

Note: This is a reference cited in AP 42, *Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at www.epa.gov/ttn/chief/ap42/

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R-34-8-7-05H

R7-107

**TACB TESTING
OF
ASPHALTIC CONCRETE PLANT STACK EMISSIONS**

**WOOD MATERIAL SUPPLY INC.
CONROE, TEXAS**

**JULY 1987
NUS PROJECT NUMBER Y963**



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2-1-107

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Texas Air Control Board

R-34-8-7-05H

**TACB TESTING
OF
ASPHALTIC CONCRETE PLANT STACK EMISSIONS**

**WOOD MATERIAL SUPPLY INC.
CONROE, TEXAS**

**JULY 1987
NUS PROJECT NUMBER Y963**

Prepared By:

**William J. Cole, P.E.
Senior Project Manager**

Approved By:

**Calvin L. Spencer, P.E.
Manager - Industrial Programs
Waste Management Services Group**



16360 PARK TEN PLACE, SUITE 300
HOUSTON, TEXAS 77084
713-482-1888

C-34-8-7-066H
August 27, 1987

Mr. Paul Wood
Wood Material Supply, Inc.
2338 Sleepy Hollow Road
Conroe, Texas 77358

Subject: Hot Mix Asphalt Concrete Plant
100 South Second Street, Conroe
Montgomery County, Texas
NUS Project Number: Y963

Dear Mr. Wood:

We hereby submit results of stack sampling analyses performed at your Conroe, Texas Asphaltic Concrete Facility, July 14, 1987.

Testing was performed by Mullins Environmental Testing Company, Inc. on behalf of NUS Corporation (NUS), in accordance with test procedures described in the Texas Air Control Board (TACB) Sampling Manual. Particulate results were computed in:

- Grains per dry standard cubic foot (gr/dscf) - front-half particulate catch
- Pounds per hour (lbs/hr) - total particulate catch

Sulfur dioxide (SO₂) emissions were computed in lbs/hr and parts per million (ppm).

Throughout the test period, NUS provided an on-site observer to monitor stack sampling operations and to take stack opacity readings. Test results are given below.

Particulates Average 0.0370 gs/dscf *
Average 5.2 lbs/hr

Opacity Average Reading 0-5% **

Sulfur Dioxides Average 6.6 ppm
Average 1.03 lbs/hr

* Allowable front-half catch - 40CFR 60.90 - Subpart I - Standards of Performance for Hot Mix Asphalt Plants - 0.04 g/dscf.

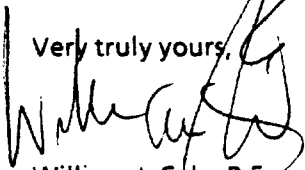
** Opacity visible emission readings by NUS on-site observer.

Copies of test results should be furnished to the Texas Air Control Board.

Mr. Paul Wood
Wood Material Supply, Inc.
August 27, 1987 - Page 2

Please contact me at (713) 492-1888 if you have any questions concerning test results or if you require any further assistance on this project.

Very truly yours,

A handwritten signature in black ink, appearing to read 'William J. Cole', written over the closing 'Very truly yours,'.

William J. Cole, P.E.
Senior Project Manager

WJC/pl



16360 PARK TEN PLACE, SUITE 300
HOUSTON, TEXAS 77084
713-492-1888

**This report contains results of testing
performed on behalf of NUS Corporation
by Mullins Environmental Testing, Inc. (METCO)
at: Wood Materials Supply Inc.
Conroe, Texas
July 1987**

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SOURCE EMISSIONS SURVEY
WOOD MATERIAL SUPPLY, INC.
CONROE, TEXAS
FOR
NUS CORPORATION
FILE NUMBER 87-88

INTRODUCTION

Mullins Environmental Testing Co., Inc., Dallas, Texas, conducted a source emissions survey of the Wood Material Supply, Inc. located in Conroe, Texas, on July 13 and 14, 1987. The purpose of this survey was to determine the emissions of particulate matter and sulfur dioxide from the Scrubber Exhaust Stack of the asphaltic concrete plant.

The sampling followed the procedures set forth in the Appendix to the Code of Federal Regulations, Title 40, Chapter I, Part 60, and in the "Sampling Procedures Manual, Texas Air Control Board, January 1983."

SUMMARY OF RESULTS

The principal conclusions are as follows:

1. The emissions of particulate matter from the stack were ^{5.2}~~4.9~~ pounds per hour (0.0370 grains per dry standard cubic foot), based on averaging the three tests using only the "front-half" collections of the EPA-type sampling train. The allowable particulate emission rate is 0.04 grains per dry standard cubic foot, as stated in the new source performance standards for asphalt concrete plants outlined in the Code of Federal Regulations, Title 40, Chapter I, Part 60, Subpart I. The actual emissions were 92.6 percent of the permitted emissions.
2. The emissions of particulate matter from the stack were 5.2 pounds per hour, based on averaging the three tests using both the "front-half" and "back-half" collections of the EPA-type sampling train. The allowable particulate emission rate, as calculated from Table I of Regulation I of the Texas Air Control Board Regulations, is equal to 28.7 pounds per hour. The actual emissions were 18.3 percent of the permitted emissions.

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3. The emissions of sulfur dioxide from the stack were 1.03 pounds per hour (6.6 parts per million), based on averaging the three tests.



SUMMARY OF RESULTS
Scrubber Exhaust Stack

Run Number	1	2	3
Stack Flow Rate - ACFM	30,180	31,120	28,854
Stack Flow Rate - DSCFM*	15,694	15,578	14,732
% Water Vapor - % Vol.	38.40	41.08	39.48
% CO ₂ - % Vol.	7.4	7.2	8.2
% O ₂ - % Vol.	10.8	10.8	9.6
% Excess Air @ Sampling Point	99	99	79
Particulates Probe, Cyclone & Filter Catch grains/dscf*	0.0317	0.0441	0.0353
grains/cf @ Stack Conditions	0.0165	0.0220	0.0180
lbs/hr	4.27	5.89	4.46
Total Catch grains/dscf*	0.0344	0.0464	0.0389
grains/cf @ Stack Conditions	0.0178	0.0231	0.0198
lbs/hr	4.63	6.19	4.92
Allowable Emission Rate EPA - 40 CFR 60 - grains/dscf	0.04	0.04	0.04
Allowable Emission Rate TACB - Reg. I - lbs/hr	28.8	29.3	28.0
Sulfur Dioxide Concentration - ppm	7.8	4.9	7.2
Sulfur Dioxide Emissions - lbs/hr	1.2	0.8	1.1

* 29.92 "Hg, 68°F (760 mm Hg, 20°C)
87-88

DISCUSSION OF RESULTS

The three tests for particulate matter taken on the Scrubber Exhaust Stack appeared to be valid representations of the actual emissions during the tests. The indicative parameters calculated from the field data were in close agreement. The moisture percentages for the three tests were within 3.6 percent of the mean value. The measured flow rates (Q_s) for the tests were within 3.9 percent of the mean value. The rates of sampling for the three tests were well within the specified limits, the greatest deviation being 6.2 percent.

The calculated emissions (grains per dry standard cubic foot) of particulate matter for the three tests showed a range of -14.4 percent to +19.1 percent variation from the mean value.

Sulfur dioxide was determined simultaneously during each test for particulate matter. The calculated emissions (pounds per hour) of sulfur dioxide showed a range of -22.6 percent to +16.1 percent variation from the mean value.

DESCRIPTION OF SAMPLING LOCATION

The sampling ports are located approximately 23 feet above the ground.

The sampling ports are located 8 feet 4 inches (2.44 stack diameters) downstream from the inlet to the stack and 3 feet 6 inches (1.02 stack diameters) upstream from the outlet of the stack.

SAMPLING AND ANALYTICAL PROCEDURES

The sampling followed the procedures outlined in the Appendix to the Code of Federal Regulations, Title 40, Chapter I, Part 60, and in the "Sampling Procedures Manual, Texas Air Control Board, January 1983."

A preliminary velocity traverse was made at each of the ports on the stack, in order to determine the uniformity and magnitude of the flow prior to testing. All points were checked for cyclonic flow and the average angle of cyclonic flow was equal to 9.5 degrees. Twelve traverse points were sampled from each of the two ports for a total of twenty-four traverse points on the Scrubber Exhaust Stack. Samples of three-minute duration were taken isokinetically at each of the twenty-four traverse points using an EPA-type, heated, glass-lined probe.

On all tests, the sampling train was leak-checked at the nozzle at 15 inches of mercury vacuum before each test, and leak-checked at the nozzle after each test at the highest vacuum reading recorded during the tests. This was done to predetermine the possibility of a diluted sample.

Also before and after each test, the pitot tube lines were checked for leaks under both a vacuum and a pressure. The lines were also checked for clearance and the manometer was zeroed before each test.

Particulate emissions were calculated from gravimetric analysis using both the "front-half" and "back-half" collections from the EPA-type sampling train. The "back-half" of the sampling train contained an 80-percent isopropyl alcohol solution to absorb sulfur trioxide, a six-percent hydrogen peroxide solution to absorb sulfur dioxide, and silica gel to absorb moisture. The isopropyl alcohol solution was checked for hydrogen peroxide contamination and none was found.

At the conclusion of each test, the sampling train was purged for fifteen minutes with ambient air at the same rate at which the sample was taken.

A grab orsat sample was taken during each test.



DESCRIPTION OF TESTS

Personnel from Mullins Environmental Testing Co., Inc. arrived at the plant at 5:30 p.m. on Monday, July 13, 1987. Arrangements were made for installation of monorail brackets on the stack. After the brackets were installed, equipment was moved onto the stack and secured for the night by 7:30 p.m.

On Tuesday, July 14, work began at 5:45 a.m. The equipment was prepared for testing, but testing was delayed because the plant was not operating due to rain. The preliminary data was collected beginning at 7:00 a.m. The first test for particulate matter and sulfur dioxide began at 8:05 a.m. Testing continued until completion of the test at 9:22 a.m. The second test began at 10:21 a.m. Testing continued until 10:30 a.m. when testing was stopped due to a temporary plant upset. Testing was resumed at 10:40 a.m. and continued until completion of the second test at 11:47 a.m. The third test began at 12:47 p.m. and was completed at 2:02 p.m.

The equipment was moved off of the stack and loaded into the sampling van. The samples were recovered and transported to Mullins Environmental Testing Co.'s laboratory in Dallas, Texas, for analysis and evaluation.

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Operations at Wood Material Supply, Inc. in Conroe, Texas, were completed at 3:30 p.m. on Tuesday, July 14, 1987.

Billy J. Mullins, Jr.
Billy J. Mullins, Jr., P.E.
President

APPENDICES

- A. Location of Sampling Points
- B. Source Emissions Calculations
- C. Calibration Data
- D. Field Testing Data
- E. Analytical Data
- F. Plant Operational Data
- G. Chain of Custody
- H. Resumes of Test Personnel

APPENDIX A

Location of Sampling Points

Scrubber Exhaust Stack

The sampling ports are located 8 feet 4 inches (2.44 stack diameters) downstream from the inlet to the stack and 3 feet 6 inches (1.02 stack diameters) upstream from the outlet of the stack. The locations of the sampling points were calculated as follows:

Port and Wall Thickness = 2 3/4 inches

Inside Stack Diameter = 41 inches

<u>Point Number</u>	<u>Percent of Diameter From Wall</u>	<u>Distance From Wall</u>
1	2.1	1 "
2	6.7	2 3/4 "
3	11.8	4 13/16"
4	17.7	7 1/4 "
5	25.0	10 1/4 "
6	35.6	14 9/16"
7	64.4	26 7/16"
8	75.0	30 3/4 "
9	82.3	33 3/4 "
10	88.2	36 3/16"
11	93.3	38 1/4 "
12	97.9	40 "

APPENDIX B

Nomenclature and Equations for Calculation of Source Emissions

Nomenclature for Particulate Calculations

<u>Symbol</u>	<u>English Units</u>	<u>Metric Units</u>	<u>Description</u>
A_s	in. ²	m ²	Stack Area
C_{an}	gr/dscf*	g/dscm*	Particulate - probe, cyclone and filter
C_{ao}	gr/dscf*	g/dscm*	Particulate - total
C_{at}	gr/CF @ stack conditions	g/m ³	Particulate - probe, cyclone and filter
C_{au}	gr/CF @ stack conditions	g/m ³	Particulate - total
C_{aw}	lbs/hr	kg/hr	Particulate - probe, cyclone and filter
C_{ax}	lbs/hr	kg/hr	Particulate - total
C_p			Pitot Tube Calibration Factor
D_n	in.	m	Sampling Nozzle Diameter
%EA			Percent Excess Air at sampling point
g	32.2 ft/sec ²		Acceleration of gravity
%I			Percent isokinetic
%M			Percent moisture in the stack gas by volume
M_d			Mole fraction of dry gas
m_f	mg	mg	Particulate - probe, cyclone and filter
M_{H_2O}	18 lb/lb-mole		Molecular Weight of Water
m_t	mg	mg	Particulate - total

* 29.92 "Hg, 528°R (760 mm Hg, 20°C) B-2

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<u>Symbol</u>	<u>English Units</u>	<u>Metric Units</u>	<u>Description</u>
MW	lb/lb-mole	g/g-mole	Molecular Weight of stack gas
MW _{air}	28.95 lb/lb-mole		Molecular Weight of air
MW _d	lb/lb-mole	g/g-mole	Molecular Weight of dry stack gas
P _b	"Hg Absolute	mm Hg	Barometric Pressure
P _m	"H ₂ O	mm H ₂ O	Orifice Pressure drop
P _s	"Hg Absolute	mm Hg	Stack Pressure
ΔP	"H ₂ O	mm H ₂ O	Velocity Head of stack gas
P _{std}	29.92 "Hg	760 mm Hg	Standard Barometric Pressure
Q _a	ACFM	m ³ /hr	Stack Gas Volume at Actual Stack Conditions
Q _s	DSCFM*	dscm/hr*	Stack Gas Volume at 29.92 "Hg, 528°R, dry
R	21.83 "Hg-ft ³ /lb-mole°R		Universal Gas Constant
T _m	°F	°C	Average Gas Meter Temperature
T _t	min	min	Net time of test
T _s	°F	°C	Stack Temperature
T _{std}	528°R	293°K	Standard Temperature
V _m	ft ³	m ³	Volume of dry gas sampled at meter conditions
V _{mstd}	dscf*	dscm*	Volume of dry gas sampled @ standard conditions
V _s	fpm	m/sec	Stack velocity @ stack conditions
V _w	ml	ml	Total Water Collected in Impingers and Silica Gel

* 29.92 "Hg, 528°R (760 mm Hg, 20°C) B-3

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<u>Symbol</u>	<u>English Units</u>	<u>Metric Units</u>	<u>Description</u>
$V_{w\text{ gas}}$	scf*	scm*	Volume of Water Vapor Collected @ standard conditions
ρ_{air}	0.0748 lbs/ft ³		Density of Air
$\rho_{\text{H}_2\text{O}}$	1 g/ml		Density of Water
ρ_{man}	51.63 lbs/ft ³		Density of Manometer Oil

Standard Conditions: 29.92 "Hg, 68°F (760 mm Hg, 20°C)

Example Particulate Calculations

1. Volume of dry gas sampled at standard conditions.*

$$V_{m_{std}} = V_m \left(\frac{T_{std}}{T_m + 460} \right) \left[\frac{P_b + \frac{P_m}{13.6}}{P_{std}} \right]$$

$$V_{m_{std}} = 17.65 V_m \left[\frac{P_b + \frac{P_m}{13.6}}{T_m + 460} \right] = \text{dscf}$$

$$V_{m_{std}} = \text{dscf} \times 0.028317 = \text{dscm}$$

2. Volume of water vapor collected at standard conditions.*

$$V_{w_{gas}} = \frac{(V_w - \text{gms SO}_2 - \text{gms H}_2\text{S}) \rho_{\text{H}_2\text{O}} R T_{std}}{P_{std} M_{\text{H}_2\text{O}} 453.6}$$

$$V_{w_{gas}} = 0.0472 (V_w - \text{gms SO}_2 - \text{gms H}_2\text{S}) = \text{scf}$$

$$V_{w_{gas}} = \text{scf} \times 0.028317 = \text{scm}$$

3. Percent moisture in stack gas.

$$\%M = \frac{V_{w_{gas}}}{V_{m_{std}} + V_{w_{gas}}} \times 100 = \%$$

4. Mole fraction of dry gas.

$$M_d = \frac{100 - \%M}{100}$$

5. Average molecular weight of dry stack gas.

$$MW_d = \left[\%CO_2 \times \frac{44}{100} \right] + \left[\%O_2 \times \frac{32}{100} \right] + \left[\%N_2 \times \frac{28}{100} \right] + \left[\%CO \times \frac{28}{100} \right] = \begin{matrix} \text{lb/lb-mole} \\ \text{= g/g-mole} \end{matrix}$$

6. Molecular weight of stack gas.

$$MW = MW_d \times M_d + 18 (1 - M_d) = \frac{\text{lb}}{\text{lb-mole}} = \text{g/g-mole}$$

7. Percent excess air at sampling point.

$$\%EA = \frac{100 (\%O_2 - 0.5\% CO)}{0.265 (\%N_2) - (\%O_2) + 0.5 (\%CO)}$$

8. Stack Pressure.

$$P_s = P_b + \frac{\text{stack pressure "H}_2\text{O}}{13.6} = \text{"Hg Absolute}$$

$$P_s = \text{"Hg Abs.} \times 25.4 = \text{mm Hg}$$

9. Stack velocity at stack conditions.

$$V_s = C_p \cdot 60 \left[\frac{2g \times \rho_{\text{man}} \times P_{\text{std}} \times MW_{\text{air}} \times (T_s + 460) \times \Delta P_s}{12 \times \rho_{\text{air}} \times P_s \times MW \times T_{\text{std}}} \right]^{\frac{1}{2}}$$

$$V_s = 5123.8 C_p \left[\frac{(T_s + 460) \times \Delta P_s}{P_s \times MW} \right]^{\frac{1}{2}} = \text{fpm}$$

$$V_s = \text{fpm} \times 0.00508 = \text{m/sec}$$

10. Dry stack gas volume at standard conditions.*

$$Q_s = \frac{1}{144} V_s \times A_s \times M_d \times \frac{T_{\text{std}}}{T_s + 460} \times \frac{P_s}{P_{\text{std}}}$$

$$Q_s = \frac{0.123 V_s \times A_s \times M_d \times P_s}{T_s + 460} = \text{DSCFM}$$

$$Q_s = \text{DSCFM} \times 1.6990 = \text{dscm/hr}$$

11. Actual stack gas volume at stack conditions.

$$Q_a = \frac{V_s \times A_s}{144} = \text{ACFM}$$

$$Q_a = \text{ACFM} \times 1.6990 = \text{m}^3/\text{hr}$$

12. Percent isokinetic.

$$\%I = \frac{V_{m_{std}} \times (T_s + 460) \times P_{std} \times 100 \times 144}{M_d \times T_{std} \times P_s \times T_t \times V_s \times \frac{\pi D_n^2}{4}}$$

$$\%I = \frac{1039 V_{m_{std}} \times (T_s + 460)}{M_d \times P_s \times T_t \times V_s \times D_n^2}$$

13. Particulate - probe, cyclone and filter.

$$C_{an} = \frac{m_f}{V_{m_{std}}} \times \frac{1 \text{ gr}}{64.8 \text{ mg}}$$

$$C_{an} = 0.0154 \frac{m_f}{V_{m_{std}}} = \text{gr/dscf}^*$$

$$C_{an} = \text{gr/dscf} \times 2.290 = \text{g/dscm}^*$$

14. Particulate total.

$$C_{ao} = 0.0154 \times \frac{m_t}{V_{m_{std}}} = \text{gr/dscf}^*$$

$$C_{ao} = \text{gr/dscf} \times 2.290 = \text{g/dscm}^*$$

* 29.92 "Hg, 528°R (760 mm Hg, 20°C) B-8

15. Particulate - probe, cyclone and filter at stack conditions.

$$C_{at} = C_{an} \times \frac{P_s}{P_{std}} \times \frac{(T_{std})}{(T_s + 460)} \times M_d$$

$$C_{at} = \frac{17.65 \times C_{an} \times P_s \times M_d}{T_s + 460} = \text{gr/CF}$$

$$C_{at} = \text{gr/CF} \times 2.290 = \text{g/m}^3$$

16. Particulate - total, at stack conditions.

$$C_{au} = \frac{17.65 \times C_{ao} \times P_s \times M_d}{T_s + 460} = \text{gr/CF}$$

$$C_{au} = \text{gr/CF} \times 2.290 = \text{g/m}^3$$

17. Particulate - probe, cyclone and filter.

$$C_{aw} = C_{an} \times Q_s \times \frac{60 \text{ min}}{1 \text{ hr}} \times \frac{1 \text{ lb}}{7000 \text{ gr}}$$

$$C_{aw} = 0.00857 \times C_{an} \times Q_s = \text{lbs/hr}$$

$$C_{aw} = \text{lbs/hr} \times 0.4536 = \text{kg/hr}$$

18. Particulate - total.

$$C_{ax} = 0.00857 \times C_{ao} \times Q_s = \text{lbs/hr}$$

$$C_{ax} = \text{lbs/hr} \times 0.4536 = \text{kg/hr}$$

SOURCE EMISSION SURVEY

JOB NUMBER: 87-88
 JOB NAME: WOOD MATERIALS SUPPLY, INC.
 LOCATION: CONROE, TX
 UNIT TESTED: SCRUBBER STACK

SOURCE EMISSION CALCULATIONS

SYMBOL	DESCRIPTION	UNITS	1	2	3
RUN #					
DATE			7/14/87	7/14/87	7/14/87
BEGIN TIME			805	1021	1247
END TIME			922	1147	1402
IP(b)	BAROMETRIC PRESSURE	"Hg Abs. (mm Hg)	29.90 (759)	29.95 (761)	29.93 (760)
IP(m)	ORIFICE PRESSURE DROP	"H ₂ O (mm H ₂ O)	1.043 (26.5)	1.211 (30.8)	1.015 (25.8)
IV(m)	VOLUME DRY GAS SAMPLED @ METER CONDITIONS	ft. ³ (m ³)	39.458 (1.117)	42.638 (1.207)	39.181 (1.109)
IT(m)	AVERAGE GAS METER TEMPERATURE	DEG. F (DEG. C)	76 (24)	78 (26)	82 (28)
IV(m(std))	VOLUME DRY GAS SAMPLED @ STANDARD CONDITIONS*	DSCF (DSCM)	38.949 (1.103)	42.019 (1.190)	38.283 (1.084)
IV(w)	TOTAL WATER COLLECTED, IMPINGERS & SILICA GEL	ml	514.3	620.8	529.2
IV(w(gas))	VOLUME WATER VAPOR COLLECTED @ STANDARD CONDITIONS*	SCF (SCM)	24.275 (0.687)	29.302 (0.830)	24.978 (0.707)
%H	MOISTURE IN STACK GAS BY VOLUME	%	38.40	41.08	39.48

* 68 Deg. F, 29.92 "Hg (20 Deg. C, 760 mm Hg)

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SOURCE EMISSION CALCULATIONS

MOOD MATERIALS SUPPLY, INC.
CONROE, TX
SCRUBBER STACK

SYMBOL	DESCRIPTION	UNITS			
IMd	IMOL FRACTION OF DRY GAS		0.6160	0.5892	0.6052
IC02		%	7.4	7.2	8.2
IO2		%	10.8	10.8	9.6
IC0		%	0.0	0.0	0.0
IN2		%	81.8	82.0	82.2
IEA	IECESS AIR @ SAMPLING IPOINT	%	99.3	98.8	78.8
IMWd	IMOLECULAR WEIGHT OF IDRY STACK GAS	LB/LB-MOLE (g/g-MOLE)	29.62 (29.62)	29.58 (29.58)	29.70 (29.70)
IMW	IMOLECULAR WEIGHT OF ISTACK GAS	LB/LB-MOLE (g/g-MOLE)	25.16 (25.16)	24.83 (24.83)	25.08 (25.08)
IDELTA P	I VELOCITY HEAD OF STACK IGAS	"H2O (mm H2O)	0.802 (20.4)	0.850 (21.6)	0.738 (18.7)
ITs	I STACK TEMPERATURE	DEG. F (DEG. C)	166 (74)	164 (73)	168 (76)
IPs	I STACK PRESSURE	"Hg Abs. (mm Hg)	29.84 (758)	29.93 (760)	29.91 (760)
IVs	I STACK VELOCITY @ STACK ICONDITIONS	FPM (m/SEC.)	3,292 (16.72)	3,395 (17.25)	3,148 (15.99)
IRs	I STACK AREA	(SQ. INCHES) (SQ. METERS)	1,320 (0.85)	1,320 (0.85)	1,320 (0.85)
IDs	IDRY STACK GAS VOLUME @ ISTANDARD CONDITIONS*	DSCFM (DSCM/HR)	15,694 (26,664)	15,578 (26,467)	14,732 (25,030)
IQa	I ACTUAL STACK GAS VOLUME I@ STACK CONDITIONS	ACFM (m ³ /HR)	30,180 (51,276)	31,120 (52,873)	28,854 (49,023)

* 68 Deg. F, 29.92 "Hg (20 Deg. C, 760 mm Hg) B-11

MULLINS ENVIRONMENTAL TESTING CO., INC.

SOURCE EMISSION CALCULATIONS

WOOD MATERIALS SUPPLY, INC.
CONROE, TX
SCRUBBER STACK

SYMBOL	DESCRIPTION	UNITS			
It	NET TIME OF TEST	MINUTES	72	72	72
Dn	SAMPLING NOZZLE DIAM.	IN. (m)	0.249 (0.006)	0.249 (0.006)	0.249 (0.006)
%I	PERCENT ISOKINETIC	%	93.8	101.9	98.2
Inf	PARTICULATE - PROBE, CYCLONE AND FILTER	mg	80.3	120.4	87.8
Int	PARTICULATE - TOTAL	mg	87.0	126.6	96.8
Can	PARTICULATE - PROBE, CYCLONE AND FILTER	gr/DSCF* (g/DSCM)	0.0317 (0.0727)	0.0441 (0.1011)	0.0353 (0.0809)
Cao	PARTICULATE - TOTAL	gr/DSCF* (g/DSCM)	0.0344 (0.0788)	0.0464 (0.1063)	0.0389 (0.0892)
Cat	PARTIC. - PROBE, CYCLONE AND FILTER @ STACK COND.	gr/CF (g/m3)	0.0165 (0.0377)	0.0220 (0.0504)	0.0180 (0.0411)
Cau	PARTICULATE - TOTAL @ STACK CONDITIONS	gr/CF (g/m3)	0.0178 (0.0408)	0.0231 (0.0529)	0.0198 (0.0453)
Cam	PARTICULATE - PROBE, CYCLONE AND FILTER	LBS/HR (Kg/HR)	4.27 (1.94)	5.89 (2.67)	4.46 (2.02)
Cax	PARTICULATE - TOTAL	LBS/HR (Kg/HR)	4.63 (2.10)	6.19 (2.81)	4.92 (2.23)

* 68 Deg.F, 29.92 "Hg (20 Deg.C, 760 mm Hg)

SULFUR DIOXIDE EMISSION DATA

JOB NUMBER:	87-88
JOB NAME:	WOOD MATERIALS SUPPLY, INC.
LOCATION:	CONROE, TX
UNIT TESTED:	SCRUBBER STACK

RUN NUMBER	1	2	3
DATE	7/14/87	7/14/87	7/14/87
START TIME	805	1021	1247
END TIME	922	1147	1402
N - NORMALITY OF Ba(ClO4)2	0.0100	0.0100	0.0100
ML(I) - ml IN IMPINGER 2	413	436	369
ML(I) - ml IN IMPINGER 3	522	392	492
ML(A) - ml IN ALIQUOT #2	10.00	10.00	10.00
ML(A) - ml IN ALIQUOT #3	10.00	10.00	10.00
ML(B) - ml OF Ba(ClO4)2 TO TITRATE #2	1.18	1.10	1.27
ML(B) - ml OF Ba(ClO4)2 TO TITRATE #3	0.52	0.12	0.45
ML(BB) - ml OF Ba(ClO4)2 TO TITRATE BLANK	0.05	0.05	0.05
Tm - AVERAGE GAS METER TEMPERATURE, DEG. F	76	78	82
Vm - VOLUME OF DRY GAS SAMPLED @ METER CONDITIONS, FT^3	39.458	42.638	39.181
Pb - BAROMETRIC PRESSURE, "Hg Abs.	29.90	29.95	29.93
Qs - STACK GAS VOLUME DRY @ STANDARD CONDITIONS, #SCFM	15,694	15,578	14,732
C(I) - SO2 IN IMPINGER #2 IN mgs	14.93	14.65	14.41
C(I) - SO2 IN IMPINGER #3 IN mgs	7.85	0.88	6.30
C(T) - TOTAL SO2 IN IMPINGERS, IN mgs	22.8	15.5	20.7
ppm SO2	7.8	4.9	7.2
C(SO2) - EMISSION RATE OF SO2, lbs/day	29.2	18.3	25.3
C(SO2) - EMISSION RATE OF SO2, lbs/hr	1.2	0.8	1.1
Cs - EMISSION RATE OF SULFUR, lbs/day	14.6	9.2	12.7

* 68 Deg.F, 29.92 "Hg (20 Deg.C, 760 mm Hg)

$$C(I) = ML(I) \div [ML(B) - ML(BB)] \div N \div 32 \div ML(A)$$

$$C(T) = C(I) \#2 + C(I) \#3$$

$$\text{ppm SO}_2 = 0.7513 \div C(T) \div [T_m + 460] \div V_m \div P_b$$

$$C(SO_2) = \text{ppm SO}_2 \div Q_s \div 0.0002392$$

SULFUR TRIOXIDE EMISSION DATA

JOB NUMBER:
JOB NAME:
LOCATION:
UNIT TESTED:

87-88
WOOD MATERIALS SUPPLY, INC.
CONROE, TX
SCRUBBER STACK

RUN NUMBER	1	2	3
DATE	7/14/87	7/14/87	7/14/87
START TIME	805	1021	1247
END TIME	922	1147	1402
N - NORMALITY OF Ba(ClO4)2	0.0100	0.0100	0.0100
ML(I) - ml IN IMPINGER	405	400	426
ML(A) - ml IN ALIQUOT	10.00	10.00	10.00
ML(B) - ml OF Ba(ClO4)2 TO TITRATE	0.30	0.30	0.25
ML(BB) - ml OF Ba(ClO4)2 TO TITRATE BLANK	0.05	0.05	0.05
Tm - AVERAGE GAS METER TEMPERATURE, DEG. F	76	78	82
Vm - VOLUME OF DRY GAS SAMPLED @ METER CONDITIONS, FT^3	39.458	42.638	39.181
Pb - BAROMETRIC PRESSURE, "Hg Abs.	29.90	29.95	29.93
Qs - STACK GAS VOLUME DRY @ STANDARD CONDITIONS, +SCFM	15,694	15,578	14,732
C(I) - SO3 IN IMPINGERS IN mgs	4.1	4.0	3.4
ppm SO3	1.1	1.0	0.9
C(SO3) - EMISSION RATE OF SO3, lbs/day	5.2	4.7	4.2
Cs - EMISSION RATE OF SULFUR, lbs/day	2.1	1.9	1.7

* 68 Deg. F, 29.92 "Hg (20 Deg. C, 760 mm Hg)

$$C(I) = \frac{ML(I) + [ML(B) - ML(BB)] \times N \times 40}{ML(A)}$$

$$ppm SO_3 = \frac{0.6021 \times C(I) \times [T_m + 460]}{V_m \times P_b}$$

$$C(SO_3) = ppm SO_3 \times Q_s \times 0.0002991$$

$$C_s = C(SO_3) / 2.5$$

APPENDIX C

Calibration Data

<u>Equipment</u>	<u>Calibration Factor</u>	<u>Calibration Date</u>
Pitot Tube #12	0.807	3/ 9/87
Probe Tip #II-4	0.249	5/18/87
Dry Gas Meter #6	1.008	4/ 1/87
Stack Unit Orifice #6		4/ 2/87
Digital Temperature Indicator #6		4/ 2/87
Barometer #1		5/15/87

PITOT TUBE CALIBRATION

Date: 3-9-87

Time: 1035

Pitot No. 12

P_b: 29.70 "Hg P_s: - "H₂O

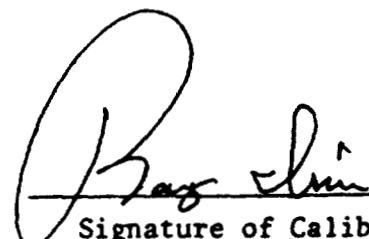
T_s: 74 °F C_{pstd}: 0.99

Motor Setting	fps mark	CALIBRATOR STANDARD START	END	STANDARD AVERAGE	HIGH	√ HIGH	CAL. FACTOR	LOW	√ LOW	CAL. FACTOR
39	20	0.10	0.10	0.316	0.15	0.387	0.808 ✓	0.15	0.387	0.808 ✓
48	30	0.20	0.20	0.447	0.30	0.548	0.808 ✓	0.30	0.548	0.808 ✓
55	40	0.35	0.34	0.587	0.52	0.721	0.806 ✓	0.52	0.721	0.806 ✓
63	50	0.60	0.60	0.775	0.90	0.949	0.808 ✓	0.89	0.943	0.813 ✓
70	60	0.85	0.85	0.922	1.30	1.140	0.801 ✓	1.30	1.140	0.801 ✓
76	70	1.00	1.00	1.00	1.50	1.225	0.808 ✓	1.50	1.225	0.808 ✓
84	80	1.40	1.40	1.183	2.10	1.449	0.808 ✓	2.10	1.449	0.808 ✓
100	90	1.60	1.60	1.265	2.40	1.549	0.808 ✓	2.40	1.549	0.808 ✓
63	50	0.60	0.60	0.775	0.90	0.949	0.808 ✓	0.90	0.949	0.808 ✓
63	50	0.60	0.60	0.775	0.90	0.949	0.808 ✓	0.90	0.949	0.808 ✓
Average							0.807 ✓			0.808

Summary of Results:

Normal high side calibration factor 0.807
variation +0.12% - 0.74%

Normal low side calibration factor 0.808
variation +0.62% - 0.87%


Signature of Calibrator
✓



NOZZLE CALIBRATION

Nozzle Set No. IIDate 18 May 1987Calibrator: Chuck Thompson

	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>
Reading 1	<u>0.188</u>	<u>0.130</u>	<u>0.253</u>	<u>0.250</u>	<u>0.319</u>	<u>0.338</u>
Reading 2	<u>0.186</u>	<u>0.129</u>	<u>0.253</u>	<u>0.248</u>	<u>0.319</u>	<u>0.337</u>
Reading 3	<u>0.187</u>	<u>0.131</u>	<u>0.252</u>	<u>0.249</u>	<u>0.318</u>	<u>0.339</u>
Reading 4	<u>0.187</u>	<u>0.130</u>	<u>0.253</u>	<u>0.249</u>	<u>0.317</u>	<u>0.338</u>
Reading 5	<u>0.186</u>	<u>0.130</u>	<u>0.251</u>	<u>0.249</u>	<u>0.318</u>	<u>0.338</u>
Reading 6	<u>0.188</u>	<u>0.130</u>	<u>0.252</u>	<u>0.250</u>	<u>0.318</u>	<u>0.337</u>
Reading 7	<u>0.187</u>	<u>0.131</u>	<u>0.252</u>	<u>0.250</u>	<u>0.318</u>	<u>0.338</u>
Reading 8	<u>0.187</u>	<u>0.130</u>	<u>0.251</u>	<u>0.249</u>	<u>0.318</u>	<u>0.338</u>
Reading 9	<u>0.187</u>	<u>0.130</u>	<u>0.251</u>	<u>0.250</u>	<u>0.318</u>	<u>0.338</u>
Reading 10	<u>0.186</u>	<u>0.131</u>	<u>0.253</u>	<u>0.248</u>	<u>0.318</u>	<u>0.337</u>
Average	0.187	0.130	0.252	0.249	0.318	0.338

	<u>7</u>	<u>8</u>	<u>9</u>	<u>10</u>	<u>11</u>
Reading 1	<u>0.357</u>	<u>0.426</u>	<u>0.504</u>	<u>0.504</u>	<u>0.189</u>
Reading 2	<u>0.358</u>	<u>0.425</u>	<u>0.504</u>	<u>0.503</u>	<u>0.190</u>
Reading 3	<u>0.356</u>	<u>0.425</u>	<u>0.504</u>	<u>0.504</u>	<u>0.190</u>
Reading 4	<u>0.357</u>	<u>0.424</u>	<u>0.504</u>	<u>0.504</u>	<u>0.190</u>
Reading 5	<u>0.357</u>	<u>0.426</u>	<u>0.504</u>	<u>0.503</u>	<u>0.190</u>
Reading 6	<u>0.357</u>	<u>0.424</u>	<u>0.504</u>	<u>0.504</u>	<u>0.191</u>
Reading 7	<u>0.357</u>	<u>0.424</u>	<u>0.502</u>	<u>0.503</u>	<u>0.190</u>
Reading 8	<u>0.356</u>	<u>0.424</u>	<u>0.503</u>	<u>0.504</u>	<u>0.189</u>
Reading 9	<u>0.356</u>	<u>0.424</u>	<u>0.503</u>	<u>0.504</u>	<u>0.190</u>
Reading 10	<u>0.357</u>	<u>0.426</u>	<u>0.504</u>	<u>0.504</u>	<u>0.191</u>
Average	0.357	0.425	0.504	0.504	0.190

Dry Gas Meter Calibration

Dry Gas Meter Number 6

Date: 1 APRIL 1987

ΔH ($"H_2O$)	C_{DG}	
0.5	<u>1.006</u>	
1.0	<u>1.003</u>	
1.5	<u>1.002</u>	
2.0	<u>1.010</u>	
3.0	<u>1.011</u>	
4.0	<u>1.008</u>	
Average	<u>1.008</u>	Variation: + <u>0.30%</u> - <u>0.50%</u>

Calibrator: John R. Smith
Checked by: DA

C_{DG} @ 2 liters/min. = 1.012 ✓ 4/2/87

METCO

DRY GAS METER CALIBRATION

Meter Number: 6

Calibrator: John R. Smith

Date: 1 APRIL 1987

$$\text{Calibration Factor } (C_{DG}) = \frac{\text{Wet Test Meter } V_{m\text{std}}}{\text{Dry Gas Meter } V_{m\text{std}}}$$

Run No.: 1 @ 0.50

P_b : 29.26 "Hg
Control Module Vacuum 5.1 "Hg

WET TEST METER (No. 2)

DRY GAS METER

	Time	Meter Reading	Temp.	P_m	Meter Reading	Temp. In	Temp. Out	P_m
End	144709	5.001 cf	74 °F	-1.25 "H ₂ O	262.577cf	71 °F	67 °F	0.50 "H ₂ O
Start	1435	0.000 cf	74 °F	-1.25 "H ₂ O	257.700cf	69 °F	65 °F	0.50 "H ₂ O
	12.09	5.001 cf	74 °F	-1.25 "H ₂ O	4.877 cf	70 °F	66 °F	0.50 "H ₂ O

$$\text{Wet Test Meter } V_{m\text{std}} = 17.65 \times 5.001 \left(\frac{29.26 + \frac{(-1.25)}{13.6}}{74 + 460} \right) \times 0.997 = 4.807 \text{ dscf} \quad (C_f)$$

$$\text{Dry Gas Meter } V_{m\text{std}} = 17.65 \times 4.877 \left(\frac{29.26 + \frac{0.50}{13.6}}{68 + 460} \right) = 4.776 \text{ dscf}$$

$$C_{DG} = \frac{4.807}{4.776} = \boxed{1.006}$$

METCO

DRY GAS METER CALIBRATION

Meter Number: 6

Calibrator: John R. Smith

Date: 1 APRIL 1987

$$\text{Calibration Factor } (C_{DG}) = \frac{\text{Wet Test Meter } V_{m_{std}}}{\text{Dry Gas Meter } V_{m_{std}}}$$

Run No.: 1 @ 1.00

P_b: 29.26 "Hg

Control Module Vacuum 5.0 "Hg

WET TEST METER (No. 2)

DRY GAS METER

	Time	Meter Reading	Temp.	P _m	Meter Reading	Temp. In	Temp. Out	P _m
End	1458.65	5.000 cf	74 °F	-1.70 "H ₂ O	268.000 cf	73 °F	68 °F	1.00 "H ₂ O
Start	1450	0.000 cf	74 °F	-1.70 "H ₂ O	263.101 cf	71 °F	67 °F	1.00 "H ₂ O
	8.65	5.000 cf	74 °F	-1.70 "H ₂ O	4.899 cf	72 °F	68 °F	1.00 "H ₂ O

$$\text{Wet Test Meter } V_{m_{std}} = 17.65 \times 5.000 \left(\frac{29.26 + \frac{4.70}{13.6}}{74 + 460} \right) \times 0.997 = 4.800 \text{ dscf} \quad (C_f)$$

$$\text{Dry Gas Meter } V_{m_{std}} = 17.65 \times 4.899 \left(\frac{29.26 + \frac{1.00}{13.6}}{70 + 460} \right) = 4.786 \text{ dscf}$$

$$C_{DG} = \frac{4.800}{4.786} = \boxed{1.003}$$

METCO

DRY GAS METER CALIBRATION

Meter Number: 6

Calibrator: John R. Smith

Date: 1 APRIL, 1987

$$\text{Calibration Factor (C}_{\text{DG}}) = \frac{\text{Wet Test Meter } V_{\text{m std}}}{\text{Dry Gas Meter } V_{\text{m std}}}$$

Run No.: 1 @ 1.50

P_b: 29.25 "Hg

Control Module Vacuum 5.1 "Hg

WET TEST METER (No. 2).

DRY GAS METER

	Time	Meter Reading	Temp.	P _m	Meter Reading	In	Temp.	Out	P _m
End	1515.17	10.000 cf	74 °F	-2.15 "H ₂ O	278.155 cf	77 °F	71 °F	1.50 "H ₂ O	
Start	1501	0.000 cf	74 °F	-2.15 "H ₂ O	268.358 cf	73 °F	69 °F	1.50 "H ₂ O	
	14.17	10.000 cf	74 °F	-2.15 "H ₂ O	9.797 cf	75 °F	70 °F	1.50 "H ₂ O	

$$\text{Wet Test Meter } V_{\text{m std}} = 17.65 \times 10.000 \left(\frac{29.25 + \frac{(-2.15)}{13.6}}{74 + 460} \right) \times 0.997 = 9.587 \text{ dscf} \quad (C_f)$$

$$\text{Dry Gas Meter } V_{\text{m std}} = 17.65 \times 9.797 \left(\frac{29.25 + \frac{1.50}{13.6}}{73 + 460} \right) = 9.525 \text{ dscf}$$

$$C_{\text{DG}} = \frac{9.587}{9.525} = \boxed{1.007}$$

METCO

DRY GAS METER CALIBRATION

Meter Number: 6

Calibrator: John R. Smith

Date: 1 APRIL 1987

$$\text{Calibration Factor } (C_{DG}) = \frac{\text{Wet Test Meter } V_{m\text{std}}}{\text{Dry Gas Meter } V_{m\text{std}}}$$

Run No.: 1 @ 2.00

P_b : 29.24 "Hg
Control Module Vacuum 5.1 "Hg

WET TEST METER (No. 2)

DRY GAS METER

	Time	Meter Reading	Temp.	P_m	Meter Reading	Temp. In	Temp. Out	P_m
End	1555.34	10.000 cf	74 °F	-2.60 "H ₂ O	308.827 cf	82 °F	74 °F	2.00 "H ₂ O
Start	1543	0.000 cf	74 °F	-2.60 "H ₂ O	299.000 cf	81 °F	73 °F	2.00 "H ₂ O
	12.34	10.000 cf	74 °F	-2.60 "H ₂ O	9.827 cf	82 °F	74 °F	"H ₂ O

$$\text{Wet Test Meter } V_{m\text{std}} = 17.65 \times 10.000 \left(\frac{29.24 + \frac{(-2.60)}{13.6}}{74 + 460} \right) \times 0.997 = 9.573 \text{ dscf} \quad (C_f)$$

$$\text{Dry Gas Meter } V_{m\text{std}} = 17.65 \times 9.827 \left(\frac{29.24 + \frac{2.00}{13.6}}{78 + 460} \right) = 9.474 \text{ dscf}$$

$$C_{DG} = \frac{9.573}{9.474} = \boxed{1.010}$$

METCO

DRY GAS METER CALIBRATION

Meter Number: 6

Calibrator: John R. Smith

Date: 1 APRIL, 1987

$$\text{Calibration Factor (C}_{\text{DG}}) = \frac{\text{Wet Test Meter } V_{\text{m std}}}{\text{Dry Gas Meter } V_{\text{m std}}}$$

Run No.: 1 @ 3.00

P_b: 29.24 "Hg

Control Module Vacuum 5.0 "Hg

WET TEST METER (No. 2)

DRY GAS METER

	Time	Meter Reading	Temp.	P _m	Meter Reading	Temp. In	Temp. Out	P _m
End	1541.10	10.001 cf	74 °F	-3.45 "H ₂ O	298.662 cf	83 °F	73 °F	3.00 "H ₂ O
Start	1531	0.000 cf	74 °F	-3.45 "H ₂ O	288.904 cf	79 °F	72 °F	3.00 "H ₂ O
	10.10	10.001 cf	74 °F	-3.45 "H ₂ O	9.758 cf	81 °F	73 °F	3.00 "H ₂ O

$$\text{Wet Test Meter } V_{\text{m std}} = 17.65 \times 10.001 \left(\frac{29.24 + \frac{(-3.45)}{13.6}}{74 + 460} \right) \times 0.997 = 9.553 \text{ dscf} \quad (C_f)$$

$$\text{Dry Gas Meter } V_{\text{m std}} = 17.65 \times 9.758 \left(\frac{29.24 + \frac{3.00}{13.6}}{77 + 460} \right) = 9.449 \text{ dscf}$$

$$C_{\text{DG}} = \frac{9.553}{9.449} = \boxed{1.011}$$

METCO

DRY GAS METER CALIBRATION

Meter Number: 6

Calibrator: John R. Smith

Date: 1 APRIL, 1987

$$\text{Calibration Factor (C}_{DG}\text{)} = \frac{\text{Wet Test Meter } V_{m\text{std}}}{\text{Dry Gas Meter } V_{m\text{std}}}$$

Run No.: 1 @ 4.00

P_b: 29.24 "Hg

Control Module Vacuum 5.0 "Hg

WET TEST METER (No. 2)

DRY GAS METER

	Time	Meter Reading	Temp.	P _m	Meter Reading	Temp. In	Temp. Out	P _m
End	1606.82	10.003 cf	74 °F	-4.30 "H ₂ O	319.065 cf	84 °F	74 °F	4.00 "H ₂ O
Start	1558	0.000 cf	74 °F	-4.30 "H ₂ O	309.300 cf	80 °F	74 °F	4.00 "H ₂ O
	8.82	10.003 cf	74 °F	-4.30 "H ₂ O	9.765 cf	82 °F	74 °F	4.00 "H ₂ O

$$\text{Wet Test Meter } V_{m\text{std}} = 17.65 \times 10.003 \left(\frac{29.24 + \frac{(-4.30)}{13.6}}{74 + 460} \right) \times 0.997 = 9.534 \text{ dscf} \quad (C_f)$$

$$\text{Dry Gas Meter } V_{m\text{std}} = 17.65 \times 9.765 \left(\frac{29.24 + \frac{4.00}{13.6}}{78 + 460} \right) = 9.461 \text{ dscf}$$

$$C_{DG} = \frac{9.534}{9.461} = \boxed{1.008}$$

METCO

DRY GAS METER CALIBRATION

Meter Number: 6

Calibrator: John R. Smith

Date: 2 APRIL 1987

$$\text{Calibration Factor (C}_{\text{DG}}) = \frac{\text{Wet Test Meter } V_{\text{m std}}}{\text{Dry Gas Meter } V_{\text{m std}}}$$

Run No.: 1 @ 2 lpm

P_b: 29.55 "Hg

Control Module Vacuum 0.5 "Hg

WET TEST METER (No. 1)

DRY GAS METER

	Time	Meter Reading	Temp.	P _m	Meter Reading	Temp. In	Temp. Out	P _m
End	0858.84	2.000 cf	71 °F	-0.50 "H ₂ O	331.861 cf	71 °F	69 °F	0.00 "H ₂ O
Start	0831	0.000 cf	71 °F	-0.50 "H ₂ O	329.900 cf	69 °F	67 °F	0.00 "H ₂ O
	27.84	2.000 cf	71 °F	-0.50 "H ₂ O	1.961 cf	70 °F	68 °F	0.00 "H ₂ O

$$\text{Wet Test Meter } V_{\text{m std}} = 17.65 \times 2.000 \left(\frac{29.55 + \frac{0.00}{13.6}}{71 + 460} \right) \times 1.002 \frac{(C_{\text{std}})}{(C_{\text{f}})} = 1.966 \text{ dscf}$$

$$\text{Dry Gas Meter } V_{\text{m std}} = 17.65 \times 1.961 \left(\frac{29.55 + \frac{0.00}{13.6}}{69 + 460} \right) = 1.933 \text{ dscf}$$

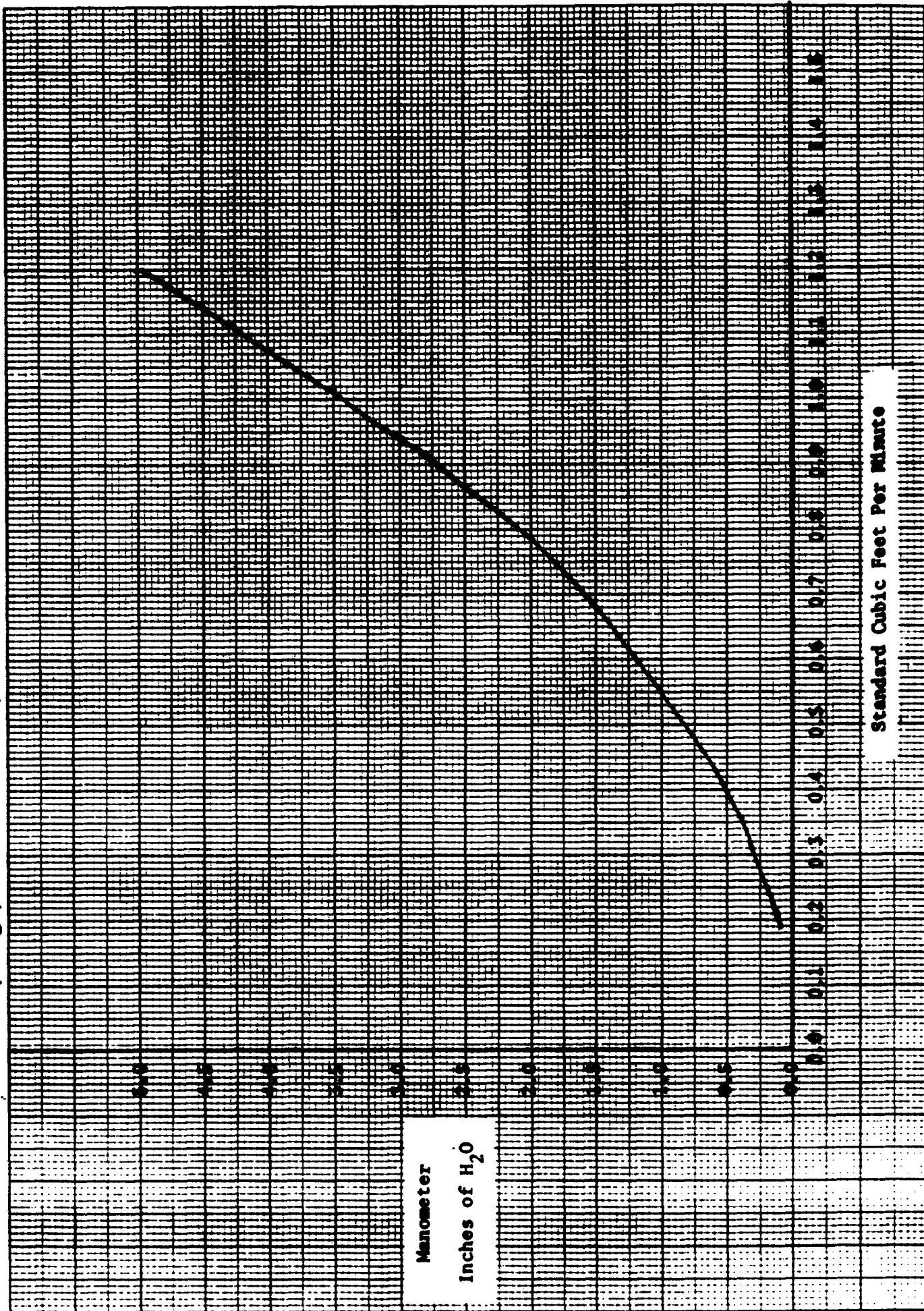
$$C_{\text{DG}} = \frac{1.966}{1.933} = \boxed{1.017}$$

(2.000 lpm)

4-2-87

DGM-6

R. Irwin



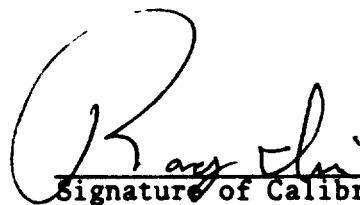
DIGITAL TEMPERATURE INDICATOR NO. 6

CALIBRATION DATA

Date: 4-2-87

<u>Media</u>	<u>Time</u>	<u>Mercury Thermometer (°F)</u>	<u>DTI (°F)</u>
Ice Bath	<u>1025</u>	<u>32</u>	<u>32</u>
Ambient Air	<u>1028</u>	<u>69</u>	<u>68</u>
Boiling Water	<u>1032</u>	<u>212</u>	<u>212</u>
Oven	<u>1041</u>	<u>148</u>	<u>150</u>
Oven	<u>1101</u>	<u>276</u>	<u>275</u>
Oven	<u>1115</u>	<u>353</u>	<u>350</u>
Oven	<u>1126</u>	<u>404</u>	<u>400</u>

Meter Adjusted? Yes No ✓


Signature of Calibrator

BAROMETER CALIBRATION

Barometer No. 1

Date: 5/15/87

Time: 0820

Barometric Pressure @ Addison Field @ 719 ft. = 30.11

- 0.719

Absolute Pressure at Addison Field = 29.391

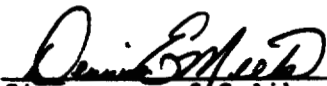
+ 0.083

Absolute Pressure @ METCO @ 636 ft. = 29.47

Barometer Reading = 29.42

Variation = -0.05

Barometer Adjusted? Yes No


Signature of Calibrator

METCO

APPENDIX D

Field Testing Data

MULLINS ENVIRONMENTAL TESTING CO., INC.

Job No. 87-88 ACT, SO2 FIELD DATA

Job Name Need Materials Supply

Run No. 1

Location Scrubber Stack

Date 13 July 1987

Operator Alexander, Orr

Sample Box No. 3 Meter Box No. 6

Ambient Temp. °F 76

Assumed Moisture % 33

Probe Length 3'

C Factor 13.7 to reference

Initial Leak @ 16.0 "Hg = 0.002 cfm

Final Leak @ 11.0 "Hg = 0.006 cfm

Read and record at the start of each test point.

Purge to: 818.433

Purge time: 0926 - 0941

Point	Clock Time	Dry Gas Meter, CF	Pitot in. H ₂ O	Δ P _s		Pump Vacuum In. Hg Gauge	Stack Temp. °F	Probe Temp. °F	Oven Temp. °F	Effluent Temp. °F	T _m		Remarks
				Desired	Actual						Inlet	Outlet	
A12	0805	772.700	1.00	1.40	1.40	4.5	163	232	228	75	74	75	
11	0808	774.65	1.10	1.50	1.50	6.5	163	236	232	70	75	75	
10	0811	776.47	1.30	1.70	1.70	8.3	164	238	237	63	75	75	
9	0814	778.57	1.35	1.80	1.80	9.2	165	251	242	63	75	75	refuge
8	0817	780.78	1.15	1.50	1.50	7.0	166	270	247	66	76	75	
7	0820	782.79	0.87	1.15	1.15	5.2	165	273	250	72	76	75	
6	0823	784.63	0.40	0.53	0.53	3.0	166	269	252	73	77	74	
5	0826	785.90	0.32	0.42	0.42	2.5	166	267	258	70	76	75	offset
4	0829	786.98	0.30	0.40	0.40	2.5	165	268	263	71	76	74	
3	0832	788.04	0.30	0.40	0.40	2.3	165	268	263	72	76	75	
2	0835	789.10	0.26	0.35	0.35	2.0	165	270	269	74	77	75	
1	0838	790.08	0.26	0.35	0.35	2.0	166	270	272	76	77	75	
END	0841	791.051	—	—	—	—	—	—	—	—	—	—	
B12	0846	791.051	1.00	1.40	1.40	5.0	168	267	280	80	76	74	ref. change 12.0
11	0849	792.92	1.00	1.40	1.40	5.3	168	254	262	65	77	75	
10	0852	794.75	1.10	1.35	1.35	5.5	168	259	264	62	79	75	
9	0855	796.70	1.05	1.30	1.30	5.3	166	260	260	63	80	74	ref. change 12.5
8	0858	798.57	0.92	1.15	1.15	5.0	168	261	260	66	80	75	

Pitot Tube Calibration Factor C_p 0.807

Volume Collected V_m 39.458 ft³ Baro. Press. P_b 29.90 "Hg

Water Collected V_w 514.3 ml Probe Tip Dia. D_n 0.249 in.

Time of Test T_t 72 min. % CO₂ 7.4 % CO 0.0

Stack Pressure P_s 0.80 "H₂O % O₂ 10.8 % N₂ 81.8

Area Stack A_c 1320 in²

Pitot Tube No. 12 Barometer No. 1

Probe Tip No. II-4

V_m = Dry Gas Meter Calibration Factor 1.008 x 39.145

[Dry Gas Meter Reading] ft³ - (T_t - min X Rate - cfm)
M_F = M_T =

Impinger Box No. 3

Impinger 1 Final Weight 841.5
Initial Weight 653.5
Increase 188.0

Impinger 2 Final Weight 878.6
Initial Weight 686.3
Increase 192.3

Impinger 3 Final Weight 763.9
Initial Weight 685.1
Increase 78.8

Impinger 4 Final Weight 498.1
Initial Weight 489.7
Increase 8.4

Impinger 5 Final Weight 872.8
Initial Weight 826.0
Increase 46.8

Impinger 6 Final Weight _____
Initial Weight _____
Increase _____

Filter # _____ Final Weight _____
Initial Weight _____
Increase _____

Water Weight Gain

$V_w =$
g SO₂ = -
 $V_w =$

Impinger 1 188.0

Impinger 2 192.3

Impinger 3 78.8

Impinger 4 8.4

Impinger 5 46.8

Impinger 6 _____

Total 514.3 = V_w

$P_b =$ 29.90

$V_m =$ 39.458

$V_w =$ 514.3

$P_m =$ 1.043

Avg $\Delta P =$ 0.802

Avg $\sqrt{\Delta P} =$ 0.872

$C_p =$ 0.807

$P_s =$ -0.80

$T_m =$ 76

$T_s =$ 166

%CO₂ = 7.4

%O₂ = 10.8

%CO = 0.0

%N₂ = 81.8

$A_s =$ 1320

$D_n =$ 0.249

$T_t =$ 72

"Hg 29.84

"R 536

"R 626

Moisture Content:

$\%M =$ 38.40 $M_d =$ 0.6160 $MW_d =$ 29.616 $MW =$ 25.16

$$V_{m_std} = 17.65 V_m \left(\frac{P_b + \frac{P_m}{13.6}}{T_m + 460} \right) = 17.65 \times 39.458 \left(\frac{29.90 + \frac{1.043}{13.6}}{76 + 460} \right) = \frac{38.949}{0.541} \text{ sft}^3$$

$$V_{w_gas} = 0.0472 \times V_w = 0.0472 \times 514.3 = 24.275 \text{ sft}^3$$

$$\% \text{ Moisture} = \frac{V_{w_gas}}{V_{m_std} + V_{w_gas}} \times 100 = \frac{24.275}{38.949 + 24.275} \times 100 = 38.40 \%$$

$$V_s = 5123.8 \times 0.807 \sqrt{\frac{626}{29.84 \times 25.16}} \times 0.872 = 3289 \text{ fpm}$$

$$\%I = \frac{1039 \times 626 \times 38.949}{29.84 \times 0.6160 \times 3289 \times 72 \times (0.249)^2} = 73.9 \%$$

ACFM: 39180

SCFM: 15680

%EA: 99.3

41.479

PARTICULATE FIELD DATA

Run No. 1

location Scrubber Shale

Date 14 July 1987

[illegible]

PART, 502 FIELD DATA

Job No. 87-88
 Job Name Wood Materials
 Run No. 2
 Location Scrubbs Stack
 Date 14 July 1987
 Operator Alexander, D.R.
 Sample Box No. 11 Meter Box No. 6

Ambient Temp. °F 84
 Assumed Moisture % 38
 Probe Length 3'
 C Factor -14 to reference
 Initial Leak @ 15.0 "Hg = 0.000 cfm
 Final Leak @ 19.0 "Hg = 0.000 cfm

Read and record at the
 start of each test point.

Purge to: 868.900
 Purge time: 1158-1208

Point	Clock Time	Dry Gas Meter, CF	ΔP_s	P_m		Pump Vacuum In. Hg Gauge	T_s		Probe Temp. °F	Oven Temp. °F	Effluent Temp. °F	T_m		Remarks
				Pitot in. H ₂ O	Orifice ΔH in. H ₂ O		Stack Temp. °F	Inlet				Outlet		
													Desired	
B 812	1021	818.600	1.05	1.50	1.50	10.8	170	270	237		83	76		
711	1024	820.40	1.05	1.50	1.50	11.2	172	252	236		66	77	76	
610	1027	822.41	1.10	1.50	1.50	11.6	171	251	244		64	78	76	
59	1030	824.40	1.50	2.10	2.10	14.3	1863	270	254		88	77	76	
48	1033	826.83	0.87	1.25	1.25	10.3	164	253	256		69	78	76	
37	1046	828.70	0.72	1.05	1.05	8.5	163	239	257		70	78	76	
26	1049	830.48	0.65	0.93	0.93	7.5	163	238	255		73	78	76	
15	1052	832.12	0.75	1.10	1.10	8.5	165	239	259		75	77	76	
5424	1055	833.80	0.86	1.20	1.20	9.2	162	237	258		76	80	76	
3	1058	835.50	0.87	1.25	1.25	10.0	161	236	263		80	80	76	
2	1103	837.40	0.89	1.30	1.30	10.8	165	235	265		83	80	76	
1	1104	839.27	0.80	1.15	1.15	10.3	166	228	261		86	81	76	
END	1107	841.032	—	—	—	—	—	—	—		—	—	—	
A12	1111	841.052	1.10	1.55	1.55	12.2	163	274	272		97	80	76	
"	1114	843.02	1.20	1.70	1.70	13.5	160	256	265		86	81	77	
10	1117	845.15	1.45	2.10	2.10	17.0	160	251	260		84	82	77	
9	1120	847.45	1.40	2.00	2.00	17.0	165	241	247		81	82	77	
8	1123	849.74	1.20	1.70	1.70	15.0	162	242	250		74	83	77	

Pitot Tube Calibration Factor C_p 0.807

Pitot Tube No. 12 Barometer No. 1

Volume Collected V_m 42.638 ft³ Baro. Press. P_b 29.95 "Hg

Water Collected V_w 620.8 ml Probe Tip Dia. D_n 0.249 in.

Time of Test T_t 72 min. % CO₂ 7.2 % CO 0.0

Stack Pressure P_s -0.30 "H₂O % O₂ 10.8 % N₂ 82.0

Area Stack A_s 1320 in²

V_m = Dry Gas Meter Calibration Factor 1.008 x 42.300

[Dry Gas Meter Reading] ft³ - $(T_t - T_c)$ min x Rate cfm
 M_F = M_T =

Impinger Box No. 11

Impinger 1 Final Weight 864.2
Initial Weight 666.4
Increase 197.8 ✓

Impinger 2 Final Weight 834.7
Initial Weight 672.2
Increase 162.5 ✓

Impinger 3 Final Weight 856.2
Initial Weight 679.9
Increase 176.3 ✓

Impinger 4 Final Weight 536.8
Initial Weight 492.8
Increase 44.0 ✓

Impinger 5 Final Weight 843.6
Initial Weight 803.4
Increase 40.2 ✓

Impinger 6 Final Weight _____
Initial Weight _____
Increase _____

Water Weight Gain

Impinger 1 197.8 ✓
Impinger 2 162.5 ✓
Impinger 3 176.3 ✓
Impinger 4 44.0 ✓
Impinger 5 40.2 ✓
Impinger 6 _____

$V_w =$
 $8 \text{ SO}_2 = -$
 $V_w =$

Total 620.8 = V_w

$P_b =$ 29.95 ✓ $\% \text{CO}_2 =$ 7.2 ✓
 $V_m =$ 42.638 ✓ $\% \text{O}_2 =$ 10.8 ✓
 $V_w =$ 620.8 ✓ $\% \text{CO} =$ 0.0 ✓
 $P_m =$ 1.211 ✓ $\% \text{N}_2 =$ 82.0 ✓
Avg $\Delta P =$ 0.850 ✓ $A_s =$ 1320 ✓
Avg $\sqrt{\Delta P} =$ 0.896 ✓ $D_n =$ 0.249 ✓
 $C_p =$ 0.807 ✓ $T_t =$ 872 ✓
 $P_s =$ -0.30 ✓ H_2O 29.93 ✓ H_2O 29.93 ✓
 $T_m =$ 78 ✓ °F 538 ✓ °R
 $T_s =$ 164 ✓ °F 624 ✓ °R

Filter # _____ Final Weight _____
Initial Weight _____
Increase _____

Moisture Content: $\%M =$ 41.08 ✓ $M_d =$ 0.5892 ✓ $MW_d =$ 29.584 ✓ $MW =$ 24.83 ✓

$$V_{m \text{ std}} = 17.65 V_m \left(\frac{P_b + \frac{P_m}{13.6}}{T_m + 460} \right) = 17.65 \times 42.638 \left(\frac{29.95 + \frac{1.211}{13.6}}{78 + 460} \right) = \frac{42.019}{0.584} \text{ sft}^3$$

$$V_{w \text{ gas}} = 0.0472 \times V_w = 0.0472 \times 620.8 = 29.302 \text{ sft}^3$$

$$\% \text{ Moisture} = \frac{V_{w \text{ gas}}}{V_{m \text{ std}} + V_{w \text{ gas}}} \times 100 = \frac{29.302}{42.019 + 29.302} \times 100 = 41.08\%$$

$$V_s = 5123.8 \times 0.807 \sqrt{\frac{624}{29.93 \times 24.83}} \times 0.896 = 3395 \text{ fpm}$$

ACFM: 31120 ✓

$$\%I = \frac{1039 \times 624 \times 42.019}{29.93 \times 0.5892 \times 34420 \times 72 \times (0.249)^2} = 101.9\%$$

SCFM: 15578 ✓

%EA: 98.8 ✓

PARTICULATE FIELD DATA

Run No. 2

Location Scrubber State

Date 14 July 1987

[illegible]

MULLINS ENVIRONMENTAL TESTING CO., INC.

Job No. 87-88PART, SO₂ FIELD DATAJob Name WOOD MATERIALS SUPPLYRun No. 3Location Scrubber StackDate 14 July 1987Operator Alexander, OrrSample Box No. 12 Meter Box No. 6Ambient Temp. °F 94Assumed Moisture % 38Probe Length 31C Factor 13.5 to referenceInitial Leak @ 16.8 "Hg = 0.000 cfmFinal Leak @ 14.6 "Hg = 0.002 cfm ΔP_s P_m T_s T_m

Point	Clock Time	Dry Gas Meter, CF	Pitot in. H ₂ O	Orifice ΔH in. H ₂ O		Pump Vacuum In. Hg Gauge	Stack Temp. °F	Probe Temp. °F	Oven Temp. °F	Effluent Temp. °F	Dry Gas Temp. °F		Remarks
				Desired	Actual						Inlet	Outlet	
A 12	1247	869.100	1.30	1.80	1.80	6.5	166	265	255	87	80	79	
11	1250	871.30	1.20	1.70	1.70	6.8	164	272	260	72	81	79	
10	1253	873.45	1.40	2.00	2.00	7.2	164	260	265	67	82	79	
9	1256	875.80	1.30	1.80	1.80	7.0	164	245	269	62	83	79	
8	1259	877.97	0.94	1.30	1.30	6.5	163	235	273	60	84	79	
7	1302	879.87	0.94	1.30	1.30	5.5	162	235	272	62	84	79	
6	1305	881.80	0.38	0.52	0.52	2.5	164	232	273	63	85	80	
5	1308	883.29	0.24	0.33	0.33	2.0	170	231	273	66	84	80	
4	1311	884.20	0.20	0.27	0.27	2.0	172	234	275	68	83	80	
3	1314	885.10	0.26	0.36	0.36	2.2	172	231	274	68	83	80	
2	1317	886.10	0.28	0.38	0.38	2.2	170	240	273	69	83	80	
1	1320	887.26	0.26	0.36	0.36	2.2	171	247	270	67	83	80	Orsat
END	1323	888.53	-	-	-	-	-	-	-	-	-	-	
B 12	1326	888.163	0.90	1.20	1.20	5.0	170	257	271	72	83	80	
11	1329	889.85	0.85	1.15	1.15	4.8	169	243	270	61	85	80	
10	1332	891.66	0.91	1.20	1.20	5.0	169	241	264	60	85	80	
9	1335	893.43	0.87	1.20	1.20	5.0	169	242	260	59	86	80	
8	1338	895.22	0.68	0.94	0.94	4.3	173	240	258	60	87	80	

Pitot Tube Calibration Factor C_p 0.807Volume Collected V_m 39.181 ft³ Baro. Press. P_b 29.93 "HgWater Collected V_w 529.2 ml Probe Tip Dia. D_n 0.249 in.Time of Test T_t 72 min. % CO₂ 82 % CO 0.0Stack Pressure P_s -0.33 "H₂O % O₂ 9.6 % N₂ 82.2Area Stack A_s 1320 in²Pitot Tube No. 12 Barometer No. 1Probe Tip No. II-4 V_m = Dry Gas Meter Calibration Factor 1.008 x 38.870

$$\left[\text{Dry Gas Meter Reading } \text{ft}^3 - \left(T_t \text{ min} \times \text{Leak Rate cfm} \right) \right]$$
 M_F = M_T =

Impinger Box No. 12

Impinger 1 Final Weight 847.2
Initial Weight 647.9
Increase 199.3 ✓

Impinger 2 Final Weight 800.5
Initial Weight 689.3
Increase 111.2 ✓

Impinger 3 Final Weight 825.8
Initial Weight 690.9
Increase 134.9 ✓

Impinger 4 Final Weight 553.8
Initial Weight 496.2
Increase 57.6 ✓

Impinger 5 Final Weight 858.7
Initial Weight 832.5
Increase 26.2 ✓

Impinger 6 Final Weight _____
Initial Weight _____
Increase _____

Water Weight Gain

Impinger 1 199.3 ✓

Impinger 2 111.2 ✓

Impinger 3 134.9 ✓

Impinger 4 57.6 ✓

Impinger 5 26.2 ✓

Impinger 6 _____

Total 529.2 = V_w ✓

$V_w =$
 $g SO_2 =$
 $V_w =$

$P_b =$ 29.93 ✓

$V_m =$ 39.181 ✓

$V_w =$ 529.2 ✓

$P_m =$ 1.015 ✓

Avg $\Delta P =$ 0.738 ✓

Avg $\sqrt{\Delta P} =$ 0.826 ✓

$C_p =$ 0.807 ✓

$P_s =$ -0.32 "H₂O ✓

$T_m =$ 82 °F ✓

$T_s =$ 168 °F ✓

%CO₂ = 8.2 ✓

%O₂ = 9.6 ✓

%CO = 0.0 ✓

%N₂ = 82.2 ✓

$A_s =$ 1320 ✓

$D_n =$ 0.249 ✓

$T_t =$ 72 ✓

29.91 "Hg ✓

542 °R ✓

628 °R ✓

Moisture Content: %M = 39.48 ✓ $M_d =$ 0.6052 ✓ $MW_d =$ 29.696 ✓ $MW =$ 25.08 ✓

$$V_{m_{std}} = 17.65 V_m \left(\frac{P_b + \frac{P_m}{13.6}}{T_m + 460} \right) = 17.65 \times 39.181 \left(\frac{29.93 + \frac{1.015}{13.6}}{82 + 460} \right) = \frac{38.283}{0.532} \text{ sft}^3 \text{ scfm}$$

$$V_{w_{gas}} = 0.0472 \times V_w = 0.0472 \times 529.2 = 24.978 \text{ sft}^3$$

$$\% \text{ Moisture} = \frac{V_{w_{gas}}}{V_{m_{std}} + V_{w_{gas}}} \times 100 = \frac{24.978}{38.283 + 24.978} \times 100 = 39.48 \%$$

$$V_s = 5123.8 \times 0.807 \times \sqrt{\frac{628}{25.08 \times 29.91}} \times \frac{0.832}{0.682} = 3125 \text{ fpm}$$

$$\% I = \frac{1039 \times 628 \times 38.283}{29.91 \times 0.6052 \times \frac{3125}{48} \times 72 \times (0.249)^2} = 98.8 \%$$

ACFM: 28646 ✓
SCFM: 14625 ✓
%EA: 78.8 ✓

Run No. 3

PARTICULATE FIELD DATA

Location Scrubber Stack

Date 14 July 1987

[illegible]

METCO

APPENDIX E

Analytical Data

Mullins Environmental Testing Co., Inc.

Particulate Analysis Summary

Job Number 87 88 Date Analysis Completed 7-21-87
 Job Name Wood Materials Supply, Inc. Unit Tested Scrubber Stack
 Location Conroe, TX.

Run No.	1	2	3		
Particulate on Filter (mg)	31.7	61.5	34.7		
Particulate in Front Wash (mg)*	48.6	58.9	53.1		
MF (mg)	80.3	120.4	87.8		
Particulate in Impinger #1 (mg)**	6.7	6.2	9.0		
MT (mg)	87.0	126.6	96.8		

TPS

Mary Gentry
 Analyst

* Less Acetone Residue

** Less Ammonium Sulfate

Mullins Environmental Testing Co., Inc.

Particulate Analysis EPA Method 5

Stack Filters

Job Number 87-88Location Conroe, TexasJob Name Wood Materials SupplyUnit Tested Scrubber Stack

Desiccator Time In	7/14 2030	1659 7/15			
Desiccator Time Out	7/15 1652	0819 7/16			

Run No. <u>1</u>	Filter No. <u>T-72</u>				
Filter & Particulate + Tare Weight (g)	2.5546	2.5549			
Tare Weight (g)	1.8796	1.8794	✓		
Filter & Particulate (g)	0.6750	0.6755	✓		

Filter & Particulate Average (g) 0.6753
 Initial Filter Weight (g) 0.6436
 Total Particulate (mg) 31.7

Run No. <u>2</u>	Filter No. <u>T-73</u>				
Filter & Particulate + Tare Weight (g)	2.5711	2.5811			
Tare Weight (g)	1.8795	1.8794	✓		
Filter & Particulate (g)	0.7016	0.7017	✓		

Filter & Particulate Average (g) 0.7017
 Initial Filter Weight (g) 0.6402
 Total Particulate (mg) 61.5

Run No. <u>3</u>	Filter No. <u>T-74</u>				
Filter & Particulate + Tare Weight (g)	2.5561	2.5563			
Tare Weight (g)	1.8292	1.8494			
Filter & Particulate (g)	0.6769	0.6769	✓		

Filter & Particulate Average (g) 0.6769
 Initial Filter Weight (g) 0.6422
 Total Particulate (mg) 34.7

M. G. Hunter
 Analyst

Mullins Environmental Testing Co., Inc.

Particulate Analysis EPA Method 5

Front Wash

Job Number 87-88Location Conroe, TXJob Name WOOD Material Supply Inc.Unit Tested 11 Stack

Desiccator Time In	11 ⁴⁵ 7/15/87	8 ¹¹ 7/16			
Desiccator Time Out	9 ⁰⁵ 7/16	8 ⁴⁵ 7/17			

Run No. <u>1</u>	Volume (ml) <u>432</u>				
Final Weight (g)	154.1788	154.1791			
Initial Weight (g)	154.1272	154.1272	✓		
Particulate Weight (g)	0.0516	0.0519	✓		

Particulate Average (mg) 51.8Less Acetone Blank (mg) 3.2Total Particulate (mg) 48.6

Run No. <u>2</u>	Volume (ml) <u>329</u>				
Final Weight (g)	176.9460	176.9459			
Initial Weight (g)	176.8846	176.8846	✓		
Particulate Weight (g)	0.0614	0.0613	✓		

Particulate Average (mg) 61.4Less Acetone Blank (mg) 2.5Total Particulate (mg) 58.9

Run No. <u>3</u>	Volume (ml) <u>425</u>				
Final Weight (g)	146.1715	146.1720			
Initial Weight (g)	146.1155	146.1155	✓		
Particulate Weight (g)	0.0560	0.0565	✓		

Particulate Average (mg) 56.3Less Acetone Blank (mg) 3.2Total Particulate (mg) 53.1

Acetone Blank	Volume (ml) <u>365</u>				
Final Weight (g)	127.9254	127.9259			
Initial Weight (g)	127.9229	127.9229	✓		
Difference (g)	0.0025	0.0030	✓		

Average (mg) 2.75* mg/l 7.5

* Note: If greater than 7.9 mg/l, use 7.9 mg/l.

M. A.

Analyst

Mullins Environmental Testing Co., Inc.

Particulate Analysis EPA Method 5

SO₂ Back Half AnalysisJob Number 87-8thLocation Copper, Ky.Job Name Wood Mat. SupplyUnit Tested Scrubber Stack

Desiccator Time In	8 ⁰⁰ 7/16/87	16 ³⁰ 7/16	18 ⁰⁰ 7/17		
Desiccator Time Out	16 ³¹ 7/16	16 ³³ 7/17	17 ²¹		

Run No. <u>1</u>	Volume (ml) <u>375</u> (405)				
Final Weight (g)	158.8317	158.8301	158.8296		
Initial Weight (g)	158.8165	158.8165	158.8165	✓	
Particulate Weight (g)	0.0152	0.0136	0.0131	-	

Particulate Average (mg) 13.4
 Less Ammonium Sulfate (mg) 6.7
 Total Particulate (mg) 6.7

Run No. <u>2</u>	Volume (ml) <u>370</u> (405)				
Final Weight (g)	177.2229	177.2203	177.2200		
Initial Weight (g)	177.2074	177.2074	177.2074	✓	
Particulate Weight (g)	0.0155	0.0129	0.0126	-	

Particulate Average (mg) 12.8
 Less Ammonium Sulfate (mg) 6.6
 Total Particulate (mg) 6.2

Run No. <u>3</u>	Volume (ml) <u>396</u> (426)				
Final Weight (g)	184.3000	184.2990	184.2986		
Initial Weight (g)	184.2842	184.2842	184.2842	✓	
Particulate Weight (g)	0.0158	0.0148	0.0144	-	

Particulate Average (mg) 14.6
 Less Ammonium Sulfate (mg) 5.6
 Total Particulate (mg) 9.0

M. Pandey
 Analyst

SO₂ EMISSION DATAJob Number 87-88Location Conroe, Tex.Job Name Wood Materials SupplyUnit Tested Scrubber Stack

Run Number	1	2	3			
N - normality of BaCl ₂	0.0100	0.0100	0.0100			
ML _I - ml in impinger #2	413	436	369			
ML _I - ml in impinger #3	522	392	492			
ML _A - ml in aliquot #2	10	10	10			
ML _A - ml in aliquot #3	10	10	10			
ML _B - ml of BaCl ₂ to titrate #2	1.15	1.10	1.25			
	1.20	1.10	1.25			
	1.20	1.10	1.30			
Average ML _B - ml of BaCl ₂	1.18	1.10	1.27			
ML _B - ml of BaCl ₂ to titrate #3	0.50	0.10	0.45			
	0.50	0.10	0.45			
	0.55	0.15	0.45			
Average ML _B - ml of BaCl ₂	0.52	0.12	0.45			
ML _{BB} - ml of BaCl ₂ to titrate blank	0.05	0.05	0.05			
T _m - average gas meter temp., °F						
V _m - volume of dry gas sampled @ meter conditions, ft. ³						
P _b - barometric pressure, "Hg Abs.						
Q _s - stack gas volume dry @ standard conditions, *SCFM						
C _I - SO ₂ in impinger #2, mgs	14.9	14.6	14.4			
C _I - SO ₂ in impinger #3, mgs	7.9	0.9	6.3			
C _T - total SO ₂ in impingers, mgs	22.8	15.5	20.7			
ppm SO ₂						
C _{SO₂} - emission rate of SO ₂ , lbs/day						
C _{SO₂} - emission rate of SO ₂ , lbs/hr						
C _S - emission rate of S, lbs/day						

* 29.92 "Hg, 68°F (760 mm Hg, 20°C)

$$C_I = \frac{ML_I \times (ML_B - ML_{BB}) \times N \times 32}{ML_A}$$

$$\text{ppm SO}_2 = \frac{0.7513 \times C_T \times (T_m + 460)}{V_m P_b}$$

$$C_{SO_2} = \text{ppm SO}_2 \times Q_s \times 239.2 \times 10^{-6}$$

$$C_T = C_I \#2 + C_I \#3$$

$$E-6 \quad C_s = \frac{C_{SO_2}}{2}$$

SULFUR TRIOXIDE EMISSION DATA

Job Number 27-88 Location Conroe, TX
 Job Name Wood Materials Unit Tested Scrubber

Run Number	1	2	3	
Date				
Time				
N - normality of BaCl ₂	0.0100	0.0100	0.0100	
ML _I - ml in impinger	405	400	426	
ML _A - ml in aliquot	10	10	10	
ML _B - ml of BaCl ₂ to titrate	0.30	0.30	0.25	
	0.30	0.30	0.25	
	0.30	0.30	0.25	
Average ML _B - ml of BaCl ₂ to titrate	0.30	0.30	0.25	
ML _{BB} - ml of BaCl ₂ to titrate blank	0.15	0.15	0.15	
T _m - average gas meter temp., °F				
V _m - volume of dry gas sampled @ meter conditions, ft. ³				
P _b - barometric pressure, "Hg Abs.				
Q _s - stack gas volume dry @ standard conditions, *SCFM				
C _I - SO ₃ in impinger, mgs	4.0	4.0	3.4	
ppm SO ₃				
C _{SO₃} - emission rate of SO ₃ , lbs/day				
C _S - emission rate of S, lbs/day				

* 29.92 "Hg, 68°F (760 mm Hg, 20°C)

$$C_I = \frac{ML_I \times (ML_B - ML_{BB}) \times N \times 40}{ML_A}$$

$$\text{ppm SO}_3 = \frac{0.6021 \times C_I \times (T_m + 460)}{V_m P_b}$$

$$C_{SO_3} = \text{ppm SO}_3 \times Q_s \times 299.1 \times 10^{-6}$$

$$C_S = \frac{C_{SO_3}}{2.5}$$

METCO

APPENDIX F

Plant Operational Data

7/13/87

Run No.	Time	Feed instant	Rate Totalizer	Burner Position	Water Pump
1	0803	204	618164	7	77
2	8:15	203	618207	7	
3	8:30	204	618263	7 1/2	
4	8:45	205	618315	7 1/2	
5	9:00	203	618369	7 1/2	
6	9:15	202	618430	6	
17	9:22 9:30	204	618450	5 1/2	77

7/14/87

#	10:20	202	618657	7	77
2	10:25 11:47	202	618937	4	77

down 5 minutes

7/14/87

III.	12:45	171	619114	4	77
3	1:10	200	619192	5	
	1:25	201	619246	6 1/8	
	1:40	204	619300	6 1/2	
	1:55	203	619351	6 1/2	
	2:05	197	619379	7	77

ASPHALTIC CONCRETE CENTRIFUGE EXTRACTION WORK SHEET

County MONTGOMERY Highway _____ Project PCT 1,2,3,4 Control _____
 Date 1-14-87 Time _____ Station _____ Sampled By _____
 Spec. Item _____ Type 340 D Mod Design No. _____

Total Sample = <u>800</u> gm. (A)	Total Solvent = <u>1620</u> ml. (2)
Final Filter = <u>27.6</u> gm. (a)	Total Ash = $\frac{1 \times 2}{100} =$ <u>4.86</u> gm. (D)
Original Filter = <u>25.2</u> gm. (b)	Fines + Aggr. + Ash = B + C + D = <u>765.26</u> gm. (E)
Fines in Filter = a - b = <u>2.4</u> gm. (B)	Total Loss = A - E = <u>34.74</u> gm. (F)
Pan + Extr. Aggr. = <u>2012</u> gm. (c)	Total Loss = $\frac{F}{A} \times 100 =$ <u>4.3</u> % (G)
Pan = <u>1254</u> gm. (d)	Moisture Content = _____ % (H)
Extr. Aggr. = c - d = <u>758</u> gm. (C)	Hydrocarbon Volatiles Content = _____ % (I)
Dish + Ash per 100 ml. = <u>138.9</u> gm. (e)	Retention Factor = _____ % (R)
Dish = <u>138.6</u> gm. (f)	Residual Bitumen = G - H - I + R = <u>4.3</u> % (J)
Ash per 100 ml. = e - f = <u>.3</u> gm. (1)	

	Percent of Total Mixture
Fines + Aggr. + Ash = $(\frac{E}{A} \times 100) - R =$	<u>95.7</u>
Moisture = H =	-
Hydrocarbon Volatiles = I =	-
Residual Bitumen = J =	<u>4.3</u>
Total =	100.0%

SIEVE ANALYSIS		
Sieve Size	Grams	Percent
1-3/4" - 7/8"		
7/8" - 3/8"		
5/8" - 3/8"		
1/2" - 3/8"		
3/8" - 4	<u>231</u>	<u>30.5</u>
1/4" - 10		
4 - 10	<u>216</u>	<u>28.5</u>
+ 10		<u>59.0</u>
10 - 40	<u>95</u>	<u>12.5</u>
40 - 80	<u>139</u>	<u>18.3</u>
80 - 200	<u>38</u>	<u>5.0</u>
Pass 200	<u>32 + 2.4 + 4.86 = 39.26</u>	<u>5.2</u>
Total	<u>758.26</u>	100.0%

MOISTURE
5.5%

A.C.
4.3%

Charles J. Hood

 Inspector

METCO

APPENDIX G

Chain of Custody

MULLINS ENVIRONMENTAL TESTING CO., INC.

Chain of Custody

Job Number 87-83Date(s) Sampled 7/14/87Job Name WOOD MATERIALS SUPPLYNumber of Tests 11Location 5 CONROE, TEXASDate Results
Required _____Unit Tested Scrubber Stack

SOURCE SAMPLES

	Number of Containers	Partic- ulate	SO ₂	SO ₃	H ₂ S	Cl ₂	H ₂ SO ₄	Metals	Other
Filter Container	<u>11</u>	<u>✓</u>	_____	_____	_____	_____	_____	_____	_____
Front Wash	<u>11</u>	<u>✓</u>	_____	_____	_____	_____	_____	_____	_____
Back Wash	_____	_____	_____	_____	_____	_____	_____	_____	_____
Impinger No. 1	<u>11</u>	<u>✓</u>	_____	<u>✓</u>	_____	_____	_____	_____	_____
Impinger No. 2	<u>11</u>	_____	<u>✓</u>	_____	_____	_____	_____	_____	_____
Impinger No. 3	<u>11</u>	_____	<u>✓</u>	_____	_____	_____	_____	_____	_____
Impinger No. 4	_____	_____	_____	_____	_____	_____	_____	_____	_____
Acetone Blank	<u>1</u>	<u>✓</u>	_____	_____	_____	_____	_____	_____	_____
NO _x	_____	_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____	_____	_____	_____	_____

Special Instructions

Outside Analysis

Firm: _____

Date Taken: _____

Analysis for: _____

Sample No. 1 Recovered by: Don C. Alexander Date: 7/14/87 Time: 1030 Location: VANSample No. 2 Recovered by: Don C. Alexander Date: 7/14/87 Time: 1330 Location: VANSample No. 3 Recovered by: Don C. Alexander Date: 7/14/87 Time: 1440 Location: VANSamples Received by: Don C. Alexander for Transport Date: 7/14/87 Time: 1530Samples Received at Lab by: Don C. Alexander Date: 7/14/87 Time: 2030Samples Analyzed by: Mary Senter Date: 7/21/87 Time: 0845

APPENDIX H

Resumes of Test Personnel

MULLINS ENVIRONMENTAL TESTING CO., INC.

P.O. Box 598

Addison, Tx 75001

(214) 931-7127



BILLY J. MULLINS, JR., President

Education

Post Graduate Study in Environmental Engineering at Southern Methodist University, Dallas, Texas, 1970.

M.S. 1969, New York University, New York, New York, in Civil Engineering (Air Resources).

B.S. 1968, Texas Tech University, Lubbock, Texas, in Civil Engineering (Water Resources).

Studies in Engineering at U.S. Naval Academy, Annapolis, Maryland, 1963-1964.

Professional
Training
Courses

Attended Short Course on Air Pollution Engineering at the University of Texas at Austin, February 1970.

Attended four-week management course presented by the American Management Association, 1976.

Certification

Registered Professional Engineer
Certified Visible Emissions Evaluator
Certified Fallout Shelter Analyst
Licensed Private Pilot (Multi-Engine-Land, Instrument)
Diplomat in the American Academy of Environmental Engineers

Professional
Memberships

Air Pollution Control Association - Past Chairman,
Southwest Section; Chairman - Consultants Committee
Source Evaluation Society - Past President
Texas Society of Professional Engineers
National Society of Professional Engineers
American Management Association

MULLINS

Technical Experience

Directed and performed stack sampling on over 1200 sources of which over 150 were sampled simultaneously using more than one sampling train at several points in the flue gas stream. 1972-present.

Directed and performed over 150 short-term ambient air studies using mobile sampling vans and various ambient air sampling equipment. 1972-present.

Designed, directed and operated over 20 permanent ambient air networks of various size and duration for a variety of parameters. 1972-present.

Designed surface and underground drainage systems for residential subdivisions, public works projects, and shopping centers. 1969-1972.

Designed several residential subdivisions including lot layout, street design, drainage design, and utility design. 1969-1972.

Research Projects

Supervised and conducted a study made by the Hawaiian Sugar Planters' Association to characterize the emissions for several bagasse-fired boilers. April-May 1976.

Supervised and conducted a study made by the Rio Grande Valley Sugar Growers, Inc. to determine the area affected by the burning of sugarcane fields prior to harvesting. November 1974-April 1975.

Supervised and conducted a study by a lightweight aggregate manufacturer to develop a material balance around the process through sampling and analysis of several parameters. November 1973.

Conducted a study in New York City to attempt to develop a correlation in the ambient air between carbon dioxide and sulfur dioxide to provide a tool for predicting air pollution episodes. January-May 1969.

MULLINS

Publications

Co-authored "Sulfur Compound Emissions of the Petroleum Production Industry," December 1974.

Co-authored "Field Procedure for Stabilizing Hydrogen Sulfide Samples to be Analyzed Using Modified Methylene Blue Technique," presented at the Conference on Ambient Air Quality Measurements, Austin, Texas, March 1975.

Co-authored "Atmospheric Emissions Survey of the Sour Gas Industry," October 1975.

Co-authored "Technique for Insuring the Validity of Samples for High Concentrations of Sulfur Dioxide Using the EPA Method 5 Sampling Train," presented at the Third National Conference on Energy and the Environment, College Corner, Ohio, September 1975.

Teaching Experience

Served as a lecturer in the Environmental Protection Agency's training course number 450, "Source Sampling for Particulate Pollutants" for two years from January 1974 to October 1975.

Conducted a two-day training course entitled "Technical Assistance in Source Sampling" at Iowa State University, Ames, Iowa, for the Environmental Protection Agency, October 1974.

Conducted EPA's training course number 450, "Source Sampling for Particulate Pollutants" for the EPA at Research Triangle Park, North Carolina, September 1975.

Conducted a two-day short course entitled "Performing and Observing Source Sampling" at Dallas, Texas, July 1976, May 1977, October 1977; at Lake Charles, Louisiana, May 1977; and at Casper, Wyoming, May 1977.

Served as a lecturer in the Environmental Protection Agency's two-day seminar entitled "Asphalt Industry Environmental Solutions," presented in Dallas, Texas, on March 21 and 22, 1979.

Conducted a two-day short course entitled "Performing and Observing Source Sampling" in Lincoln, Nebraska, in March 1980 for the State of Nebraska, Air Quality Control Division.

MULLINS ENVIRONMENTAL TESTING CO., INC.

P.O. Box 596

Addison, Tx 75001

(214) 931-7127



DON C. ALEXANDER, Manager, Field Services

Education B.S. 1978, Angelo State University, San Angelo, Texas,
in Biology with a minor in Chemistry.

Professional Two-day short course, "Performing and Observing Source
Training Sampling," Dallas, Texas, March 1982.
Courses

Certification Certified Visible Emissions Evaluator

Professional Source Evaluation Society
Membership

Technical Participated in the sampling of over 1000 sources,
Experience including several of which were sampled simultaneously,
using more than one sampling train and has supervised
the sampling of over 850 sources. 1979-present.

Thoroughly trained in the calibration techniques for all
field testing equipment and has supervised the calibration
of all field testing equipment.

Thoroughly trained and familiar with the operation of
MSA LIRA Model 202S Infrared CO Analyzer, Thermo Electron
Model 48 Gas Correlation CO Analyzer, Thermo Electron
Model 10AR Chemiluminescent NO_x Analyzer, Teledyne Oxygen
Monitor, and Shimadzu GC-Mini 2 Gas Chromatograph.

Has performed on-site gravimetric particulate analysis,
SO₂ analysis, and H₂S fuel gas analysis.

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GREGGORY M. ORR, Environmental Field Technician

Education

B.S. 1985, Louisiana Tech University, Ruston,
Louisiana, in Geology.

Technical
Experience

Participated in the sampling of over 25 sources,
including several which were sampled simultaneously
using more than one sampling train. Thoroughly
trained in all EPA testing procedures. 1986-present.

APPENDIX I

RESUMES OF NUS PERSONNEL

WILLIAM J. COLE, P.E.

SENIOR PROJECT MANAGER

EDUCATION

Graduate Work - Mechanics of Fluids and Industrial Administration - Warrington Technical College, England - 1964

Higher National Certificate - Mechanical Engineering -- Warrington Technical College, England - 1960

ADDITIONAL EDUCATION

Hazardous Waste Management Safety Practices -- 1985

GRCDA -- Hazardous Waste Management -- 1981

Institute for Boiler Improvement -- Boiler Efficiency -- 1978

Fundamentals of Industrial Hygiene -- 1977

AICHE -- Primer on Environmental Impact Statements -- 1975

AICHE -- Introduction to Pollution Control -- 1975

Additional Short Courses in:

Hazardous Waste Management 1981 - 1985

Water and Wastewater Management

Air Pollution Control

Professional Management

EXPERIENCE

NUS CORPORATION, 1987-Present

WILLIAM J. COLE & ASSOCIATES, 1984-1987

Southwestern Laboratories, Inc., 1975-1984

Langford Engineering, Inc., 1972-1975

Turner, Collie and Braden, Inc., 1964-1972

As a Senior Project manager and Environmental Management Consultant, is responsible for technical administrative aspects of environmental projects involving: environmental compliance, site remediation, wastewater treatment, groundwater monitoring, hazardous waste management, air pollution evaluation and emissions control. Areas of expertise include:

- Technical lead in the development and management of, waste materials testing, groundwater monitoring, and air emissions compliance testing.
- Development and management of ambient air testing programs to assess the effects of dry vs wet sand blasting operations and personnel exposure to wind borne respirable dust particles from such operations.
- Preparation of permit applications for Part A and Part B hazardous wastes, air emissions, and wastewater discharge.

WILLIAM J. COLE, P.E.

Page Two

- Development and management of health and safety programs, remedial site investigations, feasibility and treatability studies, closure plans, trial burns and air testing programs for major industrial clients.
- Development of innovative and cost-effective solutions for difficult to handle wastes and environmental control problems.
- Management of environmental compliance audits and corrective action programs.
- Effective interaction with regulatory agency personnel at all levels.

Manages and directs testing programs for: personnel exposure from air borne pollutants, ambient air and source emissions, pollution control system performance and hazardous waste materials, for major industrial clients. Client programs include RCRA remediation projects, which require major interaction between NUS, the Client, local, state, and Federal agencies to assure compliance with applicable regulations.

Was responsible for the lead in preparation of Part B Permits, Closure Plans, and Environmental Exposure Assessments for surface impoundments operated by the U.S. Navy, San Diego, California. Performed remedial investigations and prepared closure plans for contaminated waste sites in Texas, Louisiana, and California, under the auspices of state regulatory agencies.

Developed testing programs for Superfund Projects to provide: Waste materials evaluations, groundwater monitoring, air emissions testing. Also developed waste cleanup and site closure programs for: Petroleum, wood preserving, iron and steel production, and metals finishing facilities.

Supervised the investigation of a surface impoundment liner failure in a brine holding pond, for a major natural gas storage and terminalling facility.

Developed personnel exposure monitoring programs for waste management sites and industrial manufacturing processes.

Designed and supervised procedures for field sampling, ambient air testing, laboratory analyses and clean up of: PCB spills, leaking underground storage facilities, surface impoundments, refining wastes, and agricultural chemical wastes.

Directed groundwater monitoring activities at an agricultural chemicals manufacturing facility waste landfill site. Prepared monthly, quarterly, and annual reports for submittal to regulatory agencies.

Performed environmental audits for NASA Dryden facility, Edwards, California.

Coordinated and made presentation before regulatory agencies in Texas, Louisiana, Ohio, and California on Hazardous Waste Management projects.

Was principal of the Environmental Engineering Management firm of William J. Cole & Associates (Cole Assoc.) which was formed to provide specialized consulting services in: permitting, evaluation and management of: Indoor air pollution and work place safety, industrial air and water pollutants, wastewater, solid and hazardous wastes. Cole Assoc. provided environmental consulting services to clients through the Continental United States.

WILLIAM J. COLE, P.E.

Page Three

Was Manager of Environmental Engineering Services and responsible for marketing and directing, environmental engineering and testing services to clients throughout the southern United States. Services included engineering and analytical evaluation of: Industrial and indoor air pollutants, potable water and wastewater systems for industrial and municipal clients, health and safety programs, solid and hazardous wastes. This position entailed effective interaction between client and regulatory agencies in the permitting of industrial and municipal pollution control facilities.

Was Project Manager responsible for permitting, engineering design, and project management for new and upgraded municipal and industrial, water collection, treatment and distribution systems, and wastewater collection and treatment facilities in the State of Texas.

MEMBERSHIPS

PROFESSIONAL ENGINEER REGISTRATION - Texas

PROFESSIONAL AFFILIATION:

- Air Pollution Control Association
- Water Pollution Control Federation
- Institute of Mechanical Engineers
- National Society of Professional Engineers
- Texas Society of Professional Engineers
- American Society of Mechanical Engineers

H07217

B

MARK A. LESTER
EQUIPMENT TECHNICIAN

EDUCATION

H.S. Carrick High School, 1977 (electronics specialization)
Connelley Skills Learning Center, 1978 (electronics)
2nd Class FCC License (with radar endorsement)
Monitor Lab's Technical Training Course, 1978
(sulfur dioxide, nitrogen oxides, ozone,
data acquisition systems)
Thermo Electron Technical Training Course, 1981
(sulfur dioxide, nitrogen oxide)

EXPERIENCE

NUS CORPORATION, Houston, Texas, February 1987-Present
Energy Impact Associates, Inc., E.I.A., Inc.,
Pittsburgh, Pennsylvania, Technician, 1978 to 1982

NUS Corporation - Air Quality Equipment Technician, responsible for performing and documenting accurate and defensible calibration of instruments and equipment used in Environmental Protection Agency (EPA) and state compliance and prevention of significant deterioration (PSD) sampling. Set-up, maintain and calibrate continuous emissions monitor systems for nitrogen oxides, sulfur dioxides, oxygen, carbon monoxide and hydrocarbons at stationary sources for compliance sampling.

E.I.A., Inc. - Air Quality Technician, responsible for installation, operation and maintenance of air quality/meteorological monitoring networks for the utility and steel industry and processing and validating data. Specific projects included:

- Installation and maintenance of an air quality/meteorological system for Niagara-Mohawk Power Company to investigate the affects of air pollutants on agricultural products (1978 - 1981). Equipment included: SO₂ analyzers and O₃ analyzers, wind speed and direction, delta temperature, dew point temperature, soil moisture gauges, electronic precipitation gauges, associated calibration devices, strip chart recorders and computer data loggers with magnetic tapes.
- Conducted performance audits on air quality networks with sulfur dioxide analyzers and high volume particulate samplers (hi-vol) using Thermo Electron Corporation, Monitor Labs, Analytical Instrument Development (AID) and Bendix calibrators for SO₂ and a standard reference flow device for hi-vols.
- Conducted field tests with isokinetic sampler to assess fugitive emissions from road surfaces and material storage piles in integrated steel mills.
- Trained and supervised a staff of twelve E.I.A. personnel in strip chart recorder data reduction, and reviewed and analyzed data to insure precision, reliability and validity of strip chart and computer logged data.

MARK A. LESTER

Page Two

CERTIFICATIONS

**NUS Corporation Superfund Division Certification for Performance of Remedial Response Activities
at Uncontrolled Hazardous Substance Facilities**

Visible Emissions Evaluator, Texas Air Control Board

**Sample Packaging, Preservation and Documentation Program for Uncontrolled Hazardous
Substances Facilities - NUS Corporation**

H05147

APPENDIX J

FIELD OPACITY DATA



Test #1, 2 MAC

Date:

Relative Humidity: 95% Observer Signature: M. A. Jeter

TIME	00	15	30	45	COMMENT
0931	0	0	0	0	<i>pen shadow</i>  stack note Attached steam Plume 300'
0932	0	5	0	5	
0933	0	5	0	0	
0934	0	0	0	0	
0935	0	5	5	0	
0936	0	0	0	5	
					X
					N →
1029	0	0			
1030					

1874

2/21/22



Date: 7-14-87

Test #2

Relative Humidity: 95% Observer Signature: Mark A. Foster

TIME	00	15	30	45	COMMENT	TIME	00	15	30	45	COMMENT
1028	0	0	0	0	steam plume 500'						
1042	0	0	0	0	steam stack						
1043	0	0	0	0							
1044	0	9	10	0							
1045	0	0	0	0							
1046	0	5	5	5							
1047	0	0	0	0							
1048	5	10	5	0							
1049	0	0	0	0							
1050	0	5	5	5	observing point						
1051	10	0	0	0							
1052	0	0	5	0							
1053	10	5	10	5							
1054	10	5	5	5							
1055	0	0	0	0							
1056	0	5	0	0							
1057	0	5	0	5							
1058	0	0	0	0							
1059	5	0	0	0							
1100	5	0	5	5							



Prepared by: _____
Checked by: _____
Approved by: _____
Date: _____

Source Name: scrubber stack Observer: Mark A Lester Date Certified: 3-31
Plant: Berberis wood products Date: 3rd 7-14-87
Stack Distance From: 250 Height: 25 Wind Speed: 1-3 Direction: west
% Cloud Cover: 75 Background Used: sky Temp Dry Bulb 91 Wet Bulb
Relative Humidity: 90% Observer Signature: Mark A Lester

[illegible]