b</sup>  $\Delta D$  = maximum difference between any two diameters, mm (in.),  
 $\Delta D \leq (0.10 \text{ mm}) 0.004 \text{ in.}$

<sup>c</sup>  $D_{avg}$  = average of  $D_1$ ,  $D_2$ , and  $D_3$ .

<sup>d</sup> - CSA = cross sectional area of nozzle, actual, in  $\text{ft}^2$

# NOZZLE CALIBRATION DATA FORM

-34-

Date

1/6/87

Calibrated by

T. Matthei

| Nozzle identification number (CSA) <sup>d</sup> | Nozzle Diameter <sup>a</sup> |                     |                     | $\Delta D$ , <sup>b</sup><br>mm (in.) | $D_{avg}$ <sup>c</sup> |
|-------------------------------------------------|------------------------------|---------------------|---------------------|---------------------------------------|------------------------|
|                                                 | $D_1$ ,<br>mm (in.)          | $D_2$ ,<br>mm (in.) | $D_3$ ,<br>mm (in.) |                                       |                        |
| # 28                                            | .310                         | .301                | .310                | .003                                  | .309                   |
| # 29                                            | .310                         | .308                | .312                | .002                                  | .309                   |
| # 30                                            | .303                         | .301                | .300                | .003                                  | .301                   |
| # 31                                            | .307                         | .307                | .304                | .003                                  | .306                   |
| # 1                                             | .148                         | .148                | .149                | .001                                  | .148                   |
| # 17                                            | .248                         | .245                | .247                | .003                                  | .247                   |
| # 32                                            | .263                         | .262                | .261                | .002                                  | .262                   |
| → # 19                                          | .373                         | .376                | .374                | .003                                  | .374                   |
| # 2                                             | .193                         | .192                | .192                | .001                                  | .192                   |

Used all runs & inlet

where:

<sup>a</sup> $D_{1,2,3}$  = three different nozzles diameters, mm (in.); each diameter must be within (0.025 mm) 0.001 in.

<sup>b</sup>  $\Delta D$  = maximum difference between any two diameters, mm (in.),  $\Delta D \leq (0.10 \text{ mm}) 0.004 \text{ in.}$

<sup>c</sup>  $D_{avg}$  = average of  $D_1$ ,  $D_2$ , and  $D_3$ .

<sup>d</sup> - CSA = cross sectional area of nozzle, actual, in  $\text{ft}^2$

## STACK TEMPERATURE SENSOR CALIBRATION DATA FORM

-35-

Date 7/1/86 Thermocouple number #3 (5-1)Ambient temperature 76 F ☒ Barometric pressure 30.0 in. HgCalibrator Peter J. Rose Reference: mercury-in-glass ASTM

other \_\_\_\_\_

| Reference point number | Source <sup>a</sup> (specify) | Reference thermometer temperature, °C | Thermocouple potentiometer temperature, °C | Temperature difference, <sup>b</sup> % |
|------------------------|-------------------------------|---------------------------------------|--------------------------------------------|----------------------------------------|
|                        | Hot Oil                       | 83                                    | 85                                         | 0.56                                   |
|                        | Hot Oil                       | 140                                   | 143                                        | 0.73                                   |
|                        | Hot Oil                       | 161                                   | 164                                        | 0.69                                   |

<sup>a</sup>Type of calibration system used.<sup>b</sup>
$$\left[ \frac{(\text{ref temp, } ^\circ\text{C} + 273) - (\text{test thermom temp, } ^\circ\text{C} + 273)}{\text{ref temp, } ^\circ\text{C} + 273} \right] 100 \leq 1.5\%$$

## STACK TEMPERATURE SENSOR CALIBRATION DATA FORM

Date 10/11/86 Thermocouple number #32 (3" C.L.)Ambient temperature 63 F Barometric pressure 30.25 in. HgCalibrator CD-1000 Reference: mercury-in-glass ASTMother NONE

| Reference point number | Source <sup>a</sup> (specify) | Reference thermometer temperature, °F | Thermocouple potentiometer temperature, °F | Temperature difference, % <sup>b</sup> |
|------------------------|-------------------------------|---------------------------------------|--------------------------------------------|----------------------------------------|
|                        | BOLING WATER                  | 213                                   | 214                                        | 0.1%                                   |
|                        | "                             | 213                                   | 214                                        | 0.1                                    |
|                        | "                             | 213                                   | 214                                        | 0.1                                    |
|                        | HOT OIL                       | 386                                   | 386                                        | 0.0                                    |
|                        | "                             | 387                                   | 386                                        | 0.1                                    |
|                        | "                             | 387                                   | 387                                        | 0.0                                    |
|                        | ICE WATER                     | 35                                    | 33                                         | 0.4                                    |
|                        | "                             | 35                                    | 33                                         | 0.4                                    |
|                        | "                             | 35                                    | 33                                         | 0.4                                    |
|                        |                               |                                       |                                            |                                        |
|                        |                               |                                       |                                            |                                        |
|                        |                               |                                       |                                            |                                        |

<sup>a</sup>Type of calibration system used.<sup>b</sup>
$$\left[ \frac{(\text{ref temp, } ^\circ\text{C} + 273) - (\text{test thermom temp, } ^\circ\text{C} + 273)}{\text{ref temp, } ^\circ\text{C} + 273} \right] 100 \leq 1.5\%$$

ORIGINAL DATA AND CALCULATION SHEETS

# RECON-SYSTEMS INC.

ROUTE 202N, P.O. BOX 460, THREE BRIDGES, N.J. 08887  
201-782-5900

-38-

DAILY  
FIELD  
SAMPLING  
RECORD

## PARTICULATE STACK SAMPLING DATA BOOK

Date 9-9-87

Jobsite

Company

Macwell House

City Hoboken

State NJ

CLIENT Ernie Lard

RECON Job # 0554

FIELD Supervisor P. Marshall

Street 1127 Hudson St.

Zip 07030

### Processes, Stacks, Sites, etc. Tested:

1. INLET Condition\* STEADY
2. \_\_\_\_\_ Condition\* \_\_\_\_\_
3. \_\_\_\_\_ Condition\* \_\_\_\_\_
4. \_\_\_\_\_ Condition\* \_\_\_\_\_

\* (e.g. stack opacity, raining?, water odor, color, flowrate;  
process steady or upset; etc.)

### Milestone Times (Military)

Arrival 8<sup>00</sup> Lost Time —

Lunch 1230 to 1315

Departure 1830

Reasons For Lost Time \_\_\_\_\_

Client or Jobsite Representative Aware of Lost Time \_\_\_\_\_

### Personnel Onsite

RECON: PFM, TFM, CAR, JDK, \_\_\_\_\_, \_\_\_\_\_

\_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_

\_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_

Client: \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_

Jobsite Reps: \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_

Agencies Observing (1) NJDEP (2) NJDEP

Agency Personnel (1) TOM BROWN, \_\_\_\_\_, \_\_\_\_\_

(2) BETH ROSSI, \_\_\_\_\_, \_\_\_\_\_

## Particulate Sampling Field Data

Plant Maxwell House  
 Stack ROTOLONE INLET  
 Nozzle Size 3/16"  
 Time @ Each Point (0) 3 Min  
 Ambient Temperature 80 °F

Date 9/1/87  
 Sample No. 1 Box No. 3  
 Probe Heater @ 8 Box Heater @ 8 °F  
 Hose Heater @ 8 °F  
 Ambient Pressure (P<sub>bar</sub>) 29.90 "Hg

NOZZLE No. 19  
 THERMO. NO. 3  
 PITOTBE NO. 217  
 CONSOLE NO. 3

Stack Pressure (P) ~ 2.1 "H<sub>2</sub>O (gage) ÷ 13.6 = "Hg (gage)

Stack Pressure (P<sub>s</sub>) = P<sub>bar</sub> + P = "Hg

Dry Bulb °F

Wet Bulb °F %H<sub>2</sub>O

Operating Condition or  
 Remarks

| Port/<br>Point | Military<br>Clock<br>Time | Meter<br>Reading | Pitot<br>ΔP | Orifice<br>ΔH | Meter<br>Temp (°F)<br>IN OUT | Line<br>Vac<br>"Hg | Probe<br>Outlet<br>(°F) | Box<br>Outlet<br>Temp<br>(°F) | Box<br>Temp<br>(°F) | Stack<br>Temp<br>(°F) |
|----------------|---------------------------|------------------|-------------|---------------|------------------------------|--------------------|-------------------------|-------------------------------|---------------------|-----------------------|
| A-1            | 11:16                     | 156.718          | 1.1         | 1.45          | 98 90                        | 6                  | 178                     | 148                           | 250                 | 81                    |
| 2              | 11:19                     |                  | 2.1         | 2.70          | 106 92                       | 9                  | 198                     | 228                           | 240                 | 80                    |
| 3              | 11:22                     | 162.10           | 3.8         | 2.47          | 120 92                       | 10                 | 211                     | 244                           | 225                 | 80                    |
| 4              | 11:25                     | 164.5            | 3.5         | 4.4           | 125 95                       | 10                 | 206                     | 239                           | 230                 | 80                    |
| 5              | 11:28                     | 168.1            | 2.6         | 3.2           | 130 98                       | 10                 | 188                     | 227                           | 212                 | 80                    |
| 6              | 11:31                     | 168.8            | 1.6         | 2.1           | 130 99                       | 8                  | 180                     | 217                           | 210                 | 81                    |
| 7              | 11:34                     | 173.1            | .67         | .49           | 125 100                      | 5                  | 173                     | 207                           | 200                 | 81                    |
| 8              | 11:37                     | 175.3            | .26         | .36           | 122 98                       | 3                  | 169                     | 205                           | 215                 | 81                    |
| End            | 11:40                     | 175.934          |             |               |                              |                    |                         |                               |                     |                       |
| B-1            | 11:42                     | 175.134          | .52         | .7            | 118 101                      | 6                  | 161                     | 186                           | 230                 | 80                    |
| 2              | 11:45                     | 177.40           | 1.7         | 2.2           | 120 102                      | 7                  | 179                     | 223                           | 230                 | 81                    |
| 3              | 11:48                     | 179.7            | 2.2         | 2.2           | 125 103                      | 8                  | 185                     | 231                           | 230                 | 80                    |
| 4              | 11:51                     | 182.2            | 2.2         | 2.6           | 128 104                      |                    | 184                     | 226                           | 220                 | 81                    |
| 5              | 11:54                     | 184.8            | 1.7         | 2.2           | 130 104                      |                    | 180                     | 217                           | 205                 | 81                    |
| 6              | 11:57                     | 185              | .84         | 1.2           | 128 105                      |                    | 178                     | 207                           | 200                 | 81                    |
| 7              | 12:00                     | 189.0            | .26         | .36           | 122 105                      | 3                  | 177                     | 201                           | 200                 | 81                    |
| 8              | 12:03                     | 191.235          | .26         | .22           | 120 106                      | 2                  | 168                     | 197                           | 205                 | 82                    |
| End            | 12:06                     | 191.235          |             |               |                              |                    |                         |                               |                     |                       |
| C-1            | 12:08                     | 191.235          | .36         | .38           | 115 106                      | 3                  | 159                     | 180                           | 230                 | 83                    |
| 2              | 12:11                     |                  | .37         | .41           | 116 106                      |                    | 180                     | 215                           | 230                 | 82                    |
| 3              | 12:14                     | 193.52           | .44         | .56           | 116 106                      | 3                  | 228                     | 224                           | 225                 | 82                    |
| 4              | 12:17                     | 198.8            | .48         | .61           | 118 106                      | 3                  | 189                     | 225                           | 215                 | 82                    |
| 5              | 12:20                     | 196.08           | .26         | .37           | 118 106                      | 3                  | 184                     | 221                           | 205                 | 82                    |
| 6              | 12:23                     | 197.1            | .13         | .17           | 115 105                      | 2                  | 181                     | 210                           | 200                 | 81                    |
| 7              | 12:26                     | 197.8            | .64         | .65           | 114 105                      | 1                  | 197                     | 198                           | 200                 | 82                    |
| 8              | 12:29                     | V=               | -----       | ΔH=           | T <sub>m</sub> =             |                    |                         |                               |                     | T <sub>s</sub> =      |

\* Sum, Average, or Difference

(Convert to)  
 °F

$$V_m = V \text{ (DGMCF)} = (1.0)(41.978) = 41.978 \text{ ft}^3$$

## Other Data

| Time | Sample or<br>Measurement | Value |
|------|--------------------------|-------|
|      | FLYING O <sub>2</sub>    | 21    |
|      | CO <sub>2</sub>          | 0     |
|      | ORSAT O <sub>2</sub>     | 21    |
|      | CO <sub>2</sub>          | 0     |

$$\text{Average CO}_2 = \frac{\%}{100} \times \text{MW}/100 = \frac{\%}{100} \times 0.44 =$$

$$\text{O}_2 = \frac{\%}{100} \times 0.32 =$$

$$\text{N}_2 = \frac{\%}{100} \times 0.28 =$$

100.0

= dry MW

Pre-Leak Check 0.00 ± 15°

Post Leak Check .01 CFM

CONSOLE NO.

Box No.

8

Box Heater

 $\text{e}^{\circ}\text{F}$ 

Ambient Pressure ( $P_{bar}$ ) \_\_\_\_\_ "Hg

"Hg (qage)

"Hg

| Operating Condition or<br>Remarks |
|-----------------------------------|
|-----------------------------------|

OF

Of

$$-8\text{H}_2\text{O}$$

\* Sum, Average, or Difference.

(Convert to)  
°F

$$V_m = V \text{ (DGMCF)} = ( \quad ) ( \quad ) = \quad \text{ft}^3$$

## Other Data

$$\text{Average CO}_2 = \frac{\%}{\times 0.44} \times \text{MW}/100 =$$

$$\therefore \dot{O}_2 = \quad \times 0.32 =$$

$$N_2 = \quad \times 0.28 =$$

100.0      "      = dry MW

### Pre-Leak Check

### Post Leak Check

CLIENT: GENERAL FOODS  
 SAMPLING DATE: 9/9/87  
 SAMPLING TIME: 1116-1229  
 UNIT SAMPLED: ROTO. INLET

Date: 09/21/87  
 Time: 9:44 AM  
 Run # 1

## AVERAGE VELOCITY PRESSURE

| <u>Delta P</u><br><u>(IN H2O)</u> | <u>Delta P</u><br><u>Square Root</u> |
|-----------------------------------|--------------------------------------|
| 1.10                              | 1.05                                 |
| 2.10                              | 1.45                                 |
| 3.80                              | 1.95                                 |
| 3.50                              | 1.87                                 |
| 2.60                              | 1.61                                 |
| 1.60                              | 1.26                                 |
| 0.67                              | 0.82                                 |
| 0.26                              | 0.51                                 |
| 0.52                              | 0.72                                 |
| 1.70                              | 1.30                                 |
| 2.20                              | 1.48                                 |
| 2.20                              | 1.48                                 |
| 1.70                              | 1.30                                 |
| 0.84                              | 0.92                                 |
| 0.26                              | 0.51                                 |
| 0.11                              | 0.33                                 |
| 0.30                              | 0.55                                 |
| 0.32                              | 0.57                                 |
| 0.44                              | 0.66                                 |
| 0.48                              | 0.69                                 |
| 0.26                              | 0.51                                 |
| 0.13                              | 0.36                                 |
| 0.04                              | 0.20                                 |
| 0.04                              | 0.20                                 |

THE AVERAGE SQUARE ROOT OF DELTA P = .9298872

CLIENT: GENERAL FOODS  
 SAMPLING DATE: 9/9/87  
 SAMPLING TIME: 1116-1239  
 UNIT SAMPLED: ROTO. INLET

Date: 09/21/87  
 Time: 9:44 AM  
 Run # 1

| Delta H<br>(IN H2O) | Meter Temp (F) |        | Stack Temp (F) |
|---------------------|----------------|--------|----------------|
|                     | IN             | OUT    |                |
| 1.45                | 98.00          | 90.00  | 81.00          |
| 2.70                | 106.00         | 92.00  | 80.00          |
| 4.70                | 120.00         | 92.00  | 80.00          |
| 4.40                | 125.00         | 95.00  | 80.00          |
| 3.20                | 130.00         | 98.00  | 80.00          |
| 2.10                | 130.00         | 99.00  | 81.00          |
| 0.99                | 125.00         | 100.00 | 80.00          |
| 0.36                | 122.00         | 98.00  | 81.00          |
| 0.70                | 118.00         | 101.00 | 80.00          |
| 2.20                | 120.00         | 102.00 | 81.00          |
| 2.60                | 125.00         | 103.00 | 81.00          |
| 2.60                | 128.00         | 104.00 | 81.00          |
| 2.20                | 130.00         | 104.00 | 81.00          |
| 1.20                | 128.00         | 105.00 | 81.00          |
| 0.36                | 122.00         | 105.00 | 81.00          |
| 1.22                | 120.00         | 106.00 | 82.00          |
| 0.38                | 115.00         | 106.00 | 83.00          |
| 0.41                | 116.00         | 106.00 | 82.00          |
| 0.56                | 116.00         | 106.00 | 82.00          |
| 0.61                | 118.00         | 106.00 | 82.00          |
| 0.37                | 118.00         | 106.00 | 82.00          |
| 0.17                | 115.00         | 105.00 | 81.00          |
| 0.05                | 114.00         | 105.00 | 82.00          |
| 0.05                | 112.00         | 102.00 | 82.00          |

AVERAGES

DELTA H = 1.4825 IN H2O  
 METER TEMP. = 110.5625 F  
 STACK TEMP. = 81.125 F

# Water and Dry Particulate Collections

-43-

PLANT MAXWELL HOUSE  
 TEST FOR particulate  
 SAMPLE NO. 1 BOX NO.

STACK ROTO-INLET  
 DATE 9/9/87  
 OPERATING CONDITION

|            | Grams                                                                        | Grams                  |
|------------|------------------------------------------------------------------------------|------------------------|
| Impinger 1 | Final Weight <u>699.4</u><br>Initial Weight <u>706.0</u><br>Increase <u></u> | Impinger 1 <u>-6.6</u> |
| Impinger 2 | Final Weight <u>706.7</u><br>Initial Weight <u>696.9</u><br>Increase <u></u> | Impinger 2 <u>9.8</u>  |
| Impinger 3 | Final Weight <u>485.6</u><br>Initial Weight <u>482.4</u><br>Increase <u></u> | Impinger 3 <u>3.2</u>  |
| Silica Gel | Final Weight <u>717.3</u><br>Initial Weight <u>703.4</u><br>Increase <u></u> | Silica Gel <u>13.9</u> |

Record Water Collected  
 in cyclone, flash, if any:

~~Final Weight  gms~~  
~~Initial Weight  gms~~  
~~Increase  gms~~

20.3 grams

Total mass of water caught

Filter Diameter 4 inches

Filter Type Glass Fiber

Filter

|                |              |
|----------------|--------------|
| Final Weight   | <u>.6430</u> |
| Initial Weight | <u>.6270</u> |
| Increase       | <u>.016</u>  |

.016 gram

Total mass of particulate  
 caught on filter

Is ice present in the impinger bath at the end of this sample?  
 Yes ✓ No

RECON SYSTEMS, INC.  
 Three Bridges NJ

Lab Data - Evaporations

-44-

PLANT MAHALL HOUSE STACK ROTO INLET SAMPLE NO. 1 FOR           

SAMPLING DATE 9/9/81 OPERATING CONDITION           

Acetone Washings

Gross 535.2 GMS

TOTAL

SAMPLE Tare- 338.2 GMS

(A) Net 197.0 GMS

AMOUNT

EVAPORATED 197.0 GMS (B)

Evap. Beaker NO.

Gross 103.0497 GMS

Tare- 103.0847 GMS

Net 0.0150 (C) GMS

Acetone Blank = 0.0000 GMS

(D) 100 GMS

Corrected

Net = (C) - (B) (D)

(E)

$$= \frac{0.0150}{100} - \frac{197}{100} = \frac{0.000}{100}$$

$$= \frac{0.0150}{100} \text{ GMS}$$

Scaled Up

Net = (E)  $\frac{A}{B}$

$$= \frac{0.0150}{197.0} \left( \frac{197.0}{197.0} \right)$$

$$= \frac{0.0150}{197.0} \text{ GMS}$$

Wet Catch

Gross            GMS

TOTAL

SAMPLE Tare-            GMS

(F) Net            GMS

AMOUNT

of E/C            mls (H)

AMOUNT

EXTRACTED

(G)            GMS (mls)

Water Phase

Evap. Beaker No.           

Gross            GMS

Tare-            GMS

Net            (J) GMS

Water Blank

(L)            GMS

Corrected

Net (N) = J - (G) (L)

$$= \frac{\quad}{100} - \frac{\quad}{100}$$

$$= \frac{\quad}{100} \text{ GMS}$$

Scaled Up Net = N  $\left( \frac{F}{G} \right)$

$$= \frac{\quad}{\quad} \left( \frac{\quad}{\quad} \right)$$

$$= \frac{\quad}{\quad} \text{ GMS}$$

E/C Phase

Evap. Beaker No.           

Gross            GMS

Tare-            GMS

Net            (K) GMS

E/C Blank

(M)            GMS

Corrected

Net (P) = K - H (M)

$$= \frac{\quad}{100} - \frac{\quad}{100}$$

$$= \frac{\quad}{100} \text{ GMS}$$

Scaled Up Net = P  $\left( \frac{F}{G} \right)$

$$= \frac{\quad}{\quad} \left( \frac{\quad}{\quad} \right)$$

$$= \frac{\quad}{\quad} \text{ GMS}$$

## Particulates

Nozzle, Probe, and Acetone Washing .015 grms

Filter .0160 grms

---

Enter "0" if no Organic or Aqueous Phase

Aqueous Phase 0 grms

Organic Phase 0 grms

## Totals

GRAINS/DSCF = .0122761

POUNDS/HOUR = .3457558

HIT RETURN TO CONTINUE

# Particulate Sampling Field Data

Plant Kalwell House  
 Stack ROTACONE INLET  
 Nozzle Size 3/4  
 Time @ Each Point (0) 3 Min  
 Ambient Temperature OF

Date 9/9/87  
 Sample No. 2  
 Probe Heater @ Box Heater  
 Hose Heater @ OF  
 Ambient Pressure (P<sub>bar</sub>) 29.90 "Hg

-46-  
 NOZZLE NO. 19  
 THERMO. NO. 3  
 PITOBE NO. 217  
 CONSOLE NO. 3

Stack Pressure (P) -2.0 "H<sub>2</sub>O (gage) ÷ 13.6 = "Hg (gage)

Stack Pressure (P<sub>S</sub>) = P<sub>bar</sub> + P = "Hg  
 Dry Bulb OF  
 Wet Bulb OF %H<sub>2</sub>O

Operating Condition or  
 Remarks

| Port/<br>Point | Military<br>Clock<br>Time | Meter<br>Reading | Pitot<br>ΔP | Orifice<br>ΔH | Meter<br>Temp (OF)<br>IN OUT | Line<br>Vac<br>"Hg | Probe<br>Outlet<br>(°F) | Box<br>Outlet<br>Temp<br>(°F) | Box<br>Temp<br>(°F) | Stack<br>Temp<br>(°F) |
|----------------|---------------------------|------------------|-------------|---------------|------------------------------|--------------------|-------------------------|-------------------------------|---------------------|-----------------------|
| A-1            | 13:46                     | 198.908          | .53         | .68           | 91 93                        | 2                  | 90                      | 114                           | 189                 | 83                    |
| -2             | 14                        | 200.3            | 2.0         | 2.7           | 95 94                        |                    | 88                      | 145                           | 210                 | 83                    |
| 3              | 152                       | 202.8            | 2.5         | 3.2           | 102 93                       | 7                  | 124                     | 164                           | 236                 | 81                    |
| 4              | 155                       | 205.5            | 2.5         | 3.2           | 115 45                       | 7                  | 145                     | 180                           | 236                 | 82                    |
| 5              | 158                       | 208.4            | 2.0         | 2.7           | 120 95                       | 7                  | 158                     | 191                           | 222                 | 82                    |
| 6              | 14:01                     | 211.2            | 1.0         | 1.30          | 124 96                       | 4                  | 163                     | 190                           | 205                 | 82                    |
| 7              | 104                       | 212.8            | .45         | .58           | 119 98                       | 3                  | 167                     | 185                           | 195                 | 82                    |
| 8              | 107                       | 214.3            | .3          | .39           | 118 98                       | 2                  | 167                     | 177                           | 195                 | 83                    |
| end            | 14:10                     | 215.233          |             |               |                              |                    |                         |                               |                     |                       |
| B-1            | 14:12                     | 215.233          | .65         | .83           | 113 99                       | 3                  | 164                     | 168                           | 225                 | 84                    |
| 2              | 115                       | 216.8            | 1.9         | 2.4           | 116 100                      | 6                  | 180                     | 203                           | 225                 | 86                    |
| 3              | 118                       | 219.4            | 2.4         | 3.0           | 122 101                      | 7                  | 185                     | 212                           | 219                 | 84                    |
| 4              | 121                       | 222.0            | 2.7         | 3.45          | 126 102                      | 8                  | 195                     | 206                           | 205                 | 83                    |
| 5              | 124                       | 225.1            | 1.9         | 2.4           | 129 103                      |                    | 120                     | 186                           | 195                 | 83                    |
| 6              | 127                       | 227.0            | 1.1         | 1.4           | 128 104                      | 4                  | 135                     | 175                           | 190                 | 83                    |
| 7              | 130                       | 229.5            | .45         | .60           | 124 105                      | 3                  | 152                     | 177                           | 205                 | 83                    |
| 8              | 133                       | 230.4            | .33         | .42           | 122 105                      | 3                  | 160                     | 180                           | 230                 | 83                    |
| end            | 14:36                     | 231.882          |             |               |                              |                    |                         |                               |                     |                       |
| C-1            | 14:37                     | 231.882          | .25         | .32           | 117 105                      | 2                  | 163                     | 179                           | 230                 | 86                    |
| 2              | 140                       |                  |             | .68           | 118 106                      | 2                  | 182                     | 198                           | 215                 |                       |
| 3              | 143                       | 2142             | No Power    |               |                              |                    |                         |                               |                     |                       |
| 4              | 146                       | 2144             | No Power    |               |                              |                    |                         |                               |                     |                       |
| 1              | 146:16                    |                  | .73         | .93           | 118 106                      | 4                  | 178                     | 205                           | 190                 | 84                    |
| 1              | 149:16                    | 236.3            | .64         | .88           | 120 106                      | 4                  | 182                     | 205                           | 190                 | 83                    |
| 0              | 152:59                    | 237.4            | .65         | .83           | 120 109                      | 4                  | 183                     | 206                           | 213                 | 83                    |
| *              | 0=                        | V=               | ----        | ΔH=           | T <sub>m</sub> =             |                    |                         |                               |                     | T <sub>s</sub> =      |

• Sum, Average, or Difference

(Convert to)  
 OF

$$V_m = V \text{ (DGMCF)} = (1.0) (42.404) = 42.404 \text{ ft}^3$$

## Other Data

| Time | Sample or<br>Measurement | Value |
|------|--------------------------|-------|
|      | Filter O <sub>2</sub>    | 21.0  |
|      | CO <sub>2</sub>          | 0     |
|      | Orsat O <sub>2</sub>     | 21.0  |
|      | CO <sub>2</sub>          | 0     |

$$\text{Average CO}_2 = \frac{\%}{x 0.44} =$$

$$\text{O}_2 = \frac{\%}{x 0.32} =$$

$$\text{N}_2 = \frac{\%}{x 0.28} =$$

100.0

= dry MW

Pre-Leak Check 0.00 at 15"

Post Leak Check .61

Date 9/9/87 PITOBE NO. \_\_\_\_\_  
 \_\_\_\_\_ CONSOLE NO. \_\_\_\_\_  
 Sample No. 1 Box No. \_\_\_\_\_  
 Probe Heater @ \_\_\_\_\_ Box Heater \_\_\_\_\_  
 Hose Heater @ \_\_\_\_\_ of \_\_\_\_\_  
 Ambient Pressure (P<sub>bar</sub>) \_\_\_\_\_ "Hg

| Stack Pressure ( $P_s$ ) = $P_{bar} + P =$ | "Hg | Operating Condition or Remarks |
|--------------------------------------------|-----|--------------------------------|
| Dry Bulb °F                                |     |                                |

| Operating Condition or<br>Remarks |
|-----------------------------------|
|-----------------------------------|

[illegible]

(Convert to)  
OF

$$V_m = V \text{ (DGMCF)} = ( \quad ) ( \quad ) = \quad \text{ft}^3$$

| Time | Sample or Measurement | Value |
|------|-----------------------|-------|
|      |                       |       |
|      |                       |       |
|      |                       |       |
|      |                       |       |
|      |                       |       |

$$\text{Average CO}_2 = \frac{\%}{\times 0.44} \times \text{MW}/100 =$$

$$\therefore O_2 = \quad \times 0.32 =$$

$$N_2 = \underline{\hspace{2cm}} \times 0.28 = \underline{\hspace{2cm}}$$

100.0 = dry MW

### Post Leak Check

CLIENT: GENERAL FOODS  
 SAMPLING DATE: 9/9/87  
 SAMPLING TIME: 1346-1303  
 UNIT SAMPLED: ROTO. INLET

Date: 09/21/87  
 Time: 9:44 AM  
 Run # 2

# AVERAGE VELOCITY PRESSURE

| <u>Delta P</u><br><u>(IN H2O)</u> | <u>Delta P</u><br><u>Square Root</u> |
|-----------------------------------|--------------------------------------|
| 0.53                              | 0.73                                 |
| 2.00                              | 1.41                                 |
| 2.50                              | 1.58                                 |
| 2.50                              | 1.58                                 |
| 2.00                              | 1.41                                 |
| 1.00                              | 1.00                                 |
| 0.45                              | 0.67                                 |
| 0.30                              | 0.55                                 |
| 0.65                              | 0.81                                 |
| 1.90                              | 1.38                                 |
| 2.40                              | 1.55                                 |
| 2.70                              | 1.64                                 |
| 1.90                              | 1.38                                 |
| 1.10                              | 1.05                                 |
| 0.45                              | 0.67                                 |
| 0.33                              | 0.57                                 |
| 0.25                              | 0.50                                 |
| 0.53                              | 0.73                                 |
| 0.83                              | 0.91                                 |
| 0.69                              | 0.83                                 |
| 0.65                              | 0.81                                 |
| 0.37                              | 0.61                                 |
| 0.05                              | 0.22                                 |
| 0.05                              | 0.22                                 |

THE AVERAGE SQUARE ROOT OF DELTA P = .9507572

CLIENT: GENERAL FOODS  
 SAMPLING DATE: 9/9/87  
 SAMPLING TIME: 1346-1303  
 UNIT SAMPLED: ROTD. INLET

Date: 09/21/87  
 Time: 9:44 AM  
 Run # 2

| Delta H<br>(IN H2O) | Meter Temp (F) |        | Stack Temp (F) |
|---------------------|----------------|--------|----------------|
|                     | IN             | OUT    |                |
| 0.68                | 91.00          | 93.00  | 83.00          |
| 2.70                | 95.00          | 94.00  | 83.00          |
| 3.20                | 107.00         | 93.00  | 81.00          |
| 3.20                | 115.00         | 95.00  | 81.00          |
| 2.70                | 120.00         | 95.00  | 82.00          |
| 1.30                | 124.00         | 96.00  | 82.00          |
| 0.58                | 119.00         | 98.00  | 82.00          |
| 0.39                | 118.00         | 98.00  | 83.00          |
| 0.83                | 113.00         | 99.00  | 85.00          |
| 2.40                | 118.00         | 100.00 | 86.00          |
| 3.10                | 122.00         | 101.00 | 84.00          |
| 3.45                | 126.00         | 102.00 | 83.00          |
| 2.40                | 129.00         | 103.00 | 83.00          |
| 1.40                | 128.00         | 104.00 | 83.00          |
| 0.60                | 124.00         | 105.00 | 83.00          |
| 0.42                | 122.00         | 105.00 | 83.00          |
| 0.32                | 117.00         | 105.00 | 86.00          |
| 0.68                | 118.00         | 106.00 | 86.00          |
| 0.93                | 118.00         | 106.00 | 84.00          |
| 0.88                | 120.00         | 106.00 | 84.00          |
| 0.83                | 120.00         | 109.00 | 83.00          |
| 0.47                | 121.00         | 106.00 | 83.00          |
| 0.06                | 118.00         | 106.00 | 82.00          |
| 0.06                | 116.00         | 106.00 | 82.00          |

# AVERAGES

DELTA H = 1.399167 IN H2O  
 METER TEMP. = 109.375 F  
 STACK TEMP. = 83.20835 F

# Water and Dry Particulate Collections

-50-

PLANT Maxwell House  
 TEST FOR Particulate  
 SAMPLE NO. 2 BOX NO. 3

STACK ROTO. IN.  
 DATE 9-9-87  
 OPERATING CONDITION STEADY

|            | Grams                                                                | Grams                  |
|------------|----------------------------------------------------------------------|------------------------|
| Impinger 1 | Final Weight <u>681.0</u><br>Initial Weight <u>677.8</u><br>Increase | Impinger 1 <u>3.2</u>  |
| Impinger 2 | Final Weight <u>685.5</u><br>Initial Weight <u>690.5</u><br>Increase | Impinger 2 <u>-5.0</u> |
| Impinger 3 | Final Weight <u>506.5</u><br>Initial Weight <u>502.8</u><br>Increase | Impinger 3 <u>3.7</u>  |
| Silica Gel | Final Weight <u>802.2</u><br>Initial Weight <u>783.2</u><br>Increase | Silica Gel <u>19</u>   |

Record Water Collected  
 in cyclone flash, if any:

Final Weight \_\_\_\_\_ gms  
 Initial Weight \_\_\_\_\_ gms  
 Increase \_\_\_\_\_ gms

20.9 grams  
 Total mass of water caught

Filter Diameter 4 inches  
 Filter Type Glass Fiber

Filter Final Weight .6415  
 Initial Weight .6328  
 Increase

0.0087 gram  
 Total mass of particulate  
 caught on filter

Is ice present in the impinger bath at the end of this sample?  
 Yes ☒ No ☐

RECON SYSTEMS, INC.  
 Three Bridges NJ

PLANT MAXWELL HOUSE STACK ROTO-INLET SAMPLE NO. 2 FOR ParticulateSAMPLING DATE \_\_\_\_\_ OPERATING CONDITION STEADY

## Acetone Washings

Gross 519.6 GMS

TOTAL

SAMPLE Tare- 339.2 GMS(A) Net 180.4 GMS

## AMOUNT

EVAPORATED 180.4 GMS (B)

Evap. Beaker NO.

Gross 96.7833 GMSTare- 96.7823 GMSNet 0.001 (C) GMSAcetone Blank = 0 GMS  
(D) 100 GMS

## Corrected

Net = (C) - (B) (D)  
(E)

$$= \frac{0.001}{100} - \frac{180.4}{100} \left( \frac{0}{100} \right)$$

$$= \frac{0.001}{100} \text{ GMS}$$

## Scaled Up

Net = (E)  $\frac{A}{B}$ 

$$= \frac{0.001}{100} \left( \frac{180.4}{180.4} \right)$$

$$= \frac{0.001}{100} \text{ GMS}$$

## Wet Catch

Gross \_\_\_\_\_ GMS

TOTAL

SAMPLE Tare- \_\_\_\_\_ GMS

(F) Net \_\_\_\_\_ GMS

## AMOUNT

of E/C \_\_\_\_\_ mls (H)

## AMOUNT

EXTRACTED  
(G) \_\_\_\_\_ GMS (mls)

Water Phase

Evap. Beaker No. \_\_\_\_\_

Gross \_\_\_\_\_ GMS

Tare- \_\_\_\_\_ GMS

Net \_\_\_\_\_ (J) GMS

Water Blank

(L) = \_\_\_\_\_ GMS  
100 GMS

## Corrected

Net (N) = J - (G) (L)

$$= \frac{\quad}{100}$$

= \_\_\_\_\_ GMS

Scaled Up Net = N  $\left( \frac{F}{G} \right)$ 

$$= \frac{\quad}{\quad} \left( \frac{\quad}{\quad} \right)$$

$$= \quad \text{GMS}$$

E/C Phase

Evap. Beaker No. \_\_\_\_\_

Gross \_\_\_\_\_ GMS

Tare- \_\_\_\_\_ GMS

Net \_\_\_\_\_ (K) GM

E/C Blank

(M) = \_\_\_\_\_ GMS  
100 mls

## Corrected

Net (P) = K - H (M)

$$= \frac{\quad}{100}$$

= \_\_\_\_\_ GMS

Scaled Up Net = P  $\left( \frac{F}{G} \right)$ 

$$= \frac{\quad}{\quad} \left( \frac{\quad}{\quad} \right)$$

$$= \quad \text{GMS}$$

## Particulates

Nozzle, Probe, and Acetone Washing .0010 grms

Filter .0087 grms

.0010.0097-----  
Enter "0" if no Organic or Aqueous Phase

Aqueous Phase 0 grms

Organic Phase 0 grms

## Totals

GRAINS/DSCF = .0037955

POUNDS/HOUR = .1090658

HIT RETURN TO CONTINUE

## Particulate Sampling Field Data

Plant Maxwell House  
 Stack ROTOCLONE INLET  
 Nozzle Size 3/16"  
 Time @ Each Point (0) 3 Min  
 Ambient Temperature 80 °F

Nozzle No. 19  
 THERMO No. 3  
 PITOT No. 217  
 CONSOLE NO. 3  
 Date 9/1/71  
 Sample No. 3 Box No. 3  
 Probe Heater @ \_\_\_\_\_ % Box Heater @ \_\_\_\_\_ %  
 Hose Heater @ \_\_\_\_\_ %  
 Ambient Pressure (P<sub>bar</sub>) 29.90 "Hg

Stack Pressure (P) -2.0 "H<sub>2</sub>O (gage) ÷ 13.6 = \_\_\_\_\_ "Hg (gage)

Stack Pressure (P<sub>S</sub>) = P<sub>bar</sub> + P = \_\_\_\_\_ "Hg  
 Dry Bulb \_\_\_\_\_ °F  
 Wet Bulb \_\_\_\_\_ °F \_\_\_\_\_ %H<sub>2</sub>O

Operating Condition or  
Remarks

| Port/<br>Point | Military<br>Clock<br>Time | Meter<br>Reading | Pitot<br>ΔP | Orifice<br>ΔH | Meter<br>Temp (°F) |     | Line<br>Vac<br>"Hg | Probe<br>Outlet<br>(°F) | Box<br>Outlet<br>Temp<br>(°F) | Box<br>Temp<br>(°F) | Stack<br>Temp<br>(°F) |
|----------------|---------------------------|------------------|-------------|---------------|--------------------|-----|--------------------|-------------------------|-------------------------------|---------------------|-----------------------|
|                |                           |                  |             |               | IN                 | OUT |                    |                         |                               |                     |                       |
| C-1            | 15:51                     | 241.52           | .37         | .47           | 98                 | 99  | 3                  | 93                      | 138                           | 213                 | 84                    |
| 2              | 15:54                     | 242.7            | .24         | .31           | 99                 | 99  | 3                  | 90                      | 165                           | 197                 | 83                    |
| 3              | 15:57                     |                  | .45         | .58           | 103                | 100 |                    | 90                      | 167                           | 181                 | 84                    |
| 4              | 16:00                     | 245.0            | .55         | .70           | 107                | 100 |                    | 89                      | 167                           | 190                 | 82                    |
| 5              | 16:03                     | 246.45           | .45         | .58           | 110                | 100 | 4                  | 102                     | 165                           | 201                 | 82                    |
| 6              | 16:06                     | 247.7            | .15         | .19           | 112                | 100 |                    | 126                     | 161                           | 225                 | 83                    |
| 7              | 16:09                     | 248.5            | .08         | .10           | 110                | 106 |                    | 141                     | 163                           | 230                 | 83                    |
| 8              | 16:12                     | 249.05           | .03         | .04           | 110                | 102 | 1                  | 138                     | 160                           | 225                 | 83                    |
| End            | 16:15                     | 249.438          |             |               |                    |     |                    |                         |                               |                     |                       |
| R-1            | 16:16                     | 249.438          | .7          | .89           | 111                | 102 | 5                  | 112                     | 163                           | 207                 | 86                    |
| 2              | 16:19                     |                  | 1.0         | 1.28          | 117                | 103 |                    | 108                     | 183                           | 195                 | 84                    |
| 3              | 16:22                     | 253.1            | 2.3         | 2.9           | 128                | 103 | 13                 | 188                     | 176                           | 194                 | 83                    |
| 4              | 16:25                     | 255.6            | 2.5         | 3.2           | 128                | 104 | 15                 | 188                     | 192                           | 215                 | 83                    |
| 5              | 16:28                     | 258.5            | 2.3         | 2.95          | 132                | 106 |                    | 186                     | 198                           | 230                 | 83                    |
| 6              | 16:31                     | 261.35           | 1.5         | 1.42          | 136                | 107 |                    | 186                     | 202                           | 230                 | 83                    |
| 7              | 16:34                     | 263.5            | .63         | .81           | 135                | 109 | 5                  | 180                     | 200                           | 230                 | 83                    |
| 8              | 16:37                     | 265.1            | .60         | .77           | 130                | 109 |                    | 170                     | 199                           | 217                 | 84                    |
| End            | 16:40                     | 266.546          |             |               |                    |     |                    |                         |                               |                     |                       |
| A-1            | 16:42                     | 266.546          | 1.3         | 1.65          | 126                | 109 |                    | 177                     | 183                           | 195                 | 86                    |
| 2              | 16:45                     |                  | 2.0         | 2.55          | 130                | 110 |                    | 188                     | 196                           | 190                 | 83                    |
| 3              | 16:48                     |                  | 3.5         | 4.48          | 138                | 111 |                    | 160                     | 182                           | 190                 | 83                    |
| 4              | 16:51                     | 274.6            | 3.5         | 4.48          | 138                | 112 |                    | 165                     | 187                           | 200                 | 83                    |
| 5              | 16:54                     | 277.8            | 2.8         | 3.6           | 140                | 112 |                    | 168                     | 189                           | 225                 | 83                    |
| 6              | 16:57                     | 280.9            | 2.4         | 3.07          | 143                | 113 | 13                 | 172                     | 195                           | 230                 | 84                    |
| 7              | 17:00                     | 283.6            | .75         | .96           | 141                | 103 | 5                  | 177                     | 143                           | 223                 | 84                    |
| *              | 0=                        | V=               | -----       | ΔH=           | T <sub>m</sub> =   |     |                    |                         |                               |                     | T <sub>s</sub> =      |

\* Sum, Average, or Difference

\* Pump could only manage 4.2 (Convert to) °F

$$V_m = V \text{ (DGMCF)} = (1.0)(45.27) = \text{ft}^3$$

## Other Data

| Time | Sample or<br>Measurement | Value |
|------|--------------------------|-------|
|      | Exhale O <sub>2</sub>    | 21    |
|      | CO <sub>2</sub>          | 0     |
|      | Orsat O <sub>2</sub>     | 21    |
|      | CO <sub>2</sub>          | 0     |

$$\text{Average CO}_2 = \frac{\%}{\%} \times \text{MW}/100 = \frac{\%}{\%} \times 0.44 =$$

$$\text{O}_2 = \frac{\%}{\%} \times 0.32 =$$

$$\text{N}_2 = \frac{\%}{\%} \times 0.28 =$$

$$100.0 = \text{dry MW}$$

Pre-Leak Check 0.00 ± 15"

Post Leak Check 0.01

Date 9/1/67 PITOBEE NO. \_\_\_\_\_  
 \_\_\_\_\_ CONSOLE NO. \_\_\_\_\_  
 Sample No. 3 Box No. \_\_\_\_\_  
 Probe Heater @ \_\_\_\_\_ Box Heater \_\_\_\_\_  
 Hose Heater @ \_\_\_\_\_ OF \_\_\_\_\_  
 Ambient Pressure (P<sub>bar</sub>) \_\_\_\_\_ "Hg

| Stack Pressure ( $P_s$ ) = $P_{bar} + P =$ "Hg | Operating Condition or Remarks |
|------------------------------------------------|--------------------------------|
| Dry Bulb °F                                    |                                |

[illegible]

(Convert to)  
OF

$$V_m = V \text{ (DGMCF)} = ( \quad ) ( \quad ) = \quad \text{ft}^3$$

| Time | Sample or Measurement | Value |
|------|-----------------------|-------|
|      |                       |       |
|      |                       |       |
|      |                       |       |
|      |                       |       |
|      |                       |       |

$$\text{Average CO}_2 = \frac{\%}{\times 0.44} \times \text{MW}/100 =$$

$$O_2 = \quad \times 0.32 =$$

$$N_2 = \quad \times 0.28 =$$

100.0 = dry MW

### Post Leak Check

CLIENT: GENERAL FOODS  
 SAMPLING DATE: 9/9/87  
 SAMPLING TIME: 1551-1700  
 UNIT SAMPLED: ROTO.INLET

Date: 09/21/87  
 Time: 9:44 AM  
 Run # 3

AVERAGE VELOCITY PRESSURE

| <u>Delta P</u><br><u>(IN H2O)</u> | <u>Delta P</u><br><u>Square Root</u> |
|-----------------------------------|--------------------------------------|
| 0.37                              | 0.61                                 |
| 0.24                              | 0.49                                 |
| 0.45                              | 0.67                                 |
| 0.55                              | 0.74                                 |
| 0.45                              | 0.67                                 |
| 0.15                              | 0.39                                 |
| 0.08                              | 0.28                                 |
| 0.03                              | 0.17                                 |
| 0.70                              | 0.84                                 |
| 1.00                              | 1.00                                 |
| 2.30                              | 1.52                                 |
| 2.50                              | 1.58                                 |
| 2.30                              | 1.52                                 |
| 1.50                              | 1.22                                 |
| 0.63                              | 0.79                                 |
| 0.60                              | 0.77                                 |
| 1.30                              | 1.14                                 |
| 2.00                              | 1.41                                 |
| 3.50                              | 1.87                                 |
| 3.50                              | 1.87                                 |
| 2.80                              | 1.67                                 |
| 2.40                              | 1.55                                 |
| 0.75                              | 0.87                                 |
| 0.65                              | 0.81                                 |

THE AVERAGE SQUARE ROOT OF DELTA P = 1.01915

CLIENT: GENERAL FOODS  
 SAMPLING DATE: 9/9/87  
 SAMPLING TIME: 1551-1700  
 UNIT SAMPLED: ROTO-INLET

Date: 09/21/87  
 Time: 9:44 AM  
 Run # 3

| Delta H<br>(IN H2O) | Meter Temp (F) |        | Stack Temp (F) |
|---------------------|----------------|--------|----------------|
|                     | IN             | OUT    |                |
| 0.47                | 98.00          | 99.00  | 86.00          |
| 0.31                | 99.00          | 99.00  | 83.00          |
| 0.58                | 103.00         | 100.00 | 81.00          |
| 0.70                | 107.00         | 100.00 | 84.00          |
| 0.58                | 110.00         | 100.00 | 82.00          |
| 0.19                | 112.00         | 100.00 | 83.00          |
| 0.10                | 110.00         | 100.00 | 83.00          |
| 0.04                | 110.00         | 102.00 | 83.00          |
| 0.89                | 111.00         | 102.00 | 83.00          |
| 1.28                | 117.00         | 103.00 | 83.00          |
| 2.90                | 123.00         | 103.00 | 83.00          |
| 3.20                | 128.00         | 104.00 | 83.00          |
| 2.95                | 132.00         | 106.00 | 83.00          |
| 1.92                | 136.00         | 107.00 | 84.00          |
| 0.81                | 135.00         | 109.00 | 83.00          |
| 0.77                | 130.00         | 110.00 | 83.00          |
| 1.65                | 126.00         | 109.00 | 83.00          |
| 2.55                | 130.00         | 110.00 | 86.00          |
| 4.48                | 138.00         | 111.00 | 83.00          |
| 4.48                | 138.00         | 112.00 | 83.00          |
| 3.60                | 140.00         | 112.00 | 83.00          |
| 3.07                | 143.00         | 113.00 | 84.00          |
| 0.96                | 141.00         | 103.00 | 84.00          |
| 0.83                | 136.00         | 114.00 | 83.00          |

AVERAGES

DELTA H = 1.637917 IN H2O  
 METER TEMP. = 114.1875 F  
 STACK TEMP. = 83.29166 F

# Water and Dry Particulate Collections

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PLANT MAXWELL HOUSE  
TEST FOR Particulate  
SAMPLE NO. 3 BOX NO. 3

STACK ROTO. IN.  
DATE 9/9/81  
OPERATING CONDITION \_\_\_\_\_

|            | Grams                                                                      | Grams                  |
|------------|----------------------------------------------------------------------------|------------------------|
| Impinger 1 | Final Weight <u>671.2</u><br>Initial Weight <u>669.4</u><br>Increase _____ | Impinger 1 <u>1.8</u>  |
| Impinger 2 | Final Weight <u>693.5</u><br>Initial Weight <u>684.6</u><br>Increase _____ | Impinger 2 <u>8.9</u>  |
| Impinger 3 | Final Weight <u>502.3</u><br>Initial Weight <u>502.0</u><br>Increase _____ | Impinger 3 <u>0.3</u>  |
| Silica Gel | Final Weight <u>768.7</u><br>Initial Weight <u>750.2</u><br>Increase _____ | Silica Gel <u>18.5</u> |

Record Water Collected  
in cyclone, flash, if any:

Final Weight \_\_\_\_\_ gms  
Initial Weight \_\_\_\_\_ gms  
Increase \_\_\_\_\_ gms

29.5 grams

Total mass of water caught

Filter Diameter 4 inches

Filter Type Glass Fiber

Filter Final Weight .6353  
Initial Weight .6167  
Increase \_\_\_\_\_

0.0186 gram

Total mass of particulate  
caught on filter

Is ice present in the impinger bath at the end of this sample?  
Yes ✓ No \_\_\_\_\_

RECON SYSTEMS, INC.  
Three Bridges NJ

Lab Data - Evaporations

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PLANT MAXWELL HOUSE STACK ROTO INLET SAMPLE NO. 3 FOR Particulate

SAMPLING DATE 9/9/87 OPERATING CONDITION \_\_\_\_\_

Acetone Washings

Gross 530.6 GMS

TOTAL

SAMPLE Tare- 342.5 GMS

(A) Net 188.1 GMS

AMOUNT

EVAPORATED 188.1 GMS (B)

Evap. Beaker NO.

Gross 99.6203 GMS

Tare- 99.6179 GMS

Net 0.0024 (C) GMS

Acetone Blank = 0 GMS  
(D) 100 GMS

Corrected

Net = (C) - (B) (D)  
(E)

$$= \frac{0.0024}{188.1} - \frac{0}{100}$$

$$= \frac{0.0024}{188.1} \text{ GMS}$$

Scaled Up

Net = (E)  $\frac{A}{B}$

$$= \frac{0.0024}{188.1} \left( \frac{188.1}{188.1} \right)$$

$$= \frac{0.0024}{188.1} \text{ GMS}$$

Wet Catch

Gross \_\_\_\_\_ GMS

TOTAL SAMPLE Tare- \_\_\_\_\_ GMS

(F) Net \_\_\_\_\_ GMS

AMOUNT  
EXTRACTED

(G) \_\_\_\_\_ GMS (mls)

Water Phase

Evap. Beaker No. \_\_\_\_\_

Gross \_\_\_\_\_ GMS

Tare- \_\_\_\_\_ GMS

Net \_\_\_\_\_ (J) GMS

Water Blank \_\_\_\_\_ GMS  
(L) =  $\frac{\text{GMS}}{100 \text{ GMS}}$

Corrected  
Net (N) = J - (G) (L)

$$= \frac{\text{GMS}}{100}$$

= \_\_\_\_\_ GMS

Scaled Up Net = N  $\left( \frac{F}{G} \right)$

$$= \frac{\text{GMS}}{\text{GMS}}$$

AMOUNT  
of E/C

mls (H)

E/C Phase

Evap. Beaker No. \_\_\_\_\_

Gross \_\_\_\_\_ GMS

Tare- \_\_\_\_\_ GMS

Net \_\_\_\_\_ (K) GMS

E/C Blank \_\_\_\_\_ GMS  
(M) =  $\frac{\text{GMS}}{100 \text{ mls}}$

Corrected  
Net (P) = K - H (M)

$$= \frac{\text{GMS}}{100}$$

= \_\_\_\_\_ GMS

Scaled Up Net = P  $\left( \frac{F}{G} \right)$

$$= \frac{\text{GMS}}{\text{GMS}}$$

## Particulates

Nozzle, Probe, and Acetone Washing .0024 grms

Filter .0186 grms

.0034.0310-----  
Enter "0" if no Organic or Aqueous Phase

Aqueous Phase 0 grms

Organic Phase 0 grms

## Totals

GRAINS/DSCF = 7.756192E-03

POUNDS/HOUR = .2373201

HIT RETURN TO CONTINUE

CLIENT: GENERAL FOODS

Date: 09/21/87

Time: 9:44 AM

## ISOKINETIC CALCULATIONS

| SAMPLE NO.                                   | 1           | 2           | 3           |
|----------------------------------------------|-------------|-------------|-------------|
| DATE                                         | 9/9/87      | 9/9/87      | 9/9/87      |
| TIME                                         | 1116-1229   | 1346-1303   | 1551-1700   |
| UNIT SAMPLED                                 | ROTO. INLET | ROTO. INLET | ROTO. INLET |
| METER VOLUME<br>(VM-STD), SCU-FT             | 38.97       | 39.44       | 41.78       |
| WATER COLLECTED<br>(VW-STD), SCU-FT          | 0.96        | 0.99        | 1.40        |
| MOISTURE (VOL %)                             | 2.41        | 2.45        | 3.23        |
| ACTUAL MOLECULAR WEIGHT<br>(MW), LBS/LB-MOLE | 28.58       | 28.58       | 28.49       |
| ACTUAL VELOCITY<br>IN STACK<br>(VS), FT/SEC  | 53.86       | 55.17       | 59.24       |
| ACTUAL FLOW RATE<br>IN STACK<br>(ACFM)       | 3457.98     | 3542.23     | 3803.01     |
| VELOCITY @ STP<br>(VS-STD), FT/SEC           | 52.44       | 53.53       | 57.46       |
| STACK FLOW RATE<br>@ STP<br>(SCFM)           | 3366.94     | 3436.58     | 3689.01     |
| DRY FLOW RATE<br>(DSCFM)                     | 3285.92     | 3352.49     | 3569.72     |
| NOZZLE VELOCITY<br>@ STP<br>(VN-STD), FT/SEC | 48.20       | 48.81       | 52.13       |
| ISOKINETIC %                                 | 91.92       | 91.18       | 90.72       |

CLIENT: GENERAL FOODS

Date: 09/21/87

Time: 9:44 AM

THE FOLLOWING WERE PROGRAMMER INPUTS FOR ISOKINETICS

| SAMPLE NO.                                           | 1           | 2           | 3           |
|------------------------------------------------------|-------------|-------------|-------------|
| DATE                                                 | 9/9/87      | 9/9/87      | 9/9/87      |
| TIME                                                 | 1116-1229   | 1346-1303   | 1551-1700   |
| UNIT SAMPLED                                         | ROTO. INLET | ROTO. INLET | ROTO. INLET |
| ACTUAL NOZZLE<br>DIAMETER (ND), IN                   | 0.19        | 0.19        | 0.19        |
| PITOT FACTOR (CP)                                    | 0.85        | 0.85        | 0.85        |
| TIME @ EACH<br>POINT (MIN)                           | 3.00        | 3.00        | 3.00        |
| AMBIENT PRESSURE<br>(PBAR), IN-HG                    | 29.90       | 29.90       | 29.90       |
| STACK PRESSURE<br>(PS), IN-HG                        | -2.10       | -2.00       | -2.00       |
| METER VOLUME<br>(VM), CU-FT                          | 41.97       | 42.40       | 45.27       |
| WATER COLLECTED<br>IMPINGERS, GRMS                   | 20.30       | 20.90       | 29.50       |
| CARBON DIOXIDE<br>(CO <sub>2</sub> ), %              | 0.00        | 0.00        | 0.00        |
| OXYGEN<br>(O <sub>2</sub> ), %                       | 21.00       | 21.00       | 21.00       |
| STACK DIAMETER<br>(DIA), IN                          | 14.00       | 14.00       | 14.00       |
| STACK CROSS SECTIONAL<br>AREA (CSA), FT <sup>2</sup> | 1.07        | 1.07        | 1.07        |

# RECON SYSTEMS INC.

ROUTE 202N, P.O. BOX 460, THREE BRIDGES, N.J. 08887  
201-782-5900

-62-

DAILY  
FIELD  
SAMPLING  
RECORD

## PARTICULATE STACK SAMPLING DATA BOOK

Date 9/9/87  
Jobsite  
Company GENERAL FOODS

City Hoboken State NJ

CLIENT Ernie Lasal  
RECON Job # 0359  
FIELD Supervisor P. MARSHALL

Street 1127 Hudson St.

Zip 07030

### Processes, Stacks, Sites, etc. Tested:

1. OUTLET Condition\* STEADY
2. \_\_\_\_\_ Condition\* \_\_\_\_\_
3. \_\_\_\_\_ Condition\* \_\_\_\_\_
4. \_\_\_\_\_ Condition\* \_\_\_\_\_

• (e.g. stack opacity, raining?, water odor, color, flowrate;  
process steady or upset; etc.)

### Milestone Times (Military)

Arrival 800 Lost Time —

Lunch 12<sup>30</sup> to 13<sup>15</sup>

Departure 1830

Reasons For Lost Time \_\_\_\_\_

Client or Jobsite Representative Aware of Lost Time \_\_\_\_\_

### Personnel Onsite

RECON: PFM, Tfm, CDR, JDK, \_\_\_\_\_, \_\_\_\_\_

\_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_

\_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_

Client: \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_

Jobsite Reps: \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_

Agencies Observing (1) WJDEP (2) WJDEP

Agency Personnel (1) TOM BROWN, Beth Rossi, \_\_\_\_\_

(2) \_\_\_\_\_, \_\_\_\_\_, \_\_\_\_\_

# Particulate Sampling Field Data

Plant MAXWELL  
Stack OUTLET  
Nozzle Size 3/16"  
Time @ Each Point (t) 3 Min  
Ambient Temperature 95 °F

Date 9-9-87  
Sample No. 1 Box No. 4  
Probe Heater @ 8 Box Heater @ 8 °F  
Hose Heater @ 8 °F  
Ambient Pressure (P<sub>bar</sub>) 29.90 "Hg

NO. 34  
THERM. NO. 32  
PITOT NO. 7  
CONSOLE NO. 4

Stack Pressure (P) +1.45 "H<sub>2</sub>O (gage) ÷ 13.6 = "Hg (gage)

Stack Pressure (P<sub>s</sub>) = P<sub>bar</sub> + P = "Hg

Dry Bulb °F

Wet Bulb °F %H<sub>2</sub>O

Operating Condition or Remarks

| Port/<br>Point | Military<br>Clock<br>Time | Meter<br>Reading | Pitot<br>ΔP | Orifice<br>ΔH | Meter<br>Temp (°F) |     | Line<br>Vac<br>"Hg | Probe<br>Outlet<br>Temp (°F) | Box<br>Outlet<br>Temp (°F) | Box<br>Temp<br>(°F) | Stack<br>Temp<br>°F/°C |
|----------------|---------------------------|------------------|-------------|---------------|--------------------|-----|--------------------|------------------------------|----------------------------|---------------------|------------------------|
|                |                           |                  |             |               | IN                 | OUT |                    |                              |                            |                     |                        |
| A-1            | 11 15                     | 924.384          | 1.20        | 1.55          | 87                 | 87  | 4+                 | 99                           | 159                        | 222                 | 80                     |
| 2              | 18                        | 926.3            | 1.20        | 1.55          | 89                 | 87  | 4+                 | 99                           | 163                        | 220                 | 80                     |
| 3              | 21                        | 928.3            | 1.10        | 1.40          | 91                 | 87  | 4+                 | 101                          | 185                        | 223                 | 80                     |
| 4              | 24                        | 930.2            | 1.00        | 1.30          | 94                 | 88  | 4+                 | 133                          | 191                        | 226                 | 80                     |
| 5              | 27                        | 932.1            | 1.00        | 1.30          | 95                 | 88  | 4                  | 120                          | 192                        | 220                 | 80                     |
| 6              | 30                        | 933.9            | .93         | 1.25          | 96                 | 88  | 3+                 | 128                          | 192                        | 223                 | 79                     |
| 7              | 33                        | 936.2            | .93         | 1.25          | 97                 | 88  | 3+                 | 131                          | 196                        | 221                 | 79                     |
| 8              | 36                        | 937.7            | .85         | 1.10          | 97                 | 89  | 3+                 | 125                          | 192                        | 218                 | 80                     |
| 9              | 39                        | 939.3            | .80         | 1.05          | 97                 | 89  | 3+                 | 135                          | 189                        | 215                 | 78                     |
| 10             | 42                        | 940.7            | .80         | 1.05          | 97                 | 89  | 3+                 | 137                          | 188                        | 217                 | 80                     |
| 11             | 45                        | 942.7            | .85         | 1.10          | 98                 | 90  | 3+                 | 141                          | 183                        | 219                 | 80                     |
| 12             | 48                        | 944.2            | .72         | .95           | 98                 | 90  | 3+                 | 142                          | 185                        | 220                 | 79                     |
| END            | 11 51                     | 945.770          |             |               |                    |     |                    |                              |                            |                     |                        |
| A-1            | 11 54                     | 945.770          | 1.30        | 1.70          | 94                 | 90  | 5                  | 125                          | 186                        | 219                 | 80                     |
| 2              | 57                        | 947.5            | 1.30        | 1.70          | 95                 | 90  | 5                  | 151                          | 187                        | 220                 | 81                     |
| 3              | 12 00                     | 949.7            | 1.20        | 1.55          | 96                 | 90  | 4+                 | 191                          | 189                        | 221                 | 80                     |
| 4              | 03                        | 951.6            | 1.10        | 1.40          | 97                 | 90  | 4+                 | 212                          | 208                        | 223                 | 80                     |
| 5              | 06                        | 953.8            | 1.15        | 1.50          | 98                 | 90  | 4+                 | 168                          | 209                        | 225                 | 79                     |
| 6              | 09                        | 955.5            | 1.15        | 1.50          | 98                 | 90  | 4+                 | 170                          | 208                        | 223                 | 80                     |
| 7              | 12                        | 957.4            | .98         | 1.30          | 99                 | 91  | 4+                 | 180                          | 210                        | 220                 | 79                     |
| 8              | 15                        | 959.4            | .90         | 1.20          | 99                 | 91  | 3+                 | 200                          | 211                        | 223                 | 80                     |
| 9              | 18                        | 960.9            | .87         | 1.15          | 99                 | 91  | 3+                 | 153                          | 212                        | 225                 | 80                     |
| 10             | 21                        | 962.5            | .85         | 1.13          | 99                 | 91  | 3+                 | 176                          | 210                        | 223                 | 79                     |
| 11             | 24                        | 964.6            | .83         | 1.10          | 99                 | 91  | 3+                 | 179                          | 208                        | 220                 | 78                     |
| 12             | 27                        | 966.0            | .85         | 1.13          | 99                 | 91  | 3+                 | 180                          | 200                        | 219                 | 78                     |
| END            | 12 30                     | 967.844          | -----       | ΔH=           | T <sub>m</sub> =   |     |                    |                              |                            |                     | T <sub>s</sub> =       |

\* Sum, Average, or Difference

(Convert to)  
°F

$$V_m = V \text{ (DGMCF)} = (1.0) (43.469) = 43.460 \text{ ft}^3$$

Other Data

| Time | Sample or<br>Measurement | Value |
|------|--------------------------|-------|
|      | FWTTE 02                 | 21    |
|      | CO2                      | 0     |
|      |                          |       |
|      |                          |       |
|      |                          |       |

$$\text{Average CO}_2 = \frac{\%}{x 0.44} =$$

$$\text{O}_2 = \frac{\%}{x 0.32} =$$

$$\text{N}_2 = \frac{\%}{x 0.28} =$$

100.0

= dry MW

Pre-Leak Check 0.018 ± 10"

Post Leak Check 0.019 ± 5"

CLIENT: GENERAL FOODS

Date: 09/21/87

Time: 9:53 AM

AVERAGE VELOCITY PRESSURE

| Delta P<br>(IN H2O) | Delta P<br>Square Root |
|---------------------|------------------------|
| 1.20                | 1.10                   |
| 1.20                | 1.10                   |
| 1.10                | 1.05                   |
| 1.00                | 1.00                   |
| 1.00                | 1.00                   |
| 0.93                | 0.96                   |
| 0.93                | 0.96                   |
| 0.85                | 0.92                   |
| 0.80                | 0.89                   |
| 0.80                | 0.89                   |
| 0.85                | 0.92                   |
| 0.72                | 0.85                   |
| 1.30                | 1.14                   |
| 1.30                | 1.14                   |
| 1.20                | 1.10                   |
| 1.10                | 1.05                   |
| 1.15                | 1.07                   |
| 1.15                | 1.07                   |
| 0.98                | 0.99                   |
| 0.90                | 0.95                   |
| 0.87                | 0.93                   |
| 0.85                | 0.92                   |
| 0.83                | 0.91                   |
| 0.85                | 0.92                   |

THE AVERAGE SQUARE ROOT OF DELTA P = .9935587

CLIENT: GENERAL FOODS

Date: 09/21/87

Time: 9:53 AM

| Delta H<br>(IN H2O) | Meter Temp (F) |       | Stack Temp (F) |
|---------------------|----------------|-------|----------------|
|                     | IN             | OUT   |                |
| 1.55                | 87.00          | 87.00 | 80.00          |
| 1.55                | 89.00          | 87.00 | 80.00          |
| 1.40                | 91.00          | 87.00 | 80.00          |
| 1.30                | 94.00          | 88.00 | 80.00          |
| 1.30                | 95.00          | 88.00 | 80.00          |
| 1.25                | 96.00          | 88.00 | 79.00          |
| 1.25                | 97.00          | 88.00 | 79.00          |
| 1.10                | 97.00          | 89.00 | 80.00          |
| 1.05                | 97.00          | 89.00 | 78.00          |
| 1.05                | 97.00          | 89.00 | 80.00          |
| 1.10                | 98.00          | 90.00 | 80.00          |
| 0.95                | 98.00          | 90.00 | 79.00          |
| 1.70                | 94.00          | 90.00 | 80.00          |
| 1.70                | 95.00          | 90.00 | 81.00          |
| 1.55                | 96.00          | 90.00 | 80.00          |
| 1.40                | 97.00          | 90.00 | 80.00          |
| 1.50                | 98.00          | 90.00 | 79.00          |
| 1.50                | 98.00          | 90.00 | 80.00          |
| 1.30                | 99.00          | 91.00 | 79.00          |
| 1.20                | 99.00          | 91.00 | 80.00          |
| 1.15                | 99.00          | 91.00 | 80.00          |
| 1.13                | 99.00          | 91.00 | 79.00          |
| 1.10                | 99.00          | 91.00 | 78.00          |
| 1.13                | 99.00          | 91.00 | 78.00          |

AVERAGES

DELTA H = 1.300417 IN H2O

METER TEMP. = 92.79166 F

STACK TEMP. = 79.54166 F

# Water and Dry Particulate Collections

-66-

PLANT General Foods  
 TEST FOR Particulate  
 SAMPLE NO. 1 BOX NO.

STACK ROTO. OUT.  
 DATE 9-9-87  
 OPERATING CONDITION

|            | Grams                                                                        | Grams                  |
|------------|------------------------------------------------------------------------------|------------------------|
| Impinger 1 | Final Weight <u>666.9</u><br>Initial Weight <u>669.3</u><br>Increase <u></u> | Impinger 1 <u>-2.4</u> |
| Impinger 2 | Final Weight <u>706.2</u><br>Initial Weight <u>696.3</u><br>Increase <u></u> | Impinger 2 <u>9.9</u>  |
| Impinger 3 | Final Weight <u>507.1</u><br>Initial Weight <u>503.2</u><br>Increase <u></u> | Impinger 3 <u>3.9</u>  |
| Silica Gel | Final Weight <u>784.7</u><br>Initial Weight <u>769.4</u><br>Increase <u></u> | Silica Gel <u>15.3</u> |

~~Record Water Collected  
in cyclone, flash, if any:~~

~~Final Weight  gms  
 Initial Weight  gms  
 Increase  gms~~

26.7 grams  
 Total mass of water caught

Filter Diameter 4 inches  
 Filter Type Glass Fiber

Filter Final Weight .6318  
 Initial Weight .6311  
 Increase

0.0007 gram  
 Total mass of particulate  
 caught on filter

Is ice present in the impinger bath at the end of this sample?  
 Yes ✓ No

RECON SYSTEMS, INC.  
 Three Bridges NJ

Lab Data - Evaporations

PLANT Maxwell House STACK Roto. Out. SAMPLE NO. 1 FOR Particulates

SAMPLING DATE 9/6/87 OPERATING CONDITION \_\_\_\_\_

Acetone Washings

Gross 519.8 GMS

TOTAL

SAMPLE Tare- 342.2 GMS

(A) Net 177.6 GMS

AMOUNT

EVAPORATED 177.6 GMS (B)

Evap. Beaker NO. \_\_\_\_\_

Gross 101.2209 GMS

Tare- 101.2200 GMS

Net 0.0009 (C) GMS

Acetone Blank = 0 GMS

(D) 100 GMS

Corrected

Net = (C) - (B) (D)

(E)

$$= \frac{0.0009}{0.0009} - \frac{177.6}{100} \left( \frac{0}{100} \right)$$

$$= 0.0009 \text{ GMS}$$

Scaled Up

Net = (E)  $\frac{A}{B}$

$$= \frac{0.0009}{0.0009} \left( \frac{177.6}{177.6} \right)$$

$$= 0.0009 \text{ GMS}$$

Wet Catch

Gross \_\_\_\_\_ GMS

TOTAL

SAMPLE Tare- \_\_\_\_\_ GMS

(F) Net \_\_\_\_\_ GMS

AMOUNT

EXTRACTED

(G) \_\_\_\_\_ GMS (mls)

Water Phase

Evap. Beaker No. \_\_\_\_\_

Gross \_\_\_\_\_ GMS

Tare- \_\_\_\_\_ GMS

Net \_\_\_\_\_ (J) GMS

Water Blank

(L) =  $\frac{\text{GMS}}{100 \text{ GMS}}$

Corrected

Net (N) = J - (G) (L)

$$= \frac{\text{GMS}}{100}$$

= \_\_\_\_\_ GMS

Scaled Up Net =  $N \left( \frac{F}{G} \right)$

$$= \frac{\text{GMS}}{\text{GMS}}$$

AMOUNT

of E/C

mls (H)

E/C Phase

Evap. Beaker No. \_\_\_\_\_

Gross \_\_\_\_\_ GMS

Tare- \_\_\_\_\_ GMS

Net \_\_\_\_\_ (K) GMS

E/C Blank

(M) =  $\frac{\text{GMS}}{100 \text{ mls}}$

Corrected

Net (P) = K - H (M)

$$= \frac{\text{GMS}}{100}$$

= \_\_\_\_\_ GMS

Scaled Up Net =  $P \left( \frac{F}{G} \right)$

$$= \frac{\text{GMS}}{\text{GMS}}$$

## Particulates

Nozzle, Probe, and Acetone Washing .0009 grms

Filter .0007 grms

.0009.0016-----  
Enter "0" if no Organic or Aqueous Phase

Aqueous Phase 0 grms

Organic Phase 0 grms

## Totals

GRAINS/DSCF = 5.931919E-04

POUNDS/HOUR = 1.745396E-02

HIT RETURN TO CONTINUE

THERM NO. 32

NOZZLE NO. 34

PITOT NO. 7

CONSOLE NO. 4

## Particulate Sampling Field Data

Plant Genl Foods  
 Stack OUTLET  
 Nozzle Size 3/16"  
 Time @ Each Point (0) 3 Min  
 Ambient Temperature 80 °F

Date 9/6/81  
 Sample No. 2 Box No. 4  
 Probe Heater @      % Box Heater @      %  
 Hose Heater @      %  
 Ambient Pressure (P<sub>bar</sub>) 29.90 "Hg

Stack Pressure (P) +1.30 "H<sub>2</sub>O (gage) ÷ 13.6 = "Hg (gage)

Stack Pressure (P<sub>s</sub>) = P<sub>bar</sub> + P = "Hg  
 Dry Bulb °F  
 Wet Bulb °F %H<sub>2</sub>O

Operating Condition or  
Remarks

| Port/<br>Point | Military<br>Clock<br>Time | Meter<br>Reading | Pitot<br>ΔP | Orifice<br>ΔH | Meter<br>Temp (°F)<br>IN OUT | Line<br>Vac<br>"Hg | Probe<br>Outlet<br>Temp (°F) | Box<br>Outlet<br>Temp (°F) | Box<br>Temp<br>°F | Stack<br>Temp<br>°F |
|----------------|---------------------------|------------------|-------------|---------------|------------------------------|--------------------|------------------------------|----------------------------|-------------------|---------------------|
| A-1            | 1345                      | 968.000          | 1.20        | 1.60          | 88 88                        | 5                  | 85                           | 108                        | 185               | 80                  |
| 2              | 48                        | 970.1            | 1.30        | 1.70          | 90 88                        | 5+                 | 150                          | 127                        | 200               | 79                  |
| 3              | 51                        | 972.4            | 1.35        | 1.80          | 92 88                        | 5+                 | 165                          | 138                        | 210               | 79                  |
| 4              | 54                        | 974.7            | 1.75        | 1.50          | 93 89                        | 4+                 | 166                          | 146                        | 213               | 79                  |
| 5              | 57                        | 976.5            | 1.15        | 1.50          | 95 89                        | 4+                 | 191                          | 152                        | 220               | 79                  |
| 6              | 1400                      | 978.3            | 1.10        | 1.90          | 96 89                        | 4+                 | 220                          | 168                        | 223               | 79                  |
| 7              | 03                        | 980.5            | 1.00        | 1.30          | 97 90                        | 4+                 | 173                          | 170                        | 220               | 79                  |
| 8              | 06                        | 981.8            | .90         | 1.20          | 98 90                        | 4                  | 182                          | 185                        | 218               | 79                  |
| 9              | 09                        | 983.7            | 1.00        | 1.30          | 99 90                        | 4+                 | 215                          | 191                        | 215               | 80                  |
| 10             | 12                        | 985.6            | .90         | 1.20          | 99 91                        | 4+                 | 211                          | 205                        | 221               | 79                  |
| 11             | 15                        | 987.4            | .85         | 1.10          | 99 91                        | 3+                 | 198                          | 204                        | 222               | 79                  |
| 12             | 18                        | 989.0            | .70         | .93           | 100 91                       | 4                  | 197                          | 198                        | 220               | 79                  |
| END            | 1421                      | 990.392          |             |               |                              |                    |                              |                            |                   |                     |
| B-1            | 1423                      | 990.392          | 1.10        | 1.40          | 98 91                        | 4+                 | 198                          | 200                        | 223               | 79                  |
| 2              | 26                        | 992.3            | 1.30        | 1.70          | 98 91                        | 6+                 | 200                          | 201                        | 224               | 82                  |
| 3              | 29                        | 994.1            | 1.30        | 1.70          | 99 92                        | 6+                 | 188                          | 204                        | 222               | 82                  |
| 4              | 32                        | 996.8            | 1.20        | 1.60          | 99 91                        | 5+                 | 185                          | 203                        | 220               | 82                  |
| 5              | 35                        | 998.8            | 1.20        | 1.60          | 100 92                       | 5+                 | 189                          | 204                        | 219               | 82                  |
| 6              | 38                        | 001.1            | 1.10        | 1.40          | 102 92                       | 5+                 | 175                          | 205                        | 218               | 81                  |
| 7              | 41                        | 002.9            | 1.0         | 1.30          | 102 92                       | 5+                 | 180                          | 203                        | 220               | 80                  |
| 8              | 44                        | 004.6            | .95         | 1.25          | 103 92                       | 4+                 | 185                          | 202                        | 219               | 82                  |
| 9              | 47                        | 005.9            | .90         | 1.20          | 103 93                       | 4+                 | 183                          | 204                        | 221               | 81                  |
| 10             | 50                        | 008.0            | .78         | 1.00          | 104 93                       | 3+                 | 182                          | 205                        | 224               | 80                  |
| 11             | 53                        | 009.9            | .78         | 1.00          | 106 94                       | 3+                 | 185                          | 208                        | 223               | 80                  |
| 12             | 56                        | 011.7            | .78         | 1.00          | 106 94                       | 3+                 | 186                          | 209                        | 225               | 81                  |
| END            | 1439                      | 012.988          | ----        | ΔH=           | T <sub>m</sub> =             |                    |                              |                            |                   | T <sub>s</sub> =    |

\* Sum, Average, or Difference

(Convert to)  
°F

$$V_m = V \text{ (DGMCF)} = (1.0) (44.988) = 44.988 \text{ ft}^3$$

## Other Data

| Time | Sample or<br>Measurement | Value |
|------|--------------------------|-------|
|      | O <sub>2</sub>           | 21    |
|      | CO <sub>2</sub>          | 0     |
|      |                          |       |
|      |                          |       |
|      |                          |       |

$$\text{Average CO}_2 = \frac{\%}{100} \times \text{MW}/100 = \frac{\%}{100} \times 0.44 =$$

$$\text{O}_2 = \frac{\%}{100} \times 0.32 =$$

$$\text{N}_2 = \frac{\%}{100} \times 0.28 =$$

100.0

= dry MW

Pre-Leak Check 0.013 at 15"

Post Leak Check 0.013 at 7"

CLIENT: GENERAL FOODS

Date: 09/21/87

Time: 9:53 AM

AVERAGE VELOCITY PRESSURE

| <u>Delta P</u><br><u>(IN H2O)</u> | <u>Delta P</u><br><u>Square Root</u> |
|-----------------------------------|--------------------------------------|
| 1.20                              | 1.10                                 |
| 1.30                              | 1.14                                 |
| 1.35                              | 1.16                                 |
| 1.15                              | 1.07                                 |
| 1.15                              | 1.07                                 |
| 1.10                              | 1.05                                 |
| 1.00                              | 1.00                                 |
| 0.90                              | 0.95                                 |
| 1.00                              | 1.00                                 |
| 0.90                              | 0.95                                 |
| 0.85                              | 0.92                                 |
| 0.70                              | 0.84                                 |
| 1.10                              | 1.05                                 |
| 1.30                              | 1.14                                 |
| 1.30                              | 1.14                                 |
| 1.20                              | 1.10                                 |
| 1.20                              | 1.10                                 |
| 1.10                              | 1.05                                 |
| 1.00                              | 1.00                                 |
| 0.95                              | 0.97                                 |
| 0.90                              | 0.95                                 |
| 0.78                              | 0.88                                 |
| 0.78                              | 0.88                                 |
| 0.78                              | 0.88                                 |

THE AVERAGE SQUARE ROOT OF DELTA P = 1.016201

CLIENT: GENERAL FOODS

Date: 09/21/87

Time: 9:53 AM

| Delta H<br>(IN H2O) | Meter Temp (F) |       | Stack Temp (F) |
|---------------------|----------------|-------|----------------|
|                     | IN             | OUT   |                |
| 1.60                | 88.00          | 88.00 | 80.00          |
| 1.70                | 90.00          | 88.00 | 79.00          |
| 1.80                | 92.00          | 88.00 | 79.00          |
| 1.50                | 93.00          | 89.00 | 79.00          |
| 1.50                | 95.00          | 89.00 | 79.00          |
| 1.40                | 96.00          | 89.00 | 79.00          |
| 1.30                | 99.00          | 90.00 | 80.00          |
| 1.20                | 98.00          | 90.00 | 79.00          |
| 1.30                | 99.00          | 90.00 | 80.00          |
| 1.20                | 99.00          | 91.00 | 79.00          |
| 1.10                | 99.00          | 91.00 | 79.00          |
| 0.93                | 100.00         | 91.00 | 79.00          |
| 1.40                | 98.00          | 91.00 | 79.00          |
| 1.70                | 98.00          | 91.00 | 82.00          |
| 1.70                | 99.00          | 91.00 | 82.00          |
| 1.60                | 99.00          | 91.00 | 82.00          |
| 1.60                | 100.00         | 92.00 | 81.00          |
| 1.40                | 100.00         | 92.00 | 81.00          |
| 1.30                | 102.00         | 92.00 | 80.00          |
| 1.25                | 103.00         | 92.00 | 82.00          |
| 1.20                | 103.00         | 93.00 | 81.00          |
| 1.00                | 104.00         | 93.00 | 80.00          |
| 1.00                | 106.00         | 94.00 | 80.00          |
| 1.00                | 106.00         | 94.00 | 81.00          |

AVERAGES

DELTA H = 1.361667 IN H2O

METER TEMP. = 94.70834 F

STACK TEMP. = 80.08335 F

# Water and Dry Particulate Collections

-72-

PLANT MAXWELL HOUSE  
TEST FOR Particulates  
SAMPLE NO. 2 BOX NO. 4

STACK ROTO-047  
DATE 9/9/71  
OPERATING CONDITION \_\_\_\_\_

|            | Grams                                                                      | Grams                 |
|------------|----------------------------------------------------------------------------|-----------------------|
| Impinger 1 | Final Weight <u>671.0</u><br>Initial Weight <u>661.1</u><br>Increase _____ | Impinger 1 <u>9.9</u> |
| Impinger 2 | Final Weight <u>708.8</u><br>Initial Weight <u>703.3</u><br>Increase _____ | Impinger 2 <u>5.5</u> |
| Impinger 3 | Final Weight <u>505.2</u><br>Initial Weight <u>503.9</u><br>Increase _____ | Impinger 3 <u>1.3</u> |
| Silica Gel | Final Weight <u>787.8</u><br>Initial Weight <u>778.2</u><br>Increase _____ | Silica Gel <u>9.6</u> |

~~Record Water collected  
in cyclone, flash, if any:~~

~~Final Weight \_\_\_\_\_ gms  
Initial Weight \_\_\_\_\_ gms  
Increase \_\_\_\_\_ gms~~

26.3 grams

Total mass of water caught

Filter Diameter 4 inches

Filter Type Glass Fiber

Filter Final Weight 6406  
Initial Weight 6398  
Increase \_\_\_\_\_

0.0008 gram

Total mass of particulate  
caught on filter

Is ice present in the impinger bath at the end of this sample?  
Yes ✓ No \_\_\_\_\_

RECON SYSTEMS, INC.  
Three Bridges NJ

Lab Data - Evaporations

-73-

PLANT MAXWELL House STACK ROTO. OUT SAMPLE NO. 2 FOR Particulates

SAMPLING DATE 9/1/87 OPERATING CONDITION \_\_\_\_\_

Acetone Washings

Gross 504.4 GMS

TOTAL

SAMPLE Tare- 339.2 GMS

(A) Net 165.2 GMS

AMOUNT

EVAPORATED 165.2 GMS (B)

Evap. Beaker NO.

Gross 103.7559 GMS

Tare- 103.7554 GMS

Net 0.0005 (C) GMS

Acetone Blank = 0 GMS  
(D) 100 GMS

Corrected

Net = (C) - (B) (D)  
(E)

$$= \frac{0.0005 - 165.2}{100}$$

$$= \frac{0.0005}{100} \text{ GMS}$$

Scaled Up

Net = (E)  $\frac{A}{B}$

$$= \frac{0.0005}{165.2} \left( \frac{165.2}{165.2} \right)$$

$$= \frac{0.0005}{165.2} \text{ GMS}$$

Wet Catch

Gross \_\_\_\_\_ GMS

TOTAL

SAMPLE

Tare- \_\_\_\_\_ GMS

(F) Net \_\_\_\_\_ GMS

AMOUNT

of E/C \_\_\_\_\_ mls (H)

(G) \_\_\_\_\_ GMS (mls)

Water Phase

Evap. Beaker No. \_\_\_\_\_

Gross \_\_\_\_\_ GMS

Tare- \_\_\_\_\_ GMS

Net \_\_\_\_\_ (J) GMS

Water Blank

(L) =  $\frac{\text{GMS}}{100 \text{ GMS}}$

Corrected

Net (N) = J - (G) (L)

$$= \frac{\text{GMS}}{100}$$

= \_\_\_\_\_ GMS

Scaled Up Net = N  $\left( \frac{F}{G} \right)$

$$= \frac{\text{GMS}}{\text{GMS}}$$

= \_\_\_\_\_ GMS

E/C Phase

Evap. Beaker No. \_\_\_\_\_

Gross \_\_\_\_\_ GMS

Tare- \_\_\_\_\_ GMS

Net \_\_\_\_\_ (K) GMS

E/C Blank

(M) =  $\frac{\text{GMS}}{100 \text{ mls}}$

Corrected

Net (P) = K - H (M)

$$= \frac{\text{GMS}}{100}$$

= \_\_\_\_\_ GMS

Scaled Up Net = P  $\left( \frac{F}{G} \right)$

$$= \frac{\text{GMS}}{\text{GMS}}$$

= \_\_\_\_\_ GMS

## Particulates

Nozzle, Probe, and Acetone Washing .0005 grms

Filter .0008 grms

.0005.0013-----  
Enter "0" if no Organic or Aqueous Phase

Aqueous Phase 0 grms

Organic Phase 0 grms

## Totals

GRAINS/DSCF = 4.671436E-04

POUNDS/HOUR = 1.406405E-02

HIT RETURN TO CONTINUE

For max flow po<sup>st</sup> 1335687 MW  
INLET: 2940

RECON SYSTEMS, INC. 87.35  
NOZZLE NO. 34  
THERM NO. 32  
PITOT NO. 7  
CONSOLE NO. 4

# Particulate Sampling Field Data -75-

Plant General Foods  
Stack OUTLET  
Nozzle Size 3/16"  
Time @ Each Point (0) 3 Min  
Ambient Temperature 80 °F

Date 9/9/81  
Sample No. 3 Box No. 4  
Probe Heater @ 8 Box Heater @ 8 °F  
Hose Heater @ 8 °F  
Ambient Pressure (P<sub>bar</sub>) 13.6 "Hg

Stack Pressure (P) +1.30 "H<sub>2</sub>O (gage) ÷ 13.6 = 13.6 "Hg (gage)

Stack Pressure (P<sub>s</sub>) = P<sub>bar</sub> + P = 13.6 "Hg

Dry Bulb 80 °F

Wet Bulb 80 °F 80 %H<sub>2</sub>O

Operating Condition or Remarks

| Port/<br>Point | Military<br>Clock<br>Time | Meter<br>Reading | Pitot<br>ΔP | Orifice<br>ΔH | Meter<br>Temp (°F) |     | Line<br>Vac<br>"Hg | Probe<br>Outlet<br>(°F) | Box<br>Outlet<br>Temp<br>(°F) | Box<br>Temp<br>(°F) | Stack<br>Temp<br>°F/°C |
|----------------|---------------------------|------------------|-------------|---------------|--------------------|-----|--------------------|-------------------------|-------------------------------|---------------------|------------------------|
|                |                           |                  |             |               | IN                 | OUT |                    |                         |                               |                     |                        |
| 1              | 1540                      | 014.00           | 1.10        | 1.40          | 93                 | 93  | 4+                 | 155                     | 198                           | 218                 | 80                     |
| 2              | 53                        | 016.1            | 1.20        | 1.55          | 95                 | 93  | 4+                 | 158                     | 200                           | 222                 | 80                     |
| 3              | 54                        | 018.2            | 1.20        | 1.55          | 95                 | 93  | 4+                 | 165                     | 201                           | 221                 | 80                     |
| 4              | 59                        | 020.7            | 1.10        | 1.40          | 96                 | 93  | 4+                 | 170                     | 200                           | 220                 | 82                     |
| 5              | 1002                      | 022.6            | 1.10        | 1.40          | 97                 | 92  | 4+                 | 175                     | 202                           | 219                 | 81                     |
| 6              | 1003                      | 024.5            | 1.05        | 1.35          | 99                 | 93  | 3+                 | 180                     | 200                           | 224                 | 81                     |
| 7              | 1008                      | 026.2            | .93         | 1.20          | 100                | 93  | 3+                 | 185                     | 201                           | 224                 | 81                     |
| 8              | 1011                      | 028.2            | .90         | 1.18          | 101                | 94  | 3+                 | 183                     | 200                           | 222                 | 81                     |
| 9              | 1014                      | 030.1            | .90         | 1.18          | 101                | 93  | 3+                 | 180                     | 202                           | 223                 | 81                     |
| 10             | 1017                      | 031.7            | .85         | 1.10          | 102                | 93  | 2+                 | 185                     | 203                           | 220                 | 81                     |
| 11             | 1620                      | 033.2            | .80         | 1.05          | 102                | 93  | 2+                 | 188                     | 200                           | 221                 | 81                     |
| 12             | 1623                      | 034.6            | .80         | 1.05          | 102                | 93  | 2+                 | 187                     | 201                           | 220                 | 81                     |
| END            | 1624                      | 036.470          |             |               |                    |     |                    |                         |                               |                     |                        |
| 1              | 1628                      | 036.470          | 1.40        | 1.80          | 99                 | 94  | 5+                 | 175                     | 199                           | 218                 | 81                     |
| 2              | 31                        | 038.6            | 1.40        | 1.80          | 99                 | 94  | 5+                 | 173                     | 198                           | 217                 | 82                     |
| 3              | 34                        | 040.5            | 1.40        | 1.80          | 100                | 94  | 5+                 | 170                     | 201                           | 220                 | 82                     |
| 4              | 37                        | 042.6            | 1.20        | 1.55          | 100                | 95  | 4+                 | 166                     | 200                           | 219                 | 82                     |
| 5              | 40                        | 044.5            | 1.20        | 1.55          | 101                | 96  | 4+                 | 165                     | 205                           | 223                 | 82                     |
| 6              | 43                        | 047.0            | 1.20        | 1.55          | 102                | 94  | 4+                 | 163                     | 200                           | 221                 | 81                     |
| 7              | 46                        | 050.0            | .90         | 1.18          | 102                | 94  | 3+                 | 158                     | 203                           | 222                 | 81                     |
| 8              | 49                        | 051.0            | .80         | 1.05          | 103                | 95  | 2+                 | 168                     | 205                           | 224                 | 81                     |
| 9              | 52                        | 052.0            | .80         | 1.05          | 103                | 95  | 2+                 | 170                     | 202                           | 221                 | 81                     |
| 10             | 55                        | 053.5            | .80         | 1.05          | 103                | 95  | 2+                 | 178                     | 200                           | 220                 | 81                     |
| 11             | 58                        | 055.2            | .80         | 1.05          | 103                | 95  | 2+                 | 165                     | 201                           | 222                 | 81                     |
| 12             | 1701                      | 056.6            | .78         | 1.00          | 104                | 95  | 2+                 | 160                     | 197                           | 220                 | 81                     |
| END            |                           | 058.474          |             |               |                    |     |                    |                         |                               |                     |                        |
| Σ              |                           | 44.472           |             |               |                    |     |                    |                         |                               |                     |                        |

\* Sum, Average, or Difference

(Convert to)  
°F

$$V_m = V \text{ (DGMCF)} = (1.0) (44.472) = 44.472 \text{ ft}^3$$

## Other Data

| Time | Sample or<br>Measurement | Value |
|------|--------------------------|-------|
|      | O <sub>2</sub>           | 21    |
|      | CO <sub>2</sub>          | 0     |
|      |                          |       |
|      |                          |       |
|      |                          |       |

$$\text{Average CO}_2 = \frac{\%}{100} \times \text{MW}/100 = \frac{\%}{100} \times 0.44 =$$

$$\text{O}_2 = \frac{\%}{100} \times 0.32 =$$

$$\text{N}_2 = \frac{\%}{100} \times 0.28 =$$

100.0

= dry MW

Pre-Leak Check 0.00 at 15"

Post Leak Check 0.01 at 6"

CLIENT: GENERAL FOODS

Date: 09/21/87

Time: 9:53 AM

AVERAGE VELOCITY PRESSURE

| Delta P<br>(IN H2O) | Delta P<br><u>Square Root</u> |
|---------------------|-------------------------------|
| 1.10                | 1.05                          |
| 1.20                | 1.10                          |
| 1.20                | 1.10                          |
| 1.10                | 1.05                          |
| 1.10                | 1.05                          |
| 1.05                | 1.02                          |
| 0.93                | 0.96                          |
| 0.90                | 0.95                          |
| 0.90                | 0.95                          |
| 0.85                | 0.92                          |
| 0.80                | 0.89                          |
| 0.80                | 0.89                          |
| 1.40                | 1.18                          |
| 1.40                | 1.18                          |
| 1.40                | 1.18                          |
| 1.20                | 1.10                          |
| 1.20                | 1.10                          |
| 1.20                | 1.10                          |
| 0.90                | 0.95                          |
| 0.80                | 0.89                          |
| 0.80                | 0.89                          |
| 0.80                | 0.89                          |
| 0.80                | 0.89                          |
| 0.78                | 0.88                          |

THE AVERAGE SQUARE ROOT OF DELTA P = 1.007504

CLIENT: GENERAL FOODS

Date: 09/21/87

Time: 9:53 AM

| Delta H<br>(IN H2O) | Meter Temp (F)<br>IN | OUT   | Stack Temp (F) |
|---------------------|----------------------|-------|----------------|
| 1.40                | 93.00                | 93.00 | 80.00          |
| 1.55                | 95.00                | 93.00 | 80.00          |
| 1.55                | 95.00                | 93.00 | 80.00          |
| 1.40                | 96.00                | 93.00 | 83.00          |
| 1.40                | 97.00                | 92.00 | 81.00          |
| 1.35                | 99.00                | 93.00 | 81.00          |
| 1.20                | 100.00               | 93.00 | 81.00          |
| 1.18                | 101.00               | 94.00 | 81.00          |
| 1.18                | 102.00               | 93.00 | 81.00          |
| 1.10                | 102.00               | 93.00 | 81.00          |
| 1.05                | 102.00               | 93.00 | 81.00          |
| 1.05                | 102.00               | 93.00 | 81.00          |
| 1.80                | 99.00                | 94.00 | 81.00          |
| 1.80                | 99.00                | 94.00 | 82.00          |
| 1.80                | 100.00               | 94.00 | 82.00          |
| 1.55                | 100.00               | 95.00 | 82.00          |
| 1.55                | 101.00               | 96.00 | 82.00          |
| 1.55                | 102.00               | 94.00 | 81.00          |
| 1.18                | 102.00               | 94.00 | 81.00          |
| 1.05                | 103.00               | 95.00 | 81.00          |
| 1.05                | 103.00               | 95.00 | 81.00          |
| 1.05                | 103.00               | 95.00 | 81.00          |
| 1.05                | 103.00               | 95.00 | 81.00          |
| 1.00                | 104.00               | 95.00 | 81.00          |

AVERAGES

DELTA H = 1.326667 IN H2O

METER TEMP. = 96.97916 F

STACK TEMP. = 81.125 F

# Water and Dry Particulate Collections

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PLANT MAXWELL HOUSE  
TEST FOR Particulate  
SAMPLE NO. 3 BOX NO. 4

STACK ROTO. OLT.  
DATE 9/9/67  
OPERATING CONDITION STEADY

|            | Grams                                                                | Grams                  |
|------------|----------------------------------------------------------------------|------------------------|
| Impinger 1 | Final Weight <u>689.2</u><br>Initial Weight <u>686.0</u><br>Increase | Impinger 1 <u>3.2</u>  |
| Impinger 2 | Final Weight <u>683.2</u><br>Initial Weight <u>680.9</u><br>Increase | Impinger 2 <u>2.3</u>  |
| Impinger 3 | Final Weight <u>485.7</u><br>Initial Weight <u>484.6</u><br>Increase | Impinger 3 <u>1.1</u>  |
| Silica Gel | Final Weight <u>763.9</u><br>Initial Weight <u>742.6</u><br>Increase | Silica Gel <u>21.3</u> |

~~Record Water Collected  
in cyclone, flash, if any:~~

~~Final Weight \_\_\_\_\_ gms  
Initial Weight \_\_\_\_\_ gms  
Increase \_\_\_\_\_ gms~~

279 grams  
Total mass of water caught

Filter Diameter 4 inches  
Filter Type Glass Fiber

Filter Final Weight .6314  
Initial Weight .6308  
Increase

0.0006 gram  
Total mass of particulate  
caught on filter

Is ice present in the impinger bath at the end of this sample?  
Yes    No   

RECON SYSTEMS, INC.  
Three Bridges NJ

## Lab Data - Evaporations

PLANT MAXWELL HOUSE STACK ROTO. OUT. SAMPLE NO. 3 FOR ParticulatesSAMPLING DATE 9/9/81 OPERATING CONDITION \_\_\_\_\_

## Acetone Washings

Gross 489.8 GMS

TOTAL

SAMPLE Tare- 338.2 GMS(A) Net 151.6 GMS

## AMOUNT

EVAPORATED 151.6 GMS (B)

Evap. Beaker NO. \_\_\_\_\_

Gross 105.1326 GMSTare- 105.1319 GMSNet 0.0007 (C) GMSAcetone Blank = 0 GMS  
(D) 100 GMS

## Corrected

Net = (C) - (B) (D)  
(E)

$$= \frac{0.0007 - 151.6}{100}$$

$$= 0.0007 \text{ GMS}$$

## Scaled Up

Net = (E)  $\frac{A}{B}$ 

$$= \frac{0.0007}{100}$$

$$= 0.0007 \text{ GMS}$$

## Wet Catch

Gross \_\_\_\_\_ GMS

TOTAL SAMPLE Tare- \_\_\_\_\_ GMS

(F) Net \_\_\_\_\_ GMS

## AMOUNT

EXTRACTED

(G)

GMS (mls)

Water Phase

Evap. Beaker No. \_\_\_\_\_

Gross \_\_\_\_\_ GMS

Tare- \_\_\_\_\_ GMS

Net \_\_\_\_\_ (J) GMS

Water Blank

(L)

GMS

=  $\frac{\quad}{100}$  GMS

## Corrected

Net (N) = J - (G) (L)

$$= \frac{\quad}{100}$$

= \_\_\_\_\_ GMS

Scaled Up Net = N  $\left(\frac{F}{G}\right)$ 

$$= \frac{\quad}{\quad}$$

= \_\_\_\_\_ GMS

AMOUNT  
of E/C

mls (H)

E/C Phase

Evap. Beaker No. \_\_\_\_\_

Gross \_\_\_\_\_ GMS

Tare- \_\_\_\_\_ GMS

Net \_\_\_\_\_ (K) GMS

E/C Blank

(M)

GMS

=  $\frac{\quad}{100}$  mls

## Corrected

Net (P) = K - H (M)

$$= \frac{\quad}{100}$$

= \_\_\_\_\_ GMS

Scaled Up Net = P  $\left(\frac{F}{G}\right)$ 

$$= \frac{\quad}{\quad}$$

= \_\_\_\_\_ GMS

## Particulates

Nozzle, Probe, and Acetone Washing .0007 grms

Filter .0006 grms

.0007  
1.0013-----  
Enter "0" if no Organic or Aqueous Phase

Aqueous Phase 0 grms

Organic Phase 0 grms

## Totals

GRAINS/DSCF = 4.745402E-04

POUNDS/HOUR = 1.412562E-02

HIT RETURN TO CONTINUE

CLIENT: GENERAL FOODS

Date: 09/21/87

Time: 9:53 AM

# ISOKINETIC CALCULATIONS

| SAMPLE NO.                                   | 1           | 2           | 3           |
|----------------------------------------------|-------------|-------------|-------------|
| DATE                                         | 9/9/87      | 9/9/87      | 9/9/87      |
| TIME                                         | 1115-1230   | 1345-1459   | 1540-1704   |
| UNIT SAMPLED                                 | ROTO.OUTLET | ROTO.OUTLET | ROTO.OUTLET |
| METER VOLUME<br>(VM-STD), SCU-FT             | 41.62       | 42.95       | 42.28       |
| WATER COLLECTED<br>(VW-STD), SCU-FT          | 1.26        | 1.24        | 1.32        |
| MOISTURE (VOL %)                             | 2.95        | 2.82        | 3.03        |
| ACTUAL MOLECULAR WEIGHT<br>(MW), LBS/LB-MOLE | 28.52       | 28.54       | 28.51       |
| ACTUAL VELOCITY<br>IN STACK<br>(VS), FT/SEC  | 55.93       | 57.23       | 56.81       |
| ACTUAL FLOW RATE<br>IN STACK<br>(ACFM)       | 3590.51     | 3673.95     | 3647.49     |
| VELOCITY @ STP<br>(VS-STD), FT/SEC           | 55.09       | 56.30       | 55.78       |
| STACK FLOW RATE<br>@ STP<br>(SCFM)           | 3537.01     | 3614.25     | 3581.30     |
| DRY FLOW RATE<br>(DSCFM)                     | 3432.79     | 3512.44     | 3472.83     |
| NOZZLE VELOCITY<br>@ STP<br>(VN-STD), FT/SEC | 51.78       | 53.35       | 52.63       |
| ISOKINETIC %                                 | 93.98       | 94.76       | 94.35       |

IENT: GENERAL FOODS

Date: 09/21/87

Time: 9:53 AM

THE FOLLOWING WERE PROGRAMMER INPUTS FOR ISOKINETICS

| SAMPLE NO.                                       | 1           | 2           | 3           |
|--------------------------------------------------|-------------|-------------|-------------|
| TE                                               | 9/9/87      | 9/9/87      | 9/9/87      |
| ME                                               | 1115-1230   | 1345-1459   | 1540-1704   |
| IT SAMPLED                                       | ROTO.OUTLET | ROTO.OUTLET | ROTO.OUTLET |
| TUAL NOZZLE<br>AMETER (ND), IN                   | 0.19        | 0.19        | 0.19        |
| TOT FACTOR (CP)                                  | 0.83        | 0.83        | 0.83        |
| ME @ EACH<br>INT (MIN)                           | 3.00        | 3.00        | 3.00        |
| BIENT PRESSURE<br>BAR), IN-HG                    | 29.90       | 29.90       | 29.90       |
| ACK PRESSURE<br>S), IN-HG                        | 1.45        | 1.30        | 1.30        |
| TER VOLUME<br>M), CU-FT                          | 43.46       | 44.98       | 44.47       |
| TER COLLECTED<br>PINDERS, GRMS                   | 26.70       | 26.30       | 27.90       |
| ARBON DIOXIDE<br>O <sub>2</sub> ), %             | 0.00        | 0.00        | 0.00        |
| YGEN<br>( <sub>2</sub> ), %                      | 21.00       | 21.00       | 21.00       |
| ACK DIAMETER<br>IA), IN                          | 14.00       | 14.00       | 14.00       |
| ACK CROSS SECTIONAL<br>EA (CSA), FT <sup>2</sup> | 1.07        | 1.07        | 1.07        |

# RECON SYSTEMS, INC.

Route 202 North, P.O., Box 460

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Three Bridges, N.J. 08887

201-782-5900

## LABORATORY ORSAT OR GC GAS ANALYSIS

PLANT GENERAL FOODS STACK ROTOCLONE

SAMPLE NO. \_\_\_\_\_ OPERATING CONDITIONS \_\_\_\_\_

JOB NO. 0554

--Dry Basis--

| Sample ID     | Date   | % CO <sub>2</sub> | % O <sub>2</sub> | % CO | % N <sub>2</sub> (By Diff.) |
|---------------|--------|-------------------|------------------|------|-----------------------------|
| Inlet Run #1  | 9/9/87 | 0                 | 21.0             | —    | 79.0                        |
| Sample ID     | Date   | % CO <sub>2</sub> | % O <sub>2</sub> | % CO | % N <sub>2</sub> (By Diff.) |
| Inlet Run #2  | 9/9/87 | 0                 | 21.0             | —    | 79.0                        |
| Sample ID     | Date   | % CO <sub>2</sub> | % O <sub>2</sub> | % CO | % N <sub>2</sub> (By Diff.) |
| Inlet Run #3  | 9/9/87 | 0                 | 21.0             | —    | 79.0                        |
| Sample ID     | Date   | % CO <sub>2</sub> | % O <sub>2</sub> | % CO | % N <sub>2</sub> (By Diff.) |
| Outlet Run #1 | 9/9/87 | 0                 | 21.0             | —    | 79.0                        |
| Sample ID     | Date   | % CO <sub>2</sub> | % O <sub>2</sub> | % CO | % N <sub>2</sub> (By Diff.) |
| Outlet Run #2 | 9/9/87 | 0                 | 21.0             | —    | 79.0                        |
| Sample ID     | Date   | % CO <sub>2</sub> | % O <sub>2</sub> | % CO | % N <sub>2</sub> (By Diff.) |
| Outlet Run #3 | 9/9/87 | 0                 | 21.0             | —    | 79.0                        |
| Sample ID     | Date   | % CO <sub>2</sub> | % O <sub>2</sub> | % CO | % N <sub>2</sub> (By Diff.) |
|               |        |                   |                  |      |                             |

CHEMIST: Peter F. Marshall

Date: 9/9/87

L-18 (8.17.82)

ENGINEERING, CONSULTING, LABORATORY,  
PILOT PLANT, PLANT TEST SERVICES

POLLUTION CONTROL, WASTE DISPOSAL,  
RESOURCE RECOVERY, CHEMICAL PROCESS SYSTEMS

#3

|               |                       |
|---------------|-----------------------|
| PLANT<br>ID # | INSPECTOR<br>ASSIGNED |
| 10082         | 025                   |

## FIELD INVESTIGATION ASSIGNMENT REPORT

|                   |        |
|-------------------|--------|
| DATE<br>COMPLETED | COUNTY |
| 9-9-87            | Hudson |

GRANT General Foods Corp., Mottville House Division TYPE OF ASSIGNMENT  
 LOCATION 1125 Hudson St., Hebron ☐ COMPLAINT ☐ APPEAL  
☐ ORDER FOLLOWUP  
 THIS CLASS: A1 ☐ A2 ☐ B ☐ NSPS ☐ NESMAPS ☐ PSD ☒ OTHER (BY CODE) STD  
 APPEALS CYCLE: \_\_\_\_\_  
 GRANT (105): ☐ Yes ☐ No PLT: PT ☐ S2 ☐ CO ☐ N2 ☐ VO ☐ OTHER \_\_\_\_\_

COMPLAINANT NAME \_\_\_\_\_ PHONE # \_\_\_\_\_  
 COMPLAINANT ADDRESS \_\_\_\_\_ RECORDED BY \_\_\_\_\_  
 DATE/TIME RECEIVED: \_\_\_\_\_ COMPLAINT DETAILS: \_\_\_\_\_

PLANT CONTACT FRANIE LA SALLE  
 TITLE Plant Plant Supervisor  
 TIME AT PLANT 9:30am  
 ASSIGNMENT TIME 100  
 PLANT WAS INSPECTED 1  
 PLANT WAS INSPECTED 1  
 FILE FILED FOR SUBCHAPTERS

| SUBCHAPTER | # INSP |
|------------|--------|
| 8          | 1      |
| 6          | 1      |
|            |        |
|            |        |
|            |        |
|            |        |
|            |        |

COMPLAINT: TYPE \_\_\_\_\_  
 SUB 5 SOP FOLLOWED: ☐  
 TIME AT COMPLAINANT \_\_\_\_\_  
 VERIFIED: ☐ Yes ☐ No  
 GIVE DETAILS BELOW \_\_\_\_\_  
 VIOLATION FOLLOWUP INSPECTION  
 VIOLATION LOG # \_\_\_\_\_  
 ORDER DATED \_\_\_\_\_  
 SUBCHAPTER VIOLATED \_\_\_\_\_  
 COMPLIANCE ACHIEVED ☐ Yes ☐ No  
 GIVE DETAILS BELOW \_\_\_\_\_

FILE FILED FOR SUBCHAPTERS NA  
 COMPLAINT COLLECTED NA  
 COMPLAINT BY CODE 007  
 DIVISION'S INSTRUCTIONS: \_\_\_\_\_

FIELD INSPECTION NJ STD # 059, PLOT # 78004 WAS STACK TESTED BY RETON SYSTEMS - THERE  
IS A CHANGE IN RMC MATERIAL'S PROCESS: ~200 lb/hr of coffee beans were processed  
during the stack test. THE COFFEE ROASTOR CANNOT PROCESS >200 lb/hr of coffee beans. THEREFORE  
THE CONTINUOUS COOLER WILL NOT RECEIVE >200 lb/hr of coffee beans. THE PERMIT SHOULD BE  
AMENDED TO SHOW THE ACTUAL PROCESS; CONSEQUENTLY THE EMISSION RATE. MR. LA SALLE WAS  
INFORMED OF THE NEED TO AMEND THE PERMIT!  
THE ATLANTIC SCALE CO INC, NUTLEY, CALIBRATED THE SCALE ON 2-11-87. THE  
SCALE WHICH HAS THE BEANS AND A DIGITAL DISPLAY SHOWS THE AMOUNT PROCESSED.  
THE CALIBRATION RECORDS SHOULD BE CHECKED AS A  
MATTER OF ROUTINE INVESTIGATION.

INSPECTOR'S SIGNATURE  
Elizabeth Rossi  
 TITLE: SR ENVIRONMENTAL  
 SUPERVISOR'S REVIEW

EMISSION TEST OBSERVATION FORM

1) COMPANY GENERAL FOODS CORPORATION, Maxwell House Division  
 N.J. STACK NO. 059 DEP I.D. NO. 10082  
 PLANT LOCATION 1125 Hudson St Hoboken  
 2) PLANT CONTACT ERNE LaSalle plant manager EMISSION TEST DATE(S) 9-9-81  
 3) SOURCE 4201-3731 BEING TESTED CONTINUOUS COOLER PERMIT/  
 CERTIFICATE NO. 78004  
 DESCRIPTION OF SOURCE COOLING ZONE AFTER CONTINUOUS REASTER

4) TESTS ARE BEING CONDUCTED TO DETERMINE COMPLIANCE WITH THE FOLLOWING REGULATIONS. (Indicate all applicable regulations.)

N.J.A.C. 7:27 6.2 EPA NSPS Subpart N/A EPA NESHAPS Subpart N/A

5) TYPE OF CONTROL EQUIPMENT (if applicable) Rotoclone

CONTROL EQUIPMENT OPERATING PARAMETERS (During each test)

| PARAMETER | RUN NO. 1 | RUN NO. 2 | RUN NO. 3 |
|-----------|-----------|-----------|-----------|
|           |           |           |           |
|           |           |           |           |
|           |           |           |           |

6) SOURCE OPERATING PARAMETERS (During each test)

| PARAMETER            | 11:15 am - 12:30 pm<br>RUN NO. 1                                                                                                                                                                                                             | 1:45 pm - 3:00 pm<br>RUN NO. 2 | 3:50 pm - 5:05 pm<br>RUN NO. 3 |
|----------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------|--------------------------------|
| COOLING ZONE         |                                                                                                                                                                                                                                              |                                |                                |
| WATER SPRAY<br>(GPM) | 3 GPH                                                                                                                                                                                                                                        | 3 GPH                          | 3 GPH                          |
| Coffee beans         | 1100.0 lbs/hr                                                                                                                                                                                                                                | 120.0 lbs/hr                   | 182.4 lbs/hr                   |
| ODOR OFF<br>PROPERTY | UPWIND OF<br>CONTINUOUS COOLER<br>WHICH IS DOWNWIND<br>OF ENTIRE PLANT,<br>THERE WERE Faint<br>COFFEE ODORS,<br>DOWNWIND OF<br>CONTINUOUS<br>COOLER THERE<br>WERE Faint<br>COFFEE ODORS,<br>NO SIGNIFICANT<br>DETERMINATION<br>MADE THIS DAY | SAME AS<br>RUN NO. 1           | SAME AS<br>RUN NO. 1           |

7) TYPE OF FUEL BEING FIRED (if applicable) *NA*AMOUNT OF FUEL BEING FIRED DURING EACH TEST *NA*

| RUN NO. 1 | RUN NO. 2 | RUN NO. 3 |
|-----------|-----------|-----------|
|           |           |           |
|           |           |           |
|           |           |           |

8) WERE FUEL SAMPLES TAKEN DURING TESTS? ☐ YES ☒ NO (If yes, record fuel sample number(s) for each test.)

Run No. 1 \_\_\_\_\_

Run No. 2 \_\_\_\_\_

Run No. 3 \_\_\_\_\_

9) WERE ANY OTHER SAMPLES TAKEN DURING TEST? ☐ YES ☒ NO

(If yes, indicate type of sample, run number sample was taken, sampling location and sample numbers.)

| TYPE | RUN NO. | LOCATION | SAMPLE NUMBERS | COMMENT |
|------|---------|----------|----------------|---------|
|      |         |          |                |         |
|      |         |          |                |         |
|      |         |          |                |         |

10) ANY PROCESS OR CONTROL EQUIPMENT PROBLEMS DURING ANY TEST? ☐ YES ☒ NO

(If yes, specify the type of problem and indicate during which run it occurred.)

| RUN NO.  | PROBLEM                                                                                                                                                                                                                                                                                                      |
|----------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 1, 2 & 3 | ~200 lb/hr of coffee beans were processed during the stack test. The coffee roaster cannot process > 200 lb/hr of coffee beans. Therefore the continuous cooler will not receive > 200 lb/hr of coffee beans. The permit should be amended to show the actual process rate; consequently, the emission rate. |

11) EMISSION TESTS CONDUCTED BY ☐ DEP ☒ COMPANY CONSULTANT

Recon Systems INC

THREE BRIDGES, NJ

PETER MARSHALL

201 782-5900

INSPECTOR'S SIGNATURE

*Reginald P. Rossi*

REGIONAL OFFICE REPRESENTED

*MRO*

# Emission Test Report Review Checklist--Short Form

Reviewer: T. LAPP  
Review Date: 8/18/94

## A. Background Information

1. Facility name: GENERAL FOODS CORP / MAXWELL HOUSE Division  
Location: HOBOKEN, NJ
2. Source category: COFFEE ROASTING
3. Test date: September 9, 1987
4. Test sponsor: GENERAL FOODS
5. Testing contractor: RECON SYSTEMS, INC.
6. Purpose of test: COMPLIANCE TEST FOR PM EMISSIONS
7. Pollutants measured (include test method and indicate if valid): PM-TOTAL NJ METHOD 1 TEST  
PM MEASURED AT INLET AND OUTLET OF THE  
ROTOCLONE

8. Process overview: Attach a process description and a block diagram. Identify processes tested with letters from the beginning of the alphabet (A, B, C, etc...) and APC systems with letters from the end of the alphabet (V, W, X, etc...). Also identify test locations with Arabic numerals (1,2,3, ...). Using the ID symbols from the diagram, complete the table below.

| Test ID | Process                                    | Process ID       | Emissions tested |            | APCD (controlled emissions only) |
|---------|--------------------------------------------|------------------|------------------|------------|----------------------------------|
|         |                                            |                  | Uncontrolled     | Controlled |                                  |
|         | CONTINUOUS COOLER AFTER CONTINUOUS ROASTER | NJ STACK No. 059 |                  | ROTOCLONE  | ID:<br>Type:<br>Model #:         |
|         |                                            |                  |                  |            | ID:<br>Type:<br>Model #:         |
|         |                                            |                  |                  |            | ID:<br>Type:<br>Model #:         |
|         |                                            |                  |                  |            | ID:<br>Type:<br>Model #:         |

**B. Process Information**

1. Provide a brief narrative description of the process and attach process flow diagram. (Note: If the process description provided in the test report is adequate, attach a copy here.)

*No Process description provided*

*Measured PM at inlet and outlet of notoclone*

INLET/OUTLET

[illegible]