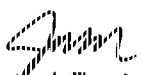


The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

Commonwealth of Pennsylvania
Environmental Resources
January 8, 1987

Subject: Source Test Review

To: Data File
Highway Materials, Inc.
Whitemarsh Township, Montgomery County

From: John N. Mitchell 
Air Pollution Control Engineer
Division of Technical Services and Monitoring
Bureau of Air Quality Control

Through: Chief, Source Testing and Monitoring Section 

Particulate and visible emission tests were conducted by Gilbert/Commonwealth Inc. on October 22-23, 1986 for the asphalt batch plant located at the Plymouth Meeting facility. The plant is a McCarter Corporation Model M-300-18 batch asphalt plant and is fired by natural gas. The particulate air contaminant emissions from the plant are controlled by a McCarter Corporation Model McC 10x10 ROB setting chamber pre-cleaner, followed by a McCarter Corporation Model McC-756-S post jet cleaning type fabric collector.

The batch asphalt plant is rated a capacity of 300 tons per hour. During the testing the plant was operated at a rate of about 10% higher than the rated capacity.

The particulate test and opacity test observations were conducted in accordance with the preapproved test protocol and are acceptable to the Department.

The following is a summary of the test results:

RUN NO.	1	2	3
Material Processed, Tons/hr.	348	336	330
Particulate Concentration, Grains/DSCF	0.0045	0.0156	0.0276
Allowable Concentration, Grains/DSCF	0.04	0.04	0.04
Particulate Emission Rate, lbs./hr.	1.31	4.12	7.28

Date File

-2-

January 8, 1987

cc: Jim Donnelly, Norristown Regional Office
File 46-30-019
Reading File
RSL/EPA

JNM:fsa

DER - RECEIVED
NORRISTOWN

DEC 23 1986

SOURCE SAMPLING REPORT FOR MEASUREMENT
OF PARTICULATE AND VISIBLE EMISSIONS

HIGHWAY MATERIALS, INC.
PLYMOUTH MEETING FACILITY
ASPHALT BATCH PLANT

PLYMOUTH MEETING
G/C, INC. REPORT R-10-0500-000-1
OCTOBER, 1986

Application No. 46-303-019

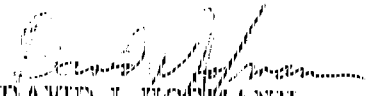
SOURCE SAMPLING REPORT FOR MEASUREMENT
OF PARTICULATE AND VISIBLE EMISSIONS

HIGHWAY MATERIALS, INC.
PLYMOUTH MEETING FACILITY
ASPHALT BATCH FACILITY

PLYMOUTH MEETING
G/C, INC. REPORT R-10-0500-000-1
OCTOBER, 1986

PREPARED BY

GILBERT/COMMONWEALTH, INC.
QUALITY ASSURANCE DIVISION
P.O. BOX 1498
READING, PENNSYLVANIA 19603


DAVID J. HOFFMANN
PROJECT COORDINATOR
TESTING SERVICES GROUP



Gilbert/Commonwealth engineers and consultants

GILBERT/COMMONWEALTH, INC., P.O. Box 1498, Reading, PA 19603/Tel. 215 775-2600/Cable Gilasoc/Tellex 836-431

December 8, 1986

Highway Materials, Inc
Plymouth Meeting, Pennsylvania

Attention: Mr. Vincent Angelo

RE: Submittal of Source Sampling Report
for Measurement of Particulate Emissions
Asphalt Batch Plant
Highway Materials, Inc.
Plymouth Meeting Facility
G/C, Inc. Report R-10-0500-000-1

Gentlemen:

We are pleased to submit four copies of our Report R-10-0500-000-1 dated December 8, 1986. This report contains results of source sampling for particulate emissions and determination of flue gas characteristics for the asphalt batch plant scrubber located at your Plymouth Meeting facility, as conducted on October 22-23, 1986.

The source sampling program defined by this report incorporates standard sampling procedures. The results of the sampling program are representative of flue gas emissions at the stack outlet of the scrubber under referenced normal operating conditions.

Information contained in this report and the accompanying Appendices includes field data, laboratory analyses, and a computer printout of all results developed by the testing program. We have attempted to present this information in a form that is readily discernible and suitable for your continued use.

Gilbert/Commonwealth, Inc., is pleased to have been of service to Highway Materials, Inc., and trusts that this report will meet your complete acceptance.

Very truly yours,

David Hofmann
Project Coordinator
Testing Services

DH:dh

FOREWORD

The source sampling program as defined by this report was confined to measurement of particulate emissions and pertinent flue gas characteristics at the stack test location of the asphalt batch plant scrubber during referenced operating conditions.

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Tables

1. Summary of Test Results

Figures

1. Location of Sample Ports and Traverse Points, Stack Location

SECTION I - SUMMARY OF TEST RESULTS

A summary of test results from the source sampling program is presented in Table 1. As such, the results are considered representative of emission characteristics from the asphalt batch plant baghouse during referenced operating conditions. The results show the particulate emissions are well below the limit of 0.04 gr/SCF.

TABLE 1

SUMMARY OF TEST RESULTS
HIGHWAY MATERIALS, INC.
ASPHALT BATCH PLANT

G/C, INC. REPORT R-10-0500-000-1

LOCATION	EXHAUST STACK		
DATE	10/22/86	10/23/86	10/23/86
RUN NO.	HM-1	HM-2	HM-3
<u>OPERATING DATA</u>			
Material Processed, Tons/Min.	5.3	5.6	5.5
<u>FLUE GAS CHARACTERISTICS</u>			
DSCFM	33,928	31,146	31,154
ACFM	52,355	53,533	51,918
Temperature, °F	261	271	242
Moisture Content, %	11.7	19.4	20.1
<u>PARTICULATE EMISSIONS</u>			
gr/dscf	0.0045	0.0156	0.0276
Allowable, gr/dscf	0.04	0.04	0.04
lbs/hr.	1.31	4.12	7.28
<u>VISIBLE EMISSIONS</u>			
Opacity, %	0.6	1.2	0.1

SECTION II - ANALYSIS

1. Introduction

The data presented in this report represents the results of source sampling exhaust emissions at the stack outlet location of the asphalt batch plant during referenced operating conditions.

Specific requirements of this source sampling program include the following:

- a. Identification of final particulate and visible emissions from the asphalt batch plant baghouse control system.
- b. Average flue gas temperature, moisture, and volume of flow at the sampling location.
- c. Orsat analysis of flue gas conditions at the point of sampling.
- d. Record of pertinent operating conditions during period of the test run.

The sampling program was completed on October 22-23 1986 by the Gilbert field test crew, with the assistance of personnel assigned by Highway Materials and witnessed by the PADER.

2. Description of Asphalt Batch Plant Exhaust System

The facility uses a McCarter Model M-300-18 asphalt plant rated at 300 tons per hour. The system uses a knock-out box followed downstream by baghouse to control emissions.

3. Sampling Program Procedures

To satisfy the objectives established for this project, the sampling program was set-up on the basis of using an individual test train positioned at the stack and completing three separate test runs. All procedures for the determination of velocity, molecular weight, moisture content, particulate loading, and visible emissions of the exhaust flue gases were made according to standard test methods as referenced in Appendix 2.

The location and number of sampling ports and traverse points are detailed in Figure 1.

4. Operating Conditions

In the execution of this sampling program, an attempt was made to achieve near normal load for the asphalt batch plant. The amount of asphalt generated was recorded by the operator. This record is included in the summary table (see Table 1).

5. Results

Test data developed by each test run, together with analytical results from laboratory analysis of samples generated by the field sampling program, are reproduced in the Appendices included with this report. Information on basic gas characteristics developed by each test run is contained in the printout of the computer program included as Appendix 8.

A summary of pertinent test results and essential information to evaluate test results developed for each test run is included with this report as Table 1.

6. Discussion

6.1 Sampling Conditions

All field sampling work was completed out of doors and subject to prevailing weather conditions; however, there were no interruptions in the operation of individual test trains due to equipment or weather problems.

During the completion of this test program, the asphalt batch plant was maintained near the normal load condition.

6.2 Exhaust Flue Gas Volume and Composition

Test data for measurement of exhaust flue gas volume and related velocities developed by traversing of the stack show that the measured gas volumes between tests were consistent with expected values. For purposes of this report, indicated emissions are based on these measured gas volumes.

6.3 Unit Operating Conditions

This sampling program was undertaken as a compliance test program for the new scrubber system on the asphalt batch during representative load operating conditions. In the execution of this program, all applicable operation conditions were referenced.

Operating conditions were monitored throughout the duration of the sampling program by Highway Materials personnel.

6.4 Emissions

6.4.1 Particulate

The reported particulate emissions as summarized in Table 1 are expressed as a concentration (grains/ACF, and grains/SCF) and emission rate (lbs/hour) as measured. The particulate emissions for all three runs are within any applicable limitations.

6.4.2 Visible

The reported visible emissions as summarized in Table 1 are expressed as a percent (%). The visible emissions for all three runs are within any applicable limitations.

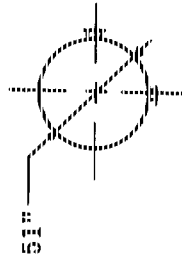
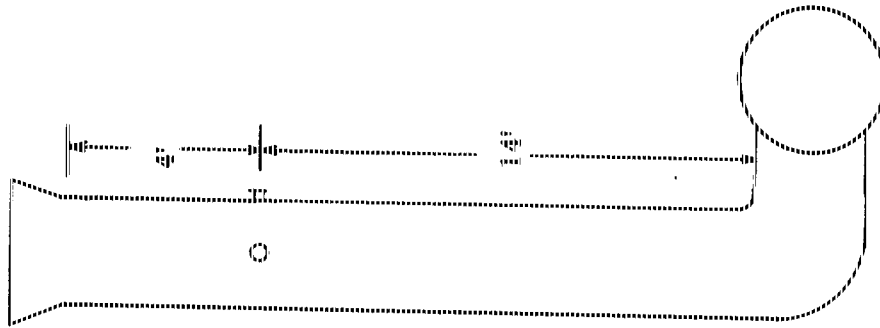


Figure 1
 Sample Pore and Traverse Path Locations
 Asphalt Batch Plant
 Highway Materials, Inc.
 Plymouth Meeting, PA
 C/O, Inc. W.O. 10-000-000-1

Sample No.	Distance From Top, inches
1	1.07
2	2.42
3	3.53
4	3.83
5	3.75
6	1.16
7	3.34
8	3.53
9	1.37
10	2.33
11	2.15
12	2.33
13	2.33

SECTION III
APPENDICES

SECTION III - APPENDICES

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7. Calibration Data
8. Computer Printout
(Flue Gas Characteristics, Isokinetic Calculations, and Test Results
for Particulate Emissions)
9. Sample Calculations

APPENDIX 1
PROJECT PARTICIPANTS

APPENDIX I
PROJECT PARTICIPANTS

The following members of Gilbert/Commonwealth's staff participated in the planning and execution of this project and preparation of this report.

Field Sampling Crews:

Dave Hofmann
Ed Burger
Don Wary

Project Coordinator
Engineering Technician
Engineering Technician

Laboratory Participants:

Carl J. Wummer
Vaughan O'Neill

Chemist
Laboratory Technician

All field tests were completed with the assistance of technical personnel from Highway Materials and witnessed by the PADER.

APPENDIX 2

TESTING AND ANALYTICAL PROCEDURES

2.2 ACTUAL SAMPLING PROCEDURES/PARTICULATES

APPENDIX 2

TESTING AND ANALYTICAL PROCEDURES

2.2 ACTUAL SAMPLING PROCEDURES/PARTICULATES

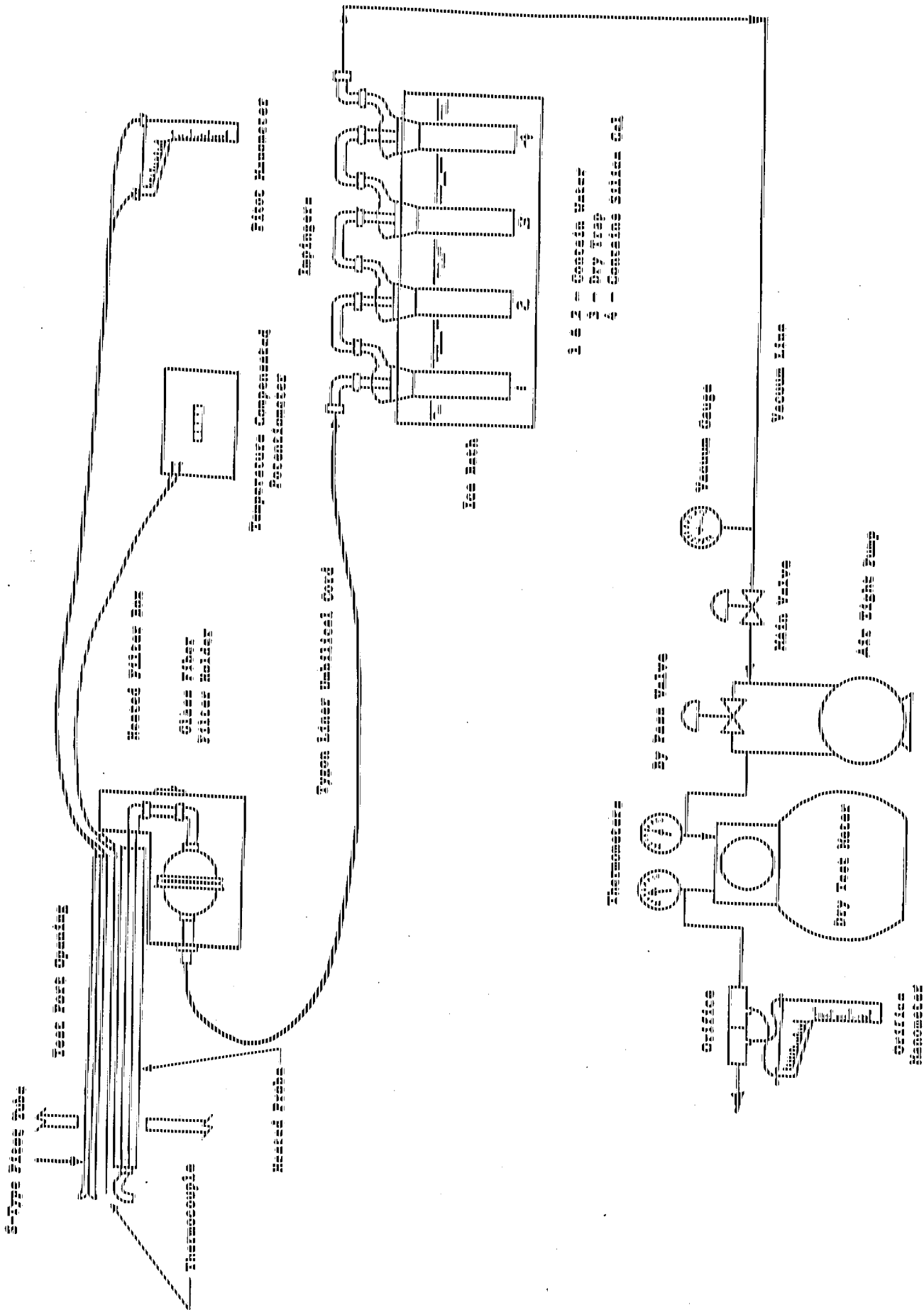
Particulate matter in the exhaust flue gas stream at the stack sampling location was sampled according to procedures and type of equipment as basically described in EPA Method 5 (see Appendix 2.1 for a complete description).

In place of the fragile glass material, the in-stack probe liner was constructed of high corrosion resistant Inconel stainless steel, which was enclosed in an outer protective sheath and heat traced to minimize condensation within the probe.

The basic test train consisted of a stainless steel nozzle followed by a heated Inconel probe liner, heated glass fiber filter, and glass impingers with all glass connectors.

The required sampling time for the compliance test, in terms of time per traverse point and overall sampling time per individual test run, was selected on the basis of maintaining a minimum sampling time of 4.5 minutes during the first test and 3 minutes for the last two tests at each of the traverse points at each sampling location.

The test program was completed with one test train located at the stack. All sampling activities were halted in the event of any test equipment malfunction or at the report of any operational problem. There was no planned interruption or extensive delay during the completion of the test runs.



APPENDIX 2

TESTING AND ANALYTICAL PROCEDURES

2.3 ANALYTICAL METHODS/PARTICULATES

APPENDIX 2

TESTING AND ANALYTICAL PROCEDURES

2.3 ANALYTICAL METHODS/PARTICULATES

The reported particulate emissions included the total particulate catch from the acetone wash of the nozzle and probe, plus accumulations on the glass fiber filter. The impinger water was filtered through a .22 micron filter. These results along with the probe wash and glass fiber filter are considered particulate emissions in the Commonwealth of Pennsylvania.

The soluble water from the impingers was dried down and weighed. This particulate weight is only reported and is not counted toward the particulate weight.

In the clean-up of the front half of the sampling equipment, the nozzle from the front of the probe was removed, brushed out, and washed with acetone. The probe liner was then brushed out and washed with water then acetone. All of the acetone wash solutions for the probe and filter holder were combined into a single sample for analysis. The glass fiber filter was removed from the fritted disc of the filter holder and replaced in its petri dish. All adhering filter particles were removed from the silicone rubber gasket and placed in the same petri dish prior to sealing for transport back to the Gilbert assigned laboratory for final analysis.

The clean-up procedure for the back half of the sampling train initially involved removal of the silica gel from the last impinger and replacement in its original container for final weighing to determine moisture pickup. Water collected in the impingers and glass connectors were rinsed with water then acetone. This rinse was also placed in sample bottles to be analyzed.

Laboratory analysis of samples collected during the test run proceeded according to EPA Method 5 (Appendix 2.1).

All critical items of sampling or analytical equipment were certified and/or calibrated for accuracy and results considered within acceptable limits for source sampling operations (see Appendix 7).

APPENDIX 3
OPERATING DATA

OPERATING DATA

Run No. 1

<u>Time</u>	<u>Minutes</u>	<u>Weight</u>	<u>Tons</u>	<u>Tons/Minute</u>
1032-1037	5	55,849	27.9	5.58
1235-1250	15	175,980	87.9	5.86
1250-1252	2	23,356	11.7	5.84
1256-1259	3	68,174	34.1	5.68
1259-1311	11	132,740	66.4	6.04
Average				5.8

Run No. 2

0804-0811	7	94,695	47.3	6.76
0811-0824	13	126,313	63.2	4.86
-0857	13	180,246	90.1	6.01
0857-0903	6	59,782	29.9	4.98
0903-0911	7	65,999	33.0	4.71
-1010	8	93,670	46.8	5.85
1010-1026	16	176,337	88.2	5.51
1026-1028	2	23,540	11.77	5.89
Average				5.57

Run No. 3

<u>Time</u>	<u>Minutes</u>	<u>Batch Weight</u>	<u>Tons</u>	<u>Tons/Minute</u>
1235	4	43,875	21.9	5.48
1240	4	43,875	21.9	5.48
1245	4	43,818	21.9	5.48
1249	4	43,958	22.0	5.50
1253	4	44,117	22.1	5.53
1257	4	43,607	21.8	5.45
1301	4	44,030	22.0	5.50
1305	4	43,938	22.0	5.50
1310	4	44,464	22.2	5.55
1317	4	44,001	22.0	5.50
1340	4	43,923	22.0	5.50
1346	4	44,248	22.1	5.53
1352	4	43,888	21.9	5.48
1356	4	43,894	21.9	5.48
1401	4	43,910	22.0	5.50
1406	4	43,891	21.9	5.48
1411	4	43,969	22.0	5.50
Average				5.50

APPENDIX 4
ANALYTICAL RESULTS FOR PARTICULATES
(CLEAN-UP SHEETS)

GILBERT ASSOCIATES, INC.
AIR POLLUTION CONTROL DEPT.
ANALYZE CLEAN UP AND REPORT FORM

Run Date: 12/22/80 Client: Highway Materials Inc
 Run No.: 114 W. O. No.: 10-2559-900
 Sample Run No.: _____ Plant: Plongin Machine
 Operator: CSH Sampling Location: Stack

ANALYSIS

Diablo-Accesor Wash
 Probe, Diablo Holder, Cyclone (By-pass),
 Flank, Press Half Filter Holder-Accesor Wash

Lab No. 67366-1
 Lab No. 4366-1

Laboratory Results

Residue: 2.5
 Residue: 5.0

Sample No.	Lab. No.	Residue, mg/m ³
.....		
.....		
.....		
.....		

Diablo particulate weight:

Sample No.	Lab. No.	Residue, mg/m ³
.....		
.....		
.....		
.....		

Filter particulate weight:

PROB. HALF Sub Total:

ANALYSIS

Endpaper, Connect and Motor Wash of Endpaper
 Connectors and Back Half of Filter Holder

Lab No. 67366-1 Rubber-Chloroform
 Extract:

Collected on 0.22µ Filter:

Aqueous Residue:

Endpaper, Connectors and Back Half of
 Filter Holder - Accesor Wash

Lab No. 67366-1 Residue:

BACK HALF Sub Total:

SPECIAL WEIGHT:

ANALYSIS

Amount: 150
3.50
1.50

Final Volume: 6.22
 Initial Volume: 3.00
 Net Volume: 3.22

ANALYSIS

Weight after test: 2.5

Weight before test: 2.2

Net Weight: 0.3

Gravimetric No.: 1. 1.37 2. 3. 4.

SPECIAL WEIGHT-Filter Gas:

SPECIAL VOLUME, Endpaper:

TOTAL WEIGHT:

Comments:

LAB: DATE RECEIVED 12/28/80
 DATE REPORTED 1/14/81

CLASNO : Disposal Material
W. O. No.: LA-976-SOC
PLANT : Plants Dept.
Sampling Location: Shed

Hochdruck-Asacont-Abzug
 Probe, Thimble Holder, System (Geymann).
 Probe, Probe Halber Plate Holder-Asacont-Abzug

11/11/11

Lab No. 4366-9
Lab No. 4366-9

Juan Salame $\frac{2046}{23}$ m
 Juan Salame $\frac{205}{25}$ m

Figure 1 consists of nine bar charts arranged in a 3x3 grid. The columns are labeled 'Male', 'Female', and 'Unknown' from left to right. The rows are labeled '0-4', '5-9', and '10-14' from top to bottom. Each chart has a horizontal axis for the number of children (0 to 10) and a vertical axis for the percentage of families (0 to 100). The 'Unknown' column shows a high concentration of families with 0 or 1 child, while the 'Male' and 'Female' columns show a more varied distribution across the number of children.

"This noble pursuit costs nothing."

182.000 perpendiculaire van die 182.400

HOUSE RAMP Sub Total 14.3

Triploggers' Consensus and Water Bank of Triploggers Consensus.com and Dock Build of PLTing Holder

Lab. No. 60368-2 Chinese-Chow Loon
Address: DE

Collected on 0.33u PSLCnr 39.4

Admission Report: Admission Report

**Impinger, Connors and Buck Build of
Polaroid Holder - Acetone Wards**

Lab No. 6366-2 296

BACK DROP Sub Total. 330.00

TOTAL WEIGHT 350.5 gm

240
786
921

Final Volume 547

Instal. Volume 300

Doc: Vietnam 3247

Weight after cover 255

Weight before conc: 220

25

Page: 11049000

Concentration No.: A, _____ B, _____ C, _____ D, _____

TOTAL WEIGHT - 25.00 g.

TOTAL. UNCLASSIFIED... 267

TELEPHONE: 397

Comment 2

DATE RECEIVED 10/26/80
DATE IMPROVED 11/6/80

NET/4PC: 1.2.0.74

MAURICE GOLDBE

Run Date: 10/23/87
Run Date: 11/1/87
Sample Run Date:
Operator: DH
Client: Highway Materials
T. C. No.: 15-0785-000
Place: Phoenix, Arizona
Sampling Location: Stage 1

Non-Resonant Wind (b)
 Push, Double Holder, Spine (Oppen)
 Push, Double Holder, Spine (Oppen)

Lab No. 4366-3
Lab No. 4366-3

Ingreso 200
 Ingreso 200

Thiobalbin (p-nitrobenzoate) weightage

Elongation.....	Modulus.....	Shrinkage.....
6% - 115%	76 - 3669	-3
.....		
.....		
.....		
.....		

Please purchase the 10, 30

PROCURE METHOD Sub: Travel 11.7

**Empire: Contain and Wagon Wheel of Empire
Cannons and Buck Ball of Empire**

Lab. No. 4366-3 Heber-Gleason
 Extract

Collected on 0-22m Water 84.4.1964

Agreement: Indefinite 25,9

Lab No. 6366-3 Date due 24 Feb 1966

BACK SLAP (See) Throat 359

TOTAL WEIGHT: 369.64

Impinger, Connors and Bock Half of
FBI's Half of a Decade Ago

Initial Volume	23.5
Final Volume	58.1
Initial Volume	32.9
Final Volume	26.1

Weight after cure: 2.58
 Weight before cure: 2.32
 Net Weight: 4.1
 Container No.: 44434 4.

TOTAL DIRECT-ELICA Gel 56

TOTAL, WORKSHEET: 231

TOTAL MEASURE: 397

LEAD: DATE RECEIVED 10/28/86
DATE IMPROVED 11/2/86

MPL/APC 1.2/16

ALL INFORMATION CONTAINED

APPENDIX 5
RAW FIELD DATA

Sheet 1 of 2

Client

Highway Materials

W. O. No.

10-0500-000

Plant

Plymouth Meeting

Run No.

114-1

Location

Stack

Date

10/21/86

Operator

McLean

Sample Box No.

Meter Box No.

1386

Meter/Min

2.15

C Factor

PARTICULATE FIELD DATA

VERY IMPORTANT - FILL IN ALL BLANKS

Read and record at the start of each test point

SKETCH

Pitot Calibration 0.84

Thimble No.

Filter No.

Ambient Temp. °F

Bar. Press. "Hg

Assumed Moisture %

Heater Box Setting, °F

Probe Tip Dia., in.

Probe Length

Probe Heater Setting

Avg. ΔP

Avg. ΔH

A
1 15
2 1.1
3 1.3
4 1.33
5 1.31
6 1.39
7 1.17
8 1.18
9 1.30
10
11
12

299.9
10
11
12

POINT	DISTANCE IN INCHES	CLOCK TIME	ACTUAL RUN	DRY GAS METER, CF	PITOT IN. H ₂ O ΔP	ORIFICE A H IN. H ₂ O		DRY GAS TEMP. OF		PUMP VACUUM IN. Hg GAUGE	BOX TEMP. OF	INFINGER TEMP. OF	STACK PRESS. IN. Hg	STACK TEMP. OF
						DES. 1	ACTUAL	INLET	OUTLET					
AV	1033	0.0	970.77		0.62	2.60	2.00	78	69	7.0	7.0			224
1	45	9.0	977.2		0.62	1.86	1.80	84	70	7.0	7.0	75		236
2	90	18.0	970.9		0.74	2.40	2.20	80	70	1.0	235	75	9.5	205
3	135	27.0	983.6		0.75	3.40	3.20	82	70	4.5	180	70	11.7	222
4	180	36.0	977.6		1.00	3.50	3.50	80	70	9.0	200	70	13.9	232
5	225	45.0	942.1		1.01	2.70	2.70	80	76	3.0	275	70	13.4	243
6	270	54.0	996.7		1.00	4.10	4.70	82	80	5.0	275	70	15.2	250
7	315	63.0	1000.8		1.10	4.10	4.10	80	84	6.0	275	70	14.9	246
8	360	72.0	1051.0		1.10	3.70	3.90	80	84	7.0	285	70	15.5	245
9	405	81.0	750.0		1.30	4.80	4.80	82	89	17.0	285	72	15.0	266

Comments:

1044.8 m/s
1159.9 m/s

3.6 15.5
2.3 14.5

5.2 13.7
4.5 14.7

Stack-772

107/6 m/s

10.0 m/s

7:00 wind 4.5 m/s
7:30 wind 4.5 m/s

0.61

Client Longway AvePARTICULATE FIELD DATA
(continued)Sheet 2 of 2W.O. No. 10-0500-000Plant Phosphate MchineryLocation StackRun No. A#4-1Date 10/22/86

POINT	DISTANCE IN INCHES	CLARK TIME ACTUAL RUN	DRY GAS METER, CF	PILOT IN. H ₂ O ΔP	ORIFICE ΔH IN. H ₂ O		DRY GAS TEMP. OF		PUMP VACUUM IN. HG GAUGE	BOX TEMP OF	FIRING TEMP OF	STACK PRESS IN. HG	STACK TEMP. OF
					DESIRED	ACTUAL	INLET	OUTLET					
Am		19.5		1.30	4.80	4.80	120.	90.	13.0	275	70		266.
Stack		540	1020320										
B1		1252.	1020320	0.52	190	190	102.	90.	1.0	270.	72		250.
1		45	10237	0.53	190	190	102.	90.	1.0	275.	72	11.1	255.
2		00	10272	0.65	240	240	110.	90.	1.0				
3		135	1030.8	0.62	225	225	110.	90.	1.0	265	70	14.3	269.
4		180	10343	0.65	240	240	110.	90.	1.0	265	70	10.1	275.
5		225	10380	0.65	240	240	108.	90.	1.0	260	70	13.7	295.
6		270	10415	0.85	300	300	111	90.	1.0	260	70	14.2	295.
7		315	10452	0.97	350	350	112.	92.	1.0	265	70	14.7	297.
8		360	10490	1.00	370	370	120.	92.	1.0	265	70	15.0	299.
9		405	10541	0.97	360	360	122.	93.	1.0	260	70	14.7	277.
10		450	10587	0.96	370	370	122.	94.	1.0	260	65	15.0	259.
11		495	10632	1.00	370	370	122.	95.	1.0				259.
Stack		540	1067584										

COMMENTS:

1800' broken pipe static - 55
1218.

Leak 0.015 @ 12" Hg

PARTICULATE FIELD DATA

Client

Highway Project

W. O. No.

10-0000-000

Plant

Phosphate Mining

Run No.

14-2

Location

Spade

Date

10/23/68

Operator

160 m m m

Sample Box No.

5

Master Box No.

1084

Master

1084

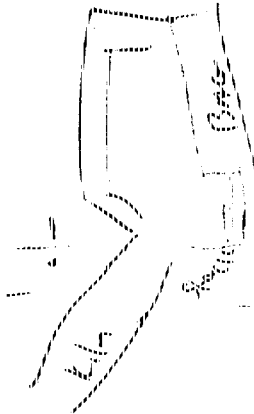
Factor

1084

VERY IMPORTANT - FILL IN ALL BLANKS

Read and record at the start of each test point

SWITCH



1084

Pitot Calibration 0.04

Thimble No.

Filter No.

Ambient Temp. °F

Bar. Press. "Hg

Assumed Moisture %

Heater Box Setting, °F

Probe Tip Dia., in.

Probe Length

Probe Heater Setting

Avg. ΔP

Avg. ΔH

POINT	DISTANCE IN INCHES	CLOCK TIME	DRY GAS RUN WATER, CF	PITOT IN. H ₂ O ΔP	ORIFICE Δ H IN. H ₂ O		DRY GAS TEMP. °F		PUMP VACUUM IN. HG GAUGE	BOX TEMP. °F	INFINGER TEMP. °F	STACK PRESS. IN. HG	STACK PLATE TEMP. °F
					DESIRED	ACTUAL	INLET	OUTLET					
1	0.00	0.00	68.230	0.02	2.50	2.50	60	55	8.0	225	58	14.6	252
2	3.0	10.4	70.4	0.79	2.80	2.80	60	55	8.0	230	58	14.3	253
3	6.0	72.8	72.8	0.79	2.75	2.75	74	58	8.5	250	60	13.0	259
4	9.0	73.1	73.1	0.82	2.60	2.60	82	60	9.0	255	60	12.2	260
5	12.0	77.4	77.4	0.90	2.80	2.80	85	60	9.0	260	61	12.8	262
6	15.0	79.9	79.9	0.95	2.90	2.90	92	60	11.0	260	62	14.4	274
7	18.0	82.2	82.2	0.94	2.90	2.90	95	62	11.0	260	62	14.2	278
8	21.0	84.5	84.5	0.96	3.30	3.30	80	64	12.0	275	65	17.3	281
9	24.0	87.1	87.1	1.00	4.10	4.10	92	64	13.0	275	65	17.3	283
10	27.0	90.9	90.9	1.10	3.80	3.80	98	65	18.5	260	65	18.5	284
11	30.0	92.6	92.6	1.10	3.80	3.80	102	66	18.5	260	65	18.1	286

Comments:

Box 14 - 402 m m m 3743

4.2 13.8

4.2 14.2

Static

- 779

* changed from graph

2037 544
10832
10836

Sheet 1 of 2

Client Hickory Associates

W. O. No. 10-0500-008

Plant Plymouth Meeting

Run No. HAM-3

Location Smoke

Date 10/23/66

Operator McMurry

Sample Box No.

Water Box No. 1386

Water/AB

C Factor 7.15

PARTICULATE FIELD DATA

VERY IMPORTANT - FILL IN ALL BLANKS

Read and record at the start of each test point

STATION

Pitot Calibration 0.84

Thimble No. 8115

Filter No.

Ambient Temp. °F

Bar. Press. "Hg 29.81

Assumed Moisture %

Heater Box Setting, °F

Probe Tip Dia., in. 0.160

Probe Length

Probe Heater Setting

Avg. ΔP Avg. ΔB

POINT	DISTANCE IN INCHES	CLOCK TIME ACTUAL RUN	DRY GAS METER, CF	PITOT IN. H ₂ O ΔP	ORIFICE A B IN. H ₂ O		DRY GAS TEMP. OF		PUMP VACUUM IN. Hg GAUGE	BOX TEMP. °F	REFRIGER TEMP. °F	SPACE STAGE PRESS. IN. Hg OF
					DES. 1	ACTUAL	INLET	OUTLET				
1		1734 0.0	125.587	0.47	1.60	1.60	80.	78.	0	23.0	37	14.7
2		3.0	127.4	0.38	2.00	2.00	84.	78.	2	22.0	37	13.6
3		6.0	129.4	0.62	2.00	2.00	90.	78.	2	22.5	37	13.6
4		9.0	131.5	0.65	2.00	2.00	96.	80.	2	23.5	37	11.8
5		12.0	133.6	0.64	2.00	2.00	100.	80.	2	24.0	37	11.7
6		15.0	135.7	0.66	2.00	2.00	104.	80.	2	24.5	38	12.3
7		18.0	137.8	0.75	2.00	2.00	108.	82.	2.0	24.5	38	13.8
8		21.0	140.0	0.82	2.00	2.00	106.	82.	2	25.0	39	12.0
9		24.0	142.1	0.87	3.00	3.00	112.	85.	2	25.0	39	11.7
10		27.0	144.1	1.20	4.00	4.00	112.	86.	3	25.8	39	12.5
11		30.0	147.4	1.10	3.80	3.80	115.	88.	3.0	24.5	39	12.5

Comments:

5.0 11.7
4.8 12.0
4.0 13.2

- 6 2

10/23/66

PARTICULATE FIELD DATA
(continued)

Client Aluminum

W.O. No. 18-0500-000

Plant Plymouth Aluminum

Location Stack

Run No. HA-3

Date 10/23/84

POINT	DISTANCE IN INCHES	CLOCK TIME ACTUAL RUN	DRY GAS ENTER, CF	PILOT IN. H ₂ O Δ P	ORIFICE Δ H IN. H ₂ O		DRY GAS TEMP. OF		PUMP VACUUM IN. HG GAUGE	BOX TEMP OF	IMFINGER TEMP OF	STACK PRESS IN. HG	STACK TEMP. OF
					DESIRED	ACTUAL	INLET	OUTLET					
12		330	1303	1.20	4.20	4.20	113	85	30	235	60	127	265
81	6	1316	152700	0.40	1.40	1.40	87	80	0	230	60	132	212
2		30	1549	0.65	2.25	2.25	90	81	0	230	60	132	220
3		40	1578	0.67	2.35	2.35	96	81	0	235	61	153	221
4		70	1601	0.64	2.35	2.35	100	81	1	235	61	141	231
5		120	1613	0.68	2.40	2.40	104	82	1	240	62	153	231
6		150	1633	0.68	2.40	2.40	106	82	1	240	62	137	230
7		180	1655	0.94	3.40	3.40	108	84	2	240	62	147	243
8		210	1708	1.05	3.50	3.50	116	86	2	240	62	173	238
9		240	1739	1.20	4.20	4.20	118	86	25	250	62	220	220
10		300	1745	1.30	4.50	4.50	122	90	30	250	62	212	212
11		330	1797	1.30	4.50	4.50	123	91	30	250	63	213	213
12		360	18240										

COMMENTS:

Down limited trucks arrive

Stack 1000 4" H₂

APPENDIX 6
VISIBLE EMISSION DATA

APPENDIX 7
CALIBRATION DATA

METER BOX CALIBRATION

Date 10/28/86

Meter box number 1386

Barometric pressure, $P_b = 29.79$ in Hg

Calibrated by Robert V. OSW

Orifice manometer setting (ΔH), in. H ₂ O	Gas volume		Wet test meter (V_w), cf	Temperatures			Time (θ), min	V_i	ΔH_{oi}
	Wet test meter (V_w), ft ³	Dry gas meter (V_d), ft ³		Dry gas meter					
				Inlet (t_{di}), °F	Outlet (t_{do}), °F	Avg ^a (t_d), °F			
0.5	4.997	5.057	67	98	85.5	91.8	13.33	101	1.04
1.0	5.045	5.054	67	95	84	89.5	9.20	101	1.18
1.5	10.022	10.112	67	101.5	83	92.3	15.22	103	1.19
2.0	9.995	9.913	70.5	95.5	79.5	85	13.65	103	1.21
3.0	11.002	11.144	67	105	88	96.5	12.65	101	1.43
4.0	9.997	10.075	70.5	102	78	90	10.30	102	1.49
5.0	10.000	10.127	70.5	101.5	82	95.8	8.65	102	1.51
Avg 1.03									

$$\Delta H = \frac{H}{13.6} \quad V_i = \frac{V_w P_b (t_d + 460)}{V_d (P_b + \frac{\Delta H}{13.6}) (t_w + 460)}$$

0.5	0.0368	$V_i = \frac{4.997 \times 29.79 \times 559.8}{5.057 \times 29.79 \times 559.8} = 1.03$
1.0	0.0711	$V_i = \frac{5.045 \times 29.79 \times 559.8}{5.054 \times 29.79 \times 55.9} = 1.03$
1.5	0.110	$V_i = \frac{10.022 \times 29.79 \times 551.3}{10.112 \times 29.79 \times 55.9} = 1.03$
2.0	0.147	$V_i = \frac{9.995 \times 29.99 \times 575}{9.913 \times 29.99 \times 575.5} = 1.03$
3.0	0.221	$V_i = \frac{11.002 \times 29.79 \times 556.5}{11.144 \times 29.79 \times 52.9} = 1.01$
4.0	0.29	$V_i = \frac{9.997 \times 29.99 \times 550}{10.075 \times 29.99 \times 570.5} = 1.02$

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NO.

PAGE

8P

DESIGNED BY

G. B. GALT

DATE 10/22/86

REVIEWED BY

G. B. GALT

DATE

SYSTEM

EXPLANATION FOR

AH Box 1386

AH	$Q_{max} = \frac{K_m (P_{h1} - P_{h2})}{(P_{h1} - P_{h2}) + (P_{h2} - P_{h3})}$	$K_m = Q_m \sqrt{\frac{(P_{h1} - P_{h2})}{(P_{h2} - P_{h3}) (AH)^3}}$	AH = 0.231
0.5	$Q_{max} = \frac{5.059 (595.5)}{(4.53) (595.5)} = 0.433$	$K_m = 0.378 \sqrt{\frac{29.79 (2.9)}{(0.5) (0.231)^3}} = 0.622$	AH = 0.231
1.0	$Q_{max} = \frac{5.059 (595.5)}{(4.53) (595.5)} = 0.433$	$K_m = 0.378 \sqrt{\frac{29.79 (2.9)}{(1.0) (0.231)^3}} = 0.650$	AH = 0.231
1.5	$Q_{max} = \frac{5.059 (595.5)}{(4.53) (595.5)} = 0.433$	$K_m = 0.378 \sqrt{\frac{29.79 (2.9)}{(1.5) (0.231)^3}} = 0.678$	AH = 0.231
2.0	$Q_{max} = \frac{5.059 (595.5)}{(4.53) (595.5)} = 0.433$	$K_m = 0.378 \sqrt{\frac{29.79 (2.9)}{(2.0) (0.231)^3}} = 0.685$	AH = 0.231
3.0	$Q_{max} = \frac{5.059 (595.5)}{(4.53) (595.5)} = 0.433$	$K_m = 0.378 \sqrt{\frac{29.79 (2.9)}{(3.0) (0.231)^3}} = 0.696$	AH = 0.231
4.0	$Q_{max} = \frac{5.059 (595.5)}{(4.53) (595.5)} = 0.433$	$K_m = 0.378 \sqrt{\frac{29.79 (2.9)}{(4.0) (0.231)^3}} = 0.702$	AH = 0.231
5.0	$Q_{max} = \frac{5.059 (595.5)}{(4.53) (595.5)} = 0.433$	$K_m = 0.378 \sqrt{\frac{29.79 (2.9)}{(5.0) (0.231)^3}} = 0.708$	AH = 0.231

G. B. GALT

METER BOX CALIBRATION

Date 10/20/96

Meter box number 1386

Barometric pressure, $P_b = 30.15$ in Hg

Calibrated by BURGER 100W

Orifice manometer setting (ΔH), in. H ₂ O	Gas volume		Wet test meter (t_w), °F	Temperatures			Time (θ), min	Y_i	ΔH_{ci}
	Wet test meter (V_w), ft ³	Dry gas meter (V_d), ft ³		Dry gas meter					
				Inlet (t_{di}), °F	Outlet (t_{do}), °F	Avg ^a (t_d), °F			
0.5	5.0	5.105	68	88	78	83	13.22	1.01	1.93
1.0	5.25	5.359	68	92	79	88	10.05	1.01	2.97
1.5	10.0	10.151	69	94	81	87.5	16.0	1.02	3.17
2.0	10.0	10.213	69	107	84	95.5	13.9	1.02	2.21
3.0	11.25	11.604	69	110	86	98	13.38	1.02	2.40
4.0	10.0	10.44	69	114	88	101	10.43	1.01	2.41
953.614								Avg 1.01	

$$\Delta H \quad \frac{H}{13.6} \quad Y_i = \frac{V_w P_b (t_d + 460)}{V_d (P_b + \frac{\Delta H}{13.6}) (t_w + 460)}$$

0.5	0.0368	$Y_i = \frac{5.0 \times 30.15 \times 573}{5.105 \times 30.17 \times 523} = 1.01$
1.0	0.0732	$Y_i = \frac{5.25 \times 30.15 \times 578}{5.359 \times 30.22 \times 528} = 1.01$
1.5	0.110	$Y_i = \frac{10.0 \times 30.15 \times 577.5}{10.151 \times 30.26 \times 529} = 1.02$
2.0	0.147	$Y_i = \frac{10.0 \times 30.15 \times 563.5}{10.213 \times 30.30 \times 529} = 1.02$
3.0	0.221	$Y_i = \frac{11.604 \times 30.15 \times 558}{11.604 \times 30.37 \times 529} = 1.02$
4.0	0.19	$Y_i = \frac{10.0 \times 30.15 \times 561}{10.44 \times 30.44 \times 529} = 1.01$

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ENGINEER

RUPPER

DATE 10/20/86

REVIEWED BY

O.B.W.

DATE

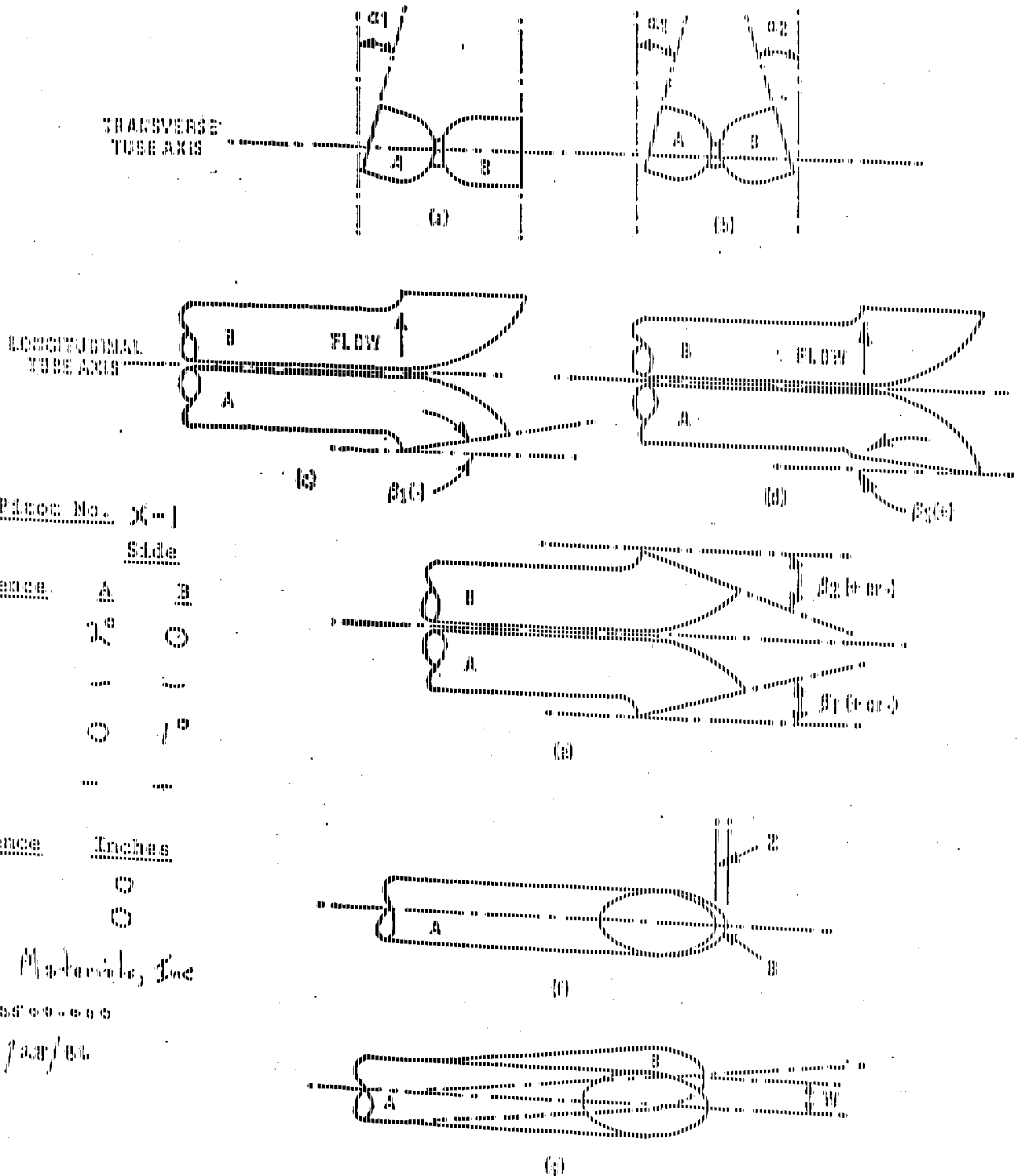
SYSTEM

COLLECTION FOR

 ΔH Box 1386

ΔH	$Q_{\text{min}} = \frac{Q_{\text{max}} (C_{\text{min}})^{1.91}}{C_{\text{min}} (C_{\text{max}})^{0.91}}$	$K_{\text{min}} = Q_{\text{min}} \sqrt{\frac{(P_{\text{min}})^{1.91}}{(C_{\text{min}})^{0.91} (K_{\text{max}})^{1.91}}}$	$\Delta H = \frac{Q_{\text{min}}^2}{(K_{\text{min}})^2}$
0.5	$Q_{\text{min}} = \frac{5105 (539)}{1372 (545)} = 383$	$K_{\text{min}} = 313 \sqrt{\frac{20.15 (2.9)}{598 (0.5)} = 691}$	$\Delta H = \frac{Q_{\text{min}}^2}{(K_{\text{min}})^2} = 1.93$
1.0	$Q_{\text{min}} = \frac{5359 (539)}{1205 (545)} = 524$	$K_{\text{min}} = 524 \sqrt{\frac{20.15 (2.9)}{539 (1.0)} = 667}$	$\Delta H = \frac{Q_{\text{min}}^2}{(K_{\text{min}})^2} = 2.07$
1.5	$Q_{\text{min}} = \frac{10151 (541)}{1600 (545)} = 627$	$K_{\text{min}} = 627 \sqrt{\frac{20.15 (2.9)}{291 (1.5)} = 651}$	$\Delta H = \frac{Q_{\text{min}}^2}{(K_{\text{min}})^2} = 2.17$
2.0	$Q_{\text{min}} = \frac{10213 (541)}{1359 (545)} = 720$	$K_{\text{min}} = 72 \sqrt{\frac{20.15 (2.9)}{549 (2.0)} = 695}$	$\Delta H = \frac{Q_{\text{min}}^2}{(K_{\text{min}})^2} = 2.21$
3.0	$Q_{\text{min}} = \frac{11604 (546)}{1338 (545)} = 949$	$K_{\text{min}} = 949 \sqrt{\frac{20.15 (2.9)}{546 (3.0)} = 620}$	$\Delta H = \frac{Q_{\text{min}}^2}{(K_{\text{min}})^2} = 2.40$
4.0	$Q_{\text{min}} = \frac{10744 (548)}{1045 (545)} = 978$	$K_{\text{min}} = 978 \sqrt{\frac{20.15 (2.9)}{548 (4.0)} = 618}$	$\Delta H = \frac{Q_{\text{min}}^2}{(K_{\text{min}})^2} = 2.41$

FILING
CODE



Highway Materials, Inc

10-5500-000

10/28/86

Figure 2-3. Types of face-opening misalignment that can result from field use or improper construction of Type S pitot tubes. These will not affect the baseline value of $C_p(s)$ so long as α_1 and $\alpha_2 < 10^\circ$, β_1 and $\beta_2 < 5^\circ$, $z < 0.32$ cm (1/8 in.) and $w < 0.08$ cm (1/32 in.) (citation 11 in Section 6).

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Highway Materials, Inc.

PROJECT

Asphalt Baghouse

FILING CODE

100500000

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PAGE

REVISION

DATE 10/28/81

REVIEWED BY

CATH

SYSTEM

CALIBRATION FOR

Pot Meter-Thermocouple Calibration

Pot Meter #

1

Thermocouple Type

K

Ice Bath Temperature °F

34

Certified Mercury Bulb °F

34

Ambient Temperature °F

81

Certified Mercury Bulb °F

81

Boiling H₂O °F

211

Certified Mercury Bulb °F

211

Hot Synthetic Oil °F

400

Certified Mercury Bulb °F

400

Remarks:

100500000

APPENDIX B
COMPUTER PRINTOUT
(FLUE GAS CHARACTERISTICS, ISOKINETIC CALCULATIONS,
AND TEST RESULTS FOR PARTICULATE EMISSIONS)

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APPENDIX 9
SAMPLE CALCULATIONS

SAMPLE CALCULATIONS

Particulate Isokinetic Sampling

I. Calculations for stack volume and Isokinetic Ratio

Time	Dry Gas Meter Ft ³	Pitot ΔP , In. H ₂ O	Orifice ΔH , In. H ₂ O	Dry Gas Temp °F		Stack Static Pressure In. H ₂ O	Stack Temp °F
T	VM	ΔP	PM	TMI	TMO	PST	TS

1. DN = Nozzle Diameter, inches

2. PB = Barometric Pressure, inches Hg

3. TT = Net Sampling Time, minutes

4. VM = VM final - VM initial = Sample Gas Volume, ft³

5. TM = Average Dry Gas Temperature at Meter, °F

$$TM = \frac{AVG. TMI + AVG. TMO}{2}$$

6. PM = Average Orifice Pressure Drop, inches H₂O

$$PM = Avg. \Delta H$$

7. Volume of dry gas sampled at standard conditions^a, DSCF

$$VMSTD = \frac{17.65 \times VM \times Y \left(\frac{BP + PM}{13.6} \right)}{(TM + 460)}$$

8. VW = Total Water Collected = gm H₂O Silica gel + ml Imp. H₂O = ml

9. Volume of water vapor at standard conditions^b, SCF

$$VW_{gas} = 0.0471 \times VW = SCF$$

10. Percent moisture in stack gas

$$\% M = \frac{100 \times VW_{gas}}{VM STD + VW_{gas}}$$

11. Mole fraction of dry gas

$$MD = \frac{100 - \%M}{100}$$

12. Molecular weight of dry stack gas

$$MWD = (\%CO_2 \times \frac{44}{100}) + (\%O_2 \times \frac{32}{100}) + \left[(\%CO + \%N_2) \times \frac{28}{100} \right]$$

$$12A. \%EA = \% \text{ Excess Air} = \frac{[(\% O_2) - 0.5 (\%CO)]}{0.264 (\%N_2) - [(\%O_2) + 0.5 (\%CO)]} \times 100$$

13. Molecular weight of wet stack gas

$$MW = MWD \times MD + 18 (1 - MD)$$

14. AS = Stack Area, square inches

15. PS = Stack Pressure, inches Hg

$$PS = PB \pm \text{Avg. PST}$$

$$\text{NOTE: PST in. Hg.} = \frac{\text{PST in. H}_2\text{O}}{13.6}$$

16. TS = Average Stack Temperature, °F

$$TS = \text{Average TS}$$

17. SDE = Average
- $\sqrt{\text{Velocity Head } (\Delta P) \times (\text{Stack Temperature} + 460)}$

(Calculated each line)

$$SDE = \text{Avg } \sqrt{\Delta P \times (TS + 460)}$$

18. Stack gas velocity at stack conditions, fpm

$$VS = 5130 \times Cp \times \text{Avg}(SDE) \times \left[\frac{1}{PS \times MD} \right]^{1/2} = \text{FPM} \quad \begin{array}{l} Cp = \text{pitot tube} \\ \text{coefficient} \end{array}$$

19. Stack gas volumetric flow rate at standard conditions
- ^c
- , DSCFM

$$Q_s = \frac{0.123 \times VS \times AS \times MD \times PS}{(TS + 460)} = \text{DSCFM}$$

20. Stack gas volumetric flow rate at stack conditions, ACFM

$$Q_a = \frac{0.05667 \times Q_s \times (TS + 460)}{PS \times MD} = \text{ACFM}$$

21. Percent isokinetic

$$\%I = \frac{1.032 \times (TS + 460) \times VMSTD}{VS \times TI \times PS \times MD \times (DN)^2}$$

NOTES: ^aDry standard cubic feet at 69°F, 29.92 in. Hg.

^bStandard conditions at 68°F, 29.92 in. Hg.

^cDry standard cubic feet per minute at 68°F, 29.92 in. Hg.

II. Calculations for grain loading and emission rates

22. Particulate, gr/DSCF

$$\text{gr/DSCF} = 0.0154 \times \frac{\text{mg}}{\text{VMSTD}}$$

23. Particulate at stack conditions, gr/ACF

$$\text{gr/ACF} = \frac{17.65 \text{ gr/DSCF} \times \text{PS} \times \text{MD}}{(\text{TS} + 460)}$$

24. Particulate, lb/hr conc. method

$$\text{lb/hr} = 0.00857 \times \text{gr/DSCF} \times \text{QS}$$

25. Particulate lb/hr area method = $0.132 \times \frac{\text{gms particulate} \times \text{AS}}{\left(\frac{\text{DN}^2}{2} \right) \times \text{TT}}$

26. Particulate, combustion

$$\frac{\text{lb/hr}}{10^6 \text{ BTU/hr}}$$

27. Particulate, process lb/ton

$$\text{lb/ton} = \frac{\text{lb/hr}}{\text{tons/hr}}$$

28. Particulate, lb/MMBTU, F-Factor Method =

Using O₂ =

$$\frac{0.0154 \times \text{mg} \times \text{F-Factor} \times 20.9}{7000 \times \text{VMSTD} \times (20.9 - \% \text{O}_2)}$$

Using CO₂:

$$\frac{0.0154 \times \text{mg} \times \text{F-Factor} \times 100}{7000 \times \text{VMSTD} \times \% \text{CO}_2}$$

29. F-Factor, dscf/mmBtu

O₂ Format:

$$\text{F-Factor} = \frac{10^6 (3.64 (\% \text{H}) + 1.53 (\% \text{C}) + 0.57 (\% \text{S}) + 0.14 (\% \text{N}) - 0.46 (\% \text{O}_2))}{\text{GCV}}$$

CO₂ Format:

$$\frac{10^6 (0.321) (\% \text{C})}{\text{GCV}}$$