

SAN DIEGO AIR POLLUTION CONTROL DISTRICT
9150 CHESAPEAKE DRIVE
SAN DIEGO, CA 92123

Note: This is a reference cited in AP 42, *Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at www.epa.gov/ttn/chief/ap42/

The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

TEST NO.: 85260

P.O. NO.: 0254

TEST DATE: September 17, 1985

SOURCE TEST: Canyon Rock Company
7500 Mission Gorge Road
San Diego, CA 92120

UNIT TESTED: Plant #2

PERFORMED BY: P. Jarman
B. Yelenosky
R. Batten (Engineer)
C. Bejar (Enforcement)
G. Carrier

REPORT PREPARED BY: G. Carrier

APPROVED BY:

C.W. Ridenour

C.W. RIDENOUR

SENIOR AIR POLLUTION CONTROL CHEMIST

10/16/85

DATE

INDEX

SUMMARY OF RESULTS	1
TEST DESCRIPTION	2
FINAL CALCULATIONS	4
TRAVERSE POINTS, FIGURE 1	6
PORT LOCATION, FIGURE 2	7
SAMPLING TRAIN, FIGURE 3	8
SAMPLE COLLECTION DATA	9
LABORATORY DATA	10
ENGINEERING REPORT	11
VISIBLE EMISSIONS	12

SAN DIEGO COUNTY AIR POLLUTION CONTROL DISTRICT

PAGE 1

TEST DATE: September 19, 1985

TEST NO: 85260

P.O. NO. 0254

SUMMARY: EMISSIONS TO ATMOSPHERE

NAME OF FIRM: CANYON ROCK COMPANY

LOCATION OF PLANT: 7500 Mission Gorge Road, San Diego, CA

TYPE OF OPERATION: Hot Mix Asphalt Plant, operating at 217 tons/hour

UNIT TESTED: Wet Scrubber

		<u>MEASURED EMISSIONS</u>		<u>ALLOWABLE EMISSIONS</u>	
Rule 52	Particulate Matter, Dry	_____	Grains per SCF	_____	Grains per SCF
Rule 53A	Sulfur Compounds as SO ₂ , Dry	_____	% by Vol.	_____	% by Vol.
Rule 53B	Combustion Contaminants	_____	Grains per SCF @12% CO ₂	_____	Grains per SCF @12% CO ₂
Rule 53C	Incinerators	_____	Grains per SCF @12% CO ₂	_____	Grains per SCF @12% CO ₂
Rule 54	Dust and Fumes	<u>18.0</u>	Lbs/Hr	<u>40.0</u>	Lbs/Hr
	NO ₂ (Final Readings)	_____	ppm by Vol. @ 3% O ₂	_____	ppm by Vol. @ 3% O ₂
		_____	ppm by Vol. @ 3% O ₂	_____	ppm by Vol. @ 3% O ₂

Gas Flow Rate, DSCFM 9982

Gas Temperature, °F 156 (Avg)

Process Weight 217 tons/hr

EMISSION RATES

Particulates: 18.0 Lbs/Hr

Oxides of Nitrogen: _____ Lbs/Hr

TEST DESCRIPTION

Introduction

This report presents the results of velocity profile and particulate loading tests performed at V.R. Dennis - Canyon Rock on September 17, 1985. The tests were performed on the exhaust from the wet scrubber serving the hot mix asphalt plant, while asphalt production averaged 217 tons/hour.

System Description

The asphalt plant combines crushed rock and sand with hot asphalt oil in batches of 6,000 pounds. Each batch can be carried by conveyor to a silo or loaded directly into trucks. The rock and sand is dried in a rotary drier, which is heated with natural gas. The exhaust from this drier is vented through a cyclone to a wet scrubber, which exhausts tangentially into a 9-foot diameter stack. The water flow rate through the wet scrubber could not be determined because of an inoperative flow meter.

Procedures

Previous testing has shown that there is significant cyclonic flow in this stack, due to the tangential inlet. EPA NSPS Methods 2 and 5 are not applicable to this stack, and require significant modification to enable testing, allowing both isokinetic sampling and the determination of the stack volumetric flow rate. The volumetric flow rate of the stack was determined by using the following procedure for the 48 traverse points, 12 from each sampling port as shown in Figure 1.

The pitot tube on the sampling probe was placed at a traverse point with the pitot tube faces in a vertical plane. The probe was then rotated until the ΔP was 0.00" H₂O. The angle of rotation (α) was measured with a clinometer and recorded. This was done for the twelve points at each sample port just prior to sampling. These measurements were taken with the sampling nozzle removed to prevent flow interference.

After the direction of flow was determined at each of the points at a particular port, the sampling nozzle was installed, and the probe placed at the first sample point. The probe was rotated α degrees from the vertical so that the nozzle was aligned with the gas flow. The ΔP was measured and a sample extracted isokinetically. In order to obtain a representative sample, the sampling time was made proportional to the cosine of α . This procedure was repeated at each of the twelve points at that sample port, adjusting the angle of rotation of the probe and the sample time for each new " α ". A sample was not taken at points where α was greater than 89°.

Calculations

The velocity at 21 points was calculated. These calculations are presented on Pages 9 and 10. The vertical component of the velocity vector was calculated by multiplying the velocity by the cosine of α . The average of these 21 components was found to be 4.0 feet per second. The particulate concentration calcula-

tions were done using normal methods. The emission rate in pounds per hour was calculated using the grain loading and the stack flow based on the vertical component of the stack vector.

Gas Analysis

Oxygen and carbon dioxide content of the stack gas was measured with an ORSAT analyzer according to EPA New Source Performance Standards Method 3. The results of this analysis are on Page 5.

Visible Emissions

A visible emissions evaluation made by R. Batten, Air Pollution Engineer, is found on Page 13 and shows the stack exhaust emissions to be in compliance with Rule 50.

Comments

The conditions inside the stack during testing made it extremely difficult to record stable readings. The plume exiting the stack was not only cyclonic, but very turbulent and would collapse back into the upper area of the stack. This effect could be observed extending approximately three feet down into the stack and swirling was observed around the sampling nozzle. Wind conditions at the stack opening also contributed to the turbulence. The plume would be caught by a gust of wind and sent cascading down the outside walls of the stack.

AIR POLLUTION CONTROL DEPARTMENT - COUNTY OF SAN DIEGO

TEST NO. 85260

TEST DATE SEPTEMBER 17, 1985

CANYON ROCK

RUN 1

A.	V _m	METER VOLUME, UNCORRECTED*FACTOR	=	34.3	cu ft
B.	P _m	METER PRESSURE, $P + H/13.6$ bar	=	29.89	in Hg
C.	T _m	METER TEMPERATURE, $460 + (T_1 + T_2)/2$	=	557.	DEG. R
D.	T _i	IMPINGER TEMPERATURE	=	70.	DEG. F
E.	T _s	AVERAGE STACK TEMPERATURE, 460+DEG. F	=	616.	DEG. R
F.	P _s	STACK PRESSURE, $P + P_g/13.6$ bar	=	29.80	in Hg
G.	VP _i	MAX. H ₂ O VP PERMITTED AT T _i (SEE APPENDIX)	=	.80	in Hg
H.	V _{lc}	VOLUME OF CONDENSED H ₂ O (SEE LAB SHEET)	=	156.	ml
I.	V _{calc 2}	H ₂ O VAPOR, METER COND., $H * C / B * 0.00267$	=	7.76	cu ft
J.	V _{wv}	MOISTURE METERED AT METER COND., $A * G / B$	=	.93	cu ft
K.	V _{dry}	SAMPLE VOLUME AT METER COND., DRY, $A - J$	=	33.36	cu ft
L.	%M _c	PER CENT MOISTURE CALC. $100 * (I + J) / (A + I)$	=	20.66	%
M.	VP _s	MAX. H ₂ O VP PERMITTED AT T _s (SEE APPENDIX)	=	8.77	in Hg
N.	%M _s	PER CENT MOISTURE PERMITTED, $M / F * 100$	=	29.4	%
	B _{ws}	ENTER LOWER OF L OR N	=	20.7	%
O.	M.C.	MOISTURE CORRECTION FACTOR, $(100 - L \text{ OR } N) / 100$	=	.793	
P.	V _{m(std)}	SAMPLE VOL., STD COND. (DRY), $K * 528 / 29.92 * B / C$	=	31.579	cu ft
S.	m _n	WEIGHT OF PARTICULATE MATTER COLLECTED	=	.430	g
T.	c _s	GRAIN LOADING (DRY), $15.43 * S / P$	=	.210	grains/scf

AIR POLLUTION CONTROL DEPARTMENT - COUNTY OF SAN DIEGO

TEST NO. B5260
CANYON ROCK
RUN 1

TEST DATE SEPTEMBER 17, 1985

G A S A N A L Y S I S				
COMPONENT	VOL. %/100*MOISTURE CORR*	MOL. WT. =WET BASIS	WT. /MOLE	
WATER, B	.2066	1.00000	18.0	3.719
OXYGEN	.1660	.79336	32.0	4.214
CARBON MONOXIDE	.0000	.79336	28.0	.000
CARBON DIOXIDE	.0240	.79336	44.0	.838
NITROGEN & INERTS	.8100	.79336	28.2	18.122
AA. M AVERAGE MOLECULAR WEIGHT				26.894

$\bar{M} = 72.670$

DD. C PITOT TUBE CORRECTION FACTOR = .829 $\rightarrow 16.0$

EE. V^p STACK VELOCITY AT CYCLONIC STACK COND. (SEE DATA= 4.01 ft/sec

FF. V^s STACK VEL. AT STD COND. (DRY), $EE * 528 / 29.92 * F / E * 0 = 10.83$ 2.71 ft/sec

GG. DURATION OF SAMPLING = 113. min

HH. AVERAGE SAMPLING RATE (DRY), P/GG = .279 scfm

II. SELECTED NOZZLE DIAMETER = .382 in

JJ. SAMPLING VELOCITY AT STD COND., $HH / II * 2 * 144 / 60 * 4 / 3 = 5.85$ ft/sec

KK. I ISOKINETIC VARIATION, $JJ / FF * 100 = 54.55 / 10.83$ %

LL. A AREA OF STACK 61.28 sq ft

MM. Q^s FLOW RATE AT STD. COND. (DRY), $FF * LL * 60 = 9982$ scfm

NN. Q^s FLOW RATE AT CYCLONIC STACK COND., $EE * LL * 60 = 14729$ acfm

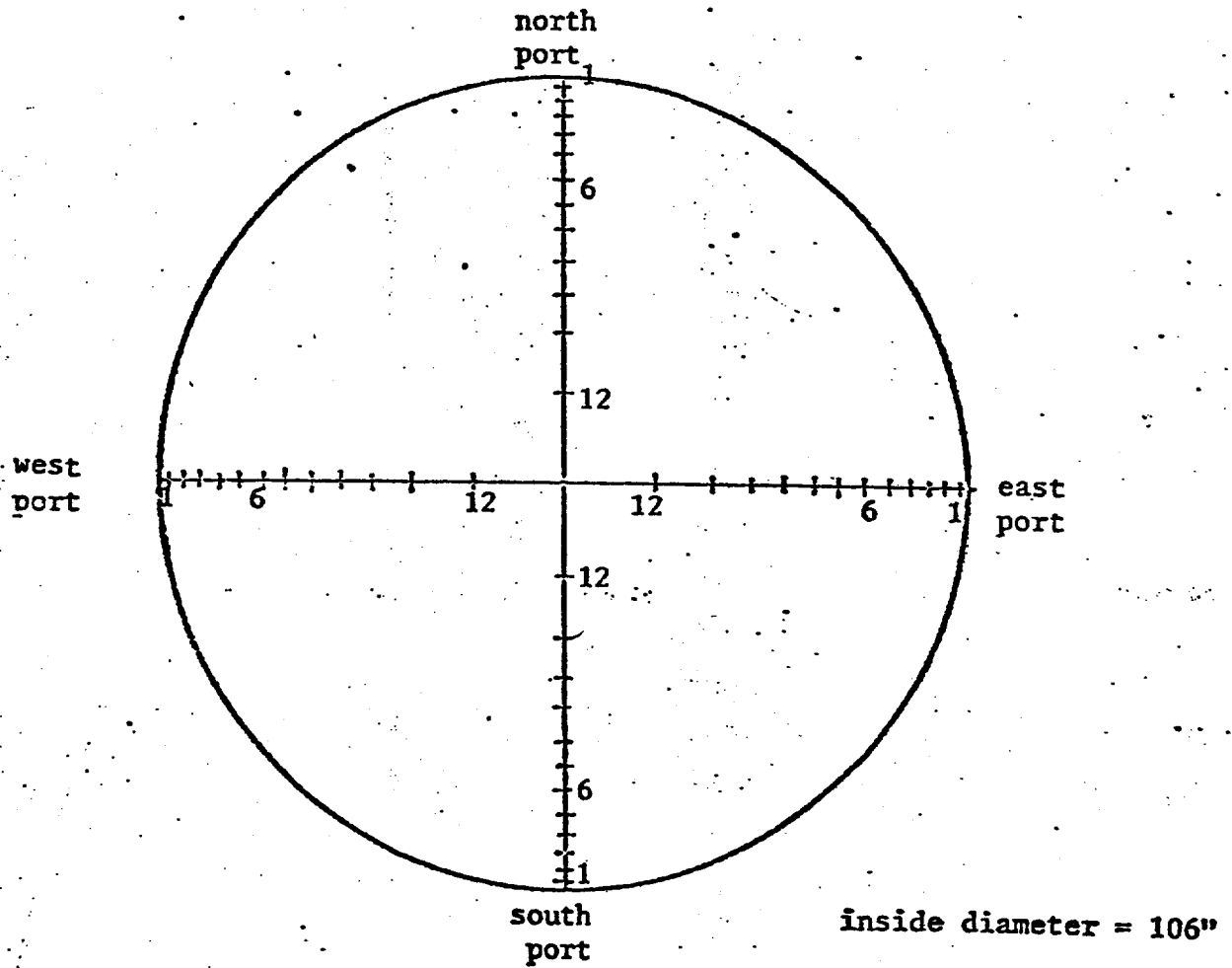
UU. PARTICULATE EMISSION RATE, $0.00847 * T * MM = 17.97$ lb/hr

Canyon Rock

PAGE 6

SAN DIEGO COUNTY AIR POLLUTION CONTROL DISTRICT

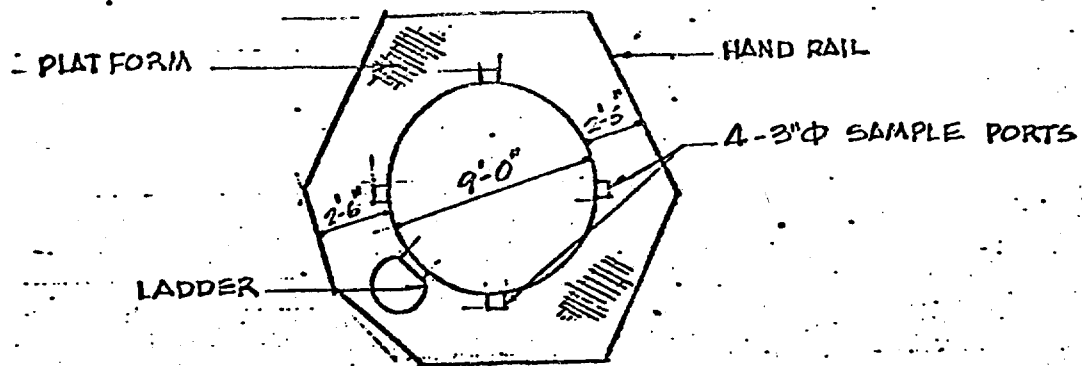
TRAVERSE POINTS



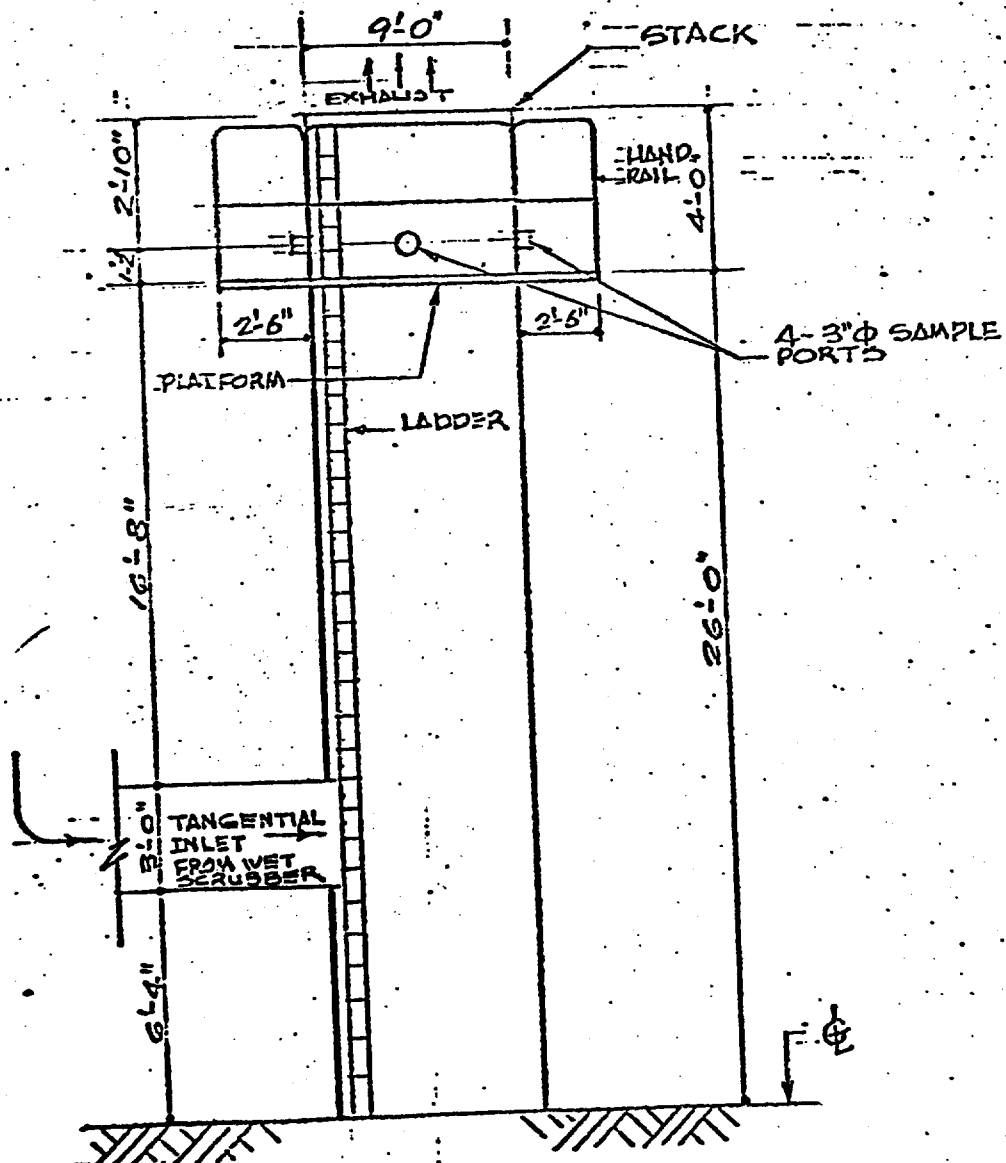
Point	Distance
1	1.1"
2	3.4"
3	5.8"
4	8.4"
5	11.1"
6	14.0"
7	17.1"
8	20.5"
9	24.4"
10	28.8"
11	34.3"
12	42.2"

FIGURE 1

SITE DESCRIPTION
SAN DIEGO AIR POLLUTION CONTROL DISTRICT
V.R. DENNIS-CANYON ROCK ASPHALT PLANT

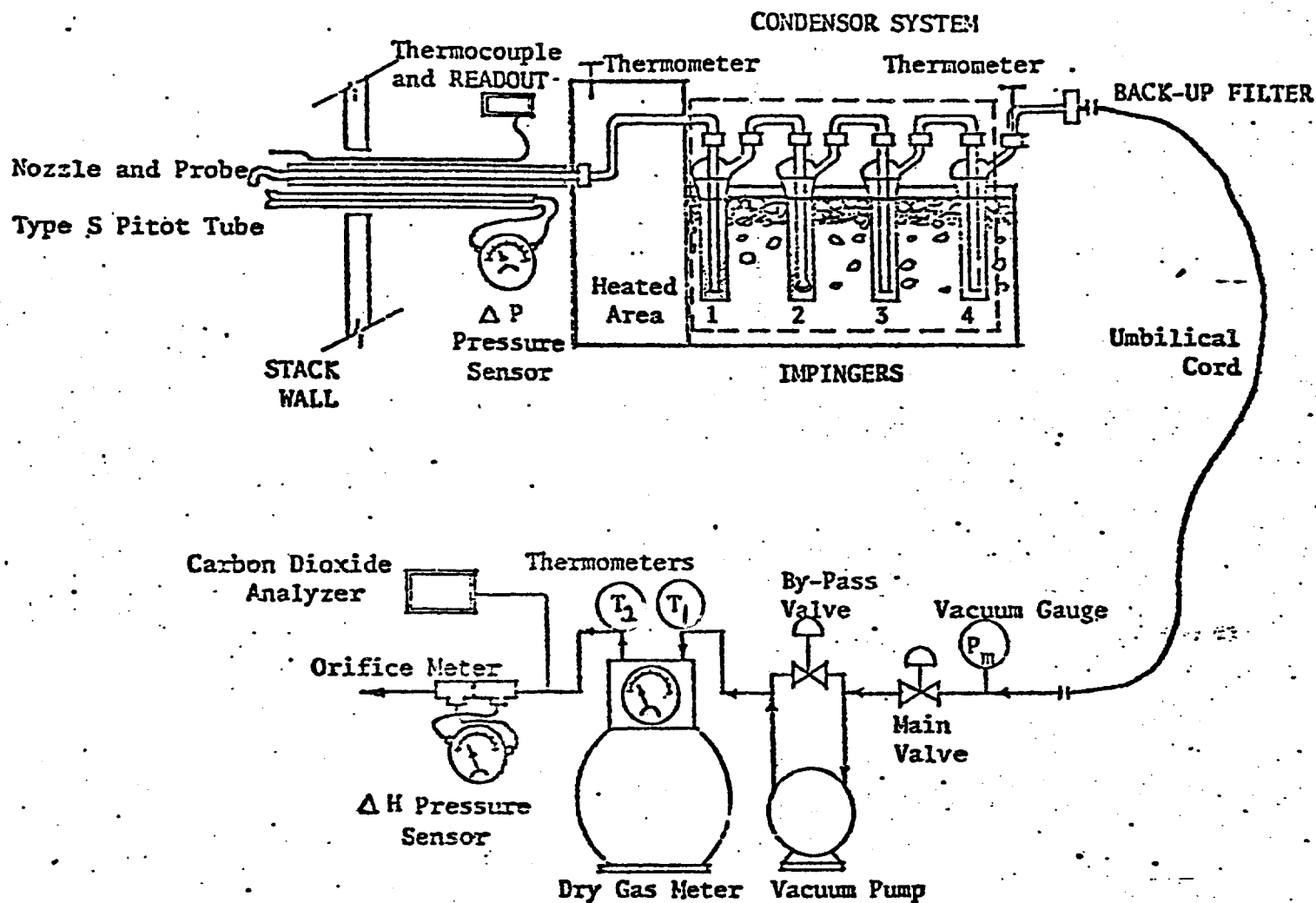


TOP VIEW
NO SCALE



SIDE VIEW
NO SCALE

SAN DIEGO COUNTY AIR POLLUTION CONTROL DISTRICT

LEGEND

Greenburg-Smith Type Impingers

No. 1 Mod- 100 ML Deionized Water

No. 2 Std- 100 ML Deionized Water

No. 3 Mod- Dry

No. 4 Mod- Dry

Mod - Modified Type

Std - Standard Type

FIELD DATA ABBREVIATIONS

PT = Point Number

 T_s = Stack Temperature, $^{\circ}\text{F}$ P = Pitot Tube Pressure Differential, in. H_2O

VEL = Stack Velocity, fps

 H = Orifice Meter Pressure Drop, in. H_2O T_1 = Meter Inlet Temperature, $^{\circ}\text{F}$ T_2 = Meter Outlet Temperature, $^{\circ}\text{F}$ P_m = Pump Vacuum, in. Hg T_i = Impinger Temperature, $^{\circ}\text{F}$ P_{bar} = Barometric Pressure, in. Hg

FIGURE 3: PARTICULATE MATTER SAMPLING TRAIN

AIR POLLUTION CONTROL DEPARTMENT - COUNTY OF SAN DIEGO

TEST NO. 85260
CANYON ROCK
RUN 1

TEST DATE SEPTEMBER 17, 1985

PT	T	P	VEL	H	T	T	P	T	ANG	(VEL)
W8.	152. ⁵	.060	15.2	1.00	93.5	83.5	3.00	64.50	70.	5.2
W7	155.	.090	18.6	1.52	105.0	83.5	1.50	64.50	75.	4.8
W6	155.	.115	21.0	1.95	92.0	84.0	1.75	64.00	75.	5.4
W5	156.	.140	23.2	2.40	109.5	84.0	2.00	64.50	75.	6.0
W4	163.	.155	24.6	2.70	110.5	84.0	2.25	62.50	75.	6.4
W3	161.	.150	24.2	2.35	112.5	84.5	2.25	63.50	75.	6.3
W2	159.	.150	24.1	2.50	112.0	80.0	.00	66.00	65.	10.2
W1	159.	.030	10.8	.50	114.0	83.0	.00	72.00	70.	3.7
N11	147.	.020	8.7	.34	103.0	86.0	.00	83.00	40.	6.7
N10	147.	.055	14.5	.92	109.5	84.5	.00	82.00	70.	4.9
N9	149.	.080	17.5	1.35	110.0	86.0	.00	79.00	80.	3.0
N8	152.	.080	17.5	1.35	110.0	86.0	.00	82.00	89.	3
N7	152.	.080	17.5	1.35	110.0	86.0	.00	82.00	89.	3
E12	144.	.020	8.7	.34	108.0	87.0	1.00	73.00	45.	6.2
E11	144.	.030	10.7	.50	111.0	86.0	.00	68.00	60.	5.3
E10	160.	.050	13.9	.85	115.0	86.0	2.00	66.00	85.	1.2
E9	160.	.060	15.3	1.03	115.0	86.0	2.00	68.00	85.	1.3
S11	159.	.010	6.2	.17	113.0	86.0	.00	68.00	45.	4.4
S10	163.	.030	10.8	.50	111.0	86.0	.00	69.00	80.	1.9
S9	167.	.050	14.0	.85	111.0	86.0	2.00	67.00	89.	2
S7	167.	.090	18.8	1.53	111.0	86.0	3.00	67.00	89.	3

AVG 156. .066 16.0 1.24 108.9 85.0 1.08 70.26 72.67 4.01

$$VEL = 85.48 * C * SQ. RT. ((P * T) / (P * M))$$

P S S S

AVERAGE DELTA P = .0736

DRY GAS METER VOLUME UNCORRECTED = 34.220 P = 29.80 in Hg
bar

METER CORRECTION FACTOR = 1.0020 P (STACK PRESSURE) = .0 in water
g

- NOTES - 1. AVG P IS THE SQUARE OF THE MEAN (SQ. RT)
2. (VEL) = $VEL * \cos(ANG)$
3. AVG CD IS THE VELOCITY WEIGHTED AVERAGE
2

COUNTY OF SAN DIEGO - AIR POLLUTION CONTROL DISTRICT

PARTICULATE MATTER
LABORATORY DATA

PARTICULATES

A. ACETONE WASH
NOZZLE, PROBE,
IMPINGERS.Final 1.5510 gNet Wt. .1489 gPan # C-2Tare 1.4021 gB. WATER WASH
NOZZLE, PROBE,
IMP., IMP. CATCH.Final 1.6608 gNet Wt. .2698 gPan # C-1Tare 1.3910 g

C. BACK-UP FILTER

Final .1216 gNet Wt. .10136 gPan # Tare gFilter Tare .1080 g

D. Blanks

610 ml Water .0003 g/100ml.00183 g Water Correction292 ml acetone .0002 g/100ml.00058 g Acetone CorrectionWater Pan # N/ANet Wt. .0024 gAcetone Pan # 151Total Weight of Particulate Matter
(A + B + C - D).4299 gCONDENSED MOISTURE Final 356 mlTare 200 mlNet Gain 156 mlSee lab note book # 1 pg 68, 69, 70
G CARRIER

MECHANICAL ENGINEERING TEST REPORT

Canyon Rock/V.R. Dennis Asphalt Plant
 7500 Mission Gorge Road
 San Diego, California

PERMIT TO OPERATE NO. 254: Renewal Compliance Test conducted by the APCD

TEST DATE: September 17, 1985

TEST PERIOD: 9:57 am to 2:50 pm

ASPHALT HOT MIX: Each batch was 3 tons.

	3/8 INCH				1/2 INCH				
	3/8" Aggregate								
	3/8 Agg.	Sand	Dust	Oil	1/2 Agg.	3/8 Agg.	Rock	Dust	Oil
LBS.	1956	1956	1656	432	804	2004	1410	1410	372
%	32.6	32.6	27.6	7.2	13.4	33.4	23.5	23.5	6.2

Only small amount % 1/2 inch mix was produced.

ROTARY DRUM BURNER FUEL: Natural Gas

BATCH COUNT: 1 batch per 0.83 minutes.

$$\frac{\text{batch}}{0.83 \text{ min.}} \times \frac{3 \text{ ton}}{\text{batch}} \times \frac{60 \text{ min}}{\text{hr.}} = 217 \text{ tons/hr}$$

Plant was operating at full 200 tons/hr capacity for duration of test.

AGGREGATE TEMPERATURE: 290 to 310°F at exit of rotary drum.

A/C OIL TEMPERATURE: 350-360°F into mixing section

COMMENTS

- o The stack exhaust was visibly checked periodically between 8:30 and 10:30 AM and appeared to be predominately water vapor. It was not apparent that the detached plume contained particulate matter.

- o "Blue smoke" emissions from the drop zone under the storage silos were quite significant. Each drop to either the truck bed or trailer bed produced opacity levels ranging between 40 and 60% for a rough average of 23 seconds each drop. Since each drop was a continuous delivery of 12 or 13 tons, the resulting elongated pile exposed more surface area to the atmosphere. The asphalt in the truck bed was measured to be 290 F. The magnitude of the emissions were 3 times that observed elsewhere where the load temperature was 300 F. It is apparent that some other parameter was the cause for the larger emissions, perhaps the quality of A/C oil being used.

- o The inverted conveyor belt on the underside of the hot mix transport (conveyor assembly) to the storage silo exhibited "blue smoke" emissions as the result of hot mix "clinging" to the belt. Positioning of the observer with relation to the sun is very critical for observing "blue smoke" emissions, especially for line emissions such as these belt emissions. A special determination should be conducted to evaluate the significance of these emissions with regard to Rule 50. A water based surfactant is being

employed to lubricate the belts. It should be determined whether or not the surfactant is contributing to the emissions. The apparent color of the emissions is the typical blue tint. A brown tint would be expected if the surfactant material was prominent in the emissions.

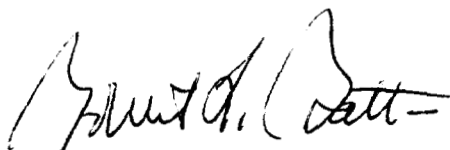
- o "Blue" smoke emissions that would violate Rule 50 were not observed at the silo load-in area as was observed before the facility management installed the fan and ducting to transfer the suspended liquid medium to the rotary drum burner.
- o The source test team encountered extreme difficulty in obtaining valid measurements in the wet collector exhaust stack, due primarily to exhaust gas turbulence.

CONCLUSIONS

The plant was operating at full capacity.

"Blue smoke" emissions at the silo load out area exceeded 40% opacity.

Detached particulate matter in the stack exhaust plume was not apparent.



ROBERT L. BATTEN
Associate Air Pollution Control Engineer

RLB:jo

092085

1 SOURCE TEST
2
3 COMPUTER INPUT DATA FORM

TEST NO.	R U N N O.	C A R R D N O.	TEST SITE																																
85260			CAUTION ROCK Neph 254																																
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36
			Source TEST P STATION, B Yellow Sky, G CARRIER R BATTERY (ENG) C BATTERY (ENG)																																

NOTE:
Start coding at Column 1. The decimal point ft also be coded, otherwise, it is assumed that the decimal point is after column 7.
Up to 7 digits can be coded.
Minus sign should also be coded for negative numbers.

WRD:ST:8-11-83

DATA

CARRD

0.1
0.2
0.3
0.4
0.5
0.6
0.7
0.8
0.9
1.0
1.1
1.2
1.3
1.4
1.5
1.6
1.7
1.8
1.9
2.0

Barometric Pressure, in. Hg

Stack Pressure, in. H₂O

Start meter Volume, ft³

Final Meter Volume, ft³

Max. Vapor Permitted at T_i, in. Hg

Max. water vapor permitted at T_s, in. Hg

Volume of condensed water, ml.

Meter calibration factor

% CO₂ (min. value = 0.04)

% CO

% O₂

% N₂

Pitot tube correction Factor

Area of stack, ft²

Nozzle diameter, in.

Duration of sampling, min.

Wt of particulate matter collected, gm.

PPM NO₂, DRY

PPM SO₂, DRY

Auxiliary Fuel Flow Rate, CFM

71 = .7648

70 = .7392

102560.55 = .0408

130.58

112.18

108.34

SOURCE TEST
P STANMAN, B YELINOSKY, G CHALIER
R BATTEN (ENG) C BEITMAN (SUC)

$$\begin{array}{r} 71 = .7648 \\ 70 = .7392 \\ \hline .0256 \cdot .55 = .01408 \end{array}$$

Barometric Pressure, in. Hg
Stack Pressure, in. H₂O
Start meter Volume, ft³
Final Meter Volume, ft³
Max. vapor permitted at T₁, in. Hg
Max. water vapor permitted at T₂, in. Hg
Volume of condensed water, ml.
Meter calibration factor
% CO₂ (min. value = 0.04)
% CO
% O₂
% N₂
Pitot tube correction Factor
Area of stack, ft²
Nozzle diameter, in.
Duration of sampling, min.
Wt of particulate matter collected, gm.
PPM NO₂, DRY
PPM SO₂, DRY
Auxiliary Fuel Flow Rate, CPM

SN # 5

130.58
112.18
1.19 ml

70.55
75.33
150.1540

Canyon Rock Asphalt

9/17/85 81

**SAN DIEGO APCD
SAMPLE COLLECTION DATA**

OPERATOR

OPERATOR
Jerman, J. Jelenosky, G. Carrier

Starting Volume 954.580

954-580
GAS VOL.

CARD

HECKS

INITIAL

Pitot

The mo

Train

INTERMEDIATE

Pitot

Trail

FINAL

Pitot

Train

DAPCD ST #53

[illegible]

**SAN DIEGO APCD
SAMPLE COLLECTION DATA**

DATE 9/17/85
TEST NO 85260
OPERATOR _____

Canyon Rock Asphalt

28

[illegible]

646

[illegible]

SAN DIEGO COUNTY AIR POLLUTION CONTROL DISTRICT

TEST# 85260
NØØ254

DATE# 9/17/85

SITE# CANYON ROCK

UNIT# _____

ABSOLUTE PRESSURE IN METER: 30.07

ABSOLUTE PRESSURE IN STACK: 29.86

ABSOLUTE TEMP. IN METER: 99°F ~~99°F~~

PRESSURE DROP ACROSS METER: 2.7

% MOISTURE OF STACK GAS: 30%

CORRECTION FACTOR: .935

STACK TEMPERATURE: 172°F

AVE. DIFFERENTIAL PRESSURE: .1

IDEAL NOZZLE DIAMETER: .382

NOZZLE USED: .382

TEST DIFFERENTIAL PRESSURE: .1 AP / 1.7 ΔH

STACK conditions
required the Nominal
Number to be changed
to 20

$$\Delta H 1.7 \text{ rate} = .577 \text{ SCFM}$$

$$\text{Required sample Vol} = 60 \text{ SCF}$$

$$\text{Time} = \frac{60 \text{ SCF}}{.577 \text{ SCFM}} = 103 \text{ min}$$

$$\text{Test points} = 48$$

$$\text{minutes per test point} = \frac{103}{48} \approx 2.1 \text{ min}$$

$$\text{Ave sampling } \phi = 78^\circ$$

$$\text{Nominal Number} = \frac{\text{min/PT}}{\cos 78^\circ} = 9.6 \text{ or } 10 \text{ min a point}$$

Canyon Rock Asphalt

9/17/85

4³⁰ Left APCD

5⁰⁰ arrived @ test site. It is dark and there are no lights @ the stack. There are a few about 100 yds away but give very little light our way.

~~We~~ must have proper lighting if we are to climb the stack in the dark.

5³⁰ There is not enough clearance between the platform and the port hole (only 14", there should be 20 1/2" for clearance of the impinger box) Bottom railing to the platform 18" (Need at least 21" for the impinger box) sent P. I. to bring longer probe (7') and longer railing.

6³⁰ P. I. returned. He had to clean the probe @ the lab before coming back.

7⁰⁰ Problems to leakcheck

7³⁰ Finally found the leaks

7⁴⁵ Leak checks completed

8⁰⁰ Problems with measuring cyclonic flow because the stack is not only cyclonic but very turbulent.

9⁵⁷ Began sampling

2⁴⁵ Production stopped. Test ended.

3⁰⁵ Leak checks OK

$$m_d = \frac{.44}{2.6} (5.92) + .32 (1.65) + .28 (83.58)$$

$$+ 3.36 + 23.4024$$

ISOTHERMIC ΔH

CAN YOU ROCK

$$D_m(Act) = .382 \left[846.872 (.382^4) (2.7) (.823^4) \cdot \frac{29.3624 (559) (29.86)}{26.18 (632) (30.07)} \right]$$

$$\Delta H_e = 2.7$$

$$C_p = .823$$

$$(1 - B_{ws}) = .17$$

$$M_D = 29.3624$$

$$T_m = 559$$

$$P_s = 29.86$$

$$M_s = 26.18$$

$$T_s = 632$$

$$P_m = 30.07$$

$$\left[846.872 \left(\frac{.0213}{.4742} \right) (2.7) (.6773) \right] \cdot \frac{490110.0}{497531.0}$$

$$\left[\frac{16.164}{32.987} = .9851 \right]$$

$$\left[15.923 \right] = K$$

$$\left[\overset{K}{15.923} \right] \cdot \overset{\Delta P_{est}}{(.1)} = 1.6$$

$$\Delta H = 1.6$$

NOZZLE Est for Canyon Rock long method

$$D_{n(est)} = \sqrt{\frac{.0358 (Q_{m}) (P_{m})}{T_{m} C_p (1-BW_s)}} \cdot \sqrt{\frac{T_s M_s}{P_s (\Delta P_{est})}}$$

$$Q_m = .577 =$$

$$P_m = 30.07$$

$$T_m = 559$$

$$C_p = .823$$

$$(1-BW_s) = .7$$

$$T_s = 632$$

$$M_s = 26.18$$

$$P_s = 29.86$$

$$\Delta P_{est} = .1$$

$$= \sqrt{\frac{.0358 (.577) (30.07)}{559 (.823) (.7)}} \cdot \sqrt{\frac{632 \cdot 26.18}{29.86 \cdot (.1)}}$$

$$= \sqrt{\frac{.62114}{322.039}} \cdot \sqrt{\frac{16545.76}{2.986}}$$

$$= \sqrt{.001929} \cdot \sqrt{5541.112}$$

$$= \sqrt{.001929 \cdot 74.4386}$$

$$= \sqrt{.143592}$$

$$D_{n est} = .379 \text{ IDEAL}$$

$$\text{use } .382$$

- Canyon Rock

- ① Probes
- ② inclinometer & level
- ③ Nomograph
- ④ center scale M2queliix - stack tube manometer
- ⑤ No site file -
- ⑥ Special Forms
- ⑦ STACK TRAVERSE POINTS
- ⑧ CALCULATIONS

ΔP

1984 - .1

1983 - .1

1981 - .1

MECHANICAL ENGINEERING TEST REPORT

Canyon Rock/V.R. Dennis Asphalt Plant
7500 Mission Gorge Road
San Diego, California

PERMIT TO OPERATE NO. 254: Renewal Compliance Test conducted by the APCD

TEST DATE: September 17, 1985

TEST PERIOD: 9:57 am to 2:50 pm

ASPHALT HOT MIX: Each batch was 3 tons.

3/8 INCH					1/2 INCH				
3/8" Aggragate									
	3/8 Agg.	Sand	Dust	Oil	1/2 Agg.	3/8 Agg.	Rock	Dust	Oil
LBS.	1956	1956	1656	432	804	2004	1410	1410	372
%	32.6	32.6	27.6	7.2	13.4	33.4	23.5	23.5	6.2

Only small amount % 1/2 inch mix was produced.

ROTARY DRUM BURNER FUEL: Natural Gas

BATCH COUNT: 1 batch per 0.83 minutes.

$$\frac{\text{batch}}{0.83 \text{ min.}} \times \frac{3 \text{ ton}}{\text{batch}} \times \frac{60 \text{ min}}{\text{hr.}} = 217 \text{ tons/hr}$$

Plant was operating at full 200 tons/hr capacity for duration of test.

AGGREGATE TEMPERATURE: 290 to 310°F at exit of rotary drum.

A/C OIL TEMPERATURE: 350-360°F into mixing section

COMMENTS

- o The stack exhaust was visibly checked periodically between 8:30 and 10:30 AM and appeared to be predominately water vapor. It was not apparent that the detached plume contained particulate matter.

- o "Blue smoke" emissions from the drop zone under the storage silos were quite significant. Each drop to either the truck bed or trailer bed produced opacity levels ranging between 40 and 60% for a rough average of 23 seconds each drop. Since each drop was a continuous delivery of 12 or 13 tons, the resulting elongated pile exposed more surface area to the atmosphere. The asphalt in the truck bed was measured to be 290 F. The magnitude of the emissions were 3 times that observed elsewhere where the load temperature was 300 F. It is apparent that some other parameter was the cause for the larger emissions, perhaps the quality of A/C oil being used.

- o The inverted conveyor belt on the underside of the hot mix transport (conveyor assembly) to the storage silo exhibited "blue smoke" emissions as the result of hot mix "clinging" to the belt. Positioning of the observer with relation to the sun is very critical for observing "blue smoke" emissions, especially for line emissions such as these belt emissions. A special determination should be conducted to evaluate the significance of these emissions with regard to Rule 50. A water based surfactant is being

employed to lubricate the belts. It should be determined whether or not the surfactant is contributing to the emissions. The apparent color of the emissions is the typical blue tint. A brown tint would be expected if the surfactant material was prominent in the emissions.

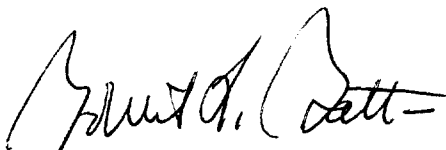
- o "Blue" smoke emissions that would violate Rule 50 were not observed at the silo load-in area as was observed before the facility management installed the fan and ducting to transfer the suspended liquid medium to the rotary drum burner.
- o The source test team encountered extreme difficulty in obtaining valid measurements in the wet collector exhaust stack, due primarily to exhaust gas turbulence.

CONCLUSIONS

The plant was operating at full capacity.

"Blue smoke" emissions at the silo load out area exceeded 40% opacity.

Detached particulate matter in the stack exhaust plume was not apparent.

A handwritten signature in black ink, appearing to read 'Robert L. Batten', with a stylized flourish at the end.

ROBERT L. BATTEN
Associate Air Pollution Control Engineer

RLB:jo

092085

TEST NO.: 85260
TEST DATE: 9/17/85
TEST SITE: CANYON ROCK 7500 MISSION GORGE RD
LOCATION: Mission Gorge + Princess View
SOURCE TEST PERSONNEL: P. JARMAN G. Carrier B. Yelonosky (B. Batten Eng.)
FACILITY CONTACT: KEN ATWELL 583-7606
APCD ENGINEER: B. Batten
APCD INSPECTOR: CARLOS
SAMPLE BOX NO.: #1
METER BOX NO.: D-337
FILTER NO.: 53
NOZZLE DIAMETER: 0.382 (#146)
STACK SIZE: 106" D
AMBIENT TEMP., °F: 71°F
ASSUMED MOISTURE, %: 30%
NO. OF SAMPLE POINTS: 48
MINUTES/POINT: 60 s • 20
START TIME: 0957
STOP TIME: 1445
TOTAL TEST TIME: 4 HRS 48 minutes
INITIAL VOLUME, FT³: 954.580
FINAL VOLUME, FT³: 988.800

LEAK CHECKS:

	INITIAL	FINAL
1. VAC. LINE (RED):	<u>ok</u>	<u>ok</u>
2. PRESSURE LINE (GREEN):	<u>ok</u>	<u>ok</u>
3. SAMPLE LINE:	<u>0.015 @ 15"</u>	<u>0.007 @ 7"</u>

(MUST BE ≤ 0.002 FT³/MIN.)

0.02

Sample Recovery
CANYON ROCK

68

Cyclonic & Turbulent stack

9/17/85 1630 - washed outside of probe

- ① Acetone 200 ml + 100 ml - 62 = 238 ml probe & nozzle wash
- ② DI H₂O 200 ml - 48 = 202 ml Probe & nozzle wash

9/18/85 IMPINGER Recovery - washed outside of all imp.

#1 IMPINGER 248 ml

#2 IMPINGER 108 ml

#3 Empty

#4 Empty

356 ml
- 200 ml charge
156 ml GAIN

H₂O WASH 200 ml + 150 ml

Acetone WASH 150 ml + 100 ml

Impinger catch light tan with red residue settling on bottom of impinger

Impinger catch & wash beaker put into oven at 105°C
Acetone Beaker left at room temperature

Filter #53 Removed from holder and put in plastic petri dish. Put in desiccator for drying

9/18/85 1420

H₂O Beaker evaporated to dryness. have to do quantitative transfer of contents. Measured out 100 ml of DI H₂O (Filtered) Used 60 ml H₂O in transfer

Sample Recovery

9/9/85 69
G. Carlier

Orinyl Rock 85260 Nφφ254

	PAN TARE	9/24/85	9/24/85 1345	9/24/85 1600	9/25/85 1145	FINAL
H ₂ O	C-1 IMPINGER	1.3910	1.6616	1.6622	1.6608	1.6608
Acetone	C-2 IMPINGER	1.4021	1.5501	1.5510	1.5510	1.5510
H ₂ O	BEAKER	26.3275				WATER correction pg 46 .0003 gm/cc
Acetone	BEAKER	27.0355				Acetone wash correction pg 63 .0002 gm/cc
H ₂ O K3P88	#53 FILTER	9/18/85 1145 1.1080 1.1245	9/18/85 1445 .1245	9/24/85 1345 .1216	9/24/85 1600 .1212	9/25/85 1145 .1216

changed silica gel in desiccator
TRANSFERRED ACETONE BEAKER contents to
PAN # C-2 MEASURED 100 ml of Acetone for
WASH. Used 42 ml in Transfer

Put 2 50 ml beakers in oven for Drying before
weighing

TARE weights

H₂O Beaker
9/20/85 1600 26.3274 gm
9/20/85 1400 26.3275
9/20/85 26.3275

9/20/85 Acetone Beaker
1000 27.0355
9/20/85 1400 27.0366
9/20/85 1600 27.0355

9/24/85 weighed Pan #40
C-1 1.6616 1345 1.6622 1600 1.6608 9/25/85 1145 1.6608
C-2 1.5501 1.5510 1.5510
Filter #53 .1216 .1212 .1216

SAMPLE Recovery CANYON ROCK 85260 N#9254 Computations

WATER Recovery & Impinger CATCH

C-1 ~~TARE~~
 FINAL 1.6608
~~TARE~~ 1.3910
 TOTAL 0.2698g

H₂O 0.2698^{ok}
 Acetone 0.1489^{ok}
 Filter 0.0136^{ok}
 0.4323^{ok}
 Correction 0.0021^{ok}
 0.4302^{ok}

Acetone WASH

C-2
 FINAL 1.5510
~~TARE~~ 1.4021
 TOTAL 0.1489

Correction
 H₂O 510ml x 0.0003 = 0.00153^{ok} gm
 Acetone 292ml x 0.0002 = 0.00584^{ok} gm
 TOTAL 0.0021^{ok}

FILTER # 53

FINAL 0.1216
 TARE 0.1080
 0.0136

WATER BEAKER
 9/26/85 26.3275

Acetone BEAKER
 9/26/85 27.0352

DATA NOT VALID
 not determination in Range
 of Weighing tolerance

H₂O used in WASH & CHANGE - Acetone used in WASH
 Charge 200
 WASH 200
 WASH 150
 WASH 150
 TMS 60
 510ml 10/1/85
 610ml (20)

WASH 150
 WASH 100
 WASH 42
 292ml

9/24/85

CANYON ROCK TOTAL SAMPLING TIME COMPUTATION

West Port Run #1

W8 3:25

W7 2:35

W6 2:35

W5 2:35

W4 2:35

W3 2:35

W2 4:14

W1 3:25

TOTAL 20:239.

Run #2

3:25

2:35

2:35

2:35

2:35

2:35

:30

0:00

13:230.

NORTH PORT Run #1

N-11 ~~8:40~~ 7:40

N-10 3:25

N-9 1:44

N-8 :10

N-7 :10

TOTAL 11:129.

Run #2

7:40

3:25

1:44

:10

:10

11:129.

CANYON ROCK TOTAL SAMPLING TIME COMPUTATION

EAST PORT

E12	14:08
E11	10:00
E10	1:44
E9	1:44
TOTAL	<u>26:96</u>

SOUTH PORT

S-12	14:08
S-10	3:28
S-9	1:20
S-7	1:20
	<u>17:76</u>

WEST PORT #1 20:239
#2 13:230

NORTH PORT #1 11:129
#2 11:129

EAST Port 26:96

SOUTH PORT 17:76
•98 : 899.

899 seconds = 14:59 OK

98 minutes OK

14:59 OK

112:59 = 113 minutes
OK PCQ

SITE. Canyon RockTEST # 85260Port # West

CYCLONIC FLOW

FIELD DATA WORK SHEET

PAGE 1 OF 4DATE 9-17-85CounterclockwiseCanyon Rock Asphalt

POINT NUMBER	NULL ANGLE	SAMPLE ANGLE	COSINE SAMPLE ANGLE	NOMINAL # <u>10</u>	SAMPLE TIME	<i>Repeat sampling if port to get more in ft. of sample</i>
12	180	180	—	—	—	
11	155	155	—		—	
10	110	110	—		—	
9	91	91	—		—	
8	70	70	0.342		3' 25"	3' 25"
7	75	75	0.259		2' 35"	2' 35"
6	75	75	0.259		2' 35"	2' 35"
5	75	75	0.259		2' 35"	2' 35"
4	75	75	0.259		2' 35"	2' 35"
3	75	75	0.259		2' 35"	2' 35"
2	65	65	0.423		4' 14"	4' 14"
1	70	70	0.342		3' 25"	3' 25"

SITE. Canyon RockTEST # 85260Port # NorthCYCLONIC FLOW
FIELD DATA WORK SHEETPAGE 2 OF 4DATE 9-17-85

POINT NUMBER	NULL ANGLE	SAMPLE ANGLE	COSINE SAMPLE ANGLE	NOMINAL # 10	SAMPLE TIME	
12	30 45	30 45	0.866 0.707		8' 40" 7' 04"	Turbulent @ sample neg ΔP
11	40	40	0.766		7' 40"	
10	70	70	0.342		3' 25"	
9	80	80	0.174		1' 44"	
8	89	89	0.0175		10"	
7	89	89	0.0175		10"	
6	100	100			—	
5	95	95			—	
4	105	105			—	
3	100	100			—	
2	110	110			—	
1	110	110			—	

SITE. Canyon RockTEST # 85260Port # EastCYCLONIC FLOW
FIELD DATA WORK SHEETPAGE 3 OF 4DATE 9-17-85

POINT NUMBER	NULL ANGLE	SAMPLE ANGLE	COSINE SAMPLE ANGLE	NOMINAL # 20	SAMPLE TIME	
12	45	45	0.707		14'.08"	
11	60	60	0.500		10'.0"	
10	85	85	0.087		1' 44"	
9	85	85	0.087		1' 44"	
8	105	105			—	
7	105	105			—	
6	110	110			—	
5	100 110	100 110			—	
4	115	115			—	
3	115	115			—	
2	120	120			—	
1	120	120				

SITE. _____

TEST # South 85260Port SouthCYCLONIC FLOW
FIELD DATA WORK SHEETPAGE 4 OF 4DATE 9/17/85

POINT NUMBER	NULL ANGLE	SAMPLE ANGLE	COSINE SAMPLE ANGLE	NOMINAL # 20	SAMPLE TIME	
12	20	20	0.940		18 ¹ / ₄ 8"	Did not sample
11	45	45	0.707		14 ¹ / ₂ 08"	
10	80	80	0.174		3' 24"	
9	89	89	0.0175		20"	
8	110	110			—	
7	89	89			20"	
6	100	100			—	
5	100	100			—	
4	100	100			—	
3	100	100			—	
2	110	110			—	
1	110	110			—	

270-8406

~~Paradise~~ - Lesue~~But~~ Citrus on desk $\frac{1}{33}$ pointsCanyon Rock
New entry points
10/2/88 (2)

W-8

160	.060	1.00	83	77	3.0	63	70
152			93.5	83.5		64.5	
144	.060	1.00	104	90	3.0	66	70

W-7

167	.090	1.5	96	78	0.0	66	75
155		1.525	105	83.5	1.5	64.5	
143	.090	1.55	114	89	3.0	63	75

W-6

165	.110	1.85	98	79	0.0	65	75
154.5	.115	1.45	92	84	1.75	64	
144	.120	2.05	116	89	3.5	63	75

W5

163	.140	2.4	102	80	0.0	68	75
155.5			109.5	84	2.0	64.5	
148	.140	2.4	117	88	4.0	61	75

W4

165	.160	2.7	102	80	0.0	65	75
162.5	.155		110.5	84	2.25	62.5	
160	.150	2.7	119	88	4.5	60	75

W3

163	.150	2.2	106	81	0.0	66	75
161		2.35	112.5	84.5	2.75	63.5	
159	.150	2.5	119	88	4.5	61	75

W2

159	.150	2.50	112	80	0.0	66	65	88%
159	.155	2.25	115.5	84	2.75	63.5		
159	.120	2.05	119	88	4.5	61	65	12%

W1

— 159 1030 .50 114.0 83 0.0 72 70

N11

148 1020 .34 100 86 0.0 81 40
 146.5 103
 145 1020 .34 106 86 0.0 85 40

N10

147 1060 1.0 108 83 0.0 81 70
 1055 .925 109.5 84.5
 147 1050 1.85 111 86 0.0 83 70

N9

147 1080 1.35 108 85 0.0 80 80
 148.5 110 86
 150 1080 1.35 112 87 0.0 78 80

N8

147 1080 1.35 108 85 0.0 80 89
 152 110 86
 157 1080 1.35 112 87 0.0 84 89

N7

147 1080 1.35 108 85 0.0 80 89
 152 110 86
 157 1080 1.35 112 87 0.0 84 89

SPECIAL EQUIPMENT:

CANYON ROCK ASPHALT.

1. NO A FRAMES
2. 9' RAIL
3. 7' PROBE
4. CLINEOMETER & POINTER
5. 0-.5" DWYER GAUGE
6. CONTACT KEN ATWELL @ 583-7611
7. SITE POTENTIALLY DANGEROUS,
 - A) STACK RUSTED/SUPPORTS RUSTED OUT.
 - B) CATWALK NARROW AND WITHOUT RETAINERS, POSSIBLE EQUIPMENT FALLING.
 - C) EXHAUST GAS 5' FROM CATWALK SO ALL WORK MUST BE CROUCHING OR SITTING ON SIDE OF CATWALK.
 - D) CHECK FOR LEAKS IN DUCTING FROM KILN DRYER TO SCRUBBER.
8. NOZZLE .312" (USED LAST)

9 NEW 16" STACK EXTENSION INSTALLED NO NEED FOR NEW PUMP

CANYON ROCK
DEMIS, D.R.
A.C.S.

AIR POLLUTION CONTROL DEPARTMENT - COUNTY OF SAN DIEGO

ORSAT FIELD DATA

Test No. 85260

Date 9/17/85

Site Canyon Rock Asphalt

Leak Check _____

AMB
AIR
#

%		1st Reading	2nd Reading	3rd Reading	4th Reading	5th Reading	Stable Reading
0	CO ₂	0	0	0	0		0
20.7	O ₂	19.4	20.4	20.7	20.7		20.7
	CO						

SAMPLE
E

2.4	CO ₂	2.4	2.4				2.4
16.5	O ₂	18.3	18.9	18.9			18.9
	CO						

SAMPLE
E

2.4	CO ₂	2.4	2.4				2.4
16.6	O ₂	18.6	19.0	19.0			19.0
	CO						

SAMPLE
#

	CO ₂						
	O ₂						
	CO						

SAMPLE
#

	CO ₂						
	O ₂						
	CO						

SAMPLE # _____

AVERAGE ANALYSIS

SAMPLE # _____

2.4	CO ₂
16.6	O ₂
	CO

	CO ₂
	O ₂
	CO

TEST NO 85 260
OPERATOR

CHECKS	POINT NO.					STACK TEMP. °F					PITOT P in.H ₂ O					GAS METER																				T _i °F					GAS VOL. FT. ³										CARD										Δ or %CO ₂																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																								
INITIAL	W	8						1	4	4				0	6			1	.	0				1	0	4				9	0			3	.	0				6	6	9	7	9			0	0	0								-		7	0																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																								
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