

The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

Commonwealth of Pennsylvania
Environmental Resources
September 25, 1990

Subject: Stack Test Review

To: Data File
Glasgow, Inc.
Catanach Plant
East Whiteland Township, Chester County

From: Rick Begley 
Air Pollution Control Engineer
Division of Technical Services and Monitoring
Bureau of Air Quality Control

Through: Chief, Source Testing and Monitoring Section 

Glasgow, Inc. operates a 350 ton per hour, batch asphalt plant fired with either natural gas or waste delivered No. 5 fuel oil in East Whiteland Township, Chester County. The plant produced an average of 328 tons per hour of asphalt and was fired with natural gas during the observed period.

Cold aggregate feed is transported by a conveyor to a rotary dryer. After passing through the rotary dryer, the heated aggregate is transported to the stackup tower where it passes through screens, an upper hot bin, a lower hot bin, a weigh hopper, a mixer where the oil is injected, and finally to an asphalt truck.

Heated air passes through the rotary dryer and is directed to a knockout box, a McCarter fabric collector and finally discharged to the atmosphere by an exhaust fan through a 54 inch diameter stack that extends to a point approximately 33 feet above grade. Fugitive emissions from the stackup tower are also collected and directed to the fabric collector along with the effluent from the rotary dryer.

The fabric collector, a McCarter Model McC-884-S, contains 884 felted Nomex bags and utilizes a reverse jet pulse to clean the bags periodically. The collector is designed to handle 72,000 ACFM at 250° Fahrenheit with a pressure drop of 2-4 inches W.G. Particulate matter collected is stored into a silo and eventually injected into the mixer bin.

Three Method 5 particulate tests were performed by personnel from Gilbert Commonwealth, Inc. to demonstrate NSPS compliance. The tests were conducted with a preapproved protocol and found to be acceptable to the Department.

Data File
 Glasgow, Inc.
 Cataract Plant
 East Whiteland Township, Chester County - 2 -

September 25, 1990

The following test results were extracted from the test report:

Run	1	2	3
Volumetric Flow Rate (DSCF/hr)	2,142,000	2,134,320	2,206,500
Rated Capacity (T/hr)		350	
Tested Rate (T/hr)	340	332	311
Actual Concentration (gr/DSCF)	0.014	0.011	0.013
Actual Emission Rate (lbs/hr)	4.14	3.49	4.05
Allowable Concentration (gr/DSCF)*	0.04		

Per New Source Performance Standards, Subpart L, 40CFR 60.90-60.93

cc: Roger A. Fitterling, Norristown Regional Office
 File 15-303-015
 Reading File
 Doug Leher

RE:staw

COMMONWEALTH OF PENNSYLVANIA
Environmental Resources
8-468-4175

DATE: September 6, 1990

SUBJECT: Glasgow, Inc.
Asphalt Concrete Plant
Catamash Plant
West Whiteland Township
Chester County

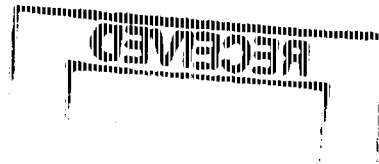
TO: L. BLAINE DeHAVEN, Chief *MM*
Source Testing & Monitoring Section
Division of Technical Services & Monitoring

FROM: Roger A. Fitterling *R*
Air Pollution Control Engineer

Technical Services personnel are requested to review the attached stack test report to determine compliance with the requirements of Chapter 139. Sampling for particulate and visible emissions from the company's concrete asphalt plant was conducted on August 18, 1990 by representatives of Gilbert/Commonwealth. The source is covered by Plan Approval No. 15-303-015. This plant is subject to the standards of 40 CFR part 60, subchapter I.

Attachments

cc: ASC
Norristown Region
Re30 RF6.2



9/26
REB



September 5, 1990

Commonwealth of Pennsylvania
Department of Environmental Resources
Bureau of Air Quality Control
625 Cherry Street
Reading, PA 19602-1188

Attention: Mr. Roger Fitterling
Air Pollution Control Engineer

Reference: Stack Test Results
Catanach Asphalt Plant
Application No. 15-303-015

Gentlemen:

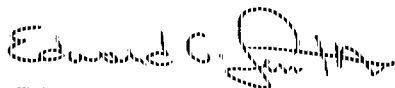
Please find enclosed two copies of the Source Sampling Report for Measurement of Particulate Emissions prepared by Gilbert Commonwealth, Inc. for our Catanach Asphalt Plant. This report indicates that the emissions from the plant are well below the allowable rates. Also enclosed are the results from the sieve analysis performed on the raw aggregate fed into the plant during the testing.

Please note that the starting gas reading for test run No. 3 is listed as not available in appendix III of the report. This reading should have been entered as 9,975,000, making the net gas consumed during the third run 70,000 cubic feet.

If you have any questions, please contact me.

Very truly yours,

GLASGOW, INC.


Edward C. Smith

ECS:rsb
Enclosures

RECEIVED
SEP 6 1990

RDG. DISTRICT OFFICE
DEPT. OF ENV. RES.

SOURCE SAMPLING REPORT FOR MEASUREMENT
OF PARTICULATE EMISSIONS

GLASGOW, INC.
CATANACH FACILITY
BATCH ASPHALT PLANT

G/C, INC., REPORT R-04-6187-000
AUGUST, 1990

SOURCE SAMPLING REPORT FOR MEASUREMENT
OF PARTICULATE EMISSIONS

GLASGOW, INC.
CATANACH FACILITY
BATCH ASPHALT PLANT

G/C, INC., REPORT R-04-6187-000
AUGUST, 1990

PREPARED BY

GILBERT/COMMONWEALTH, INC.
P.O. BOX 1498
READING, PENNSYLVANIA 19603

STEVEN G. FOLK
MANAGER
TESTING SERVICES GROUP



Gilbert/Commonwealth, Inc. engineers and consultants

P.O. Box 1400, Reading, PA 19603-1400/Telephone 215-775-2800/Cable Gilco/Telex 838-431

August 13, 1990

Mr. Ted Smith
Glasgow, Inc.
Willow Grove Ave. & Linckila Pl.
P.O. Box 248
Glennide, PA 19038-0248

Re: Submittal of Source Sampling Report for
Measurement of Particulate Emissions
and Determination of Visible Emissions
Asphalt Facility
G/C, Inc., Report R-04-6187-000

Dear Mr. Smith:

We are pleased to submit six copies of our Report R-04-6187-000, dated August 1990. This report contains results of source sampling for particulate and visible emissions for the asphalt facility exhaust stack located at your Catannach Plant, as conducted on July 13, 1990.

The source sampling program defined by this report incorporates standard sampling procedures. The results of the sampling program are representative of particulate and visible emissions at the stack outlet of the asphalt facility under referenced normal operating conditions.

Information contained in this report and the accompanying Appendices includes field data, and a computer printout of all results developed by the testing program. We have attempted to present this information in a form that is readily discernible and suitable for your continued use.

Gilbert/Commonwealth, Inc. is pleased to have been of service to Glasgow, Inc. and trusts that this report will meet your complete acceptance.

Very truly yours,

Steven G. Folk
Manager
Testing Services Group

SGF/llh

FOREWORD

The source sampling program as defined by this report was confined to measurement of particulate emissions and pertinent flue gas characteristics at referenced operating conditions and the visual determination of opacity.

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SECTION I - SUMMARY OF TEST RESULTS

A summary of test results from the source sampling program is presented in Table 1. As such the results are considered representative of emission characteristics from the Asphalt Batch Plant. The results show the Asphalt Batch Plant has an average emission rate of 0.013 gr/dscf using PAHER Method 5 procedures. The average visible emissions were 0% opacity. Both the average particulate emission rate and average opacity emission rate are well below the allowable emission rates of 0.04 gr/dscf and 20% respectively.

TABLE 1
SUMMARY OF TEST RESULTS
GLASGOW, INC.
CATANACH FACILITY
GLENSIDE, PA

04-6187-000

DATE	7/18/90	7/18/90	7/18/90
LOCATION		Stack	
RUN NO.	G-1	G-2	G-3
TIME	0835	1056	1349

OPERATING DATA

See Appendix 3

FLUE GAS CHARACTERISTICS

DSCFM	35,711	35,572	36,775
ACFM	54,264	54,208	54,372
Temperature, °F	200	202	251
Moisture, %	17.1	17.2	15.1

PARTICULATE EMISSIONS

Gr/DSCF	0.014	0.011	0.013
Lbm/Hr	4.14	3.49	4.05
Gr/DSCF, Average		0.013	
Gr/DSCF, Allowable		0.04	

VISIBLE EMISSIONS

Opacity, %	0	0	0
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SECTION II - ANALYSIS

1. Introduction

The data presented in this report represents the results of source sampling exhaust emissions at the baghouse location of the Asphalt Batch Plant during referenced operating conditions.

Specific requirements of this source sampling program include the following:

- a. Identification of final particulate emissions from Asphalt Batch Plant.
- b. Average flue gas temperature, moisture, and volume of flow at the sampling location.
- c. Orsat analysis of flue gas conditions at each point of sampling.
- d. Record of pertinent operating conditions during period of the test run.
- e. Visible Emission test during the particulate tests.

The sampling program was completed on July 18, 1990, by the Gilbert field test crew, with the assistance of personnel assigned by Glasgow, Inc.

2. Sampling Program Procedures

To satisfy the objectives established for this project, the sampling program was set-up on a basis of using one test train positioned at the test location and completing three test runs at each location. A test run consisted of a particulate test using PAJDER approved EPA Method 5, and a visible emissions test using EPA Method 9.

The location and number of sampling ports and traverse points are detailed in Figure 1.

3. Operating Conditions

In the execution of this sampling program, an attempt was made to achieve near normal load for the plant. The amount of product generated was recorded by the operator. This record is included in Appendix 3.

4. Results

Test data developed by each test run, together with analytical results from laboratory analysis of samples generated by the field sampling program, are reproduced in the Appendices included with this report. Information on basic gas characteristics developed by each test run is contained in the printout of the computer program included as Appendix 7.

A summary of pertinent test results and essential information to evaluate test results developed for each test run is included with this report as Table 1.

5. Discussion

5.1 Sampling Conditions

All field sampling work was completed out of doors and subject to prevailing weather conditions; however, there were no interruptions in the operation of individual test trains due to equipment or weather problems.

During the completion of this test program, the plant was maintained near the normal load condition.

5.2 Exhaust Flue Gas Volume and Composition

Test data for measurement of exhaust flue gas volume and related velocities developed by traversing of the stack show that the measured gas volumes between tests were consistent with expected values. For purposes of this report, indicated emissions are based on these measured gas volumes.

5.3 Unit Operating Conditions

This sampling program was undertaken as a compliance test program for the asphalt batch plant under representative load operating conditions. In the execution of this program, all applicable operation conditions were referenced.

Operating conditions were monitored throughout the duration of the sampling program by Chungow, Inc. personnel.

5.4 Emissions

5.4.1 Particulate

The reported particulate emissions as summarized in Table 1, are expressed as a concentration (grains/DSCF) and emission rate (lbs/hour) as measured.

5.4.2 Visible

The reported visible emissions as summarized in Table 1, are expressed as a percent.

TABLES AND FIGURES

Tables

1. Summary of Test Results

Figures

1. Location of Sample Ports and Traverse Points

$$P_c = 29.74 \text{ in Hg} \quad P_b + \frac{4H}{13.6} = 27.70$$

$$P_g = \text{static} = \frac{h \cdot H_2O}{13.6} = \frac{7.5}{13.6}$$

$$P = P_b + P_g = 28.5 \text{ in Hg} = 29.70$$

$$P_{ro} = 29.92 \text{ in Hg}$$

$$T_{ro} = 528$$

$$V_{we} = 216 \text{ m/s}$$

$$V_{wg} = 28 \text{ ft}$$

$$Y = 1.01$$

$$\phi_4 = \frac{2.22}{13.6} = 163 \text{ in Hg}$$

$$\phi_p = .84 \quad (TDP)_{we} = .870$$

$$T_s = 202 + 460 =$$

$$T_m = 102 + 460 =$$

$$A_s = 15.9 \text{ ft}^2$$

$$A_m = \text{ft}^2$$

$$\phi = 72 \text{ min}$$

$$V_m = 57.229$$

$$CO_2 = 2.7$$

$$O_2 = 16.1$$

$$N_2 = 81.2$$

$$M_a = 90.9 \text{ mg}$$

$$(5-1) \quad V_m(180) = K_1 V_m Y \frac{P_b + \frac{4H}{13.6}}{T_m} = 17.64 (57.229) (1.01) (27.70) = 54.35 \text{ ft}^3$$

$$V_w(180) = 0.04707 \frac{216}{\text{sec}} + 0.04715 \frac{28}{\text{ft}} = 11.2 \text{ ft}^3$$

$$B_{ws} = \frac{V_w(180)}{V_m(180) + V_w(180)} = \frac{11.2}{54.35 + 11.2} = .171 \quad (1 - B_{ws}) = .829$$

$$M_d = .44 \left(\frac{2.7}{100} \right) + .32 \left(\frac{16.1}{100} \right) + .28 \left(\frac{81.2}{100} \right) = 27.076$$

$$M_s = M_d (1 - B_{ws}) + 18 (B_{ws}) = 27.18$$

$$(9-9) \quad W_3 = K_p \phi_p (TDP)_{we} \sqrt{\frac{T_s (we)}{P_s M_s}} = \text{ft/min} = 56.58 \text{ ft/sec} = 3395 \text{ ft/min} = 3396 \text{ ft/min}$$

$$(9-10) \quad Q_{ro} = 3600 (1 - B_{ws}) W_3 A_s \left(\frac{T_{ro}}{T_{we}} \right) \left(\frac{P_g}{P_{ro}} \right) = \text{DSCF/hr} = 2145631$$

$$(5-7) \quad I = 100 \text{ ft} \left[K_3 W_3^2 + \left(\frac{V_{we}}{T_{ro}} \right) \left(P_b + \frac{4H}{13.6} \right) \right] = 351427$$

$$(1.23) (3396) (15.9) (29.07) (27.70) = 8662 \text{ DSCF/m}$$

$$\frac{21.0}{2.2} = 26.8$$

TABLE 1
SUMMARY OF TEST RESULTS
GLASGOW, INC.
CATANACH FACILITY
GLENSIDE, PA

04-6187-000

DATE	7/18/90	7/18/90	7/18/90
LOCATION		Stack	
RUN NO.	G-1	G-2	G-3
TIME	0835	1056	1349

OPERATING DATA

See Appendix 3

FLUE GAS CHARACTERISTICS

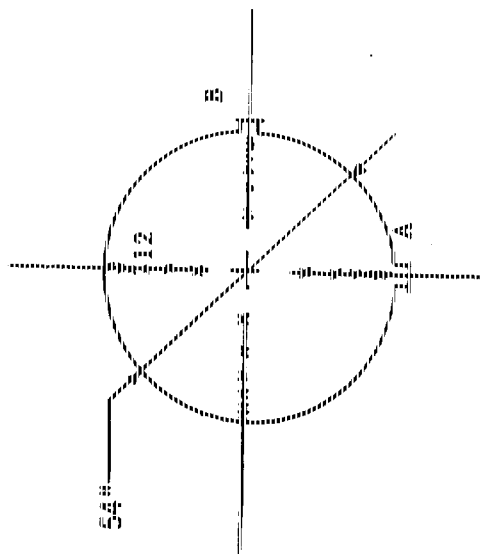
DSCFM	35,711	35,572	36,775
ACFM	54,264	54,208	54,372
Temperature, °F	200	202	251
Moisture, %	17.1	17.2	15.1

PARTICULATE EMISSIONS

Gt/DSCF	0.014	0.011	0.013
Lbs/Hr	4.14	3.49	4.05
Gt/DSCF, Average		0.013	
Gt/DSCF, Allowable		0.04	

VISIBLE EMISSIONS

Opacity, %	0	0	0
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1
2
3
4
5
6

[illegible][illegible]

SECTION III
APPENDICES

SECTION III - APPENDICES

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2. Testing and Analytical Procedures
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(Flue Gas Characteristics, Isokinetic Calculations, and Test Results for Particulate Emissions)
8. Sample Calculations

APPENDIX 1
PROJECT PARTICIPANTS

APPENDIX I
PROJECT PARTICIPANTS

The following members of Gilbert/Commonwealth's staff participated in the planning and execution of this project and preparation of this report.

Field Sampling Crews

George Albright
Mike Young
Gary Helm

Project Coordinator
Engineering Technician
Engineering Technician

Laboratory Participants

Vaughan O'Neill

Chemist

All field tests were completed with the assistance of technical personnel from Glasgow, Inc.

APPENDIX 2
TESTING AND ANALYTICAL PROCEDURES

- 2.1 STANDARD EPA TEST METHODS
- 2.2 ACTUAL SAMPLING PROCEDURES/PARTICULATE
- 2.3 ANALYTICAL METHODS/PARTICULATE

APPENDIX 2
TESTING AND ANALYTICAL PROCEDURES

2.1 STANDARD EPA TEST METHODS

APPENDIX 3

TESTING AND ANALYTICAL PROCEDURES

2.3 ACTUAL SAMPLING PROCEDURES/PARTICULATE

APPENDIX 2

TESTING AND ANALYTICAL PROCEDURES

2.2 ACTUAL SAMPLING PROCEDURES/PARTICULATE

Particulate matter in the exhaust gas stream at the stack sampling locations was sampled according to procedures and type of equipment as basically described in EPA Method 5 (see Appendix 2.1 for a complete description).

In the place of the fragile glass material, the in-stack probe liner was constructed of high corrosion resistant Inconel stainless steel, which was enclosed in an outer protective sheath and heat traced to minimize condensation within the probe.

The basic test train consisted of a stainless steel nozzle followed by a heated probe liner, glass fiber filter, and glass impingers with all glass connectors.

The required sampling time for the compliance test, in terms of time per traverse point and overall sampling time per individual test run, was selected on the basis of maintaining a minimum sampling time of 3.0 minutes at each of the traverse points.

The test program was completed with one test train located at the stack. All sampling activities were halted in the event of any test equipment malfunction or at the report of any operational problem.

APPENDIX 2
TESTING AND ANALYTICAL PROCEDURES

2.3 ANALYTICAL METHODS/PARTICULATE

APPENDIX 2

TESTING AND ANALYTICAL PROCEDURES

2.3 ANALYTICAL METHODS/PARTICULATE

The reported particulate emissions included the total particulate catch from the probe and nozzle water wash, the probe and nozzle acetone wash, the particulate accumulation on the glass fiber filter plus a .22 micron filtration of the impinger water.

The impinger water filtrate and the impinger acetone wash were dried down and weighed. These weights are reported on the laboratory certificate of analysis, but are not used to determine particulate emissions.

In the clean-up of the front half of the sampling equipment, the nozzle from the front of the probe was removed, brushed out, and washed with water then acetone. The probe liner was also brushed out and washed with water then acetone. The glass fiber filter was removed from the fritted disc of the filter holder and replaced in its petri dish. All adhering filter particles were removed from the silicone rubber gasket and placed in the same petri dish prior to sealing for transport back to the Gilbert assigned laboratory for final analysis. The filter holder was then washed with water then acetone and combined with the probe and nozzle wash.

The clean-up procedure for the back half of the sampling train initially involved removal of the silica gel from the last impinger and replacement in its original container for final weighing to determine moisture pickup. Water collected in the impingers was measured and placed in a sample bottle. The impingers and glass connectors were rinsed with water. The water rinse was added to the bottle containing the impinger contents. The impingers and glassware were then rinsed with acetone. This rinse was placed in a separate bottle.

Laboratory analysis of the particulate samples collected during the test run proceeded according to EPA Method 5 (Appendix 2.1).

APPENDIX 3
OPERATING DATA

APPENDIX 3
OPERATING DATA

FUEL CONSUMED

Date	Start Time	Stop Time	Gas Readings (Cum. Ft.)			Corresponding Particulate Run
			Start	Stop	Net	
7-18-90	0832	0952	9,884,000	9,966,000	82,000	1
7-18-90	1053	1212	9,930,000	9,998,000	78,000	2
7-18-90	1348	1502	NA	10,045,000	NA	3

ASPHALT PRODUCTION

Date	Start Time	Stop Time	Tons (Cumulative)	Corresponding Particulate Run
7-18-90	0835	0951	440.02	1
7-18-90	1055	1212	420.06	2
7-18-90	1450	1504	383.08	3

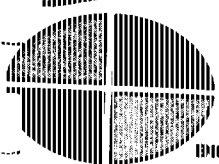
340

332

311

328.8

APPENDIX 4
ANALYTICAL RESULTS FOR PARTICULATES
(CLEAN-UP SHEETS)



SSM
 SPECIAL SERVICES and ANALYTICAL INC.
 ENGINEERS • PLANNERS • SCIENTISTS

Laboratories

CERTIFICATE OF ANALYSIS

CLIENT:

GILBERT/COMMONWEALTH INC
 P O BOX 1498
 READING PA 19603

REPORT NO.:

9040493

P.O. NO.:

52692

DATE REPORTED:

August 8, 1990

DATE RECEIVED:

July 20, 1990

WORK ORDER NO.:

SAMPLEING DATE:

JULY 18, 1990

BY: CLIENT

SAMPLE DESCRIPTION: STACK

SAMPLE IDENTIFICATION: ~~W. O. 04-6187-000~~ Glasgow
 W.O. 04-6187-000

LAB NO.	ROOM	PARTICULATE SOURCE	PARTICULATE WT (mg)
9040493-1	G-1	Impinger Water	7.9
9040493-1	G-1	Impinger Water (0.22 um Filter)	0.9
9040493-1	G-1	Impinger Acetone	6.1
9040493-1	G-1	Probe Acetone	8.4
9040493-1	G-1	Probe Water	30.7
9040493-1	G-1	Filter	7.8
9040493-2	G-2	Impinger Water	5.0
9040493-2	G-2	Impinger Water (0.22 um Filter)	3.6
9040493-2	G-2	Impinger Acetone	6.7
9040493-2	G-2	Probe Acetone	7.2
9040493-2	G-2	Probe Water	21.6
9040493-2	G-2	Filter	18.0
9040493-3	G-3	Impinger Water	5.2
9040493-3	G-3	Impinger Water (0.22 um Filter)	1.8
9040493-3	G-3	Impinger Acetone	4.8
9040493-3	G-3	Probe Acetone	14.0
9040493-3	G-3	Probe Water	16.9
9040493-3	G-3	Filter	10.2

Respectfully submitted,

Vaughan O'Neill

VAUGHAN O'NEILL - CHEMIST
 LABORATORY SERVICES

cc: Steve Folk

345 North Wyomissing Boulevard

P.O. Box 8307

Reading PA 19610-0307

(215) 376-6581

Fax (215) 376-6950

Other offices in Baltimore, Lehigh Valley and Trenton.

**STANDARD ASSOCIATES, INC.
LAB. FOLLOW-UP CONTROL DEPT.
PORTUGALASE CLEAN UP AND REPORT FORM**

Run Date: 7-19-92
Run No.: 6-23
Sample Run No.:
Comments: 2nd Run

Case: 6142900
H. C. No.:
Plant: City of New York
Sampling Location: Bay Area 44, 5th St

PORTUGALASE

Non-hazardous Sub
Pore, Thimble Holder, System Cleanup,
Place, Pore and Filter Holder-System Sub

Laboratory Results

Lab No. Backlog
Lab No. Backlog

THIMBLE, Sub.	Lab. No.	Balance, Backlog
.....		
.....		
.....		
.....		

Thimble Portugalase weight
.....

THIMBLE, Sub.	Lab. No.	Balance, Backlog
.....		
.....		
.....		
.....		

Filter Portugalase weight
.....

PORTUGALASE Sub Total
.....

PORTUGALASE

Septalase Cleanup and Pore Sub of Septalase
Cleanup and Back Half of Filter Holder

Lab No. Filter-Cleanup
Backlog
Collected on 0.33u Filter
Septalase Backlog

Septalase, Cleanup and Back Half of
Filter Holder - Septalase Sub

Lab No. Backlog
PORTUGALASE Sub Total
PORTUGALASE
.....

PORTUGALASE

Backlog

2663

THIMBLE, Sub.

Weight after clean	<u>2.35</u>		
Weight before clean	<u>36.32</u>		
Net Weight	<u>33.97</u>		
Concentration No. 1		2	

THIMBLE Volume

491

THIMBLE Volume

491

Net Volume

491

PORTUGALASE-THIMBLE Sub
.....

PORTUGALASE, Cleanup
.....

TOTAL PORTUGALASE
.....

Comments:

Lab. Date Reported
Date Reported

STANDARD ASSOCIATES

STANDARD ASSOCIATES

RAW FIELD DATA

Client Clayco

W. O. No. _____

Plant Clayco

Run No. 6-2

Location Highway Outlet

Date 7-16-96

Operator McL

Sample Box No. 2

Water Box No. 1613

Water ΔE _____

C Factor _____

FACTORY FIELD DATA

VERY IMPORTANT - FILL IN ALL SPACES

Read and record at the start of each test period

RECORD

Pilot Calibration

Table No. _____

Filter No. S-20

Ambient Temp. of 93°

Bar. Press. 29.74

Assumed Moisture % 17

Water Box Setting, of 250

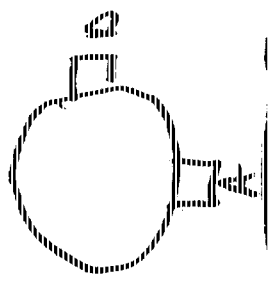
Probe Tip Dia., in. 0.244

Probe Length 1'

Probe Heater Setting _____

Avg. ΔE _____

Avg. ΔE _____



Probe Tip

ENTER	DISTANCE IN FEET	TIME TOTAL	WATER BOX NO.	WATER ΔE	WATER TEMP.		WATER PRESS.	WATER VOLUME	WATER TEMP.	WATER PRESS.	WATER VOLUME	WATER TEMP.	WATER PRESS.	WATER VOLUME
					IN	OUT								
1	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
3	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
4	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
5	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
6	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
7	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
8	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
9	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
10	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
11	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
12	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
13	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
14	1054	0.0	1613	0.65	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0

Client 614 595-2

W.O. No. _____

Plant 614 595-2Run No. 6-2PARTICULATE FIELD DATA
(continued)Location Bohemia 0.147Date 7/18/70Sheet 2 of 2

POINT	DISTANCE IN INCHES	CLARK TIME ACTUAL RUN	DRY GAS VOLUME, CF	PUMP IN. H ₂ O Δ P	ORIFICE Δ H IN. H ₂ O		DRY GAS TEMP. OF		PUMP VACUUM IN. Hg GAGE	BOX TEMP OF	REFINER TEMP OF	STACK TEMP. OF
					DESIGNED	ACTUAL	INLET	OUTLET				
A-1	11.5	6.0	141.414	0.14	1.03		101	177	6.5	250	37	193
1		2.0	120.0	0.50	1.01		100	177	1.0	250		196
2		6.0	141.414	0.50	1.01		103	177	1.0	250		196
3		10.0	141.414	0.50	1.01		103	177	1.0	250		196
4		15.0	141.414	0.50	1.01		103	177	1.0	250		196
5		20.0	141.414	0.50	1.01		103	177	1.0	250		196
6		25.0	141.414	0.50	1.01		103	177	1.0	250		196
7		30.0	141.414	0.50	1.01		103	177	1.0	250		196
8		35.0	141.414	0.50	1.01		103	177	1.0	250		196
9		40.0	141.414	0.50	1.01		103	177	1.0	250		196
10		45.0	141.414	0.50	1.01		103	177	1.0	250		196
11		50.0	141.414	0.50	1.01		103	177	1.0	250		196
12		55.0	141.414	0.50	1.01		103	177	1.0	250		196
13		60.0	141.414	0.50	1.01		103	177	1.0	250		196
14		65.0	141.414	0.50	1.01		103	177	1.0	250		196
15		70.0	141.414	0.50	1.01		103	177	1.0	250		196
16		75.0	141.414	0.50	1.01		103	177	1.0	250		196
17		80.0	141.414	0.50	1.01		103	177	1.0	250		196
18		85.0	141.414	0.50	1.01		103	177	1.0	250		196
19		90.0	141.414	0.50	1.01		103	177	1.0	250		196
20		95.0	141.414	0.50	1.01		103	177	1.0	250		196
21		100.0	141.414	0.50	1.01		103	177	1.0	250		196
22		105.0	141.414	0.50	1.01		103	177	1.0	250		196
23		110.0	141.414	0.50	1.01		103	177	1.0	250		196
24		115.0	141.414	0.50	1.01		103	177	1.0	250		196
25		120.0	141.414	0.50	1.01		103	177	1.0	250		196
26		125.0	141.414	0.50	1.01		103	177	1.0	250		196
27		130.0	141.414	0.50	1.01		103	177	1.0	250		196
28		135.0	141.414	0.50	1.01		103	177	1.0	250		196
29		140.0	141.414	0.50	1.01		103	177	1.0	250		196
30		145.0	141.414	0.50	1.01		103	177	1.0	250		196
31		150.0	141.414	0.50	1.01		103	177	1.0	250		196
32		155.0	141.414	0.50	1.01		103	177	1.0	250		196
33		160.0	141.414	0.50	1.01		103	177	1.0	250		196
34		165.0	141.414	0.50	1.01		103	177	1.0	250		196
35		170.0	141.414	0.50	1.01		103	177	1.0	250		196
36		175.0	141.414	0.50	1.01		103	177	1.0	250		196
37		180.0	141.414	0.50	1.01		103	177	1.0	250		196
38		185.0	141.414	0.50	1.01		103	177	1.0	250		196
39		190.0	141.414	0.50	1.01		103	177	1.0	250		196
40		195.0	141.414	0.50	1.01		103	177	1.0	250		196
41		200.0	141.414	0.50	1.01		103	177	1.0	250		196
42		205.0	141.414	0.50	1.01		103	177	1.0	250		196
43		210.0	141.414	0.50	1.01		103	177	1.0	250		196
44		215.0	141.414	0.50	1.01		103	177	1.0	250		196
45		220.0	141.414	0.50	1.01		103	177	1.0	250		196
46		225.0	141.414	0.50	1.01		103	177	1.0	250		196
47		230.0	141.414	0.50	1.01		103	177	1.0	250		196
48		235.0	141.414	0.50	1.01		103	177	1.0	250		196
49		240.0	141.414	0.50	1.01		103	177	1.0	250		196
50		245.0	141.414	0.50	1.01		103	177	1.0	250		196
51		250.0	141.414	0.50	1.01		103	177	1.0	250		196
52		255.0	141.414	0.50	1.01		103	177	1.0	250		196
53		260.0	141.414	0.50	1.01		103	177	1.0	250		196
54		265.0	141.414	0.50	1.01		103	177	1.0	250		196
55		270.0	141.414	0.50	1.01		103	177	1.0	250		196
56		275.0	141.414	0.50	1.01		103	177	1.0	250		196
57		280.0	141.414	0.50	1.01		103	177	1.0	250		196
58		285.0	141.414	0.50	1.01		103	177	1.0	250		196
59		290.0	141.414	0.50	1.01		103	177	1.0	250		196
60		295.0	141.414	0.50	1.01		103	177	1.0	250		196
61		300.0	141.414	0.50	1.01		103	177	1.0	250		196
62		305.0	141.414	0.50	1.01		103	177	1.0	250		196
63		310.0	141.414	0.50	1.01		103	177	1.0	250		196
64		315.0	141.414	0.50	1.01		103	177	1.0	250		196
65		320.0	141.414	0.50	1.01		103	177	1.0	250		196
66		325.0	141.414	0.50	1.01		103	177	1.0	250		196
67		330.0	141.414	0.50	1.01		103	177	1.0	250		196
68		335.0	141.414	0.50	1.01		103	177	1.0	250		196
69		340.0	141.414	0.50	1.01		103	177	1.0	250		196
70		345.0	141.414	0.50	1.01		103	177	1.0	250		196
71		350.0	141.414	0.50	1.01		103	177	1.0	250		196
72		355.0	141.414	0.50	1.01		103	177	1.0	250		196
73		360.0	141.414	0.50	1.01		103	177	1.0	250		196
74		365.0	141.414	0.50	1.01		103	177	1.0	250		196
75		370.0	141.414	0.50	1.01		103	177	1.0	250		196
76		375.0	141.414	0.50	1.01		103	177	1.0	250		196
77		380.0	141.414	0.50	1.01		103	177	1.0	250		196
78		385.0	141.414	0.50	1.01		103	177	1.0	250		196
79		390.0	141.414	0.50	1.01		103	177	1.0	250		196
80		395.0	141.414	0.50	1.01		103	177	1.0	250		196
81		400.0	141.414	0.50	1.01		103	177	1.0	250		196
82		405.0	141.414	0.50	1.01		103	177	1.0	250		196
83		410.0	141.414	0.50	1.01		103	177	1.0	250		196
84		415.0	141.414	0.50	1.01		103	177	1.0	250		196
85		420.0	141.414	0.50	1.01		103	177	1.0	250		196
86		425.0	141.414	0.50	1.01		103	177	1.0	250		196
87		430.0	141.414	0.50	1.01		103	177	1.0	250		196
88		435.0	141.414	0.50	1.01		103	177	1.0	250		196
89		440.0	141.414	0.50	1.01		103	177	1.0	250		196
90		445.0	141.414	0.50	1.01		103	177	1.0	250		196
91		450.0	141.414	0.50	1.01		103	177	1.0	250		196
92		455.0	141.414	0.50	1.01		103	177	1.0	250		196
93		460.0	141.414	0.50	1.01		103	177	1.0	250		196
94		465.0	141.414	0.50	1.01		103	177	1.0	250		196
95		470.0	141.414	0.50	1.01		103	177	1.0	250		196
96		475.0	141.414	0.50	1.01		103	177	1.0	250		196
97		480.0	141.414	0.50	1.01		103	177	1.0	250		196
98		485.0	141.414	0.50	1.01		103	177	1.0	250		196
99		490.0	141.414	0.50	1.01		103	177	1.0	250		196
100		495.0	141.414	0.50	1.01		103	177	1.0	250		196
101		500.0	141.414	0.50	1.01		103	177	1.0	250		196
102		505.0	141.414	0.50	1.01		103	177	1.0	250		196
103		510.0	141.414	0.50	1.01		103	177	1.0	250		196
104		515.0	141.414	0.50	1.01		103	177	1.0	250		196
105		520.0	141.414	0.50	1.01		103	177	1.0	250		196
106		525.0	141.414	0.50	1.01		103	177	1.0	250		196
107		530.0	141.414	0.50	1.01		103	177	1.0	250		196
108		535.0	141.414	0.50	1.01		103	177	1.0	250		196
109		540.0	141.414	0.50	1.01		103	177	1.0	250		196
110		545.0	141.414	0.50	1.01		103	177	1.0	250		196
111		550.0	141.414	0.50	1.01		103	177	1.0	250		196
112		555.0	141.414	0.50	1.01		103	177	1.0	250		196

Client Chesapeake

W.O. No. 6-3

Plant Chesapeake

Run No. 6-3

PARTICULATE FIELD DATA
(continued)

Location Chesapeake

Date 7/18/90

POINT	DISTANCE IN INCHES	CLOCK TIME ACTUAL RUN	DRY GAS VOLUME, CF	PILOT IN. H ₂ O Δ P	ORIFICE Δ H IN. H ₂ O		DRY GAS TEMP. OF		PUMP VACUUM IN. HG GAUGE	BOX TEMP OF	REFRIGER TEMP OF	STAGE TEMP. OF
					DESIGNED	ACTUAL	INLET	OUTLET				
A)	1425	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
B)	1430	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
C)	1435	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
D)	1440	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
E)	1445	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
F)	1450	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
G)	1455	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
H)	1460	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
I)	1465	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
J)	1470	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
K)	1475	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
L)	1480	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
M)	1485	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
N)	1490	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
O)	1495	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
P)	1500	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
Q)	1505	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
R)	1510	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
S)	1515	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
T)	1520	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
U)	1525	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
V)	1530	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
W)	1535	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
X)	1540	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
Y)	1545	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207
Z)	1550	20	102.106	0.33	1.61	1.61	107	71	1.0	210	37	207

COMMENTS:

15.0 - 5.0 - 0.01
15.0 - 5.0 - 0.01
15.0 - 5.0 - 0.01

APPENDIX 6
CALIBRATION DATA

Gilbert/Comamonreuth

DRY GAS METER CALIBRATION DATA

Meter box number		1625		Calibrated by : HELM		Date : 7/9/90	
1	2	3	4	5			
Critical orifice ID	1576	1572	1571	1274			
Critical orifice factor	0.2669	0.4535	0.5233	0.6670	0.8072		
Dry gas meter							
Final reading, ft	362.935	366.591	371.243	0.000	0.000		
Initial reading, ft	361.173	363.504	367.812	0.000	0.000		
Difference, in, ft	1.76	3.087	3.431	0	0		
Temperature							
Initial inlet/outlet, F	105	99	104	93	109	91	0
Final inlet/outlet, F	104	90	107	91	113	93	0
Avg. inlet/outlet temp, F	97	96	102	0	102	0	0
Avg. outlet temp, F	89.5	90.5	92	0	92	0	0
Flow, g/min/sec	300.03	306.75	305.26	0	0	0	0
air	5.301	5.115	5.037	0.000	0.000	0.000	0.000
Orifice mm. rds./in. in. H ₂ O	0.37	1.2	1.9	0	0	0	0
Bar. pressure, ps, in. Hg	30.28	30.28	30.28	0	0	0	0
Ambient temperature, F, F	87	87	87	0	0	0	0
Pump vacuum, in. Hg	20	19	16.5	0	0	0	0
vacueto, ft	1.659	2.984	3.458	0.000	0.000	0.000	0.000
Vertical, ft	1.728	3.022	3.731	0.000	0.000	0.000	0.000
Bar. cal. factor, V	1.023	1.020	1.020	ERR	ERR	ERR	ERR
Orifice factor, V/H ₂ O	1.745	1.949	2.015	ERR	ERR	ERR	ERR
	199.544	924.1253	747.7455	ERR	ERR	ERR	ERR

Glenn/Conestoga Inc.
Testing Services Group
PETER BOX CALIBRATION

DATE: 7/23/90
 BAROMETRIC PRESS. (PS) = 29.41 in. Hg
 WATER BOX NUMBER: 1672
 CALIBRATION BY: BJB

WAS VOLUME		TEMPERATURES			
Office Humidity (dew pt) in. Hg	Wet Test Meter (PS) cu. ft.	Dry Gas Meter		Time	Wet Test Meter (PS) cu. ft.
		Inlet (PS) deg. F	Outlet (PS) deg. F		
0.5	5.000	75.5	77	12.43	1.02
1.0	5.000	75.5	86	9.12	1.02
1.5	10.000	75.5	90.5	13.18	1.02
2.0	10.000	75.5	94.5	15.35	1.01
3.0	10.000	75.5	97.5	11.05	1.01
4.0	10.000	75.5	81.5	9.37	1.00
				Average Y1	1.01

FORM 27-75

Y1 = (0.0017)(16.440) = 0.028
 (0.0017)(16.440)
 (0.0017)(16.440)
 Y2 = (0.0017)(16.440) = 0.028
 (0.0017)(16.440)
 (0.0017)(16.440)
 Y3 = (0.0017)(16.440) = 0.028
 (0.0017)(16.440)
 (0.0017)(16.440)

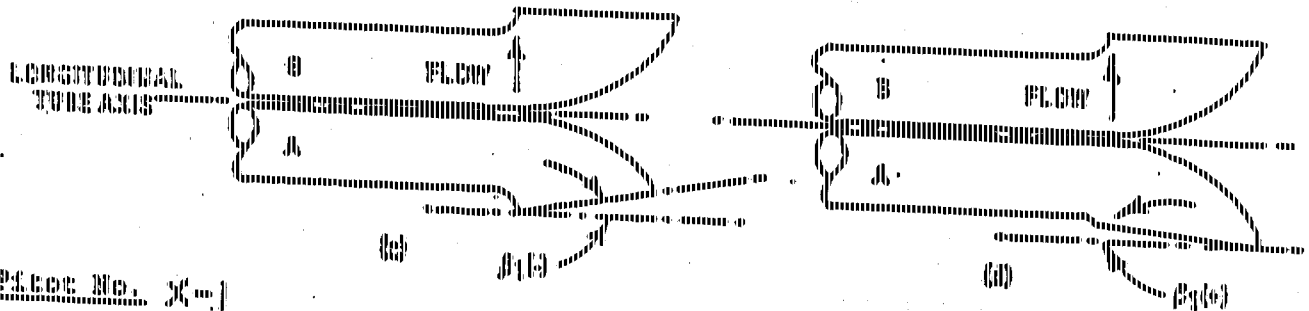
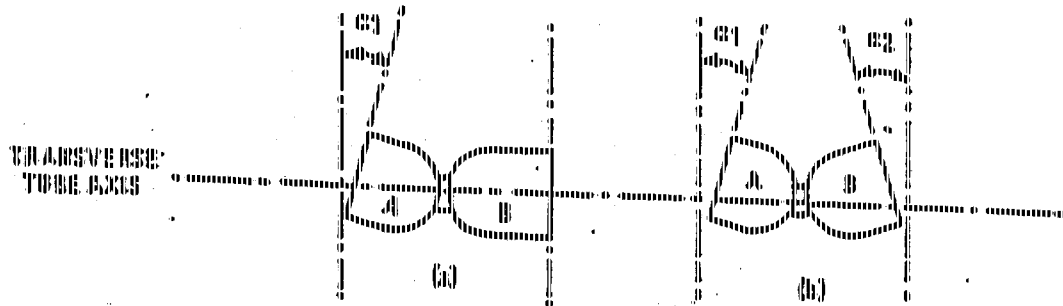
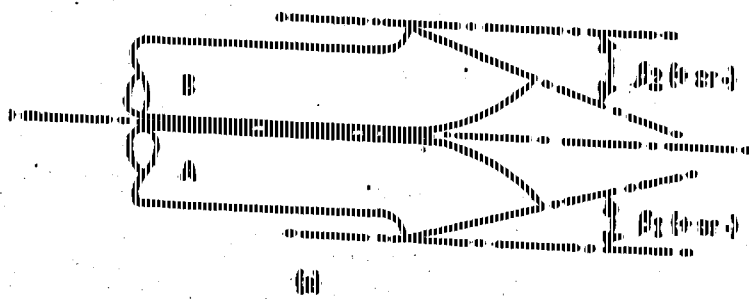


Figure No. X-1

Side

Reference	A	B
A ₁	2°	0
A ₂	—	—
B ₁	0	1°
B ₂	—	—



Reference	Ends
z	0
w	0

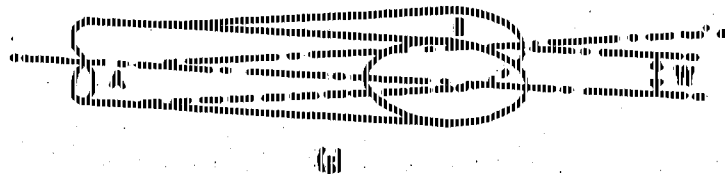
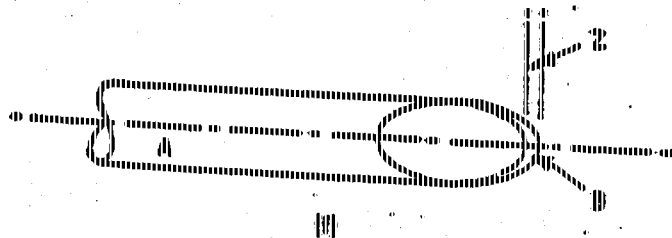


Figure 2-3. Types of face-opening misalignment that can result from field use or improper construction of Type S pilot tubes. These will not affect the baseline value of $C_p(s)$ so long as α_1 and $\alpha_2 \leq 10^\circ$, β_1 and $\beta_2 \leq 5^\circ$, $z \leq 0.32$ cm (1/8 in.) and $w \leq 0.08$ cm (1/32 in.) (citation 11 in Section 5).

GILBERT ASSOCIATES, INC.
ENGINEERS AND CONSULTANTS
READING, PA.

CLIENT

PROJECT

FILING CODE

PAGE

PAGE

REVISIONS

BY

DATE

REVIEWED BY

DATE

SYSTEM

CALIBRATION FOR

Pot Meter-Thermocouple Calibration

Pot Meter #

2

Thermocouple Type

K

Ice Bath Temperature °F

32

Certified Mercury Bulb °F

32

Ambient Temperature °F

70

Certified Mercury Bulb °F

70

Boiling H₂O °F

212

Certified Mercury Bulb °F

212

Hot Synthetic Oil °F

366

Certified Mercury Bulb °F

365

Remarks:

FILING
CODE

APPENDIX 7

COMPUTER PRINTOUT

(Flue Gas Characteristics, Isokinetic Calculations, and
Test Results for Particulate Emissions)

GILBERT/COMMONWEALTH, INC.
TESTING SERVICES GROUP
ISOKINETIC SAMPLING ANALYSIS

Client: SLASGON

Plant: Glenside, PA

Unit Tested: Baghouse Outlet

Pollutant: Particulate

Sampling Location: OUTLET

Run No: 6-1 Date: 7/18/90 Start: 635 End: 952

DATA

DN: 0.294 PB: 29.71 PST: -0.43 AS: 2250.2
O2%: 16.1 CO2%: 2.8 N2%: 82.1 VM: 238
GAS METER Y-FACTOR: 1.01 E.A.F.: 503.2

SAMPLE POINT	TIME AT POINT	GAS METER	VELOCITY HEAD	STACK TEMP.	METER IN	TEMP. OUT	PM DRIFICE	SDE	O2	CO	VEL
B-1	3.0	107.852	0.780	185	84	85	2.200	22.48	16.1		3420
2	3.0		0.870	195	89	86	2.450	23.87			3421
3	3.0		0.780	199	95	87	2.200	22.67			3439
4	3.0		0.800	201	98	88	2.250	23.00			3438
5	3.0		0.840	201	105	90	2.380	23.56			3574
6	3.0		0.880	200	108	90	2.600	24.10			3655
7	3.0		0.830	199	110	92	2.430	23.59			3547
8	3.0		0.800	199	112	93	2.350	22.96			3483
9	3.0		0.800	198	117	95	2.350	22.94			3430
10	3.0		0.810	197	118	97	2.390	23.07			3451
11	3.0		0.720	197	119	98	2.100	21.75			3219
12	3.0		0.680	197	119	95	1.980	21.14			3208
A-1	3.0		0.540	196	109	101	1.580	18.62			2853
2	3.0		0.540	195	111	102	1.580	18.61			2852
3	3.0		0.560	198	113	103	1.620	19.20			2912
4	3.0		0.580	201	115	103	1.700	19.58			2970
5	3.0		0.630	203	117	104	1.840	20.44			3100
6	3.0		0.670	204	117	104	1.960	21.09			3199
7	3.0		0.770	204	115	104	2.270	22.61			3430
8	3.0		0.850	204	115	104	2.510	23.90			3625
9	3.0		0.900	204	116	103	2.600	24.45			3708
10	3.0		0.850	205	117	103	2.510	23.91			3627
11	3.0		0.970	205	117	103	2.810	25.40			3852
12	3.0		0.920	205	117	103	2.680	24.73			3752
		165.443									

RESULTS

TT 72.0 VM 57.59% PIT TS TM PM SDE O2 CO VEL
net net avg avg avg avg avg avg
PSN= 29.87 VMSTD= 54.382 VMGAS= 11.210 MN= 17.1 RMS OF VELOCITIES = 7.6
MD= 0.83 MMD= 29.09 MN= 27.20 PS= 29.68

STACK GAS VELOCITY = 3.399 ACFM
STACK GAS VOLUME = 35.711 DSCFM
STACK GAS VOLUME = 54.254 ACFM
STACK GAS VOLUME = 1.84E+05 LBS/HR
ISOKINETIC RATIO = 103.3

PARTICULATE EMISSIONS

Weight, mg = 47.8
lb/DSCF = 0.014
LBS/HR = 4.14

GILBERT/COMMONWEALTH, INC.
TESTING SERVICES GROUP
ISOKINETIC SAMPLING ANALYSIS

Client: GLASSBORO

Plant: GLENSIDE, PA

Unit Tested: BAGHOUSE OUTLET

Pollutant:

Sampling Location: OUTLET

Run No: 6-2 Date: 7/18/90 Start: 1055 End: 1231

DATA

DN: 0.244 PB: 29.74 PST: -0.50 AS: 2290.2
O2: 16.1 CO2: 2.7 MZ: 91.2 VM: 239
GAS METER V-Factor: 1.01 E.A. %: 301.3

SAMPLE POINT	TIME AT POINT	GAS METER	VELOCITY FEET	STACK TEMP.	METER IN	TEMP. OUT	PM ORIFICE	SDE	O2	CO	VEL
8-1	3.0	166.633	0.650	195	93	95	1.900	20.63	16.1		3130
2	3.0		0.740	200	97	95	2.160	22.10			3351
3	3.0		0.760	202	101	96	2.210	22.43			3402
4	3.0		0.800	203	105	96	2.300	23.03			3493
5	3.0		0.810	204	107	97	2.350	23.19			3518
6	3.0		0.830	203	109	97	2.400	23.46			3558
7	3.0		0.770	203	105	98	2.250	22.59			3427
8	3.0		0.800	203	111	98	2.300	23.03			3493
9	3.0		0.850	203	111	99	2.450	23.46			3558
10	3.0		0.750	202	109	99	2.300	22.72			3447
11	3.0		0.740	202	109	99	2.250	22.13			3357
12	3.0		0.640	201	107	99	1.850	20.57			3120
9-1	3.0		0.470	185	101	97	1.350	17.41			2641
2	3.0		0.560	196	100	97	1.630	19.17			2907
3	3.0		0.560	200	103	97	1.610	19.22			2916
4	3.0		0.570	203	107	98	1.650	19.44			2949
5	3.0		0.590	204	108	98	1.700	19.79			3002
6	3.0		0.590	205	108	99	1.700	19.81			3004
7	3.0		0.800	205	107	99	2.300	23.07			3499
8	3.0		0.850	205	109	99	2.400	23.77			3506
9	3.0		1.050	204	109	99	3.010	26.40			4005
10	3.0		1.050	205	111	99	3.050	26.42			4008
11	3.0		1.100	204	114	99	3.200	27.03			4099
12	3.0		1.050	204	114	100	3.050	26.40			4005
		223.972									

RESULTS

TT 72.0 VM 57.338 PET 0.766 TS 202.7
net net avg avg
PM= 29.90 VMSTD= 54.364 VMGAS= 11.257 XM= 17.2
MD= 0.83 MMD= 29.07 MM= 27.12 PS= 29.70
RMS OF VELOCITIES = 9.0

STACK GAS VELOCITY = 3.396 AFPM
STACK GAS VOLUME = 35,572 DSCFM
STACK GAS VOLUME = 54,208 ACFM
STACK GAS VOLUME = 1.83E+05 LBS/HR
ISOKINETIC RATIO = 103.6

PARTICULATE EMISSIONS

Weight, mg = 40.6
GR/DSCF = 0.011
LBS/HR = 3.45

GILBERT/COMMONWEALTH, INC.
TESTING SERVICES GROUP
ISOKINETIC SAMPLING ANALYSIS

Client: GLASSBORO

Plant: GLENSIDE, PA

Unit Tested: BAGHOUSE OUTLET

Pollutant:

Sampling Location: OUTLET

Run No: 6-3 Date: 7/13/90 Start: 1349 End: 1501

DATA

DN: 0.244 PB: 29.72 PBT: -0.50 AS: 2290.2
O2%: 17.2 CO2%: 1.5 N2%: 79.1 Vn: 209
GAS METER Y-FACTOR: 1.01 E.A.%: 1219.7

SAMPLE POINT	TIME AT POINT	GAS METER	VELOCITY HEAD	STACK TEMP.	METER IN	TEMP. OUT	PM ORIFICE	SDE	O2	CO	VEL
3-1	3.0	224.220	0.150	180	93	94	0.435	9.80	17.2		1481
2	3.0		0.700	201	93	94	2.040	21.51			3252
3	3.0		0.770	205	97	94	2.290	22.83			3421
4	3.0		0.800	205	100	94	2.360	23.08			3490
5	3.0		0.830	205	103	95	2.450	23.51			3558
6	3.0		0.850	205	105	95	2.520	23.79			3597
7	3.0		0.780	207	110	96	2.300	22.81			3449
8	3.0		0.750	208	111	96	2.210	22.58			3384
9	3.0		0.760	208	112	97	2.250	22.53			3407
10	3.0		0.790	208	111	98	2.310	22.97			3473
11	3.0		0.830	207	112	98	2.450	23.53			3558
12	3.0		0.810	205	112	99	2.400	23.21			3509
A-1	3.0		0.550	203	107	99	1.610	19.10			2867
2	3.0		0.550	203	108	100	1.510	19.10			2867
3	3.0		0.580	198	107	100	1.700	19.54			2954
4	3.0		0.540	195	109	100	1.500	20.47			3096
5	3.0		0.580	189	108	100	1.580	21.01			3176
6	3.0		0.710	187	109	100	2.110	21.43			3241
7	3.0		0.910	187	111	101	2.200	24.26			3669
8	3.0		1.050	187	111	101	3.100	25.06			3941
9	3.0		1.100	187	115	101	3.220	26.68			4034
10	3.0		1.150	187	116	102	3.400	27.28			4124
11	3.0		1.150	187	116	102	3.400	27.28			4124
12	3.0		1.100	186	116	102	3.220	26.55			4030
		282.797									

RESULTS

TE 72.0 Vn 58.577 PBT 0.791 TS 199 TM 103 PM 2.311 SDE 22.53 O2 17.2 CO 1.5 VEL 3406
net net avg avg avg avg avg avg avg
PSM= 29.89 VMSD= 55.426 VMGAS= 9.844 VM= 15.1 RMS OF VELOCITIES = 15.3
MC= 0.85 MCD= 29.03 MH= 27.36 PS= 29.68

STACK GAS VELOCITY = 3.406 AFPM
STACK GAS VOLUME = 34,775 DSCFM
STACK GAS VOLUME = 54,372 ACFM
STACK GAS VOLUME = 1.86E+05 LBS/HR
ISOKINETIC RATIO = 102.2

PARTICULATE EMISSIONS

Weight, mg = 42.3
GR/DSCF = 0.012
LBS/HR = 4.05

APPENDIX 8
SAMPLE CALCULATIONS

SAMPLE CALCULATIONS

Particulate Lockdown Sampling

I. Calculations for stack volume and Lockdown Ratio

Time	Dry Gas Motor P ₂	Filter Δ P, In. H ₂ O	Orifice Δ P, In. H ₂ O	Dry Gas Temp °F In Out	Stack Static Pressure In. H ₂ O	Stack Temp °F
T	VM	Δ P	PM	TMI TMO	PST	TS

1. TM = Motor Diameter, inches

2. PM = Barometric Pressure, inches Hg

3. TT = Hot Sampling Time, minutes

4. VM = VM Final - VM Initial = Sample Gas Volume, ft³

5. TMI = Average Dry Gas Temperature at Motor, °F

$$TMI = \frac{\Delta P \cdot TMI + \Delta P \cdot TMO}{2}$$

6. PM = Average Orifice Pressure Drop, inches H₂O

$$PM = \Delta P$$

7. Volume of dry gas sampled at standard conditions, DSCP

$$VMSTD = \frac{17.45 \times VM \times T (PM + PM)}{(TMI + 460) (13.6)}$$

8. VW = Total Water Collected = gm H₂O Saturated gas + ml Imp. H₂O = ml

9. Volume of water vapor at standard conditions, SGP

$$VW_{gas} = 0.0471 \times VW = SGP$$

10. Percent moisture in stack gas

$$X M = \frac{100 \times VW_{gas}}{VM STD + VW_{gas}}$$

11. Mole fraction of dry gas

$$MO = \frac{100 - XM}{100}$$

12. Molecular weight of dry stack gas

$$MW = (CO_2 \times \frac{44}{100}) + (CO \times \frac{28}{100}) + [(CO + H_2) \times \frac{28}{100}]$$

$$12A. XEA = \frac{3 \text{ Excess Air} - [(CO_2) - 0.5 (CO)]}{0.266 (CO_2) - [(CO_2) + 0.5 (CO)]} \times 100$$

13. Molecular weight of wet stack gas

$$MG = MW \times MD + 18 (1 - MD)$$

14. AS = Stack Area, square inches

15. PS = Stack Pressure, inches Hg

$$PS = PD \pm \text{Avg. PST}$$

$$\text{NOTES: PST in. Hg.} = \frac{\text{PST in. H}_2\text{O}}{13.6}$$

16. TS = Average Stack Temperature, °F

$$TS = \text{Average TS}$$

17. SDE = Average $\sqrt{\text{Velocity Head (A.P.)} \times (\text{Stack Temperature} + 460)}$
(Calculated each 15 min)

$$SDE = \text{Avg } \sqrt{A.P. \times (TS + 460)}$$

18. Stack gas velocity at stack conditions, fpm

$$VS = 91.30 \times Cp \times \text{Avg}(SDE) \times \left[\frac{1}{PS \times MD} \right]^{1/4} = \text{fpm} \quad Cp = \text{piece cubic conditions}$$

19. Stack gas volumetric flow rate at standard conditions, DSCFM

$$Q_0 = \frac{0.123 \times VS \times AS \times MD \times PS}{(TS + 460)} = \text{DSCFM}$$

20. Stack gas volumetric flow rate at stack conditions, ACFM

$$Q_0 = \frac{0.00457 \times VS \times (TS + 460)}{PS \times MD} = \text{ACFM}$$

21. Percent moisture

$$M = \frac{1.032 \times (TS + 460) \times VMSR}{VS \times TS \times PS \times MD \times (CO)^2}$$

NOTES: a) Dry standard cubic foot at 69°F, 29.92 in. Hg.

b) Standard conditions at 68°F, 29.92 in. Hg.

c) Dry standard cubic foot per minute at 68°F, 29.92 in. Hg.

II. Calculations for grain loading and emission rates

12. Particulates, gr/DSCF

$$\text{gr/DSCF} = 0.0134 \times \frac{\text{HR}}{\text{VHSCTD}}$$

13. Particulates at each condition, gr/ACF

$$\text{gr/ACF} = \frac{17.63 \text{ gr/DSCF} \times \text{PS} \times \text{MD}}{(\text{TS} + 460)}$$

14. Particulates, lb/hr conc. method

$$\text{lb/hr} = 0.00937 \times \text{gr/DSCF} \times \text{QS}$$

15. Particulates lb/hr area method = $0.132 \times \frac{\text{1000 Particulates} \times \text{AF}}{\left(\frac{\text{DPM}^2}{4}\right) \times \text{TT}}$

16. Particulates, combustion

$$\frac{\text{lb/hr}}{10^6 \text{ BTU/hr}}$$

17. Particulates, process lb/con

$$\text{lb/con} = \frac{\text{lb/hr}}{\text{con/hr}}$$

18. Particulates, lb/MMBtu, P-Factor Method =

Using O_2 =

$$\frac{0.0134 \times \text{HR} \times \text{P-Factor} \times 20.9}{1000 \times \text{VHSCTD} \times (20.9 - \text{O}_2)}$$

Using CO_2 =

$$\frac{0.0134 \times \text{HR} \times \text{P-Factor} \times 100}{1000 \times \text{VHSCTD} \times \text{CO}_2}$$

19. P-Factor, docf/mmBtu

O_2 Percent =

$$\text{P-Factor} = \frac{10^6 (3.64 (\text{CO}) + 1.53 (\text{CO}_2) + 0.57 (\text{H}_2) + 0.16 (\text{H}_2\text{O}) + 0.44 (\text{CO}_2))}{657}$$

CO_2 Percent =

$$\frac{10^6 (0.311) (\text{CO}_2)}{657}$$

CATANACH ASPHALT PLANT - DRY SIEVE ANALYSIS

PENN DOT ID-2 BINDER (HEAVY DUTY) - 100% VIRGIN

SIZE	PRODUCT JMF	ADJ. FOR BH FINES REMOVED	DRY GRADINGS-RAW MATERIAL FEED			
			#1	#2	#3	AVERAGE
1 1/2	100.0	100.0	99.1	99.5	99.4	99.3
1	90.8	93.5	91.8	90.6	90.1	90.8
1/2	62.0	64.7	63.2	59.5	58.2	60.3
3/8	52.9	55.6				
4	44.0	46.7	46.7	36.3	34.6	39.2
8	35.0	37.7	42.4	29.9	31.0	34.4
16	25.0	27.7	32.3	21.6	25.4	26.4
30	19.0	21.7	21.1	13.6	17.9	17.5
50	11.0	13.7	10.1	7.7	8.9	8.9
100	6.0	8.7	4.3	3.7	3.5	3.8
200	3.5	5.5	1.6	1.4	1.4	1.5