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**Title: Certification Report for Continuous
Mointoring System Louisiana -
Pacific Corporation Oroville Boilers,
#4 & 5,**

Carnot

May 1994

**CERTIFICATION REPORT FOR
CONTINUOUS EMISSION
MONITORING SYSTEM
LOUISIANA-PACIFIC CORPORATION
OROVILLE BOILERS #4 AND #5**

Prepared For:

LOUISIANA-PACIFIC CORPORATION
Samoa, California

For Submittal To:

BUTTE COUNTY AIR POLLUTION CONTROL DISTRICT
Durham, California
and
U.S. ENVIRONMENTAL PROTECTION AGENCY REGION IX
San Francisco, California

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CARNOT
Concord, California

MAY 1994

REVIEW AND CERTIFICATION

All work, calculations, and other activities and tasks performed and documented in this report were carried out under my direction and supervision.

Erick Mirabella

Date 5/17/94

Erick M. Mirabella
Senior Technician

I have reviewed, technically and editorially, details, calculations, results, conclusions and other appropriate written material contained herein, and hereby certify that the presented material is authentic and accurate.

Kevin J. Crosby

Date May 17, 1994

Kevin J. Crosby
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SECTION 1.0

INTRODUCTION

Carnot was contracted to perform a series of emission measurements at the Louisiana-Pacific Corporation (L-P) facility in Oroville, California. The testing program on Boilers #4 and #5 addressed two regulatory issues. Some of the tests were performed to determine compliance with EPA New Source Performance Standards and with conditions of the permits from the Butte County Air Pollution Control District (BCAPCD). Additional tests were performed to certify the performance of the continuous emission monitoring systems (CEMS) in accordance with 40 CFR 60, Appendix B. The CEMS certification results are presented in this report.

The tests were performed by Kevin Crosby, Erick Mirabella, and John Peterson of Carnot's Northern California Division on May 3, 4 and 5, 1994. Unit operations were coordinated by Bill Webb of L-P. The tests were observed by Bob McLaughlin of the BCAPCD.

The average test results are presented in Table 1-1 for comparison with the applicable Performance Specifications. These results indicate that the CEMS on Boilers #4 and #5 meets the applicable performance specifications. The results of individual test runs are presented in Section 4.0 and in the Appendices.

TABLE 1-1
RESULTS SUMMARY
CEMS CERTIFICATION TESTS
LOUISIANA-PACIFIC OROVILLE, BOILERS #4 AND #5
MAY 1994

Analyzer	Relative Accuracy, % ¹	Calibration Drift, %	Performance Specification	
			RA %	CD % ²
Boiler #4				
NO _x ppm vol. wet	6.49	(zero) 0.8 (span) 1.5	20	2.5 2.5
O ₂ , vol. wet	4.80	(zero) 0.2 (span) 0.3	20	0.5 0.5
Opacity, %	N/A	(zero) 0.00 (span) 0.11	N/A	2.0 2.0
Boiler #5				
NO _x , ppm vol. wet	7.35	(zero) 0.4 (span) 2.2	20	2.5 2.5
O ₂ , % vol. wet	1.34	(zero) 0.1 (span) 0.4	20	0.5 0.5
Opacity, %	N/A	(zero) 0.05 (span) 0.06	N/A	2.0 2.0

¹ Calculated in comparison to the Reference Method average results.

² The calibration drift specification for O₂ is 0.5% O₂. The drift specification for opacity is 2% opacity. Other calibration drift specifications are in % of the span value.

SECTION 2.0

FACILITY DESCRIPTION

The Louisiana-Pacific Corporation facility in Oroville, California produces medium density fiberboard (MDF). Steam for the plant's fiber dryers and board presses is produced by a wood-fired boiler and by a sander dust-fired boiler known as Boilers #4 and #5.

Boiler #4 is a four-cell wood-fired system manufactured by the Wellons Company of Tualatin, Oregon and rated at 80,000 lb/hr of steam production. Fuel is typically a variable bark-wood-nutshell hogged mixture. Boiler exhaust gases pass through an air pre-heater, a multiclone, an induced draft fan, and a two-stage electrostatic precipitator.

Boiler #5 is a Cleaver-Brooks boiler with a Coen suspension burner for firing sander dust from the hardboard manufacturing operation. No combustion air heating is done with the exhaust, so the exhaust temperature is relatively high for contemporary wood fired boilers (approximately 510° F). The boiler fires at permit capacity 5,000 lbs/hr of wood (sander dust) fuel, and produces 30,000 lbs/hr of steam. Particulate emissions are controlled with a multiclone and a single-stage electrostatic precipitator. Combustion controls and flue gas recirculation (FGR) are used to keep NO_x and CO emissions within permit limits. The fuel feed system and FGR system have been recently modified to provide improved combustion conditions.

2.1 DESCRIPTION OF CEMS

The CEMS for Boilers #4 and #5 includes an Oxygen analyzer and an Opacity monitor on each Boiler, and a single NO_x analyzer which is shared by the Boilers. The Oxygen analyzers are in-situ, wet-basis units. The NO_x analyzer system uses an extractive dilution probe system on each Boiler, and a microprocessing unit which provides outputs of the two NO_x signals (i.e. the current reading for one Boiler and the most recent reading for the other). The NO_x analyzer raw output of ppm wet volume is processed to units of ppm dry volume @ 12% CO₂ using constant correction factors and the measured O₂ concentration. These corrected NO_x results are reported as a running three-hour average.

The single NO_x analyzer is a Monitor Labs, Inc. Model 8840, which uses the chemiluminescence method for measurement of NO concentrations. The analyzer uses a thermal NO₂-to-NO converter to provide measurement of total NO_x concentrations. The analyzer is

designed to measure NO_x in concentrations less than 5 ppm. The sample from each Boiler is therefore diluted with dry air for delivery to the analyzer.

The dilution system at Boiler #5 is a Phoenix Instruments Model 1010 probe dilution extraction system. At Boiler #4, a Dynatron Model 5010 system is used. Both these systems condition the sample to remove particulate matter and to dilute the wet-basis sample with dry air. The samples delivered to the NO_x analyzer are therefore diluted to reduce the moisture content so that the dew point is below the ambient temperature. The sample gas is therefore delivered without condensing any moisture, so any water-soluble gases (e.g. NO_2) are retained. The analyzer output represents the wet-basis NO_x concentration as exists in the stack.

Since the calibration gases are delivered to the analyzer through the same sampling systems, each entire system is calibrated as an integral part of the analyzer. This allows for calibration checks on the same analyzer in a different concentration range for each boiler. The analyzer output is 0 to 1000 ppm volume wet for Boiler #5, and 0 to 200 ppm volume wet for Boiler #4. The analyzer is calibrated with a high-range calibration gas and with zero gas, on an automatic cycle once each 24 hours. The calibration response is output directly to the chart recorders.

A microprocessor unit is used to control the NO_x sampling and analysis system. The Analog Devices Model umac-4000 controls the auto calibrations, blow back of the sampling probes, and associated timing and sequencing for the O_2 and NO_x analyzers. The unit provides output of the NO_x concentrations in 2-minute averages for each boiler once every six minutes. The last average data output is held until the next sequence for each boiler. The data are recorded on a circular chart recorder. The system also processes the data to provide output of the NO_x concentrations corrected to dry-basis ppm @ 12% CO_2 which is recorded on a circular chart recorder as a three-hour running average.

The O_2 analyzer on each boiler is a Dynatron, Inc. Model 401. These analyzers are in-situ, wet-basis units with a range of 0 to 25 % volume wet O_2 . The output from these analyzers is averaged, held and output to circular chart recorders with the NO_x concentration data. The analyzers are calibrated with a low-range calibration gas and with ambient air, on an automatic cycle once each 24 hours. The calibration response is output directly to the chart recorders.

The Opacity analyzer on each boiler is a Dynatron, Inc. Model 1100M. The outputs from these analyzers are output as one-minute averages to circular chart recorders on a range of 0 to 20 % opacity for both boilers. Calibration checks on both analyzers are made with calibrated neutral-density filters, on an automatic cycle each 24 hours. The calibration response is output directly to the chart recorders.

SECTION 3.0

TEST DESCRIPTION

3.1 TEST CONDITIONS

The CEMS relative accuracy test runs were conducted with each boiler at 50% capacity or more. Test conditions were established and unit operating data were collected by L-P personnel. Carnot monitored the collection of process and CEMS data.

3.2 SAMPLING LOCATIONS

Samples were collected at each boiler stack in turn, from sampling ports which meet EPA or CARB Method 1 criteria. Sampling traverse points were located according to 40CFR60 Appendix B, Section 3.2. Diagrams of the sampling locations and traverse point locations are located in Appendix B.2.

3.3 TEST PROCEDURES

The test procedures used are summarized in Table 3-1. Descriptions of standard procedures are included in Appendix A. Additional information on specific applications of and modifications to standard procedures are presented in the following sub-sections. Where any conflicts exist in the descriptions, the specific description here in Section 3.3 will take precedence.

3.3.1 Gaseous Emissions

Concentrations of the gaseous constituents of the stack gas (NO_x , O_2 and CO_2) were measured according to the procedures of the EPA Methods 7E and 3A (CARB Method 100) using Carnot's mobile Continuous Emissions Monitor (CEM) described in Appendix A. This system meets the requirements of EPA and CARB methods for gaseous species. The heated Teflon line and ice bath described in Appendix A was used to prevent loss of NO_2 in the sampling system. The CO_2 concentrations were monitored to provide data for correction of NO_x concentrations to 12% CO_2 basis.

Three gaseous emission test runs were performed to determine compliance with the permit conditions, with each run a minimum of forty minutes in duration. Each of these compliance test runs were performed during one of the three tests for particulate matter

TABLE 3-1
EMISSION TEST PROCEDURES USED FOR
CEMS RELATIVE ACCURACY TESTS AT
LOUISIANA-PACIFIC OROVILLE BOILERS # 4 AND #5

Parameter	No. Replicates	Duration of Test (min.)	Measurement Principle	Reference Method	Method Detection Limit
NO _x	3	30 to 40	Chemiluminescent	CARB 100 EPA 7E	Below 2% of instrument full scale
O ₂	3	30 to 40	Electrochemical cell	CARB 100 EPA 3A	Below 2% of instrument full scale
CO ₂	3	30 to 40	Nondispersive infrared	CARB 100 EPA 3A	Below 2% of instrument full scale

emissions. Additional 30-minute test runs were performed during and between the particulate test runs to provide data for the CEMS relative accuracy tests.

The sampling probe was placed at the three traverse points for 10 to 15 minutes each during the first test run on each boiler. Since no stratification of concentrations was detected, the probe was located near the center of the stack cross-section for the subsequent test runs.

The analyzers were calibrated with gases which have been certified by EPA Protocol 1 (NO_x) or by gravimetric analysis (O_2 and CO_2). The analyzer ranges and gas concentrations that were used are listed in Table 3-2. The NO_x calibration gases did not all meet exactly the range criteria of EPA Method 7E, but these gases were described in the Test Plan prior to the field testing program.

3.3.2 Flow Rate and Moisture Content

Stack gas volumetric flow rate and moisture content was determined by CARB Methods 2 and 4 in conjunction with every particulate test. The moisture results were used in calculation of the wet-basis NO_x and O_2 concentrations from the measured dry-basis concentrations.

3.3.3 CEMS Certification

Relative Accuracy Tests (RA Test) and Calibration Drift Tests (CD Test) were performed on the unit's continuous emission monitoring system (CEMS). The CEMS includes analyzers for measurement of concentrations of NO_x and O_2 . A minimum of nine and a maximum of twelve test runs were performed to complete the RA Test as specified in 40CFR60, Appendix B. L-P personnel provided calibration drift data to determine compliance with the CD Test specifications of 40CFR60, Appendix B.

The plant CEMS data are recorded on circular chart recorders. The NO_x analyzer output is in ppm volume, wet basis. The data handling system provides output to the recorder for a two minute average NO_x concentration from each boiler once each six minutes. The analyzer reads one boiler for three minutes (one minute to stabilize the response, then two minutes of concentration monitoring), then the other boiler for three minutes. The two-minute average NO_x concentration is held as a steady output to the recorder until the next average output for that boiler. For determination of relative accuracy, the concentration trace on the recorder chart was averaged for the time period of each reference method test run. The NO_x relative accuracy was therefore determined from the average of the two-minute averages over the period of each test run.

TABLE 3-2
CARNOT MOBILE CEM INSTRUMENT RANGES
CEMS RELATIVE ACCURACY TESTS
LOUISIANA-PACIFIC OROVILLE BOILERS #4 AND #5
MAY, 1994

Analyzer	Range	Span Gas	Mid-Scale Gas
NO _x , Boiler #4	0 to 250 ppm	241 ppm	85 ppm
NO _x , Boiler #5	0 to 1000 ppm	722 ppm	453 ppm
O ₂ both units	0 to 10%	8%	5%
CO ₂ , both units	0 to 25%	22%	15%

Each boiler has its own O₂ analyzer, which can provide continuous output of the O₂ concentration. However, the data handling system keeps the data consistent by averaging the O₂ output in the same way as the NO_x output. The O₂ relative accuracy was therefore also determined from the average of the two-minute averages from each boiler over the period of each test run.

The plant CEMS also outputs running averages of the "corrected" NO_x concentrations. The wet-basis NO_x and O₂ concentrations are used to calculate the equivalent dry-basis ppm NO_x at 12 % CO₂. Correction constants are used to correct for the stack gas moisture content and for the CO₂ equivalent from the O₂ concentration. The output to the recorders is in a three-hour running average. There is no recording of "corrected" NO_x concentrations with shorter averaging times.

3.3.4 Process Data and Analyzer Calibration Drift Data

The plant's process instrumentation was used to document process conditions during the test runs. Process data presented in the report includes steam production rate.

Data from the plant CEMS circular chart recorders was used to document the relative accuracy of the analyzers. The analyzer response to the daily calibration checks were also taken from the charts to provide seven days of calibration drift data. Copies of the charts can be found in Appendix C.

3.4 TEST SCHEDULE

The tests on Boilers #4 and #5 were performed on May 3, 4 and 5, 1994. The individual data sheets presented in Appendix C provide documentation of the test times.

SECTION 4.0

TEST RESULTS

The results of the relative accuracy and calibration drift tests are summarized in Tables 4-1 through 4-6. Average results are presented in Table 1-1 for comparison with the applicable performance specifications. The results show the CEMS components to meet the performance specifications for relative accuracy and calibration drift as set forth in 40 CFR 60, Appendix B.

Additional information is included in the Appendices. Appendix A contains brief descriptions of standard measurement procedures. Appendix B presents the quality assurance information for Carnot's measurements, including instrument calibration data and cylinder gas certificates. Field data, CEMS and process data, and emission calculation spreadsheets are included in Appendix C. Appendix D presents both the general and specific equations used for the calculations of emissions, relative accuracy and calibration drift. Appendix E contains Carnot instrument strip charts.

The process rate during the relative accuracy test runs was greater than 50% of permit capacity for both boilers. All the test runs were used for the calculation of relative accuracy, except Run 1-CEM-4 for O₂. The Carnot O₂ analyzer did not meet the calibration QA criteria for that run, so the result was deleted from the calculation. The O₂ analyzer cell was replaced so that the subsequent test runs were successful.

TABLE 4-1
RESULTS SUMMARY
CEMS CERTIFICATION TESTS
LOUISIANA-PACIFIC OROVILLE, BOILERS #4 AND #5
MAY 1994

Analyzer	Relative Accuracy, % ¹	Calibration Drift, %	Performance Specification	
			RA %	CD % ²
Boiler #4				
NO _x ppm vol. wet	6.49	(zero) 0.8 (span) 1.5	20	2.5 2.5
O ₂ , vol. wet	4.80	(zero) 0.2 (span) 0.3	20	0.5 0.5
Opacity, %	N/A	(zero) 0.00 (span) 0.11	N/A	2.0 2.0
Boiler #5				
NO _x , ppm vol. wet	7.35	(zero) 0.4 (span) 2.2	20	2.5 2.5
O ₂ , % vol. wet	1.34	(zero) 0.1 (span) 0.4	20	0.5 0.5
Opacity, %	N/A	(zero) 0.05 (span) 0.06	N/A	2.0 2.0

¹ Calculated in comparison to the Reference Method average results.

² The calibration drift specification for O₂ is 0.5% O₂. The drift specification for opacity is 2% opacity. Other calibration drift specifications are in % of the span value.

TABLE 4-2
RESULTS SUMMARY
NO. RELATIVE ACCURACY TESTS
LOUISIANA-PACIFIC OROVILLE, BOILER #4
MAY 1994

RELATIVE ACCURACY DETERMINATION NOx ppm vol. wet						
CLIENT: L. P. Oroville			DATE: 5/4&5/94			
UNIT: Boiler #4			Data By: Carnot			
LOAD: Full Load			Data By: KJC			
Run #	Time	Carnot	L.P.	Difference	n	t(0,975)
1	1220-1250	84.56	78.0	6.56	2	12.706
2	1320-1350	85.60	80.4	5.20	3	4.303
3	1545-1625	84.72	79.2	5.52	4	3.182
4	1635-1705	76.20	71.2	5.00	5	2.776
5	1720-1800	83.60	78.0	5.60	6	2.571
6	0908-0938	67.56	65.0	2.56	7	2.447
7	1013-1043	81.88	78.0	3.88	8	2.365
8	1108-1138	81.74	81.4	0.34	9	2.306
9	1208-1238	60.08	57.0	3.08	10	2.262
10	1443-1523	75.99	73.6	2.39	11	2.228
11	1538-1608	78.39	74.8	3.59	12	2.201
12	1618-1648	79.51	75.4	4.11		
AVERAGES:		78.32	74.33	3.99		
STANDARD DEVIATION				1.731103		
CONFIDENCE COEFFICIENT				1.099898		
RELATIVE ACCURACY, %					6.49	

TABLE 4-3
RESULTS SUMMARY
O₂ RELATIVE ACCURACY TESTS
LOUISIANA-PACIFIC OROVILLE, BOILER #4
MAY 1994

RELATIVE ACCURACY DETERMINATION O ₂ % vol. wet						
CLIENT: L. P. Oroville			DATE: 5/4&5/94			
UNIT: Boiler #4			Data By: Carnot			
LOAD: Full Load			Data By: KJC			
Run #	Time	Carnot	L.P.	Difference	n	t(0,975)
1	1220-1250	4.24	4.58	-0.26	2	12.706
2	1320-1350	4.12	4.25	-0.13	3	4.303
3	1545-1625	4.42	4.50	-0.08	4	3.182
4	1635-1705	4.75	4.75	0.00	5	2.776
5	1720-1800	4.89	4.70	0.19	6	2.571
6	0908-0938	4.74	4.80	-0.06	7	2.447
7	1013-1043	5.60	5.60	0.00	8	2.365
8	1108-1138	4.47	4.80	-0.33	9	2.306
9	1208-1238	3.53	4.00	-0.47	10	2.262
10	1443-1523	4.25	4.45	-0.20	11	2.228
11	1538-1608	4.35	4.38	-0.03	12	2.201
12	1618-1648	4.56	4.40	0.16		
AVERAGES:		4.52	4.60	-0.09	(Run 1 deleted, see data sheets)	
STANDARD DEVIATION				0.19423		
CONFIDENCE COEFFICIENT				0.130478		
RELATIVE ACCURACY, %					4.80	

TABLE 4-4
RESULTS SUMMARY
NO_x RELATIVE ACCURACY TESTS
LOUISIANA-PACIFIC OROVILLE, BOILER #5
MAY 1994

RELATIVE ACCURACY DETERMINATION NO _x ppm vol. wet						
CLIENT: L. P. Oroville			DATE: 5/3/94			
UNIT: Boiler #5			Data By: Carnot			
LOAD: Full Load			Data By: KJC			
Run #	Time	Carnot	L.P.	Difference	n	t(0,975)
1	0945-1025	504.13	470.0	34.13	2	12.706
2	1100-1130	502.03	465.0	37.03	3	4.303
3	1145-1215	479.80	435.0	44.80	4	3.182
4	1240-1310	487.56	465.0	22.56	5	2.776
5	1325-1405	484.22	455.0	29.22	6	2.571
6	1420-1450	489.70	460.0	29.70	7	2.447
7	1510-1540	488.73	455.0	33.73	8	2.365
8	1605-1645	466.89	445.0	21.89	9	2.306
9	1700-1730	484.53	458.0	26.53	10	2.262
10	1750-1820	467.50	440.0	27.50	11	2.228
					12	2.201
AVERAGES:		485.51	454.80	30.71		
STANDARD DEVIATION				6.948372		
CONFIDENCE COEFFICIENT				4.970221		
RELATIVE ACCURACY, %					7.35	

TABLE 4-5
RESULTS SUMMARY
O₂ RELATIVE ACCURACY TESTS
LOUISIANA-PACIFIC OROVILLE, BOILER #5
MAY, 1994

RELATIVE ACCURACY DETERMINATION O ₂ % vol. wet						
CLIENT: L. P. Oroville			DATE: 5/3/94			
UNIT: Boiler #5			Data By: Carnot			
LOAD: Full Load			Data By: KJC			
Run #	Time	Carnot	L.P.	Difference	n	t(0,975)
1	0945-1025	4.94	4.88	0.06	2	12.706
2	1100-1130	4.71	4.70	0.01	3	4.303
3	1145-1215	4.70	4.70	0.00	4	3.182
4	1240-1310	4.72	4.70	0.02	5	2.776
5	1325-1405	4.69	4.70	-0.01	6	2.571
6	1420-1450	4.67	4.75	-0.08	7	2.447
7	1510-1540	4.68	4.75	-0.07	8	2.365
8	1605-1645	4.53	4.68	-0.15	9	2.306
9	1700-1730	4.80	4.80	0.00	10	2.262
10	1750-1820	4.81	4.75	0.06	11	2.228
					12	2.201
AVERAGES:		4.73	4.74	-0.02		
STANDARD DEVIATION				0.065862		
CONFIDENCE COEFFICIENT				0.047111		
RELATIVE ACCURACY, %					1.34	

**TABLE 4-6
RESULTS SUMMARY
CEMS CALIBRATION DRIFT TESTS
LOUISIANA-PACIFIC OROVILLE, BOILERS #4 AND #5
MAY, 1994**

Boiler #4

NO _x analyzer calibration drift, % of span value:	(zero) 0.8	(span) 1.5
O ₂ analyzer calibration drift, % O ₂ :	(low cal.) 0.2	(high cal.) 0.3
Opacity analyzer calibration drift, % Opacity:	(zero) 0.00	(cal.) 0.11

Boiler #5

NO _x analyzer calibration drift, % of span value:	(zero) 0.4	(span) 2.2
O ₂ analyzer calibration drift, % O ₂ :	(low cal.) 0.1	(high cal.) 0.4
Opacity analyzer calibration drift, % Opacity:	(zero) 0.05	(cal) 0.06

APPENDIX A
MEASUREMENT PROCEDURES

Continuous Emissions Monitoring System

Oxygen (O_2) by Continuous Analyzer

NO/ NO_x by Continuous Analyzer

Determination of Moisture in Stack Gases

Continuous Emissions Monitoring System

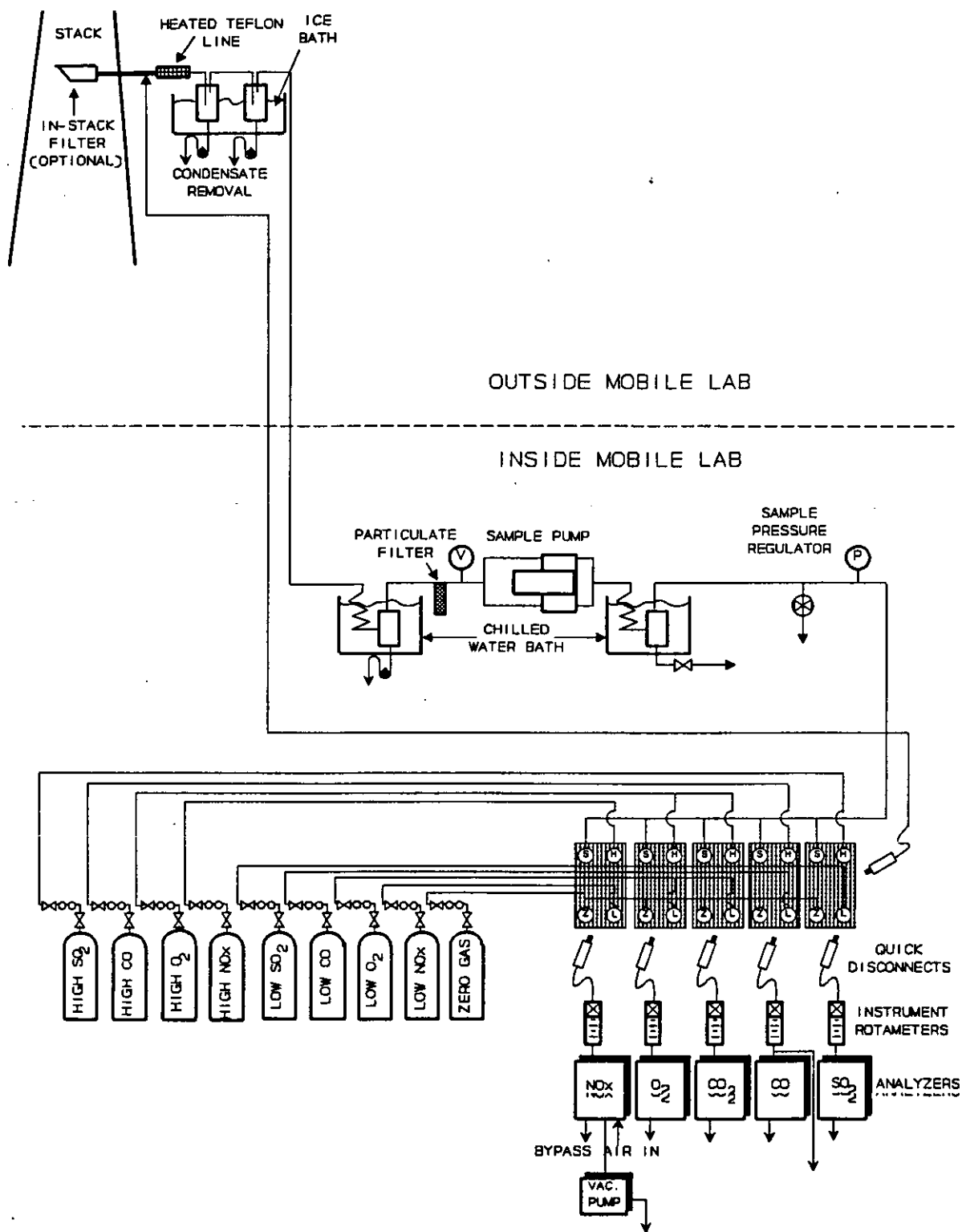
O₂, CO, CO₂, NO, NO_x and SO₂ are measured using an extractive continuous emissions monitoring (CEM) package, shown in the following figure. This package is comprised of three basic subsystems. They are: (1) the sample acquisition and conditioning system, (2) the calibration gas system, and (3) the analyzers themselves. This section presents a description of the sampling and calibration systems. Descriptions of the analyzers used in this program and the corresponding reference test methods follow. Information regarding quality assurance information on the system, including calibration routines and system performance data follows.

The sample acquisition and conditioning system contains components to extract a representative sample from the stack or flue, transport the sample to the analyzers, and remove moisture and particulate material from the sample. In addition to performing the tasks above, the system must preserve the measured species and deliver the sample for analysis intact. The sample acquisition system extracts the sample through a stainless steel probe. The probe is insulated or heated as necessary to avoid condensation. If the particulate loading in the stack is high, a sintered stainless steel filter is used on the end of the probe.

Where water soluble NO₂ and/or SO₂ are to be measured, the sample is drawn from the probe through a heated teflon sample line into an on-stack cooled (approximately 35-40°F) water removal trap. The trap consists of stainless steel flasks in a bath of ice and water. This design removes the water vapor by condensation. The contact between the sample and liquid water is minimized and the soluble NO₂ and SO₂ are conserved. This system meets the requirements of EPA Method 20. The sample is then drawn through a teflon transport line, particulate filter, secondary water removal and into the sample pump. The pump is a dual head, diaphragm pump. All sample-wetted components of the pump are stainless steel or teflon. The pressurized sample leaving the pump flows through a third condensate trap in a refrigerated water bath (≈38°F) for final moisture removal. A drain line and valve are provided to constantly expel any condensed moisture from the dryer at this point. After the dryer, the sample is directed into a distribution manifold. Excess sample is vented through a back-pressure regulator, maintaining a constant pressure of 5-6 psig to the analyzer rotameters.

The calibration system is comprised of two parts: the analyzer calibration, and the system bias check (dynamic calibration). The analyzer calibration equipment includes pressurized cylinders of certified span gas. The gases used are, as a minimum, certified to 1% by the manufacturer. Where necessary to comply with reference method requirements EPA Protocol 1 gases are used. The cylinders are equipped with pressure regulators which supply the calibration gas to the analyzers at the same pressure and flow rate as the sample. The selection of zero, span, or sample gas directed to each analyzer is accomplished by operation of the sample/calibration selector fittings.

The system bias check is accomplished by transporting the same gases used to zero and span the analyzers to the sample system as close as practical to the probe inlet. This is done either by attaching the calibration gas supply line to the probe top with flexible tubing or by actuation of a solenoid valve located at the sample conditioner inlet (probe exit). The span gas is exposed to the same elements as the sample and the system response is documented. The analyzer indications for the system calibration check must agree within 5% of the analyzer calibration. Values are adjusted and changes/repairs are made to the system to compensate for any difference in analyzer readings. Specific information on the analytical equipment and test methods used is provided in the following pages.



Schematic of CEM System

Method:	Oxygen (O ₂) by Continuous Analyzer
Applicable Reference Methods:	EPA 3A, EPA 20, ARB 100, BA ST-14, SCAQMD 100.1
Principle:	A sample is continuously drawn from the flue gas stream, conditioned, and conveyed to the instrument for direct readout of O ₂ concentration.
Analyzer:	Teledyne Model 326A
Measurement Principle:	Electrochemical cell
Ranges:	0-5, 0-10, 0-25% O ₂
Accuracy:	1% of full scale
Output:	0-100 mV, linear
Interferences:	Halogens and halogenated compounds will cause a positive interference. Acid gases will consume the fuel cell and cause a slow calibration drift.
Response Time:	90% < 7 seconds
Sampling Procedure:	A representative flue gas sample is collected and conditioned using the CEM system described previously. If Method 20 is used, that method's specific procedures for selecting sample points are used. Otherwise, stratification checks are performed at the start of a test program to select single or multiple-point sample locations.
Analytical Procedure:	An electrochemical cell is used to measure O ₂ concentration. Oxygen in the flue gas diffuses through a Teflon membrane and is reduced on the surface of the cathode. A corresponding oxidation occurs at the anode internally, and an electric current is produced that is proportional to the concentration of oxygen. This current is measured and conditioned by the instrument's electronic circuitry to give an output in percent O ₂ by volume.
Special Calibration Procedure:	The measurement cells used with the O ₂ instrument have to be replaced on a regular basis. After extended use, the cell tend to produce a nonlinear response. Therefore, a three-point calibration is performed at the start of each test day to check for linearity. If the response is not linear ($\pm$ 2% of scale), the cell is replaced.

Method: NO/NO_x by Continuous Analyzer

Applicable Reference Methods: EPA 7E, EPA 20; ARB 100, BA ST-13A, SCAQMD 100.1

Principle: A sample is continuously drawn from the flue gas stream, conditioned, and conveyed to the instrument for direct readout of NO or NO_x.

Analyzer: Teco Model No. 10AR

Measurement Principle: Chemiluminescence

Accuracy: 1% of full scale

Ranges: 0-2.5, 0-10, 0-25, 0-100, 0-250, 0-1000, 0-2500, 0-10,000 ppm

Output: 0-10 mV

Inferences: Compounds containing nitrogen (other than ammonia) may cause interference.

Response Time: 90%, 1.5 seconds (NO mode) and 1.7 seconds (NO_x mode)

Sampling Procedure: A representative flue gas sample is collected and conditioned using the CEM system described previously. If EPA Method 20 is used, that method's specific procedures for selecting sample points are used.

Analytical Procedure: The oxides of nitrogen monitoring instrument is a chemiluminescent nitric oxide analyzer. The operational basis of the instrument is the chemiluminescent reaction of NO and ozone (O₃) to form NO₂ in an excited state. Light emission results when excited NO₂ molecules revert to their ground state. The resulting chemiluminescence is monitored through an optical filter by a high sensitivity photomultiplier tube, the output of which is electronically processed so it is linearly proportional to the NO concentration. The output of the instrument is in ppmV.

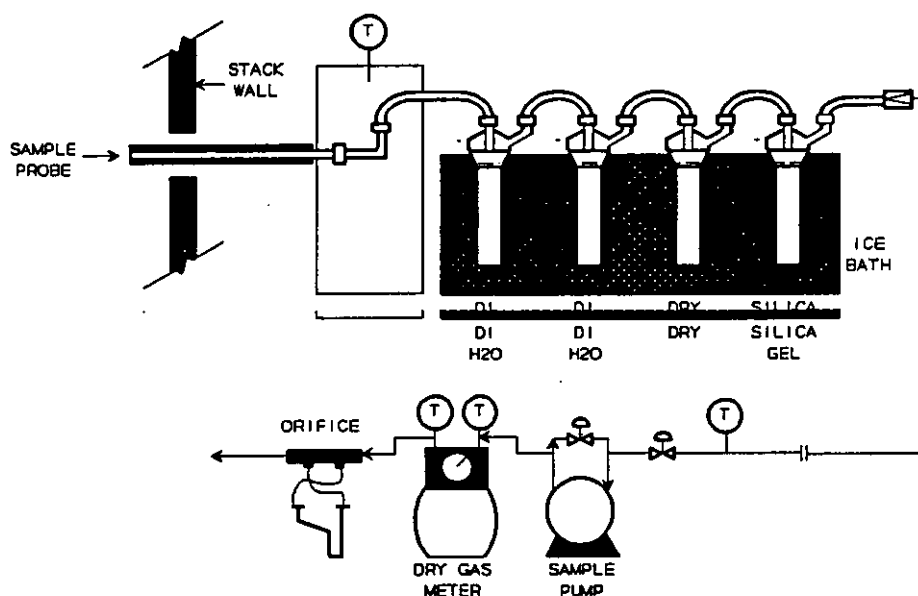
When NO₂ is expected to be present in the flue gas, a supercooled water dropout flask will be placed in the sample line to avoid loss of NO₂. Since NO₂ is highly soluble in water, "freezing out" the water will allow the NO₂ to reach the analyzers for analysis. The analyzer measures NO only. In the NO_x mode, the gas is passed through a moly converter which converts NO₂ to NO and a total NO_x measurement is obtained. NO₂ is determined as the difference between NO and NO_x. Use of a moly converter instead of a stainless steel converter eliminates NH₃ interference; NH₃ is converted to NO with a stainless converter, but not with a moly converter.

Method: **Determination of Moisture in Stack Gases**

Applicable Ref. **EPA 4, ARB 1-4, SCAQMD 4.1**
Methods:

Principle: A gas sample is extracted at a constant rate from the source; moisture is removed from the sample stream and determined volumetrically or gravimetrically.

Sampling Procedure: The sample train used in the tests is shown in the following figure. The sample is drawn at a constant rate through a stainless steel probe. The probe is connected to an impinger train by Teflon tubing. The train consists of two Greenburg-Smith impingers which contain 100 ml water, an empty impinger as a knockout, and an impinger containing silica gel to protect the pump from moisture.



Sample Train for Determination of Moisture by EPA Method 4

Sample Recovery and Analysis:

Following testing, moisture content is determined gravimetrically from initial and final impinger weights.

APPENDIX B
QUALITY ASSURANCE

Appendix B.1
Quality Assurance Program Summary and ARB Certification

QUALITY ASSURANCE PROGRAM SUMMARY AND ARB CERTIFICATION

Carnot ensures the quality and validity of its emission measurement and reporting procedures through a rigorous quality assurance (QA) program. The program is developed and administered by an internal QA Officer and encompasses seven major areas:

1. Development and use of an internal QA manual.
2. QA reviews of reports, laboratory work, and field testing.
3. Equipment calibration and maintenance.
4. Chain of custody.
5. Training.
6. Knowledge of current test methods.
7. Agency certification.

Each of these areas is discussed individually below.

Quality Assurance Manual. Carnot has prepared a QA Manual according to EPA guidelines. The manual serves to document and formalize all of Carnot's QA efforts. The manual is constantly updated, and each member of the Source Test Division is required to read and understand its contents. The manual includes details on the other six QA areas discussed below.

QA Reviews. Carnot's review procedure includes review of each source test report by the QA Officer, and spot check reviews of laboratory and field work.

The most important review is the one that takes place before a test program begins. The QA Officer works closely with Source Test Division personnel to prepare and review test protocols. Test protocol review includes selection of appropriate test procedures, evaluation of any interferences or other restrictions that might preclude use of standard test procedures, and evaluation and/or development of alternate procedures.

Equipment Calibration and Maintenance. The equipment used to conduct the emissions measurements is maintained according to the manufacturer's instructions to ensure proper operation. In addition to the maintenance program, calibrations are carried out on each measurement device according to the schedule outlined by the California Air Resources Board (CARB). The schedule for maintenance and calibrations are given in Tables B-1 and B-2. Quality control checks are also conducted in the field for each test program. The following is a partial list of checks made as part of each CEM system test series.

- Sample acquisition and conditioning system leak check.
- 2-point analyzer calibrations (all analyzers)
- 3-point analyzer calibrations (analyzers with potential for linearity errors).
- Complete system calibration check ("dynamic calibration" through entire sample system).

- Periodic analyzer calibration checks (once per hour) are conducted at the start and end of each test run. Any change between pre- and post-test readings are recorded.
- All calibrations are conducted using gases certified by the manufacturer to be + 1% of label value (NBS traceable).

Calibration and CEM performance data are fully documented, and are included in each source test report.

Chain of Custody. Carnot maintains full chain of custody documentation on all samples and data sheets. In addition to normal documentation of changes between field sample custodians, laboratory personnel, and field test personnel, Carnot documents every individual who handles any test component in the field (e.g., probe wash, impinger loading and recovery, filter loading and recovery, etc.).

Samples are stored in a locked area to which only Source Test Division personnel have access. Neither other Carnot employees nor cleaning crews have keys to this area.

Data sheets are copied immediately upon return from the field, and this first generation copy is placed in locked storage. Any notes made on original sheets are initialed and dated.

Training. Personnel training is essential to ensure quality testing. Carnot has formal and informal training programs which include:

1. Attendance at EPA-sponsored training courses.
2. Enrollment in EPA correspondence courses.
3. A requirement for all technicians to read and understand Carnot's QA Manual.
4. In-house training and QA meetings on a regular basis.
5. Maintenance of training records.

Knowledge of Current Test Methods. With the constant updating of standard test methods and the wide variety of emerging test methods, it is essential that any qualified source tester keep abreast of new developments. Carnot subscribes to services which provide updates on EPA and CARB reference methods, and on EPA, CARB and SCAQMD rules and regulations. Additionally, source test personnel regularly attend and present papers at testing and emission-related seminars and conferences. Carnot personnel maintain membership in the Air Pollution Control Association, the Source Evaluation Society, and the ASME Environmental Control Division.

AGENCY CERTIFICATION

Carnot is certified by the CARB as an independent source test contractor for gaseous and particulate measurements. Carnot also participates in EPA QA audit programs for Methods 5, 6 and 7.

TABLE B-1
SAMPLING INSTRUMENTS AND EQUIPMENT CALIBRATION SCHEDULE
As Specified by the CARB

Instrument Type	Frequency of Calibration	Standard of Comparison or Method of Calibration	Acceptance Limits
Orifice Meter (large)	12 months	Calibrated dry test meter	$\pm 2\%$ of volume measured
Dry Gas Meter	12 months or when repaired	Calibrated dry test meter	$\pm 2\%$ of volume measured
S-Type Pitot (for use with EPA-type sampling train)	6 months	EPA Method 2	Cp constant (+5%) over working range; difference between average Cp for each leg must be less than 2%
Vacuum Gauges Pressure Gauges	6 months	Manometer	$\pm 3\%$
Field Barometer	6 months	Mercury barometer	$\pm 0.2''$ Hg
Temperature Measurement	6 months	NBS mercury thermometer or NBS calibrated platinum RTD	$\pm 4^\circ\text{F}$ for $<400^\circ\text{F}$ $\pm 1.5\%$ for $>400^\circ\text{F}$
Temperature Readout Devices	6 months	Precision potentiometer	$\pm 2\%$ full scale reading
Analytical Balance	12 months (check prior to each use)	Should be performed by manufacturer or qualified laboratory	± 0.3 mg of stated weight
Probe Nozzles	12 Months	Nozzle diameter check micrometer	Range $< \pm 0.10$ mm for three measurements
Continuous Analyzers	Depends upon use, frequency and performance	As specified by manufacturers operating manuals, EPA NBS gases and/or reference methods	Satisfy all limits specified in operating specifications

TABLE B-2
EQUIPMENT MAINTENANCE SCHEDULE
Based on Manufacturer's Specifications and Carnot Experience

Equipment	Performance Requirement	Maintenance Interval	Corrective Action
Pumps	1. Absence of leaks 2. Ability to draw manufacturer required vacuum and flow	Every 500 hours of operation or 6 months, whichever is less	1. Visual inspection 2. Clean 3. Replace worn parts 4. Leak check
Flow Measuring Device	1. Free mechanical movement 2. Absence of malfunction	Every 500 hours of operation or 6 months, whichever is less After each test, if used in H ₂ S sampling or other corrosive atmospheres	1. Visual inspection 2. Clean 3. Calibrate
Sampling Instruments	1. Absence of malfunction 2. Proper response to zero, span gas	As required by the manufacturer	As recommended by manufacturer
Integrated Sampling Tanks	Absence of leaks	Depends on nature of use	1. Steam clean 2. Leak check
Mobile Van Sampling Systems	Absence of leaks	Depends on nature of use	1. Change filters 2. Change gas dryer 3. Leak check 4. Check for system contamination
Sampling Lines	Sample degradation less than 2%	After each test or test series	Blow filtered air through line until dry

State of California
AIR RESOURCES BOARD

Executive Order G-836

Approval to Carnot
To Conduct Testing as an Independent Contractor

WHEREAS, the Air Resources Board ("Board"), pursuant to Section 41512 of the California Health and Safety Code, has established the procedures contained in Section 91200-91220, Title 17, California Code of Regulations, to allow the use of independent testers for compliance tests required by the Board; and

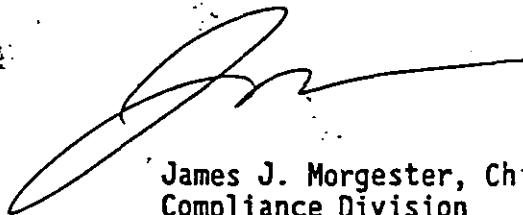
WHEREAS, pursuant to Sections 91200-91220, Title 17, California Code of Regulations, the Executive Officer has determined that Carnot meets the requirements of the Board for conducting Board Test Methods 1, 2, 3, 4, 5, 6, 8, 10, and 100 (NOx, O2) when the following conditions are met:

1. Carnot conducts Board Test Method 100 for O2 using a Teledyne 326 analyzer with either a A5 or a B1 sensor, or a paramagnetic analyzer.

NOW, THEREFORE, BE IT ORDERED that Carnot is granted an approval, from the date of execution of this order, until June 30, 1994 to conduct the tests listed above, subject to compliance with Section 91200-91220, Title 17, California Code of Regulations.

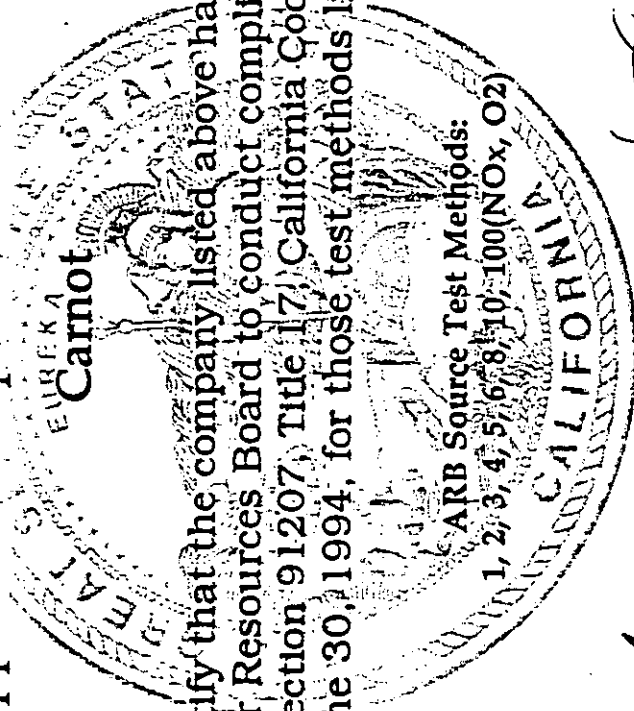
BE IT FURTHER ORDERED that during the approved period the Executive Officer or his or her authorized representative may field audit one or more tests conducted pursuant to this order for each type of testing listed above.

Executed this 14th day of July 1993, at Sacramento, California.



James J. Morgester, Chief
Compliance Division

State of California
Air Resources Board
Approved Independent Contractor



This is to certify that the company listed above has been approved by the Air Resources Board to conduct compliance testing pursuant to Section 91207, Title 17, California Code of Regulations, until June 30, 1994, for those test methods listed below:


James J. Morgester, Chief
Compliance Division


Laura McKinney, Manager
Investigation and Certification Section

Appendix B.2
Calibration Data

CARNOT SPAN GAS RECORD

CLIENT/LOCATION: LP Oroville Boiler 5 DATE: 5-3-94
BY: KSC

GAS	SPAN CYLINDER		AUX. SPAN CYLINDER	
	CYLINDER NO.	CONCENTRATION	CYLINDER NO.	CONCENTRATION
ZERO	ALM012329	99.9999%	—	—
NOx	ALM033887 ALM046278	722.7 ppm 453 ppm	ALM010961	241.2
O ₂	AAL630	8.05%	ALM12592	4.99%
CO	ALM002195	425.6 ppm	ALM013868	277.8 ppm
CO ₂	AAL630	22.3%	ALM12592	15.1%
SO ₂	—	—	—	—

CARNOT INSTRUMENT LINEARITY

	ANALYZER				
	O ₂	CO ₂	CO	NOx	SO ₂
ANALYZER RANGE	0-10	0-25	0-500	0-1000	—
SET TO HIGH STD (80-90% OF RANGE)	8.05	22.3	425.6	722.7	—
AS-FOUND LOW STD (50-60% OF RANGE)	5.08	15.00	288.8	455.1	—
ACTUAL VALUE OF LOW STD	4.99	15.1	277.8	453.0	—
DIFFERENCE IN % OF FULL SCALE	0.9	-0.4	1.8	0.8	—

ALLOWABLE DEVIATION IS 2% OF FULL SCALE (2 SQUARES ON STRIP CHART).

CARNOT SPAN GAS RECORD

CLIENT/LOCATION: L-P Oronville Boiler 4

DATE: 5-4-94

BY: KJC

GAS	SPAN CYLINDER		AUX. SPAN CYLINDER	
	CYLINDER NO.	CONCENTRATION	CYLINDER NO.	CONCENTRATION
ZERO	ALM-012329	99.999% N ₂		
NOx	ALM-010961	241.2 ppm	ALM-006725	84.4 ppm
O ₂	AAL630	8.05 %	ALM 12592	4.99 %
CO	ALM 002195	425.6 ppm	ALM 013868	277.8 ppm
CO ₂	AAL630	22.3 %	ALM 12592	15.1 %
SO ₂				

CARNOT INSTRUMENT LINEARITY

	ANALYZER				
	O ₂	CO ₂	CO	NOx	SO ₂
ANALYZER RANGE	10%	25%	500 ppm	250 ppm	
SET TO HIGH STD (80-90% OF RANGE)	8.05	22.3	425.6	241.2	
ACTUAL VALUE OF LOW STD	4.99	15.1	277.8	84.4	
AS-FOUND LOW STD (50-60% OF RANGE)	5.29 ^{5.10}	15.04 ^{*14.99}	287.0	85.2	
DIFFERENCE IN % OF FULL SCALE	3.0 ^{*1.1}	0.24 ^{0.44}	1.8	0.32	

% ERROR CALCULATION:

$$\frac{(\text{AS FOUND} - \text{ACTUAL VALUE OF SPAN})}{\text{RANGE}} \times 100$$

* 1310 hrs Reset O₂ + CO₂

ALLOWABLE DEVIATION IS 2% OF FULL SCALE (2 SQUARES ON STRIP CHART).

CARNOT SPAN GAS RECORD

CLIENT/LOCATION: LP Orrouille #4

DATE: 5/5/94

BY: KSC

GAS	SPAN CYLINDER		AUX. SPAN CYLINDER	
	CYLINDER NO.	CONCENTRATION	CYLINDER NO.	CONCENTRATION
ZERO	ALM-012329	99.999 %		
NO _x	ALM010961	241.2 ppm	ALM006725	84.4 ppm
O ₂	AAL630	8.05 %	ALM12592	4.99 %
CO	ALM002195	425.6 ppm	ALM013868	277.8 ppm
CO ₂	AAL630	22.3 %	ALM12592	15.1 %
SO ₂				

CARNOT INSTRUMENT LINEARITY

	ANALYZER				
	O ₂	CO ₂	CO	NO _x	SO ₂
ANALYZER RANGE	0-10	0-25	0-500	0-250	
SET TO HIGH STD (80-90% OF RANGE)	8.05	22.3	425.6	241.2	
ACTUAL VALUE OF LOW STD	4.99	15.1	277.8	84.4	
AS-FOUND LOW STD (50-60% OF RANGE)	5.07	14.98	287.0	85.1	
DIFFERENCE IN % OF FULL SCALE					

% ERROR CALCULATION:

$$\frac{(\text{AS FOUND} - \text{ACTUAL VALUE OF SPAN})}{\text{RANGE}} \times 100$$

ALLOWABLE DEVIATION IS 2% OF FULL SCALE (2 SQUARES ON STRIP CHART).

CARNOT SPAN GAS RECORD

CLIENT/LOCATION: LP Orville
 Analyzer ReCal before 4-PM-4

DATE: 5/5/94

BY: KJC

GAS	SPAN CYLINDER		AUX. SPAN CYLINDER	
	CYLINDER NO.	CONCENTRATION	CYLINDER NO.	CONCENTRATION
ZERO				
NOx				
O ₂				
CO				
CO ₂				
SO ₂				

Same as on previous 5/5/94 sheet.

CARNOT INSTRUMENT LINEARITY

	ANALYZER				
	O ₂	CO ₂	CO	NOx	SO ₂
ANALYZER RANGE	0-10	0-25	0-500	0-250	
SET TO HIGH STD (80-90% OF RANGE)	8.05	22.3	425.6	241.2	
ACTUAL VALUE OF LOW STD	4.99	15.1	277.8	84.4	
AS-FOUND LOW STD (50-60% OF RANGE)	5.08	14.98	286.6	85.0	
DIFFERENCE IN % OF FULL SCALE	0.9	-0.5	1.8	0.2	

% ERROR CALCULATION:

$$\frac{(\text{AS FOUND} - \text{ACTUAL VALUE OF SPAN})}{\text{RANGE}} \times 100$$

ALLOWABLE DEVIATION IS 2% OF FULL SCALE (2 SQUARES ON STRIP CHART).



Scott Specialty Gases, Inc.

Shipped
From:

5121 BRANDIN COURT
FREMONT
Phone: 510-659-0162

CA 94538

Fax: 510-659-9156

C E R T I F I C A T E O F A N A L Y S I S

CARNOT

1150 BURNETT AVE
SUITE C
CONCORD

CA 94520

PROJECT #: 09-16729-007
PO#: 1283
ITEM #: 0901811 AL
DATE: 10/18/93

CYLINDER #: ALM012329

PURE MATERIAL: NITROGEN

CAS# 7727-37-9

GRADE: U Z A M

PURITY: 99.999%

LOT#9307-560, 9308-382

ADDITIONAL CYLINDER#ALM013871

ANALYST: Paul Cowles



Scott Specialty Gases, Inc.

5121 BRANDIN COURT, FREMONT, CA 94538

(510) 659-0162 FAX: (510) 659-9156

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer :
CARNOT
1150 BURNETT AVE
SUITE C
CONCORD , CA 94520

Assay Laboratory
Scott Specialty Gases
5121 Brandin Ct.
Fremont, CA 94538

Purchase Order 1487
Scott Project # 0917987

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol 1 Procedure #G1, Section Number 3.0.4

Cylinder Number ALM-006725
Cylinder Pressure 2000 psig

Certification Date 01-14-94
Previous Certification Dates NONE

Expiration Date 01-14-96

ANALYZED CYLINDER

Components
NITRIC OXIDE
NITROGEN
NOx

Certified Concentration
83.2 PPM
Balance
84.4 PPM

Analytical Uncertainty*
1% NIST traceable

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type Expiration Date
CRM # 1684 09-17-94

Cylinder Number
ALM-024584

Concentration
95.3 PPM NO/N2

INSTRUMENTATION

Instrument/Model/Serial #
HORIBA/CLA-53A /850658092

Last Date Calibrated
01-07-94

Analytical Principle
CHEMILUMINESCENT

ANALYZER READINGS (Z=Zero Gas R= Reference Gas T=Test Gas r=Correlation Coefficient)

Components

First Triad Analysis

Second Triad Analysis

Calibration Curve

NO

01-07-94 Response Units: PPM
Z1 = -0.05 R2 = 93.79 Z3 = -0.05
R1 = 93.64 Z2 = -0.05 T3 = 81.63
T1 = 80.16 T2 = 81.64 R3 = 93.82
Conc = 81.59 Conc = 82.77 Conc = 82.93
Mean Assay = 82.43 ppm

01-14-94 Response Units: PPM
Z1 = 0.01 R2 = 95.33 Z3 = 0.02
R1 = 95.28 Z2 = 0.03 T3 = 83.34
T1 = 83.20 T2 = 83.16 R3 = 95.39
Conc = 83.21 Conc = 83.13 Conc = 83.34
Mean Assay = 83.23 ppm

Conc = A+Bx+Cx²+Dx³
A = -0.1884003
B = 97.90052

r = 0.9999957

Special Notes

Analyst MIKE HUYNH



Scott Specialty Gases, Inc.

5121 BRANDIN COURT, FREMONT, CA 94538

(510) 659-0162 FAX: (510) 659-9156

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
CARNOT
1150 BURNETT AVE
SUITE C
CONCORD, CA 94520

Assay Laboratory
SCOTT SPECIALTY GASES, INC
5121 BRANDIN CT
FREMONT, CA 94538

Purchase Order 1283
Scott Project # 0916729

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol 1 Procedure #G1, Section Number 3.0.4

Cylinder Number ALM-010961
Cylinder Pressure 2000 Psi

Certification Date 10-15-93
Previous Certification Dates NONE

General Exp. date 10-15-95

ANALYZED CYLINDER

Components

Nitric Oxide
NO_x

Balance: Nitrogen

Certified Concentration

236.2 ppm
241.2 ppm

Analytical Uncertainty*

+1 % NIST Directly Traceable

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type CRM # 1685
Expiration Date 11/18/94

Cylinder Number
ALM-024139

Concentration
244.7 ppm NO/N₂

INSTRUMENTATION

Instrument/Model/Serial #
HORIBA/CLA-53A/850658092

Last Date Calibrated
09-18-93

Analytical Principle
CHEMILUMINESCENT

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components
NITRIC OXIDE

First Triad Analysis

10-08-93 Response Units: ppm
Z1= 0.2 R2= 245.0 Z3= 0.2
R1= 244.5 Z2= 0.2 T3= 236.3
T1= 236.3 T2= 236.1 R3= 245.3
Mean Assay = 236.2 ppm
NO_x = 237.6 ppm

Second Triad Analysis

10-15-93 Response Units: ppm
Z1= 0.1 R2= 246.0 Z3= 0.2
R1= 245.9 Z2= 0.1 T3= 236.7
T1= 235.5 T2= 236.3 R3= 246.0
Mean Assay = 236.2 ppm
NO_x = 241.2 ppm

Calibration Curve

Concentration = $A + Bx + Cx^2 + Dx^3 + Cx^4$
r = 0.9999948
Constants: A = -0.2422028
B = 294.5839 C = 0

Special Notes

Mike Huynh
Analyst Mike Huynh



Scott Specialty Gases, Inc.

5121 BRANDIN COURT, FREMONT, CA 94538

(510) 659-0162 FAX: (510) 659-9156

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer :
CARNOT
1150 BURNETT AVE
SUITE C
CONCORD, CA 94520

Assay Laboratory
Scott Specialty Gases
5121 Brandin Ct.
Fremont, CA 94538

Purchase Order 1487
Scott Project # 0917986

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol 1 Procedure #G1, Section Number 3.0.4

Cylinder Number ALM-013868
Cylinder Pressure 2000 psig

Certification Date 01-06-94
Previous Certification Dates NONE

Expiration Date 01-06-97

ANALYZED CYLINDER

Components
Carbon Monoxide
Nitrogen

Certified Concentration
277.8 ppm
Balance

Analytical Uncertainty*
1% NIST traceable

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type CRM # 1680
Expiration Date 01-18-96

Cylinder Number
ALM-031341

Concentration
479.8 PPM CO/N2

INSTRUMENTATION

Instrument/Model/Serial #
HORIBA/AIA-23AS/850658016

Last Date Calibrated
10-20-93

Analytical Principle
NDIR

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components

First Triad Analysis

12-30-93 Response Units: PPM
Z1 = -0.1 R2 = 479.5 Z3 = -0.2
R1 = 479.5 Z2 = -0.0 T3 = 275.9
T1 = 275.9 T2 = 275.8 R3 = 479.4
Mean Assay = 275.9 ppm

Second Triad Analysis

01-05-94 Response Units: PPM
Z1 = 0.1 R2 = 480.6 Z3 = 0.0
R1 = 480.4 Z2 = 0.2 T3 = 277.9
T1 = 278.0 T2 = 277.5 R3 = 480.3
Mean Assay = 277.8 ppm

Calibration Curve

Conc = A + Bx + Cx² + Dx³
A = -0.1986406
B = 354.0686
C = 102.6648
D = 21.73912 r = 0.9999978

Special Notes

Mike Huynh
Analyst MIKE HUYNH



Scott Specialty Gases

CARNOT

CERIFICATE OF ANALYSIS
J No. 1487

CAS Reg. Component No.	Component	Certified Analysis
124-38-9	CARBON DIOXIDE	15.1 PCT/M
7782-44-7	OXYGEN	4.99 PCT/M
7727-37-9	NITROGEN	89L

Analytical Accuracy $\pm 1\%$

Project No 09-17986
Cylinder No. ALM012592
Item No. 0902C3000701AL



Scott Specialty Gases, Inc.

Shipped
From:

5121 BRANDIN COURT
FREMONT CA 94538
Phone: 510-659-0162

Fax: 510-659-9156

CERTIFICATE OF ANALYSIS

CARNOT

1150 BURNETT AVE.
SUITE C
CONCORD

CA 94520

PROJECT #: 09-17986-002

PO#: 1487

ITEM #: 0902C3013601AL

DATE: 1/10/94

CYLINDER #: AAL630
FILL PRESSURE: 1800 PSIG

ANALYTICAL ACCURACY: +-1%

COMPONENT

CARBON DIOXIDE
OXYGEN
NITROGEN

REQUESTED GAS

CONC MOLES

22.5 PCT

8. PCT

BAL

ANALYSIS

(MOLES)

22.3 PCT

8.05 PCT

BAL

LOT # 9312-565

ADDITIONAL CYL #: AAL9424

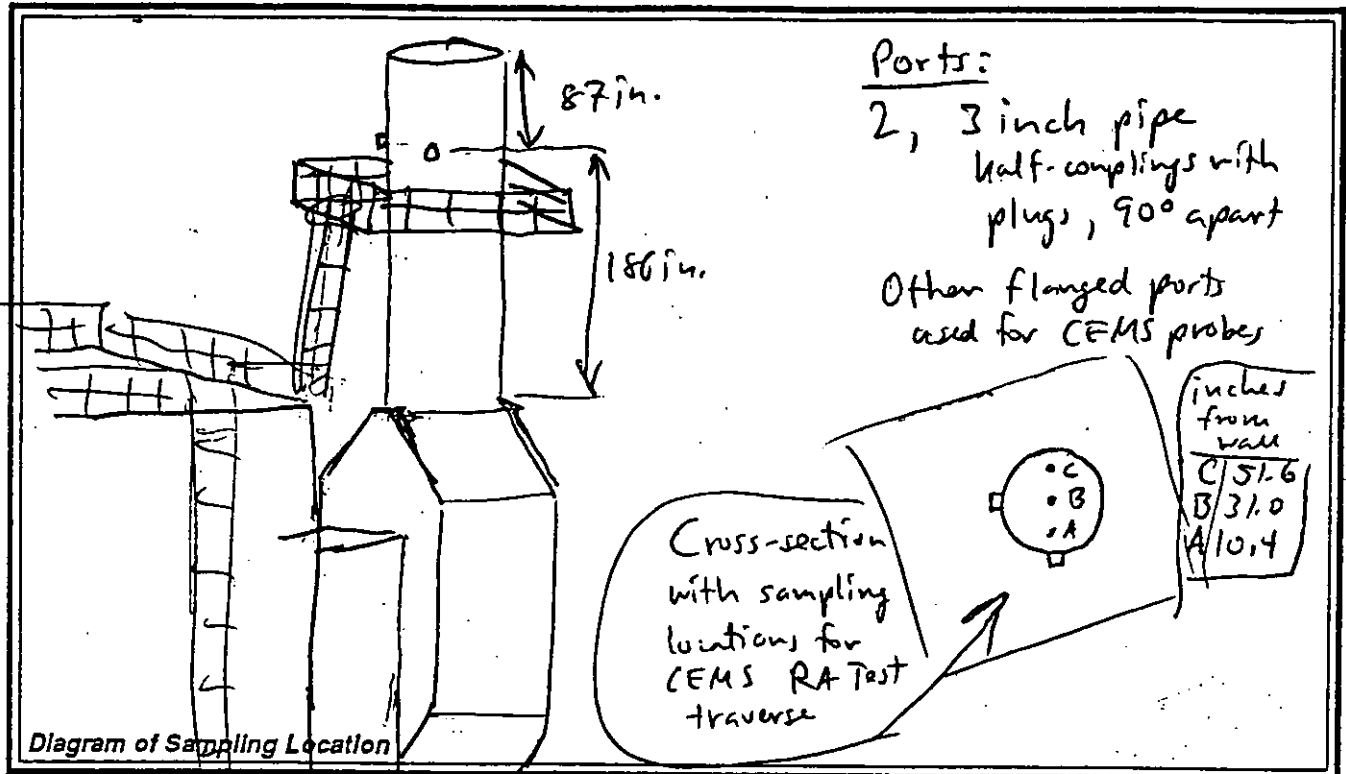
ANALYST: *[Signature]*

APPENDIX C
DATA SHEETS

Appendix C.1
Sampling Locations

CARNOT SAMPLING POINT LOCATION DATA - EPA METHOD 1

PLANT: L-P Draville DATA BY: KPC
 DATE: 5-4-94
 TEST LOCATION: Boiler 4



UPSTREAM DIST./DIA.: 87 in. / 1.41
 DOWNSTREAM DIST./DIA.: 186 in. / 3.00
 COUPLING LENGTH: 3.0 in.
 NO. OF SAMPLING PTS.: 24
 STACK DIMENSION: 62.0 in.
 STACK AREA, FT²: 20,966

SAMPLE POINT	% OF DIAMETER	IN. FROM NEAR WALL	IN. FROM NOZZLE*
1	2.1	1.34	4.3
2	6.7	4.2	7.2
3	11.8	7.3	10.3
4	17.7	11.0	14.3
5	25.0	15.5	18.5
6	35.1	22.1	25.1
7	44.4	31.9	42.9
8	55.0	46.5	49.5
9	62.3	51.0	54.0
10	68.2	54.7	57.7
11	93.3	57.8	60.8
12	97.9	60.7	63.7

*INCHES FROM WALL PLUS
 COUPLING LENGTH

CARNOT

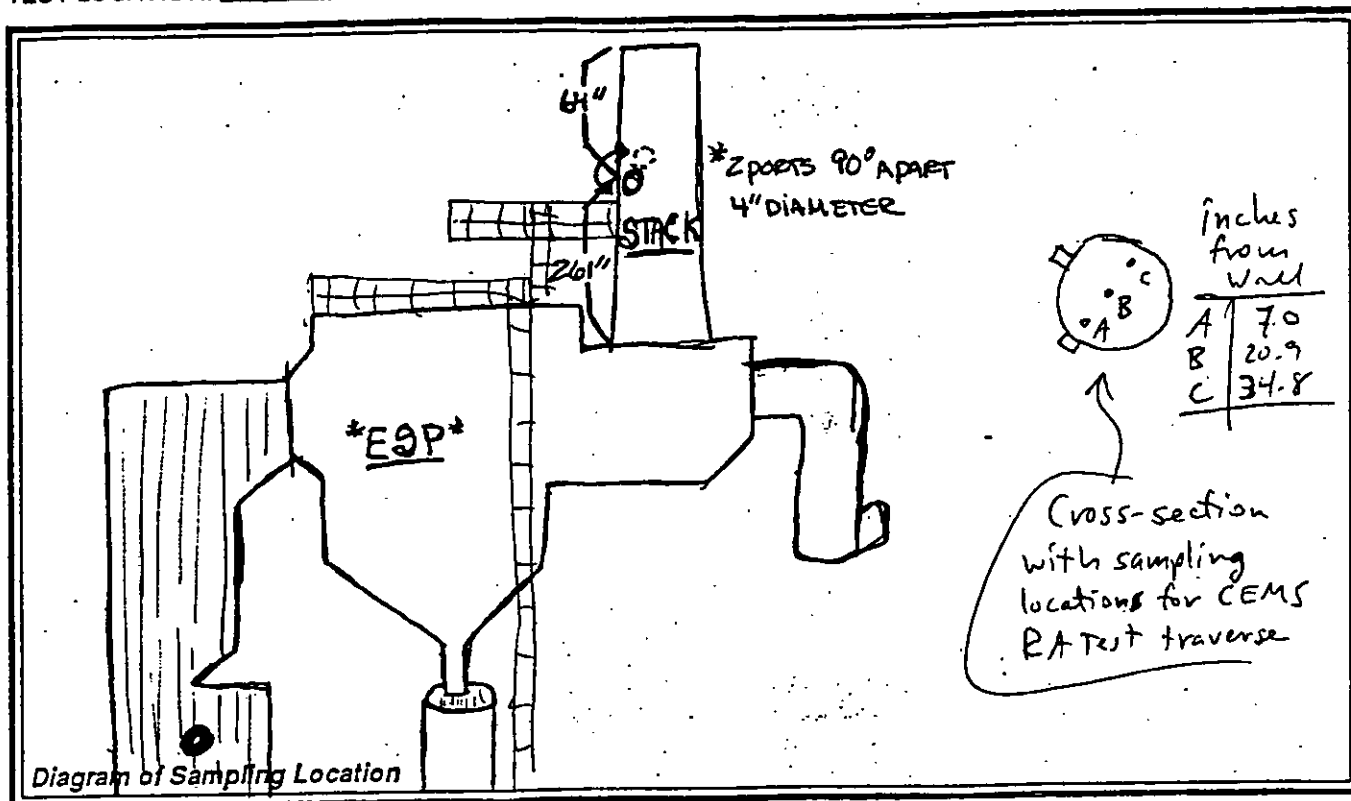
SAMPLING POINT LOCATION DATA - EPA METHOD 1

PLANT: L-P OROVILLE

DATA BY: JP

DATE: 10/22/93

TEST LOCATION: STACK



UPSTREAM DIST./DIA.: 1.53

DOWNSTREAM DIST./DIA.: 6.24

COUPLING LENGTH: 2.25"

NO. OF SAMPLING PTS.: 16

STACK DIMENSION: 41.75" diam.

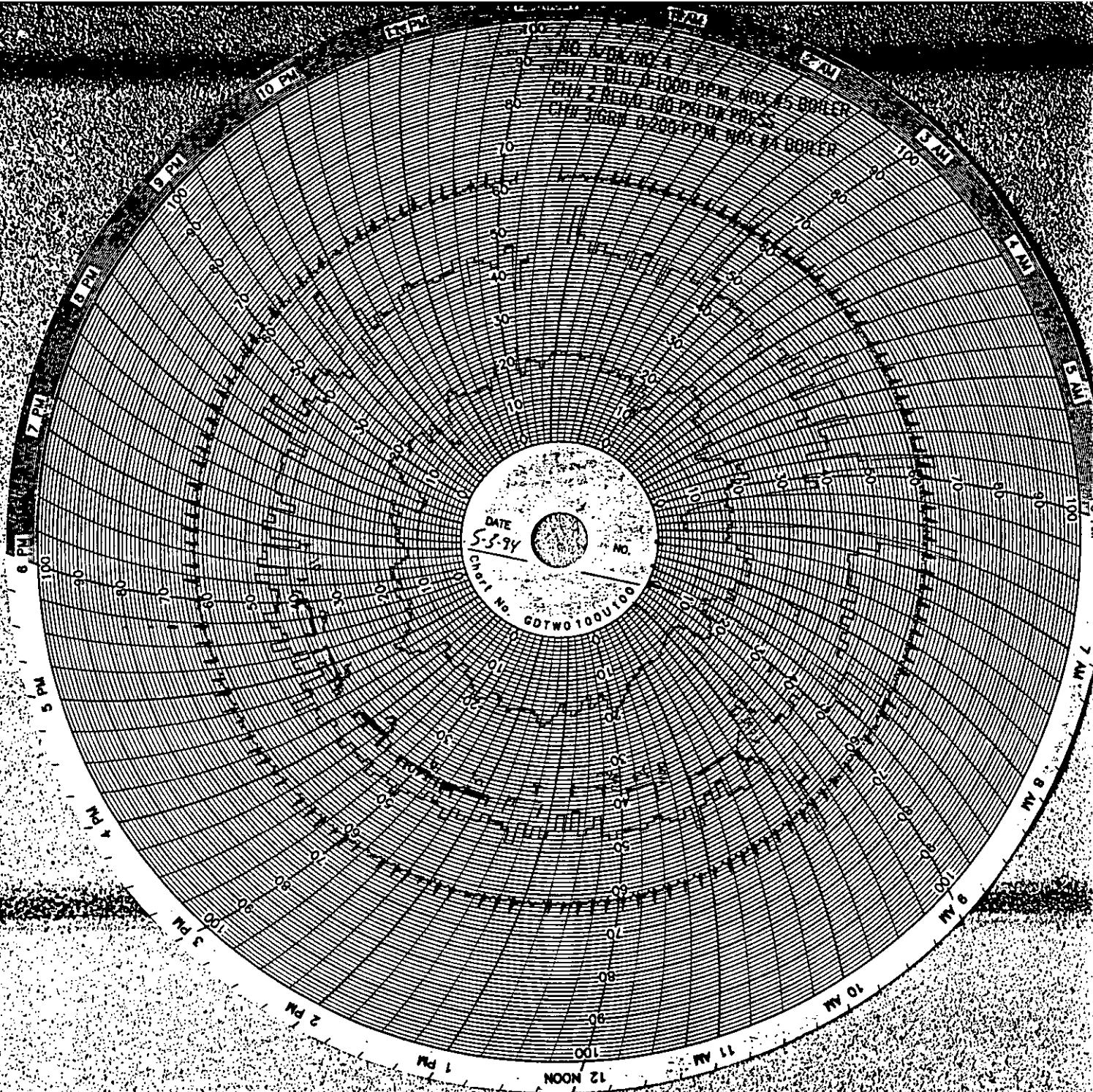
STACK AREA, FT²: 9.51

SAMPLE POINT	% OF DIAMETER	IN. FROM NEAR WALL	IN. FROM NOZZLE*
1	3.2	1.3	3.6
2	10.5	4.4	6.7
3	19.4	8.1	10.4
4	32.3	13.5	15.8
5	67.7	28.3	30.6
6	80.6	33.7	36.0
7	89.5	37.4	39.7
8	96.8	40.5	42.8

*INCHES FROM WALL PLUS COUPLING LENGTH

CARNOT

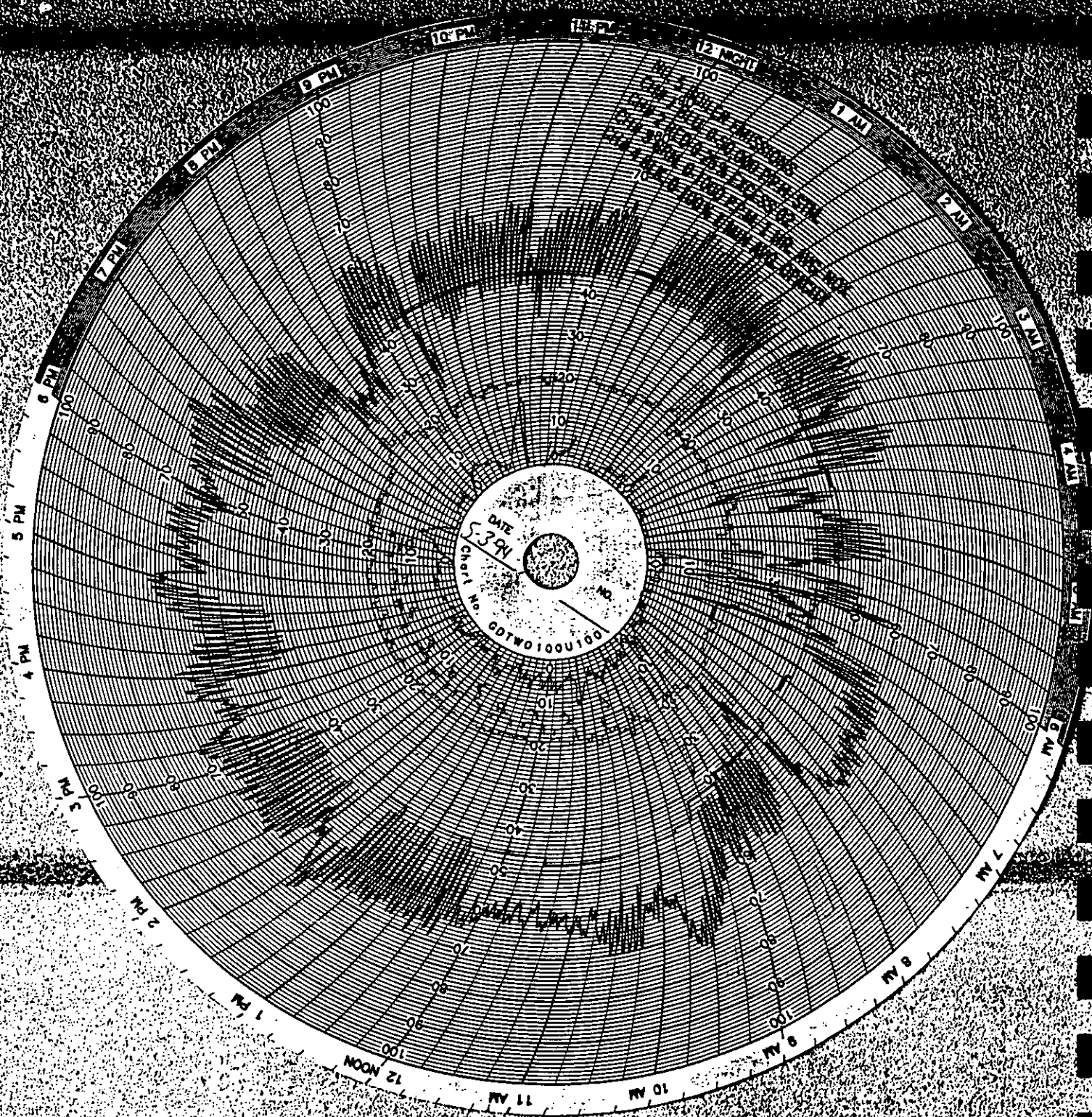
Appendix C.2
Plant Continuous Emission Monitoring System Data



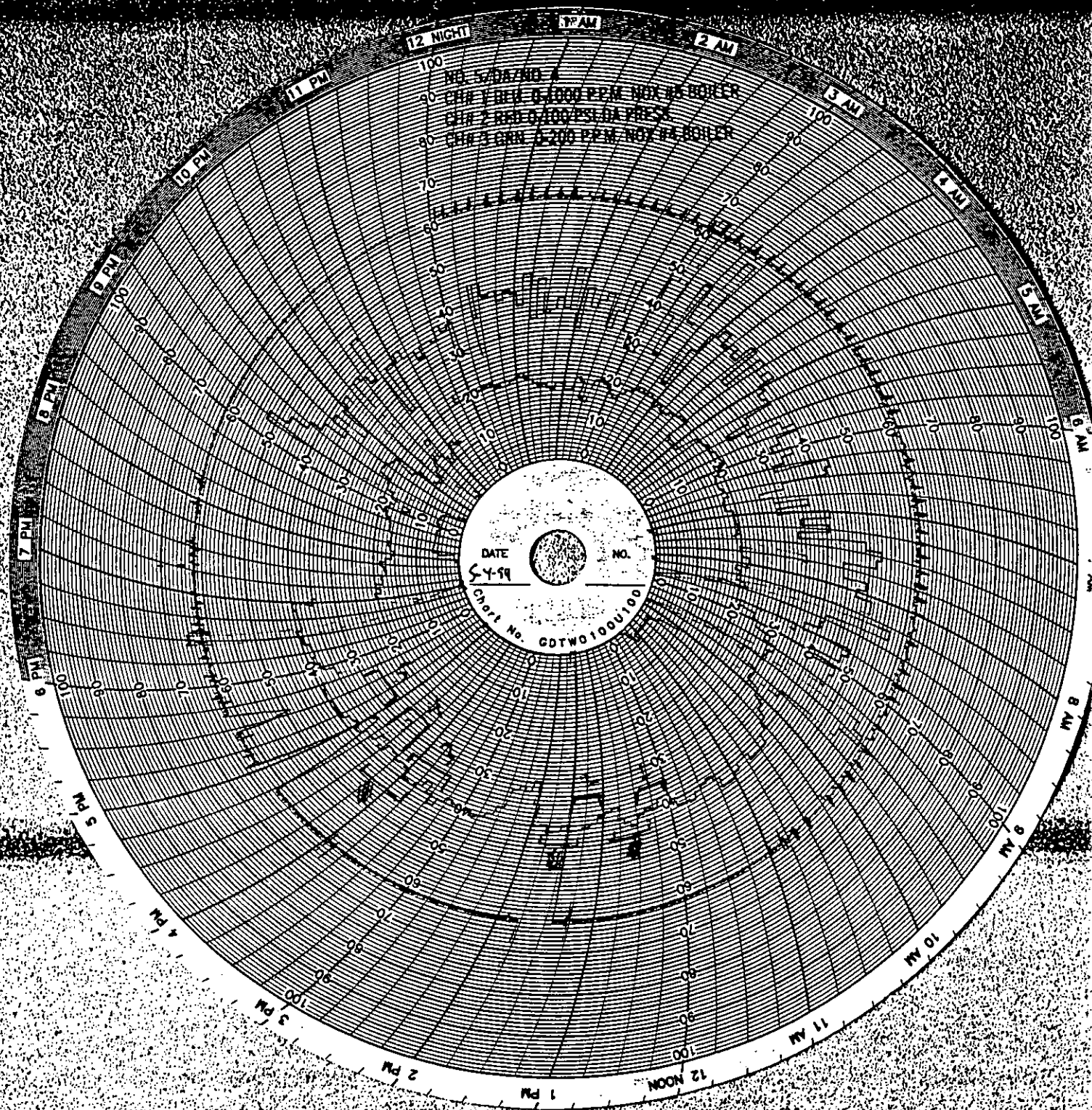
Boiler 5

RA Test Runs 5-3-94

NOx ppm vol. wet



Boiler 5
RA Test Runs 5-3-94
O₂ % vol. wet

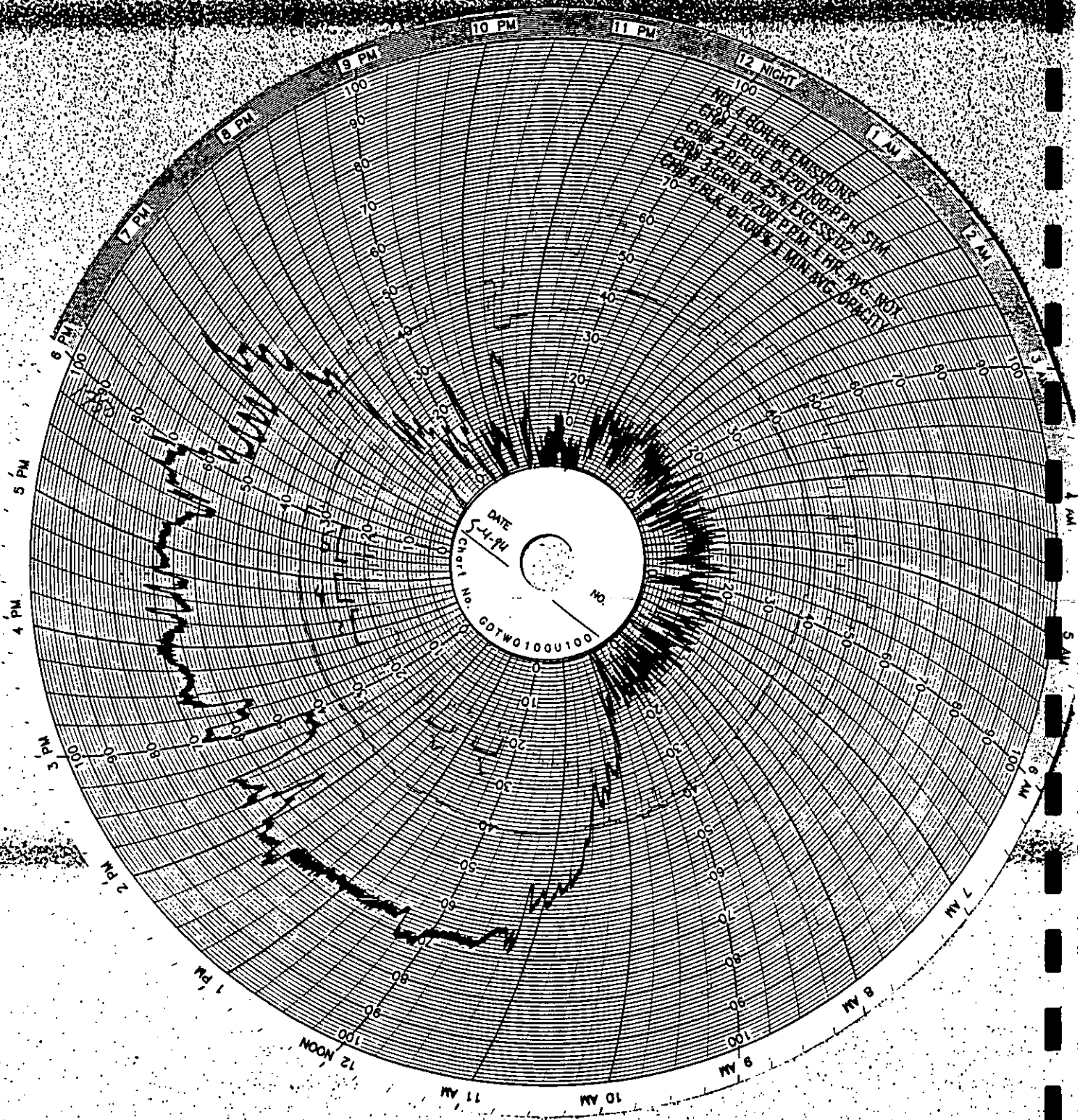


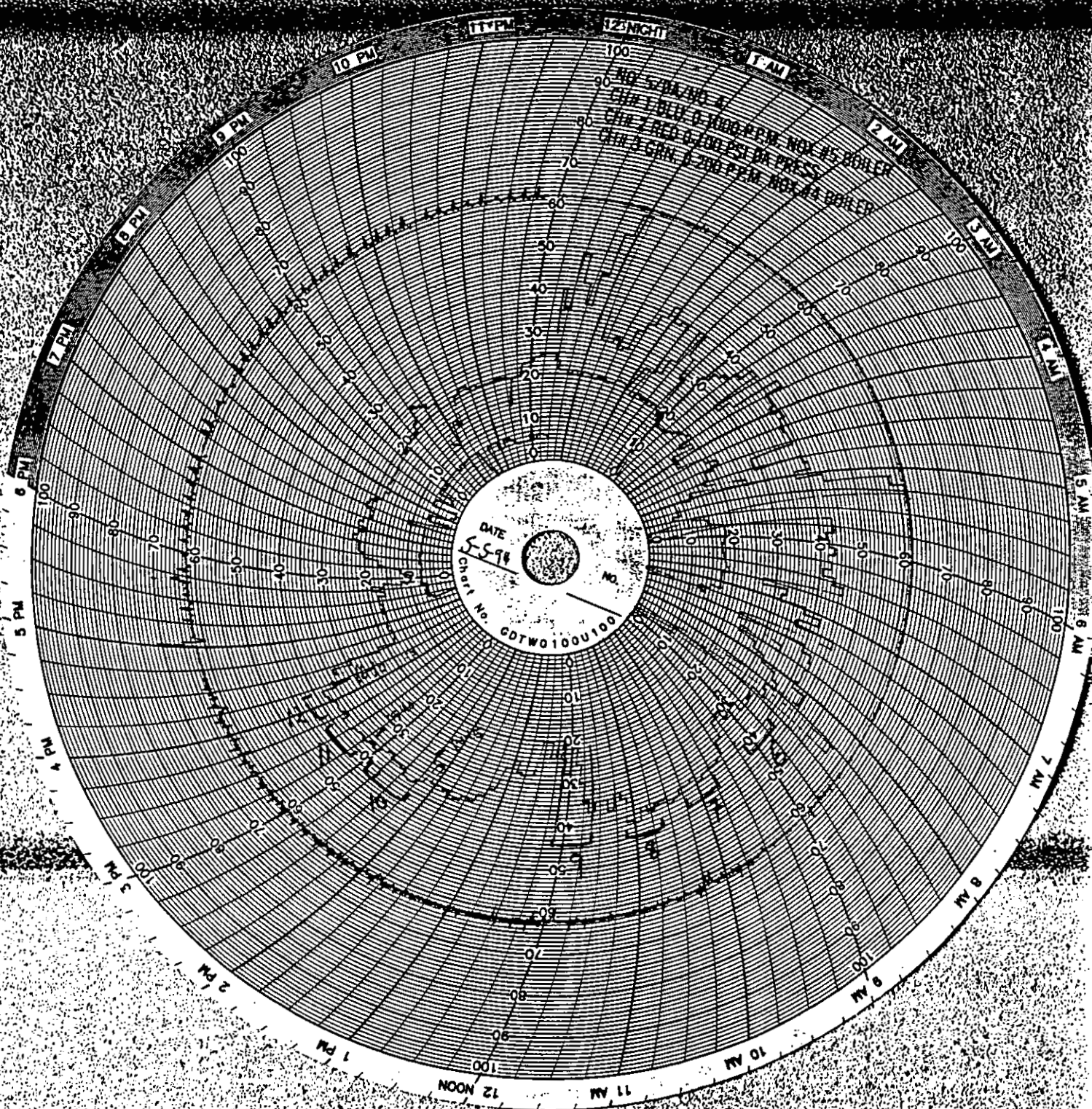
Green #4 NOx pen 20 min. behind time marks

Boiler 4

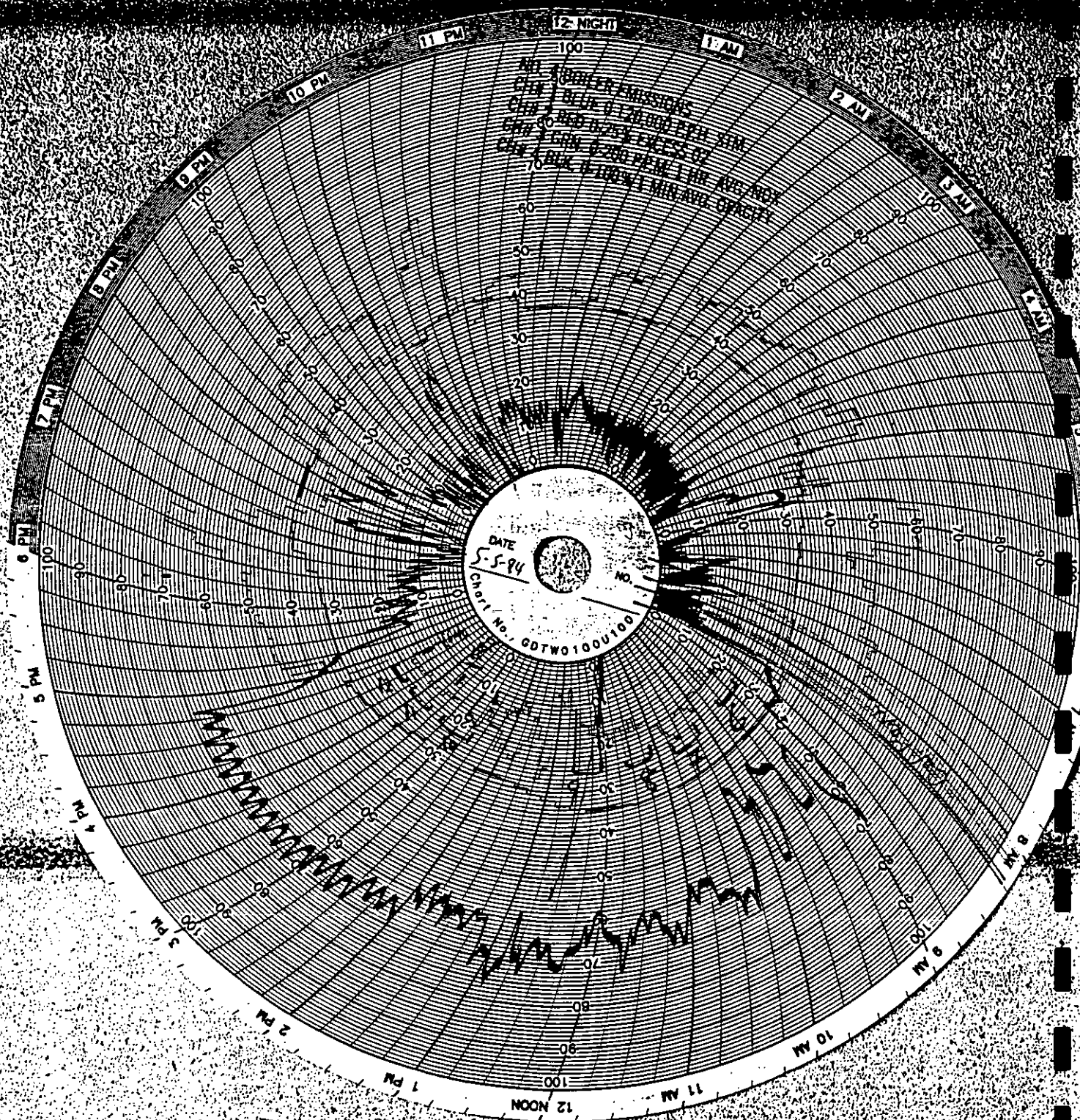
RA Test Runs 5-4-94

NOx ppm vol. wet





Boiler 4
RA test runs 5-5-94
NOx ppm vol.wet



Boiler 4
 RA test runs 5-5-94
 O₂ % vol, wet

7 S. Linden Avenue
South San Francisco, California 94080
Telephone: (415) 873-2055
Facsimile: (415) 952-1524



MOORE BROS.
3524 51ST AVENUE
SACRAMENTO, CA 95823

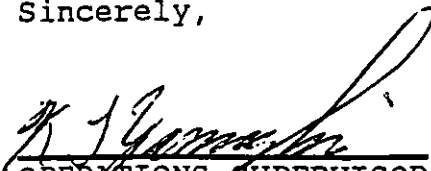
Date: 12-01-93
Altair Order No.: 701448-00
Customer Order No.: 16625

Dear Sir:

This is your Certificate of Analysis for:

<u>Cylinder Number</u>	<u>Mixture Components</u>	<u>Requested Composition</u>	<u>Certified Composition</u>
K 840817	OXYGEN	3%	3.00%
	NITROGEN	97%	97.00%

Sincerely,


OPERATIONS SUPERVISOR

COA6MC

IMPORTANT

The information contained herein has been prepared at your request by qualified experts within the Linds Division of Union Carbide Corporation. While we believe that the information is accurate within the limits of the analytical methods employed and is complete to the extent of the specific analyses performed, we make no warranty or representation as to the suitability of the use of the information for any particular purpose. The information is offered with the understanding that any use of the information is at the sole discretion and risk of the user. In no event shall Union Carbide Corporation be liable for the use of the information contained herein except the fee established for providing such information.

AGA**AGA Gas, Inc.**

Specialists in Dependable gas mixture

6421 Monclova Rd.
Maumee, Ohio 43537**SPECIALGAS****ANALYTICAL REPORT***Put up 11/15/93*

BRANCH: MOORE BROTHERS PROD: 3910205- 0 PROD CODE: 527000031 DATE: 03/14/91

CUSTOMER:

P.O.#: 002570

CYL: 1 SIZE: 031 BLEND TYPE: PP

TOLERANCE: 2% ANALYSIS

MIXTURE REQUESTED: 550 PPM NO/N2 CERTIFIED

ANALYSIS METHOD: CHEMILUMINESCENCE

ANALYSIS:

COMPRESSED GAS N.O.S.
577 PPM NITRIC OXIDE
BAL. NITROGEN

CYL #: CC84593

LOT #: 0311CT

BLENDER: CB

SHIP CODE: NON-FLAMMABLE U.N.#: 1956

CGA: 660

ANALYST: *[Signature]*

AGA

AGA Gas, Inc.

Specialists in Dependable gas mixtures

6421 Monclova Rd.

Maumee, Ohio 43537

SPECIALGAS

ANALYTICAL REPORT

BRANCH: MOORE BROTHERS PROD: 7930116- 0 PROD CODE: 545400031 DATE: 07/19/93

CUSTOMER: REF. P.O. 16229

P.O.#:

CYL: 1 SIZE: 031 BLEND TYPE: PP

TOLERANCE: 2% ANALYSIS

MIXTURE REQUESTED: 75 PPM NO/BAL. N2 CERTIFIED

ANALYSIS METHOD: CHEMILUMINESCENCE

Analysis

COMPRESSED GAS N.O.S.

71.9 PPM NITRIC OXIDE

BAL. NITROGEN

CYL #: CC7463

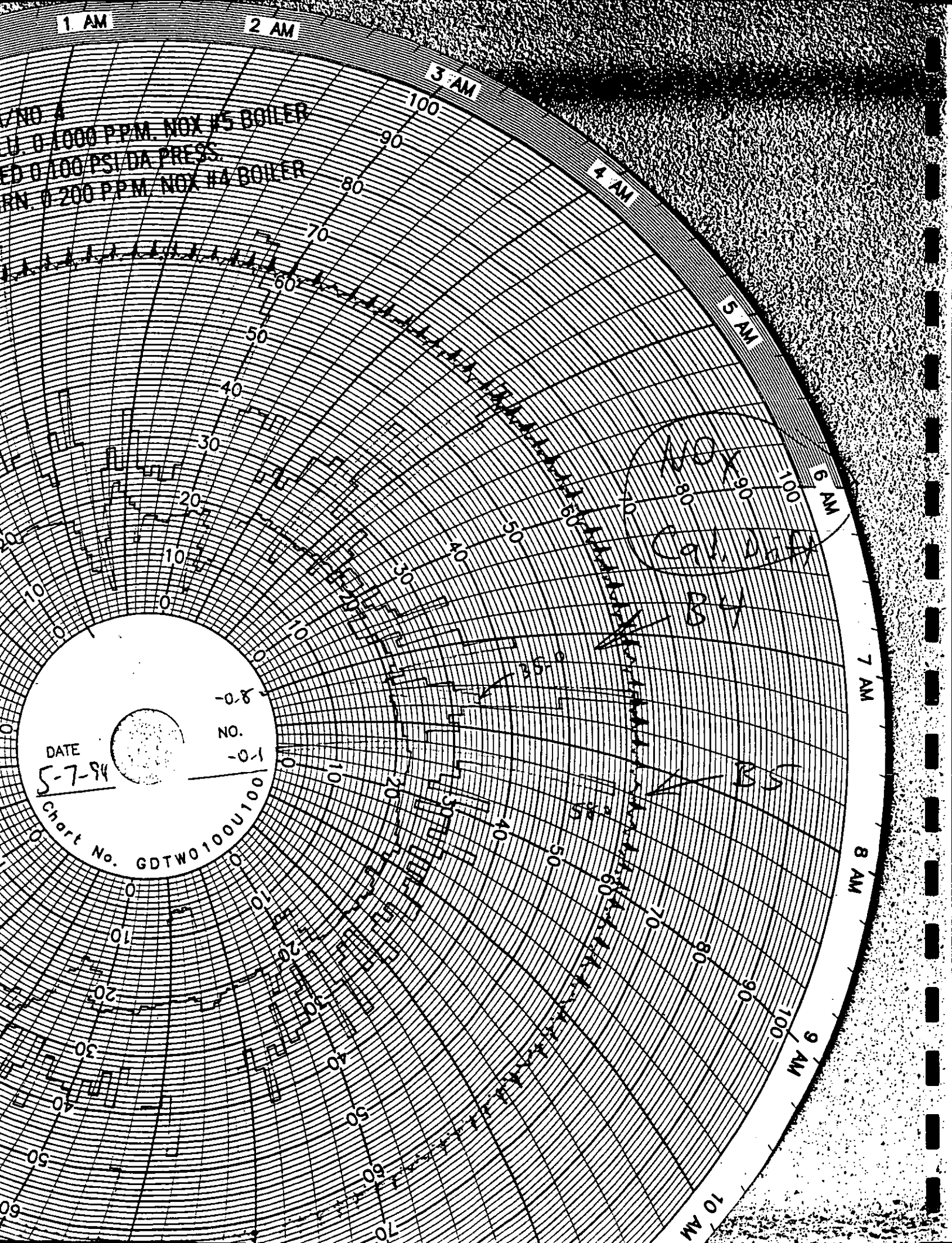
LOT #: 0716BC

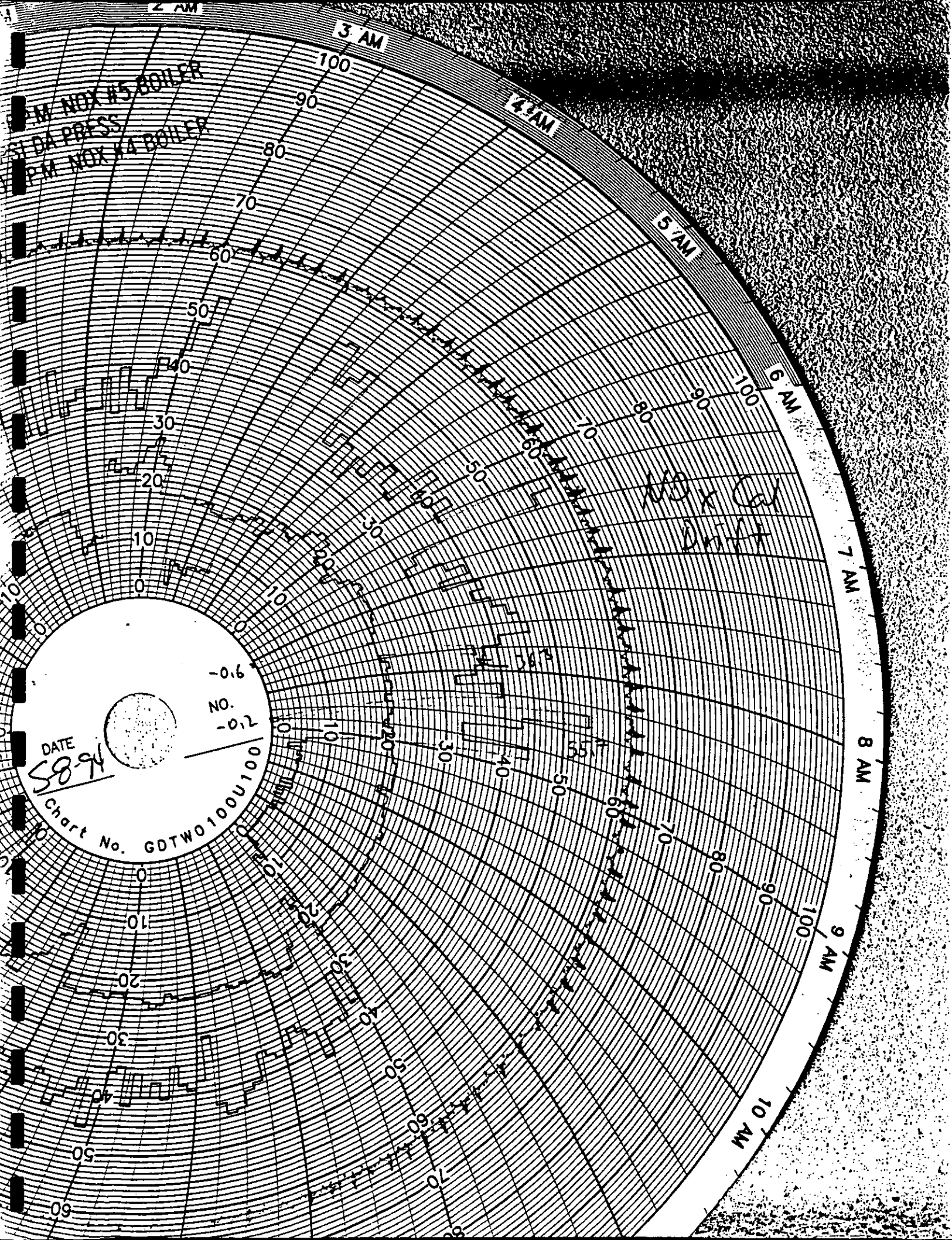
BLENDER: DB

SHIP CODE: NON-FLAMMABLE U.N.#: 1956

CGA: 660

ANALYST. 





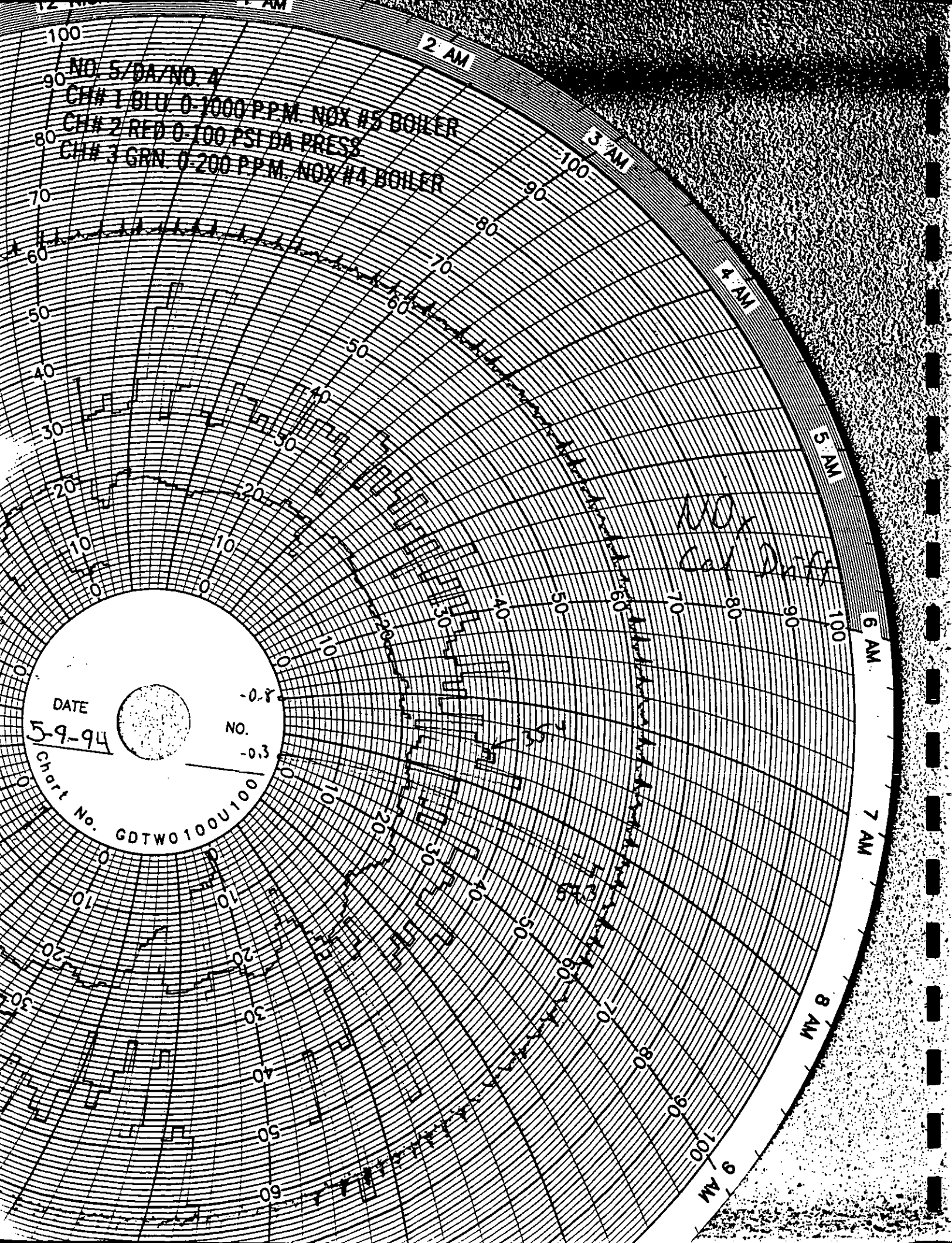
NOX #5 BOILER
SI DA PRESS
PM NOX #4 BOILER

DATE
58-94

Chart No. GDTWO100U100

-0.6
NO.
-0.2

NOx Cal
Drift



NO 5/DA/NO 4
CH#1 BLU 0-1000 PPM NOX #5 BOILER
CH#2 RED 0-100 PSI DA PRESS
CH#3 GRN 0-200 PPM NOX #4 BOILER

DATE
5-9-94
Chart No. GDTW0100U100
NO. -0.8
-0.3

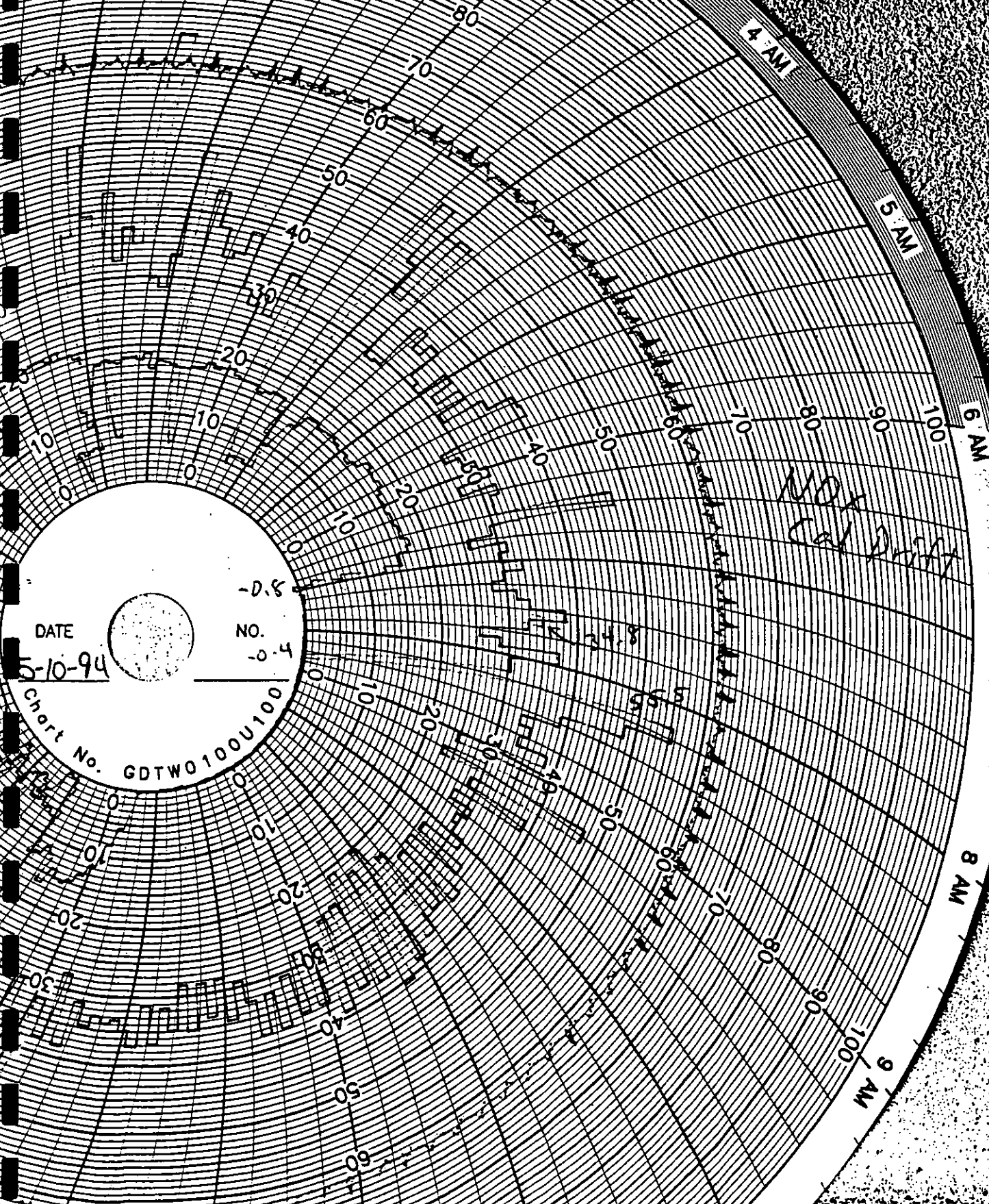
NOX
Cal Diff

5/DA/NO. 4

#1 BLU 0-7000 P.P.M. NOX #5 BOILER

#2 RED 0-100 PSI DA PRESS.

#3 GRN 0-200 P.P.M. NOX #4 BOILER



NOX
Cal Draft

DATE

NO.

5-10-94

-0.8

-0.4

Chart No.

GDTW0100U100

12 NIGHT

1 AM

2 AM

3 AM

4 AM

5 AM

6 AM

7 AM

8 AM

9 AM

NO. 5/DA/NO. 4

CH# 1 BLU. 0-1000 PPM. NOX #5 BOILER

CH# 2 RED 0-100 PSI DA PRESS

CH# 3 GRN. 0-200 PPM. NOX #4 BOILER

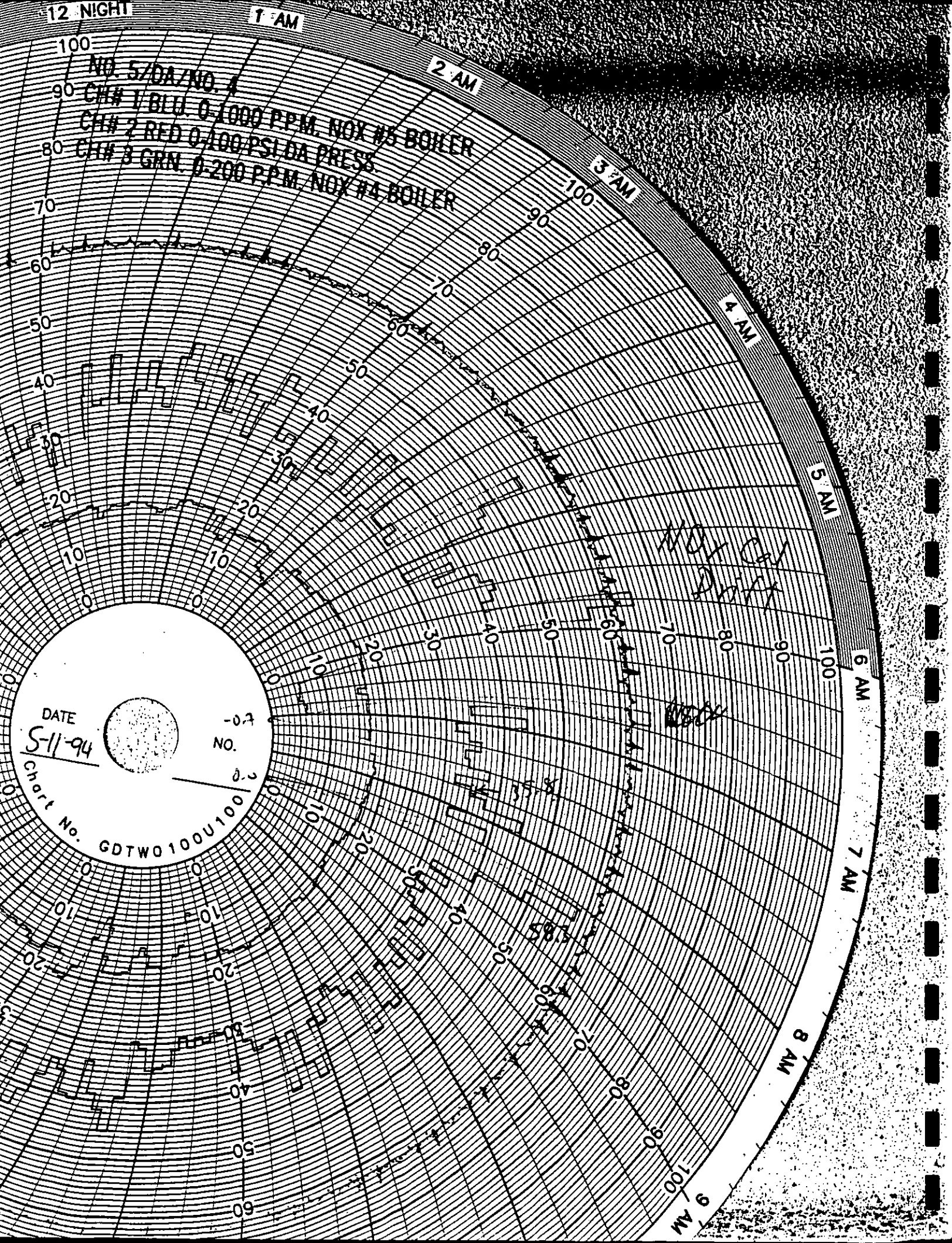
DATE
5-11-94

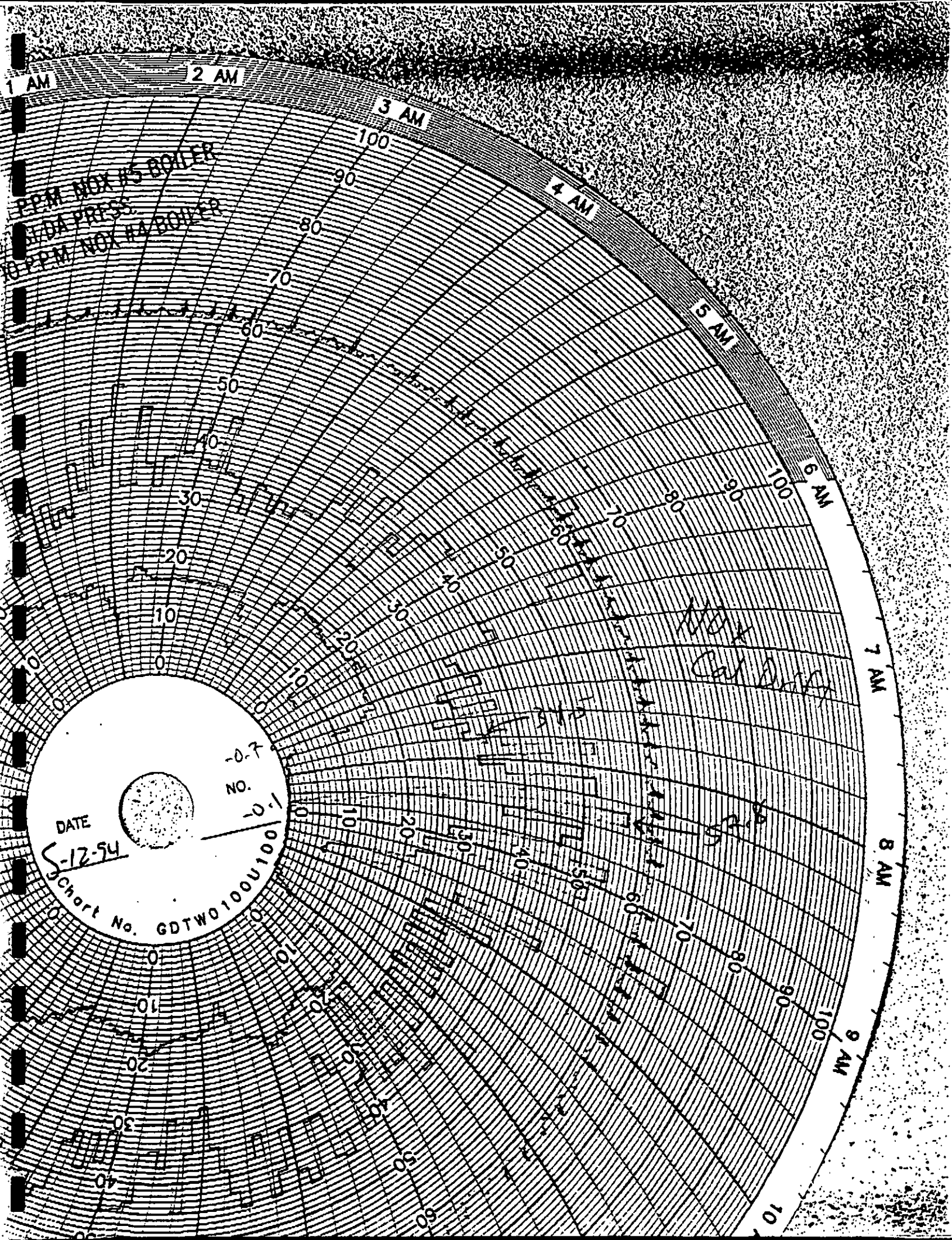
NO.
0.3

Chart No. GDTWO100U100

NOX G/Drift

WEEK



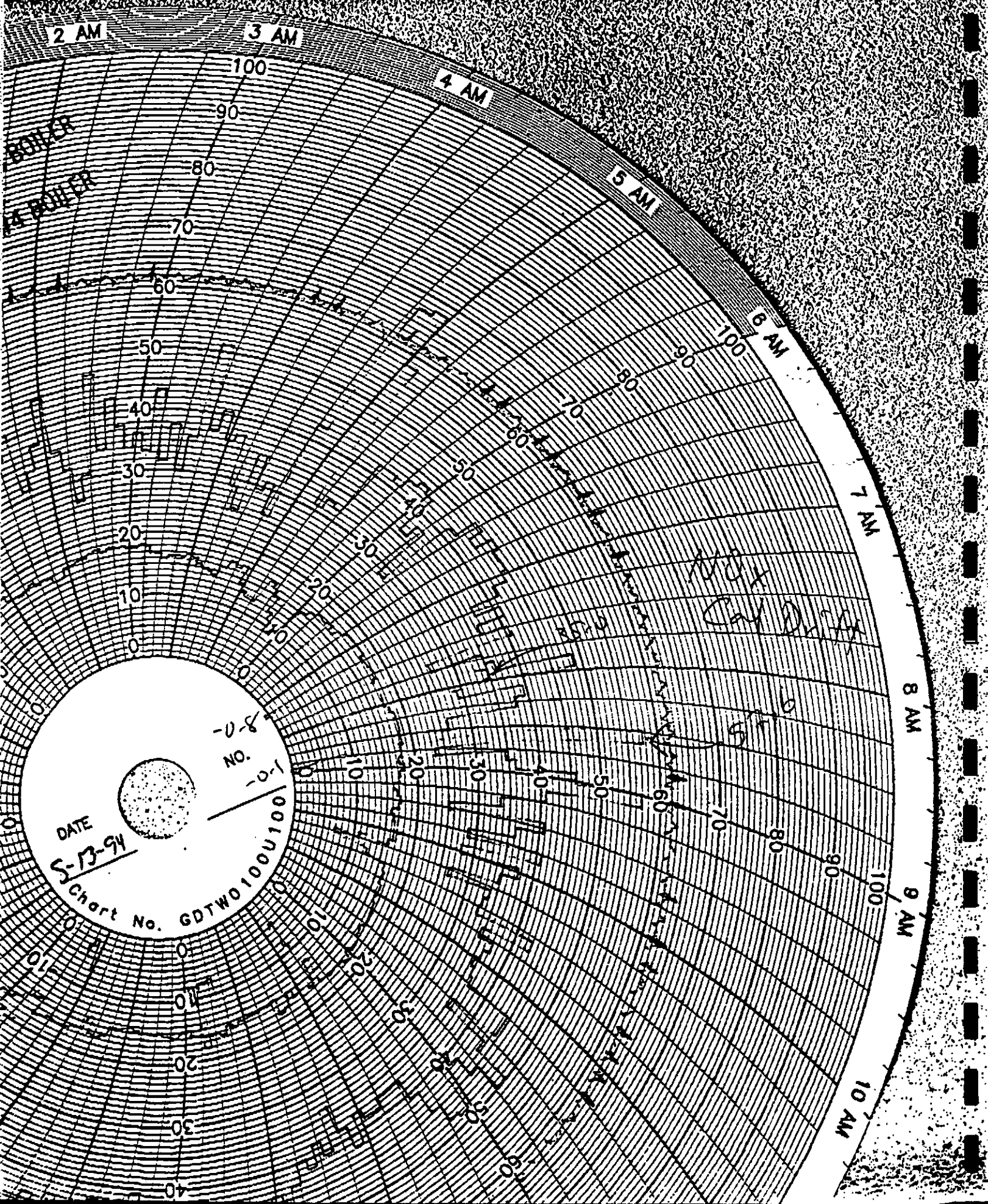


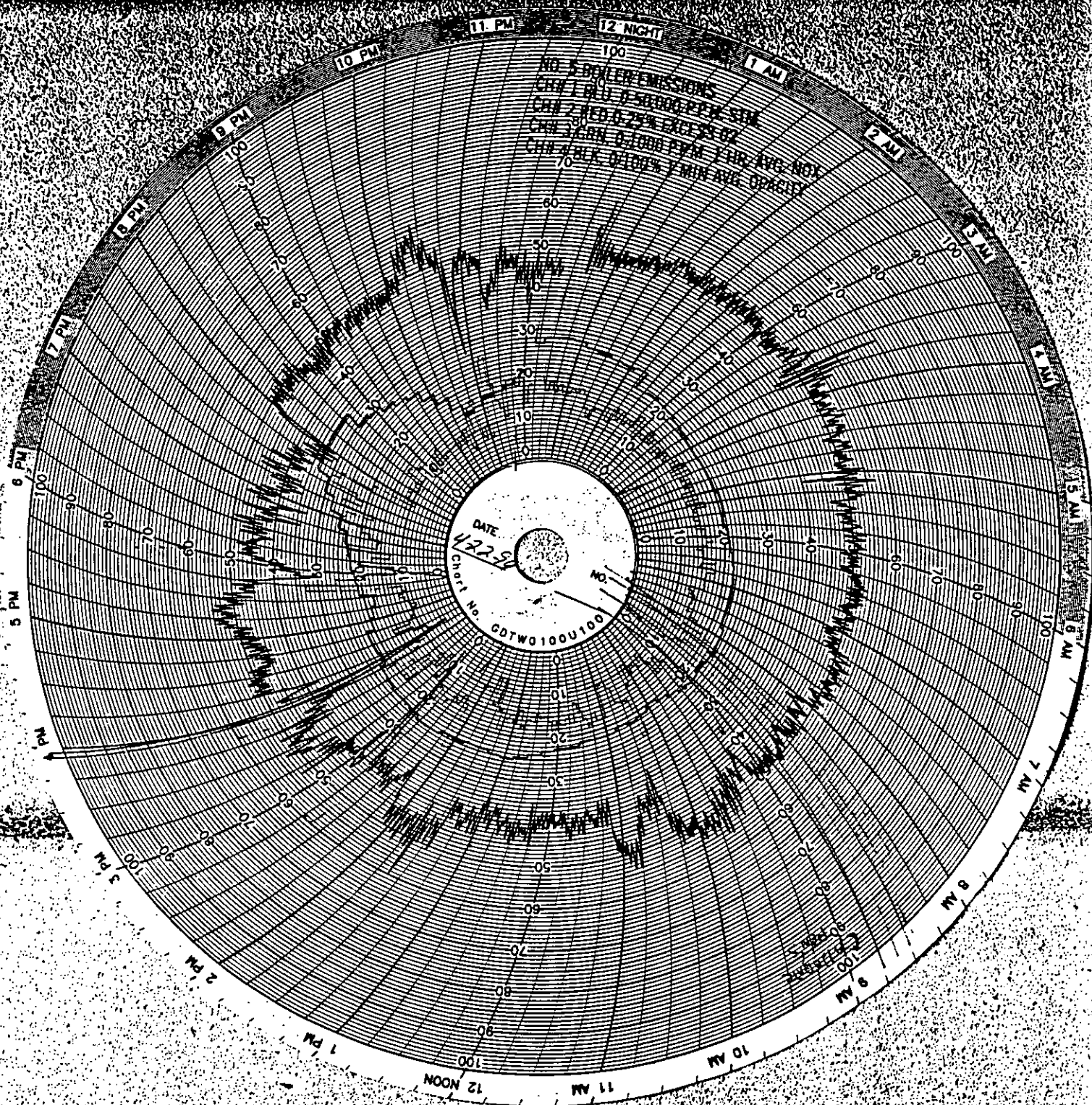
PPM NOX #5 BOILER
PPM NOX #4 BOILER
PPM NOX #3 BOILER

DATE
5-12-54
Chart No. GDTW01000100
NO. -0.7
-0.1

Cal Data

1000





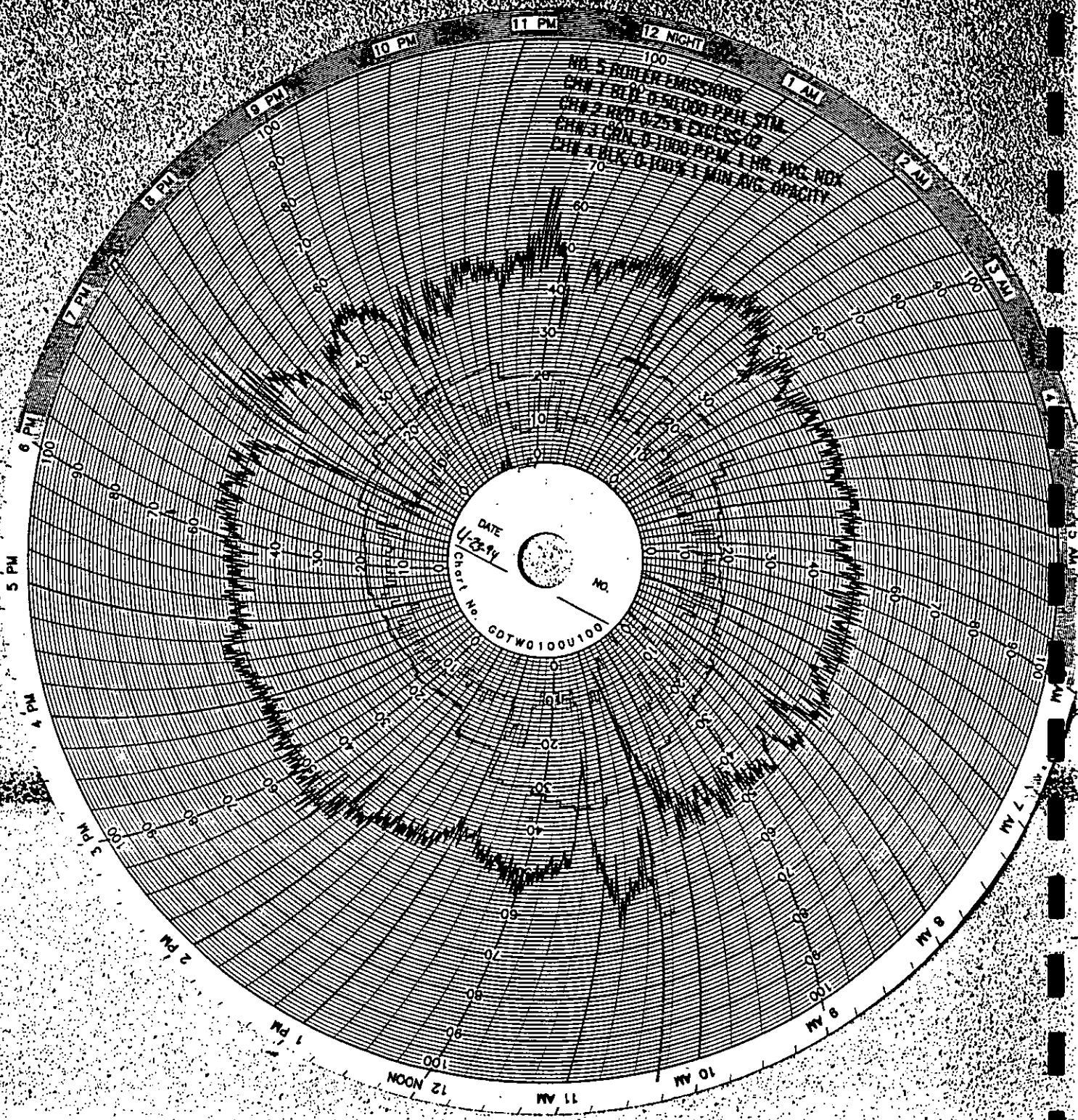
Cal. Drift

Boiler 5

Opacity cal @ 0900 AM

O₂ cal @ 0820 AM

% F.S.		
Low	High	Cal. Value (7% opacity)
-0.5	36.5	
12.2	85.2	
(3.07% O ₂)	(20.97% O ₂)	



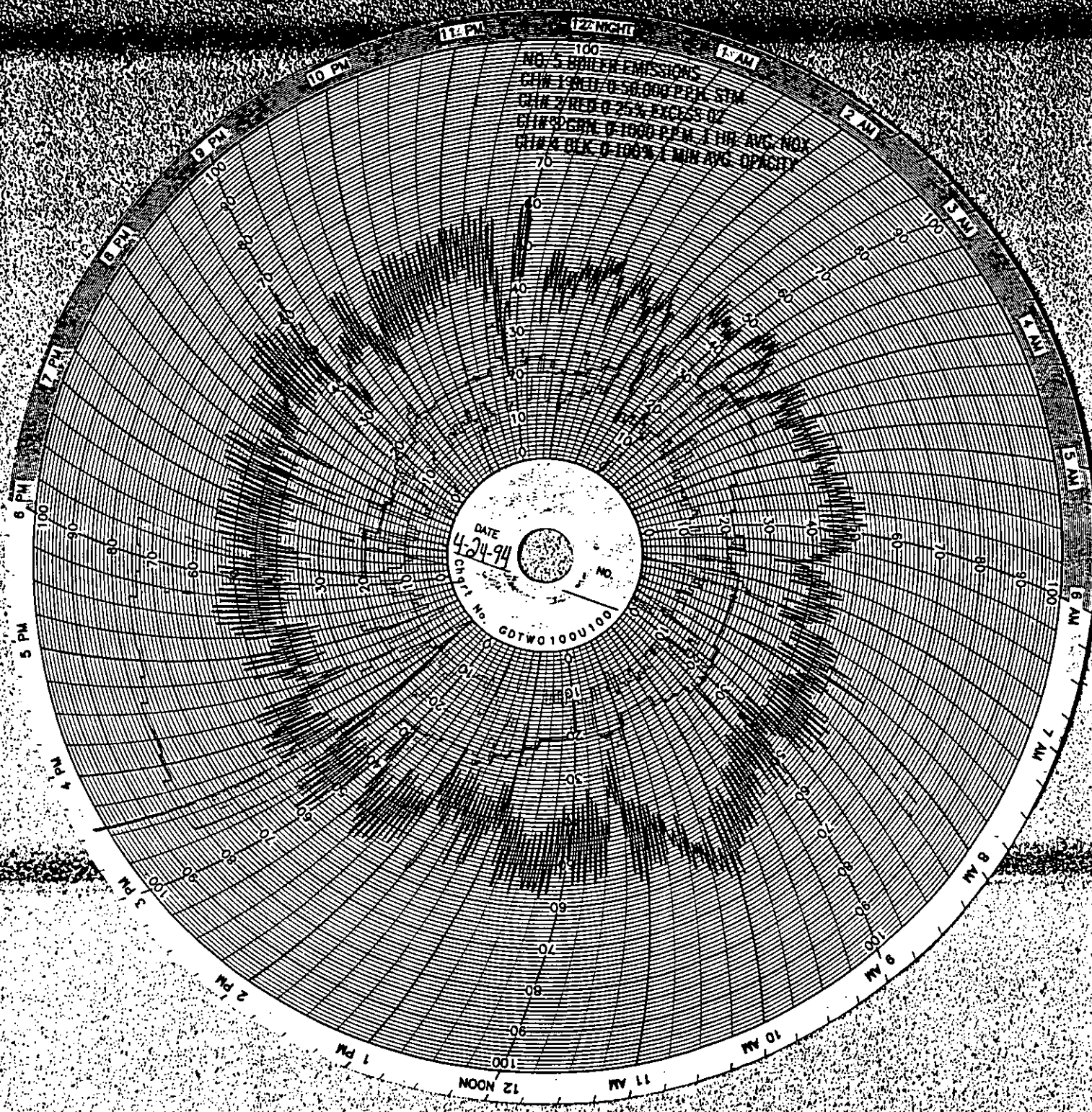
Boiler 5

Opacity

O₂

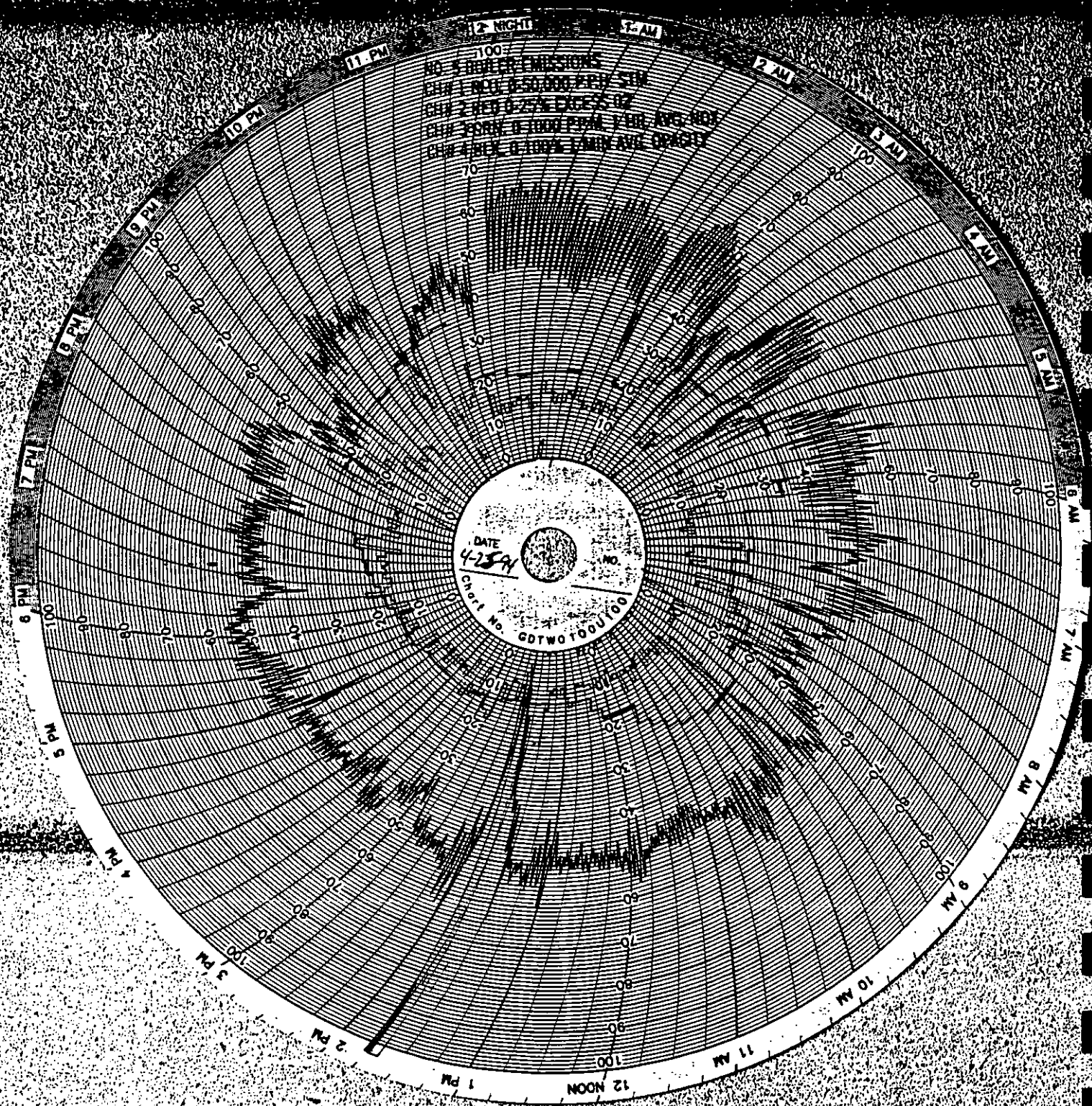
%FS

Low	High
0.0	37.0
12.0	84.8



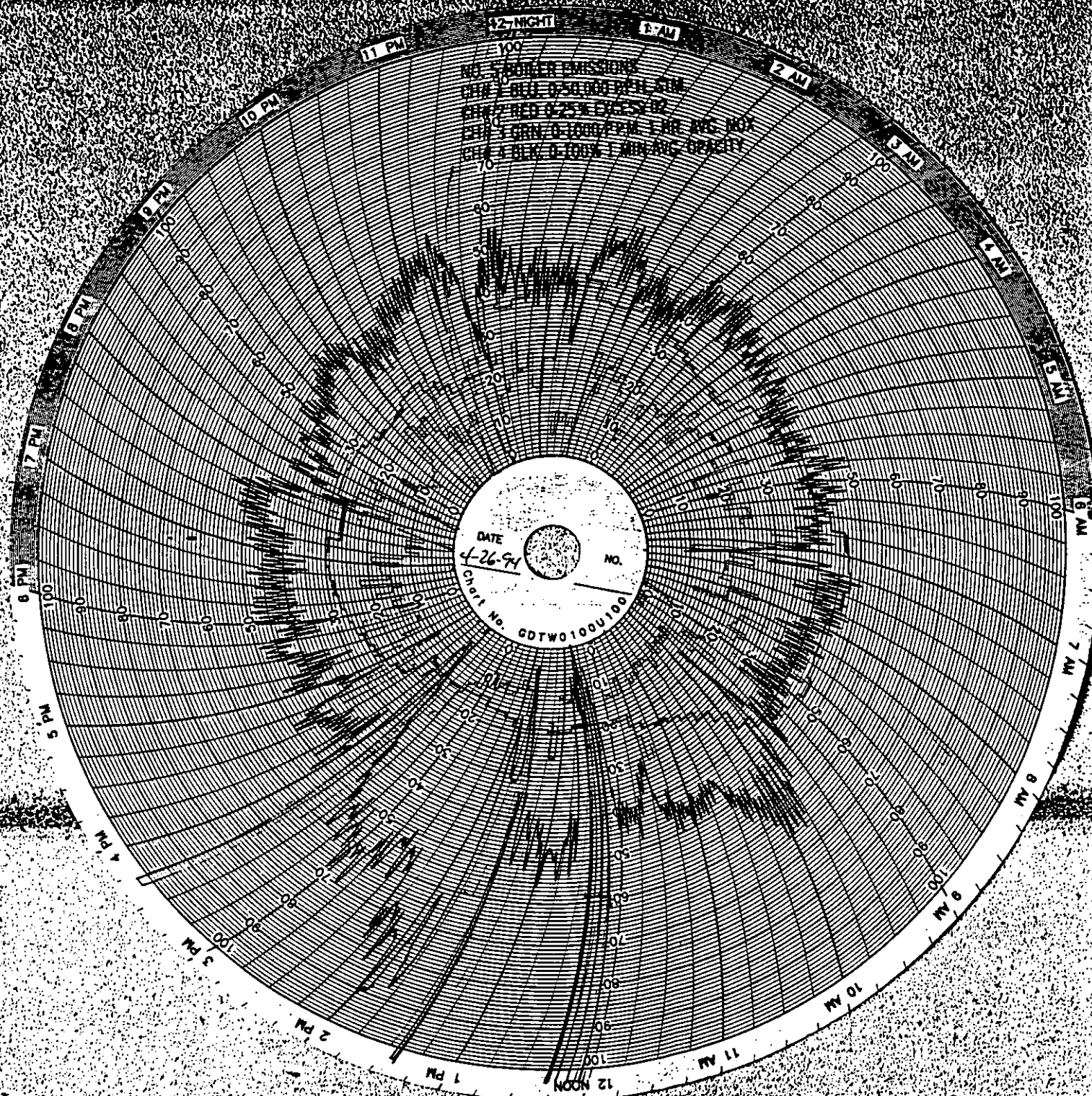
Boiler 5

	90 FS	
	Low	High
Opacity	0.0	37.0
O ₂	11.8	83.6



Boiler 5

	<u>% FS</u>	
	<u>Low</u>	<u>High</u>
O ₂ ant7	0.0	37.5
O ₂	12.2	84.0



Boiler 5

9. FS

Low	High
-----	------

Opacity

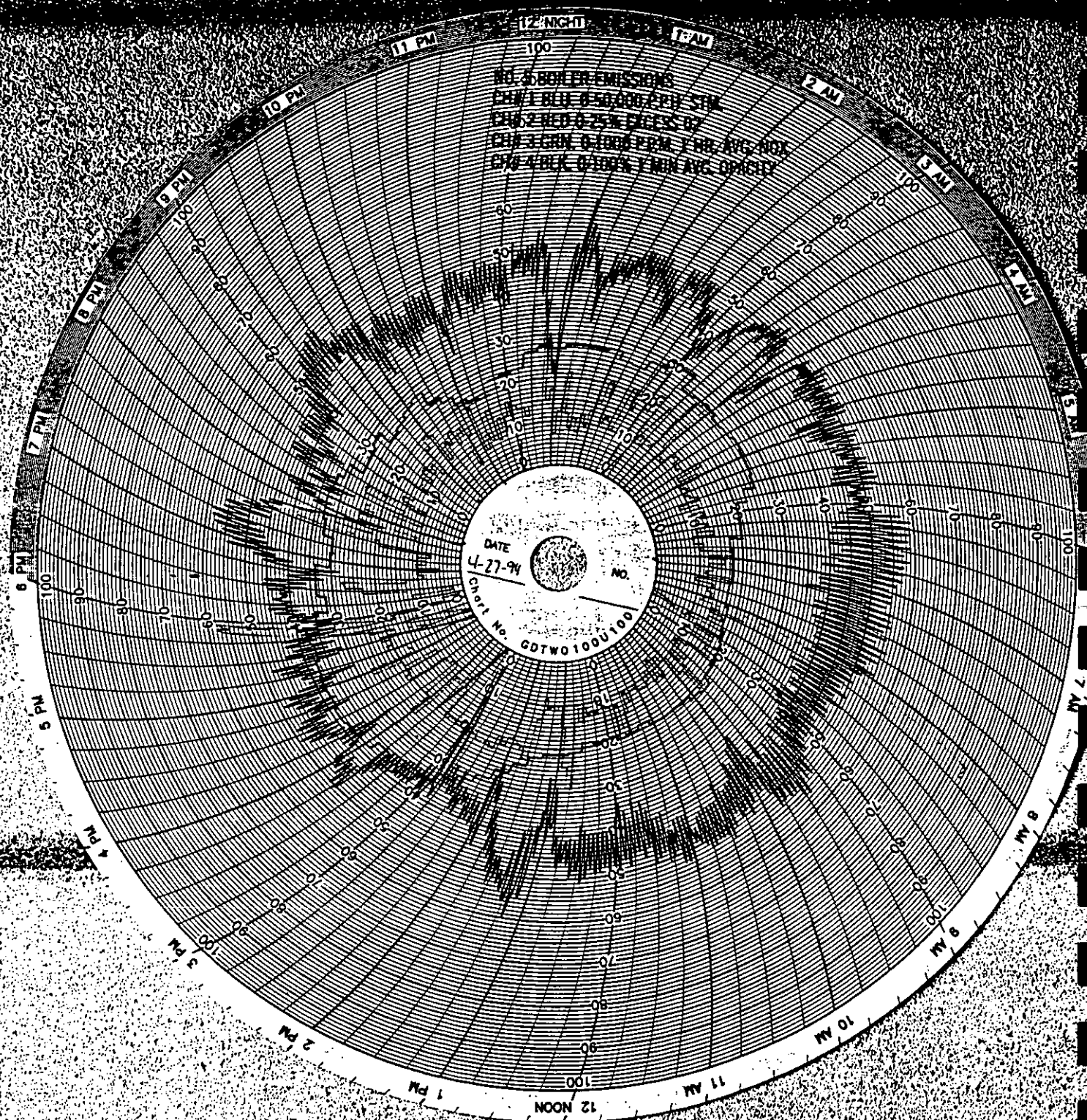
0.0

37.0

O₂

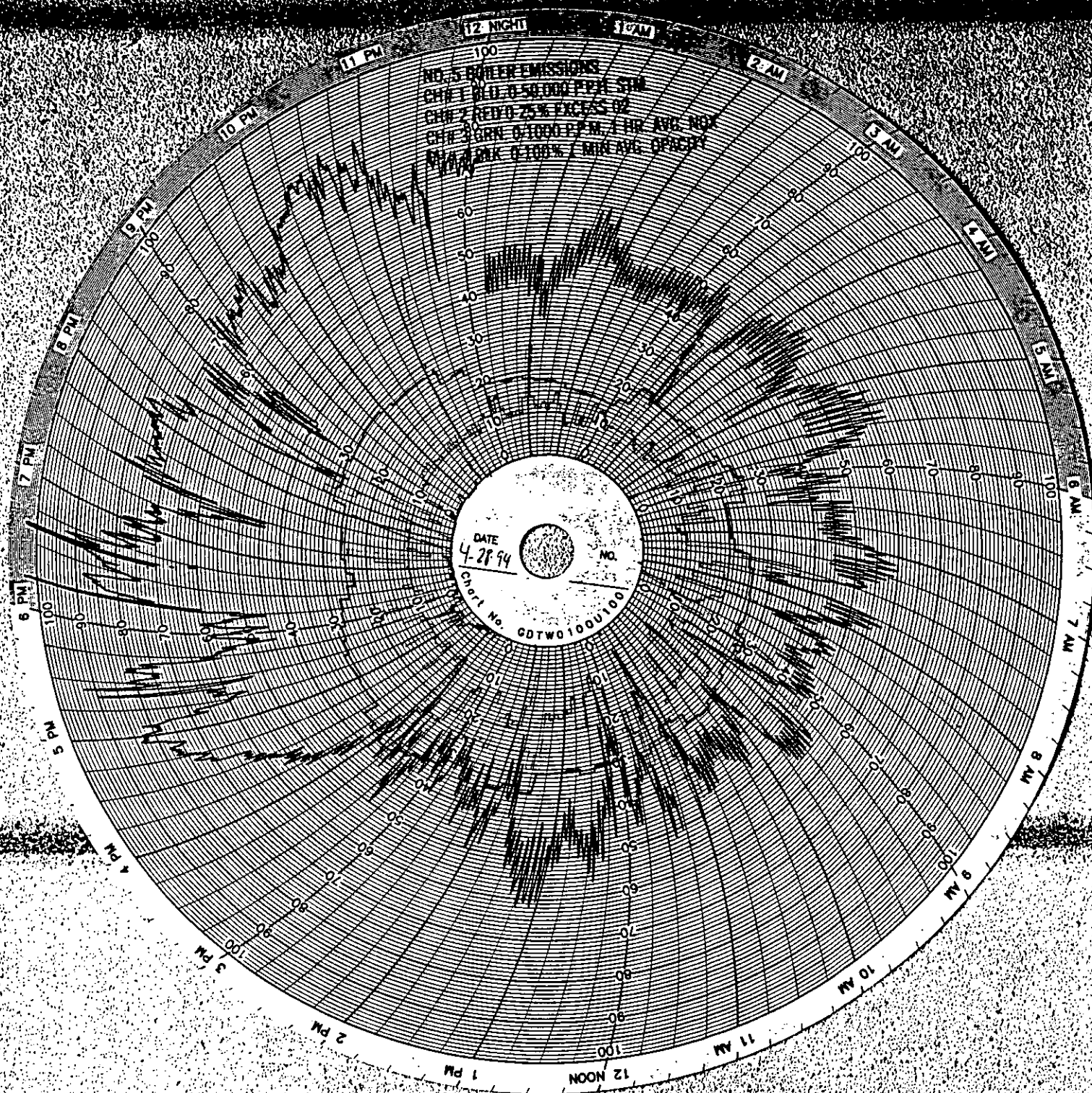
11.7

83.1



Boiler 5

	<u>% FS</u>	
	<u>Low</u>	<u>High</u>
Opacity	-0.2	368
O ₂	11.6	83.6



Boiler 5

9. F1

Low High

Opacity

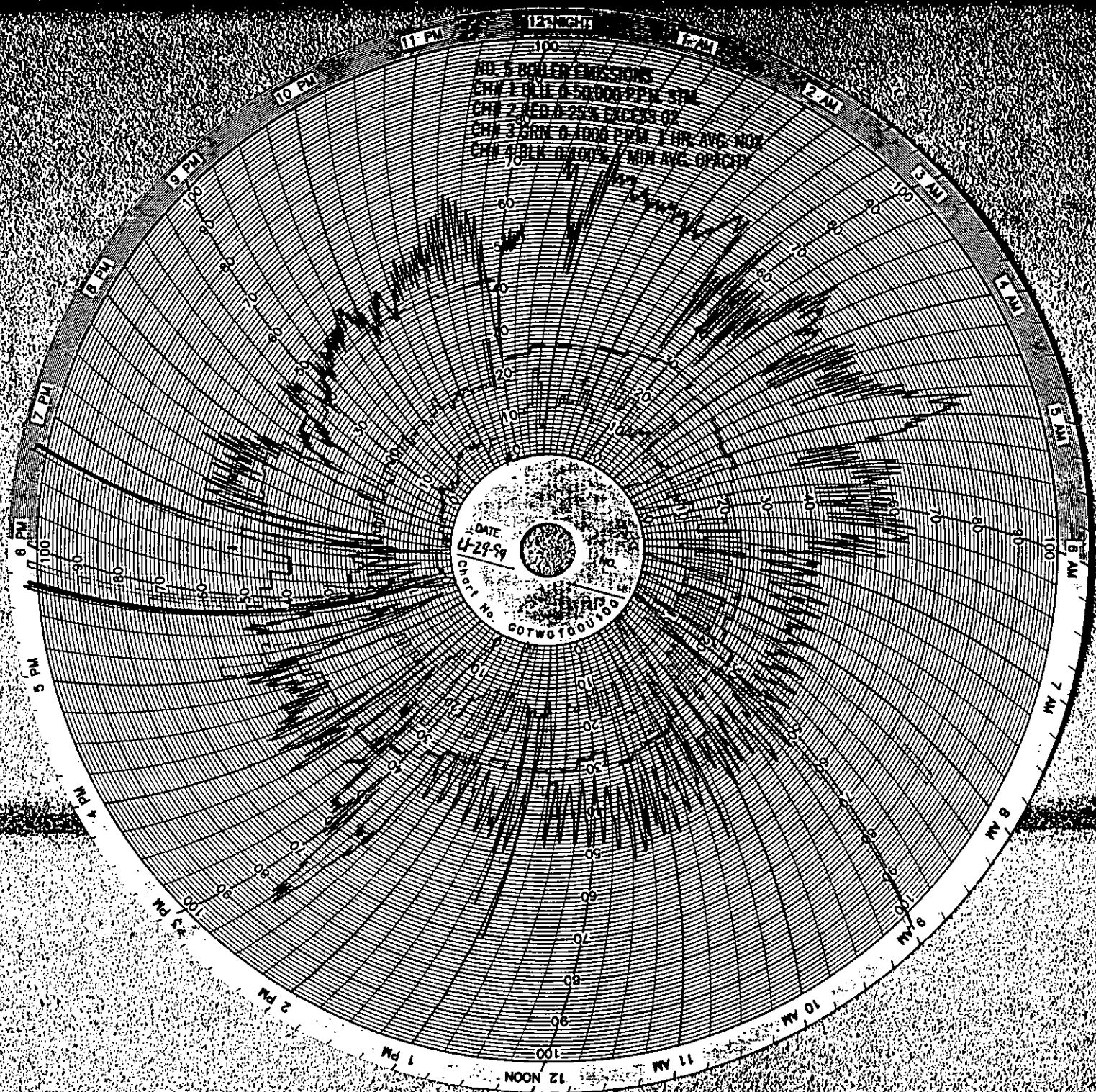
-0.1

36.8

O₂

11.8

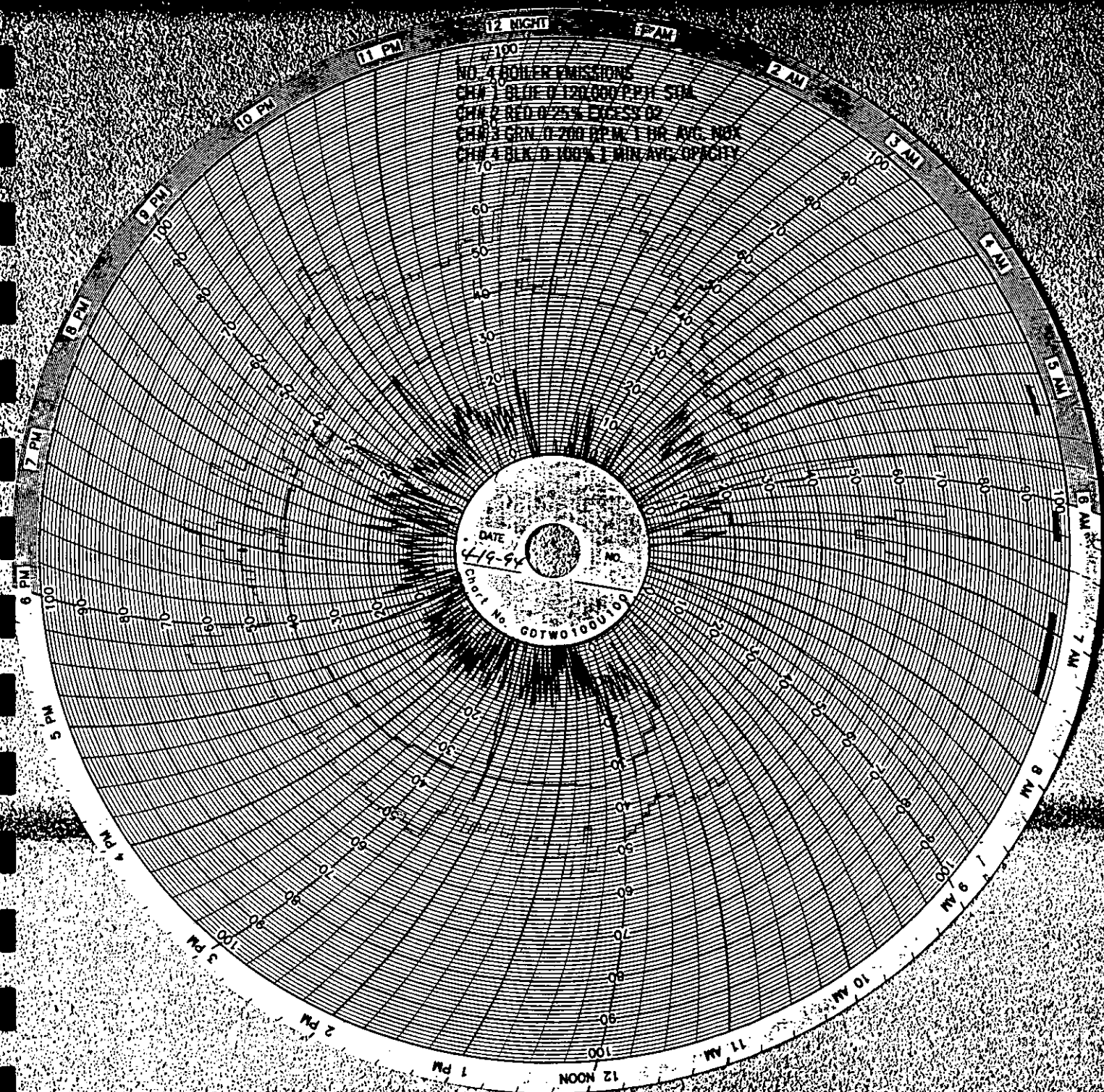
83.8



Boiler 5

Opacity

9. FS	
<u>Low</u>	<u>High</u>
0.0	36.8

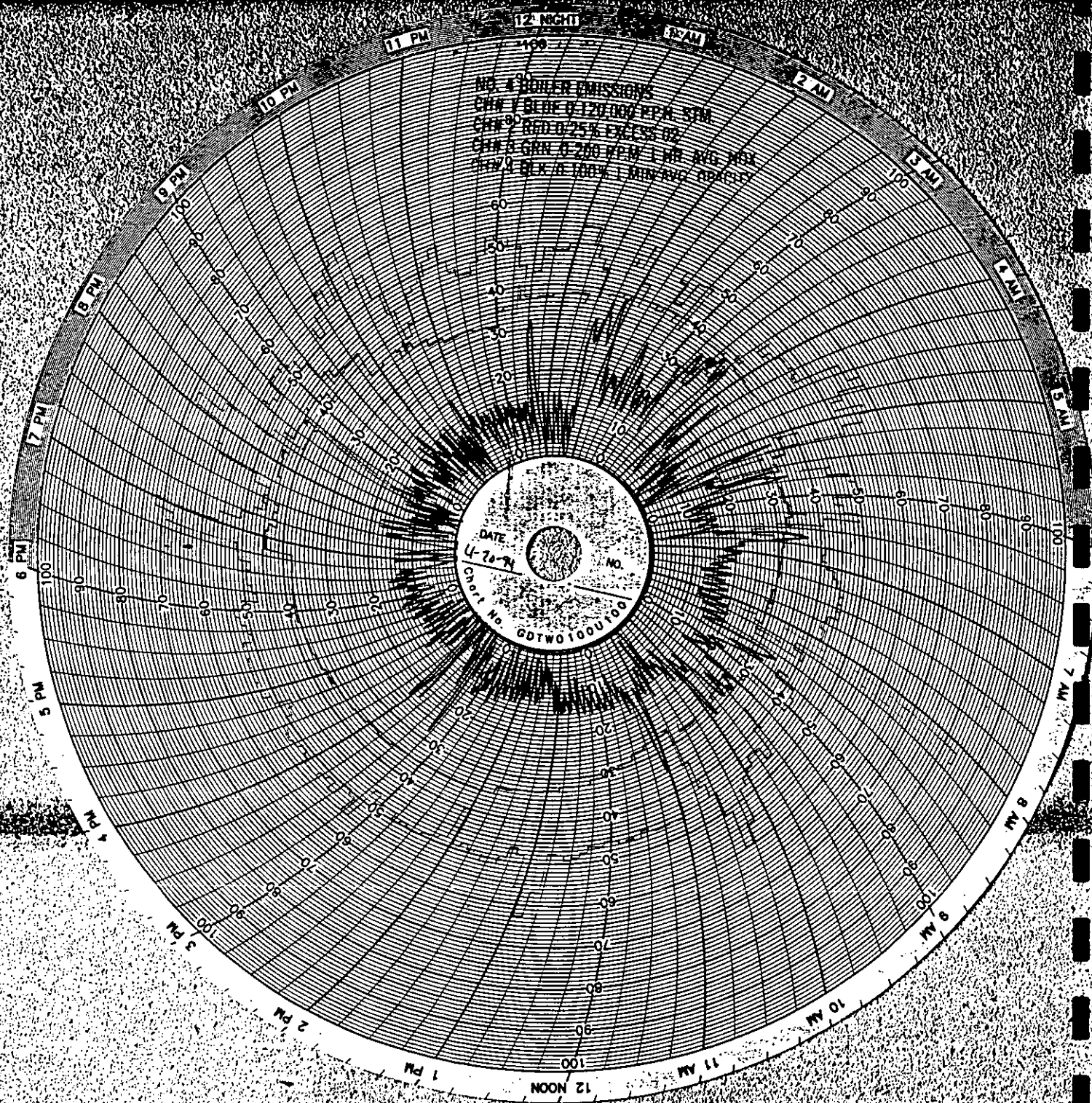


Cal-Drift

Boiler 4

~~Cal~~

Opacity Cal @ 840 PM (42.8% F.S.) zero @ (0-0 % F.S.)
 (Opacity Cal. filter 99%)



Boiler 4

O₂ Cal. @ 810 AM

Opacity

Low Cal. = 3.0% O₂

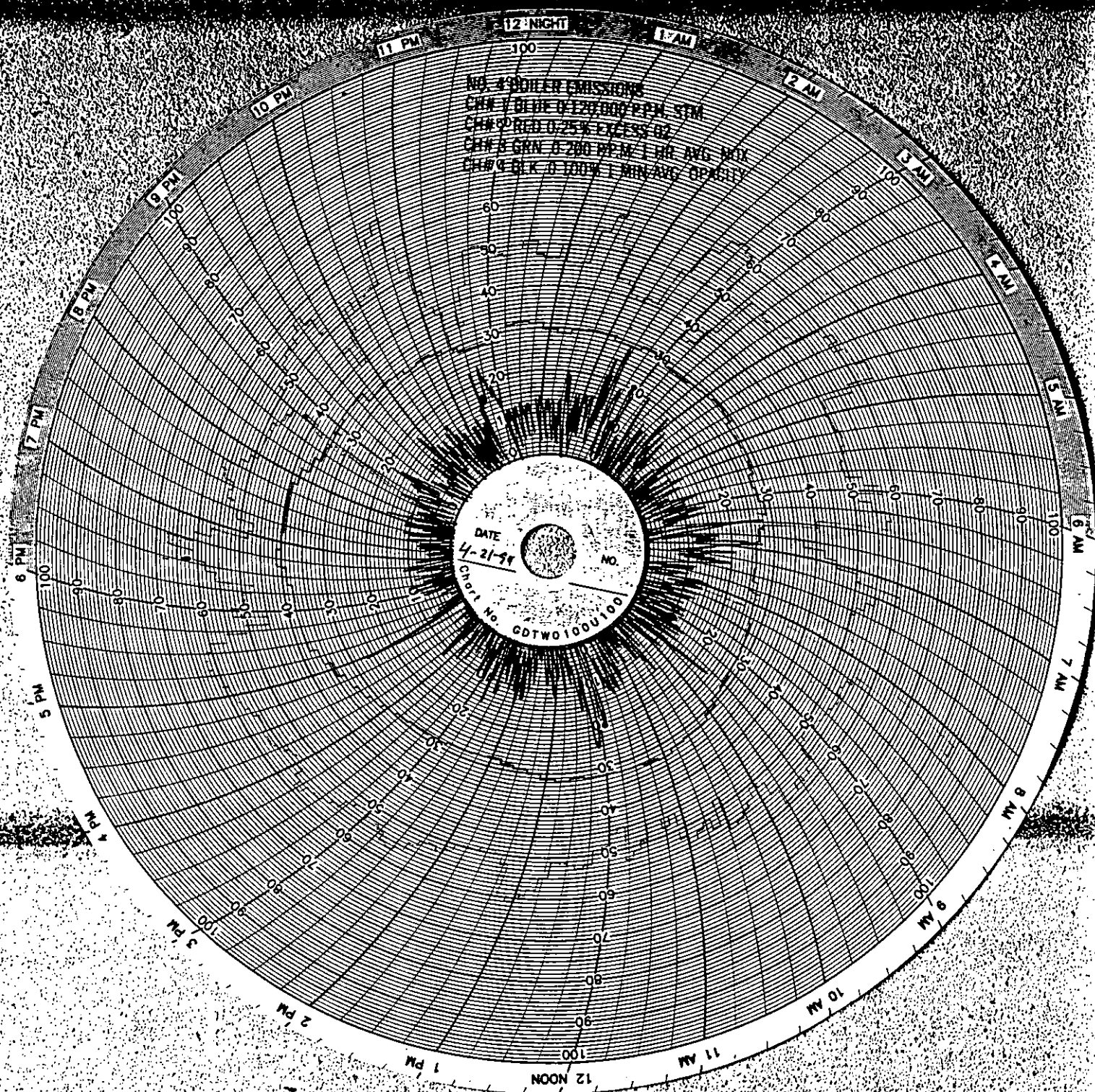
12.4% F.S.

Zero
0.0

Cal. = 20.9% O₂

83.9% F.S.

Cal
42.6



Boiler 4

O₂

Opacity

90 F.S.

Low

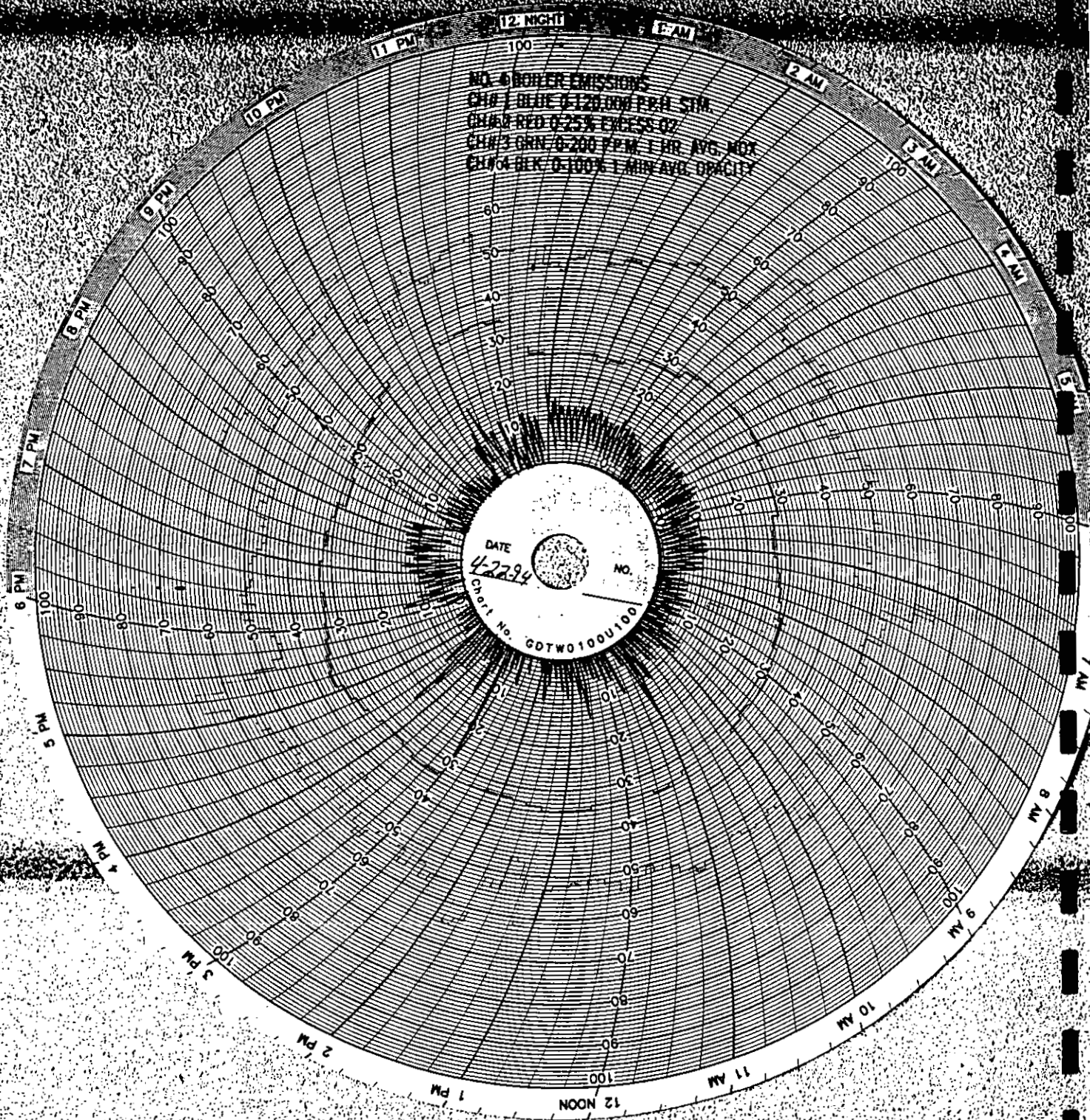
12.4

0.0

High

84.2

43.0



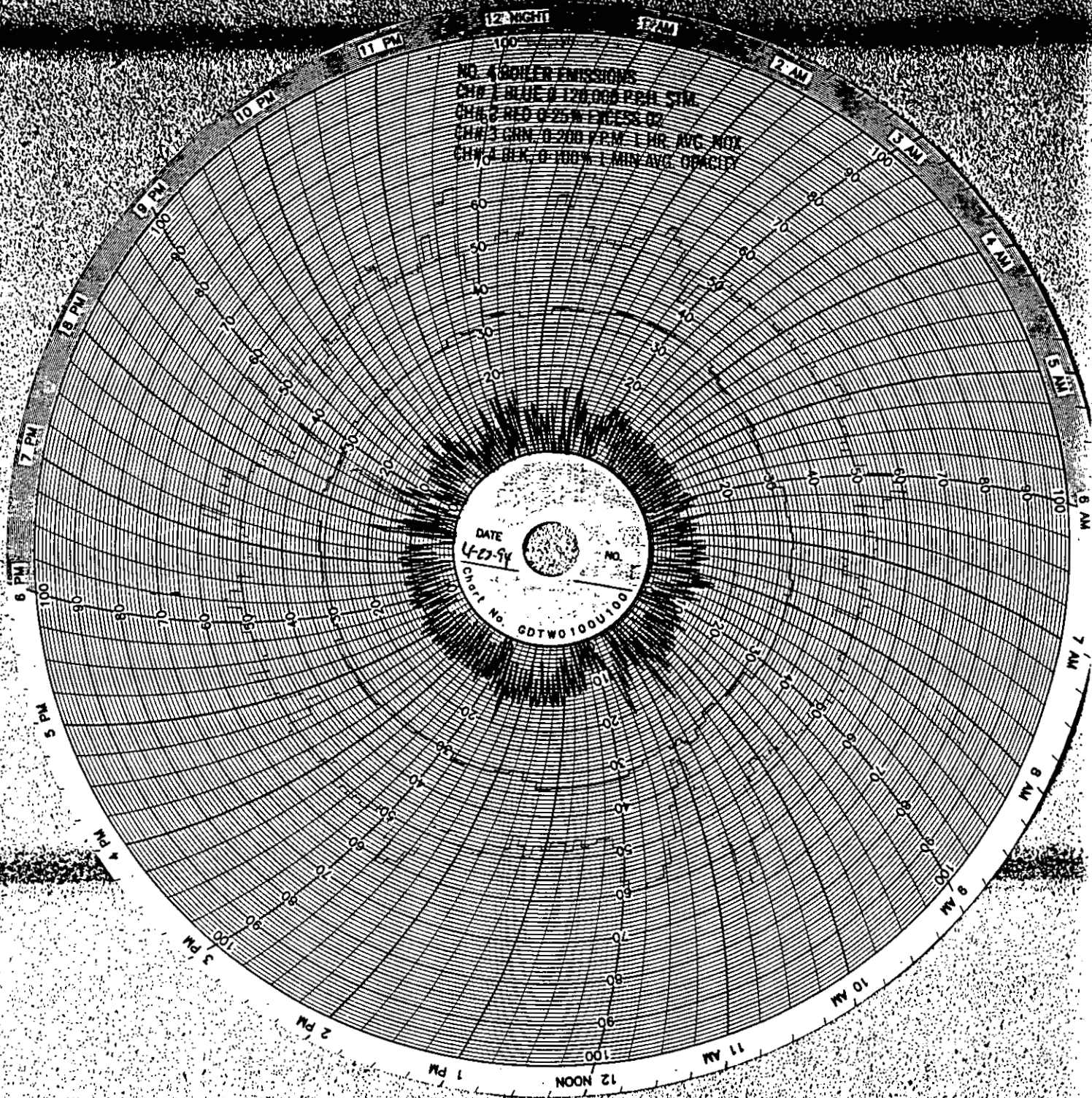
Boiler 4

O₂

Opacity

70 F.S.

Low	High
12.4	84.0
0.0	42.5

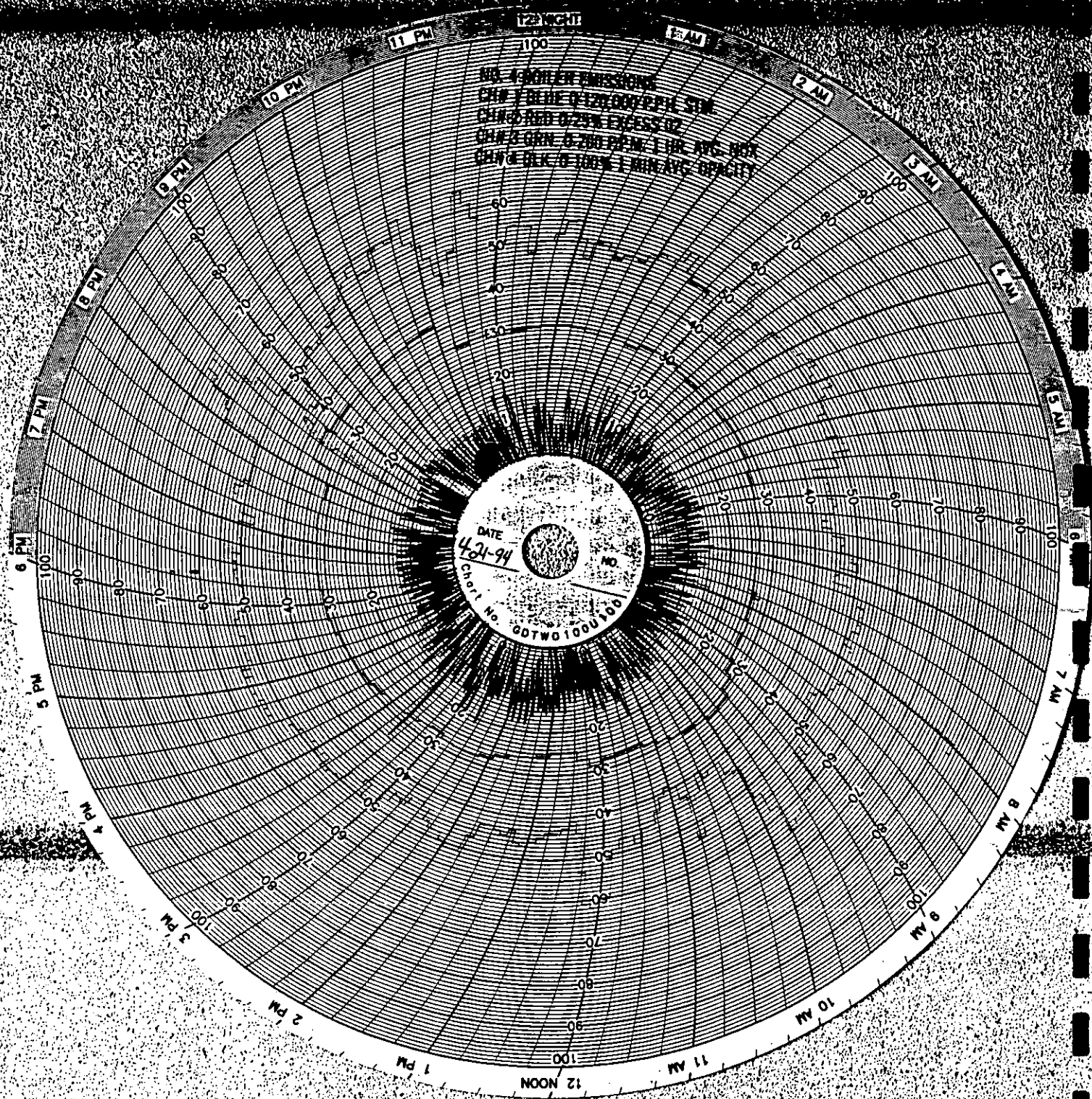


Boiler 4

9. F.S.	
Low	High
12.2	84.0
0.0	42.7

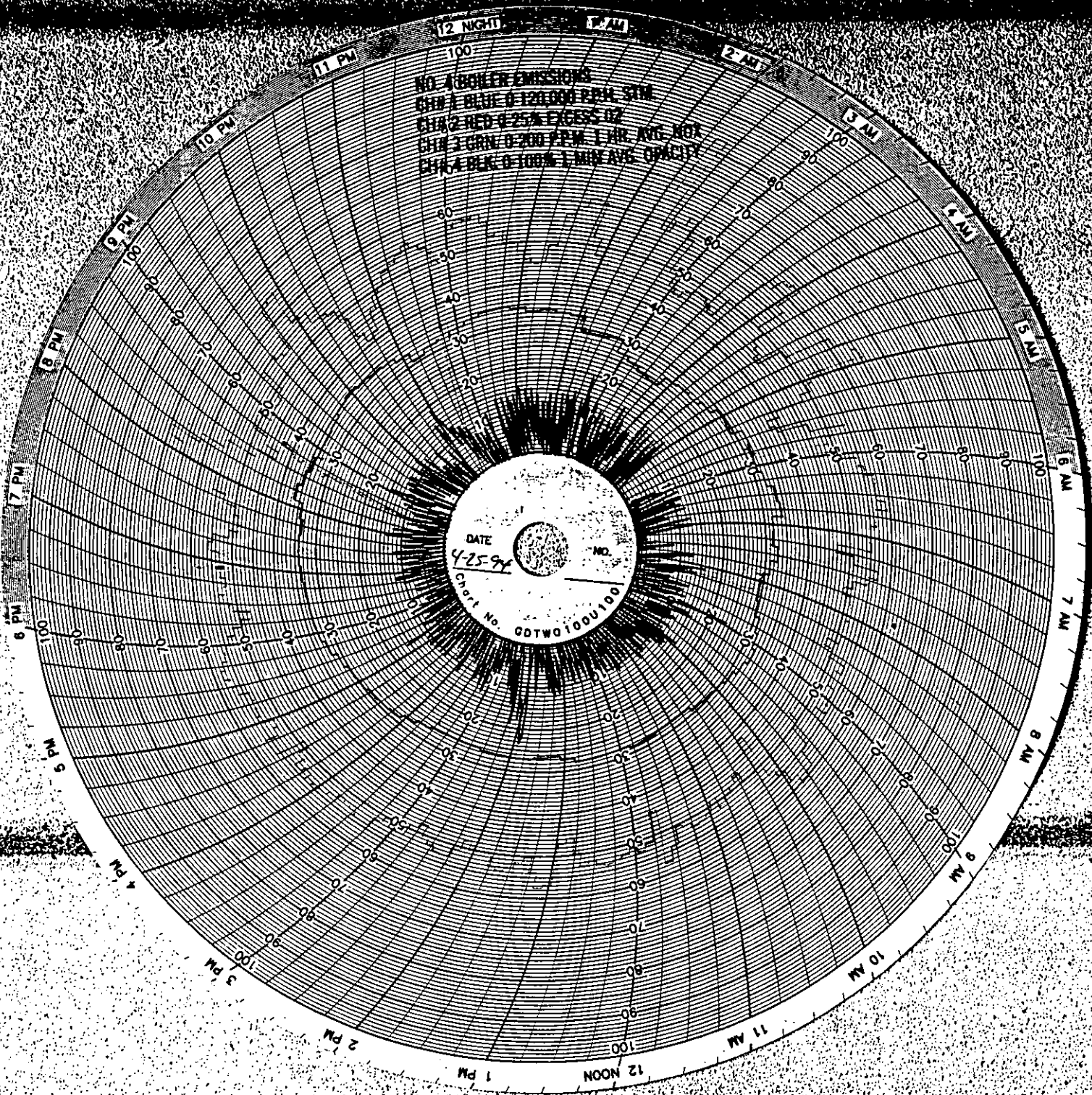
O₂

Opacity



Boiler 4

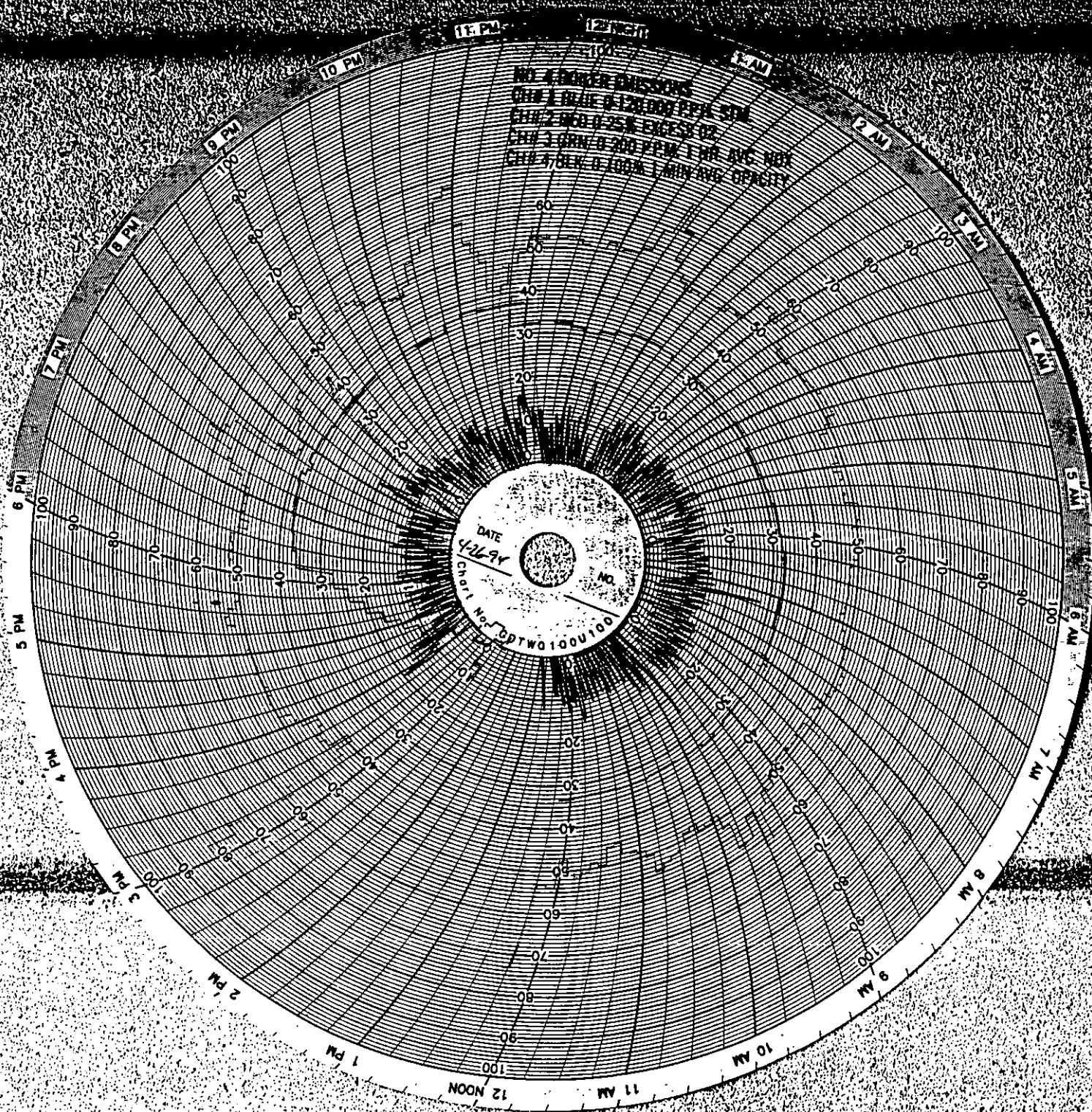
	%. F.S.	
	Low	High
O ₂	12.4	84.0
Opacity	0.0	42.8



Boiler 4

9. F.S.

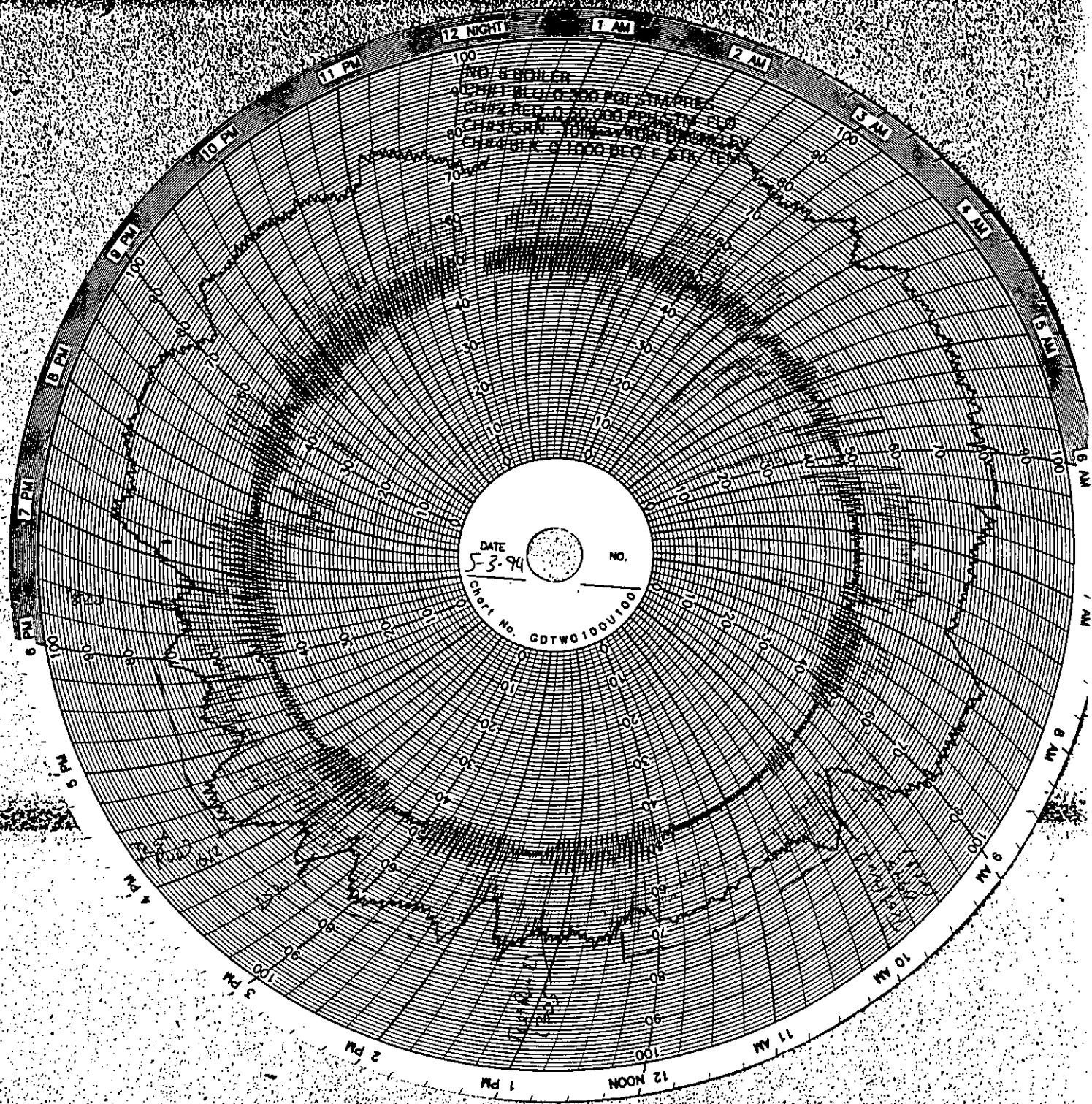
	<u>Low</u>	<u>High</u>
O ₂	12.6	84.0
Opacity	0.0	42.5



Boiler 4

	90 F.S.	
	<u>Low</u>	<u>High</u>
O ₂	12.8	84.8
Opacity	0.0	43.5

Appendix C.3
Plant Process Data



Boiler 5

Steam Flow 5-3-94

S-454 L-P Orville Kk
Boiler #4

Steam Flow Integrator

Fuel: Mixed Tan Oak, Madrone,
Doug. Fir, Pond. Pine,
Some Cedar

Time	Reading 16x10	
1-PM-4 < 1218:15 1424:00	4828277 4844784	$\frac{165070}{125.75 \text{ min}} \Rightarrow 78,761 \text{ lb/hr}$

2-PM-4 < 1545:00 1753:35	4854167 4871244	$\frac{170770}{128.58 \text{ min}} \Rightarrow 79,687 \text{ lb/hr}$
-----------------------------	--------------------	--

5-5-94

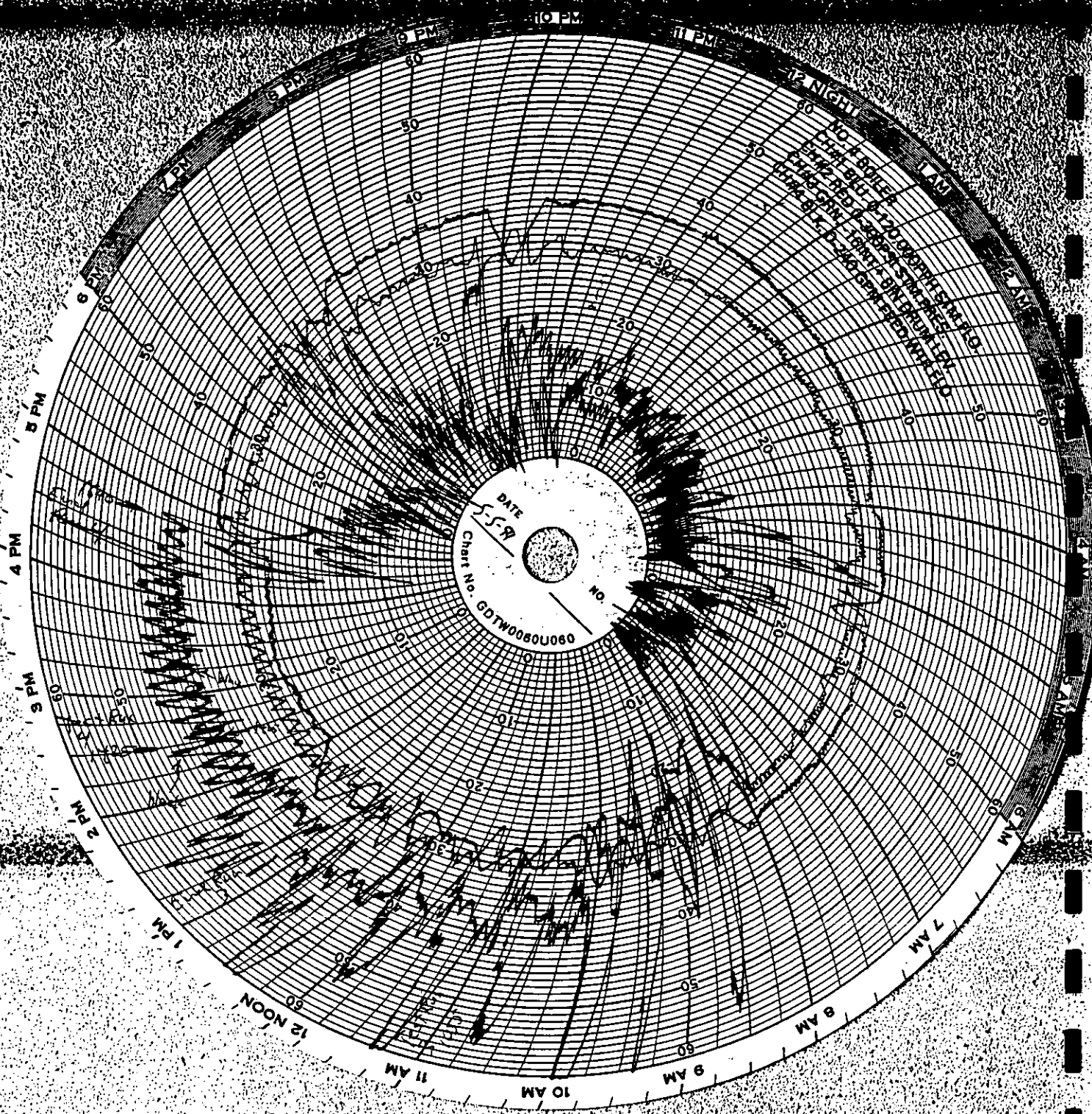
3-PM-4 < 1135:00 1313:30	4918570 4931497	
-----------------------------	--------------------	--

4-PM-4 < 1445:00 1641:30	4943069 4958566	
-----------------------------	--------------------	--

- Tried new "drier"
fuel, couldn't get
combustion in control
- Mixed in the drier fuel
and ran again

$\frac{129270}{98.5 \text{ min}} \Rightarrow 78,743 \text{ lb/hr}$

$\frac{154970}{116.5 \text{ min}} \Rightarrow 79,813 \text{ lb/hr}$



Boiler 4
Steam Flow 5-5-94

Appendix C.4
Carnot Gaseous Emission Data

**CEM System Bias and Linearity
Correction Calculations**

TEST #	1-CEM-5	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/3/94							
LINEARITY							
Analyzer Range:	10	25	500	1000			
High Cal.	8.05	22.30	425.60	722.70			
Low Cal.	4.99	15.10	277.80	453.00			
Analyzer Reads:	5.08	15.00	286.60	455.10			
Anal. Cal. Error	0.9	-0.4	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.05	0.09	-0.60	0.00	< 5%		PASS
Span	5.01	14.91	286.20	444.60	< 5%		PASS
Posttest Bias:							
Zero	0.11	0.00	-0.60	0.00	< 5%		PASS
Span	5.13	14.78	286.80	444.90	< 5%		PASS
Span Value:	4.99	15.10	277.80	453.00			
Zero Drift, %:	0.60	-0.36	0.00	0.00	< 3%		PASS
Span Drift, %:	1.20	-0.52	0.12	0.03	< 3%		PASS
Test Ave.	5.69	13.45	3.06	561.81			
Corrected Ave.	5.61	13.68	3.54	572.23			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	2-CEM-5	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/3/94							
LINEARITY							
Analyzer Range:	10	25	500	1000			
High Cal.	8.05	22.30	425.60	722.70			
Low Cal.	4.99	15.10	277.80	453.00			
Analyzer Reads:	5.08	15.00	286.60	455.10			
Anal. Cal. Error	0.9	-0.4	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.11	0.00	-0.60	0.00	< 5%		PASS
Span	5.13	14.78	286.80	444.90	< 5%		PASS
Posttest Bias:							
Zero	0.19	0.01	-0.60	0.10	< 5%		PASS
Span	5.14	14.85	287.20	445.00	< 5%		PASS
Span Value:	4.99	15.10	277.80	453.00			
Zero Drift, %:	0.80	0.04	0.00	0.01	< 3%		PASS
Span Drift, %:	0.10	0.28	0.08	0.01	< 3%		PASS
Test Ave.	5.49	13.62	2.30	559.70			
Corrected Ave.	5.35	13.88	2.80	569.84			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	3-CEM-5	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/3/94							
LINEARITY							
Analyzer Range:	10	25	500	1000			
High Cal.	8.05	22.30	425.60	722.70			
Low Cal.	4.99	15.10	277.80	453.00			
Analyzer Reads:	5.08	15.00	286.60	455.10			
Anal. Cal. Error	0.9	-0.4	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.19	0.01	-0.60	0.10	< 5%		PASS
Span	5.14	14.85	287.20	445.00	< 5%		PASS
Posttest Bias:							
Zero	0.24	0.00	-0.60	0.20	< 5%		PASS
Span	5.16	14.71	288.10	445.40	< 5%		PASS
Span Value:	4.99	15.10	277.80	453.00			
Zero Drift, %:	0.50	-0.04	0.00	0.01	< 3%		PASS
Span Drift, %:	0.20	-0.56	0.18	0.04	< 3%		PASS
Test Ave.	5.50	13.66	52.50	535.20			
Corrected Ave.	5.34	13.96	51.17	544.61			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	4-CEM-5	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/3/94							
LINEARITY							
Analyzer Range:	10	25	500	1000			
High Cal.	8.05	22.30	425.60	722.70			
Low Cal.	4.99	15.10	277.80	453.00			
Analyzer Reads:	5.08	15.00	286.60	455.10			
Anal. Cal. Error	0.9	-0.4	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.24	0.00	-0.60	0.20	< 5%		PASS
Span	5.16	14.71	288.10	445.40	< 5%		PASS
Posttest Bias:							
Zero	0.16	0.00	-0.60	0.20	< 5%		PASS
Span	5.05	14.75	288.00	443.20	< 5%		PASS
Span Value:	4.99	15.10	277.80	453.00			
Zero Drift, %:	-0.80	0.00	0.00	0.00	< 3%		PASS
Span Drift, %:	-1.10	0.16	-0.02	-0.22	< 3%		PASS
Test Ave.	5.47	13.60	4.75	542.75			
Corrected Ave.	5.36	13.94	5.15	553.42			

CEM System Bias and Linearity
Correction Calculations

TEST #	5-CEM-5	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/3/94							
LINEARITY							
Analyzer Range:	10	25	500	1000			
High Cal.	8.05	22.30	425.60	722.70			
Low Cal.	4.99	15.10	277.80	453.00			
Analyzer Reads:	5.08	15.00	286.60	455.10			
Anal. Cal. Error	0.9	-0.4	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.16	0.00	-0.60	0.20	< 5%		PASS
Span	5.05	14.75	288.00	443.20	< 5%		PASS
Posttest Bias:							
Zero	0.30	0.01	-0.60	0.00	< 5%		PASS
Span	5.13	14.58	286.50	441.20	< 5%		PASS
Span Value:	4.99	15.10	277.80	453.00			
Zero Drift, %:	1.40	0.04	0.00	-0.02	< 3%		PASS
Span Drift, %:	0.80	-0.68	-0.30	-0.20	< 3%		PASS
Test Ave.	5.41	13.41	4.08	536.50			
Corrected Ave.	5.32	13.81	4.52	549.62			

CEM System Bias and Linearity
Correction Calculations

TEST #	6-CEM-5	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/3/94							
LINEARITY							
Analyzer Range:	10	25	500	1000			
High Cal.	8.05	22.30	425.60	722.70			
Low Cal.	4.99	15.10	277.80	453.00			
Analyzer Reads:	5.08	15.00	286.60	455.10			
Anal. Cal. Error	0.9	-0.4	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.30	0.01	-0.60	0.00	< 5%		PASS
Span	5.13	14.58	286.50	441.20	< 5%		PASS
Posttest Bias:							
Zero	0.29	0.02	-0.60	0.20	< 5%		PASS
Span	5.07	14.60	286.40	444.90	< 5%		PASS
Span Value:	4.99	15.10	277.80	453.00			
Zero Drift, %:	-0.10	0.04	0.00	0.02	< 3%		PASS
Span Drift, %:	-0.60	0.08	-0.02	0.37	< 3%		PASS
Test Ave.	5.40	13.52	7.50	543.61			
Corrected Ave.	5.30	13.99	7.84	555.84			

CEM System Bias and Linearity
Correction Calculations

TEST #	7-CEM-5	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/3/94							
LINEARITY							
Analyzer Range:	10	25	500	1000			
High Cal.	8.05	22.30	425.60	722.70			
Low Cal.	4.99	15.10	277.80	453.00			
Analyzer Reads:	5.08	15.00	286.60	455.10			
Anal. Cal. Error	0.9	-0.4	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.29	0.02	-0.60	0.20	< 5%		PASS
Span	5.07	14.60	286.40	444.90	< 5%		PASS
Posttest Bias:							
Zero	0.30	0.01	-0.70	0.60	< 5%		PASS
Span	5.02	14.53	287.40	444.20	< 5%		PASS
Span Value:	4.99	15.10	277.80	453.00			
Zero Drift, %:	0.10	-0.04	-0.02	0.04	< 3%		PASS
Span Drift, %:	-0.50	-0.28	0.20	-0.07	< 3%		PASS
Test Ave.	5.35	13.49	94.70	544.30			
Corrected Ave.	5.31	13.98	92.12	554.74			

CEM System Bias and Linearity
Correction Calculations

TEST #	8-CEM-5	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/3/94							
LINEARITY							
Analyzer Range:	10	25	500	1000			
High Cal.	8.05	22.30	425.60	722.70			
Low Cal.	4.99	15.10	277.80	453.00			
Analyzer Reads:	5.08	15.00	286.60	455.10			
Anal. Cal. Error	0.9	-0.4	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.30	0.01	-0.70	0.60	< 5%		PASS
Span	5.02	14.53	287.40	444.20	< 5%		PASS
Posttest Bias:							
Zero	0.40	0.01	-0.60	0.60	< 5%		PASS
Span	5.07	14.68	289.10	440.60	< 5%		PASS
Span Value:	4.99	15.10	277.80	453.00			
Zero Drift, %:	1.00	0.00	0.02	0.00	< 3%		PASS
Span Drift, %:	0.50	0.60	0.34	-0.36	< 3%		PASS
Test Ave.	5.22	13.63	12.85	521.00			
Corrected Ave.	5.18	14.09	12.98	533.59			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	9-CEM-5	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/3/94							
LINEARITY							
Analyzer Range:	10	25	500	1000			
High Cal.	8.05	22.30	425.60	722.70			
Low Cal.	4.99	15.10	277.80	453.00			
Analyzer Reads:	5.08	15.00	286.60	455.10			
Anal. Cal. Error	0.9	-0.4	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.40	0.01	-0.60	0.60	< 5%		PASS
Span	5.07	14.68	289.10	444.20	< 5%		PASS
Posttest Bias:							
Zero	0.40	0.01	-0.60	0.30	< 5%		PASS
Span	5.14	14.42	288.70	437.10	< 5%		PASS
Span Value:	4.99	15.10	277.80	453.00			
Zero Drift, %:	0.00	0.00	0.00	-0.03	< 3%		PASS
Span Drift, %:	0.70	-1.04	-0.08	-0.71	< 3%		PASS
Test Ave.	5.57	13.27	12.13	538.55			
Corrected Ave.	5.48	13.77	12.22	553.75			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	10-CEM-5	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/3/94							
LINEARITY							
Analyzer Range:	10	25	500	1000			
High Cal.	8.05	22.30	425.60	722.70			
Low Cal.	4.99	15.10	277.80	453.00			
Analyzer Reads:	5.08	15.00	286.60	455.10			
Anal. Cal. Error	0.9	-0.4	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.40	0.01	-0.60	0.30	< 5%		PASS
Span	5.14	14.42	288.70	437.10	< 5%		PASS
Posttest Bias:							
Zero	0.36	0.00	0.00	0.30	< 5%		PASS
Span	4.94	14.44	290.30	437.10	< 5%		PASS
Span Value:	4.99	15.10	277.80	453.00			
Zero Drift, %:	-0.40	-0.04	0.12	0.00	< 3%		PASS
Span Drift, %:	-2.00	0.08	0.32	0.00	< 3%		PASS
Test Ave.	5.52	13.18	104.53	515.47			
Corrected Ave.	5.50	13.79	100.49	534.28			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	1-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/4/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.29	15.04	287.00	85.20			
Anal. Cal. Error	3.0	-0.2	1.8	0.3	< 2%		FAIL
SYSTEM BIAS							
Pretest Bias:							
Zero	0.14	-0.11	-0.60	0.10	< 5%		PASS
Span	5.28	14.87	288.00	84.00	< 5%		PASS
Posttest Bias:							
Zero	0.29	-0.01	0.00	0.20	< 5%		PASS
Span	5.07	14.81	288.00	83.30	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	1.50	0.40	0.12	0.04	< 3%		PASS
Span Drift, %:	-2.10	-0.24	0.00	-0.28	< 3%		PASS
Test Ave.	5.57	14.64	29.65	106.58			
Corrected Ave.	5.39	14.90	28.86	107.58			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	2-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/4/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.10	14.99	287.00	85.20			
Anal. Cal. Error	1.1	-0.4	1.8	0.3	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.10	-0.01	0.00	0.20	< 5%		PASS
Span	5.08	14.88	288.00	83.30	< 5%		PASS
Posttest Bias:							
Zero	0.03	0.00	0.00	0.00	< 5%		PASS
Span	5.02	14.82	283.00	82.80	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	-0.70	0.04	0.00	-0.08	< 3%		PASS
Span Drift, %:	-0.60	-0.24	-1.00	-0.20	< 3%		PASS
Test Ave.	5.30	14.82	43.58	107.13			
Corrected Ave.	5.24	15.07	42.40	108.90			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	3-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/4/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.10	14.99	287.00	85.20			
Anal. Cal. Error	1.1	-0.4	1.8	0.3	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.03	0.00	0.00	0.00	< 5%		PASS
Span	5.02	14.82	283.00	82.80	< 5%		PASS
Posttest Bias:							
Zero	0.02	0.00	0.00	0.10	< 5%		PASS
Span	4.98	14.83	285.80	82.50	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	-0.10	0.00	0.00	0.04	< 3%		PASS
Span Drift, %:	-0.40	0.04	0.56	-0.12	< 3%		PASS
Test Ave.	5.58	14.40	51.55	104.60			
Corrected Ave.	5.57	14.67	50.35	106.83			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	4-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/4/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.10	14.99	287.00	85.20			
Anal. Cal. Error	1.1	-0.4	1.8	0.3	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.02	0.00	0.00	0.10	< 5%		PASS
Span	4.98	14.83	285.80	82.50	< 5%		PASS
Posttest Bias:							
Zero	0.01	0.00	0.00	0.10	< 5%		PASS
Span	4.90	14.78	285.50	83.10	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	-0.10	0.00	0.00	0.00	< 3%		PASS
Span Drift, %:	-0.80	-0.20	-0.06	0.24	< 3%		PASS
Test Ave.	5.93	13.99	65.98	94.25			
Corrected Ave.	5.99	14.27	64.17	96.09			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	5-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/4/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.10	14.99	287.00	85.20			
Anal. Cal. Error	1.1	-0.4	1.8	0.3	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.01	0.00	0.00	0.10	< 5%		PASS
Span	4.90	14.78	285.50	83.10	< 5%		PASS
Posttest Bias:							
Zero	0.01	-0.01	-0.10	0.20	< 5%		PASS
Span	4.88	14.80	285.30	83.30	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	0.00	-0.04	-0.02	0.04	< 3%		PASS
Span Drift, %:	-0.20	0.08	-0.04	0.08	< 3%		PASS
Test Ave.	6.04	13.85	35.39	103.88			
Corrected Ave.	6.17	14.14	34.49	105.42			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	6-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/5/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.07	14.98	287.00	85.10			
Anal. Cal. Error	0.8	-0.5	1.8	0.3	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.02	0.00	0.00	0.25	< 5%		PASS
Span	4.98	14.76	284.60	82.00	< 5%		PASS
Posttest Bias:							
Zero	0.01	0.00	1.00	0.00	< 5%		PASS
Span	4.99	14.82	286.00	82.70	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	-0.10	0.00	0.20	-0.10	< 3%		PASS
Span Drift, %:	0.10	0.24	0.28	0.28	< 3%		PASS
Test Ave.	6.23	13.78	10.33	86.72			
Corrected Ave.	6.24	14.07	9.59	88.89			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	7-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/5/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.07	14.98	287.00	85.10			
Anal. Cal. Error	0.8	-0.5	1.8	0.3	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.01	0.00	1.00	0.00	< 5%		PASS
Span	4.99	14.82	286.00	82.70	< 5%		PASS
Posttest Bias:							
Zero	0.02	0.00	1.00	0.20	< 5%		PASS
Span	4.96	14.71	287.00	82.60	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	0.10	0.00	0.00	0.08	< 3%		PASS
Span Drift, %:	-0.30	-0.44	0.20	-0.04	< 3%		PASS
Test Ave.	7.34	12.61	26.70	105.48			
Corrected Ave.	7.37	12.90	25.01	107.74			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	8-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/5/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.07	14.98	287.00	85.10			
Anal. Cal. Error	0.8	-0.5	1.8	0.3	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.02	0.00	1.00	0.00	< 5%		PASS
Span	4.96	14.71	287.00	82.60	< 5%		PASS
Posttest Bias:							
Zero	0.02	0.00	0.00	0.20	< 5%		PASS
Span	4.98	14.73	286.60	83.10	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	0.00	0.00	-0.20	0.08	< 3%		PASS
Span Drift, %:	0.20	0.08	-0.08	0.20	< 3%		PASS
Test Ave.	5.85	14.03	60.97	105.55			
Corrected Ave.	5.88	14.39	58.67	107.55			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	9-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/5/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.07	14.98	287.00	85.10			
Anal. Cal. Error	0.8	-0.5	1.8	0.3	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.02	0.00	0.00	0.20	< 5%		PASS
Span	4.98	14.73	286.60	83.10	< 5%		PASS
Posttest Bias:							
Zero	0.02	0.00	0.50	0.00	< 5%		PASS
Span	4.98	14.70	287.50	83.60	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	0.00	0.00	0.10	-0.08	< 3%		PASS
Span Drift, %:	0.00	-0.12	0.18	0.20	< 3%		PASS
Test Ave.	4.63	15.11	269.12	78.07			
Corrected Ave.	4.64	15.51	260.43	79.05			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	10-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/5/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.08	14.98	286.60	85.00			
Anal. Cal. Error	0.9	-0.5	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.02	0.00	0.50	0.00	< 5%		PASS
Span	5.02	14.82	288.50	82.60	< 5%		PASS
Posttest Bias:							
Zero	0.00	0.00	0.50	0.20	< 5%		PASS
Span	5.03	14.80	288.60	83.10	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	-0.20	0.00	0.00	0.08	< 3%		PASS
Span Drift, %:	0.10	-0.08	0.02	0.20	< 3%		PASS
Test Ave.	5.60	14.42	26.31	97.49			
Corrected Ave.	5.56	14.70	24.89	99.33			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	11-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/5/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.08	14.98	286.60	85.00			
Anal. Cal. Error	0.9	-0.5	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.00	0.00	0.50	0.20	< 5%		PASS
Span	5.03	14.80	288.60	83.10	< 5%		PASS
Posttest Bias:							
Zero	0.01	0.00	0.50	0.20	< 5%		PASS
Span	5.02	14.74	287.60	82.80	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	0.10	0.00	0.00	0.00	< 3%		PASS
Span Drift, %:	-0.10	-0.24	-0.20	-0.12	< 3%		PASS
Test Ave.	5.72	14.20	23.97	100.67			
Corrected Ave.	5.68	14.52	22.67	102.47			

**CEM System Bias and Linearity
Correction Calculations**

TEST #	12-CEM-4	O2	CO2	CO	NOx	Criteria	Status
L.P. Oroville							
Date: 5/5/94							
LINEARITY							
Analyzer Range:	10	25	500	250			
High Cal.	8.05	22.30	425.60	241.20			
Low Cal.	4.99	15.10	277.80	84.40			
Analyzer Reads:	5.08	14.98	286.60	85.00			
Anal. Cal. Error	0.9	-0.5	1.8	0.2	< 2%		PASS
SYSTEM BIAS							
Pretest Bias:							
Zero	0.01	0.00	0.50	0.20	< 5%		PASS
Span	5.02	14.74	287.60	82.80	< 5%		PASS
Posttest Bias:							
Zero	0.00	0.01	0.50	0.20	< 5%		PASS
Span	5.02	14.79	289.50	83.40	< 5%		PASS
Span Value:	4.99	15.10	277.80	84.40			
Zero Drift, %:	-0.10	0.04	0.00	0.00	< 3%		PASS
Span Drift, %:	0.00	0.20	0.38	0.24	< 3%		PASS
Test Ave.	5.99	14.02	24.68	102.28			
Corrected Ave.	5.96	14.34	23.32	103.93			

CARNOT CEM PERFORMANCE DATA

CLIENT/LOCATION: L-P Oroville Boiler 4 DATE: 5-4-84
30187 BY: KJC

SYSTEM CONFIGURATION				
ANALYZERS IN SERVICE				
		ANALYZERS: <u>O₂, CO₂, CO, NO_x</u>		
PROBE				
		LENGTH: <u>6 ft.</u>		
		LINER MATERIAL: <u>stainless steel</u>		
		HEATED PROBE (Y/N): <u>Y</u>		
		HEATED LINE (Y/N): <u>Y</u>		
ON-STACK CONDITIONER				
		IN SERVICE (Y/N): <u>Y</u>		
		COOLANT: <u>ice/water</u>		
SAMPLE LINE				
		LENGTH: <u>100 ft.</u>		
		MATERIAL: <u>Teflon 3/8" o.d.</u>		
SYSTEM LEAK CHECK				
PRE-/POST-TEST				
		PRE-TEST (cfh): <u>40.1 @ 25 in. Hg vac.</u>		
		POST-TEST (cfh): <u>11 11 11 11 11</u>		
LEAK RATE (%) = $\frac{\text{POST-TEST (cfh)}}{\text{SYSTEM FLOW RATE (cfm)} \times 60} \times 100 = \underline{40.1} \%$				
SYSTEM RESPONSE TIME CHECK				
	1	2	3	Avg.
UPSCALE:	<u>30</u> sec.	<u>32</u> sec.	<u>32</u> sec.	<u>32</u> sec.
DOWNSCALE:	<u>34</u> sec.	<u>36</u> sec.	<u>36</u> sec.	<u>36</u> sec.

CARNOT CEM PERFORMANCE DATA

CLIENT/LOCATION: L-P Oroville Boiler 5 DATE: 5-3-94
30187 BY: KJ Gushy

SYSTEM CONFIGURATION				
ANALYZERS IN SERVICE				
		ANALYZERS: <u>O₂, CO₂, CO, NO_x</u>		
PROBE				
		LENGTH: <u>6 ft.</u>		
		LINER MATERIAL: <u>stainless steel</u>		
		HEATED PROBE (Y/N): <u>Y</u>		
		HEATED LINE (Y/N): <u>Y</u>		
ON-STACK CONDITIONER				
		IN SERVICE (Y/N): <u>Y</u>		
		COOLANT: <u>ice/water</u>		
SAMPLE LINE				
		LENGTH: <u>100 ft.</u>		
		MATERIAL: <u>Teflon 3/8" o.d.</u>		
SYSTEM LEAK CHECK				
PRE-POST-TEST				
		PRE-TEST (cfh): <u>40.1 @ 25 in. Hg vac</u>		
		POST-TEST (cfh): <u>11 11 11 11 11</u>		
LEAK RATE (%) = $\frac{\text{POST-TEST (cfh)}}{\text{SYSTEM FLOW RATE (cfm)} \times 60} \times 100 = \underline{40.1} \%$				
SYSTEM RESPONSE TIME CHECK				
	1	2	3	Avg.
UPSCALE:	<u>32</u> sec.	<u>30</u> sec.	<u>30</u> sec.	<u>30</u> sec.
DOWNSCALE:	<u>36</u> sec.	<u>35</u> sec.	<u>35</u> sec.	<u>35</u> sec.

CARNOT CEM PERFORMANCE DATA

CLIENT/LOCATION: L-Poroville 30187 DATE: 5-5-94
Boiler 5 BY: HJC

SYSTEM CONFIGURATION				
ANALYZERS IN SERVICE				
		ANALYZERS: <u>O₂, CO₂, CO, NO_x</u>		
PROBE				
		LENGTH: <u>6 ft.</u>		
		LINER MATERIAL: <u>Stainless steel</u>		
		HEATED PROBE (Y/N): <u>Y</u>		
		HEATED LINE (Y/N): <u>Y</u>		
ON-STACK CONDITIONER				
		IN SERVICE (Y/N): <u>Y</u>		
		COOLANT: <u>ice/water</u>		
SAMPLE LINE				
		LENGTH: <u>100 ft.</u>		
		MATERIAL: <u>Teflon 3/8" O.D.</u>		
SYSTEM LEAK CHECK				
PRE-POST-TEST				
		PRE-TEST (cfh): <u><0.1 @ 25 in. Hg vac.</u>		
		POST-TEST (cfh): <u>11 100 100 100</u>		
LEAK RATE (%) = $\frac{\text{POST-TEST (cfh)}}{\text{SYSTEM FLOW RATE (cfm)} \times 60} \times 100 = \underline{<0.1} \% $				
SYSTEM RESPONSE TIME CHECK				
	1	2	3	Avg.
UPSCALE:	<u>33</u> sec.	<u>30</u> sec.	<u>32</u> sec.	<u>32</u> sec.
DOWNSCALE:	<u>36</u> sec.	<u>35</u> sec.	<u>35</u> sec.	<u>35</u> sec.

CARNOT

PAGE ____ OF ____

REFERENCE METHOD GASEOUS MEASUREMENTS

CLIENT/LOCATION: CP OronvilleCONDITION: 30,000 lb/hr steamDATE: 5/3/94OPERATOR: EM/KCTEST NUMBER: 1-CEM-5TEST LOCATION: Boiler 5

TEST NO.	TIME		SAMPLE POINT/ CONDITION	DRY, UNCORRECTED						CORRECTED TO 12% CO ₂ DRY		
				O ₂	CO ₂	CO	NOx	NO	NO ₂	SO ₂	NOx	SO ₂
SPAN GAS CONCENTRATION				4.99	15.1	277.8	453.0					
			AS FOUND ANAL SPAN	5.08	15.05	286.6	455.1					
			SYSTEM ZERO	0.05	0.09	-0.6	0.0					
			SYSTEM SPAN	5.01	14.91	286.2	444.6					
										corrected 5.61	1368	572.23
1	BEGIN	0945	1-CEM-5	5.69	13.45	3.06	561.81					
	END	1025										
	BEGIN	---	Sys. Zero	0.11	0.0	-0.6	0.0					
	END	---										
	BEGIN	---	Sys. Span	5.13	14.78	286.8	444.9					
	END	---										
2	BEGIN	1100	1-CEM-5	5.61	13.68	3.78	572.23					
	END	1130										
	BEGIN	---	Sys. Zero	0.19	0.01	-0.6	0.1					
	END	---										
	BEGIN	---	Sys. Span	5.14	14.85	287.2	445.0					
	END	---										
	BEGIN	1145	2-CEM-5	5.35	13.88	2.80	569.84					
	END	1215										
	BEGIN	---	Sys. Zero	0.24	0.0	-0.6	0.2					
	END	---										
	BEGIN	---	Sys. Span	5.16	14.71	288.1	445.4					
	END	---										
	BEGIN	1145	3-CEM-5	5.34	13.96	51.17	544.61					
	END	1215										
	BEGIN	---	Sys. Zero									
	END	---										
	BEGIN	---	Sys. Span									
	END	---										
RAW AVERAGE												
CORRECTED AVERAGE												
COMMENTS:												

CARNOT

493.5
95.3
17415
17
1.95105
11.9

CARNOT

PAGE ____ OF ____

REFERENCE METHOD GASEOUS MEASUREMENTS

CLIENT/LOCATION: L-P OrouvilleCONDITION: 30,000 lb/hr steamDATE: 5-3-94OPERATOR: KJC /JP

TEST NUMBER: _____

TEST LOCATION: Boiler #5

TEST NO.	TIME		SAMPLE POINT/ CONDITION	DRY, UNCORRECTED						CORRECTED TO % DRY		
				O ₂	CO ₂	CO	NOx	NO	NO ₂	SO ₂	CO	NOx
SPAN GAS CONCENTRATION												
			AS FOUND ANAL SPAN									
			SYSTEM ZERO	0.24	0.0	-0.6	0.2					
			SYSTEM SPAN	5.16	14.71	288.1	445.4					
	BEGIN	1240	4-CEN-5	5.47	13.60	4.75	542.75					
	END	1310										
	BEGIN	---	Sys. Zero	0.16	0.0	-0.6	0.2					
	BEGIN	---	Sys. Span	5.05	14.75	288.0	443.2					
	BEGIN	1325	5-CEN-5	5.41	13.41	4.08	536.5					
	END	1405										
	BEGIN	---	Sys. Zero	0.3	0.01	-0.6	0.0					
	BEGIN	---	Sys. Span	5.13	14.58	286.5	441.2					
	BEGIN	1420	6-CEN-5	5.40	13.52	7.5	543.61					
	END	1450										
	BEGIN	---	Sys. Zero	0.29	0.02	7.6	0.2					
	BEGIN	---	Sys. Span	5.07	14.6	286.4	444.9					
	BEGIN	1510	7-CEN-5	5.35	13.49	94.7	544.3					
	END	1540										
	BEGIN	---	Sys. Zero	0.30	0.01	-0.7	0.6					
	BEGIN	---	Sys. Span	5.02	14.53	287.4	444.2					
			SYSTEM ZERO									
			SYSTEM SPAN									
RAW AVERAGE												
CORRECTED AVERAGE												
COMMENTS:												

CARNOT

PAGE ____ OF ____

REFERENCE METHOD GASEOUS MEASUREMENTS

CLIENT/LOCATION: L-P OronvilleCONDITION: 30,000 lb/hr steamDATE: 5-3-94OPERATOR: Kjc

TEST NUMBER: _____

TEST LOCATION: Boiler #5

TEST NO.	TIME	SAMPLE POINT/ CONDITION	DRY, UNCORRECTED						CORRECTED TO _____%____, DRY			
			O ₂	CO ₂	CO	NOx	NO	NO ₂	SO ₂	CO	NOx	SO ₂
SPAN GAS CONCENTRATION												
		AS FOUND ANAL SPAN										
		SYSTEM ZERO	0.30	0.01	-0.7	0.6						
		SYSTEM SPAN	5.02	14.53	287.4	444.2						
	BEGIN END	8-CEM-5	5.22	13.63	12.85	521.0						
	BEGIN END	Sys. Zero	0.40	0.01	-0.6	0.6						
	BEGIN END	Sys. Span	5.07	14.68	289.1	440.6						
	BEGIN END	9-CEM-5	5.57	13.27	12.13	538.55						
	BEGIN END	Sys Zero	0.40	0.01	-0.6	0.3						
	BEGIN END	Sys Span	5.14	14.42	288.7	437.1						
	BEGIN END	10-CEM-5	5.52	13.18	104.53	515.47						
	BEGIN END	Sys. Zero	0.36	0.0	0.0	0.3						
	BEGIN END	Sys. Span	4.94	14.44	290.3	437.1						
	BEGIN END	H ₂ Span	7.52	21.46	429.9	690.4						
	BEGIN END											
	BEGIN END											
		SYSTEM ZERO										
		SYSTEM SPAN										
RAW AVERAGE												
CORRECTED AVERAGE												
COMMENTS:												

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CARNOT

PAGE ____ OF ____

REFERENCE METHOD GASEOUS MEASUREMENTS

CLIENT/LOCATION: L-P DravilleCONDITION: Full LoadDATE: 5-4-94OPERATOR: KYC

TEST NUMBER: _____

TEST LOCATION: Boiler 4

TEST NO.	TIME		SAMPLE POINT/ CONDITION	DRY, UNCORRECTED						CORRECTED TO % DRY		
				O ₂	CO ₂	CO	NOx	NO	NO ₂	SO ₂	CO	NOx
SPAN GAS CONCENTRATION												
			AS FOUND ANAL SPAN									
			SYSTEM ZERO	0.14	-0.11	-0.6	0.1					
			SYSTEM SPAN	5.28	14.87	288.0	84.0					
	BEGIN	1220	1-CEM-4	5.57*	14.64	29.65	106.58					
	END	1250										
	BEGIN	---	Sys. Zero	0.29	-0.01	0.0	0.2					
	END	---										
	BEGIN	---	Sys. Span	5.07	14.81	288.0	83.3					
	END	---										
	BEGIN	Reset	2-CEM-4	5.10	-0.01	0.0	0.0					
	END	0.2+CO ₂										
	BEGIN	---	Sys. Span	5.08	14.88							
	END	---										
	BEGIN	1320	2-CEM-4	5.30	14.82	43.58	107.13					
	END	1350										
	BEGIN	---	Sys. Zero	0.03	0.0	0.0	0.0					
	END	---										
	BEGIN	---	Sys. Span	5.02	14.82	288.0	82.8					
	END	---										
	BEGIN	1545	3-CEM-4	5.58	14.40	51.55	104.6					
	END	1625										
	BEGIN	---	Sys. Zero	0.02	0.0	0.0	0.1					
	END	---										
	BEGIN	---	Sys. Span	4.98	14.83	285.8	82.5					
	END	---										
			SYSTEM ZERO									
			SYSTEM SPAN									
RAW AVERAGE												
CORRECTED AVERAGE												
COMMENTS:												

REFERENCE METHOD GASEOUS MEASUREMENTS

CLIENT/LOCATION: L-P DravilleCONDITION: Full LoadDATE: 5-4-94OPERATOR: Kyc

TEST NUMBER: _____

TEST LOCATION: Boiler 4

TEST NO.	TIME	SAMPLE POINT/ CONDITION	DRY, UNCORRECTED						CORRECTED TO ____%____ DRY			
			O ₂	CO ₂	CO	NOx	NO	NO ₂	SO ₂	CO	NOx	SO ₂
SPAN GAS CONCENTRATION												
		AS FOUND ANAL SPAN										
		SYSTEM ZERO	0.02	0.0	0.0	0.1						
		SYSTEM SPAN	4.98 4.98	14.83	285.8 285.8	82.5 82.5						
	BEGIN END	1635 1705 4-CEM-4	5.93	13.99	65.98	94.25 94.25						
	BEGIN END	----- Sys. Zero	0.01	0.0	0.0	0.1						
	BEGIN END	----- Sys. Span	4.90	14.78	285.5	83.1						
	BEGIN END	1710 1800 5-CEM-4	6.04	13.85	35.39	103.84						
	BEGIN END	----- Sys. Zero	0.01	0.01	0.1	0.2						
	BEGIN END	----- Sys. Span	4.88	14.80	285.3	83.3						
	BEGIN END	-----										
	BEGIN END	-----										
	BEGIN END	-----										
	BEGIN END	-----										
	BEGIN END	-----										
	BEGIN END	-----										
	BEGIN END	-----										
		SYSTEM ZERO										
		SYSTEM SPAN										
RAW AVERAGE												
CORRECTED AVERAGE												
COMMENTS:												

CARNOT CONTINUOUS EMISSIONS MEASUREMENTS

CLIENT: L-P Driville
 DATE: 5-5-94
 OPERATOR: KLC
 TEST LOCATION: Boiler 4
 TEST NUMBERS: _____

AMBIENT TEMP., DB/WB: _____
 BAROMETRIC PRESSURE: _____
 DUCT STATIC PRESSURE: _____
 FUEL: _____

TEST NO.	SAMPLE TIME	SAMPLE POINT/ CONDITION	DRY, UNCORRECTED							CORRECTED TO ____%____ DRY		
			O ₂	CO ₂	CO	NOx	NO	NO ₂	SO ₂	CO	NOx	SO ₂
		As-found	4.95	15.1	277.8	84.4						
		Anal. Span	5.04	15.03	286.1	85.3						
		System Zero	0.02	0.0	0.0	0.0						
		System Span	5.00	14.81	285.6	82.0						
	908-938	6-CEM-4	6.23	13.78	10.33	86.72						
		Sys. Zero	0.01	0.0	1.0	0.0						
		Sys. Span	4.99	14.82	286.0	82.7						
	1013-1043	7-CEM-4	7.34	12.61	26.70	105.48						
		Sys. Zero	0.02	0.0	1.0	0.2						
		Sys. Span	4.96	14.71	287.0	82.6						
	1108-1138	8-CEM-4	5.85	14.03	60.97	105.55						
		Sys. Zero	0.02	0.0	0.0	0.2						
		Sys. Span	4.98	14.73	286.6	83.1						
	1208-1238	9-CEM-4	4.63	15.11	269.0	78.07						
COMMENTS:			zero	0.02	0.0	0.5	0.0					
			span	4.98	14.7	287.5	83.6					

CARNOT CONTINUOUS EMISSIONS MEASUREMENTS

CLIENT: L-P Draville
 DATE: 5-5-94
 OPERATOR: KJC
 TEST LOCATION: Boiler 4
 TEST NUMBERS: 10-12-CEM-4

AMBIENT TEMP., DB/WB: _____
 BAROMETRIC PRESSURE: _____
 DUCT STATIC PRESSURE: _____
 FUEL: _____

TEST NO.	SAMPLE TIME	SAMPLE POINT/ CONDITION	DRY, UNCORRECTED							CORRECTED TO _____%____, DRY		
			O ₂	CO ₂	CO	NOx	NO	NO ₂	SO ₂	CO	NOx	SO ₂
	1430	As-found	4.99	15.1	277.8	84.4						
		Anal. Span	5.09	14.98	288.6	85.0						
		System Zero	0.00	0.0	0.5	0.0						
	1435	System Span	5.02	14.82	288.5	82.6						
	1443 -1523	10-CEM-4	5.60	14.42	26.31	97.49						
		System Zero	0.0	0.0	0.5	0.2						
		System Span	5.03	14.80	288.6	83.1						
	1538 -1608	11-CEM-4	5.72	14.20	23.77	100.67						
		System Zero	0.01	0.0	0.5	0.2						
		System Span	5.02	14.74	287.6	82.8						
	1618 -1638	12-CEM-4	5.99	14.02	24.68	102.08						
		System Zero	0.0	0.01	0.5	0.2						
		System Span	5.02	14.79	289.5	83.4						

COMMENTS:

Appendix C.5
Stack Gas Moisture Content Data

MOISTURE CORRECTION CALCULATIONS

Carnot Relative Accuracy Data

Client: L-P Oroville
Unit: Boiler 5
Date: May 3, 1994

Time	Raw Data, Dry			Raw Data, Wet		Moisture H2O, %	NOx Dry ppm @ 12% CO2
	NOx ppm	O2 %	CO2 %	NOx ppm	O2 %		
0945-1025	572.23	5.61	13.68	504.13	4.94	11.9	501.96
1100-1130	569.84	5.35	13.88	502.03	4.71	11.9	492.66
1145-1215	544.61	5.34	13.96	479.80	4.70	11.9	468.15
1240-1310	553.42	5.36	13.94	487.56	4.72	11.9	476.40
1325-1405	549.62	5.32	13.81	484.22	4.69	11.9	477.58
1420-1450	555.84	5.30	13.99	489.70	4.67	11.9	476.77
1510-1540	554.74	5.31	13.98	488.73	4.68	11.9	476.17
1605-1645	533.59	5.18	14.09	466.89	4.53	12.5	454.44
1700-1730	553.75	5.48	13.77	484.53	4.80	12.5	482.57
1750-1821	534.28	5.5	13.79	467.50	4.81	12.5	464.93

MOISTURE CORRECTION CALCULATIONS

Carnot Relative Accuracy Data

Client: L-P Oroville
Unit: Boiler 4
Date: May 4-5, 1994

Time	Raw Data, Dry			Raw Data, Wet		Moisture H2O, %	NOx Dry ppm @ 12% CO2
	NOx ppm	O2 %	CO2 %	NOx ppm	O2 %		
1220-1250	107.6	5.39	14.90	84.56	4.24	21.4	86.64
1320-1350	108.9	5.24	15.07	85.60	4.12	21.4	86.72
1545-1625	106.8	5.57	14.67	84.72	4.42	20.7	87.39
1635-1705	96.09	5.99	14.27	76.20	4.75	20.7	80.80
1720-1800	105.4	6.17	14.14	83.60	4.89	20.7	89.47
0908-0938	88.89	6.24	14.07	67.56	4.74	24.0	75.81
1013-1043	107.7	7.37	12.90	81.88	5.60	24.0	100.2
1108-1138	107.6	5.88	14.39	81.74	4.47	24.0	89.69
1208-1238	79.05	4.64	15.51	60.08	3.53	24.0	61.16
1443-1523	99.33	5.56	14.70	75.99	4.25	23.5	81.09
1538-1608	102.5	5.68	14.52	78.39	4.35	23.5	84.69
1618-1638	103.93	5.96	14.34	79.51	4.56	23.5	86.97

SOURCE TEST DATA SUMMARY

Client/Location.....	LP. Orov	*	Date.....	4-3-94
		*		
Test Number.....	1-PM-5	•	Data By.....	EMM
		•		
Test Method.....	CARB 5	*	Sample Location.....	Stack
		*		
Fuel.....	Sndr Dust	•	Unit.....	Boiler 5
		•		
Sample Train.....	ES-11	•	Start/Stop Time.....	0940-1200

Pitot Factor	0.84	*	Reference Temp (F)...	60
		*		
Stack Area (sq ft)...	9.51	*	Meter Cal Factor....	1.0120
		*		
Bar Press (in Hg)...	29.92	*	Sample Time (Min)...	120
		•		
Meter Vol (acf).....	55.475	*	Nozzle Diam (in)....	0.317
		*		
Stack Press (iwg)...	-0.06	•	Meter Temp (F).....	95.50
		*		
Vel Head (iwg).....	0.141	*	Stack Temp (F).....	490.10
		*		
Liquid Vol (ml).....	152.8	*	Stack O2 (%).....	5.60
		*		
Meter Press (iwg)...	0.88	•	Stack CO2 (%).....	13.55

Std Sample Vol (SCF).....	52.63
Moisture Fraction.....	0.119
Stack Gas Mol Wt.....	28.92
Stack Gas Velocity (ft/sec).....	28.21
Stack Flow Rate (wacfm).....	16089
Stack Flow Rate (dscfm).....	7756
Isokinetic Ratio (%).....	98.06

Particulate Catch, mg.....	
Grain Loading, gr/dscf.....	0.0000
Grain Loading @ 12% CO2.....	0.0000
Mass Emissions, lb/hr.....	0.00

SOURCE TEST DATA SUMMARY

Client/Location.....	LP. Orov	•	Date.....	4-3-94
Test Number.....	2-PM-5	•	Data By.....	EMM
Test Method.....	CARB 5	•	Sample Location.....	Stack
Fuel.....	Sndr Dust	*	Unit.....	Boiler 5
Sample Train.....	ES-11	*	Start/Stop Time.....	1305-1510

Pitot Factor	0.84	*	Reference Temp (F)...	60
Stack Area (sq ft)...	9.51	*	Meter Cal Factor....	1.0120
Bar Press (in Hg)...	29.90	*	Sample Time (Min)...	120
Meter Vol (acf).....	82.270	*	Nozzle Diam (in)....	0.371
Stack Press (iwg)...	-0.10	*	Meter Temp (F).....	96.80
Vel Head (iwg).....	0.170	*	Stack Temp (F).....	500.00
Liquid Vol (ml).....	226.8	*	Stack O2 (%).....	5.41
Meter Press (iwg)...	1.93	*	Stack CO2 (%).....	13.47

Std Sample Vol (SCF).....	78.02
Moisture Fraction.....	0.119
Stack Gas Mol Wt.....	28.90
Stack Gas Velocity (ft/sec).....	31.14
Stack Flow Rate (wacfm).....	17761
Stack Flow Rate (dscfm).....	8466
Isokinetic Ratio (%).....	97.22

Particulate Catch, mg.....	
Grain Loading, gr/dscf.....	0.0000
Grain Loading @ 12% CO2.....	0.0000
Mass Emissions, lb/hr.....	0.00

SOURCE TEST DATA SUMMARY

Client/Location.....	LP. Orov	*	Date.....	4-3-94
		*		
Test Number.....	3-PM-5	*	Data By.....	EMM
		*		
Test Method.....	CARB 5	*	Sample Location.....	Stack
		*		
Fuel.....	Sndr Dust	*	Unit.....	Boiler 5
		*		
Sample Train.....	ES-11	*	Start/Stop Time.....	1610-1820

Pitot Factor	0.84	*	Reference Temp (F)...	60
		*		
Stack Area (sq ft)...	9.51	*	Meter Cal Factor....	1.0120
		*		
Bar Press (in Hg)...	29.90	*	Sample Time (Min)...	120
		*		
Meter Vol (acf).....	83.566	*	Nozzle Diam (in)....	0.371
		*		
Stack Press (iwg)...	-0.11	*	Meter Temp (F).....	90.75
		*		
Vel Head (iwg).....	0.168	*	Stack Temp (F).....	519.80
		*		
Liquid Vol (ml).....	245.6	*	Stack O2 (%).....	5.42
		*		
Meter Press (iwg)...	1.94	*	Stack CO2 (%).....	13.38

Std Sample Vol (SCF).....	80.12
Moisture Fraction.....	0.125
Stack Gas Mol Wt.....	28.82
Stack Gas Velocity (ft/sec).....	31.34
Stack Flow Rate (wacfm).....	17879
Stack Flow Rate (dscfm).....	8296
Isokinetic Ratio (%).....	101.89

Particulate Catch, mg.....	
Grain Loading, gr/dscf.....	0.0000
Grain Loading @ 12% CO2.....	0.0000
Mass Emissions, lb/hr.....	0.00

SOURCE TEST DATA SUMMARY

Client/Location.....	LP. Orov	•	Date.....	5-4-94
Test Number.....	1-PM-4	*	Data By.....	EMM
Test Method.....	CARB 5	•	Sample Location.....	Stack
Fuel.....	Hog	*	Unit.....	Boiler 4
Sample Train.....	ES-11	•	Start/Stop Time.....	1215-1420

Pitot Factor	0.84	•	Reference Temp (F)...	60
Stack Area (sq ft)...	20.97	*	Meter Cal Factor....	1.0120
Bar Press (in Hg)...	29.80	*	Sample Time (Min)...	120
Meter Vol (acf).....	82.468	•	Nozzle Diam (in)....	0.290
Stack Press (iwg)...	-0.22	*	Meter Temp (F).....	106.20
Vel Head (iwg).....	0.365	*	Stack Temp (F).....	368.60
Liquid Vol (ml).....	447.7	•	Stack O2 (%).....	5.47
Meter Press (iwg)...	1.68	•	Stack CO2 (%).....	14.68

Std Sample Vol (SCF).....	76.60
Moisture Fraction.....	0.214
Stack Gas Mol Wt.....	27.88
Stack Gas Velocity (ft/sec).....	43.25
Stack Flow Rate (wacfm).....	54410
Stack Flow Rate (dscfm).....	26723
Isokinetic Ratio (%).....	109.15

Particulate Catch, mg.....	50.00
Grain Loading, gr/dscf.....	0.0101
Grain Loading @ 12% CO2.....	0.0082
Mass Emissions, lb/hr.....	2.31

SOURCE TEST DATA SUMMARY

Client/Location.....	LP. Orov	*	Date.....	5-4-94
		*		
Test Number.....	2-PM-4	*	Data By.....	EMM
		*		
Test Method.....	CARB 5	*	Sample Location.....	Stack
		*		
Fuel.....	Hog	*	Unit.....	Boiler 4
		*		
Sample Train.....	ES-11	*	Start/Stop Time.....	1640-1845

Pitot Factor	0.84	*	Reference Temp (F)...	60
		*		
Stack Area (sq ft)...	20.97	*	Meter Cal Factor....	1.0120
		*		
Bar Press (in Hg)...	29.71	*	Sample Time (Min)...	120
		*		
Meter Vol (acf).....	78.630	*	Nozzle Diam (in)....	0.285
		*		
Stack Press (iwg)...	-0.21	*	Meter Temp (F).....	104.60
		*		
Vel Head (iwg).....	0.387	*	Stack Temp (F).....	349.20
		*		
Liquid Vol (ml).....	409.9	*	Stack O2 (%).....	6.45
		*		
Meter Press (iwg)...	1.54	*	Stack CO2 (%).....	13.38

Std Sample Vol (SCF).....	73.00
Moisture Fraction.....	0.207
Stack Gas Mol Wt.....	27.83
Stack Gas Velocity (ft/sec).....	44.11
Stack Flow Rate (wacfm).....	55493
Stack Flow Rate (dscfm).....	28060
Isokinetic Ratio (%).....	102.57

Particulate Catch, mg.....	
Grain Loading, gr/dscf.....	0.0000
Grain Loading @ 12% CO2.....	0.0000
Mass Emissions, lb/hr.....	0.00

SOURCE TEST DATA SUMMARY

Client/Location.....	LP. Orov	•	Date.....	5-5-94
Test Number.....	3-PM-4	•	Data By.....	EMM
Test Method.....	CARB 5	•	Sample Location.....	Stack
Fuel.....	Hog	•	Unit.....	Boiler 4
Sample Train.....	ES-11	•	Start/Stop Time.....	1055-1300

Pitot Factor	0.84	•	Reference Temp (F)...	60
Stack Area (sq ft)...	20.97	•	Meter Cal Factor....	1.0120
Bar Press (in Hg)...	29.70	•	Sample Time (Min)...	120
Meter Vol (acf).....	71.996	•	Nozzle Diam (in)....	0.285
Stack Press (iwg)...	-0.23	•	Meter Temp (F).....	96.42
Vel Head (iwg).....		•	Stack Temp (F).....	
Liquid Vol (ml).....	459.3	•	Stack O2 (%).....	
Meter Press (iwg)...	1.37	•	Stack CO2 (%).....	

Std Sample Vol (SCF).....	67.77
Moisture Fraction.....	<i>Used for moisture only</i> 0.240
Stack Gas Mol Wt.....	25.68
Stack Gas Velocity (ft/sec).....	0.00
Stack Flow Rate (wacfm).....	0
Stack Flow Rate (dscfm).....	0
Isokinetic Ratio (%).....	#DIV/0!

Particulate Catch, mg.....	
Grain Loading, gr/dscf.....	0.0000
Grain Loading @ 12% CO2.....	#DIV/0!
Mass Emissions, lb/hr.....	0.00

SOURCE TEST DATA SUMMARY

Client/Location.....	LP. Orov	*	Date.....	5-5-94
		*		
Test Number.....	4-PM-4	*	Data By.....	EMM
		*		
Test Method.....	CARB 5	*	Sample Location.....	Stack
		*		
Fuel.....	Hog	*	Unit.....	Boiler 4
		*		
Sample Train.....	ES-11	*	Start/Stop Time.....	1425-1627

Pitot Factor	0.84	*	Reference Temp (F)...	60
		*		
Stack Area (sq ft)...	20.97	*	Meter Cal Factor....	1.0120
		*		
Bar Press (in Hg)...	29.68	*	Sample Time (Min)...	120
		*		
Meter Vol (acf).....	75.460	*	Nozzle Diam (in)....	0.285
		*		
Stack Press (iwg)...	-0.20	*	Meter Temp (F).....	108.90
		*		
Vel Head (iwg).....	0.360	*	Stack Temp (F).....	342.50
		*		
Liquid Vol (ml).....	459.3	*	Stack O2 (%).....	5.66
		*		
Meter Press (iwg)...	1.40	*	Stack CO2 (%).....	14.30

Std Sample Vol (SCF).....	69.44
Moisture Fraction.....	0.235
Stack Gas Mol Wt.....	27.57
Stack Gas Velocity (ft/sec).....	42.60
Stack Flow Rate (wacfm).....	53591
Stack Flow Rate (dscfm).....	26328
Isokinetic Ratio (%).....	103.98

Particulate Catch, mg.....	
Grain Loading, gr/dscf.....	0.0000
Grain Loading @ 12% CO2.....	0.0000
Mass Emissions, lb/hr.....	0.00

APPENDIX D
CALCULATIONS

Appendix D.1
General Emissions Calculations

EMISSION CALCULATIONS

1. Sample Volume and Isokinetics

- a. Sample gas volume, dscf

$$V_{m\ std} = 0.03342 V_m \left(P_{bar} + \frac{H}{13.6} \right) \left(\frac{T_{ref}}{T_m} \right) (Y)$$

- b. Water vapor volume, scf

$$V_{w\ std} = 0.0472 V_{lc} \left(\frac{T_{ref}}{528^\circ R} \right)$$

- c. Moisture content, nondimensional

$$B_{wo} = \frac{V_{w\ std}}{V_{m\ std} + V_{w\ std}}$$

- d. Stack gas molecular weight, lb/lb mole

$$MW_{dry} = 0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2)$$

$$MW_{wet} = MW_{dry} (1 - B_{wo}) + 18 (B_{wo})$$

- e. Absolute stack pressure, in Hg

$$P_s = P_{bar} + \frac{P_{sg}}{13.6}$$

- f. Stack velocity, ft/sec

$$V_s = 2.90 C_p \sqrt{\Delta PT_s} \sqrt{\left(\frac{29.92}{P_s} \right) \left(\frac{28.95}{MW_{wet}} \right)}$$

- g. Actual stack flow rate, wacfm

$$Q = (V_s)(A_s)(60)$$

- h. Standard stack gas flow rate, dscfm

$$Q_{std} = Q (1 - B_{wo}) \left(\frac{T_{ref}}{T_s} \right) \left(\frac{P_s}{29.92} \right)$$

- i. Percent isokinetic

$$I = \left(\frac{17.32 (T_s) (V_{m\ std})}{(1 - B_{wo}) (\Theta) (V_s) (P_s) (D_n^2)} \right) \left(\frac{528^\circ R}{T_{ref}} \right)$$

2. Particulate Emissions

- a. Grain loading, gr/dscf

$$C = 0.01543 \left(\frac{M_n}{V_{m \text{ std}}} \right)$$

- b. Grain loading at 12% CO
- ₂
- , gr/dscf

$$C_{12\% \text{ CO}_2} = C \left(\frac{12}{\% \text{ CO}_2} \right)$$

- c. Mass emissions, lb/hr

$$M = C(Q_{sd}) \frac{(60 \text{ min/hr})}{(7000 \text{ gr/lb})}$$

3. Gaseous Emissions, lb/hr

$$M = (\text{ppm})(10^{-6}) \left(\frac{MW_i \text{ lb/lb mole}}{SV} \right) (Q_{sd})(60 \text{ min/hr})$$

where,

SV = specific molar volume of an ideal gas:

$$SV = 385.3 \text{ ft}^3/\text{lb mole} \quad \text{for } T_{ref} = 528 \text{ }^\circ R$$

$$SV = 379.5 \text{ ft}^3/\text{lb mole} \quad \text{for } T_{ref} = 520 \text{ }^\circ R$$

4. Emissions Rates, lb/10⁶ Btu

- a. Fuel factor at 68 °F, dscf/10
- ⁶
- Btu at 0% O
- ₂

$$F_{68} = \frac{10^6 [3.64(\%H) + 1.53(\%C) + 0.14(\%N) + 0.57(\%S) - 0.46(\%O_{2, \text{fuel}})]}{HHV, \text{ Btu/lb}}$$

- b. Fuel factor at 60 °F

$$F_{60} = F_{68} \left(\frac{520 \text{ }^\circ R}{528 \text{ }^\circ R} \right)$$

- c. Gaseous Emissions factor

$$\left(\frac{\text{lb}}{10^6 \text{ Btu}} \right)_i = (\text{ppm})_i (10^{-6}) \left(\frac{MW_i \text{ lb}}{\text{lb mole}} \right) \left(\frac{1}{SV} \right) (F) \left(\frac{20.9}{20.9 - \%O_2} \right)$$

- d. Particulate emission factor

$$\left(\frac{\text{lb}}{10^6 \text{ Btu}} \right) = C \left(\frac{1 \text{ lb}}{7000 \text{ gr}} \right) (F) \left(\frac{20.9}{20.9 - \%O_2} \right)$$

Nomenclature:

A_s	=	stack area, ft ²
B_{wo}	=	flue gas moisture content
$C_{12\% CO_2}$	=	particulate grain loading, gr/dscf corrected to 12% CO ₂
C	=	particulate grain loading, gr/dscf
C_p	=	pitot calibration factor, dimensionless
D_n	=	nozzle diameter, in.
F	=	fuel F factor, dscf/10 ⁶ Btu at 0% O ₂
H	=	orifice pressure differential, iwg
I	=	% isokinetics
M_n	=	mass of collected particulate, mg
M_i	=	mass emissions of species i, lb/hr
MW	=	molecular weight of flue gas
MW_i	=	molecular weight of species i:
		NO _x : 46
		CO : 28
		SO _x : 64
		HC : 16
θ	=	sample time, min.
ΔP	=	average velocity head, iwg = $(\sqrt{\Delta P})^2$
P_{bar}	=	barometric pressure, in.Hg
P_s	=	stack absolute pressure, in.Hg
P_{sg}	=	stack static pressure, iwg

Nomenclature (Continued):

Q	=	wet stack gas flow rate at actual conditions, wacfm
Q_{sd}	=	dry stack gas flow rate at standard conditions, dscfm
SV	=	specific molar volume of an ideal gas at standard conditions, ft ³ /lb mole
T_m	=	meter temperature, °R
T_{ref}	=	reference temperature, °R
T_s	=	stack temperature, °R
V_s	=	stack velocity, ft/sec
V_{lc}	=	volume of liquid collected in impingers, ml
V_m	=	dry meter volume uncorrected, dcf
$V_{m\ std}$	=	dry meter volume at standard conditions, dscf
$V_{w\ std}$	=	volume of water vapor at standard conditions, scf
Y	=	meter calibration coefficient

Appendix D.2
Relative Accuracy and Calibration Drift Calculations

RELATIVE ACCURACY DETERMINATION NOx ppm vol. wet						
CLIENT: L. P. Oroville		DATE: 5/3/94				
UNIT: Boiler #5		Data By: Carnot				
LOAD: Full Load		Data By: KJC				
Run #	Time	Carnot	L.P.	Difference	n	t(0,975)
1	0945-1025	504.13	470.0	34.13	2	12.706
2	1100-1130	502.03	465.0	37.03	3	4.303
3	1145-1215	479.80	435.0	44.80	4	3.182
4	1240-1310	487.56	465.0	22.56	5	2.776
5	1325-1405	484.22	455.0	29.22	6	2.571
6	1420-1450	489.70	460.0	29.70	7	2.447
7	1510-1540	488.73	455.0	33.73	8	2.365
8	1605-1645	466.89	445.0	21.89	9	2.306
9	1700-1730	484.53	458.0	26.53	10	2.262
10	1750-1820	467.50	440.0	27.50	11	2.228
					12	2.201
AVERAGES:		485.51	454.80	30.71		
STANDARD DEVIATION				6.948372		
CONFIDENCE COEFFICIENT				4.970221		
RELATIVE ACCURACY, %					7.35	

RELATIVE ACCURACY DETERMINATION O2 % vol. wet						
CLIENT: L. P. Oroville		DATE: 5/3/94				
UNIT: Boiler #5		Data By: Carnot				
LOAD: Full Load		Data By: KJC				
Run #	Time	Carnot	L.P.	Difference	n	t(0,975)
1	0945-1025	4.94	4.88	0.06	2	12.706
2	1100-1130	4.71	4.70	0.01	3	4.303
3	1145-1215	4.70	4.70	0.00	4	3.182
4	1240-1310	4.72	4.70	0.02	5	2.776
5	1325-1405	4.69	4.70	-0.01	6	2.571
6	1420-1450	4.67	4.75	-0.08	7	2.447
7	1510-1540	4.68	4.75	-0.07	8	2.365
8	1605-1645	4.53	4.68	-0.15	9	2.306
9	1700-1730	4.80	4.80	0.00	10	2.262
10	1750-1820	4.81	4.75	0.06	11	2.228
					12	2.201
AVERAGES:		4.73	4.74	-0.02		
STANDARD DEVIATION				0.065862		
CONFIDENCE COEFFICIENT				0.047111		
RELATIVE ACCURACY, %					1.34	

RELATIVE ACCURACY DETERMINATION NOx ppm vol. wet						
CLIENT: L. P. Oroville		DATE: 5/4&5/94				
UNIT: Boiler #4		Data By: Carnot				
LOAD: Full Load		Data By: KJC				
Run #	Time	Carnot	L.P.	Difference	n	t(0,975)
1	1220-1250	84.56	78.0	6.56	2	12.706
2	1320-1350	85.60	80.4	5.20	3	4.303
3	1545-1625	84.72	79.2	5.52	4	3.182
4	1635-1705	76.20	71.2	5.00	5	2.776
5	1720-1800	83.60	78.0	5.60	6	2.571
6	0908-0938	67.56	65.0	2.56	7	2.447
7	1013-1043	81.88	78.0	3.88	8	2.365
8	1108-1138	81.74	81.4	0.34	9	2.306
9	1208-1238	60.08	57.0	3.08	10	2.262
10	1443-1523	75.99	73.6	2.39	11	2.228
11	1538-1608	78.39	74.8	3.59	12	2.201
12	1618-1648	79.51	75.4	4.11		
AVERAGES:		78.32	74.33	3.99		
STANDARD DEVIATION				1.731103		
CONFIDENCE COEFFICIENT				1.099898		
RELATIVE ACCURACY, %					6.49	

DATE: 5/4&5/94
Data By: Carnot
Data By: KJC

AVERAGES: 78.32 74.33 3.99

STANDARD DEVIATION	1.731103
CONFIDENCE COEFFICIENT	1.099898
RELATIVE ACCURACY, %	

**RELATIVE ACCURACY
DETERMINATION**
O₂ % vol. wet

CLIENT: L. P. Oroville
UNIT: Boiler #4
LOAD: Full Load

DATE: 5/4&5/94
Data By: Carnot
Data By: KJC

Run #	Time	Carnot	L.P.	Difference	n	t(0,975)
1	1220-1250	4.24	4.50	-0.26	2	12.706
2	1320-1350	4.12	4.25	-0.13	3	4.303
3	1545-1625	4.42	4.50	-0.08	4	3.182
4	1635-1705	4.75	4.75	0.00	5	2.776
5	1720-1800	4.89	4.70	0.19	6	2.571
6	0908-0938	4.74	4.80	-0.06	7	2.447
7	1013-1043	5.60	5.60	0.00	8	2.365
8	1108-1138	4.47	4.80	-0.33	9	2.306
9	1208-1238	3.53	4.00	-0.47	10	2.262
10	1443-1523	4.25	4.45	-0.20	11	2.228
11	1538-1608	4.35	4.38	-0.03	12	2.201
12	1618-1648	4.56	4.40	0.16		

AVERAGES: 4.52 4.60 -0.09 (Run 1 deleted,
see data sheets)

STANDARD DEVIATION 0.19423

CONFIDENCE COEFFICIENT 0.130478

RELATIVE ACCURACY, % 4.80

**POLLUTANT CALIBRATION DRIFT
DETERMINATION**

CLIENT: L. P. Oroville
UNIT: Boiler #4

Run #	Date	% Full Scale		ppm vol wet		Difference		% Cal. Drift	
		NOx Cal.	NOx Zero	NOx Cal.	NOx Zero	NOx Cal.	NOx Zero	NOx Cal.	NOx Zero
1	5-7-94	35.0	-0.8	70.0	-1.6	-1.9	-1.6	1.0	0.8
2	5-8-94	36.3	-0.6	72.6	-1.2	0.7	-1.2	0.3	0.6
3	5-9-94	35.4	-0.8	70.8	-1.6	-1.1	-1.6	0.6	0.8
4	5-10-94	34.8	-0.8	69.6	-1.6	-2.3	-1.6	1.2	0.8
5	5-11-94	35.8	-0.7	71.6	-1.4	-0.3	-1.4	0.2	0.7
6	5-12-94	34.5	-0.7	69.0	-1.4	-2.9	-1.4	1.5	0.7
7	5-13-94	35.0	-0.8	70.0	-1.6	-1.9	-1.6	1.0	0.8

Cal. Value: 71.9 0.0
Span Value: 200

	SPAN	ZERO
CALIBRATION DRIFT, %	1.45	0.8

DILUENT CALIBRATION DRIFT DETERMINATION

CLIENT: L. P. Oroville
UNIT: Boiler #4

Run #	Date	% Full Scale		% vol wet		Difference		% Cal. Drift	
		O2 High	O2 Low	O2 High	O2 Low	O2 High	O2 Low	O2 High	O2 Low
1	4-20-94	83.9	12.4	21.0	3.1	0.08	0.10	0.1	0.1
2	4-21-94	84.2	12.4	21.1	3.1	0.15	0.10	0.2	0.1
3	4-22-94	84.0	12.4	21.0	3.1	0.10	0.10	0.1	0.1
4	4-23-94	84.0	12.2	21.0	3.1	0.10	0.05	0.1	0.0
5	4-24-94	84.0	12.4	21.0	3.1	0.10	0.10	0.1	0.1
6	4-25-94	84.0	12.6	21.0	3.2	0.10	0.15	0.1	0.2
7	4-26-94	84.8	12.8	21.2	3.2	0.30	0.20	0.3	0.2

Cal. Value: 20.9 3.0
Span Value: 25

	SPAN	ZERO
CALIBRATION DRIFT, %	0.3	0.2

OPACITY CALIBRATION DRIFT DETERMINATION

CLIENT: L. P. Oroville
UNIT: Boiler #4

Run #	Date	Percent Full Scale		Percent Opacity		Drift Opacity		% Cal. Drift
		Zero	Upsc.	Zero	Upsc.	Zero	Upsc.	
1	4-19-94	0.0	42.8	0.00	8.56			
2	4-20-94	0.0	42.6	0.00	8.52	0.00	-0.04	-0.04
3	4-21-94	0.0	43.0	0.00	8.60	0.00	0.08	0.08
4	4-22-94	0.0	42.5	0.00	8.50	0.00	-0.10	-0.10
5	4-23-94	0.0	42.7	0.00	8.54	0.00	0.04	0.04
6	4-24-94	0.0	42.8	0.00	8.56	0.00	0.02	0.02
7	4-25-94	0.0	42.5	0.00	8.50	0.00	-0.06	-0.06
8	4-26-94	0.0	43.5	0.00	8.70	0.00	0.20	0.20

Arithmetic Mean:	0.00	0.02
Confidence Coefficient:	0.00	0.09

Zero Drift, % Opacity:	0.00	
Calibration Drift, % Opacity:		0.11

**POLLUTANT CALIBRATION DRIFT
DETERMINATION**

CLIENT: L. P. Oroville
UNIT: Boiler #5

Run #	Date	% Full Scale		ppm vol wet		Difference		% Cal. Drift	
		NOx Cal.	NOx Zero	NOx Cal.	NOx Zero	NOx Cal.	NOx Zero	NOx Cal.	NOx Zero
1	5-7-94	58.0	-0.1	580.0	-1.0	3.0	-1.0	0.3	0.1
2	5-8-94	55.7	-0.2	557.0	-2.0	-20.0	-2.0	2.0	0.2
3	5-9-94	57.3	-0.3	573.0	-3.0	-4.0	-3.0	0.4	0.3
4	5-10-94	55.5	-0.4	555.0	-4.0	-22.0	-4.0	2.2	0.4
5	5-11-94	58.3	0.0	583.0	0.0	6.0	0.0	0.6	0.0
6	5-12-94	57.8	-0.1	578.0	-1.0	1.0	-1.0	0.1	0.1
7	5-13-94	57.6	-0.1	576.0	-1.0	-1.0	-1.0	0.1	0.1

Cal. Value: 577.0 0.0
Span Value: 1000

	SPAN	ZERO
CALIBRATION DRIFT, %	2.2	0.4

DILUENT CALIBRATION DRIFT DETERMINATION

CLIENT: L. P. Oroville
UNIT: Boiler #5

Run #	Date	% Full Scale		% vol wet		Difference		% Cal. Drift	
		O2 High	O2 Low	O2 High	O2 Low	O2 High	O2 Low	O2 High	O2 Low
1	4-22-94	85.2	12.2	21.3	3.1	0.40	0.05	0.4	0.0
2	4-23-94	84.8	12.0	21.2	3.0	0.30	0.00	0.3	0.0
3	4-24-94	83.6	11.8	20.9	3.0	0.00	-0.05	0.0	0.0
4	4-25-94	84.0	12.2	21.0	3.1	0.10	0.05	0.1	0.0
5	4-26-94	83.1	11.7	20.8	2.9	-0.13	-0.08	0.1	0.1
6	4-27-94	83.6	11.6	20.9	2.9	0.00	-0.10	0.0	0.1
7	4-28-94	83.8	11.8	21.0	3.0	0.05	-0.05	0.1	0.0

Cal. Value: 20.9 3.0
Span Value: 25

	SPAN	ZERO
CALIBRATION DRIFT, %	0.4	0.1

OPACITY CALIBRATION DRIFT DETERMINATION

CLIENT: L. P. Oroville
UNIT: Boiler #5

Run #	Date	Percent Full Scale		Percent Opacity		Drift Opacity		% Cal. Drift
		Zero	Upsc.	Zero	Upsc.	Zero	Upsc.	
1	4-22-94	-0.5	36.5	-0.10	7.30			
2	4-23-94	0.0	37.0	0.00	7.40	0.10	0.10	0.00
3	4-24-94	0.0	37.0	0.00	7.40	0.00	0.00	0.00
4	4-25-94	0.0	37.5	0.00	7.50	0.00	0.10	0.10
5	4-26-94	0.0	37.0	0.00	7.40	0.00	-0.10	-0.10
6	4-27-94	-0.2	36.8	-0.04	7.36	-0.04	-0.04	0.00
7	4-28-94	-0.1	36.8	-0.02	7.36	0.02	0.00	-0.02
8	4-29-94	0.0	36.8	0.00	7.36	0.02	0.00	-0.02

Arithmetic Mean:	0.01	-0.01
Confidence Coefficient:	0.04	0.05

Zero Drift, % Opacity:	0.05	
Calibration Drift:		0.06

APPENDIX E
STRIP CHARTS

02aXVL
May.03 10:05
INTVL 1

NOxPPM 529.7
COaPPM 21.8
CO2aXVL 12.59
O2aXVL 16.88
May.03 10:00
INTVL 1

NOxPPM 573.4
COaPPM 21.9
CO2aXVL 13.58
O2aXVL 17.77
May.03 09:55
INTVL 1

NOxPPM 678.2
COaPPM 21.2
CO2aXVL 13.58
O2aXVL 16.59
May.03 09:50
INTVL 1

NOxPPM 575.9
COaPPM 21.5
CO2aXVL 13.51
O2aXVL 16.84
May.03 09:43
INTVL 1

NOxPPM 553.3
COaPPM 21.9
CO2aXVL 13.72
O2aXVL 16.55
May.03 09:38
INTVL 1

NOxPPM 511.18
COaPPM 21.8
CO2aXVL 13.51
O2aXVL 16.45
May.03 09:35
INTVL 1

NOxPPM 215.5
COaPPM 19.7
CO2aXVL 1.08
O2aXVL 0.72
May.03 09:26
INTVL 1

NOxPPM 137.6
COaPPM 15.1
CO2aXVL 5.05
O2aXVL 2.52
May.03 09:20
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COaPPM 39.1
CO2aXVL 0.07
O2aXVL 8.15
May.03 09:15
INTVL 1

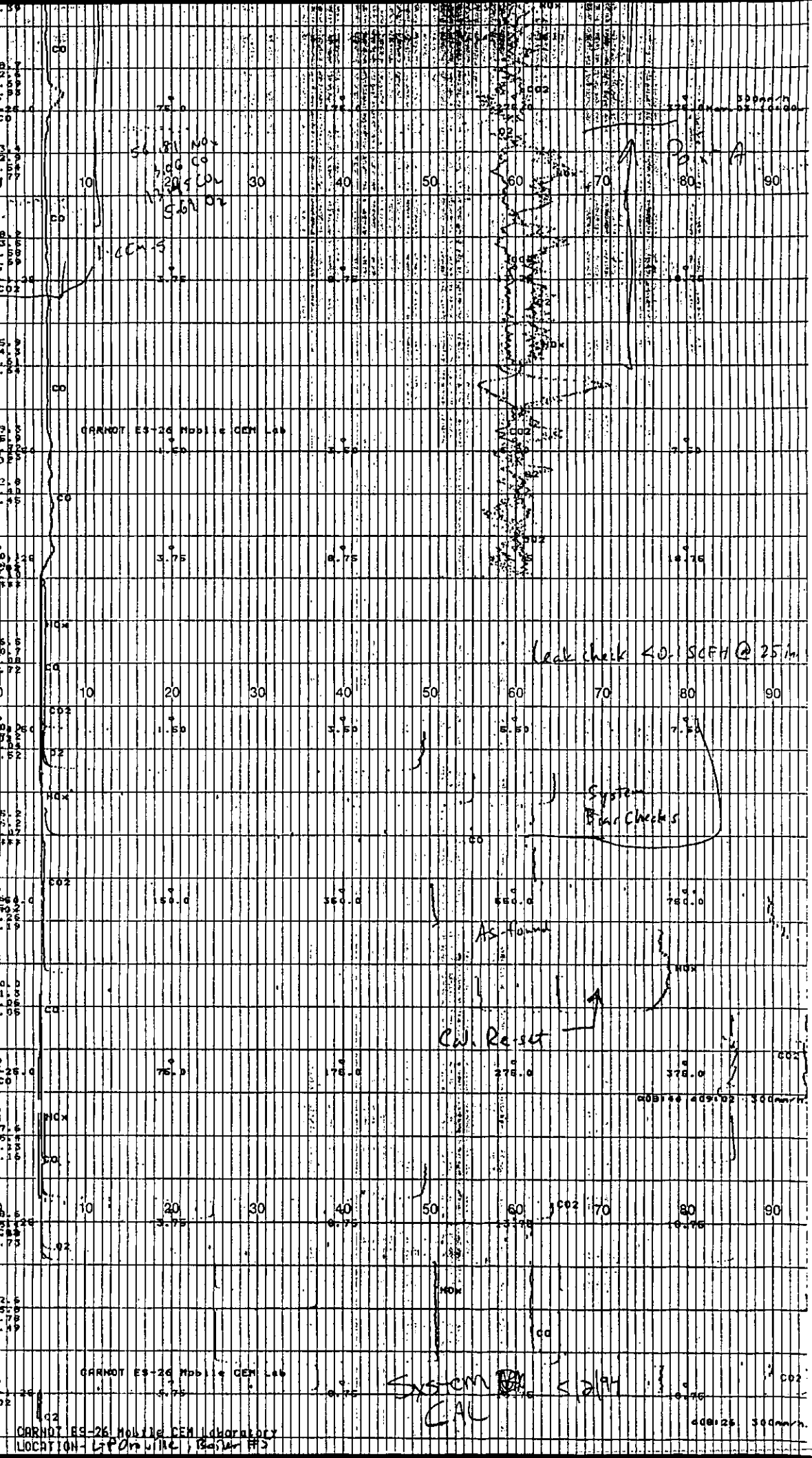
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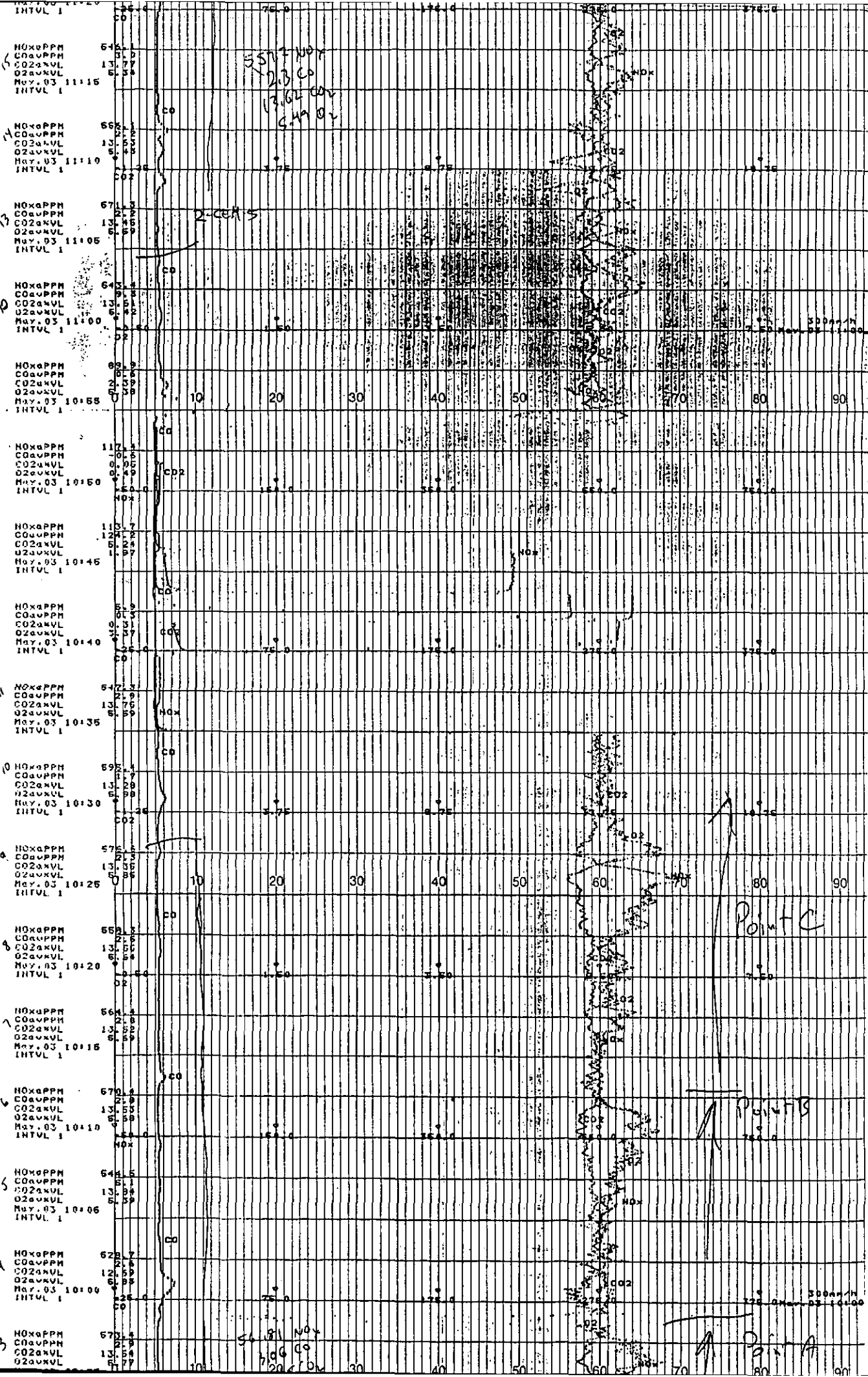
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COaPPM 15.1
CO2aXVL 4.53
O2aXVL 3.16
May.03 08:40
INTVL 1

NOxPPM 493.5
COaPPM 29.1
CO2aXVL 16.88
O2aXVL 5.73
May.03 08:35
INTVL 1

NOxPPM 302.5
COaPPM 16.5
CO2aXVL 9.78
O2aXVL 3.19
May.03 08:30
INTVL 1





0200VUL
May. 03 12:35
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 12:30
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 12:25
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 12:20
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 12:16
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 12:10
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 12:05
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 12:00
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 11:55
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 11:50
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 11:45
INTVL 1

NOxPPH
COxPPH
CO2xVUL
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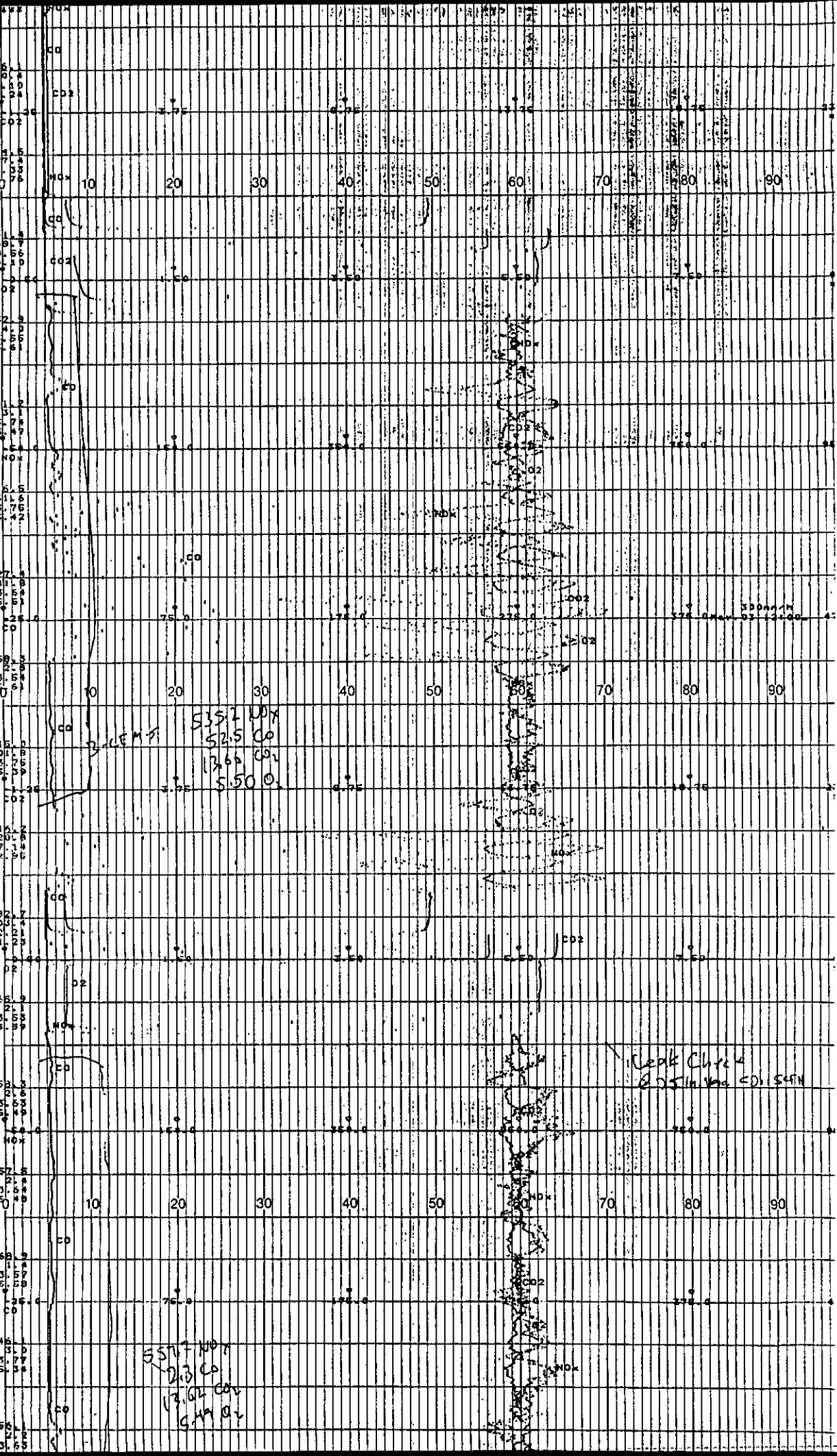
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COxPPH
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O2xVUL
May. 03 11:25
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 11:20
INTVL 1

NOxPPH
COxPPH
CO2xVUL
O2xVUL
May. 03 11:15
INTVL 1

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COxPPH
CO2xVUL
O2xVUL
May. 03 11:10
INTVL 1



INTVL 1

May. 03 1
INTVL 1

MAY 03 1964
INTL. B.

NOV. 93
INTVL 1

May. 03
INTOL 1

May, 03
INTH 1

May 03
LNU

May, 03

May. 03
INTM

May. 03
6:22 PMMay. 03
2000

NOV 1963

May 03

May, 03

024680
May, 93

02avx0
May 03

62044
May - 07

020280

INTVL 1

NOxPPM
COaPPM
CO2a%
O2a%
May. 03 16:00
INTU 1

NOx@PPH
CO@PPH
O2@xVL
O2@xVL
May. 03 14:51
INITUL 1

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NOxαPPH
COαUPPH
CO2αxVL
O2αvαVL
Muy.03 14:5
INTVL 1

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```

NOxaPPM
COaPPM
CO2aVL
O2aVL
May.03 14:41
INTVL 1

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NOx6PPH
CO26PPH
CO26xVL
O26xVL
May.03 14:4
INTVL 1

```

NOxAPPH
CO2APPH
CO2a*VL
O2a*VL
May.03 14:30
111VL 1

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NOx@PPH
CO@PPH
CO2@VL
O2@VL
May.03 14:13
INTVL 1

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```

NOxaPPM
COaPPM
CO2aXVL
O2aXVL
May.03 14:2
INTVL 1

```

```

NOx:PPM
CO:PPM
CO2:PPM
O2:PPM
MAY.03 14:2
INTVL 1

```

NUxaPPN
CO2aPPN
CO2aXVL
O2aXVL
May 03 14:13
111VL 1

NOx:0PPH
CO:0PPH
O2:2xVL
O2:0xVL
May-03 14:1
INTVL:1

NOx@PPH
COx@PPH
CO2@xVL
O2@xVL
Nov. 93 14:00
315VL 3

NOx uPPH
CO uPPH
CO2 uVL
O2 uVL
May. 03 14:0
INVL 1

NOx a PPM
CO a PPM
CO2 a VOL
O2 a VOL
May. 03 13:5
INTVL 1

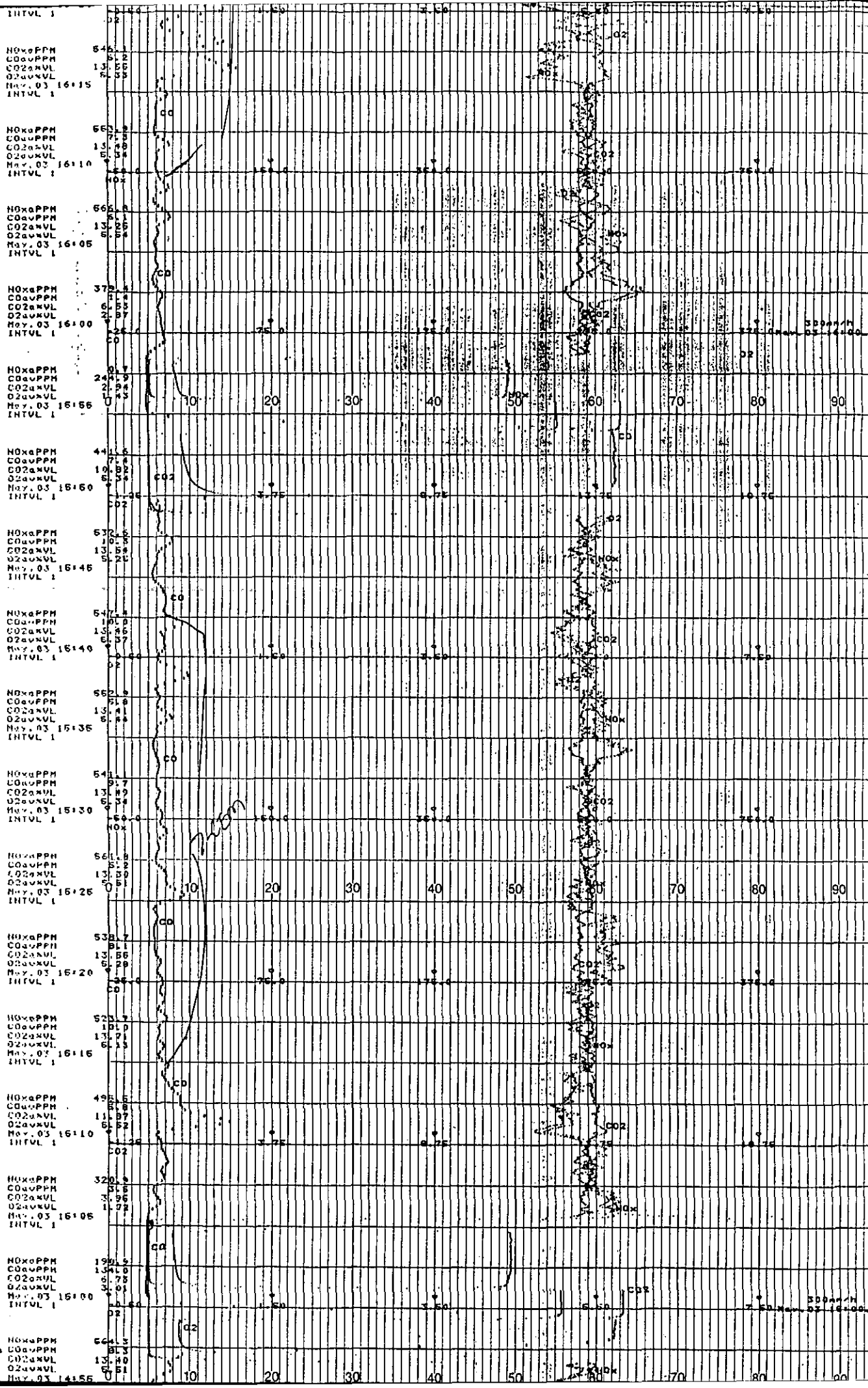
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CO:APPN
CO2:AVL
O2:AVL
May.03 13:5
INTVL 1

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NDxaPPH
COaVPPH
CO2aMVL
O2aMVL
Mo r. 03 13:4
INTVL 1

```

NOx: PPM
CO: PPM
LD2: %VL
D2: %KML



END OF RECORD - L.P. 0.112 Boilers 5 5-3-94

Leak Check @ 20.1 SCFH @ 25 in. vac

NOx PPM 1.3
CO PPM 50.4
CO2 % 13.14
O2 % 4.86
May. 03 10:40
INTVL 1

NOx PPM 485.3
CO PPM 30.4
CO2 % 13.96
O2 % 1.57
May. 03 10:35
INTVL 1

NOx PPM 109.9
CO PPM 132.6
CO2 % 6.71
O2 % 2.25
May. 03 10:30
INTVL 1

NOx PPM 386.5
CO PPM 197.7
CO2 % 11.01
O2 % 4.59
May. 03 10:25
INTVL 1

NOx PPM 472.8
CO PPM 296.6
CO2 % 13.24
O2 % 5.46
May. 03 10:20
INTVL 1

NOx PPM 511.3
CO PPM 751.3
CO2 % 13.10
O2 % 5.52
May. 03 10:15
INTVL 1

NOx PPM 521.4
CO PPM 54.6
CO2 % 13.88
O2 % 5.53
May. 03 10:10
INTVL 1

NOx PPM 502.5
CO PPM 92.6
CO2 % 13.3
O2 % 5.45
May. 03 10:05
INTVL 1

NOx PPM 557.4
CO PPM 81.6
CO2 % 12.97
O2 % 5.70
May. 03 10:00
INTVL 1

NOx PPM 526.8
CO PPM 95.6
CO2 % 13.15
O2 % 5.46
May. 03 17:55
INTVL 1

NOx PPM 342.0
CO PPM 281.2
CO2 % 41.99
O2 % 2.43
May. 03 17:50
INTVL 1

NOx PPM 701.4
CO PPM 129.5
CO2 % 11.06
O2 % 2.85
May. 03 17:45
INTVL 1

NOx PPM 512.7
CO PPM 251.2
CO2 % 13.45
O2 % 5.31
May. 03 17:40
INTVL 1

NOx PPM 525.5
CO PPM 201.9
CO2 % 13.29
O2 % 5.47
May. 03 17:35
INTVL 1

NOx PPM 523.0
CO PPM 201.6
CO2 % 13.27
O2 % 5.51
May. 03 17:30
INTVL 1

NOx PPM 537.8
CO PPM 111.4
CO2 % 13.20
O2 % 5.41
May. 03 17:25
INTVL 1

High cal. gas

Spec. Span/pins

Low cal. gas

10-GEN-5

5.547 NOx
10.453 CO
3.18 CO2
5.51 O2

50000/H

5.547 NOx
10.453 CO
3.18 CO2
5.51 O2

NOxAPPM
COaUPPM
CO2aXVL
O2aXVL
May. 04 12:50
INTVL 1

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COaUPPM
CO2aXVL
O2aXVL
May. 04 12:45
INTVL 1

NOxAPPM
COaUPPM
CO2aXVL
O2aXVL
May. 04 12:40
INTVL 1

NOxAPPM
COaUPPM
CO2aXVL
O2aXVL
May. 04 12:35
INTVL 1

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COaUPPM
CO2aXVL
O2aXVL
May. 04 12:30
INTVL 1

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COaUPPM
CO2aXVL
O2aXVL
May. 04 12:25
INTVL 1

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COaUPPM
CO2aXVL
O2aXVL
May. 04 12:20
INTVL 1

NOxAPPM
COaUPPM
CO2aXVL
O2aXVL
May. 04 12:15
INTVL 1

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COaUPPM
CO2aXVL
O2aXVL
May. 04 12:10
INTVL 1

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COaUPPM
CO2aXVL
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O2aXVL
May. 04 11:58
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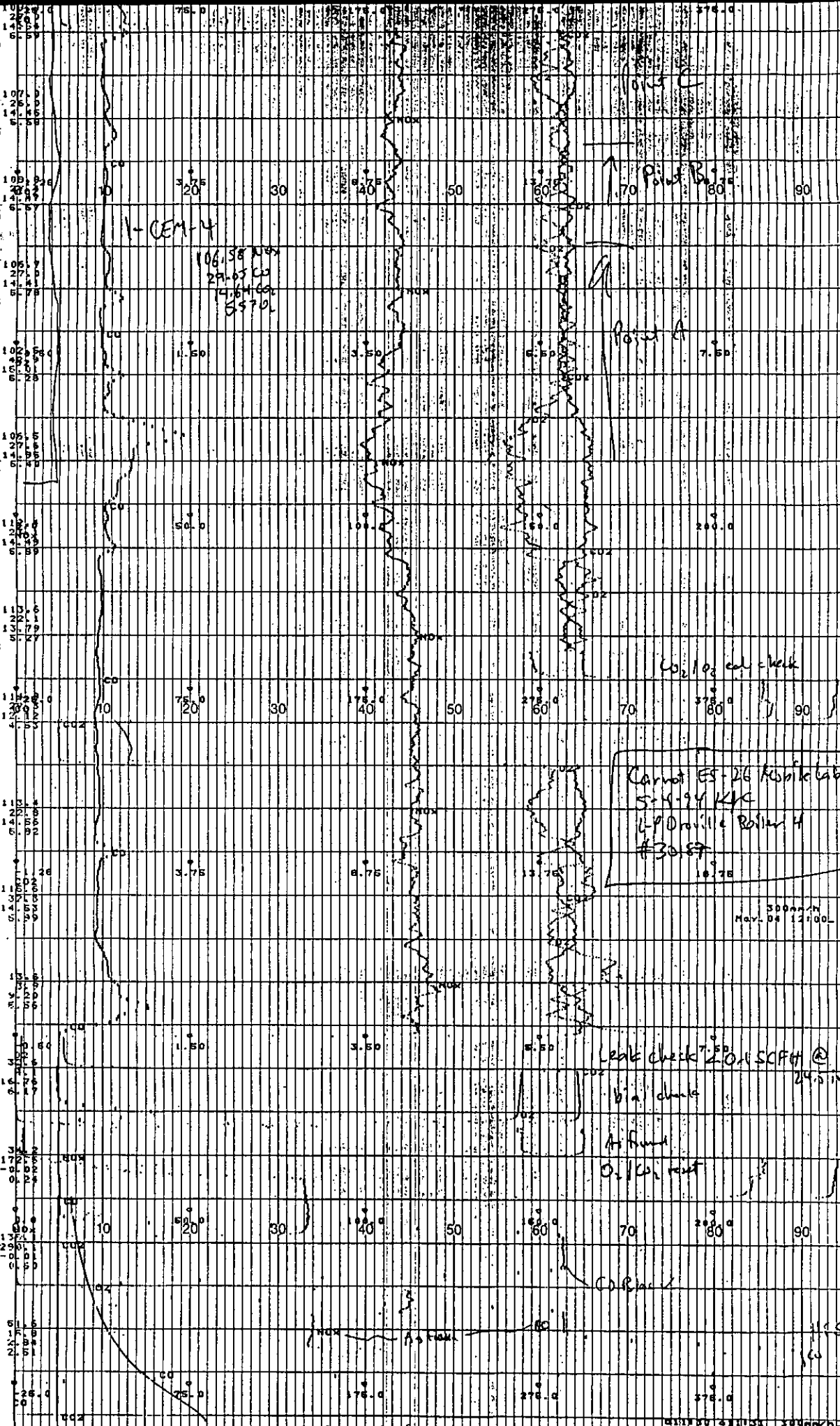
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May. 04 11:48
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CO2aXVL
O2aXVL
May. 04 11:43
INTVL 1

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CO2aXVL
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May. 04 11:38
INTVL 1

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May. 04 11:33
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May. 04 14:05
INTVL 1

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O2aXVL
May. 04 14:00
INTVL 1

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CO2aXVL
O2aXVL
May. 04 13:55
INTVL 1

NOxAPPH
CO2aXVL
O2aXVL
May. 04 13:50
INTVL 1

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CO2aXVL
O2aXVL
May. 04 13:45
INTVL 1

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CO2aXVL
O2aXVL
May. 04 13:40
INTVL 1

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CO2aXVL
O2aXVL
May. 04 13:35
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CO2aXVL
O2aXVL
May. 04 13:30
INTVL 1

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CO2aXVL
O2aXVL
May. 04 13:25
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CO2aXVL
O2aXVL
May. 04 13:20
INTVL 1

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May. 04 13:15
INTVL 1

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O2aXVL
May. 04 13:10
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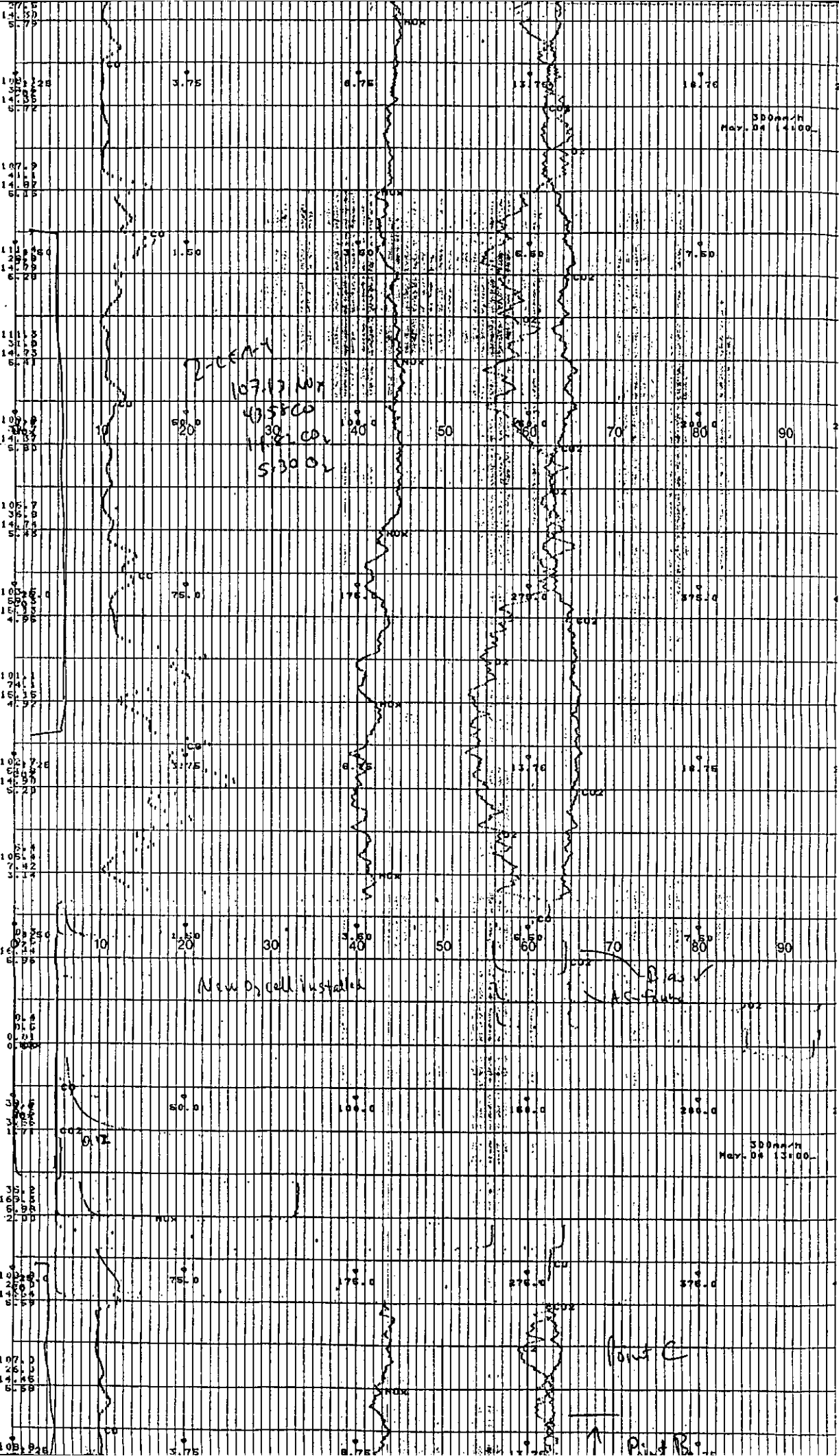
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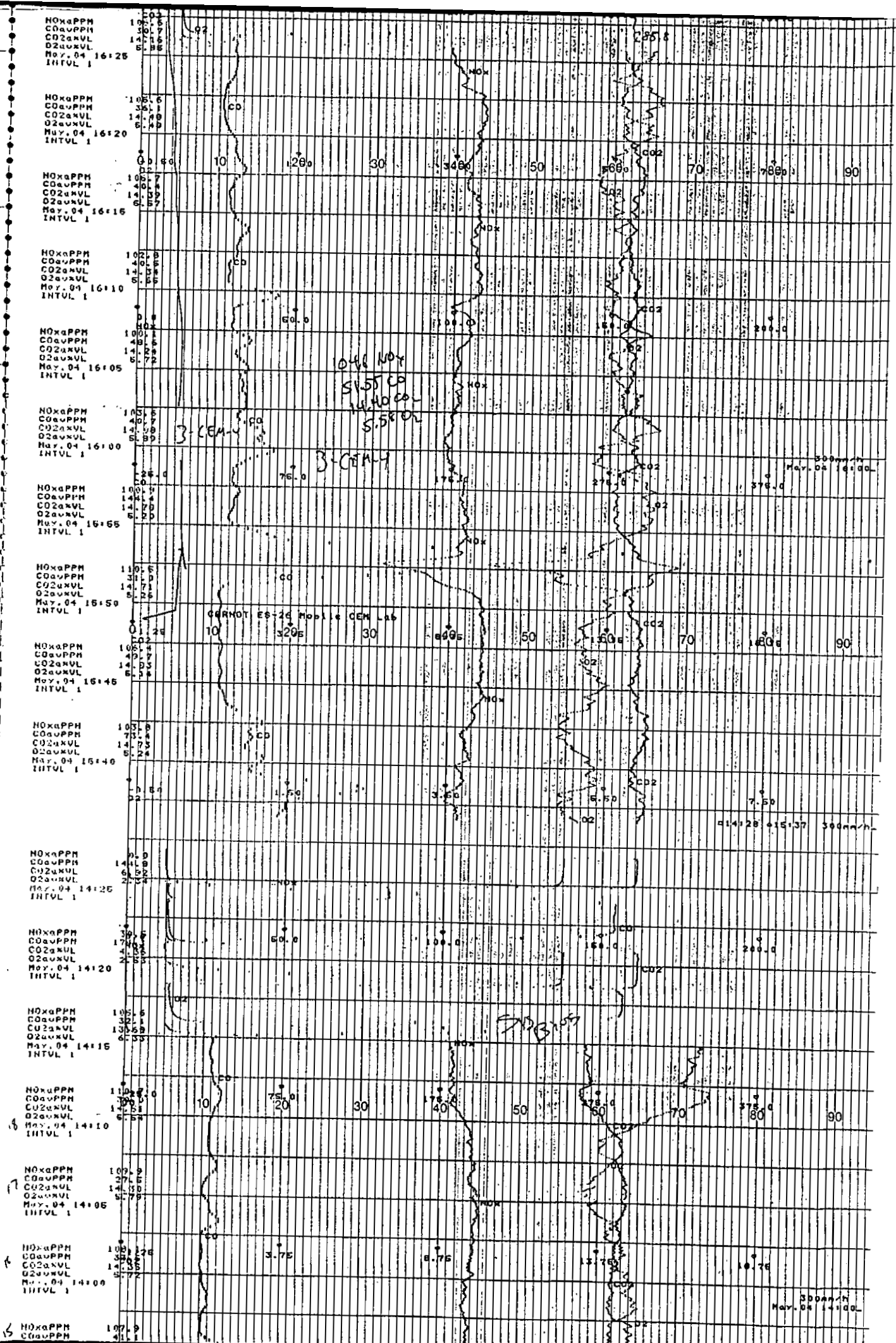
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INTVL 1

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O2aXVL
May. 04 12:55
INTVL 1

NOxAPPH
CO2aXVL
O2aXVL
May. 04 12:50
INTVL 1

NOxAPPH
CO2aXVL
O2aXVL
May. 04 12:45
INTVL 1





NOxAPPM 107.3
COAPPM 35.8
CO2ANVL 13.70
O2ANVL 6.12
May. 04 17:40
INTVL 1

S-CEM-1

107.58 NOx
35.79 CO
13.53 CO2
6.04 O2

NOxAPPM 105.2
COAPPM 35.8
CO2ANVL 13.70
O2ANVL 6.12
May. 04 17:36
INTVL 1

NOxAPPM 100.3
COAPPM 20.6
CO2ANVL 13.23
O2ANVL 6.62
May. 04 17:30
INTVL 1

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COAPPM 38.6
CO2ANVL 13.37
O2ANVL 6.69
May. 04 17:26
INTVL 1

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COAPPM 31.6
CO2ANVL 13.52
O2ANVL 6.65
May. 04 17:20
INTVL 1

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COAPPM 152.7
CO2ANVL 4.58
O2ANVL 1.55
May. 04 17:16
INTVL 1

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COAPPM 65.9
CO2ANVL 7.22
O2ANVL 4.58
May. 04 17:10
INTVL 1

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O2ANVL 5.94
May. 04 17:06
INTVL 1

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May. 04 17:00
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CO2ANVL 13.52
O2ANVL 6.08
May. 04 16:56
INTVL 1

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COAPPM 60.9
CO2ANVL 14.50
O2ANVL 5.49
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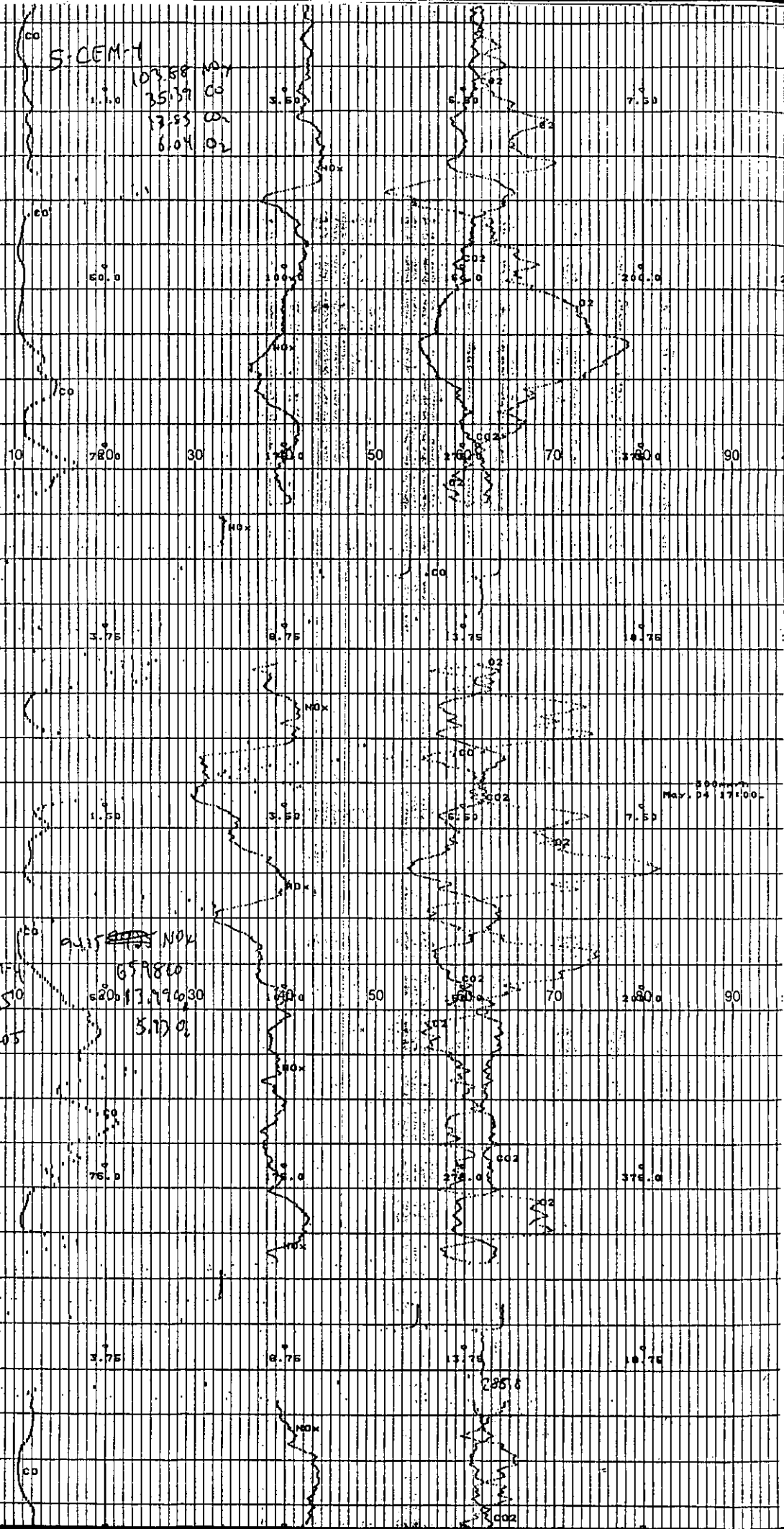
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May. 04 16:36
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COAPPM 160.7
CO2ANVL 4.98
O2ANVL 2.22
May. 04 16:30
INTVL 1

NOxAPPM 100.6
COAPPM 30.7
CO2ANVL 14.15
O2ANVL 5.85
May. 04 16:26
INTVL 1

NOxAPPM 105.6
COAPPM 35.1
CO2ANVL 14.49
O2ANVL 5.48
May. 04 16:20
INTVL 1



X
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COAPPM 30.7
O2APPM 12.30
U2APPM 7.47
May. 04 18:40
INTVL 1

X
NOxAPPM 90.8
COAPPM 20.7
O2APPM 11.70
U2APPM 7.58
May. 04 18:35
INTVL 1

X
NOxAPPM 25.2
COAPPM 0.3
O2APPM 1.98
U2APPM 1.73
May. 04 18:30
INTVL 1

X
NOxAPPM 149.9
COAPPM 3.52
O2APPM 1.71
May. 04 18:25
INTVL 1

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U2APPM 2.99
May. 04 18:20
INTVL 1

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COAPPM 12.55
O2APPM 7.20
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INTVL 1

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COAPPM 10.7
O2APPM 12.37
U2APPM 7.52
May. 04 18:10
INTVL 1

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COAPPM 10.2
O2APPM 12.78
U2APPM 7.40
May. 04 18:05
INTVL 1

X
NOxAPPM 107.7
COAPPM 13.55
O2APPM 12.78
U2APPM 6.55
May. 04 18:00
INTVL 1

X
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U2APPM 6.58
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INTVL 1

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COAPPM 13.6
O2APPM 14.15
U2APPM 6.57
May. 04 17:50
INTVL 1

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COAPPM 13.8
O2APPM 14.85
U2APPM 6.73
May. 04 17:45
INTVL 1

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NOxAPPM 107.3
COAPPM 13.70
O2APPM 14.12
U2APPM 6.52
May. 04 17:40
INTVL 1

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U2APPM 6.52
May. 04 17:35
INTVL 1

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COAPPM 13.5
O2APPM 13.25
U2APPM 6.52
May. 04 17:30
INTVL 1

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NOxAPPM 95.3
COAPPM 13.4
O2APPM 13.37
U2APPM 6.49
May. 04 17:25
INTVL 1

X
NOxAPPM 88.8
COAPPM 10.8
O2APPM 10.85
U2APPM 4.50
May. 04 17:20
INTVL 1



H0x0PPH
C00uPPH
C020xVL
0200xVL
May. 05 09:40
INTVL 1

H0x0PPH
C00uPPH
C020xVL
0200xVL
May. 05 09:43
INTVL 1

H0x0PPH
C00uPPH
C020xVL
0200xVL
May. 05 09:38
INTVL 1

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C00uPPH
C020xVL
0200xVL
May. 05 09:33
INTVL 1

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C00uPPH
C020xVL
0200xVL
May. 05 09:28
INTVL 1

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C00uPPH
C020xVL
0200xVL
May. 05 09:23
INTVL 1

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C00uPPH
C020xVL
0200xVL
May. 05 09:18
INTVL 1

H0x0PPH
C00uPPH
C020xVL
0200xVL
May. 05 09:13
INTVL 1

H0x0PPH
C00uPPH
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0200xVL
May. 05 09:08
INTVL 1

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C00uPPH
C020xVL
0200xVL
May. 05 09:03
INTVL 1

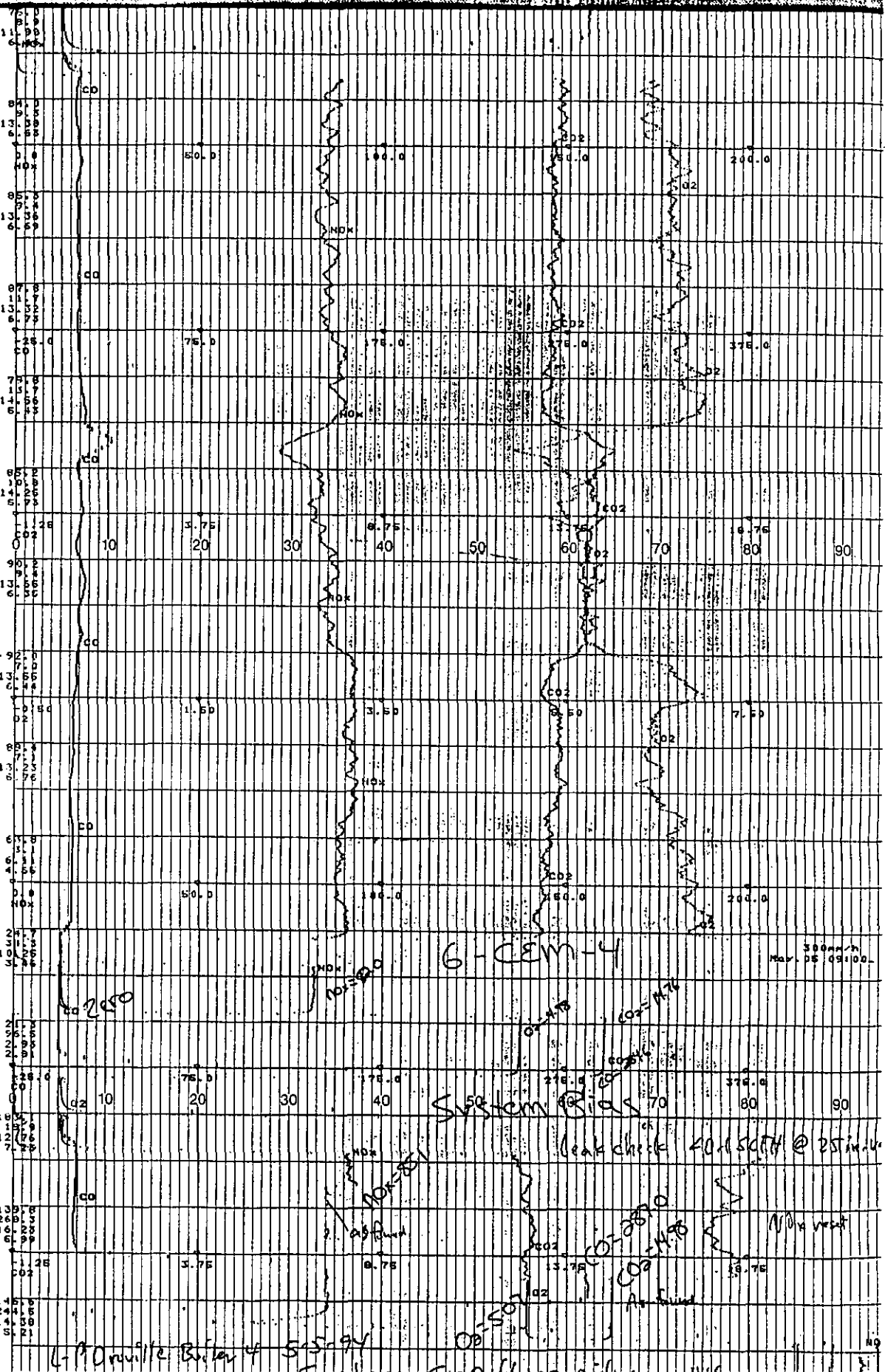
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May. 05 08:58
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C020xVL
0200xVL
May. 05 08:53
INTVL 1

H0x0PPH
C00uPPH
C020xVL
0200xVL
May. 05 08:48
INTVL 1

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C00uPPH
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0200xVL
May. 05 08:43
INTVL 1

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0200xVL
May. 05 08:38
INTVL 1



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CO2 PPM 12.38
CO2 ANVL 71.08
May. 05 10:43
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CO2 PPM 29.0
CO2 ANVL 121.89
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May. 05 10:36
INTVL 1

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CO2 PPM 30.9
CO2 ANVL 121.28
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May. 05 10:33
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CO2 ANVL 131.19
O2 ANVL 61.31
May. 05 10:23
INTVL 1

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CO2 PPM 18.5
CO2 ANVL 131.19
O2 ANVL 61.76
May. 05 10:18
INTVL 1

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CO2 ANVL 61.58
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INTVL 1

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CO2 PPM 91.5
CO2 ANVL 81.20
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May. 05 10:08
INTVL 1

NOXA PPM 61.3
CO2 PPM 01.5
CO2 ANVL 01.12
O2 ANVL 33.33
May. 05 10:03
INTVL 1

NOXA PPM 52.7
CO2 PPM 51.2
CO2 ANVL 41.59
O2 ANVL 11.04
May. 05 09:58
INTVL 1

NOXA PPM 41.2
CO2 PPM 2191.1
CO2 ANVL 11.70
O2 ANVL 0.85
May. 05 09:53
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May. 05 09:48
INTVL 1

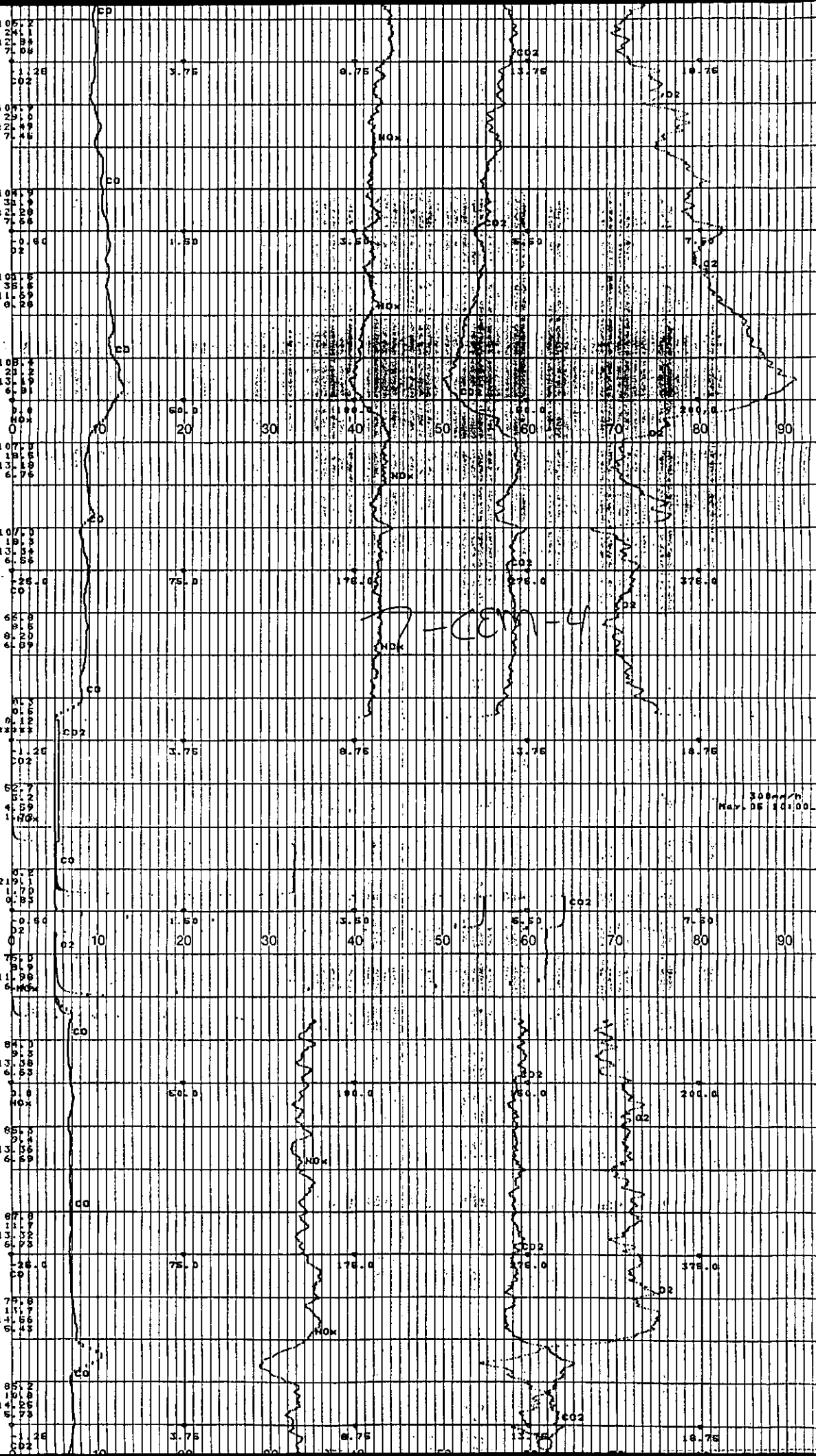
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O2 ANVL 61.59
May. 05 09:38
INTVL 1

NOXA PPM 87.8
CO2 PPM 111.7
CO2 ANVL 131.32
O2 ANVL 61.73
May. 05 09:33
INTVL 1

NOXA PPM 75.8
CO2 PPM 111.7
CO2 ANVL 141.56
O2 ANVL 61.43
May. 05 09:28
INTVL 1

NOXA PPM 85.2
CO2 PPM 101.8
CO2 ANVL 141.26
O2 ANVL 51.73
May. 05 09:23
INTVL 1



NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 11:58
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 11:53
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 11:48
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 11:43
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 11:38
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 11:33
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 11:28
INTVL 1

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CO2xVUL
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May. 05 11:23
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May. 05 11:13
INTVL 1

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COxAPPM
CO2xVUL
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May. 05 11:08
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 11:03
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 10:58
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 10:53
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 10:48
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 10:43
INTVL 1

NOxAPPM
COxAPPM
CO2xVUL
O2xVUL
May. 05 10:38
INTVL 1

300mm/h
May. 05 12:00

300mm/h
May. 05 11:00

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COAPPM 151.6
CO2ANVL 11.75
O2ANVL 6.59
May. 05 13:13
INTVL 1

NOxAPPM 62.4
COAPPM 232.2
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O2ANVL 7.94
May. 05 13:08
INTVL 1

NOxAPPM 61.7
COAPPM 391.5
CO2ANVL 13.97
O2ANVL 6.25
May. 05 13:03
INTVL 1

NOxAPPM 60.4
COAPPM 495.8
CO2ANVL 15.34
O2ANVL 3.21
May. 05 12:58
INTVL 1

NOxAPPM 65.5
COAPPM 495.7
CO2ANVL 15.76
O2ANVL 3.59
May. 05 12:53
INTVL 1

NOxAPPM 65.7
COAPPM 495.7
CO2ANVL 15.87
O2ANVL 3.95
May. 05 12:48
INTVL 1

NOxAPPM 64.1
COAPPM 310.25
CO2ANVL 10.25
O2ANVL 4.87
May. 05 12:43
INTVL 1

NOxAPPM 751.0
COAPPM 495.8
CO2ANVL 15.96
O2ANVL 3.50
May. 05 12:38
INTVL 1

NOxAPPM 65.4
COAPPM 495.8
CO2ANVL 15.59
O2ANVL 3.92
May. 05 12:33
INTVL 1

NOxAPPM 63.2
COAPPM 391.6
CO2ANVL 15.12
O2ANVL 4.51
May. 05 12:28
INTVL 1

NOxAPPM 79.5
COAPPM 110.8
CO2ANVL 14.99
O2ANVL 4.93
May. 05 12:23
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O2ANVL 5.16
May. 05 12:18
INTVL 1

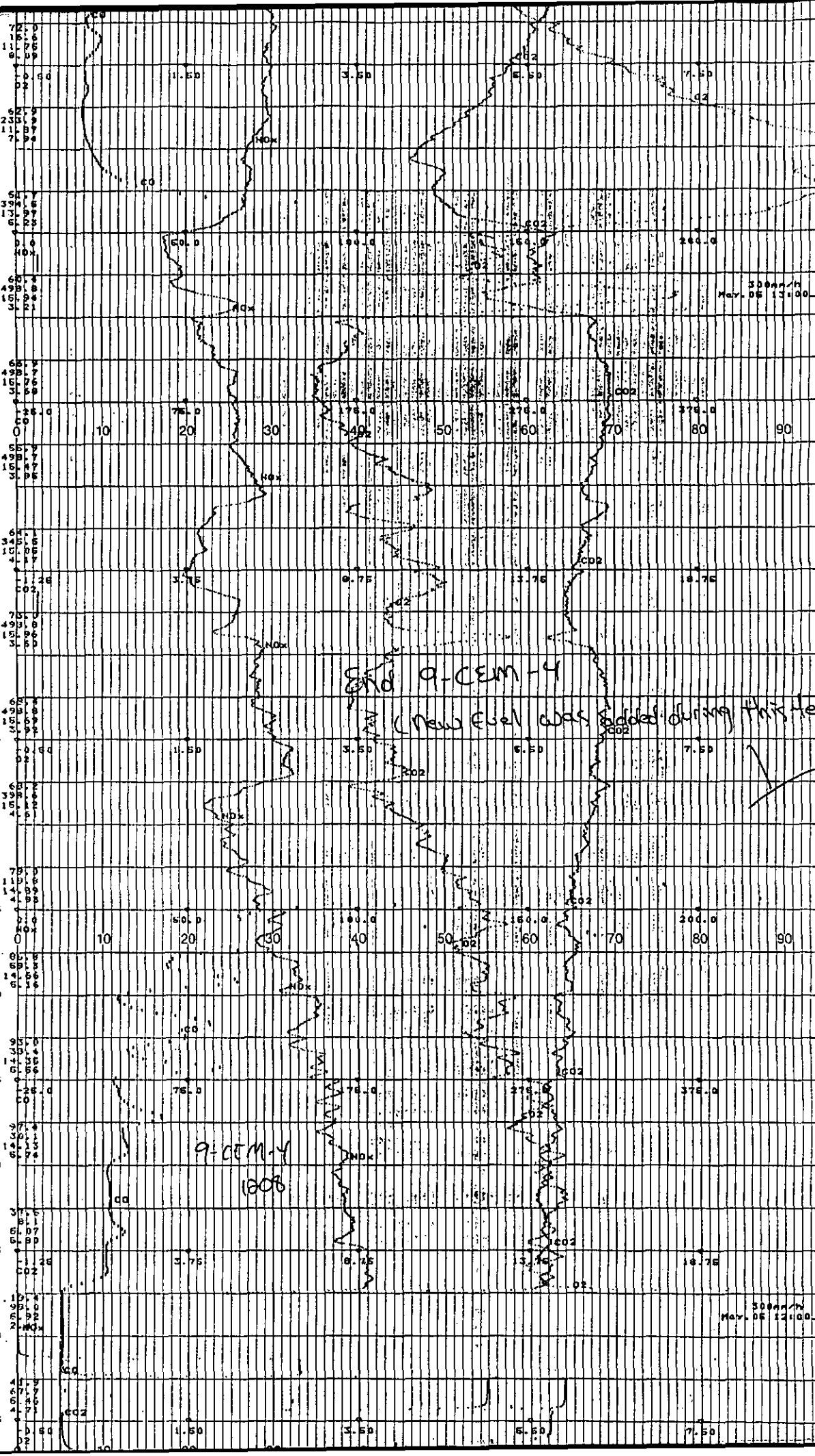
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May. 05 12:13
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CO2ANVL 14.13
O2ANVL 5.74
May. 05 12:08
INTVL 1

NOxAPPM 31.5
COAPPM 51.1
CO2ANVL 5.07
O2ANVL 5.80
May. 05 12:03
INTVL 1

NOxAPPM 10.4
COAPPM 991.0
CO2ANVL 5.92
O2ANVL 2.10
May. 05 11:58
INTVL 1

NOxAPPM 41.9
COAPPM 607.7
CO2ANVL 6.46
O2ANVL 4.71
May. 05 11:53
INTVL 1



NOxPPH 147.1
COxPPH 305.8
CO2xVVL 17.52
O2xVVL 6.10
May. 05 14:28
INTVL 1

NOxPPH 61.9
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CO2xVVL 9.82
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May. 05 14:23
INTVL 1

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COxPPH 27.5
CO2xVVL 14.06
O2xVVL 5.91
May. 05 14:18
INTVL 1

NOxPPH 105.2
COxPPH 29.1
CO2xVVL 13.90
O2xVVL 6.09
May. 05 14:13
INTVL 1

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COxPPH 30.4
CO2xVVL 12.74
O2xVVL 7.12
May. 05 14:08
INTVL 1

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COxPPH 15.7
CO2xVVL 9.96
O2xVVL 6.97
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INTVL 1

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CO2xVVL 0.02
O2xVVL 0.02
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INTVL 1

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COxPPH 0.13
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O2xVVL 0.08
May. 05 13:53
INTVL 1

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COxPPH 0.1
CO2xVVL 0.08
O2xVVL 0.08
May. 05 13:48
INTVL 1

NOxPPH 0.3
COxPPH 0.1
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May. 05 13:43
INTVL 1

NOxPPH 27.0
COxPPH 75.5
CO2xVVL 4.9
O2xVVL 2.06
May. 05 13:38
INTVL 1

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COxPPH 0.2
CO2xVVL 0.08
O2xVVL 0.08
May. 05 13:33
INTVL 1

NOxPPH 0.3
COxPPH 0.1
CO2xVVL 0.06
O2xVVL 0.06
May. 05 13:28
INTVL 1

NOxPPH 64.5
COxPPH 30.0
CO2xVVL 12.91
O2xVVL 4.90
May. 05 13:23
INTVL 1

NOxPPH 74.8
COxPPH 19.7
CO2xVVL 13.94
O2xVVL 6.98
May. 05 13:18
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COxPPH 18.0
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O2xVVL 6.09
May. 05 13:13
INTVL 1

NOxPPH 62.9
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O2xVVL 7.94
May. 05 13:08
INTVL 1

System Bias

As found

System Calibration

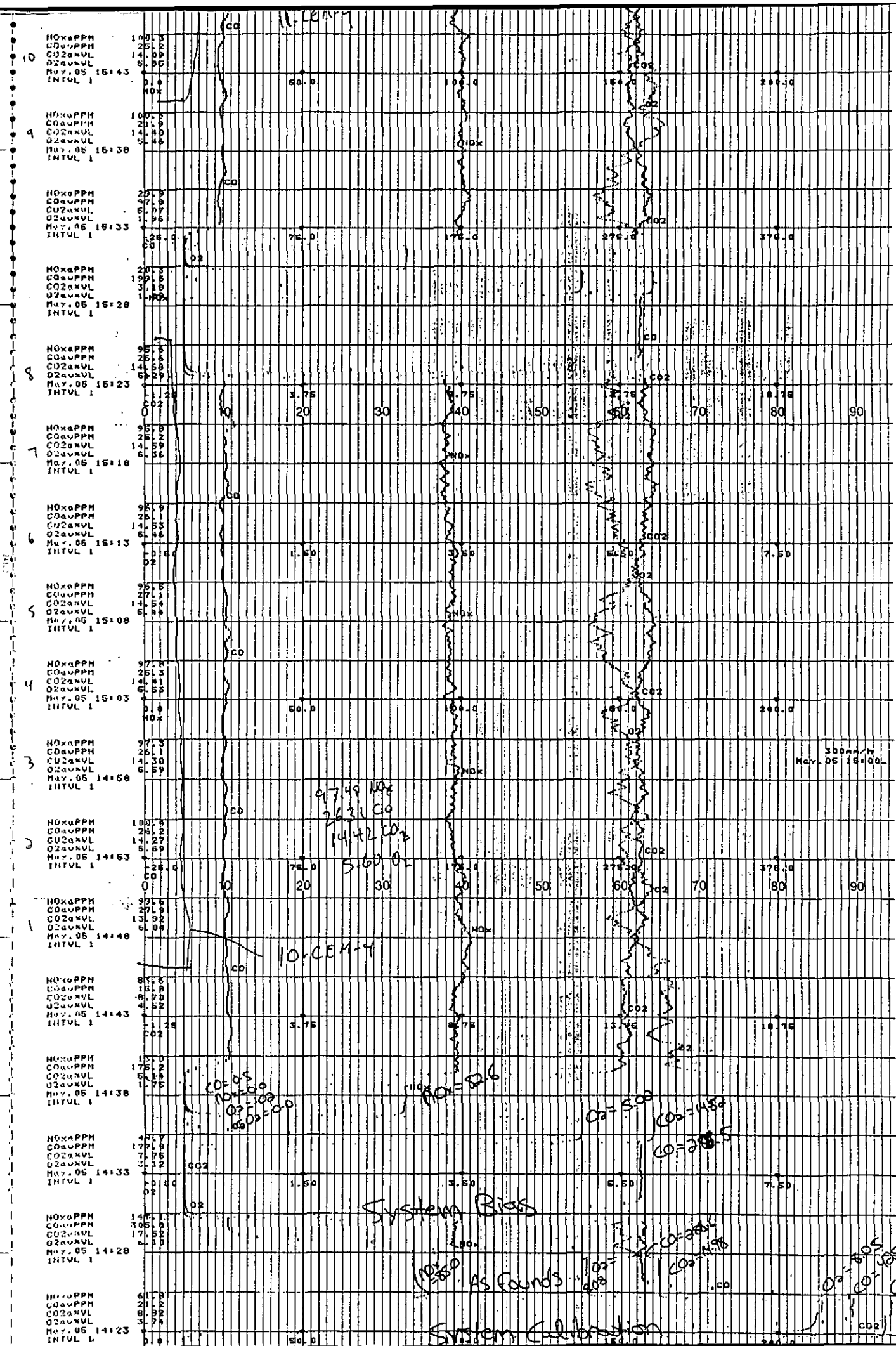
System Bias

CANNOT ES-26 Mobile GEN Lab

309ppm May. 05 14:00

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CO=498
CO2=4.7
O2=20.5



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COAPP
CO2APP
O2APP
May. 05 16:43
INTVL 1

NOxAPP
COAPP
CO2APP
O2APP
May. 05 16:38
INTVL 1

NOxAPP
COAPP
CO2APP
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May. 05 16:33
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May. 05 16:23
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May. 05 16:18
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INTVL 1

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May. 05 16:03
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May. 05 15:58
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May. 05 15:53
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May. 05 15:48
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May. 05 15:28
INTVL 1

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May. 05 15:23
INTVL 1

