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The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

Commonwealth of Pennsylvania
Environmental Resources
January 26, 1993

Subject: Stack Test Review

To: Data File
Windsor Service
Cumru Township, Berks County

From: Richard St. Louis, Chief
Source Testing Section
Division of Source Testing and Monitoring
Bureau of Air Quality Control

Through: Acting Chief, Division of Source Testing and Monitoring

Windsor Service operates a Gencor drum mix asphalt facility located in Cumru Township, Berks County. The facility has a design production capacity of 400 tons per hour and the capability of processing up to 30% by weight of recycled asphalt product (RAP).

Cold aggregate is proportioned, according to product specifications, into a drum mixer. The aggregate moves through the inclined drum into a drying zone where heat is supplied through the combustion of propane. The aggregate enters into a mixing zone where heated liquid asphaltic oil is added along with any mineral filler. RAP may be added to the mixture through a recycled aggregate feed collar located at the middle of the drum mixer. The mixed product is discharged into an enclosed slot conveyor transporting the product to heated storage silos.

The effluent from the mixer is ducted to a Gencor baghouse, Model PB-66PM designed to handle 66,000 ACFM. The material collected by this unit is recycled to the mineral filler silo. The effluent is discharged to the atmosphere from the baghouse through a 48 inch square stack.

United Energy Services conducted particulate and volatile organic compounds (VOC) tests in the stack outlet on October 21-22, 1992. Although the particulate and VOC test runs were conducted in accordance with a preapproved test protocol, they were difficulties associated with the VOC test program, especially with Run No. 2. High moisture content of the effluent resulted in the freezing of the sample trap used to collect the condensable fraction of the VOCs. Although a second trap was substituted, there was an apparent positive bias associated with this substitution as compared with Run Nos. 1 and 3. Therefore, Run No. 2 should not be included in determining the average VOC emission rate. The particulate and VOC test results, other than the test run noted above, are acceptable to the Department.

The following data was extracted from the test report:

Volatile Organic Compounds Emission Test

Test Run No.	Run #1	Run #2	Run #3	Allowable
Test Date	10/22/92	10/22/92	10/22/92	N/A
Emission Rate (lbs/ton)	0.054	0.151	0.072	0.07
Mass Rate (lbs/hr)	15.5	41.6	20.7	N/A

Particulate Emission Tests

Test Run No.	Run #1	Run #2	Run #3	Allowable
Test Date	10/21/92	10/22/92	10/22/92	N/A
Concentration (gr/dscf)	0.011	0.019	0.015	0.02
Mass Rate (lbs/hr)	3.30	5.66	4.23	N/A
Opacity %	0	0	0	N/A

cc: Roger A. Fitterling, Reading District Office
File No. 06-303-024
EPA/RSL
C&E - Jim Benson
Reading File - Source Testing

BSL:plc

SOURCE SAMPLING REPORT FOR MEASUREMENT
OF PARTICULATE, VOLATILE ORGANIC COMPOUND,
AND VISIBLE EMISSIONS

WINDSOR SERVICE, INC.
ASPHALT PLANT - BAGOUSE EXHAUST

SOUTH READING, PA

UESC, REPORT 015-664-001

NOVEMBER, 1992

Prepared by

United Energy Services Corporation
Air Quality Testing Services
525 Lancaster Avenue
Reading, Pennsylvania 19611

United Energy Services Corporation



November 24, 1992

Mr. Gary Burinsky
Windsor Service, Inc.
P.O. Box 13787
Reading, PA 19612

Re: Submittal of Source Sampling
Report For Measurement of Particulate,
Volatile Organic Compound and Visible
Emissions
UESC Report 015-664-001

Dear Mr. Burinsky:

We are pleased to submit four (4) copies of our Report 015-664-001, dated November 1992. This report contains results of source sampling for particulate, volatile organic compound, and visible emissions as conducted on October 21, 22, and 23, 1992.

The source sampling program defined by this report incorporates standard sampling procedures. The results of the sampling program are representative of flue gas emissions at the baghouse exhaust for the drum mix asphalt plant under referenced operating conditions.

Information contained in this report and the accompanying appendices includes field data, laboratory analysis, and a computer printout of all results developed by the testing program. We have attempted to present this information in a form that is readily discernible and suitable for your continued use.

United Energy Services Corp. is pleased to have been of service to Windsor Service, Inc., and trusts that this report will meet your acceptance.

Very truly yours,

M. Gary Helm
Air Quality Specialist
Air Quality Testing Services

MGI/sds

FOREWORD

The source sampling program as defined by this report was confined to the measurement of particulate, volatile organic compound, and visible emissions, and also pertinent flue gas characteristics at the baghouse exhaust serving the asphalt plant. This data was used to determine compliance with applicable Pennsylvania Department of Environmental Resources air pollution control regulations.

In the completion of the EPA Method 25 Volatile Organic Compound sampling there was a problem with the second run. During run number W-V-2, the sample trap that was sitting in dry ice became too cold and froze the sample passing through, cutting off the sample flow completely. We (UESC) elected to replace the sample trap, and completed the run. Where the problem arises, is in the analysis of these two traps. As stated in the letter from Triangle Environmental Services, dated November 18, 1992 (Appendix 4), this analysis was influenced by two factors. These two factors are the bias caused by CO_2 entrapped in ice in the sample traps, and the increased dilution factor as a result of the lower sample volumes, both of which will cause a high bias of the test results. The CO_2 trapped in the ice is reported as part of the total gaseous non-methane organics when the condensible portion of the sample is oxidized and analyzed. The low sample volumes (approximately 2 liters/trap) necessitates a greater dilution factor when analyzing the traps. This greater dilution factor will increase the significance of the high bias on the test results. For these reasons, UESC requests that the results from test W-V-2 be invalidated, and not used when determining compliance.

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SECTION II - SUMMARY OF TEST RESULTS

A summary of test results developed by the source sampling program is presented in Tables 1 and 2. As such, the results are considered representative of the emissions from the asphalt plant baghouse under referenced operating conditions.

The results show that baghouse exhaust had a particulate emission concentration of 0.015 gr/dscf. This is below the allowable emission concentration of 0.02 gr/dscf. The volatile organic compound emission rate is 0.063 lbs/ton of asphalt produced for runs W-V-1 and W-V-3. If run W-V-2 is included, the emission rate is increased to 0.092 lbs/ton of asphalt produced; however, UESC does not feel the data from W-V-2 is an accurate representation of volatile organic compound emissions. It is the opinion of UESC that the VOC compliance determination should be based on the average of test runs W-V-1 and W-V-3 which demonstrate that this source is below the allowable emission concentration. The allowable volatile organic compound emission rate is 0.07 lbs/ton of asphalt produced. The visible emission test results show an average opacity of 0.0%. This is below the allowable limit of 20% opacity.

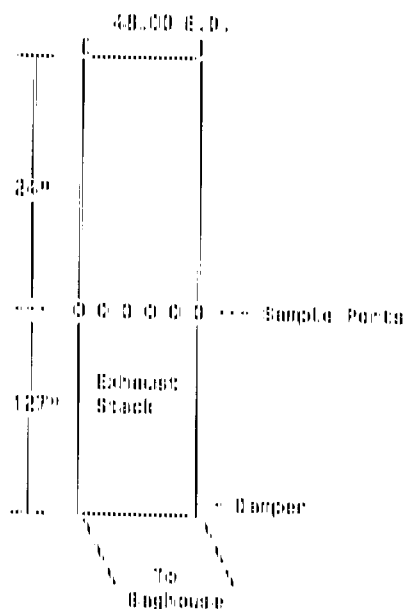
TABLE 1
SUMMARY OF TEST RESULTS
WINDSOR SERVICE, INC. - SOUTH READING, PA
PARTICULATE AND OPACITY
UESC, REPORT 015-664-001

DATE	10/21/92	10/22/92	10/22/92
LOCATION	BAGHOUSE EXHAUST		
RUN NUMBER	1	2	3
PRODUCTION RATE (tons/hr)	295	282	275
FLOW (DSCFM)	33,634	35,645	32,129
MOISTURE (%)	21.9	22.1	26.2
PARTICULATE			
GR/DSCF	0.011	0.019	0.015
AVERAGE (gr/dscf)		0.015	
ALLOWABLE (gr/dscf)		0.02	
OPACITY			
PERCENT	0.0	0.0	0.0
AVERAGE (%)		0.0	
ALLOWABLE (%)		0.0	

TABLE 2
SUMMARY OF TEST RESULTS
WINDSOR SERVICE, INC - SOUTH READING, PA
VOLATILE ORGANIC COMPOUNDS
UESC, REPORT 013-664-001

DATE	10/22/92		
LOCATION			
RUN NUMBER	1	2	3
FEED RATE (tons/hr)	285	276	288
FLOW (dscfm)	34,900	34,900	34,900
VOLATILE ORGANIC COMPOUNDS			
LBS/HR	15.5	41.6	20.7
LBS/TON	0.054	0.151	0.072
*AVERAGE (lbs/ton)		0.063	
ALLOWABLE (lbs/ton)		0.07	

*Average does not include run W-V-2. If W-V-2 is included, the average is 0.092 lbs/ton.



The exhaust stack cross section was divided into 24 equal rectangular elemental areas, with the sample points being located at the centroid of each area.

DIMENSIONS

Depth = 48 inches
 Width = 48 inches
 Equivalent diameter = 48.00
 Area = 2304

DISTANCE FROM NEAREST DISTURBANCE

	Downstream	Upstream
Feet & Inches	10 7	2 0
Inches	127	24
Diameters	2.65	0.50

NUMBER OF POINTS (Required) 24
 NUMBER OF PORTS 6

POINTS PER PORT 4.00
 (If not an integer already, use next largest integer)
 POINTS PER PORT (Revised) 6

NUMBER OF POINTS (Actual) 24

TRANSVERSE POINT LOCATION

Transverse Point	Distance From Port	
	(Inches)	(% of Dist Depth)
1	6.00	0.125
2	18.00	0.375
3	30.00	0.625
4	42.00	0.875

FIGURE 1

LOCATION OF TRANSVERSE POINTS AND SAMPLE PORTS
 ASPHALT PLANT BAGHOUSE EXHAUST
 WINDSOR SERVICE, INC. - SOUTH READING PLANT

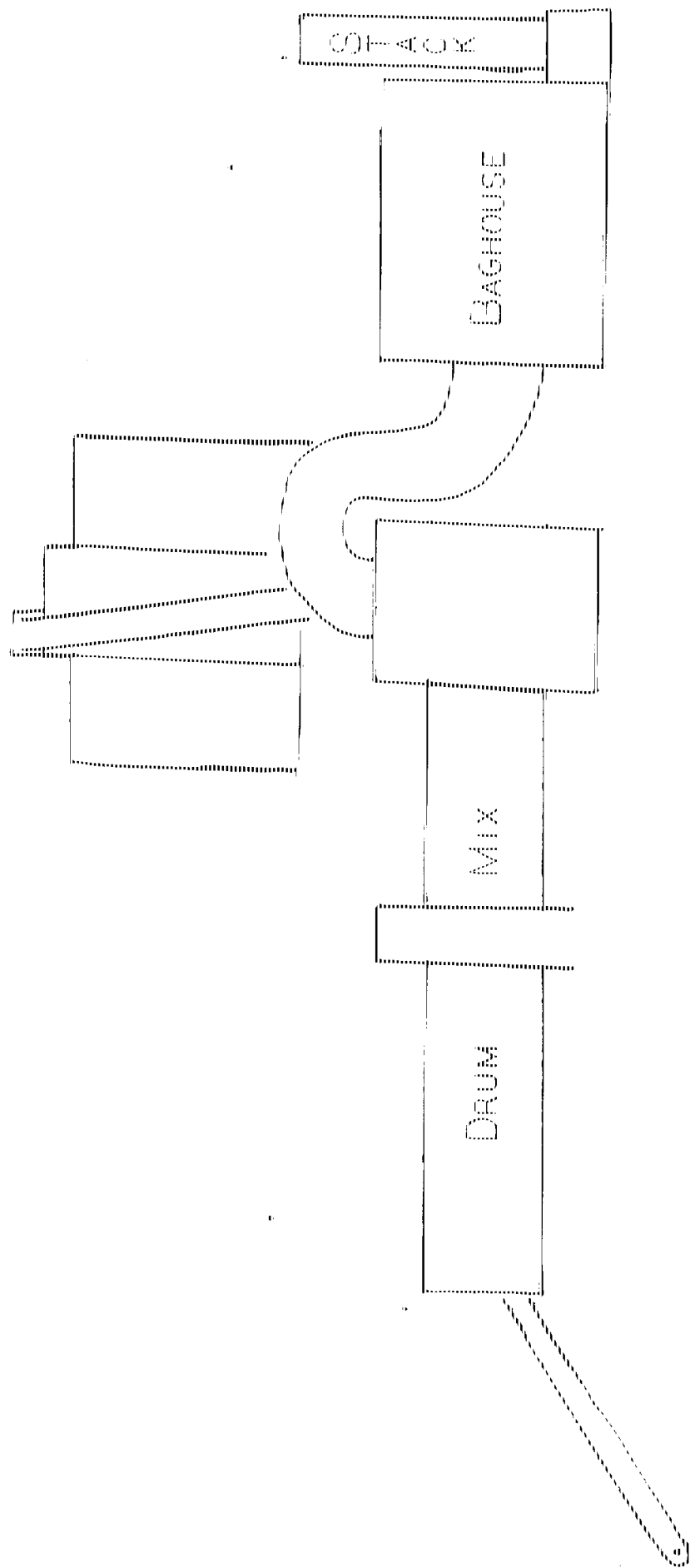


FIGURE 2
Process Flow Diagram

SECTION III - ANALYSIS

1. Introduction

The data presented in this report represents the results of a compliance source sampling program for the determination of particulate, volatile organic compound, and visible emissions, and also pertinent flue gas characteristics at the baghouse exhaust serving the asphalt plant.

Specific requirements of this source sampling program include the following:

- a. Identification of particulate emissions expressed as a concentration (gr/dscf) and an emissions rate (lbs/hr).
- b. Identification of volatile organic emissions expressed as an emission rate (lbs/hr) and (lbs/ton of asphalt produced).
- c. Identification of visible emissions expressed as a percent opacity.
- d. Average flue gas temperature, moisture, and volume of flow at the sampling location.
- e. Orsat analysis of flue gas O_2 and CO_2 concentration at the sampling location.

The sampling program was completed on October 21, 22, and 23, 1992 by the G/C, Inc./UESC field test crew, with the assistance of personnel assigned by Windsor Service.

2. Description of Process

The Windsor Service South Reading plant has one drum mix asphalt plant in operation. During testing, the plant was producing a top coat utilizing recycled asphalt products in the mix. Exact operating data may be found in Appendix III. Emissions from the drum mix traveled through the baghouse, the fan, and then out the exhaust stack.

Figure 2 represents a process flow diagram for the asphalt plant.

3. Sampling Program Procedures

Three particulate tests were conducted utilizing EPA Method 5 modified to meet PADEP requirements.

Three volatile compound tests were conducted utilizing EPA Method 25.

Three visible emission tests were conducted according to EPA Method 9.

The location and number of sampling ports and traverse points are detailed in Figure 1.

4. Results

Test data developed by the test runs, together with analytical results from the laboratory analysis of samples generated by the field sampling program, are reproduced in the Appendices included with this report. Information on basic gas characteristics developed by the test runs are located in the printouts included as Appendix V.

A summary of pertinent test results and essential information to evaluate test results are included within this report as Tables 1 and 2.

5. Discussion

5.1 Sampling Conditions

During the completion of this test program, there were a few interruptions in the operation of certain test trains.

During Test W-P-2, a ten minute delay occurred in the first port as a result of tripping a breaker which caused a power loss at the control console.

During Test W-V-2, there was a one hour, twenty-five minute delay owing to the clogging of the sample trap. This trap was subsequently replaced and the test resumed.

During Test W-V-3, there was a five minute delay to thaw the sample trap. Also, there was a one hour, twelve minute delay as a result of an operational stoppage at the asphalt plant.

5.2 Exhaust Flue Gas Volume and Composition

Test data for measurement of exhaust flue gas volume and related velocities developed by traversing of the stack show that the measured gas volumes during the tests were consistent with expected values. For the purposes of this report, indicated emissions are based on this measured gas volume.

5.3 Unit Operating Conditions

This sampling program was undertaken as a compliance test program for the drum mix asphalt plant exhaust. In the execution of this program, all applicable operating conditions were referenced. An attempt was made to operate the plant at normal conditions while producing a top coat utilizing recycled asphalt products in the mix. Operating conditions were monitored throughout the duration of the sampling program by Windsor Service personnel.

5.4 Emissions

The reported particulate emissions, as summarized in Table 1, are expressed as a concentration (gr/dscf) and an emission rate (lbs/hr) as measured. The reported volatile organic compound emissions as summarized in Table 2 are expressed as rate (lbs/hr) and (lbs/ton of asphalt produced) as measured. The reported visible emissions as summarized in Table 1 are expressed as opacity (percent).

SECTION III

APPENDICES

SECTION III - APPENDICES

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APPENDIX II
PROJECT PARTICIPANTS

APPENDIX I

PROJECT PARTICIPANTS

The following members of the G/C, Inc./UESC staff participated in the planning and execution of this project and the preparation of this report.

UESC Crew

George Albright	Senior Engineering Technician
Gary Helm	Air Quality Specialist
Eric Roland	Air Quality Specialist

Laboratory Participants

Vaughn O'Neill	SSM Laboratories
Wayne Stallings	Triangle Environmental Services

APPENDIX II
TESTING AND ANALYTICAL PROCEDURES

APPENDIX II
TESTING AND ANALYTICAL PROCEDURES

Particulate	Method 5
Visible	Method 9
Volatile Organic Compounds	Method 25

Methods appear in entirety in Title 40 of the Code of Federal Regulations (CFR), Part 60, Appendix A.

APPENDIX III
OPERATING DATA.

APPENDIX III
OPERATING DATA

- 3.1 October 21
- 3.2 October 22
- 3.3 October 23

APPENDIX III OPERATING DATA

3.1 October 21

CONCLUSIONS

44:00:49 10/21/92

2207281 3077 20770HS 0.204mc 3067 14.04BS 0.02522

[illegible]

50P	4.52
DE5	4.10
	4.34
BC7A	MEYERHOFF
" Q	
00	4.10

10,000	0.30 B
20,000	0.20 B

33:03394, 19731092

THE FIRST 33-67MS 0.20Ems 3068 (4.0Hz) - 0.00Ems

[illegible]

F	8.62
10000	4.29
100	4.24
10	8.62
0.1	
0.00	4.29

1. 0	0.27 B
2. 0	0.20 B

331.104537 10231.292

3 1728 312P 3400005 4.200000 302P 14.00000 0.00000

[illegible]

[illegible]

1.333333		
AL. 0.50F	0.52	
2. ADDED	4.62	
3.	4.15	
4.074	ENTERED	
5. 0		
6.36	4.62	
8. 10000	6.01 E	
9. 10000	6.00 E	

[illegible]

TOD:		
1. 4.60F	9.62	
AC ADDED	9.40	
	9.45	
BC11	SETBACK	
AC 4.4		
3.75	9.40	
2. (ACT)	4.75 M	
3. (REG)	4.50 M	

[illegible]

APPENDIX III OPERATING DATA

3.2 October 22

C HICK DC 0.0
 AC 0.43 4.36
 AC ACCUM. LAGSD 4.70 X
 AC ACCUM. CRGSD 4.00 X

RECOMMENDATION 70000 LOGS 100PLS 06-44-43 10022/92

F I D HICKO 2337PH 2977 152700S 4.0000mm 300P 14.0000 0.00000

	YIR	MAP	AC	BH01	BH02	BH03	BH04	BH05	BH07	BH11	BH12	DUST
DISBURSE	3.2	6.4		5.0	6.5	2.0	0.5	1.0	0.0	6.4		
PH RATE	209	24	10.3	40	49	0	0	136	0	23	4	9
ACEN	86.0	9.6	4.00	10.5	10.5	0.0	0.0	49.4	0.0	9.6	3.9	
ALPH	87.0	9.9	4.00	10.1	10.4	0.0	0.0	51.2	0.0	8.9	3.2	
NET TOTAL	137.3	13.6	6.01	30.2	31.0	0.0	0.0	90.6	0.0	13.9	5.7	0.0

Error=(BL01-0) (L02-0) (V0000-0) (B0000-0) (B0000-0) (B0000-0)

C STATISTICS:

AC 10/GAL P 60P 0.53
 AVERSED AC ADDED 4.43
 C TOTAL L 4.13
 BCT1 007000
 ACEN AC 4.0
 CR 0.42 4.43
 AC ACCUM. (ACT1) 4.00 X
 AC ACCUM. (CRG1) 4.00 X

RECOMMENDATION 70000 LOGS 100PLS 06-46-43 10022/92

F I D HICKO 2547PH 290P 173000S 4.5000mm 300P 14.0000 0.00000

	YIR	MAP	AC	BH01	BH02	BH03	BH04	BH05	BH07	BH11	BH12	DUST
DISBURSE	3.2	6.4		5.0	6.6	2.0	0.6	1.0	0.0	6.4		
PH RATE	206	25	11.2	40	60	0	0	120	0	29	9	6
ACEN	86.0	9.6	4.00	10.5	10.5	0.0	0.0	49.4	0.0	9.6	3.9	
ALPH	86.7	9.6	4.00	10.3	10.3	0.0	0.0	49.4	0.0	9.6	3.9	
NET TOTAL	155.0	12.7	7.22	30.3	31.4	0.0	0.0	95.5	0.0	12.9	6.0	0.0

Error=(BL01-0) (L02-0) (V0000-0) (B0000-0) (B0000-0) (B0000-0)

C STATISTICS:

AC 10/GAL P 60P 0.53
 AVERSED AC ADDED 4.00
 C TOTAL L 4.13
 BCT1 007000
 ACEN AC 4.0
 CR 0.39 4.40
 AC ACCUM. (ACT1) 4.00 X
 AC ACCUM. (CRG1) 4.00 X

RECOMMENDATION 70000 LOGS 100PLS 06-45-47 10022/92

F I D HICKO 2747PH 250P 190000S 4.5000mm 300P 10.0000 0.00000

	YIR	MAP	AC	BH01	BH02	BH03	BH04	BH05	BH07	BH11	BH12	DUST
DISBURSE	3.2	6.4		5.0	6.6	2.0	0.6	1.0	0.0	6.4		
PH RATE	315	26	11.0	31	30	0	0	103	0	36	9	6
ACEN	86.0	9.6	4.00	10.3	10.5	0.0	0.0	49.4	0.0	9.6	3.9	
ALPH	87.0	9.4	4.69	10.3	10.6	0.0	0.0	50.9	0.0	9.0	3.4	
NET TOTAL	173.9	12.9	8.66	30.5	30.6	0.0	0.0	106.9	0.0	30.3	2.3	0.0

Error=(BL01-0) (L02-0) (V0000-0) (B0000-0) (B0000-0) (B0000-0)

C STATISTICS:

PANEL AC	4.6	
AC	0.30	0.33
AC ASCHL. CRCT		4.71 E
AC ASCHL. CRGH		4.80 E

DECLASSIFICATION AUTHORITY DERIVED FROM:
FBI AUTOMATIC DECLASSIFICATION GUIDE
DATE 12-22-2011

[illegible]

C SPINDLES:			
AC 16/GAL P 60P	5.53		
EMERGED AC 60000	4.30		
C TOTAL X	4.14		
	ACM3	DEFERED	
C RECL AC	4.0		
E	0.43	4.38	
C ACCHL CACT		4.82	X
C ACCHL CREM		4.80	X

[illegible]

7.3. MEDICAL REPORTS 300P 239TCRS 4.503000 300P 14.000100 0.000201													
	REN	HYP	AGE	HEED	HEED2	HEED3	HEED4	HEED5	HEED6	HEED7	HEED8	HEED9	DOBT
RESUME	2.9	6.4		5.4	7.0	1.5	0.6	0.7	0.0	0.0	0.0	3.2	
1 DATE	21.6	26	11.0	50	51	0	0	233	0	0	35	9	10
REN	86.0	9.6	4.00	10.5	13.5	0.0	0.0	49.3	0.0	0.0	9.6	11.5	
HEED	86.7	9.7	4.00	10.7	13.9	0.0	0.0	49.0	0.0	0.0	9.7	11.5	
11 TOTAL	211.4	24.4	10.52	60.1	48.2	0.0	0.0	130.0	0.0	0.0	33.6	0.9	0.0
(Ren) (Hyp) (Age) (Heed) (Heed2) (Heed3) (Heed4) (Heed5) (Heed6) (Heed7) (Heed8) (Heed9) (DoBt)													

C STATISTICS:		
DEL. P. GOF	0.93	
DEL. AC. ADDED	0.43	
DEL. P.	0.35	
DEL. AC	0.01	REMOVED
DEL. P.	0.38	4.52
DEL. AC	0.00	4.00
DEL. P.	0.00	4.00

RECEIVED **TUESDAY** **MARCH 29**

	TER	RAP	CR	BLK	DEPT	DEPT	DEPT	DEPT	DEPT	DEPT	DEPT	DEPT	DEPT
2008	2.9	5.2		5.1	7.0	15.9	0.6	0.7	0.0	0.0	36.2		
DATE	229	26	12.3	94	53	0	0	140	0	0	27	10	7
0	06.0	9.6	4.00	10.5	10.5	0.0	0.0	49.0	0.0	0.0	9.6	3.5	
TE	06.7	9.7	4.00	10.9	10.9	0.0	0.0	49.0	0.0	0.0	9.7	3.9	
2008	231.2	26.6	11.63	92.5	92.7	0.0	0.0	142.0	0.0	0.0	26.0	9.7	0.0

E REEL AC 4.0
 GCR 0.36 4.30
 AC ACCUM. (ACT) 0.75 %
 AC ACCUM. (REG) 0.00 %

RECOMMENDATION 700MS 100MS 100MS 07:11:39 10/22/92

E I D REEL 279TPH 310P 205TURNS 0.004mm 300P 14.000L 0.00023

	VIR	RAP	ACC	BCH1	BCH2	BCH3	BCH4	BCH5	BCH6	BCH7	BCH8	DPFL	DUST
WIRESTONE	2.9	5.2		5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2		
TPH RATE	229	24	12.5	53	53	0	0	140	0	0	27	10	7
E REG	06.9	9.6	0.00	10.5	10.5	0.0	0.0	49.0	0.0	0.0	9.6	3.5	
E RATE	06.9	9.7	0.00	10.6	10.7	0.0	0.0	49.3	0.0	0.0	9.7	3.5	
ACT TOTAL	251.2	58.0	12.56	57.0	57.2	0.0	0.0	156.1	0.0	0.0	29.2	10.5	0.0

AC STATISTICS:
 AC Lb/GAL @ 50P 8.53
 FIBER AC ADDED 4.02
 AC TOTAL % 4.17
 BCHA DEFEND
 E REEL AC 4.0
 GCR 0.35 4.42
 AC ACCUM. (ACT) 4.70 %
 AC ACCUM. (REG) 4.00 %

RECOMMENDATION 700MS 100MS 100MS 07:15:39 10/22/92

E I D REEL 280TPH 301P 309TURNS 4.500mm 300P 14.000L 0.00021

	VIR	RAP	ACC	BCH1	BCH2	BCH3	BCH4	BCH5	BCH6	BCH7	BCH8	DPFL	DUST
WIRESTONE	2.9	5.2		5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2		
TPH RATE	226	25	12.4	54	53	0	0	142	0	0	27	10	12
E REG	06.9	9.6	0.00	10.5	10.5	0.0	0.0	49.0	0.0	0.0	9.6	3.5	
E RATE	06.7	9.6	0.00	10.4	10.6	0.0	0.0	49.3	0.0	0.0	9.6	3.5	
ACT TOTAL	271.2	31.0	12.70	54.5	53.7	0.0	0.0	166.2	0.0	0.0	31.9	11.4	0.0

AC STATISTICS:
 E Lb/GAL @ 50P 8.53
 FIBER AC ADDED 4.03
 AC TOTAL % 4.10
 BCHA DEFEND
 REEL AC 4.0
 GCR 0.36 4.43
 AC ACCUM. (ACT) 4.00 %
 AC ACCUM. (REG) 4.00 %

RECOMMENDATION 700MS 100MS 100MS 07:31:39 10/22/92

E I D REEL 280TPH 299P 332TURNS 4.500mm 300P 14.000L 0.00023

	VIR	RAP	ACC	BCH1	BCH2	BCH3	BCH4	BCH5	BCH6	BCH7	BCH8	DPFL	DUST
WIRESTONE	2.9	5.2		5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2		
TPH RATE	230	23	12.5	53	56	0	0	142	0	0	27	10	15
E REG	06.0	9.6	0.00	10.5	10.9	0.0	0.0	49.0	0.0	0.0	9.6	3.9	
E RATE	06.0	9.6	0.00	10.6	10.7	0.0	0.0	49.4	0.0	0.0	9.6	3.9	
ACT TOTAL	291.3	33.8	12.70	66.0	66.2	0.0	0.0	170.3	0.0	0.0	33.9	12.4	0.0

AC STATISTICS:
 E Lb/GAL @ 50P 8.53

RECOMMENDATION **FINDINGS** **ACTION** **DATE**

AC STATISTICS:	
AC TOTAL P GOF	0.93
BURGEN AC ADDED	0.46
AC TOTAL T	0.20
AC1	DEFERRED

DECLASSIFICATION AUTHORITY DERIVED FROM: 25X1, 25X2, 25X4, 25X5, 25X6, 25X7, 25X8, 25X9, 25Y1, 25Y2, 25Y3, 25Y4, 25Y5, 25Y6, 25Y7, 25Y8, 25Y9, 25Z1, 25Z2, 25Z3, 25Z4, 25Z5, 25Z6, 25Z7, 25Z8, 25Z9, 25Z10, 25Z11, 25Z12, 25Z13, 25Z14, 25Z15, 25Z16, 25Z17, 25Z18, 25Z19, 25Z20, 25Z21, 25Z22, 25Z23, 25Z24, 25Z25, 25Z26, 25Z27, 25Z28, 25Z29, 25Z30, 25Z31, 25Z32, 25Z33, 25Z34, 25Z35, 25Z36, 25Z37, 25Z38, 25Z39, 25Z40, 25Z41, 25Z42, 25Z43, 25Z44, 25Z45, 25Z46, 25Z47, 25Z48, 25Z49, 25Z50, 25Z51, 25Z52, 25Z53, 25Z54, 25Z55, 25Z56, 25Z57, 25Z58, 25Z59, 25Z60, 25Z61, 25Z62, 25Z63, 25Z64, 25Z65, 25Z66, 25Z67, 25Z68, 25Z69, 25Z70, 25Z71, 25Z72, 25Z73, 25Z74, 25Z75, 25Z76, 25Z77, 25Z78, 25Z79, 25Z80, 25Z81, 25Z82, 25Z83, 25Z84, 25Z85, 25Z86, 25Z87, 25Z88, 25Z89, 25Z90, 25Z91, 25Z92, 25Z93, 25Z94, 25Z95, 25Z96, 25Z97, 25Z98, 25Z99, 25Z100, 25Z101, 25Z102, 25Z103, 25Z104, 25Z105, 25Z106, 25Z107, 25Z108, 25Z109, 25Z110, 25Z111, 25Z112, 25Z113, 25Z114, 25Z115, 25Z116, 25Z117, 25Z118, 25Z119, 25Z120, 25Z121, 25Z122, 25Z123, 25Z124, 25Z125, 25Z126, 25Z127, 25Z128, 25Z129, 25Z130, 25Z131, 25Z132, 25Z133, 25Z134, 25Z135, 25Z136, 25Z137, 25Z138, 25Z139, 25Z140, 25Z141, 25Z142, 25Z143, 25Z144, 25Z145, 25Z146, 25Z147, 25Z148, 25Z149, 25Z150, 25Z151, 25Z152, 25Z153, 25Z154, 25Z155, 25Z156, 25Z157, 25Z158, 25Z159, 25Z160, 25Z161, 25Z162, 25Z163, 25Z164, 25Z165, 25Z166, 25Z167, 25Z168, 25Z169, 25Z170, 25Z171, 25Z172, 25Z173, 25Z174, 25Z175, 25Z176, 25Z177, 25Z178, 25Z179, 25Z180, 25Z181, 25Z182, 25Z183, 25Z184, 25Z185, 25Z186, 25Z187, 25Z188, 25Z189, 25Z190, 25Z191, 25Z192, 25Z193, 25Z194, 25Z195, 25Z196, 25Z197, 25Z198, 25Z199, 25Z200, 25Z201, 25Z202, 25Z203, 25Z204, 25Z205, 25Z206, 25Z207, 25Z208, 25Z209, 25Z210, 25Z211, 25Z212, 25Z213, 25Z214, 25Z215, 25Z216, 25Z217, 25Z218, 25Z219, 25Z220, 25Z221, 25Z222, 25Z223, 25Z224, 25Z225, 25Z226, 25Z227, 25Z228, 25Z229, 25Z230, 25Z231, 25Z232, 25Z233, 25Z234, 25Z235, 25Z236, 25Z237, 25Z238, 25Z239, 25Z240, 25Z241, 25Z242, 25Z243, 25Z244, 25Z245, 25Z246, 25Z247, 25Z248, 25Z249, 25Z250, 25Z251, 25Z252, 25Z253, 25Z254, 25Z255, 25Z256, 25Z257, 25Z258, 25Z259, 25Z260, 25Z261, 25Z262, 25Z263, 25Z264, 25Z265, 25Z266, 25Z267, 25Z268, 25Z269, 25Z270, 25Z271, 25Z272, 25Z273, 25Z274, 25Z275, 25Z276, 25Z277, 25Z278, 25Z279, 25Z280, 25Z281, 25Z282, 25Z283, 25Z284, 25Z285, 25Z286, 25Z287, 25Z288, 25Z289, 25Z290, 25Z291, 25Z292, 25Z293, 25Z294, 25Z295, 25Z296, 25Z297, 25Z298, 25Z299, 25Z300, 25Z301, 25Z302, 25Z303, 25Z304, 25Z305, 25Z306, 25Z307, 25Z308, 25Z309, 25Z310, 25Z311, 25Z312, 25Z313, 25Z314, 25Z315, 25Z316, 25Z317, 25Z318, 25Z319, 25Z320, 25Z321, 25Z322, 25Z323, 25Z324, 25Z325, 25Z326, 25Z327, 25Z328, 25Z329, 25Z330, 25Z331, 25Z332, 25Z333, 25Z334, 25Z335, 25Z336, 25Z337, 25Z338, 25Z339, 25Z340, 25Z341, 25Z342, 25Z343, 25Z344, 25Z345, 25Z346, 25Z347, 25Z348, 25Z349, 25Z350, 25Z351, 25Z352, 25Z353, 25Z354, 25Z355, 25Z356, 25Z357, 25Z358, 25Z359, 25Z360, 25Z361, 25Z362, 25Z363, 25Z364, 25Z365, 25Z366, 25Z367, 25Z368, 25Z369, 25Z370, 25Z371, 25Z372, 25Z373, 25Z374, 25Z375, 25Z376, 25Z377, 25Z378, 25Z379, 25Z380, 25Z381, 25Z382, 25Z383, 25Z384, 25Z385, 25Z386, 25Z387, 25Z388, 25Z389, 25Z390, 25Z391, 25Z392, 25Z393, 25Z394, 25Z395, 25Z396, 25Z397, 25Z398, 25Z399, 25Z400, 25Z401, 25Z402, 25Z403, 25Z404, 25Z405, 25Z406, 25Z407, 25Z408, 25Z409, 25Z410, 25Z411, 25Z412, 25Z413, 25Z414, 25Z415, 25Z416, 25Z417, 25Z418, 25Z419, 25Z420, 25Z421, 25Z422, 25Z423, 25Z424, 25Z425, 25Z426, 25Z427, 25Z428, 25Z429, 25Z430, 25Z431, 25Z432, 25Z433, 25Z434, 25Z435, 25Z436, 25Z437, 25Z438, 25Z439, 25Z440, 25Z441, 25Z442, 25Z443, 25Z444, 25Z445, 25Z446, 25Z447, 25Z448, 25Z449, 25Z450, 25Z451, 25Z452, 25Z453, 25Z454, 25Z455, 25Z456, 25Z457, 25Z458, 25Z459, 25Z460, 25Z461, 25Z462, 25Z463, 25Z464, 25Z465, 25Z466, 25Z467, 25Z468, 25Z469, 25Z470, 25Z471, 25Z472, 25Z473, 25Z474, 25Z475, 25Z476, 25Z477, 25Z478, 25Z479, 25Z480, 25Z481, 25Z482, 25Z483, 25Z484, 25Z485, 25Z486, 25Z487, 25Z488, 25Z489, 25Z490, 25Z491, 25Z492, 25Z493, 25Z494, 25Z495, 25Z496, 25Z497, 25Z498, 25Z499, 25Z500, 25Z501, 25Z502, 25Z503, 25Z504, 25Z505, 25Z506, 25Z507, 25Z50

AC STATISTICS:	
AC LOGAL, 0 GDP	4.53
SYNTHESIS AC ADDED	4.35
AC TOTAL, %	4.20
	REMA
	DELETED

RECORDED INDEXED
JUN 10 1968
U.S. DEPT. OF JUSTICE
FBI - NEW YORK

NY 100-374244

[illegible]

11. 10000	4.00	4
11. 10000	4.00	4

FROM: 78000 100700 100710 07 14 1979 0000221/93

1	2	3	4	5	6	7	8	9	10	11	12	13	14
1000	2000	3000	4000	5000	6000	7000	8000	9000	10000	11000	12000	13000	14000
1500	2500	3500	4500	5500	6500	7500	8500	9500	10500	11500	12500	13500	14500
1600	2600	3600	4600	5600	6600	7600	8600	9600	10600	11600	12600	13600	14600
1700	2700	3700	4700	5700	6700	7700	8700	9700	10700	11700	12700	13700	14700
1800	2800	3800	4800	5800	6800	7800	8800	9800	10800	11800	12800	13800	14800
1900	2900	3900	4900	5900	6900	7900	8900	9900	10900	11900	12900	13900	14900
2000	3000	4000	5000	6000	7000	8000	9000	10000	11000	12000	13000	14000	15000
2100	3100	4100	5100	6100	7100	8100	9100	10100	11100	12100	13100	14100	15100
2200	3200	4200	5200	6200	7200	8200	9200	10200	11200	12200	13200	14200	15200
2300	3300	4300	5300	6300	7300	8300	9300	10300	11300	12300	13300	14300	15300
2400	3400	4400	5400	6400	7400	8400	9400	10400	11400	12400	13400	14400	15400
2500	3500	4500	5500	6500	7500	8500	9500	10500	11500	12500	13500	14500	15500
2600	3600	4600	5600	6600	7600	8600	9600	10600	11600	12600	13600	14600	15600
2700	3700	4700	5700	6700	7700	8700	9700	10700	11700	12700	13700	14700	15700
2800	3800	4800	5800	6800	7800	8800	9800	10800	11800	12800	13800	14800	15800
2900	3900	4900	5900	6900	7900	8900	9900	10900	11900	12900	13900	14900	15900
3000	4000	5000	6000	7000	8000	9000	10000	11000	12000	13000	14000	15000	16000
3100	4100	5100	6100	7100	8100	9100	10100	11100	12100	13100	14100	15100	16100
3200	4200	5200	6200	7200	8200	9200	10200	11200	12200	13200	14200	15200	16200
3300	4300	5300	6300	7300	8300	9300	10300	11300	12300	13300	14300	15300	16300
3400	4400	5400	6400	7400	8400	9400	10400	11400	12400	13400	14400	15400	16400
3500	4500	5500	6500	7500	8500	9500	10500	11500	12500	13500	14500	15500	16500
3600	4600	5600	6600	7600	8600	9600	10600	11600	12600	13600	14600	15600	16600
3700	4700	5700	6700	7700	8700	9700	10700	11700	12700	13700	14700	15700	16700
3800	4800	5800	6800	7800	8800	9800	10800	11800	12800	13800	14800	15800	16800
3900	4900	5900	6900	7900	8900	9900	10900	11900	12900	13900	14900	15900	16900
4000	5000	6000	7000	8000	9000	10000	11000	12000	13000	14000	15000	16000	17000
4100	5100	6100	7100	8100	9100	10100	11100	12100	13100	14100	15100	16100	17100
4200	5200	6200	7200	8200	9200	10200	11200	12200	13200	14200	1520		

ESTIMATE		
AL	F 505	5.55
AL	ADDED	6.43
		6.23
	REVL	RETURNED
AG	6.0	
	6.43	4.42

1. 10000	4.00	1
2. 10000	4.00	1

 FROM: SAC, NEW YORK (100-158541) (P)
 TO: DIRECTOR, FBI (100-442600) (P)
 SUBJECT: MURDER OF MARTIN LUTHER KING, JR.;
 RE: NEW YORK TELETYPE TO BUREAU, APRIL TWENTY, LAST.

	(1) 367°F	(2) 900°C	(3) 300°F	(4) 150°C	(5) 300°F	(6) 150°C	(7) 300°F	(8) 150°C	(9) 300°F	(10) 150°C	(11) 300°F	(12) 150°C	(13) 300°F	(14) 150°C
YR	3.9	0.0	5.5	7.0	1.9	0.5	0.7	0.0	0.0	0.0	5.3	0.0	0.0	0.0
TR	26.1	0	16.9	76	76	120	0	0	0	0	0	7	10	10
GR	37.5	0.0	5.00	35.6	26.6	40.3	0.0	0.0	0.0	0.0	0.0	3.5	0.0	0.0
BR	37.5	0.0	5.00	35.9	26.6	40.4	0.0	0.0	0.0	0.0	0.0	3.4	0.0	0.0
OR	393.5	43.5	20.06	49.9	90.1	5.3	0.0	229.3	0.0	0.0	46.4	16.6	0.0	0.0
	(1) 367°F	(2) 900°C	(3) 300°F	(4) 150°C	(5) 300°F	(6) 150°C	(7) 300°F	(8) 150°C	(9) 300°F	(10) 150°C	(11) 300°F	(12) 150°C	(13) 300°F	(14) 150°C

9.50F	4.53
C. ADDED	2.06
8.	4.23
SCYR	DESTRUCED
4.0	
4.00	5.56

(ACT)	5,96%
(BEG)	9,00%

FROM: DIRECTOR, FBI
TO: SAC, NEW YORK
SUBJECT: [REDACTED]
[REDACTED]

[illegible]

1064
4-10-1964

[illegible][illegible]

AC TOTAL P GDP	5.53
CHARGED AC ADDED	5.04
AC TOTAL L	6.39
DCFL	REMOVED
P RECL AC	9.0
CG	0.00
AC ACCUM. LAGG	5.04
AC ACCUM. CHRG	

[illegible]

1. 100/GAL. OF GWP	0.93	
2. SWEEPER AC ASSESS	5.88	
AC TYPICAL 1"	9.42	
	NET	NETTERED
3. 100/GAL. OF GWP	4.50	
NET	0.00	5.88
4. 100/GAL. OF GWP		
5. 100/GAL. OF GWP		

	VEN	RAP	CHOCOL	CHOCOL	CHOCOL	CHOCOL	CHOCOL	CHOCOL	CHOCOL	CHOCOL	CHOCOL	CHOCOL	CHOCOL
CONSUMER	3.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
VEN RATE	256	3	16.76	77	79	126	0	0	0	0	0	0	0
RND	97.5	0.0	5.00	26.6	26.5	46.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
RACE	97.4	0.0	5.00	27.0	26.6	46.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
SAT TOTAL	400.1	43.5	23.62	113.9	113.7	201.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0

ACKNOWLEDGMENTS

9.04 36
9.00 36

004-63890 106721992

TR	MAP	ACC	ACC1	ACC2	ACC3	ACC4	ACC5	ACC6	ACC7	ACC8	ACC9	ACC10
30.9	0.0	5.1	7.0	1.5	0.6	0.7	0.0	0.0	0.0	5.2	0.0	0.0
35.1	0	16.9	75	75	129	0	0	0	0	0	7	7
97.9	0.0	5.00	26.5	35.6	44.3	0.0	0.0	0.0	0.0	0.0	2.9	
97.4	0.0	5.00	26.5	35.7	44.1	0.0	0.0	0.0	0.0	0.0	2.9	
506.7	43.5	37.03	123.9	123.3	63.6	0.0	229.3	0.0	0.0	46.4	19.4	0.0

AC. ACCUM. CHRGD 3.00 11

004.146338 200722.932

VEH	HAZ	AGE	CHRM	DEGR	DEGR	DEGR	DEGR	DEGR	DEGR	DEGR	DEGR	DEGR
36.9	0.0		36.1	7.0	1.9	0.6	0.7	0.0	0.0	0.3	0.0	0.0
363	0	146.6	77	76	137	0	0	0	0	0	0	0
997.9	0.0	9.00	36.6	36.6	46.1	0.0	0.0	0.0	0.0	0.0	3.9	
997.9	0.0	5.67	36.7	36.5	46.1	0.0	0.0	0.0	0.0	0.0	3.9	
339.4	43.9	30.39	330.1	130.6	93.1	0.0	330.3	0.0	0.0	44.0	30.0	0.0

16	ACCUPL	CHBBS	3.00	12
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Publication program

Q320	Q319	Q318	Q317	Q316	Q315	Q314	Q313	Q312	Q311	Q310	Q309	Q308
36.9	0.0	36.1	7.0	1.9	0.6	0.9	0.9	0.0	36.3	000.0	0000	
390	0	106.3	706	746	1329	0	0	0	0	7	630	
997.9	0.0	36.00	306.6	306.6	40.3	0.0	0.0	0.0	0.0	36.9		
997.9	0.0	36.00	306.7	306.7	40.0	0.0	0.0	0.0	0.0	36.9		
995.9	936.3	306.700	3306.7	1306.0	002.9	0.0	339.3	0.0	0.0	306.0	306.0	0.0

DE SPONTANEO:

3.000 0

DISSEMINATION

700000 100000 100000

00000000 00000000

P 1 0 00000 000000 0000 000000 000000 000000 000000 000000 000000 000000 000000 000000 000000

	000	000	000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
0000000	3.9	0.0		5.1	7.0	2.5	0.5	0.7	0.0	0.0	5.2		
TPH RATE	259	0	15.4	75	75	139	0	0	0	0	5.2		
1 000	55.0	9.5	4.00	10.5	10.5	0.0	0.0	0.0	0.0	0.0	0	7	6
2 000	97.7	0.0	5.00	23.3	23.3	37.1	0.0	13.4	0.0	0.0	9.6	3.5	
NET TOTAL	570.6	93.5	31.12	102.1	101.4	93.5	0.0	329.3	0.0	0.0	46.4	23.2	0.0
Estimate (0000 0) (0000 0) (0000 0) (0000 0) (0000 0) (0000 0) (0000 0) (0000 0)													

AC STATISTICS:

AC 00000 0 000	5.93
OVERSEEN AC 00000	5.75
AC TOTAL 0	4.50
00000	000000
0 0000 AC	4.0
AC0	0.00 5.75
AC 00000 (ACT)	5.75 0
AC 00000 (REG)	0.00 0

DISSEMINATION

700000 100000 100000

00000000 00000000

P 1 0 00000 000000 0000 000000 000000 000000 000000 000000 000000 000000 000000 000000

	000	000	000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
0000000	2.9	5.2		5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2		
TPH RATE	233	35	12.3	53	54	0	0	140	0	0	5.2		
1 000	55.0	9.5	0.00	10.5	10.5	0.0	0.0	49.8	0.0	0.0	9.6	3.5	
2 000	97.0	0.4	0.00	20.1	10.4	0.0	0.0	50.6	0.0	0.0	9.0	3.4	
NET TOTAL	250.4	95.1	32.35	101.7	101.9	93.5	0.0	241.6	0.0	0.0	46.4	23.0	0.0
Estimate (0000 0) (0000 0) (0000 0) (0000 0) (0000 0) (0000 0) (0000 0) (0000 0)													

AC STATISTICS:

AC 00000 0 000	0.93
OVERSEEN AC 00000	0.36
AC TOTAL 0	0.65
00000	000000
0 0000 AC	0.0
AC0	0.35 4.36
AC 00000 (ACT)	4.76 0
AC 00000 (REG)	4.00 0

DISSEMINATION

700000 100000 100000

00000000 00000000

P 1 0 00000 000000 0000 000000 000000 000000 000000 000000 000000 000000 000000 000000

	000	000	000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
0000000	3.9	5.1		5.1	7.0	0.5	0.6	0.7	0.0	0.0	5.2		
TPH RATE	233	30	12.6	53	53	0	0	140	0	0	5.2		
1 000	55.0	9.5	0.00	10.5	10.5	0.0	0.0	49.8	0.0	0.0	9.6	3.5	
2 000	96.9	0.3	0.00	10.2	10.6	0.0	0.0	50.3	0.0	0.0	9.0	3.4	
NET TOTAL	613.1	95.5	30.30	101.2	101.6	90.9	0.0	233.7	0.0	0.0	46.4	23.0	0.0
Estimate (0000 0) (0000 0) (0000 0) (0000 0) (0000 0) (0000 0) (0000 0) (0000 0)													

AC STATISTICS:

AC 00000 0 000	0.93
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1. *Phragmites australis* (Cav.) Trin. ex Steud.

ECL AC 4.0
 0.39 4.39
 ACCR. (ACT) 4.73 1
 ACCR. (REG) 4.80 1

CREATION 70000 10000 10000 00:57:00 10/22/92

1 5 00000 20000 2000 1000000 4.800000 3000 14.00000 0.00000

	YIB	RAP	AC	BIB1	BIB2	BIB3	BIB4	BIB5	BIB6	BIB7	BIB8	BIB9	BIB10	BIB11	BIB12
STARS	2.9	5.2		5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2				
DATE	235	29	12.6	53	53	0	0	145	0	0	27	10	5		
SE	56.8	9.6	4.80	18.5	18.5	0.0	0.0	49.8	0.0	0.0	9.6	3.5			
CE	56.8	9.6	4.80	18.4	18.3	0.0	0.0	50.1	0.0	0.0	9.5	3.4			
TOTAL	568.7	57.1	37.52	168.2	168.4	93.5	0.0	382.1	0.0	0.0	57.8	35.2	0.0		

(BIB1) (ACT) (VOCAL) (BIB1) (BIB2) (BIB3) (BIB4) (BIB5) (BIB6) (BIB7) (BIB8) (BIB9) (BIB10) (BIB11) (BIB12)

INVESTIG:

SAL P 60F 0.53
 AC ADDED 0.30
 TOTAL 4.60
 ACT1 DEFERRED
 ECL AC 4.0
 0.40 4.40
 ACCR. (ACT) 4.70 1
 ACCR. (REG) 4.80 1

CREATION

70000 10000 10000

09:02:30 10/22/92

1 5 00000 2000 1000000 4.800000 3000 14.00000 0.00000

	YIB	RAP	AC	BIB1	BIB2	BIB3	BIB4	BIB5	BIB6	BIB7	BIB8	BIB9	BIB10	BIB11	BIB12
STARS	2.9	5.2		5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2				
DATE	235	29	12.6	53	53	0	0	145	0	0	27	10	5		
SE	56.8	9.6	4.80	18.5	18.5	0.0	0.0	49.8	0.0	0.0	9.6	3.5			
CE	56.8	9.6	4.80	18.4	18.3	0.0	0.0	50.1	0.0	0.0	9.6	3.5			
TOTAL	568.9	56.5	38.51	172.7	172.9	93.5	0.0	384.2	0.0	0.0	60.3	37.1	0.0		

(BIB1)

(ACT)

(VOCAL)

(BIB1)

(BIB2)

(BIB3)

(BIB4)

(BIB5)

(BIB6)

(BIB7)

(BIB8)

(BIB9)

(BIB10)

(BIB11)

(BIB12)

INVESTIG:

SAL P 60F 0.53
 AC ADDED 0.42
 TOTAL 0.59
 ACT1 DEFERRED
 ECL AC 4.0
 0.41 4.41
 ACCR. (ACT) 4.83 1
 ACCR. (REG) 4.80 1

CREATION

70000 10000 10000

09:07:32 10/22/92

1 5 00000 2000 1000000 0.000000 3000 14.00000 0.00000

	YIB	RAP	AC	BIB1	BIB2	BIB3	BIB4	BIB5	BIB6	BIB7	BIB8	BIB9	BIB10	BIB11	BIB12
STARS	2.9	5.2		5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2				
DATE	226	29	12.4	53	53	0	0	143	0	0	27	10	11		
SE	56.8	9.6	4.80	18.5	18.5	0.0	0.0	49.8	0.0	0.0	9.6	3.5			
CE	56.8	9.6	4.80	18.5	18.6	0.0	0.0	49.6	0.0	0.0	9.6	3.5			
TOTAL	736.0	62.0	39.66	177.2	177.4	93.5	0.0	386.6	0.0	0.0	62.4	37.9	0.0		

(BIB1) (ACT) (VOCAL) (BIB1) (BIB2) (BIB3) (BIB4) (BIB5) (BIB6) (BIB7) (BIB8) (BIB9) (BIB10) (BIB11) (BIB12)

INVESTIG:

8 REEL AC 4.0
 ACS 0.62 4.42
 AC ACCUM. (ACT) 4.44 %
 AC ACCUM. (ERR) 4.00 %

RECORDATION

700US 100TS 100LS

09:12:14 30/22/92

P 1 0 00000 201TPH 280F 204TCMS 4.900000 300F 14.00000 0.00000

	YEN	REP	ACC	REEL	REEL	REEL	REEL	REEL	REEL	REEL	REEL	REEL	REEL
REELTIME	3.9	5.2		5.1	7.0	1.5	0.5	0.7	0.0	0.0	0.0	0.0	0.0
TPH RATE	235	20	12.4	53	53	0	0	143	0	0	0	27	4
E RSD	06.8	9.6	4.80	18.5	18.5	0.0	0.0	49.0	0.0	0.0	0.0	9.6	3.5
E RATE	06.8	9.6	4.80	18.4	18.5	0.0	0.0	49.0	0.0	0.0	0.0	9.6	3.5
REP TOTAL	756.1	64.9	60.70	111.7	182.9	93.5	0.0	356.5	0.0	0.0	0.0	54.8	20.9

AC STATISTICS:

AC 15/60 P 60P 0.53
 LENGTH AC ADDED 4.43
 AC TOTAL 1 4.97
 REEL 1 REPEATED
 8 REEL AC 4.0
 ACS 0.39 4.43
 AC ACCUM. (ACT) 4.43 %
 AC ACCUM. (ERR) 4.00 %

RECORDATION

700US 100TS 100LS

09:37:36 30/22/92

P 1 0 00000 279TPH 290F 220TCMS 4.800000 300F 14.00000 0.00000

	YEN	REP	ACC	REEL	REEL	REEL	REEL	REEL	REEL	REEL	REEL	REEL	REEL
REELTIME	3.9	5.2		5.1	7.0	1.5	0.6	0.7	0.0	0.0	0.0	0.0	0.0
TPH RATE	330	29	12.3	53	53	0	0	145	0	0	0	27	9
E RSD	06.8	9.6	4.80	18.5	18.5	0.0	0.0	49.0	0.0	0.0	0.0	9.6	3.5
E RATE	06.9	9.5	4.80	18.4	18.5	0.0	0.0	49.9	0.0	0.0	0.0	9.5	3.4
REP TOTAL	776.1	66.7	61.70	106.1	186.4	93.9	0.0	350.6	0.0	0.0	0.0	67.1	29.6

AC STATISTICS:

AC 15/60 P 60P 0.53
 LENGTH AC ADDED 4.43
 AC TOTAL 1 0.56
 REEL 1 REPEATED
 8 REEL AC 4.0
 ACS 0.41 4.42
 AC ACCUM. (ACT) 4.40 %
 AC ACCUM. (ERR) 4.00 %

RECORDATION

700US 100TS 100LS

09:52:10 30/22/92

P 1 0 00000 203TPH 292F 233TCMS 4.800000 300F 14.00000 0.00000

	YEN	REP	ACC	REEL	REEL	REEL	REEL	REEL	REEL	REEL	REEL	REEL	REEL
REELTIME	3.9	5.2		5.1	7.0	1.5	0.6	0.7	0.0	0.0	0.0	0.0	0.0
TPH RATE	229	27	12.6	53	53	0	0	146	0	0	0	27	11
E RSD	06.8	9.6	4.80	18.5	18.5	0.0	0.0	49.0	0.0	0.0	0.0	9.6	3.5
E RATE	06.9	9.5	4.80	18.3	18.3	0.0	0.0	50.6	0.0	0.0	0.0	9.5	3.4
REP TOTAL	796.3	69.1	62.70	100.7	190.9	93.5	0.0	362.7	0.0	0.0	0.0	63.6	30.9

AC STATISTICS:

AC INCL AC 4.0
ACR 0.30 4.00
AC ACCUM. (ACT) 4.00 T
AC ACCUM. (REQ) 4.00 T

RECORDATION 702NS 10CT5 10PL5 09/27/92 10/23/92

P L D 00000 2757PH 290F 2757005 4.000mc 307F (4.0000) 0.00000

	VER	RAP	AC	0001	0002	0003	0004	0005	0006	0007	0008	0009	0010
0001000	2.9	5.2		5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2		
TPH RATE	232	27	12.4	53	50	0	0	146	0	0	37	10	4
1 REQ	06.3	9.5	4.00	13.5	10.5	0.0	0.0	49.3	0.0	0.0	9.6	3.5	
2 RATE	06.5	9.5	4.00	13.3	10.4	0.0	0.0	50.2	0.0	0.0	9.6	3.4	
NET TOTAL	026.3	71.4	63.82	195.2	195.4	93.5	0.0	394.0	0.0	0.0	71.0	33.3	0.0

Errors: (Data 0) (LTC 0) (Vocals 0) (Rucals 0) (Sylburs 0) (Durs 0)

AC STATISTICS:
AC 10/60L P 60F 0.53
AVERGED AC 0000 0.45
AC TOTAL 1 0.55
ACT1 DEFERED
1 REQ. AC 4.0
ACR 0.30 4.45
AC ACCUM. (ACT) 4.35 T
AC ACCUM. (REQ) 4.50 T

RECORDATION 702NS 10CT5 10PL5 09/28/92 10/23/92

P L D 00000 2757PH 292F 2757005 4.000mc 307F (4.0000) 0.00000

	VER	RAP	AC	0001	0002	0003	0004	0005	0006	0007	0008	0009	0010
0001000	2.9	5.2		5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2		
TPH RATE	230	26	12.3	54	56	0	0	143	0	0	37	10	10
1 REQ	06.0	9.6	4.00	10.5	13.9	0.0	0.0	49.3	0.0	0.0	9.6	3.5	
2 RATE	06.0	9.6	4.00	10.7	13.9	0.0	0.0	49.3	0.0	0.0	9.6	3.5	
NET TOTAL	036.4	73.6	44.06	199.7	199.9	93.5	0.0	386.9	0.0	0.0	70.1	33.3	0.0

Errors: (Data 0) (LTC 0) (Vocals 0) (Rucals 0) (Sylburs 0) (Durs 0)

AC STATISTICS:
AC 10/60L 0 60F 0.53
AVERGED AC 0000 4.07
AC TOTAL 2 4.54
ACT1 DEFERED
1 REQ. AC 4.0
ACR 0.30 4.47
AC ACCUM. (ACT) 0.05 T
AC ACCUM. (REQ) 0.00 T

RECORDATION 702NS 10CT5 10PL5 09/30/92 10/23/92

P L D 00000 2757PH 291F 07005 5.400mc 307F (4.0000) 0.00000

	VER	RAP	AC	0001	0002	0003	0004	0005	0006	0007	0008	0009	0010
0001000	3.9	0.0		5.1	7.0	1.9	0.6	0.7	0.0	0.0	3.2		
TPH RATE	299	1	10.1	77	76	130	0	0	0	0	0	0	83
1 REQ	97.3	0.0	5.00	26.6	26.6	00.3	0.0	0.0	0.0	0.0	0.0	3.9	
2 RATE	97.3	0.0	5.00	26.9	26.3	00.3	0.0	0.0	0.0	0.0	0.0	3.9	
NET TOTAL	057.9	95.7	01.00	203.0	203.3	50.3	0.0	393.6	0.0	0.0	70.1	30.0	0.0

Errors: (Data 0) (LTC 0) (Vocals 0) (Rucals 0) (Sylburs 0) (Durs 0)

AC STATISTICS:

RECORDATION

AC RECL AC 4.0
AC 0.00 5.67
AC ACCUM (ACT) 5.67 E
AC ACCUM (RECL) 5.00 E

RECORDATION

7000S 1000S 1000S

09/03/92 10/22/92

P 1 0 0000 20000 2000 2000 5.000000 2000 14.00000 0.000000

	VER	RAP	AC	B101	B102	B103	B104	B105	B106	B107	B108	B109	B110
DOISTONE	3.9	0.0	5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2	0.0	0.0	0.0
TPH RATE	250	0	15.5	74	75	125	0	0	0	0	0	0	0
E REG	97.5	0.0	5.00	26.5	26.6	44.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
E RATE	97.5	0.0	5.00	26.5	26.6	44.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NET TOTAL	850.4	75.7	47.32	211.4	211.6	300.7	0.0	393.6	0.0	0.0	75.1	33.6	0.0

Errors: (Chan 0) (AC 0) (Vocals 0) (Bucala 0) (Driver 0) (Dang 0)

AC STATISTICS:

AC 10/000 0 500 0.53
SYNCHRON AC 10000 5.67
AC TOTAL 2 4.56
RECL 0.000000

E RECL AC 4.0
AC 0.00 5.67
AC ACCUM (ACT) 5.67 E
AC ACCUM (RECL) 5.00 E

RECORDATION

7000S 1000S 1000S

09/03/92 10/22/92

P 1 0 0000 20000 2000 2000 5.000000 2000 14.00000 0.000000

	VER	RAP	AC	B101	B102	B103	B104	B105	B106	B107	B108	B109	B110
DOISTONE	3.9	0.0	5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2	0.0	0.0	0.0
TPH RATE	250	0	15.5	74	75	125	0	0	0	0	0	0	0
E REG	97.5	0.0	5.00	26.5	26.6	44.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
E RATE	97.5	0.0	5.00	26.5	26.6	44.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NET TOTAL	850.4	75.7	47.32	211.4	211.6	300.7	0.0	393.6	0.0	0.0	75.1	33.6	0.0

Errors: (Chan 0) (AC 0) (Vocals 0) (Bucala 0) (Driver 0) (Dang 0)

AC STATISTICS:

AC 10/000 0 500 0.53
SYNCHRON AC 10000 5.67
AC TOTAL 2 4.56
RECL 0.000000

E RECL AC 4.0
AC 0.00 5.67
AC ACCUM (ACT) 5.67 E
AC ACCUM (RECL) 5.00 E

RECORDATION

7000S 1000S 1000S

09/03/92 10/22/92

P 1 0 0000 20000 2000 2000 5.000000 2000 14.00000 0.000000

	VER	RAP	AC	B101	B102	B103	B104	B105	B106	B107	B108	B109	B110
DOISTONE	3.9	0.0	5.1	7.0	1.5	0.6	0.7	0.0	0.0	5.2	0.0	0.0	0.0
TPH RATE	250	0	15.5	74	75	125	0	0	0	0	0	0	0
E REG	97.5	0.0	5.00	26.5	26.6	44.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
E RATE	97.5	0.0	5.00	26.5	26.6	44.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NET TOTAL	850.4	75.7	47.32	211.4	211.6	300.7	0.0	393.6	0.0	0.0	75.1	33.6	0.0

Errors: (Chan 0) (AC 0) (Vocals 0) (Bucala 0) (Driver 0) (Dang 0)

AC STATISTICS:

[illegible]

AC ACCBL. GREEN	5.00	1
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10412839 10722932

[illegible]

AC TOTAL, \$	6.69
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AC ACCRUAL, CHARGE	3.00
--------------------	------

108.174.02 20032.962

store=(Name: 0) (Age: 0) (Gender: 0) (Occupation: 0) (Married: 0) (Divorced: 0) (Widowed: 0) (Single: 0)

HC TSPAL, 3 4.29

7. ACCUM. & RESER.	4,000	1.
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10023140 10023143

Category	Count	Percentage
1. General	10	10.0%
2. Specific	20	20.0%
3. Other	30	30.0%
4. Unknown	40	40.0%
5. Total	100	100.0%

1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. 32. 33. 34. 35. 36. 37. 38. 39. 40. 41. 42. 43. 44. 45. 46. 47. 48. 49. 50. 51. 52. 53. 54. 55. 56. 57. 58. 59. 60. 61. 62. 63. 64. 65. 66. 67. 68. 69. 70. 71. 72. 73. 74. 75. 76. 77. 78. 79. 80. 81. 82. 83. 84. 85. 86. 87. 88. 89. 90. 91. 92. 93. 94. 95. 96. 97. 98. 99. 100. 101. 102. 103. 104. 105. 106. 107. 108. 109. 110. 111. 112. 113. 114. 115. 116. 117. 118. 119. 120. 121. 122. 123. 124. 125. 126. 127. 128. 129. 130. 131. 132. 133. 134. 135. 136. 137. 138. 139. 140. 141. 142. 143. 144. 145. 146. 147. 148. 149. 150. 151. 152. 153. 154. 155. 156. 157. 158. 159. 160. 161. 162. 163. 164. 165. 166. 167. 168. 169. 170. 171. 172. 173. 174. 175. 176. 177. 178. 179. 180. 181. 182. 183. 184. 185. 186. 187. 188. 189. 190. 191. 192. 193. 194. 195. 196. 197. 198. 199. 200. 201. 202. 203. 204. 205. 206. 207. 208. 209. 210. 211. 212. 213. 214. 215. 216. 217. 218. 219. 220. 221. 222. 223. 224. 225. 226. 227. 228. 229. 230. 231. 232. 233. 234. 235. 236. 237. 238. 239. 240. 241. 242. 243. 244. 245. 246. 247. 248. 249. 250. 251. 252. 253. 254. 255. 256. 257. 258. 259. 260. 261. 262. 263. 264. 265. 266. 267. 268. 269. 270. 271. 272. 273. 274. 275. 276. 277. 278. 279. 280. 281. 282. 283. 284. 285. 286. 287. 288. 289. 290. 291. 292. 293. 294. 295. 296. 297. 298. 299. 300. 301. 302. 303. 304. 305. 306. 307. 308. 309. 310. 311. 312. 313. 314. 315. 316. 317. 318. 319. 320. 321. 322. 323. 324. 325. 326. 327. 328. 329. 330. 331. 332. 333. 334. 335. 336. 337. 338. 339. 340. 341. 342. 343. 344. 345. 346. 347. 348. 349. 350. 351. 352. 353. 354. 355. 356. 357. 358. 359. 360. 361. 362. 363. 364. 365. 366. 367. 368. 369. 370. 371. 372. 373. 374. 375. 376. 377. 378. 379. 380. 381. 382. 383. 384. 385. 386. 387. 388. 389. 390. 391. 392. 393. 394. 395. 396. 397. 398. 399. 400. 401. 402. 403. 404. 405. 406. 407. 408. 409. 410. 411. 412. 413. 414. 415. 416. 417. 418. 419. 420. 421. 422. 423. 424. 425. 426. 427. 428. 429. 430. 431. 432. 433. 434. 435. 436. 437. 438. 439. 440. 441. 442. 443. 444. 445. 446. 447. 448. 449. 450. 451. 452. 453. 454. 455. 456. 457. 458. 459. 460. 461. 462. 463. 464. 465. 466. 467. 468. 469. 470. 471. 472. 473. 474. 475. 476. 477. 478. 479. 480. 481. 482. 483. 484. 485. 486. 487. 488. 489. 490. 491. 492. 493. 494. 495. 496. 497. 498. 499. 500. 501. 502. 503. 504. 505. 506. 507. 508. 509. 510. 511. 512. 513. 514. 515. 516. 517. 518. 519. 520. 521. 522. 523. 524. 525. 526. 527. 528. 529. 530. 531. 532. 533. 534. 535. 536. 537. 538. 539. 540. 541. 542. 543. 544. 545. 546. 547. 548. 549. 550. 551. 552. 553. 554. 555. 556. 557. 558. 559. 560. 561. 562. 563. 564. 565. 566. 567. 568. 569. 570. 571. 572. 573. 574. 575. 576. 577. 578. 579. 580. 581. 582. 583. 584. 585. 586. 587. 588. 589. 590. 591. 592. 593. 594. 595. 596. 597. 598. 599. 600. 601. 602. 603. 604. 605. 606. 607. 608. 609. 610. 611. 612. 613. 614. 615. 616. 617. 618. 619. 620. 621. 622. 623. 624. 625. 626. 627. 628. 629. 630. 631. 632. 633. 634. 635. 636. 637. 638. 639. 640. 641. 642. 643. 644. 645. 646. 647. 648. 649. 650. 651. 652. 653. 654. 655. 656. 657. 658. 659. 660. 661. 662. 663. 664. 665. 666. 667. 668. 669. 670. 671. 672. 673. 674. 675. 676. 677. 678. 679. 680. 681. 682. 683. 684. 685. 686. 687. 688. 689. 690. 691. 692. 693. 694. 695. 696. 697. 698. 699. 700. 701. 702. 703. 704. 705. 706. 707. 708. 709. 710. 711. 712. 713. 714. 715. 716. 717. 718. 719. 720. 721. 722. 723. 724. 725. 726. 727. 728. 729. 730. 731. 732. 733. 734. 735. 736. 737. 738. 739. 740. 741. 742. 743. 744. 745. 746. 747. 748. 749. 750. 751. 752. 753. 754. 755. 756. 757. 758. 759. 760. 761. 762. 763. 764. 765. 766. 767. 768. 769. 770. 771. 772. 773. 774. 775. 776. 777. 778. 779. 780. 781. 782. 783. 784. 785. 786. 787. 788. 789. 790. 791. 792. 793. 794. 795. 796. 797. 798. 799. 800. 801. 802. 803. 804. 805. 806. 807. 808. 809. 810. 811. 812. 813. 814. 815. 816. 817. 818. 819. 820. 821. 822. 823. 824. 825. 826. 827. 828. 829. 830. 831. 832. 833. 834. 835. 836. 837. 838. 839. 840. 84

RECORDATION

700RS 1000S 1000S

10/27/92 10/27/92

P 1 0 00000 2000PH 200F 400000 0.00000 300F 10.00000 0.00000

| | VEN | RAP | AC | BC11 | BC12 | BC13 | BC14 | BC15 | BC16 | BC17 | BC18 | BC19 | DUST |
|-----------|--------|------|-------|-------|-------|-------|------|-------|------|------|------|------|------|
| POSTURE | 2.9 | 5.2 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 0.0 | 0.0 | |
| TRN RATE | 200 | 20 | 12.2 | 53 | 53 | 0 | 0 | 144 | 0 | 0 | 27 | 30 | 4 |
| 1 REG | 06.0 | 9.6 | 4.00 | 10.5 | 10.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.5 | |
| 2 RATE | 06.0 | 9.6 | 4.00 | 10.5 | 10.5 | 0.0 | 0.0 | 50.0 | 0.0 | 0.0 | 9.6 | 3.5 | |
| NAT TOTAL | 1075.0 | 80.2 | 50.91 | 250.5 | 250.5 | 179.1 | 0.0 | 432.9 | 0.0 | 0.0 | 31.1 | 39.5 | 0.0 |

AC STATISTICS:

AC LOGICAL 0 60F 8.53
 200000 AC ADDED 4.37
 AC TOTAL 8 4.69
 BC11 DEFERRED
 1 REG. AC 4.0
 ACB 0.40 6.37

AC ACCUM. (ACT) 6.77 8

AC ACCUM. (DEF) 4.00 8

RECORDATION

700RS 1000S 1000S

10/27/92 10/27/92

P 1 0 00000 2000PH 200F 400000 0.00000 300F 10.00000 0.00000

| | VEN | RAP | AC | BC11 | BC12 | BC13 | BC14 | BC15 | BC16 | BC17 | BC18 | BC19 | DUST |
|-----------|--------|------|-------|-------|-------|-------|------|-------|------|------|------|------|------|
| POSTURE | 2.9 | 5.2 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 0.0 | 0.0 | |
| TRN RATE | 227 | 27 | 12.2 | 53 | 50 | 0 | 0 | 144 | 0 | 0 | 27 | 30 | 9 |
| 1 REG | 06.0 | 9.6 | 4.00 | 10.5 | 10.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.5 | |
| 2 RATE | 06.0 | 9.6 | 4.00 | 10.5 | 10.6 | 0.0 | 0.0 | 49.6 | 0.0 | 0.0 | 9.6 | 3.4 | |
| NAT TOTAL | 1095.0 | 82.6 | 50.94 | 250.0 | 250.5 | 179.1 | 0.0 | 435.0 | 0.0 | 0.0 | 31.4 | 40.4 | 0.0 |

AC STATISTICS:

AC LOGICAL 0 60F 8.53
 200000 AC ADDED 4.64
 AC TOTAL 8 4.69
 BC11 DEFERRED
 1 REG. AC 4.0
 ACB 0.59 6.44

AC ACCUM. (ACT) 4.06 8

AC ACCUM. (DEF) 4.00 8

RECORDATION

700RS 1000S 1000S

10/27/92 10/27/92

P 1 0 00000 2000PH 200F 400000 0.00000 300F 10.00000 0.00000

| | VEN | RAP | AC | BC11 | BC12 | BC13 | BC14 | BC15 | BC16 | BC17 | BC18 | BC19 | DUST |
|-----------|--------|------|-------|-------|-------|-------|------|-------|------|------|------|------|------|
| POSTURE | 2.9 | 5.2 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 0.0 | 0.0 | |
| TRN RATE | 223 | 0 | 12.1 | 53 | 53 | 0 | 0 | 144 | 0 | 0 | 27 | 30 | 10 |
| 1 REG | 06.0 | 9.6 | 4.00 | 10.5 | 10.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.5 | |
| 2 RATE | 06.0 | 9.6 | 4.00 | 10.6 | 10.4 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.5 | |
| NAT TOTAL | 1334.0 | 90.4 | 60.92 | 270.5 | 270.0 | 279.1 | 0.0 | 447.1 | 0.0 | 0.0 | 31.2 | 41.3 | 0.0 |

AC STATISTICS:

AC LOGICAL 0 60F 8.53
 100000 AC ADDED 4.96
 AC TOTAL 8 4.60
 BC11 DEFERRED

AC TOTAL 4.80
 AC RECL AC 4.0
 ACN 0.01 4.76
 AC ACCHL (ACT) 4.77 %
 AC ACCHL (REG) 4.80 %

REGISTRATION 7000S 1600S 1000S 10/22/92 10/22/92

1 1 1 10000 2917PH 293F 116700S 4.800000 306F 14.00000 0.00000

| | VEN | REP | AC | BCH1 | BCH2 | BCH3 | BCH4 | BCH5 | BCH6 | BCH7 | BCH8 | BCH9 | BCH10 | BCH11 | BCH12 |
|-----------|--------|------|-------|-------|-------|-------|------|-------|------|------|------|------|-------|-------|-------|
| ACSTONE | 2.9 | 5.2 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 5.2 | | | | |
| PH DATE | 232 | 26 | 12.1 | 54 | 53 | 0 | 0 | 141 | 0 | 0 | 27 | 10 | 6 | | |
| REG | 56.8 | 9.6 | 4.80 | 18.5 | 18.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.5 | | | |
| DATE | 56.7 | 9.6 | 4.80 | 18.7 | 18.5 | 0.0 | 0.0 | 49.3 | 0.0 | 0.0 | 9.6 | 3.5 | | | |
| ACT TOTAL | 1134.5 | 86.0 | 52.99 | 275.0 | 277.5 | 179.1 | 0.0 | 459.2 | 0.0 | 0.0 | 90.1 | 42.1 | 0.0 | | |

Errors (Chan 0) (CPC 0) (Vocal 0) (Bucalo 0) (Chaver 0) (Dant 0)

AC STATISTICS:
 AC 15/50L 0 60F 5.53
 ACCHL AC ADDED 4.47
 AC TOTAL 4.67
 AC RECL AC 4.0
 ACN 0.39 4.47
 AC ACCHL (ACT) 4.87 %
 AC ACCHL (REG) 4.80 %

REGISTRATION 7000S 1600S 1000S 10/22/92 10/22/92

1 1 1 10000 2597PH 296F 109000S 4.800000 306F 14.00000 0.00000

| | VEN | REP | AC | BCH1 | BCH2 | BCH3 | BCH4 | BCH5 | BCH6 | BCH7 | BCH8 | BCH9 | BCH10 | BCH11 | BCH12 |
|-----------|--------|------|-------|-------|-------|-------|------|-------|------|------|------|------|-------|-------|-------|
| ACSTONE | 2.9 | 5.2 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 5.2 | | | | |
| PH DATE | 235 | 24 | 12.1 | 53 | 53 | 0 | 0 | 145 | 0 | 0 | 27 | 10 | 6 | | |
| REG | 56.8 | 9.6 | 4.80 | 18.5 | 18.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.5 | | | |
| DATE | 56.9 | 9.6 | 4.80 | 18.6 | 18.4 | 0.0 | 0.0 | 50.0 | 0.0 | 0.0 | 9.6 | 3.0 | | | |
| ACT TOTAL | 1154.0 | 80.2 | 63.01 | 202.5 | 202.0 | 179.1 | 0.0 | 471.3 | 0.0 | 0.0 | 90.6 | 63.0 | 0.0 | | |

Errors (Chan 0) (CPC 0) (Vocal 0) (Bucalo 0) (Chaver 0) (Dant 0)

AC STATISTICS:
 AC 15/50L 0 60F 4.53
 ACCHL AC ADDED 4.49
 AC TOTAL 4.57
 AC RECL AC 4.0
 ACN 0.37 4.49
 AC ACCHL (ACT) 4.86 %
 AC ACCHL (REG) 4.80 %

REGISTRATION 7000S 1600S 1000S 10/22/92 10/22/92

1 1 1 10000 2747PH 297F 163700S 4.800000 306F 14.00000 0.00000

| | VEN | REP | AC | BCH1 | BCH2 | BCH3 | BCH4 | BCH5 | BCH6 | BCH7 | BCH8 | BCH9 | BCH10 | BCH11 | BCH12 |
|-----------|--------|------|-------|-------|-------|-------|------|-------|------|------|------|------|-------|-------|-------|
| ACSTONE | 2.9 | 5.2 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 5.2 | | | | |
| PH DATE | 225 | 24 | 12.2 | 53 | 54 | 0 | 0 | 149 | 0 | 0 | 27 | 10 | 30 | | |
| REG | 56.8 | 9.6 | 4.80 | 18.5 | 18.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.9 | | | |
| DATE | 57.0 | 9.6 | 4.80 | 18.1 | 18.6 | 0.0 | 0.0 | 50.3 | 0.0 | 0.0 | 9.6 | 3.4 | | | |
| ACT TOTAL | 1174.0 | 90.3 | 64.03 | 287.0 | 286.5 | 179.1 | 0.0 | 483.9 | 0.0 | 0.0 | 93.7 | 63.0 | 0.0 | | |

Errors (Chan 0) (CPC 0) (Vocal 0) (Bucalo 0) (Chaver 0) (Dant 0)

AC ACCUM. (ACT) 4.03 E
 AC ACCUM. (REQ) 4.00 E

RECOMMENDATION 700MS 100TS 10PLS 10/29/92 10/22/92

7 2 0 00000 260TPH 256F 185TORS 4.9000mc 209F 14.0000 0.000000

| | VEN | HAP | AC | B001 | B102 | B203 | B304 | B405 | B506 | B607 | BCT1 | BPL1 | DUST |
|-----------|--------|------|-------|-------|-------|-------|------|-------|------|------|------|------|------|
| DESIGNER | 2.9 | 5.2 | | 5.1 | 7.0 | 1.5 | 0.5 | 0.7 | 0.0 | 0.0 | 5.2 | | |
| VEN RATE | 229 | 24 | 12.0 | 53 | 54 | 0 | 0 | 143 | 0 | 0 | 27 | 10 | 6 |
| 1 REQ | 36.0 | 9.6 | 4.00 | 10.5 | 10.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.9 | |
| 1 RATE | 36.0 | 9.6 | 4.00 | 10.5 | 10.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.9 | |
| 107 TOTAL | 1193.8 | 92.4 | 65.00 | 293.5 | 294.0 | 179.1 | 0.0 | 695.5 | 0.0 | 0.0 | 99.1 | 44.7 | 0.0 |

Errors: (Blank 0) (AC 0) (Vocals 0) (Scale 0) (Bart 0) (Bart 0)

AC STATISTICS:
 AC 10/GAL 0 60F 0.53
 VERSED AC ADDED 4.65
 AC TOTAL % 4.65
 BCT1 DEFENSE
 1 REQ AC 4.0
 ACT 4.36 4.50
 AC ACCUM. (ACT) 4.57 E
 AC ACCUM. (REQ) 4.50 E

RECOMMENDATION 700MS 100TS 10PLS 11/03/92 10/22/92

7 2 0 00000 260TPH 256F 200TORS 4.9000mc 209F 14.0000 0.000000

| | VEN | HAP | AC | B101 | B202 | B303 | B404 | B505 | B606 | B707 | BCT1 | BPL1 | DUST |
|-----------|--------|------|-------|-------|-------|-------|------|-------|------|------|------|------|------|
| DESIGNER | 2.9 | 5.2 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 5.2 | | |
| VEN RATE | 229 | 23 | 11.0 | 53 | 53 | 0 | 0 | 143 | 0 | 0 | 27 | 10 | 6 |
| 1 REQ | 36.0 | 9.6 | 4.00 | 10.5 | 10.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.9 | |
| 1 RATE | 36.0 | 9.6 | 4.00 | 10.5 | 10.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.9 | |
| 107 TOTAL | 1213.4 | 94.5 | 66.00 | 296.0 | 296.5 | 179.1 | 0.0 | 507.7 | 0.0 | 0.0 | 99.6 | 45.9 | 0.0 |

Errors: (Blank 0) (AC 0) (Vocals 0) (Scale 0) (Bart 0) (Bart 0)

AC STATISTICS:
 AC 10/GAL 0 60F 0.53
 VERSED AC ADDED 4.65
 AC TOTAL % 4.65
 BCT1 DEFENSE
 1 REQ AC 4.0
 ACT 4.39 4.65
 AC ACCUM. (ACT) 4.00 E
 AC ACCUM. (REQ) 4.00 E

RECOMMENDATION 700MS 100TS 10PLS 11/00/92 10/22/92

7 2 0 00000 201TPH 207F 231TORS 4.0000mc 209F 14.0000 0.000000

| | VEN | HAP | AC | B001 | B102 | B203 | B304 | B405 | B506 | B607 | BCT1 | BPL1 | BCT2 |
|-----------|--------|------|-------|-------|-------|-------|------|-------|------|------|------|------|------|
| DESIGNER | 2.9 | 5.2 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 5.2 | | |
| VEN RATE | 219 | 20 | 12.0 | 53 | 54 | 0 | 0 | 143 | 0 | 0 | 27 | 10 | 33 |
| 1 REQ | 36.0 | 9.6 | 4.00 | 10.5 | 10.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.9 | |
| 1 RATE | 36.0 | 9.6 | 4.00 | 10.5 | 10.5 | 0.0 | 0.0 | 49.0 | 0.0 | 0.0 | 9.6 | 3.9 | |
| 107 TOTAL | 1233.3 | 96.7 | 67.00 | 300.5 | 300.0 | 179.1 | 0.0 | 519.0 | 0.0 | 0.0 | 99.0 | 46.4 | 0.0 |

Errors: (Blank 0) (AC 0) (Vocals 0) (Scale 0) (Bart 0) (Bart 0)

AC STATISTICS:
 AC 10/GAL 0 60F 0.53
 VERSED AC ADDED 4.65

[illegible]

LR 1704.22: 200722792

| | PM | RA | DEC | ALPHA | BETA | GAMMA | DELTA | EPSILON | ZETA | ETA | THETA | IOTA | KAPPA |
|-----------|--------|-------|-------|-------|-------|-------|-------|---------|------|-----|-------|------|-------|
| WORLDWIDE | 36.9 | 0.0 | 46.1 | 5.1 | 7.0 | 12.5 | 0.5 | 0.7 | 0.0 | 0.0 | 3.2 | 0.0 | 0.0 |
| THE DATE | 360 | 0 | 16.1 | 77 | 76 | 130 | 0 | 0 | 0 | 0 | 0 | 7 | 6 |
| 3.000 | 97.5 | 0.0 | 3.00 | 36.6 | 36.6 | 99.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.5 | |
| 3.000 | 97.5 | 0.0 | 3.00 | 36.6 | 36.6 | 99.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.5 | |
| 3.000 | 1330.1 | 102.3 | 71.00 | 332.4 | 322.0 | 301.3 | 0.0 | 342.6 | 0.0 | 0.0 | 100.9 | 0.0 | 0.0 |
| 3.000 | 1330.1 | 102.3 | 71.00 | 332.4 | 322.0 | 301.3 | 0.0 | 342.6 | 0.0 | 0.0 | 100.9 | 0.0 | 0.0 |

| AC SPENDING | |
|---------------|------|
| AC LEADERSHIP | 0.33 |
| EMERGENCY AC | 3.42 |
| AC SUPPLY | 4.69 |
| | 0.00 |
| AC LEADERSHIP | 4.0 |
| AC | 0.00 |
| AC | 3.42 |
| AC | |
| AC | |

RECOMMENDATION **PROBING LOCUS** **AMPLIS**

44-38861-1A 200-22792

[illegible]

| | |
|--------------------|------|
| AC STAPLER | |
| AC STAPLER, P. 600 | 4.99 |
| STAPLER AC 6000S | 3.00 |
| AC TONER, B | 4.67 |
| | ACPS |
| AC TONER, AC | 4.00 |
| ACPS | 0.00 |
| AC TONER, ACPS | 3.00 |
| AC TONER, CHIPS | |

ИЗДАТЕЛЬСТВО **ПЕРВОЕ** **ИЗДАНИЕ**

82-00040B 10/23/92

[illegible]

| | | |
|--------------------|------|------|
| DEBEN, DE | 0.00 | |
| DEBEN | 0.00 | 5.00 |
| AC ACQUIS. (DEBEN) | | |
| AC ACQUIS. (DEBEN) | | |

F 1 0 1101.2 277774 2943 11.17005 5.00000 3.00F 14.00000 0.00000

[illegible]

| | |
|--------------------|-----------|
| AC STATISTICS: | |
| AC AVERAGE PERIOD | 3.55 |
| OVERALL AC AVERAGE | 5.85 |
| AC TOTAL 1 | 4.70 |
| | NOTED |
| PERCENT AC | 4.00 |
| AC | 3.00 5.00 |
| AC AVERAGE (ACT) | |
| AC AVERAGE (PER) | |

1 0 000000 000000 000000 000000 000000 000000 000000 000000 000000 000000

| | Y1R | RAF | Y1C | Y1BL | Y1H2 | Y1H3 | Y1H4 | Y1H5 | Y1H6 | Y1H7 | Y1TL | Y1FL | Y1DT |
|-----|--------|-------|-------|-------|-------|-------|------|-------|------|------|-------|------|------|
| Y1R | 3.9 | 3.9 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 5.2 | 3FL | 0DT |
| Y1R | 350 | 0 | 15.4 | 76 | 75 | 155 | 0 | 0 | 0 | 0 | 0 | 7 | 9 |
| Y1R | 97.5 | 0.0 | 5.00 | 26.5 | 25.6 | 44.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.5 | |
| Y1R | 97.5 | 0.0 | 5.00 | 26.6 | 25.4 | 44.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.6 | |
| Y1R | 1000.4 | 102.1 | 77.31 | 340.0 | 342.6 | 244.0 | 0.0 | 542.6 | 0.0 | 0.0 | 104.9 | 51.0 | 0.0 |
| Y1R | 1000.4 | 102.1 | 77.31 | 340.0 | 342.6 | 244.0 | 0.0 | 542.6 | 0.0 | 0.0 | 104.9 | 51.0 | 0.0 |

| | | |
|-------------------|------|----------|
| AC SUBTOTAL: | | |
| AC SUBTOTAL P 60F | | 0.53 |
| CHARGE AC ADDED | | 5.34 |
| AC TOTAL 1 | | 4.71 |
| | ACCT | DEFERRED |
| RECL AC | 4.0 | |
| ACB | 4.00 | 5.34 |
| AC ACCHL (4.71) | | |
| AC ACCHL (REB) | | |

F 1 D 31322 2047PH 201F 1590005 5, 000mc 201F 10, 000L+ D, 000223

| | PER | RAP | CAC | 3302 | 0302 | 0103 | 0104 | 0305 | 3406 | 0307 | 0303 | 0304 | 0007 |
|----------|--------|-------|-------|-------|-------|-------|------|-------|------|------|-------|------|------|
| EXPENSE | 31.9 | 0.0 | | 31.1 | 7.0 | 1.5 | 0.5 | 0.7 | 0.0 | 0.0 | 5.2 | | |
| PER RATE | 356 | 0 | 15.3 | 76 | 76 | 126 | 0 | 0 | 0 | 0 | 0 | 9 | 14 |
| EXPENSE | 97.5 | 0.0 | 5.00 | 26.5 | 26.5 | 46.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.3 | |
| EXPENSE | 97.5 | 0.0 | 5.00 | 26.5 | 26.7 | 46.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.3 | |
| EXPENSE | 1050.9 | 102.1 | 73.68 | 356.4 | 354.0 | 350.6 | 0.0 | 502.5 | 0.0 | 0.0 | 104.9 | 93.0 | 0.0 |
| EXPENSE | 1050.9 | 102.1 | 73.68 | 356.4 | 354.0 | 350.6 | 0.0 | 502.5 | 0.0 | 0.0 | 104.9 | 93.0 | 0.0 |

SPACES:
 1000 sq. ft. 1000 sq. ft. 1000 sq. ft.

B REEL AC 4.0
 LCR 0.00 5.79
 AC ACCUM. (ACT) 5.79 L
 AC ACCUM. (REEL) 5.80 L

RECOMMENDATION

7000S 1000S 1000S

11:50:25 10/22/92

F 1 B REEL 2000PH 300P 2000PHS 5.000000 310P 10.000000 0.000000

| | VAR | RAP | AC | REEL | REEL | REEL | REEL | REEL | REEL | REEL | REEL | REEL | REEL |
|-----------|--------|-------|-------|-------|-------|-------|------|-------|------|------|------|------|------|
| DOSE/REEL | 3.9 | 0.0 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| TPH RATE | 257 | 0 | 15.4 | 76 | 77 | 125 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| R REEL | 97.5 | 0.0 | 5.00 | 26.5 | 26.6 | 94.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| R RATE | 97.5 | 0.0 | 5.00 | 26.5 | 26.7 | 94.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| NET TOTAL | 1453.4 | 102.1 | 80.05 | 350.3 | 360.4 | 253.3 | 0.0 | 502.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Errors=(Reel 0) (L/C 0) (Vacuole 0) (Recoil 0) (Overst 0) (Dust 0)

AC STATISTICS:

AC REEL 0 50P 4.53
 SYNCHRON AC ADDED 5.79
 AC TOTAL 1 4.74
 ACT1 REVERSED
 R REEL AC 4.0
 ACT 0.00 5.79
 AC ACCUM. (ACT) 5.80 L
 AC ACCUM. (REEL) 5.80 L

RECOMMENDATION

7000S 1000S 1000S

12:00:29 10/22/92

F 1 B REEL 2000PH 300P 2000PHS 5.000000 310P 10.000000 0.000000

| | VAR | RAP | AC | REEL | REEL | REEL | REEL | REEL | REEL | REEL | REEL | REEL | REEL |
|-----------|--------|-------|-------|-------|-------|-------|------|-------|------|------|------|------|------|
| DOSE/REEL | 3.9 | 0.0 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| TPH RATE | 261 | 0 | 15.4 | 76 | 75 | 125 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| R REEL | 97.5 | 0.0 | 5.00 | 26.6 | 26.6 | 94.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| R RATE | 97.5 | 0.0 | 5.00 | 26.7 | 26.5 | 94.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| NET TOTAL | 1475.9 | 102.1 | 80.05 | 367.2 | 366.8 | 276.0 | 0.0 | 502.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Errors=(Reel 0) (L/C 0) (Vacuole 0) (Recoil 0) (Overst 0) (Dust 0)

AC STATISTICS:

AC REEL 0 60P 3.53
 SYNCHRON AC ADDED 5.05
 AC TOTAL 2 4.75
 REEL REVERSED
 R REEL AC 4.0
 LCR 0.00 5.25
 AC ACCUM. (ACT) 5.45 L
 AC ACCUM. (REEL) 5.80 L

RECOMMENDATION

7000S 1000S 1000S

13:00:29 10/22/92

F 1 B REEL 2000PH 300P 2000PHS 5.000000 310P 10.000000 0.000000

| | VAR | RAP | AC | REEL | REEL | REEL | REEL | REEL | REEL | REEL | REEL | REEL | REEL |
|-----------|--------|-------|-------|-------|-------|-------|------|-------|------|------|------|------|------|
| DOSE/REEL | 3.9 | 0.0 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| TPH RATE | 253 | 0 | 15.3 | 76 | 76 | 126 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| R REEL | 97.5 | 0.0 | 5.00 | 26.6 | 26.5 | 94.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| R RATE | 97.4 | 0.0 | 5.00 | 26.6 | 26.5 | 94.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| NET TOTAL | 1490.5 | 102.1 | 82.00 | 373.6 | 373.2 | 286.6 | 0.0 | 502.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Errors=(Reel 0) (L/C 0) (Vacuole 0) (Recoil 0) (Overst 0) (Dust 0)

AC STATISTICS:

AC REEL 0 50P 0.53

| | | |
|-----------------|------|------|
| PRICE AC | 4.00 | |
| AC | 0.00 | 5.70 |
| AC ACCUM. (ACT) | | 5.70 |
| AC ACCUM. (REG) | | 5.00 |

| RECORDATION | 7BENS | 10CNS | 10PLS | | | | | | | | | | | |
|--|--------|-------|---------|----------|-------|---------|---------|-------|------|------|------|-------|------|------|
| F I D 21112 | 284778 | 3057 | 25470NS | 5.800000 | 314F | 14.0PLS | 0.00323 | | | | | | | |
| | TER | RAP | AC | BC11 | BC12 | BC13 | BC14 | BC15 | BC16 | BC17 | BC18 | BC19 | BC20 | BC21 |
| DESTRUCT | 2.9 | 0.0 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 0.0 | 5.2 | | |
| TPN RATE | 266 | 0 | 16.5 | 76 | 76 | 327 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 7 |
| E REG | 97.5 | 0.0 | 5.80 | 35.6 | 36.5 | 46.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.5 | |
| E RATE | 97.5 | 0.0 | 5.80 | 35.6 | 36.5 | 46.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.5 | |
| NET TOTAL | 1521.3 | 102.1 | 04.19 | 580.0 | 379.6 | 297.3 | 0.0 | 542.6 | 0.0 | 0.0 | 0.0 | 104.9 | 56.0 | 0.0 |
| Errors: (Data 0) (C/C 0) (Vocal 0) (Bocal 0) (Direct 0) (Cont 0) | | | | | | | | | | | | | | |

| | | | |
|------------------|----------|------|---|
| AC STATISTICS: | | | |
| AC TOTAL P GOF | | 5.53 | |
| AVERSED AC ACCUM | | 5.01 | |
| AC TOTAL L | | 4.77 | |
| BC11 | DEFERRED | | |
| E REG AC | 0.0 | | |
| ACT | 0.00 | 5.01 | |
| AC ACCUM. (ACT) | | 5.01 | % |
| AC ACCUM. (REG) | | 5.00 | % |

| RECORDATION | 7BENS | 10CNS | 10PLS | | | | | | | | | | | |
|--|--------|-------|---------|----------|-------|---------|---------|-------|------|------|------|-------|------|------|
| F I D 21112 | 284778 | 3057 | 27470NS | 5.800000 | 314F | 14.0PLS | 0.00323 | | | | | | | |
| | TER | RAP | AC | BC11 | BC12 | BC13 | BC14 | BC15 | BC16 | BC17 | BC18 | BC19 | BC20 | BC21 |
| DESTRUCT | 2.9 | 0.0 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 0.0 | 5.2 | | |
| TPN RATE | 191 | 1 | 16.5 | 52 | 43 | 0 | 0 | 228 | 0 | 0 | 0 | 0 | 7 | 9 |
| E REG | 06.0 | 3.6 | 4.00 | 18.5 | 18.5 | 0.0 | 0.0 | 49.3 | 0.0 | 0.0 | 0.0 | 9.6 | 3.5 | |
| E RATE | 97.0 | 0.0 | 5.00 | 18.9 | 18.2 | 0.0 | 0.0 | 68.5 | 0.0 | 0.0 | 0.0 | 0.0 | 3.1 | |
| NET TOTAL | 1593.9 | 102.1 | 35.50 | 386.4 | 305.9 | 307.2 | 0.0 | 543.6 | 0.0 | 0.0 | 0.0 | 104.9 | 35.4 | 0.0 |
| Errors: (Data 0) (C/C 0) (Vocal 0) (Bocal 0) (Direct 0) (Cont 0) | | | | | | | | | | | | | | |

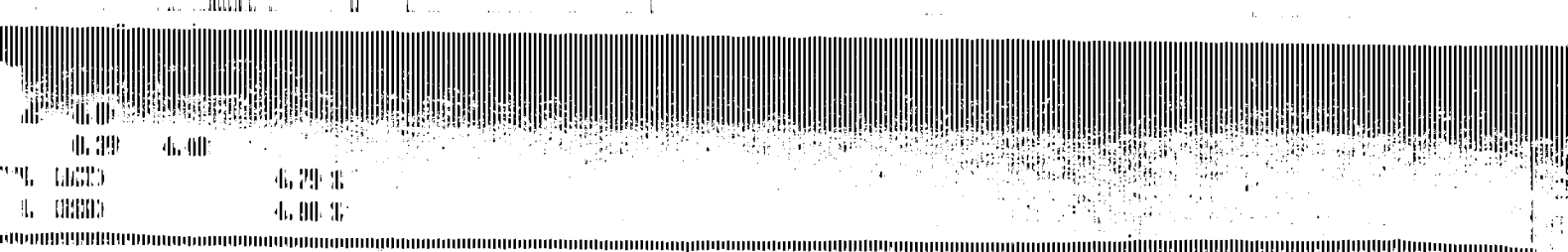
| | | | |
|------------------|------|----------|---|
| AC STATISTICS: | | | |
| AC TOTAL P GOF | 0.53 | | |
| AVERSED AC ACCUM | 5.50 | | |
| AC TOTAL L | 4.70 | | |
| | BC11 | DEFERRED | |
| E REG AC | 0.0 | | |
| ACT | 0.00 | 5.01 | |
| AC ACCUM. (ACT) | | 5.00 | 1 |
| AC ACCUM. (REG) | | 4.00 | 1 |

| RECORDATION | 7BENS | 10CNS | 10PLS | | | | | | | | | | | |
|--|--------|-------|---------|----------|-------|---------|---------|-------|------|------|------|-------|------|------|
| F I D 21112 | 272778 | 2927 | 15370NS | 4.800000 | 312F | 14.0PLS | 0.00323 | | | | | | | |
| | TER | RAP | AC | BC11 | BC12 | BC13 | BC14 | BC15 | BC16 | BC17 | BC18 | BC19 | BC20 | BC21 |
| DESTRUCT | 2.9 | 5.2 | | 5.1 | 7.0 | 1.5 | 0.6 | 0.7 | 0.0 | 0.0 | 0.0 | 5.2 | | |
| TPN RATE | 235 | 27 | 12.0 | 53 | 53 | 0 | 0 | 160 | 0 | 0 | 0 | 37 | 10 | 10 |
| E REG | 06.0 | 3.6 | 4.00 | 18.5 | 18.5 | 0.0 | 0.0 | 49.3 | 0.0 | 0.0 | 0.0 | 9.6 | 3.5 | |
| E RATE | 06.6 | 9.7 | 4.00 | 18.7 | 18.6 | 0.0 | 0.0 | 63.2 | 0.0 | 0.0 | 0.0 | 9.7 | 3.5 | |
| NET TOTAL | 1564.3 | 303.9 | 06.76 | 390.0 | 390.4 | 307.2 | 0.0 | 538.9 | 0.0 | 0.0 | 0.0 | 106.7 | 36.2 | 0.0 |
| Errors: (Data 0) (C/C 0) (Vocal 0) (Bocal 0) (Direct 0) (Cont 0) | | | | | | | | | | | | | | |

| | |
|----------------|------|
| AC STATISTICS: | |
| AC TOTAL P GOF | 0.53 |

APPENDIX III OPERATING DATA

3.2 October 23



0.39 4.40
LACTO 4.79 H
L. LACTO 4.80 H

FROM TOBACCO LIGTS AMPLS

07/23/93 10/23/93

11330 2947PH 304P 1677C08 4.80Lact 304P 10.00C08 0.00C23

| | YLR | HAP | WAC | BCH1 | BCH2 | BCH3 | BCH4 | BCH5 | BCH6 | BCH7 | BCH8 | BCH9 | BCH10 |
|---|-------|------|-------|------|------|------|------|------|------|------|------|------|-------|
| 1 | 2.9 | 5.2 | | 5.1 | 7.0 | 1.9 | 0.5 | 0.7 | 0.0 | 0.0 | 5.2 | | |
| 2 | 241 | 27 | 12.0 | 53 | 55 | 0 | 0 | 150 | 0 | 0 | 20 | 10 | 0 |
| | 86.8 | 9.6 | 4.80 | 19.5 | 38.5 | 0.0 | 0.0 | 49.8 | 0.0 | 0.0 | 9.6 | 3.9 | |
| | 86.9 | 9.5 | 4.80 | 19.2 | 38.4 | 0.0 | 0.0 | 49.7 | 0.0 | 0.0 | 9.5 | 3.4 | |
| 3 | 243.7 | 15.6 | 19.25 | 80.8 | 88.9 | 91.3 | 0.0 | 92.0 | 0.0 | 0.0 | 19.0 | 11.3 | 0.0 |

304P 01 (Lact 01) (Cocula 01) (Cocula 01) (Bavert 01) (Bant 01)

STICS:

6.0 60P 0.53
WAC LACTO 4.45
L 4.80
BCH1 DEFERED
WAC 4.0
0.38 4.45

LACTO 4.80 H

LACTO 4.80 H

FROM TOBACCO LIGTS AMPLS

07/23/93 10/23/93

11330 2947PH 304P 1677C08 4.80Lact 304P 10.00C08 0.00C23

| | YLR | HAP | WAC | BCH1 | BCH2 | BCH3 | BCH4 | BCH5 | BCH6 | BCH7 | BCH8 | BCH9 | BCH10 |
|---|-------|------|-------|------|------|------|------|-------|------|------|------|------|-------|
| 1 | 2.9 | 5.2 | | 5.1 | 7.0 | 1.9 | 0.5 | 0.7 | 0.0 | 0.0 | 5.2 | | |
| 2 | 236 | 27 | 12.9 | 56 | 56 | 0 | 0 | 100 | 0 | 0 | 20 | 10 | 0 |
| | 86.8 | 9.6 | 4.80 | 19.5 | 38.5 | 0.0 | 0.0 | 49.8 | 0.0 | 0.0 | 9.6 | 3.9 | |
| | 86.9 | 9.5 | 4.80 | 19.2 | 38.4 | 0.0 | 0.0 | 49.7 | 0.0 | 0.0 | 9.5 | 3.4 | |
| 3 | 264.5 | 17.9 | 20.30 | 93.4 | 93.6 | 91.3 | 0.0 | 104.5 | 0.0 | 0.0 | 19.4 | 11.3 | 0.0 |

304P 01 (Lact 01) (Cocula 01) (Cocula 01) (Bavert 01) (Bant 01)

STICS:

6.0 60P 0.53
WAC LACTO 4.46
L 4.80
BCH1 DEFERED
WAC 4.0
0.38 4.46

LACTO 4.80 H

LACTO 4.80 H

FROM TOBACCO LIGTS AMPLS

07/23/93 10/23/93

11330 2947PH 304P 1677C08 4.80Lact 304P 10.00C08 0.00C23

| | YLR | HAP | WAC | BCH1 | BCH2 | BCH3 | BCH4 | BCH5 | BCH6 | BCH7 | BCH8 | BCH9 | BCH10 |
|---|-------|------|-------|------|------|------|------|-------|------|------|------|------|-------|
| 1 | 3.0 | 4.6 | | 4.9 | 6.6 | 1.0 | 0.6 | 1.0 | 0.0 | 0.0 | 4.6 | | |
| 2 | 231 | 27 | 12.9 | 55 | 59 | 0 | 0 | 150 | 0 | 0 | 20 | 10 | 0 |
| | 86.8 | 9.6 | 4.80 | 19.5 | 10.5 | 0.0 | 0.0 | 49.8 | 0.0 | 0.0 | 9.6 | 3.9 | |
| | 86.9 | 9.5 | 4.80 | 19.5 | 10.5 | 0.0 | 0.0 | 49.8 | 0.0 | 0.0 | 9.5 | 3.4 | |
| 3 | 245.2 | 20.3 | 21.40 | 90.1 | 90.2 | 91.3 | 0.0 | 107.6 | 0.0 | 0.0 | 20.4 | 11.3 | 0.0 |

304P 01 (Lact 01) (Cocula 01) (Cocula 01) (Bavert 01) (Bant 01)

STICS:

| | | |
|---------------|---------|------|
| AC TOTAL 3 | 4.00 | |
| DEBIT | DEBITED | |
| ACCL AC | 4.0 | |
| ACCL | 0.37 | 4.40 |
| AC ACCL (ACT) | 4.70 | 3 |
| AC ACCL (DEB) | 4.00 | 3 |

| RECONCILIATION | | | | | | | | | | | | | | 07/30/90 10/23/92 | |
|--|-------|------|-------|-------|-------|------|------|-------|------|------|------|------|-------|-------------------|--|
| 7 1 9 11130 3553003 300P 24073003 4.000000 31.2P 14.000000 0.000000 | | | | | | | | | | | | | | | |
| | VEN | REP | AC | DEB1 | DEB2 | DEB3 | DEB4 | DEB5 | DEB6 | DEB7 | DEB8 | DEB9 | DEB10 | | |
| ESTIMATE | 3.0 | 4.6 | | 4.9 | 6.6 | 1.3 | 0.6 | 1.0 | 0.0 | 0.0 | 4.6 | | | | |
| REP RATE | 240 | 23 | 12.7 | 33 | 35 | 0 | 0 | 349 | 0 | 0 | 33 | 10 | 6 | | |
| REP | 86.0 | 9.6 | 4.00 | 10.5 | 13.5 | 0.0 | 0.0 | 49.3 | 0.0 | 0.0 | 9.6 | 3.5 | | | |
| REP | 86.9 | 9.9 | 4.00 | 10.4 | 13.2 | 0.0 | 0.0 | 50.2 | 0.0 | 0.0 | 9.5 | 3.4 | | | |
| TOTAL | 405.9 | 22.7 | 22.02 | 102.3 | 102.9 | 91.3 | 0.0 | 129.5 | 0.0 | 0.0 | 24.2 | 14.0 | 0.0 | | |
| Balance (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) | | | | | | | | | | | | | | | |

| | | | | | | | | | | | | | | | |
|---------------|---------|------|------|---|--|--|--|--|--|--|--|--|--|--|--|
| SUMMARY | | | | | | | | | | | | | | | |
| AC TOTAL 3 | 4.53 | | | | | | | | | | | | | | |
| DEBIT | DEBITED | | | | | | | | | | | | | | |
| ACCL AC | 4.0 | | | | | | | | | | | | | | |
| ACCL | 0.37 | 4.43 | | | | | | | | | | | | | |
| AC ACCL (ACT) | | | 4.00 | 3 | | | | | | | | | | | |
| AC ACCL (DEB) | | | 4.00 | 3 | | | | | | | | | | | |

| RECONCILIATION | | | | | | | | | | | | | | 07/30/92 10/23/92 | |
|--|-------|------|-------|-------|-------|------|------|-------|------|------|------|------|-------|-------------------|--|
| 11 11130 3553003 300P 24073003 4.000000 31.2P 14.000000 0.000000 | | | | | | | | | | | | | | | |
| | VEN | REP | AC | DEB1 | DEB2 | DEB3 | DEB4 | DEB5 | DEB6 | DEB7 | DEB8 | DEB9 | DEB10 | | |
| ESTIMATE | 3.0 | 4.6 | | 4.9 | 6.6 | 1.3 | 0.6 | 1.0 | 0.0 | 0.0 | 4.6 | | | | |
| REP RATE | 240 | 23 | 12.7 | 33 | 35 | 0 | 0 | 349 | 0 | 0 | 33 | 10 | 6 | | |
| REP | 86.0 | 9.6 | 4.00 | 10.5 | 13.5 | 0.0 | 0.0 | 49.3 | 0.0 | 0.0 | 9.6 | 3.5 | | | |
| REP | 86.9 | 9.9 | 4.00 | 10.4 | 13.2 | 0.0 | 0.0 | 50.2 | 0.0 | 0.0 | 9.5 | 3.4 | | | |
| TOTAL | 426.7 | 22.1 | 22.35 | 107.4 | 107.5 | 91.3 | 0.0 | 142.1 | 0.0 | 0.0 | 26.7 | 14.0 | 0.0 | | |
| Balance (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) | | | | | | | | | | | | | | | |

| | | | | | | | | | | | | | | | |
|---------------|---------|------|------|---|--|--|--|--|--|--|--|--|--|--|--|
| SUMMARY | | | | | | | | | | | | | | | |
| AC TOTAL 3 | 4.53 | | | | | | | | | | | | | | |
| DEBIT | DEBITED | | | | | | | | | | | | | | |
| ACCL AC | 4.0 | | | | | | | | | | | | | | |
| ACCL | 0.37 | 4.30 | | | | | | | | | | | | | |
| AC ACCL (ACT) | | | 4.77 | 3 | | | | | | | | | | | |
| AC ACCL (DEB) | | | 4.00 | 3 | | | | | | | | | | | |

| RECONCILIATION | | | | | | | | | | | | | | 07/30/92 10/23/92 | |
|--|-------|------|-------|-------|-------|------|------|-------|------|------|------|------|-------|-------------------|--|
| 11 11130 3553003 300P 24073003 4.000000 31.2P 14.000000 0.000000 | | | | | | | | | | | | | | | |
| | VEN | REP | AC | DEB1 | DEB2 | DEB3 | DEB4 | DEB5 | DEB6 | DEB7 | DEB8 | DEB9 | DEB10 | | |
| ESTIMATE | 3.0 | 4.6 | | 4.9 | 6.6 | 1.3 | 0.6 | 1.0 | 0.0 | 0.0 | 4.6 | | | | |
| REP RATE | 240 | 23 | 12.7 | 33 | 35 | 0 | 0 | 349 | 0 | 0 | 33 | 10 | 6 | | |
| REP | 86.0 | 9.6 | 4.00 | 10.5 | 13.5 | 0.0 | 0.0 | 49.3 | 0.0 | 0.0 | 9.6 | 3.5 | | | |
| REP | 86.9 | 9.9 | 4.00 | 10.4 | 13.2 | 0.0 | 0.0 | 50.2 | 0.0 | 0.0 | 9.5 | 3.4 | | | |
| TOTAL | 426.7 | 22.1 | 22.35 | 107.4 | 107.5 | 91.3 | 0.0 | 142.1 | 0.0 | 0.0 | 26.7 | 14.0 | 0.0 | | |
| Balance (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) (Debit) (Credit) | | | | | | | | | | | | | | | |

R RUCAL AC 4.0
 AC 0.39 4.46
 AC ACCUM. (ACT) 4.80 H
 AC ACCUM. (REQ) 4.80 H

RECORDATION 700MS 800PS 10PLS 07:40:46 10/23/92

F I R 01030 201TPH 500P 313TCMS 4.8000ms 311P (4.0000) 0.00000

| | PER | RAP | AC | BC11 | BC12 | BC13 | BC14 | BC15 | BC16 | BC17 | BC18 | BC19 | BC20 |
|-----------|-------|------|-------|-------|-------|------|------|-------|------|------|------|------|------|
| MEASURE | 3.0 | 4.6 | | 4.9 | 6.5 | 1.8 | 0.5 | 1.0 | 0.0 | 0.0 | 4.6 | | |
| TPH RATE | 240 | 27 | 12.5 | 54 | 54 | 0 | 0 | 144 | 0 | 0 | 28 | 10 | 6 |
| % REQ | 86.8 | 9.6 | 4.80 | 18.5 | 28.5 | 0.0 | 0.0 | 69.8 | 0.0 | 0.0 | 9.6 | 3.5 | |
| % RATE | 86.8 | 9.6 | 4.80 | 18.7 | 28.5 | 0.0 | 0.0 | 69.2 | 0.0 | 0.0 | 9.6 | 3.5 | |
| NET TOTAL | 467.9 | 39.8 | 29.50 | 116.7 | 116.9 | 91.3 | 0.0 | 157.2 | 0.0 | 0.0 | 31.5 | 15.6 | 0.0 |

Errors=(Blk 0) (L/C 0) (Vocals 0) (Rucals 0) (Dvort 0) (Durt 0)

AC STATISTICS:
 AC BLK/BLK P 60P 0.93
 MERGED AC ADDED 4.46
 AC TOTAL H 4.75
 BC11 DEFERRED
 RECL AC 4.0
 AC 0.39 4.46
 AC ACCUM. (ACT) 4.80 H
 AC ACCUM. (REQ) 4.80 H

RECORDATION 700MS 800PS 10PLS 07:53:40 10/23/92

F I R 01030 201TPH 500P 313TCMS 4.8000ms 311P (4.0000) 0.00000

| | PER | RAP | AC | BC11 | BC12 | BC13 | BC14 | BC15 | BC16 | BC17 | BC18 | BC19 | BC20 |
|-----------|-------|------|-------|-------|-------|------|------|-------|------|------|------|------|------|
| MEASURE | 3.0 | 4.6 | | 4.9 | 6.6 | 1.8 | 0.6 | 1.0 | 0.0 | 0.0 | 4.6 | | |
| TPH RATE | 237 | 26 | 12.9 | 55 | 54 | 0 | 0 | 152 | 0 | 0 | 28 | 10 | 7 |
| % REQ | 86.8 | 9.6 | 4.80 | 20.5 | 18.5 | 0.0 | 0.0 | 49.8 | 0.0 | 0.0 | 9.6 | 3.9 | |
| % RATE | 86.9 | 9.5 | 4.80 | 20.2 | 18.0 | 0.0 | 0.0 | 50.6 | 0.0 | 0.0 | 9.5 | 3.9 | |
| NET TOTAL | 468.4 | 32.1 | 29.75 | 121.6 | 122.5 | 91.3 | 0.0 | 179.7 | 0.0 | 0.0 | 33.9 | 17.9 | 0.0 |

Errors=(Blk 0) (L/C 0) (Vocals 0) (Rucals 0) (Dvort 0) (Durt 0)

AC STATISTICS:
 C BLK/BLK P 60P 0.93
 MERGED AC ADDED 4.41
 AC TOTAL H 4.73
 BC11 DEFERRED
 RECL AC 4.0
 AC 0.37 4.41
 AC ACCUM. (ACT) 0.79 H
 AC ACCUM. (REQ) 0.00 H

RECORDATION 700MS 800PS 10PLS 07:50:30 10/23/92

F I R 01030 2900TPH 500P 361TCMS 6.0000ms 311P (4.0000) 0.00000

| | PER | RAP | AC | BC11 | BC12 | BC13 | BC14 | BC15 | BC16 | BC17 | BC18 | BC19 | BC20 |
|-----------|-------|------|-------|-------|-------|------|------|-------|------|------|------|------|------|
| MEASURE | 3.0 | 4.6 | | 4.9 | 6.6 | 1.8 | 0.6 | 1.0 | 0.0 | 0.0 | 4.6 | | |
| TPH RATE | 239 | 29 | 12.0 | 56 | 55 | 0 | 0 | 148 | 0 | 0 | 28 | 10 | 0 |
| % REQ | 86.8 | 9.5 | 6.00 | 18.5 | 28.5 | 0.0 | 0.0 | 49.8 | 0.0 | 0.0 | 9.6 | 3.9 | |
| % RATE | 86.8 | 9.5 | 6.00 | 18.7 | 28.6 | 0.0 | 0.0 | 49.6 | 0.0 | 0.0 | 9.6 | 3.9 | |
| NET TOTAL | 509.0 | 34.5 | 27.00 | 126.0 | 126.2 | 91.3 | 0.0 | 192.2 | 0.0 | 0.0 | 36.3 | 18.4 | 0.0 |

Errors=(Blk 0) (L/C 0) (Vocals 0) (Rucals 0) (Dvort 0) (Durt 0)

AC STATISTICS:

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[illegible]

DECLASSIFICATION AUTHORITY DERIVED FROM: 28CFR 1.55(a)(1) AND (2), 50CFR 1.54(b)(1) AND (2)

| AC STATISTICS | | |
|-----------------|------|----------|
| AC DEBIL P 60F | | 0.93 |
| DEBIL AC 60F00 | | 0.35 |
| AC TOTAL T | | 0.62 |
| | ACPL | DEFERRED |
| 7 DEBIL AC | 4.0 | |
| AC8 | 0.30 | 4.35 |
| AC ACCHIL CACTY | | |
| AC ACCHIL CUBED | | |

RECORDED - THREE LOCKS BUILT 09:29:20 10/23/97

| | | |
|-------------------|------|----------|
| CC STATESTOCK: | | |
| CC BALANCE F 600 | 0.33 | |
| EXPENSES CC 6000 | 4.32 | |
| CC TOTAL T | 4.65 | |
| | CCPA | DEFERRED |
| 1. BALANCE | 4.0 | |
| CC | 0.39 | 4.32 |
| CC ACCOUNT (CCPA) | | 4.72 T |
| CC ACCOUNT (CCPA) | | 4.00 T |

RECORDED 700MS 300MS 800MS 00-30632 10-23-92

[illegible]

APPENDIX IV
ANALYTICAL RESULTS

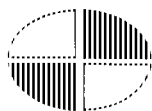
APPENDIX IV

ANALYTICAL RESULTS

- 4.1 Particulate
- 4.2 Volatile Organic Compounds

APPENDIX IV ANALYTICAL RESULTS

4.1 Particulate

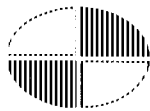
ANALYTICAL REPORT

Client: Gilbert/Commonwealth, Inc.
Report to: Steve Folck
Gilbert/Commonwealth, Inc.
P. O. Box 1498
Reading PA 19603

Project: 116814
Received: 22-OCT-92
Reported: 03-NOV-92
PURCHASE ORDER: 52977

Project Description: Windsor Service

| | RESULT | UNITS | METHOD | DATE | ANALYST |
|-------------------------------------|--------|-------|--------|-----------|---------|
| <u>W-P-1</u> | | | | | |
| SSM Sample: 1065110 | | | | | |
| sampled: 21-OCT-92 by: Client | | | | | |
| Particulate Weight - Filter | 9.4 | mg | EPA 5 | 27-OCT-92 | VJO |
| PARTICULATE WEIGHT - WASH SOLUTIONS | | | EPA 5 | 27-OCT-92 | VJO |
| Wt - Wash Soln* (0.22u Filter) | 7.6 | mg | | | |
| Wt - Acetone Impinger | 5.6 | mg | | | |
| Wt - Acetone Probe | 4.4 | mg | | | |
| Wt - Water Probe | 15.9 | mg | | | |
| Wt - Water Impinger | 3.1 | mg | | | |
| <u>W-P-2</u> | | | | | |
| SSM Sample: 1065111 | | | | | |
| sampled: 22-OCT-92 by: Client | | | | | |
| Particulate Weight - Filter | 21.6 | mg | EPA 5 | 27-OCT-92 | VJO |
| PARTICULATE WEIGHT - WASH SOLUTIONS | | | EPA 5 | 27-OCT-92 | VJO |
| Wt - Wash Soln* (0.22u Filter) | 10.9 | mg | | | |
| Wt - Acetone Impinger | 5.3 | mg | | | |
| Wt - Acetone Probe | 6.7 | mg | | | |
| Wt - Water Probe | 31.0 | mg | | | |
| Wt - Water Impinger | 2.1 | mg | | | |
| <u>W-P-3</u> | | | | | |
| SSM Sample: 1065112 | | | | | |
| sampled: 22-OCT-92 by: Client | | | | | |
| Particulate Weight - Filter | 16.7 | mg | EPA 5 | 27-OCT-92 | VJO |
| PARTICULATE WEIGHT - WASH SOLUTIONS | | | EPA 5 | 27-OCT-92 | VJO |
| Wt - Wash Soln* (0.22u Filter) | 12.4 | mg | | | |
| Wt - Acetone Impinger | 4.6 | mg | | | |
| Wt - Acetone Probe | 5.8 | mg | | | |



SSM Laboratories

page 2 of 2

C590V92_1120_P3_00611

Client: Gilbert/Commonwealth, Inc.
Project: 116814

| | RESULT | UNITS | METHOD | DATE | ANALYST |
|---|--------|-------|--------|------|---------|
| W.P.S.
SSM Sample: 1065112 - continued | | | | | |
| Wt - Water Probe | 19.7 | mg | | | |
| Wt - Water Impinger | 1.0 | mg | | | |

Respectfully submitted,

Craig L. Stewart
Inorganics Supervisor



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APPENDIX IV

ANALYTICAL RESULTS

4.2 Volatile Organic Compounds

TRIANGLE ENVIRONMENTAL SERVICES

Post Office Box 13294

November 18, 1992

Research Triangle Park, N.C. 27709

Gary Helm
Gilbert Commonwealth
PAX Transmittal

Dear Gary:

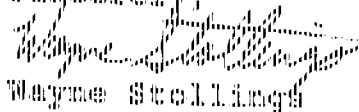
This is to confirm and further explain our conversations concerning our report 92022 and the questions associated with the samples 2, 3, and 4. These were a sample tank and two sample traps analyzed separately with the results to be used to calculate the final concentrations. The analysis of sample 2 should not have been greatly affected by the use of two traps during sampling. The analysis of the two traps did present potential problems.

The two factors that presented the potential problem were the presence of sufficient moisture to cause the traps to begin to become plugged with ice and the sample volume associated with each trap. The moisture problem is present in most Method 25 sampling projects and is only a problem when ice plugs form or if the CO₂ concentration is such that a positive bias is indicated. Normally the positive bias is not much of a problem unless the expected concentrations are very low. In this case, however, the small sample volume works with this bias and any other small problems to become larger problems.

I believe that a positive bias would be indicated due to the reported concentration of 4.9% CO₂ in sample 2 and the presence of sufficient moisture to completely plug the trap (sample 3) with ice. The indications of partial blockage by ice was present in sample 4 as well. This bias is due to CO₂ becoming trapped in the ice and when the condensible fraction is oxidized and analyzed the trapped CO₂ is reported as TGMCO. I also believe that this bias was compounded by the low sample volume associated with the two traps. The amount of 4.9% CO₂ that would significantly affect the final concentration of a 2 liter sample would not affect a 4 liter or 6 liter sample as significantly.

This low sample volume causes a much greater dilution factor for each of the separate trap samples than was used on the other two samples involved. This larger dilution factor can greatly increase any small contamination or background to much larger proportions. If the areas of each of the analyses is compared they are very close in ranges. But the dilution factor causes the final reported concentration to be two or three times the larger sample. This does not mean that the samples were the same concentration, but that the dilution factor would cause a more pronounced effect on the two separate traps than a single trap with the same total concentration.

Sincerely,


Wayne Stollings

WS/wl

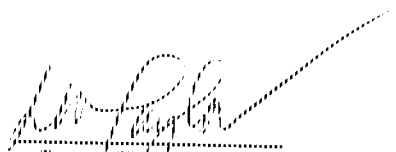
Method 225
Analytical Results

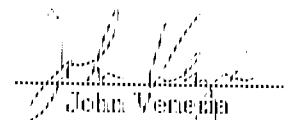
prepared for

GILBERT COMMONWEALTH

by

TRIANGLE ENVIRONMENTAL SERVICES, INC.


Larry W. Taylor
Method 225 Analyst


John Venegas
Method 225 Supervisor

Report

92022

November 16, 1992

METHOD 25 SAMPLE GAS/CO DATA

DAILY CHECKS

4.3.1.1^a

Condensate Recovery System Leak Check

Evacuate system to ≤ 10 mm Hg absolute, isolate system, and monitor for ten minutes.

Requirements: Pressure Change ≤ 3 mm Hg

4.3.1.2^a

Condensate Recovery System Background Test

Analyze recovery system effluent for CO_2 concentrations.

Requirements: $\text{CO}_2 \leq 10$ ppm

4.3.1.3^a

Condensate Oxidation Catalyst Efficiency Check

Analyze 1% Methane standard through oxidation catalyst.

Requirements: $\text{CO}_2 = \text{CH}_4$ concentration $\pm 2\%$

5.3^a

Daily Calibration

CO_2 Response Factor Check

Requirements: $\text{DRF}(\text{CO}_2) = [\text{RF}(\text{CO}_2)] \pm 5\%$

NMO Response Factor Check

Requirements: $\text{DRF}(\text{NMO}) = [\text{RF}(\text{NMO})] \pm 5\%$

Triplicate injections of high level CO_2 and a mixture of CO , CH_4 , and C_2H_6 are made before and after of each set of samples or on a daily basis, whichever occurs first.

Initial Condensate Recovery System Tests

5.1.1^a

Carrier and Auxiliary Gas Blank

$\text{CO} + \text{CH}_4 + \text{CO}_2 + \text{NMO} =$ Requirements ≤ 5 ppm

^a USEPA Method 25 Protocol Reference Number

5.1.3^a

System Performance Check Date: 8/7/92

Average Percent

| | | Recovery | % RSD |
|---------------|--------|----------------|-------------------|
| 50 mL | Hexane | <u>101/102</u> | <u>0.58/1.01</u> |
| 50 mL | Decane | <u>97/100</u> | <u>1.20/1.047</u> |
| 10 mL | Hexane | <u>104/107</u> | <u>1.18/1.143</u> |
| 10 mL | Decane | <u>98/97</u> | <u>1.19/1.232</u> |
| Requirements: | | 100 ± 10% | ≤5 |

Initial NMOC Analyzer Performance Checks

5.2.1^a

Oxidation Catalyst Efficiency Check Date: 10/29/92

FID response with reduction catalyst in bypass mode = 0

Requirements: ≤1%

5.2.2^a

Reduction Catalyst Efficiency Check Date: 10/29/92

Response of CH₄ with Oxidation and reduction catalyst in series mode compared to response with both catalysts in bypass mode.

97.6% Requirement 100 ± 5%

5.2.3^a

Analyzer Linearity Check + NMOC Calibration Date: 10/29-30/92

| | Requirement: |
|-----------------------------------|--------------|
| RF Value CO ₂ - ± 1.9% | ± 2.5% |
| RF Value NMOC - ± 2.5% | ± 2.5% |
| % RSD Values - .51% | ≤2% |
| RF (NMOC) = .98 | 1.0 ± 0.1 |
| RF (CO ₂) | |

5.2.4^a

System Performance Check Date: 10/29-30/92

| | Measured Value | Expected Value | Requirement |
|----------------|----------------|----------------|-------------|
| Propane in Mix | <u>23.8</u> | <u>25.1</u> | ± 5% |
| Hexane | <u>49.5</u> | <u>47.3</u> | ± 5% |
| Toluene | <u>20.1</u> | <u>20.1</u> | ± 5% |

^a USEPA Method 25 Protocol Reference Number

Equipment Checks

4.1.2^a

Clean Sampling Equipment Check

| | |
|-------------|-----------------|
| Sample Unit | ≤10 ppmC @ 100% |
| Trap | ≤10 ppmC @ 100% |
| Tank | ≤10 ppmC @ 100% |

4.1.2^a

Sample Tank Evacuation and Leak Check

Evacuated to ≤10 mm Hg absolute, monitor for ≥1 hour, and pass for use if no pressure change is noted.

5.4^a

Sample Tank and ICSV Volumes

Weigh empty, fill with deionized distilled water, measure temperature, and weigh to the nearest 2g and record the results. Calculate volume based on density of water at that temperature and record results in permanent file.

^a USEPA Method 25 Protocol Reference Number

Wayne Stollings
QA/QC Officer

TRIANGLE ENVIRONMENTAL SERVICES, INC.
METHOD 25 PROCEDURES

Calibration:

Initial checks and calibrations of the collection and analytical systems are repeated a maximum of three months after the previous calibrations are completed.

The daily calibration gas mixture consists of 50.0 ppm carbon monoxide, 50.9 ppm methane, 25.1 ppm propane, and .989% carbon dioxide. Triplicate injections of this gas are made immediately before and after each set of samples. The response factors (average integrated area/concentration in ppmC) are calculated daily from these injections. The average response factors must agree within 5% of the CO₂ and NMO response factors from the initial performance check. The average response factors for the before and after sets must also agree within 2% of each other before the analyses are considered valid.

Collection:

The trap is maintained at -78 °C while hydrocarbon free air is flushed through to the sample tank via the CO₂ NDIR analyzer. This flushing of CO₂ is continued until no response is noted on the NDIR. The sample tank is then pressurized to about 1060 mmHg and replaced by an intermediate collection vessel (ICV). The trap is then baked at 200 °C with hydrocarbon free air passing through the oxidation catalyst and the NDIR analyzer into the ICV. When no response is noted on the NDIR, an aliquot is injected into the NMO analyzer. Collection continues until the CO₂ concentration falls below 10 ppm as determined by the NMO analyzer. The ICV is then pressurized to about 1060 mmHg and analyzed with the sample tank.

Analysis:

The propane calibration mixture, sample tank, and ICV are analyzed identically using a computer controlled GC/FID with an automated gas sampling system.

A 1 ml aliquot is injected into the GC column, which is maintained at 80 °C. This is to elute CO, CH₄, and CO₂ which pass through the oxidation and reduction catalysts to the FID. The column is then back-flushed to elute the non-methane organic (NMO) fraction, which also passes through the oxidation and reduction catalysts to the FID. Triplicate injections are made for all samples and daily calibrations.

Calculations:

Calculations are done in accord with USEPA Method 25 procedures. A sample calculation for this set is provided. A blank is subtracted from the CO calculations to correct interference caused by the coelution of O₂ with CO. This is a constant value which is solely due to the characteristics of the column set.

Equipment:

Tanks and ICV's are evacuated and filled with ambient air filtered through charcoal twice while being baked at 150 °C. They are then evacuated to below 10 mmHg and monitored for at least an hour for leak checking (no change in pressure within an hour). They are then pressurized over ambient with hydrocarbon free air, analyzed to ensure <10 ppmC, and stored for later use.

Traps are analyzed to confirm less than 10 ppmC as per the collection of a sample, in addition each is then baked at 300 °C for thirty minutes to ensure cleanliness. A random analysis of 10% of the traps is done for an added QA/QC check of handling procedures.

Sample units are reconditioned to ensure clean filters are installed and that they operate properly. A teflon jumper replaces the trap, the unit is heated and is flushed with zero air for at least thirty minutes. An aliquot of this flow is injected into the analyzer. If the concentration of NMO is below 10 ppm the unit is made ready for use and stored for shipment.

TECHNICAL SERVICES, INC.

COMMENTS ON THE ANALYSIS
Report #92022

| | |
|------------------------------------|------------------------------|
| Traps Received: 10/26/92 w/Dry Ice | Tanks Received: 10/26/92 |
| Samples Analyzed: 11/12/92 | Chain-of-custody forms: none |

General: Due to interference caused by the coelution of O_2 with CO the analytical system reports a background concentration of CO. The reported CO concentrations reflect the deduction of a daily "blank" area count. This correction allows for more accurate reporting and comparison of the CO concentration of all analytical runs.

Sample # 3:

Trap CH arrived at TES, Inc. with the cap loose on both the long and short stems.

TRIANGLE ENVIRONMENTAL SERVICES, INC.
METHOD 25 TABLE OF RESULTS

Name: GILBERT COMMUNELACITE

ID: 092022

Date: 11/12/92

| # | Sample Description | Concentrations (ppmC) | | | | | | Mass Conc. (ugC/cm ³ m) |
|---|--------------------|-----------------------|-----------------|-----------------|---------------------|-------------------|------|------------------------------------|
| | | CO | CH ₄ | CO ₂ | Noncon-
denables | Condens-
ables | TGFM | |
| 1 | W-V-1 | 54 | 17 | 25306 | 25 | 219 | 244 | 122 |
| 2 | W-V-2 TRAP ONLY | 75 | 22 | 49189 | 0 | 0 | 0 | 0 |
| 3 | W-V-2 TRAP 1 ONLY | 0 | 0 | 0 | 0 | 750 | 750 | 380 |
| 4 | W-V-2 TRAP 2 ONLY | 0 | 0 | 0 | 0 | 551 | 551 | 275 |
| 5 | W-V-3 | 161 | 33 | 41198 | 0 | 327 | 327 | 163 |

TRIANGLE ENVIRONMENTAL SERVICES, INC.

METHOD 25 SAMPLE CALCULATION

Note: All pressure values have been converted when necessary to mm Hg and all temperature values to Kelvin.

Name: GILBERT COMMOMBEALITE

ID #92022 Date: 11/12/92

Sample # 1 W-V-1

D A T A

| | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|----------|-----------|-----------|--|---------|--|--------------|------|-------|---------------|-------|-------|-------|--------|-------|---|--|----------|-----------|--|---------|--|-------|--------|-------|
| <p>Tank 21:</p> <p>Volume (cu.m) = 0.008347</p> <table border="0"> <tr> <td></td> <td>Pressure</td> <td>Temp. (K)</td> </tr> <tr> <td></td> <td>(mm Hg)</td> <td></td> </tr> <tr> <td>Pre-sampling</td> <td>45.7</td> <td>282.0</td> </tr> <tr> <td>Post-sampling</td> <td>717.0</td> <td>284.3</td> </tr> <tr> <td>Final</td> <td>1155.0</td> <td>298.7</td> </tr> </table> | | Pressure | Temp. (K) | | (mm Hg) | | Pre-sampling | 45.7 | 282.0 | Post-sampling | 717.0 | 284.3 | Final | 1155.0 | 298.7 | <p>Trap AS Collection Vessel:</p> <p>Volume (cu.m) = 0.008317</p> <table border="0"> <tr> <td></td> <td>Pressure</td> <td>Temp. (K)</td> </tr> <tr> <td></td> <td>(mm Hg)</td> <td></td> </tr> <tr> <td>Final</td> <td>1433.0</td> <td>298.7</td> </tr> </table> | | Pressure | Temp. (K) | | (mm Hg) | | Final | 1433.0 | 298.7 |
| | Pressure | Temp. (K) | | | | | | | | | | | | | | | | | | | | | | | |
| | (mm Hg) | | | | | | | | | | | | | | | | | | | | | | | | |
| Pre-sampling | 45.7 | 282.0 | | | | | | | | | | | | | | | | | | | | | | | |
| Post-sampling | 717.0 | 284.3 | | | | | | | | | | | | | | | | | | | | | | | |
| Final | 1155.0 | 298.7 | | | | | | | | | | | | | | | | | | | | | | | |
| | Pressure | Temp. (K) | | | | | | | | | | | | | | | | | | | | | | | |
| | (mm Hg) | | | | | | | | | | | | | | | | | | | | | | | | |
| Final | 1433.0 | 298.7 | | | | | | | | | | | | | | | | | | | | | | | |

Calibration Data:

| | |
|---|--|
| <p>Response Factor (area units/ppmC)</p> <p>CO Blank (area units)</p> | <p>PoreFlush Backflush</p> <p>196.9 183.6</p> <p>501</p> |
|---|--|

Areas:

| | | | |
|-----------------|-----------|-----------|-----------|
| CO | 6,918 | 6,953 | 6,975 |
| CH4 | 1,987 | 1,984 | 2,009 |
| CO2 | 3,032,222 | 3,044,052 | 3,047,046 |
| Noncondensibles | 2,886 | 2,861 | 2,723 |
| Condensibles | 21,511 | 21,233 | 21,140 |

C A L C U L A T I O N S

Measured Concentrations, corrected for blank:

$Cn(CO) = \text{Area}(CO) - CO\text{ Blank} / RF(CO2)$
 $= 6918 - 501 / 196.9 = 32.6$
 $= 6953 - 501 / 196.9 = 32.8$
 $= 6975 - 501 / 196.9 = 32.9$

$Cn(CH4) = \text{Area}(CH4) / RF(CO2)$
 $= 1987 / 196.9 = 10.1$
 $= 1984 / 196.9 = 10.1$
 $= 2009 / 196.9 = 10.2$

$Cn(CO2) = \text{Area}(CO2) / RF(CO2)$
 $= 3032222 / 196.9 = 15399.8$
 $= 3044052 / 196.9 = 15459.9$
 $= 3047046 / 196.9 = 15475.1$

$$\begin{aligned} C_m(\text{Noncondensibles}) &= \text{Area}(\text{Noncondensibles}) / \text{RF}(\text{NMO}) \\ &= 2886 / 183.6 = 15.7 \\ &= 2861 / 183.6 = 15.6 \\ &= 2723 / 183.6 = 14.8 \end{aligned}$$

$$\begin{aligned} C_m(\text{Condensibles}) &= \text{Area}(\text{Condensibles}) / \text{RF}(\text{CO2}) \\ &= 21511 / 196.9 = 109.2 \\ &= 21233 / 196.9 = 107.8 \\ &= 21140 / 196.9 = 107.4 \end{aligned}$$

$$\text{Pressure-Temperature Ratio, Q(1)} = P(1)/T(1)$$

$$\begin{aligned} \text{post-sampling tanks } Q(1) &= 717.042 / 284.2611 = 2.522477 \\ \text{pre-sampling tanks } Q(2) &= 45.72003 / 282.0389 = 0.1621954 \\ \text{final tanks } Q(3) &= 1155 / 299.65 = 3.867464 \\ \text{final CVs } Q(4) &= 1433 / 299.65 = 4.798259 \end{aligned}$$

$$\begin{aligned} \text{Volume Sampled (dscm)} &= 0.3857 \times \text{Tank Volume} \times [Q(1) - Q(2)] \\ &= 0.3857 \times 0.008347 \times [2.5225 - 0.1621] \\ &= 0.007599 \end{aligned}$$

Averages and % Relative Standard Deviations (%RSD) of C_m 's are calculated.
(%RSD of C = %RSD of C_m)

Calculated Concentrations:

$$\begin{aligned} C(\text{CO}) &= Q(3) / [Q(1) - Q(2)] \times C_m(\text{CO}) \\ &= 3.8674 / (2.5225 - 0.1621) \times 32.7 = 53.7 \end{aligned}$$

$$\begin{aligned} C(\text{CH4}) &= Q(3) / [Q(1) - Q(2)] \times C_m(\text{CH4}) \\ &= 3.8674 / (2.5225 - 0.1621) \times 10.1 = 15.6 \end{aligned}$$

$$\begin{aligned} C(\text{CO2}) &= Q(3) / [Q(1) - Q(2)] \times C_m(\text{CO2}) \\ &= 3.8674 / (2.5225 - 0.1621) \times 15444.9 = 25306.1 \end{aligned}$$

$$\begin{aligned} C(\text{Noncondensibles}) &= Q(3) / [Q(1) - Q(2)] \times C_m(\text{Noncondensibles}) \\ &= 3.8674 / (2.5225 - 0.1621) \times 15.4 = 25.2 \end{aligned}$$

$$\begin{aligned} C(\text{Condensibles}) &= \text{Volume}(\text{CV}) / \text{Volume}(\text{Tank}) \times Q(4) / [Q(1) - Q(2)] \times C_m(\text{Condensibles}) \\ &= 0.008317 / 0.008347 \times 4.7983 / (2.5225 - 0.1621) \times 109.1 = 219.1 \end{aligned}$$

$$\begin{aligned} \text{Total Gaseous Non-Hexane Organics (TGNHO)} &= C(\text{Noncondensibles}) + C(\text{Condensibles}) \\ &= 25.2 + 219.1 \\ &= 244.3 \end{aligned}$$

$$\begin{aligned} \text{Mass Concentration} &= 0.4993 \times \text{TGNHO} \\ &= 0.4993 \times 244.3 = 122.0 \end{aligned}$$

TRIANGLE ENVIRONMENTAL SERVICES, INC.

METHOD 25 DATA REPORT

Name: GILBERT COMMONWEALTH

ID #92022 Date: 11/12/92

Sample # 1 W-V-1

TRAP AS

COLLECTION VESSEL:

Volume (cu.m) = 0.008347

Volume (cu.m) = 0.008317

| | Pressure
(mm. Hg) | Temp. (K) | | Pressure
(mm. Hg) | Temp. (K) |
|--------------|----------------------|-----------|-------|----------------------|-----------|
| Presampling | 45.7 | 292.0 | | | |
| Postsampling | 717.0 | 294.3 | | | |
| Final | 1155.0 | 298.7 | Final | 1433.0 | 298.7 |

Volume Sampled (dscm) = 0.007599

Calibration Data:

| | CO2 | Backflush |
|-----------------------------------|-------|-----------|
| Response Factor (area units/ppmC) | 196.9 | 183.6 |
| CO Blank (area units) | 501 | |

Areas:

| | | | |
|-----------------|-----------|-----------|-----------|
| CO | 6,918 | 6,953 | 6,975 |
| CH4 | 1,987 | 1,984 | 2,009 |
| CO2 | 3,032,222 | 3,044,052 | 3,047,046 |
| Noncondensibles | 2,886 | 2,861 | 2,723 |
| Condensibles | 21,511 | 21,233 | 21,140 |

Concentrations (ppmC):

| | ORSD |
|-----------------|------------|
| CO | 53.6533 |
| CH4 | 16.5872 |
| CO2 | 25306.1000 |
| Noncondensibles | 25.1953 |
| Condensibles | 219.0609 |
| TGNMCO | 244.2567 |

(= 121.9574 mgC/cu.m)

TRIANGLE ENVIRONMENTAL SERVICES, INC.

METHOD 25 DATA REPORT

Name: GILBERT COMMUNITARIAN

ID #92022 Date: 11/12/92

Sample # 2 0-0-2 TRNK ONLY

TANK 121:

Volume (cu.cm) = 0.008353

TRAP @

COLLECTION VESSEL:

Volume (cu.cm) = 0.008369

| | Pressure
(mm Hg) | Temp. (K) | | Pressure
(mm Hg) | Temp. (K) |
|---------------|---------------------|-----------|-------|---------------------|-----------|
| Pre-sampling | 12.2 | 285.9 | | | |
| Post-sampling | 402.3 | 287.6 | | | |
| Final | 1234.0 | 298.7 | Final | 0.0 | 273.2 |

Volume Sampled (discm) = 0.004370

Calibration Data:

| | CO2 | Backflush |
|-----------------------------------|-------|-----------|
| Response Factor (area units/ppmC) | 196.9 | 183.6 |
| CO Blank (area units) | 501 | |

Areas:

| | | | |
|-----------------|-----------|-----------|-----------|
| CO | 5,335 | 5,389 | 5,329 |
| CH4 | 1,443 | 1,451 | 1,438 |
| CO2 | 3,179,008 | 3,185,049 | 3,173,824 |
| Noncondensibles | 0 | 0 | 0 |
| Condensibles | 0 | 0 | 0 |

Concentrations (ppmC):

| | | WSTD |
|-----------------|------------|--------|
| CO | 75.0384 | 0.6814 |
| CH4 | 22.3413 | 0.4541 |
| CO2 | 49189.4900 | 0.1767 |
| Noncondensibles | 0.0000 | 0.0000 |
| Condensibles | 0.0000 | 0.0000 |
| TGMSO | 0.0000 | |

(= 0.0000 mgC/cu.cm)

TRIANGLE ENVIRONMENTAL SERVICES, INC.

METHOD 25 DATA REPORT

Name: GILBERT COMMONWEALTH

ID #92022 Date: 11/12/92

Sample # 3 M-W-2 TRAP 1 ONLY

TANK 121:

Volume (cu.m) = 0.008353

TRAP CH

COLLECTION VESSEL:

Volume (cu.m) = 0.008369

| | Pressure
(mm Hg) | Temp. (K) | | Pressure
(mm Hg) | Temp. (K) |
|--------------|---------------------|-----------|-------|---------------------|-----------|
| Presampling | 12.2 | 295.9 | | | |
| Postsampling | 199.6 | 296.5 | | | |
| Final | 0.0 | 273.2 | Final | 1401.0 | 298.7 |

Volume Sampled (dscm) = 0.002108

Calibration Data:

| | CO2 | Backflash |
|-----------------------------------|-------|-----------|
| Response Factor (area units/ppmC) | 196.9 | 183.6 |
| CO Blank (area units) | 501 | |

Areas:

| | | | |
|-----------------|--------|--------|--------|
| CO | 0 | 0 | 0 |
| CH4 | 0 | 0 | 0 |
| CO2 | 0 | 0 | 0 |
| Noncondensibles | 0 | 0 | 0 |
| Condensibles | 20,819 | 20,927 | 20,758 |

Concentrations (ppmC):

| | ORSD |
|-----------------|----------|
| CO | 0.0000 |
| CH4 | 0.0000 |
| CO2 | 0.0000 |
| Noncondensibles | 0.0000 |
| Condensibles | 760.1723 |
| TEGMO | 760.1723 |

(= 379.5539 mgC/cu.m)

TRIANGLE ENVIRONMENTAL SERVICES, INC.

METHOD 25 DATA REPORT

Name: GILBERT COMBOWELAKE

ID #92022 Date: 11/12/92

Sample # 4 T-4-2 TRAP 2 ONLY

TRAP 121:

TRAP BK

COLLECTION VESSEL:

Volume (ccm) = 0.008353

Volume (ccm) = 0.008353

| | Pressure
(mm Hg) | Temp. (K) | | Pressure
(mm Hg) | Temp. (K) |
|---------------|---------------------|-----------|-------|---------------------|-----------|
| Pre-sampling | 220.0 | 286.5 | | | |
| Post-sampling | 402.3 | 287.6 | | | |
| Final | 0.0 | 273.2 | Final | 1574.0 | 298.7 |

Volume Sampled (ccm) = 0.002033

Calibration Data:

| | CO2 | BackFlush |
|-----------------------------------|-------|-----------|
| Response Factor (area units/ppmC) | 196.9 | 183.6 |
| CO Blank (area units) | 501 | |

Areas:

| | | | |
|-----------------|--------|--------|--------|
| CO | 0 | 0 | 0 |
| CH4 | 0 | 0 | 0 |
| CO2 | 0 | 0 | 0 |
| Noncondensibles | 0 | 0 | 0 |
| Condensibles | 12,391 | 13,371 | 13,007 |

Concentrations (ppmC):

| | GRSD |
|-----------------|----------|
| CO | 0.0000 |
| CH4 | 0.0000 |
| CO2 | 0.0000 |
| Noncondensibles | 0.0000 |
| Condensibles | 550.8752 |
| TGROD | 550.8752 |

(= 275.0520 mgC/ccm)

TRIANGLE ENVIRONMENTAL SERVICES, INC.

METHOD 25 DATA REPORT

Name: GILBERT COMMONWEALTH

ID #92022 Date: 11/12/92

Sample # 5 W-V-3

TANK 140:

Volume (cc.m) = 0.008373

TRAP HB

COLLECTION VESSEL:

Volume (cc.m) = 0.008333

| | Pressure
(mm Hg) | Temp. (K) | | Pressure
(mm Hg) | Temp. (K) |
|--------------|---------------------|-----------|-------|---------------------|-----------|
| Presampling | 14.2 | 278.7 | | | |
| Postsampling | 385.1 | 283.7 | | | |
| Final | 1127.0 | 298.7 | Final | 1309.0 | 298.7 |

Volume Sampled (dscm) = 0.004218

Calibration Data:

| | CO2 | Backflush |
|-----------------------------------|-------|-----------|
| Response Factor (area units/ppmC) | 196.9 | 183.6 |
| CO Blank (area units) | 501 | |

Areas:

| | | | |
|-----------------|-----------|-----------|-----------|
| CO | 7,307 | 7,361 | 7,386 |
| CH4 | 2,251 | 2,259 | 2,296 |
| CO2 | 2,783,753 | 2,806,597 | 2,814,944 |
| Noncondensibles | 0 | 0 | 0 |
| Condensibles | 19,243 | 19,325 | 19,195 |

Concentrations (ppmC):

| | 96SD |
|-----------------|------------|
| CO | 100.5096 |
| CH4 | 33.3353 |
| CO2 | 41108.1100 |
| Noncondensibles | 0.0000 |
| Condensibles | 326.5531 |
| TGNDCO | 326.5531 |

(= 153.0505 mgC/cc.m)

APPENDIX V
RAW FIELD DATA

APPENDIX W

RCAPW FIELD DATA

- 5.1 Particulate
- 5.2 Volatile Organic Compounds
- 5.3 Visible Emissions

APPENDIX W RAW FIELD DATA

5.1 Particulate

Client W. O. No.

VERY IMPORTANT - FILL IN ALL BLANKS

W. O. No. _____

Plant RESEARCH

Read and record at the start of each test point

Run No. 11-8-1

SWITCH

48.4%

Location Explosive Outfit

Date 10/21/72

0.0003

Operator ROLAND

Sample Box No. _____

Water Box No. 2100

Water ΔH _____

C Factor _____

Pitot Calibration

Trimble No. _____

Filter No. _____

Ambient Temp. of 55

Bar. Press. "Hg 27.98

Assumed Moisture 2.97%

Heater Box Setting, of _____

Probe Tip Dia., in. 0.215

Probe Length 5'

Probe Heater Setting _____

Avg. ΔP _____

Avg. ΔH _____

| POINT | DISTANCE IN FEET | CLOCK TIME | DRY GAS METER, CF | PITOT IN. H ₂ O ΔP | ORIFICE ΔH IN. H ₂ O | DRY GAS TEMP. OF | PUMP VACUUM IN. HG GAUGE | BOX TEMP. OF | ENGINEER TEMP. OF | STAR TEMP. OF |
|-------|------------------|------------|-------------------|---------------------------------------|---|--------------------|--------------------------|--------------|-------------------|---------------|
| 1 | 237 | 0.0 | 133.137 | 3.00 | DES. 3.00 ACT. 3.00 | INLET 60 OUTLET 62 | 2 | 60 | 60 | 60 |
| 2 | 315 | 0.0 | 135.2 | 3.60 | DES. 3.60 ACT. 3.60 | INLET 64 OUTLET 64 | 2 | 60 | 60 | 60 |
| 3 | 375 | 0.0 | 142.4 | 3.70 | DES. 3.70 ACT. 3.70 | INLET 68 OUTLET 68 | 2 | 60 | 60 | 60 |
| 4 | 435 | 0.0 | 146.0 | 3.71 | DES. 3.71 ACT. 3.71 | INLET 68 OUTLET 68 | 2 | 60 | 60 | 60 |
| 5 | 495 | 0.0 | 148.1 | 3.71 | DES. 3.71 ACT. 3.71 | INLET 68 OUTLET 68 | 2 | 60 | 60 | 60 |
| 6 | 555 | 0.0 | 150.515 | 3.71 | DES. 3.71 ACT. 3.71 | INLET 68 OUTLET 68 | 2 | 60 | 60 | 60 |
| 7 | 615 | 0.0 | 152.515 | 3.70 | DES. 3.70 ACT. 3.70 | INLET 68 OUTLET 68 | 2 | 60 | 60 | 60 |
| 8 | 675 | 0.0 | 153.9 | 3.70 | DES. 3.70 ACT. 3.70 | INLET 68 OUTLET 68 | 2 | 60 | 60 | 60 |
| 9 | 735 | 0.0 | 154.5 | 3.70 | DES. 3.70 ACT. 3.70 | INLET 68 OUTLET 68 | 2 | 60 | 60 | 60 |
| 10 | 795 | 0.0 | 156.6 | 3.71 | DES. 3.71 ACT. 3.71 | INLET 68 OUTLET 68 | 2 | 60 | 60 | 60 |
| 11 | 855 | 0.0 | 158.8 | 3.70 | DES. 3.70 ACT. 3.70 | INLET 68 OUTLET 68 | 2 | 60 | 60 | 60 |
| 12 | 915 | 0.0 | 160.8 | 3.70 | DES. 3.70 ACT. 3.70 | INLET 68 OUTLET 68 | 2 | 60 | 60 | 60 |
| 13 | 975 | 0.0 | 162.77 | 3.70 | DES. 3.70 ACT. 3.70 | INLET 68 OUTLET 68 | 2 | 60 | 60 | 60 |

COMMENTS:

START

PARTICULATE FIELD DATA
(continued)

Client W. O. No.

W. O. No. 100000

Plant Refrigerant

Location Refrigerant

Run No. 100000

Date 10/21/68

| POINT | DISTANCE
IN
INCHES | CLOCK
TIME
ACTUAL RUN | DRY GAS
ENTER, CF | PILOT
IN. H ₂ O
Δ P | ORIFICE A/H
IN. H ₂ O | | DRY GAS TEMP.
OF | | PUMP
VACUUM
IN. HG
GAUGE | BOX
TEMP
OF | IMPINGER
TEMP
OF | STACK
TEMP
OF |
|-------|--------------------------|-----------------------------|----------------------|--------------------------------------|-------------------------------------|--------|---------------------|--------|-----------------------------------|-------------------|------------------------|---------------------|
| | | | | | DESIRABLE | ACTUAL | INLET | OUTLET | | | | |
| 1 | 112.2 | 0.0 | 162.500 | 1.250 | | 1.943 | 76 | 70 | 1 | 60 | 252 | 347 |
| 2 | | 3.5 | 165.20 | 0.666 | | 0.704 | 83 | 71 | 1 | | | 347 |
| 3 | | 7.0 | 166.8 | 0.336 | | 0.377 | 84 | 72 | 1 | | | 345 |
| 4 | | 10.5 | 168.3 | 0.134 | | 0.390 | 84 | 72 | 1 | | | 345 |
| 5 | | 14.0 | 169.5 | 0.136 | | 0.370 | 83 | 72 | 1 | | | 345 |
| 570P | 1140 | 17.5 | 170.638 | | | | | | | | | |
| 570 | 1147 | 0.0 | 170.638 | 1.05 | | 1.137 | 78 | 74 | 1 | | | 332 |
| 6 | | 3.5 | 172.0 | 0.27 | | 0.225 | 81 | 74 | 1 | | | 332 |
| 7 | | 7.0 | | 0.11 | | 0.107 | 80 | 74 | 1 | | | 332 |
| 8 | | 10.5 | 174.8 | 0.11 | | 0.109 | 74 | 74 | 1 | | | 332 |
| 570P | 1207 | 14.0 | 175.5 | 0.11 | | 0.107 | 76 | 74 | 1 | | | 332 |
| 570 | | 17.5 | 176.318 | | | | | | | | | 332 |
| 9 | 1210 | 0.0 | 176.318 | 0.56 | | 0.604 | 74 | 72 | 1 | | | 330 |
| 10 | | 3.5 | 177.8 | 0.27 | | 0.218 | 80 | 74 | 1 | | | 330 |
| 11 | | 7.0 | 179.3 | 0.08 | | 0.244 | 81 | 74 | 1 | | | 330 |
| 12 | | 10.5 | 181.4 | 0.15 | | 0.274 | 82 | 74 | 1 | | | 330 |
| 13 | | 14.0 | 183.4 | 0.04 | | 0.297 | 82 | 74 | 1 | | | 330 |
| 570P | 1208 | 17.5 | 183.564 | | | | | | | | | |

COMMENTS:

(not back 12" = 0.017)

0.016
- 0.016
- 0.014

Run Date: 10/21/03
Run By: J11-1001
Sample Ion No: _____
Operator: J11-1001
Station: J11-1001
V. of No.: _____
Place: J11-1001
Sampling Location: J11-1001

Subcategory: Language

| | |
|--------------|---------------|
| En 100 | En 1000 |
| En 100 | En 1000 |

[illegible]

Questo ha permesso di scoprire _____

| FILE NO. | FILE NO. | FILE NO. |
|----------|----------|----------|
| | | |
| | | |
| | | |
| | | |
| | | |

Plata presentada por: _____ \$

FROM ECLF Sub Model 50

Aptamer Conjugate and Water Wash of Aptamer Conjugation and Lock Half of Protein Binding

Lab No. _____ Ethanol-Chloroform = _____
Zinc acetate = _____ 24

Collected on 0.25 liter _____ 31

Aqueduct: Pasadena 18 11

**Exploiter, Constructed and Lack Skill of
Player Holder - Acquiring Basic**

| Lab No. | Revised | Ref |
|---------|---------|-----|
| 1 | 2 | 3 |

BAGGAGE TAGS: Stamp "To Card" _____ (10)

STUD. WISCONSIN _____

[illegible]

Alkhalaf, Ghol

Weekday after noon 257

Vol. 91, no. 1, 1996

??

[illegible]

CONTRACT NO. 1 1 1 6

WYOM. HERBERT-SILVER-GOLD 27

TOTAL, VOLUME, INSTRUCTIONS 373

TOTAL MEASURE 299

Commeço :

DATE RECEIVED _____

DATE REPORTED:

0033-4673 1.2/ 74

[illegible]

PARTICULATE FIELD DATA

VERY IMPORTANT - FILL IN ALL BLANKS

Pilot Calibration

W. O. No. _____
 Plant Boiler
 Run No. 61 P 2
 Location Boiler Room
 Date 11/10/66
 Operator W. O.
 Sample Box No. _____
 Meter Box No. 110 Yc 100
 Meter ΔH _____
 G Factor _____

Sketch

Read and record at the start of each test point

Thimble No. _____
 Filter No. _____
 Ambient Temp. 41
 Bar. Press. 30.17
 Assumed Moisture 2.77%
 Heater Box Setting, 07
 Probe Tip Dia., in. 0.211
 Probe Length 4 1/2"
 Probe Heater Setting _____

Avg. ΔT _____ Avg. ΔH _____

| POINT | DISTANCE IN FEET | CLOCK TIME | ACTUAL RUN TIME | DRY GAS METER, CF | PITOT IN. H ₂ O ΔP | ORIFICE ΔH IN. H ₂ O | | DRY GAS TEMP. OF | | PUMP VACUUM IN. HG GAGE | BOX TEMP. OF | HEATER TEMP. OF | STACK TEMP. OF |
|-------|------------------|------------|-----------------|-------------------|---------------------------------------|---|--------|------------------|--------|-------------------------|--------------|-----------------|----------------|
| | | | | | | DESIGNED | ACTUAL | INLET | OUTLET | | | | |
| 1 | 20.0 | 0.00 | 0.00 | 184.67 | 0.32 | 0.261 | 0.261 | 40 | 111 | 0 | 240 | 73 | 130 |
| 2 | 40.0 | 0.00 | 0.00 | 185.0 | 0.32 | 0.484 | 0.484 | 40 | 112 | 0 | 240 | 73 | 140 |
| 3 | 60.0 | 0.00 | 0.00 | 186.5 | 0.34 | 0.499 | 0.499 | 40 | 112 | 0 | 240 | 73 | 140 |
| 4 | 80.0 | 0.00 | 0.00 | 187.0 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 5 | 100.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 6 | 120.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 7 | 140.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 8 | 160.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 9 | 180.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 10 | 200.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 11 | 220.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 12 | 240.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 13 | 260.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 14 | 280.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 15 | 300.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 16 | 320.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 17 | 340.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 18 | 360.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 19 | 380.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |
| 20 | 400.0 | 0.00 | 0.00 | 187.9 | 0.34 | 0.500 | 0.500 | 40 | 112 | 0 | 240 | 73 | 140 |

COMMENTS: _____

92.0

92.0

92.0

PARTICULATE FIELD DATA (continued)

Sheet 2 of 7

Client Boeing

W.O. No. 9410

Plane Boeing 747

Location Boeing 747

Run No. 102

Date 11/22/82

| POINT | DISTANCE
IN
INCHES | CLOCK
TIME
ACTUAL | DRY GAS
METER, CF | PITOT
IN. H ₂ O
Δ P | ORIFICE Δ H
IN. H ₂ O | | DRY GAS TEMP.
OF | | PUMP
VACUUM
IN. HG
GAUGE | BOX
TEMP
OF | FINGER
TEMP
OF | STACK
TEMP.
OF |
|-------|--------------------------|-------------------------|----------------------|--------------------------------------|-------------------------------------|--------|---------------------|--------|-----------------------------------|-------------------|----------------------|----------------------|
| | | | | | DESIR | ACTUAL | INLET | OUTLET | | | | |
| 0-1 | | 0753 | 201.190 | 1.20 | | 1.30 | 52 | 48 | 1 | 250 | 45 | 344 |
| 1 | | 0754 | 203.6 | 0.85 | | 0.93 | 60 | 50 | 1 | | | 343 |
| 2 | | 0755 | 205.8 | 0.61 | | 0.67 | 61 | 50 | 0 | | | 347 |
| 3 | | 0756 | 207.6 | 0.50 | | 0.55 | 63 | 50 | 1 | | | 343 |
| 4 | | 0757 | 209.6 | 0.40 | | 0.47 | 63 | 51 | 0 | | | 340 |
| 5 | | 0813 | 211.705 | | | | | | | | | |
| 6-7 | | 0817 | 211.705 | 2.00 | | 2.21 | 58 | 50 | 0 | | | 341 |
| 8 | | 0818 | 213.1 | 1.80 | | 1.95 | 66 | 51 | 0 | | | 343 |
| 9 | | 0819 | 217.9 | 1.15 | | 1.10 | 66 | 52 | 1 | | | 347 |
| 10 | | 0820 | 220.9 | 0.77 | | 0.84 | 66 | 52 | 1 | | | 343 |
| 11 | | 0821 | 222.3 | 0.80 | | 0.87 | 63 | 52 | 1 | | | 352 |
| 12 | | 0822 | 224.02 | | | | | | | | | |
| 13 | | 0840 | 224.402 | 2.40 | | 2.61 | 61 | 52 | 2 | | | 343 |
| 14 | | 0841 | 228.0 | 2.70 | | 3.15 | 70 | 52 | 3 | | | 353 |
| 15 | | 0842 | 231.5 | 2.10 | | 2.50 | 74 | 56 | 3 | | | 353 |
| 16 | | 0843 | 234.5 | 1.10 | | 1.61 | 74 | 56 | 2 | | | 354 |
| 17 | | 0844 | 239.5 | 1.70 | | 1.85 | 82 | 58 | 2 | | | 349 |
| 18 | | 0845 | 240.145 | | | | | | | | | |

0.001

11/22/82
 11/22/82
 11/22/82

RUN NUMBER: 125000
 RUN DATE: 12-1-77
 SERIAL RUN NO.:
 OPERATOR: J. A. J.

Name: John A. Smith
 E. O. No.: 1
 Place: 12345 Main St.
 Sampling locations: 100 ft. from shore

Laboratory: 19 (Nov 1, 01)

| | |
|--------------|---------------|
| Lab No. | Ex Date |
| Lab No. | Ex Date |

| Author(s) | Year | Journal |
|---------------------|------|-------------------------------|
| Chen, H. and Li, J. | 2015 | Journal of Management Science |
| Chen, H. and Li, J. | 2016 | Journal of Management Science |
| Chen, H. and Li, J. | 2017 | Journal of Management Science |
| Chen, H. and Li, J. | 2018 | Journal of Management Science |
| Chen, H. and Li, J. | 2019 | Journal of Management Science |
| Chen, H. and Li, J. | 2020 | Journal of Management Science |
| Chen, H. and Li, J. | 2021 | Journal of Management Science |
| Chen, H. and Li, J. | 2022 | Journal of Management Science |
| Chen, H. and Li, J. | 2023 | Journal of Management Science |
| Chen, H. and Li, J. | 2024 | Journal of Management Science |
| Chen, H. and Li, J. | 2025 | Journal of Management Science |

*Obtain for personal use only, per _____ of _____

[illegible]

Plot of particle size and ϕ : _____

PROJECT TOTAL Sub Total _____ 11

Inspector General and Major Work of Inspector General

Lab No. Robert-Coleman
Bureau ng

Collected on 0.42. 1956 on _____

Aqueduct - Juncalhue 100

**Emphasis, Consistency and Back Half of
Pitcher Holding a Winning Game**

Lab Sec. _____ Dist. Sec. _____

BACHELOR'S DEGREE REPORT _____ OF _____

[illegible]

Long Runners

| | |
|-----------------|-----|
| Label: 00000000 | 300 |
| Final Volume | 300 |
| Initial Volume | 300 |
| Sr: 90.0mm | 300 |

34.4.34. God.

Weight after race: 45.91

Wavelength before onset: 239

Date: 6/2/2016

Continuation No. 1 1. _____ 2. _____ 3. _____ 4. _____

WORLD WITCHES-SLEAZES GO! 69

ISSN: 0013-788X 2000 Vol. 29 No. 1 1-10

TOTAL HOLETIDE 357

Comments: _____

DATE: DATA RECEIVED:
DATA APPROVED:

Sheet 1 of 2

PARTICULARS FIELD DATA

Client W. D. S. Co.

H. O. No. _____

Plant Portland

Run No. 117

Location Bachman culvert

Date 10/1/61

Operator Runo

Sample Box No. _____

Water Box No. 3109 1/2 1.00

Water Δ h _____

C Factor _____

VERY IMPORTANT - FILL IN ALL SPACES

Read and record at the start of each test point

SKETCH

0.0000

0.0000



Pitot Calibration

Thimble No. _____

Filter No. _____

Ambient Temp. $^{\circ}$ F _____

Bar. Press. $^{\circ}$ Hg 30.27

Assumed Moisture $\%$ 22.07

Monitor Box Setting, $^{\circ}$ F _____

Probe Tip Dia., In. 0.215

Probe Length 9.5

Probe Monitor Setting _____

Avg. Δ P _____

Avg. Δ h _____

| POINT | DISTANCE IN INCHES | CLOCK TIME | DRY GAS WATER, CF | PITOT IN. H ₂ O Δ P | ORIFICE A H IN. H ₂ O | | DRY GAS TEMP. $^{\circ}$ F | | PUMP VACUUM IN. Hg gauge | BOX TEMP. $^{\circ}$ F | INTIMID. TEMP. $^{\circ}$ F | TRACK RECD. $^{\circ}$ F |
|-------|--------------------|------------|-------------------|---------------------------------------|----------------------------------|--------|----------------------------|--------|--------------------------|------------------------|-----------------------------|--------------------------|
| | | | | | DESIRED | ACTUAL | INLET | OUTLET | | | | |
| 1 | | 0940 | 240.481 | 2.20 | | 2.35 | 50 | 52 | 1 | 22.0 | 57 | 340 |
| 2 | | 0945 | 243.1 | 2.00 | | 3.10 | 64 | 57 | 2 | | | 340 |
| 3 | | 0950 | 247.4 | 2.20 | | 2.07 | 74 | 56 | 2 | | | 341 |
| 4 | | 0955 | 250.7 | 1.00 | | 4.95 | 68 | 58 | 2 | | | 347 |
| 5 | | 1000 | 253.5 | 1.00 | | 1.72 | 64 | 58 | 1 | | | 339 |
| 6 | | 1005 | 256.291 | | | | | | | | | |
| 7 | | 1010 | 259.191 | 1.90 | | 2.08 | 58 | 58 | 2 | | | 340 |
| 8 | | 1015 | 260.3 | 1.70 | | 1.87 | 60 | 58 | 2 | | | 340 |
| 9 | | 1020 | 261.7 | 0.95 | | 1.91 | 76 | 58 | 2 | | | 340 |
| 10 | | 1025 | 264.2 | 0.77 | | 0.98 | 60 | 58 | 2 | | | 349 |
| 11 | | 1030 | 266.7 | 0.57 | | 0.64 | 60 | 58 | 2 | | | 348 |
| 12 | | 1035 | 268.715 | | | | | | | | | |

COMMENTS:

0.0000

-0.06

0.0000

PARTICULATE FIELD DATA
(continued)

Sheet 2 of 2

Client SAIC

W.O. No. 9-10178

Plant Rockwell

Location Rockwell 0.461

Run No. 0-10178

Date 10/10/92

| POINT | DISTANCE
IN
INCHES | CLOCK
TIME | | DRY GAS
VOLUME, CF | PITOT
IN. H ₂ O
Δ P | ORIFICE Δ H
IN. H ₂ O | | DRY GAS
TEMP.
OF | | PUMP
VACUUM
IN. HG
Gauge | BOX
TEMP.
OF | FINGER
TEMP.
OF | THERMISTOR
TEMP.
OF |
|-------|--------------------------|---------------|------|-----------------------|--------------------------------------|-------------------------------------|--------|------------------------|--------|-----------------------------------|--------------------|-----------------------|---------------------------|
| | | ACTUAL | RUN | | | DESIR. | ACTUAL | INLET | OUTLET | | | | |
| 1 | | 1025 | 1025 | 268.975 | 0.21 | | 1.70 | 58 | 58 | 0 | 250 | 50 | 351 |
| 2 | | | | 270.4 | 0.66 | | 0.66 | 65 | 58 | 0 | | | 350 |
| 3 | | | | 271.2 | 0.50 | | 0.54 | 65 | 58 | 0 | | | 350 |
| 4 | | | | 277.0 | 0.58 | | 0.60 | 65 | 58 | 0 | | | 350 |
| 5 | | | | 275.0 | 0.75 | | 0.81 | 65 | 59 | 0 | | | 350 |
| 6 | | 1045 | 1045 | 277.522 | | | | | | | | | |
| 7 | | 1048 | 1048 | 277.522 | 0.66 | | 0.71 | 60 | 58 | 0 | | | 348 |
| 8 | | | | 279.4 | 0.28 | | 0.40 | 60 | 60 | 0 | | | 345 |
| 9 | | | | 280.8 | 0.70 | | 0.79 | 77 | 67 | 0 | | | 340 |
| 10 | | | | 281.3 | 0.63 | | 0.67 | 64 | 67 | 0 | | | 340 |
| 11 | | 1052 | 1052 | 284.1 | 0.80 | | 0.86 | 70 | 68 | 0 | | | 348 |
| 12 | | | | 286.120 | | | | | | | | | |
| 13 | | 1112 | 1112 | 286.120 | 0.31 | | 0.33 | 67 | 67 | 0 | 242 | 27 | 340 |
| 14 | | | | 287.8 | 0.29 | | 0.29 | 70 | 69 | 0 | | | 340 |
| 15 | | | | 288.7 | 0.35 | | 0.37 | 71 | 69 | 0 | | | 340 |
| 16 | | | | 289.1 | 0.65 | | 0.70 | 73 | 69 | 0 | | | 340 |
| 17 | | 1132 | 1132 | 292.0 | 0.65 | | 0.73 | 74 | 68 | 0 | | | 340 |
| 18 | | | | 293.814 | | | | | | | | | |

9.56
10.10
10.10

10.10

10.10

10.10

10.10

REF ID: A64796

APPENDIX V

RAW FIELD DATA

5.2 Volatile Organic Compounds

VOC ANALYSIS METHOD PER 25

CLIENT Winstar S. Pa.

DATE 10/22/92

LOCATIONS Boysen's Exhaust

RUN NO. 0-V-1

| START TIME | MINUTES | Baro METER | TEMPERATURE | | FLOW RATE | VACUUM |
|------------|---------|------------|-------------|------|------------|--------|
| | | | °F | °C | liters/min | |
| 0733 | 0 | 30.30 | | | 6.5 | 31.9 |
| | 5 | | | | 6.5 | 25.6 |
| | 10 | | 25.4 | 26.5 | 6.5 | 23.0 |
| | 15 | | 25.0 | 26.4 | 6.5 | 20.4 |
| | 20 | | 24.9 | 26.5 | 6.5 | 17.9 |
| | 25 | | 25.0 | 26.6 | 6.5 | 14.3 |
| | 30 | | 25.2 | 26.3 | 6.5 | 12.3 |
| | 35 | | 25.1 | 26.5 | 6.5 | 10.0 |
| | 40 | | 25.7 | 26.5 | 6.5 | 9.3 |
| | 45 | | 24.9 | 26.5 | 6.5 | 6.2 |
| | 50 | | 24.8 | 26.5 | 6.5 | 4.2 |
| 0828 | 55 | 30.23 | 24.6 | 26.5 | 6.5 | 2.0 |
| | 60 | | | | | |

LEAK TEST PROCEDURE with probe mounted in place and connected,

1. Turn stop-cock to flow ambient air only.
2. Turn on pump and open coarse valve (red handle).
3. Open roto-meter to permit good (over 1 liter/minute) air flow.
4. Visually observe air bubbling through all impingers, and make sure gas meter dial moves.
5. Turn stop-cock to close off flow to impingers.
6. Adjust flow knob on control box to obtain 10" of vacuum.
7. Visually observe roto-meter ball fall to zero flow.
8. Visually observe bubbling in impingers. Bubbling should stop. (A single, small bubble once every few seconds is acceptable).
9. Dry gas meter dial should not move at all.
10. Carefully turn stop-cock to allow ambient air flow through impingers. Do not allow stack gas to enter. Observe bubbling and meter operation.
11. Begin to close roto-meter until low flow (0.4 liter/minute) rate is achieved.
12. Shut off red valve and pump.
13. Perform leak test before and after test.

TO SAMPLE

- (1) Heat glassware and stop-cock in hot box.
- (2) Use Dyna-pump to purge stack gas thru stop-cock; then rotate stop-cock to flow stack gas only and adjust roto-meter to obtain 0.4 liter/min flow rate.

Total sample must not exceed 1 cubic foot in one hour.

Drsat CO₂ readings are required!

| DRSAT | | |
|-----------------|--|----------------|
| CO ₂ | | O ₂ |
| | | |
| | | |
| | | |
| | | |

BAROMETER 30.20

CONTROL BOX

Y

UO2 DRY METHOD TEST 25

CLIENT WINDSOR 5, INC. DATE 10/22/91

LOCATION Regency Forest RUN NO. 40-V-2

| START TIME | MINUTES | CO ₂ METER | TEMPERATURE
C _{air} C _{probe} | FLOW RATE
L/min | VACUUM
mmHg |
|------------|---------|-----------------------|--|--------------------|----------------|
| 1045 | 0 | 30.18 | 233 266 | 65 | 29.8 |
| 56 | 5 | | 247 266 | 65 | 29.6 |
| 6 | 10 | | 256 265 | 65 | 27.3 |
| 16 | 15 | | 252 266 | 65 | 26.2 |
| 11 | 20 | | 248 265 | 65 | 25.0 |
| 16 | 25 | | 248 265 | 65 | 23.7 |
| 21 | 30 | | 247 265 | 65 | 22.4 |
| 1145 | 35 | | 230 261 | 65 | 21.6 |
| 56 | 40 | | 235 265 | 65 | 20.4 |
| 55 | 45 | 30.24 | 247 265 | 65 | 19.2 |
| 60 | 50 | | 260 265 | 65 | 17.8 |
| 65 | 55 | | 256 265 | 65 | 16.6 |
| 10 | 60 | | 251 265 | | 14.4 |

30 inches Hg
leak seal
purge at 1145
5 min

stop at 1045
Trap clogged
replace trap
purge 5 min
restart 1145

ORSAT 58

| CO ₂ | O ₂ |
|-----------------|----------------|
| | |
| | |
| | |
| | |
| | |

LEAK TEST PROCEDURE with probe mounted in place and connected,

1. Turn stop-cock to flow ambient air only.
2. Turn on pump and open coarse valve (red handle).
3. Open roto-meter to permit good (over 1 liter/minute) air flow.
4. Visually observe air bubbling through all impingers, and make sure gas meter dial moves.
5. Turn stop-cock to close off flow to impingers.
6. Adjust flow knob on control box to obtain 10" of vacuum.
7. Visually observe roto-meter ball fall to zero flow.
8. Visually observe bubbling in impingers. Bubbling should stop. (A single, small bubble once every few seconds is acceptable).
9. Dry gas meter dial should not move at all.
10. Carefully turn stop-cock to allow ambient air flow through impingers. Do not allow stack gas to enter. Observe bubbling and meter operation.
11. Begin to close roto meter until low flow (0.4 liter/minute) rate is achieved.
12. Shut off red valve and pump.
13. Perform leak test before and after test.

BAROMETER

CONTROL BOX

Y =

TO SAMPLE

- (1) Heat glassware and stop-cock in hot box.
- (2) Use Dyna-pump to purge stack gas thru stop-cock; then rotate stop-cock to flow stack gas only and adjust roto-meter to obtain 0.4 liter/min flow rate.

Total sample must not exceed 1 cubic foot in one hour.

Orsat CO₂ readings are required!

VOLU-MET METHOD SET 2.5

CLIENT Windsor

DATE 10/23/92

LOCATION Booths East

RUN NO. 0-0-3

| START TIME | MINUTES | Baro
METER | TEMPERATURE
F | TEMPERATURE
C | FLOW RATE
cc/min | VACUUM |
|------------|---------|---------------|------------------|------------------|---------------------|--------|
| 0714 | 0 | 30.10 | 251 | 265 | 65 | 29.6 |
| 23 | 5 | | 250 | 265 | 65 | 28.4 |
| 24 | 10 | | 251 | 265 | 65 | 27.1 |
| 33 | 15 | | 249 | 265 | 65 | 25.7 |
| 34 | 20 | | 250 | 265 | 65 | 24.2 |
| 43 | 25 | | 251 | 265 | 65 | 23.2 |
| 44 | 30 | | 250 | 265 | 65 | 22.1 |
| 53 | 35 | | 253 | 265 | 65 | 20.7 |
| 63 | 40 | | 250 | 265 | 65 | 19.7 |
| 04 | 45 | | 251 | 265 | 65 | 18.0 |
| 13 | 50 | | 251 | 266 | 65 | 16.7 |
| 0923 14 | 55 | | 249 | 264 | 65 | 16.2 |
| 135 23 | 60 | 30.10 | 251 | 265 | | 15.0 |

Leak rate 29.7
dead
purge at 42
65 cc 5 min
stop 60
5 min
to low top
ORSAT stop
reset 0123

| ORSAT | | |
|-----------------|--|----------------|
| CO ₂ | | O ₂ |
| | | |
| | | |
| | | |
| | | |
| | | |

LEAK TEST PROCEDURE with probe mounted in place and connected,

1. Turn stop-cock to flow ambient air only.
2. Turn on pump and open coarse valve (red handle).
3. Open roto-meter to permit good (over 1 liter/minute) air flow.
4. Visually observe air bubbling through all impingers, and make sure gas meter dial moves.
5. Turn stop-cock to close off flow to impingers.
6. Adjust flow knob on control box to obtain 10" of vacuum.
7. Visually observe roto-meter ball fall to zero flow.
8. Visually observe bubbling in impingers. Bubbling should stop. (A single, small bubble once every few seconds is acceptable).
9. Dry gas meter dial should not move at all.
10. Carefully turn stop-cock to allow ambient air flow through impingers. Do not allow stack gas to enter. Observe bubbling and meter operation.
11. Begin to close roto meter until low flow (0.4 liter/minute) rate is achieved.
12. Shut off red valve and pump.
13. Perform leak test before and after test.

TO SAMPLE

- (1) Heat glassware and stop-cock in hot box.
- (2) Use Dyna-pump to purge stack gas thru stop-cock; then rotate stop-cock to flow stack gas only and adjust roto-meter to obtain 0.4 liter/min flow rate.

Total sample must not exceed 1 cubic foot in one hour.

Orsat CO₂ readings are required!

BAROMETER

CONTROL BOX

VACUUM



GILBERT ASSOCIATES, INC.
AIR POLLUTION CONTROL DEPARTMENT
FIELD MOISTURE DETERMINATION

Client: W. D. & S. Co. W. D. No.: _____
Location: Bohannon Outlet Date: 12/21/92
Test: Bohannon Operator: James W. W.
Barometric Pressure: 30.07
COMMENTS: _____

| | Clock Time | Gas Meter C.F. VM | DATA | | PM | |
|---------|------------|-------------------|-------|--------|----------------------------------|----------------------|
| | | | TM In | TM Out | Orifice In. H ₂ O (-) | Vac. Gage In. Hg (-) |
| Stop | 0750 | 334.17 | 73 | 56 | 1.69 | 3 |
| Start | 0720 | 323.067 | 60 | 44 | 1.69 | 3 |
| Net/Avg | | | | | | |

| FINGERES | | | SILICA GEL | |
|------------|-----|-----|------------|-----------------------|
| | 1 | 2 | 3 | Container No. _____ |
| Final ml | 106 | 140 | --- | Final gm <u>244</u> |
| Initial ml | 104 | 136 | --- | Initial gm <u>232</u> |
| Net ml | 2 | 4 | --- | Net gm <u>12</u> |
| Total ml | 132 | | | <u>144</u> |

CALCULATIONS

- (1) FB = _____
(2) VM Net = _____
(3) TM Avg = _____ TM + 460 = _____
(4) EM Avg = _____ orifice IN. H₂O $\times \frac{1}{13.6}$ = _____ orifice IN. Hg.
" " Vacuum Gage IN. Hg (When meter is before pump)
(5) VMSID = $\frac{17.65 \times VM (FB + EM)}{TM + 460}$ = $\frac{17.65}{()}$ = _____
(6) VM = ml H₂O + gm Silica gel = _____
(7) VM Gas = VM $\times 0.3471$ = _____
(8) ZM = $\frac{100 \times VM Gas}{VMSID + VM Gas}$ = $\frac{100 \times ()}{() + ()}$ = $\frac{()}{()}$ = _____

PARTICULATE FIELD DATA
(continued)

Client W. O. No.

W.O. No. 10/21/79

Plant Run 10/21/79

Location 10/21/79

Run No. 10/21/79

| CMT
POINT | DISTANCE
IN
INCHES | CLOCK
TIME
ACTUAL | DRY GAS
METER, CF | PILOT
IN. H ₂ O
Δ P | ORIFICE Δ H
IN. H ₂ O | | DRY GAS TEMP.
OF | | PUMP
VACUUM
IN. HG
GAUGE | BOX
TEMP
OF | FINGER
TEMP
OF | STACK
TEMP.
OF |
|--------------|--------------------------|-------------------------|----------------------|--------------------------------------|-------------------------------------|--------|---------------------|--------|-----------------------------------|-------------------|----------------------|----------------------|
| | | | | | DESIRED | ACTUAL | INLET | OUTLET | | | | |
| A1 | 2.50 | 326 | | | | | | | | | | |
| Z | 3.00 | 328 | | | | | | | | | | |
| 1 | 7.30 | 329 | | | | | | | | | | |
| 4 | 1.50 | 329 | | | | | | | | | | |
| 5 | 1.70 | 328 | | | | | | | | | | |
| D-1 | 2.10 | 328 | | | | | | | | | | |
| Z | 2.00 | 330 | | | | | | | | | | |
| 3 | 1.10 | 331 | | | | | | | | | | |
| 4 | 0.97 | 331 | | | | | | | | | | |
| 5 | 0.92 | 331 | | | | | | | | | | |
| A-1 | 1.20 | 328 | | | | | | | | | | |
| 2 | 0.81 | 329 | | | | | | | | | | |
| 3 | 0.46 | 330 | | | | | | | | | | |
| 4 | 0.35 | 332 | | | | | | | | | | |
| 5 | 0.46 | 331 | | | | | | | | | | |
| A-1 | 0.47 | 328 | | | | | | | | | | |
| 2 | 0.48 | 329 | | | | | | | | | | |
| 3 | 0.47 | 330 | | | | | | | | | | |
| 4 | 0.47 | 331 | | | | | | | | | | |
| 5 | 0.52 | 329 | | | | | | | | | | |
| A-1 | 0.30 | 328 | | | | | | | | | | |
| Z | 0.31 | 330 | | | | | | | | | | |
| 3 | 0.32 | 330 | | | | | | | | | | |
| 4 | 0.17 | 329 | | | | | | | | | | |
| 5 | 0.73 | 329 | | | | | | | | | | |

88-70.11
STATS -0.74

0.11 / 0.0
4.0

APPENDIX V RAW FIELD DATA

5.3 Visible Emissions

VISIBLE EMISSION OBSERVATION FORM

No. 1

| | | |
|---|-------|------------------|
| COMPANY NAME
<u>Windsor Service</u> | | |
| STREET ADDRESS
<u>South Reading Facility</u> | | |
| CITY | STATE | ZIP |
| PHONE (KEY CONTACT) | | SOURCE ID NUMBER |

| | |
|--|----------------|
| PROCESS EQUIPMENT
<u>ASPHALT HOT MIX FACILITY</u> | OPERATING MODE |
| CONTROL EQUIPMENT
<u>baghouse</u> | OPERATING MODE |

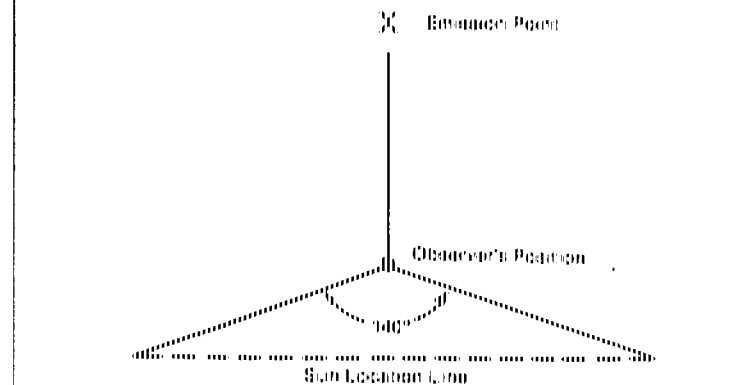
DESCRIBE EMISSION POINT
Rectangular stack

| | |
|--|---|
| HEIGHT ABOVE GROUND LEVEL
<u>20'</u> | HEIGHT RELATIVE TO OBSERVER
Start <u>20'</u> End |
| DISTANCE FROM OBSERVER
Start <u>80'</u> End | DIRECTION FROM OBSERVER
Start <u>NNW</u> End |

| | |
|--|-----|
| DESCRIBE EMISSIONS | |
| Start | End |
| EMISSION COLOR | |
| Start | End |
| POINT IN THE PLUME AT WHICH DENSITY WAS DETERMINED | |
| Start <u>Stack Exit</u> | End |

| | |
|---------------------------|-----|
| DESCRIBE PLUME BACKGROUND | |
| Start <u>SKY</u> | End |
| BACKGROUND COLOR | |
| Start <u>SKY</u> | End |
| WIND SPEED | |
| Start <u>0-2 MPH</u> | End |
| WIND DIRECTION | |
| Start <u>South</u> | End |
| AMBIENT TEMP | |
| Start | End |

| | | |
|-------------------|----------------------|------------------|
| Sketch with Plume | SOURCE LAYOUT SKETCH | Draw North Arrow |
| Start | | |
| Wind | | |



ADDITIONAL INFORMATION

| OBSERVATION DATE | | START TIME | | END TIME | |
|------------------|---|------------|----|----------|-----------|
| 10/21/92 | | 11:45 | | 12:22 | |
| SEC | 0 | 15 | 30 | 45 | COMMENTS |
| 1 | 0 | 0 | 0 | 0 | |
| 2 | 0 | 0 | 0 | 0 | |
| 3 | 0 | 0 | 0 | 0 | |
| 4 | 0 | 0 | 0 | 0 | |
| 5 | 0 | 0 | 0 | 0 | |
| 6 | 0 | 0 | 0 | 0 | |
| 7 | 0 | 0 | 0 | 0 | |
| 8 | 0 | 0 | 0 | 0 | |
| 9 | 0 | 0 | 0 | 0 | |
| 10 | 0 | 0 | 0 | 0 | Time 1:55 |
| 11 | 0 | 0 | 0 | 0 | Time 1:50 |
| 12 | 0 | 0 | 0 | 0 | |
| 13 | 0 | 0 | 0 | 0 | |
| 14 | 0 | 0 | 0 | 0 | |
| 15 | 0 | 0 | 0 | 0 | |
| 16 | 0 | 0 | 0 | 0 | |
| 17 | 0 | 0 | 0 | 0 | |
| 18 | 0 | 0 | 0 | 0 | |
| 19 | 0 | 0 | 0 | 0 | |
| 20 | 0 | 0 | 0 | 0 | |
| 21 | 0 | 0 | 0 | 0 | |
| 22 | 0 | 0 | 0 | 0 | |
| 23 | 0 | 0 | 0 | 0 | |
| 24 | 0 | 0 | 0 | 0 | |
| 25 | 0 | 0 | 0 | 0 | |
| 26 | 0 | 0 | 0 | 0 | |
| 27 | 0 | 0 | 0 | 0 | |
| 28 | 0 | 0 | 0 | 0 | 11:27 |
| 29 | 0 | 0 | 0 | 0 | 11:50 |
| 30 | 0 | 0 | 0 | 0 | |

| | |
|--|-------------------------|
| OBSERVER'S NAME (PRINT)
<u>George Blarney</u> | |
| OBSERVER'S SIGNATURE
<u>George Blarney</u> | DATE
<u>10/21/92</u> |
| ORGANIZATION
<u>Eastern Technical Assoc.</u> | |
| CERTIFIED BY
<u>Eastern Technical Assoc.</u> | DATE |
| CONTINUED ON VED FORM NUMBER | |

VISIBLE EMISSION OBSERVATION FORM
(CONTINUED)

| | |
|--|-------------------|
| COMPANY NAME
<i>Windsor Service Reading</i> | |
| CITY
<i>South Reading Facility</i> | |
| TEST NO. <i>1</i> | PAGE ____ OF ____ |

| |
|--|
| TYPE OF FACILITY
<i>Asphalt Hot Mix</i> |
| EMISSION POINT
<i>baghouse stack exit</i> |
| OBSERVER
<i>G. E. Page</i> |

| OBSERVATION DATE | | START TIME | | | | END TIME |
|------------------|-----|-----------------------|-----------------------|-----------------------|-----------------------|------------------|
| MIN | SEC | 0 | 15 | 30 | 45 | COMMENTS |
| | | | | | | |
| 1 | | ☐ | ☐ | ☐ | ☐ | <i>Time 1132</i> |
| 2 | | ☐ | ☐ | ☐ | ☐ | |
| 3 | | ☐ | ☐ | ☐ | ☐ | |
| 4 | | ☐ | ☐ | ☐ | ☐ | |
| 5 | | ☐ | ☐ | ☐ | ☐ | |
| 6 | | ☐ | ☐ | ☐ | ☐ | |
| 7 | | ☐ | ☐ | ☐ | ☐ | |
| 8 | | ☐ | ☐ | ☐ | ☐ | |
| 9 | | ☐ | ☐ | ☐ | ☐ | |
| 10 | | ☐ | ☐ | ☐ | ☐ | |
| 11 | | ☐ | ☐ | ☐ | ☐ | |
| 12 | | ☐ | ☐ | ☐ | ☐ | |
| 13 | | ☐ | ☐ | ☐ | ☐ | |
| 14 | | ☐ | ☐ | ☐ | ☐ | |
| 15 | | ☐ | ☐ | ☐ | ☐ | |
| 16 | | ☐ | ☐ | ☐ | ☐ | |
| 17 | | ☐ | ☐ | ☐ | ☐ | |
| 18 | | ☐ | ☐ | ☐ | ☐ | |
| 19 | | ☐ | ☐ | ☐ | ☐ | |
| 20 | | ☐ | ☐ | ☐ | ☐ | |
| 21 | | ☐ | ☐ | ☐ | ☐ | |
| 22 | | ☐ | ☐ | ☐ | ☐ | |
| 23 | | ☐ | ☐ | ☐ | ☐ | |
| 24 | | ☐ | ☐ | ☐ | ☐ | |
| 25 | | ☐ | ☐ | ☐ | ☐ | |
| 26 | | ☐ | ☐ | ☐ | ☐ | |
| 27 | | ☐ | ☐ | ☐ | ☐ | |
| 28 | | ☐ | ☐ | ☐ | ☐ | |
| 29 | | ☐ | ☐ | ☐ | ☐ | <i>1200</i> |
| 30 | | ☐ | ☐ | ☐ | ☐ | |

| OBSERVATION DATE | | START TIME | | | | END TIME |
|------------------|-----|-----------------------|-----------------------|-----------------------|-----------------------|------------------|
| MIN | SEC | 0 | 15 | 30 | 45 | COMMENTS |
| | | | | | | |
| 1 | | ☐ | ☐ | ☐ | ☐ | <i>Time 1200</i> |
| 2 | | ☐ | ☐ | ☐ | ☐ | |
| 3 | | ☐ | ☐ | ☐ | ☐ | |
| 4 | | ☐ | ☐ | ☐ | ☐ | |
| 5 | | ☐ | ☐ | ☐ | ☐ | |
| 6 | | ☐ | ☐ | ☐ | ☐ | |
| 7 | | ☐ | ☐ | ☐ | ☐ | |
| 8 | | ☐ | ☐ | ☐ | ☐ | |
| 9 | | ☐ | ☐ | ☐ | ☐ | |
| 10 | | ☐ | ☐ | ☐ | ☐ | |
| 11 | | ☐ | ☐ | ☐ | ☐ | |
| 12 | | ☐ | ☐ | ☐ | ☐ | |
| 13 | | ☐ | ☐ | ☐ | ☐ | |
| 14 | | ☐ | ☐ | ☐ | ☐ | |
| 15 | | ☐ | ☐ | ☐ | ☐ | |
| 16 | | ☐ | ☐ | ☐ | ☐ | |
| 17 | | ☐ | ☐ | ☐ | ☐ | |
| 18 | | ☐ | ☐ | ☐ | ☐ | |
| 19 | | ☐ | ☐ | ☐ | ☐ | |
| 20 | | ☐ | ☐ | ☐ | ☐ | |
| 21 | | ☐ | ☐ | ☐ | ☐ | |
| 22 | | ☐ | ☐ | ☐ | ☐ | |
| 23 | | ☐ | ☐ | ☐ | ☐ | |
| 24 | | ☐ | ☐ | ☐ | ☐ | |
| 25 | | ☐ | ☐ | ☐ | ☐ | <i>1227</i> |
| 26 | | ☐ | ☐ | ☐ | ☐ | |
| 27 | | | | | | |
| 28 | | | | | | |
| 29 | | | | | | |
| 30 | | | | | | |

VISIBLE EMISSION OBSERVATION FORM

No. 22

| | |
|---|--|
| COMPANY NAME
<i>Windsor Service</i> | |
| STREET ADDRESS
<i>South Reading Plant</i> | |
| CITY
<i>Reading</i> | STATE
<i>PA</i> |
| PHONE (KEY CONTACT) | SOURCE ID NUMBER |
| PROCESS EQUIPMENT
<i>Asphalt Hot Mix</i> | OPERATING MODE |
| CONTROL EQUIPMENT
<i>baghouse</i> | OPERATING MODE |
| DESCRIBE EMISSION POINT
<i>rectangular stack exit</i> | |
| HEIGHT ABOVE GROUND LEVEL
<i>20</i> | HEIGHT RELATIVE TO OBSERVER
Start <i>20</i> End |
| DISTANCE FROM OBSERVER
Start <i>30</i> End | DIRECTION FROM OBSERVER
Start <i>NNW</i> End |
| DESCRIBE EMISSIONS
<i>Detached Plume</i> | |
| Start End | IF WATER DROPLET PLUME
Attached ☐ Detached ☒ |
| POINT IN THE PLUME AT WHICH OPACITY WAS DETERMINED
Start <i>Stack Exit</i> End | |
| DESCRIBE PLUME BACKGROUND
Start <i>over clear sky</i> End | |
| BACKGROUND COLOR
Start <i>gray</i> End | SKY CONDITIONS
Start End |
| WIND SPEED
Start <i>5-8</i> End | WIND DIRECTION
Start <i>NW</i> End |
| AMBIENT TEMP
Start <i>45.0</i> End | WET BULB TEMP RH, percent |
| Black and White Photo ☒ | Sketch of Source Layout |
| Sketch of Plume ☒ | Sketch of Source Layout |
| Sketch of Source ☒ | Sketch of Source Layout |
| Sketch of Wind ☒ | Sketch of Source Layout |
| <p>Observer's Position</p> <p>Sun Location (indicated by arrow)</p> | |
| ADDITIONAL INFORMATION | |

| OBSERVATION DATE
<i>10/20/92</i> | | START TIME
<i>0730</i> | | END TIME | COMMENTS |
|-------------------------------------|---|---------------------------|----|----------|----------|
| SEC | 0 | 15 | 30 | 45 | |
| 1 | 0 | 0 | 0 | 0 | |
| 2 | 0 | 0 | 0 | 0 | |
| 3 | 0 | 0 | 0 | 0 | |
| 4 | 0 | 0 | 0 | 0 | |
| 5 | 0 | 0 | 0 | 0 | |
| 6 | 0 | 0 | 0 | 0 | |
| 7 | 0 | 0 | 0 | 0 | |
| 8 | 0 | 0 | 0 | 0 | |
| 9 | 0 | 0 | 0 | 0 | |
| 10 | 0 | 0 | 0 | 0 | |
| 11 | 0 | 0 | 0 | 0 | |
| 12 | 0 | 0 | 0 | 0 | |
| 13 | 0 | 0 | 0 | 0 | |
| 14 | 0 | 0 | 0 | 0 | |
| 15 | 0 | 0 | 0 | 0 | |
| 16 | 0 | 0 | 0 | 0 | |
| 17 | 0 | 0 | 0 | 0 | |
| 18 | 0 | 0 | 0 | 0 | |
| 19 | 0 | 0 | 0 | 0 | |
| 20 | 0 | 0 | 0 | 0 | |
| 21 | 0 | 0 | 0 | 0 | |
| 22 | 0 | 0 | 0 | 0 | |
| 23 | 0 | 0 | 0 | 0 | |
| 24 | 0 | 0 | 0 | 0 | |
| 25 | 0 | 0 | 0 | 0 | |
| 26 | 0 | 0 | 0 | 0 | |
| 27 | 0 | 0 | 0 | 0 | |
| 28 | 0 | 0 | 0 | 0 | |
| 29 | 0 | 0 | 0 | 0 | |
| 30 | 0 | 0 | 0 | 0 | |

| | | |
|---|--|-------------------------|
| OBSERVER'S NAME (PRINT)
<i>George Albright</i> | | DATE
<i>10/20/92</i> |
| OBSERVER'S SIGNATURE
<i>George Albright</i> | | DATE
<i>10/20/92</i> |
| ORGANIZATION
<i>Editor/Communications</i> | | DATE
<i>10/20/92</i> |
| CERTIFIED BY
<i>Robert J. [Signature]</i> | | DATE
<i>10/20/92</i> |
| CONTINUED ON VED FORM NUMBER | | |

VISIBLE EMISSION OBSERVATION FORM
(CONTINUED)

| | |
|---|---------------------------|
| COMPANY NAME
<i>Windsor Refining</i> | |
| CTV
<i>South Reading Plant</i> | |
| TEST NO.
<i>2</i> | PAGE <i>2</i> OF <i>2</i> |

| |
|--|
| TYPE OF FACILITY
<i>Refinery</i> |
| EMISSION POINT
<i>South Reading Plant</i> |
| OBSERVER
<i>George A. Smith</i> |

| OBSERVATION DATE | | START TIME | | | | END TIME |
|------------------|-----|------------|----|----|----|----------|
| MIN | SEC | 0 | 15 | 30 | 45 | COMMENTS |
| | | | | | | |
| 1 | | 0 | 0 | 0 | 0 | EX31 |
| 2 | | 0 | 0 | 0 | 0 | |
| 3 | | 0 | 0 | 0 | 0 | |
| 4 | | 0 | 0 | 0 | 0 | |
| 5 | | 0 | 0 | 0 | 0 | |
| 6 | | 0 | 0 | 0 | 0 | |
| 7 | | 0 | 0 | 0 | 0 | |
| 8 | | 0 | 0 | 0 | 0 | |
| 9 | | 0 | 0 | 0 | 0 | |
| 10 | | 0 | 0 | 0 | 0 | |
| 11 | | 0 | 0 | 0 | 0 | |
| 12 | | 0 | 0 | 0 | 0 | |
| 13 | | 0 | 0 | 0 | 0 | |
| 14 | | 0 | 0 | 0 | 0 | |
| 15 | | | | | | |
| 16 | | | | | | |
| 17 | | 0 | 0 | 0 | 0 | |
| 18 | | 0 | 0 | 0 | 0 | |
| 19 | | 0 | 0 | 0 | 0 | |
| 20 | | 0 | 0 | 0 | 0 | |
| 21 | | 0 | 0 | 0 | 0 | |
| 22 | | 0 | 0 | 0 | 0 | |
| 23 | | 0 | 0 | 0 | 0 | |
| 24 | | 0 | 0 | 0 | 0 | |
| 25 | | 0 | 0 | 0 | 0 | |
| 26 | | 0 | 0 | 0 | 0 | |
| 27 | | 0 | 0 | 0 | 0 | |
| 28 | | 0 | 0 | 0 | 0 | |
| 29 | | 0 | 0 | 0 | 0 | |
| 30 | | 0 | 0 | 0 | 0 | |

| OBSERVATION DATE | | START TIME | | | | END TIME |
|------------------|-----|------------|----|----|----|----------|
| MIN | SEC | 0 | 15 | 30 | 45 | COMMENTS |
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VISIBLE EMISSION OBSERVATION FORM

No. 3

| | | |
|--|--------------------|-----|
| COMPANY NAME
<i>Windsor Service</i> | | |
| STREET ADDRESS
<i>South Reading Plant</i> | | |
| CITY
<i>Reading</i> | STATE
<i>MA</i> | ZIP |
| PHONE (KEY CONTACT) | SOURCE ID NUMBER | |

| | |
|---|----------------|
| PROCESS EQUIPMENT
<i>Hot Mix Asphalt</i> | OPERATING MODE |
| CONTROL EQUIPMENT
<i>baghouse</i> | OPERATING MODE |

| | |
|--|--|
| DESCRIBE EMISSION POINT
<i>Rectangular Stack Exit</i> | |
|--|--|

| | |
|---|--|
| HEIGHT ABOVE GROUND LEVEL
<i>20</i> | HEIGHT RELATIVE TO OBSERVER
Start <i>20</i> End |
| DISTANCE FROM OBSERVER
Start <i>80</i> End | DIRECTION FROM OBSERVER
Start <i>NNW</i> End |

| | |
|--|--|
| DESCRIBE EMISSIONS
Start <i>Stack detected Plume (dark vapor)</i> End | |
| EMISSION COLOR | IF WATER DROPLET PLUME |
| Start End | Attached ☐ Detached ☒ |

| | |
|---|--|
| POINT IN THE PLUME AT WHICH OPACITY WAS DETERMINED
Start <i>Stack exit</i> End | |
|---|--|

| | |
|--|----------------|
| DESCRIBE PLUME BACKGROUND
Start <i>overcast sky</i> End | |
| BACKGROUND COLOR | SKY CONDITIONS |
| Start <i>gray</i> End | Start End |

| | |
|-------------------------------------|--------------------------------------|
| WIND SPEED
Start <i>0-5</i> End | WIND DIRECTION
Start <i>N</i> End |
| AMBIENT TEMP
Start <i>45</i> End | WET BULB TEMP |
| | REL. HUMIDITY |

| | | |
|---|--------------------------|----------------------|
| Stack with Plume ☒
Sun ☒
Wind ☒ | SOURCE LAYOUT SKETCH
 | Draw North Arrow
 |
|---|--------------------------|----------------------|

| |
|------------------------|
| ADDITIONAL INFORMATION |
|------------------------|

| OBSERVATION DATE
<i>10/22/92</i> | | | | START TIME
<i>1030</i> | END TIME
<i>1130</i> |
|-------------------------------------|---|----|----|---------------------------|-------------------------|
| SEC | 0 | 15 | 30 | 45 | COMMENTS |
| MIN | | | | | |
| 1 | 0 | 0 | 0 | 0 | |
| 2 | 0 | 0 | 0 | 0 | |
| 3 | 0 | 0 | 0 | 0 | |
| 4 | 0 | 0 | 0 | 0 | |
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| 6 | 0 | 0 | 0 | 0 | |
| 7 | 0 | 0 | 0 | 0 | |
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| 10 | 0 | 0 | 0 | 0 | |
| 11 | 0 | 0 | 0 | 0 | |
| 12 | 0 | 0 | 0 | 0 | |
| 13 | 0 | 0 | 0 | 0 | |
| 14 | 0 | 0 | 0 | 0 | |
| 15 | 0 | 0 | 0 | 0 | |
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| 19 | 0 | 0 | 0 | 0 | |
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| 23 | 0 | 0 | 0 | 0 | |
| 24 | 0 | 0 | 0 | 0 | |
| 25 | 0 | 0 | 0 | 0 | |
| 26 | 0 | 0 | 0 | 0 | |
| 27 | 0 | 0 | 0 | 0 | |
| 28 | 0 | 0 | 0 | 0 | |
| 29 | 0 | 0 | 0 | 0 | |
| 30 | 0 | 0 | 0 | 0 | |

| | |
|---|-------------------------|
| OBSERVER'S NAME (PRINT)
<i>George Albright</i> | |
| OBSERVER'S SIGNATURE
<i>George Albright</i> | DATE
<i>10/22/92</i> |
| ORGANIZATION
<i>Slater/Conway Inc</i> | |
| CERTIFIED BY
<i>Eastern Industrial Corp</i> | DATE
<i>10/22/92</i> |
| CONTINUED ON VED FORM NUMBER | |

VISIBLE EMISSION OBSERVATION FORM
(CONTINUED)

| | |
|--|---------------------------|
| COMPANY NAME
<i>Windsor Service</i> | |
| CITY <i>South Reading Plant</i> | |
| TEST NO.
<i>3</i> | PAGE <i>2</i> OF <i>2</i> |

| |
|--|
| TYPE OF FACILITY
<i>Hot Mix Asphalt</i> |
| EMISSION POINT
<i>baghouse Stack Exit</i> |
| OBSERVER
<i>George Albright</i> |

| OBSERVATION DATE | | START TIME | | | | END TIME |
|------------------|-----|------------|----|----|----|------------|
| MIN | SEC | 0 | 15 | 30 | 45 | COMMENTS |
| | | | | | | |
| 1 | | 0 | 0 | 0 | 0 | <i>Hot</i> |
| 2 | | 0 | 0 | 0 | 0 | |
| 3 | | 0 | 0 | 0 | 0 | |
| 4 | | 0 | 0 | 0 | 0 | |
| 5 | | 0 | 0 | 0 | 0 | |
| 6 | | 0 | 0 | 0 | 0 | |
| 7 | | 0 | 0 | 0 | 0 | |
| 8 | | 0 | 0 | 0 | 0 | |
| 9 | | 0 | 0 | 0 | 0 | |
| 10 | | 0 | 0 | 0 | 0 | |
| 11 | | 0 | 0 | 0 | 0 | |
| 12 | | 0 | 0 | 0 | 0 | |
| 13 | | 0 | 0 | 0 | 0 | |
| 14 | | 0 | 0 | 0 | 0 | |
| 15 | | 0 | 0 | 0 | 0 | |
| 16 | | 0 | 0 | 0 | 0 | |
| 17 | | 0 | 0 | 0 | 0 | |
| 18 | | 0 | 0 | 0 | 0 | |
| 19 | | 0 | 0 | 0 | 0 | |
| 20 | | 0 | 0 | 0 | 0 | |
| 21 | | 0 | 0 | 0 | 0 | |
| 22 | | 0 | 0 | 0 | 0 | |
| 23 | | 0 | 0 | 0 | 0 | |
| 24 | | 0 | 0 | 0 | 0 | |
| 25 | | 0 | 0 | 0 | 0 | |
| 26 | | 0 | 0 | 0 | 0 | |
| 27 | | 0 | 0 | 0 | 0 | |
| 28 | | 0 | 0 | 0 | 0 | |
| 29 | | 0 | 0 | 0 | 0 | |
| 30 | | 0 | 0 | 0 | 0 | <i>Hot</i> |

| OBSERVATION DATE | | START TIME | | | | END TIME |
|------------------|-----|------------|----|----|----|----------|
| MIN | SEC | 0 | 15 | 30 | 45 | COMMENTS |
| | | | | | | |
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APPENDIX VII
TEST RESULTS

APPENDIX VI

TEST RESULTS

- 6.1 Particulate
- 6.2 Volatile Organic Compounds
- 6.3 Visible Emissions

APPENDIX VI TEST RESULTS

6.1 Particulate

GILBERT/CONDOREALTH, INC.
TESTING SERVICES GROUP
ISOKINETIC SAMPLING ANALYSIS

Client: WINDSOR SERVICE

Plant: SOUTH READING

Unit Tested: DRUM ROCK ASPHALT PLANT

Test: PARTICULATES & FLOW

Sampling Location: DASHCUBE EXHAUST

Run No: W-P-1 Date: 10/21/92 Start: 1057 End: 1228

DATA

DW: 0.215 PB: 29.98 PBT: -0.88 AS: 2,304.0
O2%: 11.7 CO2%: 4.8 O2%: 83.5 VW: 299
GAS METER Y-FACTOR: 1.00

| SAMPLE POINT | TIME AT POINT | GAS METER | VELOCITY HEAD | STACK TEMP. | METER IN | TEMP. OUT | PM ORIFICE | SOE | O2 | CO2 | VEL |
|--------------|---------------|-----------|---------------|-------------|----------|-----------|------------|-------|------|-----|-------|
| A-1 | 3.5 | 133.137 | 3.000 | 338 | 60 | 62 | 3.195 | 48.93 | | | 7.450 |
| 2 | 3.5 | | 3.600 | 347 | 74 | 64 | 3.808 | 53.70 | | | 8.176 |
| 3 | 3.5 | | 2.700 | 347 | 80 | 65 | 2.889 | 46.50 | | | 7.087 |
| 4 | 3.5 | | 1.900 | 340 | 82 | 66 | 1.615 | 34.64 | | | 5.275 |
| 5 | 3.5 | | 1.400 | 339 | 81 | 68 | 1.514 | 33.45 | | | 5.093 |
| B-1 | 3.5 | 150.345 | 3.100 | 343 | 67 | 66 | 3.359 | 49.89 | | | 7.597 |
| 2 | 3.5 | | 1.900 | 339 | 80 | 68 | 2.018 | 38.96 | | | 5.933 |
| 3 | 3.5 | | 1.100 | 345 | 80 | 68 | 1.191 | 29.76 | | | 4.537 |
| 4 | 3.5 | | 0.740 | 348 | 82 | 68 | 0.797 | 24.45 | | | 3.723 |
| 5 | 3.5 | | 1.100 | 345 | 83 | 70 | 1.180 | 29.76 | | | 4.537 |
| C-1 | 3.5 | 162.500 | 1.800 | 347 | 76 | 70 | 1.943 | 38.11 | 11.1 | 5.4 | 5.803 |
| 2 | 3.5 | | 0.660 | 347 | 83 | 71 | 0.706 | 23.08 | | | 3.514 |
| 3 | 3.5 | | 0.350 | 345 | 84 | 72 | 0.377 | 16.75 | | | 2.556 |
| 4 | 3.5 | | 0.360 | 345 | 84 | 72 | 0.390 | 17.02 | | | 2.592 |
| 5 | 3.5 | | 0.360 | 345 | 83 | 72 | 0.390 | 17.02 | | | 2.592 |
| D-1 | 3.5 | 170.638 | 1.050 | 352 | 78 | 74 | 1.137 | 29.20 | | | 4.446 |
| 2 | 3.5 | | 0.210 | 355 | 81 | 74 | 0.225 | 13.08 | 12.0 | 5.0 | 1.992 |
| 3 | 3.5 | | 0.110 | 346 | 80 | 74 | 0.117 | 9.42 | | | 1.434 |
| 4 | 3.5 | | 0.110 | 342 | 79 | 74 | 0.119 | 9.35 | | | 1.430 |
| 5 | 3.5 | | 0.110 | 338 | 78 | 74 | 0.119 | 9.37 | | | 1.427 |
| E-1 | 3.5 | 176.218 | 0.560 | 338 | 74 | 72 | 0.604 | 21.14 | | | 3.219 |
| 2 | 3.5 | | 0.570 | 336 | 80 | 74 | 0.618 | 21.30 | 12.0 | 4.0 | 3.243 |
| 3 | 3.5 | | 0.690 | 336 | 82 | 74 | 0.744 | 23.44 | | | 3.568 |
| 4 | 3.5 | | 0.250 | 328 | 82 | 74 | 0.274 | 14.04 | | | 2.157 |
| 5 | 3.5 | | 0.460 | 327 | 82 | 74 | 0.509 | 19.03 | | | 2.897 |
| | | 183.684 | | | | | | | | | |

| RESULTS | FT | MP | P FT | TS | TM | PM | SOE | O2 | CO2 | VEL |
|---------|-------|--------|--------|--------|--------|-------|-------|---------------------|-----|-------|
| | 87.5 | 50.567 | 1.112 | 342 | 75 | 1.194 | 26.86 | 11.7 | 4.8 | 4.090 |
| | avg | net | avg | avg | avg | avg | avg | avg | avg | avg |
| PSM= | 30.07 | WASTC= | 50.158 | WAGAS= | 14.083 | SM= | 21.4 | RMS OF VELOCITIES = | | |
| PD= | 0.78 | MG= | 29.24 | MG= | 26.77 | PS= | 29.92 | | | |

STACK GAS VELOCITY = 4.089 AFPM
STACK GAS VOLUME = 33,634 DSCFM
STACK GAS VOLUME = 85,420 ACFM
STACK GAS VOLUME = 1.80E+05 LBS/HR
ISOKINETIC RATIO = 107.5

PARTICULATE EMISSIONS

MG = 37.3
GR/DSCF = 0.011
LBS/HR = 3.30

GILBERT/COMMONWEALTH, INC.
TESTING SERVICES GROUP
ISOKINETIC SAMPLING ANALYSIS

Client: WINDSOR SERVICE

Plant: SOUTH READING

Unit Tested: DRUM MIX ASPHALT PLANT

Test: PARTICULATES & FLOW

Sampling Location: BAGHOUSE EX-AUST

Run No: W-2-2 Date: 10/22/92 Start: 0651 End: 0900

DATA

OH: 0.295 PH: 30.17 PBT: -0.43 AS: 2,304.0
O2%: 11.2 CO2%: 4.9 N2%: 83.9 VM: 352
GAS METER Y-FACTOR: 1.00

| SAMPLE
POINT | TIME AT
POINT | GAS
METER | VELOCITY
HEAD | STACK
TEMP. | METER
CN | TEMP.
OUT | PM
ORIFICE | SOE | O2 | CO2 | VEL. |
|-----------------|------------------|--------------|------------------|----------------|-------------|--------------|---------------|-------|------|-----|-------|
| A-1 | 4.0 | 184.071 | 0.280 | 339 | 40 | 62 | 0.261 | 14.94 | | | 2,270 |
| 2 | 4.0 | | 0.320 | 343 | 42 | 62 | 0.294 | 16.05 | | | 2,633 |
| 3 | 4.0 | | 0.540 | 350 | 45 | 62 | 0.494 | 20.97 | | | 3,172 |
| 4 | 4.0 | | 0.790 | 352 | 50 | 62 | 0.720 | 25.33 | | | 3,844 |
| 5 | 4.0 | | 0.880 | 352 | 54 | 64 | 0.804 | 26.73 | | | 4,057 |
| B-1 | 4.0 | 191.597 | 0.520 | 355 | 45 | 66 | 0.560 | 20.60 | 10.0 | 6.0 | 3,135 |
| 2 | 4.0 | | 0.440 | 358 | 50 | 68 | 0.470 | 18.97 | | | 2,879 |
| 3 | 4.0 | | 0.740 | 359 | 55 | 68 | 0.780 | 24.52 | | | 3,735 |
| 4 | 4.0 | | 0.870 | 355 | 50 | 50 | 0.920 | 26.54 | | | 4,044 |
| 5 | 4.0 | | 1.050 | 349 | 54 | 50 | 1.120 | 29.15 | | | 4,623 |
| C-1 | 4.0 | 201.190 | 1.200 | 344 | 52 | 68 | 1.300 | 31.36 | | | 4,714 |
| 2 | 4.0 | | 0.850 | 343 | 50 | 50 | 0.930 | 26.13 | | | 3,965 |
| 3 | 4.0 | | 0.540 | 344 | 51 | 50 | 0.690 | 22.58 | | | 3,443 |
| 4 | 4.0 | | 0.790 | 343 | 53 | 50 | 0.850 | 25.19 | | | 3,823 |
| 5 | 4.0 | | 0.900 | 338 | 55 | 51 | 0.970 | 26.30 | | | 4,067 |
| D-1 | 4.0 | 211.785 | 2.000 | 341 | 58 | 50 | 2.210 | 40.32 | | | 5,075 |
| 2 | 4.0 | | 1.500 | 343 | 56 | 51 | 1.950 | 36.77 | 11.6 | 6.0 | 5,267 |
| 3 | 4.0 | | 1.100 | 347 | 56 | 52 | 1.200 | 29.79 | | | 4,522 |
| 4 | 4.0 | | 0.770 | 353 | 56 | 52 | 0.840 | 25.32 | | | 3,797 |
| 5 | 4.0 | | 0.800 | 352 | 55 | 52 | 0.870 | 25.49 | | | 3,868 |
| E-1 | 4.0 | 226.432 | 2.400 | 343 | 61 | 52 | 2.610 | 43.90 | | | 5,665 |
| 2 | 4.0 | | 2.900 | 353 | 70 | 53 | 3.150 | 48.56 | | | 7,369 |
| 3 | 4.0 | | 2.100 | 354 | 74 | 56 | 2.280 | 41.40 | | | 5,283 |
| 4 | 4.0 | | 1.500 | 354 | 74 | 56 | 1.610 | 34.94 | | | 5,305 |
| 5 | 4.0 | | 1.700 | 348 | 82 | 58 | 1.850 | 37.36 | 12.0 | 4.8 | 5,625 |
| | | 240.265 | | | | | | | | | |

RESULTS TT VM PBT TS TM PM SOE O2 CO2 VEL
100.0 56.174 1.103 349 54 1,189 20.57 11.2 4.9 4,357
net net avg avg avg avg avg avg avg avg
PSM= 30.26 VMSTD= 58.310 VMGAS= 15.579 SM= 22.1 RMS CF VELOCITIES = 29.2
MC= 0.78 MMD= 29.24 MW= 25.75 PS= 30.14

STACK GAS VELOCITY = 4,350 ACFM
STACK GAS VOLUME = 35,645 DSCFM
STACK GAS VOLUME = 69,609 ACFM
STACK GAS VOLUME = 1.89E+05 LBS/HR
ISOKINETIC RATIO = 103.1

PARTICULATE EMISSIONS
MG = 70.2
GR/DSCF = 0.019
LBS/HR = 5.56

GILBERT/COMMONWEALTH, INC.
TESTING SERVICES GROUP
ISOMETRIC SAMPLING ANALYSIS

Client: WENDSOR SERVICE

Plant: SOUTH READING

Unit Tested: DRUM MIX ASPHALT PLANT

Test: PARTICULATES & FLOW

Sampling Location: BAGHOUSE EXHAUST

Run No: W-R-3 Date: 10/22/92 Start: 0940 End: 1132

DATA

O₂: 0.215 PB: 30.27 PST: -0.39 WS: 2,304.0
CO₂: 12.1 CO₂H: 4.6 N₂H: 83.5 WH: 413
GAS METER V-Factor: 1.00

| SAMPLE
POINT | TIME AT
POINT | GAS
METER | VELOCITY
FEET | STACK
TEMP. | METER
IN | TEMP.
OUT | PM
ORIFICE | SOE | O ₂ | CO ₂ | VEL |
|-----------------|------------------|--------------|------------------|----------------|-------------|--------------|---------------|-------|----------------|-----------------|-------|
| B-1 | 4.0 | 240.681 | 2.200 | 348 | 50 | 52 | 2.350 | 42.16 | | | 6,668 |
| 2 | 4.0 | | 2.900 | 340 | 64 | 54 | 3.700 | 48.17 | | | 7,368 |
| 3 | 4.0 | | 2.200 | 341 | 74 | 56 | 2.350 | 41.98 | | | 6,620 |
| 4 | 4.0 | | 1.800 | 344 | 68 | 58 | 1.650 | 34.73 | 12.0 | 4.0 | 5,511 |
| 5 | 4.0 | | 1.600 | 339 | 66 | 58 | 1.720 | 35.75 | | | 5,468 |
| B-1 | 4.0 | 256.291 | 1.900 | 340 | 58 | 56 | 2.080 | 38.99 | | | 5,963 |
| 2 | 4.0 | | 1.700 | 340 | 65 | 58 | 1.870 | 36.88 | | | 5,640 |
| 3 | 4.0 | | 0.950 | 344 | 66 | 58 | 1.010 | 27.64 | | | 4,227 |
| 4 | 4.0 | | 0.720 | 349 | 66 | 58 | 0.780 | 24.13 | 12.0 | 5.0 | 3,691 |
| 5 | 4.0 | | 0.570 | 348 | 66 | 58 | 0.610 | 21.46 | | | 3,282 |
| C-1 | 4.0 | 268.995 | 1.200 | 351 | 58 | 56 | 1.300 | 31.20 | | | 4,771 |
| 2 | 4.0 | | 0.670 | 350 | 65 | 58 | 0.660 | 22.23 | | | 3,400 |
| 3 | 4.0 | | 0.500 | 350 | 65 | 58 | 0.540 | 20.12 | 12.1 | 4.6 | 3,078 |
| 4 | 4.0 | | 0.580 | 350 | 65 | 58 | 0.600 | 21.67 | | | 3,316 |
| 5 | 4.0 | | 0.750 | 350 | 65 | 59 | 0.810 | 24.68 | | | 3,770 |
| B-1 | 4.0 | 277.522 | 0.560 | 348 | 60 | 58 | 0.710 | 23.09 | | | 3,532 |
| 2 | 4.0 | | 0.380 | 345 | 66 | 60 | 0.400 | 17.49 | 12.2 | 4.0 | 2,675 |
| 3 | 4.0 | | 0.360 | 346 | 66 | 60 | 0.390 | 17.03 | | | 2,608 |
| 4 | 4.0 | | 0.530 | 348 | 66 | 60 | 0.670 | 22.56 | | | 3,451 |
| 5 | 4.0 | | 0.800 | 348 | 70 | 62 | 0.860 | 25.42 | | | 3,888 |
| A-1 | 4.0 | 286.120 | 0.570 | 340 | 62 | 62 | 0.330 | 15.75 | | | 2,408 |
| 2 | 4.0 | | 0.270 | 334 | 70 | 64 | 0.290 | 14.64 | | | 2,239 |
| 3 | 4.0 | | 0.350 | 334 | 71 | 64 | 0.370 | 16.67 | | | 2,550 |
| 4 | 4.0 | | 0.550 | 337 | 73 | 64 | 0.700 | 22.76 | | | 3,481 |
| 5 | 4.0 | | 0.580 | 335 | 76 | 65 | 0.720 | 23.25 | | | 3,556 |
| | | 295.814 | | | | | | | | | |

| RESULTS | TI | VM | PST | TS | TP | PM | SOE | O ₂ | CO ₂ | VEL |
|---------|-------|--------|--------|--------|--------|-------|-------|---------------------|-----------------|-------|
| | 100.0 | 33.333 | 0.999 | 344 | 62 | 1.075 | 26.82 | 12.1 | 4.6 | 4,101 |
| | net | net | avg | avg | avg | avg | avg | avg | avg | avg |
| PSH= | 30.35 | MPSTD= | 54.697 | VMGAS= | 15.452 | SP= | 26.2 | RMS OF VELOCITIES = | | |
| WD= | 0.74 | PWD= | 29.19 | WD= | 26.25 | PS= | 30.24 | | | |

| STACK GAS VELOCITY = | | | | PARTICULATE EMISSIONS | |
|----------------------|-----------------|--|--|-----------------------|-------|
| STACK GAS VOLUME = | 4,101 ACFM | | | PM = | 54.5 |
| STACK GAS VOLUME = | 32,129 DSCFM | | | SR/SCCF = | 0.015 |
| STACK GAS VOLUME = | 65,519 ACFM | | | LBS/HR = | 4.23 |
| STACK GAS VOLUME = | 1,768.05 LBS/HR | | | | |
| ISOMETRIC RATIO = | 107.3 | | | | |

GILBERT/COMMONWEALTH, INC.
 TESTING SERVICES GROUP
 ISOKINETIC SAMPLING SUMMARY SHEET

Client: WINDSOR SERVICE

Plant: SCOTH READING

Unit Tested: DRUM MIX ASPHALT PLANT

Test: PARTICULATES & FLOW

Sampling Location: BASHOUSE EXHAUST

| Run Number
Date | W-P-1
10/21/92 | W-P-2
10/22/92 | W-P-3
10/22/92 |
|--|-------------------|-------------------|-------------------|
| DN - NOZZLE DIAMETER, IN. | 0.215 | 0.215 | 0.215 |
| PB - BAROMETRIC PRESS, IN. OF H ₂ O | 29.98 | 30.17 | 30.27 |
| TT - NET SAMPLING TIME, MIN. | 87.5 | 100.0 | 100.0 |
| VM - VOLUME METERED, ACF | 50.567 | 58.174 | 53.333 |
| TM - AVG. METER TEMP., DEG. F | 75 | 54 | 62 |
| PM - AVG. DELTA H, IN. OF H ₂ O | 1.164 | 1.189 | 1.075 |
| Y - GAS METER CALIB. FACTOR | 1.00 | 1.00 | 1.00 |
| VMSTD - STD. GAS VOLL., SCF | 50.168 | 58.310 | 54.697 |
| WM - TOTAL WATER COLLECTED, ML. | 299 | 352 | 413 |
| SM - PERCENT MOISTURE | 21.9 | 22.1 | 26.2 |
| MD - MOLE FRACTION DRY | 0.78 | 0.78 | 0.74 |
| SCOD - PERCENT CO ₂ DRY | 4.5 | 4.9 | 4.4 |
| ROD - PERCENT O ₂ DRY | 11.7 | 11.2 | 12.1 |
| MMO - DRY MOLECULAR WEIGHT | 29.24 | 29.24 | 29.19 |
| MMW - WET MOLECULAR WEIGHT | 26.77 | 26.75 | 26.25 |
| SEA - PERCENT EXCESS AIR | 0.0 | 0.0 | 0.0 |
| AS - STACK AREA, SQ. IN. | 2,304.0 | 2,304.0 | 2,304.0 |
| PST - STATIC PRESS., IN. OF H ₂ O | -0.85 | -0.43 | -0.39 |
| TS - STACK TEMP., DEG. F | 342 | 349 | 344 |
| CP - PIVOT COEFFICIENT | 0.84 | 0.84 | 0.84 |
| VS - STACK GAS VELOCITY, ACFM | 4,089 | 4,350 | 4,101 |
| RMS - STD. DEV. OF VEL. | 49.1 | 29.2 | 34.6 |
| QS - STACK GAS FLOW, CFSFM | 33,634 | 35,645 | 32,129 |
| QA - STACK GAS FLOW, ACFM | 65,430 | 69,609 | 65,619 |
| KE - ISOKINETIC RATIO | 107.5 | 103.1 | 107.3 |
| GR/SCF, PARTICULATE LOADING | 0.011 | 0.019 | 0.015 |
| LBS/HR, PARTICULATE EMISSIONS | 5.30 | 5.66 | 4.23 |
| AVG. GR/SCF, EMISSION RATE | | 0.015 | |

APPENDIX VI TEST RESULTS

6.2 Volatile Organic Compounds

GILBERT/COMMONWEALTH, INC.
 TESTING SERVICES GROUP
 VOLATILE ORGANIC COMPOUND SAMPLING ANALYSIS

Client: WINDSOR SERVICE Plants: SOUTH READING

Unit Tested: DRUM MIX ASPHALT PLANT Tests: VOC

Sampling Location: BAGHOUSE EXHAUST

Run No: W-M-1 Date: 10/22/92

| START TIME | TIME (MIN) | BAROMETER (IN HG) | TEMPERATURE FILTER (°F) | TEMPERATURE PROBE (°F) | FLOW RATE (SCFM) | WACJUP (CON MG) | AMBIENT TEMP (°F) |
|------------|------------|-------------------|-------------------------|------------------------|------------------|-----------------|-------------------|
| 0753 | 0.0 | 30.20 | | | 65 | 20.4 | 48 |
| | 5.0 | | | | 65 | 25.6 | |
| | 10.0 | | 254 | 265 | 65 | 25.0 | |
| | 15.0 | | 250 | 264 | 65 | 20.4 | |
| | 20.0 | | 249 | 265 | 65 | 17.9 | |
| | 25.0 | | 250 | 266 | 65 | 16.3 | |
| | 30.0 | | 252 | 265 | 65 | 12.2 | |
| | 35.0 | | 251 | 265 | 65 | 10.0 | |
| | 40.0 | | 251 | 265 | 65 | 8.3 | |
| | 45.0 | | 249 | 265 | 65 | 6.2 | |
| | 50.0 | | 248 | 265 | 65 | 4.2 | |
| 0828 | 55.0 | 30.23 | 248 | 265 | 65 | 2.0 | 52 |
| | 60.0 | | | | | | |
| AVERAGES | | 30.22 | 250 | 265 | 65 | 16.4 | 50 |

| VOC EMISSIONS | FEED RATE | FLOW RATE |
|-----------------|-----------|-----------|
| MG S/CULN | TONS/HR | SCFM |
| GR/DSCF = 0.052 | 285 | 36,900 |
| LBS/HR = 15.51 | | |
| LBS/TON = 0.054 | | |

GILBERT/COMMONWEALTH, INC.
 TESTING SERVICES GROUP
 VOLATILE ORGANIC COMPOUND SAMPLING ANALYSIS

Client: WINDSOR SERVICE Plant: SOUTH READING
 Unit Tested: DRUM PEX ASPHALT PLANT Test: VOC

Sampling Location: BARGEHOUSE EXHAUST

Run No: J-V-2 Date: 10/22/92

| START
TIME | RUN TIME
(MIN) | BAROMETER
(IN HG) | TEMPERATURE
FILTER
(°F) | TEMPERATURE
PROBE
(°F) | FLOW
RATE
(CC/MIN) | VACUUM
(IN HG) | AMBIENT
TEMP
(°F) |
|---------------|-------------------|----------------------|-------------------------------|------------------------------|--------------------------|-------------------|-------------------------|
| 0951 | 0.0 | 30.28 | 233 | 256 | 65 | 29.8 | 55 |
| | 5.0 | | 247 | 256 | 65 | 29.6 | |
| | 10.0 | | 255 | 255 | 65 | 27.3 | |
| | 15.0 | | 252 | 256 | 65 | 26.2 | |
| | 20.0 | | 249 | 255 | 65 | 25.0 | |
| | 25.0 | | 248 | 265 | 65 | 23.7 | |
| 1021/1045 | 30.0 | | 249 | 265 | 65 | 22.4 | |
| | 35.0 | | 230 | 261 | 65 | 21.6 | |
| | 40.0 | | 235 | 265 | 65 | 20.4 | |
| | 45.0 | 30.24 | 247 | 265 | 65 | 19.2 | |
| | 50.0 | | 250 | 265 | 65 | 17.8 | |
| | 55.0 | | 256 | 265 | 65 | 16.6 | |
| 1010 | 60.0 | | 251 | 265 | | 14.4 | 58 |
| AVERAGES | | 30.25 | 247 | 265 | 65 | 22.5 | 57 |

| VOC EMISSIONS | | FEED RATE | | FLOW RATE | |
|---------------|-------|-----------|-----|-----------|--------|
| MG C/CH/CH | 327.8 | TONS/HR = | 275 | SCFM = | 34,900 |
| GR/OSCF = | 0.139 | | | | |
| LBS/HR = | 41.62 | | | | |
| LBS/TON = | 0.151 | | | | |

GILBERT/COMMONWEALTH, INC.
 TESTING SERVICES GROUP
 VOLATILE ORGANIC COMPOUND SAMPLING ANALYSIS

Client: WENDSCOR SERVICE Plant: SOUTH BEADING

Unit Tested: DRUM MIX ASPHALT PLANT Test: VOC

Sampling Location: BASHCOUSE EXHAUST

Run No: W-V-5 Date: 10/23/92

| START TIME | RUN TIME (MIN) | BAROMETER (IN HG) | TEMPERATURE FILTER (°F) | TEMPERATURE PROBE (°F) | FLOW RATE (CC/MIN) | VACUUM (IN HG) | AMBIENT TEMP (°F) |
|------------|----------------|-------------------|-------------------------|------------------------|--------------------|----------------|-------------------|
| 0700 | 0.0 | 30.16 | 251 | 265 | 55 | 29.6 | 42 |
| | 5.0 | | 250 | 265 | 55 | 29.4 | |
| | 10.0 | | 251 | 265 | 55 | 27.1 | |
| | 15.0 | | 269 | 265 | 55 | 25.7 | |
| | 20.0 | | 250 | 265 | 55 | 24.2 | |
| | 25.0 | | 251 | 265 | 55 | 23.2 | |
| | 30.0 | | 250 | 265 | 55 | 22.1 | |
| 0753/0758 | 35.0 | | 250 | 265 | 55 | 20.7 | |
| | 40.0 | | 250 | 265 | 55 | 19.7 | |
| | 45.0 | | 251 | 265 | 55 | 18.0 | |
| | 50.0 | | 251 | 266 | 55 | 16.7 | |
| 0816/0928 | 55.0 | | 269 | 264 | 55 | 15.2 | |
| 0935 | 60.0 | 30.16 | 251 | 265 | | 15.0 | 51 |
| AVERAGES | | 30.16 | 250 | 265 | 55 | 22.0 | 47 |

VOC EMISSIONS

| MG C/COLUMN | FEED RATE (TONS/HR) | FLOW RATE (SCFH) |
|-----------------|---------------------|------------------|
| 163.0 | 288 | 34,900 |
| GR/CSCP = 0.069 | | |
| LBS/HR = 20.72 | | |
| LBS/TON = 0.072 | | |

GILBERT/COMMONWEALTH, INC.
TESTING SERVICES GROUP
ISO-KINETIC SAMPLING SUMMARY SHEET

Client: WINDSOR SERVICE Plant: SOUTH READING
Unit Tested: DRUM MIX ASPHALT PLANT Tests: VOC

Sampling Location: BAGHOUSE EXHAUST

| RUN NUMBER | W-V-1 | W-V-2 | W-V-3 |
|---|----------|----------|----------|
| DATE | 10/22/92 | 10/22/92 | 10/23/92 |
| BAROMETRIC PRESS., IN. H ₂ O | 30.22 | 30.26 | 30.16 |
| FILTER TEMPERATURE, °F | 250 | 247 | 250 |
| PROBE TEMPERATURE, °F | 265 | 265 | 265 |
| FLOW RATE, CC/MIN | 65 | 65 | 65 |
| AMBIENT TEMPERATURE, °F | 50 | 57 | 47 |
| FLUE GAS VOLUME, DSCFM | 34,900 | 34,900 | 34,900 |
| FEED RATE, TONS/HR | 285 | 275 | 288 |
| EMISSIONS | | | |
| MG/CUBIC METER | 122.0 | 327.5 | 163.0 |
| GR/DSCF* | 0.052 | 0.139 | 0.069 |
| LBS/HR | 15.5 | 41.5 | 20.7 |
| LBS/TON | 0.054 | 0.151 | 0.072 |

AVERAGE EMISSIONS, LBS/TON 0.063 *

* Average emissions for runs W-V-1 and W-V-3. The average emissions for all three runs is 0.092 lbs/ton.

GILBERT/COMMERCIALITY, INC.
TESTING SERVICES GROUP
GAS FLOW ANALYSIS

Client: WINDSOR

Plant: S. REG

Unit Tested: ASPHALT

TEST : GAS FLOW

Test Location: BAHIGOSE

Run No: 1-1 Date: 10/22/92 Starts: 907 Ends: 925

DATA

PB: 30.17 PST: -0.24 AS: 2504.0

| SAMPLE
POINT | VELOCITY
HEAD | STACK
TEMP. | SOE | VELOCITY
AFPM | CO2 | O2 |
|-----------------|------------------|----------------|-------|------------------|-----|------|
| B-1 | 2.500 | 325 | 64.33 | 6,598 | 5.4 | 11.1 |
| 2 | 3.000 | 328 | 68.62 | 7,367 | | |
| 3 | 2.300 | 329 | 62.60 | 6,437 | | |
| 4 | 1.500 | 329 | 34.60 | 5,198 | 5.0 | 12.0 |
| 5 | 1.700 | 328 | 36.60 | 5,530 | | |
| C-1 | 2.100 | 328 | 60.60 | 6,167 | | |
| 2 | 2.000 | 330 | 39.75 | 6,006 | 6.0 | 12.0 |
| 3 | 1.100 | 331 | 29.50 | 6,457 | | |
| 4 | 0.970 | 331 | 27.70 | 6,185 | | |
| 5 | 0.920 | 331 | 26.90 | 6,076 | 6.0 | 10.0 |
| D-1 | 1.200 | 328 | 30.75 | 6,566 | | |
| 2 | 0.810 | 329 | 25.20 | 3,820 | | |
| 3 | 0.560 | 330 | 21.03 | 3,178 | 6.0 | 11.5 |
| 4 | 0.550 | 332 | 20.87 | 3,156 | | |
| 5 | 0.660 | 331 | 22.85 | 3,452 | | |
| B-1 | 0.470 | 328 | 19.26 | 2,908 | 6.8 | 12.0 |
| 2 | 0.480 | 329 | 19.46 | 2,961 | | |
| 3 | 0.470 | 330 | 19.27 | 2,912 | | |
| 4 | 0.470 | 330 | 19.27 | 2,912 | 6.0 | 12.0 |
| 5 | 0.550 | 329 | 20.85 | 3,148 | | |
| A-1 | 0.250 | 328 | 16.06 | 2,121 | | |
| 2 | 0.210 | 330 | 12.88 | 1,946 | 5.0 | 12.0 |
| 3 | 0.320 | 330 | 15.90 | 2,402 | | |
| 4 | 0.550 | 327 | 20.81 | 3,144 | 6.6 | 12.1 |
| 5 | 0.730 | 329 | 26.00 | 3,626 | 6.0 | 12.2 |

| RESULTS | PIT | TD | SOE | VEL | CO2 | O2 |
|---------|-------|-----|-------|-------|-----|------|
| | 1.055 | 329 | 27.11 | 6,096 | 4.7 | 11.7 |
| | avg | avg | avg | avg | avg | avg |

DB= 20.10 MB= 29.22 ME= 26.97 PS= 30.15
MD= 0.800

STACK GAS VELOCITY = 6,096 AFPM
STACK GAS VOLUME = 35,476 DSCFM
STACK GAS VOLUME = 65,775 ACFM

AVERAGE OF FLOW RATES = 34899.5

GILBERT/COMPCONREALTH, INC.
TESTING SERVICES GROUP

FIELD MOISTURE DETERMINATION

CLIENT: MICROSCOR SERVICES

LOCATION: BAGOHOUSE ECHOAST

TEST: M-1 DATE: 10/23/92 TIME: 720

OPERATOR: SCHELL

BAROMETRIC PRESSURE: 30.17

SAS METER

START: 293.887 FINAL: 314.117 NET: 20.230

Y FACTOR: 1.00

FLOW METER

AVERAGE FLOW DROP 1.69 AVE. TEMPERATURE: 56

MOISTURE

DIP 1 START: 100 FINAL: 138 NET: 38

DIP 2 START: 100 FINAL: 144 NET: 44

DIP 3 START: 0 FINAL: 0 NET: 0

GEL START: 232 FINAL: 244 NET: 12

TOTAL COLLECTED MOISTURE: 146.0

TOTAL MOISTURE BY WEIGHT: 26.4 %

SAMPLE VOLUME(VINSTD): 21.044

APPENDIX VI TEST RESULTS

6.3 Visible Emissions

GILBERT/COMMONWEALTH, INC.
 TESTING SERVICES GROUP
 VISIBLE EMISSIONS SUMMARY

| | | | |
|-------------------------------------|------------------------|--------|-------------------|
| Client: | WINDSOR SERVICE | Plant: | SOUTH READING |
| Unit Tested: | CRUIZING ASPHALT PLANT | Test: | VISIBLE EMISSIONS |
| Sampling Location: BAGHOUSE EXHAUST | | | |

| | | | |
|---|-----------|-----------|-----------|
| RUN NUMBER: | 1 | 2 | 3 |
| DATE: | 10/21/92 | 10/22/92 | 10/22/92 |
| TIME: | 1065-1227 | 0800-0900 | 1030-1130 |
| AVERAGE CAPACITY: | 0 | 0 | 0 |
| AVERAGE CAPACITY FOR
RUNS 1, 2, AND 3: | | 0 | |

APPENDIX VII
CALIBRATION DATA

Silvertown-Chenoweth, Inc.
 Testing Services Group
 METER BOX CALIBRATION

DATE: 10/12/92 METER BOX NUMBER: 3183

PARAMETRIC PRESS. (PSI) = 29.59 (at 1g) CALIBRATED BY: SCHELL

| GAS VOLUME | | | TEMPERATURES | | | | | | |
|--|---|--|---|--|---|--|--------------|------|-------------|
| Orifice
Manometer
Reading
(in H ₂ O)
in. H ₂ O | Wet
Test
Meter
(in H ₂ O)
in. H ₂ O | Dry
Gas
Meter
(in H ₂ O)
in. H ₂ O | Wet
Test
Meter
(in H ₂ O)
deg. F | Dry Gas Meter | | | Time
min. | Ys | delta (PPs) |
| | | | | Inlet
(in H ₂ O)
deg. F | Outlet
(in H ₂ O)
deg. F | Average
(in H ₂ O)
deg. F | | | |
| 0.0 | 0.004 | 0.000 | 89.5 | 91.0 | 90.0 | 90.0 | 11.01 | 1.01 | 1.00 |
| 1.0 | 0.004 | 0.000 | 89.5 | 91.0 | 91.0 | 90.0 | 3.00 | 1.00 | 1.00 |
| 1.0 | 0.006 | 0.000 | 89.5 | 91.0 | 91.0 | 90.0 | 1.00 | 1.00 | 1.00 |
| 2.0 | 0.006 | 0.000 | 89.5 | 91.0 | 91.0 | 90.0 | 5.10 | 0.99 | 1.00 |
| 3.0 | 0.000 | 0.000 | 89.5 | 91.0 | 91.0 | 90.0 | 0.10 | 0.99 | 1.00 |
| 4.0 | 0.004 | 0.000 | 89.5 | 91.0 | 91.0 | 90.0 | 4.00 | 0.99 | 1.00 |
| AVERAGE | | | | | | | | 1.00 | 1.00 |

FORMULAS

$$Ys = \frac{\text{Wet (in H}_2\text{O) (in H}_2\text{O)}}{\text{Wet (in H}_2\text{O) (in H}_2\text{O) (in H}_2\text{O)}}$$

$$\text{delta (PPs)} = \frac{\text{Wet (in H}_2\text{O)}}{\text{Wet (in H}_2\text{O)}}$$

$$Ys = \frac{\text{Wet (in H}_2\text{O)}}{\text{Wet (in H}_2\text{O) (in H}_2\text{O)}}$$

$$Ys = \frac{\text{Wet (in H}_2\text{O)}}{\text{Wet (in H}_2\text{O) (in H}_2\text{O)}}$$

Palmer-Chambersville, Inc.
 Testing Services Group
 METER SET CALIBRATION

DATE: 12/29/82 METER BOX NUMBER: 5153
 LABORATORY PRESS. (PSI) = 40.52 (2.0 MPa) CALIBRATED TO: ATMOSPHERE

| Orifice
Manufacturer
Parting
Depth (in.)
1/4" = 0.00 | GAS VOLUME | | TEMPERATURE | | | | | | |
|--|--|---|--------------------------------------|-----------------------|------------------------|-------------------------|----------------|------|--------------|
| | Wet
Test
Meter
PSIG
vol. (ft. ³) | Dry
Gas
Meter
PSIG
vol. (ft. ³) | Wet
Test
Meter
Temp.
(F) | Dry Gas Meter | | | Time
(sec.) | % | Actual (SCF) |
| | | | | Inlet
Temp.
(F) | Outlet
Temp.
(F) | Average
Temp.
(F) | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| 0.5 | 0.0003 | 0.0004 | 59 | 55.0 | 70.0 | 60.0 | 10.00 | 1.00 | 1.00 |
| 1.0 | 0.0008 | 0.0005 | 59 | 55.0 | 70.0 | 61.0 | 8.00 | 1.00 | 1.00 |
| 1.5 | 0.0009 | 0.0002 | 59 | 54.0 | 70.0 | 60.0 | 7.00 | 1.00 | 1.00 |
| 2.0 | 0.0007 | 0.0002 | 59 | 53.0 | 70.0 | 60.0 | 6.00 | 1.00 | 1.00 |
| 3.0 | 0.0006 | 0.0002 | 59 | 50.0 | 70.0 | 60.0 | 5.00 | 0.99 | 1.00 |
| 4.0 | 0.0008 | 0.0001 | 59 | 50.0 | 70.0 | 60.0 | 4.00 | 0.99 | 1.00 |
| | | | | | | | AVERAGE | 1.00 | 1.00 |

FORMULARS

$$P_s = \frac{\text{Wet Gas Volume}}{\text{Wet Gas Volume} + \text{Dry Gas Volume}}$$

$$\text{Actual SCF} = \frac{\text{Wet Gas}}{\text{Wet Gas} + \text{Dry Gas}}$$

$$Q_d = Q_w \left(\frac{P_s}{P_d} \right) \left(\frac{T_d}{T_s} \right) \left(\frac{Z_s}{Z_d} \right)$$

$$Q_d = \frac{\text{Wet (SCF @ 60°)}}{\text{Correct (70° @ 60°)}}$$

Silbert/Comprehensive Inc.
Air Quality Testing Services Group

POT METER CALIBRATION

DATE: 11-1-93 CALIBRATED BY: JCLAND
POT METER NUMBER: 3 THERMOCOUPLE TYPE: C

| REF | INSTRUMENT | TEMPERATURE | TEMPERATURE |
|-------------|---------------------|-------------|-------------|
| | | °F | °C |
| ICE WATER | MERCURY THERMOMETER | 32 | 00 |
| | POT METER | 34 | 01 |
| | difference | -2 | -0.1 |
| AMBIENT AIR | MERCURY THERMOMETER | 59 | 15 |
| | POT METER | 61 | 16 |
| | difference | -2 | -0.1 |
| HOT OIL | MERCURY THERMOMETER | 220 | 108 |
| | POT METER | 220 | 109 |
| | difference | 0 | 0 |

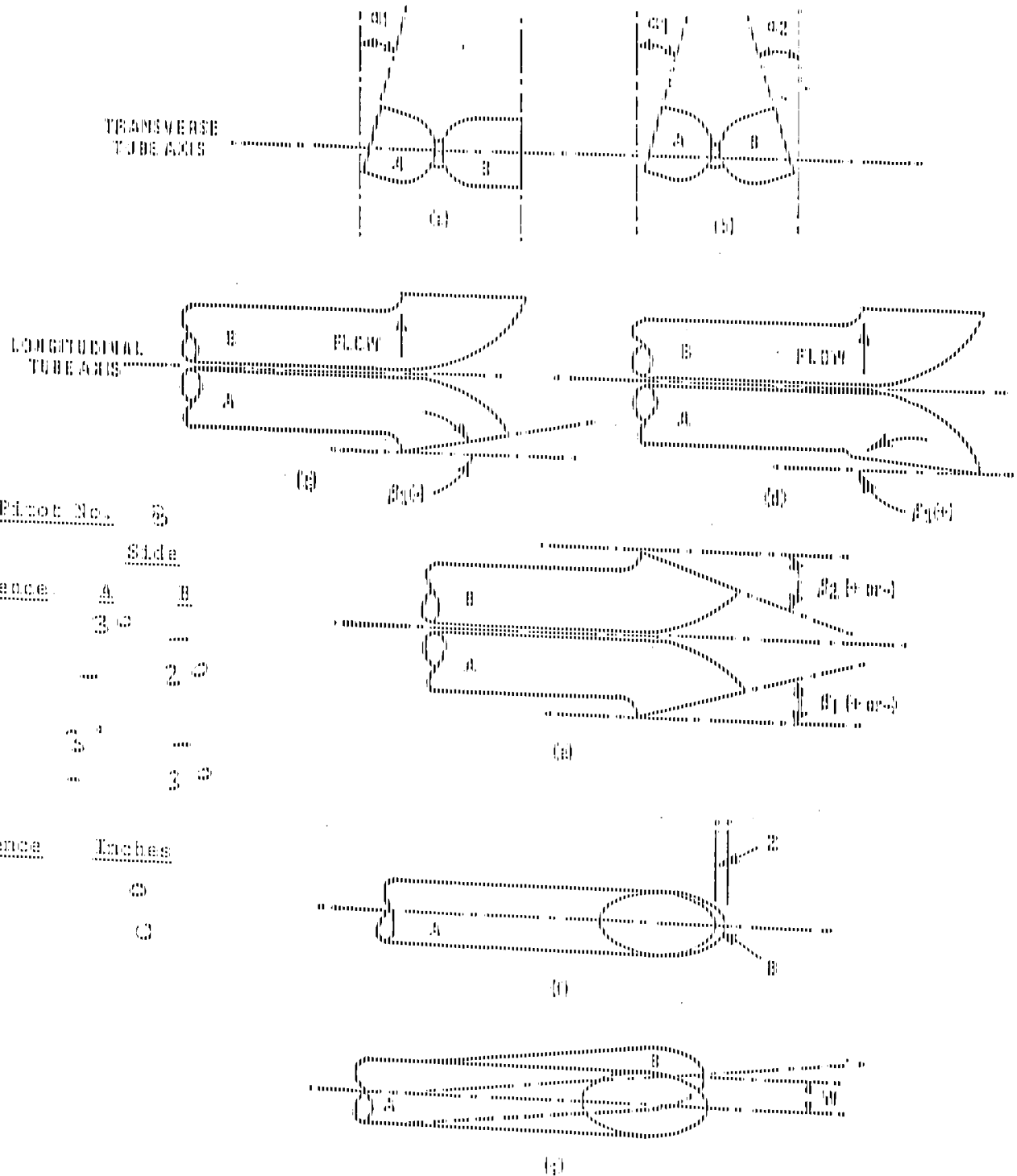


Figure 2-3. Types of face-opening misalignment that can result from field use or improper construction of Type S pitot tubes. These will not affect the baseline value of $\bar{C}_p(s)$ so long as α_1 and $\alpha_2 < 10^\circ$, β_1 and $\beta_2 < 5^\circ$, $z < 0.32$ cm (1/8 in.) and $w < 0.03$ cm (1/32 in.) (citation 11 in Section 6).

APPENDIX VIII
SAMPLE CALCULATIONS

SAMPLE CALCULATIONS

Particulate Isokinetic Sampling

I. Calculations for stack volume and Isokinetic Ratio

| Time | Dry Gas
Meter Fe^3 | Pitot
$\Delta P,$
$\text{In. H}_2\text{O}$ | Orifice
$\Delta P,$
$\text{In. H}_2\text{O}$ | Dry Gas
Temp $^{\circ}\text{F}$
In. Out | Stack
Static
Pressure
$\text{In. H}_2\text{O}$ | Stack
Temp $^{\circ}\text{F}$ |
|------|--------------------------------|--|--|--|---|----------------------------------|
| T | VM | ΔP | PM | TME TMO | PST | TS |

1. DN = Nozzle Diameter, inches

2. PB = Barometric Pressure, inches Hg

3. TE = Net Sampling Time, minutes

4. VM = $VM_{\text{final}} - VM_{\text{initial}}$ = Sample Gas Volume, Fe^3

5. TM = Average Dry Gas Temperature at Meter, $^{\circ}\text{F}$

$$TM = \frac{\text{Avg. TME} + \text{Avg. TMO}}{2}$$

6. PM = Average Orifice Pressure Drop, inches H_2O

$$PM = \text{Avg. } \Delta H$$

7. Volume of dry gas sampled at standard conditions^a, DSCF

$$V_{\text{GSTD}} = \frac{17.65 \times VM \times T \left(PB + \frac{PM}{13.6} \right)}{(TM + 460)}$$

8. WP = Total Water Collected = gm H_2O silica gel + ml Imp. H_2O = ml

9. Volume of water vapor at standard conditions^b, SCF

$$VW_{\text{gas}} = 0.0471 \times WP = \text{SCF}$$

10. Percent moisture in stack gas

$$\% M = \frac{100 \times VW_{\text{gas}}}{VM_{\text{STD}} + VW_{\text{gas}}}$$

11. Mole fraction of dry gas

$$M_D = \frac{100 - \%M}{100}$$

12. Molecular weight of dry stack gas

$$MD = (CO_2 \times \frac{44}{100}) + (CO \times \frac{28}{100}) + [(H_2O + N_2) \times \frac{29}{100}]$$

12A. Dry-Stack Air = $\frac{[(CO_2) + 0.5 (CO)]}{0.264 (CO_2) + [(CO_2) + 0.5 (CO)]} \times 100$

13. Molecular weight of wet stack gas

$$MW = MD \times MD + 18 (1 - MD)$$

14. AS = Stack Area, square inches

15. PS = Stack Pressure, inches Hg

$$PS = PH \pm Avg. PST$$

$$NOTE: PST in. Hg. = \frac{PST in. H_2O}{13.6}$$

16. TS = Average Stack Temperature, °F

$$TS = \text{Average TS}$$

17. SDE = Average $\sqrt{\text{Velocity Head (in. P)} \times (\text{Stack Temperature} + 460)}$
(Calculated each line)

$$SDE = Avg \sqrt{in. P \times (TS + 460)}$$

18. Stack gas velocity at stack condition, fpm

$$VS = 5150 \times Cp \times Avg(SDE) \times \left[\frac{1}{PS \times MD} \right]^{1/3} = \text{fpm} \quad Cp = \text{pipe tube coefficient}$$

19. Stack gas volumetric flow rate at standard conditions, DSCFM

$$Q_s = \frac{0.113 \times VS \times AS \times MD \times PS}{(TS + 460)} = \text{DSCFM}$$

20. Stack gas volumetric flow rate at stack condition, ACFM

$$Q_a = \frac{0.0567 \times VS \times (TS + 460)}{PS \times MD} = \text{ACFM}$$

21. Percent Moisture

$$M = \frac{1.032 \times (TS + 460) \times VMDT}{VS \times TT \times PS \times MD \times (DM)^2}$$

NOTES: aDry standard cubic foot at 69°F, 29.92 in. Hg.

bStandard conditions at 68°F, 29.92 in. Hg.

cDry standard cubic foot per minute at 68°F, 29.92 in. Hg.

21. Calculations for grain loading and emission rates

22. Particulate, gr/DSCF

$$\text{gr/DSCF} = 0.0154 \times \frac{\text{mg}}{\text{VDSFD}}$$

23. Particulate at stack conditions, gr/ACF

$$\text{gr/ACF} = \frac{17.65 \text{ gr/DSCF} \times \text{PS} \times \text{SD}}{(\text{PS} + 450)}$$

24. Particulate, lb/hr conc. method

$$\text{lb/hr} = 0.00857 \times \text{gr/DSCF} \times \text{QS}$$

25. Particulate lb/hr area method = $0.132 \times \frac{\text{DPM Particulate} \times \text{AS}}{\left(\frac{\text{mg}^2}{\text{ft}} \right) \times \text{TT}}$

26. Particulate, combustion

$$\frac{\text{lb/hr}}{10^6 \text{ BTU/hr}}$$

27. Particulate, process lb/ton

$$\text{lb/ton} = \frac{\text{lb/hr}}{\text{ton/hr}}$$

28. Particulate, lb/MMBTU, P-Factor Method =

Unlag CO_2 =

$$\frac{0.0154 \times \text{mg} \times \text{P-Factor} \times 20.9}{7000 \times \text{VDSFD} \times (20.9 - \text{CO}_2)}$$

Unlag CO_2 =

$$\frac{0.0154 \times \text{mg} \times \text{P-Factor} \times 100}{7000 \times \text{VDSFD} \times \text{X } \text{CO}_2}$$

29. P-Factor, dust/million

CO_2 Percent =

$$\text{P-Factor} = \frac{10^6 (3.66(\text{CH}) + 1.51(\text{HC}) + 0.57(\text{CS}) + 0.16(\text{HM}) + 0.46(\text{CO}_2))}{\text{GGV}}$$

CO_2 Percent =

$$\frac{10^6 (0.321)(\text{HC})}{\text{GGV}}$$

PARTICULATE MATTER EMISSIONS

Process Factor Formula

$$A = 0.76E^{0.42}, \text{ where:}$$

A = Allowable Emissions in LBS/HR

E = Emission Index = F x W in LBS/HR

F = Process Factor in LBS/Unit, and

W = Production or charging rate in Units/HR

F shall be obtained from the table in paragraph (1) of subsection 123.13 of the FADER Source Testing Manual.

The units for F and W shall be compatible.

VOLATILE ORGANIC COMPOUND CALCULATIONS

$$\text{GR/DSCF} = (\text{MG of C/M}^3 \times 0.015) / 35.3$$

$$\text{LBS/HR} = \text{GR/DSCF} \times 0.00857 \times \text{DSCFM}$$

$$\text{LBS/TON} = (\text{LBS/HR}) / (\text{LBS/TON})$$