

**AP42 Section: 11.1**

**Reference Number: 280**

**Title: Source Sampling For Particulate Emissions, R. E.  
Hazard Contracting Co., San Diego, CA,**

**San Diego County Air Pollution Control District,  
San Diego, CA,**

**September 5, 1991.**



AP-42 Section 11.1  
Reference  
Report Sect. 4  
Reference 278  
219

Air Pollution Cor  
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Air Pollution Control Officer  
R. J. Sommerville

October 1, 1992

Attn: Plant Supervisor  
R.E. Hazard Construction  
P.O. Box 229000  
San Diego, CA 92129

**SUBJECT: RENEWAL TEST REPORTS**

The enclosed test reports are the result of testing done at your facilities.

If you have any questions, please call me at (619) 694-3359.

Robert Yelenosky  
Senior Air Pollution Chemist

CWR:jo

Enclosures

R.E. HAZARD on 8/26/92  
SAN DIEGO AIR POLLUTION CONTROL DISTRICT, 9150 CHESAPEAKE DRIVE, SAN DIEGO, CA. 92123  
SOURCE TEST OF PARTICULATE EMISSIONS TO THE ATMOSPHERE

P.O.#442 TEST #92239

TEST SITE: R.E. Hazard  
10050 Black Mountain Road  
San Diego, CA 92126

TEST #: 92239

P.O.#: 442

TEST DATE: 8/26/92

Type of plant (Asphalt/Perlite/Combustion): ASPHALT

UNIT TESTED: Baghouse  
EQUIPMENT: Asphalt Batch Plant

|                                                |               |
|------------------------------------------------|---------------|
| TESTED BY: David N. Shina & Guy Alphin III     | DATE: 8/26/92 |
| SITE PERSONNEL: Al Tilley                      | DATE: 8/26/92 |
| APCD ENGINEER: Austen D'Lima & John McCafferty | DATE: 8/26/92 |
| LAB ANALYSIS BY: David N. Shina                | DATE: 9/3/92  |
| REPORT BY: David N. Shina                      | DATE: 9/3/92  |
| REVIEWED BY: <i>[Signature]</i>                | DATE: 9/30/92 |
| APPROVED BY: <i>[Signature]</i>                | DATE: 9/30/92 |

ROBERT YELENOSKY, SENIOR AIR POLLUTION CHEMIST

This report has been reviewed and found to be representative of the testing that was performed.

### SDAPCD RULES

| TEST                 | LIMIT     | MEASURED     | EXCEEDANCE/NON-EXCEEDANCE |
|----------------------|-----------|--------------|---------------------------|
| RULE 54 DUST & FUMES | 40 lbs/hr | 6.935 lbs/hr | NON-EXCEEDANCE            |

### TEST RESULTS SUMMARY:

| ITEM  | I   | Cs      | E      |
|-------|-----|---------|--------|
| UNITS | %   | gr/dscf | lbs/hr |
| VALUE | 104 | 0.0251  | 6.94   |

### ENGINEERING SUMMARY

| Qstd  | Fuel    | RATE | Asphalt Production |
|-------|---------|------|--------------------|
| dscfm | —       |      | tons/hr            |
| 32194 | NAT GAS |      | 229                |

### TEST PARAMETERS:

#### SYSTEM DESCRIPTION:

This asphalt plant combines crushed rock and sand with asphalt oil in batch loads of varying sizes. The rock and sand are heated in a rotary drum to dry them. The exhaust from this dryer is routed through a baghouse and finally to a stack. It is the emissions from this stack that are the subject of this report.

#### PROCEDURES:

The procedures utilized in these tests are based on EPA's 40 CFR, July 1, 1991, Part 60, Appendix A, Methods 1-5 inclusive. The sampling train was modified to utilize a back-end filter (fig. 1), as outlined in the SDAPCD QA manual.

#### CALCULATIONS

All equations are from the EPA's 40 CFR, July 1, 1991, Part 60, Appendix A, Methods 1-5 inclusive. All preliminary assumptions and calculations are based on data obtained from previous tests.

#### PARTICULATE SAMPLING:

The test consisted of sampling at 24 traverse points, 12 from each of 2 sample ports (fig.2), collected from 77 inches below the stack (fig.3). All field data was transferred to the computer printout. All calculations were done by the computer and the emissions were compared to rule 24 of the SDAPCD.

#### ANALYSES:

**Gas:** An integrated bag sample was collected during the test and analyzed at the APCD lab.

**Particulate:** All procedures follow EPA guidelines, except where noted in the SDAPCD QA manual.

#### EQUIPMENT:

All testing and analysis equipment was calibrated according to EPA guidelines (40 CFR, July 1, 1991, Part 60, Appendix A, Methods 1-5).

##### Analysis:

CO2-Anarad AR400  
O2-Teledyne Ryan 320 P4  
Macrobalance-Sargent Welch  
Microbalance-Sartorius

##### Collection:

Filter-Gelman  
Holder-Gelman  
Beakers-Pyrex  
Impingers-Ace

##### Sampling:

L/S Box-Napp  
Umbilical cord-Napp  
Cold/Hot box-Napp  
Pitot tube-Napp

##### Temp./Press.:

Thermocouples-Omega  
Temp. read out-Omega  
Aneroid Barometer-Taylor  
Press. devices-Dwyer magnehelic

**FIELD DATA:**

| Trav. Pt | Vm (ft <sup>3</sup> )<br>807.220 | ΔP<br>(in H <sub>2</sub> O) | ΔH<br>(in H <sub>2</sub> O) | Stack Temp<br>(°F) | Box Temp<br>(°F) | Imp Temp<br>(°F) | t 1 (in)<br>(°F) | t 2 (out)<br>(°F) | velocity<br>(ft/sec) |
|----------|----------------------------------|-----------------------------|-----------------------------|--------------------|------------------|------------------|------------------|-------------------|----------------------|
| 1        |                                  | 1.44                        | 1.70                        | 212                |                  | 63               | 81.00            | 101.00            | 079.95               |
| 2        |                                  | 1.70                        | 2.00                        | 212                |                  | 58               | 80.00            | 102.00            | 086.87               |
| 3        |                                  | 1.62                        | 1.90                        | 200                |                  | 58               | 79.00            | 103.00            | 084.04               |
| 4        |                                  | 1.51                        | 1.70                        | 210                |                  | 61               | 81.00            | 108.00            | 081.75               |
| 5        |                                  | 1.13                        | 1.30                        | 213                |                  | 61               | 81.00            | 110.00            | 070.88               |
| 6        |                                  | 0.85                        | 1.00                        | 212                |                  | 61               | 81.00            | 111.00            | 061.43               |
| 7        |                                  | 0.66                        | 0.75                        | 212                |                  | 61               | 82.00            | 112.00            | 054.94               |
| 8        |                                  | 0.68                        | 0.80                        | 208                |                  | 62               | 84.00            | 113.00            | 054.70               |
| 9        |                                  | 0.62                        | 0.70                        | 210                |                  | 61               | 84.00            | 113.00            | 052.36               |
| 10       |                                  | 0.63                        | 0.73                        | 211                |                  | 63               | 85.00            | 114.00            | 052.84               |
| 11       |                                  | 0.70                        | 0.80                        | 213                |                  | 63               | 85.00            | 115.00            | 055.78               |
| 12       |                                  | 0.63                        | 0.73                        | 212                |                  | 65               | 85.00            | 115.00            | 052.88               |
| 1        |                                  | 1.00                        | 1.15                        | 216                |                  | 64               | 86.00            | 109.00            | 066.82               |
| 2        |                                  | 1.05                        | 1.20                        | 215                |                  | 64               | 87.00            | 108.00            | 068.42               |
| 3        |                                  | 1.11                        | 1.30                        | 215                |                  | 65               | 87.00            | 111.00            | 070.35               |
| 4        |                                  | 1.13                        | 1.30                        | 215                |                  | 65               | 87.00            | 113.00            | 070.98               |
| 5        |                                  | 1.13                        | 1.30                        | 215                |                  | 65               | 87.00            | 113.50            | 070.98               |
| 6        |                                  | 1.22                        | 1.40                        | 216                |                  | 64               | 87.50            | 116.00            | 073.81               |
| 7        |                                  | 1.31                        | 1.50                        | 217                |                  | 62               | 87.00            | 116.00            | 076.54               |
| 8        |                                  | 1.42                        | 1.65                        | 222                |                  | 66               | 87.50            | 118.00            | 079.98               |
| 9        |                                  | 1.48                        | 1.70                        | 218                |                  | 60               | 87.50            | 118.50            | 081.30               |
| 10       |                                  | 1.63                        | 1.90                        | 218                |                  | 61               | 88.00            | 119.00            | 085.44               |
| 11       |                                  | 1.82                        | 2.10                        | 219                |                  | 61               | 88.00            | 119.50            | 090.35               |
| 12       | 846.808                          | 1.88                        | 2.20                        | 221                |                  | 61               | 88.50            | 120.00            | 091.96               |

|          | Vm<br>ft <sup>3</sup> | ΔP<br>(in H <sub>2</sub> O) | ΔH<br>(in H <sub>2</sub> O) | ts<br>(°F) | tbox<br>(°F) | ti<br>(°F) | t 1 (in)<br>(°F) | t 2 (out)<br>(°F) | vs<br>(ft/sec) |
|----------|-----------------------|-----------------------------|-----------------------------|------------|--------------|------------|------------------|-------------------|----------------|
| Average: | 39.388                | 1.15                        | 1.37                        | 214        | N/A          | 62         | 84.92            | 112.52            | 71.47          |

**DATA SUMMARY:**

| LABORATORY DATA:                                                                                                                                    | SAMPLING PARAMETERS:                                                                                                                      | SAMPLING DATA:                                                                                                                                                       |
|-----------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <b>IMPINGER CATCH:</b><br>Silica gel ? = <u>YES</u><br>Vlc = <u>238.69</u> ml                                                                       | <b>METER BOX:</b><br>Box ID = <u>C138</u><br>ΔH@ = <u>1.8883</u><br>Y = <u>0.9924</u>                                                     | <b>VOLUME &amp; TIME:</b><br>Ø (total time) = <u>60.0</u> min<br>Final leak rate = <u>0.001</u> cfm<br>Pass/Fail = <u>PASS</u><br>Vm = <u>39.388</u> ft <sup>3</sup> |
| <b>GAS ANALYSIS:</b><br>CO <sub>2</sub> = <u>2.50</u> %<br>O <sub>2</sub> = <u>14.90</u> %<br>CO = <u>0.00</u> %<br>N <sub>2</sub> = <u>82.60</u> % | <b>STACK DIMENSIONS:</b><br>Circular ? = <u>YES</u><br>Ds = <u>4.00</u> ft<br>Length = <u>N/A</u> ft<br>As = <u>12.56</u> ft <sup>2</sup> | <b>PRESSURES:</b><br>Pbar = <u>29.73</u> in Hg<br>Pg = <u>0.80</u> in H <sub>2</sub> O<br>Vpw @ ts = <u>29.92</u> in Hg<br>Vpw @ ti = <u>N/A</u> in Hg               |
| <b>PARTICULATE ANALYSIS:</b><br>mn(front) = <u>0.023708</u> g<br>mn(back) = <u>0.036292</u> g<br>mn(total) = <u>0.06000</u> g                       | <b>NOZZLE &amp; PROBE</b><br>Dn = <u>0.205</u> in<br>An = <u>0.0330</u> in <sup>2</sup><br>Cp = <u>0.8435</u>                             | <b>TEMPERATURES:</b><br>t1 = <u>84.92</u> °F    ti = <u>62</u> °F<br>t2 = <u>112.52</u> °F    tbox = <u>N/A</u> °F<br>tm = <u>98.72</u> °F    ts = <u>214</u> °F     |

**CALCULATIONS:****TEMPERATURES:**

|     |                                                                       |        |
|-----|-----------------------------------------------------------------------|--------|
| 01) | $T_s = (2 \cdot t_{sh}) / \text{total } n's$                          | 214 °F |
| 02) | $T_s = t_s + 460$                                                     | 674 °R |
| 03) | $t_m = (2 \cdot [(t_1(t_1+246))/2] / \text{total } n's = (t_1+t_2)/2$ | 99 °F  |
| 04) | $T_m = (t_1+t_2)/2 + 460$                                             | 559 °R |
| 05) | $T_d = (2 \cdot t_{hd}) / \text{total } n's$                          | 62 °F  |
| 06) | $T_{std}$                                                             | 528 °R |

**PRESSURES:**

|     |                                                                           |                            |
|-----|---------------------------------------------------------------------------|----------------------------|
| 07) | $P_{bar} = [P @ 5.1'] - \text{if above 5.1' } [-0.1 \text{ in Hg}/100ft]$ | 29.73 in Hg                |
| 08) | $P_g = \text{read from pressure sensing device}$                          | 0.80 in H <sub>2</sub> O   |
| 09) | $P_s = P_{bar} + (P_g/13.6)$                                              | 29.79 in Hg                |
| 10) | $\Delta H$                                                                | 1.37 in H <sub>2</sub> O   |
| 11) | $P_{ms} = P_{bar} + (\Delta H/13.6)$                                      | 29.83 in Hg                |
| 12) | $P_{std}$                                                                 | 29.92 in Hg                |
| 13) | $\Delta P$                                                                | 1.1475 in H <sub>2</sub> O |

**VOLUME:**

|     |                                                                                              |                                       |
|-----|----------------------------------------------------------------------------------------------|---------------------------------------|
| 14) | $V_m = V_{m(end)} - V_{m(begin)}$                                                            | 39.388 ft <sup>3</sup>                |
| 15) | $Y$                                                                                          | 0.8824                                |
| 16) | $V_m = V_m \cdot Y$                                                                          | 39.069 ft <sup>3</sup>                |
| 17) | $V_m \text{ std} = [(V_m \cdot (T_{std}/T_m) \cdot (P_m/P_{std}))]$                          | 36.829 ft <sup>3</sup>                |
| 18) | $V_{low} = \text{Volume of impurities}$                                                      | 236.89 ml                             |
| 19) | $\rho$                                                                                       | 0.002201 lb/ml                        |
| 20) | $R$                                                                                          | 21.85 in Hg-ft <sup>3</sup> /°R-lb-mo |
| 21) | $M_{wH_2O}$                                                                                  | 18.00 g/g-mo                          |
| 22) | $V_w \text{ std} = [(V_{low} \cdot \rho \cdot R \cdot T_{std}) / (P_{std} \cdot M_{wH_2O})]$ | 1.2351 ft <sup>3</sup>                |

**MOISTURE:**

|     |                                                                              |             |
|-----|------------------------------------------------------------------------------|-------------|
| 23) | $Bws(1) = (V_w \text{ std}) / (V_w \text{ std} + V_m \text{ std}) \cdot 100$ | 23.38 %     |
| 24) | $V_{pw} @ T_s = \text{from appendix}$                                        | 29.92 in Hg |
| 25) | $Bws(2) = [(V_{pw} @ T_s) / P_s] \cdot 100$                                  | 100.44 %    |
| 26) | $Bws = \text{lower value of equation 24 or 26}$                              | 23.38 %     |

**MOLECULAR WEIGHT:**

|     |                                                                        |                |
|-----|------------------------------------------------------------------------|----------------|
| 27) | %O <sub>2</sub>                                                        | 14.90 %        |
| 28) | %CO <sub>2</sub>                                                       | 2.50 %         |
| 29) | %N <sub>2</sub> +Inerts+%CO                                            | 82.60 %        |
| 30) | $M_d = 0.440[\%CO_2] + 0.320[\%O_2] + 0.280[\%N_2+\text{Inerts}+\%CO]$ | 29.00 g/g-mole |
| 31) | $M_s = M_d \cdot (1-Bws) + 18.0 \cdot (Bws)$                           | 26.43 g/g-mole |

**VELOCITY:**

|     |                                                                             |                        |
|-----|-----------------------------------------------------------------------------|------------------------|
| 32) | $C_p$                                                                       | 0.844                  |
| 33) | $D_s =$                                                                     | 4.000 ft               |
| 34) | $v_m = 85.49 \cdot C_p \cdot [(T_s \cdot \Delta P) / (P_s \cdot M_d)]^{.5}$ | 71.475 ft/sec          |
| 35) | $A_s = 3.14 \cdot [(D_s)^2 / 4]$                                            | 12.560 ft <sup>2</sup> |
| 36) | $Q_s = (v_m) \cdot A_s \cdot 60$                                            | 53863 acfm             |
| 37) | $Q_{std} = 17.64 \cdot Q_s \cdot (1-Bws) \cdot P_s / T_s$                   | 32194 dscfm            |

**EMISSIONS:****FRONT HALF**

|     |                                                                                                                     |                           |
|-----|---------------------------------------------------------------------------------------------------------------------|---------------------------|
| 38) | $m_n \text{ (front)}$                                                                                               | 0.02371 g                 |
| 39) | $C_s \text{ (front)} = 15.43 \cdot m_n \text{ (front)} / V_m \text{ std}$                                           | 0.00993 grains/dscf       |
| 40) | $7000 \text{ grains} = 1 \text{ lb. } 60 \text{ min} = 1 \text{ hr. } 60 \text{ min/hr} / 7000 \text{ grains/lb} =$ | 0.00857 lbs-min/grains-hr |
| 41) | $E \text{ (front)} = (0.00857) \cdot (Q_{std}) \cdot C_s \text{ (front)}$                                           | 2.74 lbs/hr               |

**BACK HALF**

|     |                                                                                                                     |                           |
|-----|---------------------------------------------------------------------------------------------------------------------|---------------------------|
| 42) | $m_n \text{ (back)}$                                                                                                | 0.03629 g                 |
| 43) | $C_s \text{ (back)} = 15.43 \cdot m_n \text{ (back)} / V_m \text{ std}$                                             | 0.01520 grains/dscf       |
| 44) | $7000 \text{ grains} = 1 \text{ lb. } 60 \text{ min} = 1 \text{ hr. } 60 \text{ min/hr} / 7000 \text{ grains/lb} =$ | 0.00857 lbs-min/grains-hr |
| 45) | $E \text{ (back)} = (0.00857) \cdot (Q_{std}) \cdot C_s \text{ (back)}$                                             | 4.20 lbs/hr               |

**TOTAL**

|     |                                                                                                                     |                           |
|-----|---------------------------------------------------------------------------------------------------------------------|---------------------------|
| 46) | $m_n \text{ (total)} = m_n \text{ (front)} + m_n \text{ (back)}$                                                    | 0.06000 g                 |
| 47) | $C_s \text{ (total)} = 15.43 \cdot m_n \text{ (total)} / V_m \text{ std}$                                           | 0.02514 grains/dscf       |
| 48) | $7000 \text{ grains} = 1 \text{ lb. } 60 \text{ min} = 1 \text{ hr. } 60 \text{ min/hr} / 7000 \text{ grains/lb} =$ | 0.00857 lbs-min/grains-hr |
| 49) | $E \text{ (total)} = (0.00857) \cdot (Q_{std}) \cdot C_s \text{ (total)}$                                           | 6.94 lbs/hr               |

**ISOKINETICS:**

|     |                                                                                                            |                        |
|-----|------------------------------------------------------------------------------------------------------------|------------------------|
| 50) | $D_n =$                                                                                                    | 0.205 in               |
| 51) | $A_n = 3.14 \cdot [(D_n)^2 / 4]$                                                                           | 0.0330 in <sup>2</sup> |
| 52) | $\phi$                                                                                                     | 60 min                 |
| 53) | $I = 0.9450 \cdot (T_s \cdot V_m \text{ std}) / (P_s \cdot v_s \cdot A_n \cdot (1-Bws)) \cdot 104.50 \% =$ | 104 %                  |

R.E. Hazard on 8/26/92

P.O. #:442 TEST#: 92239

SAN DIEGO AIR POLLUTION CONTROL DISTRICT, 9150 CHESAPEAKE DRIVE, SAN DIEGO, CA 92123

## PARTICULATE TEST LABORATORY ANALYSIS DATA SHEET

TEST SITE: RE HAZARD

10050 Black Mountain Road  
San Diego, CA 92126

TEST #: 92239

P.O.#: 442

TEST DATE: 8/26/92

LAB ANALYSIS BY: David N. Shina

DATE: 9/3/92

LAB REPORT BY: David N. Shina

DATE: 9/3/92

REVIEWED BY:

DATE:

## (1) IMPINGER VOLUMES

|    | FINAL WGT. | INIT WGT. | NET WGT. |                                                     |
|----|------------|-----------|----------|-----------------------------------------------------|
| #1 | 744.15 g   | 574.05 g  | 170.10 g | Total impinger charge= 200.00 ml                    |
| #2 | 618.70 g   | 573.88 g  | 44.82 g  | Partiulates from impinger charge                    |
| #3 | 496.56 g   | 485.97 g  | 10.59 g  | (Total impinger charge * H(water blank) = 0.00013 g |
| #4 | 644.90 g   | 631.72 g  | 13.18 g  | Total weight collected= 238.69 g                    |
| #5 | g          | g         | N/A g    | Total volume collected, Vlc= 238.69 ml              |
| #6 | g          | g         | N/A g    |                                                     |

## (2) BLANKS

| A     | B       | C     | D            | E             | F                   | G            | H             | I            | J               | K            | L             |
|-------|---------|-------|--------------|---------------|---------------------|--------------|---------------|--------------|-----------------|--------------|---------------|
| AREA  | SOLVENT | ID    | END WGT<br>g | INIT WGT<br>g | NET WGT.<br>(E-F) g | RINSES<br>ml | g/ml<br>(G/D) | %<br>(H*100) | ppm<br>(J*10^6) | PASS<br>FAIL | LIMITS        |
| BLANK | ACETONE | 92025 | 49.4864      | 49.4837       | 0.00270             | 325.00       | 0.0000083     | 0.0008308    | 8.3             | P            | 0.0010%=10ppm |
| BLANK | WATER   | 92001 | 30.8198      | 30.8196       | 0.00020             | 300.00       | 0.0000007     | 0.0000667    | 0.7             | P            | 0.0004%=4ppm  |
| BLANK | ORGANIC | N/A   |              |               |                     |              |               |              |                 |              |               |

## (3) WEIGHTS &amp; RINSES

| a                      | b        | c     | d            | e              | f                   | g            | h                    | i                     | j                              | k                          |
|------------------------|----------|-------|--------------|----------------|---------------------|--------------|----------------------|-----------------------|--------------------------------|----------------------------|
| AREA                   | SOLVENT  | ID    | END WGT<br>g | INIT. WGT<br>g | NET WGT.<br>(e-f) g | RINSES<br>ml | SOLV. WGT<br>(g*H) g | WGT (corr)<br>(f-h) g | Subtotal (mn (AREA))<br>(Σi) g | Total (mn (tot))<br>(Σj) g |
| F<br>R<br>O<br>N<br>T  | ACETONE  | 92086 | 29.3092      | 29.2998        | 0.0094              | 300.00       | 0.002492             | 0.00691               |                                |                            |
|                        | WATER    | 92078 | 28.8605      | 28.8435        | 0.0170              | 300.00       | 0.000200             | 0.01680               |                                |                            |
|                        | ORGANIC  | N/A   |              |                |                     |              |                      |                       |                                |                            |
|                        | FILTER   | N/A   |              |                |                     |              |                      |                       |                                |                            |
| mn(front) = 0.023708 g |          |       |              |                |                     |              |                      |                       |                                |                            |
| B<br>A<br>C<br>K       | ACETONE  | 92084 | 29.2592      | 29.2421        | 0.0171              | 330.00       | 0.002742             | 0.01436               |                                |                            |
|                        | WATER ** | 92003 | 30.2476      | 30.2254        | 0.0222              | 350.00       | 0.000367             | 0.02183               |                                |                            |
|                        | ORGANIC  | N/A   |              |                |                     |              |                      |                       |                                |                            |
|                        | FILTER   | 92099 | 1.6008       | 1.6007         | 0.0001              | -----        | -----                | 0.00010               |                                |                            |
| mn(back) = 0.036292 g  |          |       |              |                |                     |              |                      |                       |                                |                            |
| TOTAL                  |          |       |              |                |                     |              |                      |                       | mn(total) = 0.06000 g          |                            |

\*\* The Back Water-SOLV.WGT is corrected for the initial impinger charge

( [g(back water) \* H(blank water)] + [Partiulates from impinger charge] ).

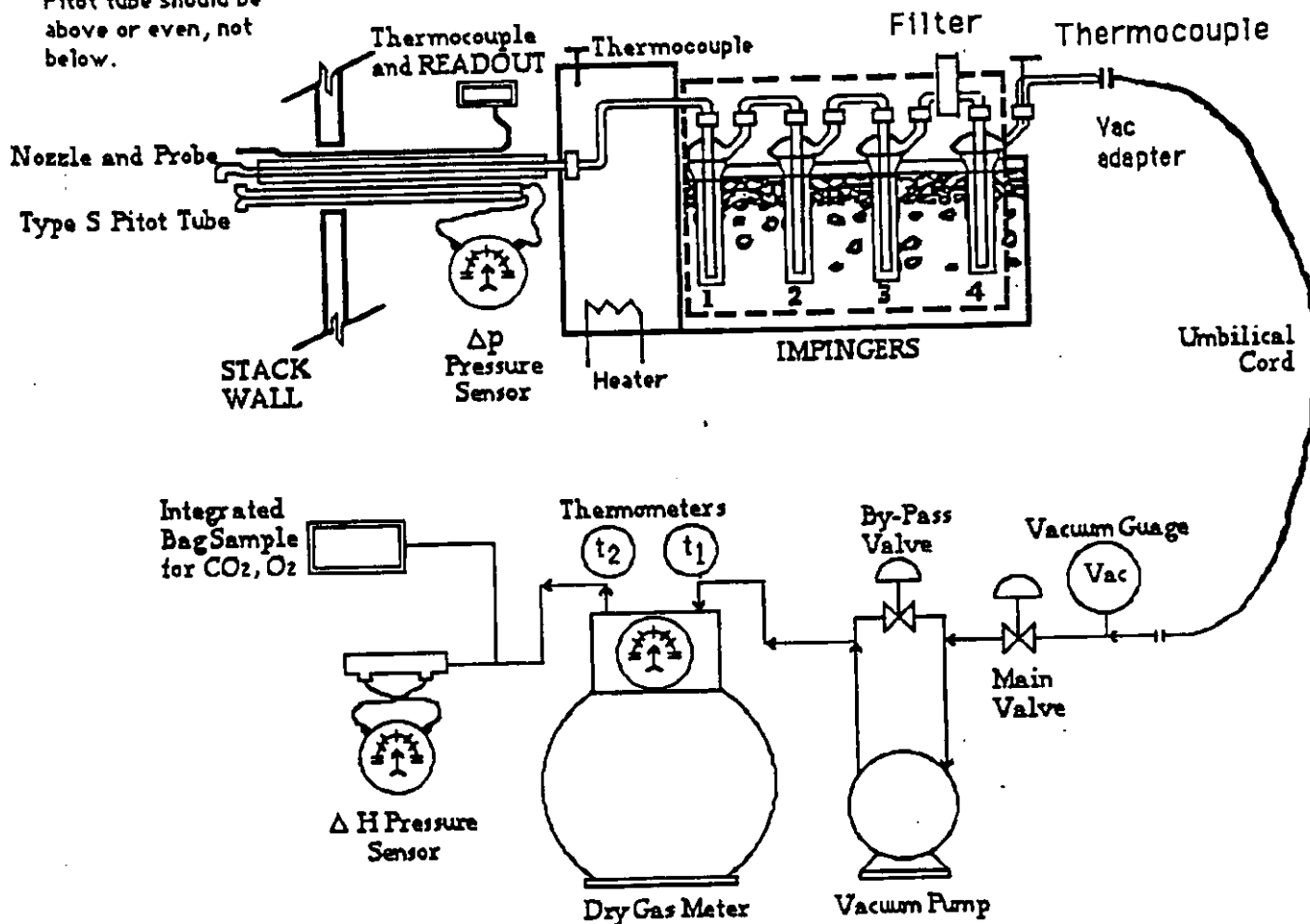
# SAN DIEGO COUNTY AIR POLLUTION CONTROL DISTRICT

FIGURE

## CONDENSER SYSTEM

Note: 2.1.3

Pitot tube should be above or even, not below.



### LEGEND

- No. 1 Mod- 100 ML Deionized Water
- No. 2 Std - 100 ML Deionized Water
- No. 3 Mod- Dry
- No. 4 Mod- Silica gel
- Mod - Modified Type Greenburg-Smith
- Std - Standard Type " "

### FIELD DATA ABBREVIATIONS

- PT = Point Number
- T<sub>s</sub> = Stack Temperature
- Δp = Pitot Tube Pressure Differential, in H<sub>2</sub>O
- V<sub>s</sub> = Stack Velocity, fps
- ΔH = Orifice Meter Pressure Drop, in H<sub>2</sub>O
- t<sub>1</sub> = Meter Inlet Temperature, °F
- t<sub>2</sub> = Meter Outlet Temperature, °F
- P<sub>m</sub> = Pump Vacuum, in Hg
- t<sub>i</sub> = Impinger Temperature
- P<sub>bar</sub> = Barometric Pressure

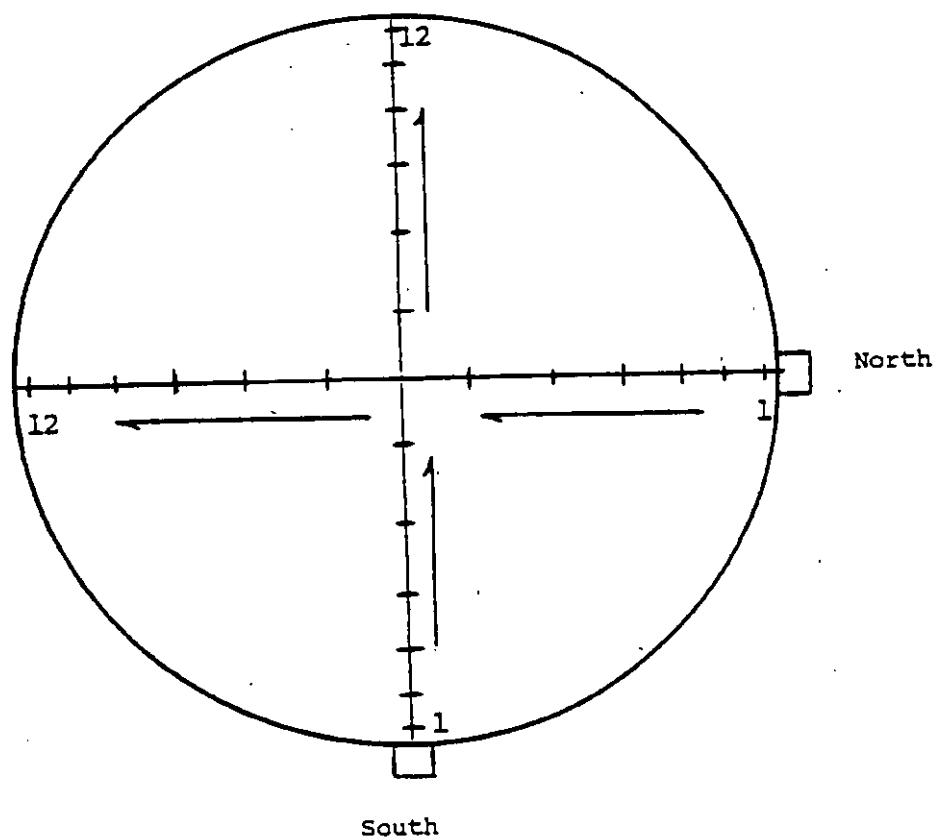
FIGURE : PARTICULATE MATTER SAMPLING TRAIN

TEST NO.

SAN DIEGO COUNTY AIR POLLUTION CONTROL DISTRICT

TRAVERSE POINTS

STACK DIAMETER 48"



| POINT | DISTANCE | POINT | DISTANCE |
|-------|----------|-------|----------|
| 1     | 47.0"    | 7     | 17.1"    |
| 2     | 44.8"    | 8     | 12.0"    |
| 3     | 42.3"    | 9     | 8.5"     |
| 4     | 39.5"    | 10    | 5.7"     |
| 5     | 36.0"    | 11    | 3.2"     |
| 6     | 30.9"    | 12    | 1.0"     |

FIGURE 2



SITE DESCRIPTION  
HAZARD ASPHALT

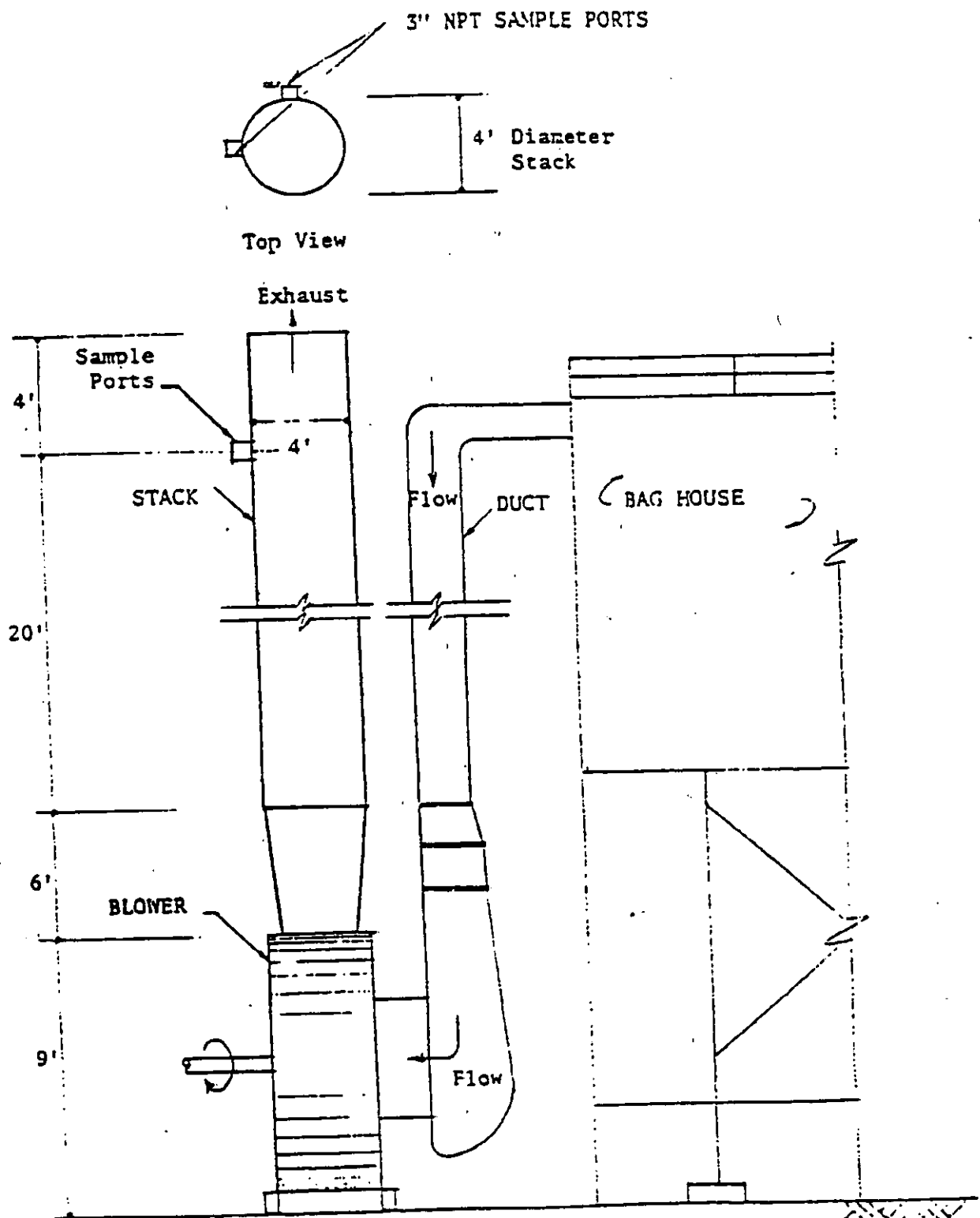


FIGURE 3

SIZE VIEW, No Scale

# NOMENCLATURE

| symbol                   | units           | explanation                                                                  | equation                                                                              |
|--------------------------|-----------------|------------------------------------------------------------------------------|---------------------------------------------------------------------------------------|
| <b>A</b>                 |                 |                                                                              |                                                                                       |
| An                       | in <sup>2</sup> | nozzle area                                                                  | $\pi/4(D_n)^2$                                                                        |
| As                       | ft <sup>2</sup> | stack area                                                                   | $\pi/4(D_s)^2$ or LxW                                                                 |
| <b>B</b>                 |                 |                                                                              |                                                                                       |
| Bws(1)                   | %               | fractional stack gas moisture-equ 1                                          | $((V_w \text{ std})/(V_w \text{ std} + V_m \text{ std}))100$                          |
| Bws(2)                   | %               | fractional stack gas moisture-equ 2                                          | $((V_{pw} @ ts)/P_s)100$                                                              |
| Bws                      | %               | water vapor in the gas stream                                                | lower of Bws(1) and Bws(2)                                                            |
| <b>C</b>                 |                 |                                                                              |                                                                                       |
| CO                       | %               | carbon monoxide                                                              | read from measuring device (0 for Asphalt plants)                                     |
| CO2                      | %               | carbon dioxide                                                               | read from measuring device                                                            |
| Corr Vwm                 | ft <sup>3</sup> | correction for Vw w/o silica gel                                             | $((V_m * (V_{pw} @ ts) / P_s) * P_m * T_{std}) / (T_m * P_{std})$                     |
| Cp                       | none            | pilot tube correction factor                                                 | see EPA method 3                                                                      |
| Cs(front)                | gr/dscf         | concentration of particulate in stack gas, corrected to STP for front        | $(15.43 * mn(\text{front})) / (V_m \text{ std})$                                      |
| Cs(back)                 | gr/dscf         | concentration of particulate in stack gas, corrected to STP for back         | $(15.43 * mn(\text{back})) / (V_m \text{ std})$                                       |
| Cs(total)                | gr/dscf         | concentration of particulate in stack gas, corrected to STP for total        | $(15.43 * mn(\text{total})) / (V_m \text{ std})$                                      |
| Cs12(front, back, total) |                 | same as Cs(front, back, total) except corrected for grain loading at 12% CO2 | $(12 / \%CO_2) * (15.43 * mn(\text{fr, back, total})) / (V_m \text{ std})$            |
| <b>D</b>                 |                 |                                                                              |                                                                                       |
| d (density)              | lb/ml           | density of water at STP                                                      | 0.002201 (see CRC)                                                                    |
| Ds                       | in or ft        | stack diameter                                                               | measure at site                                                                       |
| Dn                       | in              | nozzle diameter                                                              | avg of at least three measurements                                                    |
| <b>E</b>                 |                 |                                                                              |                                                                                       |
| E.A.                     | %               | Excess air (for combustion)                                                  | $((\%CO_2 - 5\%CO) * 100) / ((25.4 * \%N_2 - \%CO_2 - 5 * \%CO))$                     |
| E(front)                 | lbs/hr          | part. emissions rate-front                                                   | $(0.00857)(Q_s d * C_s(\text{front}))$                                                |
| E(back)                  | lbs/hr          | part. emissions rate-back                                                    | $(0.00857)(Q_s d * C_s(\text{back}))$                                                 |
| E(total)                 | lbs/hr          | part. emissions rate-total                                                   | $(0.00857)(Q_s d * C_s(\text{total}))$                                                |
| <b>H</b>                 |                 |                                                                              |                                                                                       |
| ΔH                       | in H2O          | average differential pressure across the orifice meter                       | avg of the readings from the pressure measuring device                                |
| ΔH@                      | none            | orifice pressure differential at STP                                         | see EPA Method 5 Appendix                                                             |
| <b>I</b>                 |                 |                                                                              |                                                                                       |
| I                        | %               | isokinetics                                                                  | $(0.09450 * T_s * V_m \text{ std}) / [P_s * v * Q * (A_n / 144) * (1 - (Bws / 100))]$ |
| <b>M</b>                 |                 |                                                                              |                                                                                       |
| Md                       | g/g-mole        | dry stack gas molecular wgt                                                  | $0.44(\%CO_2) + 0.320(\%O_2) + 0.280(\%N_2 + \text{inerts} + CO)$                     |
| mn(back)                 | g               | particulate in impingers                                                     | measurement from lab analysis                                                         |
| mn(front)                | g               | particulate in nozzle & probe                                                | measurement from lab analysis                                                         |
| mn(total)                | g               | total particulate collected                                                  | measurement from lab analysis                                                         |
| Ms                       | g/g-mole        | wet stack gas molecular wgt                                                  | $Md(1 - Bws) + 18.0(Bws)$                                                             |
| MW CO2                   | g/mole          | mo. wgt of carbon dioxide                                                    | 44 (see periodic table)                                                               |
| MW N2                    | g/mole          | mo. wgt of nitrogen                                                          | 28 (see periodic table)                                                               |
| MW O2                    | g/mole          | mo. wgt of oxygen                                                            | 32 (see periodic table)                                                               |
| MW H2O                   | g/mole          | mo. wgt of water                                                             | 18 (see periodic table)                                                               |
| <b>N</b>                 |                 |                                                                              |                                                                                       |
| N2                       | %               | percent nitrogen                                                             | $100 - (\%CO_2 + \%O_2 + \%CO + \text{inerts})$                                       |
| <b>O</b>                 |                 |                                                                              |                                                                                       |
| O2                       | %               | percent oxygen                                                               | read from measuring device                                                            |

## NOMENCLATURE (cont.)

## MECHANICAL ENGINEERING

①

## SOURCE TEST REPORT

## PERMIT RENEWAL TEST

TEST DATE: WEDNESDAY, AUGUST 26, 1992TESTER: APCD; DAVID SHINA, GUY ALLPIN, ENGINEERS: JOHN MCCHEATH, AUSTEN DUMATEST: PARTICULATESAPPLICABLE RULES: SO(Q)(1), SO(Q)(2), SI, 54SOURCE: R.E. HAZARD CONTRACTING CO., 10050 BLACK MTN. RD., SAN DIEGOSITE PERSONNEL: AL TILLEY, SUPT. AND "WILLIE", OPERATORPERMIT TO OPERATE: 000442, EXPIRES NOV. 1, 1992EQUIPMENT DESCRIPTION: HOT-MIX ASPHALT BATCH PLANT, 300 TONS/HR RATED CAPACITYP/O CONDITIONS: ATTACHEDOBSERVATIONS:

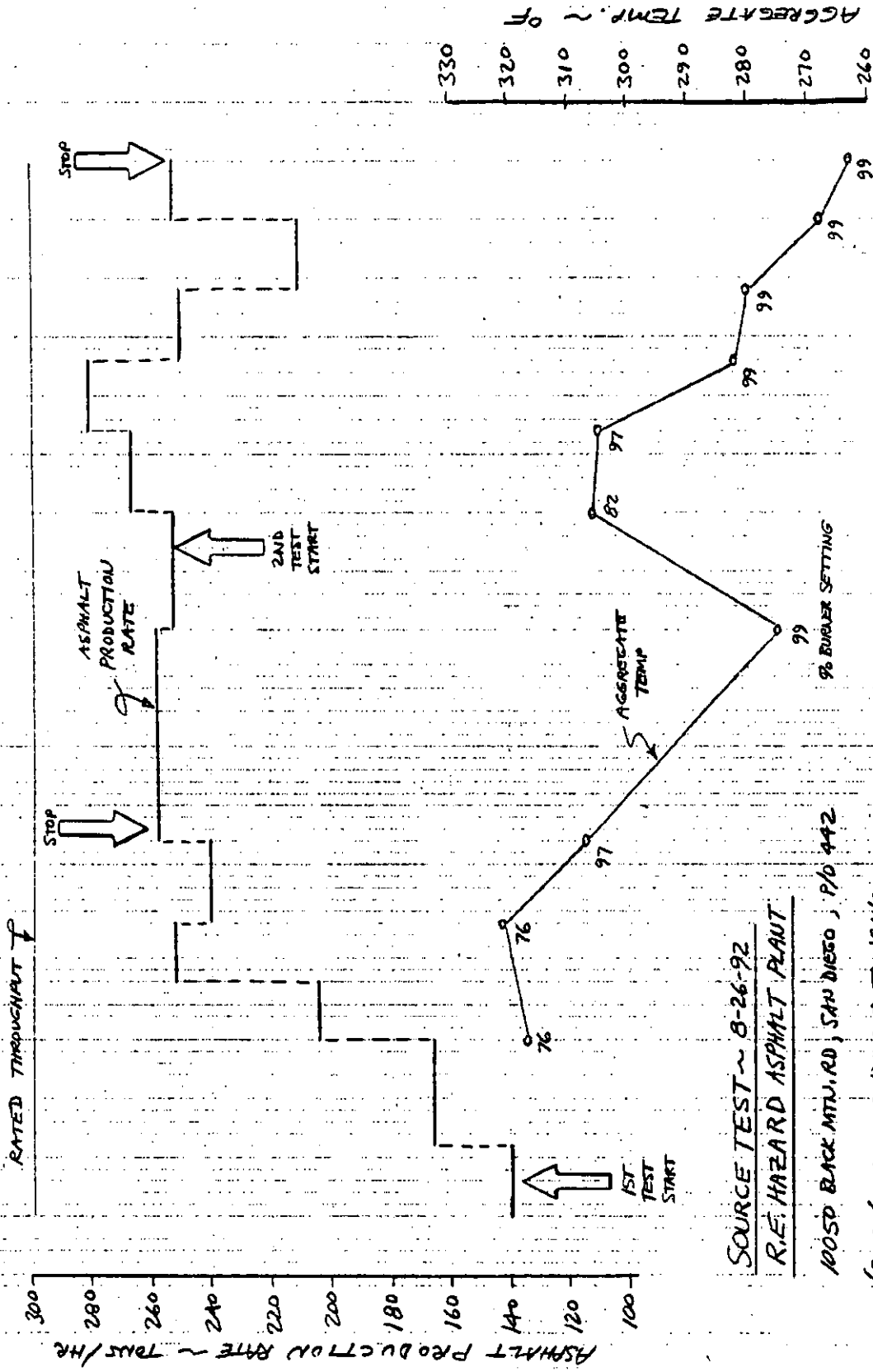
- THE RATED THROUGHPUT ON THE PERMIT IS 300 TONS/HR; DURING THE TESTS IT WAS 204 TONS/HR FOR THE FIRST (30 MIN.) TEST AND 252 TONS/HR FOR THE SECOND (33 MIN) TEST, WITH AN AVERAGE OF 229 TONS/HR.
- THE ROTARY DRUM DRYER AGGREGATE OUTPUT TEMPERATURE DROPPED FROM 317-321°F AT THE EARLY LOW PRODUCTION RATES, TO 263-282°F AT THE FINAL HIGH PRODUCTION RATES.
- THE BLUE SMOKE EXITED THE TRUCK TUNNEL AT APPROX. 20% OMCITY. NO FAN-VENTILATION WAS OCCURRING IN THE TUNNEL.

2

- THE MANHOLE LIDS ATOP THE UNDERGROUND ASPHALT OIL STORAGE TANKS HAD NO METHOD OF SEALING VAPOR; SEVERAL WERE LEAKING FUMES WITH APPROX. 20% OPACITY.
- SILO-TOP EMISSIONS AT THE DRAG-SLAT CONVEYOR WERE STEADILY VISIBLE AT APPROX 10% OPACITY.
- OCCASIONAL EMISSIONS WERE ESCAPING IN THE TOWER AREA ABOVE THE PUGMILL AND EXCEEDED 20% OPACITY.

COMMENTS:

- THIS PLANT HAS NOT DEMONSTRATED OR BEEN TESTED AT ITS RATED PRODUCTION RATE (300 TONS/HR) FOR SEVERAL YEARS. THE DRYER'S BURNER MAY BE UNDERSIZED FOR THE REMAINDER OF THE PLANT.
- NO DUST WAS OBSERVED FROM THE TRUCK TRAFFIC; ALL UNPAVED ROAD SECTIONS APPEARED TO BE DAMP OR WET.
- RULE 50(d)(2) ALLOWS 40% OPACITY SMOKE READINGS AT THE ASPHALT DROP BONE, INCLUDING THE TRUCK TUNNEL OPENINGS. OTHER FUGITIVE EMISSIONS ARE LIMITED TO 20% OPACITY BY RULE 50(d)(1); SOME OF THESE ARE CLOSE TO EXCEEDING THE RULE LIMITS.
- RULE 54 SHALL BE APPLIED TO THE RENEWAL TEST RESULTS, WHICH WILL BE IN COMPLIANCE IF THE STACK PARTICULATE EMISSIONS DO NOT EXCEED 40 LB/HR.



SOURCE TEST ~ 8-26-92  
 R.E. HAZARD ASPHALT PLANT

10050 BLACK MOUNTAIN RD, SAN DIEGO, P/O 442

(START/STOP TIMES ADJUSTED TO JCM'S  
 CLOCK... 4 MINUTES LESS THAN DAVID S. CLOCK)

|                      |      |      |      |      |      |      |      |      |      |
|----------------------|------|------|------|------|------|------|------|------|------|
| MINUTES ~ 0          | 10   | 20   | 30   | 40   | 50   | 60   | 70   | 80   | 90   |
| CLOCK TIME ~ 7:23 AM | 7:33 | 7:43 | 7:53 | 8:03 | 8:13 | 8:23 | 8:33 | 8:43 | 8:53 |

JCM

COUNTY OF SAN DIEGO  
AIR POLLUTION CONTROL DISTRICT  
915 JESAPEAKE DRIVE SAN DIEGO, CA 92123-106  
(619) 694-3307

68267  
CONTROL NO.

# PERMIT TO OPERATE

PERMIT NO.

000442

EXPIRES

NOVEMBER 1, 1991

THE FOLLOWING IS HEREBY GRANTED A PERMIT TO OPERATE THE ARTICLE, MACHINE, EQUIPMENT OR CONTRIVANCE DESCRIBED BELOW.  
THIS PERMIT IS NOT TRANSFERABLE TO A NEW OWNER, NOR IS IT VALID FOR OPERATION OF THE EQUIPMENT AT ANOTHER LOCATION,  
EXCEPT FOR PORTABLE EQUIPMENT.

## EQUIPMENT ADDRESS

HAZARD R E CONTRACTING CO  
PLANT SUPERINTENDENT  
P O BOX 229000  
SAN DIEGO CA 92122

10050 BLACK MTN RD  
SAN DIEGO CA 92126

## EQUIPMENT DESCRIPTION

REVISED COPY

FEE PAID

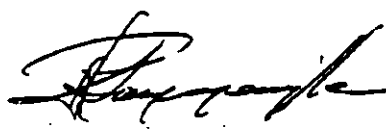
ASPHALT BATCH PLANT (300-TON/HR CAPACITY); STANDARD HOT MIX 8000 LB. BATCHER;  
109M BTU/HR INPUT ROT-DRYER; STANDARD HAVENS BAGHOUSE, 9660 SQ FT  
CLOTH AREA; 50,000 SCFM BLOWER; SUSPENDED OIL PARTICLE CONTROL; ENCLOSURE  
FOR THREE (3) ASTEC HB 200 TON STORAGE SILOS; ENCLOSED CONVEYOR TO SILO  
LOAD-IN AREA; THREE SILO BATCHERS; ONE 10,000 CFM BLOWER AND ASSOCIATED  
VENT DUCTING TO THE PLANT KNOCK-OUT BOX. RL201/91 900119  
H 00182A 000442 0139J 04A01 92A01

THIS PERMIT HAS BEEN ISSUED SUBJECT TO THE FOLLOWING CONDITIONS. FAILURE TO COMPLY WITH THESE CONDITIONS IS A MISDEMEANOR.

1. AIR POLLUTION CONTROL EQUIPMENT SHALL BE MAINTAINED IN GOOD OPERATING CONDITION AND SHALL BE IN FULL OPERATION IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS AT ALL TIMES WHEN THE PROCESS EQUIPMENT IS IN OPERATION.
2. ALL PROCESS EQUIPMENT SHALL BE MAINTAINED AND OPERATED SO THAT THERE IS NO LEAKAGE OF AIR CONTAMINANTS TO THE ATMOSPHERE PRIOR TO THEIR TREATMENT IN THE AIR POLLUTION CONTROL SYSTEM.
3. ACCESS ROADS AND YARDS IN THE GENERAL AREA OF THIS EQUIPMENT SHALL BE WATERED OR OTHERWISE TREATED TO PREVENT DUST GENERATED BY PLANT MOBILE TRAFFIC FROM EXCEEDING THE EMISSION STANDARDS OF RULE 30.
4. PERMITTEE SHALL PROVIDE ACCESS, FACILITIES, UTILITIES AND ANY NECESSARY SAFETY EQUIPMENT FOR SOURCE TESTING AND INSPECTION UPON REQUEST OF THE AIR POLLUTION CONTROL DISTRICT.
5. DAILY RECORDS OF HOT MIX ASPHALT PRODUCTION AND DELIVERY RATES SHALL BE MAINTAINED AND MADE AVAILABLE TO THE DISTRICT UPON REQUEST.
5. OPERATION MUST BE IN COMPLIANCE WITH ALL INFORMATION INCLUDED IN APPLICATIONS FOR THIS PERMIT TO OPERATE, AS APPROVED BY THE DISTRICT, AND WITH ALL CONDITIONS LISTED ABOVE.

WITHIN 10 DAYS AFTER RECEIPT OF THIS PERMIT, THE APPLICANT MAY PETITION THE HEARING BOARD TO REVIEW ANY CONDITION THAT HAS BEEN MODIFIED OR ADDED TO THE PERMIT. (RULE 25 AND REGULATION VI) IN ACCORDANCE WITH RULE 10C THIS PERMIT TO OPERATE OR A COPY MUST BE POSTED ON OR WITHIN 25 FEET OF THE EQUIPMENT, OR MAINTAINED READILY AVAILABLE AT ALL TIMES ON THE OPERATING PREMISES.

ANY AND ALL CONDITIONS WHICH HAVE BEEN APPLIED TO THIS EQUIPMENT SHALL REMAIN IN FULL FORCE AND EFFECT UNLESS EXPRESSLY MODIFIED BY THE AIR POLLUTION CONTROL DISTRICT. THIS AIR POLLUTION CONTROL DISTRICT PERMIT DOES NOT RELIEVE THE HOLDER FROM OBTAINING PERMITS OR AUTHORIZATIONS WHICH MAY BE REQUIRED BY OTHER GOVERNMENTAL AGENCIES.



R.J. Sommerville

AIR POLLUTION CONTROL OFFICER

DASHIN  
8/26/98

P.O. #442  
TEST # 041  
72234

R.E. HAZARD

# (1) IMPANGERS:

| DATE | NO | CONTENTS                | WGHT   | DATE | WGHT   | DIFF   |
|------|----|-------------------------|--------|------|--------|--------|
| 8/25 | 1  | 100 mL H <sub>2</sub> O | 574.15 | 8/26 | 744.15 | 170.10 |
|      | 2  | 100 mL H <sub>2</sub> O | 573.88 |      | 618.90 | 44.42  |
|      | 3  | MT                      | 483.97 |      | 446.66 | 10.54  |
|      | 4  | MT                      | 631.72 |      | 644.40 | 13.18  |

TOTAL = 200ML

TOTAL = 2386.9

# (2) GAS ANALYSIS:

CO<sub>2</sub>: Around AR400 : #1 = 2.6%, #2 = 2.5%, #3 = 2.5%, AVG = 2.5%  
O<sub>2</sub>: Tekdyne : #1 = 14.9%, #2 = 14.9%, AVG = 14.9%

# (3) CP:

OP (above) = 1.01 CP (above) = .8452  
AP (above) = 1.15 CP (below) = .8337  
OP (below) = 1.45

$$\left\{ \frac{(1.15 - 1.01)}{(1.45 - 1.01)} \right\} \times (.8337 - .8452) + .8452 = .8435$$

# (4) WGT'S: CAPSULES

| BLANKS: | ID      | RUNSES | TARE    | #1      | #2     | #3     | AVG     |
|---------|---------|--------|---------|---------|--------|--------|---------|
| Acetone | (92025) | 250+75 | 444837  | 49.9808 | 4864   | 4864   | 49.4864 |
| Water   | (92001) | 250+50 | 30.8146 | 30.8146 | .8198  | .8198  | 30.8198 |
| FRONT   |         |        |         |         |        |        |         |
| Ac      | (92086) | 250+50 | 24.2948 | 24.3012 | .3042  | .3042  | 24.3012 |
| Water   | (92078) | 250+50 | 20.8435 | 24.8605 | .8605  | .8605  | 24.8605 |
| BACK    |         |        |         |         |        |        |         |
| Ac      | (92084) | 280+50 | 24.2421 | 24.2590 | .2592  | .2592  | 24.2592 |
| Water   | (92003) | 300+50 | 30.2254 | 30.2477 | .2475  | .2477  | 30.2476 |
| FILTER  |         |        |         |         |        |        |         |
| Back    | (92004) | —      | 1.6007  | 1.6008  | 1.6008 | 1.6008 | 1.6008  |

6/4

??SITE NAME?? on ??TEST DATE??  
 SAN DIEGO AIR POLLUTION CONTROL DISTRICT, 9150 CHESAPEAKE DRIVE, SAN DIEGO, CA. 92123  
 SOURCE TEST OF PARTICULATE EMISSIONS TO THE ATMOSPHERE  
 TEST SITE: RE hazard

|                                                            |        |            |
|------------------------------------------------------------|--------|------------|
| TEST #:                                                    | P.O.#: | TEST DATE: |
| Type of plant (Asphalt/Perlite/Combustion): <b>ASPHALT</b> |        |            |
| UNIT TESTED:                                               |        |            |
| EQUIPMENT:                                                 |        |            |
| TESTED BY:                                                 | DATE:  |            |
| SITE PERSONNEL:                                            | DATE:  |            |
| APCD ENGINEER:                                             | DATE:  |            |
| LAB ANALYSIS BY:                                           | DATE:  |            |
| REPORT BY:                                                 | DATE:  |            |
| REVIEWED BY:                                               | DATE:  |            |
| APPROVED BY:                                               | DATE:  |            |

ROBERT YELENOSKY, SENIOR AIR POLLUTION CHEMIST

This report has been reviewed and found to be representative of the testing that was performed.

## SDAPCD RULES

| TEST                 | LIMIT     | MEASURED     | EXCEEDANCE/NON-EXCEEDANCE |
|----------------------|-----------|--------------|---------------------------|
| RULE 54 DUST & FUMES | 40 lbs/hr | 6.928 lbs/hr | NON-EXCEEDANCE            |

## TEST RESULTS SUMMARY:

| ITEM  | I   | Cs      | E      |
|-------|-----|---------|--------|
| UNITS | %   | gr/dscf | lbs/hr |
| VALUE | 105 | 0.0251  | 6.93   |

## ENGINEERING SUMMARY

| Qstd  | Fuel | Fuel Rate | Asphalt Production |
|-------|------|-----------|--------------------|
| dscfm | type | CFH       | tons/hr            |
| 32201 |      |           |                    |

## TEST PARAMETERS:

### SYSTEM DESCRIPTION:

This asphalt plant combines crushed rock and sand with asphalt oil in batch loads of varying sizes. The rock and sand are heated in a rotary drum to dry them. The exhaust from this dryer is routed through a baghouse and finally to a stack. It is the emissions from this stack that are the subject of this report.

### PROCEDURES:

The procedures utilized in these tests are based on EPA's 40 CFR, July 1, 1991, Part 60, Appendix A, Methods 1-5 inclusive. The sampling train was modified to utilize a back-end filter (fig. 1), as outlined in the SDAPCD QA manual.

### CALCULATIONS

All equations are from the EPA's 40 CFR, July 1, 1991, Part 60, Appendix A, Methods 1-5 inclusive. All preliminary assumptions and calculations are based on data obtained from previous tests.

### PARTICULATE SAMPLING:

The test consisted of sampling at 24 traverse points, 12 from each of 2 sample ports (fig.2), collected from ?? inches below the stack (fig.3). All field data was transferred to the computer printout. All calculations were done by the computer and the emissions were compared to rule ?? of the SDAPCD.

### ANALYSES:

**Gas:** An integrated bag sample was collected during the test and analyzed at the APCD lab.

**Particulate:** All procedures follow EPA guidelines, except where noted in the SDAPCD QA manual.

### EQUIPMENT:

All testing and analysis equipment was calibrated according to EPA guidelines (40 CFR, July 1, 1991, Part 60, Appendix A, Methods 1-5).

#### Analysis:

CO2-Anarad AR400  
 O2-Teledyne Ryan 320 P4  
 Macrobalance-Sargent Welch  
 Microbalance-Sartorius

#### Collection:

Filter-Gelman  
 Holder-Gelman  
 Beakers-Pyrex  
 Impingers-Ace

#### Sampling:

L/S Box-Napp  
 Umbilical cord-Napp  
 Cold/Hot box-Napp  
 Pitot tube-Napp

#### Temp./Press.:

Thermocouples-Omega  
 Temp. read out-Omega  
 Aneroid Barometer-Taylor  
 Press. devices-Dwyer magnohelic



# FIELD DATA:

| Trav. Pt | Vm (ft <sup>3</sup> ) | ΔP (in H <sub>2</sub> O) | ΔH (in H <sub>2</sub> O) | Stack Temp (°F) | Box Temp (°F) | Imp Temp (°F) | t 1 (in) (°F) | t 2 (out) (°F) | velocity (ft/sec) |
|----------|-----------------------|--------------------------|--------------------------|-----------------|---------------|---------------|---------------|----------------|-------------------|
| START    | 807.220               |                          |                          |                 |               |               |               |                |                   |
|          |                       | 1.448                    | 1.700                    | 212             |               | 63            | 81.00         | 101.00         | 079.89            |
|          |                       | 1.700                    | 2.000                    | 212             |               | 58            | 80.00         | 102.00         | 086.81            |
|          |                       | 1.620                    | 1.900                    | 200             |               | 68            | 79.00         | 105.00         | 083.98            |
|          |                       | 1.510                    | 1.700                    | 210             |               | 61            | 81.00         | 108.00         | 081.69            |
|          |                       | 1.138                    | 1.308                    | 212             |               | 61            | 81.00         | 110.00         | 070.63            |
|          |                       | 0.850                    | 1.000                    | 212             |               | 61            | 81.00         | 111.00         | 061.38            |
|          |                       | 0.650                    | 0.750                    | 212             |               | 61            | 82.00         | 112.00         | 053.68            |
|          |                       | 0.680                    | 0.800                    | 206             |               | 62            | 84.00         | 113.00         | 054.66            |
|          |                       | 0.620                    | 0.700                    | 210             |               | 61            | 84.00         | 112.00         | 052.35            |
|          |                       | 0.630                    | 0.730                    | 211             |               | 63            | 85.00         | 114.00         | 052.81            |
|          |                       | 0.700                    | 0.800                    | 213             |               | 63            | 85.00         | 115.00         | 055.74            |
|          |                       | 0.630                    | 0.730                    | 212             |               | 65            | 85.00         | 115.00         | 052.84            |
|          |                       | 1.000                    | 1.150                    | 218             |               | 64            | 88.00         | 109.00         | 066.78            |
|          |                       | 1.050                    | 1.200                    | 215             |               | 64            | 87.00         | 108.00         | 068.37            |
|          |                       | 1.110                    | 1.200                    | 215             |               | 65            | 87.00         | 111.00         | 070.30            |
|          |                       | 1.130                    | 1.300                    | 215             |               | 65            | 87.00         | 113.00         | 070.93            |
|          |                       | 1.130                    | 1.300                    | 215             |               | 65            | 87.00         | 113.50         | 070.93            |
|          |                       | 1.220                    | 1.400                    | 216             |               | 64            | 87.50         | 116.00         | 073.76            |
|          |                       | 1.310                    | 1.500                    | 217             |               | 62            | 87.00         | 116.00         | 076.40            |
|          |                       | 1.420                    | 1.650                    | 222             |               | 66            | 87.50         | 118.00         | 079.93            |
|          |                       | 1.480                    | 1.780                    | 218             |               | 60            | 87.50         | 118.50         | 081.24            |
|          |                       | 1.630                    | 1.900                    | 218             |               | 61            | 88.00         | 119.00         | 085.38            |
|          |                       | 1.820                    | 2.100                    | 219             |               | 61            | 88.00         | 119.50         | 090.28            |
|          | 846.608               | 1.880                    | 2.200                    | 221             |               | 61            | 88.50         | 120.00         | 091.90            |

|          | Vm ft <sup>3</sup> | ΔP (in H <sub>2</sub> O) | ΔH (in H <sub>2</sub> O) | ts (°F) | tbox (°F) | ti (°F) | t1 (in) (°F) | t2 (out) (°F) | vs (ft/sec) |
|----------|--------------------|--------------------------|--------------------------|---------|-----------|---------|--------------|---------------|-------------|
| Average: | 39.388             | 1.146                    | 1.367                    | 214     | na        | 62      | 84.92        | 112.52        | 71.37       |

# DATA SUMMARY:

| LABORATORY DATA:                                                                                                                                    | SAMPLING PARAMETERS:                                                                                                                      | SAMPLING DATA:                                                                                                                                                       |
|-----------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <b>IMPINGER CATCH:</b><br>Silica gel ? = <u>YES</u><br>Vlc = <u>238.69</u> ml                                                                       | <b>METER BOX:</b><br>Box ID = <u>c138</u><br>ΔH@ = <u>1.8883</u><br>Y = <u>0.9924</u>                                                     | <b>VOLUME &amp; TIME:</b><br>Ø (total time) = <u>60.0</u> min<br>Final leak rate = <u>0.001</u> cfm<br>Pass/Fail = <u>PASS</u><br>Vm = <u>39.388</u> ft <sup>3</sup> |
| <b>GAS ANALYSIS:</b><br>CO <sub>2</sub> = <u>2.50</u> %<br>O <sub>2</sub> = <u>14.90</u> %<br>CO = <u>0.00</u> %<br>N <sub>2</sub> = <u>82.60</u> % | <b>STACK DIMENSIONS:</b><br>Circular ? = <u>YES</u><br>Ds = <u>4.00</u> ft<br>Length = <u>N/A</u> ft<br>As = <u>12.56</u> ft <sup>2</sup> | <b>PRESSURES:</b><br>Pbar = <u>29.77</u> in Hg<br>Pg = <u>0.80</u> in H <sub>2</sub> O<br>Vpw @ ts = <u>29.9200</u> in Hg<br>Vpw @ ti = <u>N/A</u> in Hg             |
| <b>PARTICULATE ANALYSIS:</b><br>mn(front) = <u>0.023708</u> g<br>mn(back) = <u>0.036292</u> g<br>mn(total) = <u>0.06000</u> g                       | <b>NOZZLE &amp; PROBE</b><br>Dn = <u>0.205</u> in<br>An = <u>0.0330</u> in <sup>2</sup><br>Cp = <u>0.8435</u>                             | <b>TEMPERATURES:</b><br>t1 = <u>84.92</u> °F    ti = <u>62</u> °F<br>t2 = <u>112.52</u> °F    tbox = <u>na</u> °F<br>tm = <u>98.72</u> °F    ts = <u>214</u> °F      |

# **CALCULATIONS:**

## **TEMPERATURES:**

|     |                                                                               |        |
|-----|-------------------------------------------------------------------------------|--------|
| 01) | $T_s = (\sum t_{s(n)}) / \text{total n's}$                                    | 214 °F |
| 02) | $T_s = t_s + 460$                                                             | 674 °R |
| 03) | $T_m = (\sum (t_1(t_1) + t_2(t_2)) / 2) / \text{total n's} = (t_1 + t_2) / 2$ | 98 °F  |
| 04) | $T_m = (t_1 + t_2) / 2 + 460$                                                 | 559 °R |
| 05) | $T_s = (\sum t_{s(n)}) / \text{total n's}$                                    | 62 °F  |
| 06) | $T_{std}$                                                                     | 528 °R |

## **PRESSURES:**

|     |                                                                                 |             |
|-----|---------------------------------------------------------------------------------|-------------|
| 07) | $P_{bar} = (P @ S.L.) + [ft. \text{ above S.L.} * (-0.1 \text{ in Hg} / 1000)]$ | 29.77 in Hg |
| 08) | $P_g = \text{read from pressure sensing device}$                                | 0.80 in H2O |
| 09) | $P_s = P_{bar} + [P_g / 13.6]$                                                  | 29.83 in Hg |
| 10) | $\Delta H$                                                                      | 1.37 in H2O |
| 11) | $P_m = P_{bar} + (\Delta H / 13.6)$                                             | 29.87 in Hg |
| 12) | $P_{std}$                                                                       | 29.92 in Hg |

## **VOLUME & MOISTURE:**

|     |                                                                             |                           |
|-----|-----------------------------------------------------------------------------|---------------------------|
| 13) | $V_m = V_{m(end)} - V_{m(begin)}$                                           | 39.388 ft^3               |
| 14) | $Y$                                                                         | 0.9924                    |
| 15) | $V_m = V_m * Y$                                                             | 39.089 ft^3               |
| 16) | $V_m \text{ std} = [(V_m * (T_{std} / T_m) * (P_m / P_{std}))]$             | 38.878 ft^3               |
| 18) | $V_{ic} = (\sum \text{Volume of Impingers})$                                | 238.69 ml                 |
| 20) | $\rho$                                                                      | 0.002201 lb/ml            |
| 21) | $R$                                                                         | 21.85 in Hg-ft^3/°R-lb-mo |
| 22) | $M_{wH2O}$                                                                  | 18.00 g/g-mo              |
| 23) | $V_w \text{ std} = [(V_{ic} * R * T_{std}) / (P_{std} * M_{wH2O})]$         | 11.2351 ft^3              |
| 24) | $B_{ws}(1) = (V_w \text{ std}) / (V_w \text{ std} + V_m \text{ std}) * 100$ | 23.35 %                   |
| 25) | $V_{pw} @ t_s = \text{from appendix}$                                       | 29.92 in Hg               |
| 26) | $B_{ws}(2) = [(V_{pw} @ t_s) / P_s] * 100$                                  | 100.31 %                  |
| 27) | $B_{ws} = \text{lower value of equation 24 or 26}$                          | 23.35 %                   |

## **VELOCITY:**

|     |                                                                               |                |
|-----|-------------------------------------------------------------------------------|----------------|
| 28) | %O2                                                                           | 14.90 %        |
| 29) | %CO2                                                                          | 2.50 %         |
| 30) | %N2+Inerts+%CO                                                                | 82.60 %        |
| 31) | $M_d = [0.440(\%CO_2)] + [0.320(\%CO)] + 0.280(\%N_2 + \text{Inerts} + \%CO)$ | 29.00 g/g-mole |
| 32) | $M_s = M_d * (1 - B_{ws}) + 18.0 * (B_{ws})$                                  | 26.43 g/g-mole |
| 33) | $\Delta P$                                                                    | 1.1459 in H2O  |
| 34) | $C_p$                                                                         | 0.844          |
| 35) | $v_s = 85.49 * C_p * [(T_s * \Delta P) / (P_s * M_d)]^{1/5}$                  | 71.372 ft/sec  |
| 36) | $A_s = 3.14 * [(D_s)^2 / 4]$                                                  | 12.560 ft^2    |
| 37) | $Q_s = (v_s) * A_s * 60$                                                      | 53786 acfm     |
| 38) | $Q_{std} = 17.64 * Q_s * (1 - B_{ws}) * P_s / T_s$                            | 32201 dscfm    |

## **EMISSIONS:**

### **FRONT HALF**

|     |                                                                                                                   |                           |
|-----|-------------------------------------------------------------------------------------------------------------------|---------------------------|
| 39) | $mn \text{ (front)}$                                                                                              | 0.02371 g                 |
| 40) | $C_s \text{ (front)} = 15.43 * mn \text{ (front)} / V_m \text{ std}$                                              | 0.00992 grains/dscf       |
| 41) | $7000 \text{ grains} = 1 \text{ lb}, 60 \text{ min} = 1 \text{ hr}, 60 \text{ min/hr} / 7000 \text{ grains/lb} =$ | 0.00857 lbs-min/grains-hr |
| 42) | $E \text{ (front)} = (0.00857) * (Q_{std}) * C_s \text{ (front)}$                                                 | 2.74 lbs/hr               |

### **BACK HALF**

|     |                                                                                                                   |                           |
|-----|-------------------------------------------------------------------------------------------------------------------|---------------------------|
| 43) | $mn \text{ (back)}$                                                                                               | 0.03629 g                 |
| 44) | $C_s \text{ (back)} = 15.43 * mn \text{ (back)} / V_m \text{ std}$                                                | 0.01518 grains/dscf       |
| 45) | $7000 \text{ grains} = 1 \text{ lb}, 60 \text{ min} = 1 \text{ hr}, 60 \text{ min/hr} / 7000 \text{ grains/lb} =$ | 0.00857 lbs-min/grains-hr |
| 46) | $E \text{ (back)} = (0.00857) * (Q_{std}) * C_s \text{ (back)}$                                                   | 4.19 lbs/hr               |

### **TOTAL**

|     |                                                                                                                   |                           |
|-----|-------------------------------------------------------------------------------------------------------------------|---------------------------|
| 47) | $mn \text{ (total)} = mn \text{ (front)} + mn \text{ (back)}$                                                     | 0.06000 g                 |
| 48) | $C_s \text{ (total)} = 15.43 * mn \text{ (total)} / V_m \text{ std}$                                              | 0.02510 grains/dscf       |
| 49) | $7000 \text{ grains} = 1 \text{ lb}, 60 \text{ min} = 1 \text{ hr}, 60 \text{ min/hr} / 7000 \text{ grains/lb} =$ | 0.00857 lbs-min/grains-hr |
| 50) | $E \text{ (total)} = (0.00857) * (Q_{std}) * C_s \text{ (total)}$                                                 | 6.93 lbs/hr               |

## **ISOKEINETICS:**

|     |                                                                       |                  |
|-----|-----------------------------------------------------------------------|------------------|
| 51) | $D_n =$                                                               | 0.205 in         |
| 52) | $A_n = 3.14 * [(D_n)^2 / 4]$                                          | 0.0330 in^2      |
| 53) | $I = 0.9450 (T_s * V_m \text{ std}) / (P_s * V_{sAn} * (1 - B_{ws}))$ | 104.61 % = 105 % |

??Test Site Name?? on ??Test Date??

P.O. #:???? TEST#: ??????

SAN DIEGO AIR POLLUTION CONTROL DISTRICT, 9150 CHESAPEAKE DRIVE, SAN DIEGO, CA 92123

# PARTICULATE TEST LABORATORY ANALYSIS DATA SHEET

TEST SITE: R.E. HAZARD, Q A

|                                 |        |            |
|---------------------------------|--------|------------|
| TEST #:                         | P.O.#: | TEST DATE: |
| LAB ANALYSIS BY: David N. Shina |        | DATE:      |
| LAB REPORT BY: David N. Shina   |        | DATE:      |
| REVIEWED BY:                    |        | DATE:      |

## (1) IMPINGER VOLUMES

| FINAL WGT.  | INIT WGT. | NET WGT.   | Total impinger charge=                    |
|-------------|-----------|------------|-------------------------------------------|
| #1 744.15 g | 574.05 g  | = 170.10 g | 200.00 ml                                 |
| #2 618.70 g | 573.88 g  | = 44.82 g  | Partiulates from impinger charge          |
| #3 496.56 g | 485.97 g  | = 10.59 g  | (Total impinger charge * H(water blank) = |
| #4 644.90 g | 631.72 g  | = 13.18 g  | 0.00013 g                                 |
| #5 g        | g         | = N/A g    | Total weight collected=                   |
| #6 g        | g         | = N/A g    | 238.69 g                                  |
|             |           |            | Total volume collected, Vlc=              |
|             |           |            | 238.69 ml                                 |

## (2) BLANKS

| A     | B       | C     | D            | E             | F                   | G            | H             | I            | J               | K            | L             |
|-------|---------|-------|--------------|---------------|---------------------|--------------|---------------|--------------|-----------------|--------------|---------------|
| AREA  | SOLVENT | ID    | END WGT<br>g | INIT WGT<br>g | NET WGT.<br>g (E-F) | RINSES<br>ml | g/ml<br>(G/D) | %<br>(H*100) | ppm<br>(H*10*6) | PASS<br>FAIL | LIMITS        |
| BLANK | ACETONE | 92025 | 49.4864      | 49.4837       | 0.00270             | 325.00       | 0.0000083     | 0.0008308    | 8.3             | P            | 0.0010%=10ppm |
| BLANK | WATER   | 92001 | 30.8198      | 30.8198       | 0.00020             | 300.00       | 0.0000007     | 0.0000667    | 0.7             | P            | 0.0004%=4ppm  |
| BLANK | ORGANIC | N/A   |              |               |                     |              |               |              |                 |              |               |

## (3) WEIGHTS & RINSES

| a     | b        | c     | d            | e              | f                   | g            | h                    | i                     | j                              | k                          |
|-------|----------|-------|--------------|----------------|---------------------|--------------|----------------------|-----------------------|--------------------------------|----------------------------|
| AREA  | SOLVENT  | ID    | END WGT<br>g | INIT. WGT<br>g | NET WGT.<br>g (e-f) | RINSES<br>ml | SOLV. WGT<br>g (g*H) | WGT (corr)<br>g (i-h) | Subtotal (mn (AREA))<br>g (Σj) | Total (mn (tot))<br>g (Σk) |
| F     | ACETONE  | 92086 | 29.3092      | 29.2998        | 0.0094              | 300.00       | 0.002492             | 0.00691               |                                |                            |
| R     | WATER    | 92078 | 28.8605      | 28.8435        | 0.0170              | 300.00       | 0.000200             | 0.01680               |                                |                            |
| O     | ORGANIC  | N/A   |              |                |                     |              |                      |                       |                                |                            |
| N     | FILTER   | N/A   |              |                |                     |              |                      |                       |                                |                            |
| T     |          |       |              |                |                     |              |                      | mn(front) =           | 0.023708 g                     |                            |
| B     | ACETONE  | 92084 | 29.2592      | 29.2421        | 0.0171              | 330.00       | 0.002742             | 0.01436               |                                |                            |
| R     | WATER ** | 92003 | 30.2476      | 30.2254        | 0.0222              | 350.00       | 0.000367             | 0.02183               |                                |                            |
| C     | ORGANIC  | N/A   |              |                |                     |              |                      |                       |                                |                            |
| K     | FILTER   | 91009 | 1.0008       | 1.0007         | 0.0001              |              |                      | 0.00010               |                                |                            |
|       |          |       |              |                |                     |              |                      | mn(back) =            | 0.00020 g                      |                            |
| TOTAL |          |       |              |                |                     |              |                      |                       | mn(total) =                    | 0.05000 g                  |

\*\* The Back Water-SOLV.WGT is corrected for the initial impinger charge  
{ [g(back water) \* H(blank water)] + [Partiulates from impinger charge] }.

# METHOD 5 EQUIPMENT CHECKLIST

SITE: 11.8 HAZARD TEST#: 92234 P.O.# 442 DATE: 8/26/92

## MISCELLANEOUS

☒ Camera & film  
☒ Ice chest  
☒ Ice  
☒ Tedlar bags  
☒ Duct tape

## CALCULATION EQUIP.

☒ Source Test briefcase  
☒ Calib. notebook  
☒ Stopwatch  
☒ Nomograph  
☒ Calculator  
☒ Assorted pens  
☒ Tape measure  
☒ White out  
☒ Labels  
☒ Scissors  
☒ Teflon tape  
☒ L/S Box fuses

## LAB/FIELD EQUIPMENT

☒ Acetone  
☒ Foil  
☒ Parafilm  
☒ Distilled water  
☒ Kimwipes  
☒ Vac. grease  
☒ 100 ml grad. cylinder  
☒ Sample coll. bottles  
☒ Nozzle brush  
☒ Probe brush

## SAMPLING EQUIPMENT (reserve)

☒ L/S Box  
☒ Pitot tube leak test equipment  
☒ Umbilical cord  
☒ Cold/Hot box  
☒ Impingers (Impingers 1-4)  
☒ Imp-imp connections  
☒ Imp-probe connections  
☒ 100ml of water in 1st 2 imp.  
☒ Impinger clips  
☒ Silica gel imp. with vac. adapter  
☒ Filter & Filter holder  
☒ Heating coil

## SAMPLING EQUIPMENT (main)

☒ L/S Box  
☒ Pitot tube leak test equipment  
☒ Thermocouple - read-out  
☒ Electrical cords (50' & 100')  
☒ Umbilical cord  
☒ Cold/Hot box  
☒ Impingers (Impingers 1-4)  
☒ Imp-imp connections  
☒ Imp-probe connections  
☒ Spare set of connections  
☒ 100ml of water in 1st 2 imp.  
☒ Impinger clips  
☒ Silica gel imp. with vac. adapter  
☒ Filter & Filter holder  
☒ Spare filter & filter holder  
☒ Heating coil  
☒ Probe  
☒ Spare probe  
☒ Nozzle boxes with nuts

## TOOL BOX

☒ Assorted monkey wrenches  
☒ Assorted open-end wrenches  
☒ Assorted screwdrivers  
☒ 3' pipe wrench  
☒ Port (wire) brush  
☒ Tape measure

## STACK EQUIPMENT

☒ Unirail  
☒ Port/nipple adapters  
☒ 2 C-clamps  
☒ 2 unirails with rollers  
☒ Chains  
☒ 2 nylon straps  
☒ Rope (25' and 50')  
☒ Pail  
☒ Gloves (leather)  
☒ Gloves (heat resistant)  
☒ Rags and diapers

## MISCELLANEOUS EQUIPMENT

☒ Nomograph-reserve  
☒ Calculator-reserve  
☒ Inclometer-reserve (cyclonic flow)  
☒ Filter-reserve (high moisture)  
☒ Large pipe wrench  
☒ Cold/hot box rollers for SDG&E sites

## SAFETY

☒ First aid box  
☒ Ear plugs  
☒ Safety shoes and hat  
☒ Safety cones

## EQUIPMENT DATA SHEET

|              | MAIN  |       |      |         |          | RESERVE |      |      |         |          |
|--------------|-------|-------|------|---------|----------|---------|------|------|---------|----------|
|              | TYPE  | ID#   | SIZE | CLEANED | CAL DATE | TYPE    | ID#  | SIZE | CLEANED | CAL DATE |
| Nozzle Dia.  | NAPP  | 205   | 7    | OK      | 6/92     |         |      |      |         |          |
| Pitot Tube   | NAPP  | 5N872 | 5    | OK      | 2/92     |         |      |      |         |          |
| Tedlar Bag   | SLC   | —     | —    | OK      | —        | SLC     | —    | —    | OK      | —        |
| L/S Box      | AL305 | C138  | —    | —       | 6/92     |         |      |      |         |          |
| Stack Sensor | One9  | —     | K    | —       | 6/92     | One94   | —    | K    | —       | 6/92     |
| Box Sensor   | ↓     | —     | K    | —       | 6/92     | ↓       | —    | K    | —       | 6/92     |
| Imp. Sensor  | ↓     | —     | K    | —       | 6/92     | ↓       | —    | K    | —       | 6/92     |
| ΔP Sensor    | WATER | —     | B-5  | —       | 6/92     | WATER   | —    | —    | —       | —        |
| ΔH Sensor    | WATER | —     | O-5  | —       | 6/92     | —       | —    | —    | —       | —        |
| Cold Box     | NAPP  | G3    | —    | —       | —        | B3      | NAPP | —    | —       | —        |
| Hot Box      | NAPP  | G3    | —    | —       | —        | B3      | NAPP | —    | —       | —        |
| Temp Disp.   | One94 | —     | —    | —       | —        | One94   | —    | —    | —       | —        |

SIGNATURE: OK

DATE: 8/25/92

TIME: 4/40

# IMPINGER COLLECTION, GAS ANALYSIS DATA SHEET

SITE:  P.O.#:  TEST #:  DATE:

## IMPINGER COLLECTION MEASUREMENTS:

### PRE-TEST

| A<br>DATE | B<br>IMP<br>No. | C<br>CONTENTS of<br>IMPINGER | D<br>CHARGE AMT<br>(g) | E<br>WGT of IMPINGER<br>+CHARGE (g) |
|-----------|-----------------|------------------------------|------------------------|-------------------------------------|
| 8/25      | 1               | H <sub>2</sub> O             | 100                    | 574.05                              |
|           | 2               | H <sub>2</sub> O             | 100                    | 573.88                              |
|           | 3               | —                            | —                      | 485.97                              |
|           | 4               | Silica                       | —                      | 631.72                              |

### POST-TEST

| F<br>DATE | G<br>WGT of IMPINGER<br>+CHARGE (g) | H<br>H <sub>2</sub> O collected<br>(G-E) (g) | I<br>COMMENTS |
|-----------|-------------------------------------|----------------------------------------------|---------------|
| 8/26      | 744.15                              | 170.10                                       |               |
|           | 618.70                              | 44.82                                        |               |
|           | 496.50                              | 10.54                                        |               |
|           | 644.90                              | 13.18                                        |               |

TTL WGT OF  
CHARGE (ΣD) 200 g

TTL WGT GAIN  
FROM IMP (ΣH) 238.64 g

## BLANKS:

| TYPE    | LOT NUMBER | BRAND            | PREVIOUS                                | %PPT  | IF YES, TEST SITE |
|---------|------------|------------------|-----------------------------------------|-------|-------------------|
| WATER   |            |                  | YES <input checked="" type="radio"/> NO |       |                   |
| ACETONE | 9312       | omnisolve 3M Sci | YES <input checked="" type="radio"/> NO | 1 ppm |                   |
|         |            |                  | YES NO                                  |       |                   |

## GAS ANALYSIS:

|                 |                          |               |                  |
|-----------------|--------------------------|---------------|------------------|
| GAS= <b>CO2</b> | INSTRUMENT: AVALAN AR400 | Cal. Gas%= —  | % Cal. No.= 23.6 |
| DATE: 8/26      | RUN #1= 2.6 %            | RUN #2= 2.5 % | RUN #3= 2.5 %    |
|                 |                          |               | AVG= 2.5 %       |

|                |                      |                 |              |
|----------------|----------------------|-----------------|--------------|
| GAS= <b>O2</b> | INSTRUMENT: Teledyne | Cal. Gas%= 7.9  | % Cal. No.=  |
| DATE:          | RUN #1= 14.96 %      | RUN #2= 14.20 % | RUN #3=      |
|                |                      |                 | AVG= 14.90 % |

## FILTERS:

| DATE | LOCATION | LABEL | PRE-TEST WEIGHT |
|------|----------|-------|-----------------|
| —    | FRONT    | N/A   | g               |
| 8/26 | BACK     | 91099 | 1.6009 g        |

## Cp CALCULATION:

|            |      |           |       |
|------------|------|-----------|-------|
| ΔP (above) | 1.01 | Cp(above) | .8452 |
| ΔP (test)  | 1.15 | Cp(test)  | ?     |
| ΔP (below) | 1.45 | Cp(below) | .8337 |

Pitot Tube S/N: 50530  
 Cal. Date: 6/92  
 Cp (test)= .8435

$$Cp(test) = \{ ([\Delta P(test) - \Delta P(above)] / [\Delta P(below) - \Delta P(above)]) * [Cp(below) - Cp(above)] \} + Cp(above)$$

$$\left( \frac{1.15 - 1.01}{1.45 - 1.01} \right) * (.8337 - .8452) + .8452$$

$$.1489 * (-.0115) + .8452 = .8435$$

# METER ORIFICE CHECK

SITE: L. E. HATFIELD TEST#: 92234 P.O#: 442 DATE: 8/26/92

L/S Box= \_\_\_\_\_  $\Delta H@$ = \_\_\_\_\_ Y= \_\_\_\_\_ Cal. Date= \_\_\_\_\_

$Y_c = (\text{time}/V_m) * [((0.0319 * T_m)/P_b)^{0.5}]$  run L/S box at  $\Delta H@$  for at least 5 minutes

~~PRE-TEST 5 MINUTE Y CHECK~~

POST-TEST ONLY

|         | TIME           | VOLUME          | t1 (in)   | t2 (out)     | t <sub>m</sub> =(t1+t2)/2 |
|---------|----------------|-----------------|-----------|--------------|---------------------------|
| INITIAL | <u>0</u>       | <u>840.269</u>  | <u>89</u> | <u>100.5</u> | <u>94.75</u>              |
|         | min            | ft <sup>3</sup> | °F        | °F           | °F                        |
|         | <u>8:17.20</u> |                 |           |              |                           |
|         | <u>8:22.20</u> |                 |           |              |                           |
| FINAL   | <u>5</u>       | <u>852.195</u>  | <u>89</u> | <u>119</u>   | <u>104</u>                |
|         | min            | ft <sup>3</sup> | °F        | °F           | °F                        |

Pbar= 29.68

Y= 1.924

.97\*Y= .9623

Y<sub>c</sub>= .9875

1.03\*Y= 1.022

0.97\*Y > Y<sub>c</sub> < 1.03\*Y

PASS

FAIL

| (t <sub>final</sub> ) - (t <sub>initial</sub> ) | V <sub>m</sub> (final) - V <sub>m</sub> (initial) | t <sub>m</sub> -avg = (t <sub>m</sub> (initial) + t <sub>m</sub> (final)) / 2 | T <sub>m</sub> = t <sub>m</sub> -avg + 460°R |
|-------------------------------------------------|---------------------------------------------------|-------------------------------------------------------------------------------|----------------------------------------------|
| <u>5</u>                                        |                                                   | <u>94.80</u>                                                                  | <u>559.30</u>                                |
| min                                             | ft <sup>3</sup>                                   | °F                                                                            | °R                                           |

Y<sub>c</sub>= 5 min / 3.426 ft<sup>3</sup> \* [((0.0319 \* 559.30°R) / 29.68 in Hg)<sup>0.5</sup>] = .9875

time um T<sub>m</sub> Pbar Y<sub>c</sub>

SIGNATURE: [Signature]

DATE: 8/26/92

TIME: 9:30

POST-TEST 5 MINUTE Y CHECK

|         | TIME | VOLUME          | t1 (in) | t2 (out) | t <sub>m</sub> =(t1+t2)/2 |
|---------|------|-----------------|---------|----------|---------------------------|
| INITIAL |      |                 |         |          |                           |
|         | min  | ft <sup>3</sup> | °F      | °F       | °F                        |
| FINAL   |      |                 |         |          |                           |
|         | min  | ft <sup>3</sup> | °F      | °F       | °F                        |

Pbar= \_\_\_\_\_

Y= \_\_\_\_\_

.97\*Y= \_\_\_\_\_

Y<sub>c</sub>= \_\_\_\_\_

1.03\*Y= \_\_\_\_\_

0.97\*Y < Y<sub>c</sub> < 1.03\*Y

PASS

FAIL

| (t <sub>final</sub> ) - (t <sub>initial</sub> ) | V <sub>m</sub> (final) - V <sub>m</sub> (initial) | t <sub>m</sub> -avg = (t <sub>m</sub> (initial) + t <sub>m</sub> (final)) / 2 | T <sub>m</sub> = t <sub>m</sub> -avg + 460°R |
|-------------------------------------------------|---------------------------------------------------|-------------------------------------------------------------------------------|----------------------------------------------|
|                                                 |                                                   |                                                                               |                                              |
| min                                             | ft <sup>3</sup>                                   | °F                                                                            | °R                                           |

Y<sub>c</sub>= \_\_\_\_\_ min / \_\_\_\_\_ ft<sup>3</sup> \* [((0.0319 \* \_\_\_\_\_°R) / \_\_\_\_\_ in Hg)<sup>0.5</sup>] = \_\_\_\_\_

time um T<sub>m</sub> Pbar Y<sub>c</sub>

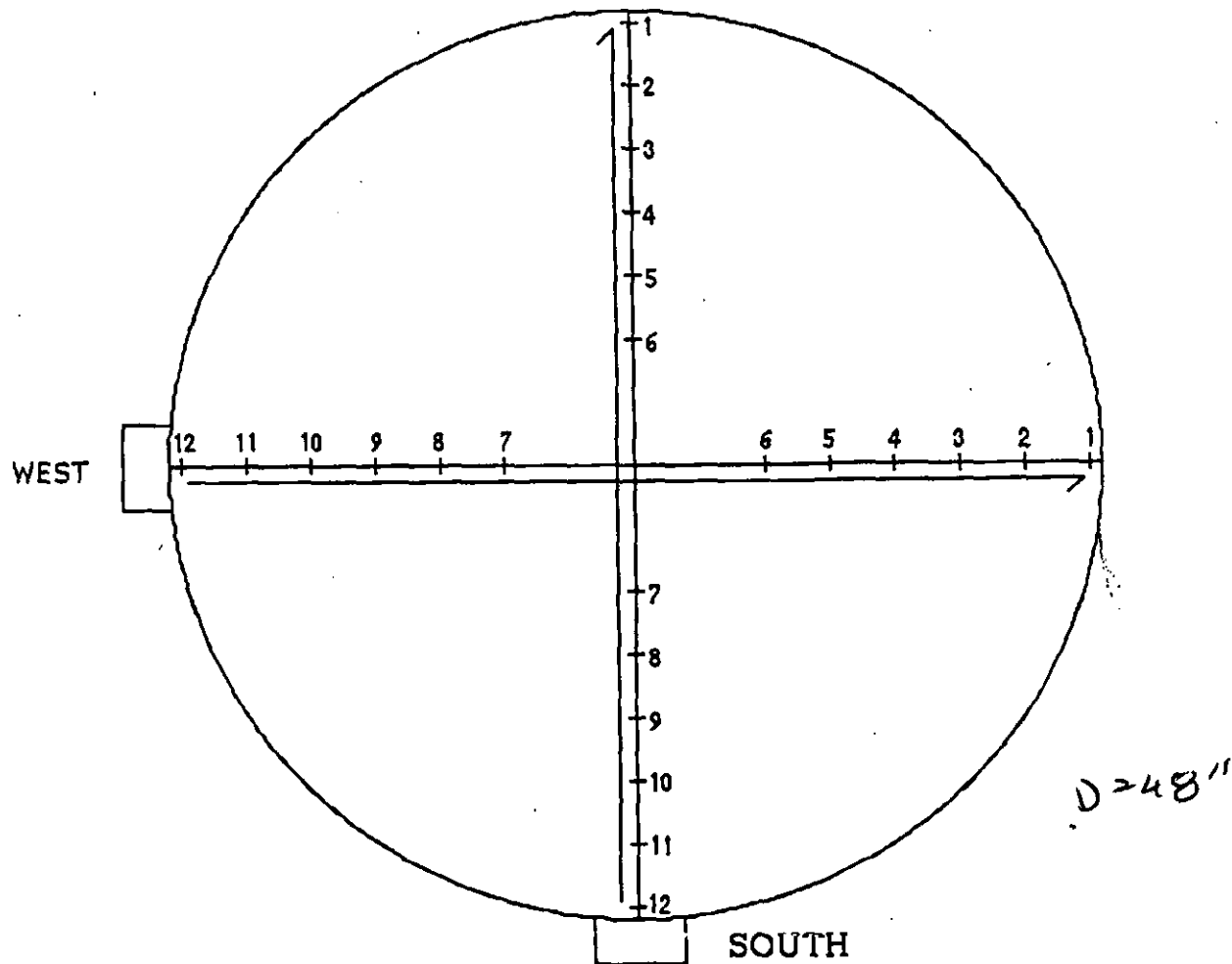
SIGNATURE: \_\_\_\_\_

DATE: \_\_\_\_\_

TIME: \_\_\_\_\_

# SAN DIEGO COUNTY AIR POLLUTION CONTROL STRICT

Figure  
TRAVERSE POINTS



| POINT | PERC%   | DIST. |
|-------|---------|-------|
| 1     | 2.1% =  | 1.0   |
| 2     | 6.7% =  | 3.2   |
| 3     | 11.8% = | 5.7   |
| 4     | 17.7% = | 8.5   |
| 5     | 25.0% = | 12.0  |
| 6     | 35.6% = | 17.1  |

| POINT | PERC%   | DIST. |
|-------|---------|-------|
| 7     | 64.4% = | 30.9  |
| 8     | 75% =   | 30    |
| 9     | 82.3% = | 34.5  |
| 10    | 88.2% = | 42.3  |
| 11    | 93.3% = | 44.8  |
| 12    | 97.9% = | 47    |



County of San Diego



R. J. Sommerville  
Air Pollution Control Officer

|               |                |
|---------------|----------------|
| AP-42 Section | 11.1           |
| Reference     |                |
| Report Sect.  | 4              |
| Reference     | <del>279</del> |

280

October 17, 1991

R .E. Hazard Contracting Co.  
Attention: Plant Superintendent  
P.O. Box 229000  
San Diego, CA 92122

SUBJECT: RENEWAL TEST REPORT

The enclosed test report is the result of testing done at your facility.

If you have any questions, please call me at (619) 694-3359.

  
C. W. Ridencour  
Senior Air Pollution Chemist

CWR:jo

Enclosures

AIR POLLUTION CONTROL DISTRICT  
9150 Chesapeake Drive, San Diego, California 92123-1095  
(619) 694-3307 FAX (619) 694-2730



SOURCE TEST OF PARTICULATE EMISSIONS TO THE ATMOSPHERE

TEST SITE: R.E. Hazard  
10050 Black Mountain Road  
San Diego, CA 92126

TEST #: 91248

P.O.# 442

TEST DATE: 9/5/91

Type of plant (Asphalt / Perlite / Combustion): asphalt

UNIT TESTED: Baghouse

EQUIPMENT: Asphalt Batch Plant

|                                                                                |               |
|--------------------------------------------------------------------------------|---------------|
| TESTED BY: David Shina                                                         | DATE: 9/5/91  |
| SITE PERSONNEL: Al Tilley                                                      | DATE: 9/5/91  |
| APCD ENGINEER: John McCafferty                                                 | DATE: 9/5/91  |
| LAB ANALYSIS BY: David Shina                                                   | DATE: 9/18/91 |
| REPORT BY: David Shina                                                         | DATE: 9/18/91 |
| REVIEWED BY: Linda Twaddle                                                     | DATE: 9/23/91 |
| APPROVED BY: <i>[Signature]</i><br>C.W. RIBENOUR, SENIOR AIR POLLUTION CHEMIST | DATE: 10/9/91 |

This report has been reviewed and found to be representative of the testing that was performed.

| TEST                 | PERMIT LIMIT | MEASURED     | PERFORMANCE |
|----------------------|--------------|--------------|-------------|
| RULE 54 DUST & FUMES | 40 lbs/hr    | 18.50 lbs/hr | PASSED      |

SUMMARY:

| ITEM  | Vm              | Bws   | Cs      | E      | I  | Qstd     | ts  | PROD RATE |
|-------|-----------------|-------|---------|--------|----|----------|-----|-----------|
| UNITS | ft <sup>3</sup> | %     | gr/dscf | lbs/hr | %  | dscfm    | °F  | tons/hr   |
| VALUE | 53.306          | 21.66 | 0.051   | 18.497 | 96 | 4.21E+04 | 217 | + 277.5   |

† No APCD engineer was at the site, so the engineering data was provided by R.E. Hazard and interpreted by the District.

**SYSTEM DESCRIPTION:**

This asphalt plant combines crushed rock and sand with asphalt oil in batch loads of varying sizes. The rock and sand are heated in a rotary drum to dry them. The exhaust from this dryer is routed through a baghouse and finally to a stack. It is the emissions from this stack that are the subject of this report.

**PROCEDURES:**

The procedures and equipment utilized in these tests are based on EPA New Source Performance Standards Method 5. The sampling train was modified to use a back-end filter only and a fifth impinger filled with silica gel (fig. 1), as outlined by the SDAPCD QA manual.

**CALCULATIONS**

All preliminary assumptions and calculations are based on data obtained from previous tests. All equations are from EPA CFR 40, July 1, 1990, Parts 53-60, Appendix A, Methods 1-5 inclusive.

**PARTICULATE SAMPLING:**

The test consisted of sampling at 24 traverse points, 12 from each of 2 sample ports (fig.2), collected from 48 inches below the stack (fig.3). All field data was transferred to the computer printout. All calculations were done by the computer and the emissions were compared to rule 54 of the SDAPCD.

**ANALYSES:**

Gas: An integrated bag sample was collected during the test and analyzed at the APCD lab.

Particulate: All procedures follow EPA guidelines, except where noted in the SDAPCD QA manual.

**EQUIPMENT:**

All testing and analysis equipment was calibrated according to EPA guidelines.

|                            |                    |                     |                          |
|----------------------------|--------------------|---------------------|--------------------------|
| <b>Analysis:</b>           | <b>Collection:</b> | <b>Sampling:</b>    | <b>Temp./Press.:</b>     |
| CO2-Anarad AR400           | Filter-Gelman      | L/S Box-Napp        | Thermocouples-Omega      |
| O2-Teledyne Ryan 320 P4    | Holder-Gelman      | Umbilical cord-Napp | Read out-Omega           |
| Macrobalance-Sargent Welch | Beakers-Pyrex      | Cold/Hot box-Napp   | Barometric-calc. by APCD |
| Microbalance-Sartorius     | Impingers-Ace      | Pitot tube-Napp     | L/S box-Dwyer magnehelic |

R.E. Hazard on 9/5/91

P.O.#442 TEST #91248

| Trav. Pt | Vm (ft <sup>3</sup> ) | ΔP                    | ΔH                    | t 1(unc) | t 2(unc) | Stack Temp | Imp Temp | velocity |
|----------|-----------------------|-----------------------|-----------------------|----------|----------|------------|----------|----------|
|          | 150.816               | (in H <sub>2</sub> O) | (in H <sub>2</sub> O) | (°F)     | (°F)     | †† (°F)    | (°F)     | (ft/sec) |
| 1        |                       | 1.800                 | 2.370                 | 83.00    | 98.00    | 217        | 58       | 85.45    |
| 2        |                       | 1.110                 | 2.620                 | 82.00    | 114.00   | 224        | 57       | 71.54    |
| 3        |                       | 1.920                 | 2.840                 | 82.00    | 118.00   | 226        | 55       | 94.22    |
| 4        |                       | 2.150                 | 3.180                 | 82.00    | 118.00   | 226        | 61       | 99.70    |
| 5        |                       | 2.310                 | 3.270                 | 81.50    | 120.00   | 219        | 61       | 100.50   |
| 6        |                       | 2.320                 | 3.430                 | 83.00    | 120.00   | 217        | 64       | 102.89   |
| 7        |                       | 2.120                 | 3.140                 | 84.00    | 120.50   | 213        | 63       | 98.08    |
| 8        |                       | 1.950                 | 2.890                 | 84.00    | 120.50   | 215        | 59       | 94.19    |
| 9        |                       | 1.800                 | 2.370                 | 84.00    | 120.50   | 215        | 58       | 85.32    |
| 10       |                       | 1.620                 | 2.340                 | 84.00    | 120.50   | 216        | 55       | 85.91    |
| 11       |                       | 1.750                 | 2.600                 | 84.00    | 120.50   | 215        | 55       | 89.23    |
| 12       |                       | 1.380                 | 2.000                 | 84.00    | 120.00   | 193        | 54       | 77.93    |
| 1        |                       | 1.820                 | 2.400                 | 84.50    | 99.00    | 221        | 55       | 86.23    |
| 2        |                       | 1.720                 | 2.500                 | 84.50    | 112.00   | 218        | 59       | 88.66    |
| 3        |                       | 1.820                 | 2.700                 | 84.00    | 116.00   | 218        | 55       | 91.20    |
| 4        |                       | 1.780                 | 2.630                 | 84.00    | 119.00   | 218        | 45       | 90.19    |
| 5        |                       | 1.760                 | 2.800                 | 84.50    | 120.50   | 218        | 48       | 89.68    |
| 6        |                       | 1.900                 | 2.800                 | 84.50    | 121.00   | 218        | 48       | 93.18    |
| 7        |                       | 2.290                 | 3.300                 | 84.50    | 121.50   | 215        | 47       | 100.73   |
| 8        |                       | 2.350                 | 3.480                 | 84.00    | 122.50   | 218        | 50       | 103.63   |
| 9        |                       | 2.420                 | 3.580                 | 84.50    | 124.00   | 218        | 49       | 105.18   |
| 10       |                       | 2.150                 | 3.180                 | 86.50    | 124.50   | 218        | 49       | 99.12    |
| 11       |                       | 2.300                 | 3.400                 | 88.00    | 124.50   | 218        | 61       | 102.52   |
| 12       | 204.122               | 2.050                 | 3.030                 | 88.00    | 125.50   | 218        | 52       | 96.79    |

†† The thermocouple wires were loose and some read-out problems were experienced. To get velocity data for points 2-6 and points 8-12, on the second traverse, the average of the stack temperatures between points 1 and 7 were used. This average is 218°F.

|          | Vm (ft <sup>3</sup> ) | ΔP (in H <sub>2</sub> O) | ΔH (in H <sub>2</sub> O) | t 1 (°F) | t 2 (°F) | ts (°F) | ti (°F) | vs (ft/sec) |
|----------|-----------------------|--------------------------|--------------------------|----------|----------|---------|---------|-------------|
| Average: | 53.306                | 1.895                    | 2.860                    | 84.10    | 118.27   | 217     | 54      | 93.00       |

|                                                                                                                                                         |                                                                                                                                               |                                                                                                                                   |
|---------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------|
| <b>MISCELLANEOUS:</b><br>Ø = 66.0 min<br>tn = 24 points<br>ø = 2.8 min                                                                                  | <b>NOZZLE &amp; PROBE:</b><br>Dn = 0.205 in<br>An = 0.0330 in <sup>2</sup><br>Cp = 0.851                                                      | <b>METER BOX PARAMETERS:</b><br>ΔH@ = 2.7254<br>Y = 0.9782<br>Box ID = D337                                                       |
| <b>PRESSURES:</b><br>Pbar = 29.46 in Hg<br>Pg = -0.63 in H <sub>2</sub> O<br>Vpw @ ts = 33.02 in Hg<br>Silica (yes/no) = yes<br>Vpw @ ti = 0.0000 in Hg | <b>VOLUME:</b><br>start leak rate = 0.000 cfm<br>Pass/Fail PASS<br>final leak rate = 0.000 cfm<br>Pass/Fail PASS<br>Vm 53.306 ft <sup>3</sup> | <b>TEMPERATURES:</b><br>t1 corr = 0.40 °F<br>t2 corr = 0.10 °F<br>tm = 101 °F<br>ts = 217 °F<br>ti = 54 °F                        |
| <b>STACK PARAMETERS:</b><br>circular (yes/no) = yes<br>Ds = 4.00 ft<br>Length = N/A<br>As = 12.56 ft <sup>2</sup>                                       | <b>LAB DATA:</b><br>mn(front) = 0.10224 g<br>mn(back) = 0.05944 g<br>mn(total) = 0.1617 g<br>Vlc 284.84 ml                                    | <b>STACK GAS MEASUREMENTS:</b><br>CO <sub>2</sub> = 3.27 %<br>O <sub>2</sub> = 14.47 %<br>CO = 0.00 %<br>N <sub>2</sub> = 82.26 % |

R.E. Hazard on 9/5/91

P.O.#442 TEST #91248

# TEMPERATURES:

|     |                                                        |        |
|-----|--------------------------------------------------------|--------|
| 01) | $t_s = (\sum t_s(n))/\text{total } n's$                | 217 °F |
| 02) | $T_s = t_s + 460$                                      | 677 °R |
| 03) | $t_m = (\sum \{t_1(n) + t_2(n)\}/2)/\text{total } n's$ | 101 °F |
| 04) | $T_m = (t_1 + t_2)/2 + 460$                            | 561 °R |
| 05) | $t_i = (\sum t_i(n))/\text{total } n's$                | 54 °F  |
| 06) | $T_{std}$                                              | 528 °R |

# PRESSURES:

|     |                                                                                     |              |
|-----|-------------------------------------------------------------------------------------|--------------|
| 07) | $P_{bar} = \{(P @ S.L.) + [ft. \text{ above } S.L. * (-0.1 \text{ in Hg}/100ft)]\}$ | 29.46 in Hg  |
| 08) | $P_g = \text{read from pressure sensing device}$                                    | -0.63 in H2O |
| 09) | $P_s = P_{bar} + (P_g/13.6)$                                                        | 29.41 in Hg  |
| 10) | $\Delta H$                                                                          | 2.86 in H2O  |
| 11) | $P_m = P_{bar} + (\Delta H/13.6)$                                                   | 29.67 in Hg  |
| 12) | $P_{std}$                                                                           | 29.92 in Hg  |

# VOLUME:

|     |                                                                                                        |                                    |
|-----|--------------------------------------------------------------------------------------------------------|------------------------------------|
| 13) | $V_m = V_m(\text{end}) - V_m(\text{begin})$                                                            | 53.306 ft <sup>3</sup>             |
| 14) | $Y$                                                                                                    | 0.9782                             |
| 15) | $V_m' = V_m * Y$                                                                                       | 52.144 ft <sup>3</sup>             |
| 16) | $V_{pw} @ t_i = \text{from appendix}$                                                                  | 0.0000 in Hg                       |
| 17) | $\text{corr } V_{wm} = \{[(V_m' * V_{pw} @ \text{imp}/P_s) * P_m * T_{std}]/(T_m * P_{std})\}$         | 0.0000 ft <sup>3</sup>             |
| 18) | $V_m \text{ std} = \{[V_m' * (T_{std}/T_m) * (P_m/P_{std})] - \text{corr } V_{wm}\}$                   | 48.629 ft <sup>3</sup>             |
| 19) | $V_{lc} = (\sum \text{Volume of impingers})$                                                           | 284.84 ml                          |
| 20) | $\partial$                                                                                             | 0.002201 lb/ml                     |
| 21) | $R$                                                                                                    | 21.85 Hg-ft <sup>3</sup> /°R-lb-mo |
| 22) | $M_{wH2O}$                                                                                             | 18.00 g/g-mo                       |
| 23) | $V_w \text{ std} = \{[(V_{lc} * \partial * R * T_{std})/(P_{std} * M_{wH2O})] + \text{corr } V_{wm}\}$ | 13.4444 ft <sup>3</sup>            |

# CALCULATIONS:

## MOISTURE-

|     |                                                                           |             |
|-----|---------------------------------------------------------------------------|-------------|
| 24) | $B_{ws}(1) = (V_w \text{ std})/(V_w \text{ std} + V_m \text{ std}) * 100$ | 21.66 %     |
| 25) | $V_{pw} @ t_s = \text{from appendix}$                                     | 33.02 in Hg |
| 26) | $B_{ws}(2) = [(V_{pw} @ t_s)/P_s] * 100$                                  | 112.26 %    |
| 27) | $B_{ws} = \text{lower value of equation 24 or 26}$                        | 21.66 %     |

## MOLECULAR WEIGHT-

|     |                                                                                  |                |
|-----|----------------------------------------------------------------------------------|----------------|
| 28) | %O2                                                                              | 14.47 %        |
| 29) | %CO2                                                                             | 3.27 %         |
| 30) | %N2+inerts+%CO                                                                   | 82.26 %        |
| 31) | $M_d = [0.440(\%CO_2)] + [0.320(\%O_2)] + [0.280(\%N_2 + \text{inerts} + \%CO)]$ | 29.10 g/g*mole |
| 32) | $M_s = M_d * (1 - B_{ws}) + 18.0 * (B_{ws})$                                     | 26.70 g/g*mole |

## FLOW-

|     |                                                               |                       |
|-----|---------------------------------------------------------------|-----------------------|
| 33) | $\Delta P$                                                    | 1.895 in H2O          |
| 34) | $C_p$                                                         | 0.851                 |
| 35) | $v_s = 85.49 * C_p * \{[(T_s * \Delta P)/(P_s * M_s)]^{.5}\}$ | 93.001 ft/s           |
| 36) | $A_s = 3.14 * [(D_s)^2/4]$                                    | 12.56 ft <sup>2</sup> |
| 37) | $Q_s = (v_s) * A_s * 60$                                      | 7.01E+04 acfm         |
| 38) | $Q_{std} = 17.64 * Q_s * (1 - B_{ws}) * P_s/T_s$              | 4.21E+04 dscfm        |

## EMISSIONS-

### FRONT HALF

|     |                                                                       |                                    |
|-----|-----------------------------------------------------------------------|------------------------------------|
| 39) | $m_n \text{ (front)}$                                                 | 0.10224 g                          |
| 40) | $C_s \text{ (front)} = 15.43 * m_n \text{ (front)} / V_m \text{ std}$ | 0.0296 gr/dscf = 0.030 grains/dscf |
| 41) | $E \text{ (front)} = (0.00857) * (Q_{std}) * C_s \text{ (front)}$     | 10.67 lbs/hr                       |

### BACK HALF

|     |                                                                     |                                    |
|-----|---------------------------------------------------------------------|------------------------------------|
| 42) | $m_n \text{ (back)}$                                                | 0.05944 g                          |
| 43) | $C_s \text{ (back)} = 15.43 * m_n \text{ (back)} / V_m \text{ std}$ | 0.0189 gr/dscf = 0.019 grains/dscf |
| 44) | $E \text{ (back)} = (0.00857) * (Q_{std}) * C_s \text{ (back)}$     | 6.80 lbs/hr                        |

### TOTAL

|     |                                                                       |                                  |
|-----|-----------------------------------------------------------------------|----------------------------------|
| 45) | $m_n \text{ (total)} = m_n \text{ (front)} + m_n \text{ (back)}$      | 0.1617 g                         |
| 46) | $C_s \text{ (total)} = 15.43 * m_n \text{ (total)} / V_m \text{ std}$ | 0.051 gr/dscf = 0.05 grains/dscf |
| 47) | $E \text{ (total)} = (0.00857) * (Q_{std}) * C_s \text{ (total)}$     | 18.50 lbs/hr                     |

# ISOKINETICS:

|     |                                                                           |                        |
|-----|---------------------------------------------------------------------------|------------------------|
| 48) | $A_n = 3.14 * [(D_n)^2/4]$                                                | 0.0330 in <sup>2</sup> |
| 49) | $I_n = .09450 * (T_s * V_m \text{ std}) / P_s * v_s * A_n * (1 - B_{ws})$ | 95.98 % = 96 %         |

## APPENDIX

SAN DIEGO AIR POLLUTION CONTROL DISTRICT, 9150 CHESAPEAKE DRIVE, SAN DIEGO, CA 92123

## LABORATORY ANALYSIS OF PARTICULATE TEST

TEST SITE: R.E. Hazard  
10050 Black Mountain Road  
San Diego, CA 92126

|                              |           |                   |
|------------------------------|-----------|-------------------|
| TEST # 91248.0               | P.O.# 442 | TEST DATE: 9/5/91 |
| LAB ANALYSIS BY: David Shina |           | DATE: 9/18/91     |
| LAB REPORT BY: David Shina   |           | DATE: 9/18/91     |
| REVIEWED BY: Linda Twaddle   |           | DATE: 9/23/91     |

**(1) IMPINGER VOLUMES**

| FINAL WEIGHT          | INITIAL WEIGHT | NET WEIGHT |
|-----------------------|----------------|------------|
| #1 848.74 g           | - 592.63 g     | = 256.11 g |
| #2 567.92 g           | - 564.94 g     | = 2.98 g   |
| #3 483.98 g           | - 474.02 g     | = 9.96 g   |
| #4 477.46 g           | - 474.15 g     | = 3.31 g   |
| SILICA GEL CONTAINER: |                |            |
| #5 877.40 g           | - 864.92 g     | = 12.48 g  |

Tot. Vol. = 284.84 g

**(2) BLANKS**

STD = Net Wgt(solv) / Tot. Vol(solv. used)

| ACETONE:                              | WATER:                             | ORGANIC:                              |
|---------------------------------------|------------------------------------|---------------------------------------|
| <b>VOLUMES:</b>                       | <b>VOLUMES:</b>                    | <b>VOLUMES:</b>                       |
| BKR ID = 91035                        | BKR ID = 91082                     | BKR ID =                              |
| Initial = 500.00 ml                   | Initial = 500.00 ml                | Initial = ml                          |
| tot. Rinses = 45.00 ml                | tot. Rinses = 15.00 ml             | tot. Rinses = ml                      |
| Tot. Vol = 545.00 ml                  | Tot. Vol = 515.00 ml               | Tot. Vol = 0.00 ml                    |
| <b>WEIGHTS:</b>                       | <b>WEIGHTS:</b>                    | <b>WEIGHTS:</b>                       |
| final = 29.1141 g                     | final = 49.5474 g                  | final = g                             |
| Initial = 29.1121 g                   | Initial = 49.5461 g                | Initial = g                           |
| net = 0.0020 g                        | net = 0.0013 g                     | net = 0.0000 g                        |
| LIMIT: 0.001% = 10 ppm = 0.000010g/ml | LIMIT: 4ppm = 4mg/L = 0.000004g/ml | LIMIT: 0.001% = 10 ppm = 0.000010g/ml |
| STD = 3.66972E-06 g/ml                | STD = 2.52427E-06 g/ml             | STD = N/A g/ml                        |
| 0.000367 %                            | 0.000252 %                         | N/A %                                 |
| 3.67 ppm                              | 2.52 ppm                           | N/A ppm                               |
| The Blank PASSED                      | The Blank PASSED                   | The Blank N/A                         |

**(3) WEIGHT****FRONT HALF****BACK HALF**

WEIGHT (uncorrected):

**ACETONE**

WEIGHT (uncorrected):

**ACETONE**

BKR ID= 91034

final= 30.8342 g

Initial= 30.7514 g

Wgt. Ac= 0.0828 g

BKR ID= 91032

final= 29.4142 g

Initial= 29.4070 g

Wgt. Ac= 0.0072 g

VOLUME:

Initial= 182.00 ml

tot. rinses= 45.00 ml

Sep funnel= ml

Tot. Vol= 227.00 ml

VOLUME:

Initial= 220.00 ml

tot. Rinses= 45.00 ml

Sep. funnel= ml

Tot. Vol= 265.00 ml

WEIGHT FROM SOLVENT:

Total Vol \* Acetone STD = 0.000833 g

WEIGHT (corrected):

Wgt(corr)= Wgt(unc)-Wgt from solvent= 0.081967 g

WEIGHT FROM SOLVENT:

Total Vol \* Acetone STD = 0.000972 g

WEIGHT (corrected):

Wgt(corr)= Wgt(unc)-Wgt from solvent= 0.006228 g

WEIGHT (uncorrected):

**WATER:**

WEIGHT (uncorrected):

**WATER:**

BKR ID= 91028

final= 29.2235 g

Initial= 29.2023 g

Wgt. Water= 0.0212 g

BKR ID= 91021

final= 29.5084 g

Initial= 29.5538 g

Wgt. Water= 0.0546 g

VOLUMES:

Initial= 322.00 ml

tot. Rinses= 45.00 ml

Tot. Vol = 367.00 ml

VOLUMES:

Initial= 428.00 ml

tot. Rinses= 45.00 ml

Imp. charge= 198.60 ml

Tot. Vol= 669.60 ml

WEIGHT FROM SOLVENT:

Total Vol \* Water STD = 0.000926 g

WEIGHT (corrected):

Wgt(corr)= Wgt(unc)-Wgt from solvent= 0.020274 g

WEIGHT FROM SOLVENT:

Total Vol \* Water STD = 0.001890 g

WEIGHT (corrected):

Wgt(corr)= Wgt(unc)-Wgt from solvent= 0.052910 g

WEIGHT (uncorrected):

**ORGANIC:**

WEIGHT (uncorrected):

**ORGANIC:**

BKR ID=

final= g

Initial= g

Wgt. Org= 0.0000 g

BKR ID=

final= g

Initial= g

Wgt. Org= 0.0000 g

VOLUMES:

tot. Rinses= ml

Tot. Vol= 0.00 ml

VOLUMES:

tot. Rinses= ml

Tot. Vol= 0.00 ml

WEIGHT FROM SOLVENT:

Total Vol \* Organic STD = N/A g

WEIGHT (corrected):

Wgt(corr)= Wgt(unc)-Wgt from solvent= N/A g

WEIGHT FROM SOLVENT:

Total Vol \* Organic STD = N/A g

WEIGHT (corrected):

Wgt(corr)= Wgt(unc)-Wgt from solvent= N/A g

WEIGHT:

**FILTERS:**

WEIGHT:

**FILTERS:**

ID No.=

final= g

Initial= g

Wgt. Filter= 0.0000 g

ID No.= 89081

final= 1.5099 g

Initial= 1.5096 g

Wgt. Filter= 0.0003 g

PARTICULATE COLLECTED (front half):

 $\Sigma$ Wgt corrected + Wgt filter= mn (front)= 0.10224 g

PARTICULATE COLLECTED (back half):

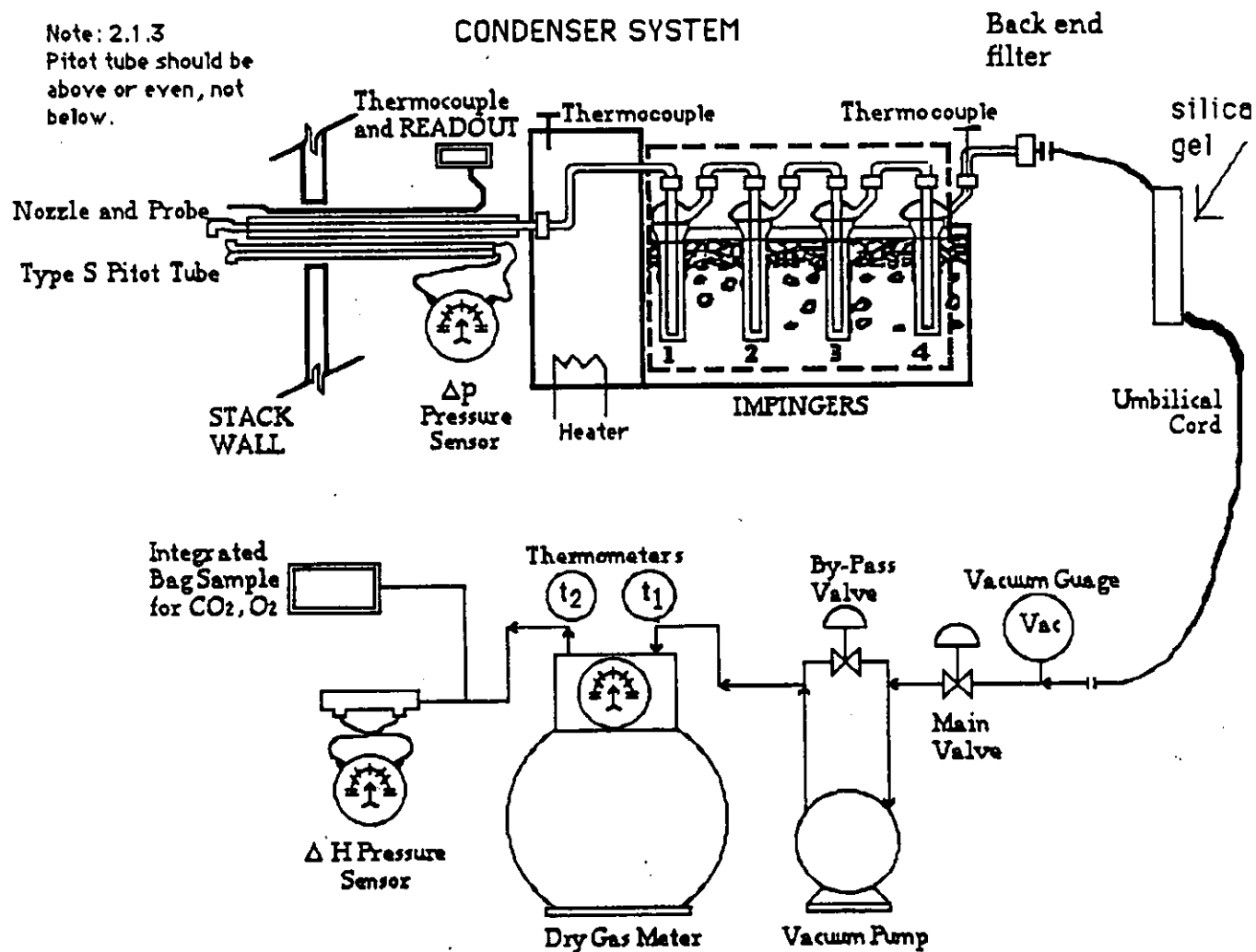
 $\Sigma$ Wgt corrected + Wgt filter= mn (back)= 0.05844 g

TOTAL PARTICULATE COLLECTED:

mn(front) + mn(back) = 0.16168 g

SAN DIEGO COUNTY AIR POLLUTION CONTROL DISTRICT

FIGURE  
CONDENSER SYSTEM



LEGEND

No. 1 Mod- 100 ML Deionized Water  
 No. 2 Std - 100 ML Deionized Water  
 No. 3 Mod- Dry  
 No. 4 Mod- Dry  
 Mod - Modified Type Greenburg-Smith  
 Std - Standard Type " "

FIELD DATA ABBREVIATIONS

PT = Point Number  
 $T_s$  = Stack Temperature  
 $\Delta P$  = Pitot Tube Pressure Differential, in  $H_2O$   
 $V_s$  = Stack Velocity, fps  
 $\Delta H$  = Orifice Meter Pressure Drop, in  $H_2O$   
 $t_1$  = Meter Inlet Temperature,  $^{\circ}F$   
 $t_2$  = Meter Outlet Temperature,  $^{\circ}F$   
 $P_m$  = Pump Vacuum, in Hg  
 $t_i$  = Impinger Temperature  
 $P_{bar}$  = Barometric Pressure

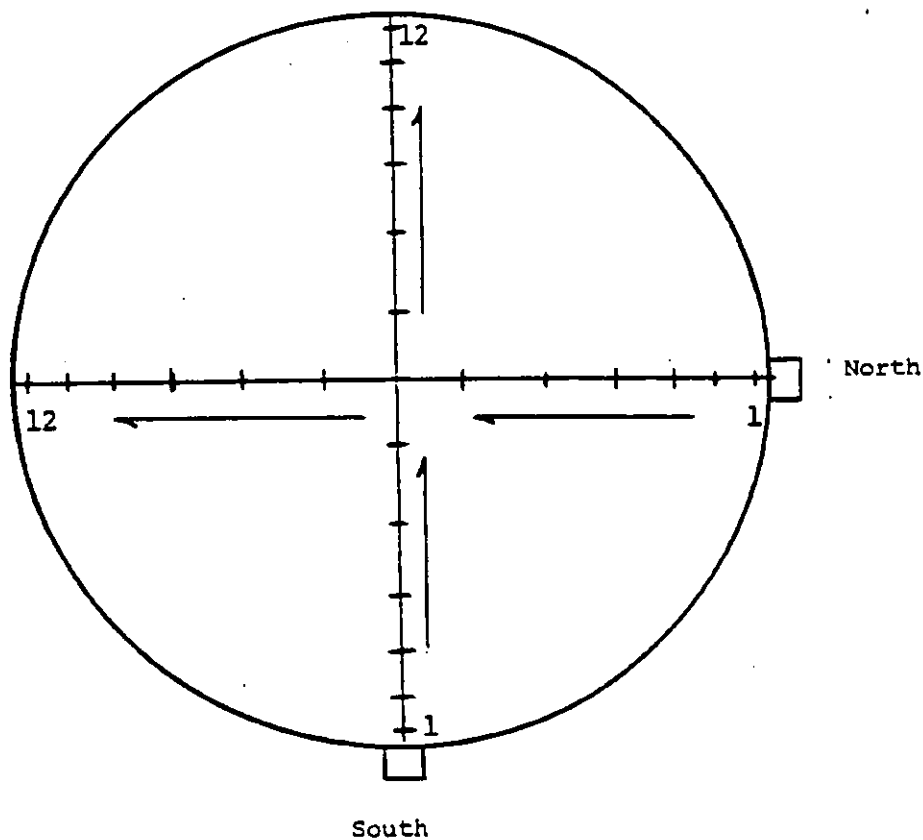
FIGURE 1 : PARTICULATE MATTER SAMPLING TRAIN

TEST NO.

SAN DIEGO COUNTY AIR POLLUTION CONTROL DISTRICT

TRAVERSE POINTS

STACK DIAMETER 48"



| POINT | DISTANCE | POINT | DISTANCE |
|-------|----------|-------|----------|
| 1     | 47.0"    | 7     | 17.1"    |
| 2     | 44.8"    | 8     | 12.0"    |
| 3     | 42.3"    | 9     | 8.5"     |
| 4     | 39.5"    | 10    | 5.7"     |
| 5     | 36.0"    | 11    | 3.2"     |
| 6     | 30.9"    | 12    | 1.0"     |

FIGURE 2



# SITE DESCRIPTION

HAZARD ASPHALT

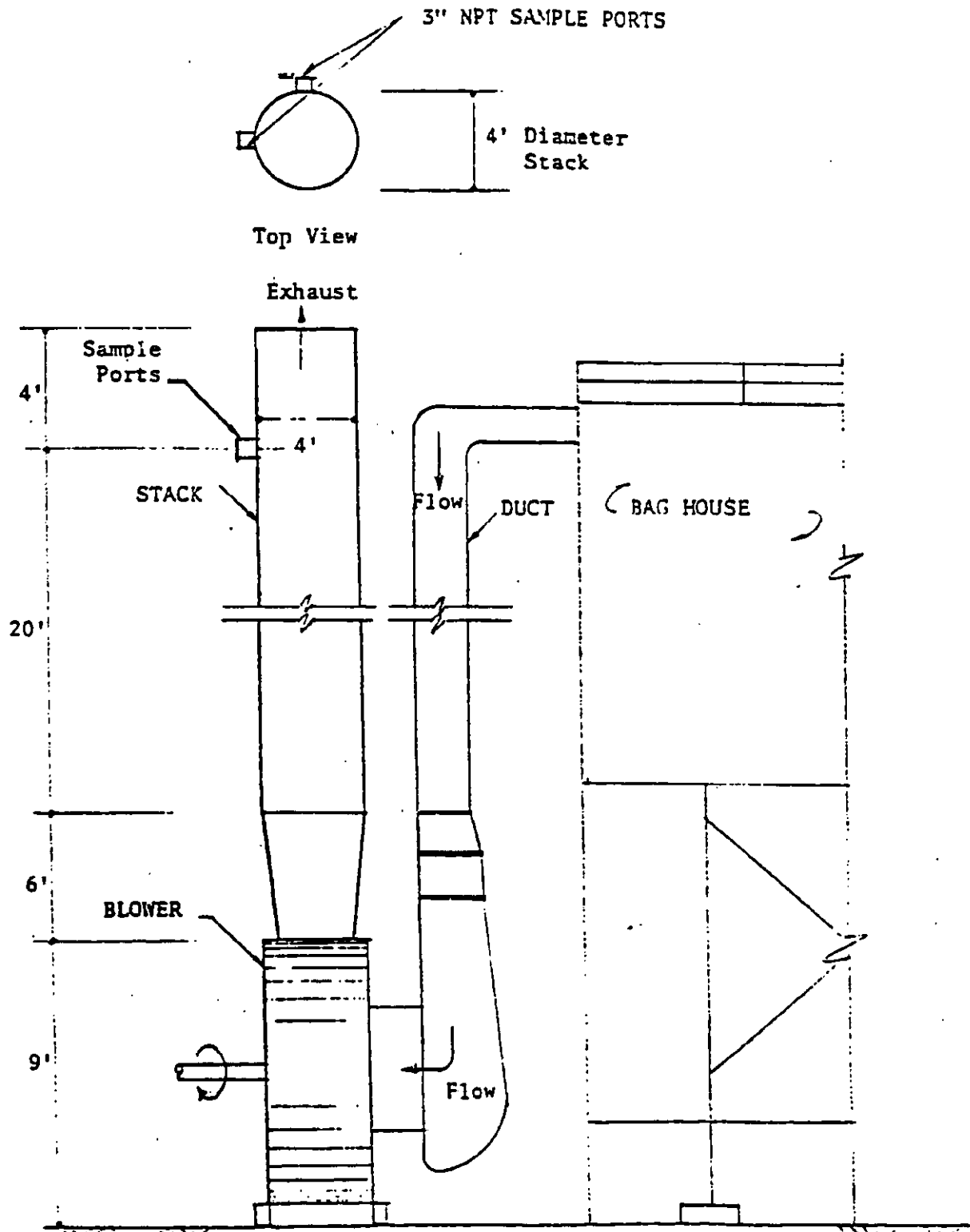


FIGURE 3

SIDE VIEW No Scale

# NOMENCLATURE

| symbol                | units               | explanation                                                           | equation                                                              |
|-----------------------|---------------------|-----------------------------------------------------------------------|-----------------------------------------------------------------------|
| <b>A</b>              |                     |                                                                       |                                                                       |
| A <sub>n</sub>        | in <sup>2</sup>     | nozzle area                                                           | $\pi/4(D_n)^2$                                                        |
| A <sub>s</sub>        | ft <sup>2</sup>     | stack area                                                            | $\pi/4(D_s)^2$ or L <sub>s</sub> W                                    |
| <b>B</b>              |                     |                                                                       |                                                                       |
| Bws(1)                | %                   | fractional stack gas moisture-equ 1                                   | $((V_w \text{ std})/(V_w \text{ std} + V_m \text{ std}))100$          |
| Bws(2)                | %                   | fractional stack gas moisture-equ 2                                   | $((V_{pw} @ ts)/P_s)100$                                              |
| Bws                   | %                   | water vapor in the gas stream                                         | lower of Bws(1) and Bws(2)                                            |
| <b>C</b>              |                     |                                                                       |                                                                       |
| C <sub>12</sub>       | gr/dscf             | corr for grain loading at 12% CO <sub>2</sub>                         | $(12\%C_s)/(\%CO_2)$                                                  |
| CO                    | %                   | carbon monoxide                                                       | read from measuring device (for Asphalt plants)                       |
| CO <sub>2</sub>       | %                   | carbon dioxide                                                        | read from measuring device                                            |
| Corr V <sub>wm</sub>  | ft <sup>3</sup>     | correction for V <sub>w</sub> w/o silica gel                          | $((V_m - (V_{pw} @ ts)/P_s)P_m T_{std}) / (T_m P_{std})$              |
| C <sub>p</sub>        | none                | phot tube correction factor                                           | see EPA method 3                                                      |
| C <sub>s(front)</sub> | gr/dscf             | concentration of particulate in stack gas, corrected to STP for front | $(15.43 \text{ mm(front)}) / (V_m \text{ std})$                       |
| C <sub>s(back)</sub>  | gr/dscf             | concentration of particulate in stack gas, corrected to STP for back  | $(15.43 \text{ mm(back)}) / (V_m \text{ std})$                        |
| C <sub>s(total)</sub> | gr/dscf             | concentration of particulate in stack gas, corrected to STP for total | $(15.43 \text{ mm(total)}) / (V_m \text{ std})$                       |
| <b>D</b>              |                     |                                                                       |                                                                       |
| ∂ (density)           | lb/ml               | density of water at STP                                               | 0.002201 (see CRC)                                                    |
| D <sub>s</sub>        | in or ft            | stack diameter                                                        | measure at site                                                       |
| D <sub>n</sub>        | in                  | nozzle diameter                                                       | avg of at least three measurements                                    |
| <b>E</b>              |                     |                                                                       |                                                                       |
| E <sub>A</sub>        | %                   | Excess air (for combustion)                                           | $((\%O_2 - \%CO)100) / ((26.1\%N_2 - \%O_2 - 5\%CO))$                 |
| E <sub>(front)</sub>  | lbs/hr              | part. emissions rate-front                                            | $(0.00857)(Q_{sd} C_{s(front)})$                                      |
| E <sub>(back)</sub>   | lbs/hr              | part. emissions rate-back                                             | $(0.00857)(Q_{sd} C_{s(back)})$                                       |
| E <sub>(total)</sub>  | lbs/hr              | part. emissions rate-total                                            | $(0.00857)(Q_{sd} C_{s(total)})$                                      |
| <b>H</b>              |                     |                                                                       |                                                                       |
| ΔH                    | in H <sub>2</sub> O | average differential pressure across the orifice meter                | avg of the readings from the pressure measuring device                |
| ΔH@                   | none                | orifice pressure differential at STP                                  | see EPA Method 5 Appendix                                             |
| <b>I</b>              |                     |                                                                       |                                                                       |
| I                     | %                   | isokinetics                                                           | $(0.09457 T_s V_m \text{ std}) / (P_s V_m^2 (A_n/144) (1 - Bws/100))$ |
| <b>M</b>              |                     |                                                                       |                                                                       |
| M <sub>d</sub>        | g/g-mole            | dry stack gas molecular wgt                                           | $0.44(\%CO_2) + 0.320(\%O_2) + 0.280(\%N_2 + \text{inerts} + CO)$     |
| mn(back)              | g                   | particulate in impingers                                              | measurement from lab analysis                                         |
| mn(front)             | g                   | particulate in nozzle & probe                                         | measurement from lab analysis                                         |
| mn(total)             | g                   | total particulate collected                                           | measurement from lab analysis                                         |
| M <sub>s</sub>        | g/g-mole            | wet stack gas molecular wgt                                           | $M_d(1 - Bws) + 18.0(Bws)$                                            |
| MW CO <sub>2</sub>    | g/mole              | mo. wgt of carbon dioxide                                             | 44 (see periodic table)                                               |
| MW N <sub>2</sub>     | g/mole              | mo. wgt of nitrogen                                                   | 28 (see periodic table)                                               |
| MW O <sub>2</sub>     | g/mole              | mo. wgt of oxygen                                                     | 32 (see periodic table)                                               |
| MW H <sub>2</sub> O   | g/mole              | mo. wgt of water                                                      | 18 (see periodic table)                                               |
| <b>N</b>              |                     |                                                                       |                                                                       |
| N <sub>2</sub>        | %                   | percent nitrogen                                                      | $100 - (\%CO_2 + \%O_2 + \%CO + \text{inerts})$                       |
| <b>O</b>              |                     |                                                                       |                                                                       |
| O <sub>2</sub>        | %                   | percent oxygen                                                        | read from measuring device                                            |

## NOMENCLATURE (cont.)

# **NOMENCLATURE (concl.)**

| symbol                 | units                             | explanation                                                                                       | equation                                                                                     |
|------------------------|-----------------------------------|---------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------|
| <b>P</b>               |                                   |                                                                                                   |                                                                                              |
| $\Delta P$             | in H <sub>2</sub> O               | pitot diff. press-velocity head of stack gas                                                      | read from measuring device                                                                   |
| $P_{bar}$<br>( $p_i$ ) | in Hg<br>none                     | barometric pressure at sampling pt.<br>the ratio of the circumference of a circle to its diameter | read from press measuring device<br>3.14169 (see CRC)                                        |
| $P_m$                  | in Hg                             | absolute meter pressure                                                                           | $P_{bar} + (Q/H/13.6)$                                                                       |
| $P_s$                  | in Hg                             | absolute stack pressure                                                                           | $P_{bar} + (P_{static}/13.6)$                                                                |
| $P_g$                  | in H <sub>2</sub> O               | static pressure of stack                                                                          | read from pressure sensing device                                                            |
| $P_{std}$              | in Hg                             | press at std conditions (29.92)                                                                   | see CFR                                                                                      |
| <b>Q</b>               |                                   |                                                                                                   |                                                                                              |
| $Q_s$                  | acfm                              | flow rate                                                                                         | $v_s \cdot A_o \cdot 60$                                                                     |
| $Q_{std}$              | dscfm                             | dry volumetric stack gas flow rate, corrected to STP                                              | $17.64 \cdot Q_s (1 - B_{ws}) \cdot (P_s / T_s)$                                             |
| <b>R</b>               |                                   |                                                                                                   |                                                                                              |
| $R$                    | in Hg-ft <sup>3</sup> /°R-lb-mole | ideal gas constant                                                                                | 21.85 (see CRC)                                                                              |
| <b>S</b>               |                                   |                                                                                                   |                                                                                              |
| S.L.                   | none                              | Sea Level                                                                                         | read from a relief map                                                                       |
| <b>T</b>               |                                   |                                                                                                   |                                                                                              |
| $t_1$                  | °F                                | dry gas meter inlet temp, uncorrected                                                             | read from temp sensing device                                                                |
| $t_2$                  | °F                                | dry gas meter outlet temp, uncorrected                                                            | read from temp sensing device                                                                |
| $t_1 \text{ corr}$     | °F                                | dry gas meter inlet temp, corrected                                                               | $t_1 + \text{temperature correction}$                                                        |
| $t_2 \text{ corr}$     | °F                                | dry gas meter outlet temp, corrected                                                              | $t_2 + \text{temperature correction}$                                                        |
| $\theta$ (theta)       | min                               | sampling time/point                                                                               | $Q/t_m$                                                                                      |
| $\Theta$ (Theta)       | min                               | total sampling time                                                                               | none                                                                                         |
| $t$                    | °F                                | impinger outlet temp                                                                              | read from temp sensing device                                                                |
| $t_m$                  | °F                                | dry gas meter temp in F                                                                           | $(t_1 + t_2)/2$                                                                              |
| $T_m$                  | °R                                | dry gas meter temp in R                                                                           | $t_m + 460$                                                                                  |
| $n$                    | none                              | tid number or traverse pts                                                                        | summation of the traverse points                                                             |
| $t_s$                  | °F                                | stack temp in F                                                                                   | read from temp sensing device                                                                |
| $T_s$                  | °R                                | stack temp in R                                                                                   | $t_s + 460$                                                                                  |
| $T_{std}$              | °R                                | temp at std conditions (528)                                                                      | see CFR                                                                                      |
| <b>V</b>               |                                   |                                                                                                   |                                                                                              |
| $V_c$                  | ml                                | water collected from impingers and the silica gel (if applicable)                                 | from lab analysis                                                                            |
| $V_m$                  | ft <sup>3</sup>                   | sample gas volume, uncorrected                                                                    | read from dry gas meter                                                                      |
| $V_m'$                 | ft <sup>3</sup>                   | sample gas volume, corrected                                                                      | $V_m \cdot Y$                                                                                |
| $V_m \text{ std}$      | ft <sup>3</sup>                   | volume of gas sample by the dry gas meter, corrected to STP                                       | $((V_m \cdot T_{std}) / P_m) / ((P_{std} \cdot T_m) - \text{corr } V_m)$                     |
| $V_{pw@ts}$            | in Hg                             | vapor pressure of water at $t_s$                                                                  | see CRC water vapor press. tables                                                            |
| $V_{pw@ti}$            | in Hg                             | vapor pressure of water at $t_i$                                                                  | see CRC water vapor press. tables                                                            |
| $v_s$                  | ft/sec                            | stack gas velocity                                                                                | $85.49 \cdot C_p \cdot ((T_s \cdot \Delta P) / (P_s \cdot M_s))^{0.5}$                       |
| $V_w \text{ std}$      | ft <sup>3</sup>                   | Vol. of water vapor in gas sample, corrected to STP                                               | $(V_c \cdot \gamma \cdot R \cdot T_{std}) / (P_{std} \cdot MW_{H_2O}) + \text{corr } V_{wm}$ |
| <b>Y</b>               |                                   |                                                                                                   |                                                                                              |
| $Y$                    | none                              | dry gas meter calibration factor                                                                  | see CFR 48, parts 53-60                                                                      |

## **Conversion Factors**

|                                 |                                                                    |                                                    |                                   |
|---------------------------------|--------------------------------------------------------------------|----------------------------------------------------|-----------------------------------|
| <b>(multiply by the number)</b> |                                                                    |                                                    |                                   |
| 0.002669                        | in Hg-ft <sup>3</sup> /°R-ml                                       | conversion to get in Hg-ft <sup>3</sup> /R         | see CRC                           |
| 0.00857                         | lb/gr-min/hr                                                       | conv from gr/min to lb/hr                          | see Lange's Handbook of Chemistry |
| 0.04707                         | ft <sup>3</sup> /ml                                                | conversion from ml to ft <sup>3</sup>              | see Lange's Handbook of Chemistry |
| 15.43                           | gr/g                                                               | conversion from g to gr                            | see Lange's Handbook of Chemistry |
| 85.49                           | (ft/sec)-(lb-in Hg/lb-mole-°R-in H <sub>2</sub> O)) <sup>0.5</sup> | conversion factor to get velocity in ft/sec        | see CRC                           |
| <b>(divide by the number)</b>   |                                                                    |                                                    |                                   |
| 144                             | in <sup>2</sup> /ft <sup>2</sup>                                   | conversion from in <sup>2</sup> to ft <sup>2</sup> | see CRC                           |
| 13.6                            | in H <sub>2</sub> O/in Hg                                          | conversion from in H <sub>2</sub> O to in Hg       | see CRC                           |
| <b>(add to the number)</b>      |                                                                    |                                                    |                                   |
| 460                             | °R/°F                                                              | conversion from F to R                             | see CRC                           |

# MECHANICAL ENGINEERING

## SOURCE TEST REPORT

### PERMIT RENEWAL TEST

TEST DATE: THURSDAY, SEPT. 5, 1991 ENGINEER: JOHN MCCAFFERTY

TESTER: APCD (DAVID SHINE & CREW)

TEST: PARTICULATES

SOURCE: R.E. HAZARD CONTRACTING CO., 10050 BLACK MTN RD, SAN DIEGO

PERMIT TO OPERATE: 000442, EXPIRES NOV. 1, 1991

EQUIPMENT DESCRIPTION: ASPHALT BATCH PLANT, HOT-MIX, 300 TONS/HR CAPACITY

P/O CONDITIONS: P/O COPY ATTACHED

#### OBSERVATIONS:

- ENGINEER MCCAFFERTY DID NOT VISIT THE SITE DURING THE SCHEDULED TEST BECAUSE OF UNAVAILABILITY OF A COUNTY POOL CAR.
- AL TILLEY (HOT PLANT SUPT) WAS PHONED AS THE TEST ENDED AND WAS ASKED TO FAX THE ASPHALT PRODUCTION DATA TO THE DISTRICT FOR THE TEST TIME PERIOD. THE TEST DATA INDICATED THAT THE SILO DISPENSING RATE FOR THE TWO "1/2-HOUR TESTS" WAS 333 TONS/HR. THAT RATE EXCEEDED THE PLANT'S RATED CAPACITY, HOWEVER THE PERMIT TO OPERATE LIMITS NEITHER THE PRODUCTION RATE NOR THE SILO DISPENSING RATE. THE ACTUAL PRODUCTION RATE DATA WERE NOT AVAILABLE BUT THE OPERATOR ESTIMATED A "LOWER-THAN-NORMAL" 275-280 TONS/HR WHICH IS ACCEPTABLE FOR THE PARTICULATES TEST - OVER 90% OF NORMAL.

# RAW DATA SHEETS