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The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

Background Report Reference

AP-42 Section Number: 11.6

Background Chapter: 4

Reference Number: 71

Title: Field Data Source Test of Lone Star
Industries at Davenport, CA

Chemecology Corp

Chemecology Corp

August 1983



CHE

AP-42 Section 11.6
Reference NOT USED
Report Sect. 4
Reference 71

690-B Garcia Avenue, Pittsburg, CA 94

FIELD DATA SOURCE TESTPREPARED FOR Lonestar IndustriesHighway 1Davenport, California 95017ATTENTION Duc VuREGARDING Particulate, NOx & SO₂ Emissions TestingREGULATORY AGENCY MBUAPCD & EPAPURPOSE ComplianceTEST DATE August 22 and 23, 1983UNIT TESTED Main Stack

ASSOCIATED REPORT NUMBERS

REPORT NUMBER 1716PREPARED BY Larry BozzelliREVIEWED BY Larry Bozzelli

Reference 49:

- (1) Unspecified kiln w/
Unspecified control
- (1) Unspecified cooler w/
Unspecified control
- (1) "Coal" stack

Delete!

Delete for above
reasons

SUMMARY

PLANT: LONE STAR - SANTA CRUZ

LOCATION: DRY SHORE CALIFORNIA

TEST/IDENTIFICATION 1698 #1716

DATE: AUG 21 1983

TESTING BY: CHEMECOLOGY CORP.

KILN/COOLER NO.

PERFORMANCE

Kiln Production Ton/Hr. 107.9 @ 1.00 K.F. Factor

Kiln Feed Rate Ton/Hr. 170

Fuel Rate (Coal) Ton/Hr. 11.2 @ 11810 BTU/lb.

" " (Oil) Gal/Hr.

Fuel Ash	%		13.7
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Fuel Sulphur	%		0.6%	<u>0.7</u>	Kiln Feed S.
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KILN (Stack)

ALLOWABLE

Exhaust Gas Flow DSCFM 143.700

Part. Concn. lb/SCF 0.000003

Emission Rate lb/Ton 0.15 / 25.9 #/hr 0.3 / 51.8 #/hr

SCX (Kiln)

(Concentration) PPM 110

Emission Rate lb/Ton 0.93 / 159512

Emission Rate 1b/MMBTU

NOX (Kiln)

(Concentration) PPM 202

Emission Rate lb/Ton 1.22/208#/hr

COOLER (Stack)

Exhaust Gas Flow DSCFM 95,700

Part. Concen. 1b/SCF 0.000002

Emission Rate 1b/Ton 0.07/11.5#/hr 0.1/17.0#/hr

REMARKS:



W. GREEN

CHEMECOLOGY
CORPORATION

690-B Garcia Avenue, Pittsburg, CA 94565 / (415) 438-5766

FIELD DATA SOURCE TEST

PREPARED FOR Lonestar Industries

Highway 1

Davenport, California 95017

ATTENTION Duc Vu

REGARDING Particulate, NOX & SO₂ Emissions Testing

REGULATORY AGENCY MBUAPCD & EPA

PURPOSE Compliance

TEST DATE August 22 and 23, 1983

UNIT TESTED Main Stack

ASSOCIATED REPORT NUMBERS _____

REPORT NUMBER 1716

PREPARED BY Larry Borrelli

REVIEWED BY *Larry Borrelli*



ABSTRACT

On August 22 and 23, 1983, Chemecology personnel performed source emissions testing for Lonestar Industries in Davenport, California. The testing team consisted of four persons; Larry Borrelli, project supervisor, Kevin Crosby, continuous analyzer operator, and Dave Ray, sampling technician. The unit tested was the main stack. The components sampled for were; particulates, NOx and SO₂. Triplicate tests for each component were performed. On the first day the Kiln and Roller Mill were both operating at full capacity. On the second day the Kiln was operating at full capacity and the Roller Mill was not operating. The purpose of the testing was to demonstrate compliance with Monterey Bay Unified APCD and Environmental Protection Agency Regulations.

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SELECTED RESULTS

SELECTED RESULTS

Client: Lonestar
Unit: Main Stack
Date: 8/22/83

Time: 1043-1232 1310-1433 1514-1635

Process Conditions:

ACFM:	225612	203645	207449
SDCFM:	146830	135406	140577
Kiln feed (TPH):	170	170	170
Roller Mill (TPH):	200	200	200
% H ₂ O:	14.8	13.7	13.0

142-397
170

Particulate Emissions:

gr/SDCF (total):	0.0089	0.0065	0.0068
gr/SDCF (front half):	0.0060	0.0035	0.0050
lbs/hr (total):	11.21	7.55	8.20
lbs/ton of feed (front half):	0.044	0.024	0.035

250

Gaseous Emissions:

Time: 1131-1203 1333-1414 1550-1637

$\frac{O_2}{\%}$ vol dry:	10.5	10.3	10.4
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NOx:				
ppm vol dry:	204	265	182	202
ppm @ 10% O ₂ :	214	273	189	
lbs/hr:	218	261	186	202

202
208

SO ₂ :				
ppm vol dry:	28	42	51	110
ppm @ 10% O ₂ :	29	43	53	
lbs/hr:	41.6	57.5	72.5	159

110
159



SELECTED RESULTS

Client: Lonestar
Unit: Main Stack
Date: 8/23/83

Time: 0826-0955 1030-1153 1305-1430

Process Conditions:

ACFM:	249973	250205	202296
SDCFM:	155939	155971	121452
Kiln feed (TPH):	170	170	170
Roller Mill (TPH):	0	0	0
% H ₂ O:	10.7	11.6	13.7

Particulate Emissions:

gr/SDCF (total):	0.0348	0.0243	0.0456
gr/SDCF (front half):	0.0030	0.0012	0.0031
lbs/hr (total):	46.56 ✓	32.52	47.52
lbs/ton of feed (front half):	0.024	0.009	0.019

Gaseous Emissions:

Time: 0833-0937 1047-1159 1300-1400

O ₂ :			
% vol dry:	12.0	11.1	8.9

NO _x :			
ppm vol dry:	138	205	218
ppm @ 10% O ₂ :	169	228	198
lbs/hr:	157	233	193

SO ₂ :			
ppm vol dry:	165	170	204
ppm @ 10% O ₂ :	202	189	185
lbs/hr:	260	268	251

VELOCITY PROFILE & VOLUME FLOW RATE



VELOCITY TRAVERSE AND VOLUME FLOW RATE

REF: Environmental Protection Agency, Code of Federal Regulations,
Title 40, Part 60, Appendix A, Method 1 and 2, 1981
: Bay Area AQMD, Manual of Procedures, San Francisco, CA, Method St-17
January, 1982
: ASME Performance Test Code #27, New York, NY, 1957
: ASTM D-2928-71
: Western Precipitation Division of Joy Manufacturing, WP-50, 1968

PROCEDURE:

Duct temperature and velocity were read at each of several traverse points within the duct. The number and location of traverse points was chosen to aid in the extraction of a representative sample (i.e. by EPA Method 1). Velocity head was determined using a calibrated type "S" pitot tube and Magnehelic differential pressure gauge. Duct temperature was measured by means of a thermocouple attached to the pitot tube. Static pressure was measured with the Magnehelic and one leg of the pitot tube. Using the molecular weight and traverse data, velocity was calculated at each traverse point. From the average velocity, duct area, temperature, pressure and composition, actual and standard gas volume flow rate were calculated for the duct.

CALCULATIONS:

Performed by computer based on the following equations:

Symbol Identification:

A_d = duct area, square feet
 C_p = pitot tube correction factor, unitless
 D = duct diameter (circular ducts), inches
 k = number of traverse points on D or W
 L = duct dimension having ports (rectangular), inches
 MW = molecular weight (wet)
 n = traverse point number on a diameter
 Δp = velocity head, "H₂O
 P_L = number of ports on dimension L
 P_d & P_{std} = duct (barometric + static) and standard pressure, "Hg
 Q_d = volume flow rate, actual CFM
 Q_{std} = volume flow rate, standard condition (wet or dry), SCFM
 T_d & T_{std} = duct and standard temperature, °R
 $t.p.$ = traverse point (distance from sample port wall), inches
 v_d = velocity at duct conditions, fps
 W = second duct dimension (rectangular), inches



VELOCITY TRAVERSE AND VOLUME FLOW RATE (cont)

Equations:

Location of Traverse Points:

Circular Duct:

$$\text{t.p. (1st half)} = D/2 - (D/2k) * \sqrt{k(k+1-2n)}$$

$$\text{t.p. (2nd half)} = D/2 + (D/2k) * \sqrt{k(2n-1)}$$

Where $n = 1$ to $k/2$

Rectangular Duct:

$$\text{t.p.} = W/2k + (n-1) * W/k$$

Where $k = (W/L) * (P_L)$
 $n = 1$ to k

Velocity & Volume Flow Rate:

$$v_d = 85.49 * C_p * \sqrt{\frac{T_d * \Delta p}{P_d * MW}}$$

$$Q_d = 60 * v_d (\text{avg}) * A_d = \text{ACFM}$$

$$Q_{\text{std(wet)}} = Q_d * \frac{T_{\text{std}}}{T_d(\text{avg})} * \frac{P_d}{P_{\text{std}}} = \text{SCFM}$$

$$Q_{\text{std(dry)}} = Q_{\text{std(wet)}} * (1 - \%H_2O/100) = \text{SDCFM}$$



VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')

DATA:

CLIENT: Lonestar

UNIT: Main Stack

DATE: 8/22/83

TIME: 1043 - 1232

RUN #: 1

Description: Four: 4-inch female ports, properly spaced approximately
8 diameters after and 2 diameters before disturbances in flow.

Duct Diameter 120 inches Area 78.54 ft²

Rectangular duct X

% H₂O 14.8 MW 29.43

Mag. Box # 375

Duct Static Pressure -0.52 inches H₂O

Temp. Unit # 5562

Standard Conditions 60 °F & 29.92 "Hg

Pitot Tube # 5293

Pitot Tube Coefficient 0.80

Trav. Pt.	Ins. From Edge	Southeast			Southwest			Northwest			Northeast		
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	5.2	220	0.46	40.8	220	0.46	40.8	225	0.76	52.6	215	0.62	47.1
2	17.6	220	0.52	43.3	220	0.56	45.0	225	0.84	55.3	220	0.84	55.1
3	35.5	220	0.56	45.0	220	0.54	44.2	220	0.80	53.8	220	0.74	51.7
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RESULTS:

Average Velocity (V_d) 47.9 FPS Average duct temp. 270 °F, press. 29.91 "Hg

Volume Flow Rate at 220 °F & 29.91 "Hg (Q_d) 225612 ACFM

Volume Flow Rate at standard conditions (Q_{std(wet)}) 172378 SCFM

Volume Flow Rate at standard conditions (Q_{std(dry)}) 146830 SDCFM



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VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')

DATA:

CLIENT: Lonestar

UNIT: Main Stack

DATE: 8/22/83

TIME: 1310 - 1433

RUN #: 2

Description: Four 4-inch ports properly located approximately 8 diameters after and 2 diameters before disturbances in flow.

Duct Diameter 120 inches Area 78.54 ft²

Rectangular duct _____ X _____

% H₂O 13.7 MW 29.54Mag. Box # 375Duct Static Pressure -0.52 inches H₂OTemp. Unit # 5562Standard Conditions 60 °F & 29.92 "HgPitot Tube # 5294Pitot Tube Coefficient 0.78

Trav. Pt.	Ins. From Edge	Northeast			Northwest			Southwest			Southeast		
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	5.2	215	0.60	45.1	220	0.60	45.3	210	0.36	34.8	210	0.50	41.1
2	17.6	215	0.68	48.1	215	0.70	48.8	215	0.48	40.4	210	0.50	41.1
3	35.5	215	0.66	47.3	215	0.64	46.6	215	0.46	39.5	220	0.48	40.5
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RESULTS:

Average Velocity (V_d) 43.2 FPS Average duct temp. 215 °F, press. 29.91 "HgVolume Flow Rate at 215 °F & 29.91 "Hg (Q_d) 203645 ACFMVolume Flow Rate at standard conditions (Q_{std(wet)}) 156940 SCFMVolume Flow Rate at standard conditions (Q_{std(dry)}) 135406 SDCFM


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VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')
DATA:

CLIENT: Lonestar

UNIT: Main Stack

DATE: 8/22/83

TIME: 1514 - 1635

RUN #: 3

Description: Ports: two 3-inch female ports, properly located, approximately 8 diameters after and 2 diameters before disturbances in flow.

Duct Diameter 120 inches Area 78.54 ft²Rectangular duct X % H₂O 13.0 MW 29.64Mag. Box # 375Duct Static Pressure -0.52 inches H₂OTemp. Unit # 5562Standard Conditions 60 °F & 29.92 "HgPitot Tube # 5293Pitot Tube Coefficient 0.80

Trav. Pt.	Ins. From Edge	Southeast			Southwest			Northwest			Northeast		
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	5.2	200	0.42	38.2	205	0.40	37.5	210	0.66	48.3	210	0.62	46.8
2	17.6	205	0.48	41.0	205	0.48	41.0	210	0.76	51.8	210	0.70	49.7
3	35.3	205	0.46	40.2	205	0.44	39.3	210	0.64	47.6	210	0.62	46.8
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RESULTS:
Average Velocity (V_d) 44.0 FPS Average duct temp. 207 °F, press. 29.91 "HgVolume Flow Rate at 207 °F & 29.91 "Hg (Q_d) 207449 ACFMVolume Flow Rate at standard conditions (Q_{std(wet)}) 161669 SCFMVolume Flow Rate at standard conditions (Q_{std(dry)}) 140577 SDCFM



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VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')

DATA:

CLIENT: Lonestar

UNIT: Main Stack

DATE: 8/23/83

TIME: 0826 - 0955

RUN #: 1

Description: Ports: two 3-inch female ports, properly located, approximately 8 diameters after and 2 diameters before disturbances in flow.

Duct Diameter 120 inches Area 78.54 ft²

Rectangular duct X

% H₂O 10.7 MW 29.50

Mag. Box # 375

Duct Static Pressure -0.52 inches H₂O

Temp. Unit # 5562

Standard Conditions 60 °F & 29.92 "Hg

Pitot Tube # 5294

Pitot Tube Coefficient 0.78

Trav. Pt.	Ins. From Edge	Northeast			Northwest			Southwest			Southeast		
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	5.2	290	0.66	50.0	285	0.84	56.2	275	0.56	45.6	270	0.58	46.2
2	17.6	290	0.84	56.4	285	0.96	60.1	280	0.70	51.1	280	0.76	53.3
3	35.5	295	0.80	55.2	285	0.92	58.8	285	0.72	52.0	275	0.72	51.7
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RESULTS:

Average Velocity (V_d) 53.0 FPS Average duct temp. 283 °F, press. 29.86 "Hg

Volume Flow Rate at 283 °F & 29.86 "Hg (Q_d) 249973 ACFM

Volume Flow Rate at standard conditions (Q_{std(wet)}) 174631 SCFM

Volume Flow Rate at standard conditions (Q_{std(dry)}) 155939 SDCFM



VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')

DATA:

CLIENT: Lonestar

UNIT: Main Stack

DATE: 8/23/83

TIME: 1030 - 1153

RUN #: 2

Description: Ports: two 3-inch female ports, properly located, approximately 8 diameters after and 2 diameters before disturbances in flow.

Duct Diameter 120 inches Area 78.54 ft²

Rectangular duct X

% H₂O 11.6 MW 29.69

Mag. Box # 375

Duct Static Pressure -0.52 inches H₂O

Temp. Unit # 5562

Standard Conditions 60 °F & 29.92 "Hg

Pitot Tube # 5293

Pitot Tube Coefficient 0.80

Trav. Pt.	Ins. From Edge	Southeast			Southwest			Northwest			Northeast		
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	5.2	275	0.62	49.0	275	0.58	47.4	275	0.80	55.7	280	0.48	43.3
2	17.6	280	0.76	54.5	275	0.76	54.3	280	0.94	60.6	275	0.54	45.8
3	35.5	275	0.76	54.3	275	0.76	54.3	275	0.90	59.1	275	0.90	59.1
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RESULTS:

Average Velocity (V_d) 53.1 FPS Average duct temp. 276 °F, press. 29.86 "Hg

Volume Flow Rate at 276 °F & 29.86 "Hg (Q_d) 250205 ACFM

Volume Flow Rate at standard conditions (Q_{std(wet)}) 176376 SCFM

Volume Flow Rate at standard conditions (Q_{std(dry)}) 155971 SDCFM



VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')

DATA:

CLIENT: Lonestar

UNIT: Main Stack

DATE: 8/23/83

TIME: 1305 - 1430

RUN #: 3

Description: Ports: two 3-inch female ports, properly located, approximately 8 diameters after and 2 diameters before disturbances in flow.

Duct Diameter 120 inches Area 78.58 ft²

Rectangular duct X

% H₂O 13.7 MW 29.71

Mag. Box # 375

Duct Static Pressure -0.52 inches H₂O

Temp. Unit # 5562

Standard Conditions 60 °F & 29.92 "Hg

Pitot Tube # 5294

Pitot Tube Coefficient 0.78

Trav. Pt.	Ins. From Edge	Northeast			Northwest			Southwest			Southeast		
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	5.2	275	0.46	41.2	285	0.50	43.2	290	0.36	36.8	300	0.40	39.0
2	17.6	280	0.58	46.4	280	0.64	48.7	290	0.44	40.7	300	0.46	41.9
3	35.5	275	0.60	47.0	280	0.60	47.2	290	0.46	41.6	290	0.46	41.6
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RESULTS:

Average Velocity (V_d) 42.9FPS Average duct temp. 286 °F, press. 29.86 "Hg

Volume Flow Rate at 286 °F & 29.86 "Hg (Q_d) 202296 ACFM

Volume Flow Rate at standard conditions (Q_{std(wet)}) 140693 SCFM

Volume Flow Rate at standard conditions (Q_{std(dry)}) 121452 SDCFM

PARTICULATE EMISSIONS



PARTICULATE EMISSIONS

REF: EPA, Code of Federal Regulations, Title 40, Part 60, Appendix A,
Method 5, 1981
: South Coast AQMD, Source Testing Manual, Los Angeles, CA, April, 1981
: State of California, Air Resources Board, Draft Stationary Source Test
Methods, Method 1-5, June, 1979

SAMPLING PROCEDURE:

The apparatus consisted of a nozzle, heater wrapped probe and heated filter holder (see data sheets for type of nozzle, probe and filter holder). A series of impinger-absorbers (see data sheet for type and contents) were connected in tandem and immersed in an ice bath. The absorption train was followed by a gas drying tube containing indicating silica gel, a diaphragm pump, dry test meter and a calibrated restriction orifice fitted with a magnehelic differential pressure gauge.

The computer was used in selection of suitable sampling points, nozzle size, and orifice constant. The apparatus was leak tested, the probe heaters were brought to temperature and the nozzle was positioned at the first sampling point. The pump was immediately started and adjusted to obtain the isokinetic sampling rate.

Duct conditions were monitored throughout the sampling period with a type "S" pitot tube and a thermocouple simultaneously positioned at the traverse point. Conditions at the sampling apparatus and metering device were constantly monitored and regularly recorded on the data sheet. Isokinetic sampling rate in terms of orifice differential pressure was calculated by computer for each set of duct and sampling apparatus conditions. Data was relayed between the computer and site by radio.

On completion of sampling from all usable traverse points, the apparatus was removed, leak-checked, sealed from possible contamination and transported to the laboratory. Replicate samples were taken as indicated by the data sheets.

Concurrent with each particulate sampling, an integrated gas sample was withdrawn from the summation of the traverse points through the train and collected at the outlet of the meter into a sample bag.

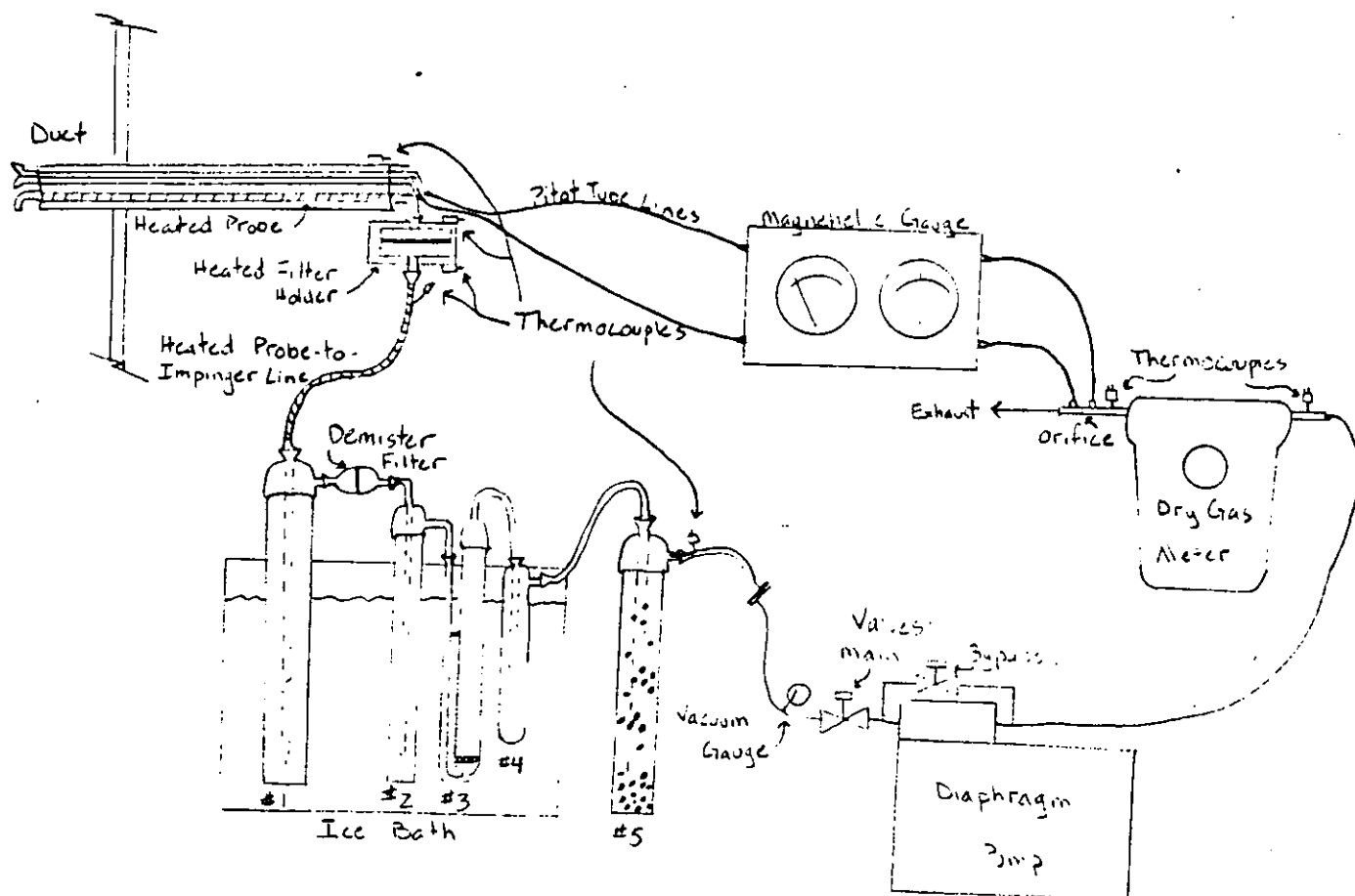
ANALYTICAL PROCEDURE:

The weight or volume increase of the impingers was measured and recorded for calculation of percent water.

The contents of the sample bladder were analyzed by Orsat for fixed gas and molecular weight determination.



METHOD 5/8 SAMPLING TRAIN



<u>Impinger #</u>	<u>Contents</u>
#1	100 mls 80 percent IPA
#2	100 mls 6% H ₂ O ₂
#3	100 mls 6% H ₂ O ₂
#4	Empty
#5	250 grms Silica Gel (8 mesh)



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PARTICULATE EMISSIONS

Calculations (cont)

Equations:

Duct gas velocity at any traverse point (see Velocity & Volume Flow Rate):

$$v_d = 85.49 * C_p * \sqrt{\frac{T_d * \Delta P}{P_d * MW}}$$

Isokinetic sampling rate at any traverse point:

$$Q_m = Q_n * \frac{P_d * T_m}{P_m * T_d} * (1 - \% H_2O/100)$$

where $Q_n = 60 * v_n * A_n$ and for isokinetic sampling, $v_n = v_d$

$$\Delta H = Q_o^2 * \frac{P_b}{k_m^2 * T_m} * \frac{[MW - (0.18 * \% H_2O)]}{(1 - \% H_2O/100)}$$

where $Q_o = 1.23 * Q_m - 0.23 * Q_m^2$ (for non-linear orifice)

Percent of isokinetic sampling:

$$I = T_d * \frac{[0.00267 * W + V_m/T_m(\text{avg}) * (P_{\text{bar}} + \Delta H(\text{avg})/13.6)]}{t * v_d(\text{avg}) * P_d * A_n * 60} * 100$$

Sampled Volume:

$$V_m(\text{std}) = V_m * \frac{T_{\text{std}}}{T_m(\text{avg})} * \frac{(P_{\text{bar}} + \Delta H(\text{avg})/13.6)}{P_{\text{std}}}$$

Particulate Concentration:

$$C_o = \frac{0.0154 * M}{V_m(\text{std})}$$

Emission Rate:

$$E.R. = 8.58 * 10^{-3} * Q_{\text{std}}(\text{dry}) * C_o$$



PARTICULATE EMISSIONS

Analytical Procedure (cont)

The filter section was recovered, placed in a 105°C drying oven and desiccated to constant weight. The weight increase was determined from the tare weight and recorded on the individual data sheet.

Sample was recovered from the nozzle and probe sections with distilled water and/or acetone and a rubber policeman or nylon bristle brush. A tared dish was used for subsequent evaporation, desiccation and weight determination.

If analysis of the condensable fraction of the particulate ("impinger catch" or "back half") was required, an aliquot of the impinger liquid was poured into a tared dish. The liquid was evaporated to dryness and the residue was desiccated to a constant weight.

Aliquots of blank impinger and/or probe wash reagents were evaporated to dryness in tared dishes. The residue was desiccated and weighed for subtraction of the blank residue from the total probe wash or condensables residue.

An estimate of sampling accuracy was performed by calculation of percent isokinetic rate over the entire sampling period.

CALCULATIONS:

Performed by computer based on the following equations:

Symbol Identification:

Subscripts d, m and n denote duct, dry gas meter and nozzle respectively
Subscripts std, bar and avg denote standard, barometric and average

A = area, square feet

C_o = particulate concentration, grains/SCCF

C_p = pitot tube correction, unitless

E.R. = emission rate of particulate, lb/hr

ΔH = orifice differential pressure, inches H₂O

I = percent of isokinetic sampling

k_m = orifice constant, unitless

M = mass of particulate collected, milligrams

MW = wet molecular weight of duct gas, g/mole

P = absolute pressure, inches Hg

Δp = velocity pressure head, inches H₂O

Q = volume flow rate, CFM

Q_o = parameter of volume flow rate through the orifice

T = absolute temperature, °R

t = time of sampling period, minutes

V = gas volume, CF

v = velocity, feet/second

W = water collected, grams

% H₂O = duct gas water content, percent volume



PARTICULATE EMISSIONS
TEST MONITOR DATA

Date 8/22/83 Run 1
 Client Lonestar
 Unit Main Stack
 Ambient Temp. °F
 Press. bar 29.95 in. Hg
 Press. static -0.52 in. H₂O
 Press. duct 29.91 in. Hg
 Assumed MW 27.70 %H₂O 10.5
 Sample Train Temp.:
 Probe 250,250,260 °F
 Filter 260,250,235 °F
 Sample Line 245, °F ²⁴⁰₂₃₅
 Post-Test Leak Check:
 Leak Rate 0.010 CFM
 @ 5 in. Hg Vac.
 Nozzle & Probe Mat. SS
 Filter Holder Mat. SS
 Filter # 31
 Nozzle # 6G i.d. 6.0 mm
 Pitot # 5293 C_p 0.80
 Temp. Unit # 5562
 Mag. # 375 Meter # 631 @ 1.016
 Orifice km 0.5

		Duct Data			Meter Data			
Trav. Point	Time	Temp. °F	Head Δ p	Velocity ft/sec	Vacuum "Hg	Temp. °F	Orifice ΔH, "H2O	Volume CF
Southeast Port								
3	1043	220	0.56	45.0		95	2.56	227.90
2	1048	220	0.52	43.3	1	95	2.40	
1	1053	220	0.46	40.8		95	2.16	
	1058	Stop to	change	ports				236.10
Southwest Port								
3	1109	220	0.54	44.2		90	2.46	
2	1114	220	0.56	45.0	2	90	2.54	
1	1119	220	0.46	40.8		95	2.16	
	1124	Stop to	change	ports, disconnect	and leak	check		244.65
Northwest Port								
3	1139	220	0.80	53.8		85	3.46	244.80
2	1144	225	0.84	55.3	2	85	3.59	
1	1149	225	0.76	52.6		85	3.29	
	1154	Stop to	change	ports				255.80
Northeast Port								
3	1200	220	0.74	51.7		70	3.16	
2	1205	220	0.84	55.1		85	3.62	
	1210	Power failure, test stopped						262.35
1	1227	215	0.64	47.1		65	2.70	
	1232	End of test						266.70



PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Lonestar Main Stack

Run: 1

Date: 8/22/83

Time: 1043 - 1232

Absorber Type	Contents	Final	Tare	Net gms H2O
Lg. Greenburg	80% IPA	604.4	547.1	57.3
Sm. Greenburg	6% Peroxide	432.8	429.0	3.8
Gas Absorber	6% Peroxide	261.1	264.5	- 3.4
liquid trap	empty	148.3	99.6	48.7
	silica gel	734.8	699.4	35.4
TOTAL				141.8

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle Wash	66.7617	66.7677	6.0	0.0025
200/ Condensables 200	84.6801	84.6729	7.2	0.0029
Filter #31	0.4358	0.4172	8.6	0.0035
Acetone blank 55mls			<0.1	<0.0001
Gas Composition:		TOTAL	21.8	0.0089

CO₂ 18.8 % volume (dry)
O₂ 10.4 % volume (dry)
CO - % volume (dry)
N₂ 70.8 % volume (dry)
H₂O 14.8 % volume

MW (wet) 29.43
Excess Air %
Sampled Volume 37.68 SDCF
Isokinetic Rate 110 %

Particulate Concentration:

Co 0.0089 grains/SDCF @ 60 °F and 29.92 "Hg
C grains/SDCF @

Emission Rate:

E.R. 11.21 lbs/hr @ Qstd(dry) 146830 SDCFM

PARTICULATE EMISSIONS
TEST MONITOR DATA

Orifice km 0.5

[illegible]



PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Main Stack
Date: 8/22/83

Run: 2
Time: 1310 - 1433

Absorber Type	Contents	Final	Tare	Net gms H2O
Lg. Greenburg	80% IPA	565.90	526.6	39.3
Sm. Greenburg	6% Peroxide	467.4	432.3	35.1
Gas Absorber	6% Peroxide	307.8	279.6	28.2
liquid trap	empty	100.0	98.7	1.3
	silica gel	718.6	703.0	15.6
TOTAL				119.5

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle Wash	53.3066	53.3032	3.4	0.0015
200/ Condensables 200	64.9487	64.9420	6.7	0.0030
Filter #32	0.4237	0.4191	4.6	0.0020
Acetone blank 67mls			<0.1	<0.0001
TOTAL			14.7	0.0065

Gas Composition:

CO₂ 18.5 % volume (dry)
O₂ 10.4 % volume (dry)
CO - % volume (dry)
N₂ 71.1 % volume (dry)
H₂O 13.7 % volume

TOTAL

MW (wet) 29.54
Excess Air %
Sampled Volume 34.75 SDCF
Isokinetic Rate 110 %

Particulate Concentration:

Co 0.0065 grains/SDCF @ 60 °F and 29.92 "Hg
C grains/SDCF @

Emission Rate:

E.R. 7.55 lbs/hr @ Qstd(dry) 135406 SDCFM



PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Main Stack
Date: 8/22/83

Run: 3
Time: 1514 - 1635

Absorber Type	Contents	Final	Tare	Net gms H2O
Lg. Greenburg	80% IPA	589.1	547.5	41.6
Sm. Greenburg	6% Peroxide	445.6	426.2	19.4
Gas Absorber	6% Peroxide	263.2	243.6	19.6
liquid trap	empty	118.5	100.0	18.5
	silica gel	731.9	718.6	13.3
TOTAL				112.4

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle Wash	62.5547	62.5466	8.1	0.0036
200/ Condensables 200	68.5172	68.5131	4.1	0.0018
Filter #33	0.4218	0.4187	3.1	0.0014
Acetone Blank 48mls			<0.1	<0.0001
TOTAL			15.3	0.0068

Gas Composition:

CO₂ 18.5 % volume (dry)
O₂ 10.6 % volume (dry)
CO - % volume (dry)
N₂ 70.9 % volume (dry)
H₂O 13.0 % volume

MW (wet) 29.64
Excess Air %
Sampled Volume 34.64 SDCF
Isokinetic Rate 106 %

Particulate Concentration:

Co 0.0068 grains/SDCF @ 60 °F and 29.92 "Hg
C grains/SDCF @ grains/SDCF

Emission Rate:

E.R. 8.20 lbs/hr @ Qstd(dry) 140577 SDCFM

PARTICULATE EMISSIONS
TEST MONITOR DATA

Sample Train Temp.:
Probe 250, 270, 250 °F
Filter 260, 250, 260 °F
Sample Line 240, °F 230
Post-Test Leak Check: 260
Leak Rate 0.012 CFM
@ 6 in. Hg Vac.

Nozzle & Probe Mat. SS
Filter Holder Mat. SS
Filter # 45
Nozzle # 6A i.d. 6.0 mm
Pitot # 5294 Cp 0.78
Temp. Unit # 5562
Mag. # 375 Meter # 631 @ 1.016
Orifice km 0.5

[illegible]



PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Main Stack

Run: 1

Date: 8/23/83

Time: 0826 - 0955

Absorber Type	Contents	Final	Tare	Net	H2O
Lg. Greenburg	80% IPA	539.3	531.8	7.5	
Sm. Greenburg	6% Peroxide	454.9	431.8	23.1	
Gas Absorber	6% Peroxide	251.4	254.9	- 3.5	
liquid trap	empty	135.8	99.2	36.6	
	silica gel	717.1	694.0	23.1	
TOTAL				86.8	

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle Wash	66.4158	66.4108	5.0	0.0023
200/ Condensables 200	81.9232	81.8541	69.1	0.0318
Filter #45	0.4218	0.4203	1.5	0.0007
Acetone blank 54mls			<0.1	<0.0001
Gas Composition:		TOTAL	75.6	0.0348

CO₂ 15.0 % volume (dry)
O₂ 12.0 % volume (dry)
CO - % volume (dry)
N₂ 73.0 % volume (dry)
H₂O 10.7 % volume

MW (wet) 29.50
Excess Air %
Sampled Volume 33.48 SDCF
Isokinetic Rate 92.4 %

Particulate Concentration:

Co 0.0348 grains/SDCF @ 60 °F and 29.92 "Hg
C grains/SDCF @

Emission Rate:

E.R. 46.56 lbs/hr @ Qstd(dry) 155940 SDCFM

[illegible]



PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Main Stack

Run: 2

Date: 8/23/83

Time: 1030 - 1153

Absorber Type	Contents	Final	Tare	Net	H2O
Lg. Greenburg	80% IPA	574.2	551.2		23.0
Sm Greenburg	6% Peroxide	450.8	426.5		24.3
Gas Absorber	6% Peroxide	251.9	241.8		10.1
liquid trap	empty	118.9	100.2		18.7
	silica gel	738.5	716.1		22.4
TOTAL					98.5

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle Wash	65.0469	65.0445	2.4	0.0011
200/ Condensables 200	68.8862	68.8337	52.5	0.0232
Filter #47	0.4133	0.4132	0.1	0.0001
49.2 mls Acetone blank			<0.1	<0.0001
TOTAL			55	0.0243

Gas Composition:

CO₂ 17.5 % volume (dry)
O₂ 10.6 % volume (dry)
CO - % volume (dry)
N₂ - % volume (dry)
H₂O 11.6 % volume

TOTAL

MW (wet) 29.69
Excess Air %
Sampled Volume 34.81 SDCF
Isokinetic Rate 96.0 %

Particulate Concentration:

Co 0.0243 grains/SDCF @ 60 °F and 29.92 "Hg
C grains/SDCF @

Emission Rate:

E.R. 32.52 lbs/hr @ Qstd(dry) 155971 SDCFM

PARTICULATE EMISSIONS
TEST MONITOR DATA

Sample Train Temp.:	Nozzle & Probe Mat.	<u>SS</u>
Probe <u>250, 240, 250</u> °F	Filter Holder Mat.	<u>SS</u>
Filter <u>245, 260, 269</u> °F	Filter # <u>44</u>	
Sample Line <u>240</u> , °F ²³⁰	Nozzle # <u>6A</u> 1.d. <u>6.0</u> mm	
Post-Test Leak Check:	Pitot # <u>5294</u> Cp <u>0.78</u>	
Leak Rate <u>0.005</u> CFM	Temp. Unit # <u>5562</u>	
@ 8 in. Hg Vac.	Mag. # <u>375</u> Meter # <u>631</u> @ 1.016	
	Orifice km <u>0.5</u>	

[illegible]



PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Main Stack
Date: 8/23/83

Run: 3
Time: 1305 - 1430

Absorber Type	Contents	Final	Tare	Net gms. H ₂ O
Lg. Greenburg	80% IPA	566.7	529.8	36.9
Sm. Greenburg	6 % Peroxide	470.0	430.4	39.6
Gas Absorber	6 % Peroxide	264.8	255.0	9.8
liquid trap	empty	101.8	99.1	2.7
	silica gel	705.4	695.3	10.1
TOTAL				99.1

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle Wash	63.7717	63.7702	1.5	0.0008
Condensables 200/200	68.6964	68.6166	79.8	0.0425
Filter #44	0.4225	0.4182	4.3	0.0023
Acetone blank 63mls			<0.1	<0.0001
TOTAL			85.6	0.0456

Gas Composition:

CO₂ 20.0 % volume (dry)
O₂ 9.0 % volume (dry)
CO - % volume (dry)
N₂ 69.5 % volume (dry)
H₂O 13.7 % volume

TOTAL

MW (wet) 29.71
Excess Air %
Sampled Volume 28.92 SDCF
Isokinetic Rate 102.5 %

Particulate Concentration:

Co 0.0456 grains/SDCF @ 60 °F and 29.92 "Hg
C grains/SDCF @

Emission Rate:

E.R. 47.52 lbs/hr @ Qstd(dry) 121452 SDCFM

CONSTANT MONITORING



CONSTANT MONITORING

REF: Bay Area AQMD, Manual of Procedures, San Francisco, CA, Methods ST-5, ST-6, ST-13A, ST-14, ST-19A, January, 1982
: State of California, Air Resources Board, Draft Stationary Source Test Methods, Method 1-100, June, 1979

METHOD SUMMARY:

A representative sample of duct gas was extracted through a probe, filter, condenser and sample line by a pump. The sample was then pumped into a sampling manifold for distribution to one or more sample analyzers. The analyzers output a continuous analog recording of the concentrations of the analyzed gases in the sample. All analyzers were calibrated with EPA Protocol gases (traceable to National Bureau of Standards SRMs) or with recently analyzed gases (analysis by EPA Reference Methods).

SAMPLING SYSTEM:

A Pyrex glass or stainless steel probe with a Pyrex wool or glass fibre mat filter was positioned in the duct. The end of the probe was located at a point of average duct flow and average pollutant concentrations. The probe was connected with a short (about 2 feet) Teflon line to a sample conditioning train. The conditioning train included three glass knockout traps connected in series with Teflon lines and immersed in an ice bath. The train was connected with a Teflon line ($\frac{1}{4}$ inch o.d.) to the pneumatic delivery system which was housed in the monitoring van.

PNEUMATIC DELIVERY SYSTEM:

The Teflon sample line delivered sample gas into a small glass knockout trap, then through an in-line Balston filter and a Hoke four-way selector valve to the Teflon-lined diaphragm sample pump (see accompanying diagram). The flow rate of the sample gas was regulated with main and bypass-flow needle valves and was read on the main flow meter (typical setting 10 SCFH). A 10 PSI pressure-relief valve kept the entire system pressure at a safe level. The manifold pressure was regulated with an exhaust needle valve and was read on the pressure gauge (typical setting 1 PSI). The sample in the manifold was delivered through needle valves and flow meters to the various analyzers.

LEAK CHECK PROCEDURE:

The sampling system was checked for leaks by plugging the end of the probe. The exhaust needle valve was closed and the entire sample flow was directed through one analyzer flow meter (range 0-1.0 SCFH). The bypass valve was closed until the vacuum gauge showed at least 15 inches Hg vacuum. The leak rate was observed at the analyzer flow meter (maximum allowable 2% of total sample flow). The system was checked for leaks before and after sampling.

**CHEMECOLOGY
CORPORATION****CONSTANT MONITORING****CALIBRATION PROCEDURE:**

Each analyzer was calibrated before and after each sample run. The Hoke four-way selector valve was used to direct the flow of the various calibration gases into the sample manifold. Each analyzer was calibrated with a zero gas (typically, ambient air or zero grade Nitrogen) and with a span gas (typical span gas concentration 60 to 90 percent of analyzer full scale and/or similar to expected sample concentration). All zero and span checks were recorded and noted on the recorder strip charts.

STRIP CHART DATA REDUCTION:

The analog recordings were averaged over time periods as shown on the data pages (typically 5 minutes, 15 minutes or 30 minutes). The data for each averaging period was digitized and recorded as average percent of full scale. These sample readings were then compared with the zero and span gas readings for calculation of the average concentration for each averaging period.

Any drift^{1/} of the zero and span readings from the beginning to the end of a sampling period was corrected by calculating apparent zero and span readings for the midpoint of each averaging period. The sample average concentrations were then calculated from the sample readings and the apparent zero and span readings.

^{1/}
Drift is defined as any change in zero or span readings of more than one percent full scale from the beginning to the end of a sampling period.



CONSTANT MONITORING (cont)

CALCULATIONS (Strip Chart Analysis):

Calculations were performed based on the following equations:

Symbol Identification

Subscripts i and f indicate initial and final respectively (beginning and end of sampling period)

z = zero reading, % full scale

s = span reading, % full scale

t = averaging time period numbered 1 to n

n = number of t's in the sampling period

Δz = rate of change of zero reading, % full scale/time interval

Δs = rate of change of span reading, % full scale/time interval

R_t = average sample reading over time t, % full scale

z_t = corrected (apparent) zero reading for midpoint of t, % full scale

s_t = corrected (apparent) span reading for midpoint of t, % full scale

C_s = span gas concentration, ppm or % vol. (as shown on data sheet)

C_t = average sample concentration for time t, ppm or % vol. (as indicated)

Equations:

Apparent Zero:

$$\Delta z = (z_f - z_i) / n$$

For each t from 1 to n,

$$z_t = \Delta z / 2 + \Delta z * (t - 1) + z_i$$

Apparent Span:

$$\Delta s = (s_f - s_i) / n$$

For each t from 1 to n,

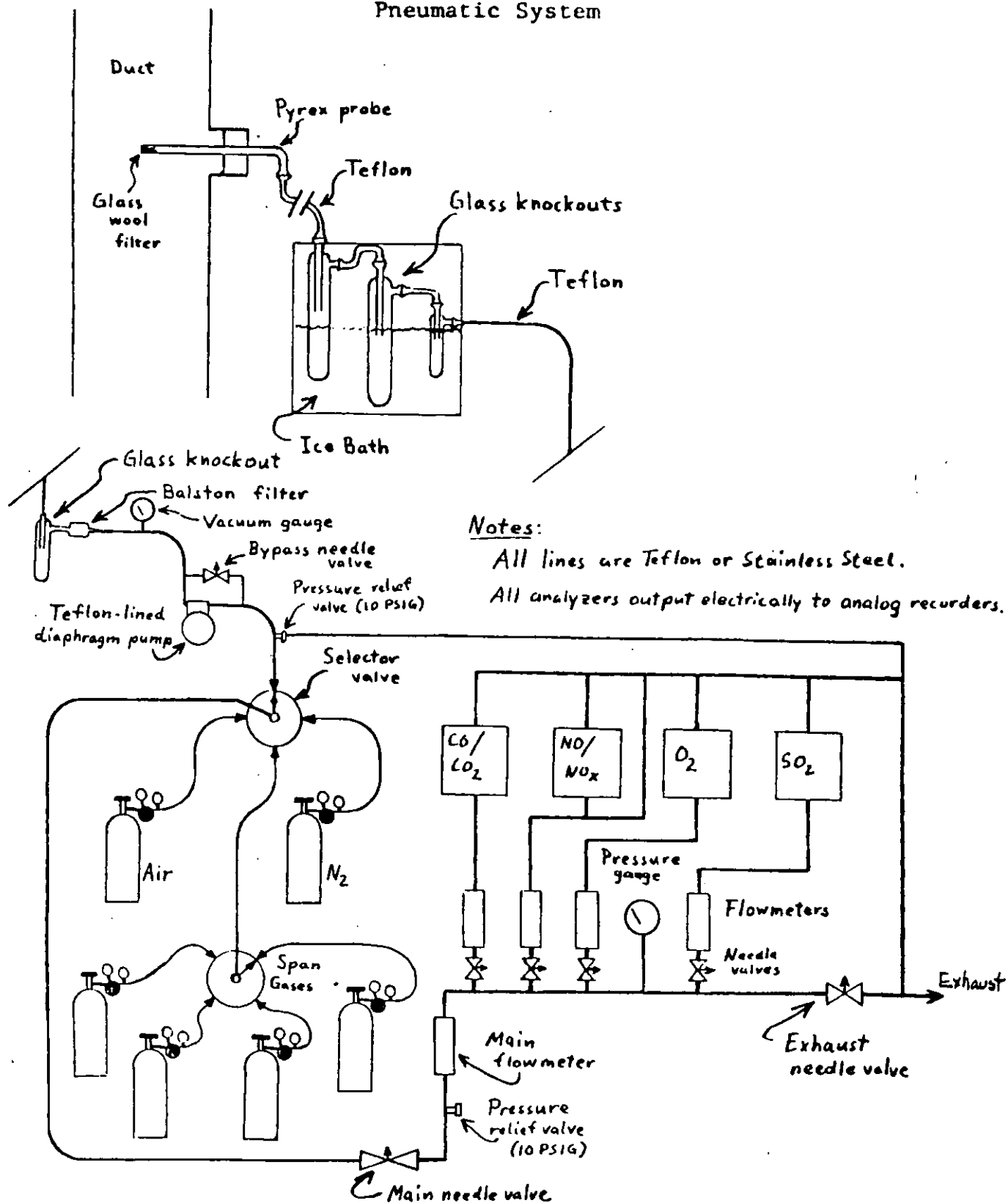
$$s_t = \Delta s / 2 + \Delta s * (t - 1) + s_i$$

Average Sample Concentration

$$C_t = \frac{R_t - z_t}{s_t - z_t} * C_s$$



CONSTANT MONITOR
Pneumatic System



5/11/82 KJC



CONSTANT MONITORING

ANALYZERS:

Taylor Servomex OA250 or OA580 Oxygen Analyzer

The Taylor paramagnetic analyzer is used to measure the percent dry volume of oxygen in the sample gas. This analyzer contains a quartz-glass "dumb-bell" that is filled with nitrogen and suspended in a non-uniform magnetic field. The spheres at the ends of the dumb-bell are repelled from the strongest part of the field by their diamagnetic property. The dumb-bell therefore rotates to a position where the repellent force and the torque-resistance of the suspension are in equilibrium.

The sample gas flows into a sample cell which encases the dumb-bell. The paramagnetism of any oxygen in the sample gas reduces the intensity of the field and therefore alters the position of the dumb-bell. A small mirror at the center of the dumb-bell reflects a beam of light onto twin photocells (see schematic diagram). The output of the photocells is amplified and fed back to a coil around the dumb-bell. The current required to keep the dumb-bell at the zero position is a direct measure of the magnetic force and is therefore a measure of the oxygen content of the sample gas.

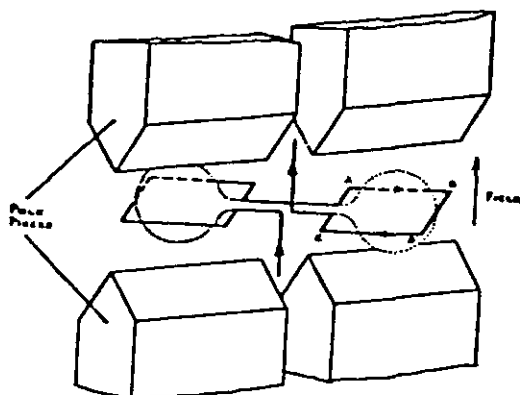


Fig. 1. Taylor Servomex Oxygen Cell
— Schematic using Munday's
principles

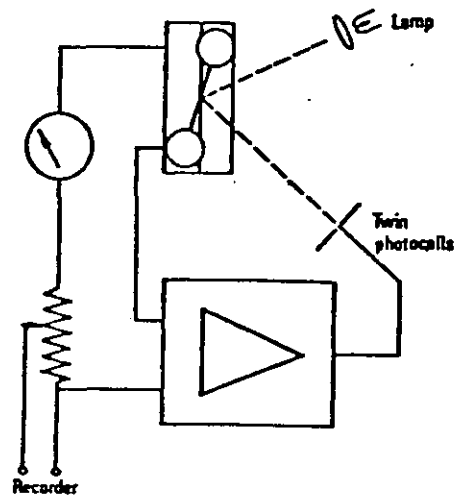


Fig. 2. Taylor Servomex Oxygen
Analyser — Schematic



CONSTANT MONITORING

ANALYZERS:

Monitor Labs 8430 Nitrogen Oxides Analyzer

The Monitor Labs chemiluminescent analyzer is used to measure parts per million dry volume of Nitrogen Oxides in the sample gas. The analyzer measures the concentration of NO_x by converting NO_x to NO and then measuring the light emitted by the reaction of NO with ozone.

The sample gas is drawn into the analyzer by a vacuum pump which partially evacuates the reaction chamber. The sample flows through a NO₂-to-NO converter^{1/} for NO_x analysis or may bypass the converter for NO analysis. The sample then flows through a temperature controlled critical orifice into the partially evacuated reaction chamber.

Ambient air is also drawn into the analyzer as an ozone carrier. The air flows through a desiccant cartridge for drying, then through an ozone generator which converts some of the oxygen in the air to ozone. The ozonated air then flows through a temperature-controlled critical orifice into the reaction chamber.

The sample gas and the ozonated air are mixed in the reaction chamber, where the following reaction takes place:



The intensity of the chemiluminescence is proportional to the concentration of NO in the reaction chamber. The light emitted by this chemiluminescent reaction shines through a window in the chamber onto a photomultiplier tube (PMT). A spinning light chopper wheel between the reaction chamber and the PMT allows the PMT output with no light to be compared electronically with the PMT output with light. The signal is processed electronically and output for recording of the concentration of NO (or NO_x if the converter is used).

^{1/} Either of two types of converter may be used—a 300°C Molybdenum-catalyst converter or a 900°C stainless steel converter.



CONSTANT MONITORING

ANALYZERS:

DuPont Series 400 Sulfur Dioxide Analyzer

The DuPont 400 analyzer is used to measure parts per million dry volume of Sulfur Dioxide in the sample gas. The analyzer measures the concentration of SO₂ by measuring its absorption of ultraviolet light.

The sample gas flows through a tubular cell 50.8 cm long. An ultraviolet lamp shines a light beam through the sample cell to a beam splitter at the other end. The split beam shines through optical filters onto phototubes which measure the beam intensity at the filtered wavelengths (see diagram). The reference phototube measures at a wavelength (578 nm) that is not absorbed by SO₂. The measuring phototube measures at a wavelength (280 nm) that is strongly absorbed by an SO₂ in the sample. Each phototube conducts a current to the logarithmic amplifier that is proportional to the light intensity striking the phototube. The signals are linearized and compared electronically to determine the absorption of 280 nm wavelength light and therefore to determine the concentration of SO₂ in the sample gas.

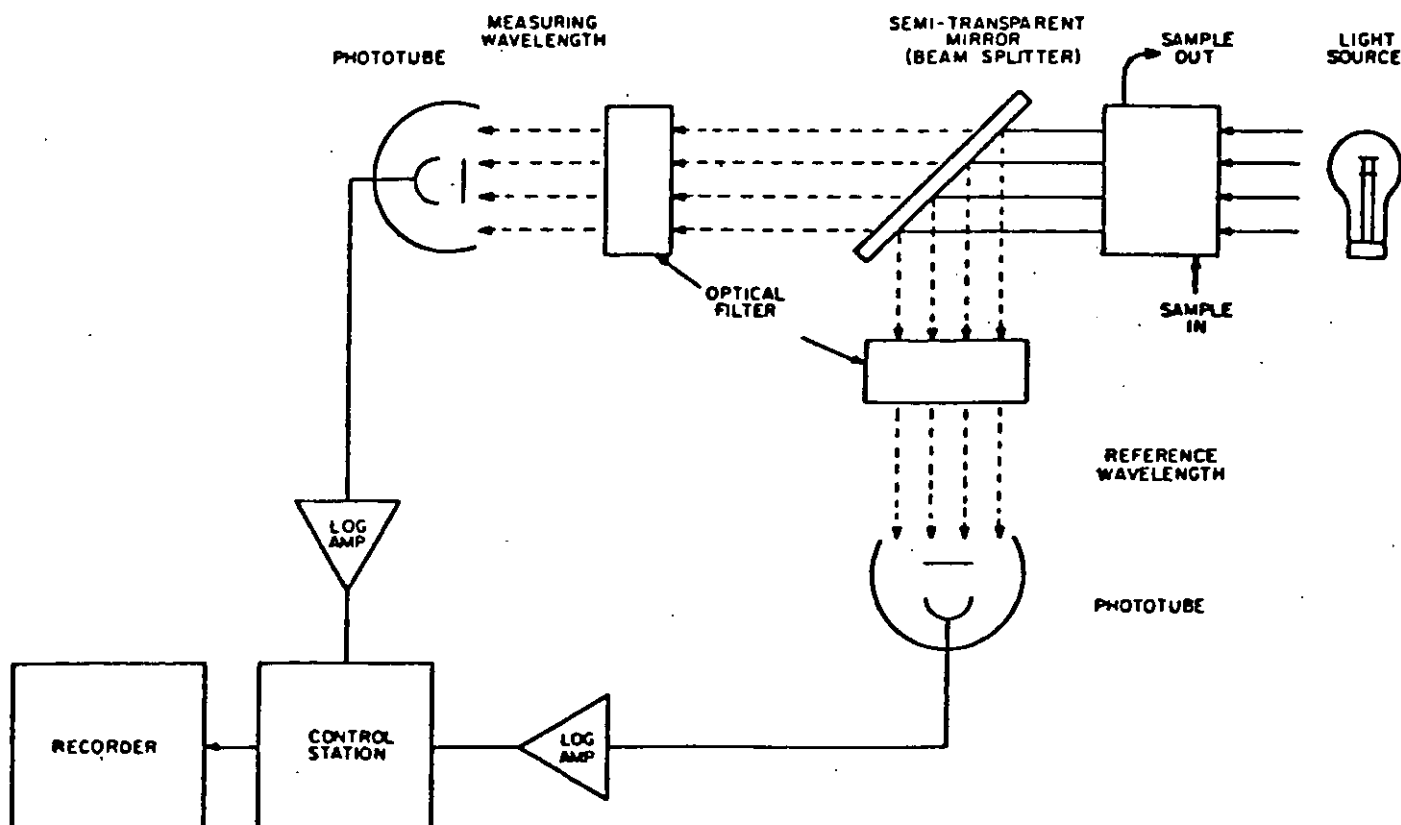


Figure 1. Analyzer Block Diagram



CONSTANT MONITORING

DATA & RESULTS

Client: Lonestar, Davenport, CA

Unit: Main Stack

Date: 8/22/83

Analyzed Gas O₂

Analyzer Range 0 to 25%

Recorder Range 0 to 25%

Zero Gas : Scott #CAL 4516 (span gas for NO_x and SO₂)

Span Gas: 21% O₂- Ambient Air

Time	% FULL SCALE						Average Concentration % O ₂	
	Initial		Final		Apparent			Sample Reading
	Zero	Span	Zero	Span	Zero	Span		
1125	0.0	84.0						
1131 to 1203					0.0	84.0	42.1	10.5
1210			0.0	84.0				
1325	0.0	84.0						
1333 to 1414					0.0	84.1	41.3	10.3
1420			0.0	84.2				
1545	0.0	84.0						
1550 to 1637					0.2	84.1	41.8	10.4
1640			0.4	84.2				



CONSTANT MONITORING

DATA & RESULTS

Client: Lonestar, Davenport, CA

Analyzed Gas NOx

Unit: Main Stack

Analyzer Range 0 to 500 ppm

Date: 8/22/83

Recorder Range 0 to 500 ppm

Zero Gas : Ambient Air

Span Gas: 309.9 ppm NOx with SO₂ in N₂ - Scott #CAL 4516

Time	% FULL SCALE						Average Concentration ppm NOx	
	Initial		Final		Apparent			Sample Reading
	Zero	Span	Zero	Span	Zero	Span		
1125	0.0	62.0						
1131 to 1203					0.0	62.4	41.0	204
1210			0.0	62.8				
1325	0.0	62.0						
1333 to 1414					0.0	62.5	53.5	265
1420			0.0	63.0				
1545	0.1	61.9						
1550 to 1637					0.1	60.6	35.5	182
1640			0.1	59.3				



CONSTANT MONITORING

DATA & RESULTS

Client: Lonestar, Davenport, CA

Unit: Main Stack

Date: 8/22/83

Zero Gas : Ambient Air

Span Gas: 522.4 ppm SO₂, with NOx in N₂ - Scott #CAL 4516

Analyzed Gas

SO₂

Analyzer Range

0 to 1000 ppm

Recorder Range

0 to 1000 ppm

(-50 to 950 ppm)

Time	% FULL SCALE						Average Concentration ppm SO ₂	
	Initial		Final		Apparent			Sample Reading
	Zero	Span	Zero	Span	Zero	Span		
1125	0.0	52.1						
1131 to 1203					- 1.0	52.8	1.9	28
1210			2.1	53.5				
1325	5.2	57.2						
1333 to 1414					5.2	57.1	9.4	42
1420			5.3	57.0				
1545	5.0	57.2						
1550 to 1637					5.0	57.2	10.1	51
1640			- 5.0	57.2				



CONSTANT MONITORING

DATA & RESULTS

Client: Lonestar, Davenport, CA

Unit: Main Stack

Date: 8/23/83

Analyzed Gas O₂

Analyzer Range 0 to 25%

Recorder Range 0 to 25%

Zero Gas : Scott #CAL 4516 (span gas for NO_x and SO₂)

Span Gas: 21% O₂ - Ambient Air

Time	% FULL SCALE						Average Concentration % O ₂	
	Initial		Final		Apparent			Sample Reading
	Zero	Span	Zero	Span	Zero	Span		
825	0.0	84.0						
833 to 937					0.0	84.0	48.0	12.0
945			0.0	84.0				
1040	0.0	83.8						
1047 to 1159					0.0	83.8	44.3	11.1
1210			0.0	83.8				
1255	0.0	83.8						
1300 to 1400					0.0	83.7	35.6	8.9
1410			0.0	83.7				



CONSTANT MONITORING

DATA & RESULTS

Client: Lonestar, Davenport, CA

Unit: Main Stack

Date: 8/23/83

Analyzed Gas NOx

Analyzer Range 0 to 500 ppm

Recorder Range 0 to 500 ppm

Zero Gas : Ambient Air

Span Gas: 309.9 ppm NOx with SO₂ in N₂ - Scott #CAL 4516

Time	% FULL SCALE						Average Concentration ppm NOx	
	Initial		Final		Apparent			Sample Reading
	Zero	Span	Zero	Span	Zero	Span		
825	0.0	61.8						
833 to 937					0.0	61.6	27.5	138
945			0.0	61.4				
1040	0.0	62.0						
1047 to 1159					0.0	58.2	38.5	205
1240			0.0	54.5				
1255	0.0	62.0						
1300 to 1400					0.0	61.5	43.2	218
1410			0.0	61.0				



CONSTANT MONITORING

DATA & RESULTS

Client: Lonestar, Davenport, CA

Unit: Main Stack

Date: 8/23/83

Analyzed Gas SO₂

Analyzer Range 0 to 1000 ppm

Recorder Range -50 to 950 ppm

Zero Gas : Ambient Air

Span Gas: 522.4 ppm SO₂ with NO_x in N₂ - Scott #CAL 4516

Time	% FULL SCALE						Average Concentration ppm SO ₂	
	Initial		Final		Apparent			Sample Reading
	Zero	Span	Zero	Span	Zero	Span		
825	5.1	57.1						
833 to 937					5.4	57.4	21.8	165
945			5.7	57.6				
1040	5.0	57.1						
1047 to 1159					4.6	57.0	21.7	170
1210			4.2	56.9				
1255	5.0	57.2						
1300 to 1400					5.2	57.2	25.5	204
1410			5.3	57.2				

CALIBRATION DATA



6/3/83

CHEMECOLOGY
CORPORATION

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PITOT TUBE CAL SUMMARY

Calibrated by DER

<u>Pitot Tube Number</u>	<u>Description</u>	<u>Cp_A</u>	<u>Cp_B</u>	<u>Cp</u>
5192	3' In	.783	.779	.781
5210	3' SS	.796	.799	.797
5211	3' SS	.799	.801	.800
5212	3' SS	.798	.795	.796
5270	6' In	.768	.771	.769
5272	6' In	.780	.778	.779
5273	6' In	.777	.777	.777
5293	6' SS	.805	.803	.804
5294	6' SS	.778	.783	.780
5295	6' SS	.780	.782	.781
5330	9' In	.771	.770	.770
5332	9' In	.782	.781	.781
5350	9' SS	.776	.778	.777
5352	9' SS	.778	.781	.779

POTENTIOMETER MAINTENANCE TEST RESULTS

OLD NO.

SIMULATOR* TEMPERATURES

PC

1064 MODEL 20

DATE	32	50	75	110	212	300	375	450	600	875	1000	1200	1500	1800
3-548														
6-28-83														
3-549	34	53	78	111	216	303	376	453	598	849	-	-	-	-
3-550														
6-15-83														
3-551	32	42	67	99	199	285	361	438	589	867	-	-	-	-
6-13-83														
3-552	31	48	71	106	208	291	369	443	595	893	999	1198	1476	1802
6-28-83														
3-554	42	61	84	119	219	305	379	455	610	886	1008	1210	1506	1807
3-555														
6-15-83														
3-556	39	57	81	115	213	299	373	449	600	876	-	-	-	-
6-28-83														
3-5561	32	53	77	112	213	300	374	448	599	876	992	1191	1492	1787
6-29-83														
3-5562	39	58	82	116	215	301	377	451	604	876	995	1195	1492	1793
6-15-83														
3-5563	33	51	76	111	212	299	373	448	600	875	993	1190	1490	1783

MAGNETIC GAUGE BOXES

LINE METER	# 374 CORR. FACTOR	# 371 CORR. FACTOR	# 373 CORR. FACTOR	# 375 CORR. FACTOR	# 376 CORR. FACTOR
DATE	1-28-83				
			0-5		
00	488 103	485 103	491 101	478 105	489 102
50	440 104	440 102	448 100	437 103	443 102
100	389 103	390 103	402 100	392 102	392 101
50	337 104	344 102	359 97	347 101	349 100
00	29 104	291 102	310 97	298 101	300 100
50	242 103	248 101	260 96	249 100	250 102
00	191 103	192 101	207 97	200 100	200 100
74	172 101	174 100	181 96	174 100	170 99
48	148 100	148 100	151 95	149 99	151 96
24	124 100	125 99	133 95	125 99	126 98
08	108 100	109 99	104 93	110 98	110 98
-1.0	101 99	100 100	105 95	102 98	102 98
E	1122	1114	1160	1106	1196
$\bar{x}$	102	101	97	101	100
$\sigma \cdot \sqrt{x}$	101	100	98	100	100
			0-1		
00	101 99	100 100	96 104	94 100	95 105
88	88 100	88 100	85 104	83 104	83 106
65	65 105	64 102	64 102	62 105	61 107
52	52 100	52 100	50 104	50 104	49 106
30	30 101	30 100	30 100	30 100	29 103
22	21 104	21 105	22 100	22 100	21 105
12	11 109	11 109	12 100	11 100	12 100
E	712	712	712	721	732
$\bar{x}$	102	102	102	103	105
$\sigma \cdot \sqrt{x}$	101	101	101	101	102

MAGNETIC GAUGE READINGS WERE COMPARED TO READINGS ON WALL MOUNTED WYOMING INCLINE MANOMETER AS A STANDARD & CALCULATED A CORRECTION

CHEMECOLOGY
ATTN: RIP HUNTER
690 GARCIA AVENUE
PITTSBURGH, CA 94565

Date Shipped 7/18/83
Our Project No: 320989
Your P.O. No: 610
Page 1 of 1

CERTIFICATE OF ANALYSIS - EPA PROTOCOL GASES*

(Concentrations are in mole % or ppm)

Cylinder Number CAL-4516 Certified Accuracy 1 % NBS Traceable Analysis Dates: First 4/28/83 Last 7/12/83

COMPONENTS	CERTIFIED CONC	EXPIRATION DATE	ANALYTICAL PRINCIPLE	PRIMARY STANDARD NBS/SRM's	REPLICATE CONCENTRATIONS	
					FIRST	SECOND
NITRIC OXIDE	309.6 ppm	1/12/84	CHEMILUMINESCENCE	1686, 1687	309.4 ppm	309.8 ppm
NOx	309.9 ppm					
SULFUR DIOXIDE	522.4 ppm	1/15/84	ELECTRO-CHEMICAL	1663, 1661	520.7 ppm	524.1 ppm

Cylinder Number _____ Certified Accuracy _____ % NBS Traceable Analysis Dates: First _____ Last _____

COMPONENTS	CERTIFIED CONC	EXPIRATION DATE	ANALYTICAL PRINCIPLE	PRIMARY STANDARD NBS/SRM's	REPLICATE CONCENTRATIONS	
					FIRST	SECOND

*We hereby certify the cylinder gas has been analyzed according to EPA Protocol No:

Analyst Penrose Hallowell, Jr. Approved By Francis E. Nevill

PENROSE HALLOWELL, JR.

FRANCIS E. NEVILL

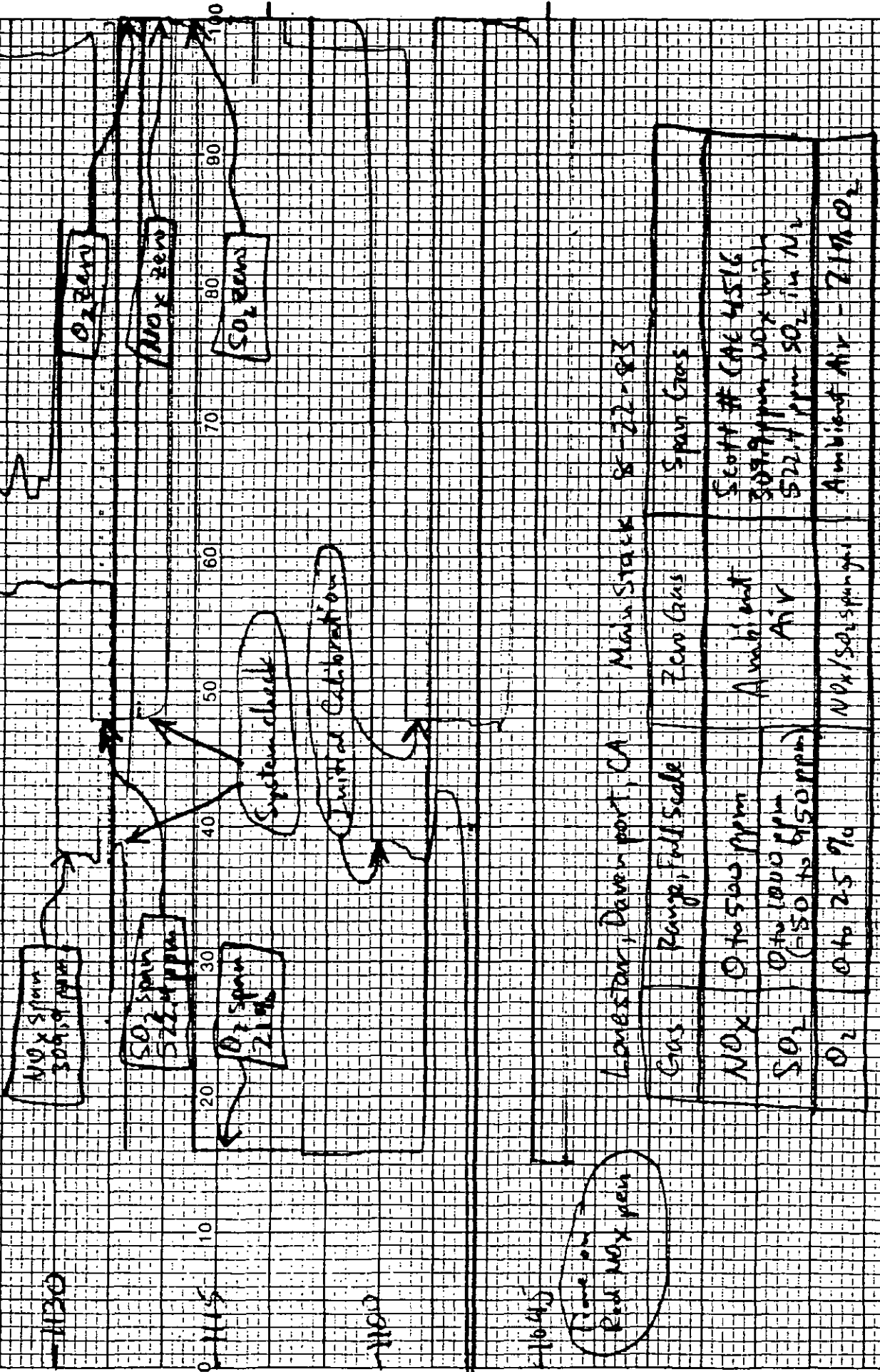
The only liability of this Company for gas which fails to comply with this analysis shall be replacement thereof by the Company without extra cost.

CERTIFIED REFERENCE MATERIALS ■ EPA PROTOCOL GASES ■ ACUBLEND® ■ CALIBRATION & SPECIALTY GAS MIXTURES
PURE GASES ■ ACCESSORY PRODUCTS ■ CUSTOM ANALYTICAL SERVICES

TROY, MICHIGAN / SAN BERNARDINO, CALIFORNIA

CHART RECORDINGS

CHART NO. C



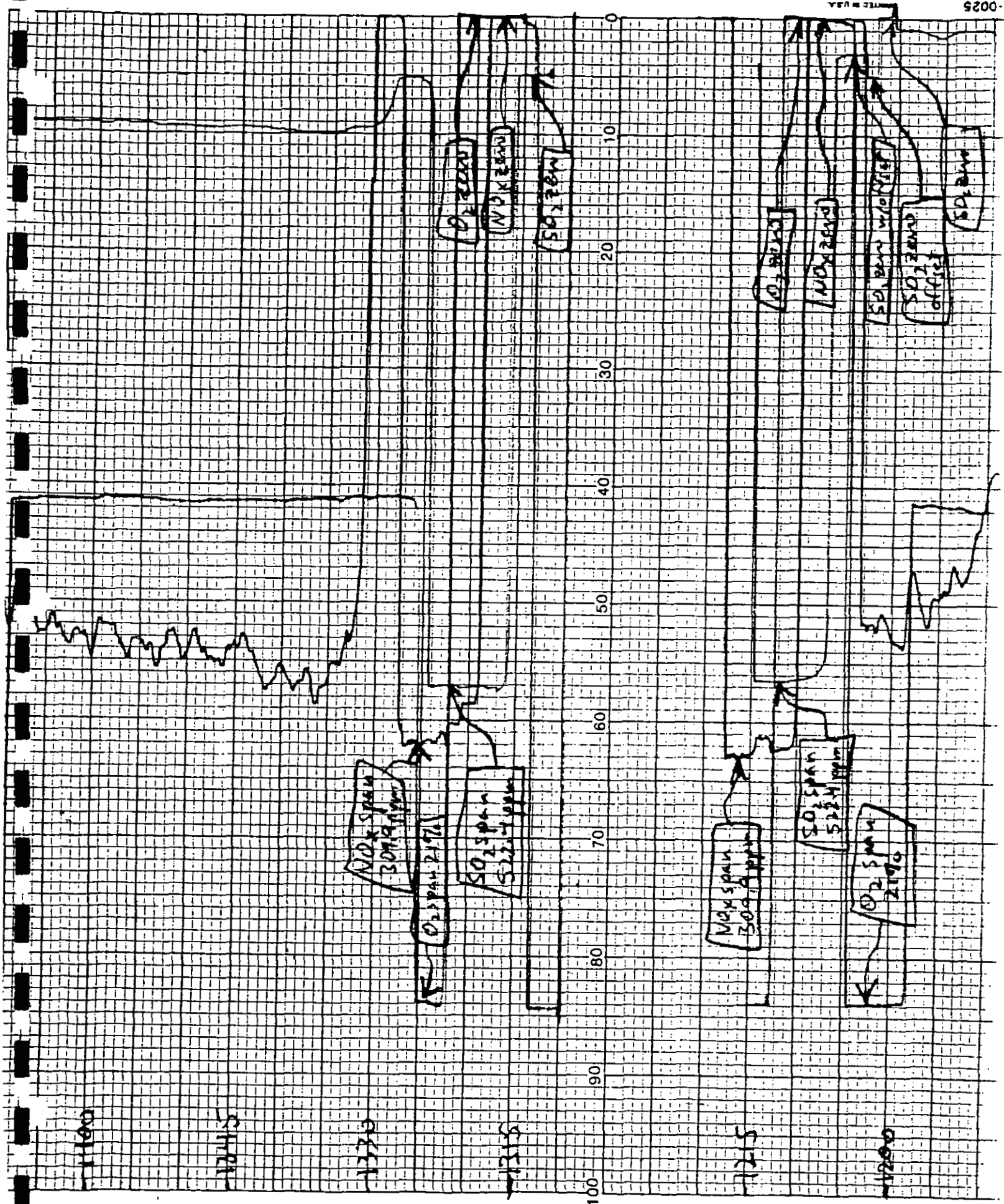
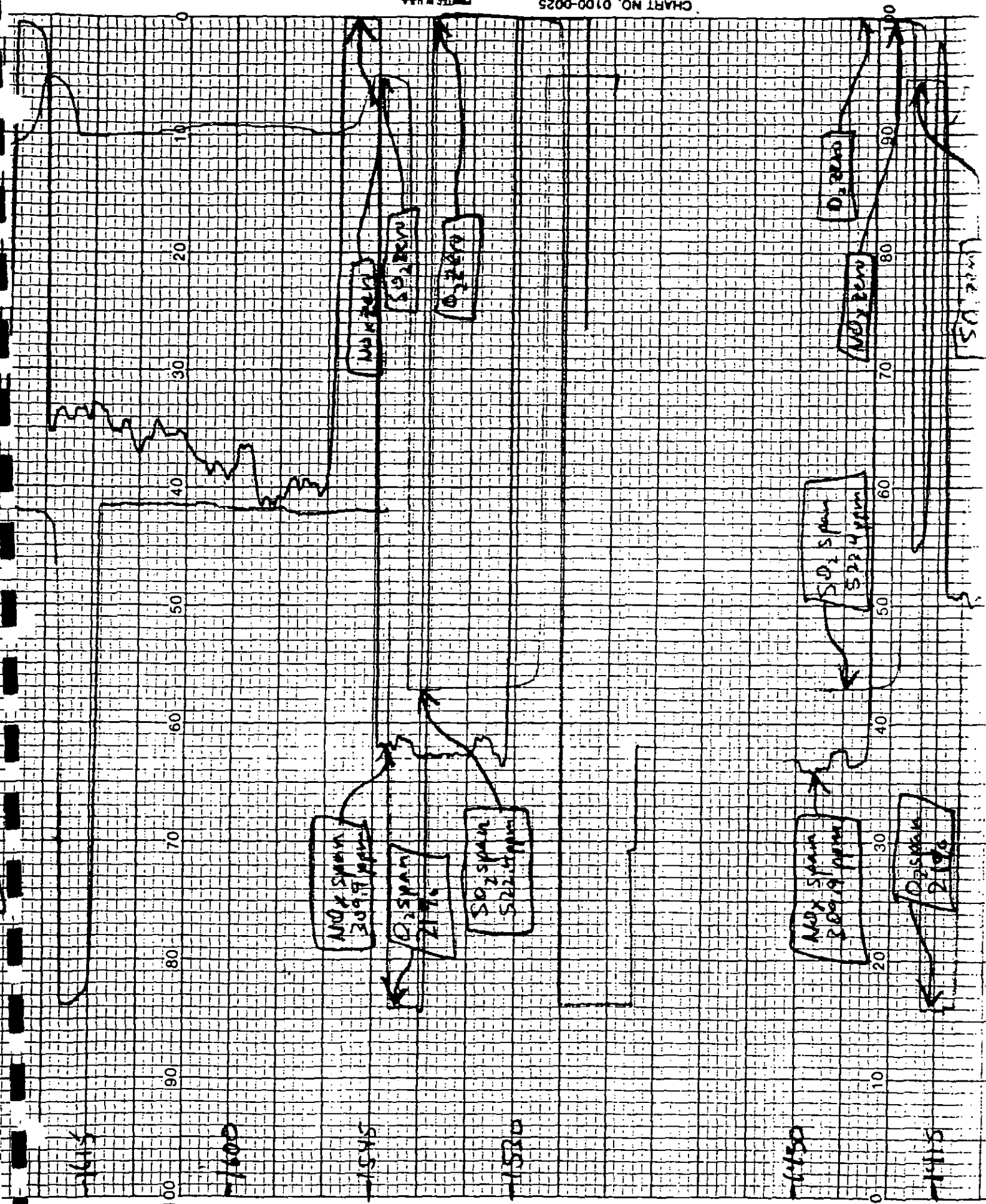


CHART NO. 0100-0025

MADE IN U.S.A.



830 0.28 ppm / 21.91

NOx span 309.1 ppm

815

SO₂ span 522.1 ppm

8/23/83 Lonestar Davenport CA = Media Stack

GAS	Range/full scale	Zero Gas	Span Gas
NOx	0 to 500 ppm	Ambient Air	Scott #CAL 4516
SO ₂	0 to 950 ppm	Air	522.1 ppm SO ₂ and 309.1 ppm NOx in Air
O ₂	0 to 25 %	Scott #CAL 4516	Ambient Air 21.91 % O ₂

END OF RECORD 8/22/83 Lonestar

NOx span 309.1 ppm

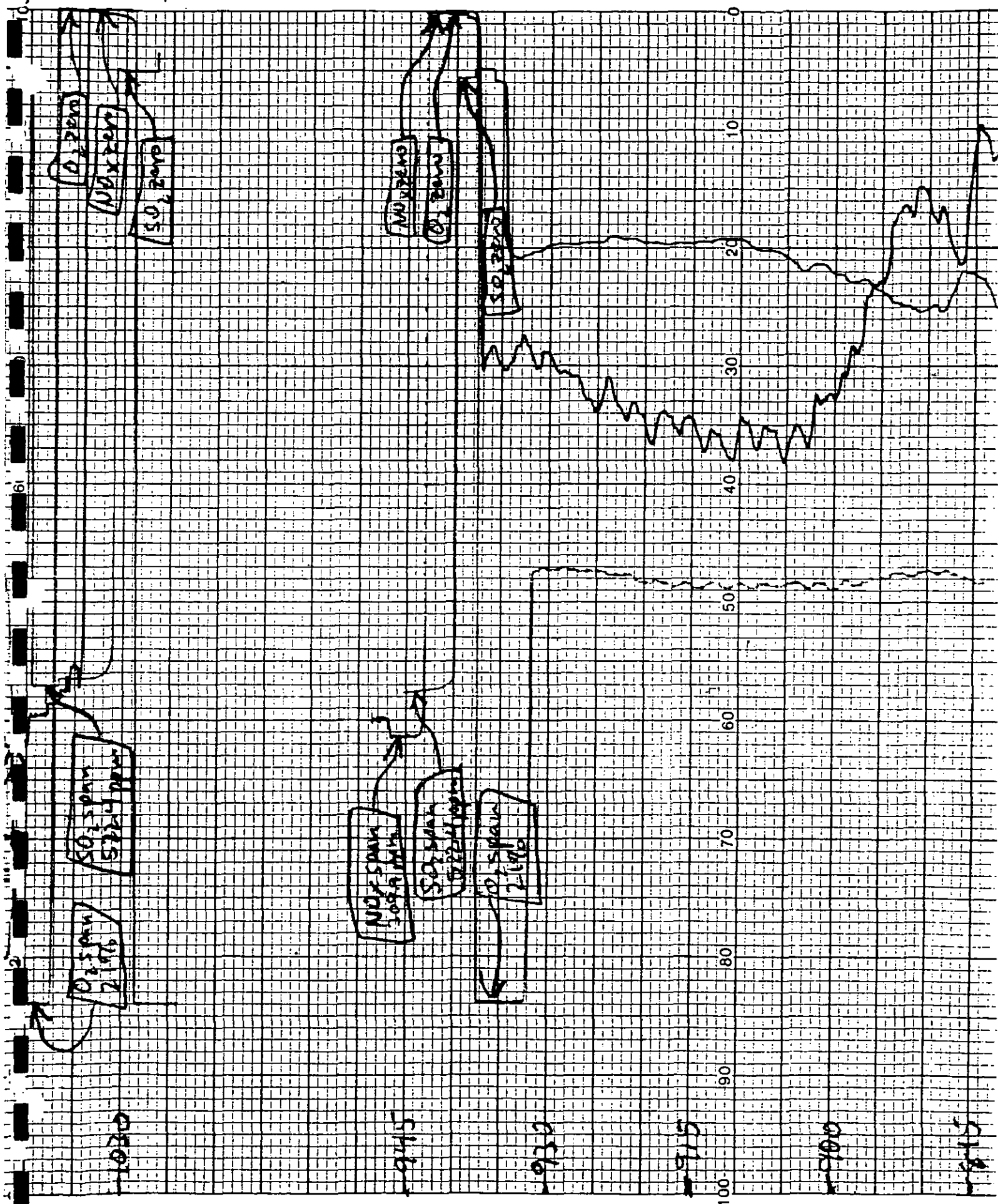
SO₂ span 522.1 ppm

O₂ span 21.91

NOx span

O₂ span

SO₂ span



PRINTED IN U.S.A.

CHART NO. 0100-0025

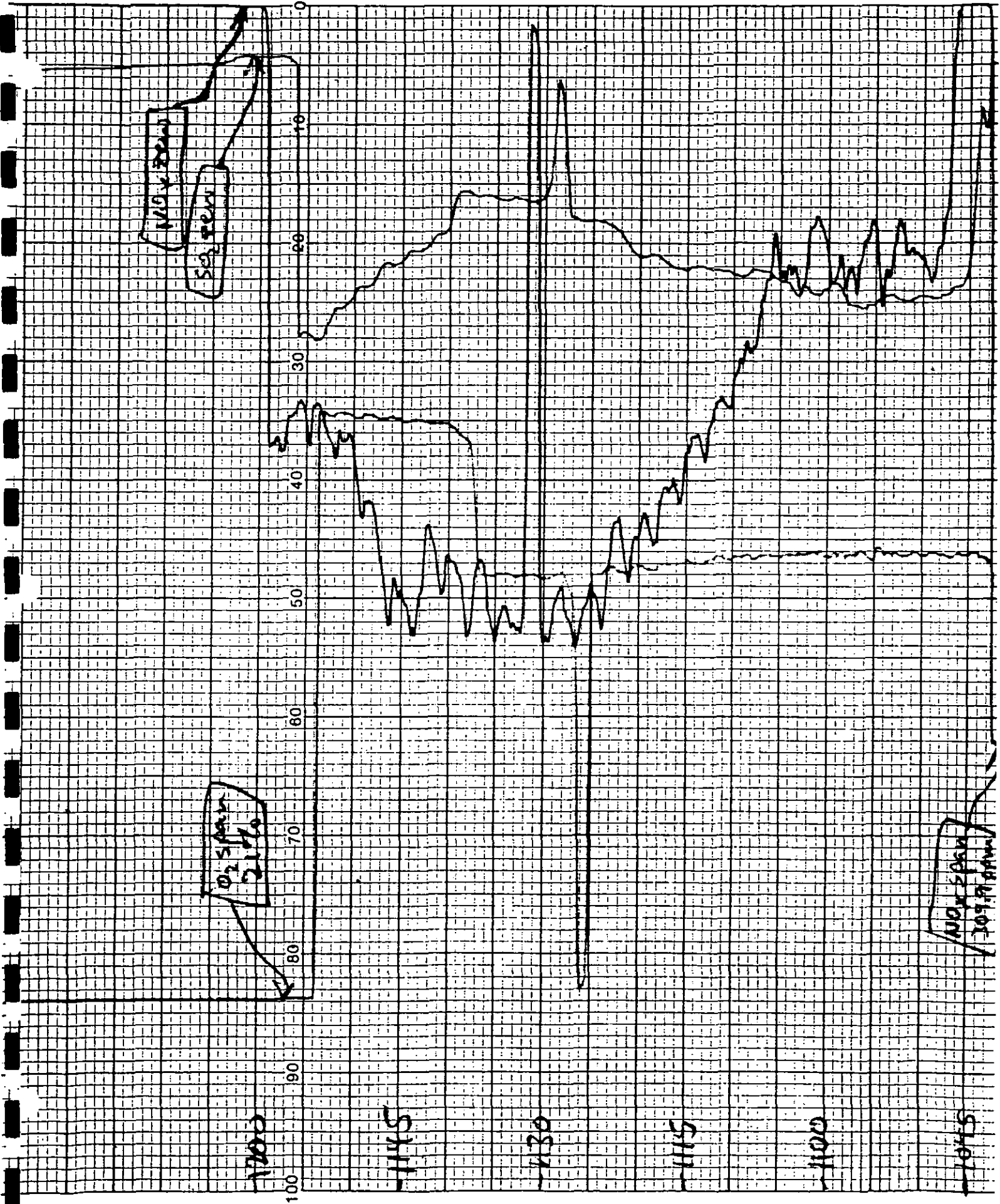
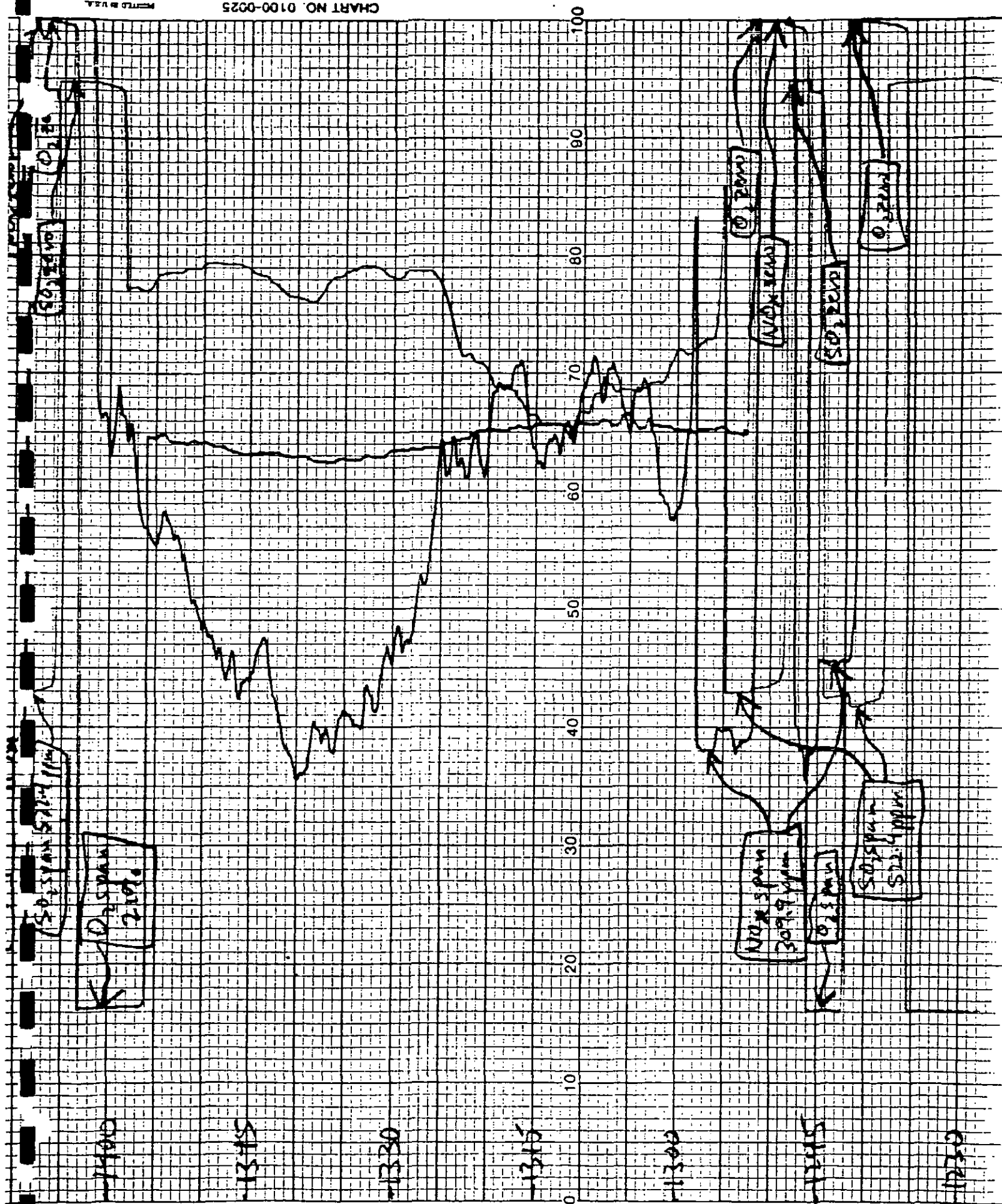
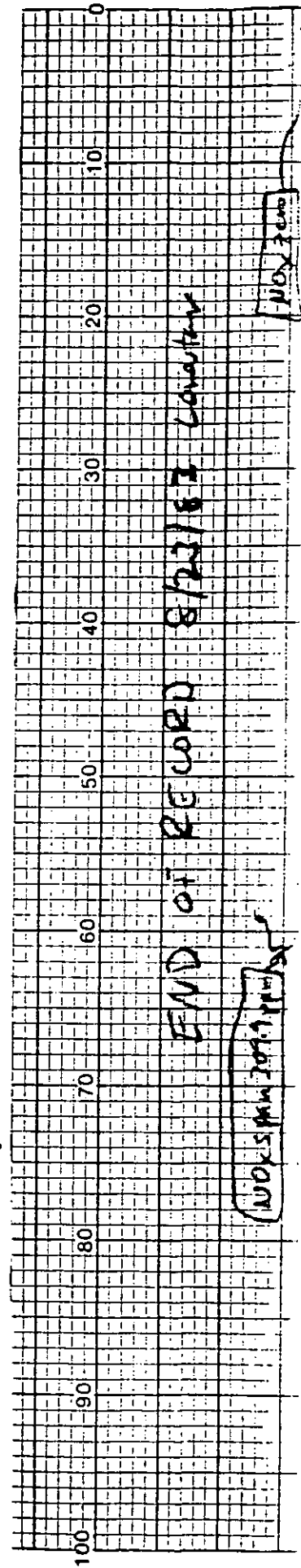


CHART NO. 0100-0025







CHEMECOLOGY
CORPORATION

690-B Garcia Avenue, Pittsburg, CA 94565 / 415-439-5766

FIELD DATA SOURCE TEST

PREPARED FOR LONESTAR INDUSTRIES

Highway 1

Davenport California 95017

ATTENTION Duc Vu

REGARDING Particulate Emissions Testing

REGULATORY AGENCY Monterey Bay Unified APO

PURPOSE Compliance

TEST DATE August 4, 1983

UNIT TESTED Clinker Cooler and Coal Stack

ASSOCIATED REPORT NUMBERS _____

REPORT NUMBER 1698

PREPARED BY Larry Bonfelli

REVIEWED BY *Larry Bonfelli*



Introduction

On August 4, 1983, Chemecology personnel; Larry Borrelli, Dave Ray and Kevin Crosby, performed particulate emissions testing at two sites simultaneously. The two sites were the Clinker Cooler and Coal Stack.

The purpose of testing was to determine compliance with Monterey Bay Unified APCD regulations.

The testing was coordinated as follows; Dave Ray conducted sampling at the Clinker Cooler Stack, Kevin Crosby sampled at the Coal Stack, and Larry Borrelli operated the computer and supervised the testing team. All samples were transported to the Pittsburgh Laboratory and analyzed the following day by Cherry Padilla, Chemecology's Lab technician.



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Method Date and Results	

SELECTED RESULTS



SELECTED RESULTS

Client: Lonestar

Unit: Clinker Cooler

Date: August 4, 1983

Time:	1105-1214 Run #1	1403-1520 Run #2	1648-1800 Run #3
-------	---------------------	---------------------	---------------------

Process Conditions:

ACFM:	163400	151600	149000
SDCFM:	95700	95430	92130
TPH (kiln feed):	170	170	170
TPH (Clinker Production):	94	94	94
CO ₂ (% vol dry):	0	0	0
O ₂ (% vol dry):	21.0	21.0	21.0
H ₂ O (% vol)	1.4	1.3	1.6

Particulate Emissions:

gr/SDCF:	0.0130	0.0127	0.0166
gr:SDCF (less condensables):	0.0120	0.0082	0.0149
lbs/hr (total):	11.5	10.40	13.12
lbs. part/Ton Feed (less condensables)	0.060	0.041	0.069

Test Conditions:

Duration (min):	60	60	60
Sample vol. (SDCF):	43.58	41.27	39.97
% isokinetic:	100.0	98.7	99.1



SELECTED RESULTS

Client: Lonestar

Unit: Coal Stack

Date: August 4, 1983

Time:	1107-1220 Run #1	1410-1519 Run #2	1654-1805 Run #3
-------	---------------------	---------------------	---------------------

Process Conditions:

ACFM:	26590	26840	27060
SDCFM:	20970	21290	21400
TPH (kiln feed):	170	170	170
TPH (Coal Mill):	15.5	15.5	15.5

CO ₂ (% vol dry):	0.5	0.5	0.4
O ₂ (% vol dry):	20.5	20.5	20.6
H ₂ O (% vol):	4.1	3.8	4.1

Particulate Emissions:

gr/SDCF:	0.0053	0.0032	0.0008
gr/SDCF (less condensables):	0.0033	0.0019	0.0005
lb/hr. (total):	0.95	0.58	0.15

Test Conditions:

Duration (min):	60	60	60
Sample vol. (SDCF):	34.26	36.57	39.38
% isokinetic:	91.5	95.8	102.6

VELOCITY PROFILE & VOLUME FLOW RATE



VELOCITY TRAVERSE AND VOLUME FLOW RATE

REF: Environmental Protection Agency, Code of Federal Regulations,
Title 40, Part 60, Appendix A, Method 1 and 2, 1981
: Bay Area AQMD, Manual of Procedures, San Francisco, CA, Method St-17
January, 1982
: ASME Performance Test Code #27, New York, NY, 1957
: ASTM D-2928-71
: Western Precipitation Division of Joy Manufacturing, WP-50, 1968

PROCEDURE:

Duct temperature and velocity were read at each of several traverse points within the duct. The number and location of traverse points was chosen to aid in the extraction of a representative sample (i.e. by EPA Method 1). Velocity head was determined using a calibrated type "S" pitot tube and Magnehelic differential pressure gauge. Duct temperature was measured by means of a thermocouple attached to the pitot tube. Static pressure was measured with the Magnehelic and one leg of the pitot tube. Using the molecular weight and traverse data, velocity was calculated at each traverse point. From the average velocity, duct area, temperature, pressure and composition, actual and standard gas volume flow rate were calculated for the duct.

CALCULATIONS:

Performed by computer based on the following equations:

Symbol Identification:

A_d = duct area, square feet
 C_p = pitot tube correction factor, unitless
 D = duct diameter (circular ducts), inches
 k = number of traverse points on D or W
 L = duct dimension having ports (rectangular), inches
 MW = molecular weight (wet)
 n = traverse point number on a diameter
 Δp = velocity head, "H₂O
 P_L = number of ports on dimension L
 P_d & P_{std} = duct (barometric + static) and standard pressure, "Hg
 Q_d = volume flow rate, actual CFM
 Q_{std} = volume flow rate, standard condition (wet or dry), SCFM
 T_d & T_{std} = duct and standard temperature, °R
 $t.p.$ = traverse point (distance from sample port wall), inches
 v_d = velocity at duct conditions, fps
 W = second duct dimension (rectangular), inches



VELOCITY TRAVERSE AND VOLUME FLOW RATE (cont)

Equations:

Location of Traverse Points:

Circular Duct:

$$t.p. (1st\ half) = D/2 - (D/2k) * \sqrt{k(k+1-2n)}$$

$$t.p. (2nd\ half) = D/2 + (D/2k) * \sqrt{k(2n-1)}$$

Where $n = 1$ to $k/2$

Rectangular Duct:

$$t.p. = W/2k + (n-1) * W/k$$

Where $k = (W/L) * (P_L)$
 $n = 1$ to k

Velocity & Volume Flow Rate:

$$v_d = 85.49 * C_p * \sqrt{\frac{T_d * \Delta p}{P_d * MW}}$$

$$Q_d = 60 * v_d (avg) * A_d = \text{ACFM}$$

$$Q_{std(wet)} = Q_d * \frac{T_{std}}{T_d(avg)} * \frac{P_d}{P_{std}} = \text{SCFM}$$

$$Q_{std(dry)} = Q_{std(wet)} * (1 - \%H_2O/100) = \text{SDCFM}$$



VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')

DATA:

CLIENT: Lonestar

UNIT: Clinker Cooler

DATE: 8/4/83

TIME: 1105 - 1214

RUN #: 1

Description: Ports: two 3-inch female ports, properly located, approximately 6 diameters after and 2 diameters before disturbances in flow.

Duct Diameter 102 inches Area 56.75 ft²

Rectangular duct X

% H₂O 1.4 MW 28.69

Mag. Box # 371

Duct Static Pressure 1.10 inches H₂O

Temp. Unit # 5562

Standard Conditions 60 °F & 29.92 "Hg

Pitot Tube # 5352

Pitot Tube Coefficient 0.78

Trav. Pt.	Ins. From Edge	Northwest Port			Southwest Port								
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	2.2	380	0.44	43.8	380	0.46	44.8						
2	6.8	390	0.53	48.3	385	0.50	46.8						
3	12.0	390	0.60	51.4	390	0.54	48.8						
4	18.1	395	0.58	50.7	390	0.54	48.8						
5	25.5	395	0.58	50.7	390	0.52	47.9						
6	36.3	395	0.57	50.3	390	0.52	47.9						
7	65.7	395	0.52	48.0	390	0.50	46.9						
8	76.5	395	0.52	48.0	390	0.56	49.7						
9	83.9	385	0.55	49.1	290	0.50	44.1						
10	90.0	385	0.55	49.1	290	0.50	44.1						
11	95.2	390	0.54	48.8	390	0.56	49.7						
12	99.8	390	0.54	48.8	385	0.48	45.8						
13													
14													
15													
16													
17													
18													
19													
20													
21													
22													
23													
24													

RESULTS:

Average Velocity (V_d) 48.0 FPS Average duct temp. 381 °F, press. 29.90 "Hg

Volume Flow Rate at 381 °F & 29.90 "Hg (Q_d) 163421 ACFM

Volume Flow Rate at standard conditions (Q_{std(wet)}) 100978 SCFM

Volume Flow Rate at standard conditions (Q_{std(dry)}) 99542 SDCFM



VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')

DATA:

CLIENT: Lonestar

UNIT: Clinker Cooler

DATE: 8/4/83

TIME: 1403 - 1520

RUN #: 2

Description: Ports: two 3-inch female ports, properly located, approximately 6 diameters after and 2 diameters before disturbances in flow.

Duct Diameter 102 inches Area 56.75 ft²

Rectangular duct _____ X _____

% H₂O 1.3 MW 28.70

Mag. Box # 371

Duct Static Pressure 1.10 inches H₂O

Temp. Unit # 5562

Standard Conditions 60 °F & 29.92 "Hg

Pitot Tube # 5352

Pitot Tube Coefficient 0.78

Trav. Pt.	Ins. From Edge	Southwest Port			Northwest Port								
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	2.2	360	0.40	41.2	365	0.50	46.2						
2	6.8	360	0.42	42.2	365	0.50	46.2						
3	12.0	360	0.46	44.2	365	0.54	48.0						
4	18.1	360	0.46	44.2	365	0.54	48.0						
5	25.5	360	0.50	46.1	365	0.53	47.6						
6	36.3	360	0.46	44.2	365	0.53	47.6						
7	56.7	370	0.40	41.5	360	0.50	46.1						
8	76.5	270	0.42	39.9	350	0.50	45.8						
9	83.9	270	0.42	39.9	350	0.50	45.8						
10	90.0	375	0.46	44.6	355	0.48	45.0						
11	95.2	375	0.45	44.1	355	0.46	44.1						
12	99.8	375	0.44	43.6	355	0.42	42.1						
13													
14													
15													
16													
17													
18													
19													
20													
21													
22													
23													
24													

RESULTS:

Average Velocity (V_d) 44.5 FPS Average duct temp. 355 °F, press. 29.90 "Hg

Volume Flow Rate at 355 °F & 29.90 "Hg (Q_d) 151550 ACFM

Volume Flow Rate at standard conditions (Q_{std(wet)}) 96685 SCFM

Volume Flow Rate at standard conditions (Q_{std(dry)}) 95434 SDCFM



VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')

DATA:

CLIENT: Lonestar

UNIT: Clinker Cooler

DATE: 8/4/83

TIME: 1648-1800

RUN #: 3

Description: Ports: two 3-inch female ports, properly located, approximately 2 diameters after and 6 diameters before disturbances in flow.

Duct Diameter 102 inches Area 56.75 ft²

Rectangular duct X

% H₂O 1.6 MW 28.67

Mag. Box # 371

Duct Static Pressure 1.10 inches H₂O

Temp. Unit # 5562

Standard Conditions 60 °F & 29.92 "Hg

Pitot Tube # 5352

Pitot Tube Coefficient 0.78

Trav. Pt.	Ins. From Edge	Northwest Port			Southwest Port								
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	2.2	370	0.42	42.5	370	0.43	43.0						
2	6.8	370	0.53	47.8	370	0.43	43.0						
3	12.0	370	0.53	47.8	370	0.40	41.5						
4	18.1	360	0.56	48.8	370	0.40	41.5						
5	25.5	370	0.54	48.2	375	0.40	41.6						
6	36.3	360	0.46	44.2	375	0.40	41.6						
7	65.7	360	0.46	44.2	380	0.37	40.1						
8	76.5	360	0.50	46.1	380	0.42	42.8						
9	83.9	360	0.50	46.1	380	0.42	42.8						
10	90.0	360	0.46	44.2	380	0.40	41.7						
11	95.2	345	0.46	43.8	365	0.42	42.4						
12	99.8	340	0.42	41.7	365	0.42	42.4						
13													
14													
15													
16													
17													
18													
19													
20													
21													
22													
23													
24													

RESULTS:

Average Velocity (V_d) 43.8 FPS Average duct temp. 367 °F, press. 29.90 "Hg

Volume Flow Rate at 367 °F & 29.90 "Hg (Q_d) 148961 ACFM

Volume Flow Rate at standard conditions (Q_{std(wet)}) 93620 SCFM

Volume Flow Rate at standard conditions (Q_{std(dry)}) 92128 SDCFM



VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')

DATA:

CLIENT: Lonestar

UNIT: Coal Stack

DATE: 8/4/83

TIME: 1107 - 1220

RUN #: 1

Description: Ports: two 3-inch female ports, properly located, approximately 8 diameters after and 8 diameters before disturbances in flow.

Duct Diameter 36.0 inches Area 7.07 ft²

Rectangular duct X

% H₂O 4.1 MW 28.45

Mag. Box # 375

Duct Static Pressure -27.0 inches H₂O

Temp. Unit # 549

Standard Conditions 60 °F & 29.92 "Hg

Pitot Tube # 5294

Pitot Tube Coefficient 0.78

Trav. Pt.	Ins. From Edge	South Port			West Port								
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	1.6	120	0.86	52.9	140	0.60	45.0						
2	5.3	128	1.20	65.5	128	1.15	61.6						
3	10.7	128	1.20	65.5	128	1.40	68.0						
4	25.3	128	1.20	65.5	128	1.50	70.4						
5	30.7	128	1.20	65.5	128	1.40	68.0						
6	34.4	128	1.15	61.6	128	1.20	62.9						
7													
8													
9													
10													
11													
12													
13													
14													
15													
16													
17													
18													
19													
20													
21													
22													
23													
24													

RESULTS:

Average Velocity (V_d) 62.7 FPS Average duct temp. 128 °F, press. 27.84 "Hg

Volume Flow Rate at 128 °F & 27.84 "Hg (Q_d) 26589 ACFM

Volume Flow Rate at standard conditions (Q_{std(wet)}) 21864 SCFM

Volume Flow Rate at standard conditions (Q_{std(dry)}) 20969 SDCFM



VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')

DATA:

CLIENT: Lonestar

UNIT: Coal Stack

DATE: 8/4/83

TIME: 1410 - 1519

RUN #: 2

Description: Ports: two 3-inch female ports, properly located, approximately 8 diameters after and 8 diameters before disturbances in flow.

Duct Diameter 36.0 inches Area 7.07 ft²

Rectangular duct _____ X _____

% H₂O 3.8 MW 28.49

Mag. Box # 375

Duct Static Pressure -27.0 inches H₂O

Temp. Unit # 549

Standard Conditions 60 °F & 29.92 "Hg

Pitot Tube # 5294

Pitot Tube Coefficient 0.78

Trav. Pt.	Ins. From Edge	West Port			South Port								
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	1.6	120	0.56	42.7	120	0.60	44.2						
2	5.3	128	1.20	62.9	128	1.25	64.2						
3	10.7	128	1.40	67.9	128	1.50	70.3						
4	25.3	128	1.50	70.3	128	1.50	70.3						
5	30.7	128	1.50	70.3	128	1.45	69.1						
6	34.4	128	1.25	64.2	128	1.20	62.9						
7													
8													
9													
10													
11													
12													
13													
14													
15													
16													
17													
18													
19													
20													
21													
22													
23													
24													

RESULTS:

Average Velocity (V_d) 633 FPS Average duct temp. 127 °F, press. 27.84 "Hg

Volume Flow Rate at 127 °F & 27.84 "Hg (Q_d) 26839 ACFM

Volume Flow Rate at standard conditions (Q_{std(wet)}) 22132 SCFM

Volume Flow Rate at standard conditions (Q_{std(dry)}) 21289 SDCFM



VELOCITY TRAVERSE & VOLUME FLOW RATE (cont')

DATA:

CLIENT: Lonestar

UNIT: Coal Stack

DATE: 8/4/83

TIME: 1654 - 1805

RUN #: 3

Description:

Duct Diameter 3.0 inches Area 7.07 ft²

Rectangular duct X

% H₂O 4.1 MW 28.44

Duct Static Pressure -27.0 inches H₂O

Standard Conditions 60 °F & 29.92 "Hg

Pitot Tube Coefficient 0.78

Mag. Box # 375

Temp. Unit # 549

Pitot Tube # 5294

Trav. Pt.	Ins. From Edge	South Port			West Port								
		Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec	Temp °F	ΔP In.	V _d ft/sec
1	1.6	120	0.40	36.1	125	0.85	52.8						
2	5.3	128	1.30	65.5	128	1.25	64.2						
3	10.7	128	1.45	69.2	128	1.45	69.2						
4	25.3	128	1.45	69.2	128	1.55	71.5						
5	30.7	128	1.40	68.0	128	1.50	70.4						
6	34.4	125	1.30	65.3	128	1.25	64.2						
7													
8													
9													
10													
11													
12													
13													
14													
15													
16													
17													
18													
19													
20													
21													
22													
23													
24													

RESULTS:

Average Velocity (V_d) 63.8 FPS Average duct temp. 127 °F, press. 27.84 "Hg

Volume Flow Rate at 127 °F & 27.84 "Hg (Q_d) 27064 ACFM

Volume Flow Rate at standard conditions (Q_{std(wet)}) 22311 SCFM

Volume Flow Rate at standard conditions (Q_{std(dry)}) 21399 SDCFM

PARTICULATE EMISSIONS



PARTICULATE EMISSIONS

REF: EPA, Code of Federal Regulations, Title 40, Part 60, Appendix A, Method 5, 1981
: South Coast AQMD, Source Testing Manual, Los Angeles, CA, April, 1981
: State of California, Air Resources Board, Draft Stationary Source Test Methods, Method 1-5, June, 1979

SAMPLING PROCEDURE:

The apparatus consisted of a nozzle, heater wrapped probe and heated filter holder (see data sheets for type of nozzle, probe and filter holder). A series of impinger-absorbers (see data sheet for type and contents) were connected in tandem and immersed in an ice bath. The absorption train was followed by a gas drying tube containing indicating silica gel, a diaphragm pump, dry test meter and a calibrated restriction orifice fitted with a magnehelic differential pressure gauge.

The computer was used in selection of suitable sampling points, nozzle size, and orifice constant. The apparatus was leak tested, the probe heaters were brought to temperature and the nozzle was positioned at the first sampling point. The pump was immediately started and adjusted to obtain the isokinetic sampling rate.

Duct conditions were monitored throughout the sampling period with a type "S" pitot tube and a thermocouple simultaneously positioned at the traverse point. Conditions at the sampling apparatus and metering device were constantly monitored and regularly recorded on the data sheet. Isokinetic sampling rate in terms of orifice differential pressure was calculated by computer for each set of duct and sampling apparatus conditions. Data was relayed between the computer and site by radio.

On completion of sampling from all usable traverse points, the apparatus was removed, leak-checked, sealed from possible contamination and transported to the laboratory. Replicate samples were taken as indicated by the data sheets.

Concurrent with each particulate sampling, an integrated gas sample was withdrawn from the summation of the traverse points through the train and collected at the outlet of the meter into a sample bag.

ANALYTICAL PROCEDURE:

The weight or volume increase of the impingers was measured and recorded for calculation of percent water.

The contents of the sample bladder were analyzed by Orsat for fixed gas and molecular weight determination.



PARTICULATE EMISSIONS

Analytical Procedure (cont)

The filter section was recovered, placed in a 105°C drying oven and desiccated to constant weight. The weight increase was determined from the tare weight and recorded on the individual data sheet.

Sample was recovered from the nozzle and probe sections with distilled water and/or acetone and a rubber policeman or nylon bristle brush. A tared dish was used for subsequent evaporation, desiccation and weight determination.

If analysis of the condensable fraction of the particulate ("impinger catch" or "back half") was required, an aliquot of the impinger liquid was poured into a tared dish. The liquid was evaporated to dryness and the residue was desiccated to a constant weight.

Aliquots of blank impinger and/or probe wash reagents were evaporated to dryness in tared dishes. The residue was desiccated and weighed for subtraction of the blank residue from the total probe wash or condensables residue.

An estimate of sampling accuracy was performed by calculation of percent isokinetic rate over the entire sampling period.

CALCULATIONS:

Performed by computer based on the following equations:

Symbol Identification:

Subscripts d, m and n denote duct, dry gas meter and nozzle respectively
Subscripts std, bar and avg denote standard, barometric and average

A = area, square feet
C_o = particulate concentration, grains/SDCF
C_p = pitot tube correction, unitless
E.R. = emission rate of particulate, lb/hr
ΔH = orifice differential pressure, inches H₂O
I = percent of isokinetic sampling
k_m = orifice constant, unitless
M = mass of particulate collected, milligrams
MW = wet molecular weight of duct gas, g/mole
P = absolute pressure, inches Hg
Δp = velocity pressure head, inches H₂O
Q = volume flow rate, CFM
Q_o = parameter of volume flow rate through the orifice
T = absolute temperature, °R
t = time of sampling period, minutes
V = gas volume, CF
v = velocity, feet/second
W = water collected, grams
% H₂O = duct gas water content, percent volume



PARTICULATE EMISSIONS

Calculations (cont)

Equations:

Duct gas velocity at any traverse point (see Velocity & Volume Flow Rate):

$$v_d = 85.49 * C_p * \sqrt{\frac{T_d * \Delta P}{P_d * MW}}$$

Isokinetic sampling rate at any traverse point:

$$Q_m = Q_n * \frac{P_d * T_m}{P_m * T_d} * (1 - \% H_2O/100)$$

where $Q_n = 60 * v_n * A_n$ and for isokinetic sampling, $v_n = v_d$

$$\Delta H = Q_o^2 * \frac{P_b}{k_m^2 * T_m} * \frac{[MW - (0.18 * \% H_2O)]}{(1 - \% H_2O/100)}$$

where $Q_o = 1.23 * Q_m - 0.23 * Q_m^{(2 - Q_m)}$ (for non-linear orifice)

Percent of isokinetic sampling:

$$I = T_d * \frac{[0.00267 * W + V_m/T_m(\text{avg}) * (P_{bar} + \Delta H(\text{avg})/13.6)]}{t * v_d(\text{avg}) * P_d * A_n * 60} * 100$$

Sampled Volume:

$$V_m(\text{std}) = V_m * \frac{T_{std}}{T_m(\text{avg})} * \frac{(P_{bar} + \Delta H(\text{avg})/13.6)}{P_{std}}$$

Particulate Concentration:

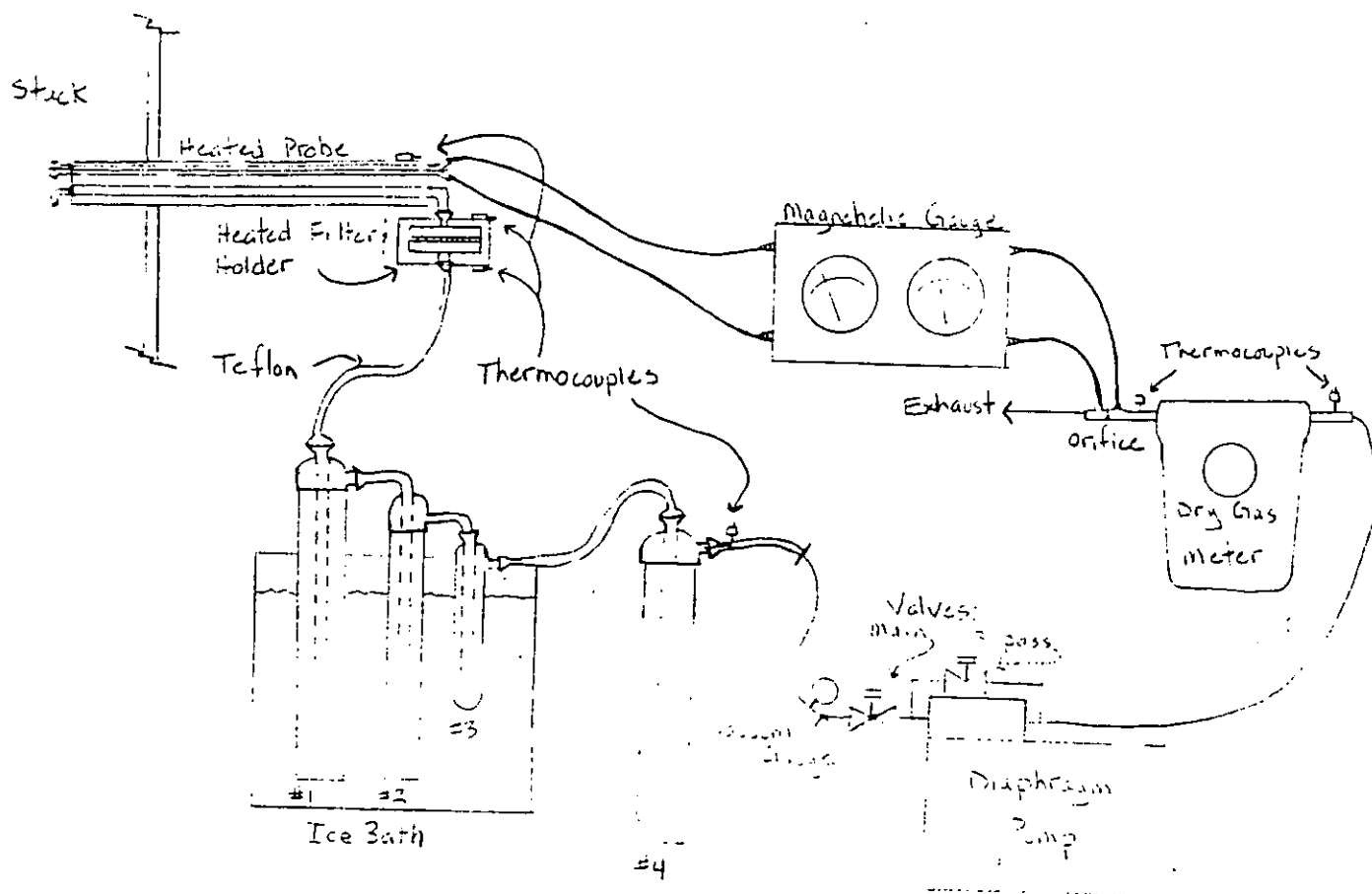
$$C_o = \frac{0.0154 * M}{V_m(\text{std})}$$

Emission Rate:

$$E.R. = 8.58 * 10^{-3} * Q_{std}(\text{dry}) * C_o$$



Method 5 Particulate Sampling Train



<u>Impinger #</u>	<u>Contents</u>
#1	100 mls Distilled Water
#2	100 mls Distilled Water
#3	Empty
#4	250 grms Silica Gel (8 mesh)



PARTICULATE EMISSIONS
TEST MONITOR DATA

Date 8/4/83 Run 1
Client Lonestar
Unit Clinker Cooler
Ambient Temp. 75 °F
Press. bar 29.82 in. Hg
Press. static 1.10 in. H₂O
Press. duct 29.90 in. Hg
Assumed MW 28.80 %H₂O 1.0

Sample Train Temp.:
Probe 400, 420, 400 °F
Filter 275, 280, 225 °F
Sample Line 230 °F
Post-Test Leak Check:
Leak Rate 0.005 CFM
5 in. Hg Vac.

Nozzle & Probe Mat. SS
Filter Holder Mat. SS
Filter # 5
Nozzle # 7G i.d. 7.0 mm
Pitot # 5352 Cp 0.78
Temp. Unit # 5562
Mag. # 371 Meter # 632
Orifice km 0.4

		Duct Data			Meter Data			
Trav. Point	Time	Temp. °F	Head Δp	Velocity ft/sec	Vacuum "Hg	Temp. °F	Orifice ΔH, "H2O	Volume CF
Northwest Port								
12	1105	390	0.54	48.8		80	3.82	754.10
11	1107.5	390	0.54	48.8		80	3.82	
10	1110	385	0.55	49.1		70	3.85	
9	1112.5	385	0.55	49.1		70	3.85	
8	1115	395	0.52	48.0	0	75	3.65	
7	1117.5	395	0.52	48.0		75	3.65	
6	1120	395	0.57	50.3		75	3.97	
5	1122.5	395	0.58	50.7		75	4.03	
4	1125	395	0.58	50.7	0	75	4.03	
3	1127.5	390	0.60	51.4		75	4.18	
2	1130	390	0.53	48.3		75	3.73	
1	1132.5	380	0.44	43.8		75	3.19	
	1135	Stop to change ports						776.26
Southwest Port								
12	1154	385	0.48	45.8		75	3.43	
11	1156.5	390	0.56	49.7		75	3.92	
10	1159	290	0.50	44.1		75	3.97	
9	1201.5	290	0.50	44.1	0	75	3.97	
8	1204	390	0.56	49.7		80	3.95	
7	1206.5	390	0.50	46.9		85	3.59	
6	1209	390	0.52	47.9	2	85	3.72	
5	1211.5	390	0.52	47.9		85	3.72	
4	1204	390	0.54	48.8		85	3.85	
3	1206.5	390	0.54	48.8		85	3.85	
2	1209	385	0.50	46.8		80	3.59	
1	1211.5	380	0.46	44.8		80	3.35	
	1214	End of test						798.90



PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Clinker Cooler
Date: 8/4/83

Run: 1
Time: 1105 - 1214

Absorber Type	Contents	Final	Tare	Net	H ₂ O
Lg. Grunbrg	Distilled H ₂ O	523.1	517.8	5.3	
Sm. Grunbrg	Distilled H ₂ O	353.1	352.8	0.3	
liquid trap	empty	98.0	97.5	0.5	
	silica gel	601.8	594.3	7.5	
TOTAL				13.6	

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle Wash	65.9606	65.9570	3.6	0.0013
Condensables ³⁵⁰ mls	83.1926	83.1898	2.8	0.0010
Filter #5	4509	4205	30.4	0.0107
H ₂ O (8.7 mls)	blank @ 8.7 mls =			<0.0001
Acetone (54.1 mls)	blank @ 54.1 mls =			<0.0001
Gas Composition:	TOTAL		36.8	0.0130

CO₂ 0 % volume (dry)
O₂ 21 % volume (dry)
CO % volume (dry)
N₂ 79 % volume (dry)
H₂O 1.4 % volume

MW (wet) 28.69
Excess Air %
Sampled Volume 43.58 SDCF
Isokinetic Rate 100.0 %

Particulate Concentration:

Co 0.0130 grains/SDCF @ 60 °F and 29.92 "Hg
C grains/SDCF @

Emission Rate:

E.R. 11.16 lbs/hr @ Qstd(dry) 99500 SDCFM



CHEMECOLOGY CORPORATION

PARTICULATE EMISSIONS TEST MONITOR DATA

Date 8/4/83 Run 2
 Client Lonestar
 Unit Clinker Cooler
 Ambient Temp. 75 °F
 Press. bar 29.82 in. Hg
 Press. static 1.10 in. H₂O
 Press. duct 29.90 in. Hg
 Assumed MW 28.69 %H₂O 1.4
 Sample Train Temp.:
 Probe 410, 420, 420 °F 410
 Filter 275, 260, 260 °F 265
 Sample Line °F
 Post-Test Leak Check:
 Leak Rate 0.004 CFM
 # 6 in. Hg Vac.
 Nozzle & Probe Mat. SS
 Filter Holder Mat. SS
 Filter # 11
 Nozzle # 7G i.d. 7.0 mm
 Pitot # 5352 Cp 0.78
 Temp. Unit # 5562
 Mag. # 371 Meter # 632
 Orifice km 0.5

Duct Data					Meter Data			
Trav. Point	Time	Temp. °F	Head Δp	Velocity ft/sec	Vacuum "Hg	Temp. °F	Orifice ΔH, "H2O	Volume CF
Southwest Port								
12	1403	375	0.44	43.6		75	3.19	779.20
11	1405.5	375	0.45	44.1	0	75	3.25	
10	1408	375	0.46	44.6		80	3.34	
9	1410.5	270	0.42	39.9		80	3.48	
8	1403	270	0.42	39.9		80	3.48	
7	1415.5	370	0.40	41.5		80	2.97	
6	1418	360	0.46	44.2	0	80	3.40	
5	1420.5	360	0.50	46.1		85	3.69	
4	1423	360	0.46	44.2		85	3.40	
3	1425.5	360	0.46	44.2		85	3.42	
2	1428	360	0.42	42.2		85	3.16	
1	1430.5	360	0.40	41.2		85	3.02	
	1433	Stop to change ports						820.10
Northwest Port								
								820.30
12	1450	355	0.42	42.1		75	3.13	
11	1452.5	355	0.46	44.1	0	75	3.39	
10	1455	355	0.48	45.0		75	3.52	
9	1457.5	350	0.50	45.8		75	3.67	
8	1500	350	0.50	45.8		75	3.67	
7	1502.5	360	0.50	46.1		80	3.66	
6	1505	365	0.53	47.6	0	80	3.84	
5	1507.5	365	0.53	47.6		80	3.84	
4	1510	365	0.54	48.0		80	3.90	
3	1512.5	365	0.54	48.0		80	3.90	
2	1515	365	0.50	46.2		80	3.64	
1	1517.5	365	0.50	46.2		80	3.64	
	1520	End of test						842.00



PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Clinker Cooler
Date: 8/4/83

Run: 2
Time: 1403 - 1520

Absorber Type	Contents	Final	Tare	Net	H2O
Lg. Grnbrg	Distilled H O	555.2	549.7	5.5	
Sm. Grnbrg	Distilled H O	387.6	387.0	0.6	
liquid trap	empty	100.2	99.9	0.3	
	silica gel	590.8	584.7	5.3	
TOTAL				11.7	

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle wash	67.3439	67.3425	1.4	0.0001
³⁰⁰ Condensables mls	84.5057	84.4946	11.1	0.0041
Filter #11	0.5368	0.5152	21.6	0.0081
H O (145 mls)	blank @ 14.5 mls	=		0.0001
Acetone (43.7 mls)	blank @ 43.7 mls	=		<0.0001
Gas Composition:		TOTAL	34.1	<0.0127

CO₂ 0 % volume (dry)
O₂ 21 % volume (dry)
CO % volume (dry)
N₂ 79 % volume (dry)
H₂O 1.3 % volume

MW (wet) 28.70
Excess Air %
Sampled Volume 47.27 SDCF
Isokinetic Rate 98.7 %

Particulate Concentration:

Co 0.0127 grains/SDCF @ 60 °F and 29.92 "Hg
C grains/SDCF @

Emission Rate:

E.R. 10.40 lbs/hr @ Qstd(dry) 95400 SDCFM

PARTICULATE EMISSIONS
TEST MONITOR DATA

Orifice k_m 0.5

		Duct Data			Meter Data			
Trav. Point	Time	Temp. °F	Head Δp	Velocity ft/sec	Vacuum "Hg	Temp. °F	Orifice ΔH , "H ₂ O	Volume CF
Northwest Port								
12	1648	340	0.42	41.7		70	3.16	842.30
11	1650.5	345	0.46	43.8		70	3.41	
10	1653	360	0.46	44.2		75	3.38	
9	1655.5	360	0.50	46.1	0	75	3.64	
8	1658	360	0.50	46.1		75	3.64	
7	1700.5	360	0.46	44.2		75	3.38	
6	1703	360	0.46	44.2		75	3.38	
5	1705.5	370	0.54	48.2		75	3.86	
4	1708	360	0.56	48.8		75	4.03	
3	1710.5	370	0.53	47.8	0	75	3.80	
2	1713	370	0.53	47.8		75	3.80	
1	1715.5	370	0.42	42.5		75	3.08	
	1718	Stop to	change	ports				863.80
Southwest Port								
12	1730	365	0.42	42.4		75	3.10	864.10
11	1732.5	365	0.42	42.4		75	3.10	
10	1735	380	0.40	41.7		75	2.92	
9	1737.5	380	0.42	42.8	0	75	3.05	
8	1740	380	0.42	42.8		75	3.05	
7	1742.5	380	0.37	40.1		75	2.73	
6	1745	375	0.40	41.6		75	2.94	
5	1747.5	375	0.40	41.6		75	2.94	
4	1750	370	0.40	41.5		75	2.95	
3	1752.5	370	0.40	41.5	1	75	2.95	
2	1755	370	0.43	43.0		75	3.15	
1	1757.5	370	0.43	43.0		75	3.15	
	1800	End of	test					883.90
Total	60 Minutes				Max. 1		TOTAL	40.9
Average	367			43.8	Average	75	3.28	

PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Clinker Cooler

Run : 3

Date: 8/4/83

Time: 1648 - 1800

Absorber Type	Contents	Final	Tare	Net H ₂ O
Lg. Grnbrg	Distilled H ₂ O	527.2	522.2	5.0
Sm. Ginbrg	Distilled H ₂ O	395.5	396.2	0.7
liquid trap	empty	102.1	99.7	2.4
	silica gel	655.9	648.6	7.3
TOTAL				14.0

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle wash	68.6317	68.6249	6.8	0.0026
Condensables (325 mls)	84.6739	84.6696	4.3	0.0017
Filter #7	0.4505	0.4186	31.9	0.0123
Acetone (102.7 mls)	blank @ 102.7 mls	=		<0.0001
H ₂ O (65.3 mls)	blank @ 65.3 mls	=		<0.0001
Gas Composition:		TOTAL	43.0	0.0166

Gas Composition:

CO ₂	O	% volume (dry)
0.00	0.00	0.00
0.01	0.01	0.01
0.02	0.02	0.02
0.03	0.03	0.03
0.04	0.04	0.04
0.05	0.05	0.05
0.06	0.06	0.06
0.07	0.07	0.07
0.08	0.08	0.08
0.09	0.09	0.09
0.10	0.10	0.10
0.11	0.11	0.11
0.12	0.12	0.12
0.13	0.13	0.13
0.14	0.14	0.14
0.15	0.15	0.15
0.16	0.16	0.16
0.17	0.17	0.17
0.18	0.18	0.18
0.19	0.19	0.19
0.20	0.20	0.20
0.21	0.21	0.21
0.22	0.22	0.22
0.23	0.23	0.23
0.24	0.24	0.24
0.25	0.25	0.25
0.26	0.26	0.26
0.27	0.27	0.27
0.28	0.28	0.28
0.29	0.29	0.29
0.30	0.30	0.30
0.31	0.31	0.31
0.32	0.32	0.32
0.33	0.33	0.33
0.34	0.34	0.34
0.35	0.35	0.35
0.36	0.36	0.36
0.37	0.37	0.37
0.38	0.38	0.38
0.39	0.39	0.39
0.40	0.40	0.40
0.41	0.41	0.41
0.42	0.42	0.42
0.43	0.43	0.43
0.44	0.44	0.44
0.45	0.45	0.45
0.46	0.46	0.46
0.47	0.47	0.47
0.48	0.48	0.48
0.49	0.49	0.49
0.50	0.50	0.50
0.51	0.51	0.51
0.52	0.52	0.52
0.53	0.53	0.53
0.54	0.54	0.54
0.55	0.55	0.55
0.56	0.56	0.56
0.57	0.57	0.57
0.58	0.58	0.58
0.59	0.59	0.59
0.60	0.60	0.60
0.61	0.61	0.61
0.62	0.62	0.62
0.63	0.63	0.63
0.64	0.64	0.64
0.65	0.65	0.65
0.66	0.66	0.66
0.67	0.67	0.67
0.68	0.68	0.68
0.69	0.69	0.69
0.70	0.70	0.70
0.71	0.71	0.71
0.72	0.72	0.72
0.73	0.73	0.73
0.74	0.74	0.74
0.75	0.75	0.75
0.76	0.76	0.76
0.77	0.77	0.77
0.78	0.78	0.78
0.79	0.79	0.79
0.80	0.80	0.80
0.81	0.81	0.81
0.82	0.82	0.82
0.83	0.83	0.83
0.84	0.84	0.84
0.85	0.85	0.85
0.86	0.86	0.86
0.87	0.87	0.87
0.88	0.88	0.88
0.89	0.89	0.89
0.90	0.90	0.90
0.91	0.91	0.91
0.92	0.92	0.92
0.93	0.93	0.93
0.94	0.94	0.94
0.95	0.95	0.95
0.96	0.96	0.96
0.97	0.97	0.97
0.98	0.98	0.98
0.99	0.99	0.99
1.00	1.00	1.00

02	21.0	% volume (dry)
----	------	----------------

CO % volume (dry)

N2		% volume (dry)
79		

H₂O $\frac{1.6}{1.6}$ % volume

TOTAL

43.0

0.0166

MW (wet) 28.67

Excess Air 20.01 %

Sampled Volume	39 97	SDCF
----------------	-------	------

Isokinetic Rate 99 1 %

Particulate Concentration:

Co 0.0166grains/SDCF @ 60 °F and 29.92 "Hg

C grains/SDCF @

Emission Rate:

E.R. 13.12 lbs/hr @ Qstd(dry) 92100 SDCFM

PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Clinker Cooler

Run : 3

Date: 8/4/83

Time: 1648 - 1800

Absorber Type	Contents	Final	Tare	Net H ₂ O
Lg. Grnbrg	Distilled H ₂ O	527.2	522.2	5.0
Sm. Ginbrg	Distilled H ₂ O	395.5	396.2	0.7
liquid trap	empty	102.1	99.7	2.4
	silica gel	655.9	648.6	7.3
TOTAL				14.0

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle wash	68.6317	68.6249	6.8	0.0026
Condensables (325 mls)	84.6739	84.6696	4.3	0.0017
Filter #7	0.4505	0.4186	31.9	0.0123
Acetone (102.7 mls)	blank @ 102.7 mls	=		<0.0001
H ₂ O (65.3 mls)	blank @ 65.3 mls	=		<0.0001
Gas Composition:	'TOTAL		43.0	0.0166

Gas Composition:

CO ₂	0	% volume (dry)
O ₂	21.0	% volume (dry)
CO		% volume (dry)
N ₂	79	% volume (dry)
H ₂ O	1.6	% volume

'TOTAL

43.0	0.0166
------	--------

MW (wet) 28.67
Excess Air %
Sampled Volume 99.97 SDCF
Isokinetic Rate 99.1 %

Particulate Concentration:

Co 0.0166 grains/SDCF @ 60 °F and 29.92 "Hg

C grains/SDCF @

Emission Rate:

E.R. 13.12 lbs/hr @ Qstd(dry) 92100 SDCFM

[illegible]



PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Coal Stack
Date: 8/4/83

Run: 1
Time: 1107 - 1220

Absorber Type	Contents	Final	Tare	Net	H2O
Lg. Ginbrg	Distilled H ₂ O	611.4	549.3	62.1	
Sm. Ginbrg	Distilled H ₂ O	364.8	402.1	-37.3	
liquid trap	empty	99.8	99.3	0.5	
	silica gel	666.6	660.3	6.3	
TOTAL				31.6	

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle wash	68.3080	68.3009	7.1	0.0032
400 Condensables mls	68.5165	68.5120	4.5	0.0020
Filter #6	0.4182	0.4180	0.2	0.0001
H ₂ O (12.1 mls)	blank @ 12.1 mls =			<0.0001
Acetone (55.3 mls)	blank @ 55.3 mls =			<0.0001
Gas Composition:				
CO ₂ 0.5 % volume (dry)			TOTAL	

Gas Composition:

CO₂ 0.5 % volume (dry)
O₂ 20.5 % volume (dry)
CO _____ % volume (dry)
N₂ 79.0 % volume (dry)
H₂O 4.1 % volume

TOTAL

MW (wet) 28.74
Excess Air _____ %
Sampled Volume 34.26 SDCF
Isokinetic Rate 91.5 %

Particulate Concentration:

Co _____ grains/SDCF @ 60 °F and 29.92 "Hg
C _____ grains/SDCF @ _____

Emission Rate:

E.R. 0.95 lbs/hr @ Qstd(dry) 21000 SDCFM



Date 8/4/83 Run 2

Client Lonestar

Unit	Coal Stack
1	1
2	2
3	3
4	4
5	5
6	6
7	7
8	8
9	9
10	10
11	11
12	12
13	13
14	14
15	15
16	16
17	17
18	18
19	19
20	20
21	21
22	22
23	23
24	24
25	25
26	26
27	27
28	28
29	29
30	30
31	31
32	32
33	33
34	34
35	35
36	36
37	37
38	38
39	39
40	40
41	41
42	42
43	43
44	44
45	45
46	46
47	47
48	48
49	49
50	50
51	51
52	52
53	53
54	54
55	55
56	56
57	57
58	58
59	59
60	60
61	61
62	62
63	63
64	64
65	65
66	66
67	67
68	68
69	69
70	70
71	71
72	72
73	73
74	74
75	75
76	76
77	77
78	78
79	79
80	80
81	81
82	82
83	83
84	84
85	85
86	86
87	87
88	88
89	89
90	90
91	91
92	92
93	93
94	94
95	95
96	96
97	97
98	98
99	99
100	100

Ambient Temp. 75 °F

Press. bar 29.82 in. Hg

Press. static -27.0 in. H₂O

Press. duct 27.84 in. Hg

Assumed MW 28.45 %H₂O 4.1

Sample Train Temp.:

Probe 245 245 250 250

Filter 240, 245, 255, 255

Sample Line

Post-Test Leak Check:

Leak Rate 0.008 CFM

0 7 in. Hg Vac.

[illegible]



PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Coal Stack
Date: 8/4/83

Run: 2
Time: 1410 - 1519

Absorber Type	Contents	Final	Tare	Net	H2O
Lg. Genbrg	Distilled H ₂ O	679.3	578.6	100.7	
Sm. Genbrg	Distilled H ₂ O	296.9	375.0	- 78.1	
liquid trap	empty	100.5	98.6	1.9	
	silica gel	654.8	648.0	6.8	
TOTAL				31.3	

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle wash	63.5920	63.5880	4.0	0.0017
350 Condensables mls	90.1761	90.1731	3.0	0.0013
Filter #10	0.4212	0.4207	0.5	0.0002
H ₂ O (11.6 mls)	blank @ 11.6 mls	=		<0.0001
Acetone (52.5 mls)	blank @ 52.5 mls	=		<0.0001
TOTAL			7.5	0.0032

Gas Composition:

CO₂ 0.5 % volume (dry)
O₂ 20.5 % volume (dry)
CO % volume (dry)
N₂ 79.0 % volume (dry)
H₂O 3.8 % volume

MW (wet) 28.49
Excess Air %
Sampled Volume 36.57 SDCF
Isokinetic Rate 95.8 %

Particulate Concentration:

Co 0.0032 grains/SDCF @ 60 °F and 29.92 "Hg
C grains/SDCF @

Emission Rate:

E.R. 0.58 lbs/hr @ Qstd(dry) 21300 SDCFM

PARTICULATE EMISSIONS
TEST MONITOR DATA

Sample Train Temp.:	Nozzle & Probe Mat.	SS
Probe 260, 260, 270 °F	Filter Holder Mat.	SS
Filter 235, 245, 260 °F	Filter #	9
Sample Line	Nozzle #	5G i.d. 5.0 mm
Post-Test Leak Check:	Pitot #	5294 Cp 0.78
Leak Rate 0.008 CFM	Temp. Unit #	549
@ 4 in. Hg Vac.	Mag. #	375 Meter # 631
	Orifice	mm 0.5

[illegible]



PARTICULATE EMISSIONS

DATA & RESULTS:

Site: Coal Stack
Date: 8/4/83

Run: 3
Time: 1654 - 1805

Absorber Type	Contents	Final	Tare	Net	H2O
Lg. Grnbrg	Distilled H ₂ O	573.0	549.4	23.6	
Sm. Ginbrg	Distilled H ₂ O	425.8	422.2	3.6	
liquid trap	empty	100.0	99.8	0.2	
	silica gel	695.2	686.3	8.9	
TOTAL				36.3	

Filter Sample: Type EPA Flat Filter

Sample Fraction	Final Wt.	Tare Wt.	Net mgram	Co, grains/SDCF
Probe & Nozzle wash	83.5999	83.5994	0.5	0.0002
³²⁵ Condensables mls	86.8324	68.8316	0.8	0.0003
Filter #9	0.4220	0.4213	0.7	0.0003
H ₂ O (19.3 mls)	blank @ 19.3 mls	=		<0.0001
Acetone (54.5 mls)	blank @ 54.5 mls	=		<0.0001
Gas Composition:		TOTAL	2.0	0.0008

CO₂ 0.4 % volume (dry)
O₂ 20.6 % volume (dry)
CO _____ % volume (dry)
N₂ 79 % volume (dry)
H₂O 4.1 % volume

MW (wet) 28.44
Excess Air _____ %
Sampled Volume 39.38 SDCF
Isokinetic Rate 102.6 %

Particulate Concentration:

Co 0.0008 grains/SDCF @ 60 °F and 29.92 "Hg
C _____ grains/SDCF @ _____

Emission Rate:

E.R. 0.15 lbs/hr @ Qstd(dry) 21400 SDCFM