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Blazer 39500201 5/22/89

~~3.13 1/4~~

105.22 $\frac{\text{ton}}{\text{hr.}}$, 101.02 $\frac{\text{ton}}{\text{hr.}}$, 91.36 $\frac{\text{ton}}{\text{hr.}}$

3.23 $\frac{\text{lb}}{\text{hr.}}$, 2.99 , 3.17

(PM)

controlled - no eff. given - front & back total

0317 $\frac{\text{lb}}{\text{hr.}}$

[A]

49.2 TPH

3.13 $\frac{\text{lb}}{\text{hr.}}$

1957/10 ...

... 1957/10 ...

... 1957/10 ...

[1] ...

... 1957/10 ...



UNITED STATES ENVIRONMENTAL PROTECTION AGENCY
REGION III

841 Chestnut Building
Philadelphia, Pennsylvania 19107

OCT 23 1989

SUBJECT: Stack Test Review of the Glasgow Company Plant #7 (Asphalt Plant)
Philadelphia, Pa.

CDS# 39-7160-01579

AFS 42-101-

FROM: Jim Gouvas 3ES-11
POS

TO: Susan Insetta, Chief 3AM-21
AEP&SC

THRU: Vic Guide, Chief 3ES-11
POS

A review of the stationary source stack sampling report titled "Source Emissions Compliance Test Report Asphaltic Aggregate Dryer Stack, Glasgow Company, Philadelphia, Pennsylvania June 1989" submitted by Roy F. Weston, Inc. (RFW) West Chester, Pa. has been completed.

The tests (EPA Method 5 & PaDER Back Half) was conducted on the Asphalt Plant Aggregate Dryer Stack May 22, 1989.

The Dryer Dryer Stack Particulate emissions are regulated by PaDER Regulation 123.13. The following is the EPA calculated Emission Standard by test run:

<u>Run #</u>	<u>Measured Emission Rate (lb/hr)</u>	<u>Allowable Emission Rate (lb/hr)</u>
#1	3.23	11.40
#2	2.99	11.20
#3	3.17	10.74

The Dryer Stack was in compliance with the PaDER emission standards for all test runs. (See the attachments for the emission rate compliance determination calculations)

I have reviewed the test report's field testing procedures, calculations, and quality assurance procedures. I have found them in agreement with procedures required by EPA/PaDER Test Methods. The calculations, as presented, appear to be correct and the test report acceptable in content. The attachments are comparisons of emission rate calculations made by the writer using the raw data from the report's field testing data sheets.

Attachments: 1. Emission Rate Calculation Comparisons (EPA vs RFW)
2. EPA-Emission Rate Compliance Determination Calculations

EMISSION RATE CALCULATION COMPARISONS

FACILITY: GLASSBORO COMPANY

PLACE: PHILADELPHIA, PA

CER#: 39-7160-01579

DATE OF TEST: 6-22-89

NSPS: NO

EIF SOURCE: YES

NEESHAF: NO

AUDIT SAMPLE: NO

PASS/FAIL: N/A

TESTING LAB: ROY F. NEETON, INC. (RFN)

ADDRESS: WEST CHESTER, PA

PHONE #: 215-692-3030

PROJECT #: 2373-01-02-0076

UNIT: ASPHALT AGGREGATE DRYER STACK
TEST METHOD: EPA METHOD 5 - PAPER BACK HALF
TEST DATA UNIT: lb/hr

TESTING PARAMETER: PARTICULATES

RUN NUMBER	1	2	2 AVERAGE	
EPA	3.23	2.99	3.17	3.13
RFN	3.23	2.99	3.19	3.17

TESTING PARAMETER: ISOKINETICS

RUN NUMBER	1	2	2
EPA	102.60	98.40	97.00
RFN	102.50	98.40	97.00

IN ACCEPTABLE RANGE (90-110%): YES

REGULATION: PAPER 123.13

EMISSION STANDARD CALCULATION: $A=0.765 \times 1.42$

$E=RFN$

$F=PROCESS FACTOR IN LB UNIT$

$F=1$

$Q=PROPORTION OF CHARGING RATE IN LB/HR$

$RFN \#1: W=115.13 TON/HR$

REPLY BY CLARENCE D. COOPER

PLC #2 0=101 TCV/HR

SA #7 REF. A TON/AS

EXCELLO: EXCELLENCE BY FIVE

$$R_{\text{eff}} = 1.46 \text{ g/g}$$

RUB #2 A= 11.20 LB/HF

SLN #3 4= 10.74 LE/yr

COMPLIANCE STATE BY REG. #

RUN #1 - IN COMPLIANCE

RUN #2- IN COMPLIANCE

FM #3-IN COMPLIANCE

EPA EMISSION RATE CALCULATION

FACILITY: BLANCK COMPANY
 LOCATION: ASPHALT PLANT #7
 CITY: PHILADELPHIA, PA
 USE# 33-7140-01579
 REGULATION: PADER 123.13

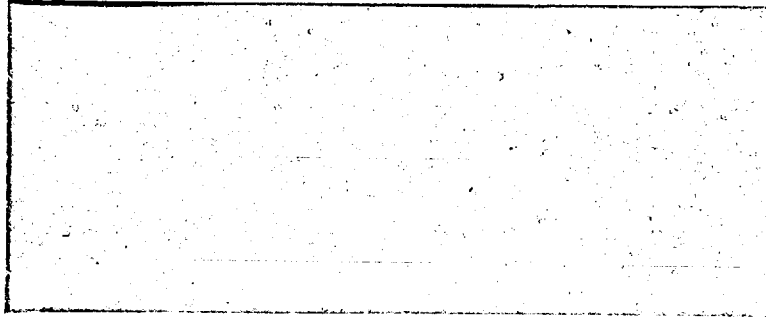
TEST METHOD: EPA METHOD 5 & PADER BACK HALF

DATE OF TEST: 5-22-89

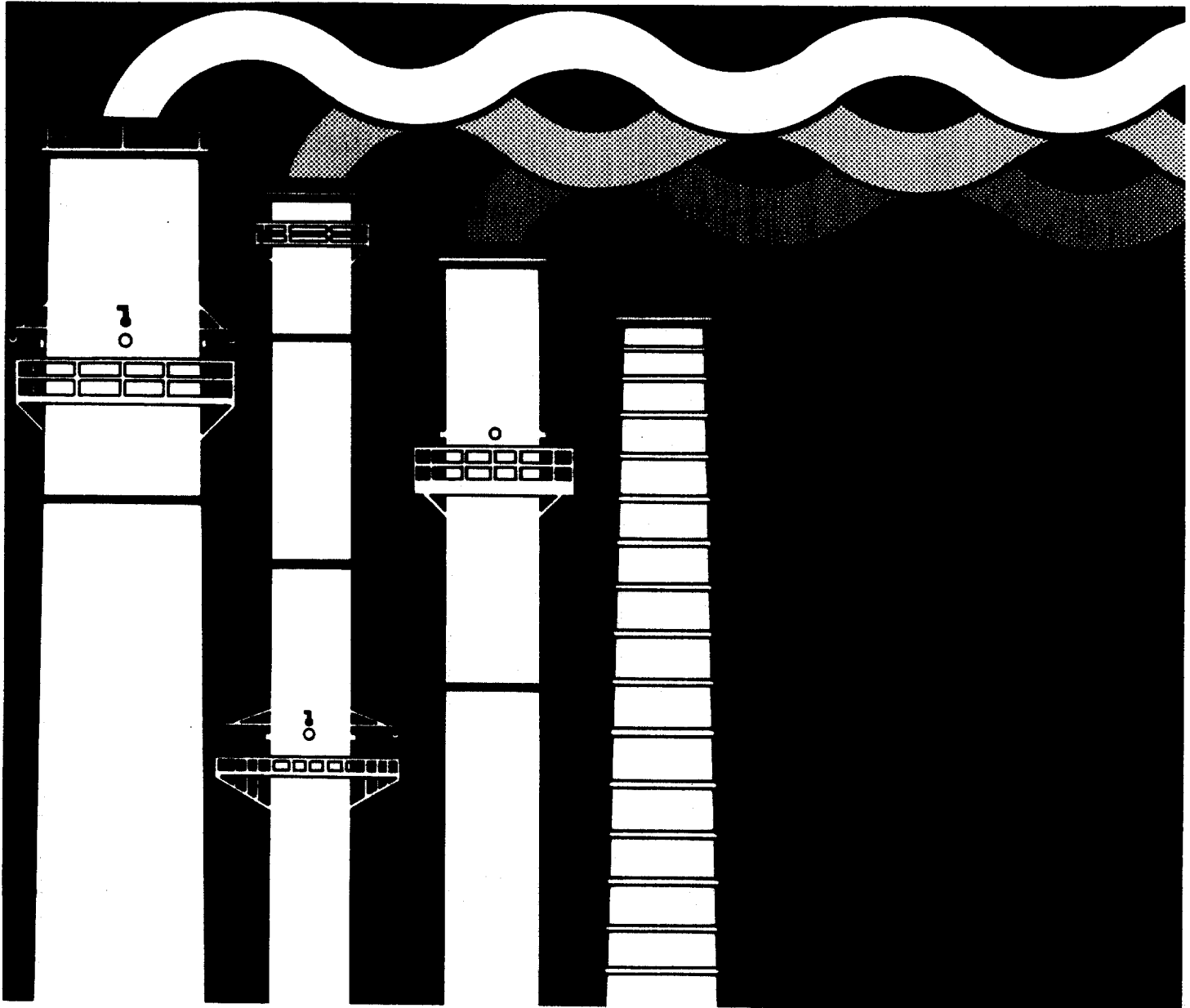
RUN #		1	2	4
NET SAMPLING TIME, T _{net}	min.	72	72	36
NOZZLE DIAMETER	in.	0.231	0.236	0.236
PISTON TUBE COEFFICIENT, C _p		0.84	0.84	0.84
GEOM. CAL. FACTOR, Y		1.003	1.003	1.003
BAROMETRIC PRESSURE	in.Hg.	29.96	29.96	29.96
METERED VOLUME, V _m	cu.ft.	50.237	52.205	26.72
METERED VOLUME, V _{m(Std)}	scf	49.139	50.618	25.975
METER TEMPERATURE	degF	84	89	89
WATER IN IMPINGERS, V _{ic}	ml.	153.5	124	49
PARTICULATE COLLECTED, M _p	mg.	66.5	61.7	32.2
FORMALDEHYDE COLLECTED	mg.			
STACK TEMPERATURE	degF	203	196	211
STACK DIAMETER	ft.	3.166	3.166	3.166
STATIC PRESSURE	in.Hg.	-0.019	-0.024	-0.046
STACK AREA	sq.ft.	7.88	7.88	7.88
% OXYGEN	%	16.5	16.9	17
% CARBON DIOXIDE	%	2.5	2.1	1.1
% MOISTURE	%	12.62	10.34	8.16
T _{me}	lb/mol	29.06	29.01	28.86
T _{me}	lb/mol	27.64	27.87	27.97
MEASURED BTU INPUT	Mbtu/hr	ERR	ERR	ERR
AVERAGE GH	in.Hg	1.66	1.71	1.65
AVERAGE BORT GH		0.854	0.953	0.676
F-FACTOR	scf/Mbtu	ERR	ERR	ERR
% EXCESS AIR	%			
% ISCHINETIC	%	102.5	98.4	97.0
SOURCE OPERATION DATA				
TOTAL AGGREGATE-F.R.	ton/hr	105.23	101	91.4
	lb/hr	210460	202000	182800
FLOW RATES				
-GRY, STD CONDITIONS	scfm	18034	18548	19305
	lb/hr	62968	65191	68190
-NET, ACTUAL CONDITIONS	scfm	25957	25665	26719
	lb/hr	90460	91237	93099
	ft ³ /min	3293	3239	3390
PARTICULATE EMISSION	gr/scf	0.0209	0.0123	0.0191
	lb/1000	0.1002	0.1073	0.2067

EPA EMISSION RATE CALCULATIONS

BTX TO	0.0000	0.0000	0.0000
10/00	0.0000	0.0000	0.0000



215-692-3630





SOURCE EMISSIONS COMPLIANCE TEST REPORT
ASPHALTIC AGGREGATE DRYER STACK
GLASGOW COMPANY
Philadelphia, Pennsylvania

JUNE 1989

WESTON PROJECT NO. 2373-01-02-0076

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1.0 SUMMARY

Glasgow Company contracted Roy F. Weston, Inc. (WESTON) to conduct a source testing and analysis program at its Philadelphia, Pennsylvania asphalt production facility. The primary objective of the program was to determine the particulate emissions compliance status of the Unit One asphalt aggregate dryer stack relative to the Pennsylvania Department of Environmental Resources (DER) allowable particulate emission limit for that source.

Testing procedures used during the survey conformed to U.S. Environmental Protection Agency (EPA) specifications modified as approved by the DER for application in Pennsylvania.

A summary of test results compared to the DER allowable emission concentration limits is presented in Table 1.

-
- 1 "Standards of Performance for New Stationary Sources," Code of Federal Regulations, Title 40, Part 60, Appendix A, Reference Methods.
 - 2 "Source Testing Manual", Pennsylvania Department of Environmental Resources, Revision No. 1, January 1983.

GLASGOW COMPANY
PHILADELPHIA, PENNSYLVANIA

TABLE 1
SUMMARY OF PARTICULATE COMPLIANCE TEST RESULTS
ASPHALTIC AGGREGATE DRYER STACK

TEST NUMBER	TEST DATE	PERIOD	MEASURED CONCENTRATION GR/DSCF ¹	MASS EMISSION RATE	
				MEASURED LB/HR	PADER Allowable ² LB/HR
One	5/22/89	0925 - 1043	0.021	3.23	11.40
Two	5/22/89	1200 - 1317	0.019	2.99	11.21
Three	5/22/89	1427 - 1503	0.019	3.16	10.74
Series Average	---	---	0.020	3.13	11.12

¹ gr/dscf = grains per dry standard cubic foot at standard conditions of 68°F and 29.92 inches mercury.

² Based on PADER Allowable Particulate Emission Rate Formula (PER), process charge rate (W) and process charge factor (F): $PER = 0.76E^{0.42}$; $E = F \times W$, where, $F = 6$ lb/ton and $W = 105.2$, 101.0 and 91.4 tons/hr respectively.



2.0 INTRODUCTION

The Glasgow Company retained WESTON to conduct a source testing and analysis program at its Philadelphia, Pennsylvania asphalt production facility. The primary objective of the program was to determine the concentration and mass rate of particulate emissions from the Unit One aggregate dryer stack for comparison with the Pennsylvania Department of Environmental Resources (DER) allowable limit for that source.

WESTON's Air Quality Testing Services personnel performed the particulate emission testing on the dryer stack on May 22, 1989.

The particulate tests were performed according to EPA procedures, modified as approved by the DER for application in Pennsylvania.

A summary of the compliance test results compared to DER allowable emission concentrations and mass emission rates are presented in Table 1 of Section 1. Detailed test data and results are presented in Table 2, Section 7, of this report. Descriptions of the test location, test equipment, test procedures, sample recovery techniques and analytical methods used during the survey are also included herein. Raw test data, laboratory reports, sample calculations, process operations data, equipment calibration records and a list of WESTON project participants are provided in Appendices A through F, respectively.

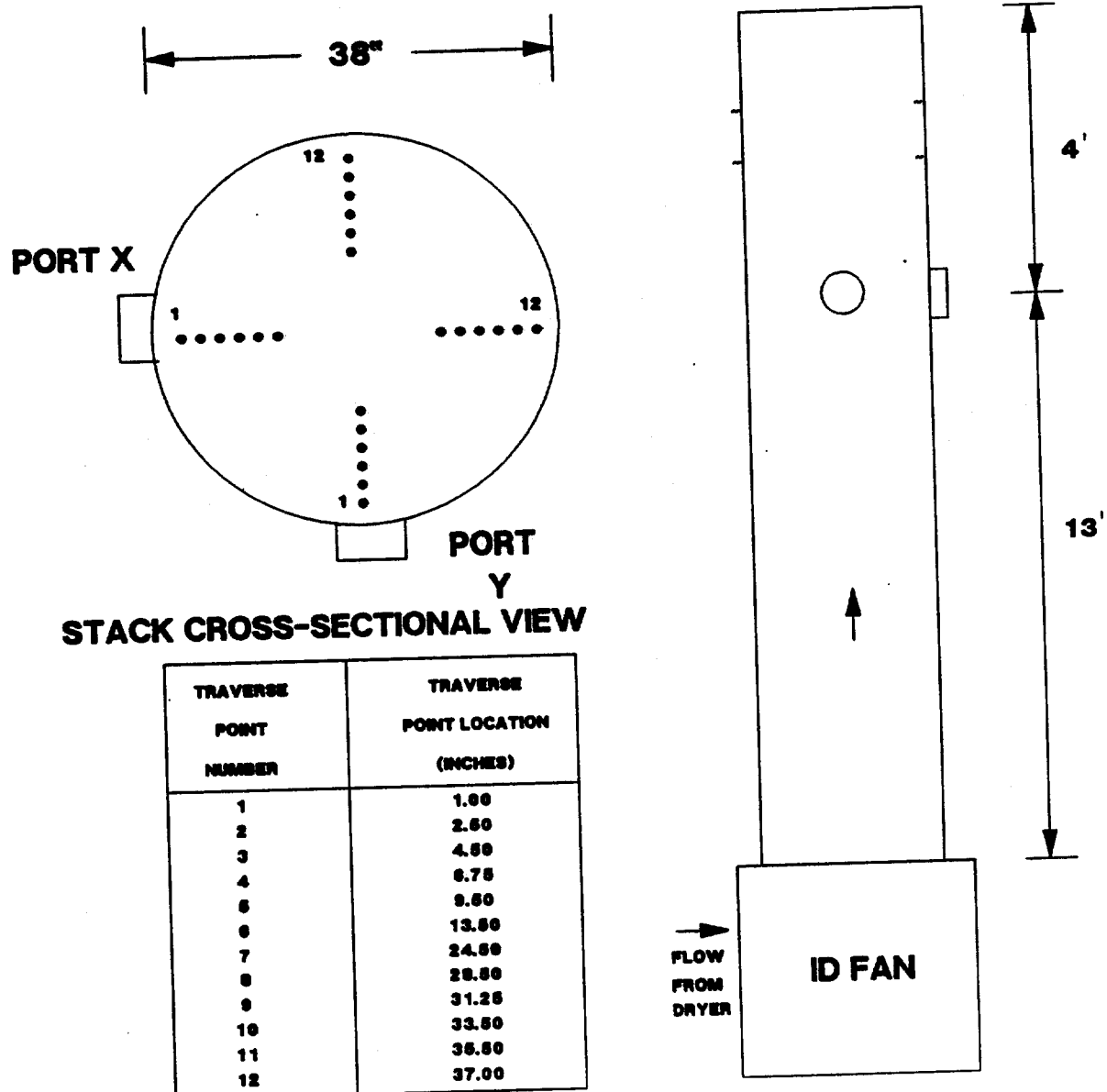


3.0 DESCRIPTION OF TEST LOCATION

Unit One Asphalt Aggregate Dryer Stack

Two 3-inch ID test ports, 90° apart, were installed in a straight section of the metal (38" ID) stack. The ports were placed > 4 diameters downstream from the ID fan discharge and > 1 diameter upstream from the stack discharge point. Twenty four traverse points (12 per port) were selected based on the minimum requirements of EPA Reference Method 1 to permit representative sampling at this test location. Figure 1 illustrates test port placement and traverse point locations.

**GLASGOW COMPANY
PHILADELPHIA, PA**



**FIGURE 1
ASPHALTIC AGGREGATE DRYER
PORT AND TRAVERSE POINT LOCATIONS**

4.0 DESCRIPTION OF SAMPLING TRAIN

Particulate

The sampling train utilized to perform the particulate sampling was an EPA Reference Method 5 train (see Figure 2).

A calibrated stainless steel nozzle was attached to a heated (~250°F) 4 ft. borosilicate probe. The probe was connected to a heated 250°F borosilicate filter holder containing a 9-cm Reeve Angel 934 AH glass fiber filter (preweighed to a constant 0.1 mg weight). The first and second impingers each contained 100 ml of distilled water, the third impinger was dry, and the fourth impinger contained 300 grams of dry preweighed silica gel. The second impinger was a standard Greenburg-Smith type; the first, third, and fourth were of a modified design. All impingers were maintained in a crushed ice bath. A Nutech control console with a leakless vacuum pump, a calibrated dry gas meter, a calibrated orifice, and inclined manometers were connected to the final impinger via an umbilical cord to complete the train.

Flue gas velocity was measured with a calibrated "S" type pitot tube (provided with extensions) fastened on the sampling probe. Flue gas temperature was monitored with a calibrated direct readout pyrometer equipped with a chromel-alumel thermocouple positioned near the sampling nozzle. Filter box and impinger exit gas temperatures were monitored with a calibrated direct readout pyrometer equipped with chromel-alumel thermocouples positioned in the heated filter chamber and in the sample gas stream after the last impinger. Stack gas stream composition (carbon dioxide, oxygen, and carbon monoxide content) was determined utilizing an Orsat apparatus to analyze multi-point integrated samples of the flue gas for each test period.

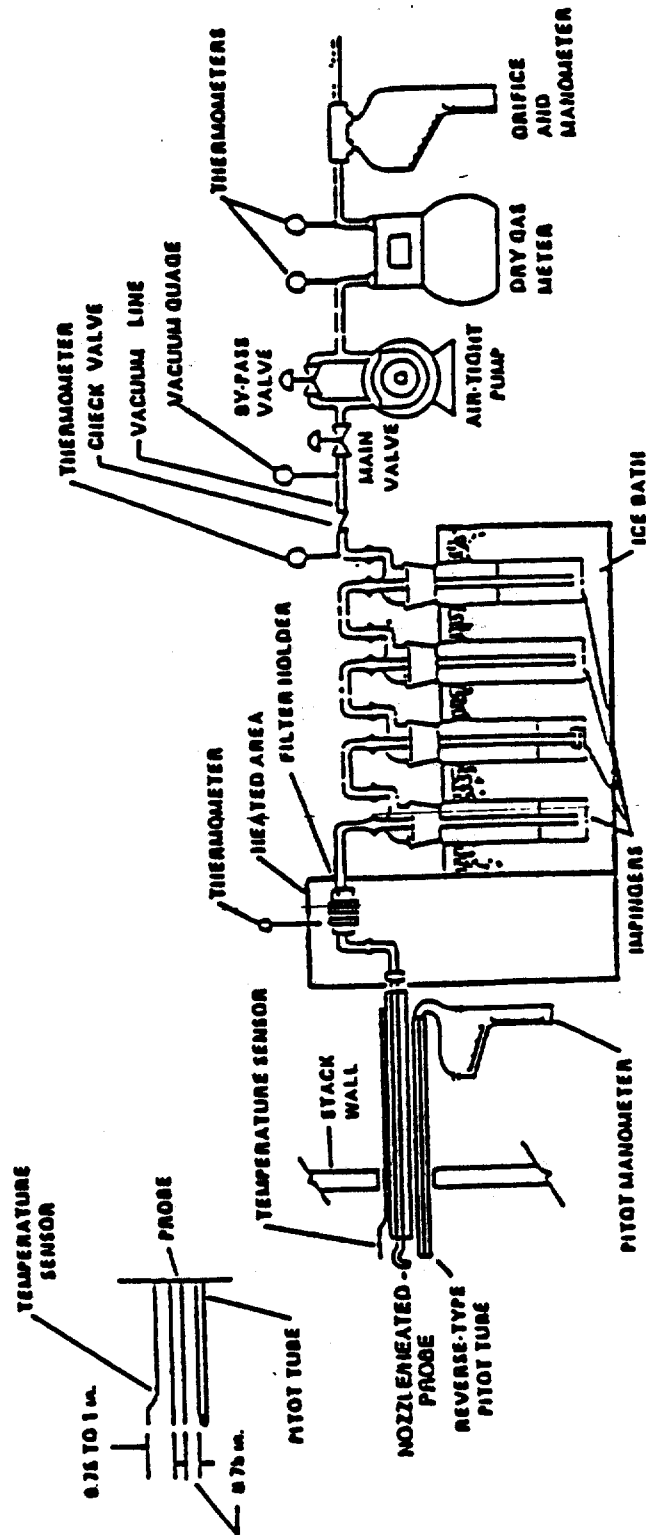


FIGURE 2
Particulate Sampling Train
EPA Reference Method 5

5.0 TEST PROCEDURES

5.1 PRELIMINARY TESTS

Preliminary test data was obtained at the stack sampling location. Stack geometry measurements were recorded, and traverse point distances calculated. A preliminary velocity traverse was performed at the location utilizing a calibrated "S"-type pitot tube and a Dwyer inclined manometer to determine velocity profiles. Flue gas temperatures were observed with a calibrated direct readout pyrometer equipped with a chromel-alumel thermocouple. Water content was measured by conducting an EPA Reference Method 4 moisture test.

A check for the presence or absence of cyclonic flow was conducted at the test location prior to formal testing. The cyclonic flow check proved to be negative ($\alpha < 20$) thus verifying the suitability of the test site for obtaining representative samples.

Preliminary test data was used for nozzle sizing and nomograph set-up for isokinetic sampling procedures. Calibration of probe nozzles, pitot tubes, metering systems, probe heaters, and temperature gauges was performed as specified in Section 5 of EPA Reference Method 5 test procedures (see Appendix D for calibration records).

5.2 FORMAL TESTS

A total of three particulate test runs were conducted on the stack during the test program.

Sampling for the first two tests consisted of twenty four traverse points, 12 per port axis. Readings were taken every two and one half minutes at each traverse point, resulting in a total test



length of 72 minutes. The third test was shortened due to the reduced production schedule. Only 12 traverse points were sampled along one axis for a test length of 36 minutes.

During particulate sampling, gas stream velocities were measured by inserting a calibrated "S"-type pitot tube into the stream adjacent to the sampling nozzle. The velocity pressure differential was observed immediately after positioning the nozzle at each point, and the sampling rate was adjusted to maintain isokineticity. Flue gas temperatures were monitored at each point with the pyrometer and thermocouple. Multi-point integrated samples of the flue gas were collected during each test for Orsat analysis.

Temperature measurements were made at the filter holder chamber, the final impinger exit, and at the dry gas meter. Leak checks were performed as per EPA Reference Method 5 instructions prior to and after each run and/or port change.

6.0 ANALYTICAL PROCEDURES

Complete laboratory results are presented in Appendix B of this report.

6.1 PARTICULATE SAMPLE RECOVERY

At the conclusion of each test, the sampling train was dismantled, openings sealed, and the components transported to the field laboratory. Sample integrity was assured by maintaining chain-of-custody records.

A consistent procedure was employed for sample recovery as follows:

- o The glass fiber filter(s) was removed from its holder with tweezers and placed in its original container (petri dish), along with any loose particulate and filter fragments (Sample 1).
- o The probe and nozzle were separated and the particulate rinsed with distilled water into a borosilicate container with a teflon-lined closure while brushing a minimum of three times. Particulate adhering to the brush was rinsed with distilled water into the same container. The front-half of the filter holder and connecting glassware were rinsed with distilled water while brushing a minimum of three times. The rinses were combined (Sample 2).
- o The sampling train components in the previous step were acetone rinsed and brushed in like manner and the particulate rinsed into a borosilicate container with a teflon-lined lid (Sample 3).



- o The total liquid content of impingers one, two and three was measured volumetrically and the sample placed in a borosilicate container fitted with a teflon-lined closure (Sample 4). Also included in this sample was a distilled water rinse of the impingers and connectors.
- o The components from the previous step were acetone washed and the sample was placed into a separate borosilicate container with a teflon-lined lid (Sample 5).
- o The silica gel was removed from the last impinger and immediately weighed to the nearest 0.5 g.
- o Samples of acetone and distilled water were retained for blank analysis.

Each sample bottle was level to clearly identify its contents. The height of the fluid was marked on each bottle. The samples were then placed in a locked shipping crate prior to transport to the WESTON laboratories.

6.2 PARTICULATE ANALYSIS

The particulate analysis proceeded as follows:

- o The filters (Sample 1) and any loose fragments were desiccated for 24-hours and weighed to the nearest 0.1 milligram to a constant ($\pm 0.5\text{mg}$) weight.
- o The front-half water and back-half impinger contents and water wash samples (Samples 2 and 4) were filtered separately using pre-weighed 0.22 micron membrane filters. The membrane filters were desiccated for 24 hours and weighed to the nearest 0.1 milligram to a

constant ($\pm 0.5\text{mg}$) weight. The resulting filtrates, along with a distilled water blank, were evaporated in an oven at 100°C in tared beakers, then desiccated to constant 0.1-mg weight.

- o The front-half and back-half acetone wash samples (Samples 3 and 5, respectively) and an acetone blank were evaporated at ambient temperature and pressure in tared beakers, then desiccated to constant 0.1-mg weight.

The total weight of material measured in the front-half water-soluble, water-insoluble, and acetone-rinse fractions, plus the weight of material collected on the glass fiber filter, plus the back-half insoluble fraction represents the "total" Pennsylvania particulate catch for each train (see Table 2). Blank corrections were made where appropriate for all sample weights.

The back-half water soluble and acetone soluble catch fractions are reported, but the weights are not included in the emission calculations.



7.0 TEST RESULTS AND DISCUSSION

A summary of compliance test results is presented in Table 1, page 2 of this report. Detailed test data and test results summaries are included in Table 2 of this section.

The third test was shortened to only 12 traverse points along one axis for a total sampling time of 36 minutes. The test was shortened due to a limited amount of production needed on the day of testing. It should also be noted that during this third test there was a mechanical problem resulting in an interruption of production for approximately 8 minutes during sampling.

A representative of the City of Philadelphia Air Management Services Department was present to observe the testing.

All test data and test results shown herein are believed to be representative of process emissions encountered during the survey periods except for the process incongruities noted during the third test. No other process, sampling or analytical difficulties were noted during the test periods.

The average concentration measured during the program was 0.020 gr/dscf. The average particulate mass emission rate measured was 3.13 lbs/hr which was below the calculated average DER allowable limit of 11.12 lbs/hr.

GLASGOW COMPANY
PHILADELPHIA, PA

TABLE 2

SUMMARY OF PARTICULATE TEST DATA AND TEST RESULTS
ASPHALTIC AGGREGATE DRYER STACK

TEST DATA:

	1	2	3
Test run number		UNIT 1 DRYER STACK	
Test location			
Test date	5-22-89	5-22-89	5-22-89
Test time period	0925-1043	1200-1317	1427-1503

SAMPLING DATA:

Sampling duration, min.	72.0	72.0	36.0
Nozzle diameter, in.	0.231	0.236	0.236
Cross sectional nozzle area, sq.ft.	0.000291	0.000304	0.000304
Barometric pressure, in. Hg	29.96	29.96	29.96
Avg. orifice press. diff., in H2O	1.56	1.71	1.85
Avg. dry gas meter temp., deg F	84	89	89
Avg. abs. dry gas meter temp., deg. R	544	549	549
Total liquid collected by train, ml	153.5	124.0	49.0
Std. vol. of H2O vapor coll., cu.ft.	7.2	5.8	2.3
Dry gas meter calibration factor	1.003	1.003	1.003
Sample vol. at meter cond., dcf	50.237	52.205	26.780
Sample vol. at std. cond., dscf (1)	49.122	50.599	25.973
Percent of isokinetic sampling	102.5	98.4	97.0

GAS STREAM COMPOSITION DATA:

CO2, % by volume, dry basis	2.5	2.1	1.1
O2, % by volume, dry basis	16.5	16.9	17.0
CO, % by volume, dry basis	0.0	0.0	0.0
N2, % by volume, dry basis	80.9	81.0	81.9
Molecular wt. of dry gas, lb/lb mole	29.07	29.02	28.86
H2O vapor in gas stream, prop. by vol.	0.128	0.103	0.082
Mole fraction of dry gas	0.872	0.897	0.918
Molecular wt. of wet gas, lb/lb mole	27.6	27.9	28.0

GAS STREAM VELOCITY AND VOLUMETRIC FLOW DATA:

Static pressure, in. H2O	-0.26	-0.33	-0.65
Static pressure, in. Hg	-0.019	-0.024	-0.048
Absolute pressure, in. Hg	29.94	29.94	29.91
Avg. temperature, deg. F	203	196	211
Avg. absolute temperature, deg.R	663	656	671
Pitot tube coefficient	0.84	0.84	0.84
Total number of traverse points	24	24	12
Avg. gas stream velocity, ft./sec.	54.9	54.3	56.5
Stack/duct cross sectional area, sq.ft.	7.88	7.88	7.88
Avg. gas stream volumetric flow, wacf/min.	25900	25700	26700
Avg. gas stream volumetric flow, dscf/min.	18000	18500	19300

LABORATORY PARTICULATE REPORT:

Frt-half acetone rinse, g	0.0050	0.0065	0.0040
Frt-half water sol., g	0.0073	0.0063	0.0066
Frt-half water insol., g	0.0206	0.0111	0.0050
Filter, g	0.0308	0.0366	0.0160
Back-half water insol., g	0.0028	0.0012	0.0006
Back-half water sol., g	0.0169	0.0238	0.0066
Back-half acetone rinse, g	0.0042	0.0028	0.0025
Total catch weight, g	0.0876	0.0883	0.0413
Total Ps. part. catch, g(2)	0.0665	0.0617	0.0322

PARTICULATE EMISSIONS:(3)

Concentration, gr/dscf	0.021	0.019	0.019
Mass rate, lbs/hr	3.23	2.99	3.16

SOURCE OPERATIONS DATA

Total aggregate, ton/hr	105.2	101.0	91.4
Total aggregate, lb/hr	210431	202036	182717

(1) Standard conditions = 68 deg. F. (20 deg. C.) and 29.92 inches Hg (760 mm Hg)

(2) Pennsylvania DER particulate catch does not include back-half water soluble and back-half acetone rinse catch fractions.

(3) Based on Pennsylvania catch weight

APPENDIX A

RAW TEST DATA

CLIENT: GLASGOW
FACILITY: PHILADELPHIA TR
TEST LOCATION: STAIR
TEST RUN NO.: 1, 2, 3
TEST DATE: 5/22/84

ROY F. WESTON, INC.

EMISSION TEST DATA/REPORT
QA/QC CHECK LIST

Raw Test Data	Initial Data Averages <u>SK</u>	Data Check 1 <u>BS</u>	Data Check 2 (if req'd) <u>JDO</u>	Data Completeness Check <u>✓</u>
Laboratory Data	Initial Lab Calculator <u>BS</u>	Check 1 <u>PM</u>	Check 2 (if req'd) _____	Data Completeness Check <u>✓</u>
Test Result Calculations	Initial Calculator <u>SK</u>	Check 1 <u>BS</u>	Check 2 (if req'd) <u>JM</u>	Reasonable-ness Check <u>✓</u>
Test Data Tables	Author <u>BS</u>	Check 1 <u>JM</u>	Check 2 (if req'd) <u>JDO</u>	Completeness Reasonable-ness Check <u>✓</u>
Report Body	Author <u>JM</u>	Check 1 <u>JM</u>	Check 2 (if req'd) <u>JDO</u>	Table of Contents, Figure, page number Check <u>✓</u>
Appendices Completeness	Originator <u>JM</u>	Check 1 <u>JDO</u>	Check 2 (if req'd) <u>PMM</u>	
Compilation Check: Page alignment and completeness			Date provided to Client	
Draft Report (if required)			<u>6/16/89</u>	
Final Report <u>✓</u>				
Final Report Review:	PD <u>BS</u>	PM <u>BS</u>		
	SM/DM _____			

GLASGOW
Philadelphia, Pa.

Test Data	1	2	3
Run number		Unit 1 DRYER STACK	
Location			
Date	5-22-89	5-22-89	5-22-89
Time period	0925-1043	1200-1317	1427-1503
Operator	Mills/Marz	Mills/Marz	Mills/Marz

Inputs For Calcs.	0.853903	0.853040	0.878468
Sq. rt. delta P	1.55917	1.71417	1.85167
Delta H	202.71	196.25	211.00
Stack temp. (deg.F)	84.19	89.21	89.04
Meter temp. (deg.F)	50.237	52.205	26.780
Sample volume (act.)	29.96	29.96	29.96
Barometric press. (in.Hg)	128.00	106.00	39.00
Volume H2O imp. (ml)	25.50	18.00	10.00
Weight chnge sil. gel (g)	2.530	2.130	1.130
% CO2	16.530	16.870	17.000
% O2	0.000	0.000	0.000
% CO	80.940	81.000	81.870
% N	7.88	7.88	7.88
Area of stack (sq.ft.)	72.00	72.00	36.00
Sample time (min.)	-0.26	-0.33	-0.65
Static pressure (in.H2O)	0.231	0.236	0.236
Nozzle dia. (in.)	1.0030	1.0030	1.0030
Meter box cal.	0.84	0.84	0.84
Cp of pitot tube			

Laboratory Report Data	0.00500	0.00650	0.00400
Frt half acetone rinse, g	0.00730	0.00630	0.00660
Frt half water sol., g	0.02060	0.01110	0.00500
Frt half water incl., g	0.03080	0.03660	0.01600
Filter, g	0.00280	0.00120	0.00060
Back-half water incl., g	0.01690	0.02380	0.00660
Back-half water sol., g	0.00420	0.00280	0.00250
Back-half acetone., g			

5. Dry molecular weight of gas stream, lb/lb-mole.

$$MW_d = 0.440(\% CO_2) + 0.320(\% O_2) + 0.280(\% N_2 + \% CO)$$

$$MW_d = (0.440 \times 2.53) + (0.320 \times 16.53) + (0.280 (80.94 + 0))$$

$$= 29.066$$

Where:

MW_d = Dry molecular weight, lb/lb-mole.

$\%CO_2$ = Percent carbon dioxide by volume, dry basis.

$\%O_2$ = Percent oxygen by volume, dry basis.

$\%N_2$ = Percent nitrogen by volume, dry basis.

$\%CO$ = Percent carbon monoxide by volume, dry basis.

0.440 = Molecular weight of carbon dioxide, divided by 100.

0.320 = Molecular weight of oxygen, divided by 100.

0.280 = Molecular weight of nitrogen or carbon monoxide, divided by 100.

6. Actual molecular weight of gas stream (wet basis), lb/lb-mole.

$$MW_s = (MW_d \times M_d) + 18 (1 - M_d)$$

$$MW_s = 29.07 \times .872 + 18 (1 - .872)$$

$$= 27.65$$

Where:

MW_s = Molecular weight of wet gas, lb/lb-mole.

18 = Molecular weight of water, lb/lb-mole.

7. Average velocity of gas stream at actual conditions, ft/sec.

$$V_s = 85.49 \times C_p \times (\sqrt{\Delta P})_{avg} \times \left[\frac{T_s (avg)}{P_s \times MW_s} \right]^{\frac{1}{2}}$$

Where:

- $V_{w(std)}$ = Volume of water vapor in the gas sample corrected to standard conditions, scf.
- V_{wc} = Volume of liquid condensed in impingers, ml.
- W_{wsg} = Weight of water vapor collected in silica gel, g.
- 0.04707 = Factor which includes the density of water (0.002201 lb/ml), the molecular weight of water (18.0 lb/lb-mole), the ideal gas constant 21.85 (in. Hg) (ft³)/(lb-mole)(°R); absolute temperature at standard conditions (528°R), absolute pressure at standard conditions (29.92 in. Hg), ft³/ml.
- 0.04715 = Factor which includes the molecular weight of water (18.0 lb/lb-mole), the ideal gas constant 21.85 (in. Hg) (ft³)/(lb-mole)(°R), absolute temperature at standard conditions (528°R), absolute pressure at standard conditions (29.92 in. Hg), and 453.6 g/lb, ft³/g.

3. Moisture content.

$$B_{ws} = \frac{V_{w(std)}}{V_{w(std)} + V_{m(std)}}$$

$$B_{ws} = \frac{7.23}{7.23 + 49.122} = 0.128 \text{ or } 12.8\%$$

Where:

- B_{ws} = Proportion of water vapor, by volume, in the gas stream, dimensionless.

4. Mole fraction of dry gas.

$$M_d = 1 - B_{ws}$$

$$M_d = 1 - 0.128 = 0.872$$

Where:

- M_d = Mole fraction of dry gas, dimensionless

EPA METHOD 5
PARTICULATE SAMPLE CALCULATIONS

Client GLASGOW

Plant Philadelphia

Test Run No. ONE

Test Date 5/22/89

Test Location Aggregate Dryer ONE

Test Period 0925-1043

1. Volume of dry gas sampled at standard conditions (68°F, 29.92 in. Hg), dscf.

$$V_{m(std)} = \frac{17.64 \times Y \times V_m \times (P_b + \frac{\Delta H}{13.6})}{(\bar{T}_m + 460)}$$

$$V_{m(std)} = \frac{17.64 \times 1.003 \times 50.237 \times (29.96 + \frac{1.559}{13.6})}{(84.19 + 460)} = 49.122$$

Where:

- $V_{m(std)}$ = Volume of gas sample measured by the dry gas meter, corrected to standard conditions, dscf.
- V_m = Volume of gas sample measured by the dry gas meter at meter conditions, dcf.
- P_b = Barometric pressure, in. Hg.
- ΔH = Average pressure drop across the orifice meter, in. H₂O.
- $\bar{T}_m$ = Average dry gas meter temperature, °F.
- Y = Dry gas meter calibration factor.
- 17.64 = Factor that includes ratio of standard temperature (528°R) to standard pressure (29.92 in. Hg), °R/in. Hg.
- 13.6 = Specific gravity of mercury.

2. Volume of water vapor in the gas sample corrected to standard conditions, scf.

$$V_{w(std)} = (0.04707 \times V_{wc}) + (0.04715 \times W_{wsg})$$

$$V_{w(std)} = (0.04707 \times 128) + (0.04715 \times 25.5) = 7.23$$

APPENDIX C

SAMPLE CALCULATIONS

0.22µm multiplex filter

Stack # 1

Run #1

ETHD

470

0.6689

0.0800

0.6111

BHND

495

0.0889

0.0917

0.0628

ETHD

420

0.5702

0.0908

0.0206

ISV

raw wt. / final wt.

Δ wt

Run #2

BHND

495

0.0822

0.0894

0.012

ETHD

470

0.0694

0.0744

0.0030

BHND

420

0.0834

0.0890

0.0006

Run #3

H₂O Blank

275

0.0886

0.0886

0.0000

Plant Glasgow Test Date 5-22-89 Test Period Stack # 1 Analyst NO Run # 002 Date 5-30-87
 Test Date 5-22-89 Test Period Stack # Process #

8905L 425-

Begker	Volume	TGFA(1)	TGFA(2)	True Avg.	Final(1)	Final(2)	Final Avg.	Δ wt.	Net Wt.
S-8	310	115.3275	115.3275	115.3275	115.3329	115.3329	115.3329	.0054	.0054
9600		.3118	.3118	.3117	.4220	.4220	.4220	.0308	.0308
3-12	300	115.1035	115.1035	115.1037	115.1145	115.1147	115.1146	.0057	.0057
S-14	300	116.8769	116.8769	116.8769	116.8877	116.8881	116.8879	.0110	.0110
S-9	135	115.7296	115.7296	115.7296	115.7340	115.7340	115.7340	.0044	.0044
FM TOTAL									
BHM									
CHA									
TOTAL									

Comments

Plant Glasgow Sampling Location Stack # 1 Run # Two Process #
 Test Date 5-22-89 Test Period

Begker	Volume	TGFA(1)	TGFA(2)	True Avg.	Final(1)	Final(2)	Final Avg.	Δ wt.	Net Wt.
S-3	300	113.3780	113.3790	113.3790	113.3858	113.3858	113.3858	.0068	.0068
9642		.3258	.3258	.3259	.4297	.4295	.4296	.0367	.0367
S-11	300	117.1842	117.1845	117.1843	117.1889	117.1893	117.1891	.0048	.0048
S-10	300	118.4194	118.4194	118.4194	118.4276	118.4296	118.4296	.0152	.0152
S-4	185	116.5312	116.5310	116.5311	116.5341	116.5341	116.5341	.0030	.0030
FM TOTAL									
BHM									
BHA									
TOTAL									

Comments

Plant Glasgow Sampling Location Stack # 1 Run # Three Process #
 Test Date 5-22-89 Test Period

Begker	Volume	TGFA(1)	TGFA(2)	True Avg.	Final(1)	Final(2)	Final Avg.	Δ wt.	Net Wt.
S-5	400	115.5221	115.5221	115.5221	115.5266	115.5266	115.5266	.0043	.0043
9674		.3881	.3881	.3881	.4044	.4040	.4042	.0161	.0161
S-1	300	117.8472	117.8472	117.8472	117.8521	117.8521	117.8521	.0050	.0050
S-13	300	115.5344	115.5344	115.5344	115.5399	115.5399	115.5399	.0055	.0055
S-6	185	116.2070	116.2070	116.2070	116.2097	116.2097	116.2097	.0027	.0027
FM TOTAL									
BHM									
BHA									
TOTAL									

Comments

003 ACETONE BLK S-7 175 117.3067 117.3067 117.3067 117.3067 117.3067 117.3067 0.0002
 002 WATER BLK S-15 275 116.9059 116.9059 116.9059 116.9059 116.9059 116.9059 0.0007
 001 Filter Bk 1103 116.9059 116.9059 116.9059 116.9059 116.9059 116.9059 0.0005
 FMA=Front half acetone wash BHM=Back half water (Impinger contents + water wash) BHA=Back half acetone wash FM TOTAL=Front half catch weight TOTAL=Total train catch weight

WESTON Analytics Use Only
89056425
Client <u>645605</u>
Work Order <u>2373-01-02</u>
Date Rec'd. <u>5/23/89</u> Date Due <u>1</u>
ARFV Contact <u>Act M.L.S.</u>
Client Contact/Phone _____

Client ID/Description	Client ID	Client Name	Client Address	Client City	Client State	Client Zip	Client Phone	Client Email	Client Website	Client Notes
014	Run 3	Front HSE	H2O							
015	Run 3	Front HSE	Acetone							
016	Run 3	Back HSE	H2O							
017	Run 3	Back HSE	Acetone							
018	Run 3	Front HSE	H2O							
019	Run 3	Front HSE	Acetone							

Special Instructions:

Marin:	W - Water	DS - Drum Solids
S - Soil	O - Oil	DL - Drum Liquids
SE - Sediment	A - Air	F - Fish
SO - Solid	WI - Wipe	X - Other

[illegible]

WESTON Analytics Use Only Samples Were: 1 Shipped or Hand-Delivered ☒ NOTES: 2 Ambient or Chilled ☒ NOTES: 3 Received Broken/Leaking (Improperly Sealed) ☒ NOTES: 4 Properly Preserved ☒ NOTES: 5 Received Within Holding Times ☒ NOTES:	COC Tape Was: 1 Present on Outer Package ☒ 2 Unbroken on Outer Package ☒ 3 Present on Sample ☒ 4 Unbroken on Sample ☒ NOTES:	COC Record Was: 1 Present Upon Receipt of Samples ☒ Discrepancies Between Sample Labels and COC Record? ☒ NOTES:
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ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 06/09/89

CLIENT: GLASGOW
WORK ORDER: 2373-01-02-0000

WESTON BATCH #: 8905L425

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-----	-----	-----	-----	-----	-----
-001	BLNK FILT 97013	PARTICULATE	0.0001	grams	0.0000
-002	BLANK WATER	PARTICULATE	0.0007	grams	0.0000
-003	BLNK ACETONE	PARTICULATE	0.0002	grams	0.0000
-004	RUN 1 FRNT HALF H2O	PARTICULATE	0.0059	grams	0.0000
-005	RUN 1 FRNT HALF ACET	PARTICULATE	0.0054	grams	0.0000
-006	RUN 1 BACK HALF H2O	PARTICULATE	0.0110	grams	0.0000
-007	RUN 1 BACK HALF ACET	PARTICULATE	0.0044	grams	0.0000
-008	FILTER #9600 RUN1	PARTICULATE	0.0309	grams	0.0000
-009	RUN 2 FRNT HALF H2O	PARTICULATE	0.0048	grams	0.0000
-010	RUN 2 FRNT HALF ACET	PARTICULATE	0.0068	grams	0.0000
-011	RUN 2 BACK HALF H2O	PARTICULATE	0.0152	grams	0.0000
-012	RUN 2 BACK HALF ACET	PARTICULATE	0.0030	grams	0.0000
-013	FILTER #9642 RUN 2	PARTICULATE	0.0367	grams	0.0000
-014	RUN 3 FRNT HALF H2O	PARTICULATE	0.0050	grams	0.0000
-015	RUN 3 FRNT HALF ACET	PARTICULATE	0.0045	grams	0.0000
-016	RUN 3 BACK HALF H2O	PARTICULATE	0.0055	grams	0.0000
-017	RUN 3 BACK HALF ACET	PARTICULATE	0.0027	grams	0.0000
-018	RUN 3 FILTER #9674	PARTICULATE	0.0161	grams	0.0000

ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- * - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M**TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M**SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M**EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I**TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.



ROY F. WESTON INC.
LIONVILLE LABORATORY

CLIENT: GLASGOW
RFW #: 8905L425
W.O. #: 2373-01-02-0000

SAMPLES RECEIVED: 05-23-89

INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. The analytical methods applied by the laboratory in the analysis of air samples contained in this batch were derived from the Federal Register, 40 CFR, Part 60, revised July 1, 1988, The Compendium of Methods for the Determination of Toxic Organic Compounds in Ambient Air, EPA - 600/4-84-041, May 1987, and NIOSH Manual of Analytical Methods, 2nd & 3rd Editions.

Mark F. Saunders 6/12/89
Mark F. Saunders Date
Wet Lab Unit Leader
Lionville Analytical Laboratory

Debra K. White 6/12/89
Debra K. White Date
Inorganic Section Manager
Lionville Analytical Laboratory

Inter-Office Memorandum



TO: Jeff O'Neill

FROM: Ben Shapiro

DATE: 15 June 1989

PROJECT: Glasgow

W.O. NO.: 2373-01-02

SUBJECT: ANALYTICAL Results for RFW Batch 8905L425

ACTION:

Enclosed are the analytical results for the above listed RFW batch. Also included are the raw data and a copy of the chain of custody record.

If I can provide any further information, please call.

APPENDIX B

LABORATORY REPORTS

GAS ANALYSIS DATA FORM

Plant GLASGOW Sample location STACK 1
 Date 5/22/89 Run no. one-2-3 Operator MILLS
 Sample type: single-point or multipoint, grab or integrated
 Analytical method ORSAT # 1 Comments Leak Check - Good
Ambient O_2 - 20.8

Sample point	24-hour clock time	% CO_2	% O_2		% CO		%N FACTOR
		Reading 1 ^a	Reading 2	Net ^a	Reading 3	Net ^b	
INT	Run 1	2.5	19.0	16.5	19.0	0.0	19
INT		2.6	19.0	16.4	19.0	0.0	19
INT		2.5	19.2	16.7	19.2	0.0	19
Ave		2.53 [✓]		16.53 [✓]		0.0	19.0
INT	Run 2	2.2	19.0	16.8	19.0	0.0	19
INT	Run 2	2.2	19.0	16.8	19.0	0.0	19
INT	Run 2	2.0	19.0	17.0	19.0	0.0	19
Ave		2.13 [✓]		16.87 [✓]		0.0	19
INT	Run 3	1.2	18.2	17.0	18.2	0.0	18.2
INT		1.2	18.2	17.0	18.2	0.0	18.2
INT		1.0	18.0	17.0	18.0	0.0	18.0
Ave		1.13 [✓]		17.00 [✓]		0.0	18.13
Averages			----		----		

% N_2 Factor

$$\% N_2 = 100 - (\% CO_2 + \% O_2 + \% CO) =$$

$$MW_d = 0.440 (\% CO_2) + 0.320 (\% O_2) + 0.280 (\% N_2 + \% CO) =$$

- ^a Net % O_2 = Reading 2 - Reading 1
^b Net % CO = Reading 3 - Reading 2

SAMPLE RECOVERY AND INTEGRITY DATA FORM

Plant GLASGOW Sample date 5/22/89
 Sample location Stack 1 Run number 3
 Sample recovery person M. L. S. Recovery date 5/22/89
 Filter/thimble number(s) 9674

187
52

MOISTURE

<u>Impingers</u>		<u>Silica gel</u>	
Final volume (wt)	<u>~39</u> ml (g)	Final wt	<u>310</u> g
Initial volume (wt)	<u>200</u> ml (g)	Initial wt	<u>300</u> g
Net volume (wt)	<u>59</u> ml (g)	Net wt	<u>10</u> g
Total moisture	<u>49</u> (g)		

Color of silica gel _____
 Description of impinger water Clear colorless

RECOVERED SAMPLE

Blank filter container number	<u>001</u> <u>97013</u>	Sealed	<u>✓</u>
Blank thimble container number	_____	Sealed	_____
Filter/thimble container number	<u>018</u> <u>#9674</u>	Sealed	<u>✓</u>
Filter/thimble container number	_____	Sealed	_____
Filter/thimble container number	_____	Sealed	_____
Filter/thimble container number	_____	Sealed	_____

Description of particulate _____

Front-half water rinse container number(s)	<u>014</u>	Liquid level marked ?	<u>✓</u>
Front-half acetone rinse container number(s)	<u>015</u>	Liquid level marked ?	<u>✓</u>
Impinger contents and back-half water rinse container number(s)	<u>016</u>	Liquid level marked ?	<u>✓</u>
Back-half acetone rinse container number	<u>017</u>	Liquid level marked ?	<u>✓</u>
Water blank container number	<u>002</u>	Liquid level marked ?	<u>✓</u>
Acetone blank container number	<u>003</u>	Liquid level marked ?	<u>✓</u>

Samples stored and locked ✓ Jm

Remarks _____

Date of laboratory custody _____

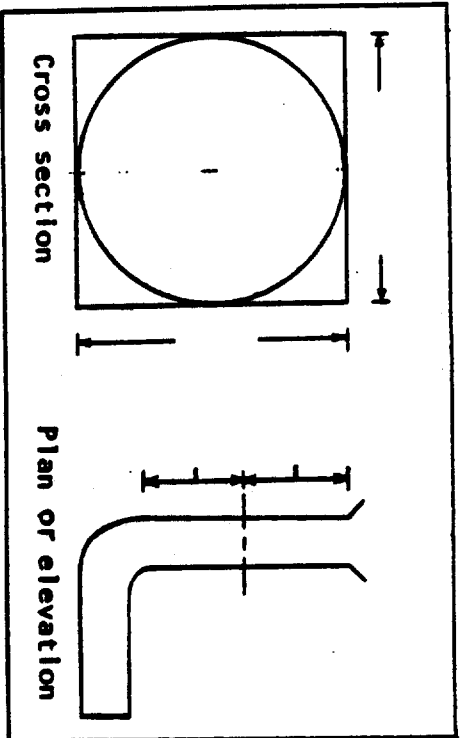
Laboratory personnel taking custody pl. Leary 5/23/89 5:45 PM

Remarks _____

PARTICULATE FIELD DATA FORM

Sheet 1 of 2

Plant Chasco
 City Philadelphia
 Location W. 4th St
 Operator W. J. 2 Date 5-22-29
 Run No. 3 of 83
 Ambient temp. 83
 Baro. press. (Pb), In. Hg. 29.96
 Sample box no. None
 Meter box no. None
 Meter box ΔH 1.922
 Meter box cal. (V) 1.003
 Probe length, ft. 4.5
 Probe liner material Monel
 Probe heater setting 35



Test point schematic B6L64-OK/line OK

Pitot tube identification no. 95
 Pitot tube cal. factor (Cp) .84
 Nozzle identification no. 210
 Avg. nozzle diameter (Dn), In. 1.236
 Pyrometer identification no. None
 Thermocouple identification no. None
 Assumed moisture, % 12
 Assumed temperature, $^{\circ}\text{F}$ 204
 Static pressure (Pstatic), In. H2O 1.63
 C factor Reference ΔP
 Initial leak rate .015 cfm @ 15 In. Hg
 Final leak rate .005 cfm @ 5 In. Hg
 Filter no. 9674

Comments:

Reverse point number	Sampling time, min.	24-hr. clock time	Velocity head (ΔP), In. H2O	Orifice meter pressure differential (ΔH), In. H2O	Gas meter reading, ft.3	Dry gas meter temperature (Tm)		Source temperature (Ts), $^{\circ}\text{F}$	Pump vacuum, In. Hg. gauge	Impinger exit gas temp., $^{\circ}\text{F}$	Filter box temp., $^{\circ}\text{F}$
X	0	1427	47	1.09	307.645	85	86	193	2.0	67	229
1	3		50	1.16	311.16	87	86	205	2.0	67	230
2	4		52	1.21	313.0	88	89	204	2.5	66	230
3	5		54	1.25	314.85	89	86	202	2.5	65	232
4	6		56	1.30	316.88	90	87	209	2.5	65	237
5	7		58	1.35	318.74	91	87	232	3.0	67	236
6	8		61	1.45	321.15	93	88	231	3.0	67	231
7	9		64	1.56	323.65	93	88	233	3.0	67	233
8	10		67	1.69	326.40	93	88	215	3.5	60	231
9	11		70	1.81	329.08	93	88	210	3.5	62	229
10	12		73	1.95	331.75	94	89	204	3.5	64	231
11	13		76	2.14	334.425	94	89	194	3.5	64	229
12	14		78	2.35	337.18	94	89	211.0	3.5	67	229
Total	8		Avg. ΔP 1.85	Avg. ΔH 1.85	Total Vm 26.780	Avg. Tm 89.04	Avg. Ts 211.00	Max. vac 3.5	Max. temp 67	Min. 229	Max. 233

Comments:

Static -1.65
-1.64

Unit was down for ~ 8 minutes at ~ 1430

SAMPLE RECOVERY AND INTEGRITY DATA FORM

Plant GLASGOW Sample date 5/22/89
 Sample location Stack -1 Run number THC
 Sample recovery person MILLS Recovery date 5/22/89
 Filter/thimble number(s) 9642

MOISTURE

Impingers

Final volume (wt) 306 ml (g)
 Initial volume (wt) 200 ml (g)
 Net volume (wt) 106 ml (g)
 Total moisture 12.4 (g)

Silica gel

Final wt 318 g
 Initial wt 300 g
 Net wt 18 g

Color of silica gel 1/2 pink 1/2 Blue

Description of impinger water clear colorless

RECOVERED SAMPLE

Blank filter container number	<u>001</u> <u>97013</u>	Sealed	☒
Blank thimble container number		Sealed	
Filter/ thimble container number	<u>013</u> <u>#9642</u>	Sealed	☒
Filter/thimble container number		Sealed	
Filter/thimble container number		Sealed	
Filter/thimble container number		Sealed	

Description of particulate

Front-half water rinse container number(s) 009 Liquid level marked? ☒

Front-half acetone rinse container number(s) 010 Liquid level marked? ☒

Impinger contents and back-half water rinse container number(s) 011 Liquid level marked? ☒

Back-half acetone rinse container number 012 Liquid level marked? ☒

Water blank container number 002 Liquid level marked? ☒

Acetone blank container number 003 Liquid level marked? ☒

Samples stored and locked ☒ jm

Remarks

Date of laboratory custody PH Morgan 5/23/89 3:40pm

Laboratory personnel taking custody

Remarks

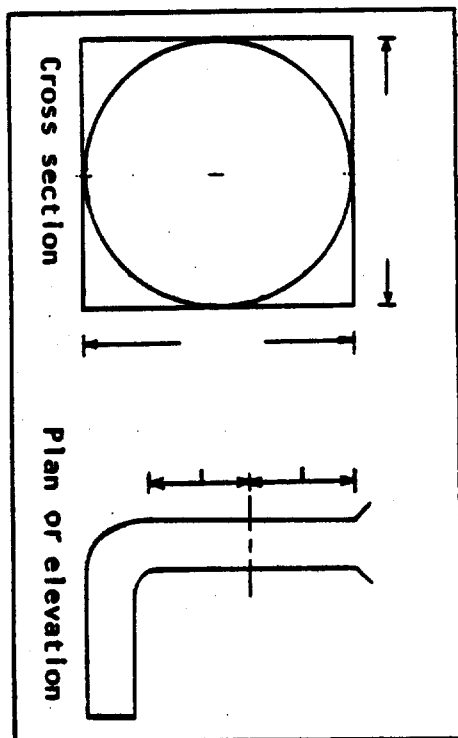
Sheet 2 of 2

[illegible]

PARTICULATE FIELD DATA FORM

Sheet 1 of 2

Plant ClaesGor
 City Ph. L. Delphino
 Location S. 400
 Operator W. A. D. 1801
 Date 5-22-79
 Ambient temp. of 30
 aro. press. (Pb), in. Hg. 29.96
 Sample box no. NA
 eter box no. NA
 eter box ΔH 1.922
 eter box cal. (V) 1.003
 robe length, ft. 4'
 robe liner material Boyc
 robe heater setting 35



Pilot tube Identification no. 15
 Pilot tube cal. factor (Cp) 2.4
 Nozzle Identification no. 215
 Avg. nozzle diameter (Dn), in. 0.037
 Pyrometer Identification no. NA
 Thermocouple Identification no. NA
 Assumed moisture, % 12.0
 Assumed temperature, of 235
 Static pressure (Pstatic), in. H2O 2.33
 C factor Reference ΔP
 Initial leak rate 0.14 cfm @ 15 in. Hg
 Final leak rate 0.05 cfm @ 5 in. Hg
 Filter no. 942

Comments:

Test point schematic

0.5 ft. Back to CE - 0.5 ft.
 Ling. LK. CK - 0.5 ft.

Reverse point number	Sampling time, min.	24-hr. clock time	Velocity head (ΔP), in. H2O	Orifice meter pressure differential (ΔH), in. H2O	Gas meter reading, ft.3	Dry gas meter temperature (Tm)		Source temperature (Ts), of	Pump vacuum, in. Hg. gauge	Impinger exit gas temp., of	Filter box temp., of
						Inlet of.	Outlet of.				
1	3	1200	1.42	98	254.425	81	82	195	2.0	65	230
2	4		1.50	1.16	358.085	83	84	197	2.0	65	229
3	9		1.53	1.23	259.82	85	84	200	2.0	66	228
4	12		1.56	1.30	261.73	85	84	196	2.0	67	226
5	15		1.57	1.32	263.68	90	86	197	2.5	67	230
6	18		1.60	1.39	265.78	90	85	195	2.5	67	236
7	21		1.87	2.03	268.13	89	86	193	3.0	65	232
8	24		1.98	2.28	270.73	92	87	194	3.0	65	230
9	27		1.1	2.56	273.26	95	87	193	3.0	63	228
10	30		1.92	2.28	275.81	93	87	188	3.0	64	234
11	33		1.97	2.26	278.42	94	88	189	3.0	65	234
12	36		1.95	2.21	280.900	95	88	189	3.0	65	234
			8562	1.75	26.285	87.5		193.8			
Total 0			Avg. $\sqrt{\Delta P}$	Avg. ΔH	Total Vm	Avg. Tm		Avg. Ts	Max. vac. 3.0	Max. temp. 67	Min. 228 Max. 236

Comments: MID JT LK CK OK, 005-10

SAMPLE RECOVERY AND INTEGRITY DATA FORM

Plant GLASGOW Sample date 3/22/89
 Sample location STACK - 1 Run number ONE
 Sample recovery person MILLS Recovery date 3/22/89
 Filter/thimble number(s) 9600

MOISTURE

<u>Impingers</u>	<u>190</u> <u>138</u>		<u>Silica gel</u>	
Final volume (wt)	<u>328</u>	ml (g)	Final wt	<u>325.5</u> g <u>9</u>
Initial volume (wt)	<u>200</u>	ml (g)	Initial wt	<u>300</u> g <u>9</u>
Net volume (wt)	<u>128</u>	ml (g)	Net wt	<u>25.5</u> g <u>9</u>
Total moisture	<u>153.5</u>	(g)		
Color of silica gel	<u>3/4 Pink - 1/4 BLUE</u>			
Description of impinger water	<u>Clear - colorless</u>			

RECOVERED SAMPLE

Blank filter container number	<u>001 #97013</u>	Sealed	<u>✓</u>
Blank thimble container number		Sealed	
Filter/ thimble container number	<u>008 #9600</u>	Sealed	<u>✓</u>
Filter/thimble container number		Sealed	
Filter/thimble container number		Sealed	
Filter/thimble container number		Sealed	
Description of particulate	<u>very FINE TAN particulate</u>		
Front-half water rinse container number(s)	<u>004</u>	Liquid level marked ?	<u>✓</u>
Front-half acetone rinse container number(s)	<u>005</u>	Liquid level marked ?	<u>✓</u>
Impinger contents and back-half water rinse container number(s)	<u>006</u>	Liquid level marked ?	<u>✓</u>
Back-half acetone rinse container number	<u>007</u>	Liquid level marked ?	<u>✓</u>
Water blank container number	<u>002</u>	Liquid level marked ?	<u>✓</u>
Acetone blank container number	<u>003</u>	Liquid level marked ?	<u>✓</u>
Samples stored and locked	<u>✓ Jm</u>		
Remarks			

Date of laboratory custody _____
 Laboratory personnel taking custody H. Leary 8:45 PM 3/23/89
 Remarks _____

66A502W

Run 1

[illegible]

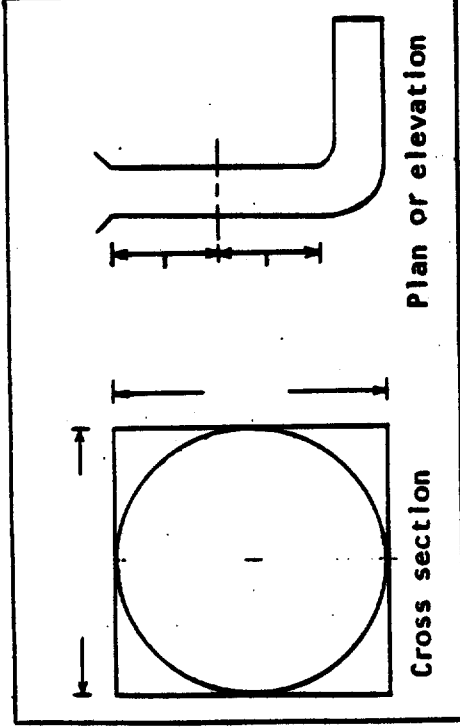
Comments: - 27 syndic

PARTICULATE FIELD DATA FORM

Sheet 1 of 2

Plant CLASCON
 City PHILADELPHIA
 Location STAGE 1
 Operator WILSON
 Run No. 001 of 80 Date 5/2/80
 Ambient temp., °F 80
 Baro. press. (Pb), in. Hg. 29.96
 Sample box no. NA
 Meter box no. WTECH 9
 Meter box ΔH 1.922
 Meter box cal. (V) 1.023
 Probe length, ft. 4.75
 Probe liner material BRASS
 Probe heater setting 35

K = 2.12



ORCA H6 late check - OK
 Test point schematic

Pitot tube identification no. P5
 Pitot tube cal. factor (Cp) 1.81
 Nozzle identification no. 213
 Avg. nozzle diameter (Dn), in. 0.231
 Pyrometer identification no. WTECH
 Thermocouple identification no. ---
 Assumed moisture, % 12.0
 Assumed temperature, °F. 230
 Static pressure (Pstatic), in. H2O - 26
 C factor Reference ΔP
 Initial leak rate 0 cfm @ 15 in. Hg
 Final leak rate 0.002 cfm @ 5 in. Hg
 Filter no. 9600

Comments: Final first run check OK
Final first run check OK

ORCA line late check OK

Traverse point number	Sampling time, min.	24-hr. clock time	Velocity head (ΔP), in. H2O	Orifice meter pressure differential (ΔH), in. H2O	Gas meter reading, ft. ³	Dry gas meter temperature (Tm)		Source temperature (Ts), °F	Pump vacuum, in. Hg. gauge	(2) Impinger exit gas temp., °F.	(3) Filter box temp., °F.
						Inlet °F.	Outlet °F.				
X 1	0	0925	44 (.44)	1.93 (93)	202.570	83	84	187	2.5	67	235
2	3	0938	49	1.03	204.245	83	84	192	2.5	67	238
3	6	0931	50	1.06	205.75	82	81	197	2.5	64	237
4	9	0934	52	1.10	207.76	81	80	200	2.5	63	237
5	12	0937	55	1.16	209.43	86	82	208	2.5	65	240
6	15	0940	59	1.25	211.82	86	82	212	2.5	65	239
7	18	0943	86	1.82	213.24	86	81	213	3.5	67	239
8	21	0946	94	1.94	215.62	86	81	213	3.5	67	238
9	24	0949	98	2.07	217.74	86	81	214	4.0	68	239
10	27	0952	98	2.03	220.04	88	83	216	4.0	66	242
11	30	0955	98	2.07	222.45	93	85	215	4.0	65	243
12	33	0958	98	2.07	224.87	95	87	311	4.0	66	241
12	36	1001	98	2.07	227.310	93	86	311	4.0	66	241
					24.74	84.91	84.91	266.58			
Total 0	36		Avg. $\sqrt{\Delta P}$ 8456	Avg. ΔH 1.54	Total Vm	Avg. Tm	Avg. Ts	Max. temp. 68	Max. vac. 4.0	Min. 235	Max. 243

Station 2.25

Comments:

Mod 12 OK - OK 207372

MOISTURE DETERMINATION FORM

Plant Glasgow Date 5/22/89
 Sample location Stack Run no. Prelim
 Operator Mills/Marz/Carver Barometric pressure (P_b), in. Hg. 29.96
 Comments: third leak check - ok
Final leak check - ok

	24-hr. clock time	Gas meter reading, ft. ³	Orifice meter pressure differential (ΔH), in. H ₂ O	Dry gas meter temperature (T_m)	
				Inlet F.	Outlet F.
Stop	0800	202.400	1.5	91	84
Start	0745	192.210	1.5	85	84
		Total V_m 10.190	Ave. ΔH 1.5	Avg. T_m 86	

Impinger volume

Final, ml 225
 Initial, ml 200
 Net, ml 25

Silica gel weight

Final, g 306
 Initial, g 300
 Net, g 6

Calculations

- (1) $P_b = 29.96$
- (2) Total $V_m = 10.190$
- (3) Avg. $\Delta H = 1.5$
- (4) Avg. $T_m = 86$
- (5) Net ml = 25
- (6) Net g = 6
- (7) $V_{m(std)} = \frac{17.64 \times V_m (P_b + \frac{\Delta H}{13.6})}{(T_m + 460)} = \frac{17.64 \times 10.190 (29.96 + \frac{1.5}{13.6})}{(86 + 460)} = 9.89$
- (8) $V_{w(std)} = (.04707 \times \text{Net ml}) + (.04715 \times \text{Net g}) =$
 $(.04707 \times 25) + (.04715 \times 6) = 1.46$
- (9) $\%H = \frac{100 \times V_{w(std)}}{V_{w(std)} + V_{m(std)}} = \frac{100 \times 1.46}{1.46 + 9.89} = 12.86\%$

GAS VELOCITY AND VOLUME DATA FORM

Plant GLASGOW

Date 5/22/89

Run no.

Prelim

24-hr. clock time

Operators

MILLS/Barker

Stack

diameter or dimensions, in,

Barometric pressure, in. Hg

Cross sectional area, ft.²

Barometric pressure, in. hg. _____
Pitot tube identification no. _____

Ср

[illegible]

^a Must be <10 degrees to be acceptable.

Diagram illustrating the sampling location for the LAR ducts. The diagram shows two vertical ducts connected by a horizontal line. The left duct has a sampling point marked with an 'X' and labeled 'OY'.

$$AREA = 7.87 \text{ Ft}^2$$
[illegible]

$$V_s = 85.49 \times .84 \times .853903 \times \left[\frac{662.71}{29.94 \times 27.65} \right]^{\frac{1}{2}}$$

$$= 54.86 \text{ Feet/sec}$$

Where:

V_s = Average gas stream velocity, ft/sec.

85.49 = Pitot tube constant, ft/sec $\times$

$$\left[\frac{(\text{lb/lb-mole})(\text{in. Hg})}{(^{\circ}\text{R})(\text{in. H}_2\text{O})} \right]^{\frac{1}{2}}$$

C_p = Pitot tube coefficient, dimensionless.

T_s = Absolute gas stream temperature, $^{\circ}\text{R.} = T_s, ^{\circ}\text{F} + 460$

P_s = Absolute gas stack pressure, in. Hg. = $P_b + \frac{P_{\text{static}}}{13.6}$

Δp = Velocity head of stack gas, in. H_2O

8. Average gas stream volumetric flow rate at actual conditions, wacf/hr.

$$Q_{s(\text{act})} = 3,600 \times V_s \times A_s$$

$$= 3,600 \times 54.86 \times 7.88 = 1556268 \text{ WACF/HR}$$

or

Where:

$Q_{s(\text{act})}$ = Volumetric flow rate of wet stack gas at actual conditions, wacf/hr.

A_s = Cross-sectional area of stack, ft.^2

9. Average gas stream dry volumetric flow rate at standard conditions, dscf/hr.

$$Q_{s(\text{std})} = 17.64 \times M_d \times \frac{P_s}{T_s} \times Q_{s(\text{act})}$$

$$= 17.64 \times 0.872 \times \frac{1556268}{662.71} \times \frac{29.94}{27.65} = 1081502 \text{ DSCF/HR}$$

or

Where:

$Q_{s(\text{std})}$ = Volumetric flow rate of dry stack gas at standard conditions, dscf/hr.

18025 DSCF/MIN

10. Isokinetic variation calculated from intermediate values, percent.

$$I = \frac{17.327 \times T_s \times V_{m(std)}}{V_s \times \theta \times P_s \times M_d \times (D_n)^2}$$

$$I = \frac{17.327 \times 662.71 \times 49.122}{54.86 \times 72 \times 29.94 \times .872 \times (.231)^2} = 102.5$$

Where:

- I = Percent of isokinetic sampling.
- θ = Total sampling time, minutes.
- D_n = Diameter of nozzle, inches.
- 17.327 = Factor which includes standard temperature (528^{OR}), standard pressure (29.92 in.Hg), the formula for calculating area of circle $\frac{D^2}{4}$, conversion of square feet to square inches (144), conversion of seconds to minutes (60), and conversion to percent (100), $\frac{(in. Hg) (in^2) (min)}{(OR) (ft^2) (sec)}$

11. Particulate concentration, gr/dscf.

$$C_1 = 15.432 \times \frac{M_t}{V_{m(std)}}$$

$$C_1 = 15.432 \times \frac{.0665}{49.12} = .0209$$

Where:

- C_1 = Particulate concentration, gr/dscf.
- M_t = Total weight of particulate caught by train, g.
- 15.432 = Conversion factor of gr/g.

12. Particulate concentration, gr/wacf.

$$C_2 = C_1 \times \frac{Q_s(std)}{Q_s(act)} = \quad \times \quad = NA$$

Where:

- C_2 = Particulate concentration, gr/wacf.

13. Particulate mass emission rate, lb/hr.

$$\begin{aligned} \text{PMR}_t &= 0.000142857 \times C_1 \times Q_s(\text{std}) \\ &= 0.000142857 \times .0209 \times 108,502 = 3.23 \end{aligned}$$

Where:

$$\begin{aligned} \text{PMR}_t &= \text{Particulate mass emission rate, lb/hr.} \\ 0.000142857 &= \text{Conversion factor relating grains to pounds (7,000), lb/gr.} \end{aligned}$$

14. Conversion Factors:

From	To	Multiply by
in.	mm.	25.40
ft.	m.	0.3048
ft. 2	m. 2	0.092903
ft. 3	m. 3	0.028317
gr/ft. 3	g/m. 3	2.28833
lbs/hr.	g/hr.	453.59

Temperature

$$^{\circ}\text{C} = 5/9 (\text{F} - 32)$$

$$^{\circ}\text{R} = ^{\circ}\text{F} + 460$$

$$^{\circ}\text{K} = ^{\circ}\text{C} + 273$$

APPENDIX D

PROCESS OPERATIONS DATA

Every 15 Minutes - Approx During Tests Only
 Unit #1 Dryer/Baghouse (of 2 Total) #4 Blend
 Pressure

Time	ΔP	TF Bag	TF Dryer	% Burner	T Asphalt	shots for Trucks
9:29 AM	4.0	240°F	350°F	80%	300°	
9:35	3.8	240°	370°	70%	300°	
9:50	3.9	220°	365°	70%	300°	
10:05	3.9	220°	340°	60%	300°	
10:20	4.1	215°	340°	60%	300°	
10:35	4.2	225°	355°	60%	300°	
11:55	4.2	235°	350°	60%	300°	
12:10	3.9	220°	350°	50%	300°	
12:25	3.9	220°	340°	50%	300°	
12:40	3.9	225°	340°	60%	300°	
12:55	4.0	225°	350°	50%	300°	
1:10	3.9	230°	350°	80%	300°	
2:25	3.4	245°	370°	70%	300°	
2:40	3.6	230°	370°	60%	300°	
2:45	3.6	240°	380°	60%	300°	
3:00	3.8	225°	340°	50%	300°	

CLIENT/SUBJECT GLASGOW IAC W.O. NO. _____

TASK DESCRIPTION TOT. AGG/HR TASK NO. _____

PREPARED BY S. Kirkpatrick DEPT 1500 DATE 31 May, 1989

MATH CHECK BY _____ DEPT _____ DATE _____

METHOD REV. BY _____ DEPT _____ DATE _____

APPROVED BY _____
 DEPT _____ DATE _____

PER TEST

 - BY TIME OF ACTUAL TEST

	TEST 1	TEST 2	TEST 3
TIME	9:25 → 10:43 1.3 hrs	12:00 → 13:17 1.2833 hrs	14:27 → 15:03 0.60 hrs
AGG TOT	136.780 TONS	129.640 TONS	54.915 TONS
	105,2154 TONS/hr 210,430.7689 lbs/hr	101,01818 TONS/hr 202,036.3642 lbs/hr	91,35845 TONS/hr 182,716.90 lbs/hr

Rw 1 $A = 0.76 E^{0.42}$

$E = F \times W$

$E = 6 \frac{\text{lbs}}{\text{TON}} (105.21 \frac{\text{TONS}}{\text{HR}})$

$E = 631 \frac{\text{lbs}}{\text{HR}}$

$A = 11.40 \frac{\text{lbs}}{\text{HR}}$

Rw 2 $E = 6 \frac{\text{lbs}}{\text{TON}} (101.02 \frac{\text{TONS}}{\text{HR}})$

$E = 606 \frac{\text{lbs}}{\text{HR}}$

$A = 11.21 \frac{\text{lbs}}{\text{HR}}$

Rw 3 $E = 6 \frac{\text{lbs}}{\text{TON}} (91.36 \frac{\text{TONS}}{\text{HR}})$

$E = 548 \frac{\text{lbs}}{\text{HR}}$

$A = 10.74 \frac{\text{lbs}}{\text{HR}}$

HAZARD WARNING: Thermal burns from
contact with liquid, vaporization,
and eye irritation hazards from
hydrogen sulfide gas.

SOLD TO: HERE BLAU INC.
CUSTOMER NO.: 1154
LOCATION: 3431 DIAMOND

TIME	DATE	USE OF
05:00	08/08/08	05:00

ORDER NO.

TICKET NO.

TRUCK NO.

PRODUCT

UNIT PRICE

DELIVERY CHARGE

☐ YES	☐ NO
------------------------------	-----------------------------

TAXABLE

DELIVERED BY

WEIGHMASTER

REC'D BY

[illegible]

NET LOAD TOTAL

41.850

INSPECTOR

HAZARD WARNING: Thermal burns from contact with hot liquid. Inhalation and eye irritation hazards from hydrogen sulfide gas.

05/22/89

DAVELLI CONST.

CUSTOMER NO.

CONFIDENTIAL

TIME

DATE _____

05/22/89

ORDER NO. 3577

TICKET NO. 57929

TRUCK NO. 2165

AMOUNT

TRUCKER CODE

5

PRODUCT

UNIT PRICE
DELIVERY CHARGE

TAXABLE

☐ YES

☐ NO

DELIVERED BY

Weightlifting

RECEIVED BY

TAXABLE		YES		NO		DELIVERED BY		WEIGHMASTER		REC'D BY		
1	0	2380	5680	0	0	0	0	5680	5680	.0	324.0	6004
2	0	2370	5690	0	0	0	0	5690	5690	.0	323.0	6013
3	0	2320	5630	0	0	0	0	5650	5650	.0	324.0	5974

50, 870 INSPECTOR

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

BEACH ST. & SUSQUEHANNA
PHILA. PA. PHONE 215-739-2821

ON JOB OFF JOB RETURN

HAZARD WARNING: Thermal burns from
contact with hot liquid, inhalation,
and eye irritation hazards from
hydrogen sulfide gas.

SOLD TO G. MASGAI & SON
CUSTOMER NO. 1762
LOCATION: ROHM, HARR

TIME 09:35 DATE 05/22/89

ORDER NO.

TICKET NO. 657932

TRUCK NO. 70

PRODUCT ID2B00VC

UNIT PRICE _____ AMOUNT _____

DELIVERY CHARGE _____ TRUCKER CODE 04

TAXABLE ☒ YES ☐ NO

DELIVERED BY:		WEIGHMASTER:		RECD BY:							
<i>David L. Cichini</i>		<i>David L. Cichini</i>		<i>Jack Parnon</i>							
1	0	1750	6340	4690	0	0	6360	6360	.0	287.0	6647
2	0	1840	6340	4670	0	0	6370	6370	.0	286.0	6656
3	0	1590	6330	4560	0	0	6350	6380	.0	285.0	6655

67,420 INSPECTOR

HAZARD WARNING: Thermal burns from contact with hot liquid. Inhalation, and eye irritation hazards from hydrogen sulfide gas.

UNIT PRICE	AMOUNT
DELIVERY CHARGE	TRUCKER CO

1	0	2410	4710	0	0	0	0	0	0	4710 4730	.0	270.0	4980 4990
2	0	1930	4690	0	0	0	0	0	0	4710 4730	.0	269.0	

68,310 . INSPECTOR

HAZARD WARNING: Thermal burns from contact with hot liquid. Inhalation and eye irritation hazards from hydrogen sulfide gas.

TIME 10100 DATE 05/22/89

JOHN J. DOUGHERTY & SON
SOLD TO

CUSTOMER NO.

CUSTOMER NO. 372
LOCATION: PENN SHIP

ORDER NO.

TICKET NO.

45794

TRUCK NO: **DL5**

PRODUCT

AMOUNT	TRUCKER CODE
2	

UNIT PRICE

DELIVERY CHARGE

TAXABLE ☐ YES ☐ NO

DELIVERED BY

WEIGHMASTER

REC'D BY

1	0	1440	5300	3940	0	0	5300	5300	0	193.0	5493
2	10	1400	5300	3820	0	0	5300	5300	0	193.0	5493
3	0	1390	5240	3820	0	0	5290	5290	0	192.0	5482
4	0	1340	5280	3820	0	0	5310	5310	0	193.0	5503

127,950 INSPECTOR

二

SOLD TO : J. J. DOUGHERTY & SON
CUSTOMER NO. 372
LOCATION: PENN SHIP

TIME 10:15 **DATE** 05/22/89

ORDER NO.:

TICKET NO. 412435

TRUCK NO. **D14**

PRODUCT **BA-1 Cyls**

UNIT PRICE	AMOUNT
------------	--------

DELIVERY CHARGE _____

TAXABLE

DELIVERED BY	WEIGHMASTER	RECEIVED BY
--------------	-------------	-------------

WEINMASTER
Dennis (C. J.)

1	0	1650	5760	4260	0	0	5790	5790	5790	.0	210.0	6000
2	0	1570	5760	4190	0	0	5790	5790	5790	.0	210.0	5900
3	0	1580	5760	4170	0	0	5790	5790	5790	.0	209.0	5999
4	0	1520	5760	4180	0	0	5770	5770	5770	.0	209.0	5979
5	0	1550	5750	4410	0	0	5800	5800	5800	.0	210.0	6010
6	10	1600	5760	4180	0	0	5790	5790	5790	.0	209.0	5999
7	0	1570	5750	4190	0	0	5800	5800	5800	.0	210.0	6010

168,380

LEACH, P.A. & PHONE 218-1199
 PHILA. PA. OFF JOB RETURN

HAZARD WARNING: Thermal burns from contact with hot liquid. Inhalation and eye irritation hazards from hydrogen sulfide gas.

SOLD TO CLEVELAND MECH.
 CUSTOMER NO. 2833
 LOCATION: *Cleveland*

TIME 10:28 DATE 05/22/69
 ORDER NO. 1764
 TICKET NO. 557936

UNIT PRICE _____ AMOUNT _____
 DELIVERY CHARGE _____ TRUCKER CODE *04*
 TAXABLE ☐ YES ☐ NO TRUCK NO. 1
 PRODUCT ID2400VC

DELIVERED BY		WEIGHMASTER		RECD BY	
<i>Paul J. O'Brien</i>		<i>Paul J. O'Brien</i>		<i>Paul J. O'Brien</i>	
1	0	2270	4960	0	0
2	0	2300	4970	0	0
3	0	2180	4960	0	0
				5040	5040
				5060	5060
				5050	5050
				288.0	288.0
				5328	5328
				5348	5348
				5338	5338

183,530 INSPECTOR

५३

DATE	05/22/89
ORDER NO.	
TICKET NO.	657939
TRUCK NO.	
PRODUCT	ID2B000VC

TIME

DATE

05/22/89

100

ORDER NO.

CUSTOMER NO. TEST RUN #1

LOCATION: AGG. BINS

TICKET NO. 657939

TRUCK NO.

AMOUNT:

1

ID2800VC

TRUCKER CODE

UNIT PRICE

DELIVERY CHARGE

TAXABLE INCOME

05

1

DELIVERED BY:

WICHTIGSTEN

NECVD-01

1	0	5010	5970	4190	6	0	0	0	5970	0	0	0	5970
---	---	------	------	------	---	---	---	---	------	---	---	---	------

2 35,130 TRUCKER

BOOKS

HAZARD WARNINGS: Thermal burns from contact with hot liquid. Inhalation and eye irritation hazards from hydrogen sulfide gas.

CUSTOMER NO.

TEST RUN #1
AGG. BINS

TIME

DATE:

05/22/09

11028 ORDER NO.

TICKET NO.

657941

TRUCK NO.

PRODUCT

1D2B00VC

UNIT PRICE

DELIVERY CHARGE

TAXABLE

☐ NO ☒ YES

DELIVERED BY

WILEY

REC'D BY

[illegible]

TRUCKER

2 315141916030

101 W I
 BEACH ST. & SUSQUEHANNA
 PHILA. PA. PHONE 215-737-2021
 ON JOB OFF JOE RETURN

TEST #2

HAZARD WARNING: Thermal burns from
 contact with hot liquid. Inhalation,
 and eye irritation hazards from
 hydrogen sulfide gas.

SOLD TO M. JOHNSON
 CUSTOMER NO. 256
 LOCATION: BRISTOL

TIME 12:01 DATE 05/22/89

ORDER NO. 1501

TICKET NO. 157344

AMOUNT 194.51

23.50

TRUCKER CODE 9.26

PRODUCT BB-100V6

UNIT PRICE

DELIVERY CHARGE

TAXABLE 104.50 9.17

DELIVERED BY *[Signature]* WEIGHTMASTER *[Signature]* REC'D BY *[Signature]*

1	0	1170	4490	3300	0	0	0	4480	4480	.0	163.0	4643
2	0	1330	4480	3290	0	0	0	4510	4510	.0	164.0	4674
3	0	1140	4480	3240	0	0	0	4510	4510	.0	164.0	4674

13,500 INSPECTOR

A 300 NI 46 5705
 BEACH ST. & SUSQUEHANNA
 PHILA. PA. PHONE 219-739-2621
 ON JOB OFF JOB RETURN

HAZARD WARNING: Thermal burns from
 contact with hot liquid. Inhalation
 and eye irritation hazards from
 hydrogen sulfide gas.

SOLD TO J. J. DOUGHERTY & SON
 CUSTOMER NO. 372
 LOCATION: PENNSHIP
 TIME 12:09 DATE 05/22/89
 ORDER NO.
 TICKET NO. 657945
 TRUCK NO. D15
 PRODUCT BB-100VS
 UNIT PRICE
 DELIVERY CHARGE
 TAXABLE ☐ YES ☐ NO
 AMOUNT
 TRUCKER CODE

DELIVERED BY		RECEIVED BY						
Paul R. Bell		V. J. J. J.						
1	0	1520	5770	4240	0	5770	209.0	5979
2	0	1610	5780	4250	0	5780	210.0	5990
3	10	1470	5770	4170	0	5800	210.0	6010
4	0	1530	5770	4180	0	5810	209.0	6019
5	0	1570	5770	4150	0	5770	209.0	5979
6	0	1470	5760	4160	0	5810	210.0	6020
7	0	1490	5760	4260	0	5800	210.0	6010

54,040 INSPECTOR

hazardous materials. Thermal burns from contact with hot liquid. Inhalation and eye irritation hazards from hydrogen sulfide gas.

TIME 1302Z DATE 05/22/89

SOLD TO J. J. DOUGHERTY & SON
CUSTOMER NO. 372
LOCATION: PENNSHIP

ORDER NO. 557946
TICKET NO.

TRUCK NO. AC173

PRODUCT BB-100VS

AMOUNT
14
TRUCKER CODE

UNIT PRICE	DELIVERY CHARGE
1.00	1.00
2.00	2.00
3.00	3.00
4.00	4.00
5.00	5.00
6.00	6.00
7.00	7.00
8.00	8.00
9.00	9.00
10.00	10.00
11.00	11.00
12.00	12.00
13.00	13.00
14.00	14.00
15.00	15.00
16.00	16.00
17.00	17.00
18.00	18.00
19.00	19.00
20.00	20.00
21.00	21.00
22.00	22.00
23.00	23.00
24.00	24.00
25.00	25.00
26.00	26.00
27.00	27.00
28.00	28.00
29.00	29.00
30.00	30.00
31.00	31.00
32.00	32.00
33.00	33.00
34.00	34.00
35.00	35.00
36.00	36.00
37.00	37.00
38.00	38.00
39.00	39.00
40.00	40.00
41.00	41.00
42.00	42.00
43.00	43.00
44.00	44.00
45.00	45.00
46.00	46.00
47.00	47.00
48.00	48.00
49.00	49.00
50.00	50.00
51.00	51.00
52.00	52.00
53.00	53.00
54.00	54.00
55.00	55.00
56.00	56.00
57.00	57.00
58.00	58.00
59.00	59.00
60.00	60.00
61.00	61.00
62.00	62.00
63.00	63.00
64.00	64.00
65.00	65.00
66.00	66.00
67.00	67.00
68.00	68.00
69.00	69.00
70.00	70.00
71.00	71.00
72.00	72.00
73.00	73.00
74.00	74.00
75.00	75.00
76.00	76.00
77.00	77.00
78.00	78.00
79.00	79.00
80.00	80.00
81.00	81.00
82.00	82.00
83.00	83.00
84.00	84.00
85.00	85.00
86.00	86.00
87.00	87.00
88.00	88.00
89.00	89.00
90.00	90.00
91.00	91.00
92.00	92.00
93.00	93.00
94.00	94.00
95.00	95.00
96.00	96.00
97.00	97.00
98.00	98.00
99.00	99.00
100.00	100.00

TAXABLE

DELIVERED BY

РЕЗЮМЕ

1	0	1410	5760	4160	0	0	5900	0	209.0	6009
2	0	1540	5760	4160	0	0	5900	0	210.0	6010
3	0	1310	5760	4160	0	0	5900	0	209.0	6009
4	0	1500	5760	4160	0	0	5790	0	209.0	5999
5	0	1550	5750	4267	0	0	5780	0	210.0	5990
6	10	1600	5760	4300	0	0	5900	0	209.0	6009
7	10	1500	5760	4160	0	0	5760	0	210.0	5970
8	10	1480	5750	4160	0	0	5790	0	209.0	5999

100,360 INSPECTOR

UNSUBS. PETRO. CO. INC. 2001 PENN
BRIDGE ST. PHILADELPHIA, PA. 19106
TEL. 215-596-1234 FAX 215-596-1235
ON JOB OFF JOB RETURN

HAZARD WARNING: Thermal burns from
contact with hot liquid. Inhalation
and eye irritation hazards from
hydrogen sulfide gas.

SOLD TO: PETRO TYPE
CUSTOMER NO. 2653
LOCATION: 2001 PENN

TIME 12:36 DATE 05/23/99
ORDER NO.
TICKET NO. 657947
TRUCK NO. /

UNIT PRICE
DELIVERY CHARGE
TAXABLE
DELIVERED BY
AMOUNT
06
PRODUCT 10240000

QTY	UNIT PRICE	AMOUNT	TAX	TOTAL	REMARKS
1	1400	1400	0	1400	
2	1070	2140	0	2140	
		3780	0	3780	
		3790	0	3790	
		216.0	0	216.0	
		216.0	0	216.0	
		3996		3996	
		4006		4006	

no known harmful effects from
contact with hazardous inhalation
and eye irritation hazards from
moderate volatility.

PRODUCT BB-100128

UNIT PRICE	DELIVERY CHARGE	TAXABLE

DELIVERED BY
YES NO

1	0	1590	5740	1250	0	5770	5770	204.0	5979
2	0	1650	5760	1200	0	5800	5800	204.0	6009
3	0	1500	5750	1400	0	5790	5790	210.0	6000
4	0	1470	5760	1140	0	5790	5790	210.0	6000
5	0	1740	5730	1230	0	5800	5800	210.0	6010
6	0	1460	5750	1170	0	5790	5790	210.0	6000
7	0	1440	5730	1170	0	5790	5790	204.0	5999

148,460 INSPECTOR

20

toxic agents. The use of these agents with hot liquids, irritants and low irritation hazards from common sulfide air.

SOLD TO: TOP SOIL PAVERS
CUSTOMER NO. 2074
LOCATION: FAYMNER OLD
TIME 12:03 DATE 05/22/84
ORDER NO.

TICKET NO. 637949

UNIT PRICE

DELIVERY CHARGE

TAXABLE INCOME 7800

DELIVERED BY

RECVD

1	0	2250	5210	0	0	0	5290	5290	0	302.0	5592
2	0	2160	5210	0	0	0	5290	5290	0	302.0	5592
3	0	2530	5220	0	0	0	5300	5300	0	303.0	5603
4	0	2200	5210	0	0	0	5290	5290	0	302.0	5592
5	0	2160	5260	0	0	0	5290	5290	0	301.0	5591

INSPECTOR
174,920

6 6 19

CLARKSON, INC.
BRANCH ST. 1153
PHILADELPHIA, PA. 19107
PHONE 761-1000

HAZARD WARNING: Thermal burns from
contact with hot liquid, inhalation,
and eye irritation hazards from
hydrogen sulfide gas.

TIME 13:00 DATE 05/22/89
ORDER NO.
TICKET NO. 657980
TRUCK NO. 3

HERB BLAU INC.
CUSTOMER NO. 1153
LOCATION: CHS DAYTON

PRODUCT ID2H00VC

AMOUNT \$0
TRUCK CODE

UNIT PRICE

DELIVERY CHARGE

TAXABLE ☐ YES ☒ NO

DELIVERED BY

RECEIVED BY

1	0	2630	6220	0	6300	6300	.0	360.0	6660
2	0	2600	6180	0	6310	6310	.0	359.0	6659
3	0	2600	6220	0	6300	6300	.0	360.0	6660

193,830 INSPECTOR

[illegible]

12000 LBS/HR. These vapors from contact with hot liquid, inhalation, and eye irritation hazards from hydrogen sulfide gas.

SOLD TO DOLENTE

CUSTOMER NO. 801
LOCATION: SECTION 50
ORDER NO.

ON 010000

TICKET NO. 657951

TRUCK NO.

PRODUCT IDZHOVC

UNIT PRICE:

DELIVERY CHARGE

TAXABLE

DELIVERED BY:

REC'D BY

1	0	2370	3430	0	0	0	5480	5490	0	323.0	6003
---	---	------	------	---	---	---	------	------	---	-------	------

199,510 INSPECTOR

HAZARD SUMMARY: Thermal burns from contact with hot liquid. Inhalation, and eye irritation hazards from hydrogen sulfide gas.

[illegible]

TICKET NO. 657933

TRUCK NO.

PRODUCT 1D2B00VC

100

TRUCKS

UNIT PRICE

DELIVERY CHARGE

TAXABLE

DELIVERED

REC'D NY

1	0	2930	5980	4200	0	0	0	5980	0	0	5980
2	10	3532	5990	4170	0	0	0	5990	0	0	5990
3	0	2943	5980	4230	0	0	0	5980	0	0	5980

217,460 INSPECTOR

50.

IN 43 DATE 60/22/69

●

100-442107

CUSTOMER NO.

CUSTOMER

ORDER NO.

TICKET NO. 579034

TRUCKING.

102800VC

UNIT PRICE

DELIVERY CHARGE

[illegible]

DELIVERED BY!

STATIONMASTER

REC'D BY

1	0	3260	6000	4240	0	0	6000	0	0	6000
2	0	2980	5990	4230	0	0	5990	0	0	5990
3	10	3030	6000	4230	0	0	6000	0	0	6000

235,450 INSPECTOR

BELLSUM I-100
 BEACH ST. 100
 PHILADELPHIA PA 19106
 ON THE OFFICE

NO WARNING - NO WARNING FROM
 CONTACT WITH HOT SURFACE MATERIAL.
 AND FOR INFORMATION FROM
 INFORMATION SULFIDE RIL

SOLD TO: TEST NAME: DATE: 05/23/64

CUSTOMER NO.
 LOCATION:

ORDER NO.

TICKET NO. 657955

TRUCK NO.

PRODUCT ID2800VC

UNIT PRICE

DELIVERY CHARGE

TAXABLE YES ☐ NO ☐

DELIVERED BY

RECEIVED BY

1	0	3580	5970	1250	0	5970	0	5970
2	0	3140	5970	4230	0	5990	0	5990
3	0	3060	5930	4240	0	5930	0	5930

253,340 INSPECTOR

DATE: 03/21/97
TIME: 11:03 PM
STATION: 637957
TRACE NO: 276
MODE: F3MODE

TAXABLE

NUCYP

DELIVERED BY	REC'D BY	DATE	TIME	LOCATION	REMARKS
1	250	250	250	250	250
2	250	250	250	250	250
3	250	250	250	250	250

10,990 INSPECTOR

124,630 MS TRUCKER
#54,615 TON/

630 A TRUCKER
#64.6157023

APPENDIX E

EQUIPMENT CALIBRATION RECORDS

NOZZLE CALIBRATION DATA FORM

Date

5/22/89

Calibrated by

John Mills

Nozzle identification number	Nozzle diameter, inches ^a			$\Delta D,^b$	D_{avg}^c
	D_1	D_2	D_3		
216	.235	.237	.237	.002	.236
21B	.232	.230	.231	.002	.231

Where:

^a $D_{1,2,3}$ = three different nozzle diameters, inches; each diameter must be measured to nearest 0.001 in.

^b ΔD = maximum difference between any two diameters, inches.
 ΔD must be ≤ 0.004 in.

^c D_{avg} = nozzle diameter = average of D_1 , D_2 and D_3 .

METER BOX CALIBRATION DATA AND CALCULATION FORM

NON CALIBRATION

Date 25 May 1988

Meter Box Number

Noted
#9

Barometric pressure, P_b = 29.78 in. Hg

Calibrated by Grace Wood

Orifice manometer setting (ΔH), In. H ₂ O	Gas volume		Temperatures				Time (θ), min	Y_i	ΔH_{ei} In. H ₂
	Wet test meter (V_w), ft ³	Dry gas meter (V_d), ft ³	Wet test meter (t_w), °F	Dry gas meter					
				Inlet (t_{di}), °F	Outlet (t_{do}), °F	Avg ^a (t_d) °F			
0.5	5	105.776 110.750	75	78 79	77 80	78	12.8	1.009	1.856
1.0	5	100.295 105.284	75	79 80	77 81	78.8	9.0	1.007	1.849
1.5	10	112.242 122.243	75	78 81	77 85	79.3	15.1	1.004	1.932
2.0	10	122.731 132.789	75	84 86	77 88	82.	13.3	1.003	1.974
3.0	10	133.793 143.955	75	86 89	77 90	83.7	10.9	1.9927	1.947
4.0	10								
Avg								Y 1.003	ΔH_e 1.922

ΔH in. H ₂ O	$\frac{\Delta H}{13.6}$	$Y_i = \frac{V_w P_b (t_d + 460)}{V_d (P_b + \frac{\Delta H}{13.6}) (t_w + 460)}$	$\Delta H_{ei} = \frac{0.0317 \Delta H}{P_b (t_d + 460)} \left[\frac{(t_w + 460) \theta}{V_w} \right]^2$
0.5	0.0368	538.24.78-5 525-29.82-4.974 1.009	101585 1000001 635-12.8 528-29.78 1.856
1.0	0.0735	538.8-29.78-5 525-29.85-4.989 1.007	10317 1000002 525-9.0 538.8-29.78 1.849
1.5	0.110	539.3-29.78-10 525-29.89-10.001 1.004	104755 1000003 535-15.1 539.3-29.78 1.932
2.0	0.147	542.29.78-10 536-29.93-10.058 1.0029	10634 10000039 535-13.3 542-29.78 1.974
3.0	0.221	543.7-29.78-10 525-30.00-10.162	10951 10000059 535-10.9 543.7-29.78 1.997
4.0	0.294		

If there is only one thermometer on the dry gas meter, record the temperature under t_d .

Test numbers _____ Date 25 MAY 89 Meter box number 10724 Plant GLASGOW

Barometric pressure, $P_b =$ 29.95 in. Hg Dry gas meter number 6843913 Pretest $\gamma =$ 1.007

Orifice no. setting. (ΔH) in. H ₂ O	Gas volume		Temperature			Time (θ), min	Vacuum setting, in. Hg.	γ_1	$\gamma_1 = \frac{V_w P_b (\tau_d + 460)}{V_d (P_b + \frac{\Delta H}{13.6}) (\tau_w + 460)}$
	Wet test meter (V_w), ft ³	Dry gas meter (V_d), ft ³	Wet test meter (τ_w), °F	Inlet (τ_{d1}), °F	Outlet (τ_{d2}), °F				
1.0	10	408.557	70	86	85	18:06	4"	1.004	
1.0	10	398.310	70	86	85	18:06	4"	1.006	
1.0	10	418.917	70	86	85	18:00	4"	1.008	
		429.134		86	85				
		418.917		86	85				
									$\gamma = 1.006$

If there is only one thermometer on the dry gas meter, record the temperature under τ_d .

V_w = Gas volume passing through the wet test meter, ft³.

V_d = Gas volume passing through the dry gas meter, ft³.

τ_w = Temperature of the gas in the wet test meter, °F.

τ_{d1} = Temperature of the inlet gas of the dry gas meter, °F.

τ_{d2} = Temperature of the outlet gas of the dry gas meter, °F.

τ_d = Average temperature of the gas in the dry gas meter, °F.

ΔH = Pressure differential across orifice, in H₂O.

γ_1 = Ratio of accuracy of wet test meter to dry gas meter for each run.

γ = Average ratio of accuracy of wet test meter to dry gas meter for all three runs; tolerance = pretest $\gamma \pm 0.05\gamma$

P_b = Barometric pressure, in. Hg.

θ = Time of calibration run, min.

$$\gamma_1 = \frac{V_w P_b (\tau_d + 460)}{V_d (P_b + \frac{\Delta H}{13.6}) (\tau_w + 460)}$$

$$\Delta H \rho_1 = \frac{0.0317 \Delta H}{P_b (\tau_d + 460)} \left[\frac{(\tau_w + 460) \theta}{V_w} \right]$$

M. J. Barker

TYPE S PITOT TUBE INSPECTION DATA FORM

PITOT TUBE P5

Pitot tube assembly level? ☒ yes ☐ no

Pitot tube openings damaged? ☐ yes (explain below) ☒ no

$\alpha_1 = 2^\circ (<10^\circ)$, $\alpha_2 = 1^\circ (<10^\circ)$, $\beta_1 = 1^\circ (<5^\circ)$,
 $\beta_2 = 0^\circ (<5^\circ)$

$\gamma = 2^\circ$, $\theta = 1^\circ$, $A = .952$ cm (in.)

$z = A \sin \gamma = .033$ cm (in.); <0.32 cm ($<1/8$ in.),

$w = A \sin \theta = .017$ cm (in.); $<.08$ cm ($<1/32$ in.)

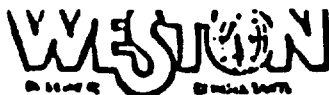
$P_A = .476$ cm (in.) $P_B = .476$ cm (in.)

$D_t = .372$ cm (in.)

Comments:

Inspected 9/2/88 J. M. D.

Calibration required? ☐ yes ☒ no



STACK TEMPERATURE SENSOR CALIBRATION DATA FORM

Date 1/17/89 ~~POTENTIOMETER~~ number Nitech 19
Ambient temperature 67 °F Barometric pressure 29.57 in. Hg
Calibrator JH Mill Reference: mercury-in-glass yes
other

Reference point number	Source (specify)	Reference thermometer temperature, °F	Thermocouple potentiometer temperature, °F	Temperature difference, %
	ICE BATH	32°F	34°F	+ 0.41%
	AMBIENT	67°F	67°F	0
	HOT OIL	301°F	306°F	+ 0.66%

Type of calibration system used.

$$\left[\frac{(\text{ref temp, } ^\circ\text{F} + 459.67) - (\text{test thermom temp, } ^\circ\text{F} + 459.67)}{\text{ref temp, } ^\circ\text{F} + 459.67} \right] 100 \leq 1.5\%$$

APPENDIX F

PROJECT PARTICIPANTS

PROJECT PARTICIPANTS

The following WESTON employees participated in this project:

Barry L. Jackson
Project Director

EconENVIRONomics

Jeffrey D. O'Neill
Section Manager

EconENVIRONomics

Jack Mills
Project Scientist Assistant

EconENVIRONomics

Rick Marz
Project Scientist Assistant

EconENVIRONomics

Ted Barker
Senior Field Technician

EconENVIRONomics

Nancy Robertson
Senior Laboratory Technician

EconENVIRONomics

