

Note: This is a reference cited in *AP 42, Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at www.epa.gov/ttn/chief/ap42/

The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

PARTICULATE EMISSION TEST
KLUG BROTHERS, INCORPORATED
MOUNDSVILLE, WEST VIRGINIA

by

TraDet Laboratories, Inc.
P. O. Box 2019
Wheeling, West Virginia 26003
(304) 547-9094

September 1987

TABLE OF CONTENTS

	Page No.
Process Description	1
Process Operation	2
Regulations	2
Procedure	3
Results and Discussion	9

Appendices

- I. Calibrations
- II. Particulate Analytical Data
- III. Velocity Data
- IV. Field Data

PROCESS DESCRIPTION

The facility tested is an Asphalt Drum Mixers, Inc. (ADM) asphalt plant owned and operated by Klug Brothers, Inc., Moundsville, West Virginia. The facility is located on State Route 2 immediately south of Moundsville. The unit is an ADM Model 6026 designed to produce 100 TPH of hot asphalt mix at 5% product moisture. The typical production process includes heating a mixture of 40% sand, 60% gravel, and AC-20 asphalt bitum in a No. 2 Fuel Oil fired rotary kiln. The product mix is conveyed from the discharge end of the rotary kiln to a 38 ton capacity bin which also serves as the truck loadout facility.

The emissions from the operation consists of combustion by-products and any fine particulate (sand/gravel) that has become entrained in the heated air stream. Combustion air for the No. 2 Fuel Oil is added at the feed end of the rotary kiln by means of a 20 horsepower blower. The air/fuel mixture is fed through a Hauck Shape A Flame Jet Burner and ignited inside the rotary kiln. A 50 horsepower induced draft fan removes combustion gases by pulling them through a venturi scrubber and a horizontal, tangentially fed circular mist eliminator. The scrubber consists of a series of nozzles ahead of the venturi plate and utilizes 40 gpm of water at 30 psi. A portion of the scrubber water is diverted and directed into the bottom of the mist eliminator

and is used as push water to prevent solids buildup. The water exits the system through the bottom of the mist eliminator and is discharged through appropriate treatment facilities. Scrubber feed water is supplied from the public water distribution system. The saturated gas stream exits the system through the induced draft fan and the 60-inch diameter circular stack.

PROCESS OPERATION

The facility is designed to process 100 TPH of asphalt product. Due to limitations of the product conveyor the facility can only produce 90 TPH, with this quantity being marginal due to spillage from the product conveyor. Normal operating rate is in the range of 75 TPH. During the three particulate emission tests the facility was operated at an average of 82.3 TPH. This operation rate was a balance between overloading the product conveyor and removal of the material from the storage bin for final transportation. The final product temperature was maintained in the range of 250 to 280 °F.

REGULATIONS

The emissions from the Klug Brother, Inc. asphalt drum mix plant are required to meet New Source Performance standards as specified in 40 CFR, Part 60.90 through 60.92, Subpart I - Standards of Performance for Hot Mix Asphalt

Facilities. The standard specifies that the particulate emission rate from the facility shall not exceed 0.04 gr./DSCF as determined by Method 5.

PROCEDURE

PARTICULATE SAMPLING

PRINCIPLE - Particulates were sampled isokinetically according to Federal Test Methods 1, 2, 3, 4, and 5 as given in the Federal Register, Vol. 36, No. 247 of December 23, 1971, and as amended in the Federal Register, Vol. 40, No. 60, of July 1, 1984, and Vol. 40, No. 60 of December 27, 1985. The weight of the particulate was determined gravimetrically after the removal of uncombined water. The molecular weight of the stack gas was determined by FYRITE analysis and the percent moisture by the condensation method. Particulate grain loading was then calculated using filter and probe catch weights.

EQUIPMENT - The equipment utilized included a Research Appliance Company, Model 2343, stacksampler train with a combination heated stainless steel probe and S-type pitot tubes, and the associated glassware. The equipment utilized is shown schematically in Figure 1.

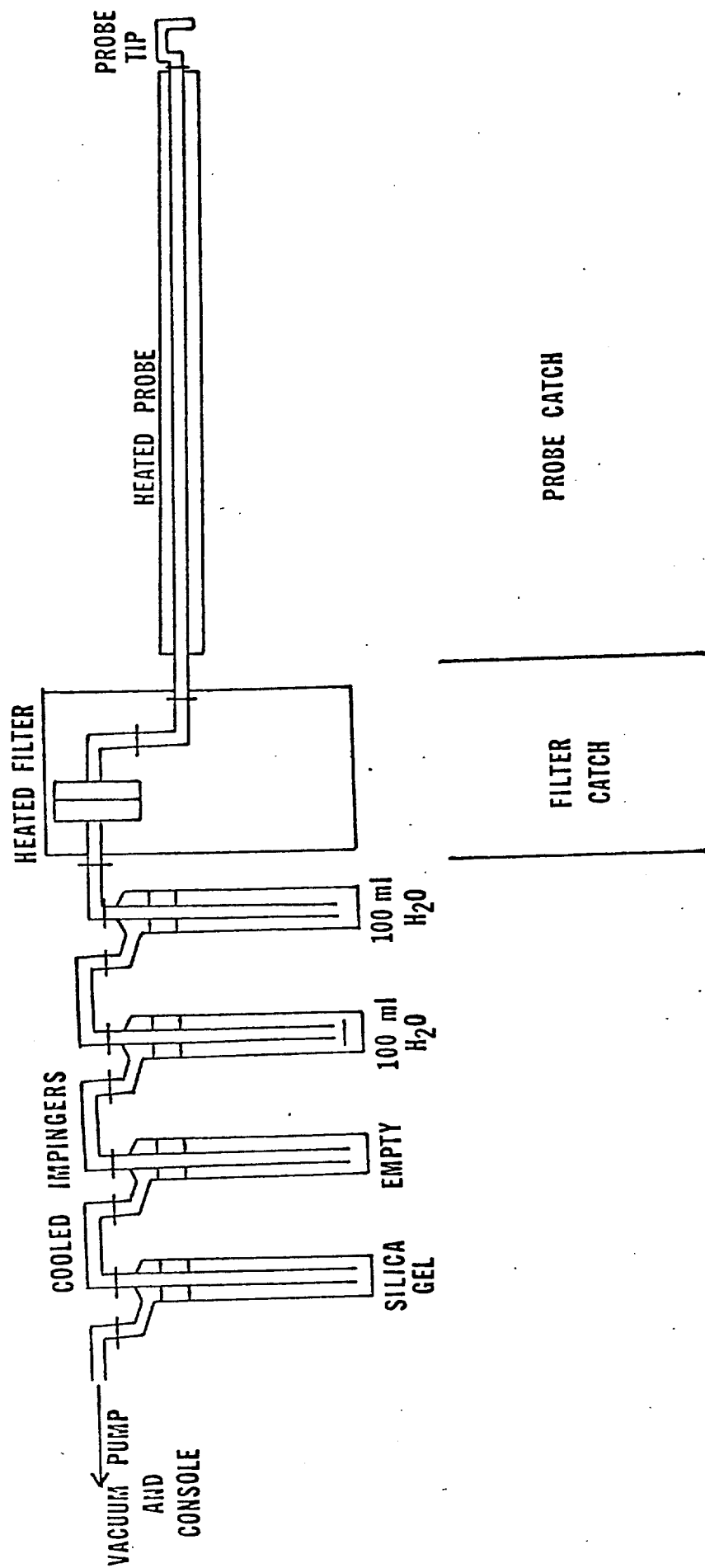


Figure 1. Schematic diagram of EPA Method V isokinetic sampling train for particulates.

PROCEDURE - After allowing 10 to 15 minutes for stabilization of the asphalt dryer mix plant after start-up, the stack was sampled at each of 24 traverse points, 12 points taken from each traverse diameter as shown in Figure 2. The stack schematic showing the location of the sampling ports and the upstream and downstream disturbances are presented in Figure 3. The total sampling time for Run 2 was 78 minutes. Total sampling time for Runs 3 and 4 was 84 minutes each. The sampling rate for all three tests met the 0.53 DSCF/minute criteria.

SAMPLING MEDIA - The major portion of the particulate was collected on a 4-inch dessicated and pre-weighed glass fibre filter contained in a glass filter holder, with a sintered glass frit, and enclosed in a heated compartment to prevent moisture condensation from plugging the filter during sampling. Some particulate was also deposited in the probe and on other sample exposed surfaces prior to the filter. These were cleaned after each test by rinsing with acetone and brushing.

The impinger train, for concurrent moisture collection, consisted of four impingers connected in series with glass ball joint fittings. The first, third, and fourth were of the straight bubbler type (modified Greenburg-Smith) and the second was of the standard Greenburg-Smith type. For the combined particulate and moisture determinations, the first

FIGURE 2.

TRAVERSE POINT LOCATION FOR CIRCULAR DUCTS

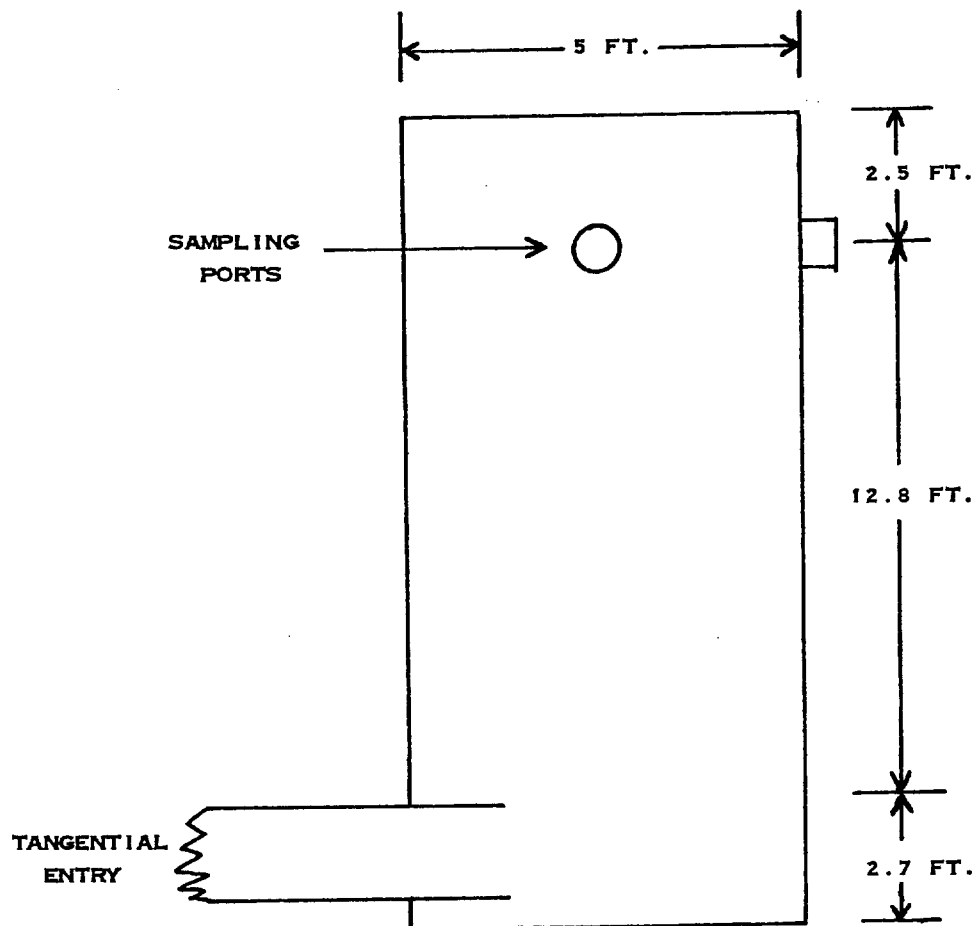
PLANT Klug Brothers, Inc.
DATE _____
SAMPLING LOCATION Asphalt Mix Plant
INSIDE OF FAR WALL TO
OUTSIDE OF NIPPLE, (DISTANCE A) _____
INSIDE OF NEAR WALL TO
OUTSIDE OF NIPPLE, (DISTANCE B) _____
STACK I.D., (DISTANCE A - DISTANCE B) 60 inches
NEAREST UPSTREAM DISTURBANCE _____
NEAREST DOWNSTREAM DISTURBANCE _____
CALCULATOR Whitt

SCHEMATIC OF SAMPLING LOCATION

[illegible]

FIGURE 3.

STACK SCHEMATIC
KLUG BROTHERS, INCORPORATED
MOUNDSVILLE, WEST VIRGINIA



two impingers contained 100-ml. of deionized water each, the third was empty, and the fourth contained between 200 and 300-grams of pre-weighed silica gel. After the test the volume of the condensate was measured and the percent moisture of the gas stream calculated.

The dry molecular weight of the stack gas was determined by FYRITE analysis for CO₂ and O₂ (CO and N₂ by difference) on a series of grab samples during each run.

SAMPLE ANALYSIS - Each sample filter and any loose particulate matter from the filter container was heated at 103 °C for two hours, cooled in a dessicator, and then weighed to the nearest 0.1 mg. on a analytical balance. The filters were then dessicated for another 24-hours and re-weighed. This was repeated until successive weighings agreed within 0.5-mg. or until a weight increase was noted. A control filter (extra pre-weighed filter taken through the same handling, dessication, and weighing as the sample filters) was used to determine a net change in weight, which was then applied as a blank to the sample filter weights.

The acetone washings from the probe and glassware forward of the filter were transferred to a previously dessicated and tared beaker, and evaporated to near dryness in a hood at room temperature and pressure. The nearly dry weighings were then placed in a laboratory drying oven at

103 - 105 °C for two hours to drive off residual water, then cooled in a dessicator and weighed. The oven drying, dessicator cooling cycle was repeated until successive weights agreed with 0.5-mg. or until a weight increase was noted. A acetone blank, from the same lot of acetone used for the probe washings was carried through the above evaporation and drying procedure along with the samples, and the net weight change found in the blank was applied as a correction to the particulate weight obtained from the samples.

RESULTS AND DISCUSSION

The particulate emission tests were conducted on September 3 and 4, 1987. Runs 2 and 3 being conducted on September 3, and Run 4 being conducted on September 4, 1987.

The results of the particulate emission tests are summarized in Table 1. The three determinations had an average particulate emission concentration of 0.0262 grs./DSCF compared to the emission standard of 0.04 grs./DSCF. The average total particulate emission rate was 1.16 lb./hr.

Process monitoring conducted during the three emission tests is summarized in Table 2. Dry aggregate feedrate was held fairly consistent during each of the three tests averaging 82.3 tons per hour. AC-20 asphalt bitum feedrate

TABLE 1.

Stack Gas Particulate Sampling Summary

<u>Sampling Data</u>	<u>Symbol</u>	<u>RUN 2</u>	<u>RUN 3</u>	<u>RUN 4</u>
Volume of Dry Gas Sampled at Standard Conditions, ^a DSCF ^b	$V_{m, std}$	41.351	53.334	51.155
@ Percent Isokinetic	%I	105.7	108.5	104.2
<u>Stack Gas Composition and Flow</u>				
Molecular Weight of Stack Gas, Dry Basis	MW_d	29.516	29.780	29.740
Molecular Weight of Stack Gas, Wet Basis	MW	25.969	25.585	25.828
Mole Fraction of Dry Gas	M_d	0.692	0.644	0.667
Percent Moisture in Stack Gas, by Volume	%M	30.8	35.6	33.3
Average Stack Gas Temperature, °F	T_g	163.0	167.0	165.9
Stack Gas Velocity at Stack Conditions, fpm	V_a	404.1	510.0	490.0
Stack Gas Volumetric Flow Rate at Stack Conditions, ACFM ^c	Q_a	7934.4	10,013.8	9622.1
Dry Stack Gas Volumetric Flow Rate at Standard Conditions, DSCFM ^d	Q_g	4608.0	5376.8	5307.6
<u>Total Particulate Emissions</u>				
Concentration of Particulates in Stack Gas, gr./DSCF	C'_g	0.0232	0.0290	0.0265
Total Particulate Emission Rate, lb/hr.	P_{tr}	0.92	1.34	1.22

^aStandard Conditions are 70°F and 29.92 in. Hg. ^bDry Standard Cubic Feet. ^cActual Cubic Feet per Minute (stack conditions). ^dDry Standard Cubic Feet per Minute.

TABLE 2.

PROCESS MONITORING SUMMARY

ASPHALT PLANT

KLUG BROTHERS, INCORPORATED

MOUNDSVILLE, WEST VIRGINIA

	Feed Bin Motor Speed			Aggregate Instantaneous	AC-20 Instantaneous	Aggregate Totalizer	Fuel Feedrate	Exhaust Set Point	Exhaust Temperature
	1	2	3	TPH	TPH	TPH	%	°F	°F
Run 2 Average	50.1	42	59.5	84.8	4.6	87.4	29.8	226	227
Run 3 Average	54	--	32	78.6	5.1	74.8	30.4	226	225.2
Run 4 Average	48	--	48	83.5	4.4	85.6	28.7	228.4	235.5

averaged 4.7 tons per hour. The fuel feedrate averaged 29.6% with an average exhaust temperature of 229 °F. The circular chart recording the asphalt product temperature plus the process monitoring data is presented in the appendix.

The pressure drop across the scrubber was not continuously monitored during the test. A magna-helic installed within the mist eliminator showed a consistent negative 14 to 15 inch water column during the three tests. The manufacture representative indicated that the static pressure before the scrubber remains fairly consistent at negative one-half inch water column.

The scrubber water analysis is presented in Table 3. Samples of the scrubber influent and effluent were composited during each test run and analyzed for pH and total suspended solids. The pH levels remained fairly constant during each of the three runs. The total suspended solids analysis showed that the scrubber was removing an average of 183 lbs./hr. of solids based on a 40 gallon per minute flowrate.

Cyclonic flow determinations were conducted at the facility to document the presence or absence of cyclonic flow patterns as a result of a tangential entry into the discharge stack. The preliminary (pre-test) determinations

TABLE 3. SCRUBBER WATER ANALYSIS
 KLUG BROTHERS, INCORPORATED
 MOUNDSVILLE, WEST VIRGINIA

		PH	Total Suspended Solids	
		S.U.	mg/l.	lbs./hr.*
Run 2	Feed	7.41	14.1	
	Discharge	7.31	10,400	
	Difference		10,386	208
Run 3	Feed	7.14	5.3	
	Discharge	7.30	7,360	
	Difference		7,355	147
Run 4	Feed	7.27	<1.0	
	Discharge	7.27	9,740	
	Difference		9,740	195

* Based on a scrubber water influent rate of 40 gpm

indicated cyclonic flow patterns that were unacceptable. The cyclonic flow was reduced by placing a baffle arrangement in the bottom of the stack.

The cyclonic flow determinations were conducted in accordance with the methodology as outlined in Part 60, Appendix A, Method 1, Section 2.4. During the preliminary cyclonic flow determinations and prior to the final installation of the baffles, the average rotation angle was 28.9 degrees. At that time modifications were made to the baffle assembly which resulted in an acceptable average rotation angle of 11.3 degrees. This determination was made with only the induced draft fan and scrubber sprays operating. Due to timing constraints the plant was not producing asphalt. A final cyclonic flow determination was completed at the time of the particulate emission test with the plant operating under load. The average rotational angle was then determined to be 0 degrees, which is an acceptable flow pattern for the particulate emission test.

APPENDIX I
CALIBRATIONS

7 July 1987

Console No. 51340

$$\text{Barometric Pressure, } P_b = \frac{28.86}{\text{in. Hg}}$$

Dry Gas Meter No. 3017861

operator(s) KLEMM

Orifice anometer Setting	Volume						Temperature				Elapsed Time	
	Wet Test Meter			Dry Gas Meter			Wet Test	Dry Gas Meter				
	Start	Stop	Volume	Start	Stop	Volume		Meter	Inlet	Outlet		Average
∞ H			V_w			V_d	T_w				T_d	0
in. H ₂ O	ft ³	ft ³	ft ³	ft ³	ft ³	ft ³	OF	OF	OF	OF	OF	min.
0.5 (s)	018.375	023.121	4.746	632.002	637.006	5.004	60°	100 } 102 } 106 }	76 } 78 } 80 }	94.9		12:01.75 12:02.9
1.0 (s)	024.060	028.758	4.698	638.001	643.003	5.002	60	106 } 111 } 114 }	80 } 82 } 84 }	100.7		8:37.61 8:60
2.0 (10)	029.717	039.158	9.441	644.004	654.106	10.102	60	114 } 123 } 124 }	84 } 90 }	108.2		12:31.39 12:52
4.0 (10)	040.000	049.325	9.325	655.005	665.007	10.002	60	120 } 122 } 133 }	88 } 90 }	114.9		8:53.24 8:59
6.0 (10)	050.251	059.583	9.332	666.006	676.044	10.038	60	130 } 134 } 135 }	95 } 98 }	119.2		7:21.50 7:37
8.0 (10)	060.577	069.886	9.309	677.110	687.134	10.024	60	132 } 136 } 138 }	99 } 100 }	122.1		6:23.44 6:40

2 of 2

Staksamplr Calibration Calculations

7/7/87

ΔH	$P_b + \frac{\Delta H}{13.6}$	$T_w + 460$	$T_d + 460$	γ	$H@$	
				$\frac{V_w P_b (T_d + 460)}{V_d \left(P_b + \frac{\Delta H}{13.6} \right) (T_w + 460)}$	$\frac{0.0317 \Delta H}{P_b (T_d + 460)}$	$\left[\frac{(T_w + 460) \phi}{V_w} \right]^2$
0.5	28.90	520	554.9	1.014	1.719	
1.0	28.93	520	560.9	1.010	1.800	
2.0	29.01	520	568.2	1.016	1.839	
4.0	29.15	520	574.9	1.020	1.877	
6.0	29.30	520	579.2	1.020	1.916	
8.0	29.45	520	582.1	1.019	1.929	

CONSOLE CALIBRATION WORKSHEET

Date: 7 July 1987

Operator: R.B.Klemm Jr.

Console # S-1340

Barometer: 28.86

Dry Gas Meter # 3017861 (T=60°F)

dH (in W.C.)	V(w) (ft ³)	V(d) (ft ³)	T(i) (°F)	T(o) (°F)	T(d) (°R)	Time (min)	Pb+dH (in Hg)	Gamma	H@
0.5	18.375	632.002	100.0	76.0					
	23.121	637.006	102.0	78.0					
	4.746	5.004	106.0	80.0	554.9	12.03	28.90	1.011	1.719
1.0	24.060	638.001	106.0	80.0					
	28.758	643.003	111.0	82.0					
	4.698	5.002	114.0	84.0	560.7	8.66	28.93	1.010	1.800
2.0	29.717	644.004	114.0	84.0					
	39.158	654.106	123.0	87.0					
	9.441	10.102	124.0	90.0	568.2	12.52	29.01	1.016	1.839
4.0	40.000	655.005	122.0	90.0					
	49.325	665.007	130.0	93.0					
	9.325	10.002	133.0	94.0	574.9	8.89	29.15	1.020	1.877
6.0	50.251	666.006	130.0	95.0					
	59.583	676.044	134.0	96.0					
	9.332	10.038	135.0	98.0	579.2	7.37	29.30	1.020	1.916
8.0	60.577	677.110	132.0	98.0					
	69.886	687.134	136.0	100.0					
	9.309	10.024	138.0	101.0	582.1	6.40	29.45	1.019	1.929

Stacksample Calibration

14 Sept 1987

Console No. S-1340

Barometric Pressure, $P_b = 28.83$ in. Hg

Dry Gas Meter No. 3017861

Operator(s) Klemm

After Kline Bros. Asphar Emissions Testing.

1200-1400

Ice meter testing	Volume						Temperature			Elapsed Time		
	Wet Test Meter			Dry Gas Meter			Wet Test	Dry Gas Meter				
	Start	Stop	Volume	Start	Stop	Volume		Meter	Inlet		Outlet	Average
H			V_w			V_d	T_w	$+4.65^{\circ}$	$+2.90^{\circ}$	T_d	ϕ	
H ₂ O	ft ³	ft ³	ft ³	ft ³	ft ³	ft ³	OF	OF	OF	OF	min.	
0.5	087.953	092.640	4.687	894.200	899.201	5.001	60°F	61 82 83	99 102 108	96.3	11:54.62	
1.0	098.070	102.720	4.650	905.001	910.002	5.001	60°F	88 90 91	112 119 120	107.1	8:36.46	
1.5	103.179	112.429	9.250	910.503	920.505	10.002	60°F	92 95 98	120 128 132	114.6	12:14.72	
2.0	113.364	122.589	9.225	921.505	931.506	10.001	60°F	98 100 102	132 139 144	122.9	8:51.38	
2.5	123.510	132.758	9.248	932.509	942.515	10.006	60°F	102 104 106	142 146 150	128.8	7:18.69	
3.0	135.076	144.324	9.248	945.008	955.012	10.004	60°F	108 108 108	146 147 149	131.4	6:22.05	

Leak check: $\phi t = 0 \rightarrow 086.752 \text{ ft}^3$

Pretest: $\phi t = 1 \text{ min} \rightarrow 086.752 \text{ ft}^3$

Vac = 13 in Hg.

Staksamplr Calibration Calculations

14 Sept 1987

ΔH	$P_b + \frac{\Delta H}{13.6}$	$T_w + 460$	$T_d + 460$	γ	HQ	
					$\frac{0.0317 \Delta H}{P_b (T_d + 460)}$	$\left[\frac{(T_w + 460) \phi}{V_w} \right]^2$
0.5	28.87	520	556.3	1.001	1.726	
1.0	28.90	520	567.1	1.011	1.796	
2.0	28.98	520	574.6	1.017	1.814	
4.0	29.12	520	582.9	1.024	1.880	
6.0	29.17	520	588.8	1.031	1.894	
8.0	29.42	520	591.4	1.030	1.917	

CONSOLE CALIBRATION WORKSHEET

Date: 14 September 1987

Operator: R.B.Klemm Jr.

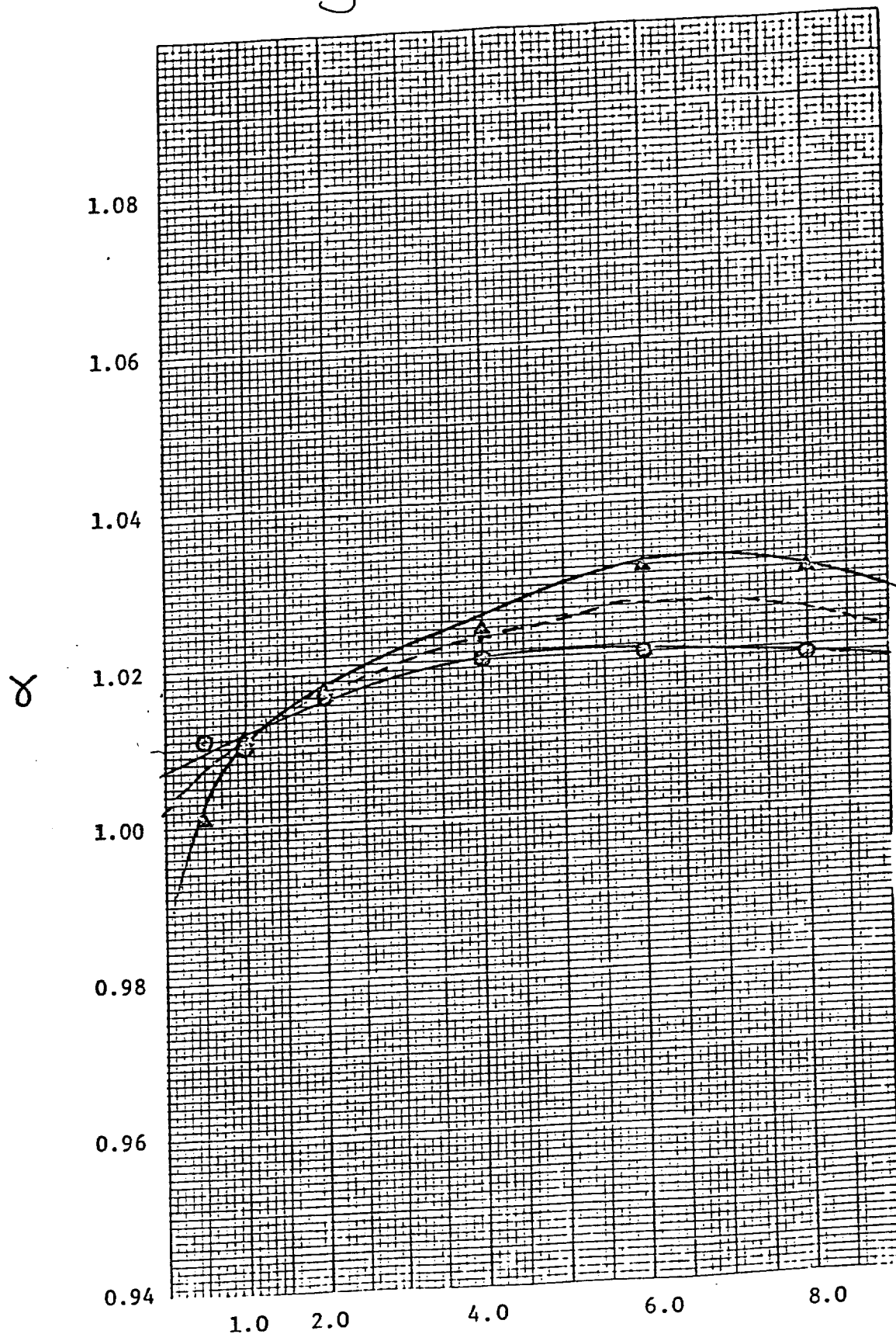
Console # S-1340

Barometer: 28.83

Dry Gas Meter # 3017861 (T=60°F)

dH (in W.C.)	V(w) (ft ³)	V(d) (ft ³)	T(i) (°F)	T(o) (°F)	T(d) (°R)	Time (min)	Pb+dH (in Hg)	Gamma	H _e
0.5	87.953	894.200	99.0	81.0					
	92.640	899.201	102.0	82.0					
	4.687	5.001	108.0	83.0	556.3	11.91	28.87	1.001	1.726
1.0	98.070	905.001	112.0	88.0					
	102.720	910.002	119.0	90.0					
	4.650	5.001	120.0	91.0	567.1	8.61	28.90	1.011	1.796
2.0	103.179	910.503	120.0	92.0					
	112.429	920.505	128.0	95.0					
	9.250	10.002	132.0	98.0	574.6	12.25	28.98	1.017	1.814
4.0	113.364	921.505	132.0	98.0					
	122.589	931.506	139.0	100.0					
	9.225	10.001	144.0	102.0	582.9	8.86	29.12	1.024	1.880
6.0	123.510	932.509	142.0	102.0					
	132.758	942.515	146.0	104.0					
	9.248	10.006	150.0	106.0	588.8	7.31	29.27	1.031	1.894
8.0	135.076	945.008	146.0	108.0					
	144.324	955.012	147.0	108.0					
	9.248	10.004	149.0	108.0	591.4	6.38	29.42	1.030	1.917

CONSOLE CALIBRATION
Klug Bros. Asphalt.



S-Type Pitot Tube Calibration Data

Date 9/2/87 Calibrated by Whitt/Coleman

S-Type Pitot Tube Identification SS / 5 ft Probe $c_p = R = 0.760$

Calibration Setup: Normal - Pitot Leads Down
Reverse - Pitot Leads Up

$$C_p = 0.99 \sqrt{\frac{\Delta P_{STD}}{\Delta P_{S-TYPE}}}$$

Test No.	Pitot Tube Readings (in. H ₂ O)				
	Standard	S-Type			
		Normal	C_p	Reversed	C_p
1	0.26	0.43	0.770	0.43	0.770
2	0.26	0.43	0.770	0.45	0.753
3	0.27	0.43	0.784	0.46	0.758
Average			0.775	Average	0.760

APPENDIX II
PARTICULATE ANALYTICAL DATA

Klug Bros. Inc.
Moundsville, W.V.

Concentration of Particulate Matter in Stack, grs./DSCF

$$C'_s = 0.0154 \frac{M_p}{V_{m, \text{std}}}$$

Where M_p = Milligrams of particulate collected

Run 2

$$C'_s = 0.0154 \left(\frac{62.4}{41.351} \right)$$

$$C'_s = 0.0232 \checkmark \text{ grs./DSCF}$$

Run 3

$$C'_s = 0.0154 \left(\frac{100.4}{53.334} \right)$$

$$C'_s = 0.0290 \checkmark \text{ grs./DSCF}$$

Run 4

$$C'_s = 0.0154 \left(\frac{88.0}{51.155} \right)$$

$$C'_s = 0.0265 \checkmark \text{ grs./DSCF}$$

Klug Bros. Inc.
Moundsville, W. V.

Total Particulate Emission Rate, lb./hr:

$$P_{tr} = 0.008571(C'_s)(Q_s)$$

Run 2

$$P_{TR} = 0.008571(0.0232)(4608)$$

$$P_{TR} = 0.92 \checkmark \text{ lb/hr}$$

Run 3

$$P_{TR} = 0.008571(0.0290)(5377)$$

$$P_{TR} = 1.34 \checkmark \text{ lb/hr}$$

Run 4

$$P_{TR} = 0.008571(0.0265)(5370)$$

$$P_{TR} = 1.22 \text{ lb/hr}$$

Average P_{TR} = 1.16 lb/hr

TRADE LABORATORIES

930 Kinnear Road, Columbus, Ohio

Phone: 614-299-9229

Mailing Address: P.O. Box 12069, Columbus, Ohio 43212

Wheeling-Ohio County Airport, Wheeling, W.Va. 26003 Phone: 304-277-4350

PARTICULATE ANALYTICAL DATA

Plant Klug Bros, Inc. Run 2

Location Moundsville, W.V. Date 9/3/87

MOISTURE:

Impinger	<u>1</u>	<u>2</u>	<u>4</u>
Final Volume	<u>364 ml</u>	<u>212 ml</u>	<u>298.4-52.5</u>
Initial Volume	<u>100 ml</u>	<u>100 ml</u>	<u>286.1-52.5</u>
Net Volume	<u>264 ml</u>	<u>112 ml</u>	<u>12.3</u>

Total Weight of Water Collected 388.3 grams

PARTICULATES:	<u>Filter</u>	<u>Probe Wash</u>	<u>Wet Catch</u>
Designation Number	<u>171</u>	<u>127 ml</u>	<u>—</u>
Final Weight (1)	<u>0.7993</u>	<u>73.8471</u>	<u>—</u>
Final Weight (2)	<u>0.7983</u>	<u>73.8470</u>	<u>—</u>
Final Weight (3)	<u>0.7982</u>	<u>73.8470</u>	<u>—</u>
Final Weight (4)	<u>0.7983</u>	<u>—</u>	<u>—</u>
Initial Weight (1)	<u>0.7461</u>	<u>73.8368</u>	<u>—</u>
Initial Weight (2)	<u>0.7460</u>	<u>—</u>	<u>—</u>
Net Weight	<u>0.0522</u> ✓	<u>0.0102</u>	<u>—</u>
Blank Correction	<u>negligible</u> ✓	<u>negligible</u>	<u>—</u>
Corrected Net Weight	<u>0.0522</u>	<u>0.0102</u> ✓	<u>—</u>
Total Weight Without Wet Catch	<u>0.0624</u> ✓	<u>—</u>	<u>—</u> grams
Total Weight With Wet Catch	<u>—</u>	<u>—</u>	<u>—</u> grams

TRADEI LABORATORIES

930 Kinnear Road, Columbus, Ohio

Phone: 614-299-9229

Mailing Address: P.O. Box 12069, Columbus, Ohio 43212

Wheeling-Ohio County Airport, Wheeling, W.Va. 26003 Phone: 304-277-4350

PARTICULATE ANALYTICAL DATA

Plant Klug Bros. Inc. Run 3

Location Moundsville, W.V. Date 9/3/87

MOISTURE:

Impinger	<u>1</u>	<u>2</u>	<u>4</u>
Final Volume	<u>378 ml</u>	<u>412 ml</u>	<u>278.3-52.5</u>
Initial Volume	<u>100 ml</u>	<u>100 ml</u>	<u>246.0-52.5</u>
Net Volume	<u>278 ml</u>	<u>312 ml</u>	<u>32.3</u>

Total Weight of Water Collected 622.3 grams

PARTICULATES:

	<u>Filter</u>	<u>Probe Wash</u>	<u>Wet Catch</u>
Designation Number	<u>173</u>	<u>261 ml</u>	<u>—</u>
Final Weight (1)	<u>0.8351</u>	<u>76.6647</u>	<u>—</u>
Final Weight (2)	<u>0.8346</u>	<u>76.6646</u>	<u>—</u>
Final Weight (3)	<u>0.8343</u>	<u>—</u>	<u>—</u>
Final Weight (4)	<u>0.8347</u>	<u>—</u>	<u>—</u>
Initial Weight (1)	<u>0.7522</u>	<u>76.6463</u>	<u>—</u>
Initial Weight (2)	<u>0.7522</u>	<u>—</u>	<u>—</u>
Net Weight	<u>0.0821</u> ✓	<u>0.0183</u> ✓	<u>—</u>
Blank Correction	<u>negligible</u>	<u>negligible</u>	<u>—</u>
Corrected Net Weight	<u>0.0821</u>	<u>0.0183</u>	<u>—</u>
Total Weight Without Wet Catch	<u>0.1004</u> ✓	<u>—</u>	<u>—</u> grams
Total Weight With Wet Catch	<u>—</u>	<u>—</u>	<u>—</u> grams

TRADEI LABORATORIES

930 Kinnear Road, Columbus, Ohio

Phone: 614-299-9229

Mailing Address: P.O. Box 12069, Columbus, Ohio 43212

Wheeling-Ohio County Airport, Wheeling, W.Va. 26003 Phone: 304-277-4350

PARTICULATE ANALYTICAL DATA

Plant Klug Bros., Inc. Run 4

Location Moundsville, W.V. Date 9/4/87

MOISTURE:

Impinger	<u>1</u>	<u>2</u>	<u>4</u>
Final Volume	<u>398 ml</u>	<u>316 ml</u>	<u>428.7-52.5 g</u>
Initial Volume	<u>100 ml</u>	<u>100 ml</u>	<u>455.9-105.0</u>
Net Volume	<u>298 ml</u>	<u>216 ml</u>	<u>25.3 g</u>

Total Weight of Water Collected 539.3 grams

PARTICULATES:	<u>Filter</u>	<u>Probe Wash</u>	<u>Wet Catch</u>
Designation Number	<u>174</u>	<u>388 ml</u>	<u>—</u>
Final Weight (1)	<u>0.8240</u>	<u>80.7878</u>	<u>—</u>
Final Weight (2)	<u>0.8234</u>	<u>80.7875</u>	<u>—</u>
Final Weight (3)	<u>0.8240</u>	<u>—</u>	<u>—</u>
Final Weight (4)	<u>0.8241</u>	<u>—</u>	<u>—</u>
Initial Weight (1)	<u>0.7513</u>	<u>80.7716</u>	<u>—</u>
Initial Weight (2)	<u>0.7513</u>	<u>—</u>	<u>—</u>
Net Weight	<u>0.0721</u> ✓	<u>0.0159</u> ✓	<u>—</u>
Blank Correction	<u>negligible</u>	<u>negligible</u>	<u>—</u>
Corrected Net Weight	<u>0.0721</u>	<u>0.0159</u>	<u>—</u>
Total Weight Without Wet Catch	<u>0.0880</u> ✓	<u>—</u>	<u>—</u> grams
Total Weight With Wet Catch	<u>—</u>	<u>—</u>	<u>—</u> grams

TRADET LABORATORIES

930 Kinnear Road, Columbus, Ohio

Mailing Address: P.O. Box 12069, Columbus, Ohio 43212

Phone: 614-299-9229

Wheeling-Ohio County Airport, Wheeling, W.Va. 26003 Phone: 304-277-4350

PARTICULATE ANALYTICAL DATA

Plant Klug Bros. Inc Run Blacks

Location Tradet, Inc Date 9/3/87

MOISTURE:

	<u>1</u>	<u>2</u>	<u>4</u>
Impinger			
Final Volume			
Initial Volume			
Net Volume			

Total Weight of Water Collected _____ grams

PARTICULATES:	<u>Filter</u>	<u>Probe Wash</u>	<u>Wet Catch</u>
Designation Number	<u>175</u>	<u>100ml</u>	—
Final Weight (1)	<u>0.7532</u>	<u>72.2560</u>	
Final Weight (2)	<u>0.7528</u>	<u>72.2563</u>	
Final Weight (3)	<u>0.7529</u>	<u>72.2567</u>	
Final Weight (4)	<u>0.7529</u>		
Initial Weight (1)	<u>0.7529</u>	<u>72.2559</u>	
Initial Weight (2)	<u>0.7529</u>		
Net Weight	<u>0.0001</u>	<u>0.0001</u>	
Blank Correction	<u>negligible</u>	<u>negligible</u>	
Corrected Net Weight	<u>—</u>	<u>—</u>	
Total Weight Without Wet Catch			grams
Total Weight With Wet Catch			grams

Stack Sampling Data Input

RUN 2

```

PARTICULATE
STACK SAMPLING

SAMPLING DATA

RUN NO? 2.000 ✓
BAR. PRESS. IN. HG? 29.520 ✓
STACK DIAM. IN? 60.000 ✓
NOZZLE DIAM. IN? 0.625 ✓
RUN TIME, MIN? 28.000 ✓
CORR. DRY GAS VOL 44.199 ✓
AVG DELTA H? 1.000 ✓
AVG. STACK TEMP? 163.000 ✓
AVG. METER TEMP? 130.200 ✓
AVG. SORT. DELTA P 0.115 ✓
PITOT COEFF. ? 0.760 ✓
STACK STAT. PRESS 29.520 ✓
TOT. INFLING. H? 600.300 ✓
CORR. DRY GAS VOL 44.199 ✓
% OXYGEN? 7.800 ✓
6.700 ✓

```

RUN 3

```

PARTICULATE
STACK SAMPLING

SAMPLING DATA

RUN NO? 3.000 ✓
BAR. PRESS. IN. HG? 29.520 ✓
STACK DIAM. IN? 60.000 ✓
NOZZLE DIAM. IN? 0.625 ✓
RUN TIME, MIN? 34.000 ✓
CORR. DRY GAS VOL 57.966 ✓
AVG DELTA H? 1.480 ✓
AVG. STACK TEMP? 167.000 ✓
AVG. METER TEMP? 110.300 ✓
AVG. SORT. DELTA P 0.144 ✓
PITOT COEFF. ? 0.760 ✓
STACK STAT. PRESS 29.520 ✓
TOT. INFLING. H? 622.300 ✓
CORR. DRY GAS VOL 57.966 ✓
% OXYGEN? 7.800 ✓
7.100 ✓

```

RUN 4

```

PARTICULATE
STACK SAMPLING

SAMPLING DATA

RUN NO? 4.000 ✓
BAR. PRESS. IN. HG? 29.580 ✓
STACK DIAM. IN? 60.000 ✓
NOZZLE DIAM. IN? 0.625 ✓
RUN TIME, MIN? 34.000 ✓
CORR. DRY GAS VOL 52.768 ✓
AVG DELTA H? 1.280 ✓
AVG. STACK TEMP? 165.900 ✓
AVG. METER TEMP? 88.100 ✓
AVG. SORT. DELTA P 0.139 ✓
PITOT COEFF. ? 0.760 ✓
STACK STAT. PRESS 29.580 ✓
TOT. INFLING. H? 621.300 ✓
CORR. DRY GAS VOL 52.768 ✓
% OXYGEN? 7.800 ✓
7.200 ✓

```

Stack Sampling Calculated Data

RUN 2

V(W) STD., DSCF=
41.351

V(W) GAS, SCF=
18.405

%MOISTURE=30.801
%

M(D)= 0.692

MW(D)= 29.518

MW= 25.969

V(A), FPM=404.097

%I= 105.705%

Q(A), ACFM=
7934.426

Q(S), DSCFM=
4608.000

P(S), LBS./CU.FT=
0.056

RUN 3

V(W) STD., DSCF=
53.334

V(W) GAS, SCF=
29.497

%MOISTURE=35.611
%

M(D)= 0.644

MW(D)= 29.780

MW= 25.585

V(A), FPM=509.996

%I= 108.497%

Q(A), ACFM=
10013.745

Q(S), DSCFM=
5376.797

P(S), LBS./CU.FT=
0.055

RUN 4

V(W) STD., DSCF=
51.155

V(W) GAS, SCF=
25.563

%MOISTURE=33.321
%

M(D)= 0.667

MW(D)= 29.740

MW= 25.828

V(A), FPM=490.048

%I= 134.185%

Q(A), ACFM=
9622.062

Q(S), DSCFM=
5370.573

P(S), LBS./CU.FT=
0.056

APPENDIX III
VELOCITY DATA

PRELIMINARY VELOCITY TRAVERSE

Plant Klug Bros, Inc

Date 7/24/87

Location Asphalt Plant - Martinsville, W.V.

Stack I.D. 5 feet

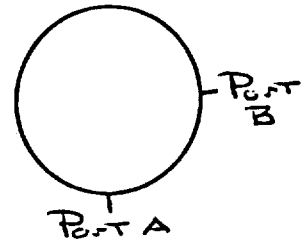
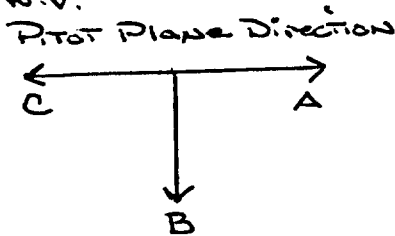
Barometric Pressure, in Hg —

Stack Gauge Pressure, in. H₂O —

Operators W.M.P. / H.V. and

Pitot Coefficient (Cp) —

Run Number —



Schematic of Traverse Point Layout

Traverse Point Number	Stack Temperature (Ts), °F	Velocity Head (ΔPs), in H ₂ O	$\sqrt{\Delta Ps}$ ROTATED ANGLE
1 A	Port A		27°
B			
C			0°
2 A			26°
B			
C			0°
3 A			30°
B			
C			0°
4 A			32°
B			
C			0°
5 A			32°
B			
C			0°
6 A			15°
B			
C			0°
Average			

Traverse Point Number	Stack Temperature (Ts), °F	Velocity Head (ΔPs), in H ₂ O	$\sqrt{\Delta Ps}$ ROTATION ANGLE
7 A			0°
B			
C			15°
8 A			0°
B			
C			26°
9 A			0°
B			
C			31°
10 A			0°
B			
C			27°
11 A			0°
B			
C			21°
12 A			0°
B			
C			20°
Average			25.2°

PRELIMINARY VELOCITY TRAVERSE

Plant Klug Bros, Inc.

Date 7/24/87

Location Asphalt Plant - Moundsville, W.V.

Stack I.D. 5 feet

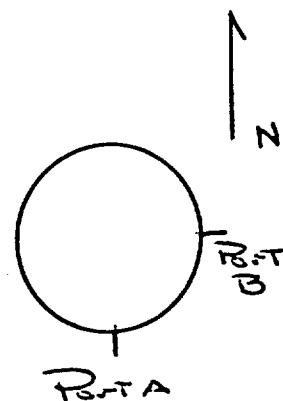
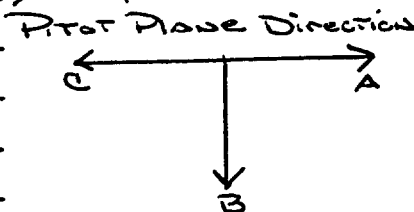
Barometric Pressure, in Hg -

Stack Gauge Pressure, in. H₂O -

Operators W.H.P. / H.V.A.W.

Pitot Coefficient (Cp) -

Run Number -



Schematic of Traverse Point Layout

Traverse Point Number	Stack Temperature (Ts), °F	Velocity Head (ΔPs), in H ₂ O	$\sqrt{\Delta Ps}$ ROTATION ANGLE
1 A	Re-T B		75°
B			
C			0°
2 A			45°
B			
C			0°
3 A			45°
B			
C			0°
4 A			42°
B			
C			0°
5 A			0°
B			
C			0°
6 A			0°
B			
C			0°
Average			

Traverse Point Number	Stack Temperature (Ts), °F	Velocity Head (ΔPs), in H ₂ O	$\sqrt{\Delta Ps}$ ROTATION ANGLE
7 A			0°
B			
C			15°
8 A			0°
B			
C			29°
9 A			0°
B			
C			29°
10 A			0°
B			
C			35°
11 A			0°
B			
C			32°
12 A			0°
B			
C			46°
Average			32.75°

PRELIMINARY VELOCITY TRAVERSE

Plant Klug Bros., Inc

Date 8/5/87

Location Asphalt Plant - Moundsville, W.V.

Stack I.D. 5 feet

Barometric Pressure, in Hg -

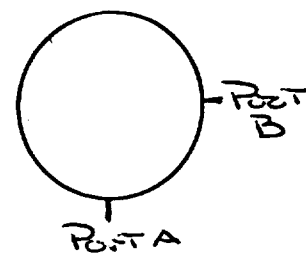
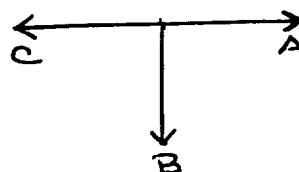
Stack Gauge Pressure, in. H₂O -

Operators W. J. W. / K. L. W.

Pitot Coefficient (Cp) -

Run Number -

Pitot Plane Direction



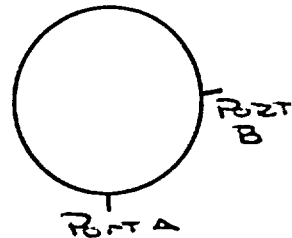
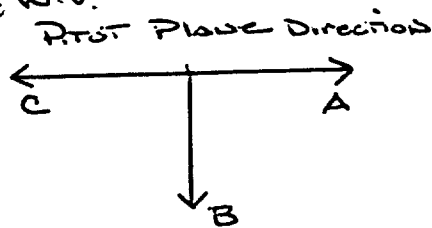
Schematic of Traverse Point Layout

Traverse Point Number	Stack Temperature (Ts), °F	Velocity Head (ΔPs), in H ₂ O	Rotation Angle
1 A	Port A	0.01	15°
1 B		0.01	
1 C		0.0	0°
2 A		0.01	20°
2 B		0.01	
2 C		0.0	0°
3 A		0.0	0°
3 B		0.01	
3 C		0.0	0°
4 A		0.0	0°
4 B		0.01	
4 C		0.0	0°
5 A		0.0	0°
5 B		0.015	
5 C		0.0	0°
6 A		0.0	0°
6 B		0.02	
6 C		0.0	0°
Average			

Traverse Point Number	Stack Temperature (Ts), °F	Velocity Head (ΔPs), in H ₂ O	Rotation Angle
7 A		0.0	0°
7 B		0.03	
7 C		0.0	0°
8 A		0.0	0°
8 B		0.03	
8 C		0.01	2.5°
9 A		0.0	0°
9 B		0.03	
9 C		0.0	0°
10 A		0.0	0°
10 B		0.03	
10 C		0.02	10°
11 A		0.0	0°
11 B		0.045	
11 C		0.03	15°
12 A		0.0	0°
12 B		0.06	
12 C		0.05	27.5°
Average			7.5°

PRELIMINARY VELOCITY TRAVERSE

Plant Klug Buses, Inc.
 Date 8/5/87
 Location Asphalt Plant - Moundsville, W.V.
 Stack I.D. 5 Feet
 Barometric Pressure, in Hg -
 Stack Gauge Pressure, in. H₂O -
 Operators W.H. / K. / M.
 Pitot Coefficient (Cp) -
 Run Number -



Schematic of Traverse Point Layout

Traverse Point Number	Stack Temperature (Ts), °F	Velocity Head (ΔPs), in H ₂ O	√ΔPs Rotation Angle
1 A	Pit B	0.05	37.5°
B		0.065	
C		0.0	0°
2 A		0.03	35°
B		0.05	
C		0.0	0°
3 A		0.03	27.5°
B		0.05	
C		0.0	0°
4 A		0.025	27.5°
B		0.04	
C		0.0	0°
5 A		0.02	20°
B		0.035	
C		0.0	0°
6 A		0.0	0°
B		0.02	
C		0.0	0°
Average			

Traverse Point Number	Stack Temperature (Ts), °F	Velocity Head (ΔPs), in H ₂ O	√ΔPs Rotation Angle
7 A		0.0	0°
B		0.04	
C		0.01	2.5°
8 A		0.0	0°
B		0.04	
C		0.01	2.5°
9 A		0.0	0°
B		0.04	
C		0.02	10°
10 A		0.0	0°
B		0.045	
C		0.025	7.5°
11 A		0.0	0°
B		0.025	
C		0.01	2.0°
12 A		0.0	0°
B		0.04	
C		0.03	10°
Average			15.2°

PRELIMINARY VELOCITY TRAVERSE

Plant Klug Bros. Inc.

Date 9/4/87

Location Asphalt - Mountville, W.V.

Stack I.D. 5 feet

Barometric Pressure, in Hg -

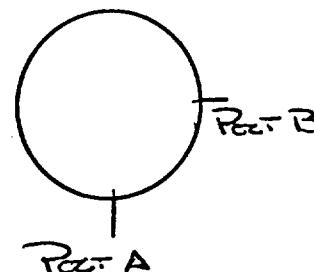
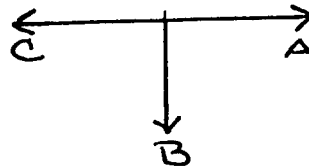
Stack Gauge Pressure, in. H₂O -

Operators W.H.P. / Coleman

Pitot Coefficient (Cp) -

Run Number -

Pitot Plane Direction



Schematic of Traverse Point Layout

Traverse Point Number	Stack Temperature (T _s), °F	Velocity Head (ΔPs), in H ₂ O	ΔPs Rotated Angle
A	Pitot A	0.0	0°
B			
C		0.0	0°
A		0.0	0°
B			
C		0.0	0°
A		0.0	0°
B			
C		0.0	0°
A		0.0	0°
B			
C		0.0	0°
A		0.0	0°
B			
C		0.0	0°
A		0.0	0°
B			
C		0.0	0°
Average			

Traverse Point Number	Stack Temperature (T _s), °F	Velocity Head (ΔPs), in H ₂ O	ΔPs Rotated Angle
7 A		0.0	0°
B			
C		0.0	0°
8 A		0.0	0°
B			
C		0.0	0°
9 A		0.0	0°
B			
C		0.0	0°
10 A		0.0	0°
B			
C		0.0	0°
11 A		0.0	0°
B			
C		0.0	0°
12 A		0.0	0°
B			
C		0.0	0°
Average			0°

PRELIMINARY VELOCITY TRAVERSE

Plant Klug Bros, Inc.

Date 9/4/87

Location Asphalt Plant - Meadowsville, W.V.

Stack I.D. 5 feet

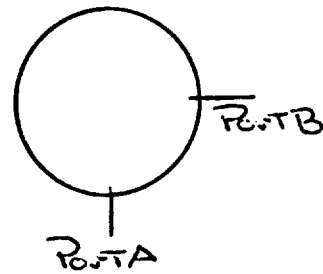
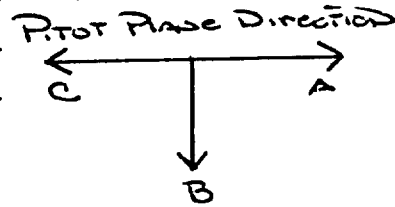
Barometric Pressure, in Hg -

Stack Gauge Pressure, in. H₂O -

Operators Whitt / Coleman

Pitot Coefficient (Cp) -

Run Number -



Schematic of Traverse Point Layout

Traverse Point Number	Stack Temperature (Ts), °F	Velocity Head (ΔPs), in H ₂ O	$\sqrt{\Delta Ps}$ ROTATION ANGLE
1 A	P-2TB	0.0	0°
1 B			
1 C		0.0	0°
2 A		0.0	0°
2 B			
2 C		0.0	0°
3 A		0.0	0°
3 B			
3 C		0.0	0°
4 A		0.0	0°
4 B			
4 C		0.0	0°
5 A		0.0	0°
5 B			
5 C		0.0	0°
6 A		0.0	0°
6 B			
6 C		0.0	0°
Average			

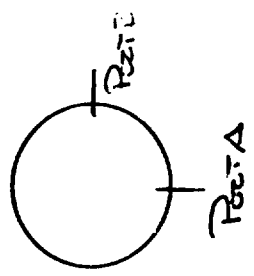
Traverse Point Number	Stack Temperature (Ts), °F	Velocity Head (ΔPs), in H ₂ O	$\sqrt{\Delta Ps}$ ROTATION ANGLE
7 A		0.0	0°
7 B			
7 C		0.0	0°
8 A		0.0	0°
8 B			
8 C		0.0	0°
9 A		0.0	0°
9 B			
9 C		0.0	0°
10 A		0.0	0°
10 B			
10 C		0.0	0°
11 A		0.0	0°
11 B			
11 C		0.0	0°
12 A		0.0	0°
12 B			
12 C		0.0	0°
Average			0°

APPENDIX IV

FIELD DATA

2

PROBE LENGTH AND TYPE 5FT 3/8
 NOZZLE I.D. 3/8" = 0.625 inches
 ASSUMED MOISTURE, % 24
 SAMPLE BOX NUMBER _____
 METER BOX NUMBER _____
 METER ΔH _____
 C FACTOR Cp (Rev) 0.760
 PROBE HEATER SETTING 80-90%
 HEATER BOX SETTING 200-250
 REFERENCE $V_s = 71$



SCHEMATIC OF TRAVERSE POINT LAYOUT
READ AND RECORD ALL DATA EVERY _____ MIN

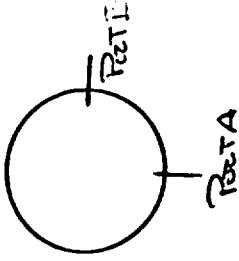
[illegible]

COMMENTS: Prec. Leak Check
SINTER - 7732. 713
③ 8" Hg for 60 sec.

FIELD TA

PLANT Kiva Buss Inc.
 DATE 9/3/87
 SAMPLING LOCATION Asphalt Plant
 SAMPLE TYPE Particulate
 RUN NUMBER 170 (2)
 OPERATOR W. H. H.
 AMBIENT TEMPERATURE 60.50 F
 BAROMETRIC PRESSURE 29.52
 STATIC PRESSURE, (P_s) -
 FILTER NUMBER (s) 171

PROBE LENGTH AND TYPE 5 ft 5/8
 NOZZLE I.D. 3/8" = 0.625 in.
 ASSUMED MOISTURE, % 2.9
 SAMPLE BOX NUMBER -
 METER BOX NUMBER -
 METER ΔH -
 C FACTOR CP (REV) 0.760
 PROBE HEATER SETTING 80-90%
 HEATER BOX SETTING 200-250
 REFERENCE VS = 71



SCHEMATIC OF TRAVERSE POINT LAYOUT

READ AND RECORD ALL DATA EVERY _____ MINUTES

TRAVERSE POINT NUMBER	CLOCK TIME SAMPLING TIME, min	GAS METER READING (V _m), ft ³	VELOCITY HEAD (ΔP _s), in. H ₂ O	ORIFICE PRESSURE DIFFERENTIAL (ΔH), in. H ₂ O		STACK TEMPERATURE (T _s), °F	DRY GAS METER TEMPERATURE		PUMP VACUUM, in. Hg	SAMPLE BOX TEMPERATURE, °F	IMPIPING TEMPERATURE, °F
				DESIRED	ACTUAL		INLET (T _{m in}), °F	OUTLET (T _{m out}), °F			
A-1	0	744.742	0.015	1.05	1.05	151.1	98	90	4.0	0.1225	56
2	3.5	747.0	0.02	1.42	1.42	153.4	94	90	4.5	0.1414	60
3	7.0	749.4	0.025	1.75	1.75	158.1	102	96	5.5	0.1581	59
4	10.5	752.0	0.022	1.51	1.51	158.1	106	91	4.0	0.1483	58
5	14.0	754.4	0.015	1.05	1.05	158.3	110	92	4.0	0.1225	59
6	17.5	756.5	0.01	0.71	0.71	157.8	110	94	3.0	0.1000	59
7	21.0	758.2	0.005	0.36	0.36	158.7	110	94	3.0	0.0707	59
8	24.5	759.6	0.005	0.36	0.36	160.7	110	96	3.0	0.0707	59
9	28.0	760.8	0.005	0.36	0.36	159.3	110	97	3.0	0.0707	59
10	31.5	762.1	0.005	0.36	0.36	159.8	110	98	3.0	0.0707	59
11	35.0	763.3	0.005	0.36	0.36	164.5	110	99	3.0	0.0707	59
12	38.5	764.5	0.009	0.64	0.64	164.6	112	100	3.0	0.0949	59
STOP	42.0	766.437									
		AV _m = 21.695		0.83	158.7	158.7	106	94.2		0.1034	59.1
						161.4	107.7	97.1			
		V _m = 43.718		1.00	163.0	163.0	107.8	97.7		0.1150	59.4
							100.2				

COMMENTS:

POST LEAK CHECK

START 766.454

STOP 766.457

0.003 FT³ @ 5.5" Hg for 60 sec.

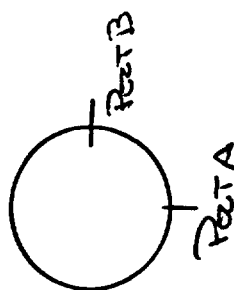
A (Out) 235

472

2

PROBE LENGTH AND TYPE 5ft 5/8
NOZZLE I.D. 5/8" = 0.625 in
ASSUMED MOISTURE, % 29
SAMPLE BOX NUMBER _____
METER BOX NUMBER _____
METER ΔH _____
C FACTOR Cp(Rev) 6.766
PROBE HEATER SETTING 80-90%
HEATER BOX SETTING 200-250
REFERENCE 40 $K=71$

Worms, 110, 120, 130.



SCHEMATIC OF TRAVERSE POINT LAYOUT

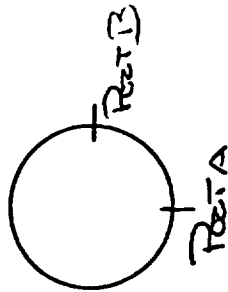
READ AND RECORD ALL DATA EVERY _____ MINUTES

[illegible]

COMMENTS: Pre-Leak Check 6" Hg for 60 sec.
START 766.520
STOP 766.533

PLANT King Bros, Inc
DATE 9/3/87
SAMPLING LOCATION Asphalt Paved
SAMPLE TYPE Particulate
RUN NUMBER Three (3)
OPERATOR WLM/PT
AMBIENT TEMPERATURE 70°F
BAROMETRIC PRESSURE 29.52
STATIC PRESSURE, (P_s) -
FILTER NUMBER (g) 173

PROBE LENGTH AND TYPE 5 ft 5/8
NOZZLE I.D. 3/8" = 0.375 in.
ASSUMED MOISTURE, % 29
SAMPLE BOX NUMBER _____
METER BOX NUMBER _____
METER ΔH _____
C FACTOR CP (REV) 0.760
PROBE HEATER SETTING 90-90%
HEATER BOX SETTING 200-250
REFERENCE AD. K = 71



SCHEMATIC OF TRAVERSE POINT LAYOUT

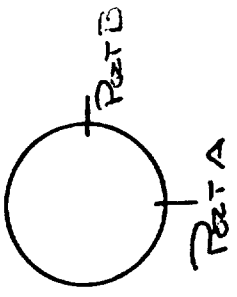
READ AND RECORD ALL DATA EVERY _____ MINUTES

TRAVERSE POINT NUMBER	CLOCK TIME		GAS METER READING (V_m), ft ³	VELOCITY HEAD (Δp_f), in. H ₂ O	ORIFICE PRESSURE DIFFERENTIAL (ΔH), in. H ₂ O		STACK TEMPERATURE (T_s), °F	DRY GAS METER TEMPERATURE		PUMP VACUUM, in. Hg	SAMPLE BOX TEMPERATURE, °F	IMPIGNER TEMPERATURE, °F
	SAMPLING TIME, min	(24-hr CLOCK)			DESIRED	ACTUAL		INLET ($T_{m\ in}$), °F	OUTLET ($T_{m\ out}$), °F			
PORT B												
B-1	0	1745	795.172	0.001	0.72	0.72	162.1	93	94	4.0	0.1000	60
2	3.5	1748.5	797.0	0.002	1.41	1.41	161.2	98	95	5.0	0.1414	60
3	7.0	1752	799.2	0.0025	1.75	1.75	164.0	105	95	6.0	0.1581	60
4	10.5	1755.5	801.8	0.0025	1.75	1.75	165.2	112	96	6.0	0.1581	60
5	14.0	1759	804.3	0.0025	1.75	1.75	166.3	117	96	6.0	0.1581	58
6	17.5	1762.5	806.9	0.0025	1.75	1.75	164.2	118	96	6.5	0.1581	56
7	21.0	1766	—	0.002	1.41	1.41	166.3	120	97	6.0	0.1414	56
8	24.5	1769.5	811.8	0.005	1.05	1.05	166.5	120	98	6.0	0.1225	58
9	28.0	1773	—	0.002	1.41	1.41	167.7	120	99	6.0	0.1414	58
10	31.5	1776.5	816.1	0.002	1.41	1.41	168.3	123	100	6.0	0.1414	60
11	35.0	1780	818.6	0.0025	1.79	1.79	167.9	124	100	6.5	0.1581	60
12	38.5	1783.5	821.1	0.0025	1.79	1.79	168.2	126	100	6.5	0.1581	61
	42.0	1787	823.699									
			$V_m = 28.527$			1.50	165.6	114.7	97.2		0.1447	58.9
							168.3	119.4	100.1			
			$V_m = 57.1666$			1.48	167.0	119.6	101.0		0.1436	59.8
								110.3				

COMMENTS: ROSE LEAK CHECK @ 7:11

COMMENTS: Post Leak Check -
 100% - 072.719
 @ 7" Hg for 60 sec.

1 N



FIELD DATA

PLANT KING BROS. INC.
 DATE 9/4/67
 SAMPLING LOCATION Asphalt Plant, Mountainville WV
 SAMPLE TYPE Particulate
 RUN NUMBER Four (4)
 OPERATOR W.R.T.
 AMBIENT TEMPERATURE 65.0 F
 BAROMETRIC PRESSURE 29.58
 STATIC PRESSURE, (P_s) -
 FILTER NUMBER (s) 174

PROBE LENGTH AND TYPE 5 ft 5/8
 NOZZLE I.D. 5/8" = 0.625 inches
 ASSUMED MOISTURE, % 30
 SAMPLE BOX NUMBER -
 METER BOX NUMBER -
 METER ΔH_g -
 C FACTOR Cp 0.760
 PROBE HEATER SETTING 855%
 HEATER BOX SETTING 250
 REFERENCE K-65

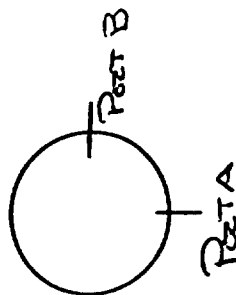
SCHMATIC OF TRAVERSE POINT LAYOUT
 READ AND RECORD ALL DATA EVERY _____ MINUTES

TRAVERSE POINT NUMBER	CLOCK TIME (24-hr CLOCK)	GAS METER READING (V _m), ft ³	VELOCITY HEAD (ΔP _v), in. H ₂ O	ORIFICE PRESSURE DIFFERENTIAL (ΔH), in. H ₂ O		STACK TEMPERATURE (T _s), °F	DRY GAS METER TEMPERATURE		PUMP VACUUM, in. Hg	SAMPLE BOX TEMPERATURE, °F	IMPIGNER TEMPERATURE, °F
				DESIRED	ACTUAL		INLET (T _{m in}), °F	OUTLET (T _{m out}), °F			
<u>Part B</u>											
B-1	0 0845.5	823.754	0.015	0.98	0.98	119.2	54	52	3.0	0.1225	55
2	3.5 0849	825.8	0.03	1.95	1.95	157.8	64	54	5.0	0.1732	52
3	7.0 0852.5	828.4	0.02	1.30	1.30	159.5	69	54	4.0	0.1414	49
4	10.5 0856	830.6	0.015	0.98	0.98	161.1	74	56	3.5	0.1225	50
5	14.0 0859.5	832.5	0.015	0.98	0.98	160.9	77	56	3.5	0.1225	50
6	17.5 0903	834.5	0.015	0.98	0.98	160.3	81	58	3.5	0.1225	50
7	21.0 0906.5	836.4	0.015	0.98	0.98	161.2	84	66	3.5	0.1225	52
8	24.5 0910	838.3	0.015	0.98	0.98	162.7	89	64	3.5	0.1225	52
9	28.0 0913.5	846.3	0.015	0.98	0.98	162.6	90	64	3.5	0.1225	53
10	31.5 0917	842.1	0.02	1.30	1.30	161.4	93	66	4.0	0.1414	54
11	35.0 0920.5	844.3	0.02	1.30	1.30	162.5	95	68	4.0	0.1414	54
12	38.5 0924	846.5	0.02	1.30	1.30	165.0	97	68	4.0	0.1414	56
STOP	42.0 0927.5	848.763									
		<u>V_m = 25.009 ft³</u>		<u>1.17</u>	<u>1.17</u>	<u>161.4</u>	<u>80.9</u>	<u>160.0</u>		<u>0.1330</u>	<u>52.2</u>
						<u>90.2</u>	<u>85.2</u>	<u>162.9</u>			

COMMENTS: Prelevel checked @ 7" Hg for 60 sec.
START 823.745
STOP 823.754

PLANT KING CROSS. INC.
DATE 9/4/87
SAMPLING LOCATION ASBESTOS PLANT
SAMPLE TYPE PARTICULATE
RUN NUMBER 5387 (4)
OPERATOR VDB:JR
AMBIENT TEMPERATURE 65°F
BAROMETRIC PRESSURE 29.58
STATIC PRESSURE, (P_s) -
FILTER NUMBER (s) 174

PROBE LENGTH AND TYPE 5 FT 2/3
NOZZLE I.D. 5/8" = 0.625 inches
ASSUMED MOISTURE, % 36
SAMPLE BOX NUMBER _____
METER BOX NUMBER _____
METER ΔH _____
C FACTOR CP (REV) 0.760
PROBE HEATER SETTING 85%
HEATER BOX SETTING 250
REFERENCE # V-65



SCHEMATIC OF TRAVERSE POINT LAYOUT

READ AND RECORD ALL DATA EVERY _____ MINUTES

[illegible]

COMMENTS: Post Leak Crew - 6' H²O for 60 sec

EPA (3-π) 235

Process Monitoring
Kling Brothers, Inc

9/23/81
24

	Motor Speed %		AGGREGATE GATE TPH	AC-20 TPH	AGGREGATE GATE TOTALIZER TONS	Fuel Feed Rate %	Exhaust Set-Point OF	Exhaust Temp. OF
	Feed Bid 1	Feed Bid 2/3						
30	49%	NA	49%	4.4	8.5	34	225	228
35	49%	N/A	49%	4.5	13	32	226	223
40	49%	N/A	49%	4.5	24.5	30	226	229
45	49%	N/A	49%	4.5	32.4	30	226	229
50	49%	N/A	49%	4.5	36.4	29	226	228
55	49%	N/A	49%	4.5	43	31	226	224
60	49%	N/A	49%	4.6	47.7	31	226	223
65	49%	N/A	49%	4.6	55.9	31	226	223
70	49%	N/A	49%	4.5	62.5	31	226	227
75	49%	N/A	49%	4.5				
80	49%	N/A	49%	4.5				
85	49%	N/A	49%	4.5				
90	49%	N/A	49%	4.5				
95	49%	N/A	49%	4.5				
100	49%	N/A	49%	4.5				
avg	49%	N/A	49%	4.5		31	226	226

gph

Process Monitor

Kling Brothers, Inc

11/18/1

2B

Time	Motor Speed %		AGGREGATE TPH	AC-20 TPH	AGGREGATE TOTALIZER TONS	Fuel Feed Rate %	Exhaust Set-Point °F	Exhaust Temp. °F	
	Feed Bid 1	Feed Bid 2 3							
15	50%	N/A	84	4.4	6.5	30	226	230	
20	50%	N/A	84	4.4	15.3	26	226	230	
25	50%	N/A	84	4.4	25.	32	226	221	
30	50%	N/A	84	4.4	31	33	226	223	
35	50%	N/A	84	4.4	37	32	226	227	
40	50%	N/A	84	4.4	45	29	226	235	
45	50%	N/A	84	4.4	50	26	226	230	
50	54	N/A	79	5.0	61.5	27	226	228	
50	54	N/A	79	5.1	66	26	226	230	
55	54	N/A	79	5.1	69	26	226	230	
avg	51.2	42	82.5	4.6		28.7	226	228	

h₁

worming

Process Monitor
Kling Brothers, Inc.

9/12/81
3A

3 Not Used Weaving

e	MOTOR SPEED % Feed Bid. Feed Bid 1 2	AGGREGATE GATE TPH	AC-20 TPH	AGGREGATE GATE TOTALIZER TONS	FUEL FEED RATE %	EXHAUST SET-POINT OF	EXHAUST TEMP. OF	
05	54	42	78.5	5.1	8.3	31	226	221
10	54	42	79	5.1	12	30	226	230
15	54	42	78	5.1	18	31	226	232
20	54	42	80	5.1	27	28	226	229
25	54	42	78	5.1	33.9	28	226	229
30	54	42	79	5.1	39	28	226	228
35	54	42	79	5.2	46	28	226	229
40	54	42	79	5.2	53	27	226	230
45	54	42	79	5.1	62	28	226	226
50	54	42	79	5.1	65.5	26	226	225
55	54	42	78.8	5.1		28.5	226	228

Process Monitoring

Klog Brothers, Inc

3B

#3 Not Used

- Wearing

	Motor Speed Feed Bid 1	Feed Bid 2	AGGREGATE GATE TPH	AC-20 TPH	AGGREGATE GATE TOTALIZER TONS	Fuel Feed Rate %	Exhaust Set-Point °F	Exhaust Temp. °F
45	54	22	78	5.1	78.2 9.7	29	226	222
0	54	22	78	5.1	9.7	28	226	223
5	54	22	78	5.1	17.1	33	226	222
0	54	22	78	5.1	24	33	226	224
5	54	22	78	5.1	33	33	224	223
0	54	22	79	5.1	42	33	224	223
5	54	22	79	5.1	47	33	224	222
0	54	22	79	5.1	52.4	34	224	222
25	54	22	79	5.1	58.3	34	224	222
30	54	22	79	5.1	64	33	224	222
35	54	22	79	5.1	68	33	224	223

Process Monitoring
Klog Brothers, Inc

7-9/14/1
ON AB

	Motor Speed Feed Bid. %		AC-20 TPH	AGGR- GATE TOTALIZER TONS	Fuel Feed Rate %	Exhaust Set-Point OF	Exhaust Temp. OF
	1	2					
00	46	48	84	6.3	32	228	234
05	48	48	84	17.3	30	228	231
10	48	48	84	25.5	30	228	231
15	46	46	84	32	30	228	236
20	46	46	85	38	30	228	236
25	48	48	85	45.1	30	228	235
30	48	48	85	52	30	228	240
35	46	46	85	60	29	226	242
40	48	48	85	67	28	226	238
45	46	46	85	68.7	28	226	238
	48	48	84.6		29.7	227.4	236.7

