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AP42 Section: 11.1

Reference Number: 297

**Title: Source Sampling For Particulate Emissions, Syar Industries, Inc., Vallego, CA,
Bay Area Air Quality Management District, San Francisco, CA,**

April 4, 1990.

DISTRIBUTION:

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BAY AREA
AIR QUALITY MANAGEMENT DISTRICT
839 Ellis Street
San Francisco, California 94109
(415) 771-6000

SUMMARY OF SOURCE TEST RESULTS

AP-42 Section 11.1
Reference
Report No. 90 Report Sect. 4
Reference 296
Test Date: 4/4/ 297
Test Times:
Run A: 0813-1038 (54 min)
Run B: 1112-1219 (54 min)
Run C: 1256-1428 (48 min)

SOURCE INFORMATION		BAAQMD REPRESENTATIVES
Firm Name and Address SYAR INDUSTRIES, INC. Lake Herman Road Vallejo, CA 94591	Firm Representative and Title Mike Burneson, Plant Manager Phone No. (707)252-8711	Source Test Engineers C. McClure/H. Doi
	Source: S-23 Asphalt Plant Plant No. 128 Operates on demand	Permit Services Division / Enforcement Division T. Hirata Test Requested by: B. Nishimura (CDS)
Permit Conditions None		

Operating Parameters:

Kiln is natural gas fired. 1200 tons of 1/2" aggregate were produced. Baghouse inlet temperature averaged 325°F with a differential of 3 inches W.C.

Applicable Regulations: **6-310, 6-311**VN Recommended: **NO**

Source Test Results and Comments:

METHOD: TEST	RUN A	RUN B	RUN C	AVERAGE	LIMIT
ST-17 Stack Volume Flowrate, SDCFM	28,500	27,000	29,500	28,500	
Stack Gas Temperature °F	254	250	259	254	
ST-23 Water Content, Volume %	26.9	31.5	27.3	28.6	
ST-24 Oxygen, Volume %	9.0	8.7	9.0	8.9	
ST-24 Carbon Dioxide, Volume %	7.1	7.1	9.4	7.9	
ST-24 Carbon Monoxide, ppm	* >1950	>1950	>1950	>1950	
Carbon Monoxide, lb/hr	>239	>229	>252	>240	
ST-15 Particulate, gr/SDCF	.038	.036	.035	.036	.15
Particulate, lb/hr	9.2	8.3	8.9	8.8	40
Isokinetic Ratio, act/theo.	1.01	1.08	1.01		

* ">" indicates results greater than instrument full scale.

NO COMMERCIAL USE OF THESE RESULTS IS AUTHORIZED

Source Test Team Leader <i>C. McClure</i> C. McClure	Date <i>4/25/90</i>	Senior Source Test Engineer <i>K. Kunaniec</i> K. Kunaniec	Date <i>4/25/90</i>	Approved by Source Test Manager <i>G. Karels</i> G. Karels	Date <i>4/25/90</i>
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939 Ellis Street, San Francisco, Calif. 94109-771-6000

Source Test Data Sheet

Source Operation ASPHALT
Plant SYAR 12P
Sample Type PART
Process Cycle 002-002
Duct Size 25" H₂O
Duct Pressure 4" X 60" 5' 13.5" COM.
ASSUMED H₂O 2.6%

Source Test No. 12A
Run No. 014190
Date: 11/19/90

5.4" Nozzle Diameter
2.84" Pitot Tube
111112 Gas Collector No.
2894 Barometric Pressure
002-002 Leak Rate @ 15" Hg
TIME EACH POINT
OF POINTS
TIME EACH RUN

Sampling Train: PROBE → FILTER → 364 → 71 MPH P₁ → 111 MPH P₂ → 111 MPH

Traverse Point	Dist. From inches	INITIAL TRAVERSE		SAMPLING										REMARKS	
		Duct Temp of H ₂ O	H	Traverse Point	h H ₂ O	V _g FPS	Time	Rate CFM	METER Temp of	Volume Ft. ³	Vac "Hg	Sat'd Gas Temp of	T _g Duct Temp of	AP ₁ CFM	V ₁ /POINT
A-1	.65			A-1	.65	53.3	9.0	11125	60	756.76	6	36	739	24.7	
A-2	.75			A-2	.75	55.2	18	1528	60	760.46	9	37	725	27.5	
B-1	.56			B-1	.45	43.4	27	3539	60	673.79	7	37	677	21.1	
B-2	.70			B-2	.62	51.7	36	10439	60	711.43	9	37	769	24.3	
C-1	.50			C-1	.32	36.32	45	2775	61	74.11	5	38	735	17.8	
C-2	.24			C-2	.60	51.29	103	3952.61	61	771.67	9	38	779	23.7	
D-1	.30					48.51			60.33	20.91		37.17	754		
D-2	.25								52.38			497.17	7142		
E-1	.40	AP=70													
E-2	.25	T _g =767°R													
F-1	.33														
F-2	.20														

$$D_n = 13.7 \left[\frac{T_g + 460}{V_g (100 - 11120)} \right]^{1/2} = 5.18$$

$$Q_m = \left[(2.638 \times 10^{-3}) \left(\frac{100 - 11120}{74} \right) \right] \left(\frac{100 - 11120}{6.47} \right) \left(\frac{V_g}{T_g} \right)$$

$$V_s = 2.9 (k_p) \left(\frac{T_g}{T_m} \right) \left(\frac{V_m}{V_p} \right) \left(\frac{P_p}{P_m} \right) \left(\frac{100 - 11120}{20.41} \right) \left(\frac{100 - 11120}{21.30} \right)$$

$$V_o = 17.71 (V_m \times P_p) \left(\frac{100 - 11120}{20.41} \right) \left(\frac{100 - 11120}{21.30} \right)$$

Source Test Team
CHUCK MCCLURE
Source Test Engineer I
H. DOE

412	.	.	.	.	.
412	.	.	.	.	.
412	.	.	.	.	.
412	.	.	.	.	.

4460 244160 = 1076
4460
51" 1202

BS70471PM



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Source Test Data Sheet

Source Operation ASPHALT
Plant STAR #12P
Sample Type PREHEATED GAS
Process Cycle RAE-HYDRE
Duct Size 41X60+3"200
Duct Pressure -0.25" H₂O
ASSUMED H₂O
2.6%

Source Test No. _____
Run No. B
Date: 4/14/90

5.4 in Nozzle Diameter
0.84 Pitot Tube
VAR #12 Gas Collector No.
29.94 Barometric Pressure
0.00142 Leak Rate @ 15" Hg
9 TIME EACH POINT
6 # OF POINTS
54 TIME EACH RUN

Sampling Train: PROBE FILTER 365 SIMP# P3 SIMP# P4 7 AMP

Traverse Point	Dist. From inches	INITIAL TRAVERSE		SAMPLING										REMARKS	
		Duct Temp °F	H ₂ O °F	Traverse Point	h H ₂ O	V _s FPS	Time	Rate CFM	METER Temp °F	Volume Ft ³	Vac "Hg	Sat'd Gas Temp °F	T _s Duct Temp °F	DATE	TIME
				B-1	.60	.86	1112.0	9.41652	62	777.84	8	39	205	25	
				B-2	.75	.563	570.0	4.4178	62	781.596	10	38	253	27	
				D-1	.45	.429	27	35412	64	785.65	6	38	230	21.2	
				D-2	.60	.5045	36	40169	64	792.45	8	39	258	24.1	
				F-1	.60	.5174	45	39168	64	796.99	8	39	272	23.5	
				F-2	.41	.4197	1219.54	3.2998	64	798.99	5	40	264	19.8	
						.4257			63.53	21.15		38.7	249.8		
									523.33			41.0	708.98		

$$D_n = 13.7 \left[\frac{T_s + 460}{V_s (100 - \%H_2O)} \right]^{1/2}$$
$$Q_m = \left[(2.638 \times 10^{-3}) (100 - \%H_2O) D_n^2 \right] \frac{V_s}{T_s}$$

Condensate (9)
21.43 g
11120

$$V_s = 2.9 (k_p) \left[\frac{T_s \cdot h_{H_2O}}{21.6 (V_m \times P_b)} \right] = 21.43$$
$$T_m \text{ OR } 623.33$$

Source Test Team
CHUCK McCURE
Source Test Engineer I
H.001



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Source Test Data Sheet

Source Operation ACQUINAPTY
Plant SYNTHETIC GAS
Sample Type ACQUINAPTY
Process Cycle ACQUINAPTY
Duct Size 1 X 60
Duct Pressure -2.25 H₂O
ASSUMED H₂O 2.6 H₂O

Source Test No. 4490

Run No. 4490

Date: 4/4/90

5.4 Nozzle Diameter
2.84 Pitot Tube
1.00 Gas Collector No.
29.94 Barometric Pressure
2.00 Leak Rate @ 15"Hg
3 TIME EACH POINT
8 # OF POINTS
48 TIME EACH RUN

NOTE ⇒

Sampling Train: PROBE ⇒ FILTER # 363 ⇒ IMPT # 15 ⇒ IMPT # 16 ⇒ FILTER

Traverse Point	Dist. From inches	INITIAL TRAVERSE		METER							SAMPLING		REMARKS	
		Duct Temp °F	H ₂ O H ₂ O	h H ₂ O	Vg FPS	Time	Rate CFM	Temp °F	Volume Ft ³	Vac "Hg	Sat'd Gas Temp °F	Tg Duct Temp °F		
				A-1	70	5334	8.44327	64	799.55	7	39	225	26.6	
				A-2	75	554	4.5716	64	803.11	9	40	230	27.4	
				C-1	47	445	24.3596	64	803.65	6	40	239	21.6	
				C-2	48	546	38.42177	64	13.02	8	41	235	25.3	
				H ₂ O AT C-2	40	5164	40.39247	64	16.17	7	41	249	23.5	
				END OF SAMPLE	40	5165	142.48	64	18.30	7	41	245	23.4	
				END OF SAMPLE	40	5167		64	19.75		40.33	258.83		
				END OF SAMPLE	40	5168		64	19.75		500.33	718.83		
				C-2										

$D_h = 13.7 \left[\frac{T_a + 460}{V_g (100 - H_2O)} \right]^{1/2}$

Condensate (g) 500 500

$Q_m = \left[(2.638 \times 10^{-3}) (100 - H_2O) D^2 \right] \frac{V_g}{T_g}$

$V_s = 2.9 (k_p) \sqrt{T_s \cdot h_{H_2O}}$

$V_o = \frac{17.71 (V_m \times P_b)}{T_m \times P_r}$

Source Test Team
CHUCK MCCLURE
Source Test Engineer I
H. ADI

SOURCE TEST LAB DATA SHEET

PLANT: Syar Asphalt
 SOURCE OPERATION: Asphalt Plant, Baghouse
 SOURCE TEST NO.: _____
 FILTER MEDIA: _____

PAGE 1 OF 1
 INITIAL 1+D
 TEST DATE 4/4/90

Drying Procedure: 105 °C 24 hours before
 and after test, desiccated

~~WATER DATA~~

RUN NO.	FILTER NO.	TARE WEIGHT (g)			FINAL WEIGHT (g)	SAMPLE WEIGHT (µg)

~~PROBE & NOZZLE RINSE DATA (Total All Tests)~~

RUN NO.	FILTER NO.	JAR TARE WEIGHT (g)	JAR FINAL WEIGHT (g)	SAMPLE WEIGHT (µg)

~~PROBE & NOZZLE RINSE DATA (each run)~~

RUN NO.	PROBE/NOZZLE NOS.	JAR TARE WEIGHT (g)	JAR FINAL WEIGHT (g)	SAMPLE WEIGHT (µg)

~~OVERFLOW DATA~~

SOLUTION	NO.	A TARE WEIGHT	B FILLED WEIGHT	C FINAL WEIGHT	C-A SAMPLE WEIGHT	C-B CONDENSATE WEIGHT
H ₂ O	P-1	463.4	564.0	728.4	265.0	164.4
	P-2	506.3	606.4	606.8	100.5	0.4
	P-3	491.6	591.8	797.6	306.0	205.8
	P-4	496.3	596.0	597.7	101.4	1.7
	P-5	494.6	594.3	750.7	256.1	156.4
	P-6	487.6	587.7	588.3	100.7	0.6

164.8
144.8
207.5
20
157.0
15

SOURCE TEST LAB DATA SHEET

PLANT: Syar Asphalt Plant #128
 SOURCE OPERATION: Baghouse
 SOURCE TEST NO.: _____
 FILTER MEDIA: 110 mm Glass fibre filter

PAGE 1 OF 1
 INITIAL CM/HD/CTM
 TEST DATE 4/4/90

Drying Procedure: 105°C 24 hours before
 and after test, desiccated

PROBE & NOZZLE RINSE DATA (total all runs)

RUN NO.	FILTER NO.	TARE WEIGHT (g) 15 PM 1/12 AM	FINAL WEIGHT (g) 11 PM 4/10 PM	SAMPLE WEIGHT (g) 3
A	364	.6580 .6581	0.6809 0.6712	0.0228 ✓
B	365	.6661 .6661	0.6910 0.6911	0.0249 ✓
C	363	.6570 .6570	0.6792 0.6792	0.0222 ✓

PROBE & NOZZLE RINSE DATA (total all runs)

RUN NO.	FILTER NO. & JAR #	FINAL JAR TARE WEIGHT (g)	FILTER TARE WEIGHT (g)	SAMPLE WEIGHT (g) 3
A	364 + 12	0.0298	0.0228	0.0526 ✓
B	365 + 13	0.0255	0.0249	0.0504 ✓
C	363 + 14	0.0228	0.0222	0.0450 ✓

PROBE & NOZZLE RINSE DATA (each run)

RUN NO.	PROBE/NOZZLE NOS.	JAR TARE WEIGHT (g) 4-4 PM 4-13 PM	JAR FINAL WEIGHT (g) 4-13 PM 4-16 PM	SAMPLE WEIGHT (g) 3
A	12	56.5380 56.5381	56.5679 56.5680	0.0298 ✓
B	13	54.5962 54.5963	54.5720 54.5722	0.0255 ✓
C	14	54.6199 54.6196	54.6424 54.6426	0.0228 ✓

INTERFER DATA

SOLUTION	NO.	A TARE WEIGHT	B FILLED WEIGHT	C FINAL WEIGHT	C-A SAMPLE WEIGHT	C-B CONDENSATE WEIGHT

$$10.6) \quad G = 15.43 \cdot \frac{W_P}{V_D}$$

SYARING #12B
4/4/90

$$RUN A) \quad G_A = 15.43 \cdot \frac{0.0526}{21.30}$$

$$W_{PA} = 0.0526 \text{ g}$$

$$V_{DA} = 21.30 \text{ SDCF}$$

$$G_A = 0.038 \text{ gr/SDCF}$$

$$RUN B) \quad G_B = 15.43 \cdot \frac{0.0504}{21.42}$$

$$W_{PB} = 0.0504 \text{ g}$$

$$V_{DB} = 21.42 \text{ SDCF}$$

$$G_B = 0.036 \text{ gr/SDCF}$$

$$RUN C) \quad G_C = 15.43 \cdot \frac{0.0450}{19.98}$$

$$W_{PC} = 0.0450 \text{ g}$$

$$V_{DC} = 19.98 \text{ SDCF}$$

$$G_C = 0.035 \text{ gr/SDCF}$$

$$G_{\text{AUG}} = 0.036 \text{ gr/SDCF}$$

$$10.7) \quad M_A = \frac{G \cdot Q_D}{116.7} = \frac{(0.038)(28252)}{116.7}$$

$$Q_{DA} = 28252 \text{ SDCFM}$$

$$M_A = 9.2 \text{ Lb/HR}$$

$$M_B = \frac{(0.036)(27021)}{116.7}$$

$$Q_{DB} = 27021 \text{ SDCFM}$$

$$M_B = 8.3 \text{ Lb/HR}$$

$$M_C = \frac{(0.035)(29714)}{116.7}$$

$$Q_{DC} = 29714 \text{ SDCFM}$$

$$M_C = 8.9 \text{ Lb/HR}$$

$$M_{\text{AUG}} = 8.8 \text{ Lb/HR}$$

$$R_I = \frac{(T_s)(V_m) \times 100}{(60)(100 - \%H_2O)(A_n)(V_{s_{avg}})(TIME)(T_m)}$$

SYARIND #12P
4/4/90

RUN A) $V_{s_{avgA}} = 48.51 \text{ FPS}$ $T_{mA} = 520.33^\circ R$

$$A_n = 0.0002465 \text{ ft}^2$$

$$R_{IA} = \frac{(714)(20.91) \times 100}{(60)(73.05)(0.0002465)(48.51)(54)(520.33)}$$

$$(100 - \%H_2O_A) = 73.05$$

$$V_{mA} = 20.91 \text{ ft}^3$$

$$T_{sA} = 254^\circ 714^\circ R$$

$$TIME = 54 \text{ min}$$

$$R_{IA} = 1.01$$

RUN B) $(100 - \%H_2O)_B = 68.49$ $V_{mB} = 21.15 \text{ ft}^3$ $T_{sB} = 709.8^\circ R$
 $V_{sB} = 48.67 \text{ FPS}$ $T_{mB} = 523.33^\circ R$

$$R_{IB} = \frac{(709.8)(21.15) \times 100}{(60)(68.49)(0.0002465)(48.67)(54)(523.33)}$$

$$R_{IB} = 1.08$$

RUN C) $(100 - \%H_2O)_C = 72.68$ $V_{mC} = 19.75 \text{ ft}^3$ $T_{sC} = 718.83^\circ R$

$$R_{IC} = \frac{(718.83)(19.75) \times 100}{(60)(72.68)(0.0002465)(51.81)(48)(524)}$$

$$T_{mC} = 524^\circ R$$

$$V_{sC} = 51.81 \text{ FPS}$$

$$R_{IC} = 1.01$$

PPM TO Lb/Hr (CO)

STARING #128
4/4/90

$$\text{Lb/Hr} = \frac{(\text{PPM})(\overline{\text{MW}})(60)(Q_0)}{386.9 \times 10^6}$$

RUN A)

$$\text{Lb/Hr}_{\text{ACO}} = \frac{(>1950)(28.01)(60)(28252)}{386.9 \times 10^6}$$

$$\text{Lb/Hr}_{\text{ACO}} = 72.393 \times 10^2 \Rightarrow \underline{\underline{>239 \text{ Lb/Hr}}}$$

$$\overline{\text{MW}}_{\text{CO}} \Rightarrow \begin{array}{l} c = 12.011 \\ o = 15.9994 \\ \hline 28.0104 \end{array}$$

$$\overline{\text{MW}}_{\text{CO}} = 28.01$$

$$Q_{0A} = 28252 \text{ SCFM}$$

$$\text{PPM}_A > 1950$$

RUN B)

$$\text{Lb/Hr}_B = \frac{(>1950)(28.01)(60)(27021)}{386.9 \times 10^6}$$

$$Q_B = 27021 \text{ SCFM}$$

$$\text{Lb/Hr}_{\text{CO}_B} = > 228.8 \Rightarrow \underline{\underline{>229 \text{ Lb/Hr}}}$$

RUN C)

$$\text{Lb/Hr}_{\text{CO}_C} = \frac{(>1950)(28.01)(60)(29714)}{386.9 \times 10^6}$$

$$Q_C = 29714 \text{ SCFM}$$

$$\text{Lb/Hr}_{\text{CO}_C} = > 251.6 \Rightarrow \underline{\underline{>252 \text{ Lb/Hr}_{\text{CO}_C}}}$$

GAS ANALYSIS

(u = UNITS ON CHART PAPER)

SYARINO #128

VALLEJO CA 4/4/90

RUN A) O₂
 3.92
 4.00
 3.23
 4.00
 3.58
 3.48
3.48
 $\bar{X} = 3.70u$

CO₂
 1.95
 2.30
 2.20
 2.23
 2.30
2.30
 $\bar{X} = 2.20u$

CO
 >1950PPM
 $\frac{4.94}{2.02} = \frac{X}{3.70}$
 $\frac{14.8}{4.6} = \frac{X}{2.20}$

RUN A

O₂ = 9.05%

CO₂ = 7.1%

CO = >1950PPM

RUN B) O₂
 4.0
 3.45
 3.10
 3.76
 3.50
 3.58
3.58
 $\bar{X} = 3.56u$

CO₂
 2.0
 2.18
 2.35
 2.20
 2.30
 2.20
2.20
 $\bar{X} = 2.205u$

CO
 >1950PPM
 $\frac{4.94}{2.02} = \frac{X}{3.56}$
 $\frac{14.8}{4.6} = \frac{X}{2.205}$

RUN B

O₂ = 8.7%

CO₂ = 7.1%

CO = >1950PPM

RUN C) O₂
 4.10
 3.50
 3.74
 3.50
 3.60
3.60
 $\bar{X} = 3.69u$

CO₂
 2.98
 3.12
 3.22
 3.29
 2.10
2.10
 $\bar{X} = 2.94u$

CO
 >1950PPM
 $\frac{4.94}{2.02} = \frac{X}{3.69}$
 $\frac{14.8}{4.6} = \frac{X}{2.94}$

RUN C

O₂ = 9.02%

CO₂ = 9.4%

CO = >1950PPM

PLANT: SYAR #128

ADDRESS:

DATE: 4/4/90

OPERATOR: *CMP*

PLANT #: 128

- 1) What are you producting: 1/4", 1/2" 3/4"
- 2) What rate are you producing at: 300T/HR Tons/Hour - Average
- 3) What is your maximum rate of production: 350T/HR Tons/Hour
- 4) How much will you produce today: 1200 Tons-Average
- 5) What type of fuel are you burning: NAT'L GAS.
- 6) What is your rate of fuel useage? $\approx \approx$
- 7) What is your baghouse inlet temperature averaging: 325°F
- 8) What is your baghouse differential pressure: 3 "H₂O
- 9) What is the mositure content of the agregate: 2% H₂O
- 10) Are there any abnormal conditions in the plant today: NO
GOOD

Thank You

CMP

PLANT# 128

Syar Industries, Inc
Lake Herman Road
Vallejo, CA 94591

Sources:

- 1 PRIMARY CRUSHER
- 2 CONE CRUSHER
- 3 TURBO CRUSHER
- 4 SPOKANE CRUSHER (SOUTH)
- 5 SPOKANE CRUSHER (NORTH)
- 8 A.S.B. PLANT PRIMARY CRUSHER
- 15 DIESEL TANK
- 16 DIESEL TANK
- 17 DIESEL TANK
- 18 DIESEL TANK
- 19 Description not found
- 20 DIESEL PUMP
- 21 DIESEL PUMP
- 23 ASPHALTIC CONCRETE PLANT WITH ROTARY DRYER AND HEATER
- 24 ASPHALTIC CONCRETE SURGE BIN NO. 1
- 25 ASPHALTIC CONCRETE SURGE BIN NO. 2
- 28 DIESEL PUMP
- 29 TRANSFER POINTS COLLECTION SYSTEM
- 30 Stationary Tilt Type Concrete Mixer
- 31 Surge Bins
- 32 Cement Batcher
- 33 Pozzalan Silo
- 34 Cement Storage Silo (1)
- 35 Cement Storage Silo (2)
- 36 10-Yard Aggregate Weigh Batcher
- 37 ASB Plant Impact Crusher
- 40 Above Ground Asphalt Storage Tanks (AR4000)
- 41 Above Ground Asphalt Storage Tanks (AR4000)
- 42 Above Ground Asphalt Storage Tanks (AR8000)
- 43 Above Ground Asphalt Storage Tanks (SS-1)

Abatement Devices:

- 2 BAGHOUSE
- 4 BAGHOUSE
- 5 WATER SPRAY SYSTEM-TRANSFER POINTS
- 6 WATER SPRAY SYSTEM-TRANSFER POINTS
- 30 Pulse Jet Baghouse
- 31 Shaker Baghouse
- 32 Shaker Baghouse
- 33 Pulse Jet Baghouse
- 34 Shaker Baghouse
- 35 Pulse Jet Baghouse
- 36 Pulse Jet Baghouse
- 23 ASPHALT PLANT HEATER

Emission Points:

- 1 train: ,A2,/
- 3 train: ,A4,/

list source information for source # >> 23

PLANT 128 Syar Industries, Inc; Vallejo

SOURCE 23 MINERL> Mining/quarry, Burns multi-fuels, Asphaltic concrete

ASPHALTIC CONCRETE PLANT WITH ROTARY DRYER AND HEATER

Primary Use: Other

External combustion: Dryer (non-foods)

Combustion products-

P/O \$1470 Fee

Insp Freq: 12 mo

Emission train: S25,S24> @ >A2

list source information for plant # >>

LINE	MODIFY	BLOCK	REMOTE	193	40	FORMAT	MEMORY	DISPLAY	AUTO
MODIFY	ALL	MODE	MODE *	CN		MODE	LOCK	FUNCTNS	LF