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Reference:	25
Title:	<i>Stationary Source Sampling Report Reference No. 14448, Triangle Brick, Merry Oaks, North Carolina, Emissions Testing For: Carbon Monoxide, Condensable Particulate, Metals, Methane, Nitrogen Oxides, Particulate, Particulate # 10 Microns, Sulfur Dioxide, Total Hydrocarbons, Entropy, Inc., Research Triangle Park, NC, October, 1995.</i>

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STATIONARY SOURCE SAMPLING REPORT

REFERENCE NO. 14448

TRIANGLE BRICK
MERRY OAKS, NORTH CAROLINA

EMISSIONS TESTING FOR:
CARBON MONOXIDE
CONDENSIBLE PARTICULATE
METALS
METHANE
NITROGEN OXIDES
PARTICULATE
PARTICULATE $\leq$ 10 MICRONS
SULFUR DIOXIDE
TOTAL HYDROCARBONS

BRICK KILN NO. 2 STACK

PERFORMED FOR: WITHERS & RAVENEL ENVIRONMENTAL ENGINEERING, INC.

OCTOBER, 1995

CONTACT REPORT--MRI Project No. 4603-01

From: Brian Shrager, Environmental Engineering
Department

Date of Contact: June 25, 1996

Contacted by: Telephone

Company/Agency: Withers and Ravenel
Cary, NC

Telephone Number: (919) 460-6006

Person(s) Contacted/Title(s)

Bill Colby

CONTACT SUMMARY: Mr. Colby was contacted to determine the production rate for the emission test conducted at Triangle Brick in Merry Oaks, NC for the Brick Institute of America. He no longer works at Withers and Ravenel; he moved to New Hampshire, and his new phone number is (603) 623-3600. The process rate was not readily available, but Mr. Colby provided emission factors for several pollutants measured during the test, and I subsequently calculated a process rate of **10.56 tons of brick produced per hour**. This process rate was constant throughout testing, and was confirmed for three different emission factors provided by Mr. Colby. He did not have any documentation of the production rates, but stated that they were measured by weighing several fired bricks and multiplying by the total number of bricks produced.

REPORT CERTIFICATION

El Reference Number 14448

The sampling and analysis performed for this report were carried out under my direction and supervision, and I hereby certify that the test report is authentic and accurate.

Signature:

Vincent Jude Tomaino

Date:

4/16/95

Vincent Jude Tomaino
Project Director
Chemical and Manufacturing Services Division

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1.0 INTRODUCTION

1.1 Background

Testing was performed at the Triangle Brick facility in Merry Oaks, North Carolina to determine emission factors to be used by the Brick Association of North Carolina. During the testing, the brick kiln fired a brick which is common to many other brick manufacturing facilities and which has no facing material or other additives. The emissions measured originated either from the combustion of natural gas or from the bulk of the brick itself.

The actual feed rate (lb-brick/hr) was continuously monitored throughout the testing program. No facing materials or other additives were supplied to the bricks during this period.

1.2 Outline of Test Program

Table 1-1 is a test log which presents the sampling locations, sampling objectives, sampling methods, test dates, and run numbers for the test program. Several runs utilized volumetric air flow rates and/or flue gas composition data from other runs; refer to Table 1-1.

**TABLE 1-1
TEST LOG
BRICK KILN NO. 2 STACK
OCTOBER, 1995**

Sampling Objective	Test Method	Test Date	Run Numbers	Flue Gas Composition	Volumetric Air Flow Rate
Metals	EPA 29	10/17	S-M29-1	S-M29/M3-1	NA
		10/17	S-M29-2	S-M29/M3-2	
		10/17	S-M29-3	S-M29/M3-3	
SO ₂ , NO _x , CO, & THC	EPA 6C, 7E, 10, & 25A	10/17	S-CEM-1	NA	S-M29-1
		10/17	S-CEM-2		S-M29-2
		10/17	S-CEM-3		S-M29-3
Particulate	EPA 5	10/18	S-M5-1	S-M5/M3-1	NA
		10/18	S-M5-2	S-M5/M3-2	
		10/18	S-M5-3	S-M5/M3-3	
Particulate ≤ 10 _μ & Condensable Particulate	EPA 201A & 202	10/18	S-M201A/202-1	S-M5/M3-1	NA
		10/18	S-M201A/202-2	S-M5/M3-2	
		10/18	S-M201A/202-3	S-M5/M3-3	

1.3 Test Participants

Table 1-2 lists the personnel involved in the test program.

TABLE 1-2
TEST PARTICIPANTS
OCTOBER, 1995

460-4004

Withers & Ravenel Environmental Engineering, Inc.	William G. Colby Test Coordinator
Entropy, Inc.	Vincent Jude Tomaino Project Director
	Dennis D. Holzschuh Project Manager
	Joseph P. Daley Sampling Team Leader
	Julie R. Ruff Sampling Team Leader
	Dan Wise Engineering Technician
	Joseph R. Winslow Laboratory Technician

2.0 SUMMARY OF RESULTS

2.1 Presentation

Table 2-1 presents the test results versus the permitted limits. Table 2-2 presents additional test concentrations. Detailed test results are presented in **Appendix A**; field data are given in **Appendix B**; and analytical data can be found in **Appendix C**.

2.2 Cyclonic Flow Checks

A cyclonic flow check was performed at the sampling location to determine if any cyclonic flow existed. An average yaw angle of $< 8^\circ$ was measured, indicating an acceptable location with respect to EPA Method 1 requirements.

2.3 Metals Results

The reagent blank analytical results for antimony, arsenic, chromium, manganese, and nickel were as follows:

<u>Metal</u>	<u>Blank (μg)</u>
Antimony	1.45
Arsenic	3.49
Chromium	1.73
Manganese	1.27
Nickel	1.06

In accordance with Section 3.1.8.4.3 of the method, the runs' analytical results were adjusted to account for the reagent blank results. The adjusted results were used in the concentration and emission rate calculations.

2.4 Orsat Analyses

Twenty-seven (27) consecutive identical Orsat analyses were conducted, yielding 2.4% CO_2 and 16.6% O_2 . These Orsat analyses did not agree with the Fyrite analyses of approximately 5% CO_2 . The causes of these differences were explored on-site. Orsat measurements and re-analyses were witnessed by Mr. John Brown of USEPA, and the results confirmed. A leak-check was performed of the Orsat sampling line with no leak found. No explanation of these unusual results have been found. In any case, any possible error in the measurement of O_2 and CO_2 would only have a small effect on the calculated flow rates and emission rates.

TABLE 2-1
TEST RESULTS VERSUS PERMITTED LIMITS
EMISSION RATE, LB/HR
BRICK KILN NO. 2 STACK
OCTOBER, 1995

	Rep 1	Rep 2	Rep 3	Average	Permit Limit
Emission Rate, lb/hr					
Carbon Monoxide	6.19	5.96	6.14	6.09	15.95
Nitrogen Oxides as NO ₂	1.31	1.34	1.34	1.33	8.70
Sulfur Dioxide	0.778	0.623	0.587	0.663	7.25
Methane	< 0.0756	< 0.0710	< 0.0706	< 0.0724	--
Total Hydrocarbons as C	0.585	0.600	0.616	0.600	--
Total Non-Methane Hydrocarbons as C	0.585	0.600	0.616	0.600	1.35
Filterable Particulate	0.367	0.330	0.414	0.370	5.08
Particulate ≤ 10 Microns	0.561	0.477	0.528	0.522	1.74
Condensable Particulate	1.54	2.07	2.10	1.90	--
Metals					
Antimony	0.0	3.40 E-05	1.99 E-03	6.75 E-04	--
Arsenic	8.03 E-05	1.20 E-04	5.25 E-04	2.42 E-04	--
Beryllium	< 4.39 E-06	< 4.41 E-06	< 4.73 E-06	< 4.51 E-06	0.0
Cadmium	3.48 E-05	7.46 E-05	7.34 E-05	6.09 E-05	4.79 E-04
Chromium	1.82 E-04	2.40 E-04	2.41 E-04	2.21 E-04	1.09 E-01
Cobalt	< 4.39 E-05	< 4.41 E-05	< 4.73 E-05	< 4.51 E-05	1.60 E-03
Lead	1.41 E-04	1.29 E-04	2.48 E-03	9.17 E-04	1.15 E-03
Manganese	1.05 E-03	8.25 E-04	8.09 E-04	8.95 E-04	--
Mercury	< 1.03 E-04	< 1.04 E-04	< 1.11 E-04	< 1.06 E-04	--
Nickel	1.57 E-04	2.04 E-04	4.64 E-05	1.36 E-04	--
Selenium	4.83 E-04	4.48 E-04	4.27 E-04	4.53 E-04	--

TABLE 2-2
TEST CONCENTRATIONS SUMMARY
BRICK KILN NO. 2 STACK
OCTOBER, 1995

	Rep 1	Rep 2	Rep 3	Average
Concentration, ppmvd				
Carbon Monoxide	92.8	91.8	95.6	93.4
Nitrogen Oxides as NO ₂	12.0	12.6	12.7	12.4
Sulfur Dioxide	5.10	4.20	4.00	4.43
Methane	< 1.98	< 1.91	< 1.92	< 1.94
Total Hydrocarbons as C	20.5	21.6	22.4	21.5
Total Non-Methane Hydrocarbons as C	20.5	21.6	22.4	21.5
Concentration, gr/DSCF				
Filterable Particulate	0.00293	0.00246	0.00325	0.00288
Particulate ≤ 10 Microns	0.00447	0.00380	0.00422	0.00416
Condensable Particulate	0.0122	0.0165	0.0168	0.0152
Metals				
Antimony	0.0	2.67 E-07	1.58 E-05	5.36 E-06
Arsenic	6.13 E-07	9.42 E-07	4.16 E-06	1.91 E-06
Beryllium	< 3.35 E-08	< 3.46 E-08	< 3.75 E-08	< 3.52 E-08
Cadmium	2.65 E-07	5.85 E-07	5.82 E-07	4.77 E-07
Chromium	1.39 E-06	1.88 E-06	1.91 E-06	1.73 E-06
Cobalt	< 3.35 E-07	< 3.46 E-07	< 3.75 E-07	< 3.52 E-07
Lead	1.08 E-06	1.01 E-06	1.96 E-05	7.23 E-06
Manganese	8.01 E-06	6.47 E-06	6.42 E-06	6.97 E-06
Mercury	< 7.87 E-07	< 8.13 E-07	< 8.82 E-07	< 8.27 E-07
Nickel	1.20 E-06	1.60 E-06	3.68 E-07	1.06 E-06
Selenium	3.68 E-06	3.51 E-06	3.39 E-06	3.53 E-06

3.0 PROCESS DESCRIPTION AND OPERATION

3.1 General

Triangle Brick in Merry Oaks, North Carolina operates a brick kiln. Brick Kiln No. 2 is a tunnel brick kiln designed to fire 29,000 lb/hr of triassic shale bricks. The kiln was fired utilizing only natural gas during the testing. No control equipment is installed on the kiln exhaust. The testing covered in this report was performed at the Brick Kiln No. 2 Stack.

3.2 Source Air Flow

Figure 3-1 is an air flow schematic which shows the passage of flue gases exhausted from the kiln.

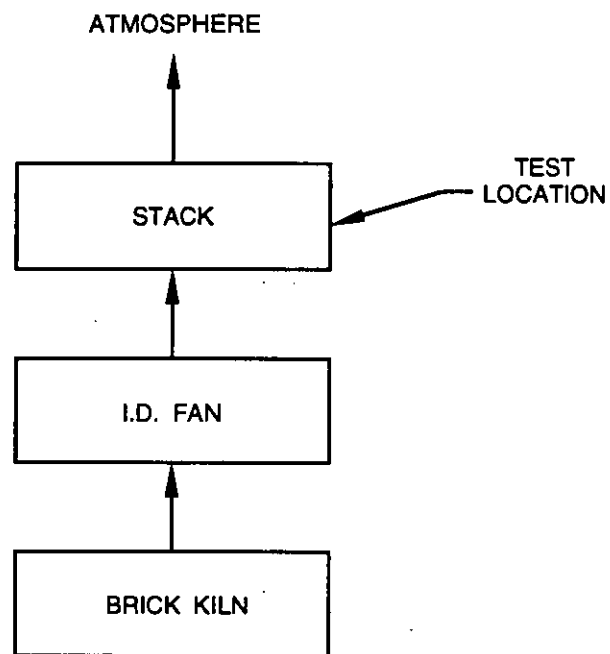


FIGURE 3-1. BRICK KILN NO. 2 AIR FLOW SCHEMATIC

4.0 SAMPLING AND ANALYTICAL PROCEDURES

4.1 General

All sampling and analytical procedures were those recommended by the United States Environmental Protection Agency and the North Carolina Department of Environment, Health, and Natural Resources. This section provides brief descriptions of the sampling and analytical procedures.

4.2 Sampling Points

The number and location of the sampling points were determined according to the procedures outlined in EPA Method 1. As shown in **Figure 4-1**, the stack cross section was divided into 24 equal areas with 12 sampling points on each of two axes.

4.3 Cyclonic Flow Check

A Type S Pitot tube assembly, Magnehelic gauges, and a universal protractor (angle finder) were used to determine the flow angles at each of the sampling or velocity traverse points. At each point, the Pitot tube was positioned at a right angle to the air flow. The angles were determined by rotating the Pitot tube until a null reading was obtained on the Magnehelic gauges. When the null reading was obtained, the angle of the Pitot tube was recorded.

4.4 Volumetric Air Flow Rates

4.4.1 Flue Gas Velocity

The flue gas velocity and volumetric flow rate were determined according to the procedures outlined in EPA Method 2. Velocity head measurements (ΔP) were made using Type S Pitot tubes conforming to the geometric specifications outlined in EPA Method 2. Accordingly, each has been assigned a coefficient of 0.84. Differential pressures were measured with Magnehelic gauges of appropriate range. Flue gas temperatures were measured with chromel-alumel thermocouples equipped with hand-held digital readouts.

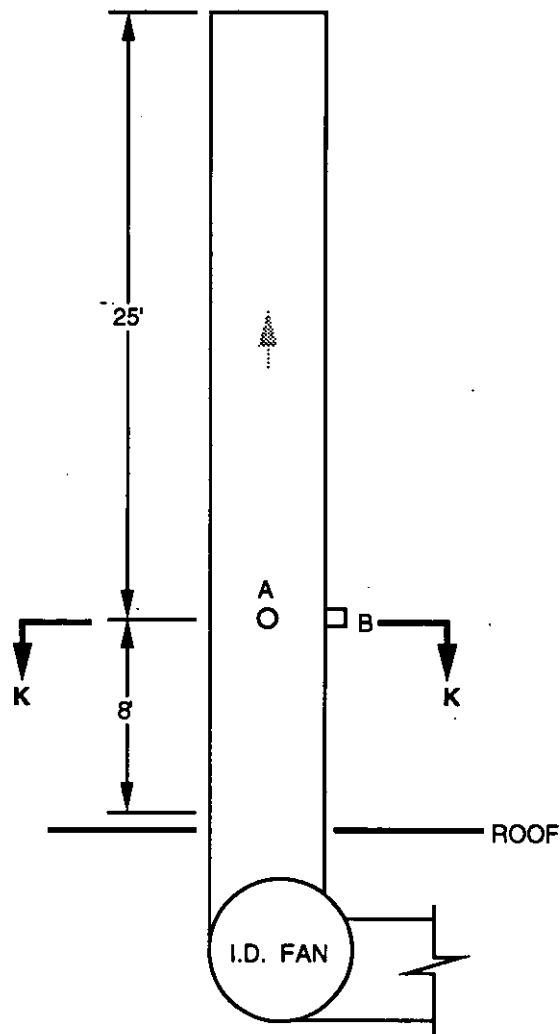
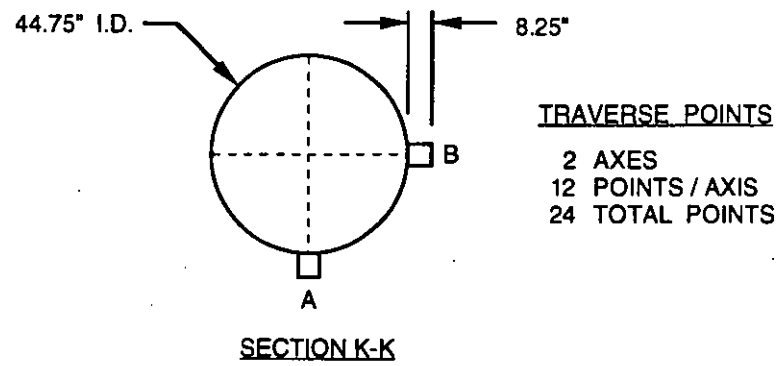


FIGURE 4-1. BRICK KILN NO. 2 STACK TEST LOCATION

4.4.2 Flue Gas Composition

Sample Collection. Flue gas samples were collected using the multipoint, integrated sampling technique outlined in EPA Method 3. A stainless steel probe and a peristaltic pump delivering 500 to 750 mL/min of flue gas were used to fill a Tedlar bag. Moisture was removed by means of a knockout jar located prior to the pump. Sampling was of the same duration (except purges following port changes) as the pollutant emissions runs.

Sample Analysis. Analysis for carbon dioxide and oxygen was performed using an Orsat apparatus. The analytical results were used to determine the flue gas composition, molecular weight, excess air, and emissions correction factor.

4.4.3 Flue Gas Moisture Content

The moisture content was determined in conjunction with the appropriate pollutant emissions methods discussed in the following sections.

4.5 Emissions Determinations

4.5.1 Carbon Monoxide, Sulfur Dioxide, Nitrogen Oxides, and Total Hydrocarbons

Continuous emissions monitoring (CEM) was conducted for sulfur dioxide (SO₂), nitrogen oxides (NO_x), carbon monoxide (CO), and total hydrocarbons (THC) emissions. The sampling and analytical procedures for SO₂, NO_x, CO, and THC were in accordance with EPA Methods 6C, 7E, 10, and 25A, respectively.

The extractive monitors require that the effluent gas sample be conditioned to eliminate any possible interference (i.e., water vapor and/or particulate matter) before being transported and injected into each analyzer. All components of the sampling system which contacted the sample were constructed of Type 316 stainless steel or Teflon. The outputs from the monitors were connected to a computerized data acquisition system (DAS).

The SO₂, NO_x, and CO sample collection system consisted of a heated probe with an in-stack glass wool particulate filter, heated sample lines, a moisture removal trap, an out-of-stack secondary particulate filter, and a pump. The THC sample collection system was the same except no moisture removal trap or secondary particulate filter were used. All samples were routed through a distribution manifold board for delivery to the analyzers. The configuration of the sampling system allows for the injection of calibration gases directly to the analyzers or through the sampling system. All pretest and posttest calibration procedures were performed as outlined in the specific EPA methods. The operation of each analyzer and the DAS are described below.

Thermo Environmental Instrument Model 48/GFC CO Analyzer. The analyzer utilizes the gas filter correlation (GFC) technique to determine CO concentrations. The GFC technique involves the use of a high CO concentration filter which, when inserted into the infrared light beam, produces a reference beam, i.e., no further infrared radiation can be attenuated by the CO in the effluent sample. The CO filter is located on a modulated copper wheel which allows the use of a single infrared source and detector. A multiple pass optical bench/sample chamber of the white cell design provides improved sensitivity with a smaller chamber length.

Thermo Environmental Instrument Model 10 NO/NO_x Analyzer. This analyzer automatically and continuously determines the concentration of the nitric oxide (NO) or nitrogen oxides (NO_x) in the effluent. The analytical technique is chemiluminescence. The sample is routed through a converter where the NO₂ is dissociated to form NO. The sample is then passed through a reaction chamber where the NO is quantitatively converted to NO₂ by gas phase oxidation with molecular ozone produced within the analyzer. In this reaction, the NO₂ molecules are elevated to an electronically excited state and immediately reverted to a nonexcited ground state. This reversion is accompanied by the emission of photons, which impinge on a photomultiplier detector and generate a low level DC current. The current is then amplified and used to drive a front panel meter and a data recorder. The NO_x concentration seen by the instrument includes the contributions of both the NO in the sample and the NO resulting from the dissociation of the NO₂ in the sample.

Western Research Model 721AT2 SO₂ Analyzer. This analyzer provides continuous analysis of SO₂ in a gas stream. The basic analytical principle involves quantitative measurement of the absorption of UV radiation by SO₂ molecules. The analyzer uses a single light source which emits an appropriate wavelength, illuminating a cell through which the sample is continuously passed. Narrow band optical filters are rotated through the beam, and the radiation passed is detected by a single photodetector. The signal pulses from the photodetector are separated by a demultiplexor into a measuring channel and a reference channel. A log ratio amplifier computes the logarithm of the ratio of the input signals, producing a signal that is proportional to the concentration of the SO₂. An isolated 4-20 mA output signal is provided. In addition, SO₂ concentrations are displayed on the front panel digital display meter. Measurement ranges are 0-300 ppm and 0-2,000 ppm.

Ratfisch Model RS-55 THC Analyzer. This analyzer automatically and continuously monitors the THC concentrations in a flowing gas mixture. The theory of operation is based on the principle of flame ionization detection. In the flame ionization detector, hydrogen is mixed with the sample gas and is burned in a small jet. The ionization current in the hydrogen flame is measured. In a pure hydrogen flame, very few ions are produced, but if an organic component or hydrocarbon is burned in the flame, the ion current is greatly increased. The current provides a

quantitative measure of the amount of hydrocarbons in the flame. The current is converted to a voltage output. The hydrogen flame ionization detector is extremely sensitive and is capable of detecting hydrocarbon levels in the low parts per million range and is insensitive to inorganic gases such as nitrogen, carbon dioxide, and water vapor.

Data Acquisition System. The DAS uses an IBM-compatible computer with hard disk storage and an internal 12-bit analog-to-digital converter with a 16-channel multiplexer. In addition to providing an instantaneous display of analyzer responses, the DAS compiles the analyzer data collected once each second and averages them, calculates emission rates, and documents analyzer calibrations. The DAS integrates the real-time measurements and provides printouts of 1-minute, 15-minute, and 60-minute averaged emissions.

4.5.2 Metals

Sample Collection. Samples were withdrawn isokinetically from the source using an EPA Method 29 sampling train. The sampling train consisted of a glass nozzle, a heated glass probe with a Type S Pitot tube attached, a filter, seven chilled impingers, and a metering console. The particulate sample was collected on a Pallflex 2500QAT-UP quartz filter maintained at a temperature of $248^{\circ}\text{F} \pm 25^{\circ}\text{F}$. The first impinger remained empty, the second and third impingers each contained 100 mL of 5% nitric acid (HNO_3)/10% hydrogen peroxide (H_2O_2), the fourth remained empty, the fifth and sixth impingers each contained 100 mL of 4% potassium permanganate (KMnO_4)/10% sulfuric acid (H_2SO_4), and the seventh contained preweighed silica gel. Each of the 24 points was sampled for 2.5 minutes, resulting in net run times of 60 minutes.

Sample Recovery. A Teflon spatula and Teflon coated tweezers were used to remove the filter from the filter holder and place it in a 250 mL glass jar. The reagents were returned to the original bottles, weighed, the weights recorded on the labels, and the liquid levels marked. The silica gel was returned to the original container, weighed, and the weight recorded on the label. The volume of water vapor condensed in the impingers and the volume of water vapor collected in the silica gel were summed and entered into moisture content calculations.

The nozzle, probe, and fronthalf of the filter holder were rinsed with 100 mL of 0.1N HNO_3 into a 500 mL glass jar. A Teflon probe brush was used for cleaning the probe.

The backhalf of the filter holder and the first, second, and third impingers were rinsed with 100 mL of 0.1N HNO_3 into the bottle containing the $\text{HNO}_3/\text{H}_2\text{O}_2$ reagent. The fourth impinger was rinsed with 100 mL of 0.1N HNO_3 into a 500 mL glass jar. The fifth and sixth impingers were rinsed with 100 mL of acidified KMnO_4 followed by a rinse with 100 mL of DI water into the 500 mL bottle containing the $\text{KMnO}_4/\text{H}_2\text{SO}_4$ reagent. To remove residual brown deposits, the fifth and sixth impingers were rinsed with 25 mL of 8N HCl into a 500 mL glass jar containing 200 mL of water.

Sample Analyses. The fronthalf HNO_3 rinse was evaporated to near dryness in a Teflon beaker. The filter, loose particulate, 3 mL of concentrated HNO_3 , and 5 mL of concentrated HF were added to the beaker. The sample was digested on a hotplate until brown fumes were evident, indicating the destruction of organic matter. After the addition of concentrated HNO_3 , the reagent and impinger rinses were evaporated to near dryness in a Teflon beaker on a hotplate. After cooling, 3 mL of concentrated HNO_3 and 5 mL of concentrated HF were added to the beaker and the sample was fumed on a hotplate to destroy organic residue. The prepared filter and $\text{HNO}_3/\text{H}_2\text{O}_2$ reagent samples were combined, brought to a final volume of 100 mL with 10% HNO_3 , and analyzed for all metals with a Perkin Elmer 3030 atomic absorption analyzer using the appropriate SW-846 methods. Cold vapor atomic absorption (CVAA) techniques were used to analyze the samples for mercury. The fourth impinger rinse, $\text{KMnO}_4/\text{H}_2\text{SO}_4$ reagent/rinse, and the HCl rinse were also analyzed for mercury by CVAA. Duplicate analyses were performed for approximately 10% of the emissions samples for all metals except mercury. For mercury, all samples were analyzed in duplicate.

4.5.3 Methane

Sample Collection. Flue gas samples were collected using the single-point, integrated sampling technique. A peristaltic pump delivering 500 to 750 mL/min of flue gas was used to fill a Tedlar bag. Moisture was removed by means of a knockout jar located prior to the pump. The sample was collected at a point approximately in the centroid of the cross section.

Sample Recovery. The Tedlar bag sample was transferred to an evacuated stainless steel tank to prevent any sample degradation that might occur during transport to the laboratory for analysis.

Sample Analysis. Sample analysis was performed according to EPA Method 18 with a GC/FID. Since an evacuated tank was used, a correction to the methane concentration as analyzed was made to adjust for the dilution of the sample caused by the pressurization procedures. EPA Method 10B temperature and pressure correction equations were used to make the "as analyzed" diluted methane results reflect the original undiluted sample concentration.

4.5.4 Particulate

Sample Collection. Samples were withdrawn isokinetically from the source using an EPA Method 5 sampling train. The sampling train consisted of a stainless steel nozzle, a heated glass probe with a Type S Pitot tube attached, a filter, four chilled impingers, and a metering console. The particulate sample was collected on a Whatman EPM2000 glass fiber filter maintained at a temperature of $248^\circ\text{F} \pm 25^\circ\text{F}$. The first two impingers each contained 100 mL of deionized, distilled

(DI) water, the third remained empty, and the fourth contained preweighed silica gel. Each of the 24 points was sampled for 2.5 minutes, resulting in net run times of 60 minutes.

Sample Recovery. The filter was removed from the filter holder and placed in a 250 mL glass jar. The DI water reagent was returned to the original 1000 mL glass jar, weighed, the weight recorded on the label, and the liquid level marked. The silica gel was returned to the original tared container, weighed, and the weight recorded on the label. The volume of water vapor condensed in the impingers and the volume of water vapor collected in the silica gel were summed and entered into moisture content calculations.

All fronthalf components of the sampling train including the nozzle, probe, and filter holder were rinsed with acetone into a 500 mL glass jar.

Sample Analysis. EPA Method 5 analytical procedures were used to analyze the filter and fronthalf acetone rinse for particulate.

4.5.5 Particulate $\leq$ 10 Microns and Condensable Particulate

Sample Collection. Samples were withdrawn isokinetically from the source using a combined EPA Method 201A and EPA Method 202 sampling train. The sampling train consisted of a precutter nozzle, an in situ sizing device (cyclone), a heated probe with a Type S Pitot tube attached, a heated filter, four chilled impingers, and a metering console.

The fine particulate filter was placed in the EPA Method 5 sampling box (as requested by Ron Meyers and John Brown of USEPA) so that the results would be more readily comparable to the EPA Method 5 results. The particulate with an aerodynamic size of ≤ 10 microns (PM10) was collected on a Whatman EPM2000 glass fiber filter maintained at a temperature of $248^{\circ}\text{F} \pm 25^{\circ}\text{F}$. The first two impingers each contained 100 mL of deionized, distilled (DI) water, the third remained empty, and the fourth contained preweighed silica gel.

The sampling time at each traverse point was adjusted proportionally to the velocity at that point to provide a velocity weighted sample. A preliminary velocity traverse was performed to determine which points were to be sampled and for how long. From this data, the average flue gas velocity was calculated. Based on the flue gas parameters, the appropriate ACFM into the nozzle was selected for the PM10 cut. The desired nozzle size was calculated, a nozzle with a diameter as close to the desired size was chosen, and the desired velocity into the nozzle was calculated. The sampling rate remained constant for the duration of each run.

Sample Recovery. At the conclusion of each run, the precutter nozzle/cyclone, probe, and filter were removed and the impinger contents were purged with nitrogen (N_2) to remove dissolved sulfur dioxide (SO_2) gases. The posttest nitrogen purge was at a rate of 20 L/min for a duration of 60 minutes.

After the nitrogen purge, the DI water reagent was returned to the original 1000 mL glass jar, weighed, the weight recorded on the label, and the liquid level marked. The silica gel was returned to the original tared container, weighed, and the weight recorded on the label. The volume of water vapor condensed in the impingers and the volume of water vapor collected in the silica gel were summed and entered into moisture content calculations.

The precutter nozzle and cyclone were rinsed with acetone into a 500 mL glass jar. The filter was removed from the filter holder and placed into a separate sample jar and the fronthalf of the filter holder was rinsed with acetone into the appropriate sample jar. The backhalf of the filter holder, impingers, and connecting glassware were rinsed twice with water into the 1000 mL jar containing the DI water reagent then twice with methylene chloride (MeCl_2) into a separate 500 mL glass jar.

Sample Analysis. EPA Method 5 analytical procedures were used to analyze the precutter nozzle, cyclone, and filter catch for filterable particulate. EPA Method 202 analytical procedures were used to analyze the combined DI water reagent/DI water rinses and MeCl_2 rinses for condensible particulate. The precutter nozzle and cyclone catch and nozzle/cyclone acetone rinse analytical results are reported as particulate > 10 microns. The filter catch and filters' fronthalf acetone rinses and the impingers DI water reagent and MeCl_2 rinse analytical results are reported as particulate $\leq$ 10 microns.

4.6 Equipment Calibration

Pertinent calibration data are provided in Appendix D.

5.0 QUALITY ASSURANCE/QUALITY CONTROL

5.1 General

Entropy, Inc. (EI) is committed to the continued implementation of a Quality Assurance Program to assure the quality of sampling and analytical procedures of environmental measurement data. The Quality Assurance measures taken during this test project equal or exceed the minimum QA/QC recommendations as set forth by the U.S. Environmental Protection Agency (EPA) for a particular method.

The following sections outline the QA program implemented by EI to justify the validity of test procedures. As applicable, the QA system for the various test programs addresses the following areas:

- Preventive Maintenance & Equipment Calibration
- Sample Processing
- Analytical Instrument Calibration
- Blanks and Spiked Samples
- Internal/External System Checks
- Data Reduction & Validation
- QA/QC Summary

5.2 Preventive Maintenance and Equipment Calibration

An effective preventive maintenance program decreases downtime and thus increases data completeness and quality. Pretest and posttest equipment calibrations are conducted in a manner and at a frequency which meets or exceeds U.S. EPA specifications.

Each item transported to the field is inspected to detect equipment problems which may originate during periods of storage. All equipment returning from the field is cleaned, repaired, reconditioned, and recalibrated as necessary. Routine maintenance on equipment (dry gas meters, pumps, Magnehelics, manometers, Pitot tubes, and nozzles) is carried out periodically for leaks, corrosion, dents, or any other damage. **Table 5-1** shows the activities for equipment calibration.

TABLE 5-1
IN-HOUSE EQUIPMENT CALIBRATION

Apparatus	Calibration Method And Frequency	Specifications	Corrective Action
Type S Pitot Tubes	Standards contained in EPA Method 2	Coefficient of 0.84 ± 0.02	Refurbish or recalibrate
	Visual inspection prior to shipment to test site and again prior to each day of testing		
Manometers	Leak checked before and after each field use		Adjust or replace
Magnehelic Gauges	Initially calibrate over full range	0-10" water column	
	After each field use, checked against inclined manometer at average settings encountered during testing	Within $\pm 5\%$	Repair and Recalibrate
Thermometers - Impinger - Dry Gas Meter - Filter Box	After purchase and prior to each field use, using ASTM Hg-in-glass thermometer	Impinger = $\pm 2^\circ\text{F}$ DGM = $\pm 5.4^\circ\text{F}$ FB = $\pm 5.4^\circ\text{F}$	Adjust, determine correction factor, or reject
	After purchase and prior to each field use, using ASTM mercury-in-glass thermometer		
Thermocouple/ Potentiometer	After purchase. 3-point (ice bath, boiling water, and hot oil) using ASTM Hg-in-glass thermometer	$\pm 1.5\%$ of absolute temperature	Adjust, determine correction factor, or reject
	Before and after each field use, compared to ASTM Hg-in-glass thermometer at ambient conditions		
Dry Gas Meter and Orifice	Full calibration (every 6 months) over wide range of orifice settings to obtain calibration factor (isokinetic meter box) as per EPA Method 5	DGM = ± 0.02 from avg. coeff. for each run Orifice = $\pm 0.15"$ H ₂ O over delta H range of 0.4"-4.0"	Adjust or replace
	10-minute quick calibration before sending to test site and again prior to each day of field use (isokinetic)	$\pm 3\%$ of full calibration $\bar{Y}$ $\pm 5\%$ of full calibration $\bar{Y}$	Use if no backup Do not use
	Calculate $\bar{Y}_{qa}$ on-site for each test run to determine if the meter gamma ($\bar{\gamma}$) has changed (EPA Method 5 Section 5.3.2 Alternate Procedures as approved by Administrator)	Average $\bar{Y}_{qa}$ must be within $\pm 5\%$ of full calibration $\bar{Y}$	Perform post test calibration at average delta H and highest vacuum encountered during testing to determine if meter gamma has changed (isokinetic)
	A post test isokinetic meter box calibration is performed after every job at the approximate average delta H to determine if meter gamma has changed (isokinetic) as per EPA Method 5	$\pm 5\%$ of full calibration Gamma (initial or recalibration) that yields the lowest sample volume for the testing is used for calculations	Recalibrate or replace
Dry Gas Meter Transfer Standard	Annual calibrations conducted in triplicate using EPA wet test meter. Calibrations conducted at 7 flow rates from 0.25 to 1.40 cfm.	$\pm 2\%$ of average factor for each calibration run	Adjust and recalibrate

• See Appendix D for EMTIC guideline document

TABLE 5-1 (Continued)
IN-HOUSE EQUIPMENT CALIBRATION

Apparatus	Calibration Method And Frequency	Specifications	Corrective Action
Barometer	Before and after each field use against an aneroid barometer	$\pm 0.1''$ mercury	Adjust to agree
	Reference barometer adjusted for elevation differences		
Probe Nozzle	Average of 5 I.D. measurements using a micrometer. Visual inspection before and after each field use	Difference between high and low measurement $\leq 0.004''$	Repair and recalibrate

5.3 Sample Processing

Entropy, Inc. employs systems which ensure the integrity of an environmental sample from the time of acquisition, through analysis, and ultimately to proper disposal. These systems are necessary to allow valid conclusions to be drawn from analytical results separated in time and space from the sampling operation. In addition, these systems recognize that samples are occasionally of value even after analytical results have been reported.

Samples are collected, transported, and stored in clean containers which are constructed of materials inert to the analytical matrix. Containers are used which allow air tight seals. When necessary, containers are employed which prevent photochemical reactions. All sample containers are labeled with the following information:

- Unique source identifier
- Sample run identifier
- Analyte identifier
- Sample matrix identifier
- Sample analyst identifier

Additional information relating to the sample is recorded on the data sheet for the sampling run that afforded the subject sample. Accordingly, the sampling data sheet contains all the information listed above, plus the date and time the sample was acquired and supplemental information such as observations pertinent to the quality of the sample. For condensed samples, e.g., samples in liquid media, the sample levels are marked on the outside of the container; this mark is used to indicate sample loss, and as such, may serve as a reference in adjusting results accordingly.

For transport from the field to the laboratory, samples are stored in sealed containers and secured in a fashion which minimizes movement and thus prevents breakage of containers. Containers used for transporting glass are packed with foam. Samples which require chilling are kept cold until analyzed.

Samples remain in the custody of the sampler, from acquisition until conveyance to the sample custodian. All custody transfers are signed and documented on a record of custody form, which remains with the sample until turned over to the custodian.

Analytical data are identified in a manner identical to that of the sampling data. Accordingly, all data generated from the analysis of samples are documented with the following information:

- Source identifier
- Sample run identifier
- Analyte identifier
- Sample matrix identifier
- Analyst identifier
- Analysis date

Portions of samples remaining after analysis are returned to their original sample containers. These samples are stored in designated storage areas until their destruction is authorized.

5.4 Instrument Calibration

Instrument calibration is one of the most important functions in generating precise and accurate quality data. All of the contract laboratories involved in the analytical testing for the test program maintain rigorous QA programs for instrument calibration.

5.5 Blanks and Spikes

Field blanks, method blanks, trip blanks, lab-proof blanks and filter blanks are obtained, digested and analyzed when applicable. The blanks reflect the background contamination obtained from the various sources during the sampling and analysis. Thus, data adjustment or correction can be made accordingly.

In most cases, it is not necessary to digest and analyze the method blanks, reagent blanks or the lab-proof blanks unless the field blank shows a high level of contamination. If a high level of contamination is present, it is imperative to individually analyze the above blanks to help determine the cause of contamination.

Spiked samples are used to check on the performance of a routine analysis or the recovery efficiency of a method. During spiking, a known amount of stock solutions of the substance of interest is added to the sample prior to sample extraction, digestion, and analysis.

5.6 Internal/External System Audit Checks

System and performance audits are routine elements of all Entropy QA/QC programs.

Internal Systems Audit: The following sampling equipment checks were conducted prior to sample collection.

- All sampling equipment was thoroughly checked to ensure clean and operable components.
- Equipment was inspected for possible damage from shipment.
- The oil manometers or Magnehelic gauges were leveled and zeroed.
- The temperature measurement systems were checked for damage and operability by measuring the ambient temperature.

Performance Audits: Performance audits of the laboratory are conducted prior to the processing of any compliance samples for analysis. Audit materials typically include samples available from the EPA prior to new source testing. Also, samples of known concentration are prepared in-house or obtained from the EPA for Internal QA checks.

External Systems Audits: Entropy is subject to a system audit each time a test is conducted for any Air Pollution Control agency. This procedure entails an EPA observer on-site to do qualitative evaluation of performance to demonstrate compliance with the applicable regulations.

5.7 Data Reduction and Validation

The test team leader is responsible for reviewing and validating data as they are acquired. Each team leader has extensive knowledge of sampling methodology and the characteristics of the process being measured and is capable of evaluating the accuracy, representativeness, and completeness of raw data on-site. Action to replace inadequate data can be taken immediately.

Data obtained during calibrations and test runs are recorded on standardized forms which are checked twice for completeness and accuracy by the QA Director or his designated representative. Data reduction and consistency are achieved by using the standardized forms and using Entropy's in-house computer facilities.

5.8 QA/QC Summary

All chemicals used were American Chemical Society (ACS), High Performance Liquid Chromatography (HPLC), or pesticide grade. The deionized, distilled water utilized met or

exceeded the American Society for Testing and Materials (ASTM) specifications for Type-I reagent water. Pretest and posttest leak checks were conducted on each sampling train.

5.8.1 Carbon Monoxide, Nitrogen Oxides and Sulfur Dioxide

Three-point analyzer calibration error checks were conducted before initiating any testing. Zero and upscale calibration drift checks were conducted for each run. The calibration error, percent of span drift, and percent of span system calibration checks met the $\pm 2\%$, $\pm 3\%$, and $\pm 5\%$, respectively.

5.8.2 Metals

Filter and reagent blanks were prepared and analyzed for mercury; a matrix spike was conducted; and duplicate analyses were conducted. **Table 5-2** presents the results.

Filter and reagent blanks were prepared and analyzed for metals; a matrix spike was conducted; and duplicate analyses were conducted. **Table 5-3** presents the results.

5.8.3 Particulate

An acetone reagent blank was analyzed for particulate with 0.5 mg/300 mL detected.

5.8.4 Particulate $\leq$ 10 Microns and Condensible Particulate

An acetone reagent blank was analyzed for particulate with 0.5 mg/300 mL detected. A MeCl_2 reagent blank was analyzed for condensible particulate with 1.2 mg/285 mL detected. A DI H_2O reagent blank was analyzed for condensible particulate with 1.4 mg/295 mL detected.

5.8.5 Total Hydrocarbons

Pretest and posttest calibrations were performed for each test run. The 3-point linearity checks were all within 3% of the known cylinder gas concentrations.

TABLE 5-2
MERCURY DUPLICATE ANALYSES RESULTS
BRICK KILN NO. 2 STACK
OCTOBER, 1995

	First Analysis	Second Analysis	Relative % Difference
S-M29-1			
Front half	< 0.470	< 0.470	NA
Back half	< 1.79	< 1.79	NA
HNO ₃	< 0.940	< 0.940	NA
KMnO ₄	< 2.35	< 2.35	NA
HCl	< 2.35	< 2.35	NA
S-M29-2			
Front half	< 0.470	< 0.470	NA
Back half	< 1.76	< 1.76	NA
HNO ₃	< 0.940	< 0.940	NA
KMnO ₄	< 2.35	< 2.35	NA
HCl	< 2.35	< 2.35	NA
S-M29-3			
Front half	< 0.470	< 0.470	NA
Back half	< 1.74	< 1.74	NA
HNO ₃	< 0.940	< 0.940	NA
KMnO ₄	< 2.35	< 2.35	NA
HCl	< 2.35	< 2.35	NA
S-M29-FB			
Front half	< 0.470	< 0.470	NA
Back half	< 1.36	< 1.36	NA
HNO ₃	< 0.940	< 0.940	NA
KMnO ₄	< 2.35	< 2.35	NA
HCl	< 2.35	< 2.35	NA

* Not applicable if one or both results are below the detection limit.

TABLE 5-3
METALS (EXCEPT MERCURY) BLANKS, MATRIX SPIKES,
AND DUPLICATE ANALYSES RESULTS
BRICK KILN NO. 2 STACK
OCTOBER, 1995

	Reagent Blank, μg^a	Field Blank, μg^a	Matrix Spike Recovery, % ^b	First Analysis, μg	Second Analysis, μg^c	Relative % Difference ^d
Antimony	1.45	< 1.00	90.9	2.22	2.21	0.226
Arsenic	3.49	2.02	104	6.46	5.95	4.11
Beryllium	< 0.100	< 0.100	87.4	< 0.100	< 0.100	NA
Cadmium	< 0.400	< 0.400	102	1.71	1.66	1.48
Chromium	1.73	2.18	99.0	7.10	7.24	0.976
Cobalt	< 1.00	< 1.00	106	< 1.00	< 1.00	NA
Lead	< 1.00	< 1.00	82.4	3.03	2.83	3.41
Manganese	1.27	2.56	89.9	21.0	19.0	5.00
Nickel	1.06	2.97	90.9	5.62	5.74	1.06
Selenium	< 1.00	< 1.00	106	10.30	9.99	1.53

(a) Combined filter, fronthalf 0.1N HNO_3 rinse, acetone rinse, and $\text{HNO}_3/\text{H}_2\text{O}_2$ reagent.

(b) Conducted on repetition 3.

(c) Conducted on repetition 2.

(d) Not applicable if one or both results are below the detection limit.

APPENDIX A. TEST RESULTS

1. Brick Kiln No. 2 Stack

a. Carbon Monoxide, Nitrogen Oxides, Sulfur Dioxide, and Total Hydrocarbons

FIELD DATA AND RESULTS TABULATION

PLANT: Triangle Brick, Merry Oaks, NC
 SAMPLING LOCATION: Brick Kiln No. 2 Stack
 OPERATOR: Julie R. Ruff

		<u>S-CEM-1</u>	<u>S-CEM-2</u>	<u>S-CEM-3</u>
	Test Date	10/17/95	10/17/95	10/17/95
	Run Start Time	1010	1150	1330
	Run Finish Time	1110	1250	1430
Theta	Net Run Time, min	60.0	60.0	60.0
Pbar	Barometric Pressure, in Hg	30.50	30.50	30.50
Mfd	Dry Mole Fraction	0.929	0.928	0.929
%CO ₂	Carbon Dioxide, % by volume	2.4	2.4	2.4
%O ₂	Oxygen, % by volume	16.6	16.6	16.6
Pg	Flue Gas Static Pressure, in H ₂ O	-0.350	-0.350	-0.350
ts	Flue Gas Temperature, °F	510	517	508
Qsd	Volumetric Flow Rate, dry SCFM*	15,284	14,877	14,714
	<u>Carbon Monoxide</u>			
Fwt	Formula Weight, gm/gm-mole	28.01	28.01	28.01
ppm _{vd}	Concentration, ppmvd	92.8	91.8	95.6
lb/hr	Emission Rate, lb/hr	6.19	5.96	6.14
	<u>Nitrogen Oxides as NO₂</u>			
Fwt	Formula Weight, gm/gm-mole	46.01	46.01	46.01
ppm _{vd}	Concentration, ppmvd	12.0	12.6	12.7
lb/hr	Emission Rate, lb/hr	1.31	1.34	1.34
	<u>Sulfur Dioxide</u>			
Fwt	Formula Weight, gm/gm-mole	64.06	64.06	64.06
ppm _{vd}	Concentration, ppmvd	5.1	4.2	4.0
lb/hr	Emission Rate, lb/hr	0.778	0.623	0.587
	<u>THC as Carbon</u>			
Fwt	Formula Weight, gm/gm-mole	12.01	12.01	12.01
ppm _{vw}	Concentration, ppmvw	19.0	20.0	20.8
ppm _{vd}	Concentration, ppmvd	20.5	21.6	22.4
lb/hr	Emission Rate, lb/hr	0.585	0.600	0.616
	<u>Methane</u>			
Fwt	Formula Weight, gm/gm-mole	16.04	16.04	16.04
ppm _{vd}	Concentration, ppmvd	< 1.98	< 1.91	< 1.92
lb/hr	Emission Rate, lb/hr	< 0.0756	< 0.0710	< 0.0706
	<u>Total Non-methane Hydrocarbons as Carbon</u>			
Fwt	Formula Weight, gm/gm-mole	12.01	12.01	12.01
ppm _{vd}	Concentration, ppmvd	20.5	21.6	22.4
lb/hr	Emission Rate, lb/hr	0.585	0.600	0.616

TOTAL HYDROCARBON MEASUREMENT RESULTS SUMMARY

PLANT NAME: Withers and Ravenel / Triangle Brick

TEST LOCATION: Brick Kiln #2 Stack

TEST-DATE: 10-17-95

OPERATOR: Julie Ruff

----- Pre-Test Calibration Error Check -----

SPAN VALUE: 100 (ppm as C)	CALIBRATION GAS VALUE (ppmC)*	SYSTEM CAL. ERROR RESPONSE	CAL. ERROR %
THC Zero Gas	0.0	0.7	0.70
Low-Level Gas	29.8	28.7	-3.69
Mid-Level Gas	51.9	51.9	0.00
High-Level Gas	83.1	84.4	1.56

* ppmC values = ppmC3H8 values x 3

----- Drift Determinations -----

Run Number	2-M25A-1	2-M25A-2	2-M25A-3
Zero Sys.Cal.Response	0.7	0.7	0.7
Zero Drift Response	1.4	0.7	0.1
Zero Drift	0.7	0.0	-0.6
Upscale Sys.Cal.Resp.	51.9	51.9	51.9
Upscale Drift Response	50.5	50.9	50.4
Upscale Drift	-1.4	-1.0	-1.5

----- Test Results -----			
RUN NO.:	2-M25A-1	2-M25A-2	2-M25A-3
RUN TIME:	1010-1110	1150-1250	1330-1430
THC (ppmWC):	19.0	20.0	20.8
%H2O:	7.10	7.20	7.10
THC (ppmdC):	20.5	21.6	22.4
DSCFM:	15,284	14,877	14,714
THC (lb/hr C):	0.585	0.600	0.616

$$\text{ppmd} = \text{ppmW} / (1 - (\%H_2O/100))$$

$$\text{lb/hr} = (\text{ppmd} \times \text{DSCFM} \times 60 \times \text{Mol.Wt.}) / 385.3 \text{ E06}$$

$$\text{Where: Mol.Wt. Carbon} = 12.01 \text{ lb/lb mole}$$

$$\text{Cal.Error} = \frac{\text{System Cal.Response} - \text{Cal.Gas Value}}{\text{** Cal.Gas Value}} \times 100$$

$$\text{Drift} = \frac{\text{Drift Response} - \text{System Cal.Response}}{\text{Span Value}} \times 100$$

** For zero gas calibration error use span value

CALCULATION OF AVERAGE SO2, NOx AND CO EMISSIONS

COMPANY: Withers and Ravenel / Triangle Brick

SOURCE: Brick Kiln #2 Stack

RUN: 1 (10:10 - 11:10)

DATE: 10/17/95

GAS VALUE	INITIAL CAL	FINAL CAL	MEAN CAL
0.0 ppm SO2	0.6	2.5	1.6
45.1 ppm SO2	41.2	42.9	42.1
0.0 ppm NOx	0.8	1.7	1.3
46.3 ppm NOx	42.8	42.1	42.5
0.0 ppm CO	1.3	3.6	2.5
59.9 ppm CO	59.7	61.5	60.6

Uncorrected Data: 6.2 ppm SO2
 12.0 ppm NOx
 92.5 ppm CO 15,284 DSCFM

CORRECTED RESULTS

5.1 ppm SO2
 12.0 ppm NOx
 92.8 ppm CO 0.776 lb SO2/hr
 1.31 lb NOx/hr
 6.18 lb CO/hr

Corrected Conc. = $C_{ma}(\bar{C} - C_o) / (C_m - C_o)$

Where: $\bar{C}$ = mean reference measurement
 C_o = mean zero calibration response
 C_m = mean mid or upscale calibration gas response
 C_{ma} = actual mid or upscale calibration gas concentration

lb/hr = (ppm pollutant) (DSCFM flow) (Conv. Factor) (60)

Where: SO2 Conv. Factor = 1.660E-07 lb SO2/DSCF - ppm SO2
 NOx Conv. Factor = 1.194E-07 lb NO2/DSCF - ppm NO2
 CO Conv. Factor = 7.263E-08 lb CO/DSCF - ppm CO

CALCULATION OF AVERAGE SO2, NOx AND CO EMISSIONS

COMPANY: Withers and Ravenel / Triangle Brick

SOURCE: Brick Kiln #2 Stack

RUN: 2 (11:50 - 12:50)

DATE: 10/17/95

GAS VALUE	INITIAL CAL	FINAL CAL	MEAN CAL
0.0 ppm SO2	2.5	1.9	2.2
45.1 ppm SO2	42.9	42.9	42.9
0.0 ppm NOx	1.7	2.4	2.1
46.3 ppm NOx	42.1	41.5	41.8
0.0 ppm CO	3.6	1.2	2.4
59.9 ppm CO	61.5	58.9	60.2

Uncorrected Data: 6.0 ppm SO2
 12.9 ppm NOx
 91.0 ppm CO 14,877 DSCFM

CORRECTED RESULTS

4.2 ppm SO2
 12.6 ppm NOx
 91.8 ppm CO 0.622 lb SO2/hr
 1.34 lb NOx/hr
 5.95 lb CO/hr

Corrected Conc. = $C_{ma}(\bar{C} - C_o) / (C_m - C_o)$

Where: $\bar{C}$ = mean reference measurement
 C_o = mean zero calibration response
 C_m = mean mid or upscale calibration gas response
 C_{ma} = actual mid or upscale calibration gas concentration

lb/hr = (ppm pollutant) (DSCFM flow) (Conv. Factor) (60)

Where: SO2 Conv. Factor = 1.660E-07 lb SO2/DSCF - ppm SO2
 NOx Conv. Factor = 1.194E-07 lb NO2/DSCF - ppm NO2
 CO Conv. Factor = 7.263E-08 lb CO/DSCF - ppm CO
 #VALUE!

CALCULATION OF AVERAGE SO2, NOx AND CO EMISSIONS

COMPANY: Withers and Ravenel / Triangle Brick

SOURCE: Brick Kiln #2 Stack

RUN: 3 (13:30 - 14:30)

DATE: 10/17/95

GAS VALUE	INITIAL CAL	FINAL CAL	MEAN CAL
0.0 ppm SO2	1.9	1.7	1.8
45.1 ppm SO2	42.9	41.6	42.3
0.0 ppm NOx	2.4	3.5	3.0
46.3 ppm NOx	41.5	41.3	41.4
0.0 ppm CO	1.2	0.8	1.0
59.9 ppm CO	58.9	60.3	59.6

Uncorrected Data: 5.4 ppm SO2
13.5 ppm NOx
94.5 ppm CO 14,714 DSCFM

CORRECTED RESULTS

4.0 ppm SO2
12.7 ppm NOx
95.6 ppm CO 0.586 lb SO2/hr
1.34 lb NOx/hr
6.13 lb CO/hr

Corrected Conc. = $C_{ma}(\bar{C} - C_o) / (C_m - C_o)$

Where: $\bar{C}$ = mean reference measurement
 C_o = mean zero calibration response
 C_m = mean mid or upscale calibration gas response
 C_{ma} = actual mid or upscale calibration gas concentration

lb/hr = (ppm pollutant) (DSCFM flow) (Conv. Factor) (60)

Where: SO2 Conv. Factor = 1.660E-07 lb SO2/DSCF - ppm SO2
NOx Conv. Factor = 1.194E-07 lb NO2/DSCF - ppm NO2
CO Conv. Factor = 7.263E-08 lb CO/DSCF - ppm CO

SYSTEM CALIBRATION BIAS AND DRIFT CALCULATIONS

COMPANY: Withers and Ravenel / Triangle Brick

SOURCE: Brick Kiln #2 Stack

TEST DATE: 10/17/95

RUN NUMBER: 1 (10:10 - 11:10)

SPAN VALUES: 100.0 ppm SO2
100.0 ppm NOx
100.0 ppm CO

>E>

	-----INITIAL VALUES-----			-----FINAL VALUES-----		
	ANALYZER	SYSTEM	SYSTEM	SYSTEM	SYSTEM	DRIFT
	CAL. RESPONSE	CAL. RESPONSE	CAL. BIAS (% OF SPAN)	CAL. RESPONSE	CAL. BIAS (% OF SPAN)	
SO2 ZERO GAS	0.4	0.6	0.20	2.5	2.10	1.90
SO2 UP-SCALE	46.1	41.2	-4.90	42.9	-3.20	1.70
NOx ZERO GAS	0.4	0.8	0.40	1.7	1.30	0.90
NOx UP-SCALE	46.1	42.8	-3.30	42.1	-4.00	-0.70
CO ZERO GAS	0.6	1.3	0.70	3.6	3.00	2.30
CO UP-SCALE	60.3	59.7	-0.60	61.5	1.20	1.80

SYSTEM CAL. RESPONSE - ANALYZER CAL. RESPONSE
SYSTEM CAL. BIAS = _____ X 100
SPAN

FINAL SYSTEM CAL. RESPONSE - INITIAL CAL. RESPONSE
DRIFT = _____ X 100
SPAN

\$\$

SYSTEM CALIBRATION BIAS AND DRIFT CALCULATIONS

COMPANY: Withers and Ravenel / Triangle Brick

SOURCE: Brick Kiln #2 Stack

TEST DATE: 10/17/95

RUN NUMBER: 2 (11:50 - 12:50)

SPAN VALUES: 100.0 ppm SO2
100.0 ppm NOx
100.0 ppm CO

	-----INITIAL VALUES-----			-----FINAL VALUES-----		
	ANALYZER CAL. RESPONSE	SYSTEM CAL. RESPONSE	SYSTEM CAL. BIAS (% OF SPAN)	SYSTEM CAL. RESPONSE	SYSTEM CAL. BIAS (% OF SPAN)	DRIFT (% OF SPAN)
SO2 ZERO GAS	0.4	2.5	2.10	1.9	1.50	-0.60
SO2 UP-SCALE	46.1	42.9	-3.20	42.9	-3.20	0.00
NOx ZERO GAS	0.4	1.7	1.30	2.4	2.00	0.70
NOx UP-SCALE	46.1	42.1	-4.00	41.5	-4.60	-0.60
CO ZERO GAS	0.6	3.6	3.00	1.2	0.60	-2.40
CO UP-SCALE	60.3	61.5	1.20	58.9	-1.40	-2.60

SYSTEM CAL. RESPONSE - ANALYZER CAL. RESPONSE

SYSTEM CAL. BIAS = _____ X 100

SPAN

FINAL SYSTEM CAL. RESPONSE - INITIAL CAL. RESPONSE

DRIFT = _____ X 100

SPAN

SYSTEM CALIBRATION BIAS AND DRIFT CALCULATIONS

COMPANY: Withers and Ravenel / Triangle Brick
 SOURCE: Brick Kiln #2 Stack

TEST DATE: 10/17/95

RUN NUMBER: 3 (13:30 - 14:30)

SPAN-VALUES: 100.0 ppm SO2
 100.0 ppm NOx
 100.0 ppm CO

	-----INITIAL VALUES-----			-----FINAL VALUES-----		
	ANALYZER CAL. RESPONSE	SYSTEM CAL. RESPONSE	SYSTEM CAL. BIAS (% OF SPAN)	SYSTEM CAL. RESPONSE	SYSTEM CAL. BIAS (% OF SPAN)	DRIFT (% OF SPAN)
SO2 ZERO GAS	0.4	1.9	1.50	1.7	1.30	-0.20
SO2 UP-SCALE	46.1	42.9	-3.20	41.6	-4.50	-1.30
NOx ZERO GAS	0.4	2.4	2.00	3.5	3.10	1.10
NOx UP-SCALE	46.1	41.5	-4.60	41.3	-4.80	-0.20
CO ZERO GAS	0.6	1.2	0.60	0.8	0.20	-0.40
CO UP-SCALE	60.3	58.9	-1.40	60.3	0.00	1.40

$$\text{SYSTEM CAL. BIAS} = \frac{\text{SYSTEM CAL. RESPONSE} - \text{ANALYZER CAL. RESPONSE}}{\text{SPAN}} \times 100$$

$$\text{DRIFT} = \frac{\text{FINAL SYSTEM CAL. RESPONSE} - \text{INITIAL CAL. RESPONSE}}{\text{SPAN}} \times 100$$

APPENDIX A. TEST RESULTS

1. Brick Kiln No. 2 Stack

b. Metals

FIELD DATA AND RESULTS TABULATION

PLANT: Triangle Brick, Merry Oaks, NC

LOCATION: Brick Kiln No. 2 Stack

RUN #	DATE	OPERATOR
S-M29-1	10/17/95	Joseph P Daley
S-M29-2	10/17/95	Joseph P Daley
S-M29-3	10/17/95	Joseph P Daley

		S-M29-1	S-M29-2	S-M29-3
	Run Start Time	1010	1150	1330
	Run Finish Time	1117	1255	1436
	Net Traversing Points	24	24	24
Theta	Net Run Time, Minutes	60.00	60.00	60.00
Dia	Nozzle Diameter, Inches	0.313	0.313	0.306
Cp	Pitot Tube Coefficient	0.840	0.840	0.840
Y	Dry Gas Meter Calibration Factor	1.0013	1.0013	1.0013
Pbar	Barometric Pressure, Inches Hg	30.50	30.50	30.50
Delta-H	Avg. Pressure Differential of Orifice Meter, Inches H ₂ O	2.02	1.92	1.61
Vm	Volume Of Metered Gas Sample, Dry ACF	46.870	45.745	41.770
tm	Dry Gas Meter Temperature, Degrees F	91	96	89
Vmstd	Volume Of Metered Gas Sample, Dry SCF*	46.070	44.583	41.129
Vlc	Total Volume of Liquid Collected in Impingers & Silica Gel, ml	74.7	73.5	66.6
Vwstd	Volume of Water Vapor, SCF*	3.516	3.460	3.135
XH ₂ O	Moisture Content, Percent by Volume	7.1	7.2	7.1
Mfd	Dry Mole Fraction	0.929	0.928	0.929
XCO ₂	Carbon Dioxide, Percent By Volume, Dry	2.4	2.4	2.4
XO ₂	Oxygen, Percent By Volume, Dry	16.6	16.6	16.6
Fo	Fuel Factor	1.792	1.792	1.792
Md	Gas Molecular Weight, lb/lb-Mole, Dry	29.05	29.05	29.05
Ms	Gas Molecular Weight, lb/lb-Mole, Wet	28.26	28.25	28.27
Pg	Flue Gas Static Pressure, Inches H ₂ O	-0.35	-0.35	-0.35
Ps	Absolute Flue Gas Pressure, Inches Hg	30.47	30.47	30.47
ts	Flue Gas Temperature, Degrees F	510	517	508
Delta-p	Average Velocity Head, Inches H ₂ O	0.3531	0.3374	0.3263
vs	Flue Gas Velocity, Feet/Second	45.29	44.43	43.48
A	Stack/Duct Area, Square Inches	1,573	1,573	1,573
Qsd	Volumetric Air Flow Rate, Dry SCFM*	15,284	14,877	14,714
Qaw	Volumetric Air Flow Rate, Wet ACFM	29,680	29,114	28,491
XI	Isokinetic Sampling Rate, Percent	102.7	102.1	99.6

* 68° F (20° C) -- 29.92 Inches of Mercury (Hg)

FIELD DATA AND RESULTS TABULATION
(Continued)

PLANT: Triangle Brick, Merry Oaks, NC

		S-M29-1	S-M29-2	S-M29-3
<u>Antimony</u>				
fw	Formula Weight, lb/lb-Mole	121.75	121.75	121.75
ug	Catch Weight, Micrograms	0	.77	42
ug/DSCM	Concentration, ug/DSCM	0.0	0.610	36.1
gr/DSCF	Concentration, grains/DSCF *	0.0	2.67E-007	1.58E-005
lb/hr	Emission Rate, lb/hr	0.0	3.40E-005	1.99E-003
<u>Arsenic</u>				
fw	Formula Weight, lb/lb-Mole	74.92	74.92	74.92
ug	Catch Weight, Micrograms	1.83	2.72	11.1
ug/DSCM	Concentration, ug/DSCM	1.40	2.15	9.53
gr/DSCF	Concentration, grains/DSCF *	6.13E-007	9.42E-007	4.16E-006
lb/hr	Emission Rate, lb/hr	8.03E-005	1.20E-004	5.25E-004
<u>Beryllium</u>				
fw	Formula Weight, lb/lb-Mole	9.01	9.01	9.01
ug	Catch Weight, Micrograms	< .1	< .1	< .1
ug/DSCM	Concentration, ug/DSCM	< 0.0766	< 0.0792	< 0.0859
gr/DSCF	Concentration, grains/DSCF *	< 3.35E-008	< 3.46E-008	< 3.75E-008
lb/hr	Emission Rate, lb/hr	< 4.39E-006	< 4.41E-006	< 4.73E-006
<u>Cadmium</u>				
fw	Formula Weight, lb/lb-Mole	112.41	112.41	112.41
ug	Catch Weight, Micrograms	.792	1.69	1.55
ug/DSCM	Concentration, ug/DSCM	0.607	1.34	1.33
gr/DSCF	Concentration, grains/DSCF *	2.65E-007	5.85E-007	5.82E-007
lb/hr	Emission Rate, lb/hr	3.48E-005	7.46E-005	7.34E-005
<u>Chromium</u>				
fw	Formula Weight, lb/lb-Mole	52.00	52.00	52.00
ug	Catch Weight, Micrograms	4.15	5.44	5.09
ug/DSCM	Concentration, ug/DSCM	3.18	4.31	4.37
gr/DSCF	Concentration, grains/DSCF *	1.39E-006	1.88E-006	1.91E-006
lb/hr	Emission Rate, lb/hr	1.82E-004	2.40E-004	2.41E-004
<u>Cobalt</u>				
fw	Formula Weight, lb/lb-Mole	58.93	58.93	58.93
ug	Catch Weight, Micrograms	< 1	< 1	< 1
ug/DSCM	Concentration, ug/DSCM	< 0.766	< 0.792	< 0.859
gr/DSCF	Concentration, grains/DSCF *	< 3.35E-007	< 3.46E-007	< 3.75E-007
lb/hr	Emission Rate, lb/hr	< 4.39E-005	< 4.41E-005	< 4.73E-005
<u>Lead</u>				
fw	Formula Weight, lb/lb-Mole	207.19	207.19	207.19
ug	Catch Weight, Micrograms	3.21	2.93	52.3
ug/DSCM	Concentration, ug/DSCM	2.46	2.32	44.9
gr/DSCF	Concentration, grains/DSCF *	1.08E-006	1.01E-006	1.96E-005
lb/hr	Emission Rate, lb/hr	1.41E-004	1.29E-004	2.48E-003
<u>Manganese</u>				
fw	Formula Weight, lb/lb-Mole	54.94	54.94	54.94
ug	Catch Weight, Micrograms	23.9	18.7	17.1
ug/DSCM	Concentration, ug/DSCM	18.3	14.8	14.7
gr/DSCF	Concentration, grains/DSCF *	8.01E-006	6.47E-006	6.42E-006
lb/hr	Emission Rate, lb/hr	1.05E-003	8.25E-004	8.09E-004

* 68° F (20° C) -- 29.92 Inches of Mercury (Hg)
< Indicates the value is below the detection limit.

FIELD DATA AND RESULTS TABULATION
(Continued)

PLANT: Triangle Brick, Merry Oaks, NC

		S-M29-1	S-M29-2	S-M29-3
	<u>Mercury</u>			
fw	Formula Weight, lb/lb-Mole	200.59	200.59	200.59
ug	Catch Weight, Micrograms	< 2.35	< 2.35	< 2.35
ug/DSCM	Concentration, ug/DSCM	< 1.80	< 1.86	< 2.02
gr/DSCF	Concentration, grains/DSCF *	< 7.87E-007	< 8.13E-007	< 8.82E-007
lb/hr	Emission Rate, lb/hr	< 1.03E-004	< 1.04E-004	< 1.11E-004
	<u>Nickel</u>			
fw	Formula Weight, lb/lb-Mole	58.71	58.71	58.71
ug	Catch Weight, Micrograms	3.58	4.62	.98
ug/DSCM	Concentration, ug/DSCM	2.74	3.66	0.841
gr/DSCF	Concentration, grains/DSCF *	1.20E-006	1.60E-006	3.68E-007
lb/hr	Emission Rate, lb/hr	1.57E-004	2.04E-004	4.64E-005
	<u>Selenium</u>			
fw	Formula Weight, lb/lb-Mole	78.96	78.96	78.96
ug	Catch Weight, Micrograms	11	10.15	9.03
ug/DSCM	Concentration, ug/DSCM	8.43	8.04	7.75
gr/DSCF	Concentration, grains/DSCF *	3.68E-006	3.51E-006	3.39E-006
lb/hr	Emission Rate, lb/hr	4.83E-004	4.48E-004	4.27E-004

* 68° F (20° C) -- 29.92 Inches of Mercury (Hg)

< Indicates the value is below the detection limit.

APPENDIX A. TEST RESULTS

1. Brick Kiln No. 2 Stack

c. Particulate

FIELD DATA AND RESULTS TABULATION

PLANT: Triangle Brick, Merry Oaks, NC

LOCATION: Brick Kiln No. 2 Stack

RUN #		DATE	OPERATOR		
S-M5-1		10/18/95	Joseph P Daley		
S-M5-2		10/18/95	Joseph P Daley		
S-M5-3		10/18/95	Joseph P Daley		
			S-M5-1	S-M5-2	S-M5-3
	Run Start Time		0901	1039	1221
	Run Finish Time		1005	1142	1324
	Net Traversing Points		24	24	24
Theta	Net Run Time, Minutes		60.00	60.00	60.00
Dia	Nozzle Diameter, Inches		0.313	0.306	0.313
Cp	Pitot Tube Coefficient		0.840	0.840	0.840
Y	Dry Gas Meter Calibration Factor		1.0013	1.0013	1.0013
Pbar	Barometric Pressure, Inches Hg		30.53	30.50	30.53
Delta-H	Avg. Pressure Differential of Orifice Meter, Inches H ₂ O		1.69	1.84	1.84
Vm	Volume Of Metered Gas Sample, Dry ACF		42.407	44.945	45.098
tm	Dry Gas Meter Temperature, Degrees F		78	102	106
Vmstd	Volume Of Metered Gas Sample, Dry SCF*		42.663	43.266	43.146
Vlc	Total Volume of Liquid Collected in Impingers & Silica Gel, ml		66.4	64.3	68.6
Vwstd	Volume of Water Vapor, SCF*		3.125	3.027	3.229
%H ₂ O	Moisture Content, Percent by Volume		6.8	6.5	7.0
Mfd	Dry Mole Fraction		0.932	0.935	0.930
%CO ₂	Carbon Dioxide, Percent By Volume, Dry		2.4	2.4	2.4
%O ₂	Oxygen, Percent By Volume, Dry		16.6	16.6	16.6
Fo	Fuel Factor		1.792	1.792	1.792
Md	Gas Molecular Weight, lb/lb-Mole, Dry		29.05	29.05	29.05
Ms	Gas Molecular Weight, lb/lb-Mole, Wet		28.29	28.33	28.28
Pg	Flue Gas Static Pressure, Inches H ₂ O		-0.35	-0.35	-0.35
Ps	Absolute Flue Gas Pressure, Inches Hg		30.50	30.47	30.50
ts	Flue Gas Temperature, Degrees F		518	516	519
Delta-p	Average Velocity Head, Inches H ₂ O		0.3241	0.3681	0.3356
vs	Flue Gas Velocity, Feet/Second		43.51	46.33	44.32
A	Stack/Duct Area, Square Inches		1,573	1,573	1,573
Qsd	Volumetric Air Flow Rate, Dry SCFM*		14,628	15,634	14,856
Qaw	Volumetric Air Flow Rate, Wet ACFM		28,515	30,363	29,047
%I	Isokinetic Sampling Rate, Percent		99.4	98.6	98.9

* 68° F (20° C) -- 29.92 Inches of Mercury (Hg)

(Continued next page)

FIELD DATA AND RESULTS TABULATION
(Continued)

PLANT: Triangle Brick, Merry Oaks, NC

		S-M5-1	S-M5-2	S-M5-3
	<u>Filterable Particulate</u>			
mg	Catch Weight, Milligrams	8.1	6.9	9.1
gr/DSCF	Concentration, grains/DSCF *	0.00293	0.00246	0.00325
lb/hr	Emission Rate, lb/hr	0.367	0.330	0.414

* 68° F (20° C) -- 29.92 Inches of Mercury (Hg)

APPENDIX A. TEST RESULTS

1. Brick Kiln No. 2 Stack

**d. Particulate $\leq$ 10 Microns and
Condensible Particulate**

FIELD DATA AND RESULTS TABULATION

Plant: Triangle Brick, Merry Oaks, NC
Sampling Location: Brick Kiln No. 2 Stack
Operator: Dennis D. Holzschuh

		S-M201A/202-1	S-M201A/202-2	S-M201A/202-3
	Test Date	10/18/95	10/18/95	10/18/95
	Run Start Time	901	1039	1210
	Run Finish Time	1006	1143	1322
	Net Traversing Points	12	12	12
Theta	Net Run Time, minutes	60.0	60.0	60.0
Dia	Nozzle Diameter, inches	0.252	0.249	0.249
Cp	Pitot Tube Coefficient	0.84	0.84	0.84
Y	Dry Gas Meter Calibration Factor	0.9776	0.9776	0.9776
Pbar	Barometric Pressure, in Hg	30.53	30.53	30.53
Delta H	Average Pressure Differential of Meter, inches H ₂ O	0.68	0.68	0.68
Vm	Volume of Metered Gas Sample, cu. feet	28.475	28.870	28.510
tm	Dry Gas Meter Temperature, °F	77	100	95
Vmstd	Volume of Metered Gas Sample, DSCF*	27.974	27.188	27.086
Vlc	Total Volume of Liquid Collected in Impingers and Silica Gel, ml	39.6	38.1	38.2
Vwstd	Volume of Water Vapor, SCF	1.864	1.793	1.798
%H ₂ O	Moisture Content, % by volume	6.2 **	6.2 **	6.2 **
%H ₂ OSAT	Moisture Sat. at Flue Gas Conditions, %	4979.2	5226.2	5225.6
Mfd	Dry Mole Fraction	0.938	0.938	0.938
%CO ₂	Carbon Dioxide, % by volume, dry	2.4	2.4	2.4
%O ₂	Oxygen, % by volume, dry	16.6	16.6	16.6
%CO + N ₂	CO + N ₂ , Percent by Volume, dry	81.0	81.0	81.0
Fo	Fuel Factor	1.792	1.792	1.792
Md	Gas Molecular Weight, Lb/Lb-Mole, dry	29.05	29.05	29.05
Ms	Gas Molecular Weight, Lb/Lb-Mole, wet	28.36	28.36	28.36
Pg	Flue Gas Static Pressure, in. H ₂ O	-0.35	-0.35	-0.30
Ps	Absolute Flue Gas Pressure, in. Hg	30.50	30.50	30.51
ts	Flue Gas Temperature, °F	505.0	510.4	510.4
Delta-p	Average Velocity Head, inches H ₂ O	0.3176	0.3176	0.3176
vs	Flue Gas Velocity, feet per second	42.74	42.86	42.86
A	Stack/Duct Area, square inches	1,573	1,573	1,573
Qsd	Volumetric Air Flow Rate, dry SCFM*	14,650	14,618	14,615
Qmsd	Volumetric Air Flow Rate, dry SCMM*	415	414	414
Qaw	Volumetric Air Flow Rate, wet ACFM*	28,012	28,091	28,091
%t	Isokinetic Sampling Rate, percent	100.4	100.1	99.8

* 68°F (20°C) – 29.92 inches of mercury

** Value used for calculations

FIELD DATA AND RESULTS TABULATION

Plant: Triangle Brick, Merry Oaks, NC
 Sampling Location: Brick Kiln No. 2 Stack
 Operator: Dennis D. Holtschuh

Test Date		<u>S-M201A/202-1</u> 10/18/95	<u>S-M201A/202-2</u> 10/18/95	<u>S-M201A/202-3</u> 10/18/95
<u>PM10 Calculations</u>				
u _s	Stack Gas Viscosity	285.2	286.7	286.6
Q _s	PM10 Flow, at Cyclone Conditions, ACFM	0.892	0.871	0.868
D50	Dia. of Particles in Cyclone, Microns	9.55	9.76	9.78
<u>Particulate Catch</u>				
mg < D50	≤ 10 Microns, milligrams	8.1	6.7	7.4
mg > D50	> 10 Microns, milligrams	2.8	2.3	2.3
mg	Total Catch, milligrams	10.9	9.0	9.7
<u>Percent of Total Particulate</u>				
% < D50	≤ 10 Microns, percent	74.3	74.4	76.3
% > D50	> 10 Microns, percent	25.7	25.6	23.7
<u>Particulate < 10 Microns</u>				
mg	Catch Weight, milligrams	8.1	6.7	7.4
gr/DSCF	Concentration, grains/DSCF	0.00447	0.00380	0.00422
lb/hr	Emission Rate, lb/hr	0.561	0.477	0.528
<u>Condensible Particulate</u>				
mg	Catch Weight, milligrams	22.2	29.1	29.4
gr/DSCF	Concentration, grains/DSCF	0.0122	0.0165	0.0168
lb/hr	Emission Rate, lb/hr	1.54	2.07	2.10

APPENDIX A. TEST RESULTS

2. Example Calculations

NOTE

The example values shown in these calculations have been rounded for presentation purposes. Any hand calculations conducted using these example values may produce slightly different results than those presented.

CONSTANTS, DEFINITIONS, NOMENCLATURE, AND UNITS

460	0 degrees Fahrenheit in degrees Rankin. The sum of 460 and the standard temperature (60, 68, 77, etc. in °F) gives Tstd in degrees Rankin.
273	0 degrees Celsius in degrees Kelvin. The sum of 273 and the standard temperature (18, 20, 25, etc. in °C) gives Tstd in degrees Kelvin.
29.92	Standard absolute pressure (Pstd), inches of mercury. English unit.
760	Standard absolute pressure (Pstd), millimeters of mercury. Metric unit.
24.056*	Liters per gram-mole at standard conditions.
385.3*	Molar volume cubic feet/pound-mole at standard conditions.
0.04707*	Standard cubic feet per gram or mL of H2O at standard conditions.
7000	Grains per pound.
453.592	Grams per pound.
0.02832	Cubic meters per cubic foot.
28.32	Liters per cubic foot.
0.03531	Cubic feet per liter.
35.31	Cubic feet per cubic meter.
1000	Conversion from milligrams to grams, milliliters to liters, and liters to cubic meters.
10 ⁶	Conversion factor for decimal fraction to parts per million.
144	Square inches per square foot.
60	Minutes per hour and seconds per minute.
13.6	Specific gravity of mercury (1 inch of mercury = 13.6 inches of H2O).
20.9	Percent O2 by volume (dry basis) in ambient air.
85.49	Pitot tube constant (Kp): $\frac{\text{feet}}{\text{second}} \sqrt{\frac{(\text{lb} / \text{lb} - \text{mole}) \cdot (\text{inches Mercury})}{(\text{degrees Rankin}) \cdot (\text{inches H2O})}}$
A	Stack cross-sectional area, square inches.

* Where applicable, these constants must be corrected (if the standard temperature is not 68°F) by multiplying them by the ratio of the standard temperatures. For example to convert to 77° F: (460 + 77)/(460 + 68)

EXAMPLE TEST CALCULATIONS RUN S-M5-1

Brick Kiln No. 2 Stack

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$Vmstd = Y \cdot Vm \cdot \frac{Pbar + (\Delta H/13.6)}{(460 + tm)} \cdot \frac{460 + tstd}{Pstd}$$

$$Vmstd = 1.0013 \cdot 42.407 \cdot \frac{30.53 + (1.690/13.6)}{(460 + 78)} \cdot \frac{460 + 68}{29.92} = 42.663 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$Vwstd = 0.04707 \cdot Vlc \cdot (460 + tstd)/528$$

$$Vwstd = 0.04707 \cdot 66.4 \cdot (460 + 68)/528 = 3.125 \text{ SCF}$$

PERCENT MOISTURE, BY VOLUME, AS MEASURED IN FLUE GAS

$$\%H_2O = 100 \cdot Vwstd / (Vwstd + Vmstd)$$

$$\%H_2O = \frac{3.125}{3.125 + 42.663} \cdot 100 = 6.8 \%$$

ABSOLUTE FLUE GAS PRESSURE

$$Ps = Pbar + (Pg / 13.6)$$

$$Ps = 30.53 + (-0.35/13.6) = 30.50 \text{ inches Hg}$$

DRY MOLE FRACTION OF FLUE GAS

$$Mfd = 1 - \%H_2O / 100$$

$$Mfd = 1 - 6.8/100 = 0.932$$

DRY MOLECULAR WEIGHT OF FLUE GAS

$$Md = (\%CO_2/100 \cdot 44) + (\%O_2/100 \cdot 32) + ((100 - \%CO_2 - \%O_2)/100 \cdot 28)$$

$$Md = (2.4/100 \cdot 44) + (16.6/100 \cdot 32) + ((100 - 2.4 - 16.6)/100 \cdot 28)$$

$$Md = 29.05 \text{ lb/lb-Mole}$$

WET MOLECULAR WEIGHT OF FLUE GAS

$$Ms = (Md \cdot Mfd) + (0.18 \cdot \%H_2O)$$

$$Ms = (29.05 \cdot 0.932) + (0.18 \cdot 6.8) = 28.29 \text{ lb/lb-Mole}$$

AVERAGE FLUE GAS VELOCITY [Note: (Delta p)avg is square of average square root]

$$v_s = 85.49 * C_p * \left[\frac{(\Delta P)_{avg} * (460 + t_s)}{P_s * M_s} \right]^{\frac{1}{2}}$$

$$v_s = 85.49 * 0.840 * \left[\frac{0.3241 * (460 + 518)}{30.50 * 28.29} \right]^{\frac{1}{2}} = 43.51 \text{ ft/sec}$$

DRY VOLUMETRIC FLUE GAS FLOW RATE AT STANDARD CONDITIONS

$$Q_{sd} = \frac{60}{144} * M_{fd} * v_s * A * \frac{460 + t_{std}}{460 + t_s} * \frac{P_s}{P_{std}}$$

$$Q_{sd} = \frac{60}{144} * 0.932 * 43.51 * 1,572.8 * \frac{460 + 68}{460 + 518} * \frac{30.50}{29.92}$$

$$Q_{sd} = 14,628 \text{ DSCFM}$$

WET VOLUMETRIC FLUE GAS FLOW RATE AT ACTUAL CONDITIONS

$$Q_{aw} = 60 / 144 * v_s * A$$

$$Q_{aw} = 60 / 144 * 43.51 * 1,572.8 = 28,515 \text{ ACFM}$$

PERCENT ISOKINETIC OF SAMPLING RATE

$$\%I = \frac{P_{std}}{460 + t_{std}} * \frac{100}{60} * \frac{(t_s + 460) * V_{mstd}}{P_s * v_s * M_{fd} * \Theta * (\pi * (\text{NozzleDia}/2)^2 / 144)}$$

$$\%I = \frac{29.92}{460 + 68} * \frac{100}{60} * \frac{(518 + 460) * 42.663}{30.50 * 43.51 * 0.932 * 60.00 * (\pi * (0.313/2)^2 / 144)}$$

$$\%I = 99.4 \%$$

CONCENTRATION, GRAINS PER DRY STANDARD CUBIC FOOT, FILTERABLE PARTICULATE

$$\text{gr/DSCF} = \frac{7,000}{453.592} * \frac{(\text{mg} / 10^3)}{V_{mstd}}$$

$$\text{gr/DSCF} = \frac{7,000}{453.592} * \frac{(8.1/10^3)}{42.663} = 0.00293 \text{ gr/DSCF}$$

EMISSION RATE, POUNDS PER HOUR, FILTERABLE PARTICULATE

$$\text{lb/hr} = \frac{60}{453.592} * \frac{(\text{mg} / 10^3)}{\text{Vmstd}} \bullet \text{Qsd}$$

$$\text{---} \quad \text{lb/hr} = \frac{60}{453.592} * \frac{(8.1/10^3)}{42.663} \bullet 14,628 = 0.367 \text{ lb/hr}$$

EXAMPLE TEST CALCULATIONS RUN S-M29-1

Brick Kiln No. 2 Stack

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$Vmstd = Y * Vm * \frac{Pbar + (\Delta H/13.6)}{(460 + tm)} * \frac{460 + tstd}{Pstd}$$

$$Vmstd = 1.0013 * 46.870 * \frac{30.50 + (2.020/13.6)}{(460 + 91)} * \frac{460 + 68}{29.92} = 46.070 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$Vwstd = 0.04707 * Vlc * (460 + tstd)/528$$

$$Vwstd = 0.04707 * 74.7 * (460 + 68)/528 = 3.516 \text{ SCF}$$

PERCENT MOISTURE, BY VOLUME, AS MEASURED IN FLUE GAS

$$\%H_2O = 100 * Vwstd / (Vwstd + Vmstd)$$

$$\%H_2O = \frac{3.516}{3.516 + 46.070} * 100 = 7.1 \%$$

ABSOLUTE FLUE GAS PRESSURE

$$Ps = Pbar + (Pg / 13.6)$$

$$Ps = 30.50 + (-0.35/13.6) = 30.47 \text{ inches Hg}$$

DRY MOLE FRACTION OF FLUE GAS

$$Mfd = 1 - \%H_2O / 100$$

$$Mfd = 1 - 7.1/100 = 0.929$$

DRY MOLECULAR WEIGHT OF FLUE GAS

$$Md = (\%CO_2/100 * 44) + (\%O_2/100 * 32) + ((100 - \%CO_2 - \%O_2)/100 * 28)$$

$$Md = (2.4/100 * 44) + (16.6/100 * 32) + ((100 - 2.4 - 16.6)/100 * 28)$$

$$Md = 29.05 \text{ lb/lb-Mole}$$

WET MOLECULAR WEIGHT OF FLUE GAS

$$Ms = (Md * Mfd) + (0.18 * \%H_2O)$$

$$Ms = (29.05 * 0.929) + (0.18 * 7.1) = 28.26 \text{ lb/lb-Mole}$$

AVERAGE FLUE GAS VELOCITY [Note: (Delta p)avg is square of average square root]

$$v_s = 85.49 * C_p * \left[\frac{(\Delta P)_{avg} * (460 + t_s)}{P_s * M_s} \right]^{\frac{1}{2}}$$

$$v_s = 85.49 * 0.840 * \left[\frac{0.3531 * (460 + 510)}{30.47 * 28.26} \right]^{\frac{1}{2}} = 45.29 \text{ ft/sec}$$

DRY VOLUMETRIC FLUE GAS FLOW RATE AT STANDARD CONDITIONS

$$Q_{sd} = \frac{60}{144} * M_{fd} * v_s * A * \frac{460 + t_{std}}{460 + t_s} * \frac{P_s}{P_{std}}$$

$$Q_{sd} = \frac{60}{144} * 0.929 * 45.29 * 1,572.8 * \frac{460 + 68}{460 + 510} * \frac{30.47}{29.92}$$

$$Q_{sd} = 15,284 \text{ DSCFM}$$

WET VOLUMETRIC FLUE GAS FLOW RATE AT ACTUAL CONDITIONS

$$Q_{aw} = 60 / 144 * v_s * A$$

$$Q_{aw} = 60 / 144 * 45.29 * 1,572.8 = 29,680 \text{ ACFM}$$

PERCENT ISOKINETIC OF SAMPLING RATE

$$\%I = \frac{P_{std}}{460 + t_{std}} * \frac{100}{60} * \frac{(t_s + 460) * V_{mstd}}{P_s * v_s * M_{fd} * \Theta * (\pi * (\text{NozzleDia}/2)^2 / 144)}$$

$$\%I = \frac{29.92}{460 + 68} * \frac{100}{60} * \frac{(510 + 460) * 46.070}{30.47 * 45.29 * 0.929 * 60.00 * (\pi * (0.313/2)^2 / 144)}$$

$$\%I = 102.7 \%$$

CONCENTRATION, MICROGRAMS PER DRY STANDARD CUBIC METER, ANTIMONY

$$\text{ug/DSCM} = \frac{(\text{ug} / 10^6)}{V_{mstd} * 0.02832} * 10^6$$

$$\text{ug/DSCM} = \frac{(0.0/10^6)}{46.070 * 0.02832} * 10^6 = 0.0 \text{ ug/DSCM}$$

CONCENTRATION, GRAINS PER DRY STANDARD CUBIC FOOT, ANTIMONY

$$\text{gr/DSCF} = \frac{7,000}{453.592} * \frac{(\text{ug} / 10^6)}{\text{Vmstd}}$$

$$\text{gr/DSCF} = \frac{7,000}{453.592} * \frac{(0.0/10^6)}{46.070} = 0.0 \text{ gr/DSCF}$$

EMISSION RATE, POUNDS PER HOUR, ANTIMONY

$$\text{lb/hr} = \frac{60}{453.592} * \frac{(\text{ug} / 10^6)}{\text{Vmstd}} * \text{Qsd}$$

$$\text{lb/hr} = \frac{60}{453.592} * \frac{(0.0/10^6)}{46.070} * 15,284 = 0.0 \text{ lb/hr}$$

EXAMPLE TEST CALCULATIONS
Brick Kiln No. 2 Stack
Run Number: S-M201A/202-1

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$Vmstd = Y \cdot Vm \cdot \frac{(Pbar + \Delta H / 13.6)}{(460 + tm)} \cdot \frac{(460 + tstd)}{Pstd}$$

$$Vmstd = 0.9776 \cdot 28.475 \cdot \frac{(30.53 + 0.68 / 13.6)}{(460 + 77.0)} \cdot \frac{(460 + 68)}{29.92}$$

$$Vmstd = 27.974 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$Vwstd = 0.04707 \cdot Vlc \cdot [(460 + tstd) / 528]$$

$$Vwstd = 0.04707 \cdot 39.6 \cdot [(460 + 68) / 528]$$

$$Vwstd = 1.864 \text{ SCF}$$

PERCENT MOISTURE, BY VOLUME, AS MEASURED IN FLUE GAS

$$\%H_2O = 100 \cdot Vwstd / (Vwstd + Vmstd)$$

$$\%H_2O = 100 \cdot 1.864 / (1.864 + (27.974))$$

$$\%H_2O = 6.2 \%$$

MOISTURE SATURATION @ FLUE GAS CONDITIONS, %

$$H_2OSAT = \frac{100 \cdot 10^{(6.691 - (3144 / (ts + 390.86)))}}{Ps}$$

$$H_2OSAT = \frac{100 \cdot 10^{(6.691 - (3144 / (505 + 390.86)))}}{30.53 + (-0.35 / 13.6)}$$

$$H_2OSAT = 4,979.2 \%$$

EXAMPLE TEST CALCULATIONS
Brick Kiln No. 2 Stack
Run Number: S-M201A/202-1

DRY MOLE FRACTION OF FLUE GAS

$$M_{fd} = 1 - (\%H_2O / 100)$$

$$M_{fd} = 1 - (6.2 / 100)$$

$$M_{fd} = 0.938$$

GAS MOLECULAR WEIGHT, LB/LB-MOLE, DRY

$$M_d = (\%CO_2 * \text{fwt } CO_2 / 100) + (\%O_2 * \text{fwt } O_2 / 100) + [(100 - \%CO_2 - \%O_2) * \text{fwt } CO \& N_2 / 100]$$

$$M_d = (2.4 * 44 / 100) + (16.6 * 32 / 100) + [(100 - 2.4 - 16.6) * 28 / 100]$$

$$M_d = 29.05$$

GAS MOLECULAR WEIGHT, LB/LB-MOLE, WET

$$M_s = (M_d * M_{fd}) + [\text{fwt } H_2O * (\%H_2O / 100)]$$

$$M_s = (29.05 * 0.938) + [18.0 * (6.2 / 100)]$$

$$M_s = 28.36$$

ABSOLUTE FLUE GAS PRESSURE, INCHES MERCURY

$$P_s = P_{bar} + (P_g / 13.6)$$

$$P_s = 30.53 + (-0.35 / 13.6)$$

$$P_s = 30.50$$

AVERAGE FLUE GAS VELOCITY, FEET/SECOND

$$v_s = 85.49 * C_p * \text{SQRT}[(\text{Avg Delta } p) * (460 + t_s) / (P_s * M_s)]$$

$$v_s = 85.49 * 0.84 * \text{SQRT}[(0.3176) * (460 + 505) / (30.50 * 28.36)]$$

$$v_s = 42.74 \text{ feet/second}$$

EXAMPLE TEST CALCULATIONS
Brick Kiln No. 2 Stack
Run Number: S-M201A/202-1

VOLUMETRIC AIR FLOW RATE, DRY STANDARD CUBIC FEET PER MINUTE (DRY SCFM)

$$Q_{sd} = (60 / 100) * Mfd * v_s * A * (460 + t_{std}) / (460 + t_s) * (P_s / P_{std})$$

$$Q_{sd} = (60 / 100) * 0.938 * 42.74 * 1572.81 * (460 + 68) / (460 + 505) * (30.50 / 29.92)$$

$$Q_{sd} = 14,650 \text{ Dry SCFM}$$

VOLUMETRIC AIR FLOW RATE, DRY STANDARD CUBIC METERS PER MINUTE (DRY SCMM)

$$Q_{msd} = Q_{sd} * 0.02832$$

$$Q_{msd} = 14,650 * 0.02832$$

$$Q_{msd} = 415 \text{ Dry SCMM}$$

VOLUMETRIC AIR FLOW RATE, WET ACTUAL CUBIC FEET PER MINUTE (WET SCFM)

$$Q_{aw} = (60 / 144) * v_s * A$$

$$Q_{aw} = (60 / 144) * 42.74 * 1572.81$$

$$Q_{aw} = 28,012 \text{ Dry SCFM}$$

ISOKINETIC SAMPLING RATE, PERCENT

$$\%I = \frac{100}{60} * \frac{P_{std}}{(460 + t_{std})} * \frac{(460 + t_s)}{P_s} * \frac{V_{mstd}}{v_s * Mfd * \text{Theta} * [\text{Pi} * (\text{nozzle diameter} / 2)^2 / 144]}$$

$$\%I = \frac{100}{60} * \frac{29.92}{(460 + 68)} * \frac{(460 + 505)}{30.50} * \frac{27.974}{42.74 * 0.938 * 60.0 * [\text{Pi} * (0.252 / 2)^2 / 144]}$$

$$\%I = 100.4 \%$$

STACK GAS VISCOSITY

$$\mu_s = 51.05 + [0.207 * (460 + t_s)] + [0.0000324 * (460 + t_s)^2] + [53.147 * (\%O_2/100)] - [74.143 * (\%H_2O/100)]$$

$$\mu_s = 51.05 + [0.207 * (460 + 505)] + [0.0000324 * (460 + 505)^2] + [53.147 * (16.6/100)] - [74.143 * (6.2/100)]$$

$$\mu_s = 285.2$$

EXAMPLE TEST CALCULATIONS
Brick Kiln No. 2 Stack
Run Number: S-M201A/202-1

PM10 FLOW RATE, ACTUAL CUBIC FEET PER MINUTE AT CYCLONE CONDITIONS

$$Q_s = [(460 + ts) / (17.64 * Ps)] * [(Vmstd + Vwstd) / Theta]$$

$$Q_s = [(460 + 505) / (17.64 * 30.50)] * [(27.974 + 1.864) / 60.0]$$

$$Q_s = 0.892 \text{ ACFM}$$

DIAMETER OF PARTICULES IN THE CYCLONE, MICRONS

$$D_{50} = 0.15625 * [(460 + ts) / (Ms * Ps)]^{0.2091} * [u_s / Q_s]^{0.7091}$$

$$D_{50} = 0.15625 * [(460 + 505) / (28.36 * 30.50)]^{0.2091} * [285.2 / 0.892]^{0.7091}$$

$$D_{50} = 9.55 \text{ Microns}$$

CONCENTRATION, PARTICULATE < 10 MICRONS, gr/DSCF

$$\text{gr/DSCF} = (7000 / 453.592) * [(mg / 1000) / Vmstd]$$

$$\text{gr/DSCF} = (7000 / 453.592) * [(8.1 / 1000) / 27.974]$$

$$\text{gr/DSCF} = 0.00447 \text{ gr/DSCF}$$

EMISSION RATE, PARTICULATE < 10 MICRONS, LB/HR

$$\text{lb/hr} = (60 / 453.592) * [(mg / 10^3) / (Vmstd)] * Qsd$$

$$\text{lb/hr} = (60 / 453.592) * [(8.1 / 10^3) / (27.974)] * 14,650$$

$$\text{lb/hr} = 0.561 \text{ lb/hr}$$

EXAMPLE TEST CALCULATIONS

Brick Kiln No. 2 Stack

RUN NUMBER: S-CEM-1

EMISSION RATE, CARBON MONOXIDE, lb/hr

$$\text{lb/hr} = (60 * \text{ppm}_{\text{vd}} * \text{fwt} * Q_{\text{sd}}) / (385.3 * (460 + t_{\text{std}}) / 528 * 10^6)$$

$$\text{lb/hr} = (60 * 92.80 * 28.01 * 15,284) / (385.3 * (460 + 68) / 528 * 10^6)$$

$$\text{lb/hr} = 6.19 \text{ lb/hr}$$

APPENDIX B. FIELD DATA

1. Brick Kiln No. 2 Stack

**a. Carbon Monoxide, Nitrogen Oxides,
Sulfur Dioxide, and Total Hydrocarbons**

CALIBRATION SUMMARY

SOURCE: Triangle Brick

REASON: CALIBRATION ERROR CHECK

DATE : 10-17-1995 TIME: 08:14 - 08:40

A/D CHAN	MONITOR DESCRIPTION	UNITS	GAS VALUE	MONITOR RESPONSE
8	STACK2	ppmNOX	0.0	0.4
8	STACK2	ppmNOX	26.0	26.5
8	STACK2	ppmNOX	46.3	46.1
8	STACK2	ppmNOX	80.2	81.1
6	STACK2	ppmSO2	0.0	0.4
6	STACK2	ppmSO2	45.1	46.1
6	STACK2	ppmSO2	92.8	92.7

CALIBRATION SUMMARY

SOURCE: Triangle Brick

REASON: CALIBRATION ERROR CHECK CONTINUED

DATE : 10-17-1995 TIME: 08:41 - 08:47

A/D CHAN	MONITOR DESCRIPTION	UNITS	GAS VALUE	MONITOR RESPONSE
7	STACK2	ppmCO	0.0	0.6
7	STACK2	ppmCO	30.2	31.2
7	STACK2	ppmCO	59.9	60.3
7	STACK2	ppmCO	90.9	89.4

CALIBRATION SUMMARY

SOURCE: Triangle Brick

REASON: SYSTEM BIAS CHECK

DATE : 10-17-1995 TIME: 09:14 - 09:52

A/D CHAN	MONITOR DESCRIPTION	UNITS	GAS VALUE	MONITOR RESPONSE
8	STACK2	ppmNOX	0.0	0.8
8	STACK2	ppmNOX	46.3	42.8
7	STACK2	ppmCO	0.0	1.3
7	STACK2	ppmCO	59.9	59.7
6	STACK2	ppmSO2	0.0	0.6
6	STACK2	ppmSO2	45.1	41.2

CALIBRATION SUMMARY

SOURCE: Triangle Brick

REASON: SYSTEM BIAS CHECK

DATE : 10-17-1995 TIME: 09:53 - 10:01

A/D CHAN	MONITOR DESCRIPTION	UNITS	GAS VALUE	MONITOR RESPONSE
1	STACK2	ppmTHC	0.0	0.7
1	STACK2	ppmTHC	29.8	28.7
1	STACK2	ppmTHC	51.9	51.9
1	STACK2	ppmTHC	83.1	84.4

Triangle Brick 10-17-1995

	CHAN 8	CHAN 7	CHAN 6	CHAN 1
	STACK2	STACK2	STACK2	STACK2
TIME	ppmNOX	ppmCO	ppmSO2	ppmTHC
10:11	12.0	91.5	5.6	18.5
10:12	12.1	92.3	5.7	19.3
10:13	12.2	92.9	5.9	19.4
10:14	12.2	93.4	6.0	19.6
10:15	12.3	94.0	6.1	19.7
10:16	12.3	94.4	6.1	19.5
10:17	12.3	94.7	6.2	20.6
10:18	12.4	95.1	6.3	20.0
10:19	12.5	94.5	6.4	19.5
10:20	12.4	94.4	6.5	19.1
10:21	12.3	94.8	6.5	19.7
10:22	12.3	94.8	6.4	19.9
10:23	12.2	94.9	6.2	19.5
10:24	12.2	94.7	5.8	19.0
10:25	12.2	94.6	5.7	18.7
10:26	12.3	95.1	5.6	19.2
10:27	12.3	94.7	5.5	18.7
10:28	12.2	94.8	5.6	18.3
10:29	12.3	94.5	5.7	18.1
10:30	10.7	67.8	5.8	17.0
10:31	6.0	96.2	5.2	16.7
10:32	13.3	90.4	5.0	16.7
10:33	11.7	90.4	5.3	17.7
10:34	11.8	91.0	5.5	18.5
10:35	11.9	91.7	5.8	18.5
10:36	12.1	92.3	6.2	19.3
10:37	12.1	92.7	6.4	19.4
10:38	12.2	93.1	6.7	19.6
10:39	12.3	93.5	6.9	19.7
10:40	12.4	93.8	6.8	19.4

AVERAGE VALUES FOR THE LAST 30 MINUTES

10:40	12.0	92.8	6.0	18.9
10:41	12.4	94.0	6.8	19.4
10:42	12.4	94.3	6.8	19.5
10:43	12.5	94.3	6.8	19.6
10:44	12.4	94.8	6.9	19.6
10:45	12.5	95.1	7.0	19.6
10:46	12.5	94.8	6.9	19.7
10:47	12.5	94.6	6.9	19.5
10:48	12.5	93.9	7.0	18.9
10:49	12.4	93.9	6.8	18.9
10:50	12.4	93.8	6.8	18.8
10:51	12.4	93.8	6.7	19.6
10:52	12.3	93.5	6.6	18.4
10:53	9.4	61.3	6.5	17.0
10:54	8.6	104.3	6.0	17.6
10:55	12.5	89.7	5.9	17.8
10:56	11.8	89.6	5.8	18.3
10:57	11.8	89.9	5.9	18.5

Triangle Brick 10-17-1995

	CHAN 8	CHAN 7	CHAN 6	CHAN 1
	STACK2	STACK2	STACK2	STACK2
TIME	ppmNOX	ppmCO	ppmSO2	ppmTHC
10:58	11.9	90.6	6.0	18.8
10:59	12.0	91.9	6.1	19.0
11:00	11.9	91.4	6.2	18.7
11:01	12.0	92.1	6.2	18.9
11:02	12.0	92.5	6.3	20.5
11:03	12.1	92.6	6.5	20.2
11:04	12.1	92.7	6.5	20.0
11:05	12.2	92.9	6.6	19.8
11:06	12.3	93.0	6.7	19.4
11:07	12.3	93.2	6.5	19.4
11:08	12.3	93.3	6.5	19.1
11:09	12.4	93.3	6.5	19.5
11:10	12.4	93.3	6.6	19.7

AVERAGE VALUES FOR THE LAST 30 MINUTES

11:10	12.0	92.3	6.5	19.1
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AVERAGE VALUES FOR THE LAST HOUR: 60 MINUTES OF VALID DATA

11:10	12.0	92.5	6.2	19.0

11:11	12.4	93.2	6.4	19.8
11:12	12.4	93.1	6.5	19.4
11:13	12.4	93.1	6.5	19.2
11:14	12.3	93.1	6.3	19.0
11:15	12.4	92.9	6.3	18.1
11:16	8.0	60.0	6.2	17.1
11:17	10.7	104.4	5.8	17.8

~~100~~ ~~92.5~~ ~~100~~ ~~19.0~~

CALIBRATION SUMMARY

SOURCE: Triangle Brick

REASON: SYSTEM BIAS CHECK - POST 2-CEM-1

DATE : 10-17-1995 TIME: 11:17 - 11:36

A/D CHAN	MONITOR DESCRIPTION	UNITS	GAS VALUE	MONITOR RESPONSE
8	STACK2	ppmNOX	0.0	1.7
8	STACK2	ppmNOX	46.3	42.1
7	STACK2	ppmCO	0.0	3.6
7	STACK2	ppmCO	59.0	61.5
6	STACK2	ppmSO2	0.0	2.5
6	STACK2	ppmSO2	45.1	42.9
1	STACK2	ppmTHC	0.0	1.4
1	STACK2	ppmTHC	51.9	50.5

Triangle Brick 10-17-1995

	CHAN 8	CHAN 7	CHAN 6	CHAN 1
	STACK2	STACK2	STACK2	STACK2
TIME	ppmNOX	ppmCO	ppmSO2	ppmTHC
11:51	12.9	91.4	7.7	19.6
11:52	12.9	92.1	7.5	19.6
11:53	13.0	92.3	7.2	19.7
11:54	13.0	92.2	7.1	19.4
11:55	13.0	92.2	6.9	19.8
11:56	13.0	92.1	6.8	19.4
11:57	13.0	92.0	6.7	19.2
11:58	13.0	92.1	6.5	19.1
11:59	13.0	92.3	6.4	19.1
12:00	13.0	92.2	6.3	19.1
12:01	13.0	87.9	6.2	18.7
12:02	6.1	73.9	6.0	17.5
12:03	14.1	91.9	5.6	17.7
12:04	12.7	88.7	5.5	18.2
12:05	12.8	89.1	5.4	19.0
12:06	12.9	89.8	5.5	19.2
12:07	13.0	90.5	5.6	19.7
12:08	13.0	90.9	5.6	19.8
12:09	13.2	91.3	5.9	21.0
12:10	13.2	93.2	5.9	20.9
12:11	13.4	92.8	6.0	20.3
12:12	13.2	92.6	6.1	20.6
12:13	13.3	92.6	6.1	25.5
12:14	13.3	93.0	6.2	26.3
12:15	13.3	93.2	6.2	21.4
12:16	13.3	93.0	6.2	23.0
12:17	13.3	93.1	6.1	21.1
12:18	13.3	93.1	6.1	21.5
12:19	13.3	92.9	6.1	20.8
12:20	13.3	92.9	6.0	20.4

AVERAGE VALUES FOR THE LAST 30 MINUTES

12:20	12.9	91.2	6.2	20.2
12:21	13.2	92.8	6.0	20.8
12:22	13.2	92.7	6.0	20.3
12:23	13.2	92.5	5.9	20.1
12:24	13.2	81.8	5.8	20.1
12:25	4.8	80.0	5.6	18.6
12:26	15.8	91.2	5.1	18.7
12:27	12.9	89.6	5.1	19.2
12:28	13.0	90.2	5.2	19.6
12:29	13.1	90.7	5.3	20.8
12:30	13.3	91.2	5.6	20.2
12:31	13.3	91.6	5.8	20.1
12:32	13.4	92.2	5.9	20.1
12:33	13.4	92.3	6.0	19.9
12:34	13.4	92.6	6.2	20.8
12:35	13.5	92.6	6.3	20.5
12:36	13.5	92.8	6.3	20.0
12:37	13.5	93.5	6.3	20.4

Triangle Brick 10-17-1995

	CHAN 8	CHAN 7	CHAN 6	CHAN 1
	STACK2	STACK2	STACK2	STACK2
TIME	ppmNOX	ppmCO	ppmSO2	ppmTHC
12:38	13.5	93.5	6.3	20.2
12:39	13.5	95.8	6.3	19.8
12:40	13.5	93.4	6.4	19.5
12:41	13.5	93.4	6.3	20.1
12:42	13.5	93.2	6.2	19.8
12:43	13.5	93.8	6.1	19.7
12:44	13.5	93.6	6.0	19.1
12:45	13.5	93.5	5.9	19.3
12:46	13.5	93.4	5.8	19.8
12:47	13.2	74.7	5.7	17.9
12:48	4.6	85.9	5.3	17.9
12:49	16.5	91.2	4.8	18.5
12:50	13.1	90.0	4.8	19.2

AVERAGE VALUES FOR THE LAST 30 MINUTES

12:50	13.0	90.9	5.8	19.7
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AVERAGE VALUES FOR THE LAST HOUR: 60 MINUTES OF VALID DATA

12:50	12.9	91.0	6.0	20.0
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COMMENTS: END OF RUN 2

CALIBRATION SUMMARY

SOURCE: Triangle Brick

REASON: SYSTEM BIAS CHECK - POST RUN 2 PRE RUN 3

DATE : 10-17-1995 TIME: 12:50 - 13:04

A/D CHAN	MONITOR DESCRIPTION	UNITS	GAS VALUE	MONITOR RESPONSE
8	STACK2	ppmNOX	0.0	2.4
8	STACK2	ppmNOX	46.3	41.5
7	STACK2	ppmCO	0.0	1.2
7	STACK2	ppmCO	59.9	58.9
6	STACK2	ppmSO2	0.0	1.9
6	STACK2	ppmSO2	45.1	42.9
1	STACK2	ppmTHC	0.0	0.7
1	STACK2	ppmTHC	51.9	50.9

Triangle Brick		10-17-1995		
	CHAN 8	CHAN 7	CHAN 6	CHAN 1
	STACK2	STACK2	STACK2	STACK2
TIME	ppmNOX	ppmCO	ppmSO2	ppmTHC
13:31	13.5	95.5	6.0	19.4
13:32	13.5	95.4	6.0	20.1
13:33	12.0	68.2	5.8	18.6
13:34	7.9	99.7	5.2	18.9
13:35	14.8	93.8	4.9	19.2
13:36	13.3	93.1	5.0	19.4
13:37	13.4	93.4	5.1	19.9
13:38	13.5	94.0	5.5	20.1
13:39	13.6	94.4	5.7	20.1
13:40	13.7	95.0	5.9	20.6
13:41	13.8	95.6	6.0	20.5
13:42	13.9	95.8	6.0	22.8
13:43	13.8	95.9	6.1	37.5
13:44	13.9	96.6	6.0	22.1
13:45	14.0	96.8	6.0	21.6
13:46	13.9	96.5	6.0	21.5
13:47	13.9	96.8	5.9	20.7
13:48	13.9	96.7	5.9	20.8
13:49	13.9	96.8	5.9	20.4
13:50	13.9	96.4	5.9	20.7
13:51	13.9	96.5	6.0	20.3
13:52	13.9	96.6	5.8	20.3
13:53	13.8	96.6	5.8	19.8
13:54	13.8	96.4	5.7	19.9
13:55	13.8	96.0	5.6	19.6
13:56	10.8	60.3	5.5	17.6
13:57	10.4	106.0	4.7	18.7
13:58	14.2	93.9	4.6	19.1
13:59	13.5	93.4	4.9	19.8
14:00	13.6	93.8	5.2	20.0

AVERAGE VALUES FOR THE LAST 30 MINUTES

14:00	13.3	93.9	5.6	20.7
14:01	13.6	94.0	5.4	20.2
14:02	13.7	94.2	5.7	20.3
14:03	13.7	94.6	5.8	20.2
14:04	13.8	95.1	5.9	20.6
14:05	13.8	95.2	5.9	21.1
14:06	13.8	95.4	6.0	20.8
14:07	13.9	95.4	6.0	20.7
14:08	13.9	96.0	6.0	20.6
14:09	13.9	96.3	5.8	21.2
14:10	13.9	96.3	5.8	21.2
14:11	13.8	96.1	5.6	21.3
14:12	13.8	96.1	5.5	20.9
14:13	13.7	96.2	5.5	20.6
14:14	13.8	96.1	5.3	20.4
14:15	13.8	96.3	5.2	20.3
14:16	13.8	96.4	5.0	20.2
14:17	13.9	96.5	4.8	20.7

Triangle Brick 10-17-1995

CHAN 8 CHAN 7 CHAN 6 CHAN 1
STACK2 STACK2 STACK2 STACK2

TIME ppmNOX ppmCO ppmSO2 ppmTHC

14:18	13.8	96.1	4.7	21.1
14:19	9.6	67.5	4.4	19.0
14:20	12.3	109.0	3.6	20.0
14:21	13.9	94.2	3.7	20.5
14:22	13.8	94.1	3.9	20.9
14:23	13.9	94.6	4.3	21.5
14:24	14.0	94.9	4.5	21.0
14:25	14.2	95.4	4.8	21.1
14:26	14.3	96.0	5.0	21.5
14:27	14.3	96.4	5.2	22.5
14:28	14.3	96.3	5.4	22.8
14:29	14.3	96.7	5.4	21.9
14:30	14.3	97.4	5.4	21.7

AVERAGE VALUES FOR THE LAST 30 MINUTES

14:30	13.7	95.1	5.2	20.9
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AVERAGE VALUES FOR THE LAST HOUR: 60 MINUTES OF VALID DATA

14:30	13.5	94.5	5.4	20.8
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COMMENTS: END OF RUN 3

CALIBRATION SUMMARY

SOURCE: Triangle Brick

REASON: SYSTEM BIAS CHECK - POST RUN 3

DATE : 10-17-1995 TIME: 14:30 - 14:48

A/D CHAN	MONITOR DESCRIPTION	UNITS	GAS VALUE	MONITOR RESPONSE
8	STACK2	ppmNOX	0.0	3.5
8	STACK2	ppmNOX	46.3	41.3
7	STACK2	ppmCO	0.0	0.8
7	STACK2	ppmCO	59.9	60.3
6	STACK2	ppmSO2	0.0	1.7
6	STACK2	ppmSO2	45.1	41.6
1	STACK2	ppmTHC	0.0	0.1
1	STACK2	ppmTHC	51.9	50.4

APPENDIX B. FIELD DATA

1. Brick Kiln No. 2 Stack

b. Metals

METHOD 3 (ORSAT) FIELD DATA

Client W. Thers and Ravenel
 Plant Name Triangle Brick
 City/State Merry Oaks N.C.
 Sampling Location Brick Kiln No. 2 Stack

Job No. 14448
 Fuel Type Nat. Gas

Run/Sample No. <u>S-M3-1</u> Date <u>10-17-95</u> Leak ☒ OK?							Operator <u>DDH</u>
Time of Sample Collection	Time of Analysis	CO ₂ Reading (A)	O ₂ Reading (B)	CO Reading (C)	% O ₂ (B-A)	% CO (C-B)	Concurrent Runs to Share Orsat Data
1017	1305	2.4	19.0	—	16.6	—	<u>S-M29-1</u>
—	—	2.4	19.0	—	16.6	—	
1117	1315	2.4	19.0	—	16.6	—	
Avg.		2.4	Avg.		16.6	—	
Orsat I.D. <u>1</u>		Tedlar Bag I.D. <u>—</u>		F ₀ <u>—</u>			

Run/Sample No. <u>S-M3-2</u> Date <u>10-17-95</u> Leak ☒ OK?							Operator <u>DDH</u>
Time of Sample Collection	Time of Analysis	CO ₂ Reading (A)	O ₂ Reading (B)	CO Reading (C)	% O ₂ (B-A)	% CO (C-B)	Concurrent Runs to Share Orsat Data
1150 1010	1344 1305	2.4	19.0	—	16.6	—	<u>S-M29-2</u>
—	—	2.4	19.0	—	16.6	—	
1255 1117	1352 1315	2.4	19.0	—	16.6	—	
Avg.		2.4	Avg.		16.6	—	
Orsat I.D. <u>1</u>		Tedlar Bag I.D. <u>—</u>		F ₀ <u>—</u>			

Run/Sample No. <u>S-M3-3</u> Date <u>10-17-95</u> Leak ☒ OK?							Operator <u>DDH</u>
Time of Sample Collection	Time of Analysis	CO ₂ Reading (A)	O ₂ Reading (B)	CO Reading (C)	% O ₂ (B-A)	% CO (C-B)	Concurrent Runs to Share Orsat Data
1330	1440	2.4	19.0	—	16.6	—	<u>S-M29-3</u>
—	—	2.4	19.0	—	16.6	—	
1436	1450	2.4	19.0	—	16.6	—	
Avg.		2.4	Avg.		16.6	—	
Orsat I.D. <u>1</u>		Tedlar Bag I.D. <u>—</u>		F ₀ <u>—</u>			

SAMPLING DATA - METHOD(S) 29

CLIENT Withers and Ravenel RUN NO. 5-29-1
 PLANT Triangle Brick JOB NO. 14448 DATE 10/17/95
 CITY/STATE Merry Oaks, NC TIME START 1010
 SAMPLING LOC. Brick Kila #2 Stack TIME FINISH 1117
 BAROMETRIC PRESSURE, IN. HG 30.05 STATIC PRESSURE, IN. H₂O -0.35 TEST PERSONNEL TPD, DBW
 LEAK J, VACUUM IN. HG 15 4 POSTTEST POS PRESS LEAK / OK? ☒
 LEAK RATE, CFM .007 .002

• CONDUCT POSTTEST POSITIVE PRESSURE LEAK CHECK FOLLOWING THE LAST RUN PER LOCATION. FOR OTHER RUNS, ENTER "N/A".

EQUIPMENT CHECKS		EQUIPMENT I.D. NUMBERS				LEAK CHECKS	
☒ PITOT, PRETEST	REAGENT BOX <u>M116</u>	METER BOX <u>N-14</u>	Y <u>1.0013</u>	B <u>97.565</u>	B		
☒ PITOT, POSTTEST	PITOT <u>5-24</u>	CP <u>0.84</u>	NOZ'L <u>GLP 1447</u>	DIA. <u>0.313</u>	E <u>97.612</u>	E	
☒ NOZZLE, PRE/POST	TC READOUT <u>F-14</u>	TC PROBE <u>R-385</u>	UMBILICAL <u>11131</u>	B		B	
☒ TC <u>63</u> °F PRE	SAMPL'G BOX <u>54</u>	ORSAT PUMP <u>7</u>	TEDLAR BAG <u>25</u>	E		E	
☒ TC <u>66</u> °F POST					B		B
☒ ORSAT SYSTEM					E		E
		NOMOGRAPH DATA					
FILTER/XAD		TARE WT.	DELTA-H ₂	METER TEMP.		Fyriles, %	
<u>N/A</u>	<u>N/A</u>		<u>1.928</u>	<u>80</u>		<u>5</u>	YOB
			EST. XH ₂ O				<u>961</u>
			"C" FACTOR	<u>1.060</u>			←5% OF CAL'D Y?
			STACK TEMP.	<u>515</u>			(Y) (N)
			REF DELTA-P	<u>0.320</u>			
			"K" FACTOR	<u>5.745</u>			

LINE	SAMPLE POINT	CLOCK TIME, MINUTES	DRY GAS METER READING, CUBIC FEET	PITOT READING, IN. H ₂ O	GAS METER TEMP., °F	STACK TEMP., °F	ORIFICE SETTING, IN. H ₂ O		GAUGE VACUUM, IN. HG	GAS TEMPERATURES, °F		PROBE OR COND EXIT**	✓
							ACTUAL	IDEAL		FILTER *	IMPING. EXIT		
1	A-1	0	75.541	0.18	78	495	1.05	1.05	2	215	58	N/A	
2	2	2 1/2	77.01	0.19	81	495	1.05	1.11	2	245	57		
3	3	5	78.45	0.25	82	498	1.36	1.46	2	242	53		
4	4	7 1/2	80.05	0.25	83	506	1.35	1.45	2	240	52		
5	5	10	81.66	0.24	84	517	1.28	1.38	2	240	52		
6	6	12 1/2	83.23	0.29	86	523	1.57	1.67	2	243	50		
7	7	15	84.95	0.40	87	528	2.19	2.29	2	245	50		
8	8	17 1/2	86.89	0.41	89	532	2.24	2.34	2	245	50		
9	9	20	89.04	0.45	90	516	2.52	2.62	3	248	50		
10	10	22 1/2	91.22	0.43	92	512	2.42	2.52	3	248	50		
11	11	25	93.36	0.42	92	510	2.37	2.47	2	250	50		
12	12	27 1/2	95.48	0.38	94	514	2.13	2.23	2	253	52		
13	B-1	30/0	97.565	0.40	92	487	2.31	2.41	2	258	56		
14	2	2 1/2	99.75	0.49	95	498	2.83	2.93	3	260	52		
15	3	5	102.04	0.53	96	501	3.06	3.16	3	264	49		
16	4	7 1/2	104.52	0.56	96	510	3.21	3.31	3	265	49		
17	5	10	106.98	0.52	96	513	2.96	3.06	3	262	50		
18	6	12 1/2	109.37	0.51	96	514	2.90	3.00	3	262	50		
19	7	15	111.74	0.35	97	517	1.96	2.06	2	260	52		
20	8	17 1/2	113.74	0.30	96	516	1.67	1.77	2	260	53		
21	9	20	115.56	0.28	96	515	1.50	1.65	2	255	53		
22	10	22 1/2	117.28	0.28	96	516	1.50	1.65	2	252	53		
23	11	25	119.01	0.31	95	517	1.67	1.82	2	246	53		
24	12	27 1/2	120.79	0.26	94	496	1.41	1.56	2	240	53		
25	End	60	122.458										

FINAL

* FILTER EXIT for NJ Method 1. FILTER BOX for all others.

** PROBE EXIT & J (probe & filter heat off) apply to NJ Method 1. COND EXIT applies if sampling train has a condenser.

60 46.87 35 91 510 2.02 **58**
 Min. (θ) Vm (ΔP)² tm ts ΔH

SAMPLING DATA - METHOD(S) 29

CLIENT Withers and Ravenel

PLANT Triangle Brick

RUN NO. 5-29-2

CITY/STATE Merry Oaks, NC

JOB NO. 14448

DATE 10/17/95

SAMPLING LOC. Brick Kiln #2 Stack

TIME START 1150

BAROMETRIC PRESSURE, IN. HG 30.50

STATIC PRESSURE, IN. H₂O -0.35

TIME FINISH 1255

LEAK $\checkmark$, VACUUM IN. HG 15

5

TEST PERSONNEL JPD, DAW

LEAK RATE, CFM .004

.002

POSTTEST POS PRESS LEAK $\checkmark$ OK? $\checkmark$

• CONDUCT POSTTEST POSITIVE PRESSURE LEAK CHECK FOLLOWING THE LAST RUN PER LOCATION. FOR OTHER RUNS, ENTER "N/A".

EQUIPMENT CHECKS		EQUIPMENT I.D. NUMBERS		LEAK CHECKS			
$\checkmark$ PITOT, PRETEST	REAGENT BOX <u>M116</u>	METER BOX <u>N-14</u>	V <u>1.0013</u>	B	B		
$\checkmark$ PITOT, POSTTEST	PITOT <u>S-22</u>	Cp <u>0.84</u>	NOZ'L <u>GLP1449</u>	DIA. <u>0.313</u>	E		
$\checkmark$ NOZZLE, PRE/POST	TC READOUT <u>F-14</u>	TC PROBE <u>R325</u>	UMBILICAL <u>U131</u>	B	B		
$\checkmark$ TC <u>68</u> °F PRE	SAMPL'G BOX <u>95</u>	ORSAT PUMP <u>7</u>	TEDLAR BAG <u>88</u>	E	E		
$\checkmark$ TC <u>70</u> °F POST	NOMOGRAPH DATA				B	B	
$\checkmark$ ORSAT SYSTEM					DELTA-H ₂ O <u>1.928</u>	METER TEMP. <u>95</u>	EST. XH ₂ O <u>4</u>
FILTER/XAD	TARE WT.	"CM" FACTOR <u>1.089</u>	STACK TEMP. <u>515</u>	REF DELTA-P <u>0.312</u>	"KM" FACTOR <u>5.905</u>	Fyrites, %	Y ₉₀
<u>N/A</u>	<u>N/A</u>					<5% OF CAL'D Y?	
						(Y)	(N)

L I N E	SAMPLE POINT	CLOCK TIME, MINUTES	DRY GAS METER READING, CUBIC FEET	PITOT READING, IN. H ₂ O	GAS METER TEMP., °F	STACK TEMP., °F	ORIFICE SETTING, IN. H ₂ O		GAUGE VACUUM, IN. HG	GAS TEMPERATURES, °F		PROBE OR COND EXIT**	$\checkmark$
							ACTUAL	IDEAL		FILTER *	IMPING. EXIT		
1	A-12	0	122.698	0.38	88	515	2.11	2.21	3	235	60	N/A	
2	11	2 1/2	124.68	0.40	89	520	2.21	2.31	3	239	56		
3	10	5	126.86	0.38	90	530	2.08	2.18	3	240	56		
4	9	7 1/2	128.85	0.40	92	535	2.19	2.29	3	240	55		
5	8	10	130.85	0.40	92	512	2.25	2.35	4	238	55		
6	7	12 1/2	132.89	0.37	93	518	2.06	2.16	3	235	55		
7	6	15	134.87	0.31	94	521	1.71	1.81	3	235	56		
8	5	17 1/2	136.69	0.26	95	520	1.42	1.52	3	240	56		
9	4	20	138.35	0.23	95	521	1.25	1.35	2	244	57		
10	3	22 1/2	139.93	0.24	95	519	1.31	1.41	2	246	56		
11	2	25	141.51	0.21	95	495	1.16	1.26	2	250	56		
12	1	27 1/2	143.03	0.17	96	485	0.94	1.04	2	250	57		
13	B-12	30/0	144.392	0.28	94	512	1.55	1.65	3	245	58		
14	11	2 1/2	146.13	0.28	96	509	1.56	1.66	3	245	56		
15	10	5	147.86	0.25	96	515	1.37	1.47	3	245	56		
16	9	7 1/2	149.52	0.30	97	520	1.66	1.76	3	247	54		
17	8	10	151.29	0.34	98	516	1.91	2.01	3	248	52		
18	7	12 1/2	153.23	0.42	99	529	2.35	2.45	4	248	52		
19	6	15	155.31	0.46	99	531	2.58	2.68	4	250	51		
20	5	17 1/2	157.54	0.48	100	532	2.70	2.80	4	250	51		
21	4	20	159.82	0.52	100	535	2.92	3.02	5	250	50		
22	3	22 1/2	162.17	0.48	100	513	2.75	2.85	4	252	50		
23	2	25	164.49	0.38	100	511	2.16	2.26	3	255	52		
24	1	27 1/2	166.56	0.31	100	485	1.80	1.90	3	255	53		
25	End	60	168.443										

FINAL

* FILTER EXIT for NJ Method 1. FILTER BOX for all others.

** PROBE EXIT & $\checkmark$ (probe & filter heat off) apply to NJ Method 1. COND EXIT applies if sampling train has a condenser.

60 45.745 .34 96 517 1.928
Min. (θ) Vm (ΔP)² tm ts ΔH

59

SAMPLING DATA - METHOD(S) 29

CLIENT Withers and Ravenel RUN NO. S-29-3
 PLANT Triangle Brick JOB NO. 14448 DATE 10/17/95
 CITY/STATE Merry Oaks, NC TIME START 1330
 SAMPLING LOC. Brick Kiln #2 Stack TIME FINISH 1436
 BAROMETRIC PRESSURE, IN. HG 30.50 STATIC PRESSURE, IN. H₂O -0.35 TEST PERSONNEL JPD, DRW
 LEAK $\checkmark$, VACUUM IN. HG 15 5 POSTTEST POS PRESS LEAK $\checkmark$ OK? *
 LEAK RATE, CFM 0.002 0.000

* CONDUCT POSTTEST POSITIVE PRESSURE LEAK CHECK FOLLOWING THE LAST RUN PER LOCATION. FOR OTHER RUNS, ENTER "N/A".

EQUIPMENT CHECKS		EQUIPMENT I.D. NUMBERS			LEAK CHECKS	
$\checkmark$ PITOT, PRETEST	REAGENT BOX <u>M116</u>	METER BOX <u>N-14</u>	$\checkmark$ <u>1.0013</u>	B	B	
$\checkmark$ PITOT, POSTTEST	PITOT <u>5-24</u>	Cp <u>0.84</u>	NOZ'L <u>GLP714</u>	DIA. <u>0.306</u>	E	E
$\checkmark$ NOZZLE, PRE/POST	TC READOUT <u>F-14</u>	TC PROBE <u>R385</u>	UMBILICAL <u>U131</u>	B	B	
$\checkmark$ TC <u>68</u> °F PRE	SAMPL'G BOX <u>128</u>	ORSAT PUMP <u>7</u>	TEDLAR BAG <u>25</u>	E	E	
$\checkmark$ TC <u>72</u> °F POST	MONOGRAPH DATA			B	B	
$\checkmark$ ORSAT SYSTEM				E	E	
FILTER/XAD	TARE WT.	DELTA-H ₂	METER TEMP.	EST. XH ₂ O	"C" FACTOR	STACK TEMP.
<u>N/A</u>	<u>N/A</u>	<u>1.928</u>	<u>95</u>	<u>7</u>	<u>1.034</u>	<u>515</u>
		REF DELTA-P	"K" FACTOR			
		<u>0.359</u>	<u>5.121</u>			
				Fyrites, %	T ₉₀	
					<u>0.996</u>	
				**5% OF CAL'D T ₉₀		
				(Y) $\checkmark$ (N) <u></u>		

L I N E	SAMPLE POINT	CLOCK TIME, MINUTES	DRY GAS METER READING, CUBIC FEET	PITOT READING, IN. H ₂ O	GAS METER TEMP., °F	STACK TEMP., °F	ORIFICE SETTING, IN. H ₂ O		GAUGE VACUUM, IN. HG	GAS TEMPERATURES, °F		PROBE OR COND EXIT**	$\checkmark$
							ACTUAL	IDEAL		FILTER	IMPING. EXIT		
1	A-12	0	168.692	0.36	88	521	1.80	1.90	3	260	62	N/A	
2	11	2 1/2	170.51	0.34	86	511	1.71	1.81	3	260	60		
3	10	5	172.41	0.37	86	505	1.88	1.98	3	257	60		
4	9	7 1/2	174.25	0.36	86	507	1.82	1.82	3	255	59		
5	8	10	176.11	0.38	85	510	1.82	1.92	3	260	59		
6	7	12 1/2	177.92	0.37	85	513	1.76	1.86	3	264	59		
7	6	15	179.73	0.25	85	514	1.16	1.26	3	268	58		
8	5	17 1/2	181.26	0.23	84	512	1.06	1.16	2	265	58		
9	4	20	182.69	0.22	84	512	1.01	1.11	2	262	58		
10	3	22 1/2	184.09	0.22	84	498	1.02	1.12	2	255	58		
11	2	25	185.48	0.23	84	485	1.09	1.19	2	253	58		
12	1	27 1/2	186.94	0.18	85	478	0.84	0.94	2	250	59		
13	B-12	30/0	188.264	0.28	87	507	1.32	1.42	2	250	58		
14	11	2 1/2	189.87	0.30	90	512	1.42	1.52	2	247	57		
15	10	5	191.52	0.29	91	518	1.37	1.47	2	248	57		
16	9	7 1/2	193.16	0.27	92	521	1.26	1.36	2	255	57		
17	8	10	194.72	0.28	92	525	1.31	1.41	2	255	57		
18	7	12 1/2	196.29	0.34	93	506	1.65	1.75	3	255	56		
19	6	15	198.05	0.44	94	510	2.16	2.26	4	256	54		
20	5	17 1/2	200.05	0.45	96	513	2.20	2.36	4	260	54		
21	4	20	202.11	0.55	97	515	2.72	2.82	5	260	52		
22	3	22 1/2	204.37	0.49	98	507	2.41	2.51	4	260	52		
23	2	25	206.55	0.40	98	493	2.00	2.10	4	262	53		
24	1	27 1/2	208.54	0.38	97	488	1.90	2.00	4	264	53		
25	End	60	210.462										

FINAL

* FILTER EXIT for NJ Method 1. FILTER BOX for all others.

** PROBE EXIT $\checkmark$ (probe & filter heat off) apply to NJ Method 1. COND EXIT applies if sampling train has a condenser.

60 41.77 33 89.5 508 1.61
 Min. (θ) Vm ($\sqrt{\Delta P}$)² tm ts ΔH

60

MOISTURE ANALYTICAL RESULTS FOR MULTIMETAL SAMPLING TRAINS AND/OR SAMPLING TRAINS USING KMnO₄ REAGENT FOR Hg

Client Withers and Ravenel Job No. 14448
 Plant Name Triangle Brick Job No. 14884
 City/State Merry Oaks, N.C. Sampling Loc. Brick Kiln #2 Stack

Run Number	S-M29-1	S-M29-2	S-M29-3
Sampling Date	<u>10/17/95</u>	<u>10/17/95</u>	<u>10/17/95</u>
Analysis Date	<u>10/17/95</u>	<u>10/17/95</u>	<u>10/17/95</u>
Analyst	<u>JRW</u>	<u>JRW</u>	<u>JRW</u>
Reagent ^{200 mL} (5% HNO ₃ /10% H ₂ O ₂)			
Final Weight, g	<u>316.5</u>	<u>332.5</u>	<u>315.0</u>
Tared Weight, g	<u>265.1</u>	<u>277.9</u>	<u>266.0</u>
Water Catch, g	<u>51.4</u>	<u>54.6</u>	<u>49.0</u>
Reagent (3 Impinger (bnd.)			
Final Weight, g	<u>225.6</u>	<u>221.4</u>	<u>220.9</u>
Tared Weight, g	<u>219.8</u>	<u>219.3</u>	<u>218.7</u>
Water Catch, g	<u>5.8</u>	<u>2.1</u>	<u>2.2</u>
Reagent ^{200 mL} (4% KMnO ₄ /10% H ₂ SO ₄)			
Final Weight, g	<u>442.6</u>	<u>447.2</u>	<u>443.3</u>
Empty Tared Weight, g	<u>217.6</u>	<u>219.7</u>	<u>218.7</u>
Difference, g	<u>225</u>	<u>227.5</u>	<u>224.6</u>
mL used, KMnO ₄ , g •	<u>(200 mL) = 220g</u>	<u>(200 mL) = 220g</u>	<u>(200 mL) = 220g</u>
Water Catch, g	<u>9.0</u>	<u>7.5</u>	<u>4.6</u>
CONDENSED WATER, g	<u>62.2</u>	<u>64.2</u>	<u>55.8</u>

• Since 4% KMnO₄/10% H₂SO₄ weighs 1.1 g/mL, multiply mL KMnO₄ used • 1.1 g/mL = total g tare to be subtracted.
 Enter/deduct actual mL KMnO₄ used.

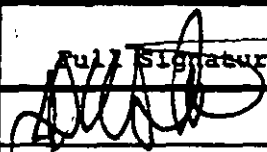
Silica Gel			
Final Weight, g	<u>197.2</u>	<u>199.2</u>	<u>206.4</u>
Tared Weight, g	<u>184.7</u>	<u>189.9</u>	<u>195.6</u>
ADSORBED WATER, g	<u>12.5</u>	<u>9.3</u>	<u>10.8</u>

TOTAL WATER COLLECTED, g	<u>74.7</u>	<u>73.5</u>	<u>66.6</u>
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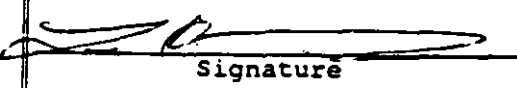
Balance No. EEI 13 Type (✓) Triple Beam ☒ Electronic _____ Reagent Box No. M116
 Balance located in stable, draft-free area (✓) Yes ☒ No _____ (If "No", explain below.)
 Comments _____

RECORD OF CUSTODY, CONTAINER No. M116

Client The Brick Association Job No. 14884
 Plant Name Triangle Brick
 City/State Merry Oaks, N.C.
 Sampling Method(s) EPA M29 (EPA, NIOSH, etc.)
 Container Type (V) Reagent Box ☒ Cooler ☐ Other (specify) _____

Seal No. or "PC"	Date	Time	*	Signature	Reason for Breaking Seal**
608	10/13	1627	S		
	10/16	1130	B	Joe W. Winder	change train
2518	10/18	0932	S	Joe W. Winder	
			B		
			S		
			B		
			S		
			B		
			S		
			B		
			S		
			B		
			S		
			B		

PC = Personal Custody * S = Sealed By; B = Broken By ** Use "REMARKS" Section if more space needed.

Container Received by Entropy Sample Custodian			Seal Intact? **	
	10/23/95	10:20	Yes ☒	No ☐ NA ☐
Signature	Date	Time		

As Applicable:

All liquid levels at mark (✓) YES ☐ NO ☐ (Estimate loss if not at mark; describe in "REMARKS")

As Applicable:

TUBE SAMPLES put in freezer by _____ Date _____ Time _____

CONDENSATE SAMPLES put in refrige. by _____ Date _____ Time _____

REMARKS _____ 62

FIELD SAMPLE RECOVERY QUALITY CONTROL

Box No. M116 Assembly Date 10/13/95 Assembled By JIS
 Client The Brick Association Job No. 14884
 Plant Triangle Brick City/State Merry Oaks, N.C.
 Sampling Loc. Stack Brick Kiln #2 Stack Method EPA 29
 Individual Tare Of Reagent 200 (Ml) (g) of 5% H₂O₃ / 10% H₂O₂ K
 Individual Tare Of Reagent _____ (Ml) (gm) Of _____
 Individual Tare Of Reagent _____ (Ml) (gm) Of _____
 Individual Tare Of Sil. Gel _____ Gm _____
 other (specify) _____

Run Number	Run Date	Filter or XAD Number	Tare, grams	Liquid Tare at Mark? @	Init.	Sample Recov. Date	%Sil. Gel Spent	Liquid Level Marked?	Init.
S-M29-1	10/17	AT		✓	JRN	10/17	30	✓	JRN
		unnumbered, untared							
S-M29-2	10/17	unnumbered untared		✓	JRN	10/17	30	✓	JRN
S-M29-3	10/17	unnumbered untared		✓	JRN	10/17	20	✓	JRN

* Use "REMARKS" section if needed.

@ All liquid levels at mark? (check) YES ___ NO ___ (estimate loss if not at mark; use "REMARKS" section).

REMARKS _____

RECORD OF CUSTODY, CONTAINER No. M151

Client Withers and Ravenel Job No. 14448
 Plant Name Triangle Brick
 City/State Merry Oaks, N.C.
 Sampling Method(s) EPA 1129 (EPA, NIOSH, etc.)
 Container Type (V) Reagent Box ☒ Cooler ☐ Other (specify) ☐

Seal No. or "PC"	Date	Time	*	Full Signature	Reason for Breaking Seal**
416	9/18	1621	S	<i>[Signature]</i>	
1525	9/17/95	0835	B	<i>Joe W. Withers</i>	label jars
2732	10/18	0954	S	<i>Joe W. Withers</i>	
			B		
			S		
			B		
			S		
			B		
			S		
			B		
			S		
			B		

PC = Personal Custody * S = Sealed By; B = Broken By ** Use "REMARKS" Section if more space needed.

Container Received by Entropy Sample Custodian			Seal Intact? **	
<i>[Signature]</i>	<u>10/23/95</u>	<u>1023</u>	Yes ☒	No ☐ NA ☐
Signature	Date	Time		

As Applicable:

All liquid levels at mark (✓) YES ☐ NO ☐ (Estimate loss if not at mark; describe in "REMARKS")

As Applicable:

TUBE SAMPLES put in freezer by _____ Date _____ Time _____

CONDENSATE SAMPLES put in refrige. by _____ Date _____ Time _____

REMARKS _____

FIELD SAMPLE RECOVERY QUALITY CONTROL

Box No. M151 Assembly Date 9-18-95 Assembled By JLS
 Client Withers and Ravenel Job No. 14448
 Plant Triangle Brick City/State Cherry Oaks, N.C.
 Sampling Loc. Brick Kiln #2 Stack Method EPA m29
 Individual Tare Of Reagent 200 (Ml) (gm) Of 5% H₂O₃/10% H₂O₂ K
 Individual Tare Of Reagent _____ (Ml) (gm) Of _____
 Individual Tare Of Reagent _____ (Ml) (gm) Of _____
 Individual Tare Of Sil. Gel _____ Gm _____
 other (specify) _____

Run Number	Run Date	Filter or XAD Number	Tare, grams	Liquid Tare at Mark? @	Init.	Sample Recov. Date	%Sil. Gel Spent	Liquid Level Marked?	Init.
4-m29--FB	10/17	UNNUMBERED	untested	✓	JRN	10/17	NA	✓	JRN
				Filter Appearance*					
				clean					
				Reagents Appearance*					
				clear / purple					
				Filter Appearance*					
				Reagents Appearance*					
				Filter Appearance*					
				Reagents Appearance*					
				Filter Appearance*					
				Reagents Appearance*					

* Use "REMARKS" section if needed.

@ All liquid levels at mark? (check) YES _____ NO _____ (estimate loss if not at mark; use "REMARKS" section).

REMARKS _____

RECORD OF CUSTODY, CONTAINER No. 1008

client The Brick Association

Job No. 14448
14837

Plant Name Triangle Brick

City/State Merry Oaks, N.C.

Sampling Method(s) EPA M29 (EPA, NIOSH, etc.)

Container Type (V) Reagent Box ☒ Cooler ☐ Other (specify) _____

Seal No. or "PC"	Date	Time	*	Full Signature	Reason for Breaking Seal**
2239	10/18	0943	S	<i>[Signature]</i>	
			B		
			S		
			B		
			S		
			B		
			S		
			B		
			S		
			B		
			S		
			B		
			S		
			B		

PC = Personal Custody

* S = Sealed By; B = Broken By

** Use "REMARKS" Section if more space needed.

Container Received by Entropy Sample Custodian

Seal Intact?**

Signature *[Signature]*

Date 10/23/85

Time 1021

Yes ☒ No ☐ NA ☐

As Applicable:

All liquid levels at mark (✓) YES ☐ NO ☐ (Estimate loss if not at mark; describe in "REMARKS")

As Applicable:

TUBE SAMPLES put in freezer by _____ Date _____ Time _____

CONDENSATE SAMPLES put in refrige. by _____ Date _____ Time _____

REMARKS _____

FIELD SAMPLE QUALITY CONTROL

14-CAPACITY CONTAINER

Box No. 1008 Assembly Date _____ Assembled By _____
 Client The Brick Association Job No. 14448
14884
 Plant Triangle Brick City/State Merry Oaks, N.C.

Run/Sample ID	Component*	Recovery		
		Date	Time	Initials
S-m29-1	KMnO ₄ Reagent	10/17	NA	JRW
S-m29-1	HCl Rinse	10/17		JRW
S-m29-2	KMnO ₄ Reagent	10/17		JRW
S-m29-2	HCl Rinse	10/17		JRW
S-m29-3	KMnO ₄ Reagent	10/17		JRW
S-m29-3	HCl Rinse	10/17		JRW
S-m29-FB	KMnO ₄ Reagent	10/17		JRW
S-m29-FB	HCl Rinse	10/17		JRW
K29-RB	KMnO ₄ Reagent	10/17	✓	JRW

* Component = rinses, reagents, etc. (e.g., H₂SO₄ Rinse, NaOH Rinse, H₂SO₄ Reagent, Probe Rinse, etc.)

All liquid levels at mark (check)? Yes ☐ No ☐
 (estimate loss if not at mark; use REMARKS section).

Remarks

APPENDIX B. FIELD DATA

1. Brick Kiln No. 2 Stack

c. Methane

EVACUATED TANK PARAMETERS

Client Withers and Ravenel
 Plant Name Triangle Brick Job No. 14884
 City/State Merry Oaks, N.C. Sampling Loc. Brick Kiln #2 Stack

Tank No. 183 Tank Volume, liters 4.59 Sampling Time Start 1010
 From Sampling Run No. S-M29-1 Sampling Time Finish 1117
 Sample Transfer Run No. S-M18MOD-1 Sample Transfer Date & Time 10/17/95, 1130

Parameter	Barometric Pressure *		Tank Temp. *		Tank Pressure Gauge *		Leak Check cm Hg change	
	In. Hg	mm Hg	°F	°C	In. Hg	mm Hg	Tank	System
Pretest	30.5	774.7	58		-751	-752	0.00	0.00
Posttest	30.5	774.7	58		-	-752	0.00	0.00
1st (Field) Pressurization					+		JRW Operator	

Tank No. 233 Tank Volume, liters 4.51 Sampling Time Start 1150
 From Sampling Run No. S-M29-2 Sampling Time Finish 1255
 Sample Transfer Run No. S-M29-2 S-M18MOD-2 Sample Transfer Date & Time 10/17/95, 1324

Parameter	Barometric Pressure *		Tank Temp. *		Tank Pressure Gauge *		Leak Check cm Hg change	
	In. Hg	mm Hg	°F	°C	In. Hg	mm Hg	Tank	System
Pretest	30.5	774.7	62		-	-756	0.00	0.00
Posttest	30.5	774.7	62		-	0	0.00	0.00
1st (Field) Pressurization					+		JRW Operator	

Tank No. 242 Tank Volume, liters 4.51 Sampling Time Start 1330
 From Sampling Run No. S-M29-3 Sampling Time Finish 1436
 Sample Transfer Run No. S-M18MOD-3 Sample Transfer Date & Time

Parameter	Barometric Pressure *		Tank Temp. *		Tank Pressure Gauge *		Leak Check cm Hg change	
	In. Hg	mm Hg	°F	°C	In. Hg	mm Hg	Tank	System
Pretest	30.5	774.7	65		-	-756	0.00	0.00
Posttest	30.5	774.7	65		-	0	0.00	0.00
1st (Field) Pressurization					+		JRW Operator	

* As applicable, use In. Hg or mm Hg, and °F or °C. Note: mm Hg = In. Hg * 25.401

APPENDIX B. FIELD DATA

1. Brick Kiln No. 2 Stack

d. Particulate

5

RUN NO. S-MS-1

JOB NO. 14448

DATE 10/18/95

TIME START 0901

STATIC PRESSURE, IN. H₂O -0.35

TIME FINISH 1005

15 10"

TEST PERSONNEL JPD, DDH

.003 0003

POSTTEST POS PRESS LEAK ✓ OK? ●

* CONDUCT POSTTEST POSITIVE PRESSURE LEAK CHECK FOLLOWING THE LAST RUN PER LOCATION. FOR OTHER RUNS, ENTER "N/A".

[illegible]

• FILTER EXIT for NJ Method 1. FILTER BOX for all others.

** PROBE EXIT & √ (probe & filter heat off) apply to NJ Method 1. COND EXIT applies if sampling train has a condenser.

$$\frac{60}{\text{Min. } (\theta)} \quad \frac{42.407}{V_m} \quad \frac{.32}{(\sqrt{A_P})^2} \quad \frac{78}{t_m} \quad \frac{518}{t_s} \quad \frac{1.69}{\Delta H} \quad 75$$

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SAMPLING DATA - METHOD(S) 5

CLIENT Withers and Ravenel
 PLANT Triangle Brick
 CITY/STATE Merry Oaks, NC
 SAMPLING LOC. Brick Kiln #2 Stack
 BAROMETRIC PRESSURE, IN. HG 30.50 STATIC PRESSURE, IN. H₂O -0.35
 LEAK $\checkmark$, VACUUM IN. HG 15 10" TEST PERSONNEL JPD, DDH
 LEAK RATE, CFM .002 0.002 POSTTEST POS PRESS LEAK $\checkmark$ OK? *

RUN NO. 5-15-8
 JOB NO. 14448 DATE 10/18/95
 TIME START 1039
 TIME FINISH 1142

• CONDUCT POSTTEST POSITIVE PRESSURE LEAK CHECK FOLLOWING THE LAST RUN PER LOCATION. FOR OTHER RUNS, ENTER "N/A".

EQUIPMENT CHECKS		EQUIPMENT I.D. NUMBERS		LEAK CHECKS	
$\checkmark$ PITOT, PRETEST	REAGENT BOX <u>0210</u>	METER BOX <u>N-14</u>	<u>Y 1.0033</u>	B	B
$\checkmark$ PITOT, POSTTEST	PITOT <u>5-24</u>	<u>0.84</u> NOZ'L <u>GLP714</u>	DIA. <u>0.306</u>	E	E
$\checkmark$ NOZZLE, PRE/POST	TC READOUT <u>F-14</u>	TC PROBE <u>R-385</u>	UMBILICAL <u>1131</u>	B	B
$\checkmark$ TC <u>70</u> °F PRE	SAMPL'G BOX <u>128</u>	ORSAT PUMP <u>7</u>	TEDLAR BAG <u>66</u>	E	E
$\checkmark$ TC <u>76</u> °F POST				B	B
$\checkmark$ ORSAT SYSTEM				E	E
		NOMOGRAPH DATA		B	B
		DELTA-H ₂ <u>1.928</u>		E	E
FILTER/XAD	TARE WT.	METER TEMP. <u>95</u>		B	B
<u>TGF060</u>	<u>0.4707</u>	EST. XH ₂ O <u>7</u>		E	E
		"C" FACTOR <u>1.034</u>		Fyrites, % <u>96.9</u>	
		STACK TEMP. <u>515</u>		Y ₉₀ <u>96.9</u>	
		REF DELTA-P <u>0.359</u>		←5% OF CAL'D Y? <u>(Y)</u>	
		"K" FACTOR <u>5.121</u>		(Y) (N)	

L I N E	SAMPLE POINT	CLOCK TIME, MINUTES	DRY GAS METER READING, CUBIC FEET	PITOT READING, IN. H ₂ O	GAS METER TEMP., °F	STACK TEMP., °F	ORIFICE SETTING, IN. H ₂ O ACTUAL IDEAL	GAUGE VACUUM, IN. HG	GAS TEMPERATURES, °F FILTER * IMPING. EXIT	PROBE OR COND EXIT**	
1	B-12	0	253.302	0.28	92	515	1.33 1.43	2	265 62	N/A	
2	11	2 1/2	254.95	0.29	94	517	1.38 1.48	2	262 61		
3	10	5	256.54	0.33	96	520	1.58 1.68	2	260 58		
4	9	7 1/2	258.28	0.31	98	525	1.48 1.58	2	260 58		
5	8	10	259.98	0.32	98	529	1.52 1.62	2	262 58		
6	7	12 1/2	261.69	0.37	98	531	1.80 1.90	3	265 56		
7	6	15	263.56	0.48	100	514	2.38 2.48	4	263 53		
8	5	17 1/2	265.67	0.55	102	518	2.73 2.83	4	260 52		
9	4	20	267.95	0.56	104	519	2.79 2.89	4	259 52		
10	3	22 1/2	270.28	0.57	104	512	2.86 2.96	4	255 52		
11	2	25	272.64	0.47	106	510	2.35 2.45	4	255 53		
12	1	27 1/2	274.78	0.42	106	508	2.10 2.20	3	255 53		
13	A-12	30/0	276.797	0.40	102	518	1.96 2.06	3	250 57		
14	11	2 1/2	278.78	0.42	105	511	2.09 2.19	3	250 55		
15	10	5	280.78	0.38	106	509	1.89 1.99	3	251 54		
16	9	7 1/2	282.69	0.41	106	510	2.05 2.15	3	252 54		
17	8	10	284.71	0.39	106	513	1.93 2.03	3	250 54		
18	7	12 1/2	286.64	0.40	106	518	1.98 2.08	3	247 54		
19	6	15	288.59	0.37	106	521	1.81 1.91	3	246 55		
20	5	17 1/2	290.47	0.27	106	521	1.30 1.40	2	248 55		
21	4	20	292.10	0.28	104	522	1.34 1.44	2	248 56		
22	3	22 1/2	293.72	0.26	104	522	1.24 1.34	2	249 56		
23	2	25	295.29	0.27	104	511	1.31 1.41	2	247 56		
24	1	27 1/2	296.91	0.19	103	512	0.89 0.99	2	247 57		
25	End	60	298.247								

FINAL

* FILTER EXIT for NJ Method 1. FILTER BOX for all others.

** PROBE EXIT & $\checkmark$ (probe & filter heat off) apply to NJ Method 1. COND EXIT applies if sampling train has a condenser.

60 44.94 0.37 102 516 1.83
 Min. (θ) Vm (ΔP)² tm ts ΔH

76

SAMPLING DATA - METHOD(S) 5

CLIENT Withers and Ravenel

PLANT Triangle Brick

RUN NO. 5-M5-3

CITY/STATE Mary Oaks, NC

JOB NO. 14448

DATE 10/18/95

SAMPLING LOC. Brick Kiln #2 Stack

TIME START 1221

BAROMETRIC PRESSURE, IN. HG 30.53

STATIC PRESSURE, IN. H₂O -0.35

TIME FINISH 1324

LEAK V, VACUUM IN. HG 15 10"

TEST PERSONNEL JPD, DPH

LEAK RATE, CFM .006 0.006

POSTTEST POS PRESS LEAK / OK?

* CONDUCT POSTTEST POSITIVE PRESSURE LEAK CHECK FOLLOWING THE LAST RUN PER LOCATION. FOR OTHER RUNS, ENTER "N/A".										
EQUIPMENT CHECKS		EQUIPMENT I.D. NUMBERS						LEAK CHECKS		
☒ PITOT, PRETEST	REAGENT BOX <u>0210</u>	METER BOX <u>N-14</u>	V <u>1.0013</u>	B						
☒ PITOT, POSTTEST	PITOT <u>5-22</u>	Cp <u>0.84</u>	NOZ'L <u>GLP1449</u>	DIA. <u>0.313</u>	E					
☒ NOZZLE, PRE/POST	TC READOUT <u>F-14</u>	TC PROBE <u>R-325</u>	UMBILICAL <u>U131</u>	B						
☒ TC <u>76</u> °F PRE	SAMPL'G BOX <u>95</u>	ORSAT PUMP <u>7</u>	TEDLAR BAG <u>25</u>	E						
☒ TC <u>77</u> °F POST							B			
☒ ORSAT SYSTEM							E			
FILTER/XAD		NOMOGRAPH DATA						Fyrites, %		
<u>E4512</u>	TARE WT. <u>0.4491</u>	DELTA-H ₂ O <u>1.928</u>	METER TEMP. <u>100</u>	EST. XH ₂ O <u>7</u>	"C" FACTOR <u>1.043</u>	STACK TEMP. <u>515</u>	REF DELTA-P <u>0.325</u>	"K" FACTOR <u>5.657</u>	Y₉₈	
								≤5% OF CAL'D Y?		
								(Y) (N)		

LINE	SAMPLE POINT	CLOCK TIME, MINUTES	DRY GAS METER READING, CUBIC FEET	PITOT READING, IN. H ₂ O	GAS METER TEMP., °F	STACK TEMP., °F	ORIFICE SETTING, IN. H ₂ O		GAUGE VACUUM, IN. HG	GAS TEMPERATURES, °F		PROBE OR COND. EXIT**
							ACTUAL	IDEAL		FILTER °	IMPING. EXIT	
1	B-12	0	298.566	0.30	99	522	1.58	1.68	2	238	63	N/A
2	11	2 1/2	300.26	0.32	101	518	1.70	1.80	2	240	61	
3	10	5	302.05	0.29	102	513	1.55	1.65	2	244	59	
4	9	7 1/2	303.80	0.28	102	511	1.49	1.59	2	245	59	
5	8	10	305.51	0.27	102	515	1.43	1.53	2	245	59	
6	7	12 1/2	307.19	0.26	104	518	1.37	1.47	2	247	58	
7	6	15	308.84	0.28	104	523	1.48	1.58	2	250	58	
8	5	17 1/2	310.54	0.46	106	529	2.49	2.59	4	250	55	
9	4	20	312.71	0.47	106	531	2.53	2.63	4	250	54	
10	3	22 1/2	314.93	0.53	107	532	2.87	2.97	5	251	52	
11	2	25	317.29	0.57	107	513	3.15	3.25	5	250	51	
12	1	27 1/2	319.79	0.35	108	508	1.91	2.01	4	252	53	
13	A-12	30/0	321.775	0.35	105	513	1.90	2.00	4	253	56	
14	21	2 1/2	323.67	0.39	106	517	2.12	2.22	4	253	55	
15	10	5	325.69	0.36	108	522	1.94	2.04	4	251	54	
16	9	7 1/2	327.66	0.39	108	528	2.10	2.20	4	250	54	
17	8	10	329.66	0.38	109	532	2.04	2.14	4	250	54	
18	7	12 1/2	331.66	0.40	110	536	2.15	2.25	4	252	54	
19	6	15	333.69	0.35	111	525	1.89	1.99	4	251	54	
20	5	17 1/2	335.65	0.26	110	512	1.40	1.50	3	251	55	
21	4	20	337.34	0.27	110	514	1.45	1.55	3	253	55	
22	3	22 1/2	339.03	0.26	109	514	1.39	1.49	3	254	55	
23	2	25	340.69	0.23	109	509	1.23	1.33	2	254	56	
24	1	27 1/2	342.29	0.18	108	506	0.94	1.04	2	253	56	
25	End	60	343.664									

FINAL

* FILTER EXIT for NJ Method 1. FILTER BOX for all others.

** PROBE EXIT & / (probe & filter heat off) apply to NJ Method 1. COND EXIT applies if sampling train has a condenser.

160 45.098 .34 106 519 1.84
Min. (B) Vm (ΔP)² tm ts ΔH

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MOISTURE ANALYTICAL RESULTS

Client Withers and Ravenel

Plant Name Triangle Brick

Job No. 14448
14884

City/State Merry Oaks, N.C. Sampling Loc. Brick Kiln #2 Stack

Run Number	S-M5-1	S-M5-2	S-M5-3
Sampling Date	<u>10/18/95</u>	<u>10/18/95</u>	<u>10/18/95</u>
Analysis Date	<u>10/18/95</u>	<u>10/18/95</u>	<u>10/18/95</u>
Analyst	<u>JRW</u>	<u>JRW</u>	<u>JRW</u>

200mk Reagent 1 (DI H₂O) Final Weight, g Tared Weight, g Water Catch, g	749.8 693.2 52.6	740.9 689.3 51.6	749.2 690.6 58.6
Reagent 2 () Final Weight, g Tared Weight, g Water Catch, g			
Reagent 3 () Final Weight, g Tared Weight, g Water Catch, g			
CONDENSED WATER, g			

Silica Gel Final Weight, g Tared Weight, g	205.5 191.7	208.9 196.2	201.8 191.8
ADSORBED WATER, g	13.8	12.7	10.0

TOTAL WATER COLLECTED, g	66.4	64.3	68.6
--------------------------	------	------	------

Balance No. EEI 13 Type ☒ Triple Beam ☒ Electronic Reagent Box No. 0210

Balance located in stable, draft-free area ☒ Yes ☐ No (If "No", explain below.)

Comments _____

RECORD OF CUSTODY, CONTAINER No. 210

client Withers & Ravenel Job No. 14884
 Plant Name Triangle Brick
 City/State Merry Oaks, N.C.
 Sampling Method(s) EPA Method 5 (EPA, NIOSH, etc.)
 Container Type (v) Reagent Box ☒ Cooler ☐ Other (specify) ☐

Seal No. or "PC"	Date	Time	*	Full Signature	Reason for Breaking Seal**
911	9/26	1544	S	<i>[Signature]</i>	
	10/16/95	1535	B	<i>Joe Winder</i>	label jars
2261	10/18/95	1520	S	<i>Joe Winder</i>	
			B		
			S		
			B		
			S		
			B		
			S		
			B		
			S		
			B		

PC = Personal Custody * S = Sealed By; B = Broken By ** Use "REMARKS" Section if more space needed.

Container Received by Entropy Sample Custodian			Seal Intact?**	
<u>Sean Daley</u>	<u>10/24/95</u>	<u>1320</u>	Yes ☒	No ☐ NA ☐
Signature	Date	Time		

As Applicable:

All liquid levels at mark (✓) YES ☐ NO ☐ (Estimate loss if not at mark; describe in "REMARKS")

As Applicable:

TUBE SAMPLES put in freezer by _____ Date _____ Time _____

CONDENSATE SAMPLES put in refrige. by _____ Date _____ Time _____

REMARKS _____

FIELD SAMPLE RECOVERY QUALITY CONTROL

Box No. 210 Assembly Date 9.26.95 Assembled By JUS
 Client Withers and Ravenel Job No. 14884
 Plant Triangle Brick City/State Merry Oaks, NC
 Sampling Loc. Brick Kiln #2 Stack Method EPA M5
 Individual Tare Of Reagent 200 (Ml) (gm) of D1 H₂O
 Individual Tare Of Reagent _____ (Ml) (gm) Of _____
 Individual Tare Of Reagent _____ (Ml) (gm) Of _____
 Individual Tare Of Sil. Gel _____ Gm _____

other (specify) _____

Run Number	Run Date	Filter or XAD Number	Tare, grams	Liquid Tare at Mark? @	Init.	Sample Recov. Date	%Sil. Gel Spent	Liquid Level Marked?	Init.
S-M5-1	10/18	TGFCX	0.4673	✓	JRN	10/18	50	✓	JRN
				Filter Appearance*					
				<u>very light coating w/ small granules</u>					
				Reagents Appearance*					
				<u>light coag clear</u>					
S-M5-2	10/18	TGFC0	0.470R	✓	JRN	10/18/95	60	✓	JRN
				Filter Appearance*					
				<u>light coating</u>					
				Reagents Appearance*					
				<u>clear</u>					
S-M5-3	10/18	F4512	0.4491	✓	JRN	10/18	50	✓	JRN
				Filter Appearance*					
				<u>very light coating</u>					
				Reagents Appearance*					
				<u>clear</u>					
				Filter Appearance*					
				Reagents Appearance*					

* Use "REMARKS" section if needed.

@ All liquid levels at mark? (check) YES _____ NO _____ (estimate loss if not at mark; use "REMARKS" section).

REMARKS _____

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RECORD OF CUSTODY, CONTAINER No.

565

Client Withers and Ravenel Job No. 14448
 Plant Name Triangle Brick
 City/State Merry Oaks, N.C.
 Sampling Method(s) EPA 149, 201A, 202 (EPA, NIOSH, etc.)
 Container Type (v) Reagent Box ☒ Cooler ☐ Other (specify) ☐

Seal No. or "PC"	Date	Time	*	Signature	Reason for Breaking Seal**
14	9/26	1544	S	<i>[Signature]</i>	
	10/17/95	0930	B	<i>Joe W. Wilson</i>	label jars
2135	10/18/95	1519	S	<i>Joe W. Wilson</i>	
			B		
			S		
			B		
			S		
			B		
			S		
			B		
			S		
			B		
			S		
			B		

PC = Personal Custody * S = Sealed By; B = Broken By ** Use "REMARKS" Section if more space needed.

Container Received by Entropy Sample Custodian			Seal Intact? **
<i>Sean Daler</i> Signature	10/24/95 Date	1315 Time	Yes ☒ No ☐ NA ☐

As Applicable:

All liquid levels at mark (✓) YES ☐ NO ☐ (Estimate loss if not at mark; describe in "REMARKS")

As Applicable:

TUBE SAMPLES put in freezer by _____ Date _____ Time _____

CONDENSATE SAMPLES put in refrige. by _____ Date _____ Time _____

REMARKS _____

FIELD SAMPLE RECOVERY QUALITY CONTROL

Box No. 565 Assembly Date 9.26.95 Assembled By JLS

Client Withers and Ravel Job No. 1444P

Plant Triangle Brick City/State Merry Oaks, NC

Sampling Loc. Brick Kiln #2 Stack Method EPA 5, 201A,

Individual Tare Of Reagent 200 (Ml) (gm) Of DI H₂O 202

Individual Tare Of Reagent _____ (Ml) (gm) Of _____

Individual Tare Of Reagent _____ (Ml) (gm) Of _____

Individual Tare Of Sil. Gel _____ Gm _____

other (specify)

Run Number	Run Date	Filter or XAD Number	Tare, grams	Liquid Tare at Mark? @	Init.	Sample Recov. Date	%Sil. Gel Spent	Liquid Level Marked?	Init.

Reagent Blanks:
Acetone
DI H₂O
HCl

Filter Appearance*

Reagents Appearance*

--	--	--	--	--	--	--	--	--	--

Filter Appearance*

Reagents Appearance*

--	--	--	--	--	--	--	--	--	--

Filter Appearance*

Reagents Appearance*

--	--	--	--	--	--	--	--	--	--

Filter Appearance*

Reagents Appearance*

* Use "REMARKS" section if needed.

@ All liquid levels at mark? (check) YES _____ NO _____ (estimate loss if not at mark; use "REMARKS" section).

REMARKS _____

APPENDIX B. FIELD DATA

1. Brick Kiln No. 2 Stack

**e. Particulate $\leq$ 10 Microns and
Condensible Particulate**

Sampling and Velocity Traverse Point Determination EPA Method 1

CLIENT Withers & Ravenel
 PLANT NAME Triangle Brick
 CITY, STATE Merry Oaks N.C.
 SAMPLING LOCATION Brick Kiln No. 2 Stack

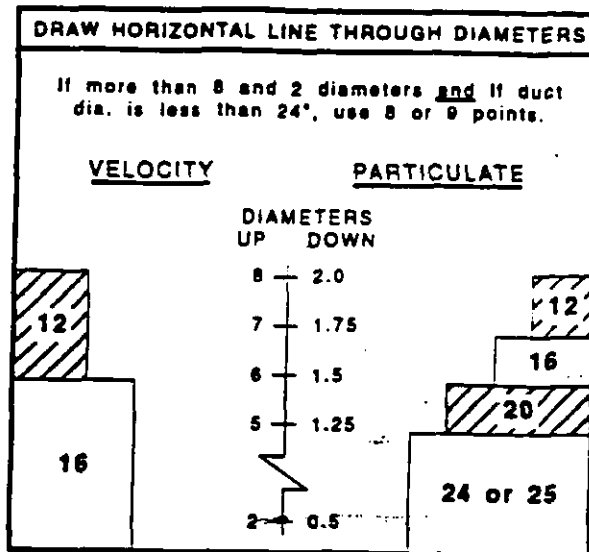
NO. OF PORTS AVAILABLE 2
 NO. OF PORTS USED 2
 PORT INSIDE DIAMETER 6"

DISTANCE FROM FAR WALL TO OUTSIDE OF PORT 59
 NIPPLE LENGTH AND/OR WALL THICKNESS 8 1/4
 DEPTH OF STACK OR DUCT 44 3/4
 STACK OR DUCT WIDTH (IF RECTANGULAR)

EQUIVALENT DIAMETER:
 $DE = \frac{2 \times \text{DEPTH} \times \text{WIDTH}}{\text{DEPTH} + \text{WIDTH}} = \frac{2(44.75)(6)}{44.75 + 6} = 11.22$

DISTANCE FROM PORTS TO FLOW DISTURBANCES
 UPSTREAM DOWNSTREAM
 6' 25'
 DIAMETERS 2.14 6.7

STACK/DUCT AREA = $\pi(2.237)^2 = 1572.81 \text{ IN}^2$



PITOT USED ☒ TYPE "S" ☐ STANDARD

POINT	% OF DUCT DEPTH	DISTANCE FROM INSIDE WALL	DISTANCE FROM OUTSIDE OF PORT
1	4.4 14.6	1.969	9 1/2 = 7 1/2
2	14.6	6.5335	11 1/4
3	29.2	13.246	13 1/2
4	70.4	31.504	16 1/2
5	85.4	38.2465	19 1/2
6	95.6	42.781	24 1/2
7			37
8			41 3/4
9			45
10			47 3/4
11			50
12			52
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

PM10
 7 1/2
 10 1/4
 14 3/4
 21 1/2
 39 3/4
 46 1/2
 51 —

PM10

LOCATION OF POINTS IN CIRCULAR STACKS OR DUCTS

	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	28.0	14.6	10.5	8.2	6.7	5.7	4.8	4.4	3.8	3.6	3.2
3	75.0	29.8	19.4	14.6	11.8	9.9	8.5	7.6	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.6
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.9	19.4
9				91.9	82.3	73.1	62.5	39.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.6	39.8	31.5	27.2
11					93.3	85.4	76.0	70.4	61.2	39.9	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.6
13						94.3	87.5	81.2	75.0	68.6	60.2
14						96.2	91.5	85.4	79.6	73.9	67.7
15							95.1	89.1	83.5	78.2	72.8
16							96.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								96.6	93.3	89.4	83.9
19									96.1	91.3	86.6
20									98.7	94.0	89.5
21										98.6	92.1
22										98.9	94.5
23											98.8
24											98.9

LOCATION OF POINTS IN RECTANGULAR STACKS OR DUCTS

	2	3	4	5	6	7	8	9	10	11	12
1	25.0	16.7	12.5	10.0	8.3	7.1	6.3	5.8	5.0	4.5	4.2
2	75.0	50.0	37.5	30.0	25.0	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50.0	43.8	38.9	35.0	31.8	28.2
5				90.0	75.0	64.3	56.3	50.0	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50.0	45.6
7						92.9	81.3	72.2	65.0	59.1	54.2
							93.8	83.3	75.0	68.2	62.6
								94.4	85.0	77.9	70.9
									95.0	88.4	79.2
11										96.6	87.5
12											95.8

AIR FLOW RATE DETERMINATIONS

Client Withers and Ravenel Job No. 14448
 Plant Triangle Brick Run No. 5-m2-1
 City/State Merry Oaks, NC Date 10/16/95
 Test Location Brick Kiln #2 Stack Personnel JPD
 Barometric Pressure (Pbar) 30.12 "Hg Static Pressure (Pg) -0.33 "H₂O
 Pitot/Orifice ID DP72-5 Pitot Coef. (C_p) 0.84 Pres. Gauge Set ID MS-37
 Thermocouple ID R140 Duct Depth/Diameter 48" Width N/A
 ---Specify inches (") or feet (')---

VELOCITY TRAVERSES		
Start-Finish Times:		
<u>1400 - 1420</u>		
Point No.	AP In. H ₂ O	Temp. °F
A-1	0.20	510
2	0.25	511
3	0.27	513
4	0.27	512
5	0.30	515
6	0.28	516
7	0.34	516
8	0.35	519
9	0.35	518
10	0.33	515
11	0.31	514
12	0.27	512
B-1	0.38	516
2	0.48	513
3	0.53	515
4	0.52	516
5	0.48	513
6	0.43	512
7	0.33	508
8	0.31	506
9	0.24	526
10	0.24	522
11	0.23	521
12	0.20	509
Avg. *		

ORSAT DATA						
Sampling Time	Analysis Time	CO ₂ (A) Reading	O ₂ (B) Reading	%O ₂ (B-A)	CO (C) Reading	%CO (C-B)
Average						
Orsat ID		Bag ID		F _o		

FYRITE DATA, % CO ₂				
--------------------------------	--	--	--	--

MOISTURE DATA (WET BULB/DRY BULB)					
Port	Time	Dry Bulb °F	Wet Bulb °F	Diff.	% H ₂ O

MOISTURE DATA (STOICHIOMETRIC)	
Free Water in Fuel, %	
Water from Fuel Combustion, %	
Ambient Water, %	
Relative Humidity, %	
Ambient Temperature, °F	
Total %	

VOLUMETRIC AIR FLOW RATES	
Dry at Standard Conditions, Q _{sd} =	SCFM
Wet at Stack Conditions, Q _{aw} =	ACFM

ADDITIONAL DATA

* AP average is square of average square root.

METHOD 3 (ORSAT) FIELD DATA

Client Withers and Ravenel
 Plant Name Triangle Brick
 City/State Merry Oaks N.C
 Sampling Location Brick Kiln No. 2 Stack

Job No. 14448
 Fuel Type Nat. GAS

Run/Sample No. <u>S-M3-1</u>		Date <u>10/18/95</u>		Leak v OK? ☒		Operator <u>DDH</u>	
Time of Sample Collection	Time of Analysis	CO ₂ Reading (A)	O ₂ Reading (B)	CO Reading (C)	% O ₂ (B-A)	% CO (C-B)	Concurrent Runs to Share Orsat Data
0901	1330	2.4	19.0	—	16.6	—	S-M5-1 S-M201A/20-1
—	—	2.4	19.0	—	16.6	—	
1005	1340	2.4	19.0	—	16.6	—	
Avg.		2.4	Avg.		16.6	—	
Orsat I.D. <u>1</u>		Tedlar Bag I.D. <u>88</u>		F ₀ <u> </u>			

Run/Sample No. <u>S-M3-2</u>		Date <u>10/18/95</u>		Leak v OK? ☒		Operator <u>DDH</u>	
Time of Sample Collection	Time of Analysis	CO ₂ Reading (A)	O ₂ Reading (B)	CO Reading (C)	% O ₂ (B-A)	% CO (C-B)	Concurrent Runs to Share Orsat Data
1039	1340	2.4	19.0	—	16.6	—	S-M5-2 S-M201A/20-2
—	—	2.4	19.0	—	16.6	—	
1142	1350	2.4	19.0	—	16.6	—	
Avg.		2.4	Avg.		16.6	—	
Orsat I.D. <u>1</u>		Tedlar Bag I.D. <u>66</u>		F ₀ <u> </u>			

Run/Sample No. <u>S-M3-3</u>		Date <u>10/18/95</u>		Leak v OK? ☒		Operator <u>DDH</u>	
Time of Sample Collection	Time of Analysis	CO ₂ Reading (A)	O ₂ Reading (B)	CO Reading (C)	% O ₂ (B-A)	% CO (C-B)	Concurrent Runs to Share Orsat Data
1221	1350	2.4	19.0	—	16.6	—	S-M5-3 S-M201A/20-3
—	—	2.4	19.0	—	16.6	—	
1324	1400	2.4	19.0	—	16.6	—	
Avg.		2.4	Avg.		16.6	—	
Orsat I.D. <u>1</u>		Tedlar Bag I.D. <u>25</u>		F ₀ <u> </u>			

SAMPLING DATA - METHOD(S) 201A/300

CLIENT Withers and Ravenel
 PLANT Triangle Brick RUN NO. 5-M201A-1
 CITY/STATE Mercer - OAKS N.C JOB NO. 4448 DATE 10-18-95
 SAMPLING LOC. Brick Kiln No. 2 Stack TIME START 901
 BAROMETRIC PRESSURE, IN. HG 30.53 STATIC PRESSURE, IN. H₂O -0.35 TIME FINISH 1006
 LEAK 1, VACUUM IN. HG 15" 10" TEST PERSONNEL JDH JPI
 LEAK RATE, CFM 0.000 cfm POSTTEST POS PRESS LEAK 1 OK? ☒

* CONDUCT POSTTEST POSITIVE PRESSURE LEAK CHECK FOLLOWING THE LAST RUN PER LOCATION. FOR OTHER RUNS, ENTER "N/A".											
EQUIPMENT CHECKS			EQUIPMENT I.D. NUMBERS						LEAK CHECKS		
☒ PITOT, PRETEST ☒ PITOT, POSTTEST ☒ NOZZLE, PRE/POST ☒ TC <u>56</u> °F PRE ☒ TC <u> </u> °F POST <u>N/A</u> ORSAT SYSTEM			REAGENT BOX <u>0237</u> METER BOX <u>N-8</u> Y <u>9776</u> PITOT <u>DP-725</u> CP <u>.84</u> NOZ'L <u>2004</u> DIA. <u>.252</u> TC READOUT <u>F-53</u> TC PROBE <u>R394</u> UMBILICAL <u>12103</u> SAMPL'G BOX <u>33</u> ORSAT PUMP <u>N/A</u> TEDLAR BAG <u>N/A</u>						B <u> </u> B <u> </u> E <u> </u> E <u> </u> B <u> </u> B <u> </u> E <u> </u> E <u> </u> B <u> </u> B <u> </u> E <u> </u> E <u> </u>		
MONOGRAPH DATA											
DELTA-H ₂ <u>1.900</u> METER TEMP. <u>80</u> EST. XH ₂ O <u>7</u> "C" FACTOR <u>N/A</u> STACK TEMP. <u>505</u> REF DELTA-P <u>.318</u> "K" FACTOR <u>N/A</u>											
FILTER/XAD TARE WT. <u>TGF (42)</u> <u>1.4757</u>											
			Fyrites, % Y_{CO} <5% OF CAL'D Y? (Y) (N)								

L I N E	SAMPLE POINT	CLOCK TIME, MINUTES	DRY GAS METER READING, CUBIC FEET	PITOT READING, IN. H ₂ O	GAS METER TEMP., °F	STACK TEMP., °F	ORIFICE SETTING, IN. H ₂ O		GAUGE VACUUM, IN. HG	GAS TEMPERATURES, °F			✓
							ACTUAL	IDEAL		FILTER °	IMPING. EXIT	PROBE OR COND EXIT**	
1	A1	0	465.425	.25	70	480	.68	.68	2	250	48	N/A	
2	2	4 1/2	467.51	.23	64	485	.68	.68	2	250	49		
3	3	8 3/4	469.51	.24	68	500	.68	.68	2	250	49		
4	4	13	471.525	.34	71	510	.68	.68	2	250	49		
5	5	18 1/4	474.000	.37	74	515	.68	.68	2	250	50		
6	6	23 3/4	476.632	.35	77	525	.68	.68	2	250	50		
7	B1	29	479.100	.40	78	515	.68	.68	2	250	51		
8	2	34 1/2	481.732	.43	82	510	.68	.68	2	250	51		
9	3	40 1/4	484.425	.38	84	510	.68	.68	2	255	52		
10	4	45 3/4	487.45	.30	84	505	.68	.68	2	255	51		
11	5	50 1/2	489.200	.28	84	500	.68	.68	2	260	50		
12	6	55 1/4	491.615	.28	84	510	.68	.68	2	260	51		
13	END	60	493.900										
14													
15													
16													
17													
18													
19													
20													
21													
22													
23													
24													
25													

FINAL

* FILTER EXIT for NJ Method 1. FILTER BOX for all others.
 ** PROBE EXIT & ✓ (probe & filter heat off) apply to NJ Method 1. COND EXIT applies if sampling train has a condenser.

60 28.475 .318 77 505 .68
 Min. (θ) Vm (√ΔP)² tm ts ΔH

88

SAMPLING DATA - METHOD(S) 201A/3C

CLIENT Withers and Ravenel RUN NO. S-M201A/3C-2
 PLANT Triangle Brick JOB NO. 14448 DATE 10-18-95
 CITY/STATE Maryland CAKS N.C. TIME START 1039
 SAMPLING LOC. Brick Kiln No. 2 Stack TIME FINISH 1143
 BAROMETRIC PRESSURE, IN. HG 30.53 STATIC PRESSURE, IN. H₂O -.35 TEST PERSONNEL DDH, JPD
 LEAK $\downarrow$, VACUUM IN. HG 15" 10" POSTTEST POS PRESS LEAK $\downarrow$ OK? ✓
 LEAK RATE, CFM not 0.000

• CONDUCT POSTTEST POSITIVE PRESSURE LEAK CHECK FOLLOWING THE LAST RUN PER LOCATION. FOR OTHER RUNS, ENTER "N/A".

EQUIPMENT CHECKS		EQUIPMENT I.D. NUMBERS		LEAK CHECKS	
☒ PITOT, PRETEST	REAGENT BOX <u>0237</u>	METER BOX <u>N-8</u>	<u>V 9776</u>	B <u>0249</u>	B
☒ PITOT, POSTTEST	PITOT <u>18-25</u>	<u>84</u> NOZ'L	<u>2824</u> DIA.	E	E
☒ NOZZLE, PRE/POST	TC READOUT <u>F-53</u>	TC PROBE <u>R364</u>	UMBILICAL <u>1103</u>	B	B
☒ TC <u>6.4</u> °F PRE	SAMPL'G BOX <u>49</u>	ORSAT PUMP <u>N/A</u>	TEDLAR BAG <u>N/A</u>	E	E
☒ TC <u>1.4</u> °F POST				B	B
<u>N/A</u> ORSAT SYSTEM				E	E
		NOMOGRAPH DATA			
FILTER/XAD	TARE WT.	DELTA-H ₂		Fyrites, %	Y ₉₈
<u>766-0099</u>	<u>.4700</u>	METER TEMP. <u>80</u>			
		EST. H ₂ O <u>7</u>			
		"C" FACTOR <u>N/A</u>			
		STACK TEMP. <u>505</u>			
		REF DELTA-P <u>.31</u>			
		"K" FACTOR <u>N/A</u>			
				±% OF CAL'D Y? (Y) (N)	

L I N E	SAMPLE POINT	CLOCK TIME, MINUTES	DRY GAS METER READING, CUBIC FEET	PITOT READING, IN. H ₂ O	GAS METER TEMP., °F	STACK TEMP., °F	ORIFICE SETTING, IN. H ₂ O		GAUGE VACUUM, IN. HG	GAS TEMPERATURES, °F			✓
							ACTUAL	IDEAL		FILTER	IMPING. EXIT	PROBE OR COND EXIT**	
1	A1	0	494.130	.25	88	480	.68	.68	2	250	49	N/A	
2	2	4 1/2	496.322	.23	92	490	.68	.68	2	250	50		
3	3	8 3/4	498.392	.24	94	500	.68	.68	2	260	51		
4	4	13	500.460	.34	96	510	.68	.68	2	260	51		
5	5	18 1/4	502.950	.37	100	515	.68	.68	2	260	52		
6	6	23 3/4	505.715	.35	102	525	.68	.68	2	260	51		
7	B1	29	508.255	.40	102	515	.68	.68	0	260	52		
8	2	34 1/2	510.862	.43	104	510	.68	.68	2	260	52		
9	3	40 1/4	513.160	.38	106	525	.68	.68	2	260	50		
10	4	45 3/4	516.230	.30	106	505	.68	.68	2	260	51		
11	5	50 1/2	518.653	.28	106	500	.68	.68	2	250	52		
12	6	55 1/4	520.730	.28	106	510	.68	.68	2	250	52		
13		60	523.000										
14													
15													
16													
17													
18													
19													
20													
21													
22													
23													
24													
25													

FINAL

* FILTER EXIT for NJ Method 1. FILTER BOX for all others.

** PROBE EXIT & / (probe & filter heat off) apply to NJ Method 1. COND EXIT applies if sampling train has a condenser.

60 28.37 3176 100.7 510.4 .68 **89**
 Min. (θ) Vm ($\sqrt{\Delta P}$)² tm ts ΔH

SAMPLING DATA - METHOD(S) 201A

CLIENT Withers & Ravenel
 PLANT Triangle Brick RUN NO. 5-M201A/200-5
 CITY/STATE Mesa, Okla N.C. JOB NO. 14448 DATE 10-18-95
 SAMPLING LOC. Brick Kiln No 2 Stack TIME START 1218
 BAROMETRIC PRESSURE, IN. HG 30.53 STATIC PRESSURE, IN. H₂O - .30 TIME FINISH 1322
 LEAK 1, VACUUM IN. HG 15" TEST PERSONNEL DDH, JPD
 LEAK RATE, CFM 0.000 POSTTEST POS PRESS LEAK 1 OK? ✓

• CONDUCT POSTTEST POSITIVE PRESSURE LEAK CHECK FOLLOWING THE LAST RUN PER LOCATION. FOR OTHER RUNS, ENTER "N/A".

EQUIPMENT CHECKS		EQUIPMENT I.D. NUMBERS				LEAK CHECKS	
☒ PITOT, PRETEST	REAGENT BOX <u>0237</u>	METER BOX <u>N-8</u>	Y <u>.9776</u>	B	B		
☒ PITOT, POSTTEST	PITOT <u>DP-725</u>	NOZ'L <u>3/4</u>	DIA. <u>.249</u>	E	E		
☒ NOZZLE, PRE/POST	TC READOUT <u>F-53</u>	TC PROBE <u>R 394</u>	UMBILICAL <u>U103</u>	B	B		
☒ TC <u> </u> °F PRE	SAMPL'G BOX <u>33</u>	ORSAT PUMP <u>N/A</u>	TEDLAR BAG <u>N/A</u>	E	E		
☒ TC <u> </u> °F POST				B	B		
<u>N/A</u> ORSAT SYSTEM				E	E		
FILT./XAD		TARE WT.		MONOGRAPH DATA			
				DELTA-H ₂ <u>1.900</u>			
				METER TEMP. <u>80</u>			
				EST. XH ₂ O <u>7</u>			
				"C" FACTOR <u>N/A</u>			
				STACK TEMP. <u>505</u>			
				REF DELTA-P <u>.31</u>			
				"K" FACTOR <u>N/A</u>			
				Fyrites, %		Y ₉₀	
						±5% OF CAL'D Y?	
						(Y) (N)	

L I N E	SAMPLE POINT	CLOCK TIME, MINUTES	DRY GAS METER READING, CUBIC FEET	PITOT READING, IN. H ₂ O	GAS METER TEMP., °F	STACK TEMP., °F	ORIFICE SETTING, IN. H ₂ O		GAUGE VACUUM, IN. HG	GAS TEMPERATURES, °F			✓
							ACTUAL	IDEAL		FILTER *	IMPING. EXIT	PROBE OR COND EXIT**	
1	A1	0	523.148	.25	90	480	.68	.68	2	250	49	N/A	
2	2	4 1/2	525.310	.23	92	490	.68	.68	2	250	49		
3	3	8 3/4	527.255	.24	92	521	.68	.68	2	250	50		
4	4	13	529.242	.34	92	510	.68	.68	2	255	51		
5	5	18 1/2	531.743	.37	94	515	.68	.68	2	260	52		
6	6	23 3/4	534.350	.35	96	525	.68	.68	2	260	50		
7	B1	29 1/2	536.776	.40	97	515	.68	.68	2	260	50		
8	2	34 1/2	539.422	.43	97	510	.68	.68	2	260	50		
9	3	40 1/4	542.215	.38	98	523	.68	.68	2	260	51		
10	4	45 3/4	544.850	.30	99	505	.68	.68	2	260	52		
11	5	50 1/2	547.142	.28	99	521	.68	.68	2	260	50		
12	6	55 1/4	549.530	.28	99	510	.68	.68	2	260	51		
13		60	551.658										
14													
15													
16													
17													
18													
19													
20													
21													
22													
23													
24													
25													

FINAL

* FILTER EXIT for NJ Method 1. FILTER BOX for all others.

** PROBE EXIT & / (probe & filter heat off) apply to NJ Method 1. COND EXIT applies if sampling train has a condenser.

60 283.510 0.3176 45.3 510.4 0.68
 Min. (θ) Vm (√ΔP)² tm ts ΔH_f

MOISTURE ANALYTICAL RESULTS

Client Withers and Ravenel
 Plant Name Triangle Brick Job No. 14448
 City/State Merry Pk, NC Sampling Loc. Brick Kiln #2 Stack

Run Number	4-M201A/202-1	5-M201A/202-2	5-M201A/202-3
Sampling Date	<u>10/18/95</u>	<u>10/18/95</u>	<u>10/18/95</u>
Analysis Date	<u>10/18/95</u>	<u>10/18/95</u>	<u>10/18/95</u>
Analyst	<u>JRW</u>	<u>JRW</u>	<u>JRW</u>

Reagent 1 (<u>350 ml DI H₂O</u>)			
Final Weight, g	<u>798.9</u>	<u>796.6</u>	<u>807.4</u>
Tared Weight, g	<u>776.4</u>	<u>775.3</u>	<u>782.1</u>
Water Catch, g	<u>22.1</u>	<u>21.3</u>	<u>25.3</u>
Reagent 2 ()			
Final Weight, g			
Tared Weight, g			
Water Catch, g			
Reagent 3 ()			
Final Weight, g			
Tared Weight, g			
Water Catch, g			
CONDENSED WATER, g			

Silica Gel			
Final Weight, g	<u>223.0</u>	<u>226.1</u>	<u>223.3</u>
Tared Weight, g	<u>205.5</u>	<u>209.3</u>	<u>210.4</u>
ADSORBED WATER, g	<u>17.5</u>	<u>16.8</u>	<u>12.9</u>

TOTAL WATER COLLECTED, g	<u>39.6</u>	<u>38.1</u>	<u>38.2</u>
--------------------------	-------------	-------------	-------------

Balance No. EET 13 Type ☒ Triple Beam ☐ Electronic Reagent Box No. 0237

Balance located in stable, draft-free area ☒ Yes ☐ No (If "No", explain below.)

Comments

RECORD OF CUSTODY, CONTAINER No. 237

client The Brick Association Job No. 14448
14884
 Plant Name Triangle Brick
 City/State Merry Oaks, N.C.
 Sampling Method(s) EPA M 201A/202 (EPA, NIOSH, etc.)
 Container Type (V) Reagent Box ☒ Cooler ☐ Other (specify) _____

Seal No. or "PC"	Date	Time	*	Signature	Reason for Breaking Seal**
264	9/26	1544	S	<i>[Signature]</i>	
	10/16/95	1507	B	<i>Joe Windsor</i>	label jars
2309	10/18/95	1518	S	<i>Joe Windsor</i>	
			B		
			S		
			B		
			S		
			B		
			S		
			B		
			S		
			B		
			S		
			B		

PC = Personal Custody * S = Sealed By; B = Broken By ** Use "REMARKS" Section if more space needed.

Container Received by Entropy Sample Custodian			Seal Intact? **	
<i>Sam Deley</i>	10/24/95	1310	Yes ☒	No ☐ NA ☐
Signature	Date	Time		

As Applicable:

All liquid levels at mark (✓) YES ☐ NO ☐ (Estimate loss if not at mark; describe in "REMARKS")

As Applicable:

TUBE SAMPLES put in freezer by _____ Date _____ Time _____

CONDENSATE SAMPLES put in refrige. by _____ Date _____ Time _____

REMARKS _____

Box No. 237 Assembly Date 9.26.95 Assembled By JUS
 Client The Brick Association Job No. 14448
 Plant Triangle Brick City/State Merry Oaks, NC
 Sampling Loc. Brick Kiln #2 Stack Method EPA 201A/202
 Individual Tare Of Reagent 200 (Ml) (gm) Of D1 H₂O
 Individual Tare Of Reagent _____ (Ml) (gm) Of _____
 Individual Tare Of Reagent _____ (Ml) (gm) Of _____
 Individual Tare Of Sil. Gel _____ Gm _____

Run Number	Run Date	Filter or XAD		Liquid Tare at Mark? @	Init.	Sample Recov. Date	%Sil. Gel Spent	Liquid Level Marked?	Init.
		Number	Tare, grams						
S-M201A/202-1	10/18	T6F042	0.4757	✓	JRW	10/18	30	✓	JRW
			0.4757	Filter Appearance* clean					
				Reagents Appearance* clear					
S-M201A/202-2	10/18	T6F055	0.4700	✓	JRW	10/18	30	✓	JRW
				Filter Appearance* clean					
				Reagents Appearance* clear					
S-M201A/202-3	10/18	E4513	0.4520	✓	JRW	10/18	70	✓	JRW
				Filter Appearance* clean					
				Reagents Appearance* clear					
				Filter Appearance*					
				Reagents Appearance*					

@ All liquid levels at mark? (check) YES ☒ NO ☐ (estimate loss if not at mark; use "REMARKS" section).

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APPENDIX B. FIELD DATA

**2. Sampling Point Determinations and
Cyclonic Flow Checks**

Sampling and Velocity Traverse Point Determination EPA Method 1

CLIENT Withers and Ravenel
 PLANT NAME Triangle Brick
 CITY, STATE Rocky Cabs NC
 SAMPLING LOCATION Brick Kiln No. 2 Stack

NO. OF PORTS AVAILABLE 2
 NO. OF PORTS USED 2
 PORT INSIDE DIAMETER 6"

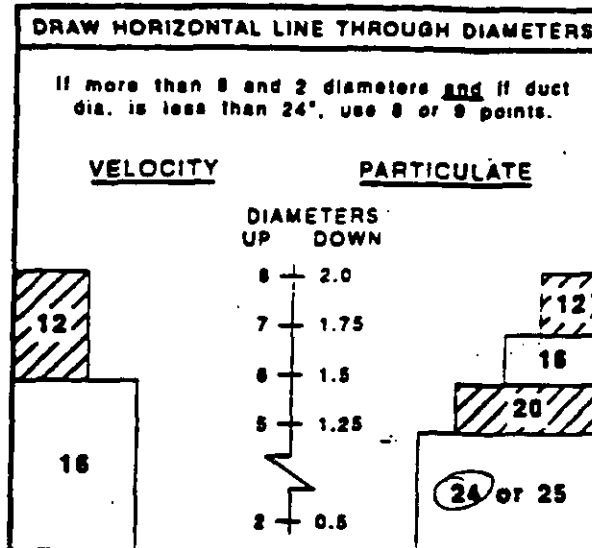
DISTANCE FROM FAR WALL TO OUTSIDE OF PORT 53"
 NIPPLE LENGTH AND/OR WALL THICKNESS 8 1/4"
 DEPTH OF STACK OR DUCT 44 3/4"
 STACK OR DUCT WIDTH (IF RECTANGULAR)

EQUIVALENT DIAMETER:
 $D_e = \frac{2 \times \text{DEPTH} \times \text{WIDTH}}{\text{DEPTH} + \text{WIDTH}} = \frac{2(-)(-)}{(-)+(-)} = \underline{\hspace{2cm}}$

DISTANCE FROM PORTS TO FLOW DISTURBANCES

	UPSTREAM	DOWNSTREAM
DIAMETERS	<u>8'</u>	<u>25'</u>
	<u>2.14</u>	<u>6.70</u>

STACK/DUCT AREA = $\pi (22.37)^2 = 1572.81 \text{ IN}^2$



PITOT USED (✓) TYPE "B" ✓ STANDARD

LOCATION OF POINTS IN CIRCULAR STACKS OR DUCTS

	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	26.0	14.6	10.5	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.8	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	83.3	70.4	32.3	22.8	17.7	14.9	12.6	10.9	9.7	8.7	7.9
5		86.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6			85.8	65.8	35.8	28.9	22.0	18.9	16.5	14.6	13.2
7				89.8	77.4	64.4	50.6	36.3	23.0	20.4	18.1
8					88.8	75.0	63.4	51.5	38.0	25.0	21.8
9						81.5	73.1	62.5	50.6	38.2	25.0
10							79.0	71.7	61.8	50.8	37.2
11								83.3	76.4	66.4	56.6
12									84.3	77.5	67.5
13										85.4	78.6
14											86.4
15											
16											
17											
18											
19											
20											
21											
22											
23											
24											

LOCATION OF POINTS IN RECTANGULAR STACKS OR DUCTS

	2	3	4	5	6	7	8	9	10	11	12
1	25.0	18.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75.0	50.0	37.5	30.0	25.0	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.9
4			87.5	70.0	58.3	50.0	43.8	38.9	35.0	31.5	29.2
5				90.0	75.0	64.3	56.3	50.0	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50.0	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	79.2
11										95.5	87.5
12											95.8

Page 1 of 1

Job No. 14448

Date 10/16/85

Personnel JPD

Static Pres. (Pg) -0.35 In. H₂O

Pres. Gauge Set ID MS-37

Width *N/A*

---Specify inches (") or feet (')--

Test Pt.	Yaw Ang. ° ϕ	ΔP "H ₂ O	Temp. °F
B-1	-15		
2	-10		
3	-6		
4	-4		
5	-4		
6	-5		
7	-5		
8	-7		
9	-8		
10	-9		
11	-11		
12	-8		
A-1	-10		
2	-12		
3	-6		
4	-5		
5	-2		
6	-4		
7	-7		
8	-9		
9	-9		
10	-8		
11	-9		
12	-8		
Avg.	-7.5		

[illegible]

Note: Yaw angle average is sum of the absolute values divided by number of measurements, and must be $\leq 20^\circ$.

Δ^2 average is square of average square root.

* From isokinetic sampling field data sheet.

**** Minutes/Point = cos ϕ (Base Time).**

*** Average $\Delta P_v = [(2 \cos \theta \sqrt{\Delta P}) / n]^2$.

APPENDIX C. ANALYTICAL DATA

1. Condensible Particulate

Corrections to mr according to the SO4 results of the ALIQUOT

- x Correct for NH4+ resulting from the reaction of NH3 with H2SO4
Correct for NH4+ (as above) and the water associated with H2SO4

K 0.184

Run Number	<u>S-M201A/202-1</u>	<u>S-M201A/202-2</u>	<u>S-M201A/202-3</u>
<u>Sulfates Analysis</u>			
Vb, aliquot volume, mL	10	10	10
SO4 Concentration (CSO4), mg/ml	0.00361	0.00362	0.00438
Final Volume (Vlc), ml	485.0	480.0	480.0
mc, correction mass ^a	0.3222	0.3198	0.3868
<u>Inorganic Condensible Particulate</u>			
Uncorrected Catch Weight (mr), mg ^b	19.8	28.8	25.9
Corrected Catch Weight (mi), mg ^c	19.9	29.1	26.1
<u>Organic Condensible Particulate</u>			
Catch Weight (mo-mb), mg ^b	2.3	0.0	3.3
<u>Total Condensible Particulate</u>			
Catch Weight cpm, mg ^d	22.2	29.1	29.4

^a $mc = K \cdot CSO4 \cdot Vlc$

^b From laboratory data sheet.

^c $mi = mr \cdot [Vlc / (Vlc - Vb)] - mc$

^d $cpm = mi + mo$

TRIANGLE LABS**FAX COVER SHEET**

From: Nancy Bragg, Senior Project Scientist
Direct Phone Line: (919) 544-8348
TL-RTP Main Number: (919) 544-5729

Date: 3 November 1995

To: Company: Entropy

Name: Alan Senzel

Fax Number: 787-8442

Subject: Gravimetric Results for Project: 34683B

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Nancy at (919) 544-8348.

Environmental Division
801 Capitola Drive
Durham, NC 27713-4411
919-544-5729

P.O. Box 13485
Research Triangle Park, NC 27709-3485
Fax # 919-544-5491

TLI Project: 34683-B

NSPS Method 202

Client Project: Triangle Brick 11989-14448-18
Matrix: Methylene Chloride Rinse & DI Water

Date Received: 10/24/95

Sample ID: 100-00-40 100-00-41 100-00-42

Sample ID: 100-00-40 100-00-41 100-00-42

Baggie Tare Wt., g:	3.2736	3.4268	3.8136
Raw Weight, g:	3.2750	3.4466	3.8424
INORGANIC CATCH, g:	0.0014	0.0198	0.0288

Sample ID: 100-00-40 100-00-41 100-00-42

Tare Wt., g:	3.3779	3.3713	3.1594
Raw Weight, g:	3.3791	3.3756	3.1614
ORGANIC CATCH, g:	0.0012	0.0043	0.0020
Inorganic Catch, mg:	1.4	19.8	28.8
Organic Catch, mg:	1.2	4.3	2.0
Subtract Blank Residue, mg:		2.0	2.0
Condensable Particulate, mg:	1.2	22.1	28.8

VISUAL ANALYSIS OF WATERS

Color:	white brown	brown	brown
Texture:	stain tint	stain	stain
Foreign Matter:	none	none	none
Rel. Comp.:	equal	equal	x2
Volume, mL:	295	485	480
Cloudy:	no	no	no
Baggie Number:	441	442	443

VISUAL ANALYSIS OF FLOUSES

Color:	white	brown	brown
Texture:	film	stain oily	oily residue
Foreign Matter:	none	none	none
Rel. Comp.:	equal	x2	equal
Volume, mL:	285	150	150
Baggie Number:	448	438	439

Triangle Laboratories, Inc.®
801 Capitola Drive • Durham, North Carolina 27713
Phone: (919) 544-5729 • Fax: (919) 544-5491

PRDGRV 02.13.00ES W.11.05

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Page: 1 of 2

TLI Project: 34683-B

NSPS Method 202

Client Project: Triangle Brick 11989-14448-18
Matrix: Methylene Chloride Rinse & DI Water

Date Received: 10/24/95

Baggie Tare Wt., g: 3.4057
Raw Weight, g: 3.4316

INORGANIC CATCH, g: 0.0259

Tare Wt., g: 3.4181
Raw Weight, g: 3.4234

ORGANIC CATCH, g: 0.0053

Inorganic Catch, mg: 25.9
Organic Catch, mg: 5.3
Subtract Blank Residue, mg: 2.0

Condensable Particulate, mg: 29.2

VISUAL ANALYSIS OF WATERS

Color: brown
Texture: stain
Foreign Matter: none
Rel. Comp.: x2
Volume, mL: 480
Cloudy: no
Baggie Number: 444

VISUAL ANALYSIS OF GINGER

Color: brown
Texture: oily residue
Foreign Matter: none
Rel. Comp.: x1.5
Volume, mL: 150
Baggie Number: 440Triangle Laboratories, Inc.®
801 Capitol Drive • Durham, North Carolina 27713
Phone: (919) 544-5729 • Fax: (919) 544-5491

PROG 2.13, MILES 4.11.05

Printed: 10:05 11/03/95
Page: 2 of 2

TOTAL P.03

TRIANGLE LABS

CASE NARRATIVE

Analysis of Samples for the Presence of

Ammonium Sulfate

by

Ion Chromatography

METHOD 300.0

Date : November 07, 1995

Client ID : Entropy, Inc.

TLI Project Number : 34683C

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Triangle Laboratories, Inc.
801 Capitola Drive
Durham, NC 27713-4411
919-544-5729

P.O. Box 13485
Research Triangle Park, NC 27709-3485
Fax # 919-544-5491

Objective: Analysis of three deionized water train portion samples and one deionized water blank for ammonium sulfate by Method 300.0.

Method: Four train samples were received by Triangle Laboratories, Inc. on October 24, 1995 without coolant at ambient temperature and in good condition. The deionized water samples were analyzed for ammonium sulfate content by ion chromatography using Method 300.0 with suppressed conductivity detection. The results reported relate only to the items tested.

The analysis conditions are listed below:

Instrument: Dionex DX300 Ion Chromatograph with a PED-II Conductivity Detector
Eluent flow: 1.5 mL/min. (1.8 mM sodium carbonate/1.7mM sodium bicarbonate)
Suppressor: Anion self-regenerating suppressor-1
Sample Loop: 50 uL
Detection: Conductivity - suppressed ion
Data Recording: Dionex AI 450 software

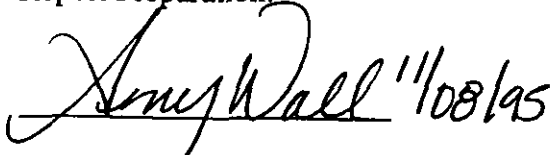
Report: Enclosed with the case narrative are copies of the client paperwork, sample log-in sheets, and log book pages. The data are reported as quantitation reports and chromatograms. Two five point calibration curves were performed ranging from 1.0 ppm to 100 ppm both before and after sample analysis. Reported concentrations are mean values determined from duplicate analyses.

Results: Ammonium sulfate was detected in all samples except the DI BLANK sample at levels within the calibration range. Ammonium sulfate was not detected in the laboratory blank.

The data in this package has been judged to be valid according to the guidelines of Method 300.0 except as noted above. Should you have any questions, please feel free to contact our Project Scientist, Nancy Bragg at (919) 544-8348.

For Triangle Laboratories, Inc.,

Report Preparation:



Amy Wall
Report Preparation Chemist

Quality Control:



Selena Armistead
Report Preparation Chemist

The total number of pages in this data package is _____.

ENTROPY

Environmentalists, Inc.

P.O. Box 12291
Research Triangle Park
North Carolina 27709-2291
919-781-3550 FAX 919-787-8442

REQUEST FOR ANALYSIS

34683C

PO#:11989 - 14448-18

Customer Name: Withers and Ravenel
Triangle Brick

Laboratory: TLI

Date Transmitted: 10/24/95

Results Due By: 11/07/95

Sample Matrix: Method 201A

PM: VJT

Analysis: Analyze samples for PM10 Particulate according to EPA Method 201A, and Condensibles according to EPA Method 202.

Sample #	Sample ID	Components/Comments
1	S-M201A/202-1	DI H2O, MeCl2, F1/2 Ace, Noz.Ace, Filter
2	S-M201A/202-2	DI H2O, MeCl2, F1/2 Ace, Noz.Ace, Filter
3	S-M201A/202-3	DI H2O, MeCl2, F1/2 Ace, Noz.Ace, Filter
4	Blanks	DI H2O, MeCl2, Acetone

107

Submitted By 

SAMPLE TRANSFER RECORD OF CUSTODY

Please include this form with the final (typed) results, and whenever the final results are faxed to Entropy.

The samples referenced in Entropy Environmentalists Inc. RFA or purchase order No. 11989-14448-18 were shipped by Entropy on 10/24/95 (date) via PERSONAL CUSTODY (mode) to TLI (laboratory) by Sam DeLong (signature)

The samples were received for analysis on 10/24/95 (date) at Triangle Labs (laboratory) by John G. Smith (signature)

As applicable, note any broken seals, leakage, spillage, or damage to samples. If discrepancy, specify seal No., jar No., sample No., etc.

Custody Seal	: Absent	Sample Seals:	Absent	TLI Project Number	: 34683	Book	
Chain of Custody	: Present			Client:	EEI01	Entropy, Inc.	108
Sample Tags	: Present			Date Received	10/24/95	By <i>J. Swartz</i>	Page
Sample Tag Numbers:	Listed						
SNO Forms	: N/A						
Box	NO COOLANT	Carrier and Number	SEAN DALEY				89
TLI Number	Matrix	To LAB	To STORAGE	To LAB	To STORAGE	To LAB	To STORAGE
MR/H:CPM	Client ID	Location	Date/Init	Date/Init	Date/Init	Date/Init	Date/Init
108-89-1A	S-M201A/202-1	FILTER					
		GRAV LAB					
108-89-1B	S-M201A/202-1	FH/ACE					
		GRAV LAB					
108-89-1C	S-M201A/202-1	BH/MECL2					
		GRAV LAB					
108-89-1D	S-M201A/202-1	NOZ.ACE					
		GRAV LAB					
108-89-1E	S-M201A/202-1	DI H2O					
		GRAV LAB					
108-89-2A	S-M201A/202-2	FILTER					
		GRAV LAB					
108-89-2B	S-M201A/202-2	FH/ACE					
		GRAV LAB					
108-89-2C	S-M201A/202-2	BH/MECL2					
		GRAV LAB					
108-89-2D	S-M201A/202-2	NOZ.ACE					
		GRAV LAB					
108-89-2E	S-M201A/202-2	DI H2O					
		GRAV LAB					
Receiving Remarks:							
109							
Archive Remarks:							

Custody Seal : Absent		Sample Seals: Absent		TLI Project Number : 34683		Book	
Chain of Custody : Present				Client: EE101		Entropy, Inc.	
Sample Tags : Present				Date Received : 10/24/95		By <i>[Signature]</i>	
Sample Tag Numbers: Listed						Page	
SMD Forms : N/A							
Box		NO COOLANT		Carrier and Number : SEAN DALEY		89	
TLI Number	Client ID	Matrix Location	To LAB Date/Init	To STORAGE Date/Init	To LAB Date/Init	To STORAGE Date/Init	To LAB Date/Init
108-89-3A	S-M201A/202-3	FILTER					
		GRAV LAB					
108-89-3B	S-M201A/202-3	FH/ACE					
		GRAV LAB					
108-89-3C	S-M201A/202-3	BH/MECL2					
		GRAV LAB					
108-89-3D	S-M201A/202-3	NOZ.ACE					
		GRAV LAB					
108-89-3E	S-M201A/202-3	DI H2O					
		GRAV LAB					
108-89-4A	BLANK	ACETONE					
		GRAV LAB					
108-89-4B	BLANK	MECL2					
		GRAV LAB					
108-89-4C	BLANK	DI H2O					
		GRAV LAB					
Receiving Remarks:							
110							
Archive Remarks:							

DIONEX SCHEDULE - C:\DX\SCHEDULE\34683C.SCH

Inj#	Sample Name	Method	Data File	Vol.	Dil.	Int.Std.
1	STD 1.0 PPM	..\7ANION.m	STD001	1	1	1
2	STD 1.0 PPM	..\7ANION.m	STD001	1	1	1
3	STD 3.0 PPM	..\7ANION.m	STD003	1	1	1
4	STD 3.0 PPM	..\7ANION.m	STD003	1	1	1
5	STD 10.0 PPM	..\7ANION.m	STD010	1	1	1
6	STD 10.0 PPM	..\7ANION.m	STD010	1	1	1
7	STD 30.0 PPM	..\7ANION.m	STD030	1	1	1
8	STD 30.0 PPM	..\7ANION.m	STD030	1	1	1
9	STD 100.0 PPM	..\7ANION.m	STD100	1	1	1
10	STD 100.0 PPM	..\7ANION.m	STD100	1	1	1
11	H2O BLANK	..\7ANION.m	H2OBLK	1	1	1
12	H2O BLANK	..\7ANION.m	H2OBLK	1	1	1
13	QC	..\7ANION.m	QC	1	1	1
14	QC	..\7ANION.m	QC	1	1	1
15	DI WATER BLANK	..\7ANION.m	108894C	1	1	1
16	DI WATER BLANK	..\7ANION.m	108894C	1	1	1
17	S-M201A/202-1	..\7ANION.m	108891E	1	1	1
18	S-M201A/202-1	..\7ANION.m	108891E	1	1	1
19	S-M201A/202-2	..\7ANION.m	108892E	1	1	1
20	S-M201A/202-2	..\7ANION.m	108892E	1	1	1
21	S-M201A/202-3	..\7ANION.m	108893E	1	1	1
22	S-M201A/202-3	..\7ANION.m	108893E	1	1	1
23	STD 1.0 PPM	..\7ANION.m	STD001	1	1	1
24	STD 1.0 PPM	..\7ANION.m	STD001	1	1	1
25	STD 3.0 PPM	..\7ANION.m	STD003	1	1	1
26	STD 3.0 PPM	..\7ANION.m	STD003	1	1	1
27	STD 10.0 PPM	..\7ANION.m	STD010	1	1	1
28	STD 10.0 PPM	..\7ANION.m	STD010	1	1	1
29	STD 30.0 PPM	..\7ANION.m	STD030	1	1	1
30	STD 30.0 PPM	..\7ANION.m	STD030	1	1	1
31	STD 100.0 PPM	..\7ANION.m	STD100	1	1	1
32	STD 100.0 PPM	..\7ANION.m	STD100	1	1	1
33	END	..\STANDCL.	..\END	1	1	1

Comment:

11-06-95 PROJECT #34683C ANALYZED ON THIS FOR ((NH4)2 SO4)BY (M-300)
 SCHEDULE. (STD"S) FOR THIS PROJECT ARE ICS-109-4-5 AND ICS-110-1
 THRU-3 QC LOT# K-ION02093 , ANION ELUENT 103095 TIMOTHY BELLAMY.
 LOOP SIZE (25 uL)

TRIANGLE LABORATORIES, INC.

TLI# 34683C-AMMONIUM SULFATE
CLIENT SAMPLES
ENTROPY, INC.
06-NOVEMBER-95

TLI ID	CLIENT ID	RT	AREA	LOG AREA	RUN CONC (ppm)	DILUTION FACTOR	SAMPLE CONC (ppm)	AVG CONC (ppm)	RFG	TOTAL FL	TOTAL ug SO4	TOTAL ug (NH4)2SO4	PH
108-89-4C	DI WATER BLANK	ND	ND	ND	ND	1	ND	ND	ND	285	ND	ND	7
108-89-1E	S-M201A/202-1	9.70	16558172	7.22	3.63	1	3.63	3.61	1.1	485	1751	2406	2
		9.70	16384009	7.21	3.59	1	3.59						
108-89-2E	S-M201A/202-2	9.69	16558680	7.22	3.63	1	3.63	3.62	0.6	480	1738	2389	3
		9.69	16448330	7.22	3.61	1	3.61						
108-89-3E	S-M201A/202-3	9.70	20268747	7.31	4.38	1	4.38	4.38	0.2	480	2102	2890	3
		9.69	20217947	7.31	4.37	1	4.37						

*TOTAL ug (NH4)2SO4 = ((w. (NH4)2SO4 / m.w. SO4) x [SO4])
ND = NONE DETECTED

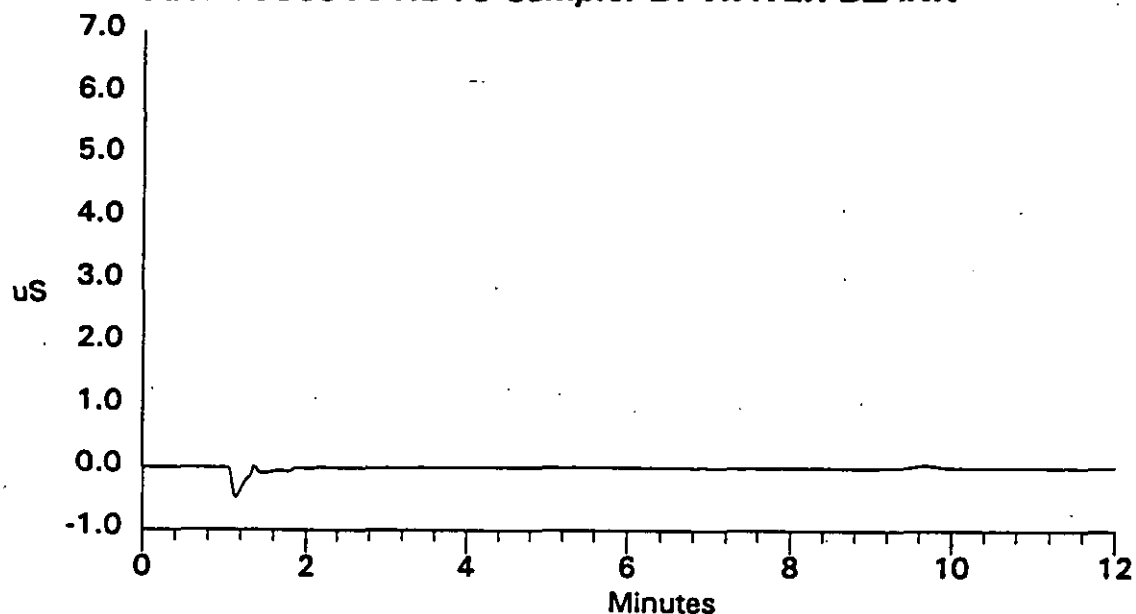
Sample Name: DI WATER BLANK	Date: 11/06/1995 20:45:04
Data File : C:\DX\DATA\34683C\108894C1.D15	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 15	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
0	0.00	SULFATE	0.000	0	0	0	0.00
Totals			0.000	0	0		

File: 108894C1.D15 Sample: DI WATER BLANK



Data Reprocessed On 11/07/1995 08:41:06

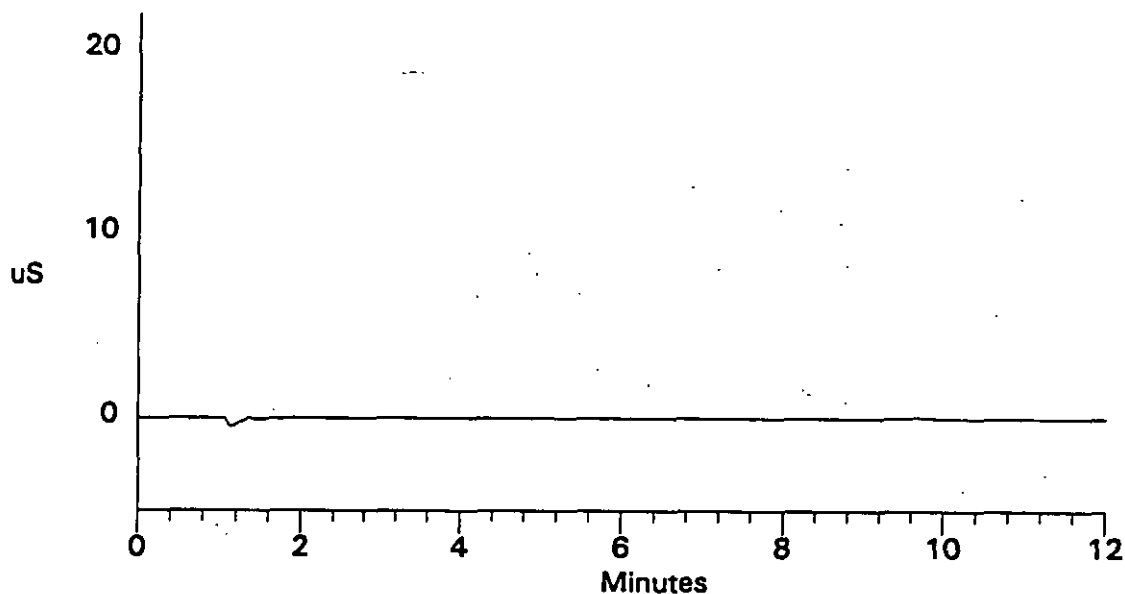
Sample Name: DI WATER BLANK	Date: 11/06/1995 20:58:51
Data File : C:\DX\DATA\34683C\108894C1.D16	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 16	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
0	0.00	SULFATE	0.000	0	0	0	0.00
Totals			0.000	0	0		

File: 108894C1.D16 Sample: DI WATER BLANK



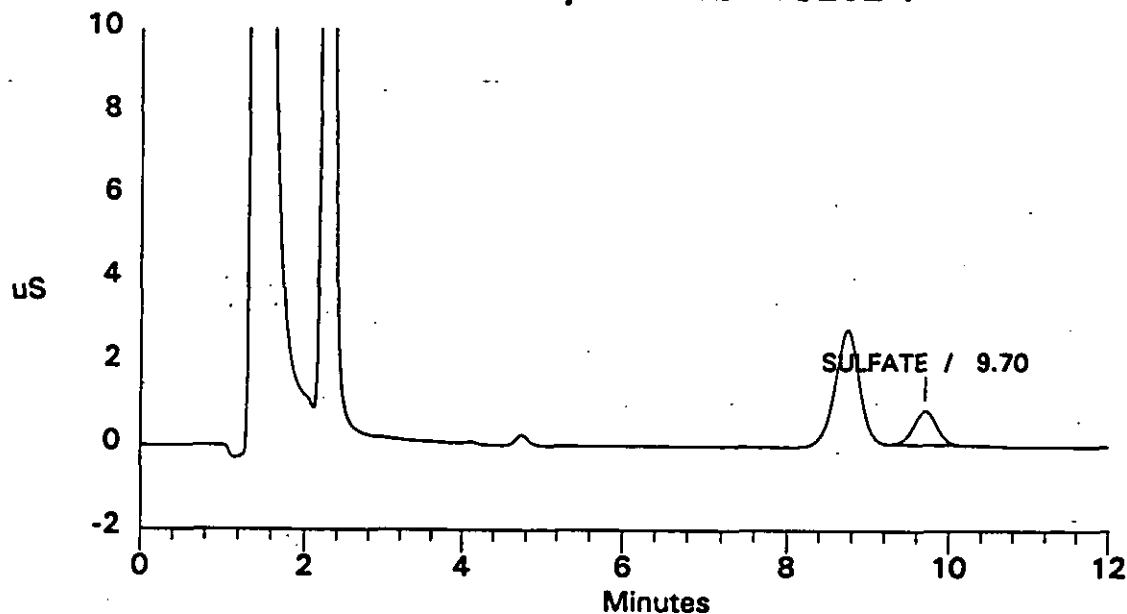
Sample Name: S-M201A/202-1	Date: 11/06/1995 21:12:39
Data File : C:\DX\DATA\34683C\108891E1.D17	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 17	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.70	SULFATE	0.000	808391	16556172	1	-0.21
Totals			0.000	808391	16556172		

File: 108891E1.D17 Sample: S-M201A/202-1



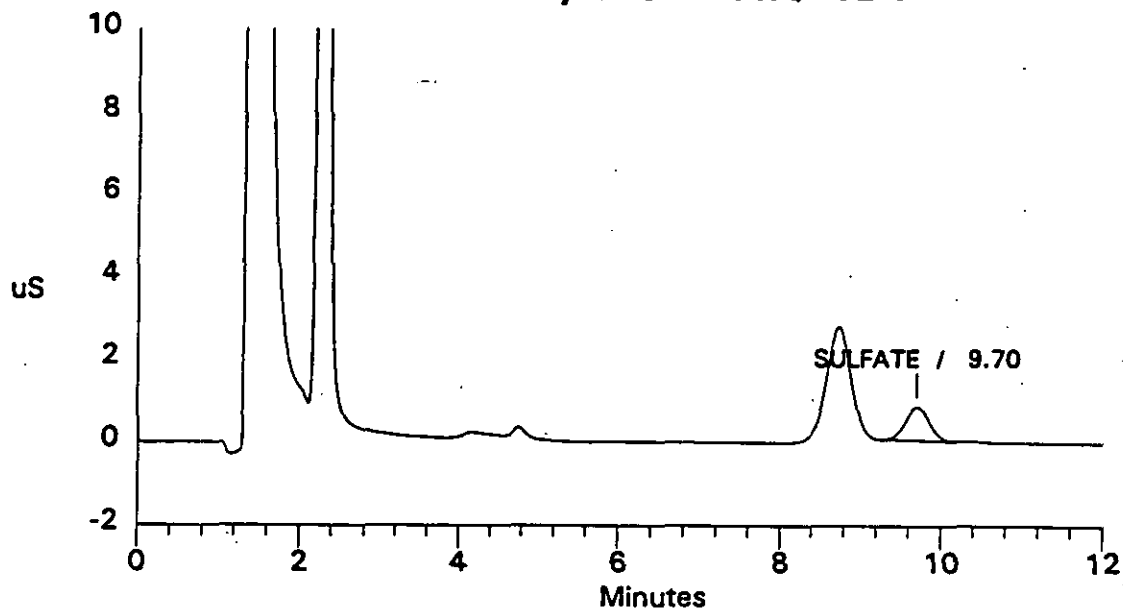
Sample Name: S-M201A/202-1	Date: 11/06/1995 21:26:27
Data File : C:\DX\DATA\34683C\108891E1.D18	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 18	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.70	SULFATE	0.000	806137	16364009	1	-0.24
Totals			0.000	806137	16364009		

File: 108891E1.D18 Sample: S-M201A/202-1



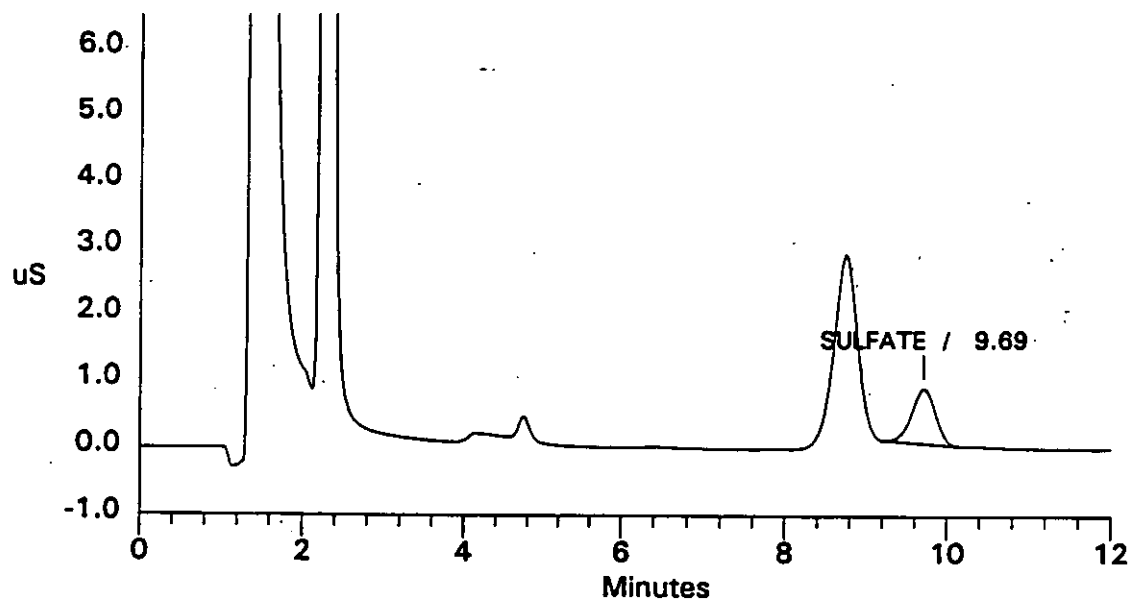
Sample Name: S-M201A/202-2	Date: 11/06/1995 21:40:15
Data File : C:\DX\DATA\34683C\108892E1.D19	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 19	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.69	SULFATE	0.000	816087	16558660	1	-0.27
Totals			0.000	816087	16558660		

File: 108892E1.D19 Sample: S-M201A/202-2



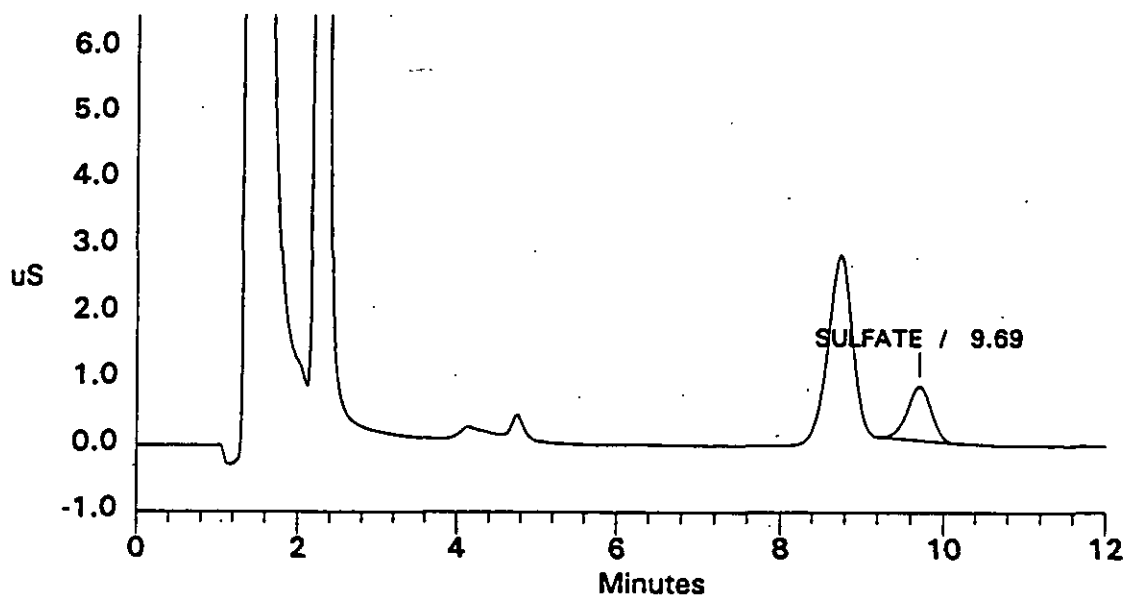
Sample Name: S-M201A/202-2	Date: 11/06/1995 21:54:02
Data File : C:\DX\DATA\34683C\108892E1.D20	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 20	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.69	SULFATE	0.000	814205	16448330	1	-0.31
Totals			0.000	814205	16448330		

File: 108892E1.D20 Sample: S-M201A/202-2



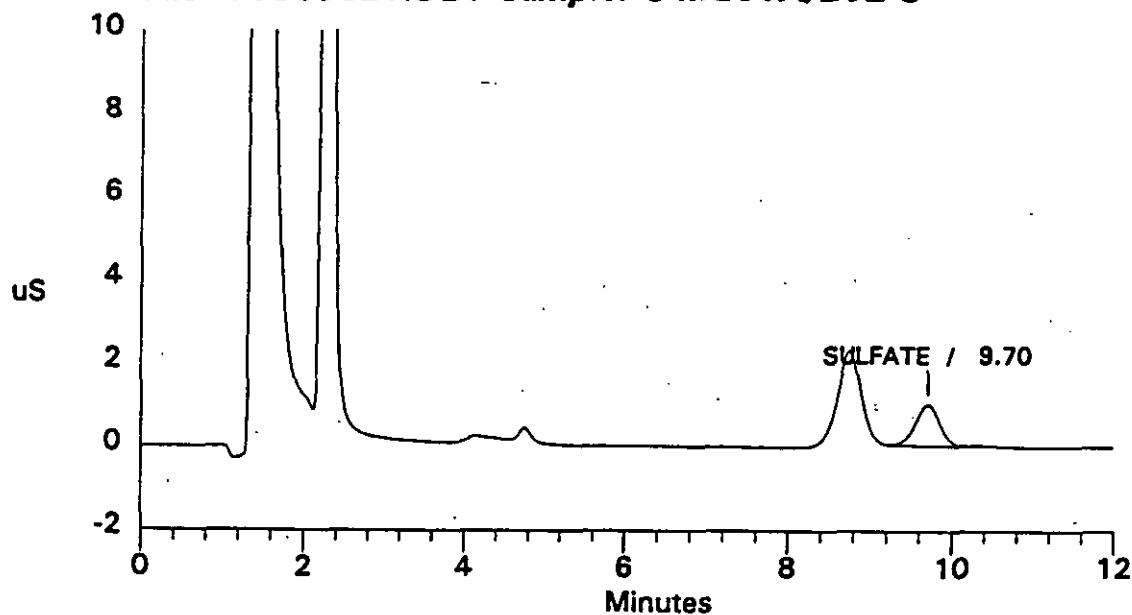
Sample Name: S-M201A/202-3	Date: 11/06/1995 22:07:50
Data File : C:\DX\DATA\34683C\108893E1.D21	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 21	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.70	SULFATE	0.000	990220	20266747	1	-0.24
Totals			0.000	990220	20266747		

File: 108893E1.D21 Sample: S-M201A/202-3



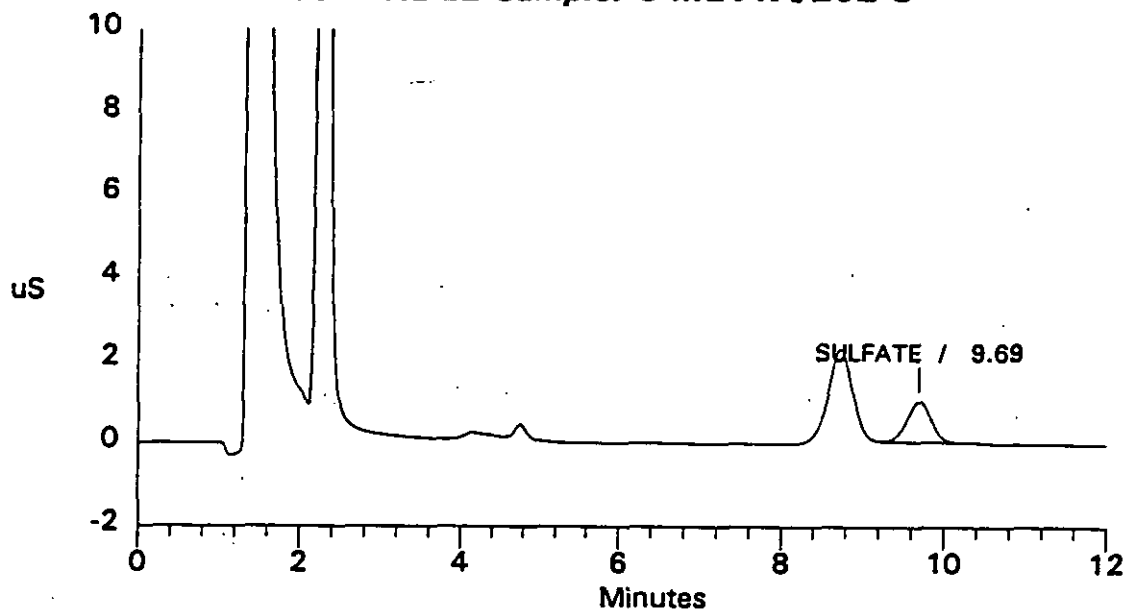
Sample Name: S-M201A/202-3	Date: 11/06/1995 22:21:38
Data File : C:\DX\DATA\34683C\108893E1.D22	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 22	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.69	SULFATE	0.000	980159	20217947	1	-0.27
Totals			0.000	980159	20217947		

File: 108893E1.D22 Sample: S-M201A/202-3



TLI# 34883C-AMMONIUM SULFATE
CALIBRATION
08-07-NOVEMBER-85

CONC (ppm)	RT	AREA	LOG CONC	LOG AREA	PREDICTED (ppm)	SDIFF	RESPONSE (CONC/AREA)
100	9.41	600505086	2.000	6.779	103.33	3.2	1.97E-07
30	9.56	155380984	1.477	6.191	29.29	-2.4	1.93E-07
10	9.63	48573138	1.000	7.686	9.91	-1.0	2.08E-07
3	9.65	12831835	0.477	7.112	2.88	-4.0	2.32E-07
1	9.68	4330129	0.000	6.637	1.04	3.8	2.31E-07
100	9.40	603040058	2.000	6.780	103.73	3.6	1.98E-07
30	9.56	156082998	1.477	6.193	29.42	-2.0	1.92E-07
10	9.62	48008322	1.000	7.681	9.80	-2.1	2.08E-07
3	9.64	12738862	0.477	7.105	2.84	-5.5	2.38E-07
1	9.64	4422430	0.000	6.846	1.06	8.7	2.28E-07

Regression Output:

Constant 6.61940
Std Err of Y Est 0.01897
R Squared 0.99950
No. of Observations 10
Degrees of Freedom 8

X Coefficient(s) 1.07243
Std Err of Coef. 0.00848

EXTERNAL CALIBRATION CHECK

CONC (ppm)	RT	AREA	LOG AREA	PREDICTED (ppm)	SDIFF
30.0	9.56	14968778	6.175	28.29	-6.0
30.0	9.58	147661657	6.170	27.87	-7.3

BLANKS

TYPE	RT	AREA	AVERAGE AREA
H2O		ND	
H2O		ND	

MATRIX SPIKE

SAMPLE ID	RT	AVG CONC UNSPKED (PPM)	AVG CONC SPKED (PPM)	% RECOVERY
93-07-250-05 MS 1PPM				0

% RECOVERY = [(AVG. CONC SPKED - AVG. CONC UNSPKED) / ADDED SPIKE VALUE OF 10PPM] X 100

Data Reprocessed On 11/07/1995 08:17:38

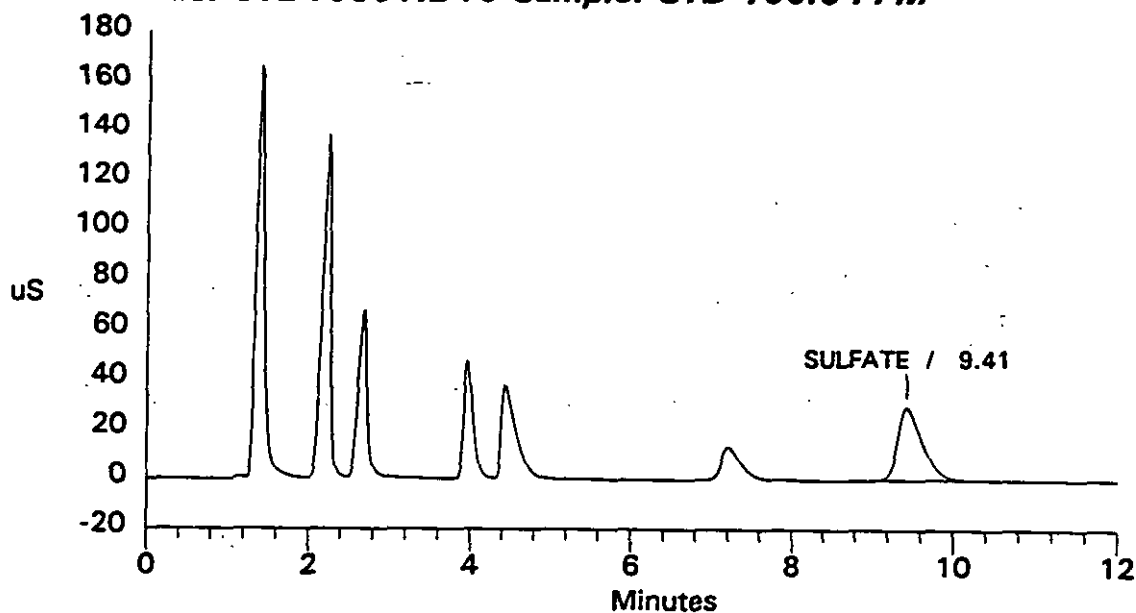
Sample Name: STD 100.0 PPM	Date: 11/06/1995 19:36:07
Data File : C:\DX\DATA\34683C\STD10001.D10	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 10	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.41	SULFATE	0.000	29091848	600505086	1	-3.16
Totals			0.000	29091848	600505086		

File: STD10001.D10 Sample: STD 100.0 PPM



123

19

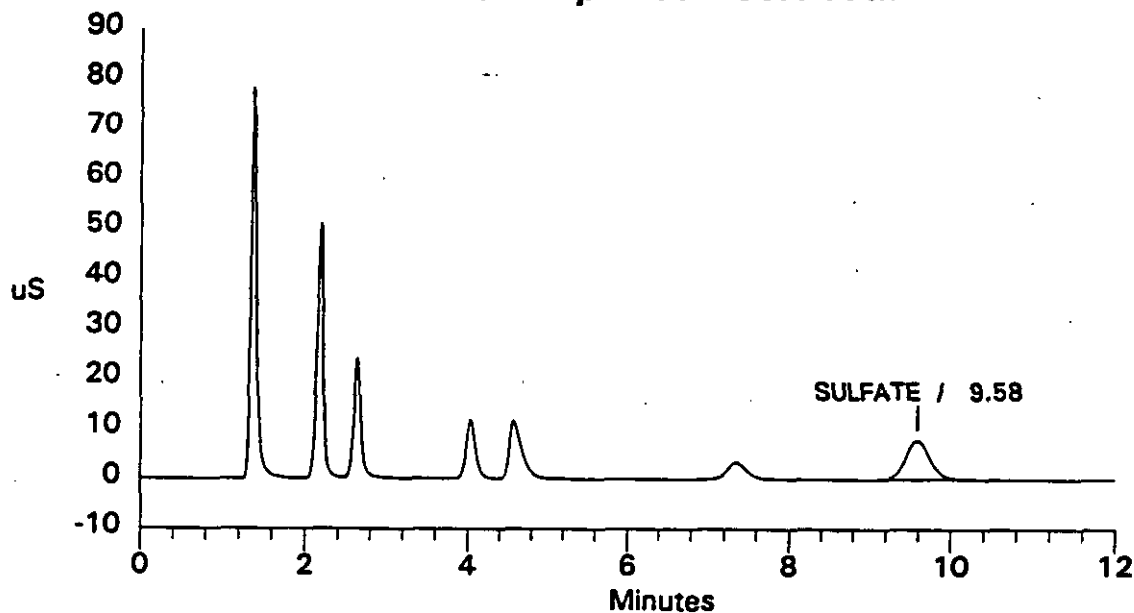
Sample Name: STD 30.0 PPM	Date: 11/06/1995 19:08:33
Data File : C:\DX\DATA\34683C\STD03001.D08	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 8	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.58	SULFATE	0.000	7668245	155380964	1	-1.47
Totals			0.000	7668245	155380964		

File: STD03001.D08 Sample: STD 30.0 PPM



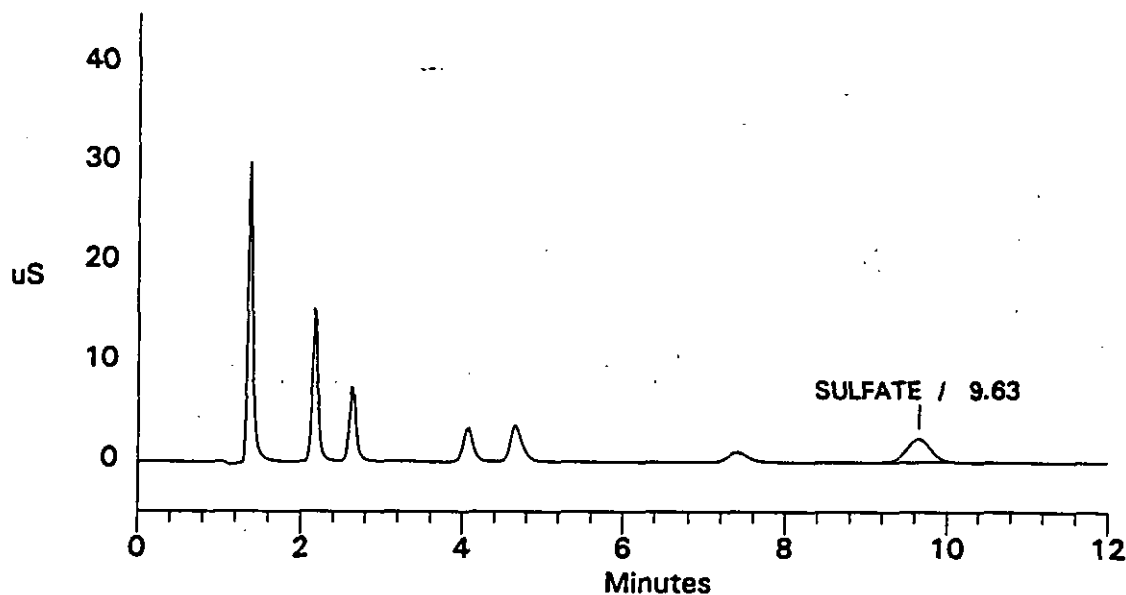
Sample Name: STD 10.0 PPM	Date: 11/06/1995 18:40:59
Data File : C:\DX\DATA\34683C\STD01001.D06	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 6	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.63	SULFATE	0.000	2345067	48573136	1	-0.93
Totals			0.000	2345067	48573136		

File: STD01001.D06 Sample: STD 10.0 PPM



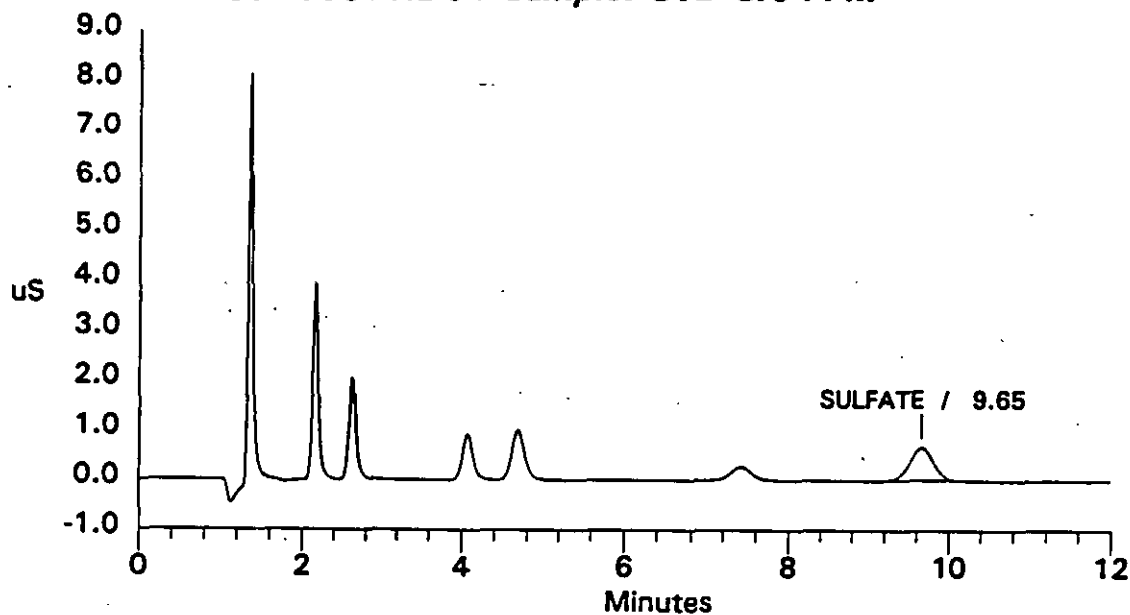
Sample Name: STD 3.0 PPM	Date: 11/06/1995 18:13:25
Data File : C:\DX\DATA\34683C\STD00301.D04	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 4	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.65	SULFATE	0.000	648082	12931835	1	-0.69
Totals			0.000	648082	12931835		

File: STD00301.D04 Sample: STD 3.0 PPM



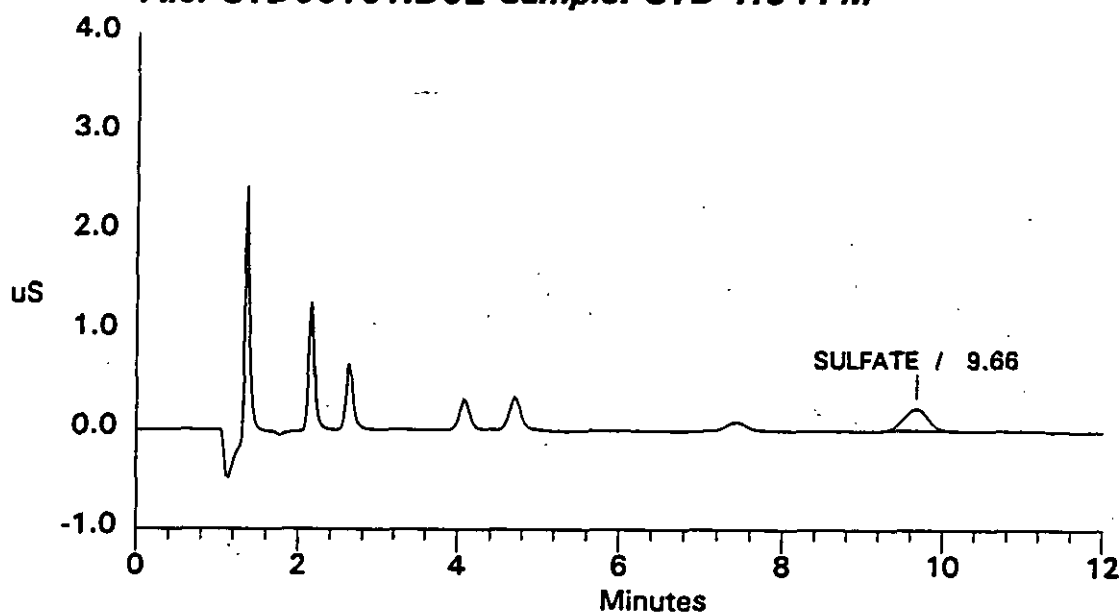
Sample Name: STD 1.0 PPM	Date: 11/06/1995 17:45:51
Data File : C:\DX\DATA\34683C\STD00101.D02	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 2	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.66	SULFATE	0.000	217307	4330129	1	-0.58
Totals			0.000	217307	4330129		

File: STD00101.D02 Sample: STD 1.0 PPM



Data Reprocessed On 11/07/1995 08:18:47

Sample Name: STD 100.0 PPM Date: 11/07/1995 00:39:31
Data File : C:\DX\DATA\34683C\STD10001.D32
Method : C:\DX\METHOD\7ANION.met
ACI Address: 1 System: 1 Inject#: 32 Detector: PED-Cond.
Analyst : Column:

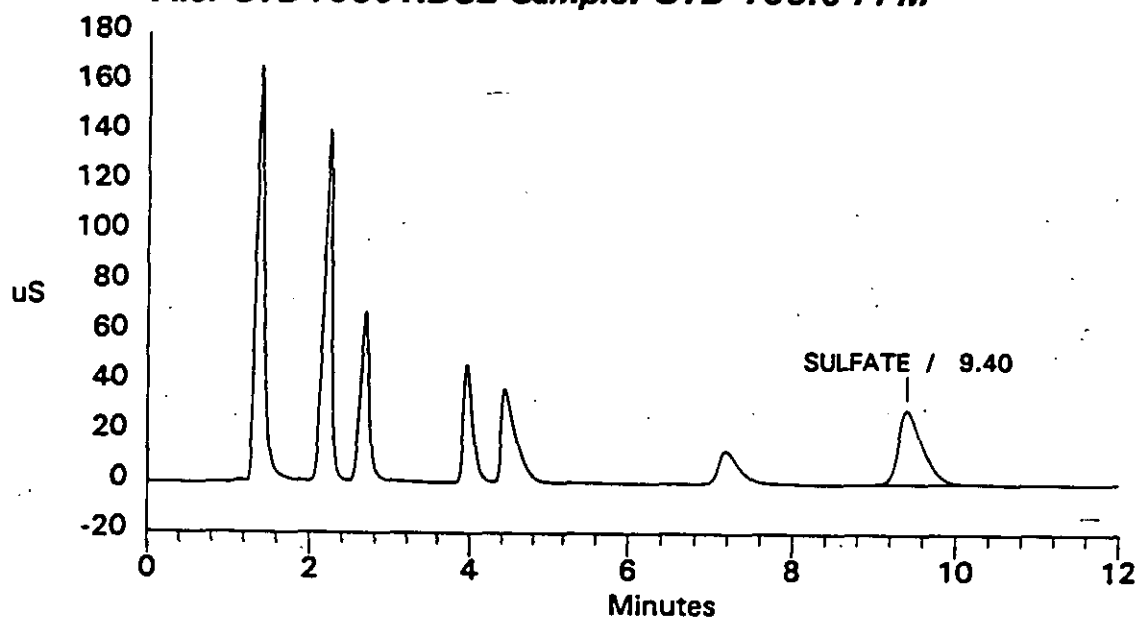
Calibration Volume Dilution Points Rate Start Stop Area Reject

External 1 1 3600 5Hz 0.00 12.00 1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.40	SULFATE	0.000	29349972	603040038	1	-3.33
Totals			0.000	29349972	603040038		

File: STD10001.D32 Sample: STD 100.0 PPM



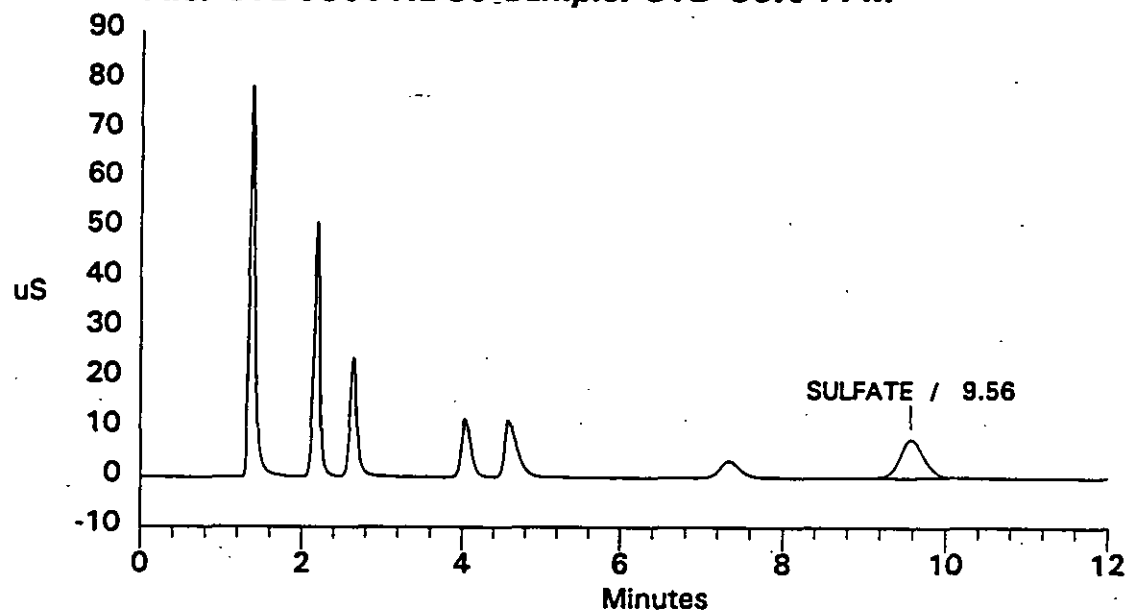
Sample Name: STD 30.0 PPM	Date: 11/07/1995 00:11:57
Data File : C:\DX\DATA\34683C\STD03001.D30	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 30	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5HZ	0.00	12.00	1000	

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.56	SULFATE	0.000	7770477	156082998	1	-1.61
Totals			0.000	7770477	156082998		

File: STD03001.D30 Sample: STD 30.0 PPM



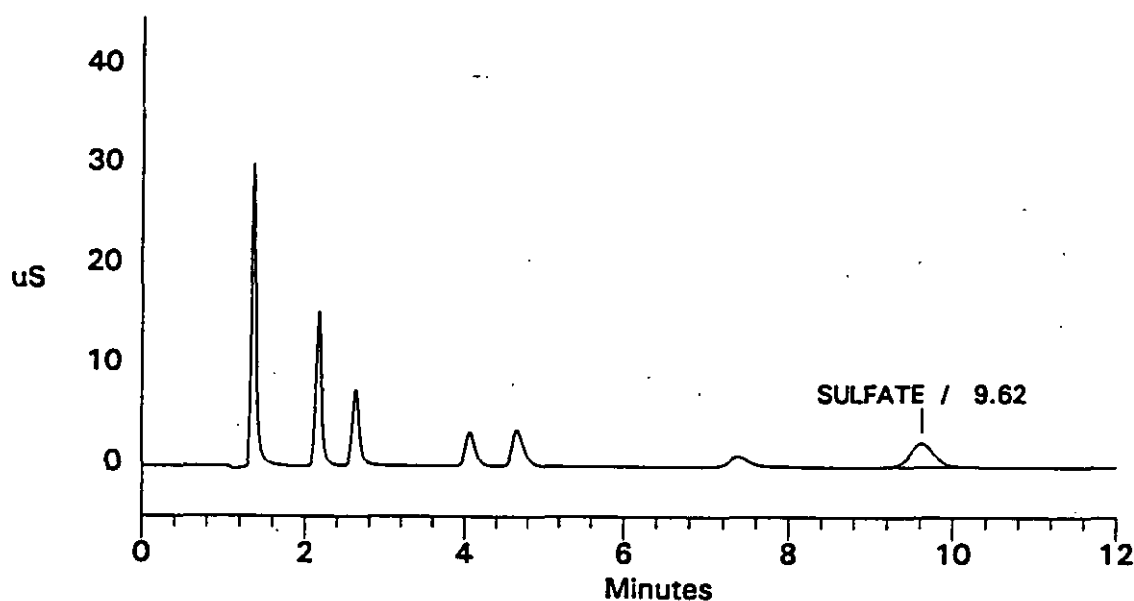
Sample Name: STD 10.0 PPM	Date: 11/06/1995 23:44:23
Data File : C:\DX\DATA\34683C\STD01001.D28	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 28	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.62	SULFATE	0.000	2355181	48009322	1	-1.03
Totals			0.000	2355181	48009322		

File: STD01001.D28 Sample: STD 10.0 PPM



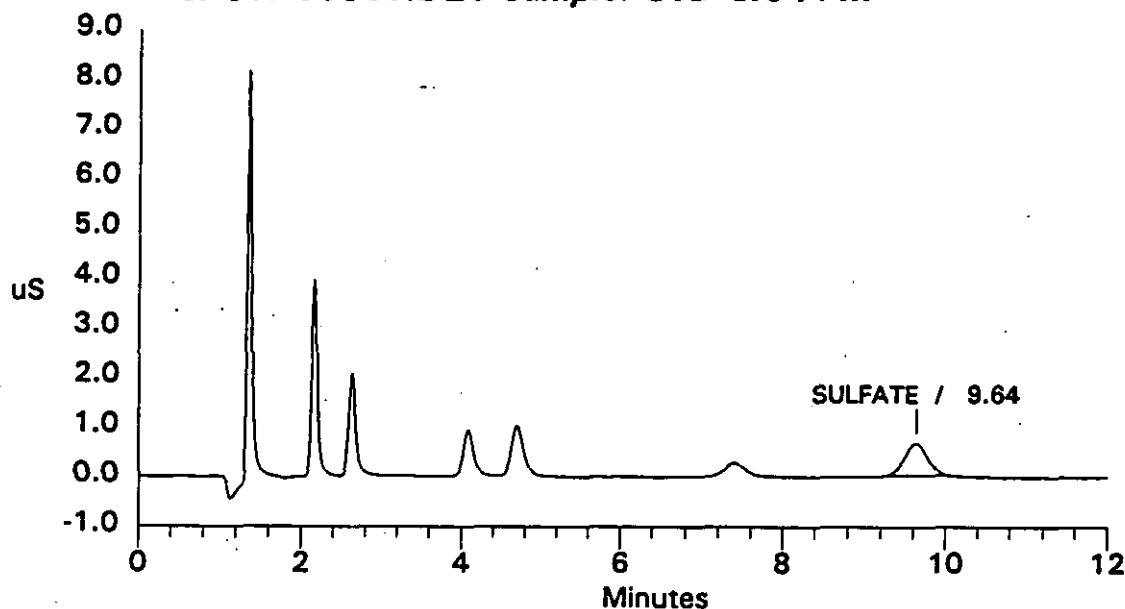
Sample Name: STD 3.0 PPM	Date: 11/06/1995 23:16:47
Data File : C:\DX\DATA\34683C\STD00301.D26	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 26	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.64	SULFATE	0.000	648249	12736862	1	-0.86
Totals			0.000	648249	12736862		

File: STD00301.D26 Sample: STD 3.0 PPM



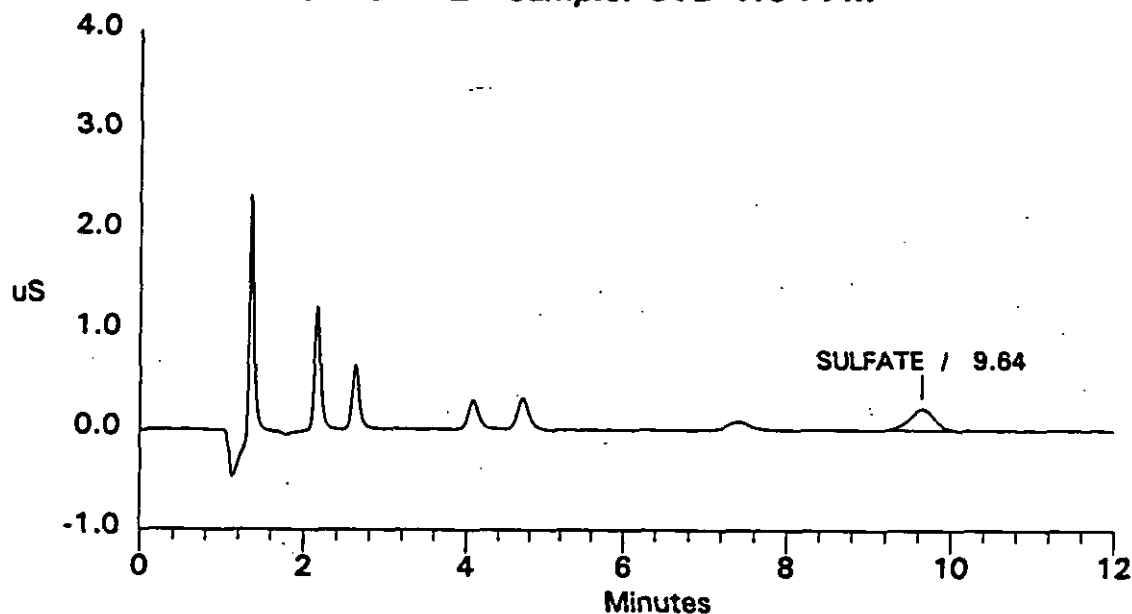
Sample Name: STD 1.0 PPM	Date: 11/06/1995 22:49:11
Data File : C:\DX\DATA\34683C\STD00101.D24	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 24	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.64	SULFATE	0.000	212067	4422430	1	-0.86
Totals			0.000	212067	4422430		

File: STD00101.D24-Sample: STD 1.0 PPM



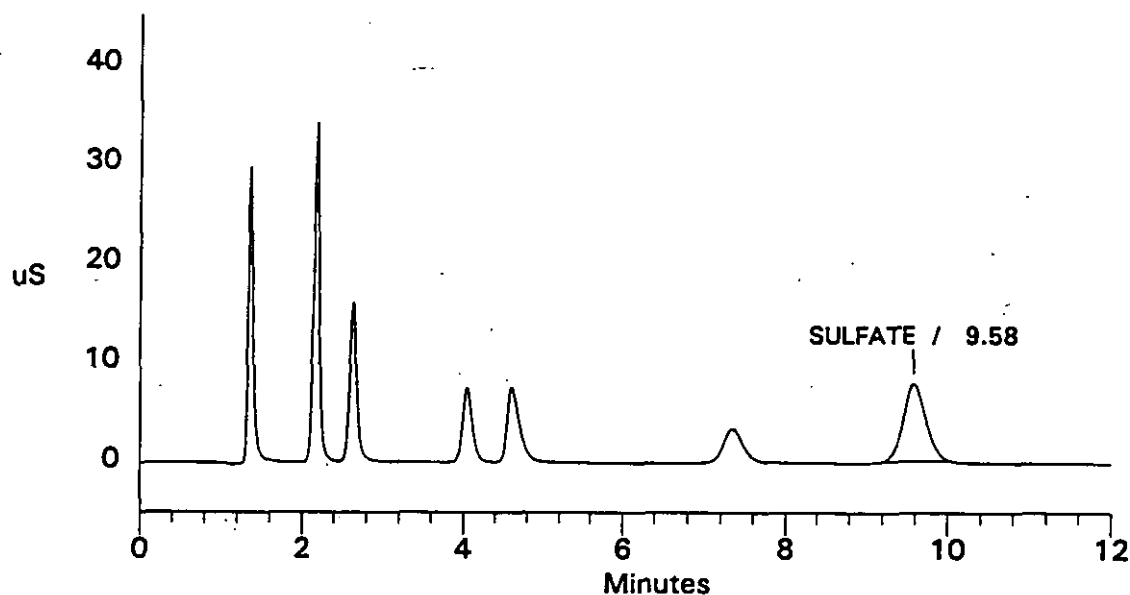
Sample Name: QC	Date: 11/06/1995 20:17:30
Data File : C:\DX\DATA\34683C\QC000001.D13	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 13	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.58	SULFATE	0.000	7707287	149698778	1	-1.47
Totals			0.000	7707287	149698778		

File: QC000001.D13-Sample: QC



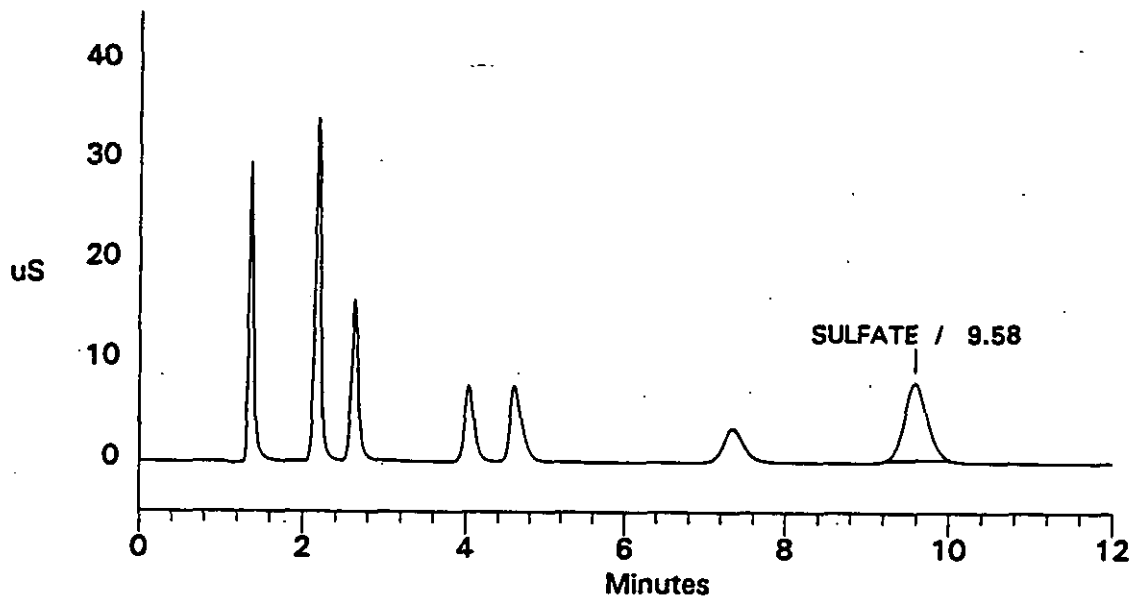
Sample Name: QC	Date: 11/06/1995 20:31:17
Data File : C:\DX\DATA\34683C\QC000001.D14	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 14	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	12.00		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
1	9.58	SULFATE	0.000	7671049	147861657	1	-1.47
Totals			0.000	7671049	147861657		

File: QC000001.D14 Sample: QC



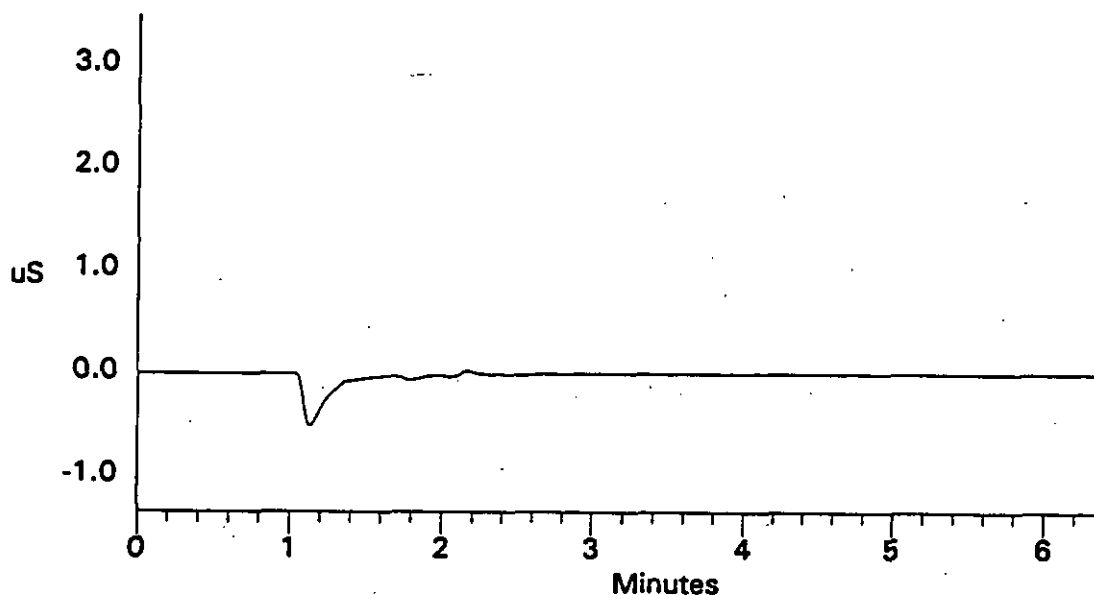
Sample Name: H2O BLANK	Date: 11/06/1995 19:49:54
Data File : C:\DX\DATA\34683C\H2OBLK01.D11	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 11	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	6.42		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
0	0.00	SULFATE	0.000	0	0	0	0.00
Totals			0.000	0	0		

File: H2OBLK01.D11 Sample: H2O BLANK



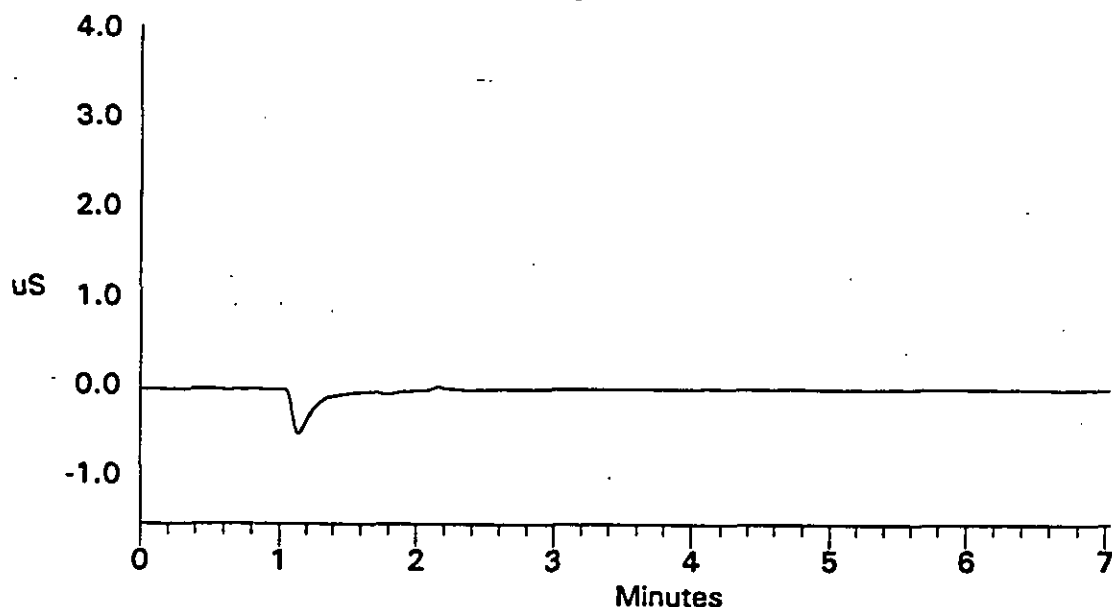
Sample Name: H2O BLANK	Date: 11/06/1995 20:03:42
Data File : C:\DX\DATA\34683C\H2OBLK01.D12	
Method : C:\DX\METHOD\7ANION.met	
ACI Address: 1 System: 1 Inject#: 12	Detector: PED-Cond.
Analyst :	Column:

Calibration	Volume	Dilution	Points	Rate	Start	Stop	Area	Reject
External	1	1	3600	5Hz	0.00	7.04		1000

***** Component Report: All Components *****

Pk. Num	Ret Time	Component Name	Concentration	Height	Area	Bl. Code	%Delta
0	0.00	FLUORIDE	0.000	0	0	0	0.00
0	0.00	CHLORIDE	0.000	0	0	0	0.00
0	0.00	NITRITE	0.000	0	0	0	0.00
0	0.00	BROMIDE	0.000	0	0	0	0.00
0	0.00	NITRATE	0.000	0	0	0	0.00
0	0.00	PHOSPHATE	0.000	0	0	0	0.00
0	0.00	SULFATE	0.000	0	0	0	0.00
Totals			0.000	0	0		

File: H2OBLK01.D12-Sample: H2O BLANK



APPENDIX C. ANALYTICAL DATA

2. Metals



Analytical and Consulting Chemists

1316 South Fifth Street
Wilmington, N.C. 28401
(910) 763-9793
Fax (910) 343-9688

DATE RECEIVED 10-24-95
DATE REPORTED 11-09-95
95W1638

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ENTROPY ENVIRONMENTALIST INC.
P. O. BOX 12291
RESEARCH TRIANGLE PARK, NC 27709-2291

P.O. # 11973-14448-18

ATTENTION: ALAN SENZEL

SAMPLE DESCRIPTION: METHOD 29

1. S-M29-1
2. S-M29-2
3. S-M29-2 DUPLICATE
4. S-M29-3
5. S-M29-3 MATRIX SPIKE % RECOVERY
6. S-M29-FB

RESULTS

	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>
Antimony, as Sb, Total ug	1.26	2.22	2.21	43.4	90.9%	<1.00
Arsenic, as As, Total ug	5.32	6.46	5.95	14.6	104%	2.02
Beryllium, as Be, Total ug	<.100	<.100	<.100	<.100	87.4%	<.100
Cadmium, as Cd, Total ug	.792	1.71	1.66	1.55	102%	<.400
Chromium, as Cr, Total ug	5.88	7.10	7.24	6.82	99.0%	2.18
Cobalt, as Co, Total ug	<1.00	<1.00	<1.00	<1.00	106%	<1.00
Lead, as Pb, Total ug	3.21	3.03	2.83	52.3	82.4%	<1.00
Manganese, as Mn, Total ug	25.2	21.0	19.0	18.4	89.9%	2.56
Nickel, as Ni, Total ug	4.64	5.62	5.74	2.04	90.9%	2.97
Selenium, as Se, Total ug	11.0	10.3	9.99	9.03	106%	<1.00



Analytical and Consulting Chemists

1316 South Fifth Street
Wilmington, N.C. 28401
(910) 763-9793
Fax (910) 343-9688

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95W1638

PAGE 2 OF 4

ENTROPY ENVIRONMENTALIST INC.
P. O. BOX 12291
RESEARCH TRIANGLE PARK, NC 27709-2291

P.O. # 11973-14448-18

ATTENTION: ALAN SENZEL

SAMPLE DESCRIPTION: METHOD 29

1. S-M29-1
2. S-M29-2
3. S-M29-2 DUPLICATE
4. S-M29-3
5. S-M29-3 MATRIX SPIKE % RECOVERY
6. S-M29-FB

RESULTS

	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>
RESULTS: FOR MERCURY, TOTAL-UG						
Mercury, Front 1/2, T ug	<.470	<.470	X	<.470	100%	<.470
Mercury, Front 1/2, T ug	<.470	<.470	X	<.470	X	<.470
Mercury, Back 1/2, T ug	<1.79	<1.76	X	<1.74	107%	<1.36
Mercury, Back 1/2, T ug	<1.79	<1.76	X	<1.74	X	<1.36
Mercury, HNO3, T ug	<.940	<.940	X	<.940	102%	<.940
Mercury, HNO3, T ug	<.940	<.940	X	<.940	X	<.940
Mercury, KMNO4, T ug	<2.35	<2.35	X	<2.35	102%	<2.35
Mercury, KMNO4, T ug	<2.35	<2.35	X	<2.35	X	<2.35
Mercury, HCL, T ug	<2.35	<2.35	X	<2.35	101%	<2.35
Mercury, HCL, T ug	<2.35	<2.35	X	<2.35	X	<2.35



Analytical and Consulting Chemists

1316 South Fifth Street

Wilmington, N.C. 28401

(910) 763-9793

Fax (910) 343-9688

DATE RECEIVED 10-24-95

DATE REPORTED 11-09-95

95W1638

PAGE 3 OF 4

ENTROPY ENVIRONMENTALIST INC.

P.O. # 11973-14448-18

P. O. BOX 12291

RESEARCH TRIANGLE PARK, NC 27709-2291

ATTENTION: ALAN SENZEL

SAMPLE DESCRIPTION: METHOD 29

7. REAGENT BLANKS

8. METHOD CODE - SW846

RESULTS

	<u>7</u>	<u>8</u>
Antimony, as Sb, Total ug	1.45	7041
Arsenic, as As, Total ug	3.49	7060
Beryllium, as Be, Total ug	<.100	7091
Cadmium, as Cd, Total ug	<.400	7131
Chromium, as Cr, Total ug	1.73	7191
Cobalt, as Co, Total ug	<1.00	7201
Lead, as Pb, Total ug	<1.00	7421
Manganese, as Mn, Total ug	1.27	7461
Nickel, as Ni, Total ug	1.06	GF
Selenium, as Se, Total ug	<1.00	7740

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Analytical and Consulting Chemists

1316 South Fifth Street
Wilmington, N.C. 28401
(910) 763-9793
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DATE RECEIVED 10-24-95
DATE REPORTED 11-09-95
95W1638

PAGE 4 OF 4

ENTROPY ENVIRONMENTALIST INC.
P. O. BOX 12291
RESEARCH TRIANGLE PARK, NC 27709-2291

P.O. # 11973-14448-18

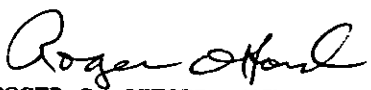
ATTENTION: ALAN SENZEL

SAMPLE DESCRIPTION: METHOD 29

- 7. REAGENT BLANKS
- 8. METHOD CODE - SW846

RESULTS

	<u>7</u>	<u>8</u>
RESULTS: FOR MERCURY, TOTAL UG		
Mercury, Front 1/2, T ug	<.470	7470
Mercury, Front 1/2, T ug	<.470	7470
Mercury, Back 1/2, T ug	<1.41	7470
Mercury, Back 1/2, T ug	<1.41	7470
Mercury, HNO ₃ , T ug	X	7470
Mercury, HNO ₃ , T ug	X	7470
Mercury, KMNO ₄ , T ug	<2.35	7470
Mercury, KMNO ₄ , T ug	<2.35	7470
Mercury, HCL, T ug	<2.35	7470
Mercury, HCL, T ug	<2.35	7470


ROGER C. OXFORD, CHEMIST

SAMPLE TRANSFER RECORD OF CUSTODY

Please include this form with the final (typed) results, and
whenever the final results are faxed to Entropy.

The samples referenced in Entropy Environmentalists Inc. RFA or
purchase order No. 11973-1440-18 were shipped by Entropy
on 10/23/95 (date) via Pony Express (mode)
to Oxford Labs (laboratory)
by [Signature] (signature)

The samples were received for analysis on 10-24-95 (date)
at OLI (laboratory)
by M. Congleton (signature)

As applicable, note any broken seals, leakage, spillage, or damage
to samples. If discrepancy, specify seal No., jar No., sample No.,
etc.

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OXFORD LABORATORY INC.

SAMPLE NARRATIVE SUMMARY OLI #: 95W1638
REPORT DATE: 11-02-95

CLIENT: ENTROPY

PROJECT #: 11973-14448-18

SAMPLE ARRIVAL DATE: 10-24-95

CHAIN OF CUSTODY: YES

SAMPLE ARRIVAL CONDITION/COMMENT: SHIPPED via PONY EXPRESS, NO
PROBLEMS NOTED.

OBSERVED DISCREPANCY/COMMENT: ALL VOLUMES MARKED; UNABLE TO READ
THE VOLUME MARKED ON THE KMnO4
DUE TO SOME SAMPLE LEAKAGE

REQUESTED METHOD OF ANALYSIS: METHOD 29

SAMPLE PREPARATION PER: METHOD 29 (Front Half & Back Half Combined)

SAMPLE ANALYSIS PER: SW-846-7000 series

INSTRUMENTATION USED:

PE 3030 FAA.....NO
PE 5100 FAA.....YES (CVAA Hg)
PE ZEEMAN 5100 GFAA.....YES (All Others)
PE ICP-MS ELAN 5000.....NO

QC REQUIREMENTS: SPIKE RECOVERY OF 90-110 PERCENT HAS BEEN MET
WITH THE FOLLOWING EXCEPTION; #5 Be @ 87.4%,
#5 Mn @ 89.9%, #5 Pb @ 82.4%

FOR DUPLICATES: RELATIVE PERCENT DIFFERENCE OF + OR - 10 PERCENT
WAS MET

SAMPLE NOTE: #6(FB) As @ 2.02ug, #7(Blks) As @ 3.49ug,
#7(Blks) Sb @ 1.45ug, #6(FB) Ni @ 2.97ug,
#7(Blks) Ni @ 1.06ug, #6(FB) Mn @ 2.56ug,
#7(Blks) Mn @ 1.27ug, #6(FB) Cr @ 2.18ug,
#7(Blks) Cr @ 1.73ug

LABORATORY CONTROL BLANK: ALL LESS THAN

LABORATORY CONTROL SPIKE: 90-110 PERCENT HAS BEEN MET WITH
THE FOLLOWING EXCEPTION; Sb @ 116%

DETECTION LIMIT: ALL HAVE BEEN MET WITH THE FOLLOWING
EXCEPTION; As @ 5.6ug/ml (112%) As was also
analyzed at 4.83ug/ml

CALIBRATION VERIFICATION: OUTSIDE QC WAS MET (90% TO 110%)

CALIBRATION COEFFICIENT: ALL ELEMENTS AT LEAST .996

THIS DATA PACKAGE CONTAINS 16 SUMMARY PAGES TO INCLUDE THE
NARRATIVE SUMMARY; ALL PERTINENT DATA ON FILE AT OLI.

FRONT HALF & BACK HALF COMBINED FINAL VOLUMES ARE 100ml * 2

Hg VOLUMES:		BEGINNING VOLUME	FINAL VOLUME
BH	#1	380ml	380ml
BH	#2 & #3	375ml	375ml
BH	#4 & #5	370ml	370ml
BH	#6	290ml	290ml
BH	#7	300ml	300ml
FH	#1	79ml	100ml
FH	#2 & #3	98ml	100ml
FH	#4 & #5	110ml	100ml
FH	#6	75ml	100ml
FH	#7	100ml	100ml
HN03	#1	65ml	200ml
HN03	#2 & #3	65ml	200ml
HN03	#4 & #5	65ml	200ml
HN03	#6	50ml	200ml
HN03	#7		
KMn04	#1	360ml	500ml
KMn04	#2 & #3	350ml	500ml
KMn04	#4 & #5	375ml	500ml
KMn04	#6	290ml	500ml
KMn04	#7	200ml	500ml
HCl	#1	225ml	500ml
HCl	#2 & #3	220ml	500ml
HCl	#4 & #5	220ml	500ml
HCl	#6	230ml	500ml
HCl	#7	225ml	500ml

CALCULATION FOR TOTAL uG REPORTED:

GFAA uG/L * DILUTION FACTOR * FINAL VOLUME / 1000 = TOTAL uG

Hg uG * DILUTION FACTOR * FINAL VOLUME / ALIQUOT USED = TOTAL uG

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A.A. SUMMARY REPORT

CLIENT: ENTROPY
P.O.#/PROJECT #: 11973-14448-18
ANALYST: SYLVIA THOMPSON/KEN SMITH
DATE: 10/30/95

WT. STDS
x CONC STDS
5.000 INST LIMIT ug/L
6.25 SPK LEVEL ug/L
1.00 MAX ALIQUOT
1 METHOD DET. TOTAL ug

SAMPLE I.D.	EL	ug/L		F.V. X	DILUTION	TOTAL ug	% REC OR <	ug/L SPK
		MEAN ABS	READING					
1638-001	Sb	.0267456	6.3	1	200	1.26		
1638-002	Sb	.0465523	11.09	1	200	2.22		
1638-003-#2dup	Sb	.0463784	11.05	1	200	2.21		
1638-004	Sb	.0455156	10.84	1	4000	43.4		
1638-005-#4spk	Sb	.0675929	16.52	1	4000	66.1	90.9	6.25
1638-006	Sb	.0177401	4.16	1	200 <		1.00	
1638-007	Sb	.0306414	7.23	1	200	1.45		
OLI 0ug	Sb	.0076545	1.79	1	100 <		.500	
OLI 5ug spk	Sb	.0499699	11.94	1	500	5.97	116	10

						ug/ml	
Blank	Sb	-.000087	-.02	1	1 <		.005
D.L.=.005ug/ml	Sb	.0227996	5.36	1	1	.0054	
Known=.010ug/ml	Sb	.0430009	10.22	1	1	.0102	
QC=12.5ug/L	Sb	.0495118	11.83	1	1	.0118	
QC=12.5ug/L	Sb	.0540864	12.98	1	1	.0130	
QC=12.5ug/L	Sb	.0492777	11.77	1	1	.0118	

Std Blank	Sb	.0015349					
Std 1=5.00ug/L	Sb	.0219335					
Std 2=10.0ug/L	Sb	.0401485	9.15				
Std 3=15.0ug/L	Sb	.0607176	16.89				
Std 4=20.0ug/L	Sb	.0803404	21.13				
Std 5=25.0ug/L	Sb	.0956695	24.75				

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A.A. SUMMARY REPORT

CLIENT: ENTROPY

P.O.#/PROJECT #: 11973-14448-18

ANALYST: SYLVIA THOMPSON/KEN SMITH

DATE: 10/27/95

WT. STDS
x CONC STDS
5.000 INST LIMIT ug/L
8.33 SPK LEVEL ug/L
1.00 MAX ALIQUOT
1 METHOD DET. TOTAL ug

SAMPLE I.D.	EL	MEAN ABS	READING	INSTRU	SAMPLE	F.V.	X	ALIQ	DILUTION	TOTAL ug	% REC	OR <	ug/L SPK
1638-001	As	.0761336	13.3			1		400		5.32			
1638-002	As	.0621823	10.76			1		600		6.46			
1638-003-#2dup	As	.0574772	9.92			1		600		5.95			
1638-006	As	.0393894	6.72			1		300		2.02			
1638-007	As	.0669509	11.63			1		300		3.49			

Blank	As	.0046549	.78	1	1	<				ug/ml		.005	
D.L.=.005ug/ml	As	.0285246	4.83	1	1					.0048			
Known=.010ug/ml	As	.0553705	9.54	1	1					.0095			
QC=12.5ug/L	As	.0683587	11.88	1	1					.0119			
QC=12.5ug/L	As	.065416	11.35	1	1					.0114			
QC=12.5ug/L	As	.0704053	12.25	1	1					.0123			
Std Blank	As	.001789	.31										
Std 1=5.00ug/L	As	.0298856	5.12										
Std 2=10.0ug/L	As	.0581026	9.72										
Std 3=15.0ug/L	As	.0822398	14.51										
Std 4=20.0ug/L	As	.1125602	39.45										
Std 5=25.0ug/L	As	.1388108	25.79										

1638-004	As	.0786918	14.55	1	1000					TOTAL ug			
1638-005-#4spk	As	.1256721	23.21	1	1000					14.6			
OLI 0ug	As	.0151518	2.81	1	100	<				23.2	104	8.33	
OLI 5ug spk	As	.0535447	9.91	1	500					4.96	.500	10	

Blank	As	.0009163	.17	1	1	<				ug/ml		.005	
D.L.=.005ug/ml	As	.0302033	5.6	1	1					.0056			
QC=12.5ug/L	As	.0675428	12.5	1	1					.0125			
QC=12.5ug/L	As	.0718465	13.29	1	1					.0133			
Std Blank	As	-.001883	-.23										
Std 1=5.00ug/L	As	.0266486	3.65										
Std 2=10.0ug/L	As	.0548689	10.29										
Std 3=15.0ug/L	As	.0814606	14.46										
Std 4=20.0ug/L	As	.1074471	19.49										
Std 5=25.0ug/L	As	.135333	24.96										

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A.A. SUMMARY REPORT

CLIENT: ENTROPY
P.O.#/PROJECT #: 11973-14448-18
ANALYST: SYLVIA THOMPSON/KEN SMITH
DATE: 10/30/95

WT. STDS
x CONC STDS
.500 INST LIMIT ug/L
1.67 SPK LEVEL ug/L
1.00 MAX ALIQUOT
.1 METHOD DET. TOTAL ug

SAMPLE I.D.	EL	uG/L		INSTRU	SAMPLE	F.V.	X	DILUTION	TOTAL ug	% REC OR <	ug/L	SPK
		MEAN	ABS READING									
1638-001	Be	.0047452	.08		1	200	<				.100	
1638-002	Be	.0056079	.1		1	200	<				.100	
1638-003-#2dup	Be	.0052067	.09		1	200	<				.100	
1638-004	Be	.0041633	.07		1	200	<				.100	
1638-005-#4spk	Be	.086373	1.53		1	200		.306		87.4	1.67	
1638-006	Be	.0021502	.04		1	200	<				.100	
1638-007	Be	.0005819	.01		1	200	<				.100	
OLI 0ug	Be	.0002241	0		1	100	<				.050	
OLI 5ug spk	Be	.055725	.97		1	5000		4.85		97.0		1

D.L.=.0005ug/ml	Be	.0274411	.47	1	1	ug/ml	.00047
Known=.010ug/ml	Be	.0902187	1.61	1	6		.00966
QC=2.50ug/L	Be	.1353096	2.47	1	1		.00247
QC=2.50ug/L	Be	.1357209	2.47	1	1		.00247
QC=2.50ug/L	Be	.1383259	2.53	1	1		.00253
QC=2.50ug/L	Be	.1356306	2.47	1	1		.00247

Std Blank	Be	.0034778					
Std 1=1.00ug/L	Be	.0587948					
Std 2=2.00ug/L	Be	.1084905	1.85				
Std 3=3.00ug/L	Be	.1591191	3.21				
Std 4=4.00ug/L	Be	.2077849	4.19				
Std 5=5.00ug/L	Be	.2630584	5.18				

A.A. SUMMARY REPORT

CLIENT: ENTROPY

P.O.#/PROJECT #: 11973-14448-18

ANALYST: SYLVIA THOMPSON/KEN SMITH

DATE: 11/01/95

WT. STDS
x CONC STDS
2.000 INST LIMIT ug/L
3.33 SPK LEVEL ug/L
1.00 MAX ALIQUOT
.4 METHOD DET. TOTAL ug

SAMPLE I.D.	EL	MEAN ABS	uG/L READING	INSTRU SAMPLE	F.V. X DILUTION	TOTAL ug	% REC OR <	ug/L SPK
1638-001	Cd	.3689539	3.96	1	200	.792		
1638-002	Cd	.3886034	4.28	1	400	1.71		
1638-003-#2dup	Cd	.3808988	4.15	1	400	1.66		
1638-004	Cd	.3629881	3.87	1	400	1.55		
1638-005-#4spk	Cd	.5323133	7.28	1	400	2.91	102	3.33
1638-006	Cd	.03647	.29	1	200 <		.400	
1638-007	Cd	.0130752	.1	1	200 <		.400	
OLI 0ug	Cd	.002819	.02	1	100 <		.200	
OLI 5ug spk	Cd	.4162151	4.75	1	1000	4.75	95.0	5

D.L.=.002ug/ml	Cd	.2113162	1.92	1	1	.0019		
Known=.010ug/ml	Cd	.6221708	10.24	1	1	.0102		
QC=5.00ug/L	Cd	.4172183	4.77	1	1	.0048		
QC=5.00ug/L	Cd	.4293438	4.99	1	1	.0050		
QC=5.00ug/L	Cd	.4190776	4.8	1	1	.0048		

Std Blank	Cd	.0005819	0					
Std 1=2.00ug/L	Cd	.2178337	2.11					
Std 2=4.00ug/L	Cd	.3767421	3.46					
Std 3=6.00ug/L	Cd	.4721541	5.53					
Std 4=8.00ug/L	Cd	.5543672	9.88					
Std 5=10.0ug/L	Cd	.6222377	11.24					

(9)

A.A. SUMMARY REPORT

CLIENT: ENTROPY

P.O.#/PROJECT #: 11973-14448-18

ANALYST: SYLVIA THOMPSON/KEN SMITH

DATE: 10/31/95

WT. STDS
 x CONC STDS
 5.000 INST LIMIT ug/L
 6.25 SPK LEVEL ug/L
 1.00 MAX ALIQUOT
 1 METHOD DET. TOTAL ug

SAMPLE I.D.	EL	MEAN ABS	uG/L READING	INSTRU	SAMPLE X ALIQUOT	F.V. DILUTION	TOTAL ug	% REC	OR <	ug/L SPK
1638-001	Cr	.3325641	14.69	1	400	5.88				
1638-002	Cr	.2749799	11.83	1	600	7.10				
1638-003-#2dup	Cr	.2797585	12.06	1	600	7.24				
1638-006	Cr	.2556513	10.9	1	200	2.18				
1638-007	Cr	.2079186	8.67	1	200	1.73				
OLI 0ug	Cr	.0259129	.99	1	100	<		.500		
OLI 5ug spk	Cr	.2498595	10.63	1	500	5.32		104		10

D.L.=.005ug/ml	Cr	.1138744	4.55	1	1	.0046	ug/ml
Known=.010ug/ml	Cr	.2221374	9.33	1	1	.0093	
QC=12.5ug/L	Cr	.280638	12.1	1	1	.0121	
QC=12.5ug/L	Cr	.2941378	12.76	1	1	.0128	

Std Blank	Cr	-.018549	-.81				
Std 1=5.00ug/L	Cr	.1247826	5.55				
Std 2=10.0ug/L	Cr	.2390716	9.58				
Std 3=15.0ug/L	Cr	.3333934	14.47				
Std 4=20.0ug/L	Cr	.4298554	24.03				
Std 5=25.0ug/L	Cr	.5261469	26.81				

1638-004	Cr	.27397	11.37	1	600	TOTAL ug 6.82			
1638-005-#4spk	Cr	.3984449	17.56	1	600	10.5	99.0	6.25	

D.L.=.005ug/ml	Cr	.1202949	4.65	1	1	.0047	
Known=.010ug/ml	Cr	.2465288	10.1	1	1	.0101	
QC=12.5ug/L	Cr	.2843164	11.85	1	1	.0119	
QC=12.5ug/L	Cr	.3098213	13.07	1	1	.0131	

Std Blank	Cr	.0011202	.04				
Std 1=5.00ug/L	Cr	.1260968	4.83				
Std 2=10.0ug/L	Cr	.2564405	10.17				
Std 3=15.0ug/L	Cr	.3327982	12.85				
Std 4=20.0ug/L	Cr	.450555	21.07				
Std 5=25.0ug/L	Cr	.5280831	24.75				

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A.A. SUMMARY REPORT

CLIENT: ENTROPY

P.O.#/PROJECT #: 11973-14448-18

ANALYST: SYLVIA THOMPSON/KEN SMITH

DATE: 10/30/95

WT. STDS
X CONC STDS
5.000 INST LIMIT ug/L
8.33 SPK LEVEL ug/L
1.00 MAX ALIQUOT
1 METHOD DET. TOTAL ug

SAMPLE I.D.	EL	MEAN ABS	READING	INSTRU	SAMPLE	F.V.	X	ALIQ	DILUTION	TOTAL ug	% REC	OR <	ug/L	SPK
1638-001	Co	.0106608	1.13		1	200	<				1.00			
1638-002	Co	.0089453	.94		1	200	<				1.00			
1638-003-#2dup	Co	.0103631	1.1		1	200	<				1.00			
1638-004	Co	.0055009	.58		1	200	<				1.00			
1638-005-#4spk	Co	.0876404	9.42		1	200				1.88	106		8.33	
1638-006	Co	.0028157	.3		1	200	<				1.00			
1638-007	Co	.0012005	.13		1	200	<				1.00			
OLI 0ug	Co	.0013844	.15		1	100	<				.500			
OLI 5ug spk	Co	.1000134	10.78		1	500				5.39	108		10	

D.L.=.005ug/ml	Co	.0461777	4.92	1	1	ug/ml	.0049
Known=.010ug/ml	Co	.0921147	9.91	1	1		.0099
QC=12.5ug/L	Co	.1227361	13.29	1	1		.0133
QC=12.5ug/L	Co	.1098214	11.86	1	1		.0119

Std Blank	Co	.0021402	.21				
Std 1=5.00ug/L	Co	.0467563	4.6				
Std 2=10.0ug/L	Co	.093566	10.01				
Std 3=15.0ug/L	Co	.1360553	14.53				
Std 4=20.0ug/L	Co	.1867342	20.83				
Std 5=25.0ug/L	Co	.2225889	—				

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A.A. SUMMARY REPORT

CLIENT: ENTROPY
P.O.#/PROJECT #: 11973-14448-18
ANALYST: SYLVIA THOMPSON/KEN SMITH
DATE: 11/01/95

WT. STDS
x CONC STDS
5.000 INST LIMIT ug/L
13.33 SPK LEVEL ug/L
1.00 MAX ALIQUOT
1 METHOD DET. TOTAL ug

SAMPLE I.D.	EL	MEAN ABS	UG/L READING	INSTRU	SAMPLE X	F.V. DILUTION	TOTAL ug	% REC	OR <	ug/L SPK
1638-001	Pb	.045101	8.02	1	400		3.21			
1638-002	Pb	.0824103	15.14	1	200		3.03			
1638-003-#2dup	Pb	.0775214	14.17	1	200		2.83			
1638-004	Pb	.0582631	10.46	1	5000		52.3			
1638-005-#4spk	Pb	.1123796	21.45	1	5000		107		82.4	13.33
1638-006	Pb	.011343	1.98	1	200 <				1.00	
1638-007	Pb	.0153056	2.67	1	200 <				1.00	
OLI 0ug	Pb	.0021001	.36	1	100 <				.500	
OLI 5ug spk	Pb	.0552267	9.9	1	500		4.95		98.3	10

D.L.=.005ug/ml	Pb	.0275448	4.84	1	1		.0048			
Known=.010ug/ml	Pb	.0549826	9.85	1	1		.0099			
QC=12.5ug/L	Pb	.0746154	13.6	1	1		.0136			
QC=12.5ug/L	Pb	.0684223	12.4	1	1		.0124			
QC=12.5ug/L	Pb	.0667636	12.08	1	1		.0121			
QC=12.5ug/L	Pb	.0711209	12.92	1	1		.0129			
QC=12.5ug/L	Pb	.0677936	12.28	1	1		.0123			

Std Blank	Pb	.0016386	.26							
Std 1=5.00ug/L	Pb	.0288891	4.8							
Std 2=10.0ug/L	Pb	.0542335	9.39							
Std 3=15.0ug/L	Pb	.0821161	16.31							
Std 4=20.0ug/L	Pb	.1055778	20.04							
Std 5=25.0ug/L	Pb	.1287051								

A.A. SUMMARY REPORT

CLIENT: ENTROPY

P.O.#/PROJECT #: 11973-14448-18

ANALYST: SYLVIA THOMPSON/KEN SMITH

DATE: 10/31/95

WT. STDS
x CONC STDS
5.000 INST LIMIT ug/L
6.25 SPK LEVEL ug/L
1.00 MAX ALIQUOT
1 METHOD DET. TOTAL ug

SAMPLE I.D.	EL	MEAN ABS	UG/L INSTRU READING	SAMPLE ALIQUOT	F.V. X DILUTION	TOTAL ug	* REC OR <	ug/L SPK
1638-001	Mn	.2569957	12.6	1	2000	25.2		
1638-002	Mn	.225448	10.51	1	2000	21.0		
1638-003-#2dup	Mn	.2089386	9.52	1	2000	19.0		
1638-004	Mn	.2033941	9.21	1	2000	18.4		
1638-005-#4spk	Mn	.2858914	14.83	1	2000	29.7	89.9	6.25
1638-006	Mn	.2596909	12.79	1	200	2.56		
1638-007	Mn	.1492509	6.37	1	200	1.27		
OLI 0ug	Mn	.0165061	.64	1	100 <	.500		
OLI 5ug spk	Mn	.231688	10.9	1	500	5.45	108	10

D.L.=.005ug/ml	Mn	.1261269	5.28	1	1	.0053
Known=.010ug/ml	Mn	.214493	9.85	1	1	.0099
QC=12.5ug/L	Mn	.2708801	13.62	1	1	.0136
QC=12.5ug/L	Mn	.2516552	12.22	1	1	.0122
QC=12.5ug/L	Mn	.2612693	12.9	1	1	.0129
QC=12.5ug/L	Mn	.2687834	13.46	1	1	.0135

Std Blank	Mn	.0035781	.13
Std 1=5.00ug/L	Mn	.1199973	4.78
Std 2=10.0ug/L	Mn	.2175929	9.07
Std 3=15.0ug/L	Mn	.2885566	14.33
Std 4=20.0ug/L	Mn	.333049	19.64
Std 5=25.0ug/L	Mn	.3705958	27.23

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A.A. SUMMARY REPORT

CLIENT: ENTROPY

P.O.#/PROJECT #: 11973-14448-18

ANALYST: SYLVIA THOMPSON/KEN SMITH

DATE: 10/31/95

WT. STDS

x CONC STDS

5.000 INST LIMIT ug/L

8.33 SPK LEVEL ug/L

1.00 MAX ALIQUOT

1 METHOD DET. TOTAL ug

SAMPLE I.D.	EL	MEAN ABS	READING	INSTRU	SAMPLE	F.V.	TOTAL ug	% REC	OR <	ug/L SPK
					ALIQUOT	X				
1638-001	Ni	.0580992	7.74		1	600	4.64			
1638-002	Ni	.0701478	9.37		1	600	5.62			
1638-003-#2dup	Ni	.0715222	9.56		1	600	5.74			
1638-004	Ni	.076264	10.2		1	200	2.04			
1638-005-#4spk	Ni	.1313168	17.77		1	200	3.55	90.9		8.33
1638-006	Ni	.1102193	14.85		1	200	2.97			
1638-007	Ni	.0400682	5.32		1	200	1.06			
OLI 0ug	Ni	.0023876	.31		1	100	<	.500		
OLI 5ug spk	Ni	.0780063	10.44		1	500	5.22	104		10

						ug/ml
D.L.=.005ug/ml	Ni	.0404895	5.37	1	1	.0054
Known=.010ug/ml	Ni	.0718599	9.6	1	1	.0096
QC=12.5ug/L	Ni	.0948769	12.74	1	1	.0127
QC=12.5ug/L	Ni	.0922619	12.38	1	1	.0124
QC=12.5ug/L	Ni	.0920178	12.35	1	1	.0124

Std Blank	Ni	.0014413	.3			
Std 1=5.00ug/L	Ni	.0372826	7.87			
Std 2=10.0ug/L	Ni	.0761403	10.21			
Std 3=15.0ug/L	Ni	.1104467	14.25			
Std 4=20.0ug/L	Ni	.1477929	20.01			
Std 5=25.0ug/L	Ni	.1821528	24.8			

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A.A. SUMMARY REPORT

CLIENT: ENTROPY
P.O.#/PROJECT #: 11973-14448-18
ANALYST: SYLVIA THOMPSON/KEN SMITH
DATE: 10/27/95

WT. STDS
x CONC STDS
5.000 INST LIMIT ug/L
8.33 SPK LEVEL ug/L
1.00 MAX ALIQUOT
1 METHOD DET. TOTAL ug

SAMPLE I.D.	EL	ug/L		F.V.	X	TOTAL ug	% REC OR <	ug/L SPK
		MEAN ABS	READING					
1638-001	Se	.0389814	11	1	1000	11.0		
1638-002	Se	.0365403	10.27	1	1000	10.3		
1638-003-#2dup	Se	.0355872	9.99	1	1000	9.99		
1638-004	Se	.0522171	15.05	1	600	9.03		
1638-005-#4spk	Se	.0793171	23.89	1	600	14.3	106	8.33
1638-006	Se	.0091392	2.46	1	200 <		1.00	
1638-007	Se	.0032939	.88	1	200 <		1.00	
OLI 0ug	Se	-.001073	-.29	1	100 <		.500	
OLI 5ug spk	Se	.0362594	10.19	1	500	5.10	102	10

D.L.=.005ug/ml	Se	.0166934	4.55	1	1	.0046
Known=.010ug/ml	Se	.0338483	9.48	1	1	.0095
QC=12.5ug/L	Se	.0441847	12.57	1	1	.0126
QC=12.5ug/L	Se	.0431481	12.26	1	1	.0123

Std Blank	Se	-.003391	-.37			
Std 1=5.00ug/L	Se	.0185995	3.94			
Std 2=10.0ug/L	Se	.0338316	9.09			
Std 3=15.0ug/L	Se	.0536717	18.23			
Std 4=20.0ug/L	Se	.0682985	19.92			
Std 5=25.0ug/L	Se	.0816212	24.28			

4G1020.WKS

A.A. SUMMARY REPORT

=====

CLIENT:ENTROPY

L.O.#/PROJECT #:11973-14448-18

ANALYST: KEN SMITH/SC/AJ

DATE: 11/01/95

X WT. STDS
CONC STDS
.047 INST LIMIT uG
.2 SPK LEVEL uG
10.00 MAX ALIQUOT mL
.047 M.D.L. uG/mL

DATE: 11/01/95		UG		mL		F.V.		.047 M.D.L.		UG/mL	
		INSTR		SAMPLE		X		TOTAL UG		.2	
SAMPLE-I.D.	EL	MEAN ABS	READ	ALIQ	DILUTION	ANSWER	% REC	OR	<	UG	SPK
=====											
-1638-001	Hg	.0019061	.008	10	200	<			.940	.2	
-1638-001	Hg	.0013042	.006	10	200	<			.940	.2	
-1638-002	Hg	.0005016	.002	10	200	<			.940	.2	
-1638-002	Hg	.0006019	.003	10	200	<			.940	.2	
-1638-004	Hg	.0005016	.002	10	200	<			.940	.2	
-1638-004	Hg	.0011035	.005	10	200	<			.940	.2	
-1638-005-SPK	Hg	.0472512	.203	10	200		4.06		102	.2	
-1638-005-SPK	Hg	.045947	.198	10	200		3.96		99.0	.2	
-1638-006	Hg	.0009029	.004	10	200	<			.940	.2	
-1638-006	Hg	.0010032	.004	10	200	<			.940	.2	
-1638-001	Hg	.0044141	.019	10	500	<			2.35	.2	
-1638-001	Hg	.0043138	.019	10	500	<			2.35	.2	
-1638-002	Hg	.0042135	.018	10	500	<			2.35	.2	
-1638-002	Hg	.0040128	.018	10	500	<			2.35	.2	
-1638-004	Hg	.0029093	.013	10	500	<			2.35	.2	
-1638-004	Hg	.0032103	.014	10	500	<			2.35	.2	
-1638-005-SPK	Hg	.0456461	.196	10	500		9.80		98.0	.2	
-1638-005-SPK	Hg	.0471509	.203	10	500		10.2		102	.2	
-1638-006	Hg	.0013042	.006	10	500	<			2.35	.2	
-1638-006	Hg	.0017055	.007	10	500	<			2.35	.2	
-1638-007	Hg	.0010032	.004	10	500	<			2.35	.2	
-1638-007	Hg	.0014045	.006	10	500	<			2.35	.2	
H-1638-001	Hg	.0088282	.039	10	380	<			1.79	.2	
H-1638-001	Hg	.0083266	.036	10	380	<			1.79	.2	
H-1638-002	Hg	.0083266	.036	10	375	<			1.76	.2	
H-1638-002	Hg	.008126	.035	10	375	<			1.76	.2	
H-1638-004	Hg	.0077247	.034	10	370	<			1.74	.2	
H-1638-004	Hg	.0071228	.031	10	370	<			1.74	.2	
H-1638-005-SPK	Hg	.0523676	.225	10	370		8.33		113	.2	
H-1638-005-SPK	Hg	.0497592	.214	10	370		7.92		107	.2	
H-1638-006	Hg	.0040128	.018	10	290	<			1.36	.2	
H-1638-006	Hg	.002809	.012	10	290	<			1.36	.2	
H-1638-007	Hg	.0034109	.015	10	300	<			1.41	.2	
H-1638-007	Hg	.00311	.014	10	300	<			1.41	.2	
-1638-001	Hg	.0004013	.002	10	500	<			2.35	.2	
-1638-001	Hg	.001104	.005	10	500	<			2.35	.2	
-1638-002	Hg	.0004013	.002	10	500	<			2.35	.2	
-1638-002	Hg	.0006019	.003	10	500	<			2.35	.2	
-1638-004	Hg	.0004013	.002	10	500	<			2.35	.2	
-1638-004	Hg	.0002006	.001	10	500	<			2.35	.2	
-1638-005-SPK	Hg	.0475522	.205	10	500		10.3		103	.2	
-1638-005-SPK	Hg	.0467496	.201	10	500		10.1		101	.2	
-1638-006	Hg	.0016051	.007	10	500	<			2.35	.2	
-1638-006	Hg	.0009029	.004	10	500	<			2.35	.2	
-1638-007	Hg	.0009029	.004	10	500	<			2.35	.2	
-1638-007	Hg	.0006019	.003	10	500	<			2.35	.2	
H-1638-001	Hg	.000301	.001	10	100	<			.470	.2	
H-1638-001	Hg	.000301	.001	10	100	<			.470	.2	
H-1638-002	Hg	.000301	.001	10	100	<			.470	.2	
H-1638-002	Hg	.000301	.001	10	100	<			.470	.2	
H-1638-004	Hg	.000301	.001	10	100	<			.470	.2	

PH-1638-004	Hg	.0007022	.003	10	100 <		.470	.2
PH-1638-005-SPK	Hg	.046248	.199	10	100	1.99	100	.2
PH-1638-005-SPK	Hg	.0463483	.199	10	100	1.99	100	.2
PH-1638-006	Hg	.000301	.001	10	100 <		.470	.2
PH-1638-006	Hg	.0002006	.001	10	100 <		.470	.2
PH-1638-007	Hg	.0005016	.002	10	100 <		.470	.2
PH-1638-007	Hg	.0014045	.006	10	100 <		.470	.2
=====								
STANDARD BLANK	Hg	.0018058	.009					
STANDARD .1uG	Hg	.0220706	.103					
STANDARD .2uG	Hg	.048756	.221					
STANDARD .3uG	Hg	.0709269	.27					
STANDARD .4uG	Hg	.0933989	.376					
STANDARD .5uG	Hg	.1184791	.491					
=====								
STD #2	Hg	.0481541	.207	1	1	.207		.2
STD #2	Hg	.0445425	.192	1	1	.192		.2
Std .1uG	Hg	.0233748	.101	1	1	.101		.2
Std .1uG	Hg	.0227729	.099	1	1	.099		.2
Std .2uG	Hg	.0446428	.192	1	1	.192		.2
Std .4uG	Hg	.0881822	.374	1	1	.374		.2
Std .5uG	Hg	.1183788	.496	1	1	.496		.2
Std .5uG	Hg	.1040329	.438	1	1	.438		.2
STD BLANK	Hg	-.000803	-.004					
STD BLANK	Hg	.000301	.001					
STD BLANK	Hg	.0005016	.002					
STD BLANK	Hg	-.001404	-.006					
STD BLANK	Hg	.0002006	.001					
STD BLANK	Hg	.0015048	.007					
WASH	Hg	.0001003	0					
Blank-Std	Hg	-.000201	-.001					
Blank-Std	Hg	.0010032	.004					
Det Lmt=.02 uG	Hg	.0047151	.021	1	1 <		.047	.2
Det Lmt=.02 uG	Hg	.0050161	.022	1	1 <		.047	.2
Det Lmt=.02 uG	Hg	.0052167	.023	1	1 <		.047	.2

Mercury Duplicate Analyses Results

Plant: Triangle Brick
Job #: 14448

	First Analysis	Second Analysis	Average	Relative % Difference
Brick Kiln Stack				
S-M29-1				
Front half	< 0.470	< 0.470	< 0.470	NA
Back half	< 1.79	< 1.79	< 1.79	NA
HNO ₃	< 0.940	< 0.940	< 0.940	NA
KMnO ₄	< 2.35	< 2.35	< 2.35	NA
HCl	< 2.35	< 2.35	< 2.35	NA
	SUM		0.0	
S-M29-2				
Front half	< 0.470	< 0.470	< 0.470	NA
Back half	< 1.76	< 1.76	< 1.76	NA
HNO ₃	< 0.940	< 0.940	< 0.940	NA
KMnO ₄	< 2.35	< 2.35	< 2.35	NA
HCl	< 2.35	< 2.35	< 2.35	NA
	SUM		0.0	
S-M29-3				
Front half	< 0.470	< 0.470	< 0.470	NA
Back half	< 1.74	< 1.74	< 1.74	NA
HNO ₃	< 0.940	< 0.940	< 0.940	NA
KMnO ₄	< 2.35	< 2.35	< 2.35	NA
HCl	< 2.35	< 2.35	< 2.35	NA
	SUM		0.0	
S-M29-FB				
Front half	< 0.470	< 0.470	< 0.470	NA
Back half	< 1.36	< 1.36	< 1.36	NA
HNO ₃	< 0.940	< 0.940	< 0.940	NA
KMnO ₄	< 2.35	< 2.35	< 2.35	NA
HCl	< 2.35	< 2.35	< 2.35	NA
	SUM		0.0	

METALS BLANK CORRECTION CALCULATIONS

Revised: 2/15/94

COMBINED

Run Number, Metal	Filter Diameter (Inches)	p r g	Catch Weight (mt)	p r g	Blank Catch (mtb)	Corrected Result (m)	1 + 1.4*Area (A')	5% mt (5mt)	Result to Use
S-M29-1, Antimony	3.348		1.26		1.45	-0.19	13.310	0.063	0.00
S-M29-2, Antimony	3.348		2.22		1.45	0.77	13.310	0.111	0.770
S-M29-3, Antimony	3.348		43.4		1.45	41.95	13.310	2.17	42.0
S-M29-1, Arsenic	3.348		5.32		3.49	1.83	13.310	0.268	1.83
S-M29-2, Arsenic	3.348		6.21		3.49	2.72	13.310	0.311	2.72
S-M29-3, Arsenic	3.348		14.6		3.49	11.11	13.310	0.73	11.1
S-M29-1, Chromium	3.348		5.88		1.73	4.15	13.310	0.294	4.15
S-M29-2, Chromium	3.348		7.17		1.73	5.44	13.310	0.359	5.44
S-M29-3, Chromium	3.348		6.82		1.73	5.09	13.310	0.341	5.09
S-M29-1, Manganese	3.348		25.2		1.27	23.93	13.310	1.26	23.9
S-M29-2, Manganese	3.348		20		1.27	18.73	13.310	1	18.7
S-M29-3, Manganese	3.348		18.4		1.27	17.13	13.310	0.92	17.1
S-M29-1, Nickel	3.348		4.64		1.06	3.58	13.310	0.232	3.58
S-M29-2, Nickel	3.348		6.68		1.06	4.62	13.310	0.284	4.62
S-M29-3, Nickel	3.348		2.04		1.06	0.98	13.310	0.102	0.880

Metals Duplicate Analysis Results

Plant: Triangle Brick
Job #: 14448

	Reagent Blank ⁽¹⁾	Field Blank	Matrix Spike ⁽²⁾	First Analysis ⁽³⁾	Second Analysis	Average	Relative % Difference ⁽⁴⁾
Antimony	1.45	< 1.00	90.9	2.22	2.21	2.22	0.226
Arsenic	3.49	2.02	104	6.46	5.95	6.21	4.11
Beryllium	< 0.100	< 0.100	87.4	< 0.100	< 0.100	< 0.100	NA
Cadmium	< 0.400	< 0.400	102	1.71	1.68	1.69	1.48
Chromium	1.73	2.18	89.0	7.10	7.24	7.17	0.976
Cobalt	< 1.00	< 1.00	106	< 1.00	< 1.00	< 1.00	NA
Lead	< 1.00	< 1.00	82.4	3.03	2.83	2.93	3.41
Manganese	1.27	2.56	89.9	21.0	19.0	20.0	5.00
Nickel	1.06	2.97	90.9	5.62	5.74	5.68	1.06
Selenium	< 1.00	< 1.00	106	10.30	9.99	10.15	1.53

⁽¹⁾ Combined filter, front-half 0.1N HNO₃ rinse, acetone rinse, and HNO₃/H₂O₂ reagent.

⁽²⁾ Performed on repetition 3.

⁽³⁾ Performed on repetition 2.

⁽⁴⁾ Not applicable if one or both results are below the detection limit.

APPENDIX C. ANALYTICAL DATA

3. Methane

Entropy/Withers & Ravenel (14448)

**Analytical Report
(1095-18)**

Location: S

***Compound:* Methane**



Enthalpy Analytical, Inc.

3211 Bramer Drive

Raleigh, NC 27604

919/850-4392

Request for Analysis



ENTHALPY analytical, inc.

ENTROPY

Environmentalists, Inc.

P.O. Box 12291
Research Triangle Park
North Carolina 27709-2291
919-781-3550 FAX 919-787-8442

REQUEST FOR ANALYSIS

PO#: 11988 - 14448-18

Customer Name: Withers and Ravenel
Triangle Brick

Laboratory: ENT

Date Transmitted: 10/24/95

Results Due By: 11/07/95

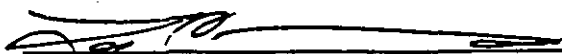
Sample Matrix: Method 18

PM: VJT

Analysis: Analyze samples for Methane according to EPA Method 18.

Sample #	Sample ID	Components/Comments
1	S-M18MOD-1	Tank #183, 4.591
2	S-M18MOD-2	Tank #233, 4.511
3	S-M18MOD-3	Tank #242, 4.511

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Submitted By: 

Summary of Results



Company:	Entropy/Withers & Ravenel	Enthalpy #:	1095-18
Analyst:	DMB	Sampled:	10/17/95
Parameters:	Methane	Received:	10/24/95
# Samples:	3	Analyzed:	10/25/95

Compound	Concentration (PPMV)
	Methane
S-M18MOD-1	< 1.98
S-M18MOD-2	< 1.91
S-M18MOD-3	< 1.92



Results



CH4 MDL: 1 ppm
 CH4 LOQ: 5 ppm
 CH4 Curve Values (64, 128, 513, 1025 ppmv)

Company:	Entropy/Witthers & Ravenel	Client #:	14448
Analyst:	DMB	Exhaler #:	1095-18
Parameters:	Methane	PO #:	11988-14448-18
# Samples:	3	Date:	10/31/95

Reviewed: SLC
 Date: 11/1/95

Sample Identification	Retention Time (min.)		Percent Difference		Concentration		% Difference of Mean	As Analyzed Concentration	Cal. Curve	Dilution Factor	As Sampled PPMV
	Inj. # 1	Inj. # 2	Inj. # 1	Inj. # 2	Inj. # 1	Inj. # 2					
S-M18MOD-1	NA	NA	NA	NA	< 1.00	< 1.00	0.00	< 1.00	1095-18	1.983	< 1.98
S-M18MOD-2	NA	NA	NA	NA	< 1.00	< 1.00	0.00	< 1.00	1095-18	1.907	< 1.91
S-M18MOD-3	NA	NA	NA	NA	< 1.00	< 1.00	0.00	< 1.00	1095-18	1.921	< 1.92



Narrative Summary



Enthalpy Analytical Narrative Summary

Company:	Entropy/Withers & Ravenel
Client #:	14448
PO #:	11988-14448-18

Enthalpy #:	1095-18
Analyst:	DMB
Parameters	Methane

Custody

Samples were picked up from Les Murray of Entropy by Scott Grosshandler of Enthalpy on 10/24/95. No apparent container problems were noted upon receipt. Prior to and during analysis, the samples were kept under lock with access only to authorized personnel of Enthalpy Analytical, Inc.

Analysis

Tank pressures were measured upon receipt. Each tank was then pressurized to around 600 mmHg. A dilution ratio was calculated for each tank based on the temperature and pressure after sample transfer and the final temperature and pressure (see Reporting Notes).

Each tank was analyzed for Methane using a Hewlett Packard 5980 Series II gas chromatograph equipped with a flame ionization detector. All samples were separated using a Restek 2.0 m x 1.0 ID HayeSep-S Micropacked column. Hydrogen was used as the carrier gas. Samples were injected into the GC using a VICI ten port valve with a 0.2 mL gas sample loop.

Methane eluted at the approximate retention time listed below:

Methane 1.04 min

The following chromatographic conditions were present during analysis:

Detector temperature: 250° C
 Initial Oven Temp. - 45°C for 2.00 minutes
 Level 1 - 10°C/minute to 150°C hold 2.00 minutes
 Net Run Time: 14.50 minutes
 Pressure Constant: 11.0 psi at 45°C

Labeling

OK

Reproducibility

All standards were within 10% of their tag value.

Reporting Notes

The symbols MDL and LOQ represent the Minimum Detection Limit and the Limit of Quantification. The values that are between the MDL and the LOQ are represent by a tilde (~).

All tanks were adjusted from "as analyzed" concentrations to "as sampled" concentrations using a dilution factor which was calculated based on the following formula:

$$\frac{(\text{Final mmHg} + (\text{Pbar} * 25.401))}{(\text{Initial mmHg} + (\text{Pbar} * 25.401))} * \frac{(\text{Temp. Initial} + 460)}{(\text{Temp. Final} + 460)}$$



Narrative (cont'd)

Pressurization Data is as follows:

Barometric Pressure = 758 mm Hg

Temperature = 72 degrees F

<u>Run ID</u>	<u>Initial mmHg</u>	<u>Final mmHg</u>
Run 1	33	764
Run 2	25	699
Run 3	22	704



Sample Custody



ENTHALPY analytical, inc.

SAMPLE TRANSFER RECORD OF CUSTODY

Please include this form with the final (typed) results, and whenever the final results are faxed to Entropy.

The samples referenced in Entropy Environmentalists Inc. RFA or purchase order No. 11988-14448-18 were shipped by Entropy on 10/24/95 (date) via Personal Custody (mode) to Enthalp-1 (laboratory) by [Signature] (signature)

The samples were received for analysis on 10-24-95 (date) at Entropy (laboratory) by [Signature] (signature)

As applicable, note any broken seals, leakage, spillage, or damage to samples. If discrepancy, specify seal No., jar No., sample No., etc.

ENTROPY/ Withers & Ravenel

Pbar 758

T (F) 72

Sample #	Sample ID	P initial	P final	Dilution
1	S-M18MOD-1	33	764	1.92
2	S-M18MOD-2	25	699	1.86
3	S-M18MOD-3	22	704	1.87

EVACUATED TANK PARAMETERS

Client Withers and Ravenel
 Plant Name Triangle Brick Job No. 14884
 City/State Merry Oaks, ALA. Sampling Loc. Brick Kiln #2 Stack

Tank No. 183 Tank Volume, liters 4.59 Sampling Time Start 1010
 From Sampling Run No. S-M29-1 Sampling Time Finish 1117
 Sample Transfer Run No. S-M18MOD-1 Sample Transfer Date & Time 10/17/95 1130

Parameter	Barometric Pressure *		Tank Temp. *		Tank Pressure Gauge *		Leak Check	
	In. Hg	mm Hg	°F	°C	In. Hg	mm Hg	cm Hg change	Tank System
Pretest	30.5	774.7	58		-751	-752	0.00	0.00
Posttest	30.5	774.7	58		-	-42	0.00	0.00
1st (Field) Pressurization					+			JRW Operator

Tank No. 233 Tank Volume, liters 4.51 Sampling Time Start 1150
 From Sampling Run No. S-M29-2 Sampling Time Finish 1255
 Sample Transfer Run No. S-M18MOD-2 Sample Transfer Date & Time 10/17/95 1324

Parameter	Barometric Pressure *		Tank Temp. *		Tank Pressure Gauge *		Leak Check	
	In. Hg	mm Hg	°F	°C	In. Hg	mm Hg	cm Hg change	Tank System
Pretest	30.5	774.7	62		-	-756	0.00	0.00
Posttest	30.5	774.7	62		-	0	0.00	0.00
1st (Field) Pressurization					+			JRW Operator

Tank No. 242 Tank Volume, liters 4.51 Sampling Time Start 1330
 From Sampling Run No. S-M29-3 Sampling Time Finish 1436
 Sample Transfer Run No. S-M18MOD-3 Sample Transfer Date & Time

Parameter	Barometric Pressure *		Tank Temp. *		Tank Pressure Gauge *		Leak Check	
	In. Hg	mm Hg	°F	°C	In. Hg	mm Hg	cm Hg change	Tank System
Pretest	30.5	774.7	65		-	-756	0.00	0.00
Posttest	30.5	774.7	65		-		0.00	0.00
1st (Field) Pressurization					+			JRW Operator

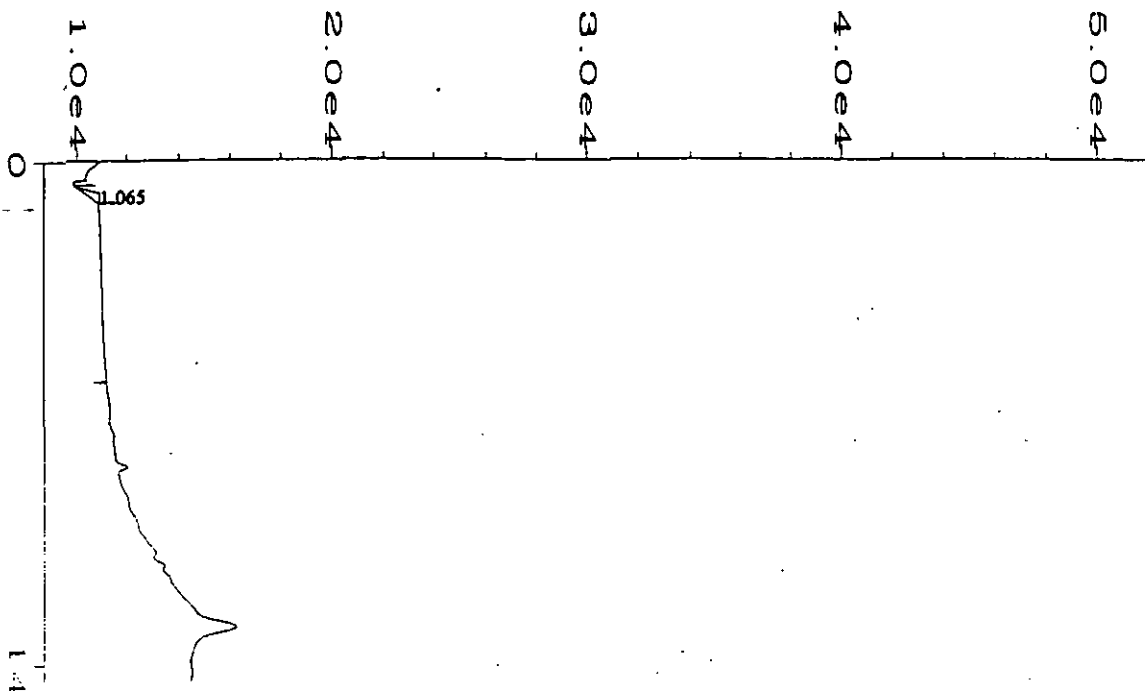
176

* As applicable, use In. Hg or mm Hg, and °F or °C. Note: mm Hg = In. Hg * 25.401

Chromatograms



ENTHALPY analytical, inc.



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External Standard Report

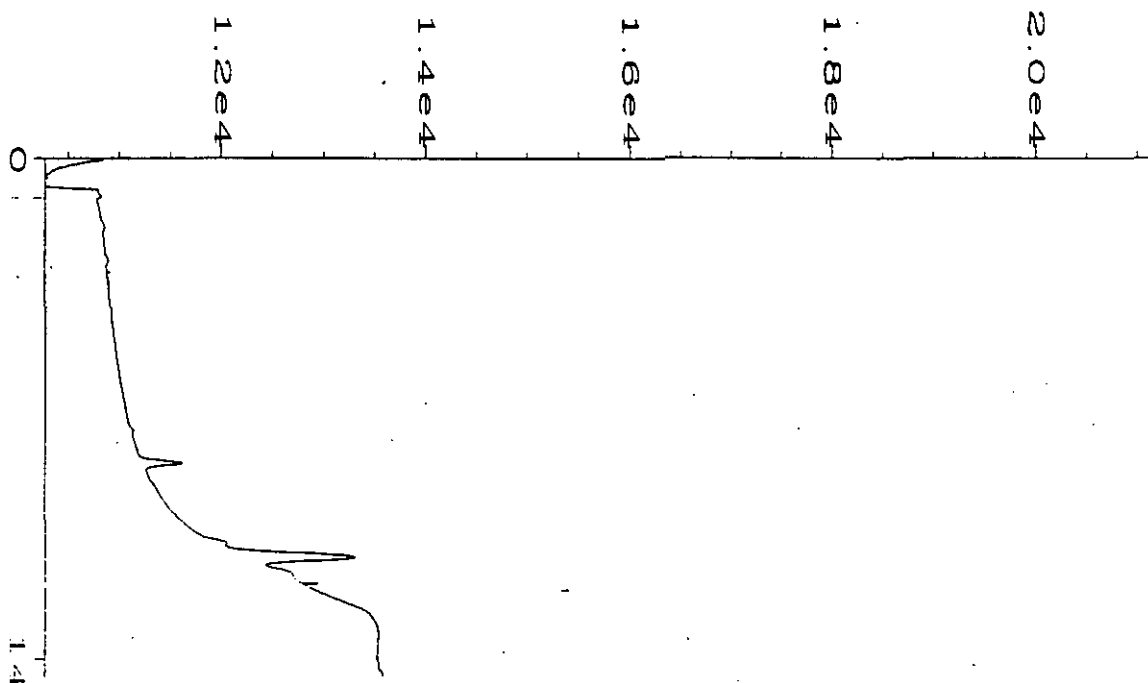
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a File Name	: C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0110.D	
Operator	: dmb	Page Number : 1
Instrument	: TELLER	Vial Number :
Sample Name	: S-M18MOD-1	Injection Number :
Run Time Bar Code:		Sequence Line :
Acquired on	: 26 Oct 95 01:00 PM	Instrument Method: 1095-18.MTH
Report Created on:	26 Oct 95 02:31 PM	Analysis Method : 1095-18A.MTH
Last Recalib on	: 26 Oct 95 02:06 PM	Sample Amount : 0
Multiplier	: 1	ISTD Amount :

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0110.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.065	7682	BB	0.420	1	5.005	Methane

28 10/26/95



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 External Standard Report
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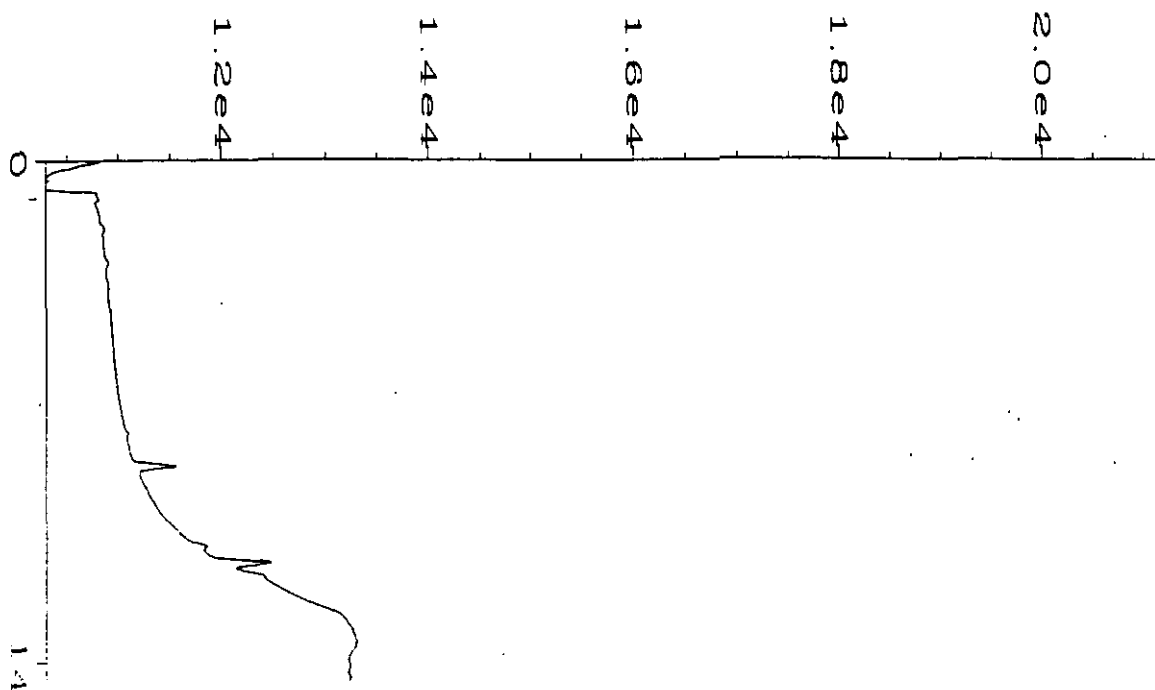
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Instrument        : TELLER                           Vial Number       :
Sample Name       : S-M18MOD-1                       Injection Number  :
Run Time Bar Code:                                   Sequence Line    :
Acquired on      : 26 Oct 95  01:37 PM                 Instrument Method: 1095-18.MTH
Report Created on: 26 Oct 95  02:31 PM                 Analysis Method  : 1095-18A.MTH
Last Recalib on  : 26 Oct 95  02:06 PM                 Sample Amount    : 0
Multiplier       : 1                                   ISTD Amount      :
  
```

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0111.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.040	*	not found	*	1		Methane

Not all calibrated peaks were found



External Standard Report

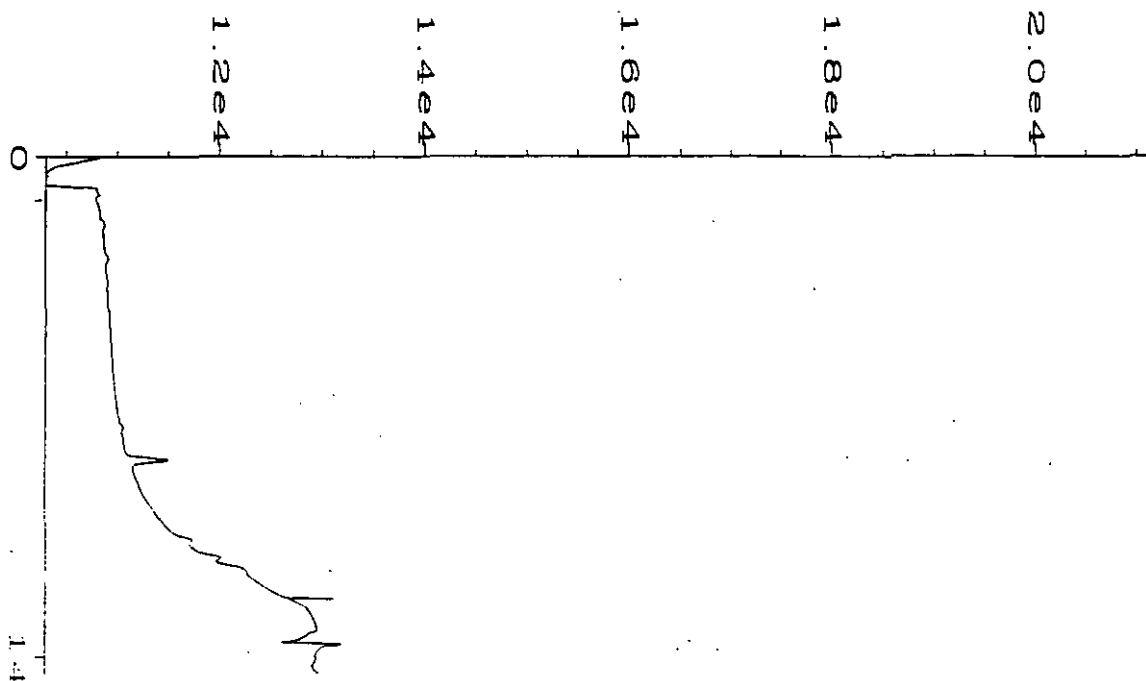
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a File Name      : C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0112.D
Operator         : dmb                               Page Number      : 1
Instrument        : TELLER                           Vial Number       :
Sample Name      : S-M18MOD-2                       Injection Number  :
Run Time Bar Code:                               Sequence Line     :
Acquired on      : 26 Oct 95  02:03 PM               Instrument Method: 1095-18.MTH
Report Created on: 26 Oct 95  02:31 PM               Analysis Method   : 1095-18A.MTH
Last Recalib on  : 26 Oct 95  02:06 PM               Sample Amount    : 0
Multiplier       : 1                               ISTD Amount      :
  
```

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0112.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.040	* not found *			1		Methane

Not all calibrated peaks were found



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External Standard Report

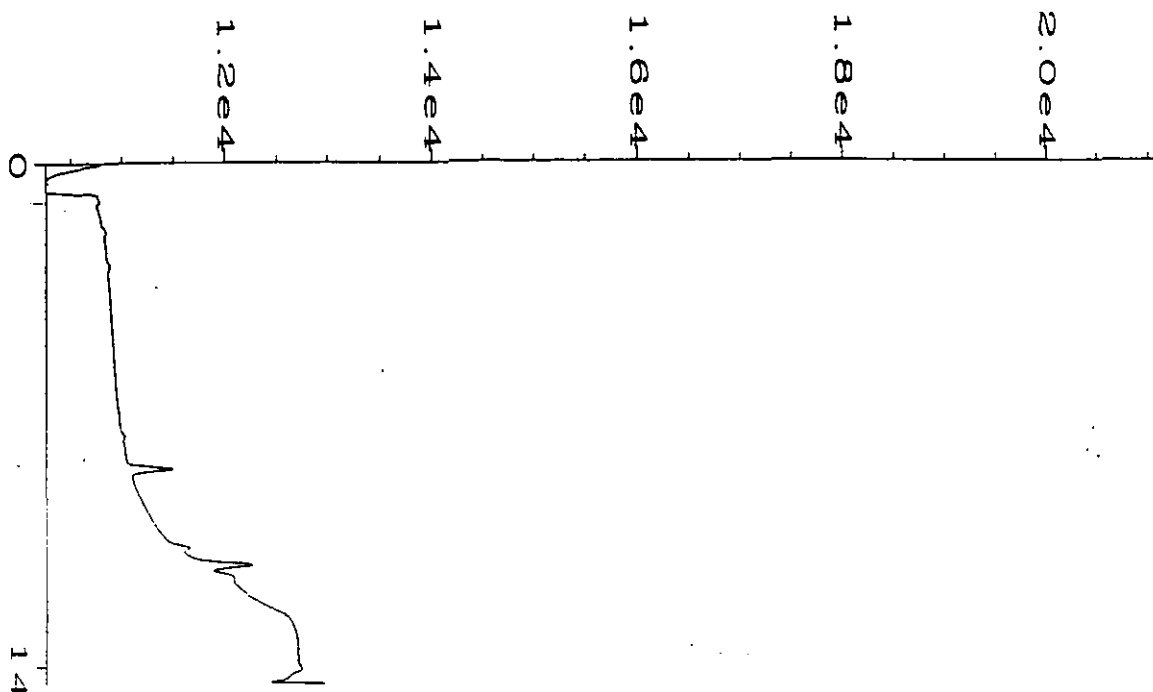
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Operator	: dmb	Page Number : 1
Instrument	: TELLER	Vial Number :
Sample Name	: S-M18MOD-2	Injection Number :
Run Time Bar Code:		Sequence Line :
Acquired on	: 26 Oct 95 02:26 PM	Instrument Method: 1095-18.MTH
Report Created on:	26 Oct 95 03:01 PM	Analysis Method : 1095-18A.MTH
Last Recalib on	: 26 Oct 95 02:06 PM	Sample Amount : 0
Multiplier	: 1	ISTD Amount :

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0113.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.040	* not found *			1		Methane

Not all calibrated peaks were found



External Standard Report

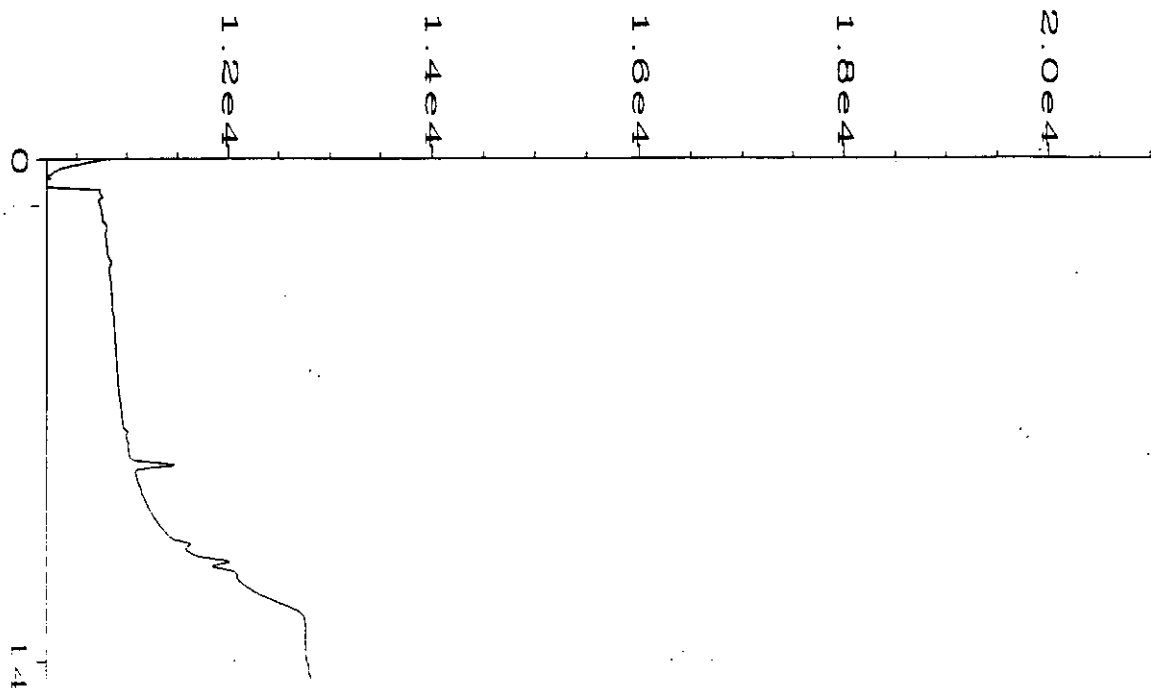
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a File Name      : C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0114.D
Operator         : dmb                               Page Number      : 1
Instrument       : TELLER                           Vial Number       :
Sample Name      : S-M18MOD-3                       Injection Number  :
Run Time Bar Code:                               Sequence Line    :
Acquired on      : 26 Oct 95  02:46 PM               Instrument Method: 1095-18.MTH
Report Created on: 26 Oct 95  03:01 PM               Analysis Method  : 1095-18A.MTH
Last Recalib on  : 26 Oct 95  02:06 PM               Sample Amount    : 0
Multiplier       : 1                                ISTD Amount      :
  
```

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0114.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.040	*	not found	*	1		Methane

Not all calibrated peaks were found



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 External Standard Report
 =====

a File Name	: C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0115.D	Page Number	: 1
Operator	: dmb	Vial Number	:
Instrument	: TELLER	Injection Number	:
Sample Name	: S-M18MOD-3	Sequence Line	:
Run Time Bar Code:		Instrument Method:	1095-18.MTH
Acquired on	: 26 Oct 95 03:04 PM	Analysis Method	: 1095-18A.MTH
Report Created on:	26 Oct 95 03:30 PM	Sample Amount	: 0
Last Recalib on	: 26 Oct 95 02:06 PM	ISTD Amount	:
Multiplier	: 1		

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0115.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.040	* not found *			1		Methane

Not all calibrated peaks were found

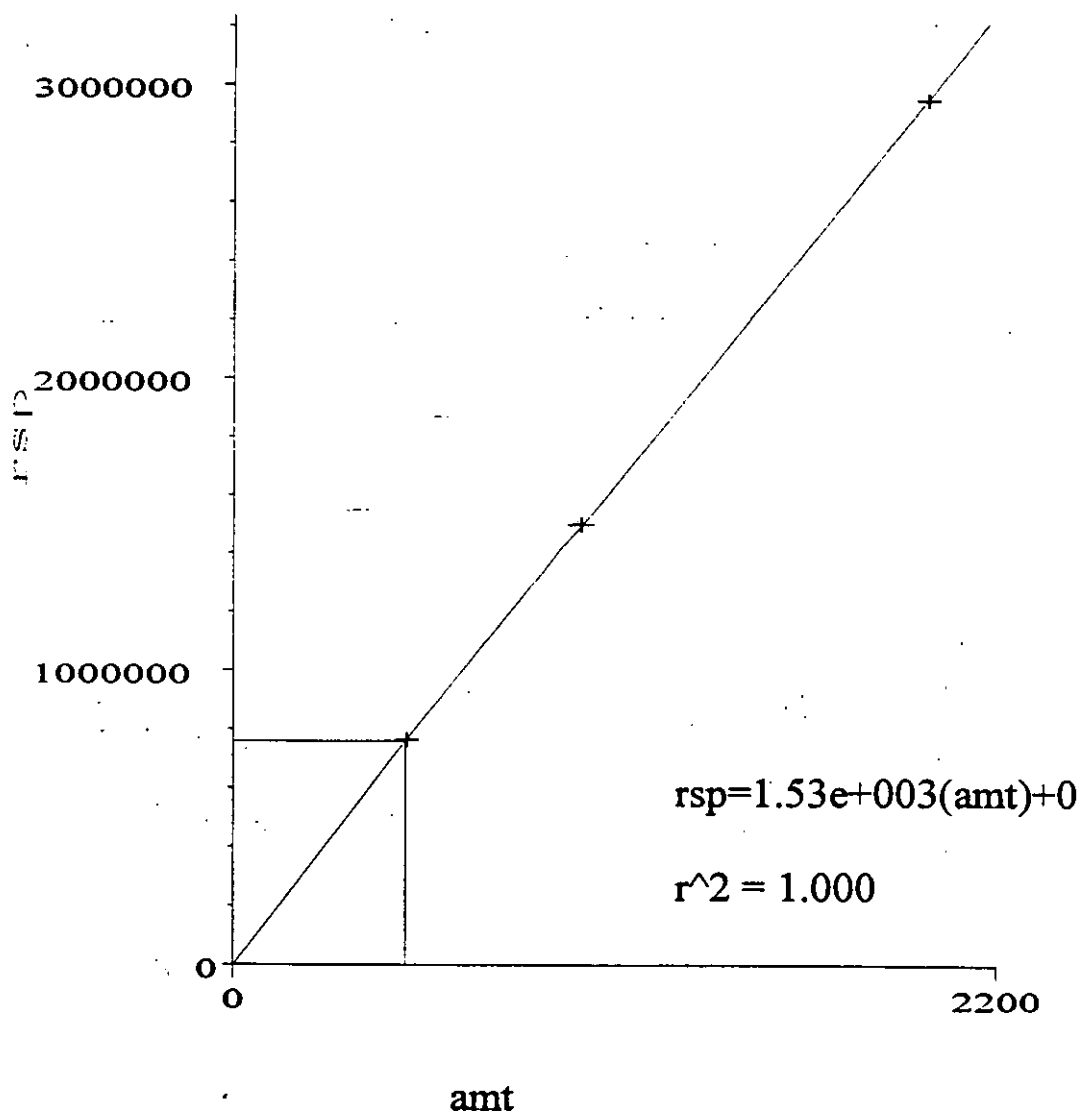
Curve # 1

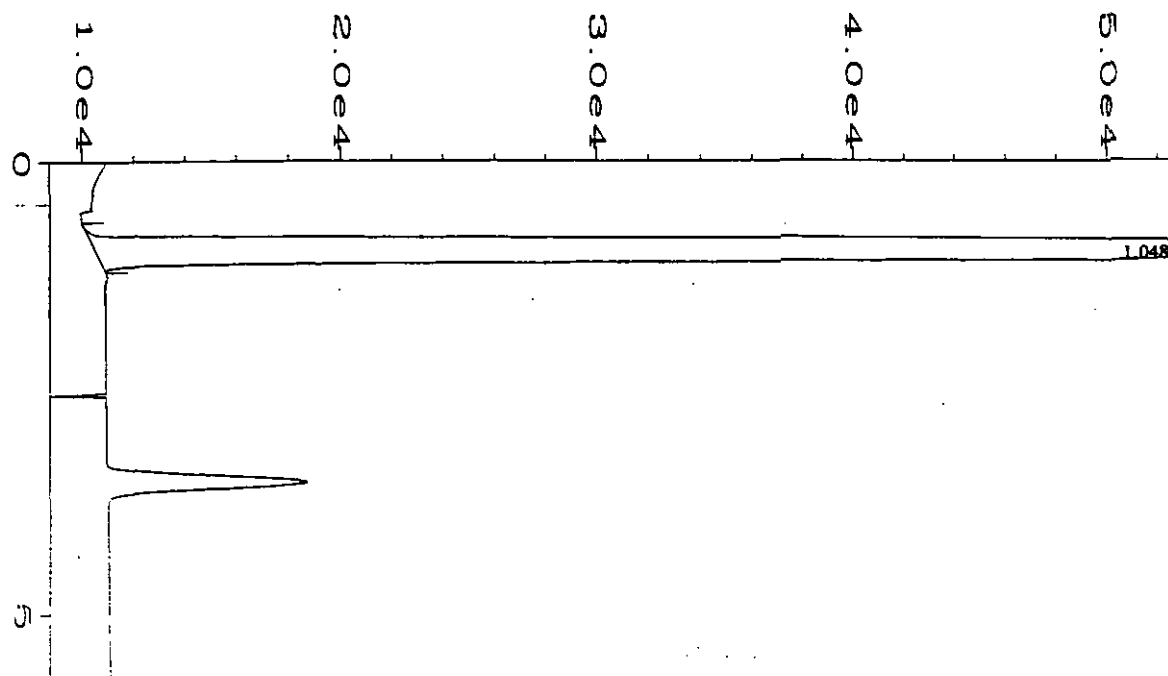


ENTHALPY analytical, inc.

Method Name	1095-18
Date	10/26/95
Directory	1095-18
Vial #	Concentration
04/05	2000
05/05	1000
08/09	500
RT = 1.05	

Methane





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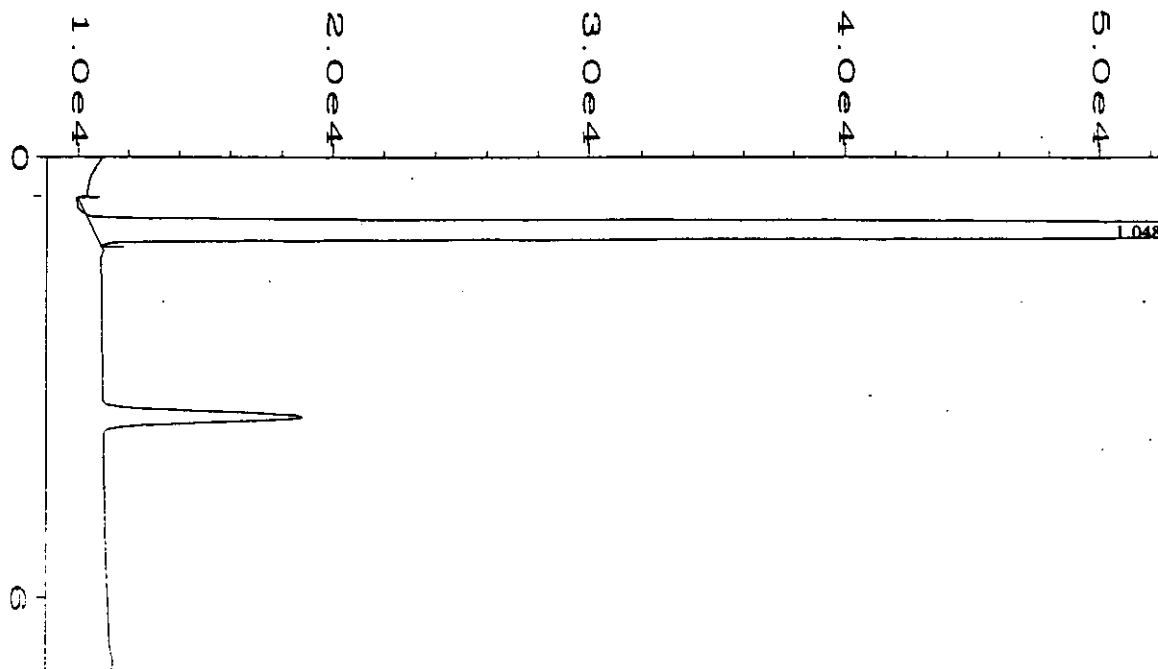
External Standard Report

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a File Name	: C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0109.D	
Operator	: dmb	Page Number : 1
Instrument	: TELLER	Vial Number :
Sample Name	: 500 ppm CH4	Injection Number :
Run Time Bar Code:		Sequence Line :
Acquired on	: 26 Oct 95 12:51 PM	Instrument Method: 1095-18.MTH
Report Created on:	26 Oct 95 02:07 PM	Analysis Method : 1095-18A.MTH
Last Recalib on	: 26 Oct 95 02:06 PM	Sample Amount : 0
Multiplier	: 1	ISTD Amount :

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0109.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.048	760818	BV	0.232	1	495.746	Methane



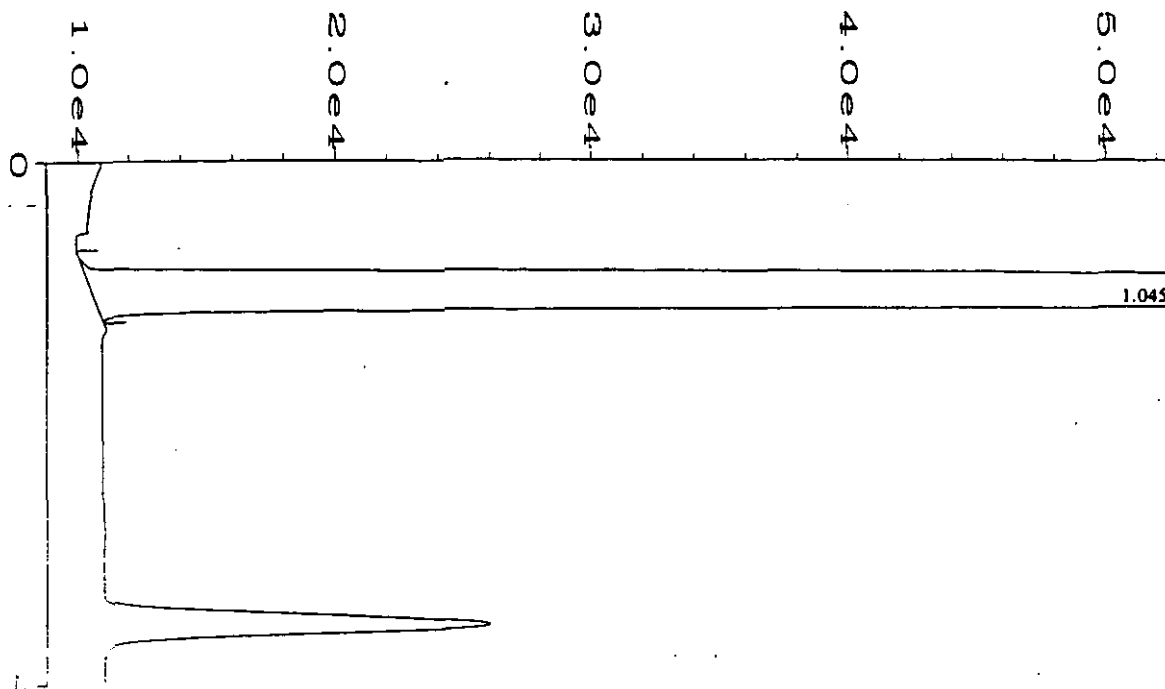
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 External Standard Report
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```

a File Name      : C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0108.D
Operator         : dmb                               Page Number      : 1
Instrument        : TELLER                           Vial Number       :
Sample Name       : 500 ppm CH4                      Injection Number  :
Run Time Bar Code:                               Sequence Line     :
Acquired on      : 26 Oct 95  12:42 PM                Instrument Method: 1095-18.MTH
Report Created on: 26 Oct 95  02:07 PM                Analysis Method   : 1095-18A.MTH
Last Recalib on  : 26 Oct 95  02:06 PM                Sample Amount    : 0
Multiplier       : 1                                ISTD Amount      :
  
```

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0108.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.048	765476	BV	0.231	1	498.781	Methane



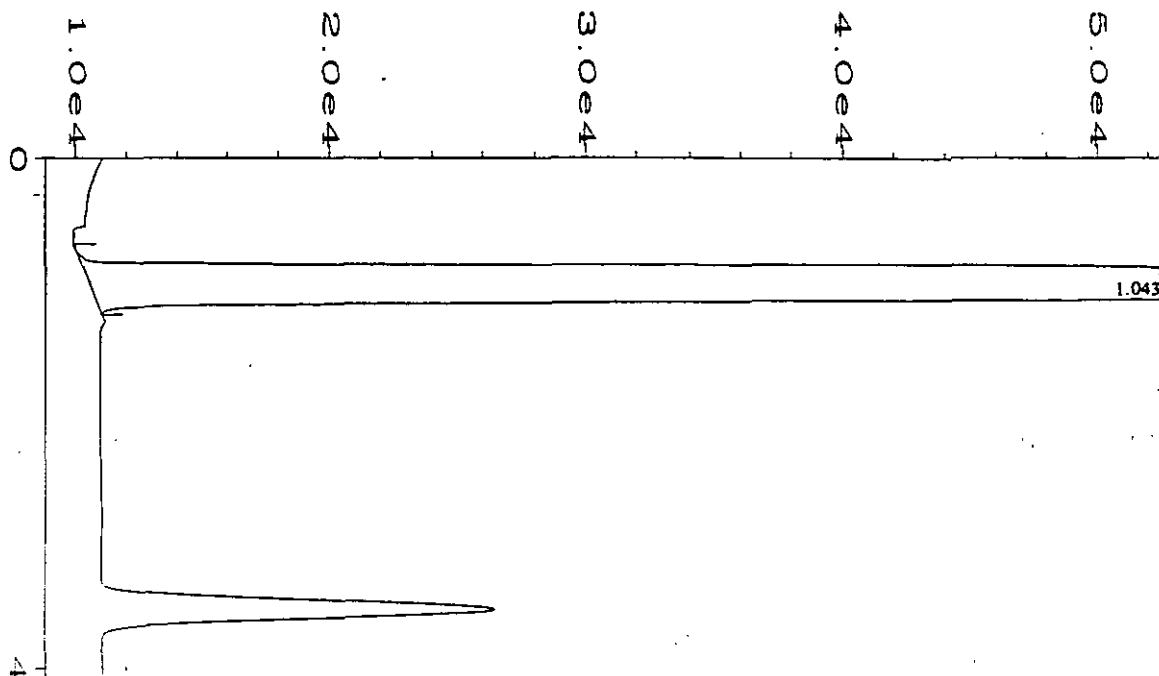
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 External Standard Report
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```

a File Name      : C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0107.D
Operator         : dmb                               Page Number      : 1
Instrument        : TELLER                           Vial Number       :
Sample Name       : 2000 ppm CH4                     Injection Number  :
Run Time Bar Code:                               Sequence Line    :
Acquired on      : 26 Oct 95  12:36 PM                Instrument Method: 1095-18.MTH
Report Created on: 26 Oct 95  02:07 PM                Analysis Method  : 1095-18A.MTH
Last Recalib on  : 26 Oct 95  02:06 PM                Sample Amount    : 0
Multiplier       : 1                                ISTD Amount      :
  
```

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0107.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.045	1487478	BV	0.232	1	996.145	Methane



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 External Standard Report
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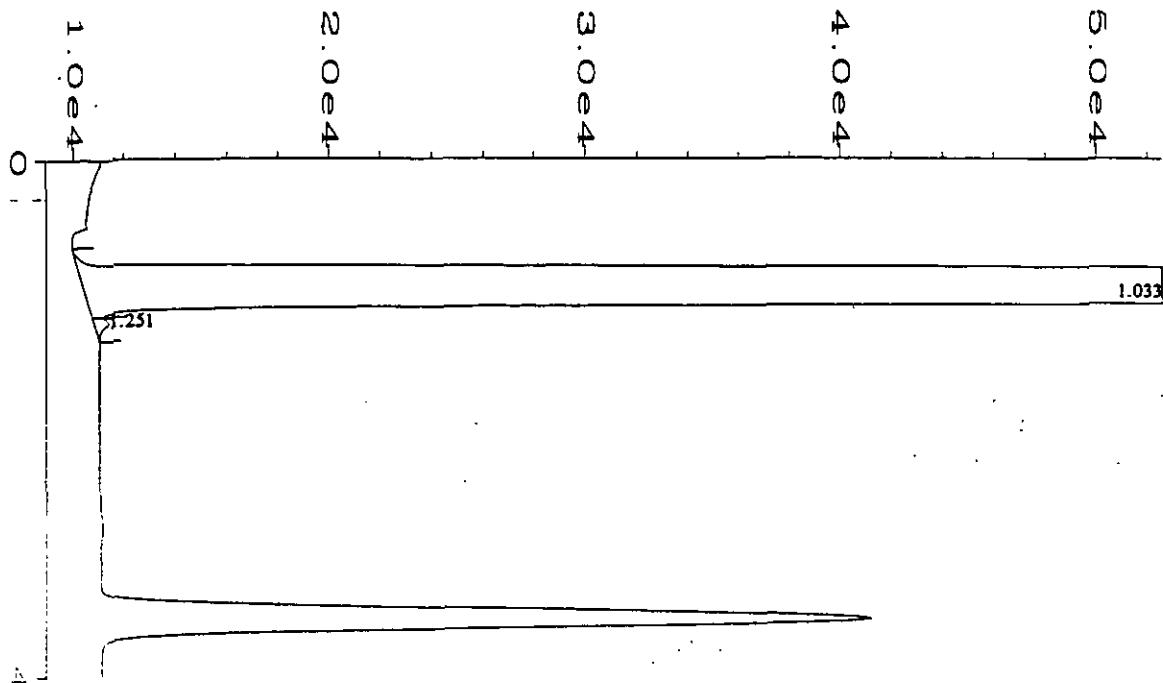
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a File Name      : C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0106.D
Operator         : dmb                               Page Number      : 1
Instrument        : TELLER                           Vial Number       :
Sample Name       : 2000 ppm CH4                     Injection Number  :
Run Time Bar Code:                               Sequence Line     :
Acquired on      : 26 Oct 95  12:30 PM               Instrument Method: 1095-18.MTH
Report Created on: 26 Oct 95  02:07 PM               Analysis Method  : 1095-18A.MTH
Last Recalib on  : 26 Oct 95  02:06 PM               Sample Amount    : 0
Multiplier       : 1                                ISTD Amount      :
  
```

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0106.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.043	1511267	BV	0.232	1	1012.536	Methane

=====



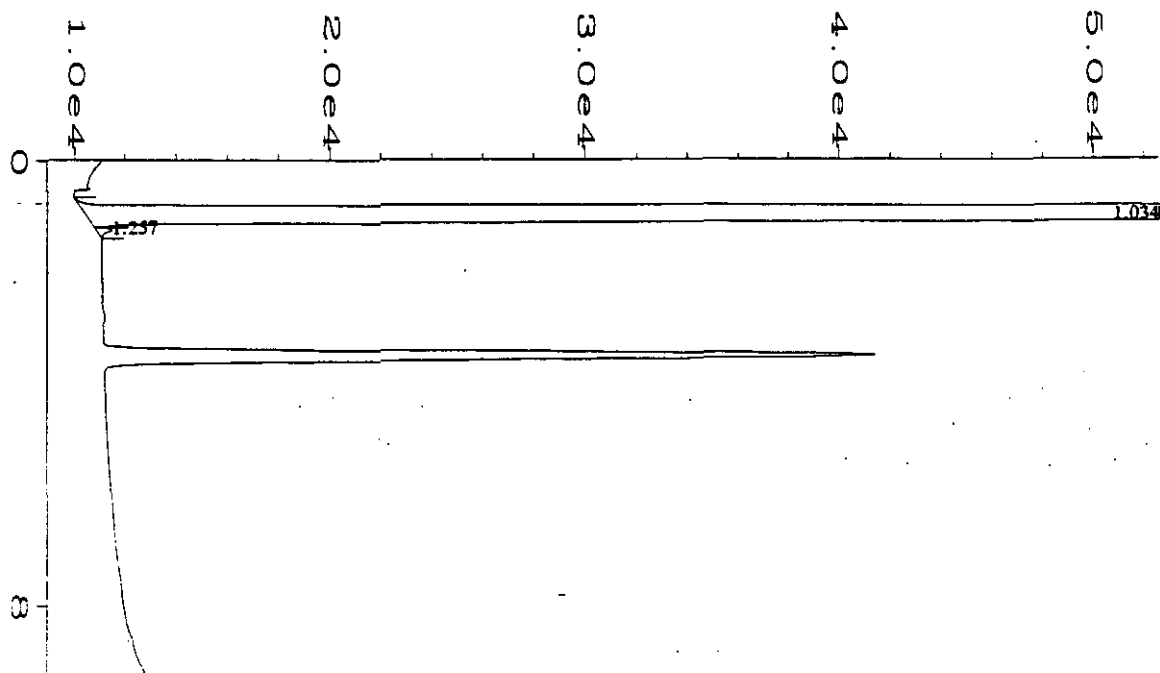
External Standard Report

```

a File Name      : C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0105.D
Operator         : dmb                               Page Number      : 1
Instrument       : TELLER                           Vial Number       :
Sample Name     : 2000 ppm CH4                      Injection Number  :
Run Time Bar Code:                               Sequence Line    :
Acquired on     : 26 Oct 95 12:24 PM                Instrument Method: 1095-18.MTH
Report Created on: 26 Oct 95 02:07 PM                Analysis Method  : 1095-18A.MTH
Last Recalib on : 26 Oct 95 02:06 PM                Sample Amount    : 0
Multiplier      : 1                                ISTD Amount      :
  
```

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0105.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.033	2906199	BV	0.234	1	1973.596	Methane



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 External Standard Report
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```

a File Name      : C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0104.D
Operator         : dmb                               Page Number      : 1
Instrument        : TELLER                           Vial Number       :
Sample Name       : 2000 ppm CH4                     Injection Number  :
Run Time Bar Code:                               Sequence Line    :
Acquired on      : 26 Oct 95 12:13 PM                Instrument Method: 1095-18.MTH
Report Created on: 26 Oct 95 02:08 PM                Analysis Method  : 1095-18A.MTH
Last Recalib on  : 26 Oct 95 02:06 PM                Sample Amount    : 0
Multiplier       : 1                                ISTD Amount      :
  
```

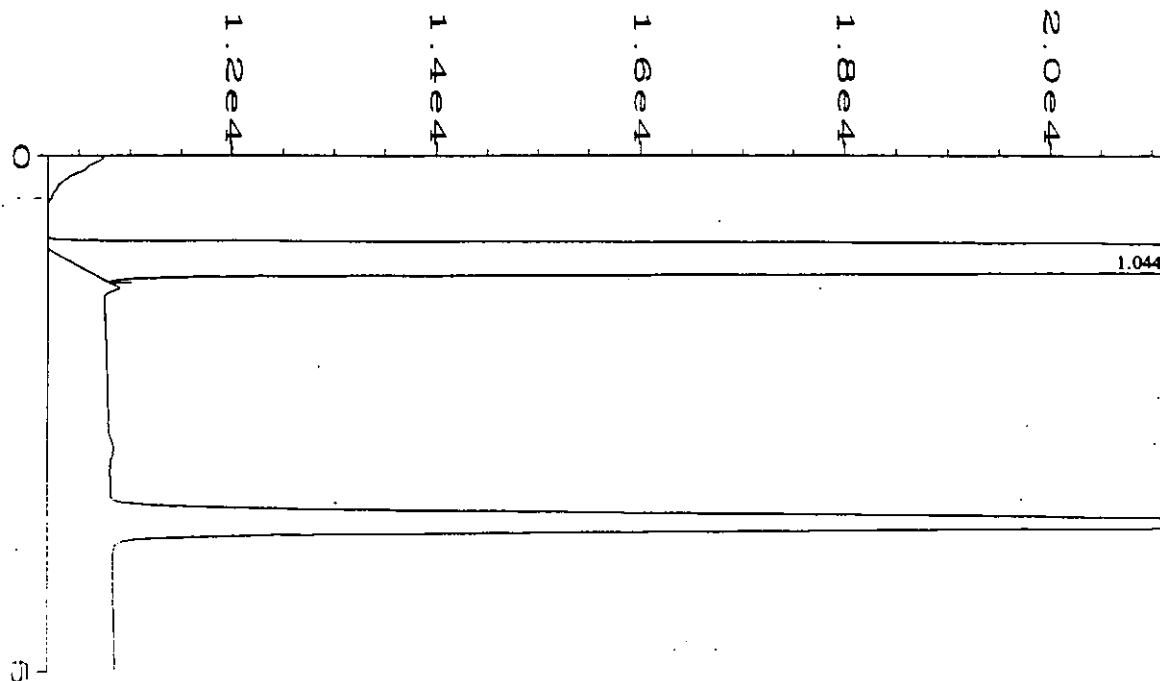
Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0104.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.034	2978648	BV	0.233	1	2023.511	Methane

QA Standards (10 %)



ENTHALPY analytical, inc.

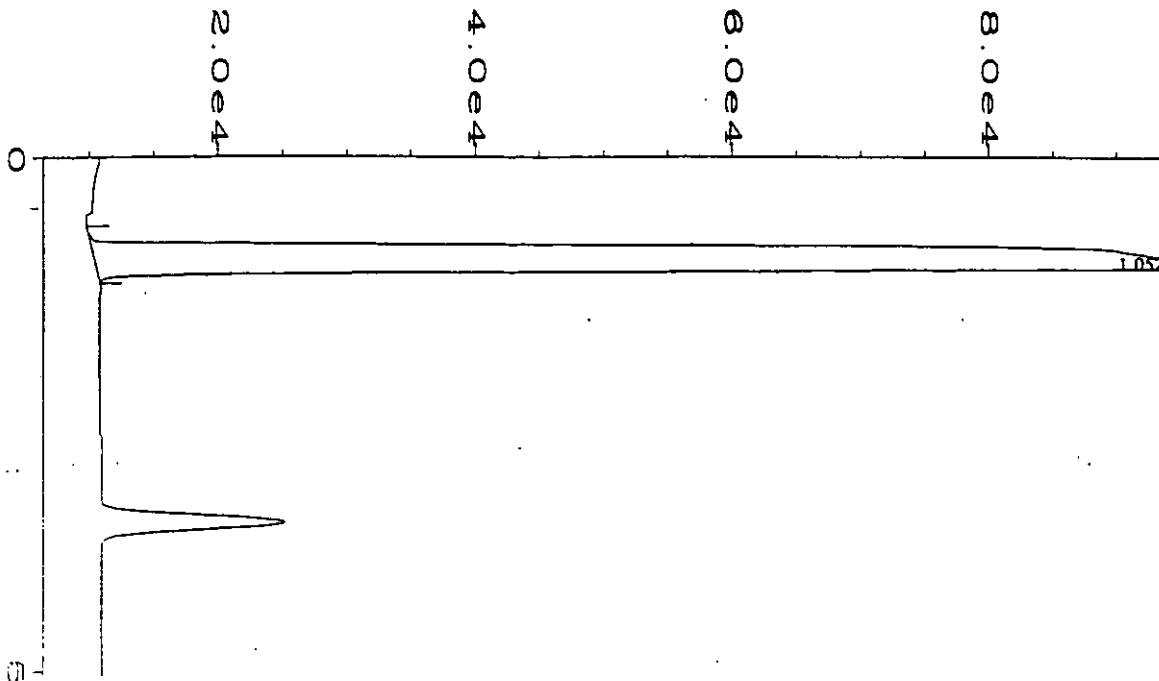


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 External Standard Report
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a File Name	: C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0116.D	
Operator	: dmb	Page Number : 1
Instrument	: TELLER	Vial Number :
Sample Name	: 1000 PPM CH4	Injection Number :
Run Time Bar Code:		Sequence Line :
Acquired on	: 26 Oct 95 03:23 PM	Instrument Method: 1095-18.MTH
Report Created on:	26 Oct 95 03:30 PM	Analysis Method : 1095-18A.MTH
Last Recalib on	: 26 Oct 95 02:06 PM	Sample Amount : 0
Multiplier	: 1	ISTD Amount :

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0116.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.044	1325485	BV	0.232	1	884.538	Methane



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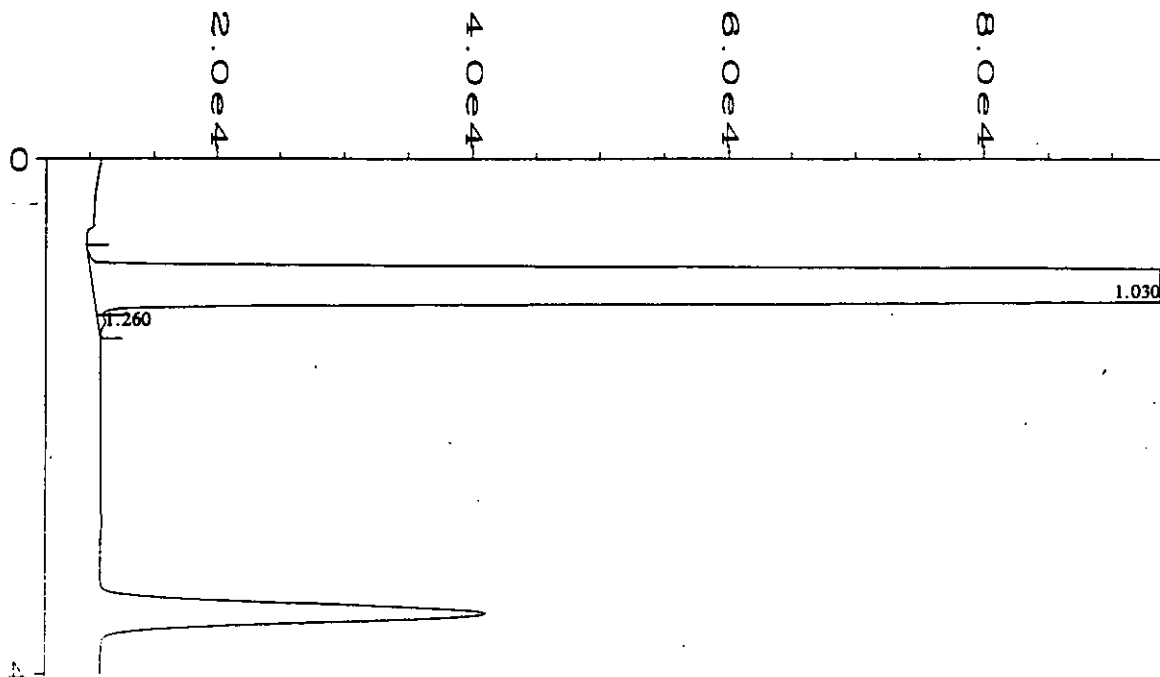
External Standard Report

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Operator	: dmb	Page Number : 1
Instrument	: TELLER	Vial Number :
Sample Name	: 1000 PPM CH4	Injection Number :
Run Time Bar Code:		Sequence Line :
Acquired on	: 26 Oct 95 03:29 PM	Instrument Method: 1095-18.MTH
Report Created on:	26 Oct 95 03:35 PM	Analysis Method : 1095-18A.MTH
Last Recalib on	: 26 Oct 95 02:06 PM	Sample Amount : 0
Multiplier	: 1	ISTD Amount :

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0117.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.052	1298972	BV	0.230	1	866.272	Methane



External Standard Report

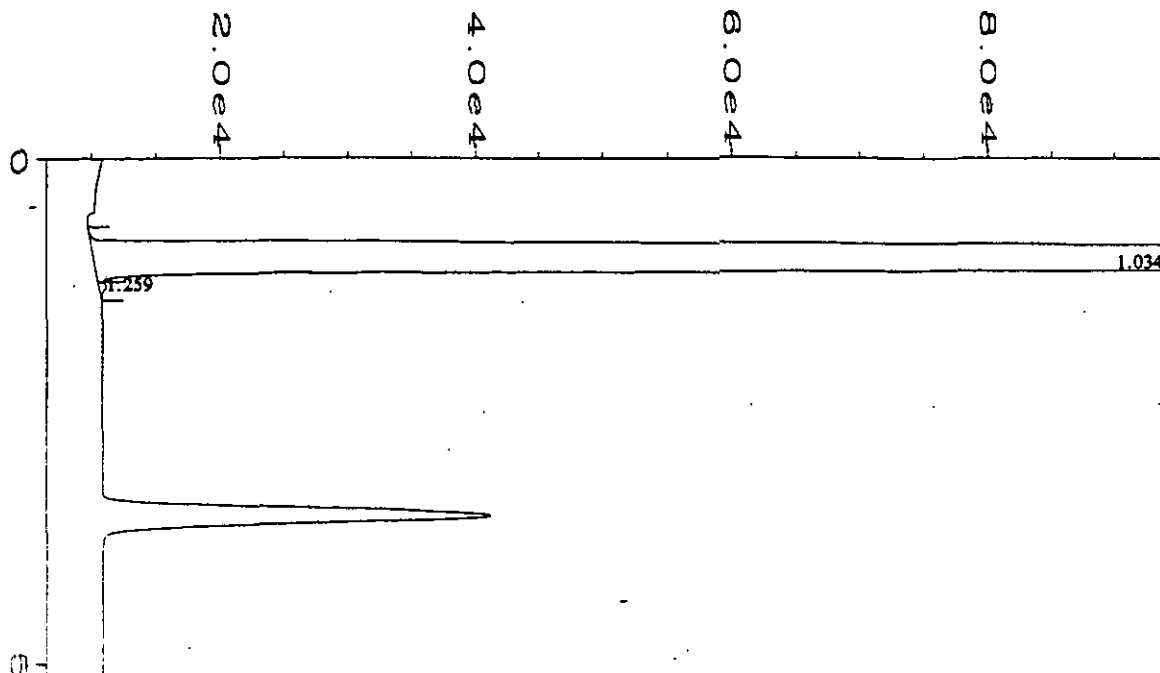
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Operator          : dmb                               Page Number       : 1
Instrument        : TELLER                             Vial Number          :
Sample Name       : 2000 PPM CH4                       Injection Number     :
Run Time Bar Code:                                     Sequence Line        :
Acquired on       : 26 Oct 95  03:37 PM                 Instrument Method    : 1095-18.MTH
Report Created on : 26 Oct 95  03:41 PM                 Analysis Method      : 1095-18A.MTH
Last Recalib on  : 26 Oct 95  02:06 PM                 Sample Amount        : 0
Multiplier        : 1                                   ISTD Amount          :
=====

```

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0118.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.030	2975280	BV	0.234	1	2021.190	Methane



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External Standard Report

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a File Name	: C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0119.D	
Operator	: dmb	Page Number : 1
Instrument	: TELLER	Vial Number :
Sample Name	: 2000 PPM CH4	Injection Number :
Run Time Bar Code:		Sequence Line :
Acquired on	: 26 Oct 95 03:43 PM	Instrument Method: 1095-18.MTH
Report Created on:	26 Oct 95 03:48 PM	Analysis Method : 1095-18A.MTH
Last Recalib on	: 26 Oct 95 02:06 PM	Sample Amount : 0
Multiplier	: 1	ISTD Amount :

Sig. 1 in C:\HPCHEM\1\DATA\OCT95\1095-18\NV-F0119.D

Ret Time	Area	Type	Width	Ref#	ppmv	Name
1.034	2993951	BV	0.208	1	2034.054	Methane

Tank Samples

Methyl chloride was quantified using a modification of EPA Method 18. This procedure is based upon the Evacuated Flask Procedure; however, instead of using a flask, a stainless steel canister was used. Prior to the field mobilization, all numbered canisters were first leak-tested (pressurized and allowed to stand for 24 hours), then analyzed by GC/FID to certify a less than 1.0 ppm concentration of total organic constituents. Upon completion of sample collection, the tanks were be transported from the site, under sample custody, to Enthalpy Analytical, Inc. for analysis. At the lab, the initial tank vacuum, barometric pressure, and temperature were measured and recorded. The tanks were then pressurized to ~ 600 mmHg and the final tank pressure measured and recorded. These initial and final tank pressures, barometric pressure, and temperature recordings are used to convert the "as analyzed" concentrations to "as sampled" concentrations using a dilution factor which is calculated based: on the following formula

$$\frac{(\text{Final mmHg} + (\text{Pbar} \cdot 25.401))}{(\text{Initial mmHg} + (\text{Pbar} \cdot 25.401))} \cdot \frac{(\text{Temp. Initial} + 460)}{(\text{Temp. Final} + 460)}$$

In the lab, all samples were introduced into the GC/FID using a heated VICI gas phase ten-port valve. Method 18 section 7.4.4 Quality Assurance criteria were met; including: duplicate injection of each sample aliquot with agreement of both injections to within 5% of the mean; three point calibration curves for methyl chloride (based on least squared regression analysis), calibration curves each day; and all calibration points agreed with the theoretical value within 10%.

Tube Samples

To determine the emissions of epichlorohydrin, octane, 1,3 dichloropropane, and octanol the adsorbent tube procedure of EPA Method 18 was used. Three chacoal tubes were placed in series. During sampling, moisture condensation was observed in the sample probe. The moisture was revovered into a zero headspace VOA vial at the end of the run. A disparger was placed in the probe for the second run. Again, the disparger contents were recovered into a zero headspace VOA vial at the end of the run. The water fractions were analyzed and added to the charcoal catches. The first charcoal tube was desorbed in carbon disulfide with 5%dimethyl formamide and analyzed by GC/FID. The second tube in series was split into two fractions and desorbed and analyzed in the same manner. The samples were analyzed on a Hewlett Packard Series II gas chromatograph coupled with a flame ionization detector. The compounds were separated using a Restek 60m x 0.53 RTX Volatiles capillary column. The quality assurance procedures are the same as mentioned above. Desorption efficiencies were determined for each compound by spiking charcoal tubes then processing them in the same manner as the samples. Catch weights are adjusted for desorption efficiency.

APPENDIX C. ANALYTICAL DATA

4. Particulate

Case Narrative
Triangle Laboratories, Inc.
801 Capitola Drive
Durham, NC 27713
Phone: (919) 544-5729
Fax: (919) 544-5491

Project Number: 34684

Date: October 31, 1995

Objective: Analysis of three filter and acetone rinse samples and one acetone blank sample for filterable particulate according to the guidelines of Method 5.

Three filter and acetone rinse samples were received on October 24, 1995 by Triangle Laboratories, Inc. in good condition. The acetone blank received with TLI project number 34683A was utilized for the acetone blank analysis with this project, also. The pre-tared filters and rinses were transferred to tared Teflon baggies and desiccated for a minimum of 24 hours. After this time period, each baggie was weighed using a Mettler AT 100 analytical balance. All weights were recorded to the nearest 0.1 milligram. Each baggie was then desiccated for at least an additional six hours and weighed again. The process was continued until two consecutive weights agreed within +/- 0.5 milligrams. Results reported relate only to the items tested.

The filterable particulate results are reported in units of milligrams (mg) and are the sum of the filter and rinse catches. The lowest weight obtained for each fraction was used in the calculations. Any particulate catch found in the acetone blank was adjusted based on the relative volume of the blank and sample.

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The data in this package has been judged to be valid according to the guidelines of Method 201A except as noted above. If there are questions about the data, please feel free to contact Project Scientist, Nancy Bragg at 919/544-8348.

For Triangle Laboratories, Inc.:

Report Preparation

Patricia C. Berkowitz
Patricia C. Berkowitz 10/31/95
Report Preparation Chemist

Quality Control

Jerry P. Roach 10/31/95
Jerry P. Roach
Report Preparation Chemist

The total number of pages in this data package is: 9

Entropy, Inc.

TLI Project: 34684

NSPS Method 5

Client Project: Triangle Brick 11990-1418-18
Matrix: Filters and FH-Acetone Rinses

Date Received: 10/24/95

TLI Number:	TLI Blank #1	108-90-1	108-90-2	108-90-3
Sample ID:		S-M5-1	S-M5-2	S-M5-3

Filter Tare Wt., g:	0.4633	0.4707	0.4491
Baggie Tare Wt., g:	3.3659	3.2786	3.2757
Raw Weight, g:	<u>3.8342</u>	<u>3.7515</u>	<u>3.7304</u>
FILTER SAMPLE WEIGHT, g:	0.0050	0.0022	0.0056

Sample ID:	Acetone Blank 108-89-4A	S-M5-1	S-M5-2	S-M5-3
------------	-------------------------	--------	--------	--------

Tare Wt., g:	3.2773	3.2852	3.1371	3.1689
Raw Weight, g:	<u>3.2778</u>	<u>3.2886</u>	<u>3.1420</u>	<u>3.1726</u>
RINSE SAMPLE WEIGHT, g:	0.0005	0.0034	0.0049	0.0037
Filter Catch, mg:		5.0	2.2	5.6
Rinse Catch, mg:	0.5	3.4	4.9	3.7
Rinse Blank Residue, mg:		0.3	0.2	0.2
Net Rinse Catch, mg:	<u>0.5</u>	<u>3.1</u>	<u>4.7</u>	<u>3.5</u>
Filterable Particulate, mg:	0.5	8.1	6.9	9.1

VISUAL ANALYSIS OF FILTERS

Color:		light brown	light brown	brown
Texture:		stain	stain	stain
Foreign Matter:		none	none	none
Rel. Comp.:		equal	equal	equal
Baggie Number:		421	423	425

VISUAL ANALYSIS OF RINSES

Color:	colorless	brown	light brown	brown
Texture:	n/a	stain	stain	stain
Foreign Matter:	none	none	glass	none
Rel. Comp.:	equal	equal	equal	equal
Volume, mL:	300	150	100	100
Fragments:	no	no	no	no
Baggie Number:	436	422	424	426

ENTROPY

Environmentalists, Inc.

P.O. Box 12291
Research Triangle Park
North Carolina 27709-2291
919-781-3550 FAX 919-787-8442

REQUEST FOR ANALYSIS

34684

PO#: 11990 - 14448-19

Customer Name: Withers and Ravenel
Triangle Brick

Laboratory: TLI

Date Transmitted: 10/24/95

Results Due By: 11/07/95

Sample Matrix: Method 5

PM: VJT

Analysis: Analyze samples for Particulate according to EPA Method 5.
Use Acetone Blank from Method 201A/202's.

(34683A) ^{JB}₁₀₋₂₄₋₉₅

Sample #	Sample ID	Components/Comments
1	S-M5-1	Acetone, Filter
2	S-M5-2	Acetone, Filter
3	S-M5-3	Acetone, Filter

Submitted By: 

203

3

SAMPLE TRANSFER RECORD OF CUSTODY

Please include this form with the final (typed) results, and whenever the final results are faxed to Entropy.

The samples referenced in Entropy Environmentalists Inc. RFA or purchase order No. 1199D-14448-18 were shipped by Entropy on 10/24/95 (date) via PERSONAL CUSTODY (mode) to TLI (laboratory) by Sean Deley (signature)

The samples were received for analysis on 10/24/95 (date) at Triong Le Labs (laboratory) by John Guenther (signature)

As applicable, note any broken seals, leakage, spillage, or damage to samples. If discrepancy, specify seal No., jar No., sample No., etc.

Custody Seal : Absent	Sample Seals: Absent	TLI Project Number : 34684	Book
Chain of Custody : Present		Client: EEI01	Entropy, Inc.
Sample Tags : Present		Date Received : 10/24/95	By <i>J. Smith</i>
Sample Tag Numbers: Listed			Page
SNO Forms : N/A			

Box	NO COOLANT	Carrier and Number : SEAN DALEY	90
-----	------------	---------------------------------	----

TLI Number	Client ID	Matrix Location	To LAB Date/Init	To STORAGE Date/Init	To LAB Date/Init	To STORAGE Date/Init	To LAB Date/Init	To STORAGE Date/Init	To LAB Date/Init	To STORAGE Date/Init
108-90-1A	S-M5-1	Filter								
		GRAV LAB								
108-90-1B	S-M5-1	FH Acetone Rinse								
		GRAV LAB								
108-90-2A	S-M5-2	Filter								
		GRAV LAB								
108-90-2B	S-M5-2	FH Acetone Rinse								
		GRAV LAB								
108-90-3A	S-M5-3	Filter								
		GRAV LAB								
108-90-3B	S-M5-3	FH Acetone Rinse								
		GRAV LAB								

Receiving Remarks:

Archive Remarks:

205

---TRIANGLE LABORATORIES, INC.--CHAIN OF CUSTODY--REVISED 02/17/95---

5

Custody Seal	: Absent	Sample Seals:	Absent	TLI Project Number	: 34683	Book	
Chain of Custody	: Present			Client:	EEIO1	Entropy, Inc.	108
Sample Tags	: Present			Date Received	10/24/95	By <i>A. Swerth</i>	Page
Sample Tag Numbers:	Listed						
SHO Forms	: N/A						
Box	NO COOLANT	Carrier and Number	SEAN DALEY				89

TLI Number	Matrix	To LAB	To STORAGE	To LAB	To STORAGE	To LAB	To STORAGE	To LAB	To STORAGE
MA/H:CPM	Client ID	Location	Date/Init	Date/Init	Date/Init	Date/Init	Date/Init	Date/Init	Date/Init
108-89-1A	FILTER								
S-M201A/202-1	GRAV LAB								
108-89-1B	FH/ACE								
S-M201A/202-1	GRAV LAB								
108-89-1C	BH/MECL2								
S-M201A/202-1	GRAV LAB								
108-89-1D	NOZ.ACE								
S-M201A/202-1	GRAV LAB								
108-89-1E	OI H2O								
S-M201A/202-1	GRAV LAB								
108-89-2A	FILTER								
S-M201A/202-2	GRAV LAB								
108-89-2B	FH/ACE								
S-M201A/202-2	GRAV LAB								
108-89-2C	BH/MECL2								
S-M201A/202-2	GRAV LAB								
108-89-2D	NOZ.ACE								
S-M201A/202-2	GRAV LAB								
108-89-2E	OI H2O								
S-M201A/202-2	GRAV LAB								

Receiving Remarks:

206

Archive Remarks:

-----TRIANGLE LABORATORIES, INC.--CHAIN OF CUSTODY--REVISED 02/17/95-----

Custody Seal : Absent		Sample Seals: Absent		TLI Project Number : 34683		Book	
Chain of Custody : Present				Client: EEI01		Entropy, Inc.	
Sample Tags : Present				Date Received		10/24/95	
Sample Tag Numbers: Listed				By <i>[Signature]</i>		Page	
SNO Forms : N/A				Carrier and Number : SEAN DALEY		89	

Box	NO COOLANT	Carrier and Number	SEAN DALEY	89					
TLI Number	Matrix	To LAB	To STORAGE	To LAB	To STORAGE	To LAB	To STORAGE	To LAB	To STORAGE
MR/H:CPM	Client ID	Location	Date/Init	Date/Init	Date/Init	Date/Init	Date/Init	Date/Init	Date/Init
108-89-3A	S-M201A/202-3	FILTER							
		GRAV LAB							
108-89-3B	S-M201A/202-3	FH/ACE							
		GRAV LAB							
108-89-3C	S-M201A/202-3	BH/MECL2							
		GRAV LAB							
108-89-3D	S-M201A/202-3	NOZ.ACE							
		GRAV LAB							
108-89-3E	S-M201A/202-3	DI H2O							
		GRAV LAB							
108-89-4A	BLANK	ACETONE							
		GRAV LAB							
108-89-4B	BLANK	MECL2							
		GRAV LAB							
108-89-4C	BLANK	DI H2O							
		GRAV LAB							
Receiving Remarks:									
207									
Archive Remarks:									
TRIANGLE LABORATORIES, INC.--CHAIN OF CUSTODY--REVISED 02/17/95--7									

TRIANGLE LABORATORIES, INC.

Gravimetrics Sample Tracking & Management Form

Project: 34684

Client: Entropy, Inc. (SEI01)

Sample Information

Method: 5Start Date: 10/25/95Temperature: 18.72 14 17Solvent/Acids: AcetoneLot: 953042Humidity: 41 53 41

Sample	TLI	CLIENT	Baggie	Filter	Solvent	Sample Weight
Sample ID	Sample ID	Sample ID	Weight	Number & Tare Weight	Volume	Sample Weight
#	crd		(g)	Number (g)	(mL)	(g)
000	TLI Blank #1					
	Acetone Blank 108-89-4A		3.2773	436	300	3.2776 3.2776
001	108-90-1A	S-M5-1	3.3659	421 0.4633		3.8342 3.8343
002	108-90-1B	S-M5-1	3.2852	422	150	3.2886 3.2886
003	108-90-2A	S-M5-2	3.2786	423 0.4707		3.7521 3.7515 3.7517
004	108-90-2B	S-M5-2	3.1371	424	100	3.1420 3.1420
005	108-90-3A	S-M5-3	3.2774	425 0.4491		3.7304 3.7304
006	108-90-3B	S-M5-3	3.1689	426	100	3.1726 3.1726

Comments:

① Redish Brown Residue sample #2, 4, and 6 have yellow or gold spots.

ERI01-Entropy, Inc.
S-M5-1
Project: 34684
108-90-1A

Qorpak

QORPAK®
CORPORATE ONE WEST
1195 WASHINGTON PIKE
BRIDGEVILLE, PA 15017-2851
412-257-3100 800-922-7551

SITE NAME	DATE
Triangle Brick	10/18/95
ANALYSIS	TIME
S-M5-1	14448
	PRESERVATIVE

LOT # 10/18/95



ERI01-Entropy, Inc.
S-M5-1
Project: 34684
108-90-1B

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CORPORATE ONE WEST
1195 WASHINGTON PIKE
BRIDGEVILLE, PA 15017-2851
412-257-3100 800-922-7551

SITE NAME	DATE
Triangle Brick	10/18/95
ANALYSIS	TIME
S-M5-1	14448
	PRESERVATIVE

LOT # 10/18/95

ERI01-Entropy, Inc.
S-M5-2
Project: 34684
108-90-2A

Qorpak

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1195 WASHINGTON PIKE
BRIDGEVILLE, PA 15017-2851
412-257-3100 800-922-7551

SITE NAME	DATE
Triangle Brick	10/18/95
ANALYSIS	TIME
S-M5-2	14448
	PRESERVATIVE

LOT # Filter

SPECIALLY CLEANED CONTAINER

ERI01-Entropy, Inc.
S-M5-2
Project: 34684
108-90-2B

PLANT: Triangle Brick
JOB #: 14448 DATE: 10/18/95

RUN #: S-M5-2

Front 1/2 Rinse w/ Ace.

MARK LIQ
IF APPL.

ERI01-Entropy, Inc.
S-M5-3
Project: 34684
108-90-3A

Qorpak

QORPAK®
CORPORATE ONE WEST
1195 WASHINGTON PIKE
BRIDGEVILLE, PA 15017-2851
412-257-3100 800-922-7551

SITE NAME	DATE
Triangle Brick	10/18/95
ANALYSIS	TIME
S-M5-3	14448
	PRESERVATIVE

LOT # 10/18/95



ERI01-Entropy, Inc.
S-M5-3
Project: 34684
108-90-3B

PLANT: Triangle Brick
JOB #: 14448 DATE: 10/18/95

RUN #: S-M5-3

Front 1/2 Rinse w/ Acetone

MARK LIQUID LEVEL ON LABEL
IF APPLICABLE

APPENDIX C. ANALYTICAL DATA

5. Particulate ≤ 10 Microns

Case Narrative
Triangle Laboratories, Inc.
801 Capitola Drive
Durham, NC 27713
Phone: (919) 544-5729
Fax: (919) 544-5491

Project Number: 34683A

Date: October 31, 1995

Objective: Analysis of three filter, acetone rinse and nozzle & cyclone rinse samples and one acetone blank sample for filterable particulate according to the guidelines of Method 201A.

Three filter, acetone rinse, and nozzle & cyclone rinse samples and one blank were received on October 24, 1995 by Triangle Laboratories, Inc. in good condition. The pre-tared filters and rinses were transferred to tared Teflon baggies and desiccated for a minimum of 24 hours. After this time period, each baggie was weighed using a Mettler AT 100 analytical balance. All weights were recorded to the nearest 0.1 milligram. Each baggie was then desiccated for at least an additional six hours and weighed again. The process was continued until two consecutive weights agreed within +/- 0.5 milligrams. Results reported relate only to the items tested.

The filterable particulate results are reported in units of milligrams (mg) and are the sum of the filter and rinse catches. The lowest weight obtained for each fraction was used in the calculations. Any particulate catch found in the acetone blank was adjusted based on the relative volume of the blank and sample.

The filter and acetone rinse results are reported for particles ≤ 10 micrograms (μg). The nozzle/cyclone rinse results are reported for particles $> 10 \mu\text{g}$.

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The data in this package has been judged to be valid according to the guidelines of Method 201A except as noted above. If there are questions about the data, please feel free to contact Project Scientist, Nancy Bragg at 919/544-8348.

For Triangle Laboratories, Inc.:

Report Preparation

Patricia C. Berkowitz
Patricia C. Berkowitz 10/31/95
Report Preparation Chemist

Quality Control

Jerry P. Roach 10/31/95
Jerry P. Roach
Report Preparation Chemist

The total number of pages in this data package is: 10

Entropy, Inc.

TLI Project: 34683-A

NSPS Method 201A

Client Project: Triangle Brick 11989-14448-18
Matrix: Filters, Acetone, Nozzle/Cyclone

Date Received: 10/24/95

TLI Number: TLI Blank #1 108-89-1 108-89-1 ~~108-89-1~~ 108-89-2

Sample ID: S-M201A/202-1 S-M201A/202-2

Filter Tare Wt., g:	0.4757	0.4700
Baggie Tare Wt., g:	3.3184	3.2853
Raw Weight, g:	<u>3.7976</u>	<u>3.7582</u>

FILTER SAMPLE WEIGHT, g:	0.0035	0.0029
--------------------------	--------	--------

Sample ID: Acetone Blank 108-89-4A S-M201A/202-1 S-M201A/202-2

Tare Wt., g:	3.2773	3.8711	3.4408	3.2660
Raw Weight, g:	<u>3.2778</u>	<u>3.8760</u>	<u>3.4438</u>	<u>3.2701</u>

RINSE SAMPLE WEIGHT, g:	0.0005	0.0049	0.0030	0.0041
-------------------------	--------	--------	--------	--------

Filter Catch, mg:		3.5		2.9
Rinse Catch, mg:	0.5	4.9	3.0	4.1
Rinse Blank Residue, mg:		0.3	0.2	0.3
Net Rinse Catch, mg:	<u>0.5</u>	<u>4.6</u>	<u>2.8</u>	<u>3.8</u>

Filterable Particulate, mg:	0.5	8.1	2.8	6.7
Size:	n/a	≤10μm	>10μm	≤10μm

VISUAL ANALYSIS OF FILTERS

Color:	Light brown	Light brown
Texture:	stain	stain
Foreign Matter:	none	none
Rel. Comp.:	equal	equal
Baggie Number:	427	430

VISUAL ANALYSIS OF RINSES

Color:	colorless	brown	redish brown	brown
Texture:	n/a	stain	stain	stain
Foreign Matter:	none	none	none	none
Rel. Comp.:	equal	equal	equal	equal
Volume, mL:	300	170	100	150
Fragments:	no	no	no	no
Baggie Number:	436	428	429	431

Entropy, Inc.

TLI Project: 34683-A

NSPS Method 201A

Client Project: Triangle Brick 11989-14448-18
Matrix: Filters, Acetone, Nozzle/Cyclone

Date Received: 10/24/95

TLI Number: 108-89-20 D 572 108-89-3 108-89-30 D 572 3145

Sample ID: S-M201A/202-3

Filter Tare Wt., g: 0.4520
Baggie Tare Wt., g: 3.2393
Raw Weight, g: 3.6959

FILTER SAMPLE WEIGHT, g: 0.0046

Sample ID: S-M201A/202-2 S-M201A/202-3 S-M201A/202-3

Tare Wt., g: 3.4533 3.3887 3.3892
Raw Weight, g: 3.4557 3.3918 3.3916

RINSE SAMPLE WEIGHT, g: 0.0024 0.0031 0.0024

Filter Catch, mg: 4.6
Rinse Catch, mg: 2.4 3.1 2.4
Rinse Blank Residue, mg: 0.1 0.3 0.1
Net Rinse Catch, mg: 2.3 2.8 2.3

Filterable Particulate, mg: 2.3 7.4 2.3
Size: >10µm ≤10µm >10µm

VISUAL ANALYSIS OF FILTERS

Color: Light brown
Texture: stain
Foreign Matter: none
Rel. Comp.: equal
Baggie Number: 433

VISUAL ANALYSIS OF RINSES

Color: redish brown brwon redish brown
Texture: stain stain stain
Foreign Matter: none none none
Rel. Comp.: equal equal equal
Volume, mL: 55 180 50
Fragments: no no no
Baggie Number: 432 434 435

ENTROPY

Environmentalists, Inc.

P.O. Box 12291
Research Triangle Park
North Carolina 27709-2291
919-781-3550 FAX 919-787-8442

REQUEST FOR ANALYSIS

34683A

PO#: 11989 - 14448-18

Customer Name: Withers and Ravenel
Triangle Brick

Laboratory: TLI

Date Transmitted: 10/24/95

Results Due By: 11/07/95

Sample Matrix: Method 201A

PM: VJT

Analysis: Analyze samples for PM10 Particulate according to EPA Method 201A, and Condensibles according to EPA Method 202.

Sample #	Sample ID	Components/Comments
1	S-M201A/202-1	DI H2O, MeCl2, Fl/2 Ace, Noz.Ace, Filter
2	S-M201A/202-2	DI H2O, MeCl2, Fl/2 Ace, Noz.Ace, Filter
3	S-M201A/202-3	DI H2O, MeCl2, Fl/2 Ace, Noz.Ace, Filter
4	Blanks	DI H2O, MeCl2, Acetone

216

Submitted By: 

4

SAMPLE TRANSFER RECORD OF CUSTODY

Please include this form with the final (typed) results, and whenever the final results are faxed to Entropy.

The samples referenced in Entropy Environmentalists Inc. RFA or purchase order No. 11989-14448-18 were shipped by Entropy on 10/24/95 (date) via PERSONAL CUSTODY (mode) to TLI (laboratory) by Sean Delery (signature)

The samples were received for analysis on 10/24/95 (date) at Triangle Labs (laboratory) by John G. Smith (signature)

As applicable, note any broken seals, leakage, spillage, or damage to samples. If discrepancy, specify seal No., jar No., sample No., etc.

Custody Seal	: Absent	Sample Seals: Absent	TLI Project Number	: 34683	Book
Chain of Custody	: Present		Client: EEI01	Entropy, Inc.	108
Sample Tags	: Present		Date Received	10/24/95	By <i>J. Swentke</i> Page
Sample Tag Numbers	: Listed				
SND Forms	: N/A				
Box	NO COOLANT	Carrier and Number	SEAN DALEY		89
TLI Number	Matrix	To LAB	To STORAGE	To LAB	To STORAGE
MR/H:CPM	Client ID	Location	Date/Init	Date/Init	Date/Init
108-89-1A	S-M201A/202-1	FILTER			
		GRAY LAB			
108-89-1B	S-M201A/202-1	FH/ACE			
		GRAY LAB			
108-89-1C	S-M201A/202-1	BH/NECL2			
		GRAY LAB			
108-89-1D	S-M201A/202-1	NOZ.ACE			
		GRAY LAB			
108-89-1E	S-M201A/202-1	DI H2O			
		GRAY LAB			
108-89-2A	S-M201A/202-2	FILTER			
		GRAY LAB			
108-89-2B	S-M201A/202-2	FH/ACE			
		GRAY LAB			
108-89-2C	S-M201A/202-2	BH/NECL2			
		GRAY LAB			
108-89-2D	S-M201A/202-2	NOZ.ACE			
		GRAY LAB			
108-89-2E	S-M201A/202-2	DI H2O			
		GRAY LAB			
Receiving Remarks:					
218					
Archive Remarks:					

Custody Seal : Absent		Sample Seals: Absent		TLI Project Number : 34683		Book	
Chain of Custody : Present							
Sample Tags : Present				Client: EE101		Entropy, Inc.	
Sample Tag Numbers: Listed						108	
SMD Forms : N/A				Date Received : 10/24/95		By <i>[Signature]</i> Page	
Box		NO COOLANT		Carrier and Number : SEAN DALEY		89	

TLI Number	Client ID	Matrix Location	To LAB Date/Init	To STORAGE Date/Init	To LAB Date/Init	To STORAGE Date/Init	To LAB Date/Init	To STORAGE Date/Init	To LAB Date/Init	To STORAGE Date/Init
108-89-3A	S-M201A/202-3	FILTER								
		GRAY LAB								
108-89-3B	S-M201A/202-3	FH/ACE								
		GRAY LAB								
108-89-3C	S-M201A/202-3	BH/MECL2								
		GRAY LAB								
108-89-3D	S-M201A/202-3	NOZ.ACE								
		GRAY LAB								
108-89-3E	S-M201A/202-3	DI H2O								
		GRAY LAB								
108-89-4A	BLANK	ACETONE								
		GRAY LAB								
108-89-4B	BLANK	MECL2								
		GRAY LAB								
108-89-4C	BLANK	DI H2O								
		GRAY LAB								
Receiving Remarks:										
219										
Archive Remarks:										
1										

TRIANGLE LABORATORIES, INC.
Gravimetrics Sample Tracking & Management Form

Project: 34683A

Client: Entropy, Inc. (EEI01)

Sample Information
Method: 201-A Start Date: 10/25/92 Temperature: 72 68 71
Solvent/Acids: Acetone Lot: 953042 Humidity: 48 49 31 33 41 72

	TLI	CLIENT	Weight	Baggie	Tare Weight	Volume	Sample Weight
[Sample]	SAMPLE ID		(g)	Number	(g)	(mL)	
[# crd]		SAMPLE ID					
[A]	TLI Blank #1						
[000]	Acetone Blank 108-89-4A	S-M201A/202-1	3.2773	436	300		3.2778 3.2778
[A]	108-89-1A	S-M201A/202-1	3.3184	427	0.4757		3.7977 3.7976
[A]	108-89-1B	S-M201A/202-1	3.8711	428	170		3.8761 3.8760
[A]	108-89-1D	S-M201A/202-1	3.4608	429	100		3.4438 3.4438
[A]	108-89-2A	S-M201A/202-2	3.2853	430	0.4700		3.7583 3.7582
[A]	108-89-2B	S-M201A/202-2	3.2666	431	150		3.2701 3.2703
[A]	108-89-2D	S-M201A/202-2	3.4533	432	55		3.4557 3.4561
[A]	108-89-3A	S-M201A/202-3	3.2393	433	0.4520		3.6959 3.6959
[A]	108-89-3B	S-M201A/202-3	3.3877	434	180		3.3918 3.3922
[A]	108-89-3D	S-M201A/202-3	3.3992	435	50		3.3916 3.3918

Comments:

220

8

EEI01-Entropy, Inc.
S-M201A/202-1
Project: 34683
108-89-1A

T6F 042

.4757

I-CHEM

CLIENT/SOURCE	☐ GRAB ☐ COMPOSITE OTHER:
SITE NAME	DATE
SAMPLE #	TIME
ANALYSIS	PRESERVATIVE
COLL BY	

EEI01-Entropy, Inc.
S-M201A/202-1
Project: 34683
108-89-1B

Qorpak
CORPAC*
CORPORATE ONE WAY
1195 WASHINGTON PI
BRIDGEVILLE, PA 150
412-257-3100 800-921

SITE NAME Triangle Brick	DATE 10/18/95
ANALYSIS S-M201A/202-1	TIME 1448 1449 PRESERVATIVE
LOTS Plant & Rinse	

EEI01-Entropy, Inc.
S-M201A/202-1
Project: 34683
108-89-1D

PLANT: Triangle Brick
JOB #: 1448
DATE: 10/18/95

RUN #: S-M201A/202-1

Nozzle & Cyclone
Rinse

MARK LIQUID LEVEL ON LABEL
IF APPLICABLE

EEI01-Entropy, Inc.
S-M201A/202-2
Project: 34683
108-89-2A

T6F 055

.4700

CHEM

SOURCE

SITE NAME	DATE
SAMPLE #	TIME
ANALYSIS	PRESERVATIVE
COLL BY	

EEI01-Entropy, Inc.
S-M201A/202-2
Project: 34683
108-89-2B

Qorpak
CORPAC*
CORPORATE ONE WAY
1195 WASHINGTON PI
BRIDGEVILLE, PA 150
412-257-3100 800-921

SITE NAME Triangle Brick	DATE 10/18/95
ANALYSIS S-M201A/202-2	TIME 1448 1449 PRESERVATIVE
LOTS Plant & Rinse	

EEI01-Entropy, Inc.
S-M201A/202-2
Project: 34683
108-89-2D

PLANT: Triangle Brick
JOB #: 1448
DATE: 10/18/95
RUN #: S-M201A/202-2

Nozzle & Cyclone
Rinse

EEI01-Entropy, Inc.
S-M201A/202-3
Project: 34683
108-89-3A

221

I-CHEM

CLIENT/SOURCE	DATE
SITE NAME	DATE
SAMPLE #	TIME
ANALYSIS	PRESERVATION

ERI01-Entropy, Inc.
S-M201A/202-3
Project: 34683
108-89-3B

Qorpak

QORPAC
CORPORATION ONE WEST
1195 WASHINGTON RD
BRIDGEVILLE, PA 15001
412-257-3700 800-755-3838

SITE NAME	DATE
ANALYSIS	DATE
LOT#	DATE

ERI01-Entropy, Inc.
S-M201A/202-3
Project: 34683
108-89-3D

PLANT: Triangle Brick
JOB #: 14448 DATE: 10/18/95
RUN #: 5-M201A/202-3
Nozzle & Cyclone
Rinse

MARK LIQUID
IF APPLICABLE

ERI01-Entropy, Inc.
BLANK
Project: 34683
108-89-4A

PLANT: Triangle Brick
JOB #: 14448 DATE: 10/18/95
RUN #: 5-M201A
Alcohol Reagent
Blank

APPENDIX D. CALIBRATION DATA

SAMPLING EQUIPMENT AUDIT

Client Withers and Ravenel
 Plant Triangle Brick Job No. 14448
 City/State Merry Oaks, NC Team Leader JPD
 Test Location Brick Kiln #2 Stack

BAROMETER		Barometer (Van) No. _____		Checked OK? (✓) _____		Shop Auditor _____	
Entropy In-House Ref. Barometer _____		°Hg		vs Van Barometer _____		°Hg	
Date Compared _____		Dev. _____		°Hg (Max. Allowable Dev.: ± 0.1 °Hg)			
Test Loc. Elevation Above Ground (Van) _____		Ft.		Date _____		Field Auditor _____	
Field Barometric Pressure Reduced for Test Location Elevation by _____ °Hg							

Ref. Therm. Initial Ambient Temp., °F _____	Allowable Deviation From Ambient _____	Date _____	Auditor _____	✓
		Ambient Temperature, °F _____		OK

THERMOMETERS

Dry Gas Meter	± 5.4 °F	_____	(Meterbox I.D. _____)	_____
Impinger Exit	± 2.0 °F	_____	_____	_____
Filter Box	± 5.4 °F	_____	_____	_____

THERMOCOUPLES

TC No. / °F	✓	TC No. / °F	✓	TC No. / °F	✓	TC No. / °F	✓	TC No. / °F	✓
_____	OK	_____	OK	_____	OK	_____	OK	_____	OK
(Including Temp. Change and Direction)		(Including Temp. Change and Direction)		(Including Temp. Change and Direction)		(Including Temp. Change and Direction)		(Including Temp. Change and Direction)	
Auditor _____		Auditor _____		Auditor _____		Auditor _____		Auditor _____	

Allowable Deviation from Ambient: ± 8.0°F * (or ± 2.0°F) **
 * ± 8.0 °F = ± 1.5% of ambient absolute temperature.
 ** (± 2.0 °F if used in saturated or water droplet-laden gas stream.)

ISOKINETIC METERBOX

I.D. N-8 Gamma (Y) 0.9776 AHE 1.900

As Applicable (check): Zero Magnetics? ☒ Zero/Level Manometer? N/A

Barometric Pressure (Pbar) 30.12 Auditor J Date 10/16/95

Dry Gas Meter Reading (Cubic Ft.)	Meter Temperature (°F)	Lower and Upper Limits for Audit Gamma
Final <u>465.292</u>	Final <u>96</u>	0.96 • Y = <u>0.9384</u>
Initial <u>457.507</u>	Initial <u>94</u>	1.04 • Y = <u>1.0167</u>

Dry Gas Volume Metered (Cubic Ft.)	Average Meter Temp. (°F)	Run Time (Base = 10)	
Vm = <u>7.773</u>	Tm = <u>95</u>	(Minutes)	(Seconds)
		<u>10</u>	<u>0</u>

$$Y_c = \frac{(\frac{10}{7.773} + (\frac{0}{60}))}{\left[\frac{0.0319 (\frac{95}{30.12} + 460)}{30.12} \right]^{.5}} = \frac{0.9863}{\text{Audit Gamma}}$$

Audit Gamma Acceptable (between lower & upper limits)? (✓) Yes ☒ No _____

Ideal Sampling Rate = 0.75

225

Positive Pressure Leak Check OK? Yes _____ No _____

SAMPLING EQUIPMENT AUDIT

client Withers and Ravenel
 Plant Triangle Brick Job No. 14448
 City/State Merry Oaks, NC Team Leader JPD
 Test Location Brick Kiln #2 Stack

BAROMETER	
Barometer (Van) No. _____	Checked OK? (V) _____ Shop Auditor _____
Entropy In-House Ref. Barometer _____ "Hg	Van Barometer _____ "Hg
Date Compared _____	Dev. _____ "Hg (Max. Allowable Dev.: ± 0.1 "Hg)
Test Loc. Elevation Above Ground (Van) _____ Ft.	Date _____ Field Auditor _____
Field Barometric Pressure Reduced for Test Location Elevation by _____ "Hg	
Ref. Therm. Initial Ambient Temp., °F _____	Allowable Deviation From Ambient _____ Date _____ Auditor _____
	Ambient Temperature, °F _____ ☒ OK
THERMOMETERS	
Dry Gas Meter	± 5.4 °F _____ (Meterbox I.D. _____)
Impinger Exit	± 2.0 °F _____
Filter Box	± 5.4 °F _____
THERMOCOUPLES	
TC No. / °F ☒ OK	TC No. / °F ☒ OK
TC No. / °F ☒ OK	TC No. / °F ☒ OK
TC No. / °F ☒ OK	TC No. / °F ☒ OK
TC No. / °F ☒ OK	TC No. / °F ☒ OK
TC No. / °F ☒ OK	TC No. / °F ☒ OK
(Including Temp. Change and Direction)	(Including Temp. Change and Direction)
(Including Temp. Change and Direction)	(Including Temp. Change and Direction)
(Including Temp. Change and Direction)	(Including Temp. Change and Direction)
Auditor _____	Auditor _____
Auditor _____	Auditor _____
Auditor _____	Auditor _____
Allowable Deviation from Ambient: ± 8.0 °F * (or ± 2.0 °F) ** * ± 8.0 °F = $\pm 1.5\%$ of ambient absolute temperature. ** (± 2.0 °F if used in saturated or water droplet-laden gas stream.)	
ISOKINETIC METERBOX	
I.D. <u>N-14</u>	Gamma (Y) <u>1.0013</u> ΔH_e <u>1.928</u>
As Applicable (check): Zero Magnehelics? ☒	Zero/Level Manometer? <u>N/A</u>
Barometric Pressure (P _{bar}) <u>30.12</u>	Auditor <u>JPD</u> Date <u>10/16/95</u>
Dry Gas Meter Reading (Cubic Ft.)	Meter Temperature (°F)
Final <u>66.656</u>	Final <u>84</u>
Initial <u>58.982</u>	Initial <u>78</u>
Dry Gas Volume Metered (Cubic Ft.)	Average Meter Temp. (°F)
V _m = <u>7.674</u>	T _m = <u>81</u>
Lower and Upper Limits for Audit Gamma	
0.96 * Y = <u>0.9612</u>	
1.04 * Y = <u>1.0143</u>	
Run Time (Base = 10)	
(Minutes)	(Seconds)
<u>10</u>	<u>0</u>
$Y_c = \frac{(10 + (0 / 60))}{7.674} \cdot \left[\frac{0.0319 (81 + 460)}{30.12} \right]^{.5} = \frac{0.9863}{\text{Audit Gamma}}$	
Audit Gamma Acceptable (between lower & upper limits)? (V) Yes ☒ No _____	
Ideal Sampling Rate = 0.75	
Positive Pressure Leak Check OK? Yes _____ No _____	

NOZZLE CALIBRATION

NOZZLE NUMBER GLP714

[illegible]

Note: 1. All diameters measured in inches.
2. Maximum 0.004 inches from lowest to highest diameter.

R-0033 rev. 3-90

227

ENTROPY

NOZZLE NUMBER GLP 1447

Note: 1. All diameters measured in inches.
2. Maximum 0.004 inches from lowest to highest diameter.

228

NOZZLE NUMBER GLP1448

Note: 1. All diameters measured in inches.
2. Maximum 0.004 inches from lowest to highest diameter.

R-0033a rev. 3-91

ENTROPY

NOZZLE NUMBER GLP1449

Note: 1. All diameters measured in inches.
2. Maximum 0.004 inches from lowest to highest diameter.

ENTROPY

NOZZLE NUMBER: 1004

[illegible]

NOTE: All diameters measured in inches.

231

NOZZLE CALIBRATION

NOZZLE NUMBER 2004

[illegible]

Note: 1. All diameters measured in inches.

2. Maximum 0.004 inches from lowest to highest diameter.

R-0033a rev. 3-91

232

ENTROPY

NOZZLE NUMBER 3004

Note: 1. All diameters measured in inches.
2. Maximum 0.004 inches from lowest to highest diameter.

R-0033, rev. 3-91

STANDARD DRY GAS METER CALIBRATION

Meter Number 1017057

Date 10-5-94

Auditor(s) PS/mc

Barometric Press. (P_{bar}) 29.64

Spirometer		Dry Gas Meter			Time Min. (θ)	Aprox. Flow Rate cfm	Calc'd Flow Rate cfm (Q)	Meter Coeff. Gamma (Y _{ds})
Gas Volume Cubic Feet (V _s)	Temp. °F (t _s)	Gas Volume Cubic Feet (V _{ds})	Temp. °F (t _{ds})	Pressure In. H ₂ O (ΔP)				
2.823	71.6	2.793	64	-.34	10	.2793	.2777	.9972
2.714	↓	2.723	69	-.35	↓	.2723	.2669	.9927
2.687	↓	2.696	69.5	-.35	↓	.2696	.2642	.9925
5.009	75.2	5.103	74.5	-.795	↓	.5103	.4894	.9823
4.973	↓	5.113	76	-.795	↓	.5113	.4858	.9759
5.064	↓	5.106	76.5	-.795	↓	.5106	.4947	.9961
8.488	75.2	8.697	77	-1.7	↓	.8697	.8292	.9834
8.470	77	8.649	78	-1.7	↓	.8649	.8247	.9853
8.452	77	8.638	77.5	-1.7	↓	.8638	.8229	.9835
12.213	80.6	12.562	78	-3.4	↓	1.2562	1.1812	.9758
12.350	↓	12.592	↓	-3.4	↓	1.2592	1.1944	.9843
12.295	↓	12.583	↓	-3.4	↓	1.2583	1.1891	.9724
13.953	↓	14.286	↓	-4.2	↓	1.4286	1.3495	.9822
13.971	↓	14.305	↓	-4.2	↓	1.4305	1.3512	.9822
13.934	↓	14.262	↓	-4.2	↓	1.4262	1.3477	.9826
Average								.9846

$$Y_{ds} = \frac{(V_s) (t_{ds} + 460) (P_{bar})}{(V_{ds}) (t_s + 460) [P_{bar} + (\Delta P / 13.6)]}$$

$$Q = (17.64) \left[\frac{(P_b) (V_s)}{(t_s + 460) (\theta)} \right]$$

ISOKINETIC METERBOX FULLTEST CALIBRATION RESULTS

Meterbox No.: N8 Date: 10-11-95 Calibrated By: P. JUDD
 Standard Meter No: 1017057 Barometric Pressure, Pb, in. Hg: 29.74
 Standard Meter Coefficient, Yds: 0.9846 Meterbox Vacuum, in. Hg: 0

STANDARD METER

Gas Volume (Vds) cf	Temp. (tds) °F	Time (theta) Min.
4.977	71	13
4.937	71	13
5.268	71	7
5.264	71	7
9.186	71	8
5.722	71	5

METERBOX METERING SYSTEM

Orifice Setting (Delta H) In. H2O	Gas Volume (Vd) cf	Temp. (td) °F	Coeff. (Yd)	Delta H@ in. H2O @ 68°F
0.5	5.367	109.5	0.9780	1.867
0.5	5.386	113.5	0.9736	1.884
2	5.772	119	0.9750	1.901
2	5.824	122.5	0.9714	1.893
4.8	10.082	128.5	0.9826	1.928
4.8	6.313	133	0.9849	1.927

Average: 0.9776 1.900

$$Yd = \frac{Yds \cdot Vds \cdot (td + 460) \cdot Pb}{Vd \cdot (tds + 460) \cdot (Pb + (\text{delta H} / 13.6))}$$

$$\text{delta H@} = \frac{0.0319 \cdot \text{delta H}}{Pb \cdot (tds + 460)} \cdot \left[\frac{(td + 460) \cdot \text{theta}}{Yds \cdot Vds} \right]^2$$

ISOKINETIC METERBOX POSTTEST CALIBRATION RESULTS

Meterbox No.: N8 Date: 10/20/95 Calibrated By: P. JUDD
 Job Number: 14448 Plant: WITHERS
 Standard Meter No: 1017057 Barometric Pressure, Pb, In. Hg: 29.6
 Standard Meter Coefficient, Yds: 0.9846 Meterbox Vacuum, In. Hg: 2

STANDARD METER

Gas Volume (Vds) cf	Temp. (tds) °F	Time (theta) Min.
4.983	71	8
4.953	71	8
4.941	71	8

METERBOX METERING SYSTEM

Orifice Setting (Delta H) In. H2O	Gas Volume (Vd) cf	Temp. (td) °F	Coeff. (Yd)	Delta H@ in. H2O @ 68°F
1.3	5.241	87	0.9612	1.919
1.3	5.233	93.5	0.9683	1.919
1.3	5.242	99.5	0.9747	1.908

Average: 0.9681 1.915

Fulltest Yd: 0.9776

Date: 10/11/95

% Deviation*: -1.0%

* maximum allowed deviation = ±5%

$$Yd = \frac{Yds \cdot Vds \cdot (td + 460) \cdot Pb}{Vd \cdot (tds + 460) \cdot (Pb + (\text{delta H} / 13.6))}$$

$$\text{delta H@} = \frac{0.0319 \cdot \text{delta H}}{Pb \cdot (tds + 460)} \cdot \left[\frac{(td + 460) \cdot \text{theta}}{Yds \cdot Vds} \right]^2$$

ISOKINETIC METERBOX FULLTEST CALIBRATION RESULTS

Meterbox No.: N14 Date: 10-12-95 Calibrated By: P. JUDD
 Standard Meter No: 1017057 Barometric Pressure, Pb, In. Hg: 29.77
 Standard Meter Coefficient, Yds: 0.9846 Meterbox Vacuum, In. Hg: 0

STANDARD METER			METERBOX METERING SYSTEM				
Gas Volume (Vds) cf	Temp. (tds) °F	Time (theta) Min.	Orifice Setting (Delta H) In. H2O	Gas Volume (Vd) cf	Temp. (td) °F	Coeff. (Yd)	Delta H@ in. H2O @ 68°F
4.981	69	13	0.5	5.147	97.5	1.0029	1.888
4.907	69	13	0.5	5.159	105.5	0.9999	1.918
5.201	69	7	2	5.52	114.5	1.0025	1.949
5.195	69	7	2	5.549	119	1.0040	1.938
5.714	69	5	4.8	6.169	125.5	0.9976	1.940
5.708	69	5	4.8	6.177	129	1.0012	1.933
Average:						1.0013	1.928

$$Yd = \frac{Yds \cdot Vds \cdot (td + 460) \cdot Pb}{Vd \cdot (tds + 460) \cdot (Pb + (\Delta H / 13.6))}$$

$$\Delta H@ = \frac{0.0319 \cdot \Delta H}{Pb \cdot (tds + 460)} \cdot \left[\frac{(td + 460) \cdot \theta}{Yds \cdot Vds} \right]^2$$

ISOKINETIC METERBOX POSTTEST CALIBRATION RESULTS

Meterbox No.: N14 Date: 10/20/95 Calibrated By: P. JUDD
 Job Number: 14448 Plant: WITHERS
 Standard Meter No: 1017057 Barometric Pressure, Pb, In. Hg: 29.6
 Standard Meter Coefficient, Yds: 0.9846 Meterbox Vacuum, In. Hg: 2

STANDARD METER

Gas Volume (Vds) cf	Temp. (tds) °F	Time (theta) Min.
4.999	71	8
4.991	71	8
5.582	71	9

METERBOX METERING SYSTEM

Orifice Setting (Delta H) In. H2O	Gas Volume (Vd) cf	Temp. (td) °F	Coeff. (Yd)	Delta H@ in. H2O @ 68°F
1.3	5.151	96	0.9973	1.875
1.3	5.185	101.5	0.9990	1.863
1.3	5.858	107.5	0.9995	1.865
Average:			0.9986	1.868

Fulltest Yd: 1.0013

Date: 10/12/95

% Deviation*: -0.3%

* maximum allowed deviation = ±5%

$$Yd = \frac{Yds \cdot Vds \cdot (td + 460) \cdot Pb}{Vd \cdot (tds + 460) \cdot (Pb + (\Delta H / 13.6))}$$

$$\Delta H@ = \frac{0.0319 \cdot \Delta H}{Pb \cdot (tds + 460)} \cdot \left[\frac{(td + 460) \cdot \theta}{Yds \cdot Vds} \right]^2$$

THERMOCOUPLE CALIBRATION

Thermocouple No.: R325

Date: 3/26/92

Calibrated By: JPW

Barometric Pressure, Inches Hg: 29.32

Ambient Temperature, °F: 72.0

Mercury-In-Glass Thermometer I.D. No.: 7121K

Calibration System Used	Potentiometer I.D. Number	Reference Thermometer Temperature		Mean Temperature of Hg Column T_m °F	Thermocouple Thermometer Temperature T_t °F	Temperature Diff., % (Allowable: ≤ 1.5 %)
		T_o °F	T_c °F			
Ice Bath	F64	32.0	31.96	69.0	32.0	-.01
		32.0	31.96	69.0	32.0	-.01
		32.0	31.96	69.0	33.0	-.22
Boiling Water	F64	210.0	211.71	110.0	210.6	.17
		210.0	211.71	110.0	210.4	.20
		210.0	211.71	110.0	210.4	.20
Boiling Oil	F64	409.0	418.98	124.0	409.8	1.04
		409.0	418.98	124.0	410.0	1.02
		409.0	418.98	124.0	409.8	1.04

$$\text{Corrected Temperature} = T_c = T_o + [(.00009) \cdot (T_o - 20) \cdot (T_o - T_m)]$$

$$\text{Temperature Difference} = \frac{[(T_c + 460) - (T_t + 460)]}{(T_c + 460)} \cdot 100$$

THERMOCOUPLE CALIBRATION

Thermocouple No.: R364

Date: 6/17/93

Calibrated By: CCB

Barometric Pressure, Inches Hg: 29.80

Ambient Temperature, °F: 72.0

Mercury-In-Glass Thermometer I.D. No.: T2/T3

Calibration System Used	Potentiometer I.D. Number	Reference Thermometer Temperature		Mean Temperature of Hg Column T_m °F	Thermocouple Thermometer Temperature T_t °F	Temperature Diff., % (Allowable: ≤ 1.5 %)
		T_o °F	T_c °F			
Ice Bath	F64	32.0	31.96	68.0	31.9	.01
		32.0	31.96	68.0	31.8	.03
		32.0	31.96	68.0	31.8	.03
Boiling Water	F64	211.2	212.93	110.9	211.3	.24
		211.2	212.93	110.9	211.2	.26
		211.2	212.93	110.9	211.2	.26
Boiling Oil	F64	396.1	405.65	114.0	393.6	1.39
		396.1	405.65	114.0	393.6	1.39
		396.1	405.65	114.0	393.4	1.41

$$\text{Corrected Temperature} = T_c = T_o + [(.00009) * (T_o - 20) * (T_o - T_m)]$$

$$\text{Temperature Difference} = \frac{[(T_c + 460) - (T_t + 460)]}{(T_c + 460)} * 100$$

THERMOCOUPLE CALIBRATION

THERMOCOUPLE No. R385

Date 7-29-94

Calibrated By MC

Barometric Pressure, "Hg 29.57

Ambient Temperature, °F 71

Calibration System Used	Ref. Digital Thermometer & Thermocouple I.D. Nos.	Reference Thermocouple Temperature (T _r °F)	Test Digital Thermometer I.D. No.	Test Thermocouple Temperature (T _t °F)	Temperature Diff., % (Allowable: ≤ 1.5 %)
ICE BATH	<u>T-102829</u> <u>T-0</u>	<u>31.4</u>	<u>HH-97</u>	<u>32.4</u>	<u>0.2</u>
		<u>31.3</u>		<u>32.4</u>	<u>0.2</u>
		<u>31.2</u>		<u>32.4</u>	<u>0.2</u>
BOILING WATER	<u>/</u>	<u>212.6</u>	<u>/</u>	<u>213.2</u>	<u>0.1</u>
		<u>212.5</u>		<u>213.0</u>	<u>0.1</u>
		<u>212.5</u>		<u>210.2</u>	<u>0.3</u>
BOILING OIL	<u>/</u>	<u>404.6</u>	<u>α</u>	<u>400.2</u>	<u>0.5</u>
		<u>413.9</u>		<u>411.2</u>	<u>0.3</u>
		<u>413.1</u>		<u>409.6</u>	<u>0.4</u>

$$\text{Temperature Difference} = \frac{T_r - T_t}{T_r + 460} \cdot 100$$

THERMOCOUPLE CALIBRATION

THERMOCOUPLE No. R394

Date 7-29-94

Calibrated By MC

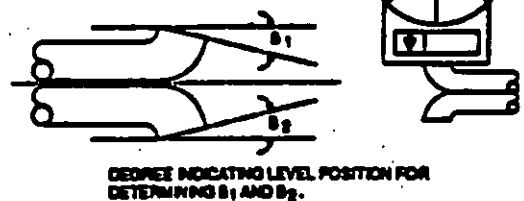
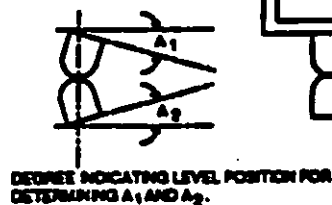
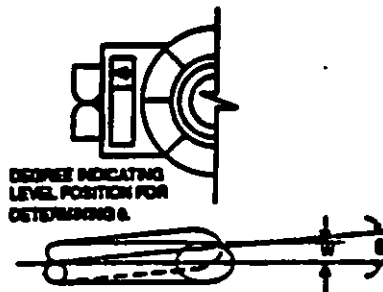
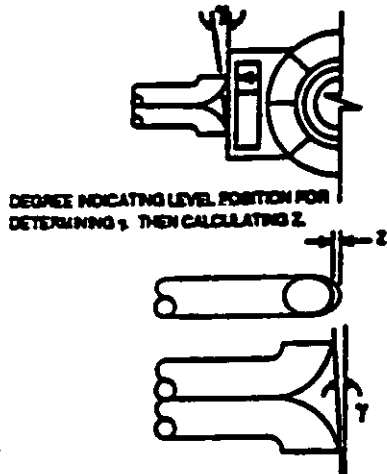
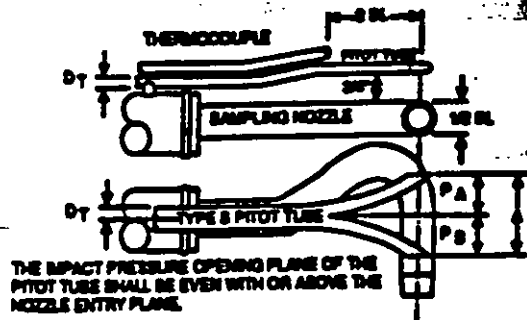
Barometric Pressure, "Hg 29.57

Ambient Temperature, °F 71

Calibration System Used	Ref. Digital Thermometer & Thermocouple I.D. Nos.	Reference Thermocouple Temperature (T _r °F)	Test Digital Thermometer I.D. No.	Test Thermocouple Temperature (T _t °F)	Temperature Diff., % (Allowable: ≤ 1.5 %)
ICE BATH	<u>I-102829</u>	31.3	<u>HH-97</u>	32.4	0.2
	<u>I-0</u>	31.3		32.2	0.2
		31.2		32.6	0.3
BOILING WATER	<u>/</u>	212.6	<u>/</u>	210.4	0.3
	<u>/</u>	212.6		209.5	0.5
	<u>/</u>	212.5		212.8	0
BOILING OIL	<u>✓</u>	414.6	<u>✓</u>	409.6	0.6
	<u>✓</u>	413.7		408.6	0.6
	<u>✓</u>	413.5		406.0	0.9

$$\text{Temperature Difference} = \frac{T_r - T_t}{T_r + 460} \times 100$$

PITOT TUBE INSPECTION



level?	Yes
obstructions?	NONE
damaged?	NONE
$-10^\circ < \alpha_1 < +10^\circ$	0
$-10^\circ < \alpha_2 < +10^\circ$	0
$-5^\circ < B_1 < +5^\circ$	0
$-5^\circ < B_2 < +5^\circ$	0
γ	0
θ	0
A	.945
$1.05 D_1 < P_0 < 1.5 D_1$	.476
$1.05 D_2 < P_0 < 1.5 D_2$	.469
$3/16" < D_1 < 3/8"$	.375
$A \tan \gamma < 0.125"$	0
$A \tan \theta < 0.03125"$	0
$P_0 = P_s \pm 0.063"$	Yes .007

See 40 CFR 60, Vol. 42 No. 160 EPA Method 2. Verify the minimum 2-inch setback of the thermocouple and the minimum 3/4-inch separation between the pitot tube and the nozzle as shown at the top of this page.

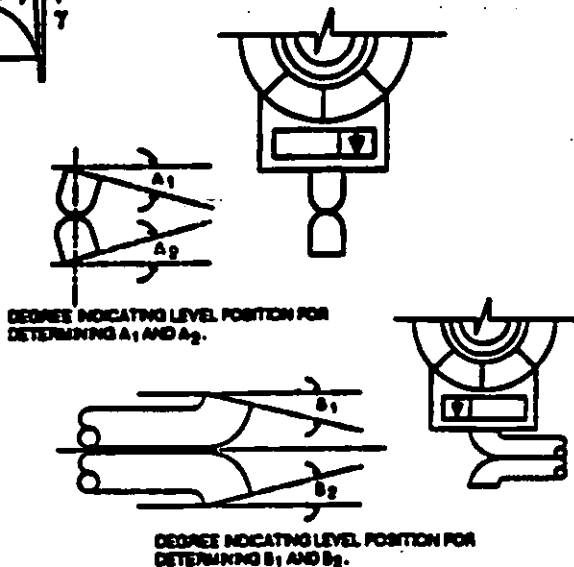
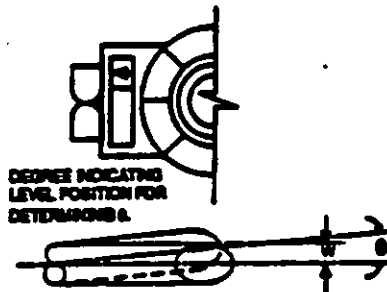
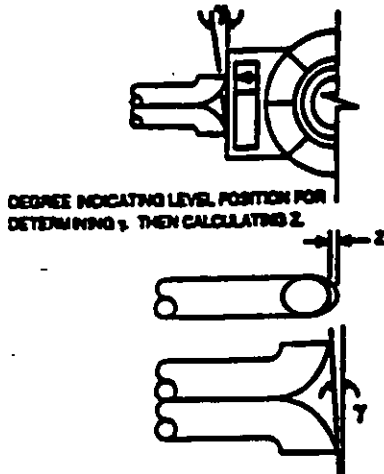
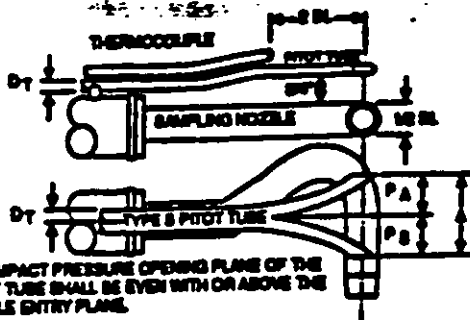
Comments: _____

I certify that pitot tube/probe number 5-22 meets or exceeds all specifications, criteria and/or applicable design features and is hereby assigned a pitot tube calibration factor of 0.84.

Signature W.L. Sherrill

Date 12-20-91

PITOT TUBE INSPECTION



level?	yes
obstructions?	NONE
damaged?	NONE
$-10^\circ < \alpha_1 < +10^\circ$	0
$-10^\circ < \alpha_2 < +10^\circ$	0
$-5^\circ < B_1 < +5^\circ$	0
$-5^\circ < B_2 < +5^\circ$	0
γ	1°
θ	0
A	.926
$1.05 D_1 < P_1 < 1.5 D_1$	.459
$1.05 D_2 < P_2 < 1.5 D_2$	.467
$3/16^\circ < D_1 < 3/8^\circ$	.375
$A \tan \gamma < 0.125^\circ$	.014
$A \tan \theta < 0.03125^\circ$	0
$P_1 = P_2 \pm 0.063^\circ$	yes .008

See 40 CFR 60, Vol. 42 No. 160 EPA Method 2. Verify the minimum 2-inch setback of the thermocouple and the minimum 3/4-inch separation between the pitot tube and the nozzle as shown at the top of this page.

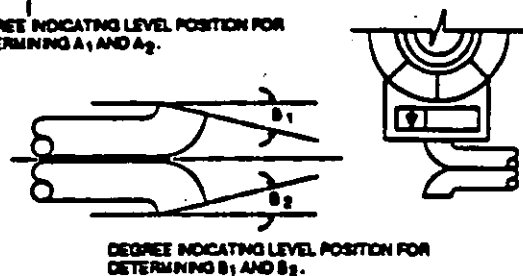
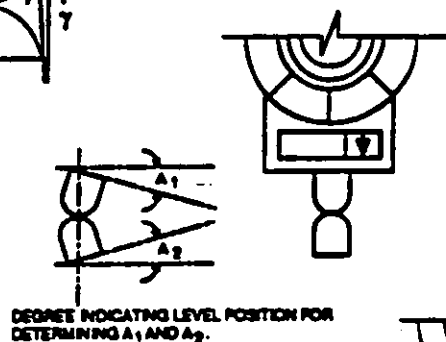
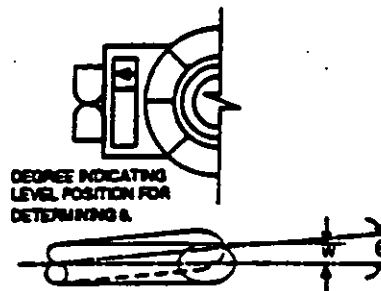
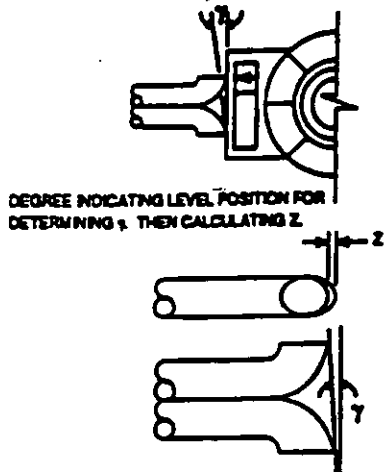
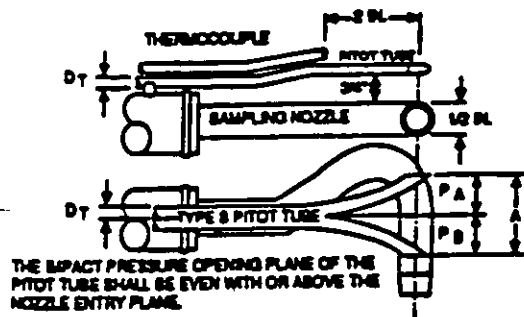
Comments: _____

I certify that pitot tube/probe number 5-24 meets or exceeds all specifications, criteria and/or applicable design features and is hereby assigned a pitot tube calibration factor of 0.84.

Signature W. L. Shull

Date 12-30-91

PITOT TUBE INSPECTION



level?	yes
obstructions?	NONE
damaged?	NONE
$-10^\circ < \alpha_1 < +10^\circ$	1°
$-10^\circ < \alpha_2 < +10^\circ$	1°
$-5^\circ < B_1 < +5^\circ$	0
$-5^\circ < B_2 < +5^\circ$	0
γ	2°
θ	1°
A	1.63
$1.05 D_1 < P_1 < 1.5 D_1$	= 815
$1.05 D_1 < P_1 < 1.5 D_1$	.815
$3/16" < D_1 < 3/8"$	.375
$A \tan \gamma < 0.125"$	.0512
$A \tan \theta < 0.03125"$	.026
$P_1 = P_2 \pm 0.063"$	yes 0

See 40 CFR 60, Vol. 42 No. 160 EPA Method 2. Verify the minimum 2-inch setback of the thermocouple and the minimum 3/4-inch separation between the pitot tube and the nozzle as shown at the top of this page.

Comments: NEW

I certify that pitot tube/probe number OP-72-5 meets or exceeds all specifications, criteria and/or applicable design features and is hereby assigned a pitot tube calibration factor of 0.84.

Signature [Signature]

Date 3-3-92



Scott Specialty Gases

6141 Easton Road, PO Box 310 Plumsteadville PA 18949-0310 PHONE: (215) 766-8861 FAX: (215) 766-0320

CERTIFICATE OF ANALYSIS: Interference-Free™ EPA Protocol Gas

Customer	Assay Laboratory	Purchase Order
ENTROPY ENVIRONMENTALISTS	Scott Specialty Gases, Inc.	5011-MANWELL
ATT: J. MAXWELL/ACCTS PAY.	6141 Easton Road	Scott Project # 7122922B
P O BOX 12291	Plumsteadville, PA 18949	
RESEARCH TRIANGLE PARK, NC 27709		

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay and Certification of Gaseous Calibration Standards; Procedure G1, September, 1993.

Cylinder Number	ALM031872	Previous Certification Dates	Certification Date	8/25/95
Cylinder Pressure+	1915 psig		Expiration Date	2/25/96
ANALYZED CYLINDER				
Components		Certified Concentration	Analytical Accuracy*	
Sulfur Dioxide		45.1 ppm	± 1% Directly NIST Traceable	
Nitrogen		Balance Gas		

* Do not use when cylinder pressure is below 150 psig.

* Analytical accuracy is inclusive of usual known error sources which at least include precision of the measurement processes.

REFERENCE STANDARD

Type/Sample No.	Expiration Date	Cylinder Number	Concentration
NTRM1693	2/21/97	ALM021561	47.1 ppm SO2 in N2

INSTRUMENTATION

Instrument/Model/Serial #	Last Date Calibrated	Analytical Method
Nicolet FTIR/8220/AAB9300174	8/10/95 :SO2	Scott Enhanced FTIR

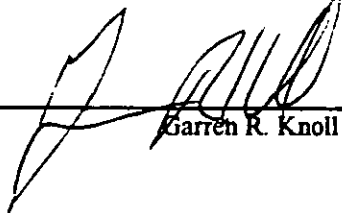
ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components	First Triad Analysis	Second Triad Analysis	Calibration Curve
SO2	Date: 8/18/95 Exp. Date: ppm Z1= 0.05 R1= 47.1 T1= 45.3 R2= 47.5 Z2= 0.05 T2= 45.3 Z3= 0.05 T3= 45.3 R3= 47.5 Avg. Concentration: 45.3 ppm	Date: 8/25/95 Exp. Date: ppm Z1= 0.001 R1= 47.1 T1= 44.8 R2= 47.2 Z2= 0.00 T2= 45.1 Z3= 0.00 T3= 44.9 R3= 47.1 Avg. Concentration: 44.9 ppm	Concentration = A+BX+CX ² +DX ³ +EX ⁴ R= 0.99999 ALM021561 Constants: A= 5.68E-02 B= 1.02E-00 C= -3.55E-03 D= 4.30E-05 E= 0.0E+00

Special Notes:

246

Analyst:


Garren R. Knoll



Scott Specialty Gases

6141 Easton Road, PO Box 310 Plumsteadville, PA 18949-0310 PHONE: (215) 766-8861 FAX: (215) 766-0320

CERTIFICATE OF ANALYSIS: Interference-Free™ EPA Protocol Gas

Customer ENTROPY ENVIRONMENTALISTS ATT: J. MAXWELL, ACCTS. PAY. P. O. BOX 12291 RESEARCH TRIANGLE PA, NC 27709	Assay Laboratory Scott Specialty Gases, Inc. 6141 Easton Road Plumsteadville, PA 18949	Purchase Order 5011-MAXWELL Scott Project # 7122928B
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ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay and Certification of Gaseous Calibration Standards, Procedure G1, September, 1993.

Cylinder Number AAL17344	Previous Certification Dates	Certification Date 8/24/95
Cylinder Pressure+ 1905 psig		Expiration Date 8/24/97
ANALYZED CYLINDER		
Components	Certified Concentration	Analytical Accuracy*
Sulfur Dioxide	92.8 ppm	± 1% Directly NIST Traceable
Nitrogen	Balance Gas	

+ Do not use when cylinder pressure is below 150 psig.

* Analytical accuracy is inclusive of usual known error sources which at least include precision of the measurement processes.

REFERENCE STANDARD

Type/Sample No.	Expiration Date	Cylinder Number	Concentration
NTRM1694	5/11/97	ALM040139	94.4 ppm SO ₂ in N ₂

INSTRUMENTATION

Instrument/Model/Serial #	Last Date Calibrated	Analytical Method
Nicolet FTIR/8220/AAB9300174	8/10/95 :SO ₂	Scott Enhanced FTIR

ANALYZER READINGS

(Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components	First Triad Analysis			Second Triad Analysis			Calibration Curve
SO ₂	Date: 8/17/95	Exp. Date: ppm		Date: 8/24/95	Exp. Date: ppm		Concentration = A+Br+Cx ² +Dx ³ +Ex ⁴
	Z1= 0.00	R1= 94.4	T1= 93.2	Z1= 0.00	R1= 94.4	T1= 92.8	R= 0.99999 ALM031875
	R2= 94.3	Z2= 0.00	T2= 92.7	R2= 94.1	Z2= 0.00	T2= 92.6	Constants: A= 3.89E-01
	Z3= 0.00	T3= 92.7	R3= 94.3	Z3= 0.02	T3= 92.7	R3= 94.5	B= 2.57E-01 C= 7.73E-06
	Avg. Concentration: 92.9 ppm			Avg. Concentration: 92.7 ppm			D= 6.6E+00 E= 6.6E+00

Special Notes:

247

Analyst:

Garren R. Knoll



Scott Specialty Gases

6141 EASTON ROAD, P.O. BOX 310, PLUMSTEADVILLE, PA 18949-0310 (215) 766-6881 FAX: (215) 766-0320

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
Entropy
Chem Division
8724 Glenwood Avenue
Raleigh, NC 27612

Assay Laboratory
Scott Specialty Gases, Inc.
6141 Easton Road
P.O. Box 310
Plumsteadville, PA 18949-0310

Purchase Order 5011-MAXWELLJ
Scott Project # 01-70629-001

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay & Certification of Gaseous Calibration Standards; 1 Procedure #GL Section Number 3.0.4; September, 1993.

Cylinder Number A1.M035396
Cylinder Pressure 2000 psig+

Certification Date 08-14-95
Previous Certification Dates None

Expiration Date 08-14-97

ANALYZED CYLINDER

Components
Nitric Oxide
Total Oxides of Nitrogen
Balance Gas: Nitrogen

Certified Concentration
25.9 ppm
26.0 ppm

Analytical Uncertainty*
±1% NIST Traceable
Reference Value Only

*Do not use when cylinder is less than 150 psig.

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement process.

REFERENCE STANDARD

Type NTRM2629
Expiration Date 11-21-96

Cylinder Number KLM001188

Concentration
19.87 ppm NO in N₂

INSTRUMENTATION

Instrument/Model/Serial #
NO: 10/9741111S

Last Date Calibrated
08-14-95

Analytical Principle
Chemiluminescent

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components	First Triad Analysis	Second Triad Analysis	Calibration Curve
Nitric Oxide	Date: 08-07-95 Z1=0.0422 R1=1.9942 T1=2.9996 Z2=2.0054 Z3=0.9028 T2=2.6220 Z3=0.0281 T3=2.5980 R3=1.9936 Avg. Conc. of Cust. Cyl. 25.9 ppm	Date: 08-14-95 Z1=0.0134 R1=1.5185 T1=1.9793 Z2=1.5050 Z3=0.0138 T2=1.9680 Z3=0.0041 T3=1.9529 R3=1.5135 Avg. Conc. of Cust. Cyl. 25.9 ppm	Concentration = A + B * C + D * C ² + E * C ³ r = 1.0000 NTRM2629 Constants A = 1.8654E-01 B = 1.5871E+01 C = 0.0000E+00 D = 0.0000E+00 E = 0.0000E+00

Special Notes:

Wesley Elder
Analyst Wesley Elder



Scott Specialty Gases

6141 EASTON ROAD, P.O. BOX 310, PLUMSTEADVILLE, PA 18949-0310

(215) 788-0321 FAX (215) 788-0320

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
Entropy
Cam Division
8724 Glenwood Avenue
Raleigh, NC 27612

Assay Laboratory
Scott Specialty Gases, Inc.
6141 Easton Road
P.O. Box 310
Plumsteadville, PA 18949-0310

Purchase Order 5011-MAXWELLJ
Scott Project # 01-70629-002

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay & Certification of Gaseous Calibration Standards; 1 Procedure #G1, Section Number 3.0.4; September, 1993.

Cylinder Number AAL14753
Cylinder Pressure 2000 psig+

Certification Date 08-14-95
Previous Certification Dates None

Expiration Date 08-14-97

ANALYZED CYLINDER

Components
Nitric Oxide
Total Oxides of Nitrogen
Balance Gas Nitrogen

Certified Concentration
46.3 ppm
46.3 ppm

Analytical Uncertainty*
±1% NIST Traceable
Reference Value Only

* Do not use when cylinder is less than 150 psig.

* Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement process.

REFERENCE STANDARD

Type NERM648B
Expiration Date 07-10-97

Cylinder Number ALMD47706

Concentration
94.4 ppm NO in N₂

INSTRUMENTATION

Instrument/Model/Serial #
NO_x Test/10/9741111S

Last Date Calibrated
08-14-95

Analytical Principle
Chemiluminescent

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components

Nitric Oxide

First Triad Analysis

Date: 08-07-95 Response Units: Volts
Z1=0.0143 R1=2.0062 T1=4.6877
R2=2.0025 T2=0.0018 T2=4.7119
Z3=0.0159 T3=4.6976 R3=2.0110
Avg. Conc. of Cust. Cyl. 46.5 ppm

Second Triad Analysis

Date: 08-14-95 Response Units: Volts
Z1=0.0312 R1=7.3691 T1=3.5961
R2=7.4276 Z2=0.0411 T2=0.6104
Z3=0.0282 T3=3.5910 R3=7.3324
Avg. Conc. of Cust. Cyl. 46.0 ppm

Calibration Curve

Concentration = $A + Bx + Cx^2 + Dx^3 + Ex^4$
 $r = 1.0000$ NERM2629
Constant: A = -1.0534E-01
B = 1.9871E+01 C = 0.0000E+00
D = 0.0000E+00 E = 0.0000E+00

Special Notes:

Wesley R. Risher
Analyst Wesley Risher



Scott Specialty Gases

1750 EAST CLUB BOULEVARD, DURHAM, NC 27704

(919) 220-0803 FAX: (919) 220-0808

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
Entropy Environmentalists
Attn: K. Spears
P.O. Box 12291
Research Triangle Park, NC 27709

Assay Laboratory
Scott Specialty Gases, Inc.
1750 East Club Boulevard
Durham, NC 27704

Purchase Order 4922
Scott Project # 12-11576

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol Procedure #G1, issued September, 1993.

Cylinder Number	ALM-024066	Certification Date	05-10-95	Expiration Date	05-10-97
Cylinder Pressure	1901 PSIG	Previous Certification	None		

ANALYZED CYLINDER

Components	Certified Concentration	Analytical Uncertainty*
Nitric Oxide	80.2 PPM	+/- 1% NIST Directly Traceable
NOX	80.2 PPM	Reference Value Only
Nitrogen		Balance

Do not use when cylinder pressure is less than 150 PSIG.

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type	Expiration Date	Cylinder Number	Concentration
NTRM# 1685	08-96	ALM-025103	245.3 PPM NO Balance in N2

INSTRUMENTATION

Instrument/Model/Serial #	Last Date Calibrated	Analytical Principle
NICOLET / 8220 / AAB9400252	05-04-95	FTIR

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components	First Triad Analysis	Second Triad Analysis	Calibration Curve
Nitric Oxide	Date: 05-03-95 Response Units: PPM Z1=0.546 R2=245.5 Z3=0.511 R1=245.3 Z2=1.942 T3=80.2 T1=79.8 T2=80.3 R3=246.2	Date: 05-10-95 Response Units: PPM Z1=0.666 R2=245.1 Z3=0.631 R1=245.3 Z2=1.856 T3=80.4 T1=80.3 T2=79.9 R3=245.4	Date: 05-04-95
	Date: Response Units: Z1= R2= Z3= R1= Z2= T3= T1= T2= R3=	Date: Response Units: Z1= R2= Z3= R1= Z2= T3= T1= T2= R3=	Date:
	Date: Response Units: Z1= R2= Z3= R1= Z2= T3= T1= T2= R3=	Date: Response Units: Z1= R2= Z3= R1= Z2= T3= T1= T2= R3=	Date:

M. Morris
Analyst M. Morris



Scott Specialty Gases, Inc.

1750 EAST CLUB BOULEVARD, DURHAM, NC 27704

(919) 220-0803 FAX: (919) 220-0808

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
Entropy
Attn: Mr. John Maxwell
CEM Division
8724 Glenwood Avenue
Raleigh, NC 27612

Assay Laboratory
Scott Specialty Gases, Inc.
1750 East Club Boulevard
Durham, NC 27704

Purchase Order 4739-MAXWELLJ
Scott Project # 12-09458

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol Procedure #G1, issued September, 1993.

Cylinder Number ALM-037394
Cylinder Pressure 2000 PSIG

Certification Date 12-19-94
Previous Certification None

Expiration Date 12-19-97

ANALYZED CYLINDER

Components

Carbon Monoxide
Nitrogen

Certified Concentration
30.2 PPM

Analytical Uncertainty*

+/- 1% NIST Directly Traceable
Balance

Do not use when cylinder pressure is less than 150 PSIG.

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type NTRM# 1678
Expiration Date 07-96

Cylinder Number
ALM-000901

Concentration
45.76 PPM Balance in Nitrogen

INSTRUMENTATION

Instrument/Model/Serial #
LOW CO: Horiba/AIA23AS/850658012

Last Date Calibrated
12-12-94

Analytical Principle
NDIR

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components

First Triad Analysis

Date: 12-11-94 Response Units: PPM
Z1=0.1 R2=46.1 Z3=0.2
R1=46.1 Z2=0.3 T3=30.4
T1=30.4 T2=30.5 R3=46.0

Second Triad Analysis

Date: 12-19-94 Response Units: PPM
Z1=0.1 R2=45.7 Z3=0.1
R1=45.6 Z2=0.1 T3=30.1
T1=30.1 T2=30.1 R3=45.7

Calibration Curve

Date: 12-12-94

Date: Response Units:
Z1= R2= Z3=
R1= Z2= T3=
T1= T2= R3=

Date: Response Units:
Z1= R2= Z3=
R1= Z2= T3=
T1= T2= R3=

Date:

Date: Response Units:
Z1= R2= Z3=
R1= Z2= T3=
T1= T2= R3=

Date: Response Units:
Z1= R2= Z3=
R1= Z2= T3=
T1= T2= R3=

Date:

Analyst K. Cooke



Scott Specialty Gases, Inc.

1750 EAST CLUB BOULEVARD, DURHAM, NC 27704

(919) 220-0803 FAX: (919) 220-0808

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

Customer
Entropy
Attn: Mr. John Maxwell
CEM Division
8724 Glenwood Avenue
Raleigh, NC 27612

Assay Laboratory
Scott Specialty Gases, Inc.
1750 East Club Boulevard
Durham, NC 27704

Purchase Order 4739-MAXWELLJ
Scott Project # 12-09458

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol Procedure #G1, issued September, 1993.

Cylinder Number	AAL-12512	Certification Date	12-16-94	Expiration Date	12-16-97
Cylinder Pressure	2000 PSIG	Previous Certification	None		

ANALYZED CYLINDER

Components

Carbon Monoxide
Nitrogen

Certified Concentration
59.9 PPM

Analytical Uncertainty*

+/- 1% NIST Directly Traceable
Balance

Do not use when cylinder pressure is less than 150 PSIG.

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

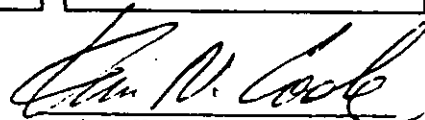
Type	Expiration Date	Cylinder Number	Concentration
NTRM# 1679	04-96	ALM-024772	96.2 PPM Balance in Nitrogen

INSTRUMENTATION

Instrument/Model/Serial #	Last Date Calibrated	Analytical Principle
LOW CO: Horiba/ALA23AS/850658012	12-12-94	NDIR

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components	First Triad Analysis	Second Triad Analysis	Calibration Curve
Carbon Monoxide	Date: 12-05-94 Response Units: PPM Z1=0.1 R2=96.3 Z3=0.1 R1=96.3 Z2=0.1 T3=60.0 T1=60.1 T2=59.9 R3=96.3	Date: 12-16-94 Response Units: PPM Z1=0.1 R2=96.2 Z3=0.1 R1=96.2 Z2=0.1 T3=59.8 T1=59.9 T2=59.9 R3=96.3	Date: 12-12-94
	Date: Response Units: Z1= R2= Z3= R1= Z2= T3= T1= T2= R3=	Date: Response Units: Z1= R2= Z3= R1= Z2= T3= T1= T2= R3=	Date:
	Date: Response Units: Z1= R2= Z3= R1= Z2= T3= T1= T2= R3=	Date: Response Units: Z1= R2= Z3= R1= Z2= T3= T1= T2= R3=	Date:


Analyst K. Cooke



Scott Specialty Gases

6141 Easton Road, PO Box 310 Plumsteadville PA 18949-0310 PHONE: (215) 766-8861 FAX: (215) 766-0320

CERTIFICATE OF ANALYSIS: Interference-Free™ EPA Protocol Gas

Customer

ENTROPY

ATTN: MR. J. MAXWELL/CEM DIV.

8724 GLENWOOD AVE.

RALEIGH, NC 27612

Assay Laboratory

Scott Specialty Gases, Inc.

6141 Easton Road

Plumsteadville, PA 18949

Purchase Order: 4886-MAXWELLJ

Scott Project # 6710705B

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay and Certification of Gaseous Calibration Standards; Procedure G1; September, 1993.

Cylinder Number ALM045962

Previous Certification Dates

Certification Date 4/25/95

Cylinder Pressure+ 1850 psig

Expiration Date 4/25/98

ANALYZED CYLINDER

Components

Carbon Monoxide

Nitrogen

Certified Concentration

90.9 ppm

Balance Gas

Analytical Accuracy*

± 1% Directly NIST Traceable

+ Do not use when cylinder pressure is below 150 psig.

* Analytical accuracy is inclusive of usual known error sources which at least include precision of the measurement processes.

REFERENCE STANDARD

Type/Sample No.

Expiration Date

Cylinder Number

Concentration

NTRM1697

8/11/96

ALM041943

97.1 ppm CO in N2

INSTRUMENTATION

Instrument/Model/Serial #

Last Date Calibrated

Analytical Method

Nicolet FTIR/8220/AAB9300174

3/29/95

Scott Enhanced FTIR

ANALYZER READINGS

(Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components	First Triad Analysis			Second Triad Analysis			Calibration Curve
CO	Date: 4/18/95	Exp. Date: ppm		Date: 4/25/95	Exp. Date: ppm		Concentration = A+Br+Cr+Dr+Ez
	Z1= 0.00	R1= 97.10	T1= 90.64	Z1= 0.00	R1= 97.10	T1= 91.17	R= 0.99999 ALM019933
	R2= 96.78	Z2= 0.00	T2= 90.91	R2= 96.97	Z2= 0.00	T2= 90.80	Constants: A= -7.99E-01
	Z3= 0.00	T3= 90.72	R3= 96.72	Z3= 0.00	T3= 90.94	R3= 97.07	B= 2.62E-01 C= 1.60E-04
	Avg. Concentration: 90.76 ppm			Avg. Concentration: 90.97 ppm			D= 4.36E-06 E= -3.94E-09

Special Notes:

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Analyst:

Garren R. Kroll



Scott Specialty Gases

6141 EASTON ROAD, P.O. BOX 310, PLUMSTEADVILLE, PA 18949-0310 (215) 766-8861 FAX (215) 766-0320

CERTIFICATE OF ANALYSIS EPA PROTOCOL GAS

Customer
Entropy
8724 Glenwood Ave
Raleigh, NC 27612

Assay Laboratory
Scott Specialty Gases, Inc.
6141 Easton Road
P.O. Box 310
Plumsteadville, PA 18949-0310

Purchase Order 4783-MAXWELJ
Scott Project # 01-63890-008

ANALYTICAL INFORMATION

Certified to exceed the minimum specifications of EPA Protocol 1 Procedure #G1, Section Number 3.0.4

Cylinder Number ALM026207
Cylinder Pressure 2000 psig

Certification Date 01-11-95 **Expiration Date** 01-11-98
Previous Certification Dates None

ANALYZED CYLINDER

Components
Propane
Balance Gas: Air

Certified Concentration
27.7 ppm

Analytical Uncertainty*
±1% NIST Traceable

*Do not use when cylinder is less than 150 psig

*Analytical uncertainty is inclusive of usual known error sources which at least includes reference standard error & precision of the measurement processes.

REFERENCE STANDARD

Type NTRM1668
Expiration Date 06-07-96

Cylinder Number
ALM032011

Concentration
95.5 ppm C₃H₈ in N₂

INSTRUMENTATION

Instrument/Model/Serial #
C3H8: Varian/VA3300/7945

Last Date Calibrated
01-10-95

Analytical Principle
FID

ANALYZER READINGS (Z=Zero Gas R=Reference Gas T=Test Gas r=Correlation Coefficient)

Components	First Triad Analysis	Second Triad Analysis	Calibration Curve
Propane	Date: 01-11-95 Response Units: Area Z1=000000 R1=100558 T1=029170 R2=100553 Z2=000000 T2=029119 R3=000000 T3=029040 R3=100308 Avg. Conc. of Cust. Cyl: 27.7 ppm		Concentration = A + Bx + Cx ² + Dx ³ + Ex ⁴ r=1.00000 NTRM1668 Constants: A=1.6316E-02 B=9.6052E-04 C=0.0000E+00 D=0.0000E+00 E=0.0000E+00

Special Notes:

☐ Check this box if certified concentration has been corrected for analytical differences.

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[Signature]
Analyst Robert K. Kufrovich