

Note: This is a reference cited in *AP 42, Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at www.epa.gov/ttn/chief/ap42/

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APPENDIX K

OEPA STACK TEST REVIEW SUMMARY FORM

APPLICATION NUMBER 08-1448 P002 0857071296
 FACILITY NAME WEIDLE SAND & GRAVEL
 SOURCE DESCRIPTION (OR SCC CODE) 120 TPH ASPHALT BATCH PLANT
 CONTROL EQUIPMENT FABRIC FILTER BAGHOUSE

DATE(S) OF TEST 5/25/94
 FINAL TEST REPORT RECEIVED ON 6/24/94
 POLLUTANT(S) TESTED PARTICULATE
 TEST METHOD M5
 TEST FIRM PES. JWA 8/8/94

EMISSION RATES*:
 ACTUAL (~~lb~~ ^g/hr) 1.795 $\times 10^{-3}$ g/dscf ALLOWABLE** 0.04 g/dscf

OPERATING RATES*:
 DURING TEST** 80.03 TPH* MAXIMUM** 84.86 TPH

EMISSION FACTOR***

COMMENTS: RUN #2 ONLY COLLECTED 26.012 CU.FT. OF STACK GAS. SUBPART J REQUIRES AT LEAST 31.8 DSCF. RUN #2 HAS BEEN DISCARDED AND THE AVERAGE OF RUNS #1 & #3 ARE USED.

I HEREBY VERIFY THAT THE INFORMATION CONTAINED WITHIN THE STACK TEST REPORT HAS BEEN REVIEWED AND IT HAS BEEN DETERMINED THAT THE TEST PROCEDURES, ANALYSES AND CALCULATIONS ARE:

☒ AN ACCEPTABLE DEMONSTRATION OF CONFORMANCE WITH THE APPROVED TESTING METHODOLOGY.

☐ AN UNACCEPTABLE DEMONSTRATION OF CONFORMANCE WITH THE APPROVED TESTING METHODOLOGY.

7/18/94
 DATE OF REVIEW

[Signature]
 REVIEWED BY

* BASED ON 3 RUN AVERAGE

** SPECIFY APPLICABLE UNITS

***SPECIFY IN UNITS OF MASS/INPUT

* TONS per hour

=====

PARTICULATE EMISSION TEST DATA

FACILITY :WEIDLE SAND AND GRAVEL
 PROCESS/RUN NUMBER :
 SOURCE/RUN :1
 TEST DATE :5/25/94

VOLUME METERED AT STD. CONDITIONS	= 33.64693689857778 DSCF
VOLUME WATER COLLECTED AT STP.	= 7.695945000000001 SCF
PERCENT MOISTURE BY VOLUME	= 18.61492147276928 %
MOLECULAR WEIGHT OF STACK GAS	= 27.11512879504984 LB/LB-MOL
PERCENT EXCESS AIR	= 630.252100840336 %
AVERAGE STACK GAS VELOCITY	= 62.02771822210665 FT/SEC
ABSOLUTE STACK PRESSURE	= 29.14911764705882 IN. HG
STACK FLOW RATE AT ACTUAL COND.	= 19472.44609423202 ACFM
STACK FLOW RATE AT STD. COND.	= 12812.44975622692 DSCFM
STACK EMISSIONS	= 1.19000431215159E-003 GR/DSCF
	= 1.700516162064622E-007 LB/DSCF
STACK EMISSION RATE	= .1307266673166288 LB/HR
ISOKINETIC VARIATION	= 104.9730258269964 %

1.2×10^{-3}
 test
 0.131
 104.8

TIME OF TEST	= 60 MIN
VOLUME METERED	= 34.15 CU.FT
DRY GAS METER CALB. FACT.	= 1.019
TEST BAR. PRESSURE	= 29.23 IN HG
AVERAGE DELTA H	= 1.29
AVG. METER TEMP.	= 75 DEG. F
VOL. H2O (IMPINGERS)	= 154.8 ML
WEIGHT GAIN OF SILICA GEL	= 8.699999999999999 GM
%CO2	= 3 %
%CO	= 0 %
%O2	= 18 %
%N2	= 79 %
STATIC P OF STACK	= -1.1 IN. H2O
STACK TEMP.	= 176 DEG. F
PITOT COEFFICIENT	= .84
AVG. ROOT DELTA P	= .9629
STACK DIAMETER	= 0 IN.
MASS PARTICULATE	= 2.6 MG
NOZZLE DIAMETER	= .2 IN

=====

PARTICULATE EMISSION TEST DATA

FACILITY :WEIDLE SAND AND GRAVEL
 PROCESS/RUN NUMBER :
 SOURCE/RUN :2
 TEST DATE :5/25/94

DISCARD Due
 to low volume
 per SUBPART I

 31.8

VOLUME METERED AT STD. CONDITIONS = 25.61472467207219 DSCF

VOLUME WATER COLLECTED AT STP. = 6.763959000000001 SCF
 PERCENT MOISTURE BY VOLUME = 20.89016054051069 %

MOLECULAR WEIGHT OF STACK GAS = 26.8603020194628 LB/LB-MOL
 PERCENT EXCESS AIR = 630.252100840336 %

AVERAGE STACK GAS VELOCITY = 49.09403820199745 FT/SEC
 ABSOLUTE STACK PRESSURE = 29.76911764705882 IN. HG

STACK FLOW RATE AT ACTUAL COND. = 15412.15830338011 ACFM
 STACK FLOW RATE AT STD. COND. = 9911.194285463711 DSCFM

STACK EMISSIONS = 2.525110100852297E-003 GR/DSCF
 = 3.608382334117932E-007 LB/DSCF

STACK EMISSION RATE = .2145802702180671 LB/HR

ISOKINETIC VARIATION = 103.3071552685019 %

2.62×10^{-3}
 $\frac{1}{10}$
 0.218
 101.9

TIME OF TEST = 60 MIN
 VOLUME METERED = 26.062 CU.FT
 DRY GAS METER CALB. FACT. = 1.019
 TEST BAR. PRESSURE = 29.85 IN HG
 AVERAGE DELTA H = .723
 AVG. METER TEMP. = 86.90000000000001 DEG. F
 VOL. H2O (IMPINGERS) = 138.8 ML
 WEIGHT GAIN OF SILICA GEL = 4.9 GM
 %CO2 = 3 %
 %CO = 0 %
 %O2 = 18 %
 %N2 = 79 %
 STATIC P OF STACK = -1.1 IN. H2O
 STACK TEMP. = 186 DEG. F
 PITOT COEFFICIENT = .84
 AVG. ROOT DELTA P = .7606000000000001
 STACK DIAMETER = 0 IN.
 MASS PARTICULATE = 4.2 MG
 NOZZLE DIAMETER = .2 IN

PARTICULATE EMISSION TEST DATA

FACILITY :WEIDLE SAND AND GRAVEL
PROCESS/RUN NUMBER :
SOURCE/RUN :3
TEST DATE :5/25/94

VOLUME METERED AT STD. CONDITIONS	= 38.58327040207596 DSCF
VOLUME WATER COLLECTED AT STP.	= 8.147817 SCF
PERCENT MOISTURE BY VOLUME	= 17.4355390660951 %
MOLECULAR WEIGHT OF STACK GAS	= 27.31327119334447 LB/LB-MOL
PERCENT EXCESS AIR	= 312.4999999999999 %
AVERAGE STACK GAS VELOCITY	= 48.96233482696189 FT/SEC
ABSOLUTE STACK PRESSURE	= 28.73911764705882 IN. HG
STACK FLOW RATE AT ACTUAL COND.	= 15370.81248340935 ACFM
STACK FLOW RATE AT STD. COND.	= 10138.22481316844 DSCFM
STACK EMISSIONS	= 2.354906648740468E-003 GR/DSCF
	= 3.36516160105013E-007 LB/DSCF
STACK EMISSION RATE	= .2047005890645285 LB/HR
ISOKINETIC VARIATION	= 101.3743505549967 %

2.39×10^{-3}
test
0.207
~~10.3~~
98.7

TIME OF TEST	= 60 MIN
VOLUME METERED	= 40.678 CU.FT
DRY GAS METER CALB. FACT.	= 1.019
TEST BAR. PRESSURE	= 28.82 IN HG
AVERAGE DELTA H	= 1.73
AVG. METER TEMP.	= 88.58 DEG. F
VOL. H2O (IMPINGERS)	= 165.3 ML
WEIGHT GAIN OF SILICA GEL	= 7.8 GM
%CO2	= 4 %
%CO	= 0 %
%O2	= 16 %
%N2	= 80 %
STATIC P OF STACK	= -1.1 IN. H2O
STACK TEMP.	= 174.6 DEG. F
PITOT COEFFICIENT	= .84
AVG. ROOT DELTA P	= .7583
STACK DIAMETER	= 0 IN.
MASS PARTICULATE	= 5.9 MG
NOZZLE DIAMETER	= .245 IN

Subpart I - @ least 60 min @ 31.8
PARTICULATE EMISSION TEST REVIEW SHEET
DSCFM

1. Facility Name: _____
2. Run Number: _____
3. Test Date: _____
4. Time of Test: _____ (min)
5. Volume Metered: 34.15 26.01.2 115.628 (ft³)
6. Dry Gas Meter Calb. Factor: 1.00
7. Test Barometric Pressure: 29.23 31.15 (in. Hg)
8. Avg. Delta H: 1.21 2.723 1.73 (in. H₂O)
9. Avg. Meter Temp: 75 86.7 77.7 (Deg. F)
10. Volume H₂O (Impingers): 54.7 121.8 165.3 (ML)
11. Weight Gain of Silica Gel: 2.7 4.9 7.7 (GM)
12. % CO₂: 3 3 4
13. % CO: 1 1 1
14. % O₂: 18 18 18
15. % N₂: 77 77 77
16. Static Pressure of Stack: -1.1 (in. H₂O)
17. Stack Temp: 172 172 174 (Deg. F)
18. Pitot Coefficient: 0.24
19. Avg. Root Delta P: 0.71629 0.76016 0.7583
20. Stack Diameter: 24.5 24.5 (in.)
21. Mass Particulate: 2.6 4.6 5.1 (mg)
22. Nozzle Diameter: 0.2 0.2 0.245 (in.)

Coal Data

- | | |
|---------------------------------|----------------------|
| 1. % Hydrogen: _____ | 4. % Nitrogen: _____ |
| 2. % Carbon: _____ | 5. % Oxygen: _____ |
| 3. % Sulfur: _____ | 6. F Factor: _____ |
| 7. Gross Calorific Value: _____ | |

100.5 100.5 100.5
100.5 100.5 100.5
100.5 100.5 100.5

CONTACT REPORT

FACILITY: Weidle Sand and Gravel, Inc.
CONTACT: Ron Weidle
RAPCA REP.: Cathy O'Neill
DATE: May 25, 1994
RE: Source P002 Stack Test

On Sept. 16, 1993 a stack test was conducted at Weidle Sand and Gravel Inc. on an asphalt batch plant (OEPA source no. P903). The test incorporated (3) one hour runs. Jon Hilty was on site observing the stack test crew's implementation of USEPA approved testing procedures. Meanwhile, I observed the asphalt operating parameters in the control room and took visible emission readings (VE's) during each run.

Run # 1	Started at	9:30	and ended at		10:45
Time		9:30	10:01	10:40	
Rate (Tons/hr.)		80/85	80/85	84/85	
Photohelic		4.5	4.5	6	
Total tons made			44		84 + 15 in hot storage bins
Run # 2	Started at	11:50	and ended at		1:00
Time		11:50	12:18	12:58	1:02
Rate (Tons/hr.)		80/85	80/85	80/85	
Photohelic		6	6	6	
Total tons made		14	52		98
Run # 3	Started at	2:00	and ended at		3:10
Time		2:00	2:25	3:05	
Rate (Tons/hr.)		80	80	84	
Photohelic		4.5	4.5	6	
Total tons made			42	84	84 +10/15 in hot storage bins

The new filters made a great improvement on the operations. But they were getting clogged up. The plant operator physically shook the filters out during the shut-down break between runs.

Visible Emission Observation Form

Run# 3

SOURCE NAME			OBSERVATION DATE				START TIME				STOP TIME			
ADDRESS			5/25/94				2:04							
			MIN	0	15	30	45	MIN	0	15	30	45		
CITY			1				31							
STATE			2				32							
ZIP			3				33							
PHONE			4				34							
SOURCE ID NUMBER			5				35							
PROCESS EQUIPMENT			6				36							
OPERATING MODE			7				37							
CONTROL EQUIPMENT			8				38							
OPERATING MODE			9				39							
DESCRIBE EMISSION POINT			10				40							
START			11				41							
STOP			12				42							
HEIGHT ABOVE GROUND LEVEL			13				43							
HEIGHT RELATIVE TO OBSERVER			14				44							
START			15				45							
STOP			16				46							
DISTANCE FROM OBSERVER			17				47							
DIRECTION FROM OBSERVER			18				48							
START			19				49							
STOP			20				50							
DESCRIBE EMISSIONS			21				51							
START			22				52							
STOP			23				53							
EMISSION COLOR			24				54							
PLUME TYPE: CONTINUOUS ☐			25				55							
FUGITIVE ☐ INTERMITTENT ☐			26				56							
WATER DROPLETS PRESENT:			27				57							
NO ☐ YES ☐			28				58							
IF WATER DROPLET PLUME:			29				59							
ATTACHED ☐ DETACHED ☐			30				60							
POINT IN THE PLUME AT WHICH OPACITY WAS DETERMINED														
START														
STOP														
DESCRIBE BACKGROUND														
START														
STOP														
BACKGROUND COLOR														
SKY CONDITIONS														
START														
STOP														
WIND SPEED														
WIND DIRECTION														
START														
STOP														
AMBIENT TEMP.														
WET BULB TEMP.														
RH. percent														
START														
STOP														
Source Layout Sketch														
Draw North Arrow														
The diagram shows a vertical line representing the 'Emission Point'. A horizontal line below it represents the 'Sun Location Line'. A diagonal line from the emission point to the bottom right represents the 'Wind' direction. A horizontal line from the emission point to the left represents the 'Plume and Stack'. The angle between the 'Sun Location Line' and the 'Wind' line is marked as 140°. A north arrow is drawn pointing towards the top right.														
AVERAGE OPACITY FOR HIGHEST PERIOD														
NUMBER OF READINGS ABOVE % WERE														
RANGE OF OPACITY READINGS														
MINIMUM														
MAXIMUM														
OBSERVER'S NAME (PRINT)														
OBSERVER'S SIGNATURE														
DATE														
ORGANIZATION														
I HAVE RECEIVED A COPY OF THESE OPACITY OBSERVATIONS														
SIGNATURE														
TITLE														
DATE														
CERTIFIED BY														
VERIFIED BY														
DATE														

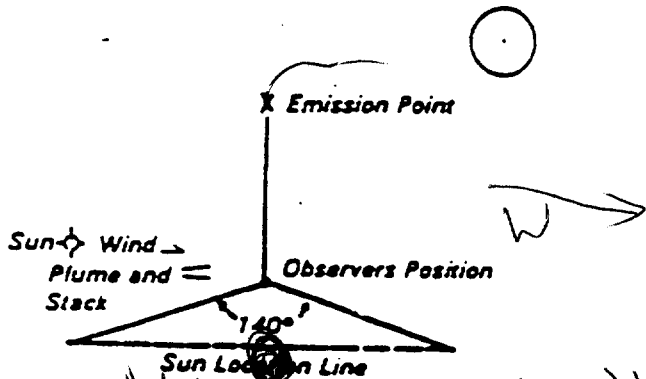
Visible Emission Observation Form

Run 2

SOURCE NAME <i>Wedge</i>		OBSERVATION DATE <i>5/25/94</i>		START TIME <i>11:57 AM</i>		STOP TIME <i>12:15 PM</i>	
ADDRESS		SEC MIN		SEC MIN		SEC MIN	
		0 15 30 45		0 15 30 45		0 15 30 45	
CITY <i>German town</i>		STATE <i>Oh</i>		ZIP			
PHONE		SOURCE ID NUMBER					
PROCESS EQUIPMENT <i>Hot-mix Asphalt Plant</i>		OPERATING MODE <i>ON</i>					
CONTROL EQUIPMENT <i>Bag house</i>		OPERATING MODE <i>ON</i>					
DESCRIBE EMISSION POINT <i>Stack w/ curved outlet</i>							
START <i>Square metal STOP</i>							
HEIGHT ABOVE GROUND LEVEL START <i>230'</i> STOP <i>✓</i>		HEIGHT RELATIVE TO OBSERVER START <i>230'</i> STOP <i>✓</i>					
DISTANCE FROM OBSERVER START <i>2100'</i> STOP <i>✓</i>		DIRECTION FROM OBSERVER START <i>NW</i> STOP <i>✓</i>					
DESCRIBE EMISSIONS START <i>heat like waves</i> STOP <i>✓</i>							
EMISSION COLOR START <i>Clear</i> STOP <i>✓</i>		PLUME TYPE: CONTINUOUS ☒ FUGITIVE ☐ INTERMITTENT ☐					
WATER DROPLETS PRESENT: <i>NO</i> ☒ YES ☐ END <i>✓</i>		IF WATER DROPLET PLUME: ATTACHED ☒ DETACHED ☐					
POINT IN THE PLUME AT WHICH OPACITY WAS DETERMINED START <i>1 stack width from top of stack</i> STOP <i>End of steam plume</i>							
DESCRIBE BACKGROUND START <i>Sky/HMA Plant</i> STOP <i>✓</i>							
BACKGROUND COLOR START <i>Blue</i> STOP <i>✓</i>		SKY CONDITIONS START <i>Cloudy</i> STOP <i>✓</i>					
WIND SPEED <i>1 Beaufort</i> STOP <i>✓</i>		WIND DIRECTION START <i>3-5 mph</i> STOP <i>✓</i>					
AMBIENT TEMP. START <i>70°F</i> STOP <i>✓</i>		WET BULB TEMP.		RH. percent			

Source Layout Sketch

Draw North Arrow



Comments: *Depending on the baghouse cleaning cycle, the stack emissions had periods of steam in the exhaust*

I HAVE RECEIVED A COPY OF THESE OPACITY OBSERVATIONS

SIGNATURE

TITLE

DATE

AVERAGE OPACITY FOR HIGHEST PERIOD

NUMBER OF READINGS ABOVE % WERE

RANGE OF OPACITY READINGS MINIMUM MAXIMUM

OBSERVER'S NAME (PRINT)

OBSERVER'S SIGNATURE

DATE *5/25/94*

ORGANIZATION

CERTIFIED BY

DATE *3/2/94*

VERIFIED BY

Visible Emission Observation Form

SOURCE NAME <u>W. edle</u>			OBSERVATION DATE <u>5/25/94</u>			START TIME <u>9:42</u>			STOP TIME					
ADDRESS			SEC			MIN			SEC			MIN		
			0			15			30			45		
			1			0			0			0		
CITY <u>German town</u>			STATE <u>Oh</u>			ZIP			2			0		
PHONE			SOURCE ID NUMBER			3			5			0		
PROCESS EQUIPMENT <u>Hot mix Asphalt Plant</u>			OPERATING MODE <u>ON</u>			4			0			0		
CONTROL EQUIPMENT <u>Bo shaw</u>			OPERATING MODE <u>ON</u>			5			0			5		
DESCRIBE EMISSION POINT <u>Square Metal Stack w/ curved outlet</u>			START <u>Square Metal Stack</u>			6			5			10		
HEIGHT ABOVE GROUND LEVEL <u>START ~30' STOP</u>			HEIGHT RELATIVE TO OBSERVER <u>START ~30' STOP</u>			7			0			5		
DISTANCE FROM OBSERVER <u>START ~100' STOP</u>			DIRECTION FROM OBSERVER <u>START NW STOP</u>			8			0			0		
DESCRIBE EMISSIONS <u>START looping plume STOP</u>			EMISSION COLOR <u>START Wt STOP</u>			9			0			0		
WATER DROPLETS PRESENT: <u>NO</u>			IF WATER DROPLET PLUME: <u>ATTACHED</u>			10			0			0		
POINT IN THE PLUME AT WHICH OPACITY WAS DETERMINED <u>START end of stack STOP</u>			PLUME TYPE: CONTINUOUS ☒ FUGITIVE ☐ INTERMITTENT ☐			11			0			0		
DESCRIBE BACKGROUND <u>START Clouds, sky STOP</u>			BACKGROUND COLOR <u>START Wt STOP</u>			12			0			0		
WIND SPEED <u>START ~3.5 mph STOP</u>			WIND DIRECTION <u>START STOP</u>			13			0			0		
AMBIENT TEMP. <u>START ~60° STOP</u>			WET BULB TEMP.			14			0			0		
			RH. percent			15			0			0		
Source Layout Sketch Draw North Arrow			16			0			0			15		
			17			0			5			10		
			18			15			15			10		
			19			0			0			0		
			20			0			0			0		
			21			0			0			0		
			22			0			0			0		
			23			0			0			0		
			24			0			0			0		
			25			0			0			0		
			26			0			0			0		
			27			0			0			0		
			28			0			0			0		
			29			0			0			0		
			30			0			0			0		
			AVERAGE OPACITY FOR HIGHEST PERIOD						NUMBER OF READINGS ABOVE % WERE					
RANGE OF OPACITY READINGS						RANGE OF OPACITY READINGS								
MINIMUM						MAXIMUM								
OBSERVER'S NAME (PRINT) <u>Cathy O'Neill</u>						OBSERVER'S SIGNATURE <u>Cathy O'Neill</u>								
DATE <u>5/25/94</u>						ORGANIZATION <u>RAPCA</u>								
I HAVE RECEIVED A COPY OF THESE OPACITY OBSERVATIONS SIGNATURE						CERTIFIED BY <u>ETA</u>								
TITLE						DATE <u>3/2/94</u>								

CONTACT REPORT

FACILITY: Weidle Sand and Gravel, Inc.
CONTACT: Ron Weidle
RAPCA REP.: Cathy O'Neill
DATE: May 25, 1994
RE: Source P002 Stack Test

On Sept. 16, 1993 a stack test was conducted at Weidle Sand and Gravel Inc. on an asphalt batch plant (OEPA source no. P903). The test incorporated (3) one hour runs. Jon Hilty was on site observing the stack test crew's implementation of USEPA approved testing procedures. Meanwhile, I observed the asphalt operating parameters in the control room and took visible emission readings (VE's) during each run.

Run # 1	Started at 9:30	and ended at 10:45	
Time	9:30	10:01	10:40
Rate (Tons/hr.)	80/85	80/85	84/85
Photohelic	4.5	4.5	6
Total tons made		44	84 + 15 in hot storage bins

Run # 2	Started at 11:50	and ended at 1:00	
Time	11:50	12:18	12:58 1:02
Rate (Tons/hr.)	80/85	80/85	80/85
Photohelic	6	6	6
Total tons made	14	52	98

Run # 3	Started at 2:00	and ended at 3:10	
Time	2:00	2:25	3:05
Rate (Tons/hr.)	80	80	84
Photohelic	4.5	4.5	6
Total tons made		42	84 + 10/15 in hot storage bins

The new filters made a great improvement on the operations. But they were getting clogged up. The plant operator physically shook the filters out during the shut-down break between runs.

RECEIVED

JUN 24 1994

REGIONAL AIR POLLUTION
CONTROL AGENCY

PARTICULATE COMPLIANCE EVALUATION
BATCH ASPHALT PLANT
WEIDLE SAND AND GRAVEL, INC.
GERMANTOWN, OHIO

Prepared for

Weidle Sand and Gravel, Inc.
Routes 4 & 123
Germantown, Ohio 45327

June, 1994
4794-001\REPORT

Submitted by

Pacific Environmental Services, Inc.
4700 Duke Drive, Suite 150
Mason, Ohio 45040
(513) 398-2556
Fax: (513) 398-3342

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SECTION 1

INTRODUCTION

Pacific Environmental Services, Inc. (PES) was retained by Weidle Sand and Gravel, Inc. (Weidle) to conduct a particulate compliance evaluation of their asphalt batch plant. The testing was conducted on May 25, 1994.

PES utilized EPA Reference Methods 1-5 to measure flue gas velocity, flow rate, temperature, composition (O_2 and CO_2) and particulate (filterable and condensable) concentrations and mass emission rates. A total of three 60-minute sample runs were conducted.

The process was correlated with PES test times by Weidle personnel. Mr. Robert Henry directed process operations. Testing and process operations were observed by Mr. Jon Hilty of the Regional Air Pollution Control Agency (RAPCA). Mr. Andrew Weisman and Mr. Peter Hilty conducted the test program for PES.

SECTION 2

SUMMARY OF TEST RESULTS

Particulate sampling was conducted on May 25, 1994. A total of three sampling runs were conducted. Table 2.1 details the stack gas conditions measured at the baghouse. Stack gas velocity averaged 53.68 feet per second (fps) at 179°F. Stack gas volumetric flow rates averaged 16,851 actual cubic feet per minute (acfm) or 10,929 dry standard cubic feet per minute (dscfm). Moisture content averaged 19.3%. Composition of the stack gas (dry molecular weight) averaged 3.3% carbon dioxide (CO₂) and 17.3% oxygen (O₂).

Table 2.2 details the filterable and condensible particulate matter concentrations and mass emission rates. Filterable particulate concentrations averaged 2.07×10^{-3} grains per dry standard cubic foot (gr/dscf) or 2.95×10^{-7} pounds per dry standard cubic foot (lb/dscf). Mass emission rates averaged 0.185 pounds per hour (lb/hr) or 2.3×10^{-3} pounds per ton (lb/ton) of asphalt produced. Process feed rates were supplied by plant personnel. Condensible particulate concentrations averaged 1.14×10^{-4} gr/dscf or 1.45×10^{-7} lb/dscf, for a corresponding mass emission rate of 0.093 lb/hr.

TABLE 2.1
SUMMARY OF STACK GAS CONDITIONS
WEIDLE SAND AND GRAVEL
MAY 25, 1994

Run No.	Time	Stack Gas Velocity, fps ^a	Volumetric Flow Rate		Stack Temp., °F	Moisture, %	Composition	
			acfm ^b	dscfm ^c			CO ₂ , %	O ₂ , %
B0-1	0930-1040	62.04	19,474	12,806	176	18.7	3.0	18.0
B0-2	1145-1300	50.01	15,697	9,862	186	21.5	3.0	18.0
B0-3	1400-1515	49.00	15,381	10,119	175	17.6	4.0	16.0
Average		53.68	16,851	10,929	179	19.3	3.3	17.3

^aFeet per second

^bActual cubic feet per minute

^cDry standard cubic feet per minute

MAY 25, 1994

*Grains per dry standard cubic foot.
^bPound per dry standard cubic foot.
^cPound per hour.
^dPound per ton.

SECTION 3

SAMPLING LOCATION AND TEST METHODS

Sampling was conducted at the outlet duct of the air pollution control system (baghouse and filter). Figure 3.1 shows the outlet sample locations and traverse points. The outlet ports are located 5.94 diameters downstream and 1.21 duct diameters upstream from the nearest flow disturbances. Twenty four sampling points, (four ports--6 points per port) were used to traverse the cross-sectional area of the 24.5" X 30.75" rectangular duct, with an equivalent diameter 27.27".

STACK GAS VOLUMETRIC FLOW RATE

EPA Method 1, "Determination of Stack Gas Velocity and Volumetric Flow Rate," was used to determine volumetric flow rate. A Type "S" pitot tube having an assigned coefficient of 0.84 and an inclined manometer were used to measure velocity pressure. A calibrated Type "K" thermocouple attached directly to the pitot tube was used to measure stack gas temperature. The average stack gas velocity was calculated from the average velocity pressure, average stack gas temperature, stack gas molecular weight, and absolute static pressure. The volumetric flow rate is the product of velocity and the stack cross-sectional area.

EMISSION RATE CORRECTION FACTOR, DRY MOLECULAR WEIGHT, AND EXCESS AIR

EPA Method 3, "Gas Analysis for Carbon Dioxide, Oxygen, Excess Air, and Dry Molecular Weight," was used to determine emission rate correction factors, dry molecular weight, and excess air. Integrated gas samples were collected in Tedlar bags by traversing the stack cross-sectional area simultaneously with each particulate test run. The samples were then analyzed using an Orsat analyzer.

STACK GAS MOISTURE CONTENT

EPA Method 4, "Determination of Moisture Content in Stack Gases," was used to determine stack gas moisture content. These samples was conducted simultaneously with each particulate measurement run. The initial and final contents of all impingers were determined gravimetrically.

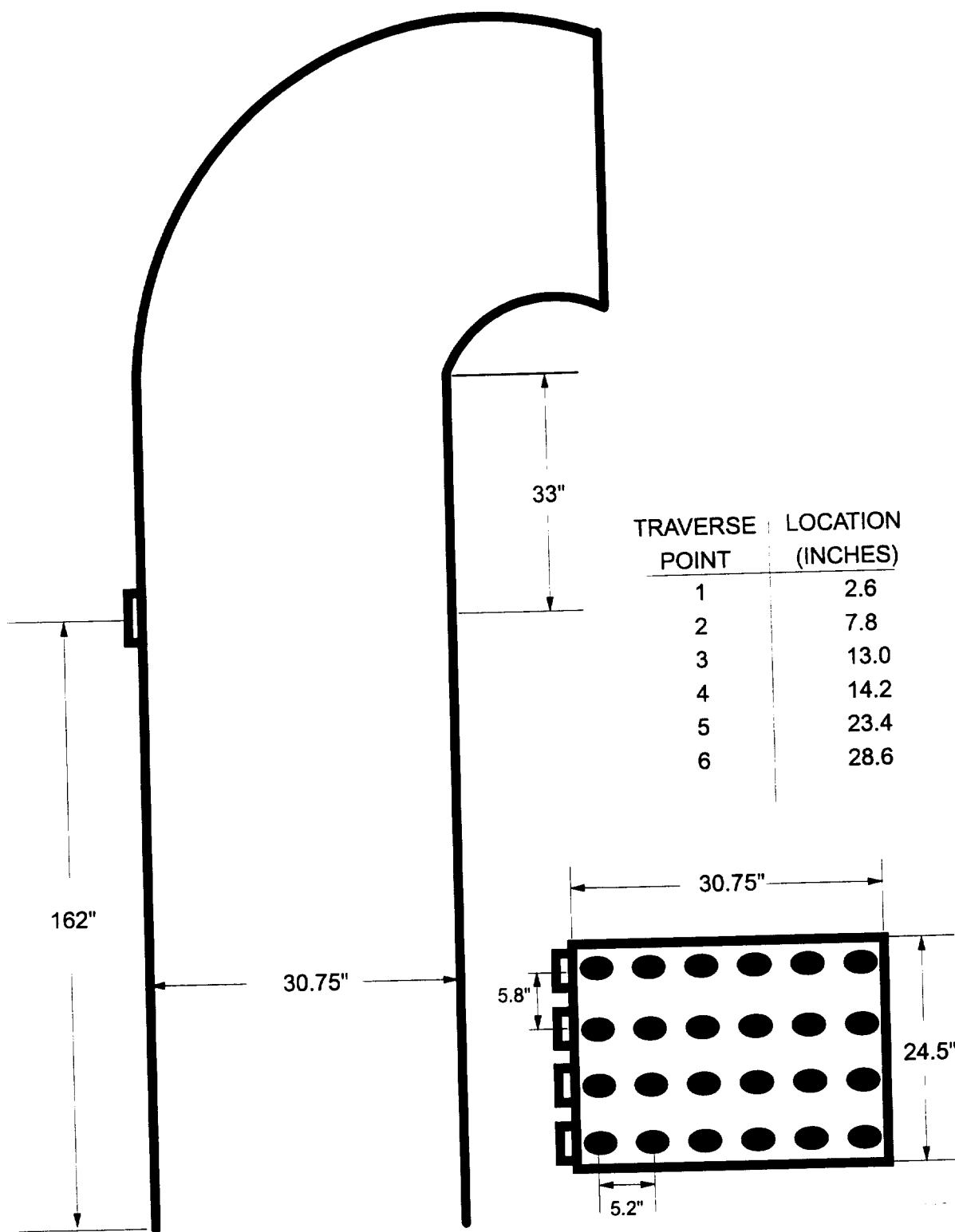


FIGURE 3.1 BAGHOUSE OUTLET SAMPLING LOCATION

FILTERABLE AND CONDENSIBLE PARTICULATE MATTER

EPA Method 5, "Determination of Particulate Emissions from Stationary Sources," was used to determine filterable and condensible particulate matter. The sample train consisted of a heated glass-lined probe, heated glass fiber filter, and a series of impingers followed by a vacuum pump, dry gas meter, and calibrated orifice. The filter temperature was maintained at $248 \pm 25^{\circ}\text{F}$. Thermocouples were used to monitor temperatures of the stack gas, sample probe, filter, and impinger exit gas. Figure 3.2 is a diagram of the sampling train.

SECTION 4

PROCESS DESCRIPTION

Weidle operates an asphalt batch plant at the intersection of routes 4 and 123 in Germantown, Ohio. This batch plant typically operates from May through October supplying asphalt for road and parking lot construction. The plant operated at an average production rate of 80 tons per hour during testing.

Particulate emissions generated from the gravel dryer and asphalt production are routed from the dryer to a pulse-air baghouse and an auxiliary filter before being exhausted to the atmosphere via the 24.5 X 30.75 inch outlet stack.

SECTION 5

QUALITY ASSURANCE AND QUALITY CONTROL

The field sampling quality assurance for this project included the use of: calibrated source sampling equipment; reference test methods; and traceability protocols, for the recording and calculation of data. The analytical quality assurance included: use of validated analytical procedures; calibration of analytical instruments; and analysis of control samples and blanks. The calibration and quality control procedures used for this test program are described in the following subsections.

CALIBRATIONS PROCEDURES AND FREQUENCY

All manual stack gas sampling equipment was calibrated before the test program in accordance with the procedures outlined in the *Quality Assurance Handbook for Air Pollution Measurement Systems, Volume III*, EPA-600/4-72-027B. Summarized in Table 5.1 are the stack gas sampling equipment calibrations which were performed in preparation for this project. The meter boxes were calibrated after the test.

Listed in Table 5.2 are the additional calibration checks which were performed on the sampling equipment on-site, just prior to the testing, to ensure that equipment was not damaged during transport.

TABLE 5.1
FIELD EQUIPMENT CALIBRATION SUMMARY*

Equipment	Calibrated against	Allowable error
Method 5 meter box	Reference test meter	$Y \pm 0.02 Y$ $\Delta H @ \pm 0.15$ post-test $Y \pm 0.05 Y$
Orsat	Certified cylinder gas	$\pm 0.5\%$
Pitot tube	Geometric specifications	See EPA Method 2
Thermocouple	ASTM-3F thermometer	$\pm 1.5\%$
Impinger (or condenser thermometer)	ASTM-3F	$\pm 2^\circ F$
Dry gas thermometer	ASTM-3F	$\pm 5^\circ F$
Probe nozzles	Caliper	± 0.004 in.
Barometer	NBS traceable barometer	± 0.1 in.Hg

*As recommended in the Quality Assurance Handbook for Air Pollution Measurement Systems: Volume III. Stationary Source-Specific Methods. EPA-600/4-77-027b, August 1977.

TABLE 5.2
FIELD CHECKS OF SAMPLING EQUIPMENT

Equipment	Checked against	Allowable difference
Pitot tube	Inspection	No visible damage
Thermocouples	ASTM 2F or 3F	$\pm 1.5\%$
Probe nozzles	Caliper	± 0.004 in.

APPENDIX A
EXAMPLE/COMPUTER CALCULATIONS

PACIFIC ENVIRONMENTAL SERVICES EMISSIONS CALCULATIONS

EXAMPLE CALCULATION

CLIENT/PROJECT NUMBER:

SAMPLE LOCATION:

DATE/TIME:

RUN #:

1.METER CORRECTIONS:

$$\begin{aligned} V_{mc} &= V_m - (L_p - L_a) * \text{Time} = V_m - (L_p - 0.02) * \text{Time} = & 34.150 \\ V_{m(std)} &= 17.647 * V_{mc} * Y * (P_{bar} + \Delta H / 13.6) / T_m(^{\circ}R) = & 33.473 \end{aligned}$$

2.MOISTURE FRACTION:

$$\begin{aligned} V_{w(sc)} &= V_{wc} * 0.04707 = & 7.70 \\ B_{ws} &= V_{w(std)} / (V_{w(std)} + V_{m(std)}) * 100 = & 0.187 \\ \%H_2O &= B_{ws} * 100 = & 18.69 \end{aligned}$$

3.MOLECULAR WEIGHT:

$$\begin{aligned} M_d &= 0.44 * (\%CO_2) + 0.32 * (\%O_2) + 0.28 * (\%N_2 + \%CO) = & 29.20 \\ M_s &= M_d * (1 - B_{ws}) + (18.0 * B_{ws}) = & 27.11 \end{aligned}$$

$$\begin{aligned} V_s &= 85.49 * C_p * \text{Avg}(\Delta P^{0.5}) * [T_s(^{\circ}R) / (P_s * H_g * M_s)]^{0.5} = & 62.04 \\ Q_a &= V_s * 60 * A_s(ft^2) = & 19474.1 \\ Q_{std} &= Q_a * 17.647 * (1 - \%H_2O) * P_s / T_s(^{\circ}R) = & 12806.2 \end{aligned}$$

5.ISOKINETIC:

$$\%I = 0.0945 * T_s(^{\circ}R) * V_{m(std)} / [P_s * V_s * A_n * \text{Time} * (1 - B_{ws})] = 104.53$$

6.CONCENTRATION(Cs):

$$\begin{aligned} C_s(\text{gr/dscf}) &= 0.0154 * W_t(\text{mg}) / V_{m(std)} = & 1.20E-03 \\ C_s(\text{lb/dscf}) &= 1.429E-04 * C_s(\text{gr/dscf}) = & 1.71E-07 \end{aligned}$$

7.EMISSION RATE(Er):

$$E_r(\text{lb/hr}) = C_s(\text{lb/dscf}) * Q_{std} * 60 = 0.13$$

PACIFIC ENVIRONMENTAL SERVICES EMISSIONS CALCULATIONS

CLIENT/PROJECT #: Weidle Sand & Gravel
SAMPLE LOCATION: Baghouse Outlet
DATE/TIME: 25May94/0941
RUN #: BO-1

STATIC PRESSURE("H2O):	-1.10	"HG	29.15
BAROMETRIC("HG):	29.23		
SAMPLE TIME(min):	60.00	Vm(corr)	34.150
ACTUAL METER VOLUME:	34.150	DSCF	33.473
SQ. ROOT P:	0.963		
AVG ORIFICE H:	1.29		
AVG STACK TEMP °F:	176.0	°R	636.0
AVG METER TEMP °F:	78.0		
Cp PITOT :	0.84		
NOZZLE DIA.(inches):	0.200	An(ft^2)	2.18E-04
METER GAMMA:	1.019		
LEAK RATE(IF <0.02):	0.000		
CIRC STACK? 1=Y,0=N:	0	As(ft^2)	5.23
DIA OR DIM (inches):	753.38		
% O2 :	18.00	DRY MOLE	29.20
% CO2 :	3.00	T MOLE WT	27.11
VOL CONDENSATE(ml):	163.50	% H2O	18.69
FILTER GAIN(mg):	0.10		
RINSE GAIN(mg):	2.50	NET WT(mg)	2.60

***** CALCULATED RESULTS *****

GAS VELOCITY (Vs):	62.04	FT/SEC
STACK GAS FLOW (Qs):	19474.1	ACFM
:	12806.2	DSCFM
STACK GAS TEMP :	176	Deg F
MOISTURE (%H2O):	18.69	%
ISOKINETIC :	104.53	%
CONCENTRATION (Cs):	1.20E-03	Gr/DSCF
:	1.71E-07	lb/DSCF
EMISSION RATE (Er):	0.131	lb/hr

COMMENTS:

PACIFIC ENVIRONMENTAL SERVICES EMISSIONS CALCULATIONS

CLIENT/PROJECT #: Weidle Sand & Gravel
SAMPLE LOCATION: Baghouse Outlet
DATE/TIME: 25May94/1150
RUN #: BO-2

STATIC PRESSURE("H2O):	-1.10	"HG	28.77
BAROMETRIC("HG):	28.85		
SAMPLE TIME(min):	60.00	Vm(corr)	26.062
ACTUAL METER VOLUME:	26.062	DSCF	24.673
SQ. ROOT P:	0.761		
AVG ORIFICE H:	0.72		
AVG STACK TEMP °F:	186.0	°R	646.0
AVG METER TEMP °F:	89.0		
Cp PITOT :	0.84		
NOZZLE DIA.(inches):	0.200	An(ft^2)	2.18E-04
METER GAMMA:	1.019		
LEAK RATE(IF < 0.02):	0.000		
CIRC STACK? 1=Y,0=N:	0	As(ft^2)	5.23
DIA OR DIM (inches):	753.38		
% O2 :	18.00	DRY MOLE	29.20
% CO2 :	3.00	T MOLE WT	26.79
VOL CONDENSATE(ml):	143.70	% H2O	21.52
FILTER GAIN(mg):	0.20		
RINSE GAIN(mg):	4.00	NET WT(mg)	4.20

CALCULATED RESULTS

GAS VELOCITY (Vs):	50.01	FT/SEC
STACK GAS FLOW (Qs):	15697.1	ACFM
:	9682.0	DSCFM
STACK GAS TEMP :	186	Deg F
MOISTURE (%H2O):	21.52	%
ISOKINETIC :	101.91	%
CONCENTRATION (Cs):	2.62E-03	Gr/DSCF
:	3.75E-07	lb/DSCF
EMISSION RATE (Er):	0.218	lb/hr

COMMENTS:

PACIFIC ENVIRONMENTAL SERVICES EMISSIONS CALCULATIONS

CLIENT/PROJECT #: Weidle Sand & Gravel
SAMPLE LOCATION: Baghouse Outlet
DATE/TIME: 25May94/1404
RUN #: BO-3

ATIC PRESSURE("H2O):	-1.10	"HG	28.74
BAROMETRIC("HG):	28.82		
SAMPLE TIME(min):	60.00	Vm(corr)	40.678
TUAL METER VOLUME:	40.678	DSCF	38.083
SQ. ROOT P:	0.758		
AVG ORIFICE H:	1.73		
AVG STACK TEMP °F:	175.0	°R	635.0
AVG METER TEMP °F:	96.0		
Cp PITOT :	0.84		
NOZZLE DIA.(inches):	0.245	An(ft^2)	3.27E-04
METER GAMMA:	1.019		
LEAK RATE(IF < 0.02):			
CIRC STACK? 1=Y,0=N:	0	As(ft^2)	5.23
DIA OR DIM (inches):	753.38		
% O2 :	16.00	DRY MOLE	29.28
% CO2 :	4.00	T MOLE WT	27.29
VOL CONDENSATE(ml):	173.10	% H2O	17.62
FILTER GAIN(mg):	0.40		
RINSE GAIN(mg):	5.50	NET WT(mg)	5.90

***** CALCULATED RESULTS *****

GAS VELOCITY (Vs):	49.00	FT/SEC
STACK GAS FLOW (Qs):	15380.5	ACFM
:	10119.1	DSCFM
STACK GAS TEMP :	175	Deg F
MOISTURE (%H2O):	17.62	%
ISOKINETIC :	100.30	%
CONCENTRATION (Cs):	2.39E-03	Gr/DSCF
:	3.41E-07	lb/DSCF
EMISSION RATE (Er):	0.207	lb/hr

COMMENTS:

PACIFIC ENVIRONMENTAL SERVICES EMISSIONS CALCULATIONS

CLIENT/PROJECT #: Weidle Sand & Gravel
 SAMPLE LOCATION: Baghouse Outlet
 DATE/TIME: 25May94/0941
 RUN #: BO-1 condensibles

STATIC PRESSURE("H2O):	-1.10	"HG	29.15
BAROMETRIC("HG):	29.23		
SAMPLE TIME(min):	60.00	Vm(corr)	34.150
ACTUAL METER VOLUME:	34.150	DSCF	33.473
SQ. ROOT P:	0.963		
AVG ORIFICE H:	1.29		
AVG STACK TEMP °F:	176.0	°R	636.0
AVG METER TEMP °F:	78.0		
Cp PITOT :	0.84		
NOZZLE DIA.(inches):	0.200	An(ft^2)	2.18E-04
METER GAMMA:	1.019		
LEAK RATE(IF < 0.02):	0.000		
CIRC STACK? 1=Y,0=N:	0	As(ft^2)	5.23
DIA OR DIM (inches):	753.38		
% O2 :	18.00	DRY MOLE	29.20
% CO2 :	3.00	T MOLE WT	27.11
VOL CONDENSATE(ml):	163.50	% H2O	18.69
FILTER GAIN(mg):	0.00		
RINSE GAIN(mg):	1.90	NET WT(mg)	1.90

CALCULATED RESULTS

GAS VELOCITY (Vs):	62.04	FT/SEC
STACK GAS FLOW (Qs):	19474.1	ACFM
:	12806.2	DSCFM
STACK GAS TEMP :	176	Deg F
MOISTURE (%H2O):	18.69	%
ISOKINETIC :	104.53	%
CONCENTRATION (Cs):	8.74E-04	Gr/DSCF
:	1.25E-07	lb/DSCF
EMISSION RATE (Er):	0.096	lb/hr

COMMENTS:

PACIFIC ENVIRONMENTAL SERVICES EMISSIONS CALCULATIONS

CLIENT/PROJECT #: Weidle Sand & Gravel
SAMPLE LOCATION: Baghouse Outlet
DATE/TIME: 25May94/1150
RUN #: BO-2 condensibles

STATIC PRESSURE("H2O):	-1.10	"HG	28.77
BAROMETRIC("HG):	28.85		
SAMPLE TIME(min):	60.00	Vm(corr)	26.062
ACTUAL METER VOLUME:	26.062	DSCF	24.673
SQ. ROOT P:	0.761		
AVG ORIFICE H:	0.72		
AVG STACK TEMP °F:	186.0	°R	646.0
AVG METER TEMP °F:	89.0		
Cp PITOT :	0.84		
NOZZLE DIA.(inches):	0.200	An(ft^2)	2.18E-04
METER GAMMA:	1.019		
LEAK RATE(IF < 0.02):	0.000		
CIRC STACK? 1=Y,0=N:	0	As(ft^2)	5.23
DIA OR DIM (inches):	753.38		
% O2 :	18.00	DRY MOLE	29.20
% CO2 :	3.00	T MOLE WT	26.79
VOL CONDENSATE(ml):	143.70	% H2O	21.52
FILTER GAIN(mg):	0.00		
RINSE GAIN(mg):	2.20	NET WT(mg)	2.20

***** CALCULATED RESULTS *****

GAS VELOCITY (Vs):	50.01	FT/SEC
STACK GAS FLOW (Qs):	15697.1	ACFM
:	9682.0	DSCFM
STACK GAS TEMP :	186	Deg F
MOISTURE (%H2O):	21.52	%
ISOKINETIC :	101.91	%
CONCENTRATION (Cs):	1.37E-03	Gr/DSCF
:	1.96E-07	lb/DSCF
EMISSION RATE (Er):	0.114	lb/hr

COMMENTS:

PACIFIC ENVIRONMENTAL SERVICES EMISSIONS CALCULATIONS

CLIENT/PROJECT #: Weidle Sand & Gravel
SAMPLE LOCATION: Baghouse Outlet
DATE/TIME: 25May94/1404
RUN #: BO-3 condensibles

STATIC PRESSURE("H2O):	-1.10	"HG	28.74
BAROMETRIC("HG):	28.82		
SAMPLE TIME(min):	60.00	Vm(corr)	40.678
ACTUAL METER VOLUME:	40.678	DSCF	38.083
SQ. ROOT P:	0.758		
AVG ORIFICE H:	1.73		
AVG STACK TEMP °F:	175.0	°R	635.0
AVG METER TEMP °F:	96.0		
Cp PITOT :	0.84		
NOZZLE DIA.(inches):	0.245	An(ft^2)	3.27E-04
METER GAMMA:	1.019		
LEAK RATE(IF < 0.02):			
CIRC STACK? 1=Y,0=N:	0	As(ft^2)	5.23
DIA OR DIM (inches):	753.38		
% O2 :	16.00	DRY MOLE	29.28
% CO2 :	4.00	T MOLE WT	27.29
VOL CONDENSATE(ml):	173.10	% H2O	17.62
FILTER GAIN(mg):	0.00		
RINSE GAIN(mg):	2.00	NET WT(mg)	2.00

CALCULATED RESULTS

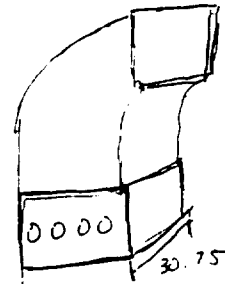
GAS VELOCITY (Vs):	49.00
STACK GAS FLOW (Qs):	15380.5
:	10119.1
STACK GAS TEMP :	175
MOISTURE (%H2O):	17.62
ISOKINETIC :	100.30
CONCENTRATION (Cs):	8.09E-04
:	1.16E-07
EMISSION RATE (Er):	0.070

COMMENTS:

27.27

TRAVERSE POINT LOCATION FOR RECTANGULAR DUCTS

Plant: Weir 16 Sand & Gravel
 Date: 23 MAY 94
 Sampling Location: Bighaus Outlet
 Duct Width, inches: 24.5
 Inside of Far Wall to Outside of Nipple: 35"
 Inside of Near Wall to Outside of Nipple (Nipple Length): 4.25"
 Duct Length, inches: ~~28~~ 30.75
 Equivalent Diameter = $2 \times L \times W / (L + W) =$ 27.27
 Distance Downstream from Flow Disturbance (Distance B):
16.2 inches / Equivalent Diameter = 5.94 dd
 Distance Upstream from Flow Disturbance (Distance A):
~~16~~ 33 inches / Equivalent Diameter = 1.21 dd
 Calculated By: _____



Schematic of
Sampling Location

Traverse Point Number	Fraction of Length	Length (inches)	Product of Columns 2 & 3* (To nearest 1/8")	Nipple Length (inches)	Traverse Point Location (Sum of Col. 4 & 5)
1	.083	30.75	2.55	4.25	6.8
2	.250		7.69		11.94
3	.417		12.82		17.07
4	.583		17.93		22.18
5	.750		23.06		27.3
6	.917		28.20		32.45

If No Ports, Calculate Distances From Stack Walls For Port Locations

Number of Ports	Fraction of Width	Width (inches)	Port Location Product of Col. 2 & 3* (To Nearest 1/8")

* All points or ports should be an equal distance from each other (D) and 1/2 of that distance from the stack walls (D/2), where D = Width / # of points or ports

DU -197
 V = 2.46 i 42

GAS VELOCITY AND VOLUMETRIC FLOW RATE

Plant: Weldle sand & gravel Date: 25 MAY 94
 Sampling Location: _____ Clock Time: _____
 Run #: prelim Operators: AW / PH
 Barometric Pressure, in. Hg: 29.23 Static Pressure, in. H₂O: -1.1
 Moisture, %: 11.2 Molecular wt., Dry: _____ Pitot Tube, Cp: 0.84
 Stack Dimension, in. Diameter or Side 1: 30.75 Side 2: 24.5
 Wet Bulb, °F: _____ Dry Bulb, °F: _____

Traverse Point Number	Velocity Head in. H ₂ O	Stack Temp. °F
A 1	1.9	73
2	2.0	74
3	1.8	74
4	1.2	74
5	.68	74
6	.26	74
B 1	3.0	73
2	3.0	74
3	2.5	74
4	1.8	74
5	.78	74
6	.31	74
C 1	3.0	73
2	3.1	73
3	2.3	73
4	1.5	74
5	.76	73
6	.36	74
D 1	2.5	73
2	2.8	73
3	1.8	73
4	1.1	73
5	.56	73
6	.22	73
$\overline{\Delta P} = 1.26$		$\overline{T_s} =$

$\overline{\Delta P} = 1.64$ 74

$T_s = 246$

$$M_d = (0.44 \times \%CO_2) + (0.32 \times \%O_2) + (0.28 \times \%N_2)$$

$$M_d = (0.44 \times 2.95) + (0.32 \times 16.9) + (0.28 \times)$$

$$M_d = 29.15$$

$$M_s = M_d \times (1 - \frac{\%H_2O}{100}) + 18 (\frac{\%H_2O}{100})$$

$$M_s = (29.15) \times (1 - \frac{11.2}{100}) + 18 (\frac{11.2}{100})$$

$$M_s = 27.90$$

$$T_s = \frac{246}{74} ^\circ F = \frac{706}{534} ^\circ R (^\circ F + 460)$$

$$P_s = P_b + \frac{S.P.}{13.6} = (29.23) + \frac{-1.1}{13.6}$$

$$P_s = 29.15 \text{ in. Hg}$$

$$\overline{\Delta P} = 1.26$$

$$V_s = 85.49 \times C_p \times \sqrt{\overline{\Delta P}} \times \sqrt{\frac{T_s (^\circ R)}{P_s \times M_s}}$$

$$V_s = 85.49 \times (.84) \times (1.26) \times \sqrt{\frac{534}{(29.15 \times 27.90)}}$$

$$V_s = 73.32 \text{ ft/s}$$

$$A_s = 5.23 \text{ ft}^2$$

$$Q_s = V_s \times A_s \times 60 \text{ s/min}$$

$$Q_s = 73.32 \times 5.23 \times 60$$

$$Q_s = 23,007.0 \text{ acfm}$$

$$Q_{s, \text{std}} = Q_s \times 17.647 \times \frac{P_s}{T_s} \times (1 - \frac{\%H_2O}{100})$$

$$Q_{s, \text{std}} = 23,007.0 \times 17.647 \times \frac{29.15}{534} \times (1 - \frac{11.2}{100})$$

$$Q_{s, \text{std}} = 21,720.5 \text{ dscfm}$$

FIELD DATA SHEET

NO = 1-121

Plant: Weldle Sand & Gravel
 Sampling Location: Bughouse Outlet
 Run Number: B01 Date: 25 MAY 94
 Pretest Leak Rate: .004 cfm @ 15 in. Hg.
 Pretest Leak Check: Pitot: Orsat:

Sample Type: M5 Operator: Hilly
 Pbar: 29.23 Ps: -1.1
 CO2: 3 O2: 18
 Probe Length/Type: 5' glass Pitot #: 5.61
 Stack Diameter: 30.15 x 24.5 As:

Nozzle ID: .200 Thermocouple #: 5002
 Assumed Bws: 11% Filter #: 300099
 Meter Box #: 15 Y: 1.014 ΔH@: 1.861
 Post-Test Leak Rate: .001 cfm @ 5 in. Hg.
 Post-Test Leak Check: Pitot: Orsat:

Traverse Point Number	Sampling Time (min)	Clock Time (24-hour clock)	Gas Meter Reading (Nm) ft ³	Velocity Head (Δp) In H ₂ O	Orifice Pressure Differential (ΔH) In H ₂ O		Stack Temp. (T _s)	Temperature °F		Impinger Temp. °F	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)
					Desired	Actual		Probe	Filter		Inlet (T _m in °F)	Outlet (T _m out °F)	
—	—	—	—	—	—	—	—	—	—	—	—	—	—
1	0	0941	538.446	0.13	0.156	0.16	165	256	253	65	70	69	0
2	2.5		539.036	0.26	0.312	0.31	167	254	252	63	71	69	2
3	5		539.781	0.70	0.836	0.84	176	252	252	59	71	69	2
4	7.5		540.961	1.0	1.20	1.2	171	254	252	55	72	70	2
5	10		542.421	2.0	2.30	2.4	174	256	252	53	73	70	3.5
6	12.5		544.433	2.1	2.52	2.5	171	252	253	54	76	71	4
7	15		546.519	0.18	0.22	0.22	160	258	253	58	77	71	0
8	17.5		547.218	0.41	0.495	0.5	168	253	253	58	77	72	2
9	20		548.221	0.88	1.06	1.1	171	256	253	58	78	73	2
10	22.5		549.691	1.5	1.79	1.8	177	253	253	58	80	73	3
11	25		551.311	2.1	2.51	2.5	180	255	253	59	82	74	4
12	27.5		553.591	2.2	2.62	2.6	182	255	254	60	84	74	4
13	30		555.566	0.21	0.257	0.26	163	255	255	60	80	75	0
14	32.5		556.403	0.51	0.609	0.61	181	256	252	53	82	76	2
15	35		557.341	1.0	1.19	1.2	183	253	252	57	83	77	2
16	37.5		558.803	1.6	1.91	1.9	184	252	251	57	85	77	3
17	40		560.601	2.2	2.64	2.6	183	254	255	54	87	78	3.5
18	42.5		563.961	2.1	2.52	2.5	183	257	255	55	88	78	4
19	45		564.924	0.11	0.14	0.14	170	256	256	60	87	79	0
20	47.5		565.471	0.33	0.394	0.4	183	255	257	57	86	79	2
21	50		566.428	0.58	0.696	0.7	185	252	252	63	87	80	2
22	52.5		567.688	0.95	1.14	1.1	187	258	254	63	91	83	2
23	55		568.948	1.4	1.69	1.7	183	260	255	60	84	81	3
24	57.5		570.731	1.4	1.70	1.7	179	253	253	61	91	82	3
60/END			572.596	—	—	—	—	—	—	—	—	—	—

ΔV_m = 34.150 $\sqrt{\Delta p}$ = 0.9629 ΔH = 1.29 T_s = 176 T_m = 78



SAMPLE RECOVERY DATA

Plant: WLEOLC Run No.: 30-1

Date: 25 MAY 94 Sample Box No.: N-7 Job No.: 4794001

Sample Location: Baghouse Duct

Sample Type: m-s Filter No.: 32099

Sample Recovery Person: U. H.

Comments: _____

FRONT HALF

Acetone Container No.: _____ Liquid Level Marked: _____ Sealed: _____

Filter Container No.: _____ Sealed: _____

Description of Filter: _____

Samples Stored and Locked: _____

BACK HALF/MOISTURE

Container No.: _____

Liquid Level Marked: _____ Sealed: _____

IMP. NO.	CONTENTS	INITIAL VOL (ml)	WEIGHT (grams)		
			INITIAL	FINAL	NET
1	H ₂ O	100	585.9	719.1	133.2
2	H ₂ O	100	568.6	588.2	19.6
3	—		468.0	470.0	2.0
4	S/G		692.1	700.8	8.7
5					
6					
TOTAL					163.5

Description of Impinger Catch: clear H₂O

FIELD DATA SHEET

20 = 124

3621

Plant: Welding Sand & Gravel
 Sampling Location: Bughouse Outlet
 Run Number: B0-2 Date: 25 MAY 94
 Pretest Leak Rate: 100-1 cfm @ 15 in. Hg.
 Pretest Leak Check: Pitot: ✓ Orsat: ✓

Sample Type: M5 Operator: HLH-1
 Pbar: 28.85 Ps: -1.1
 CO2: 3 O2: 18
 Probe Length/Type: 5' 1/2" SS Pitot #: 5-61
 Stack Diameter: 30.15 x 24.5" As

Nozzle ID: 0.200 Thermocouple #: 566
 Assumed Bws: 18% Filter #: 30098
 Meter Box #: 15 Y: 1.019 ΔH@: 1.801
 Post-Test Leak Rate: 0.001 cfm @ 4 in. Hg.
 Post-Test Leak Check: Pitot: Orsat:

Traverse Point Number	Sampling Time (min)	Clock Time (24-hour clock)	Gas Meter Reading (Nm) ft ³	Velocity Head (Δp) in H ₂ O	Orifice Pressure Differential (ΔH) in H ₂ O		Stack Temp. (T _s)	Temperature °F		Impinger Temp. °F	Dry Gas Meter Temp. (T _m in °F)		Pump Vacuum (in. Hg)
					Desired	Actual		Probe	Filter		Inlet	Outlet (T _m out °F)	
A1	0	1150	572.689	0.11	0.12	0.12	156	256	263	65	83	83	0
2	2.5		573.189	0.23	0.245	0.25	173	257	257	56	84	83	2
3	5		573.917	0.58	0.614	0.61	177	257	253	60	85	83	2
4	7.5		575.031	0.95	1.01	1.0	176	258	252	55	85	84	2
5	10		576.481	1.50	1.6	1.5	172	253	252	51	87	84	2.5
6	12.5		578.151	1.3	1.38	1.4	180	254	253	50	84	84	2.5
B1	15		579.718	0.12	0.13	0.13	169	253	255	54	84	85	2
2	17.5		580.274	0.28	0.297	0.3	178	256	252	54	84	85	2
3	20		581.028	0.58	0.616	0.62	178	253	253	55	84	85	2
4	22.5		582.144	0.98	1.03	1.0	184	255	253	57	90	86	2
5	25		583.554	1.3	1.35	1.4	197	256	252	54	91	86	2.5
6	27.5		585.188	1.4	1.45	1.5	200	260	254	53	93	86	2.5
C1	30		586.817	0.08	0.086	0.09	170	254	253	58	92	81	0
2	32.5		587.258	0.24	0.253	0.25	187	258	253	60	92	88	2
3	35		588.013	0.47	0.493	0.49	190	259	253	60	92	88	2
4	37.5		589.927	0.82	0.857	0.86	194	254	251	60	94	88	2
5	40		590.186	1.5	1.58	1.6	189	257	253	59	94	84	2.5
6	42.5		591.928	1.4	1.48	1.5	187	257	253	56	96	84	2.5
01	45		593.583	0.06	0.06	0.06	188	256	252	60	97	90	0
2	47.5		593.981	0.13	0.14	0.14	193	256	255	63	95	90	2
3	50		594.549	0.25	0.259	0.26	199	254	253	62	95	91	2
4	52.5		595.271	0.49	0.509	0.51	200	260	255	61	95	91	2
5	55		596.338	0.75	0.774	0.77	205	255	254	61	96	91	2
6	57.5		597.434	0.90	0.921	0.9	211	259	253	60	97	91	2
60/END			598.751										

ΔV_m = 26.062 $\sqrt{\Delta p}$ = 0.7606 ΔH = 0.723 T_s = 186 T_m = 89



SAMPLE RECOVERY DATA

Plant: WIEDLE Run No.: B0-2
Date: 25 MAY 94 Sample Box No.: N-5 Job No.: 4794001
Sample Location: Baghouse outlet
Sample Type: M-5 Filter No.: 300098
Sample Recovery Person: WEISMAN
Comments: _____

FRONT HALF

Acetone Liquid
Container No.: _____ Level Marked: _____ Sealed: _____

Filter
Container No.: _____ Sealed: _____

Description of Filter: _____

Samples Stored and Locked: _____

BACK HALF/MOISTURE

Container No.: _____

Liquid Level Marked: _____ Sealed: _____

IMP. NO.	CONTENTS	INITIAL VOL (ml)	WEIGHT (grams)		
			INITIAL	FINAL	NET
1	H ₂ O	100	564.1	^{A.W.} 136 691.0	126.9
2	H ₂ O	100	607.1	618.6	11.5
3	—	—	452.0	452.4	0.4
4	S/G		631.2	636.1	4.9
5					
6					
TOTAL					143.7

Description of Impinger Catch: _____

FIELD DATA SHEET

✓ 2.98

Plant: Wendle Sand & Gravel
 Sampling Location: Bachhoux O.Het
 Run Number: B0-3 Date: 25 MAY 94
 Pretest Leak Rate: cfm @ in. Hg.
 Pretest Leak Check: Pitot: Orsat:

Sample Type: M5 Operator: Hilt
 Pbar: 28.82 Ps: 1.1
 CO2: 4 O2: 16
 Probe Length/Type: 5' 4.55 Pitot #: 56A
 Stack Diameter: 30.75 x 24.5 As:

Nozzle ID: 0.245 Thermocouple #: 56
 Assumed Bws: 18% Filter #: 300042
 Meter Box #: 15 Y: 1019 ΔH@: 1.801
 Post-Test Leak Rate: 3.001 cfm @ 6 in. Hg.
 Post-Test Leak Check: Pitot: Orsat:

Traverse Point Number	Sampling Time (min)	Clock Time (24-hour clock)	Gas Meter Reading (Nm) ft ³	Velocity Head (Ap) in H2O	Orifice Pressure Differential (ΔH) in H2O		Stack Temp. (Ts)	Temperature of		Impinger Temp. of	Dry Gas Meter Temp.		Pump Vacuum (in. Hg)
					Desired	Actual		Probe	Filter		Inlet (Tm in °F)	Outlet (Tm out °F)	
A1	0	1404	599.410	0.29	0.245	0.25	142	258	256	60	90	89	2
2	2.5		600.176	0.17	0.452	0.45	156	252	254	59	90	89	2
3	5		601.177	0.34	0.856	0.86	190	253	251	60	90	89	2
4	7.5		602.431	0.64	1.61	1.6	191	256	252	56	91	89	2.5
5	10		604.108	1.1	2.78	2.8	189	257	254	55	91	89	4
6	12.5		606.471	1.1	2.80	2.8	186	258	252	54	95	89	4
B1	15		608.778	0.09	0.235	0.24	168	255	256	60	95	90	2
2	17.5		609.453	0.22	0.568	0.57	177	254	253	57	95	90	2
3	20		610.531	0.45	1.16	1.2	181	253	252	54	95	90	2
4	22.5		612.028	0.78	2.01	2.0	182	254	252	55	97	91	3
5	25		614.062	1.3	3.35	3.4	182	252	254	54	94	92	5
6	27.5		616.438	1.4	3.62	3.6	182	251	253	60	101	92	5
C1	30		619.028	0.15	0.40	0.4	161	256	255	61	98	92	2
2	32.5		620.996	0.27	0.708	0.71	172	253	252	54	100	93	2
3	35		621.120	0.60	1.58	1.6	173	253	252	54	100	94	3
4	37.5		622.861	0.94	2.47	2.5	174	252	252	55	102	94	4
5	40		624.948	1.2	3.15	3.2	175	252	253	55	104	94	5
6	42.5		627.408	1.1	2.88	2.9	177	253	253	55	106	95	5
D1	45		629.768	0.09	0.241	0.24	164	257	255	60	104	96	2
2	47.5		630.531	0.24	0.63	0.63	171	254	252	60	102	96	2
3	50		631.578	0.456	1.47	1.5	174	252	254	61	103	96	3
4	52.5		633.338	0.86	2.27	2.3	174	260	252	57	104	97	4
5	55		635.292	1.1	2.90	2.9	174	252	253	56	106	97	4
6	57.5		637.652	1.1	2.89	2.9	177	255	253	57	107	97	4
60/EM			640.088	—	—	—	—	—	—	—	—	—	—

ΔVm = 40.678 $\sqrt{\Delta p}$ = 0.7583 ΔH = 1.73 T_s = 175

T_m = 96



SAMPLE RECOVERY DATA

Plant: WIEDER Run No.: 30-3

Date: 25 MAY 94 Sample Box No.: 10-1 Job No.: 4794.001

Sample Location: Engelmann Oak

Sample Type: MS Filter No.: 300097

Sample Recovery Person: W. ISMAN

Comments: _____

FRONT HALF

Acetone Liquid
Container No.: _____ Level Marked: _____ Sealed: _____

Filter
Container No.: _____ Sealed: _____

Description of Filter: _____

Samples Stored and Locked: _____

BACK HALF/MOISTURE

Container No.: _____

Liquid Level Marked: _____ Sealed: _____

IMP. NO.	CONTENTS	INITIAL VOL (ml)	WEIGHT (grams)		
			INITIAL	FINAL	NET
1	H ₂ O	100	570.1	714.5	144.4
2	H ₂ O	100	581.8	601.3	19.5
3	—		482.9	484.3	1.4
4	S/G		683.5	691.3	7.8
5					
6					
TOTAL					173.1

Description of Impinger Catch: _____



ISOKINETIC CALCULATION

SITE Weidle Sand & Gravel

TEST NO. 130-1, 2, 3

		RUN 1	RUN 2	RUN 3
1. Volume of dry gas sampled corrected to standard conditions. Note: V_m must be corrected for leakage if any leakage rates exceed L_g . $V_{m_{std}} = 17.65 \times V_m \times Y \left[\frac{P_{bar} + \frac{\Delta H}{13.6}}{T_m} \right] =$	V_m, ft^3	<u>34.150</u>	26.062	40.678
	Y	<u>1.019</u>	1.014	1.019
	$P_{bar}, in.Hg$	<u>29.23</u>	28.85	28.82
	$\Delta H, in.H_2O$	<u>1.29</u>	0.723	1.73
	$T_m, ^\circ R$	<u>538.</u>	549	556
	$V_{m_{std}}, dscf$	<u>33.48</u>	24.638	38.09 47.3
2. Volume of water vapor at standard conditions, ft^3 . $V_{w_{std}} = 0.04707 V_{lc} =$	V_{lc}, g	<u>163.5</u>	143.7	173.1
	$V_{w_{std}}, ft^3$	<u>7.69</u>	6.76	8.15
3. Moisture content in stack gas. $B_{ws} = \frac{V_{w_{std}}}{(V_{m_{std}} + V_{w_{std}})} =$	B_{ws}	<u>0.188</u>	0.215	0.167
	$1-B_{ws}$	<u>0.812</u>	0.785	0.833
4. Dry molecular weight of stack gas, lb/lb-mole. $M_d = 0.440 (\% CO_2) + 0.320 (\% O_2) + 0.280 (\% N_2 + \% CO) =$	$\% CO_2$	<u>3.0</u>	3	4
	$\% O_2$	<u>18.0</u>	18	16
	$\% N_2 + \% CO$	<u>79.0</u>	79	80
	$M_d, lb/lb-mole$	<u>29.20</u>	29.2	29.28
5. Molecular weight of stack gas. $M_s = M_d (1-B_{ws}) + 18 B_{ws} =$	$M_s, lb/lb-mole$	<u>27.18</u>	26.79	27.01
6. Stack velocity at stack conditions, fps. $V_s = 85.49 C_p \left(\text{avg. } \sqrt{\Delta P} \right) \sqrt{\frac{T_s}{P_s M_s}} =$ NOTE: $P_s = P_{bar} + \left(\frac{P_{range}}{13.6} \right)$	$P_{static}, in.H_2O$	<u>1.1</u>	-1.1	-1.1
	$P_s, in.Hg$	<u>29.15</u>	28.77	28.74
	$T_s, ^\circ R$	<u>636.</u>	646	635
	$\sqrt{\Delta P}$	<u>0.9629</u>	0.7606	0.7583
	C_p	<u>0.84</u>	0.84	0.84
	V_s, fps	<u>61.95</u>	50.00	49.25
	$D_n, in.$	<u>2.00 0.2</u>	0.2	0.245
	$\theta, min.$	<u>60.</u>	60	60
7. Isokinetic variation $\% I = \frac{V_{m_{std}} \times T_s \times 17.32}{V_s \times D_n \times \theta \times P_s \times (1-B_{ws})}$	$\% I$	<u>104.8</u>	101.7	98.7



PROJECT ANALYTICAL SHEET

SITE: Widite Sand & Gravel RUN NO.: B0-2

FILTER NO.: 300099 I.D. NO.: 94-312

FINAL MASS: TARE MASS: 341.8

DATE/TIME	NAME	MASS
#1 <u>3/2/94</u> <u>1027</u>	<u>Uity</u>	<u>341.8</u>
#2 <u>6/7/94</u> <u>1513</u>	<u>DJM</u>	<u>341.9</u>
#3 _____	_____	_____
#4 _____	_____	_____

AVG. MASS: 341.9

NET GAIN: 0.1

F/H BEAKER NO.: 235 I.D. NO.: 94-313

FINAL MASS: TARE MASS: 111,542.1

DATE/TIME	NAME	MASS
#1 <u>3/2/94</u> <u>1028</u>	<u>Uity</u>	<u>111,542.1</u>
#2 <u>6/7/94</u> <u>1523</u>	<u>DJM</u>	<u>111,544.6</u>
#3 <u>6/8/94</u> <u>0853</u>	<u>DJM</u>	<u>111,544.6</u>
#4 _____	_____	_____

AVG. MASS: 111,544.6

NET GAIN: 2.5

B/H BEAKER NO.: 239 I.D. NO.: 94-314

FINAL MASS: TARE MASS: 110,383.2

DATE/TIME	NAME	MASS
#1 <u>6/7/94</u> <u>1523</u>	<u>DJM</u>	<u>110,384.9</u>
#2 <u>6/8/94</u> <u>0854</u>	<u>DJM</u>	<u>110,385.3</u>
#3 _____	_____	_____
#4 _____	_____	_____

AVG. MASS: 110,385.1

NET GAIN: 1.9



PROJECT ANALYTICAL SHEET

SITE: Windle Sand & Gravel

RUN NO.: B-2

FILTER NO.: 300078

I.D. NO.: 94-315

FINAL MASS:

TARE MASS: 336.85

DATE/TIME

NAME

MASS

#1 3 JUN 94 / 1040 1048

Hilty

337.1

#2 6/7/94 1515

DJM

337.0

#3 _____

#4 _____

AVG. MASS: 337.1

NET GAIN: 0.2

F/H BEAKER NO.: 241

I.D. NO.: 94-316

FINAL MASS:

TARE MASS: 109,148.1

DATE/TIME

NAME

MASS

#1 43 JUN 94 / 1042

Hilty

109,150.8

#2 6/7/94 1521

DJM

109,151.9

#3 6/8/94 0855

DJM

109,152.3

#4 _____

AVG. MASS: 109,152.1

NET GAIN: 4.0

B/H BEAKER NO.: 243

I.D. NO.: 94-317

FINAL MASS:

TARE MASS: 109,754.65
~~109,745.65~~ DJM

DATE/TIME

NAME

MASS

#1 6/7/94 1520

DJM

109,757.0

#2 6/8/94 0856

DJM

109,756.7

#3 _____

#4 _____

AVG. MASS: 109,756.9

NET GAIN: 2.2



PROJECT ANALYTICAL SHEET

SITE: Wedge Sand & Gravel

RUN NO.: B0-3

FILTER NO.: 300077

I.D. NO.: 94-318

FINAL MASS:

TARE MASS: 114.50 339.5

DATE/TIME

NAME

MASS

#1 3 Jun 94 / 1046

U.Ily

339.9

#2 6/7/94 1517

DJM

339.8

#3

#4

AVG. MASS: 339.9

NET GAIN: 0.4

F/H BEAKER NO.: 240

I.D. NO.: 94-319

FINAL MASS:

TARE MASS: 114.50 95

DATE/TIME

NAME

MASS

#1 3 Jun 94 / 1044

U.Ily

114,514.0

#2 6/7/94 1518

DJM

114,515.4

#3 6/8/94 0859

DJM

114,515.5

#4

AVG. MASS: 114,515.5

NET GAIN: 5.5

B/H BEAKER NO.: 248

I.D. NO.: 94-320

FINAL MASS:

TARE MASS: 106,714.7

DATE/TIME

NAME

MASS

#1 6/7/94 1519

DJM

106,716.8

#2 6/8/94 0858

DJM

106,716.9

#3

#4

AVG. MASS: 106,716.7

NET GAIN: 2.0

PRODUCTION CALCULATIONS

RUN 1

Total Production during test - 99 tons
Time to conduct test - 1 hour, 10 minutes

$$\frac{99 \text{ tons}}{1.166 \text{ hours}} = 84.86 \text{ tons/hour}$$

$$\text{Emission rate} = 0.131 \text{ lb/hr}$$

$$\frac{0.131 \text{ lb/hr}}{84.86 \text{ ton/hr}} = 0.0015 \text{ lb/ton}$$

RUN 2

Total Production during test - 104 tons
Time to conduct test - 1 hour, 15 minutes

$$\frac{104 \text{ tons}}{1.25 \text{ hours}} = 83.20 \text{ tons/hour}$$

$$\text{Emission rate} = 0.218 \text{ lb/hr}$$

$$\frac{0.218 \text{ lb/hr}}{83.20 \text{ ton/hr}} = 0.0026 \text{ lb/ton}$$

RUN 3

Total Production during test - 94 tons
Time to conduct test - 1 hour, 15 minutes

$$\frac{94 \text{ tons}}{1.25 \text{ hours}} = 75.20 \text{ tons/hour}$$

$$\text{Emission rate} = 0.207 \text{ lb/hr}$$

$$\frac{0.207 \text{ lb/hr}}{75.20 \text{ ton/hr}} = 0.0028 \text{ lb/ton}$$

first-2m

CUSTOMER NAME Weidle Sand & Gravel #
ATE 5/25/94 JOB # Pes JOB NAME Stack test

Start time - 9:30

D-3

TOTAL TON: 99

PRICE PER TON: _____

Second Key

Zef 3

RUCK #	MATERIAL	TONS
--------	----------	------

Start Time 11:45

D-4

TOTAL TON: 104

PRICE PER TON: _____

21-11-42

last Run

*****3083*****

RUCK #	MATERIAL	TONS
1	1000	1000
2	1000	1000
3	1000	1000
4	1000	1000
5	1000	1000
6	1000	1000
7	1000	1000
8	1000	1000
9	1000	1000
10	1000	1000
11	1000	1000
12	1000	1000
13	1000	1000
14	1000	1000
15	1000	1000
16	1000	1000
17	1000	1000
18	1000	1000
19	1000	1000
20	1000	1000
21	1000	1000
22	1000	1000
23	1000	1000
24	1000	1000
25	1000	1000
26	1000	1000
27	1000	1000
28	1000	1000
29	1000	1000
30	1000	1000
31	1000	1000
32	1000	1000
33	1000	1000
34	1000	1000
35	1000	1000
36	1000	1000
37	1000	1000
38	1000	1000
39	1000	1000
40	1000	1000
41	1000	1000
42	1000	1000
43	1000	1000
44	1000	1000
45	1000	1000
46	1000	1000
47	1000	1000
48	1000	1000
49	1000	1000
50	1000	1000
51	1000	1000
52	1000	1000
53	1000	1000
54	1000	1000
55	1000	1000
56	1000	1000
57	1000	1000
58	1000	1000
59	1000	1000
60	1000	1000
61	1000	1000
62	1000	1000
63	1000	1000
64	1000	1000
65	1000	1000
66	1000	1000
67	1000	1000
68	1000	1000
69	1000	1000
70	1000	1000
71	1000	1000
72	1000	1000
73	1000	1000
74	1000	1000
75	1000	1000
76	1000	1000
77	1000	1000
78	1000	1000
79	1000	1000
80	1000	1000
81	1000	1000
82	1000	1000
83	1000	1000
84	1000	1000
85	1000	1000
86	1000	1000
87	1000	1000
88	1000	1000
89	1000	1000
90	1000	1000
91	1000	1000
92	1000	1000
93	1000	1000
94	1000	1000
95	1000	1000
96	1000	1000
97	1000	1000
98	1000	1000
99	1000	1000
100	1000	1000

# Z	404	14
# 95	"	"
# i	"	"
# Z	"	"
# 95	"	"
# Z	"	"

Stop time 3:15	(Not Bins)	$\frac{10}{94}$

TOTAL TON: 94

PRICE PER TON: _____

24

POSTTEST DRY GAS METER CALIBRATION

MB #: 15 BAROMETRIC PRESS. 29.91 (in. hg.)
 DATE: 5-26-94 PERFORMED BY: G GAY
 PLANT: WIEDEL PRETEST Y : 1.020
 PRETEST ΔH@: 1.801

	RUN 1 -----	RUN 2 -----	RUN 3 -----
VACUUM ("Hg)	6.00	6.00	6.00
ΔH ("H2O)	1.10	1.10	1.10
INITIAL RTM	229.342	235.236	241.113
FINAL RTM	235.236	241.113	246.989
INITIAL DGM	687.310	693.149	699.070
FINAL DGM	693.149	699.070	704.809
TEMP. RTM (F)	76.0	77.0	78.0
TEMP. DGM (F)	84.0	85.0	87.0
TEST TIME (MIN.)	10.0	10.0	10.0

NET VOLUME RTM	5.894	5.877	5.876
NET VOLUME DGM	5.839	5.921	5.739
Y	1.022	1.005	1.038
ΔH@	1.772	1.786	1.787

PRIOR Y = 1.020
 RECHECK Y = 1.022
 % DIFFERENCE = 0.168

AVERAGE ΔH@ = 1.782

$Y = (V_w \times P_b \times (T_d + 460)) / (V_d (P_b + (dH_d / 13.6)) \times (T_w + 460))$

$\Delta H@ = 0.0317 \times \Delta H / (P_b (T_d + 460)) \times ((T_w + 460) \times \text{time}) / V_w)^2$

PITOT TUBE CALIBRATION DATA SHEET

Calibrated By: PAUL SIEGEL

Date: 2-8-94

Pitot I.D. No.: 5-100

Effective Length: 104" - 5-14"

Pitot Tube Assembly Level? Yes ☒ No ☐

Pitot Tube Openings Damaged? Yes (explain below) ☐ No ☒

$\alpha_1 =$ 2 $^\circ$ ($<10^\circ$)

$\alpha_2 =$ 0 $^\circ$ ($<10^\circ$)

$\beta_1 =$ 1 $^\circ$ ($<5^\circ$)

$\beta_2 =$ 1 $^\circ$ ($<5^\circ$)

$\gamma =$ 0 $^\circ$

$\theta =$ 0 $^\circ$

$A =$ 1.128 $^\circ$

$z = A \sin \gamma =$ 0 cm (in.) 0.32 cm ($<1/8$ in.)

$w = A \sin \theta =$ 0 cm (in.) 0.08 cm ($<1/32$ in.)

$P_A =$ 0.563 cm (in.)

$P_B =$ 0.565 cm (in.)

$D_t =$ 0.375 cm (in.)

Comments: _____

Calibration Required? Yes ☐ No ☒

TEMPERATURE SENSOR CALIBRATION DATA FORM

Date 1/6/94 Thermocouple number S-6e
 Ambient temperature 75 °F Barometric pressure 29.05 in Hg
 Calibrator Rings Reference: mercury-in-glass ✓
 other _____

Reference point number ^a	Source ^b (specify)	Reference thermometer temperature, °F	Thermocouple potentiometer temperature, °F	Temperature difference, °C %
1	Ambient	75	74	.18
2	Cold H ₂ O	38	39	.20
3	Hot H ₂ O	206	210	.60
4	Hot Oil	418	419	.11

^aEvery 30°C (50° for each reference point).

^bType of calibration system used.

^c
$$\left[\frac{(\text{ref temp, } ^\circ\text{F} + 460) - (\text{test thermom temp, } ^\circ\text{F} + 460)}{\text{ref temp, } ^\circ\text{F} + 460} \right] 100 \leq 1.5\%.$$