

Note: This is a reference cited in *AP 42, Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at www.epa.gov/ttn/chief/ap42/

The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

Background Report Reference

AP-42 Section Number: 10.6.1

Background Report Section: 4

Reference Number: 81

**Title: Report of Air Emissions and Inlet
Loading Tests for Louisiana Pacific
Corporation, Hanceville OSB Plant
Hanceville, Alabama**

**Environmental Monitoring
Laboratories, Inc.**

May 1994

74
4-81

REPORT OF AIR
EMISSIONS AND INLET LOADING TESTS
FOR
LOUISIANA PACIFIC CORPORATION
HANCEVILLE OSB PLANT

Hanceville, Alabama
March 31, 1994

RECEIVED
MAR 4 1994
LOUISIANA PACIFIC CORP.
HAYWARD, WISCONSIN

Prepared for
Louisiana Pacific Corporation
Post Office Box 3107
Conroe, Texas 77305

ph: 409/760-5921
Contact: Dr. James T. Boswell

DOO
TO
LIST
74

#33194

Performed By:
Environmental Monitoring Laboratories
Ridgeland, Mississippi
(601-856-3092)

Rep # 33194

ENVIRONMENTAL MONITORING LABORATORIES, INC.

O. Box 655 • 606 B Highway 51 North

phone: 601/856-3092

Kidgeland, Mississippi 39158

fax : 601/853-2151

May 3, 1994

Subject: Louisiana Pacific Corporation
Hanceville, Alabama OSB Plant

On March 31, 1994, Environmental Monitoring Laboratories conducted air emissions and inlet loading tests at Louisiana Pacific Corporation's OSB facility in Hanceville, Alabama. Testing was performed to determine emissions of particulate matter (PM), volatile organic compounds (VOC), nitrogen oxides (NOx), and carbon monoxide (CO) from the regenerative thermal oxidizer (RTO) system controlling emissions from five OSB dryers. Testing was also done at the RTO inlets to determine removal efficiency.

Results:

DRYERS RTO	PM		VOC		CO		NOx	
	gr/dscf	#/hr	ppm as C	#/hr	ppm	#/hr	ppm	#/hr
WEST RTO	.0036	2.78	12	1.98	61	23.89	24	15.26
EAST RTO	.0036	2.52	7	1.04	57	20.63	24	14.14
Dryer 4 Inlet	0.116	25.28	1656	78.52	71	7.84	17	3.08
Dryer 3 Inlet	0.163	38.18	1225	62.42	34	4.01	22	4.28
Projected Inlet total	0.140	158.7	1441	352.4	53	29.6	20	18.4
REMOVAL EFFICIENCY	96.7		99.1		- 50.3		- 59.8	

The testing project was coordinated by Dr. James T. Boswell of Louisiana Pacific Corporation. Danny Russell of Environmental Monitoring Laboratories coordinated sample collection and analysis and report preparation.

Following is a report of the test:

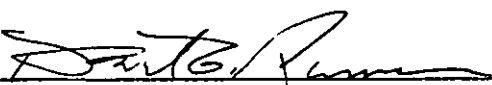
REPORT OF AIR EMISSIONS AND INLET LOADING TESTS
FOR LOUISIANA PACIFIC CORPORATION
HANCEVILLE OSB PLANT
HANCEVILLE, ALABAMA
MARCH 31, 1994

CONTENTS

1.0 Test Results	page	1
2.0 Source Description		5
3.0 Test Procedures		5
4.0 Data Reduction		6
5.0 Nomenclature		13
6.0 Calibration		14
7.0 Appendices:		15
A. Sampling and Analytical Data		
B. Calibration Data		
C. Instrument Recorder Traces		

REPORT CERTIFICATION

I certify that I have examined the information submitted herein, and based upon my inquiries of those directly responsible for obtaining the data or upon my direct acquisition of the data, I believe the submitted information is true, accurate and complete.

Signed 

Daniel G. Russell

1.0 TEST RESULTS: The following tables present the measured flow parameters and test results for emissions and inlet loading testing for Louisiana Pacific Corporation's Hanceville, Alabama OSB facility on March 31, 1994.

1.1 OSB Dryers RTO

RTO		WEST	EAST	TOTAL
Date		03-31-94	03-31-94	-----
Time Start		1612	1747	---
Time End		1713	1848	----
PARTICULATE EMISSIONS	#/hr.	2.78	2.52	5.30
PARTICULATE EMISSIONS	gr/dscf	.0036	.0036	.0036
VOC EMISSIONS	#/hr	1.98	1.04	3.03
VOC EMISSIONS	ppm as C	11.92	6.76	9.44
NO _x EMISSIONS	#/hr	15.26	14.14	29.40
NO _x EMISSIONS	ppm	24	24	24
CO EMISSIONS	#/hr	24.5	22.3	46.8
CO EMISSIONS	ppm	63	62	63
VOLUMETRIC FLOWRATE	acfm	138170	128254	266424
VOLUMETRIC FLOWRATE	dscfm	89066	82493	171559
VELOCITY	ft./sec.	57.76	53.61	----
STACK TEMPERATURE	° F	259	265	---
MOISTURE	%	11.9	11.3	----
SAMPLE RATE	% isokinetic	95	98	

1.2 No. 4 Dryer Multiclone Inlet

Run No.....		1	2	avg.
Date		03-31-94	03-31-94	—
Time Start		1106	1627	—
Time End		1506	1729	—
PARTICULATE EMISSIONS	#/hr.	25.88	24.68	25.28
PARTICULATE EMISSIONS	gr/dscf	0.119	0.113	0.116
VOC EMISSIONS	#/hr	78.79	78.26	78.53
VOC EMISSIONS	ppm	1669	1643	1656
NO _x EMISSIONS	#/hr	3.07	3.09	3.08
NO _x EMISSIONS	ppm	17	17	17
CO EMISSIONS	#/hr	8.15	8.22	8.19
CO EMISSIONS	ppm	7.80	7.87	7.84
VOLUMETRIC FLOWRATE	acfm	40201	40363	40282
VOLUMETRIC FLOWRATE	dscfm	25253	25475	25364
VELOCITY	ft./sec.	70.5	70.8	70.6
STACK TEMPERATURE	° F	157	163	160
MOISTURE	%	24.5	23.3	23.9
SAMPLE RATE	% isokinetic	93	98	96

1.3 No. 3 Dryer Multiclone Inlet

Run No.....		1	2	avg.
Date		03-31-94	03-31-94	-----
Time Start		1342	1430	---
Time End		1417	1506	---
PARTICULATE EMISSIONS	#/hr.	32.40	43.95	38.18
PARTICULATE EMISSIONS	gr/dscf	0.137	0.190	0.163
VOC EMISSIONS	#/hr	1210	1239	1225
VOC EMISSIONS	ppm	62.42	62.42	62.42
NO _x EMISSIONS	#/hr	4.33	4.23	4.28
NO _x EMISSIONS	ppm	22	22	22
CO EMISSIONS	#/hr	4.06	3.97	4.01
CO EMISSIONS	ppm	34	34	34
VOLUMETRIC FLOWRATE	acfm	41852	41966	41909
VOLUMETRIC FLOWRATE	dscfm	27586	26937	27262
VELOCITY —	ft./sec.	73.4	73.6	73.5
STACK TEMPERATURE	° F	167	169	168
MOISTURE	%	19.4	21.3	20.4
SAMPLE RATE	% isokinetic	95	90	92

1.4. Efficiency Summary: The following summary of system removal efficiency is based on mass emission rates. Emissions expressed in the tables are in pounds per hour. It should be noted that the inlet total used for calculating efficiency is the average measured values of the two dryer inlets multiplied by 5 dryers.

	PM	VOC	CO	NO _x
RTO TOTAL	5.30	3.03	44.5	29.4
INLET TOTAL (projected)	158.6	352.4	29.6	18.4
REMOVAL %	96.7	99.1	-50.3	-59.8

2.0 SOURCE DESCRIPTION: Process description here is limited to a brief description of the sources and their sampling locations. Detailed descriptions of the process and records of operating rates and conditions during testing may be supplied by Louisiana Pacific Corporation.

Five rotary dryers are used for drying wood flakes. Each dryer exhausts to a primary cyclone, then to high efficiency multicyclones. Exhausts from all five dryers join to a common header and enter the mixing chamber of the regenerative thermal oxidizer (RTO). The RTO consists of two mirrored sections. RTO inlet sampling was done at the inlets to the multiclones. The multiclone inlets are 41.75 inch diameter downflow ducts. Two sample ports at 90 degrees were installed at a location 8.6 diameters downstream of an elbow and 3.1 diameters upstream of a vertical to horizontal elbow. Two dryers were selected for testing -- Nos. 3 and 4. Two sample runs of 30 minutes duration were taken from each of those two dryers. The two RTO sides each exhaust to the atmosphere by way of a vertical 85.5 inch diameter stack. Two sample ports are provided at a location that is 3.7 diameters downstream of the inlet duct and 6.4 diameters below the stack exit.

3.0 TEST PROCEDURES: Test procedures used are those described in 40 CFR, Part 60, Appendix A.

Particulate sampling was done as described in Method 5. An exception was the inclusion of the condenser section particulate as described in Method 202. Reported particulate is based on three fractions: the front half, the back half organic (methylene chloride extraction), and the back half aqueous. The contribution of each fraction can be reviewed in Section 4.0.

Carbon monoxide concentration was continuously monitored as described in Method 10. CO concentrations were monitored using a TECO Model 48H gas correlation filter NDIR in various ranges. Instrument calibration was performed prior to and following each series of tests, and a mid range system bias check was made prior to and following each run by directing calibration to the gas sampling probe.

Nitrogen oxides were continuously monitored as described in Method 7E. A TECO Model 10S analyzer was used. Instrument calibration was performed prior to and following each series of tests, and a mid range system bias check was made prior to and following each run by directing calibration to the gas sampling probe.

VOC concentrations were measured using Method 25A (continuous monitoring with a flame ionization detector). A TECO Model 51 was used. The 0 to 100 ppm scale and the 0 to 1000 ppm scale were used for calibrations using zero air, and appropriate low, mid and high range concentrations of EPA protocol propane in nitrogen. Since calibrations are made with propane (C_3H_8), results as methane (CH_4) (or as carbon) are determined by increasing the measured concentration by a factor of three. A continuous trace of VOC as propane was recorded and manually integrated for each 60 minute test period. Instrument calibration was performed initially, and following each 60 minute test period. Any necessary adjustments were made after recording the response of the mid range calibration gas, which was introduced at the inlet to the VOC sampling probe. The gas samples were directed to the heated FID analyzers by way of heated teflon sample lines maintained at a minimum temperature of 275°F.

4.0 DATA REDUCTION

Louisiana Pacific Corporation - Hanceville, Alabama
 No. 4 Dryer Multiclone Inlet
 PM/VOC/NOx/CO Loading Test - March 31, 1994

Collected Test Data:

RUN 1

RUN 2

Date	:	3/31/94	3/31/94
Time start	:	1033	1146
Time end	:	1106	1220
1. As	: sq ft	9.5069	9.5069
2. Dn	: in.	0.234	0.234
3. Cp	: dimensionless	0.84	0.84
4. Theta	: minutes	30.00	30.00
5. Y	: dimensionless	1.01	1.01
6. Pbar	: in. Hg	29.8	29.8
7. Pg	: in. H2O	-10	-10
8. Vm	: cf (dry gas)	22.576	24.406
9. $\text{sqr}(\text{DP})_{\text{avg}}$	: in.H2O ^{.5}	1.0926	1.0938
10. DH	: in. H2O	1.6667	2.0208
11. ts	: degrees F	156.50	163.17
12. tm	: degrees F	82.42	91.88
13. Vlc	: ml	153	152.5
14. CO2	: percent	1.20	1.20
15. O2	: percent	19.70	19.70
16. CO	: ppm	71	71
17. M,PM	: milligrams		
	front half	146.6	141.5
	back half organic	17.4	20.2
	back half aqueous	8	11.2
18. VOC	: ppm, wet as propane	420	420
19. NOx	: ppm	17	17

159.84

No. 4 Dryer Multiclone Inlet

PM/VOC/NOx/CO Loading Test - March 31, 1994

Calculations:

RUN 1

RUN 2

AVG.

1. Pm	: in.Hg (DH/13.6)+Pbar	29.9226	29.9486	
2. Ps	: in. Hg (Pg/13.6)+Pbar	29.0647	29.0647	
3. An	: sq ft ((Dn/24) ²)(3.1416)	2.99E-04	2.99E-04	
4. Vmstd	: dscf Vm Y(Pm/Pstd)(Tstd/Tm)	22.197	23.606	22.902
5. Vwstd	: scf (.04707cf/ml)(Vlc)	7.202	7.178	
6. Bws	: dimensionless Vwstd/(Vwstd+Vmstd)	0.2450	0.2332	0.2391
7. Md	: mol.wt. dry basis .44 CO2+.32 O2+.28(CO+N2)	28.98	28.98	
8. Ms	: mol.wt. wet basis Md(1-Bws)+18 Bws	26.29	26.42	
9. Vs	: ft/sec Kp Cp (sqrDP)sqr(Ts/(Ps Ms))	70.48	70.76	70.62
10. Q	: cfm Vs As(60 sec/min)	40201	40363	40282
11. Qstw	: scfm Q(Ps/Pstd)(Tstd/Ts)	33446	33221	33333
12. Qstd	: dscfm Qstw(1-Bws)	25253	25475	25364
13. I	: percent [(100 Ts)(.002669 Vlc+(Vm Pm/Tm))/(60 theta Vs Ps An)]	93.29	98.34	95.81
14. E,PM	: pounds/hr (M,PM/Vmstd)(Qstd)(60)(453590)			
front half		22.061	20.199	21.130
back half organic		2.618	2.884	2.7510
back half aqueous		1.204	1.599	1.401
Total		25.883	24.681	25.282
15. C,PM	: grains/dscf (M,PM/Vmstd)(.0154 grains/mg)			
front half		0.1017	0.0923	0.0970
back half organic		0.0121	0.0132	0.0126
back half aqueous		0.0056	0.0073	0.0064
Total		0.1193	0.1128	0.1161
16. E,CO	: pounds/hr (C,CO)(7.27e-8)(Qstd)(60)	7.80	7.87	7.84
17. C,VOC	: ppm as Carbon, dry ((C,VOC)*3)/(1-Bws)	1669	1643	1656
18. C,VOC	: pounds/hr (C,VOC)(3.116e-8)(Qstd)(60)	78.79	78.26	78.52
19. E,NOx	: pounds/hr C,NOx(1.19e-7)(Qstd)(60)	3.07	3.09	3.08

No. 3 Dryer Multiclone Inlet
PM/VOC/NOx/CO Loading Test - March 31, 1994

Collected Test Data:

RUN 1

RUN 2

Date :	3/31/94	3/31/94
Time start :	1342	1430
Time end :	1417	1506
1. As : sq ft	9.5069	9.5069
2. Dn : in.	0.234	0.234
3. Cp : dimensionless	0.84	0.84
4. Theta : minutes	30.00	30.00
5. Y : dimensionless	1.01	1.01
6. Pbar : in. Hg	29.8	29.8
7. Pg : in. H2O	-10	-10
8. Vm : cf (dry gas)	25.494	23.997
9. $\text{sq}(\text{DP})_{\text{avg}}$: in.H2O ^{0.5}	1.1399	1.1370
10. DH : in. H2O	2.2292	1.8792
11. ts : degrees F	166.83	168.58
12. tm : degrees F	89.79	103.25
13. Vlc : ml	127	131
14. CO2 : percent	1.20	1.20
15. O2 : percent	19.70	19.70
16. CO : ppm	34	34
17. M,PM : milligrams		
front half	196.8	228.1
back half organic	13	39
back half aqueous	10.1	13.3
18. VOC : ppm, wet as propane	325	325
19. NOx : ppm	22	22

167.71

No. 3 Dryer Multiclone Inlet

PM/VOC/NO_x/CO Loading Test - March 31, 1994

Calculations:

RUN 1

RUN 2

AVG.

1. Pm : in.Hg (DH/13.6)+Pbar	29.9639	29.9382	
2. Ps : in. Hg (Pg/13.6)+Pbar	29.0647	29.0647	
3. An : sq ft ((Dn/24)^2)(3.1416)	2.99E-04	2.99E-04	
4. Vmstd : dscf Vm Y(Pm/Pstd)(Tstd/Tm)	24.765	22.734	23.749
5. Vwstd : scf (.04707cf/ml)(Vlc)	5.978	6.166	
6. Bws : dimensionless Vwstd/(Vwstd+Vmstd)	0.1944	0.2134	0.2039
7. Md : mol.wt. dry basis .44 CO2+.32 O2+.28(CO+N2)	28.98	28.98	
8. Ms : mol.wt. wet basis Md(1-Bws)+18 Bws	26.84	26.64	
9. Vs : ft/sec Kp Cp (sqrdP)sqrt(Ts/(Ps Ms))	73.37	73.57	73.47
10. Q : cfm Vs As(60 sec/min)	41852	41966	41909
11. Qstw : scfm Q(Ps/Pstd)(Tstd/Ts)	34245	34243	34244
12. Qstd : dscfm Qstw(1-Bws)	27586	26937	27262
13. I : percent [(100 Ts)(.002669 Vlc+(Vm Pm/Tm))/(60 theta Vs Ps An)	95.27	89.57	92.42
14. E,PM : pounds/hr (LPM/Vmstd)(Qstd)(60)/(453590)			
front half	28.998	35.751	32.375
back half organic	1.916	6.113	4.0141
back half aqueous	1.488	2.085	1.786
Total	32.402	43.948	38.175
15. C,PM : grains/dscf (LPM/Vmstd)(.0154 grains/mg)			
front half	0.1224	0.1545	0.1384
back half organic	0.0081	0.0264	0.0173
back half aqueous	0.0063	0.0090	0.0076
Total	0.1367	0.1899	0.1633
16. E,CO : pounds/hr (C,CO)(7.27e-8)(Qstd)(60)	4.06	3.97	4.01
17. C,VOC : ppm as Carbon, dry ((C,VOC)*3)/(1-Bws)	1210	1239	1225
18. C,VOC : pounds/hr (C,VOC)(3.116e-8)(Qstd)(60)	62.42	62.42	62.42
19. E,NO _x : pounds/hr C,NO _x (1.19e-7)(Qstd)(60)	4.33	4.23	4.28

West and East RTO Outlet

PM/VOC/NOx/CO Emissions Test - March 31, 1994

Collected Test Data:

West

East

Date	:	3/31/94	3/31/94
Time start	:	1612	1747
Time end	:	1713	1848
1. As	: sq ft	39.8712	39.8712
2. Dn	: in.	0.27	0.27
3. Cp	: dimensionless	0.84	0.84
4. Theta	: minutes	60.00	60.00
5. Y	: dimensionless	1.01	1.01
6. Pbar	: in. Hg	29.8	29.8
7. Pg	: in. H2O	0	0
8. Vm	: cf (dry gas)	52.735	50.827
9. sqrt(DP),avg	: in.H2O ^{0.5}	0.8617	0.7972
10. DH	: in. H2O	2.5250	2.3645
11. ts	: degrees F	258.83	265.38
12. tm	: degrees F	99.06	99.90
13. Vlc	: ml	144.5	131
14. CO2	: percent	1.40	1.40
15. O2	: percent	19.30	19.30
16. CO	: ppm	61	57
17. M,PM	: milligrams		
	front half	9.6	9.7
	back half organic	1.9	1.1
	back half aqueous	0.4	0.4
18. VOC	: ppm, wet as propane	3.5	2
19. NOx	: ppm	24	24

262.11

West and East RTO Outlet
PM/VOC/NOx/CO Emissions Test - March 31, 1994

Calculations:

	WEST	EAST	Totals
1. Pm : in. Hg (DH/13.6)+Pbar	29.9857	29.9739	
2. Ps : in. Hg (Pg/13.6)+Pbar	29.8000	29.8000	
3. An : sq ft ((Dn/24)^2)(3.1416)	3.98E-04	3.98E-04	
4. Vmstd : dscf Vm Y(Pm/Pstd)(Tstd/Tm)	50.414	48.498	
5. Vwstd : scf (.04707cf/ml)(Vlc)	6.802	6.166	
6. Bws : dimensionless Vwstd/(Vwstd+Vmstd)	0.1189	0.1128	
7. Md : mol.wt. dry basis .44 CO2+.32 O2+.28(CO+N2)	28.996	28.996	
8. Ms : mol.wt. wet basis Md(1-Bws)+18 Bws	27.69	27.76	
9. Vs : ft/sec Kp Cp (sqrDP)sqr(Ts/(Ps Ms))	57.76	53.61	
10. Q : cfm Vs As(60 sec/min)	138170	128254	266424
11. Qstw : scfm Q(Ps/Pstd)(Tstd/Ts)	101083	92981	194064
12. Qstd : dscfm Qstw(1-Bws)	89066	82493	171559
13. I : percent [(100 Ts)(.002669 Vlc+(Vm Pm/Tm))/(60 theta Vs Ps An)]	94.61	98.26	
14. E,PM : pounds/hr (M,PM/Vmstd)(Qstd)(60)/(453590)			
front half	2.243	2.183	4.426
back half organic	0.444	0.248	0.692
back half aqueous	0.093	0.090	0.183
Total	2.781	2.520	5.301
15. C,PM : grains/dscf (M,PM/Vmstd)(.0154 grains/mg)			
front half	0.0029	0.0031	
back half organic	0.0006	0.0003	
back half aqueous	0.0001	0.0001	
Total	0.0036	0.0036	
16. E,CO : pounds/hr (C,CO)(7.27e-8)(Qstd)(60)	23.89	20.63	44.52
17. C,VOC : ppm as Carbon, dry ((C,VOC)*3)/(1-Bws)	11.92	6.76	
18. C,VOC : pounds/hr (C,VOC)(3.116e-8)(Qstd)(60)	1.98	1.04	3.03
19. E,NOx : pounds/hr C,NOx(1.19e-7)(Qstd)(60)	15.26	14.14	29.40

5.0 NOMENCLATURE

SYMBOL	UNITS	DESCRIPTION
A_n	ft^2	Nozzle cross sectional area
A_s	ft^2	Stack cross sectional area
B_{ws}	dimensionless	Wet gas fraction
CO_2	percent	Carbon dioxide content by volume
CO	percent	Carbon monoxide content by volume
C_p	dimensionless	Pitot correction factor
C_X	as labeled	Concentration of pollutant X
DGF	dimensionless	Dry gas fraction
D_n	inches	Nozzle diameter
ΔH (delta H)	in. H_2O	Pressure drop across meter orifice
ΔP (delta P)	in. H_2O	Stack gas velocity pressure
E_X	$\#/\text{hr}$	Emission rate of pollutant X
EX	$\#/\text{MM Btu}$	Emission rate of pollutant X
F	dscf	Volume of flue gas per MM Btu
I	percent	Nozzle velocity/stack gas velocity
K_p	consistent	Pitot tube constant
M_X	milligrams	Sample weight of pollutant X
M_d	$\#/\# \text{ mole}$	Dry molecular weight of stack gas
M_s	$\#/\# \text{ mole}$	Wet molecular weight of stack gas
N_2	percent	Nitrogen content by volume, dry basis
O_2	percent	Oxygen content by volume, dry basis
P_{bar}	in. Hg	Barometric pressure
P_g	in. Hg	Stack static pressure
P_m	in. Hg	Total pressure at meter ($P_{bar} + (\Delta H/13.6)$)
P_s	in. Hg	Total stack pressure ($P_{bar} + (P_g/13.6)$)
P_{std}	in. Hg	Standard barometric pressure = 29.92
Q	acfm	Volumetric flow rate at stack conditions
Q_{std}	dscfm	Volumetric flow rate at standard conditions, dry basis
Q_{stdw}	scfm	Volumetric flow rate at standard conditions, wet basis
θ (theta)	minutes	Sample duration
t_m	$^{\circ}\text{F}$	Meter temperature (T_m denotes $^{\circ}\text{R}$)
t_s	$^{\circ}\text{F}$	Stack temperature (T_s denotes $^{\circ}\text{R}$)
T_{std}	$^{\circ}\text{R}$	Standard temperature = 528 $^{\circ}\text{R}$
V_{lc}	ml	volume of water collected
V_m	ft^3	Volume of dry gas sampled through meter
V_{mstd}	dscf	Sample volume at standard conditions
V_{wstd}	scf	Sample volume of water vapor
Y	dimensionless	Meter coefficient
X_{sair}	percent	Excess air

6.0 CALIBRATIONS: Measurement devices used by Environmental Monitoring Laboratories and subject to changes in measurement precision are initially calibrated prior to use. Those instruments for which calibration factors are subject to change or for which calibration checks are required, are calibrated following each field use or as otherwise directed and noted. Calibration procedures for specific equipment are as follows.

Dry Gas Meter:

Dry gas meters are periodically removed from the sampling consoles and cleaned and repaired (new gaskets etc. as required). Following the overhaul of a meter, the measuring precision is checked by the Bell Prover Method and adjusted when necessary to read to within 2% of 100% accuracy. This service is provided by Big Three Meter Company in Jackson, Mississippi. Overhaul service or any six month period is followed by a five point calibration described in APTD-0576 using either a wet test meter or calibrated dry gas meter (used exclusively for calibrations) as a standard reference. Following field use, a gas meter calibration is checked in one of two ways. [1] Three calibration checks at intermediate orifice settings are performed or [2] orifice meter coefficients are used.

If a meter coefficient obtained from pre-test and post-test checks differs by more than 5%, the coefficient (Y) giving the lower sample volume is used in the calculations.

Orifice:

The orifice coefficient is initially determined and is rechecked following a major gas meter repair and calibration.

Nozzles:

Nozzles are checked before each field use with a precision (.001 in.) dial caliper. Three measurements on different axes are made; an average of those three readings is used in calculations. If the tolerance among measurements exceeds 0.004 inches (highest to lowest reading) the nozzle is repaired and recalibrated or discarded.

Pitot Tubes:

Pitot tubes meeting EPA geometry standards are assigned a coefficient of 0.84. Pitot tubes are visually inspected for damage before, during and after use. Those pitot tubes not meeting the geometry standards are assigned a coefficient from the manufacturer's calibration which it retains unless damaged. All pitot tubes used by Environmental Monitoring Laboratories are manufactured by NAPP, Inc.

Temperature Measuring Instruments:

Most temperature measurements are made with a type K thermocouple and an Omega digital thermocouple thermometer which has an initial calibration traceable to NBS. Other measurements are made using bimetallic dial thermometers. The thermocouples and dial thermometers are checked following or during a test series against an ASTM mercury in glass thermometer.

Barometer:

Aneroid field barometers are checked against and adjusted to readings from a mercury barometer or readings obtained from local weather authorities.

Differential Pressure Gauges:

Velocity head (ΔP) and orifice pressure differential (ΔH) measurements are made using water manometers of the appropriate range unless otherwise noted in the test data. Manometers do not require calibration.

Flame Ionization Detector (FID):

VOC measurements were made with a Ratfish portable flame ionization detector set in a range of 0 to 100 ppm or 0 to 1000 ppm propane. Following a sufficient warm up period the instrument was set to respond to and measure 22.1 ppm and 796 ppm calibration propane. Prior to and following each sample run, the instrument's zero and span were checked and adjusted if necessary using supplies of air and calibration propane.

Non-dispersive Infrared Analyzer (NDIR):

Carbon monoxide measurements are made with a Beckman 864 infrared instrument calibrated in ranges of 0 to 1000 ppm and 0 to 5000 ppm. Following a sufficient warm up period of at least 1 hour and prior to each sample run, the instrument's zero and span are checked and adjusted if necessary using a supply of 100% nitrogen and 850 ppm CO respectively. An intermediate check at 150 ppm CO is also performed. These calibrations and adjustments are repeated at the conclusion of each sampling period.

Chemiluminescent NOx Analyzer:

Nitrogen oxide concentrations measurements are made with a multi-range TECO Model 10-S NOx analyzer. Following a sufficient warm up period and prior to each sample run, the instrument's zero and span are checked and adjusted if necessary using a supply of zero air and 86 ppm protocol 1 nitrogen dioxide. These calibrations and adjustments are repeated at the conclusion of the sampling period.

7.0 APPENDICES

A. Sampling and Analytical Data

B. Recorder Traces/Data Log

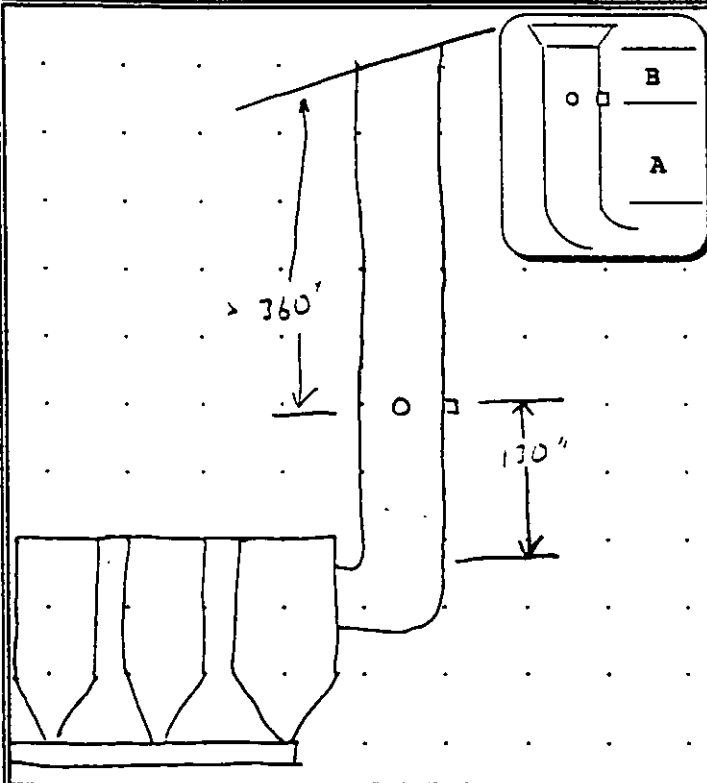
C. Calibration Data

STACK CONFIGURATION AND SAMPLE POINT LAYOUT FOR CIRCULAR STACKS

PLANT: L.P. - Hanceville
SOURCE: Dwyer Multicore 2-2-68
TEST FOR: Ph Sat. ay
TEST OPERATORS: R. W. Jones

Date:

SKETCH OF STACK



PERCENT OF DIAMETER

Points on a diameter

[illegible]

STACK DIAMETER:

41.75

Distance from ports to disturbance:

A. to upstream disturbance

360"

8. to downstream disturbance

130"

Upstream diameters: ---

8.6

Downstream diameters:

3.

Minimum No. sample points required:

12

No. sample points selected:

$$L \times \mathbb{Z}$$

Port Length:

4.0'

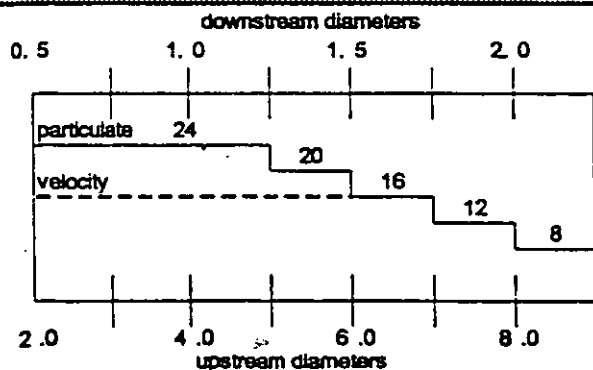
Port Type:

?" signifik

Port Access:

Mr. L. J. / 10th /

MINIMUM NO. OF POINTS ON A DIAMETER

Point
No.

Dances
from well

velocity head

[illegible]

Pilot ID :

Phot Cop:

Stack Temp:

Remarks:

Meter Box	<u>Anderson</u>	No. Sample Pts.	<u>612</u>	Gas Analysis	_____	Remarks:	_____
Sample Box	<u>10 9</u>	Minutes/Pt.	<u>2.5</u>	CO ₂	_____		_____
Probe/Pitot	<u>5' in</u>			O ₂	_____		_____
Pitot Cp	<u>.86</u>	NOMOGRAPH		CO	_____		_____
Nozzle Dia.	<u>2 1/4 2 1/0</u>	ΔH@	<u>1.80</u>	Time	_____		_____
Filter No.	_____	Meter Temp.	<u>100</u>				_____
		% H ₂ O	<u>12</u>	Condensate:	<u>321</u>		_____
Amb. Temp. °F	<u>65</u>	C-Factor	<u>.72</u>	tare	<u>200</u>	fin	<u>247</u>
Bar. Press. "Hg	<u>29.80</u>	Stack Temp.	<u>170</u>	Silica gel:			_____
Static Press. "H ₂ O	_____	Ref. ΔP	<u>1.10</u>	tare	_____	fin	<u>46</u>

Environmental Monitoring Laboratories — Ridgeland, Mississippi — 601-856-3092

Meter Box	<u>Anderson</u>	No. Sample Pts.	<u>6x2</u>	Gas Analysis		Remarks:	
Sample Box	<u>10.3</u>	Minutes/Pt.	<u>2.9</u>		CO ₂		
Probe/Pitot	<u>5' au</u>				O ₂		
Pitot Cp	<u>.84</u>	NOMOGRAPH		CO			
Nozzle Dia.	<u>.210</u>	ΔH@	<u>1180</u>	Time			
Filter No.		Meter Temp.	<u>10°</u>				
		% H ₂ O	<u>12 / 20</u>	Condensate:			
Amb. Temp. °F	<u>65</u>	C-Factor	<u>92 / 79</u>	tare <u>200</u>	fin <u>320</u>		
Bar. Press. "Hg	<u>29.60</u>	Stack Temp.	<u>170 / 170</u>	Silica gel:			
Static Press. "H ₂ O		Ref. Δ P	<u>1.3 / 1.3</u>	tare	fin <u>11</u>		

RUN No. 1
Date 7-31-44
Time start 1033 end 1105

Remarks:

Plant L.P. Knoxville, AL
 Sampling Location #4 Oxygen Inlet
 Test For PM1 / AOKI
 Test Operators _____

RUN No. 2
 Date 3-31-94
 Time start 1146 end 1220

Meter Box	<u>Reck</u>	No. Sample Pts.	<u>652</u>	Gas Analysis	<u>air</u>	Remarks: <u>100 ml water</u> <u>of dist'd</u> <u>water</u>
Sample Box	<u>10.3</u>	Minutes/Pt.	<u>25</u>	CO,	_____	
Probe/Pitot	<u>5' long</u>			O,	_____	
Pitot Cp	<u>.84</u>	NOMOGRAPH		CO	_____	
Nozzle Dia.	<u>210</u>	$\Delta H @$	<u>1.90</u>	Time	_____	
Filter No.	_____	Meter Temp.	<u>120</u>	Condensate: <u>347</u>		
Amb. Temp. °F	<u>65</u>	% H ₂ O	<u>13</u>	tare <u>200</u>	fin <u>247</u>	
Bar. Press. "Hg	<u>29.82</u>	C-Factor	<u>80.92</u>	Silica gel: <u>5.5</u>		
Static Press. "H ₂ O	_____	Stack Temp.	<u>170</u>	tare _____	fin _____	
		Ref. ΔP	<u>1.10</u>			

Port Point	El. Time, Min.	DGM Reading, Ft.	Velocity Head ΔP , in. H ₂ O	Orifice ΔH in. H ₂ O	Stack Temp. °F	Meter Temp., °F In	Meter Temp., °F Out	Oven Temp. °F	Imp. Temp. °F	Vac in. Hg
1	000	985.977	1.10	1.85	161	81	80	260	60	4
2	230	987.9	1.30	2.20	163	85	80	258	58	4
3	500	989.9	1.30	2.20	165	90	80	261	55	4
4	730	992.0	1.10	1.85	164	95	80	257	55	4
5	1000	993.9	1.60	2.70	164	99	81	262	55	5
6	1230	996.1	1.10	1.85	162	105	82	260	55	5
1	1510	998.410	1.20	2.00	163	99	84	265	55	4
2	2330	001.2	1.30	2.20	164	106	85	262	52	4
3	500	002.6	1.20	2.00	164	108	86	260	50	4
4	730	004.6	1.10	1.85	163	110	87	258	50	4
5	1000	006.4	0.92	1.55	163	112	88	259	50	4
6	1230	008.3	1.20	2.00	162	113	89	260	51	4
230/00		010.3183								
		230.251		057		006	114	8	714	
		24.406	1.0938	2.0208	113.17		91.88			

PARTICULATE CATCH ANALYSIS

SAMPLES: L.P. Hamaville - RTO hlets

DATE TAKEN: _____ DATE ANALYZED: _____

DELIVERED BY: _____ RECEIVED BY: _____

ANALYZED BY: _____

(Attach chain of custody if additional exchanges occur)

FILTERS: _____

RUN NO.	D3 R1	D3 R2	D4 R1	D4 R2
FILTER NO.	701	816	702	832
FILTER TARE, gms.	.5414	.5450	.5478	.5470
	.7319	.7650	.6894	.6764
FINAL WEIGHT, gms.	.7319	.7650	.6894	.6764
NET GAIN, gms.				

PROBE WASH: _____

RUN NO.	D3 R1	D3 R2	D4 R1	D4 R2
CONTAINER I.D.	D3 R1	D3 R2	D4 R1	D4 R2
VOLUME INTACT?	✓	✓	✓	✓
VOLUME, ml	140	200	200	200
TARE WEIGHT, gms.	(9) 114.8182	(26) 98.6682	(12) 112.5364	(85) 109.1512
	114.8245	98.6763	112.5414	109.1633
FINAL WEIGHT, gms.	114.8245	98.6763	112.5414	109.1633
NET GAIN, gms.	.0063	.0081	.0050	.0121
LESS BLANK, gms.				

PARTICULATE SAMPLE WEIGHT:

D3

D4

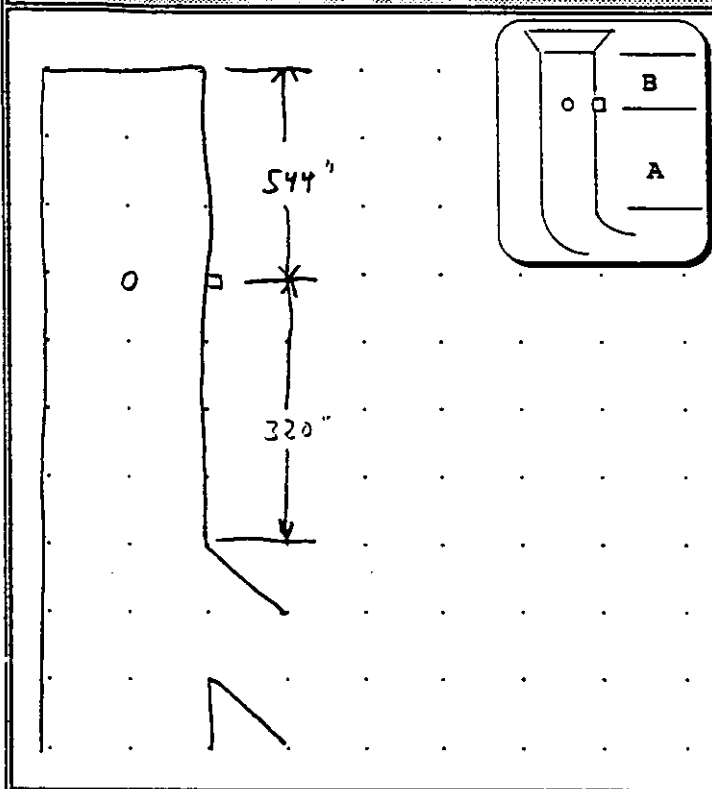
RUN NO.	1	2	1	2
filter + probe, mg.	196.8	228.1	146.6	141.5

STACK CONFIGURATION AND SAMPLE POINT LAYOUT FOR CIRCULAR STACKS

PLANT: L.P. Hanceville
SOURCE: West/East RTO
TEST FOR: PM Setup
TEST OPERATORS: Rumsey

Date:

SKETCH OF STACK



PERCENT OF DIAMETER

points on a diameter

[illegible]

STACK DIAMETER:

85.5

Distance from ports to disturbance:

A. to upstream disturbance

320"

B. to downstream disturbance

544

Upstream diameters:

3.7

Downstream diameters:

6.4

Minimum No. sample points required:

24

No. sample points selected:

12x2

Port Length:

425"

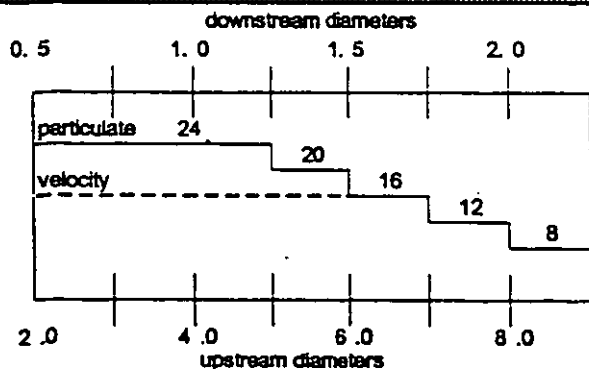
Port Type:

4" pipe nipple

Port Access:

Platform

MINIMUM NO. OF POINTS ON A DIAMETER

Point
No.

Index
Front Wall

velocity head

1	1.8	
2	5.7	
3	10.1	
4	15.1	
5	21.4	
6	30.4	
7	55.1	
8	64.1	
9	70.4	
10	75.4	
11	79.8	
12	83.3	

Pilot ID :

Phat Cp:

Stack Temp:

Remarks:

Plant L.P. Hancock, AL
 Sampling Location West ATO Outlet
 Test For PM / NOx
 Test Operators None / B. Mckenicht
 RUN No. 1
 Date 3-31-94
 Time start 1612 end 1713

Meter Box	<u>Quincy</u>	No. Sample Pts.	<u>12x2</u>	Gas Analysis	CO ₂ _____ O ₂ _____ CO _____ Time _____	Remarks:
Sample Box	<u>10.4</u>	Minutes/Pt.	<u>2.5</u>			
Probe/Pitot	<u>8' in</u>	NOMOGRAPH				
Pitot Cp	<u>.84</u>	ΔH@				
Nozzle Dia.	<u>.270</u>	Meter Temp.	<u>100</u>	Condensate:		
Filter No.		% H ₂ O	<u>20</u>	tare <u>200</u> fin <u>330</u>		
Amb. Temp. °F	<u>59</u>	C-Factor	<u>.79</u>	Silica gel:		
Bar. Press. "Hg	<u>29.80</u>	Stack Temp.	<u>275</u>	tare _____ fin <u>44.5</u>		
Static Press. "H ₂ O		Ref. ΔP	<u>.56</u>			

Port Point	El. Time, Min.	DGM Reading, Ft.	Velocity Head Δ P, in. H ₂ O	Orifice Δ H in. H ₂ O	Stack Temp. °F	Meter Temp., °F		Oven Temp. °F	Imp. Temp. °F	Vac. in. Hg
						In	Out			
1	0.20	061.429	0.98	3.25	260	79	81	257	50	4
2	2.70	063.8	0.88	2.90	262	85	80	260	48	4
3	5.20	066.2	0.96	3.20	259	91	79	258	48	4
4	7.70	068.7	0.85	2.85	261	97	79	264	45	4
5	10.20	071.1	0.95	3.20	260	101	79	258	45	4
6	12.70	073.5	0.92	3.05	262	105	80	256	42	4
7	15.20	076.0	0.71	2.40	259	109	81	262	45	4
8	17.70	078.3	0.52	1.70	260	110	83	264	45	4
9	20.20	080.1	0.47	1.55	259	108	84	270	45	4
10	22.70	081.9	0.41	1.35	256	107	85	264	48	3
11	25.20	083.5	0.39	1.30	249	105	86	262	48	3
12	27.70	085.1	0.35	1.15	249	106	86	264	49	3
13										
14	30.20	086.6	0.85	3.50	251	96	86	262	51	4
15	32.70	089.1	1.10	3.50	258	115	88	262	51	4
16	35.20	091.7	1.10	3.50	261	120	89	263	50	4
17	37.70	094.4	1.05	3.50	259	124	91	264	55	4
18	40.20	096.9	1.05	3.50	261	126	93	259	58	4
19	42.70	099.6	0.90	3.00	263	127	95	257	60	4
20	45.20	102.0	0.81	2.70	261	126	96	253	61	4
21	47.70	104.2	0.67	2.25	258	126	96	260	62	4
22	50.20	106.4	0.60	2.00	262	123	97	257	59	3
23	52.70	108.4	0.53	1.75	256	121	97	267	54	3
24	55.20	110.3	0.60	2.00	263	120	98	270	55	3
25	57.70	112.3	0.45	1.50	263	121	98	266	56	3
26	60.20	114.1	0.59	1.5						
27										
28										
29										
30										
31										
32										
33										
34										
35										
36										
37										
38										
39										
40										
41										
42										
43										
44										
45										
46										
47										
48										
49										
50										
51										
52										
53										
54										
55										
56										
57										
58										
59										
60										
61										
62										
63										
64										
65										
66										
67										
68										
69										
70										
71										
72										
73										
74										
75										
76										
77										
78										
79										
80										
81										
82										
83										
84										
85										
86										
87										
88										
89										
90										
91										
92										
93										
94										
95										
96										
97										
98										
99										
100										

Plant L.P. Hanceville, AL
 Sampling Location East ATO Outlet
 Test For PM10
 Test Operators Wm/B Backus

RUN No. 1
 Date 3-31-94
 Time start 1747 end 1848

Meter Box Andover
 Sample Box No. 3
 Probe/Pitot 8" in
 Pitot Co 80
 Nozzle Dia. 2.70
 Filter No.
 Amb. Temp. °F 55
 Bar. Press. "Hg 29.60
 Static Press. "H₂O

No. Sample Pts. 12 x 2
 Minutes/Pt. 2.5
 NOMOGRAPH
 ΔH@ 1.90
 Meter Temp. 100
 % H₂O 14
 C-Factor .89
 Stack Temp. 275
 Ref. ΔP .50

Gas Analysis
 CO₂
 O₂
 CO
 Time
 Condensate:
 tare 200 fin 318
 Silica gel:
 tare fin 412

Remarks:

Port Point	El. Time, Min.	DGM Reading, Ft.	Velocity Head ΔP, in. H ₂ O	Orifice ΔH in. H ₂ O	Stack Temp. °F	Meter Temp., °F In	Meter Temp., °F Out	Oven Temp. °F	Imp. Temp. °F	Vac. in. Hg
1	100	114.4	0.71	2.60	269	91	89	259	60	3
2	230	116.6	0.72	2.65	261	96	88	258	55	3
3	500	118.8	0.66	2.45	273	99	87	267	52	2
4	730	121.1	0.68	2.60	271	103	86	260	50	3
5	1000	123.3	0.70	2.60	270	106	86	262	51	3
6	1230	125.5	0.69	2.60	269	108	87	262	51	7
7	1500	127.7	0.64	2.40	269	110	87	260	52	3
8	1730	129.8	0.56	2.10	267	111	88	258	50	3
9	2000	131.9	0.47	1.75	265	111	88	260	45	3
10	2230	133.7	0.48	1.80	265	109	88	259	42	3
11	2500	135.6	0.34	1.30	269	108	88	261	42	3
12	2730	137.1	0.26	1.35	269	105	89	263	45	3
13										
1	2000	138.1	0.98	3.35	275	94	86	260	45	3
2	2300	141.0	0.98	3.35	276	112	89	263	48	3
3	500	143.9	0.95	3.60	275	118	90	265	48	3
4	730	146.6	0.96	3.60	266	121	90	265	49	3
5	1000	149.0	0.92	3.50	272	123	92	266	49	3
6	1230	151.7	0.79	2.95	267	123	92	258	40	3
7	1500	153.9	0.63	2.30	275	121	92	260	51	3
8	1730	156.0	0.54	2.00	266	118	93	260	51	3
9	2000	158.1	0.51	1.90	272	116	93	259	52	3
10	2230	160.0	0.48	1.80	269	115	93	260	52	3
11	2500	161.8	0.46	1.70	270	115	94	261	52	3
12	2730	163.6	0.40	1.50	265	113	94	270	50	3
amb	1600	165.1	2.41							
27		26.16								
30										
33										

PARTICULATE CATCH ANALYSIS

SAMPLES: L.P. Hamwill - RTU outlet

DATE TAKEN: _____ DATE ANALYZED: _____

DELIVERED BY: DR RECEIVED BY: DR

ANALYZED BY: DR

(Attach chain of custody if additional exchanges occur)

FILTERS: _____

RUN NO.	EAST	WEST		
FILTER NO.	818	817		
FILTER TARE, gms.	.5467	.5468		
	.5525	.5531		
FINAL WEIGHT, gms.	.5525	.5531		
NET GAIN, gms.	.0058	.0063		

PROBE WASH: _____

RUN NO.	EAST	WEST		
CONTAINER I.D.	EAST R1	WEST R1		
VOLUME INTACT?	✓	✓		
VOLUME, ml	120	150		
TARE WEIGHT, gms.	(45) 107.2512	(87) 107.2360		
	107.2550	107.2334		
FINAL WEIGHT, gms.	107.2550	107.2334		
NET GAIN, gms.	.0038	.0034		
LESS BLANK, gms.				

PARTICULATE SAMPLE WEIGHT:

RUN NO.	EAST	WEST		
filter + probe, mg.	9.6	9.7		

DRY GAS METER CALIBRATION

Meter ID Andersen
 Calibration Method DGM/DGM By DGR
 Calibration Meter ID 651729 Pbar 29.80
 Date 4/11/94

Vac. In. Hg	DH In. H2O	Time min	Calibrating Meter			Field Meter						Y	Q	K	DH@
			Vi cf	Vf cf	Temp F	Vi cf	Vf cf	Temp. In		Temp out					
								init	final	init	final				
1	4.00	10.00	346.87	358.001	82	93.507	104.898	100	117	102	103	1.010	1.14	0.71	1.815
1	3.00	11.00	358.001	368.729	84	104.898	115.935	113	129	103	107	1.016	1.01	0.72	1.774
1	2.00	13.00	368.729	379.137	84	115.935	126.714	118	133	107	111	1.020	0.83	0.73	1.738
1	1.00	18.00	379.137	389.442	84	126.714	137.456	118	127	111	115	1.016	0.6	0.74	1.683
1	0.75	20.00	389.442	399.506	84	137.456	148.024	112	125	113	118	1.008	0.53	0.75	1.626
Averages:												1.01			1.73

$$Y = [V_{cal}](P_{bar})(T_{dgm}) / [(V_{dgm})(P_m)(T_{cal})]$$

$$K = Q(\sqrt{(P_m M_m)} / ((T_m \text{ out})(DH)))$$

$$Q = ((V_{mi} - V_{mf}) / \text{min.})(T_{m, out} / T_{m, avg})(Y)$$

$$DH@ = 0.921 / K^2$$

Where:

Y = Meter correction factor, dimensionless

Vcal = Volume of gas through calibrating meter, cubic feet

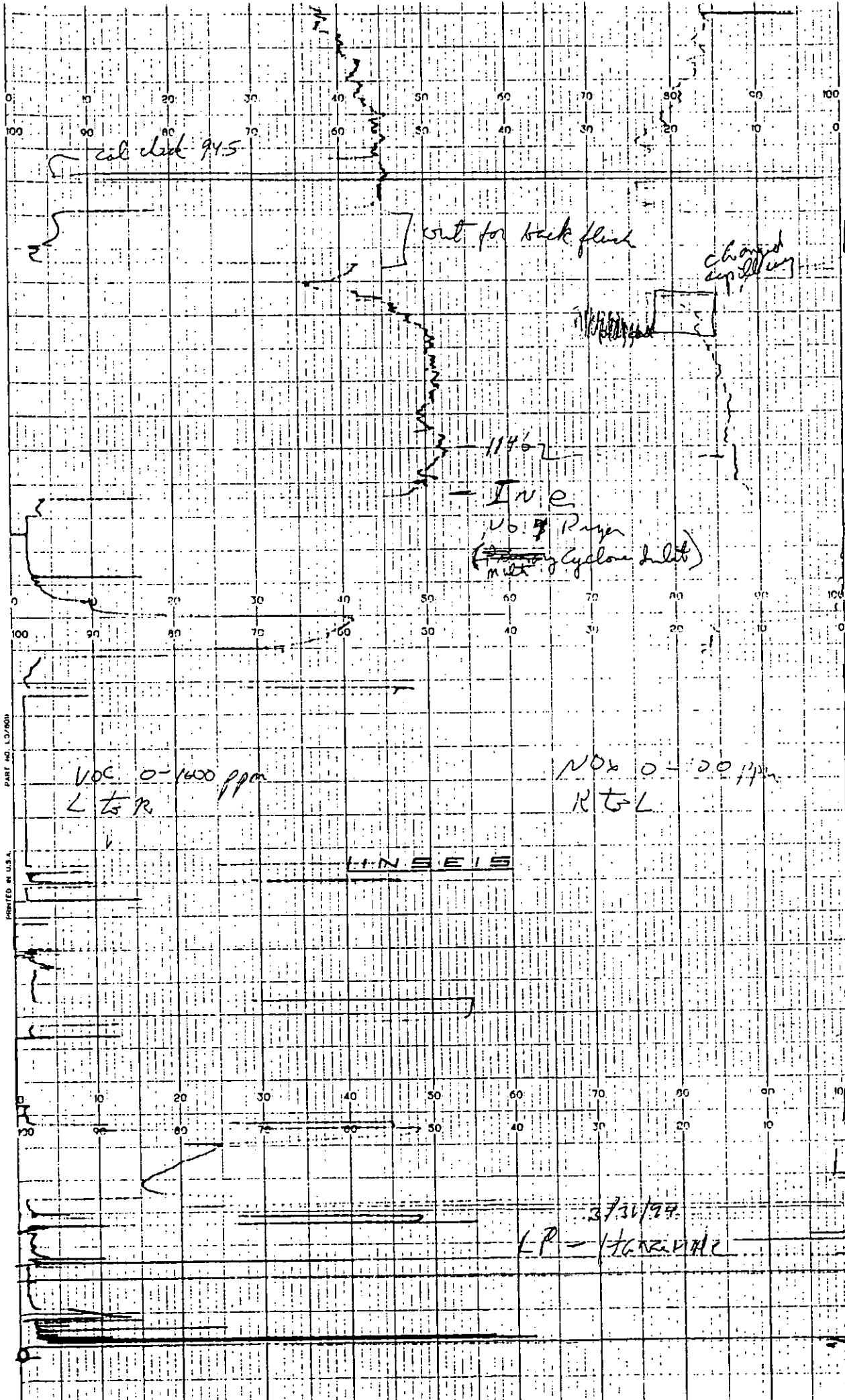
Vdgm = Volume of gas through field dry gas meter, cubic feet

Pbar = Barometric pressure, in. Hg

Pm = Meter pressure, (Pbar = DH/13.6)

Tdgm = Average dry gas meter temp, degrees R

Tcal = Temperature of gas at calibrating meter, degrees R



calc clock 945

out for back flink

changed sup. 11/11/97

11462

In e

No. 7 Payer
(Cyclone Inlet)
mult

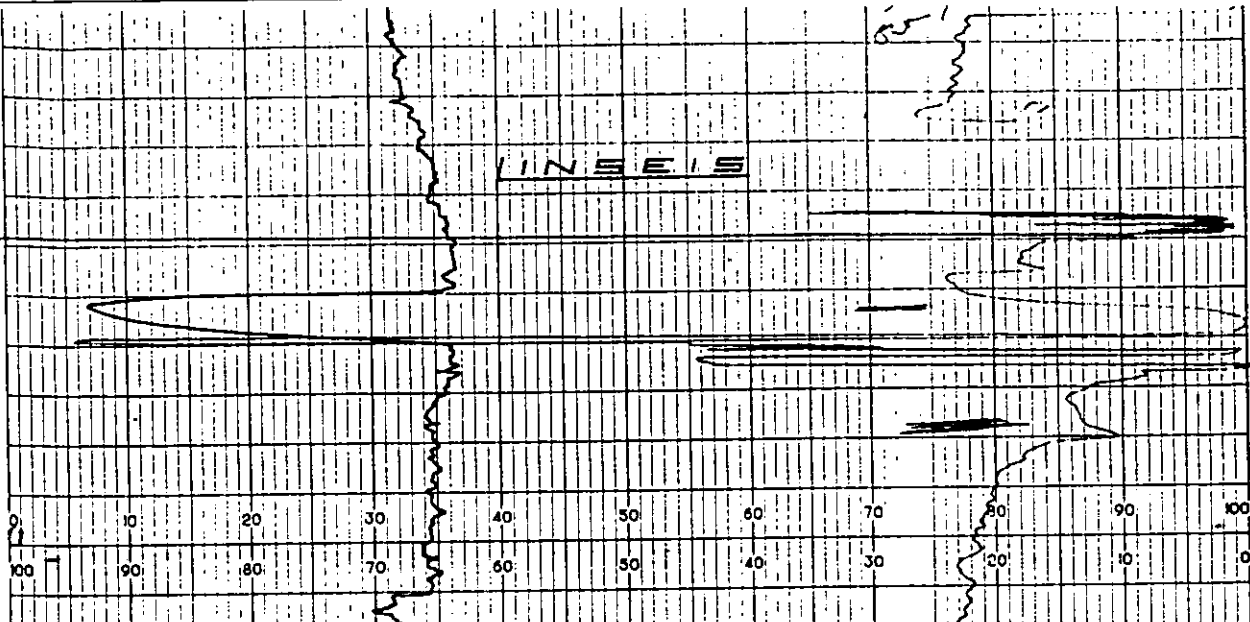
VOC 0-1400 ppm
L to R

NOx 0-200 ppm
R to L

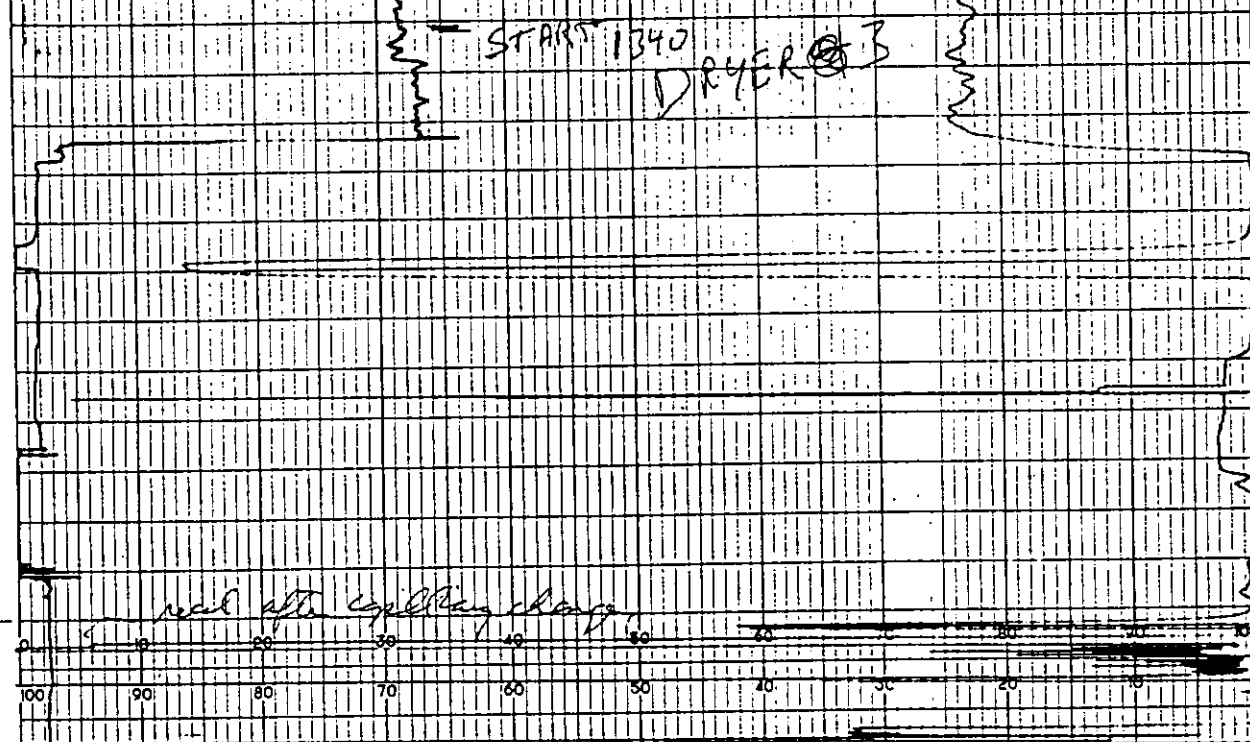
INSEIS

3/31/99

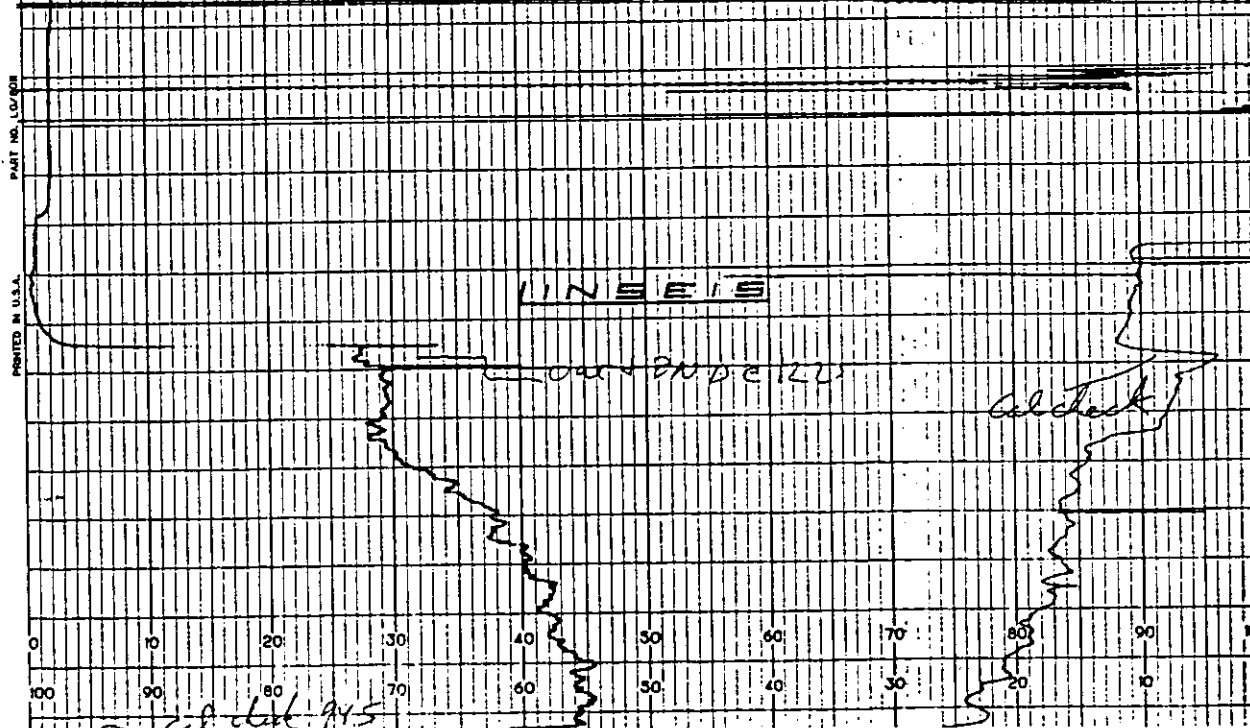
LP - 16.22.14.12



STARTS 1340
DRYER 3



read after copy change



040-2ND 122

Cal Check

Cal Check 945

PART NO. 19,000

PRINTED IN U.S.A.

START EAST RTD @ 1745

LINSEIS

GO ON E. WEST TO 0.000
170

check to 0-100

START RUN E WEST TO 0.000
8.000

10.5 is

Check to 0-100

START RUN 2 WEST 60 0.021
TLCAL

0 10 20 30 40 50 60 70 80 90 100
100 90 80 70 60 50 40 30 20 10 0

645 CAL

PART NO. LD/808

PRINTED IN U.S.A.

LINE 15

0 10 20 30 40 50 60 70 80 90 100
100 90 80 70 60 50 40 30 20 10 0

at end

0 10 20 30 40 50 60 70 80 90 100
100 90 80 70 60 50 40 30 20 10 0

PART NO. LD/808

PRINTED IN U.S.A.

LINE 15

0 10 20 30 40 50 60 70 80 90 100
100 90 80 70 60 50 40 30 20 10 0

0 10 20 30 40 50 60 70 80 90 100
100 90 80 70 60 50 40 30 20 10 0

PART NO. 10-0000

PRINTED IN U.S.A.

UNSEIS

10 20 30 40 50 60 70 80 90 100
100 90 80 70 60 50 40 30 20 10 0