

Victorville #2

D. Y. MA AP-42 Section 11.6  
Reference 56  
Report Sect. 4  
Reference 61

Recal - coal

Note: This is a reference cited in AP 42, *Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at [www.epa.gov/ttn/chief/ap42/](http://www.epa.gov/ttn/chief/ap42/)

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PERFORMANCE GUARANTEE TESTING AT  
SOUTHWESTERN PORTLAND CEMENT

February 5 through 8, 1985

Prepared for

Southwestern Portland Cement  
15000 Seventh Street, Suite 201  
Victorville, California 92392

February 1985

Prepared by

Pape & Steiner Environmental Services  
5801 Norris Road  
Bakersfield, California 93308

Report PS-85-382/Project 5371-85

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## SECTION 1

### INTRODUCTION

At the request of Southwestern Portland Cement, Pape & Steiner Environmental Services conducted a series of emission tests on the effluent from #2 Kiln Stack, the #2 Raw Mill Stack, the #12 Finish Mill and the #2 Clinker Cooler Stack from February 5 to February 8, 1985. The purpose of these tests was to determine if the air pollution control devices serving each of these point sources met the manufacturer's performance guarantee.

Section 2 of this report summarizes the test matrix for this program. Section 3 presents the test results. Sections 4 and 5 describe the sampling and analysis procedures used to obtain these results. Section 6 summarizes the QA/QC steps taken on this program. Finally, the Appendix contains all the raw data and calculations.

## SECTION 2

### TEST MATRIX

Recently, Southwestern Portland Cement (SWPC) completed a large expansion of their cement plant located near Victorville, California. A new kiln (#2) equipped with a baghouse, a new clinker cooler (#2) equipped with a gravel bed filter, a new raw mill (#2) equipped with a baghouse, and a new finish mill (#12) also equipped with a baghouse for air pollution control have been added to the existing plant.

The purpose of this test program was to determine if the particulate and gaseous emissions from these sources met the performance guarantee stated by the supplier (Humboldt Wedag). According to the contract with SWPC, the performance guarantee tests were to be run over a three day period to insure each control device operated within the specifications over different process conditions. Table 2-1 summarizes the tests performed on these control devices. Since operational difficulties occurred with the kiln during this week, SWPC shortened the test period on the kiln to two days, instead of three days, to insure all the tests would be completed that week.

TABLE 2-1. SWPC PERFORMANCE GUARANTEE TEST MATRIX

| <u>Unit</u> | <u>Date</u> | <u>Pollutant</u>                           | <u>Test No.</u> | <u>Test Time</u>                 |
|-------------|-------------|--------------------------------------------|-----------------|----------------------------------|
| Kiln        | 02/06/85    | Particulates                               | 1               | 10:20 am - 12:40 pm <sup>a</sup> |
|             |             |                                            | 2               | 2:47 pm - 5:06 pm <sup>b</sup>   |
|             | 02/07/85    | Particulates                               | 3               | 8:37 am - 10:54 am <sup>a</sup>  |
|             | 02/06/85    | NO <sub>x</sub> , SO <sub>2</sub> , CO, HC |                 | 7:45 am - 10:20 am <sup>a</sup>  |
|             |             |                                            |                 | 10:35 am - 1:10 pm <sup>a</sup>  |
|             |             |                                            |                 | 1:35 pm - 5:15 pm <sup>b</sup>   |
|             | 02/07/85    | NO <sub>x</sub> , SO <sub>2</sub> , CO, HC |                 | 7:40 am - 12:00 pm <sup>a</sup>  |
|             |             |                                            |                 | 12:30 pm - 4:30 pm <sup>a</sup>  |
|             | 02/08/85    | NO <sub>x</sub> , SO <sub>2</sub> , CO, HC |                 | 7:30 am - 12:00 pm <sup>a</sup>  |
| Clinker     | 02/06/85    | Particulates                               | 1               | 11:00 am - 12:33 pm <sup>a</sup> |
|             |             |                                            | 2               | 2:45 pm - 4:21 pm <sup>b</sup>   |
|             | 02/08/85    | Particulates                               | 3               | 9:26 am - 10:52 am <sup>a</sup>  |
| Finish Mill | 02/05/85    | Particulates                               | 1               | 1:05 pm - 3:09 pm                |
|             | 02/07/85    | Particulates                               | 2               | 11:53 am - 4:00 pm               |
|             | 02/08/85    | Particulates                               | 3               | 9:25 am - 11:31 am               |
| Raw Mill    | 02/05/85    | Particulates                               | 1               | 11:44 am - 1:50 pm               |
|             | 02/07/85    | Particulates                               | 2               | 9:35 am - 11:43 am               |
|             | 02/08/85    | Particulates                               | 3               | 1:26 pm - 3:31 pm                |

<sup>a</sup>215 TPH<sup>b</sup>190 TPH ← Kiln Feed

## SECTION 3

### TEST RESULTS

Tables 3-1 to 3-4 summarize the results of the particulate tests performed on the Kiln, Clinker Cooler, Finish Mill and Raw Mill. Table 3-5 compares the measured volumetric flowrates to the design value for each point source. Finally Table 3-6 presents the results of the gaseous emissions performed on the #2 Kiln.

#### 3.1 PARTICULATE TESTS

All of the point sources tested with the exception of the Clinker Cooler Gravel Bed Filter were well within the specification guaranteed by the equipment manufacturer. It should be noted that the actual volumetric flowrate through the baghouses serving the Kiln, Finish Mill and Raw Mill were considerably less than the design flowrate. Since the volume of gas handled by these baghouses is less than design, the face velocity across the bags is reduced which is very beneficial to the performance of the baghouse.

The volume of gas being processed by the gravel bed filter serving the Clinker Cooler greatly exceeds the design specification. This may be causing some carryover of fine dust particles out of the bed. It should be

noted that the results of Test #1 on February 6, 1985 are suspect. An examination of the residue after evaporation of the sampling nozzle and probe acetone rinsing revealed several large particles which were not present in the remaining samples. The high nozzle and probe catch measured for Test #1 may be the result of contamination (i.e., the nozzle may have touched the stack wall or scraped the sample port during the test).

### 3.2 GASEOUS TESTS

$\text{NO}_x$  and CO emissions from the Kiln were variable but  $\text{SO}_2$  emissions were constant and very low.  $\text{NO}_x$  and CO emissions decreased when the Kiln production rate decreased from 215 TPH to 190 TPH. CO emissions on February 8, 1985, were very much higher than previous tests.  $\text{NO}_x$  emissions were lower but so was the Kiln  $\text{O}_2$  content.

HC emissions were also variable even at the same Kiln production rate.



TABLE 3-1. SUMMARY OF SOURCE EMISSION TEST DATA

UNIT TESTED: #2 KilnLOCATION: Baghouse Outlet

| Test number                                        | 1        | 2        | 3        | Average |
|----------------------------------------------------|----------|----------|----------|---------|
| Date                                               | 02/06/85 | 02/06/85 | 02/07/85 |         |
| Test condition                                     | 215 TPH  | 190 TPH  | 215 TPH  |         |
| Barometric pressure (in. Hg)                       | 26.46    | 26.43    | 26.52    |         |
| Stack pressure (in. Hg)                            | 26.44    | 26.42    | 26.50    |         |
| Stack area (Ft <sup>2</sup> )                      | 139.63   | 139.63   | 139.63   |         |
| Elapsed sampling time (min)                        | 120      | 120      | 120      |         |
| Volume gas sampled (dscf)                          | 75.9941  | 72.3753  | 76.2440  |         |
| F factor                                           |          |          |          |         |
| GAS DATA                                           |          |          |          |         |
| Average gas velocity (fps)                         | 36.0     | 33.6     | 36.0     | 35.2    |
| Average gas temperature (°F)                       | 381.1    | 362.8    | 380.3    | 374.7   |
| Gas flowrate (dscfm)                               | 159,581  | 152,109  | 159,898  | 157,196 |
| Gas analysis (dry percent basis)                   |          |          |          |         |
| Carbon dioxide                                     | 18.70    | 18.69    | 19.04    |         |
| Oxygen                                             | 9.17     | 9.30     | 9.10     |         |
| Carbon monoxide - <i>See Table 3-6.</i>            | ---      | ---      | ---      |         |
| Water                                              | 4.58     | 4.59     | 4.63     | 4.60    |
| EMISSION CONCENTRATION - <i>Also See Table 3-6</i> |          |          |          |         |
| Filterable particulate (gr/dscf)                   | 0.0025   | 0.0015   | 0.0020   | 0.0020  |
| Total particulate (gr/dscf)                        |          |          |          |         |
| Total sulfate (gr/dscf)                            |          |          |          |         |
| SO <sub>3</sub> (ppm)                              |          |          |          |         |
| SO <sub>2</sub> (ppm)                              |          |          |          |         |
| NO <sub>x</sub> (ppm)                              |          |          |          |         |
| EMISSION RATE                                      |          |          |          |         |
| Filterable particulate (lb/hr)                     | 3.42     | 2.00     | 2.69     | 2.70    |
| Total particulate (lb/hr)                          |          |          |          |         |
| Total sulfate (lb/hr)                              |          |          |          |         |
| SO <sub>3</sub> (lb/hr)                            |          |          |          |         |
| SO <sub>2</sub> (lb/hr)                            |          |          |          |         |
| NO <sub>x</sub> (lb/hr)                            |          |          |          |         |
| Lb/MMBtu-EMISSION FACTOR                           |          |          |          |         |
| Filterable particulate                             |          |          |          |         |
| Total particulate                                  |          |          |          |         |
| Total sulfate                                      |          |          |          |         |
| SO <sub>2</sub>                                    |          |          |          |         |
| NO <sub>x</sub>                                    |          |          |          |         |
| Lb/Bbl-EMISSION FACTOR                             |          |          |          |         |
| Total particulate                                  |          |          |          |         |
| Total sulfate                                      |          |          |          |         |
| SO <sub>2</sub>                                    |          |          |          |         |
| NO <sub>x</sub>                                    |          |          |          |         |

TABLE 3-2. SUMMARY OF SOURCE EMISSION TEST DATA

UNIT TESTED: #2 Clinker cooler LOCATION: Gravel Bed Filter Outlet

| #295                             |          |          |          |         |
|----------------------------------|----------|----------|----------|---------|
| Test number                      | 1        | 2        | 3        | Average |
| Date                             | 02/06/85 | 02/06/85 | 02/08/85 |         |
| Test condition                   | 215 TPH  | 190 TPH  | 215 TPH  |         |
| Barometric pressure (in. Hg)     | 26.46    | 26.43    | 26.43    |         |
| Stack pressure (in. Hg)          | 26.42    | 26.39    | 26.41    |         |
| Stack area (Ft <sup>2</sup> )    | 92.18    | 92.18    | 92.18    |         |
| Elapsed sampling time (min)      | 72       | 72       | 72       |         |
| Volume gas sampled (dscf)        | 46.2141  | 49.7283  | 48.4111  |         |
| F factor                         |          |          |          |         |
| GAS DATA                         |          |          |          |         |
| Average gas velocity (fps)       | 47.5     | 52.2     | 48.4     | 49.4    |
| Average gas temperature (°F)     | 358.1    | 377.8    | 361.7    | 365.9   |
| Gas flowrate (dscfm)             | 149,158  | 159,950  | 150,857  | 153,322 |
| Gas analysis (dry percent basis) |          |          |          |         |
| Carbon dioxide                   | 0.00     | 0.00     | 0.00     |         |
| Oxygen                           | 20.90    | 20.90    | 20.90    |         |
| Carbon monoxide                  | ---      | ---      | ---      |         |
| Water                            | 0.39     | 0.36     | 0.64     | 0.46    |
| EMISSION CONCENTRATION           |          |          |          |         |
| Filterable particulate (gr/dscf) | 0.0800   | 0.0233   | 0.0198   | 0.0410  |
| Total particulate (gr/dscf)      |          |          |          |         |
| Total sulfate (gr/dscf)          |          |          |          |         |
| SO <sub>3</sub> (ppm)            |          |          |          |         |
| SO <sub>2</sub> (ppm)            |          |          |          |         |
| NO <sub>x</sub> (ppm)            |          |          |          |         |
| EMISSION RATE                    |          |          |          |         |
| Filterable particulate (lb/hr)   | 102.25   | 31.99    | 25.63    | 53.29   |
| Total particulate (lb/hr)        |          | 28.81    |          |         |
| Total sulfate (lb/hr)            |          |          |          |         |
| SO <sub>3</sub> (lb/hr)          |          |          |          |         |
| SO <sub>2</sub> (lb/hr)          |          |          |          |         |
| NO <sub>x</sub> (lb/hr)          |          |          |          |         |
| Lb/MMBtu-EMISSION FACTOR         |          |          |          |         |
| Filterable particulate           |          |          |          |         |
| Total particulate                |          |          |          |         |
| Total sulfate                    |          |          |          |         |
| SO <sub>2</sub>                  |          |          |          |         |
| NO <sub>x</sub>                  |          |          |          |         |
| Lb/Bbl-EMISSION FACTOR           |          |          |          |         |
| Total particulate                |          |          |          |         |
| Total sulfate                    |          |          |          |         |
| SO <sub>2</sub>                  |          |          |          |         |
| NO <sub>x</sub>                  |          |          |          |         |

TABLE 3-3. SUMMARY OF SOURCE EMISSION TEST DATA

UNIT TESTED: #12 Finish Mill

LOCATION: Baghouse Outlet

| Test number                      | 1        | 2        | 3        | Average |
|----------------------------------|----------|----------|----------|---------|
| Date                             | 02/05/85 | 02/07/85 | 02/07/85 |         |
| Test condition                   | Normal   | Normal   | Normal   |         |
| Barometric pressure (in. Hg)     | 27.35    | 27.28    | 27.18    |         |
| Stack pressure (in. Hg)          | 27.34    | 27.27    | 27.17    |         |
| Stack area (Ft <sup>2</sup> )    | 19.63    | 19.63    | 19.63    |         |
| Elapsed sampling time (min)      | 120      | 120      | 120      |         |
| Volume gas sampled (dscf)        | 81.7199  | 73.0523  | 75.8621  |         |
| F factor                         |          |          |          |         |
| GAS DATA                         |          |          |          |         |
| Average gas velocity (fps)       | 22.0     | 21.0     | 21.1     | 21.4    |
| Average gas temperature (°F)     | 186.0    | 195.3    | 185.6    | 189.0   |
| Gas flowrate (dscfm)             | 17,914   | 16,504   | 17,007   | 17,142  |
| Gas analysis (dry percent basis) |          |          |          |         |
| Carbon dioxide                   | 0.0      | 0.00     | 0.00     |         |
| Oxygen                           | 20.90    | 20.90    | 20.90    |         |
| Carbon monoxide                  | ---      | ---      | ---      |         |
| Water                            | 7.23     | 9.18     | 8.02     | 8.14    |
| EMISSION CONCENTRATION           |          |          |          |         |
| Filterable particulate (gr/dscf) | 0.0054   | 0.0050   | 0.0013   | 0.0039  |
| Total particulate (gr/dscf)      |          |          |          |         |
| Total sulfate (gr/dscf)          |          |          |          |         |
| SO <sub>3</sub> (ppm)            |          |          |          |         |
| SO <sub>2</sub> (ppm)            |          |          |          |         |
| NO <sub>x</sub> (ppm)            |          |          |          |         |
| EMISSION RATE                    |          |          |          |         |
| Filterable particulate (lb/hr)   | 0.84     | 0.71     | 0.19     | 0.58    |
| Total particulate (lb/hr)        |          |          |          |         |
| Total sulfate (lb/hr)            |          |          |          |         |
| SO <sub>3</sub> (lb/hr)          |          |          |          |         |
| SO <sub>2</sub> (lb/hr)          |          |          |          |         |
| NO <sub>x</sub> (lb/hr)          |          |          |          |         |
| Lb/MMBtu-EMISSION FACTOR         |          |          |          |         |
| Filterable particulate           |          |          |          |         |
| Total particulate                |          |          |          |         |
| Total sulfate                    |          |          |          |         |
| SO <sub>2</sub>                  |          |          |          |         |
| NO <sub>x</sub>                  |          |          |          |         |
| Lb/Bbl-EMISSION FACTOR           |          |          |          |         |
| Total particulate                |          |          |          |         |
| Total sulfate                    |          |          |          |         |
| SO <sub>2</sub>                  |          |          |          |         |
| NO <sub>x</sub>                  |          |          |          |         |

TABLE 3-4. SUMMARY OF SOURCE EMISSION TEST DATA

UNIT TESTED: #2 Raw Mill

LOCATION: Baghouse Outlet

| Test number                      | 1        | 2        | 3        | Average |
|----------------------------------|----------|----------|----------|---------|
| Date                             | 02/05/85 | 02/07/85 | 02/07/85 |         |
| Test condition                   | Normal   | Normal   | Normal   |         |
| Barometric pressure (in. Hg)     | 26.45    | 26.52    | 26.52    |         |
| Stack pressure (in. Hg)          | 26.42    | 26.49    | 26.49    |         |
| Stack area (Ft <sup>2</sup> )    | 28.27    | 28.27    | 28.27    |         |
| Elapsed sampling time (min)      | 120      | 120      | 120      |         |
| Volume gas sampled (dscf)        | 86.8368  | 87.6826  | 92.2257  |         |
| F factor                         |          |          |          |         |
| GAS DATA                         |          |          |          |         |
| Average gas velocity (fps)       | 46.8     | 49.0     | 51.6     | 49.1    |
| Average gas temperature (°F)     | 157.4    | 171.3    | 169.7    | 166.1   |
| Gas flowrate (dscfm)             | 56,826   | 58,851   | 61,797   | 59,158  |
| Gas analysis (dry percent basis) |          |          |          |         |
| Carbon dioxide                   | 0.00     | 0.00     | 0.00     |         |
| Oxygen                           | 20.90    | 20.90    | 20.90    |         |
| Carbon monoxide                  | ---      | ---      | ---      |         |
| Water                            | 5.14     | 4.45     | 4.89     | 4.83    |
| EMISSION CONCENTRATION           |          |          |          |         |
| Filterable particulate (gr/dscf) | 0.0034   | 0.0036   | 0.0036   | 0.0035  |
| Total particulate (gr/dscf)      |          |          |          |         |
| Total sulfate (gr/dscf)          |          |          |          |         |
| SO <sub>3</sub> (ppm)            |          |          |          |         |
| SO <sub>2</sub> (ppm)            |          |          |          |         |
| NO <sub>x</sub> (ppm)            |          |          |          |         |
| EMISSION RATE                    |          |          |          |         |
| Filterable particulate (lb/hr)   | 1.65     | 1.82     | 1.93     | 1.80    |
| Total particulate (lb/hr)        |          |          |          |         |
| Total sulfate (lb/hr)            |          |          |          |         |
| SO <sub>3</sub> (lb/hr)          |          |          |          |         |
| SO <sub>2</sub> (lb/hr)          |          |          |          |         |
| NO <sub>x</sub> (lb/hr)          |          |          |          |         |
| Lb/MMBtu-EMISSION FACTOR         |          |          |          |         |
| Filterable particulate           |          |          |          |         |
| Total particulate                |          |          |          |         |
| Total sulfate                    |          |          |          |         |
| SO <sub>2</sub>                  |          |          |          |         |
| NO <sub>x</sub>                  |          |          |          |         |
| Lb/Bbl-EMISSION FACTOR           |          |          |          |         |
| Total particulate                |          |          |          |         |
| Total sulfate                    |          |          |          |         |
| SO <sub>2</sub>                  |          |          |          |         |
| NO <sub>x</sub>                  |          |          |          |         |

TABLE 3-5. COMPARISON OF ACTUAL AND DESIGN DATA FOR  
AIR POLLUTION CONTROL DEVICES

| Point Source  | Actual Flowrate<br>(acfm)    | Design Flowrate<br>(acfm)        | Actual Emissions    |        | Design Emissions                    |       |
|---------------|------------------------------|----------------------------------|---------------------|--------|-------------------------------------|-------|
|               |                              |                                  | gr/scf              | lb/hr  | gr/scf                              | lb/hr |
| Kiln Baghouse | <sup>a</sup> 301,454 @ 381°F | 400,000 @ 400°F                  | 0.0024              | 3.42   |                                     |       |
|               | <sup>b</sup> 281,359 @ 363°F |                                  | 0.0014              | 2.00   |                                     |       |
|               | <sup>a</sup> 301,321 @ 380°F |                                  | 0.0019              | 2.69   |                                     |       |
|               | 294,711 @ 375°F              |                                  | 0.0019              | 2.69   | 0.015                               | 22.6  |
| Clinker GBF   | <sup>a</sup> 262,704 @ 358°F | 187,700 @ 428°F<br><i>gr/acf</i> | 0.0517 <sup>d</sup> | 102.25 |                                     |       |
|               | <sup>b</sup> 288,760 @ 378°F |                                  | 0.0148              | 31.99  |                                     |       |
|               | <sup>a</sup> 267,693 @ 362°F |                                  | 0.0127              | 25.63  |                                     |       |
|               | 273,052 @ 366°F              |                                  | 0.0264 <sup>c</sup> | 53.29  | 0.010 <sup>a</sup><br><i>gr/acf</i> | 17.5  |
| Finish Mill   | 25,855 @ 186°F               | 35,000 @ 230°F                   | 0.0050              | 0.84   |                                     |       |
|               | 24,741 @ 195°F               |                                  | 0.0045              | 0.71   |                                     |       |
|               | 24,903 @ 186°F               |                                  | 0.0012              | 0.19   |                                     |       |
|               | 25,166 @ 189°F               |                                  | 0.0036              | 0.58   | 0.015                               | 19.5  |
| Raw Mill      | 79,346 @ 157°F               | 95,000 @ 195°F                   | 0.0032              | 1.65   |                                     |       |
|               | 83,170 @ 171°F               |                                  | 0.0034              | 1.82   |                                     |       |
|               | 87,507 @ 170°F               |                                  | 0.0034              | 1.93   |                                     |       |
|               | 83,341 @ 166°F               |                                  | 0.0033              | 1.80   | 0.015                               | 24.2  |

<sup>a</sup>215 TPH      <sup>b</sup>190 TPH      <sup>c</sup>gr/acf      <sup>d</sup>contamination in probe and nozzle;  
result too high

From Bill Ogle 4/2/85

$$CI = \frac{KF \times 0.27}{1.65} + \text{Coal H}_2\text{O} = 15 \text{ T/H} = .625 \text{ T/hr}$$

14.62 T/hr Coal 14.6 T/hr Coal  
114 TCE/hr 114 TCE/hr

13.37 T/hr Coal  
100.8 TCE/hr

TABLE 3-6. GASEOUS EMISSIONS FROM KILN

| Concentration (ppm, dry) | Date                                                                                          | Time                               |                                       |                                                   |                    |
|--------------------------|-----------------------------------------------------------------------------------------------|------------------------------------|---------------------------------------|---------------------------------------------------|--------------------|
|                          | 02/06/85                                                                                      | 7:45 am - 10:20 am <sup>a</sup>    | 10:55 am - 1:10 pm <sup>a</sup>       | 1:55 pm - 4:15 pm <sup>b</sup>                    | Avg 2              |
| Range                    | NO <sub>x</sub><br>SO <sub>2</sub><br>CO <sub>2</sub>                                         | 460 - 510<br>4<br>275 - 400        | 510 - 600<br>0 - 3<br>150 - 270       | 470 - 550<br>0 - 5<br>70 - 220                    |                    |
| Average                  | NO <sub>x</sub><br>SO <sub>2</sub><br>CO <sub>2</sub><br>* C <sub>1</sub> > C <sub>1</sub> HC | 487<br>4<br>306                    | 549<br>2<br>210<br>Methane → 2.6/49.1 | 498<br>3<br>158<br>3.2/23.5                       |                    |
| Emission Rate (lb/hr)    |                                                                                               |                                    | Greater than Methane                  |                                                   |                    |
| Range                    | NO <sub>x</sub><br>SO <sub>2</sub><br>CO <sub>2</sub>                                         | 526 - 583<br>6.4<br>191 - 278      | 583 - 686<br>0 - 4.8<br>104 - 188     | 512 - 599<br>0 - 7.6<br>46 - 146                  |                    |
| Average                  | NO <sub>x</sub><br>SO <sub>2</sub><br>CO <sub>2</sub><br>* C <sub>1</sub> > C <sub>1</sub> HC | 557<br>6.4<br>213<br>4.88<br>0.054 | 628<br>3.2<br>146<br>5.51<br>0.024    | 543<br>4.6<br>105<br>539<br>0.046<br>= 4.7<br>155 | 576<br>4.7<br>5.26 |

| Concentration (ppm, dry) | Date                                                                                          | Time                                  |                                     |  |
|--------------------------|-----------------------------------------------------------------------------------------------|---------------------------------------|-------------------------------------|--|
|                          | 02/07/85                                                                                      | 7:40 am - 12:00 pm                    | 12:30 pm - 4:30 pm                  |  |
| Range                    | NO <sub>x</sub><br>SO <sub>2</sub><br>CO <sub>2</sub>                                         | 460 - 570<br>4 - 5<br>250 - 350       | 410 - 510<br>3 - 4<br>225 - 330     |  |
| Average                  | NO <sub>x</sub><br>SO <sub>2</sub><br>CO <sub>2</sub><br>* C <sub>1</sub> > C <sub>1</sub> HC | 481<br>4<br>306<br>7.6/15.4           | 455<br>3<br>273                     |  |
| Emission Rate (lb/hr)    |                                                                                               | 14.5 T/hr Coal                        | 14.5 T/hr                           |  |
| Range                    | NO <sub>x</sub><br>SO <sub>2</sub><br>CO <sub>2</sub>                                         | 527 - 653<br>6.4 - 8.0<br>174 - 244   | 470 - 584<br>4.8 - 6.4<br>157 - 230 |  |
| Average                  | NO <sub>x</sub><br>SO <sub>2</sub><br>CO <sub>2</sub><br>* C <sub>1</sub> > C <sub>1</sub> HC | 551<br>6.5<br>213<br>0.057<br>3.0/5.1 | 521<br>5.4<br>190<br>0.047          |  |

| Concentration (ppm, dry) | Date                                                  | Time                            |  |
|--------------------------|-------------------------------------------------------|---------------------------------|--|
|                          | 02/08/85                                              | 7:30 am - 12:00 pm              |  |
| Range                    | NO <sub>x</sub><br>SO <sub>2</sub><br>CO <sub>2</sub> | 340 - 370<br>6 - 8<br>400 - 750 |  |
| Average                  | NO <sub>x</sub><br>SO <sub>2</sub><br>CO <sub>2</sub> | 358 - ppm<br>7.1<br>575         |  |

14.4 T/hr Coal  
11.5 - 101.4  
190 TPH

<sup>a</sup> 215 TPH

Avg Emissions  
#/hr  
560 - NO<sub>x</sub> - 5.03 #/TCE  
5.2 - SO<sub>2</sub> - 0.046  
174 - CO - 1.52  
NO<sub>x</sub> = 1.549 # NO<sub>x</sub> / MMBTU

Coal @ 12,800 BTU/lb

\* see page 5-2

## SECTION 4

### SAMPLING EQUIPMENT AND PROCEDURES

This section of the report describes the equipment and procedures used to conduct the particulate gaseous tests on this program.

#### 4.1 PRELIMINARY MEASUREMENTS

Before conducting the stack tests a series of preliminary measurements were made to determine:

- The location of the sampling site and the number and location of the sampling points to be used (EPA Method 1)
- The velocity, temperature, and pressure of the gases in the stack (EPA Method 2)
- The composition of the stack gases (EPA Method 3)
- The moisture content of the stack gases (psychrometric chart)

Using the results of these preliminary measurements and the calibration constants for the sampling train, a series of calculations were made to determine the value of K, a constant, and  $N_d$ , ideal nozzle diameter, required to run an isokinetic test according to the equation:

$$\Delta H = \left\{ \frac{60^2 \pi^2 K_p^2 C_p^2 (1 - B_{wo})^2 P_s MW_d}{576^2 K_o^2 MW_s P_m} \right\} \left( N_d^4 \right) \left( \frac{T_m}{T_s} \right) (\Delta P)$$

where

$$K = \left\{ \frac{60^2 \pi^2 K_p^2 C_p^2 (1 - B_{wo})^2 P_s^{MW_d}}{576^2 K_o^2 P_s^{MW_s}} \right\}$$

An actual nozzle, whose diameter was as close as possible to the ideal nozzle diameter, was selected for the test. Isokinetic sampling rates for each sampling point in the stack were computed using the equation:

$$\Delta H = (K)(N_d^4) \left( \frac{T_m}{T_s} \right) (\Delta P)$$

Since K and  $N_d$  are known, and remain constant during a test, the only variables are the meter temperature, the stack temperature and the velocity pressure for each sampling point.

#### 4.2 PREPARATION OF THE PARTICULATE SAMPLING TRAIN

All sampling train components were cleaned in the laboratory (soap and water, tap water rinse, distilled water rinse, and IPA rinse) to eliminate previous contamination. The sampling train components were sealed and transported to the sampling site in a mobile lab. The EPA Method 5 equipment used to measure particulates (filterable) consisted of:

- A calibrated 316 stainless steel nozzle for isokinetic sampling
- A heated Pyrex glass sampling probe (8' long for Raw Mill; 6' long for Kiln, Clinker and Finish Mill) equipped with an S-type



pitot tube and a thermocouple to measure stack velocity, pressure and temperature

- A heated Pyrex glass filter holder containing a weighed 100-mm Reeve Angel 934 AH glass fiber filter
- A Pyrex glass impinger train in an icebath (impingers 1 and 2 contained 100 ml distilled water; impinger 3 was dry; bubbler 4 contained a weighed amount of silica gel)
- An umbilical to connect the probe and sample box to the control module
- A control module containing a vacuum pump, a calibrated dry gas meter and a calibrated orifice meter to measure the pressure, temperature and flowrate throughout the train.

The sampling train was charged in the mobile lab using freshly prepared reagents. Each impinger and its contents was weighed to the nearest 0.1 gm on a calibrated electronic balance. Blanks of all filters and reagents were retained for subsequent analysis. The sampling point locations were marked on the probe using a high-temperature marker. The sampling train was completely assembled and lifted to the sampling site.

#### 4.3 SAMPLING PROCEDURES FOR PARTICULATE SAMPLING TRAIN

Prior to a test, the sampling train was heated and leak-checked at 15 inches Mercury to insure leakage was less than 0.02 cfm. The S-type pitot tube was also leak-checked. The sampling train was installed on the unirail and the probe was inserted into the stack at the farthest point.

An isokinetic sampling rate was calculated using an HP-41CV calculator for each sampling point on the traverse (6 points per traverse, 4 traverses @ 90° for Kiln; 6 points per traverse, 4 traverses @ 90° for Clinker; 8 points per traverse, 2 traverses @ 90° for Finish Mill; 6 points per traverse, 2 traverses @ 90° for Raw Mill). Each point was sampled for an equal period of time (5 minutes for Kiln; 3 minutes for Clinker; 7.5 minutes for Finish Mill; 10 minutes for Raw Mill) and all pertinent data was recorded on the data sheet for each point. The probe and sample box were maintained at 250°F throughout the traverse. The gases leaving the impinger train were maintained at <70°F. At the end of a traverse, the probe was withdrawn from the stack and the entire sampling train was transferred (intact) to the next sampling port. Another traverse of the stack was completed and the sampling train was withdrawn for the final leak check. This leak check was performed at 15 inches Mercury or at the highest vacuum achieved during the test. The S-type pitot tube was also checked at this time. The probe, nozzle, filter holder, and impinger train were sealed with tin foil and lowered to the mobile lab for sample recovery.

#### 4.4 SAMPLE RECOVERY PROCEDURES FOR PARTICULATE SAMPLING TRAIN

Sample recovery occurred in the mobile lab. The nozzle and probe were brushed and rinsed three times using ACS reagent grade acetone into a polyethylene sample bottle. The 100-mm filter was removed from the 4-inch filter holder and sealed in its petri dish. The front half of the 4-inch glass filter holder was brushed and rinsed with acetone. Each impinger was

removed from the icebath, wiped dry and weighed to the nearest 0.1 gm. All sample bottles and petri dishes were marked and labeled. A chain-of-custody log was completed and the field data sheet was also labeled with the sample ID numbers. The sampling train was then recharged in preparation for the next test.

#### 4.5 SAMPLING PROCEDURES FOR CONTINUOUS MONITORING

The continuous monitors used in the Pape & Steiner Mobile Monitoring Lab are shown in Table 4-1. Figure 4-1 is a schematic of the continuous monitoring system. The procedures used to continuously monitor stack gases for  $\text{NO}_x$ ,  $\text{SO}_2$ , CO,  $\text{CO}_2$ , and  $\text{O}_2$  strictly follow CARB Method 1-100.

Sample was taken from the stack using a 316 stainless steel probe. A Balston filter holder and fiberglass filter (99.9999 percent efficiency retention of 0.6 micron particles) was connected to the outlet of the probe. Sample gas was transported through heated Teflon sample line (maintained at  $>250^\circ\text{F}$ ) by a Teflon-lined diaphragm pump to a 316 stainless steel refrigeration type conditioner (Hankison Model E-4G-SS). The sample gas was passed through the conditioner two separate times under vacuum before entering the pump, then two additional times under pressure. The clean, dry sample gas ( $\sim 35^\circ\text{F}$ ) was then transported to the continuous analyzer system through an unheated Teflon line. A series of flowmeters, valves, and regulators maintain constant flow through the system at a constant pressure.

TABLE 4-1. CONTINUOUS MONITORING LAB

NO<sub>x</sub> CHEMILUMINESCENT ANALYZER -- THERMO ELECTRON MODEL 10

|                       |                                                                           |
|-----------------------|---------------------------------------------------------------------------|
| Response Time (0-90%) | 1.5 sec -- NO mode<br>1.7 sec -- NO <sub>x</sub> mode                     |
| Zero Drift            | Negligible after 1/2 hour warmup                                          |
| Linearity             | +1% of full scale                                                         |
| Accuracy              | Derived from the NO or NO <sub>2</sub> calibration gas, +1% of full scale |
| Output                | 0.100 mV, 0-10 mV, 0-5 V, 0-10 V                                          |

O<sub>2</sub> ANALYZER, FUEL TYPE -- TELEDYNE MODEL 326

|                       |                                                                                                                                      |
|-----------------------|--------------------------------------------------------------------------------------------------------------------------------------|
| Response Time (0-90%) | 60 seconds                                                                                                                           |
| Accuracy              | +1% of scale at constant temperatures;<br>+1% of scale of +5% of reading, whichever is greater, over the operating temperature range |
| Output                | 0-1 V                                                                                                                                |

CO<sub>2</sub>/CO INFRARED ANALYZER -- ANARAD MODEL AR-600

|                       |                            |
|-----------------------|----------------------------|
| Response Time (0-90%) | 5 seconds                  |
| Zero Drift            | +1%                        |
| Span Drift            | +1%                        |
| Linearity             | 1%                         |
| Resolution            | Less than 1% of full scale |
| Output                | 0-1 V                      |

SO<sub>2</sub> UV ANALYZER -- DUPONT MODEL 400

|                       |                                     |
|-----------------------|-------------------------------------|
| Response Time (0-90%) | Less than 1 second                  |
| Zero Drift            | Less than 1% full scale in 24 hours |
| Linearity             | +1% full scale                      |
| Accuracy              | +2% full scale                      |
| Output                | 0-10 mV                             |
| Operating Ranges      | 0-100 ppm, 0-1000 ppm               |

## STRIP CHART RECORDERS (3) -- LINEAR MODEL 486

|                    |                                                                            |
|--------------------|----------------------------------------------------------------------------|
| Pen Response       | 20 inches/second                                                           |
| Span -- full scale | 1 mV through 10 V                                                          |
| Zero Set           | Electronically adjustable full scale with 1 full scale of zero suppression |
| Accuracy           | Total limit of error <u>+0.5%</u>                                          |
| Dead Band          |                                                                            |
| Linearity          |                                                                            |
| Repeatability      |                                                                            |

## SCOTSMAN TRAILER

Fully Insulated  
Air conditioned  
8-ft x 14-ft x 11-ft

1. Filter 0.6  $\mu$ , 99.9999 percent efficient
2. Duct
3. 316 stainless steel probe
4. 3/8-inch, heated (250°F) Teflon
5. Four-pass conditioner-dryer, 316 stainless steel internals
6. 3/8-inch, unheated Teflon
7. Teflon-lined sample pump
8. 3/8-inch unheated Teflon
9. Rotameter
10. 1/4-inch Teflon tubing
11. Calibration gas manifold
12. Calibration gas selector valve
13. Calibration gas cylinders
14. Backpressure regulator
15. Auxiliary analysis port

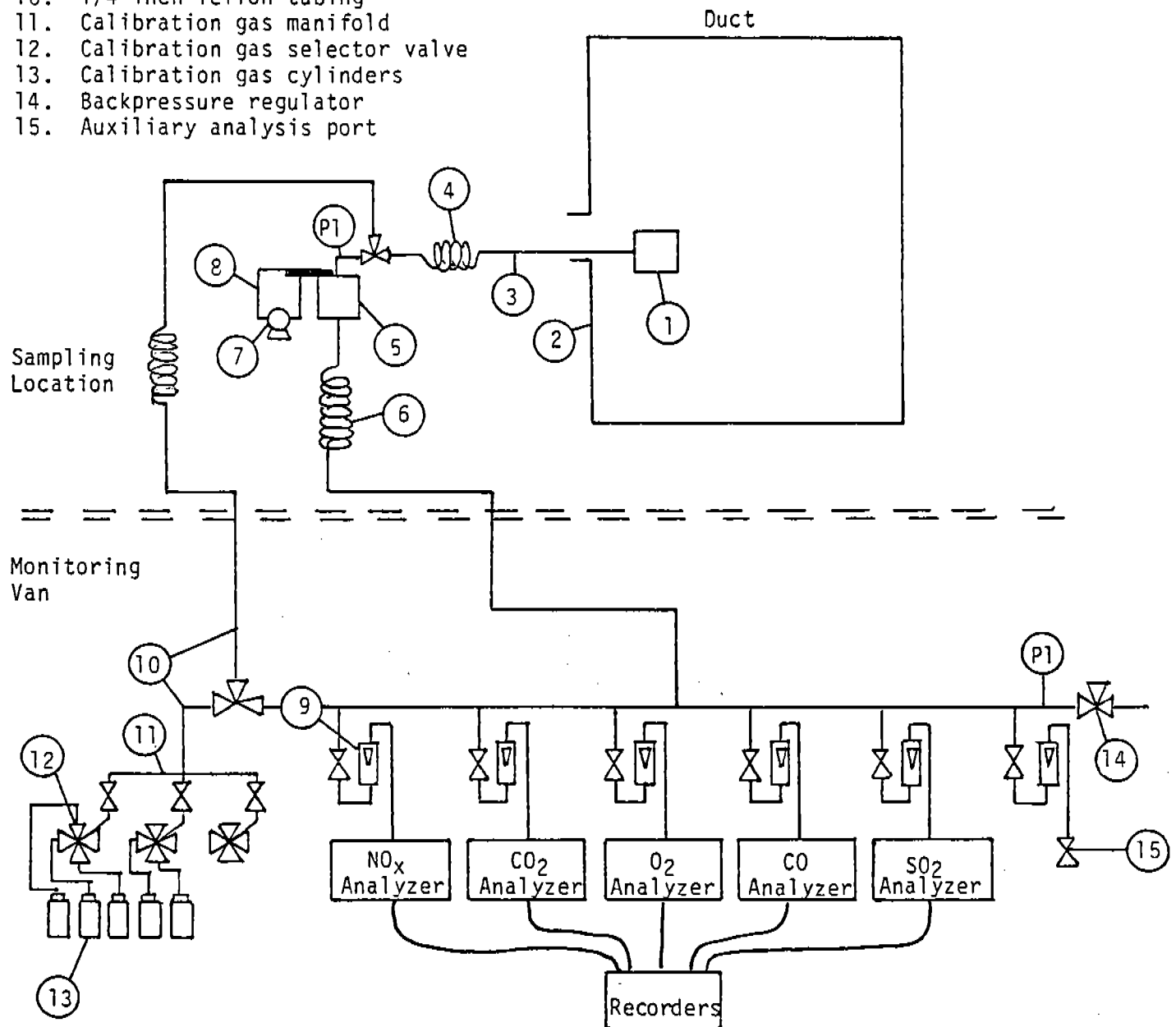


Figure 4-1. Schematic of Continuous Monitoring System.

Calibrations of the continuous analyzers were performed using EPA Protocol 1 calibration gases ( $\pm 1$  percent) for criteria pollutant analysis ( $\text{NO}_x/\text{SO}_2$ ) and certified calibration gases ( $\pm 1$  percent) for fixed gas analysis. Copies of the gas certifications are included in the Appendix of this report. All pertinent data (date, time, test locations, analyzer range, cal gas value) were recorded on both the field data sheets and continuous analyzer strip charts in the field.

At the start of the test, a leak-check was performed. The sample probe was removed from the stack and the end was sealed with a Swagelok cap. A leak-check is successful only if pressure at the analyzer system and flow through the rotameters to the individual analyzers all drop to zero. A mandatory leak-check was performed at the completion of each test.

An initial calibration was performed at the start of the test period by introducing zero and span gases for each analyzer and making the necessary adjustments. Calibration gas values were recorded on the continuous monitor strip charts and field data sheets. A calibration check was completed at the end of the test and adjustments (if necessary) to the analyzers were made in preparation for another test.

Test data was collected by continuously recording data onto strip charts for each test.

#### 4.6 SAMPLING PROCEDURES FOR HYDROCARBONS

The sampling train for hydrocarbons consisted of a probe (short piece of stainless steel), a Teflon sample line, a 500 ml glass sampling bomb; and a squeeze bulb. The entire train was purged with stack gas several

times before collecting a sample. After sample collection, the glass bomb was taken to the mobile lab for immediate analysis. One grab sample was collected during each test on the Kiln.

## SECTION 5

### ANALYSIS PROCEDURES

This section of the report describes the procedures used to analyze the samples collected during the test program. All analyses were performed in the Pape & Steiner climate-controlled laboratory in Bakersfield.

#### 5.1 ANALYSIS OF PARTICULATE SAMPLES

##### 5.1.1 Nozzle, Probe, Filter Holder Wash

The volume of the acetone washings were measured and the washings were transferred to clean, tared, aluminum weighing dishes. The dishes were placed on a hot plate in a fume hood and gently heated to dryness. The dishes with the dry residue were desiccated and weighed repeatedly at 6-hour intervals until a constant weight was achieved (to the nearest 0.01 mg with a tolerance of <0.1 mg between weighings). The ACS reagent grade acetone blank was treated in the same manner.

##### 5.1.2 Filter

The 100 mm filter was removed from its petri dish and transferred to an oven where it was heated for 2 hours at 105°C. The filter was then desiccated and weighed repeatedly at 6-hour intervals until a constant weight was achieved (to nearest 0.01 mg with a tolerance of <0.1 mg between weighings). An unused, tared blank filter was treated in the same manner.



## 5.2 ANALYSIS OF HYDROCARBON SAMPLES

The grab sample of hydrocarbons was analyzed using Carle Model 211 AGC-FID. After purging the syringe three times, a 1-ml syringe sample was extracted from the syringe port on the glass bomb and injected onto a 6-foot long, 1/8-inch stainless steel column containing 80/100 mesh Porapak Q, maintained at 150°C. Any C<sub>1</sub> through C<sub>5</sub> hydrocarbons were speciated and the greater than C<sub>5</sub> hydrocarbons were backflushed to the detector for quantitation as a single peak. An HP Model 3390A reporting integrator was used to record and integrate the signal from the GC. A  $\pm 1$  percent certified calibration gas (C<sub>1</sub>-C<sub>6</sub> HC in N<sub>2</sub>) was used to calibrate the GC and to quantitate the C<sub>1</sub> through C<sub>5</sub> and greater than C<sub>5</sub> hydrocarbons.

## SECTION 6

### QUALITY ASSURANCE

#### 6.1 PARTICULATE SAMPLING EQUIPMENT

A detailed record of repair and maintenance to each sampling train is kept. Preventative maintenance to each system is performed periodically to avoid complete component breakdown during a field test.

A detailed record of sampling system calibrations is also kept. Calibration data for the sampling nozzles, pitot tubes, dry gas meters and orifice meters are available for review. Results of the EPA Quality Assurance Branch biannual audits of the dry gas meter and orifice meter combinations are also logged and verify our in-house calibration data. The calibration data for the equipment used on this program can be found in the Appendix.

#### 6.2 LAB ANALYSIS

All field samples are assigned a label and an ID number. This ID is also affixed to a chain-of-custody log and to the field data sheet to eliminate any chance of sample mixup.

Prior to analysis, all glassware is thoroughly cleaned (soap and water, tap water rinse, distilled water rinse, IPA rinse) to eliminate any contamination. The evaporating dishes used to evaporate the washings are

treated the same as a sample (dried in an oven, desiccated and weighed repeatedly at 6-hour intervals until a constant weight is achieved). The glassware used to measure volumes and make transfers and dilutions are all NBS Class A to insure accurate measurements. All weighings are carried out on a Mettler Model H54AR analytical balance supported by a marble table in a separate room from the main analytical laboratory. The balance is calibrated regularly against an NBS Class S-1 weight.

All reagents used in the field and in the laboratory are ACS reagent grade and blanks of these reagents are evaluated for every set of tests. Blanks are taken in the field from the squeeze bottles and not the original container. Records are kept on these blanks to insure consistent quality of the reagents.

### 6.3 CONTINUOUS MONITORS

Prior to the test program, an internal and external calibration of the sampling system was performed using the calibration gases. There was excellent agreement between the internal and external calibrations (indicating no sample loss in the system) over the test period. The calibration gas certificates for the gases used on this test program appear in the Appendix.

## APPENDIX

- Sampling Point Locations
- Velocity Traverse Data Sheets
- Particulate Data Sheets
- Continuous Monitor Data Sheets
- Continuous Monitor Strip Charts
- GC Strip Chart
- Sample Handling Log
- Analytical Reports
- Isokinetic Calculations
- Emission Rate Calculations
- Equipment Calibration Data
- Calibration Gas Certificates

SAMPLING POINT LOCATION DATA SHEET

Plant Southwestern Portland

Date 2/4/85

Test Location #2 Kiln Outlet

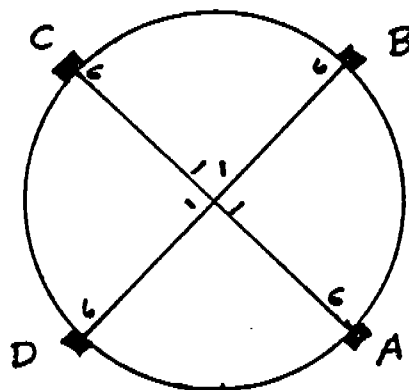
Upstream Dist./Dia. 92" / 0.6  $\phi$

Downstream Dist./Dia. 416" / 2.6  $\phi$

No. of Sampling Points 24

Stack Dimension 160"

Coupling Length 5.5"



| Sample Point | Dist | Sample Point | Dist | Sample Point | Dist | Sample Point | Dist |
|--------------|------|--------------|------|--------------|------|--------------|------|
| 1            | 8.9  |              |      |              |      |              |      |
| 2            | 16.2 |              |      |              |      |              |      |
| 3            | 24.4 |              |      |              |      |              |      |
| 4            | 33.9 |              |      |              |      |              |      |
| 5            | 45.5 |              |      |              |      |              |      |
| 6            | 62.4 |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |

SAMPLING POINT RELOCATION:

SAMPLING POINT LOCATION DATA SHEET

Plant Southwestern Portland

Date 2/4/85

Test Location Clinker Outlet

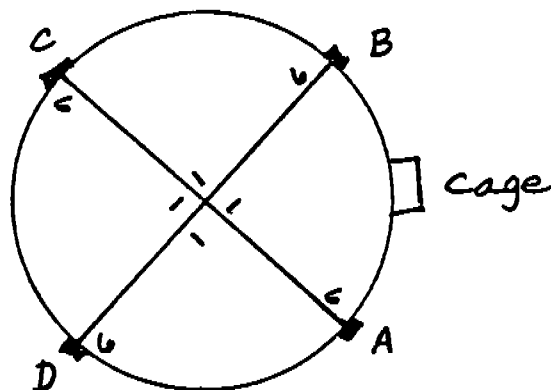
Upstream Dist./Dia. 76" / 0.6  $\phi$

Downstream Dist./Dia. 300" / 2.3  $\phi$

No. of Sampling Points 24

Stack Dimension 130"

Coupling Length 4.5"



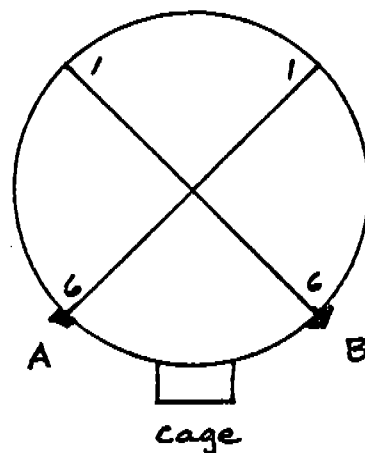
| Sample Point | Dist | Sample Point | Dist | Sample Point | Dist | Sample Point | Dist |
|--------------|------|--------------|------|--------------|------|--------------|------|
| 1            | 7.3  |              |      |              |      |              |      |
| 2            | 13.2 |              |      |              |      |              |      |
| 3            | 19.9 |              |      |              |      |              |      |
| 4            | 27.5 |              |      |              |      |              |      |
| 5            | 37.0 |              |      |              |      |              |      |
| 6            | 50.7 |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |

SAMPLING POINT RELOCATION:



## SAMPLING POINT LOCATION DATA SHEET

Plant Southwestern Portland  
Date 2/4/85  
Test Location #2 Raw Mill Outlet  
Upstream Dist./Dia. 168" / 2.3  $\phi$   
Downstream Dist./Dia. 706" / 9.8  $\phi$   
No. of Sampling Points 12  
Stack Dimension 72"  
Coupling Length 13.25"



| Sample Point | Dist | Sample Point | Dist | Sample Point | Dist | Sample Point | Dist |
|--------------|------|--------------|------|--------------|------|--------------|------|
| 1            | 16.4 |              |      |              |      |              |      |
| 2            | 23.8 |              |      |              |      |              |      |
| 3            | 34.6 |              |      |              |      |              |      |
| 4            | 63.9 |              |      |              |      |              |      |
| 5            | 74.7 |              |      |              |      |              |      |
| 6            | 82.1 |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |
|              |      |              |      |              |      |              |      |

SAMPLING POINT RELOCATION: none

VELOCITY TRAVERSE DATA SHEET

Plant SWPC  
 Date 2/6/85  
 Test Location Kiln  
 Static Pressure (in. wg) \_\_\_\_\_  
 Barometric Pressure 26.46  
 Probe Type/Length glass / 6'  
 Pitot Coefficient 0.84  
 Stack Dimension 160

| Smp1 Pt. | $\Delta P$ | Ts  | Smp1 Pt. | $\Delta P$ | Ts  | Smp1 Pt. | $\Delta P$ | Ts | Smp1 Pt. | $\Delta P$ | Ts |
|----------|------------|-----|----------|------------|-----|----------|------------|----|----------|------------|----|
| 7:12 B 1 | 0.29       | 376 | 9:31 D 1 | 0.18       | 372 |          |            |    |          |            |    |
| 2        | 0.35       | 376 | 2        | 0.17       | 374 |          |            |    |          |            |    |
| 3        | 0.41       | 376 | 3        | 0.15       | 374 |          |            |    |          |            |    |
| 4        | 0.43       | 376 | 4        | 0.18       | 374 |          |            |    |          |            |    |
| 5        | 0.47       | 376 | 5        | 0.18       | 372 |          |            |    |          |            |    |
| 6        | 0.39       | 376 | 6        | 0.17       | 372 |          |            |    |          |            |    |
| 9:18 A 1 | 0.24       | 376 | 9:39 D 1 | 0.16       | 369 |          |            |    |          |            |    |
| 2        | 0.30       | 373 | 2        | 0.14       | 370 |          |            |    |          |            |    |
| 3        | 0.35       | 375 | 3        | 0.14       | 369 |          |            |    |          |            |    |
| 4        | 0.40       | 376 | 4        | 0.13       | 369 |          |            |    |          |            |    |
| 5        | 0.43       | 375 | 5        | 0.11       | 368 |          |            |    |          |            |    |
| 6        | 0.38       | 375 | 6        | 0.10       | 368 |          |            |    |          |            |    |

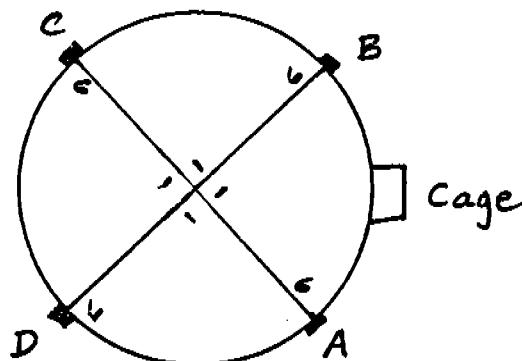
SAMPLING POINT RELOCATION:

Avg  $\sqrt{\Delta P} = 0.4963$   
 Avg  $\Delta P = 0.2463$   
 Avg Ts  $\sim 373$



VELOCITY TRAVERSE DATA SHEET

Plant SUPC  
 Date 2-6-85  
 Test Location CLIMBER  
 Static Pressure (in. wg) -0.48  
 Barometric Pressure 30.45  
 Probe Type/Length Glass 6'  
 Pitot Coefficient 0.840  
 Stack Dimension 130"



| Smpl Pt. | ΔP  | Ts  | Smpl Pt. | ΔP  | Ts  | Smpl Pt. | ΔP  | Ts  | Smpl Pt. | ΔP  | Ts  |
|----------|-----|-----|----------|-----|-----|----------|-----|-----|----------|-----|-----|
|          |     |     | 0931     |     |     | 0950     |     |     | 0956     |     |     |
| 1        | .41 | 350 | A        | .53 | 358 | B        | .52 | 351 | C        | .23 | 335 |
| 2        | .42 | 350 | 2        | .65 | 361 | 2        | .55 | 358 | 2        | .36 | 340 |
| 3        | .37 | 356 | 3        | .75 | 365 | 3        | .64 | 362 | 3        | .35 | 346 |
| 4        | .35 | 358 | 4        | .78 | 367 | 4        | .68 | 365 | 4        | .32 | 349 |
| 5        | .30 | 360 | 5        | .78 | 368 | 5        | .68 | 365 | 5        | .28 | 353 |
| 6        | .21 | 356 | 6        | .55 | 348 | 6        | .56 | 358 | 6        | .22 | 350 |
|          |     |     |          |     |     |          |     |     |          |     |     |
|          |     |     |          |     |     |          |     |     |          |     |     |
|          |     |     |          |     |     |          |     |     |          |     |     |
|          |     |     |          |     |     |          |     |     |          |     |     |
|          |     |     |          |     |     |          |     |     |          |     |     |
|          |     |     |          |     |     |          |     |     |          |     |     |
|          |     |     |          |     |     |          |     |     |          |     |     |

SAMPLING POINT RELOCATION:

VELOCITY TRAVERSE DATA SHEET

Plant SWPC  
 Date 2/5/85  
 Test Location #12 Finish Mill  
 Static Pressure (in. wg) -0.11  
 Barometric Pressure 26.35  
 Probe Type/Length glass/6'  
 Pitot Coefficient 0.84  
 Stack Dimension 60

12:29

12:39

| Smp1 Pt. | $\Delta P$ | Ts  | Smp1 Pt. | $\Delta P$ | Ts  | Smp1 Pt. | $\Delta P$ | Ts | Smp1 Pt. | $\Delta P$ | Ts |
|----------|------------|-----|----------|------------|-----|----------|------------|----|----------|------------|----|
| A1       | 0.11       | 186 | B1       | 0.11       | 187 |          |            |    |          |            |    |
| 2        | 0.12       | 187 | 2        | 0.11       | 187 |          |            |    |          |            |    |
| 3        | 0.12       | 187 | 3        | 0.11       | 188 |          |            |    |          |            |    |
| 4        | 0.12       | 188 | 4        | 0.11       | 189 |          |            |    |          |            |    |
| 5        | 0.12       | 189 | 5        | 0.13       | 190 |          |            |    |          |            |    |
| 6        | 0.11       | 189 | 6        | 0.12       | 191 |          |            |    |          |            |    |
| 7        | 0.10       | 189 | 7        | 0.11       | 191 |          |            |    |          |            |    |
| 8        | 0.07       | 189 | 8        | 0.09       | 189 |          |            |    |          |            |    |
|          |            |     |          |            |     |          |            |    |          |            |    |
|          |            |     |          |            |     |          |            |    |          |            |    |
|          |            |     |          |            |     |          |            |    |          |            |    |
|          |            |     |          |            |     |          |            |    |          |            |    |

SAMPLING POINT RELOCATION:

Avg  $\sqrt{\Delta P} = 0.3309$   
 Avg Ts  $\approx 189$

# VELOCITY TRAVERSE DATA SHEET

Plant SUPC  
 Date 2-5-85  
 Test Location RAW Mill  
 Static Pressure (in. wg) -0.47  
 Barometric Pressure 26.45  
 Probe Type/Length CPA 8'  
 Pitot Coefficient .840  
 Stack Dimension 22"

SW  
10:30

| Smp1 Pt. | ΔP  | Ts  | Smp1 Pt.    | ΔP  | Ts  | Smp1 Pt. | ΔP | Ts | Smp1 Pt. | ΔP | Ts |
|----------|-----|-----|-------------|-----|-----|----------|----|----|----------|----|----|
| 1        | .52 | 153 | NW<br>10:45 | .58 | 156 |          |    |    |          |    |    |
| 2        | .57 | 154 |             | .58 | 157 |          |    |    |          |    |    |
| 3        | .55 | 155 |             | .55 | 157 |          |    |    |          |    |    |
| 4        | .50 | 156 |             | .52 | 158 |          |    |    |          |    |    |
| 5        | .49 | 155 |             | .49 | 157 |          |    |    |          |    |    |
| 6        | .41 | 153 |             | .37 | 156 |          |    |    |          |    |    |
|          |     |     |             |     |     |          |    |    |          |    |    |
|          |     |     |             |     |     |          |    |    |          |    |    |
|          |     |     |             |     |     |          |    |    |          |    |    |
|          |     |     |             |     |     |          |    |    |          |    |    |
|          |     |     |             |     |     |          |    |    |          |    |    |
|          |     |     |             |     |     |          |    |    |          |    |    |

SAMPLING POINT RELOCATION:

Date 2/6/85 Barometric Pressure 30.46  
 Test Location RAW 2 Static in. wg. -0.33  
 Run Number #1 Probe Type/Length g/155.6'  
 Stack Diameter 160 Pitot Coefficient 0.84  
 Operator JB Meter Box No. 18635/11.0098  
 Filter No. 10-270 Nozzle No./Size 1548/3207

| Impinger Volumes/Weights |       |         |      | Gas Composition |                 |                |     |
|--------------------------|-------|---------|------|-----------------|-----------------|----------------|-----|
| Contents                 | Final | Initial | Net  | Time            | CO <sub>2</sub> | O <sub>2</sub> | CO  |
| Wet DE                   | 616.0 | 579.9   | 46.1 |                 | 18.70           | 9.13           |     |
| Wet DE                   | 545.5 | 539.6   | 15.9 |                 |                 |                |     |
| Dry                      | 470.9 | 468.9   | 2.0  |                 |                 |                |     |
|                          |       |         |      | Leak Rate       | cfm             |                | "Hg |
| S.G.                     | 628.3 | 614.8   | 13.5 | Initial         |                 | 0.019          | 15  |
|                          |       | Total   | 77.5 | Final           |                 |                |     |

| Sample Point | Time  | ΔP in wg | ΔH in wg | Gas Meter Volume Ft <sup>3</sup> | Temperature °F |       |      |      | Pump Vacuum in. Hg | √ΔP   | Comments |
|--------------|-------|----------|----------|----------------------------------|----------------|-------|------|------|--------------------|-------|----------|
|              |       |          |          |                                  | Stack          | Probe | Oven | Imp. |                    |       |          |
| 1            | 10:20 | 0.15     | 0.98     | 402.785                          | 370            | 275   | 254  | 55   | 2.5                | 0.387 | pitotok  |
| 2            | 5     | 0.15     | 0.98     | 405.565                          | 379            | 255   | 258  | 49   | 2.0                | 0.387 |          |
| 3            | 10    | 0.13     | 0.87     | 408.310                          | 376            | 254   | 258  | 47   | 2.0                | 0.361 |          |
| 4            | 15    | 0.12     | 0.80     | 410.940                          | 376            | 269   | 255  | 46   | 2.0                | 0.346 |          |
| 5            | 20    | 0.10     | 0.67     | 413.460                          | 375            | 272   | 256  | 44   | 1.5                | 0.316 |          |
| 6            | 25    | 0.08     | 0.53     | 415.810                          | 375            | 275   | 252  | 43   | 1.0                | 0.283 |          |
|              | 30    |          |          | 417.943                          |                |       |      |      |                    |       |          |
| 1            | 10:55 | 0.145    | 0.96     | 417.943                          | 374            | 269   | 253  | 37   | 2.0                | 0.381 |          |
| 2            | 5     | 0.15     | 1.00     | 420.647                          | 380            | 236   | 255  | 35   | 2.5                | 0.387 |          |
| 3            | 10    | 0.17     | 1.14     | 423.490                          | 382            | 225   | 255  | 35   | 2.5                | 0.412 |          |
| 4            | 15    | 0.19     | 1.27     | 426.470                          | 384            | 227   | 253  | 34   | 3.0                | 0.436 |          |
| 5            | 20    | 0.18     | 1.21     | 429.665                          | 380            | 241   | 254  | 35   | 3.0                | 0.424 |          |
| 6            | 25    | 0.15     | 1.01     | 432.797                          | 380            | 251   | 255  | 37   | 2.0                | 0.387 |          |
|              | 30    |          |          | 435.710                          |                |       |      |      |                    |       |          |

Date 2/6/85 Barometric Pressure 30.46  
 Test Location Kilm Static in. wg. -0.33  
 Run Number 1 Probe Type/Length glass/6'  
 Stack Diameter 160 Pitot Coefficient 0.84  
 Operator JS Meter Box No. 18635/1.0000  
 Filter No. 10-270 Nozzle No./Size 1548/3307

| Impinger Volumes/Weights |       |         |     | Gas Composition |                 |                |     |
|--------------------------|-------|---------|-----|-----------------|-----------------|----------------|-----|
| Contents                 | Final | Initial | Net | Time            | CO <sub>2</sub> | O <sub>2</sub> | CO  |
|                          |       |         |     |                 |                 |                |     |
|                          |       |         |     |                 |                 |                |     |
|                          |       |         |     |                 |                 |                |     |
|                          |       |         |     |                 |                 |                |     |
| S.G.                     |       |         |     | Leak Rate       |                 | c fm           | "Hg |
|                          |       |         |     | Initial         |                 |                |     |
|                          |       |         |     | Final           |                 |                |     |
|                          | Total |         |     |                 |                 | 0.009          | 9.0 |

| Sample Point | Time  | $\Delta P$<br>in wg | $\Delta H$<br>in wg | Gas<br>Meter<br>Volume Ft <sup>3</sup> | Temperature °F |       |      |      |           |       | Pump<br>Vacuum<br>in. Hg | $\sqrt{\Delta P}$ | Comments        |
|--------------|-------|---------------------|---------------------|----------------------------------------|----------------|-------|------|------|-----------|-------|--------------------------|-------------------|-----------------|
|              |       |                     |                     |                                        | Stack          | Probe | Oven | Imp. | Gas Meter |       |                          |                   |                 |
|              |       |                     |                     |                                        |                |       |      |      | In        | Out   |                          |                   |                 |
| 1            | 11:32 | 0.295               | 1.96                | 435.710                                | 380            | 275   | 245  | 38   | 69        | 68    | 4.5                      | 0.543             |                 |
| 2            | 5     | 0.36                | 2.41                | 439.555                                | 383            | 275   | 244  | 38   | 81        | 68    | 5.5                      | 0.600             |                 |
| 3            | 10    | 0.405               | 2.72                | 443.795                                | 383            | 275   | 248  | 38   | 84        | 69    | 6.0                      | 0.636             |                 |
| 4            | 15    | 0.46                | 3.08                | 448.300                                | 386            | 275   | 248  | 37   | 84        | 70    | 7.0                      | 0.678             |                 |
| 5            | 20    | 0.51                | 3.43                | 453.060                                | 385            | 275   | 251  | 38   | 86        | 70    | 8.0                      | 0.714             |                 |
| 6            | 25    | 0.41                | 2.77                | 458.100                                | 385            | 275   | 253  | 39   | 87        | 72    | 6.5                      | 0.640             |                 |
|              | 30    |                     |                     | 462.941                                |                |       |      |      |           |       |                          |                   |                 |
| 1            | 12:10 | 0.28                | 1.90                | 467.941                                | 380            | 275   | 247  | 49   | 80        | 76    | 4.0                      | 0.529             |                 |
| 2            | 5     | 0.305               | 2.07                | 466.800                                | 385            | 265   | 249  | 42   | 89        | 75    | 4.5                      | 0.552             |                 |
| 3            | 10    | 0.365               | 2.48                | 470.725                                | 386            | 262   | 248  | 40   | 92        | 76    | 5.5                      | 0.604             | Accel<br>855876 |
| 4            | 15    | 0.42                | 2.85                | 475.075                                | 388            | 264   | 248  | 41   | 94        | 77    | 6.5                      | 0.648             |                 |
| 5            | 20    | 0.37                | 2.51                | 479.715                                | 388            | 266   | 249  | 40   | 92        | 78    | 5.5                      | 0.608             | FL71<br>855877  |
| 6            | 25    | 0.315               | 2.14                | 484.185                                | 388            | 267   | 249  | 40   | 92        | 78    | 5.0                      | 0.561             |                 |
|              | 30    |                     |                     | 488.412                                |                |       |      |      |           |       |                          |                   | pitot           |
|              |       |                     | 1.74                | 85.657                                 | 381.08         |       |      |      |           | 74.04 |                          | 0.422             |                 |

| Impinger Volumes/Weights |       |         | Gas Composition |           |                 |                |    |
|--------------------------|-------|---------|-----------------|-----------|-----------------|----------------|----|
| Contents                 | Final | Initial | Net             | Time      | CO <sub>2</sub> | O <sub>2</sub> | CO |
| OF                       | 565.4 | 524.1   | 41.3            |           | 18.69           | 9.30           |    |
| OF                       | 576.4 | 510.9   | 15.5            |           |                 |                |    |
| DSX                      | 439.2 | 437.6   | 1.6             |           |                 |                |    |
|                          |       |         |                 | Leak Rate | cfm             | "Hg            |    |
|                          |       |         |                 | Initial   |                 |                |    |
| S.G.                     | 642.0 | 326.5   | 15.5            | Final     |                 | 0.09           | 15 |
|                          |       | Total   | 73.9            |           |                 |                |    |

[illegible]

Nozzle No./Size 154B/3207

| Sample Point | Time      | $\Delta P$ in wg | $\Delta H$ in wg | Gas Meter Volume Ft <sup>3</sup> | Temperature °F |       |      |      |           |       | Pump Vacuum in. Hg | $\sqrt{\Delta P}$ | Comments       |
|--------------|-----------|------------------|------------------|----------------------------------|----------------|-------|------|------|-----------|-------|--------------------|-------------------|----------------|
|              |           |                  |                  |                                  | Stack          | Probe | Oven | Imp. | Gas Meter |       |                    |                   |                |
|              |           |                  |                  |                                  |                |       |      |      | In        | Out   |                    |                   |                |
| D 1          | 4:03<br>0 | 0.15             | 1.03             | 538.554                          | 365            | 264   | 275  | 40   | 71        | 69    | 2.5                | 0.387             |                |
| 2            | 5         | 0.14             | 0.96             | 541.330                          | 362            | 245   | 262  | 42   | 80        | 70    | 2.5                | 0.374             |                |
| 3            | 10        | 0.13             | 0.90             | 544.138                          | 359            | 237   | 260  | 40   | 84        | 69    | 2.5                | 0.361             |                |
| 4            | 15        | 0.15             | 1.04             | 546.845                          | 359            | 244   | 268  | 37   | 85        | 69    | 2.5                | 0.387             |                |
| 5            | 20        | 0.16             | 1.11             | 549.715                          | 359            | 248   | 257  | 37   | 87        | 69    | 3.0                | 0.400             |                |
| 6            | 25        | 0.145            | 1.01             | 552.725                          | 359            | 247   | 253  | 37   | 88        | 69    | 2.5                | 0.361             |                |
|              | 30        |                  |                  | 556.640                          |                |       |      |      |           |       |                    |                   |                |
| C 1          | 4:36<br>0 | 0.14             | 0.96             | 555.640                          | 357            | 275   | 237  | 40   | 72        | 69    | 2.5                | 0.374             |                |
| 2            | 5         | 0.12             | 0.83             | 558.420                          | 359            | 275   | 252  | 40   | 85        | 71    | 2.0                | 0.346             | Acc. 85 5880   |
| 3            | 10        | 0.13             | 0.91             | 561.080                          | 357            | 274   | 253  | 36   | 86        | 71    | 2.5                | 0.361             |                |
| 4            | 15        | 0.11             | 0.77             | 563.800                          | 357            | 265   | 265  | 39   | 87        | 71    | 2.0                | 0.332             | F. 172 85 5881 |
| 5            | 20        | 0.10             | 0.70             | 566.360                          | 355            | 258   | 252  | 41   | 87        | 71    | 2.0                | 0.316             |                |
| 6            | 25        | 0.085            | 0.59             | 568.930                          | 355            | 249   | 253  | 40   | 87        | 71    | 1.5                | 0.292             | pilot ok       |
|              | 30        |                  |                  | 571.050                          |                |       |      |      |           |       |                    |                   |                |
|              |           |                  | 1.57             | 61.805                           | 362.75         |       |      |      |           | 74.67 |                    | 0.4647            |                |

Date 2/7/85  
 Test Location Kila  
 Run Number 3  
 Stack Diameter 160  
 Operator JB  
 Filter No. 271  
 Barometric Pressure 26.52  
 Static in. wg. -0.33  
 Probe Type/Length glass/6'  
 Pitot Coefficient 0.84  
 Meter Box No./Size 635/1.0098  
 Nozzle No./Size 648/3A07

| Impinger Volumes/Weights |       |         |      |  | Gas Composition |                 |                |    |
|--------------------------|-------|---------|------|--|-----------------|-----------------|----------------|----|
| Contents                 | Final | Initial | Net  |  | Time            | CO <sub>2</sub> | O <sub>2</sub> | CO |
| DI                       | 665.5 | 616.1   | 49.4 |  |                 |                 |                |    |
| DI                       | 596.6 | 583.3   | 13.3 |  |                 |                 |                |    |
| dry                      | 434.6 | 433.7   | 0.9  |  |                 |                 |                |    |
|                          |       |         |      |  | Leak Rate       | cfm             | "Hg            |    |
| S.G.                     | 626.6 | 611.5   | 15.1 |  | Initial         | 0.019           |                | 15 |
|                          |       | Total   | 28.7 |  | Final           |                 |                |    |

| Sample Point | Time | $\Delta P$ in wg | $\Delta H$ in wg | Gas Meter Volume Ft <sup>3</sup> | Temperature °F |       |      |      | Pump Vacuum in. Hg | $\sqrt{\Delta P}$ | Comments |
|--------------|------|------------------|------------------|----------------------------------|----------------|-------|------|------|--------------------|-------------------|----------|
|              |      |                  |                  |                                  | Stack          | Probe | Oven | Imp. |                    |                   |          |
| C 1          | 8:31 | 0.14             | 0.92             | 581.177                          | 375            | 225   | 225  | 50   | 61                 | 0.374             | pitotok  |
| 2            | 5    | 0.14             | 0.93             | 583.910                          | 381            | 244   | 234  | 44   | 73                 | 0.374             |          |
| 3            | 10   | 0.14             | 0.94             | 586.610                          | 378            | 268   | 249  | 44   | 77                 | 0.374             |          |
| 4            | 15   | 0.13             | 0.87             | 589.335                          | 379            | 270   | 252  | 44   | 79                 | 0.361             |          |
| 5            | 20   | 0.095            | 0.64             | 591.975                          | 376            | 268   | 252  | 44   | 81                 | 0.308             |          |
| 6            | 25   | 0.09             | 0.61             | 594.330                          | 376            | 262   | 252  | 44   | 80                 | 0.300             |          |
|              | 30   |                  |                  | 596.591                          |                |       |      |      |                    |                   |          |
| D 1          | 4:00 | 0.17             | 1.13             | 596.591                          | 376            | 273   | 255  | 42   | 67                 | 0.412             |          |
| 2            | 5    | 0.16             | 1.07             | 599.615                          | 380            | 251   | 256  | 37   | 80                 | 0.400             |          |
| 3            | 10   | 0.17             | 1.14             | 602.700                          | 381            | 245   | 255  | 35   | 82                 | 0.412             |          |
| 4            | 15   | 0.175            | 1.18             | 605.475                          | 381            | 240   | 255  | 36   | 84                 | 0.418             |          |
| 5            | 20   | 0.185            | 1.25             | 608.520                          | 380            | 245   | 254  | 35   | 85                 | 0.430             |          |
| 6            | 25   | 0.17             | 1.15             | 611.690                          | 380            | 250   | 255  | 35   | 86                 | 0.412             |          |
|              | 30   |                  |                  | 614.965                          |                |       |      |      |                    |                   |          |



Barometric Pressure 26.52  
 Static in. wg. -0.33  
 Probe Type/Length glass/6'  
 Pitot Coefficient 0.84  
 Meter Box No./8 635/10098  
 Nozzle No./Size 1548/1.3207

| Sample Point | Time  | $\Delta P$<br>in wg | $\Delta H$<br>in wg | Gas<br>Meter<br>Volume Ft <sup>3</sup> | Temperature °F |       |      |      |           |     | Pump<br>Vacuum<br>in. Hg | $\sqrt{\Delta P}$ | Comments                      |
|--------------|-------|---------------------|---------------------|----------------------------------------|----------------|-------|------|------|-----------|-----|--------------------------|-------------------|-------------------------------|
|              |       |                     |                     |                                        | Stack          | Probe | Oven | Imp. | Gas Meter |     |                          |                   |                               |
|              |       |                     |                     |                                        |                |       |      |      | In        | Out |                          |                   |                               |
| B 1          | 9:40  | 0.28                | 1.86                |                                        | 379            | 238   | 245  | 39   | 69        | 67  | 4.0                      | 0.529             |                               |
| 2            | 5     | 0.34                | 2.28                |                                        | 383            | 225   | 245  | 37   | 81        | 68  | 5.0                      | 0.583             |                               |
| 3            | 10    | 0.42                | 2.82                |                                        | 384            | 225   | 240  | 37   | 84        | 69  | 6.5                      | 0.648             |                               |
| 4            | 15    | 0.45                | 3.02                |                                        | 386            | 225   | 242  | 36   | 85        | 70  | 7.0                      | 0.671             |                               |
| 5            | 20    | 0.465               | 3.14                |                                        | 383            | 239   | 242  | 37   | 86        | 72  | 7.5                      | 0.682             |                               |
| 6            | 25    | 0.42                | 2.84                |                                        | 383            | 242   | 243  | 37   | 87        | 73  | 6.5                      | 0.648             |                               |
| .            | 30    |                     |                     | 641.774                                |                |       |      |      |           |     |                          |                   |                               |
| A 1          | 10:24 | 0.27                | 1.83                | 641.774                                | 380            | 275   | 245  | 40   | 80        | 75  | 4.0                      | 0.520             |                               |
| 2            | 5     | 0.29                | 1.96                | 645.540                                | 381            | 272   | 247  | 41   | 84        | 74  | 4.5                      | 0.539             |                               |
| 3            | 10    | 0.34                | 2.31                | 649.390                                | 381            | 265   | 247  | 40   | 87        | 74  | 5.0                      | 0.583             | FL73<br>855885 Ace3<br>855884 |
| 4            | 15    | 0.40                | 2.72                | 653.600                                | 383            | 257   | 245  | 41   | 90        | 74  | 6.0                      | 0.632             |                               |
| 5            | 20    | 0.41                | 2.79                | 658.030                                | 383            | 261   | 242  | 40   | 91        | 74  | 6.5                      | 0.640             |                               |
| 6            | 25    | 0.35                | 2.39                | 662.445                                | 380            | 264   | 247  | 38   | 90        | 74  | 5.5                      | 0.592             | pilot ok                      |
|              | 30    |                     |                     | 667.057                                |                |       |      |      |           |     |                          |                   |                               |
|              |       |                     | 1.74                | 85.880                                 | 380.29         |       |      |      | 74.88     |     |                          | 0.4935            |                               |

Date 2-6-85 Barometric Pressure 30.45  
 Test Location CLIMBER 2 Static in. wg. - .48  
 Run Number 1 Probe Type/Length 6000 6'  
 Stack Diameter 130" Pitot Coefficient .840  
 Operator CEO Meter Box No. 18609/1.98  
 Filter No. 295 Nozzle No./Size 408/2.180

| Impinger Volumes/Weights |       |         |      |      | Gas Composition |                |    |  |
|--------------------------|-------|---------|------|------|-----------------|----------------|----|--|
| Contents                 | Final | Initial | Net  | Time | CO <sub>2</sub> | O <sub>2</sub> | CO |  |
| Wet                      | 530.4 | 540.2   | -9.8 |      |                 |                |    |  |
| Dry                      | 537.9 | 534.6   | 3.3  |      |                 |                |    |  |
|                          | 448.5 | 447.3   | 1.2  |      |                 |                |    |  |
| Leak Rate                |       |         |      |      | cfm             |                |    |  |
| Initial                  |       |         |      |      | Initial         |                |    |  |
| Final                    |       |         |      |      | Final           |                |    |  |
| S.G.                     |       |         |      |      | Initial         |                |    |  |
| Total                    |       |         |      |      | Total           |                |    |  |

| Sample Point | Time | ΔP in wg | ΔH in wg | Gas Meter Volume Ft <sup>3</sup> | Temperature °F |       |      | Pump Vacuum in. Hg | √ΔP | Comments |
|--------------|------|----------|----------|----------------------------------|----------------|-------|------|--------------------|-----|----------|
|              |      |          |          |                                  | Stack          | Probe | Oven | Imp.               |     |          |
| A 1          | 0    | .56      | 2.07     | 190.807                          | 341            | 262   | 228  | 42                 | 5.0 | 0.248    |
| 2            | 3    | .66      | 2.42     | 193.30                           | 354            | 267   | 245  | 39                 | 7.0 | 0.812    |
| 3            | 6    | .70      | 2.63     | 195.98                           | 338            | 272   | 250  | 39                 | 7.5 | 0.837    |
| 4            | 9    | .73      | 2.74     | 198.87                           | 342            | 251   | 254  | 43                 | 8.0 | 0.854    |
| 5            | 12   | .64      | 2.39     | 201.82                           | 348            | 265   | 255  | 46                 | 7.0 | 0.800    |
| 6            | 15   | .56      | 2.16     | 204.44                           | 323            | 261   | 256  | 47                 | 6.0 | 0.748    |
|              | 18   |          |          | 206.940                          |                |       |      |                    |     |          |
| D 1          | 0    | .34      | 1.30     | 206.940                          | 328            | 235   | 258  | 49                 | 3.5 | 0.583    |
| 2            | 3    | .36      | 1.35     | 208.97                           | 343            | 237   | 256  | 50                 | 4.0 | 0.600    |
| 3            | 6    | .31      | 1.15     | 210.98                           | 355            | 245   | 256  | 57                 | 3.0 | 0.557    |
| 4            | 9    | .29      | 1.09     | 213.00                           | 350            | 252   | 256  | 49                 | 3.0 | 0.539    |
| 5            | 12   | .27      | 1.01     | 214.81                           | 352            | 258   | 257  | 51                 | 3.0 | 0.520    |
| 6            | 15   | .22      | 0.82     | 216.16                           | 359            | 260   | 256  | 52                 | 2.5 | 0.469    |
|              | 18   |          |          | 218.436                          |                |       |      |                    |     |          |

| Impinger Volumes/Weights |       |         |     | Gas Composition |                 |                |     |
|--------------------------|-------|---------|-----|-----------------|-----------------|----------------|-----|
| Contents                 | Final | Initial | Net | Time            | CO <sub>2</sub> | O <sub>2</sub> | CO  |
|                          |       |         |     |                 |                 |                |     |
|                          |       |         |     |                 |                 |                |     |
|                          |       |         |     |                 |                 |                |     |
|                          |       |         |     |                 |                 |                |     |
|                          |       |         |     | Leak Rate       |                 | cfm            | "Hg |
|                          |       |         |     | Initial         |                 |                |     |
| S.G.                     |       |         |     | Final           |                 |                |     |
| Total                    |       |         |     |                 |                 | cfm            | 10  |

| Sample Point | Time | $\Delta P$ in wg | $\Delta H$ in wg | Gas Meter Volume Ft <sup>3</sup> | Temperature °F |       |      |      |           |     | Pump Vacuum in. Hg | $\sqrt{\Delta P}$ | Comments        |                 |
|--------------|------|------------------|------------------|----------------------------------|----------------|-------|------|------|-----------|-----|--------------------|-------------------|-----------------|-----------------|
|              |      |                  |                  |                                  | Stack          | Probe | Oven | Imp. | Gas Meter |     |                    |                   |                 |                 |
|              |      |                  |                  |                                  |                |       |      |      | In        | Out |                    |                   |                 |                 |
| B 1          | 1150 | .40              | 1.47             | 218.436                          | 364            | 229   | 252  | 50   | 75        | 74  | 4.0                | 0.632             |                 |                 |
| 2            | 3    | .50              | 1.79             | 221.00                           | 390            | 234   | 251  | 45   | 81        | 71  | 5.0                | 0.707             |                 |                 |
| 3            | 6    | .55              | 1.94             | 222.80                           | 410            | 249   | 252  | 45   | 87        | 72  | 5.5                | 0.742             |                 |                 |
| 4            | 9    | .60              | 2.15             | 225.34                           | 395            | 253   | 250  | 44   | 87        | 72  | 6.0                | 0.775             |                 |                 |
| 5            | 12   | .60              | 2.11             | 227.91                           | 412            | 255   | 250  | 44   | 88        | 73  | 6.0                | 0.775             |                 |                 |
| 6            | 15   | .45              | 1.59             | 230.49                           | 409            | 254   | 249  | 43   | 89        | 73  | 5.0                | 0.671             |                 |                 |
|              | 18   |                  |                  | 232.861                          |                |       |      |      |           |     |                    |                   |                 |                 |
| C 1          | 1215 | .28              | 1.04             | 232.261                          | 363            | 228   | 253  | 48   | 78        | 75  | 3.0                | 0.529             |                 |                 |
| 2            | 3    | .24              | 0.89             | 234.70                           | 364            | 229   | 253  | 49   | 81        | 73  | 3.0                | 0.490             |                 |                 |
| 3            | 6    | .26              | 0.97             | 236.48                           | 360            | 246   | 256  | 53   | 86        | 73  | 3.0                | 0.510             |                 |                 |
| 4            | 9    | .26              | 1.01             | 238.28                           | 331            | 254   | 256  | 53   | 87        | 74  | 3.0                | 0.510             |                 |                 |
| 5            | 12   | .24              | 0.93             | 240.13                           | 334            | 253   | 255  | 51   | 87        | 77  | 3.0                | 0.49              | Acc!<br>85 5878 |                 |
| 6            | 15   | .17              | 0.66             | 242.00                           | 330            | 256   | 253  | 47   | 87        | 73  | 2.5                | 0.412             |                 |                 |
|              | 18   |                  |                  | 243.505                          |                |       |      |      |           |     |                    |                   |                 |                 |
|              |      |                  | 1.57             | 522.698                          | 358.13         |       |      |      | 74.40     |     |                    |                   | 0.6379          | Acc!<br>85 5879 |

| Impinger Volumes/Weights |       |         | Gas Composition |           |                 |                |     |
|--------------------------|-------|---------|-----------------|-----------|-----------------|----------------|-----|
| Contents                 | Final | Initial | Net             | Time      | CO <sub>2</sub> | O <sub>2</sub> | CO  |
| 1                        | 533.4 | 533.6   | -9.7            |           |                 |                |     |
| DI                       | 545.1 | 544.0   | 1.1             |           |                 |                |     |
| DI                       | 438.2 | 437.3   | 0.9             |           |                 |                |     |
| DI                       |       |         |                 |           |                 |                |     |
|                          |       |         |                 | Leak Rate |                 | cfm            | "Hg |
|                          |       |         |                 | Initial   |                 |                |     |
|                          |       |         |                 | Final     |                 |                |     |
| S.G.                     | 654.6 | 643.1   | 11.5            |           |                 | 0.17           | 15  |
|                          |       | Total   | 3.0             |           |                 |                |     |

[illegible]

Nozzle No./Size 1408/3680

| Sample Point | Time             | $\Delta P$ in wg | $\Delta H$ in wg | Gas Meter Volume Ft <sup>3</sup> | Temperature °F |       |      |      |           |     | Pump Vacuum in. Hg | $\sqrt{\Delta P}$ | Comments   |
|--------------|------------------|------------------|------------------|----------------------------------|----------------|-------|------|------|-----------|-----|--------------------|-------------------|------------|
|              |                  |                  |                  |                                  | Stack          | Probe | Oven | Imp. | Gas Meter |     |                    |                   |            |
|              |                  |                  |                  |                                  |                |       |      |      | In        | Out |                    |                   |            |
| B 1          | 15 <sup>40</sup> | .55              | 1.98             | 223.0-229                        | 382            | 242   | 233  | 53   | 25        | 74  | 7.0                | 0.242             |            |
| 2            | 3                | .62              | 2.23             | 225.0-54                         | 370            | 257   | 233  | 52   | 83        | 72  | 8.0                | 0.282             |            |
| 3            | 6                | .62              | 2.26             | 228.0-32                         | 383            | 268   | 239  | 51   | 86        | 73  | 8.0                | 0.282             |            |
| 4            | 9                | .70              | 2.59             | 280.94                           | 369            | 271   | 238  | 52   | 86        | 73  | 10.0               | 0.832             |            |
| 5            | 12               | .68              | 2.46             | 283.71                           | 389            | 248   | 234  | 50   | 86        | 73  | 10.0               | 0.825             |            |
| 6            | 15               | .60              | 2.16             | 286.61                           | 392            | 231   | 233  | 51   | 85        | 72  | 8.0                | 0.270             |            |
| 7            | 18               |                  |                  | 289.189                          | 369            | 228   | 237  | 52   | 86        | 72  |                    |                   |            |
| C 1          | 16 <sup>03</sup> | .36              | 1.35             | 289.189                          | 352            | 233   | 238  | 53   | 76        | 73  | 5.0                | 0.600             |            |
| 2            | 3                | .30              | 1.12             | 291.48                           | 359            | 233   | 230  | 50   | 82        | 73  | 4.0                | 0.548             |            |
| 3            | 6                | .30              | 1.10             | 293.30                           | 375            | 238   | 228  | 48   | 85        | 72  | 4.0                | 0.548             |            |
| 4            | 9                | .33              | 1.21             | 295.35                           | 378            | 240   | 230  | 46   | 86        | 73  | 4.5                | 0.574             |            |
| 5            | 12               | .30              | 1.12             | 297.21                           | 364            | 239   | 235  | 44   | 86        | 72  | 4.0                | 0.548             |            |
| 6            | 15               | .23              | 0.85             | 299.23                           | 370            | 236   | 233  | 43   | 86        | 72  | 3.0                | 0.480             |            |
| 7            | 18               |                  |                  | 300.945                          | 377.83         |       |      |      | 76.25     |     |                    | 0.6925            | Pilot - OK |

56.928

Nozzle No./Size 1438/2/80

[illegible]

| Impinger Volumes/Weights |       |         |     | Gas Composition |                 |                |    |
|--------------------------|-------|---------|-----|-----------------|-----------------|----------------|----|
| Contents                 | Final | Initial | Net | Time            | CO <sub>2</sub> | O <sub>2</sub> | CO |
|                          |       |         |     |                 |                 |                |    |
|                          |       |         |     |                 |                 |                |    |
|                          |       |         |     |                 |                 |                |    |
|                          |       |         |     | Leak Rate       |                 |                |    |
|                          |       |         |     | Initial         | cfm             |                |    |
| S.G.                     |       |         |     | Initial         | Initial         |                |    |
|                          |       |         |     | Final           | Final           |                |    |
|                          |       |         |     | Total           |                 |                |    |

Date 3-8-85 Barometric Pressure 26.43  
 Test Location CLINCHER #1 Static in. wg. -0.30  
 Run Number #3 Probe Type/Length Class 6'  
 Stack Diameter 130" Pitot Coefficient .840  
 Operator gco Meter Box No. 18 109/1.98  
 Filter No. 397 Nozzle No./Size 1428/1.2680

| Sample Point | Time  | $\Delta P$ in wg | $\Delta H$ in wg | Gas Meter Volume Ft <sup>3</sup> | Temperature °F |       |      |      |           | Pump Vacuum in. Hg | $\sqrt{\Delta P}$ | Comments |                         |
|--------------|-------|------------------|------------------|----------------------------------|----------------|-------|------|------|-----------|--------------------|-------------------|----------|-------------------------|
|              |       |                  |                  |                                  | Stack          | Probe | Oven | Imp. | Gas Meter |                    |                   |          |                         |
|              |       |                  |                  |                                  |                |       |      |      | In        |                    |                   |          | Out                     |
| B 1          | 10:15 | 0.46             | 1.64             | 339.509                          | 392            | 233   | 247  | 45   | 72        | 69                 | 4.0               | 0.678    |                         |
| 2            | 3     | 0.54             | 2.00             | 332.60                           | 366            | 237   | 243  | 37   | 81        | 68                 | 5.0               | 0.735    |                         |
| 3            | 6     | 0.54             | 1.98             | 334.95                           | 379            | 239   | 242  | 38   | 84        | 69                 | 5.0               | 0.735    |                         |
| 4            | 9     | 0.56             | 2.05             | 337.58                           | 380            | 250   | 242  | 40   | 85        | 70                 | 5.0               | 0.748    |                         |
| 5            | 12    | 0.58             | 2.10             | 340.10                           | 363            | 265   | 242  | 41   | 85        | 70                 | 5.0               | 0.748    |                         |
| 6            | 15    | 0.50             | 1.86             | 342.67                           | 368            | 270   | 251  | 42   | 86        | 70                 | 5.0               | 0.707    |                         |
|              | 18    |                  |                  | 345.172                          | 338            | 275   | 251  | 42   | 85        | 70                 |                   |          |                         |
| 1            | 10:34 | 0.26             | 0.94             | 345.172                          | 376            | 266   | 239  | 41   | 71        | 69                 | 3.0               | 0.510    |                         |
| 2            | 3     | 0.28             | 1.03             | 347.08                           | 367            | 246   | 235  | 37   | 75        | 68                 | 3.0               | 0.529    | BAce 855896 BFT 855897  |
| 3            | 6     | 0.30             | 1.09             | 348.97                           | 382            | 229   | 232  | 35   | 80        | 68                 | 3.0               | 0.548    |                         |
| 4            | 9     | 0.34             | 1.22             | 350.92                           | 393            | 226   | 235  | 34   | 81        | 67                 | 3.0               | 0.583    | Acc3 855892 FLT3 855893 |
| 5            | 12    | 0.32             | 1.18             | 353.02                           | 370            | 228   | 235  | 34   | 82        | 67                 | 3.0               | 0.566    |                         |
| 6            | 15    | 0.30             | 1.09             | 355.08                           | 382            | 227   | 237  | 35   | 82        | 67                 | 3.0               | 0.548    |                         |
|              | 18    |                  |                  | 356.857                          |                |       |      |      |           |                    |                   |          |                         |
|              |       |                  | 1.62             |                                  | 361.67         |       |      |      | 74.44     |                    |                   | 0.6481   |                         |

BACE  
 855896  
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 FLT3  
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55.268

| Impinger Volumes/Weights |       |         | Gas Composition |           |                 |                |     |
|--------------------------|-------|---------|-----------------|-----------|-----------------|----------------|-----|
| Contents                 | Final | Initial | Net             | Time      | CO <sub>2</sub> | O <sub>2</sub> | CO  |
| normal O <sub>2</sub>    | 639.3 | 540.5   | 88.8            |           |                 |                |     |
| normal O <sub>2</sub>    | 556.9 | 538.6   | 18.3            |           |                 |                |     |
| dry                      | 437.7 | 434.4   | 3.3             |           |                 |                |     |
|                          |       |         |                 | Leak Rate |                 | cfm            | "Hg |
|                          |       |         |                 | Initial   |                 | 2.0/5          | 15  |
| S.G.                     | 620.9 | 605.9   | 15.0            | Final     |                 |                |     |
|                          |       | Total   | 135.4           |           |                 |                |     |

[illegible]



| Impinger Volumes/Weights |       |         |     | Gas Composition |                 |                |     |
|--------------------------|-------|---------|-----|-----------------|-----------------|----------------|-----|
| Contents                 | Final | Initial | Net | Time            | CO <sub>2</sub> | O <sub>2</sub> | CO  |
|                          |       |         |     |                 |                 |                |     |
|                          |       |         |     |                 |                 |                |     |
|                          |       |         |     |                 |                 |                |     |
|                          |       |         |     |                 |                 |                |     |
| S.G.                     |       |         |     | Leak Rate       |                 | cfm            | "Hg |
|                          |       |         |     | Initial         |                 |                |     |
|                          |       |         |     | Final           |                 |                |     |
|                          | Total |         |     |                 |                 | 0.004          | 6.5 |

[illegible]

Date 2/7/85 Barometric Pressure 27.28  
 Test Location Finish Mill Static in. wg. -0.115  
 Run Number 2 Probe Type/Length 9/65 1/2'  
 Stack Diameter 60 Pitot Coefficient 0.84  
 Operator JF Meter Box No. 18 646/948  
 Filter No. 222 Nozzle No./Size 1265/3652

| Impinger Volumes/Weights |       |         |       | Gas Composition |                 |                |      |
|--------------------------|-------|---------|-------|-----------------|-----------------|----------------|------|
| Contents                 | Final | Initial | Net   | Time            | CO <sub>2</sub> | O <sub>2</sub> | CO   |
| <i>DI</i>                | 685.0 | 565.3   | 119.7 |                 |                 |                |      |
| <i>DI</i>                | 547.7 | 526.3   | 21.4  |                 |                 |                |      |
| <i>dry</i>               | 441.4 | 439.1   | 2.3   |                 |                 |                |      |
|                          |       |         |       | Leak Rate       |                 | cfm            | "Hg  |
|                          |       |         |       | Initial         |                 | 0.016          | 15.5 |
| S.G.                     | 639.7 | 626.4   | 13.4  | Final           |                 |                |      |
|                          |       | Total   | 156.8 |                 |                 |                |      |

[illegible]

Filter No. 272Nozzle No./Size 1265/1.3652[illegible]

Filter No.

[illegible]

er No. 300

Nozzle No./Size 1265/.3652

[illegible]

Date 2-5-85  
 Test Location Basin Mill #2  
 Run Number 1  
 Stack Diameter 72"  
 Operator RCO  
 Filter No. 292  
 Barometric Pressure 26.45  
 Static in. wg. -0.47  
 Probe Type/Length 66 in. 8'  
 Pitot Coefficient 0.890  
 Meter Box No. 18446/19838  
 Nozzle No./Size 466/0.2330

| Impinger Volumes/Weights |       |         |      | Gas Composition |                 |                |     |
|--------------------------|-------|---------|------|-----------------|-----------------|----------------|-----|
| Contents                 | Final | Initial | Net  | Time            | CO <sub>2</sub> | O <sub>2</sub> | CO  |
| <i>Wash DI</i>           | 608.6 | 548.6   | 60.0 |                 |                 |                |     |
| <i>Wash DI</i>           | 581.0 | 561.7   | 19.3 |                 |                 |                |     |
| <i>DRY</i>               | 437.3 | 435.0   | 2.3  |                 |                 |                |     |
|                          |       |         |      | Leak Rate       | cfm             |                | "Hg |
|                          |       |         |      | Initial         |                 | 12.7           | 15  |
| S.G.                     | 674.5 | 656.1   | 18.4 | Final           |                 | 12.3           | 11  |
|                          | Total |         |      |                 |                 |                |     |

| Sample Point | Time  | $\Delta P$ in wg | $\Delta H$ in wg | Gas Meter Volume Ft <sup>3</sup> | Temperature °F |       |      |      |           | Pump Vacuum in. Hg | $\sqrt{\Delta P}$ | Comments |                  |
|--------------|-------|------------------|------------------|----------------------------------|----------------|-------|------|------|-----------|--------------------|-------------------|----------|------------------|
|              |       |                  |                  |                                  | Stack          | Probe | Oven | Imp. | Gas Meter |                    |                   |          |                  |
|              |       |                  |                  |                                  |                |       |      |      | In        | Out                |                   |          |                  |
| 1            | 11:44 | 0.54             | 1.94             | 218.012                          | 155            | 263   | 238  | 47   | 57        | 58                 | 8.5               | 0.735    | 11.7-0.4         |
| 2            | 10    | 0.58             | 2.09             | 226.30                           | 156            | 236   | 243  | 47   | 62        | 58                 | 10.0              | 0.762    |                  |
| 3            | 10    | 0.56             | 2.02             | 234.87                           | 157            | 233   | 241  | 48   | 64        | 57                 | 10.0              | 0.748    |                  |
| 4            | 10    | 0.52             | 1.87             | 243.45                           | 158            | 235   | 241  | 46   | 64        | 58                 | 9.0               | 0.721    |                  |
| 5            | 10    | 0.50             | 1.80             | 251.72                           | 157            | 237   | 237  | 45   | 64        | 58                 | 8.5               | 0.707    |                  |
| 6            | 50    | 0.73             | 1.55             | 259.81                           | 157            | 261   | 237  | 44   | 65        | 59                 | 7.5               | 0.656    |                  |
|              | 60    |                  |                  | 267.385                          |                |       |      |      |           |                    |                   |          |                  |
| 1            | 12:50 | 0.52             | 1.87             | 267.38                           | 156            | 259   | 238  | 48   | 61        | 59                 | 8.5               | 0.721    |                  |
| 2            | 10    | 0.55             | 2.00             | 225.68                           | 157            | 265   | 243  | 49   | 67        | 62                 | 9.0               | 0.742    |                  |
| 3            | 10    | 0.54             | 1.95             | 284.27                           | 159            | 238   | 243  | 47   | 67        | 61                 | 9.0               | 0.735    |                  |
| 4            | 30    | 0.52             | 1.88             | 292.157                          | 159            | 238   | 235  | 47   | 67        | 61                 | 9.0               | 0.721    | Acc 1<br>85 5872 |
| 5            | 40    | 0.48             | 1.75             | 300.75                           | 158            | 264   | 233  | 48   | 70        | 64                 | 8.0               | 0.693    | 85 5873          |
| 6            | 50    | 0.43             | 1.57             | 308.90                           | 160            | 270   | 239  | 59   | 72        | 66                 | 7.5               | 0.656    |                  |
|              | 60    |                  |                  | 316.718                          |                |       |      |      |           |                    |                   |          | Plot - 0.4       |
|              |       |                  | 0.86             | 98.406                           | 157.42         |       |      |      | 62.54     |                    |                   | 0.7164   |                  |

Acc 1  
85 5872

Plt 1  
85 5873

Plt 1  
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Plt 1  
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Date 1-7-85 Barometric Pressure 36.52  
 Test Location RAW MILL Static in. wg. - .35  
 Run Number #2 Probe Type/Length Alum. 6'  
 Stack Diameter 22" Pitot Coefficient .810  
 Operator JCO Meter Box No. 18446/18828  
 Filter No. 294 Nozzle No./Size 141/03530

| Impinger Volumes/Weights |       |         |      | Gas Composition |                 |                |     |
|--------------------------|-------|---------|------|-----------------|-----------------|----------------|-----|
| Contents                 | Final | Initial | Net  | Time            | CO <sub>2</sub> | O <sub>2</sub> | CO  |
| DI                       | 569.7 | 523.9   | 45.8 |                 |                 |                |     |
| DE                       | 563.6 | 545.2   | 18.4 |                 |                 |                |     |
| DAY                      | 441.6 | 438.2   | 3.4  |                 |                 |                |     |
|                          |       |         |      | Leak Rate       | cfm             |                | "Hg |
|                          |       |         |      | Initial         |                 |                | 17  |
| S.G.                     | 664.3 | 645.1   | 19.2 | Final           |                 |                | 17  |
|                          |       | Total   | 86.8 |                 |                 |                |     |

| Sample Point | Time | $\Delta P$ in wg | $\Delta H$ in wg | Gas Meter Volume Ft <sup>3</sup> | Temperature °F |       |      |      | Pump Vacuum in. Hg | $\sqrt{\Delta P}$ | Comments                       |
|--------------|------|------------------|------------------|----------------------------------|----------------|-------|------|------|--------------------|-------------------|--------------------------------|
|              |      |                  |                  |                                  | Stack          | Probe | Oven | Imp. |                    |                   |                                |
| NW 0933      |      |                  |                  |                                  |                |       |      |      |                    |                   |                                |
| 1            | 0    | 0.96             | 3.23             | 323.645                          | 170            | 228   | 221  | 27   | 16.0               | 0.980             | P, F, OI - OK                  |
| 2            | 10   | 0.56             | 1.91             | 333.90                           | 167            | 243   | 234  | 37   | 8.5                | 0.748             | case noted went down for 6 min |
| 3            | 30   | 0.60             | 2.08             | 342.56                           | 163            | 255   | 240  | 39   | 9.05               | 0.775             | high velocity                  |
| 4            | 30   | 0.56             | 1.95             | 351.17                           | 162            | 238   | 233  | 40   | 9.0                | 0.748             |                                |
| 5            | 40   | 0.51             | 1.79             | 359.58                           | 161            | 262   | 234  | 47   | 8.0                | 0.714             | 855889                         |
| 6            | 50   | 0.44             | 1.55             | 367.64                           | 159            | 267   | 231  | 48   | 7.0                | 0.663             |                                |
|              | 60   |                  |                  | 325.205                          | 15             |       |      |      |                    |                   | 855888                         |
| SW 1043      |      |                  |                  |                                  |                |       |      |      |                    |                   |                                |
| 1            | 0    | 0.60             | 2.11             | 325.205                          | 159            | 223   | 230  | 51   | 9.0                | 0.775             |                                |
| 2            | 10   | 0.63             | 2.22             | 383.91                           | 165            | 271   | 234  | 46   | 10.0               | 0.794             |                                |
| 3            | 20   | 0.55             | 1.72             | 392.93                           | 169            | 241   | 244  | 43   | 8.0                | 0.742             |                                |
| 4            | 30   | 0.45             | 1.56             | 400.97                           | 171            | 261   | 232  | 47   | 7.5                | 0.671             |                                |
| 5            | 40   | 0.43             | 1.50             | 408.58                           | 168            | 267   | 230  | 47   | 7.0                | 0.656             |                                |
| 6            | 50   | 0.40             | 1.57             | 416.00                           | 170            | 237   | 232  | 49   | 7.5                | 0.671             |                                |
|              | 60   |                  |                  | 423.543                          |                |       |      |      |                    |                   |                                |
|              |      |                  | 1.93             | 99.898                           | 171.033        |       |      |      |                    | 0.7447            |                                |

Nozzle No./Size 1411/1530

| Sample Point | Time | $\Delta P$ in wg | $\Delta H$ in wg | Gas Meter Volume Ft <sup>3</sup> | Temperature °F |       |      |      |           |     | Pump Vacuum in. Hg | $\sqrt{\Delta P}$ | Comments        |
|--------------|------|------------------|------------------|----------------------------------|----------------|-------|------|------|-----------|-----|--------------------|-------------------|-----------------|
|              |      |                  |                  |                                  | Stack          | Probe | Oven | Imp. | Gas Meter |     |                    |                   |                 |
|              |      |                  |                  |                                  |                |       |      |      | In        | Out |                    |                   |                 |
| SW 1         | 1326 | 0.61             | 2.11             | 424.460                          | 164            | 245   | 248  | 44   | 63        | 64  | 2.0                | 0.781             | P.TOT-OK        |
| 2            | 10   | .66              | 2.33             | 433.06                           | 162            | 248   | 253  | 46   | 75        | 69  | 8.05               | 0.812             |                 |
| 3            | 30   | .63              | 2.23             | 442.032                          | 165            | 228   | 256  | 49   | 78        | 72  | 8.0                | 0.794             | 98433<br>855890 |
| 4            | 30   | .63              | 2.22             | 451.038                          | 169            | 252   | 255  | 47   | 80        | 74  | 8.0                | 0.794             |                 |
| 5            | 40   | .60              | 2.11             | 460.47                           | 172            | 259   | 254  | 46   | 81        | 74  | 7.5                | 0.775             | 98433<br>855891 |
| 6            | 50   | .52              | 1.83             | 469.30                           | 172            | 262   | 254  | 47   | 81        | 75  | 7.0                | 0.721             |                 |
|              | 60   |                  |                  | 477.536                          |                |       |      |      |           |     |                    |                   |                 |
| NW 1         | 1431 | 0.66             | 2.31             | 477.536                          | 170            | 235   | 255  | 49   | 76        | 75  | 8.0                | 0.812             |                 |
| 2            | 10   | .70              | 2.46             | 486.70                           | 173            | 239   | 262  | 45   | 81        | 76  | 9.0                | 0.837             |                 |
| 3            | 30   | .66              | 2.31             | 496.18                           | 175            | 231   | 257  | 46   | 82        | 76  | 8.0                | 0.812             |                 |
| 4            | 30   | .62              | 2.17             | 505.49                           | 175            | 236   | 257  | 45   | 82        | 77  | 8.0                | 0.787             |                 |
| 5            | 40   | .60              | 2.11             | 514.47                           | 172            | 254   | 258  | 48   | 82        | 76  | 7.5                | 0.725             |                 |
| 6            | 50   | .50              | 1.78             | 523.25                           | 167            | 260   | 258  | 48   | 82        | 77  | 6.5                | 0.707             |                 |
|              | 60   |                  |                  | 531.329                          |                |       |      |      |           |     |                    |                   |                 |
|              |      |                  | 2.16             | 106.869                          | 169.67         |       |      |      | 76.17     |     |                    |                   | 0.7839          |



CONTINUOUS MONITOR DATA SHEET

Plant SUN PC Ambient Temperature \_\_\_\_\_  
 Date 2-6-85 Barometric Pressure \_\_\_\_\_  
 Test Location Kilauea Static Pressure Duct \_\_\_\_\_  
 Run Number load 218 TPH Fuel \_\_\_\_\_  
 Operator geo

| Time | Sample Point | Fuel Flow | Dry Uncorrected  |                   |        |                     |        |                     | 3% O <sub>2</sub> Dry |                     | Hydrocarbons |                 |                     | Comments         |
|------|--------------|-----------|------------------|-------------------|--------|---------------------|--------|---------------------|-----------------------|---------------------|--------------|-----------------|---------------------|------------------|
|      |              |           | O <sub>2</sub> % | CO <sub>2</sub> % | CO ppm | SO <sub>2</sub> ppm | NO ppm | NO <sub>x</sub> ppm | ppm                   | NO <sub>x</sub> ppm | THC          | CH <sub>4</sub> | Non CH <sub>4</sub> |                  |
| 0800 |              |           | 2.57             | 16.0              | 403.2  | 80.9                |        | 452.25              |                       |                     |              |                 |                     | span gas reading |
| 0805 | 20 min Avg   |           | 9.70             | 18.8              | 300    | 4                   |        | 510                 |                       |                     |              |                 |                     | span gas reading |
| 0810 |              |           | 9.50             | 18.6              | 280    | 4                   |        | 500                 |                       |                     |              |                 |                     |                  |
| 0815 |              |           | 9.55             | 18.8              | 320    | 4                   |        | 510                 |                       |                     |              |                 |                     |                  |
| 0820 |              |           | 9.50             | 18.8              | 275    | 4                   |        | 490                 |                       |                     |              |                 |                     |                  |
| 0825 |              |           | 9.25             | 19.0              | 300    | 4                   |        | 460                 |                       |                     |              |                 |                     |                  |
| 0830 |              |           | 9.25             | 19.0              | 320    | 4                   |        | 470                 |                       |                     |              |                 |                     |                  |
| 0835 |              |           | 9.25             | 19.0              | 325    | 4                   |        | 470                 |                       |                     |              |                 |                     |                  |
| 0840 |              |           | 9.10             | 19.0              | 340    | 4                   |        | 470                 |                       |                     |              |                 |                     |                  |
| 0845 |              |           | 9.10             | 19.0              | 285    | 4                   |        | 500                 |                       |                     |              |                 |                     |                  |
| 0850 |              |           | 0                | 0                 | 0      | 0                   |        | 0                   |                       |                     |              |                 |                     | good reading     |
| 0855 |              |           | 7.38             | 15.9              | 403    | 79.9                |        | 447                 |                       |                     |              |                 |                     | span reading     |
| 0900 |              |           | 9.00             | 19.2              | 270    | 3                   |        | 510                 |                       |                     |              |                 |                     |                  |
| 0905 |              |           | 9.25             | 18.6              | 220    | 2                   |        | 570                 |                       |                     |              |                 |                     |                  |
| 0910 |              |           | 9.08             | 18.8              | 210    | 3                   |        | 580                 |                       |                     |              |                 |                     |                  |
| 0915 |              |           | 9.38             | 19.0              | 205    | 2                   |        | 600                 |                       |                     |              |                 |                     |                  |
| 0920 |              |           | 9.20             | 18.4              | 220    | 2                   |        | 540                 |                       |                     |              |                 |                     |                  |
| 0925 |              |           | 9.25             | 18.2              | 150    | 1                   |        | 510                 |                       |                     |              |                 |                     |                  |
| 0930 |              |           | 9.00             | 18.4              | 200    | 1                   |        | 550                 |                       |                     |              |                 |                     |                  |
| 0935 |              |           | 8.90             | 18.8              | 235    | 2                   |        | 530                 |                       |                     |              |                 |                     |                  |
| 0940 |              |           | 9.00             | 18.4              | 180    | 2                   |        | 550                 |                       |                     |              |                 |                     |                  |
| 0945 |              |           | -0.2             | 0                 | 10     | 0                   |        | 73                  |                       |                     |              |                 |                     | good reading     |
| 0950 |              |           | 7.15             | 15.8              | 423    | 80.2                |        | 436                 |                       |                     |              |                 |                     | span reading     |

11

Ambient Temperature \_\_\_\_\_  
Barometric Pressure \_\_\_\_\_  
Static Pressure Duct \_\_\_\_\_  
Fuel \_\_\_\_\_

[illegible]

CONTINUOUS MONITOR DATA SHEET

1 of 2

Plant SUPC Ambient Temperature \_\_\_\_\_  
 Date 2-7-85 Barometric Pressure \_\_\_\_\_  
 Test Location Kilom Static Pressure Duct \_\_\_\_\_  
 Run Number 2187PH Fuel \_\_\_\_\_  
 Operator geo

| Time | Sample Point | Fuel Flow | Dry Uncorrected  |                   |        |                     |        |                     | 3% O <sub>2</sub> Dry |     | Hydrocarbons |                 |                     | Comments                         |
|------|--------------|-----------|------------------|-------------------|--------|---------------------|--------|---------------------|-----------------------|-----|--------------|-----------------|---------------------|----------------------------------|
|      |              |           | O <sub>2</sub> % | CO <sub>2</sub> % | CO ppm | SO <sub>2</sub> ppm | NO ppm | NO <sub>x</sub> ppm | ppm                   | ppm | THC          | CH <sub>4</sub> | Non CH <sub>4</sub> |                                  |
|      |              |           | 14.57            | 16.0              | 403.2  | 80.9                |        | 457.25              |                       |     |              |                 |                     | span gas valve, good leak check. |
| 0740 |              |           | 9.50             | 18.8              | 350    | 4                   |        | 460                 |                       |     |              |                 |                     |                                  |
| 0800 |              |           | 9.50             | 18.6              | 250    | 4                   |        | 480                 |                       |     |              |                 |                     |                                  |
| 0820 |              |           | 9.25             | 19.0              | 250    | 5                   |        | 460                 |                       |     |              |                 |                     |                                  |
| 0840 |              |           | 9.25             | 18.8              | 260    | 4                   |        | 480                 |                       |     |              |                 |                     |                                  |
| 0900 |              |           | 9.25             | 19.0              | 250    | 4                   |        | 490                 |                       |     |              |                 |                     |                                  |
| 0920 |              |           | 9.38             | 19.0              | 260    | 4                   |        | 570                 |                       |     |              |                 |                     |                                  |
| 0940 |              |           | 9.10             | 19.0              | 290    | 4                   |        | 570                 |                       |     |              |                 |                     |                                  |
| 1000 |              |           | 9.10             | 19.1              | 320    | 4                   |        | 490                 |                       |     |              |                 |                     | lost fire                        |
| 1020 |              |           |                  |                   |        |                     |        | 4                   |                       |     |              |                 |                     |                                  |
| 1040 |              |           | 8.80             | 19.0              | 325    | 4                   |        | 450                 |                       |     |              |                 |                     |                                  |
| 1100 |              |           | 8.80             | 19.4              | 350    | 4                   |        | 470                 |                       |     |              |                 |                     |                                  |
| 1120 |              |           | 9.00             | 19.0              | 370    | 4                   |        | 480                 |                       |     |              |                 |                     |                                  |
| 1140 |              |           | 8.80             | 19.0              | 350    | 4                   |        | 450                 |                       |     |              |                 |                     |                                  |
| 1200 |              |           | 8.80             | 19.0              | 350    | 4                   |        | 480                 |                       |     |              |                 |                     |                                  |
|      |              |           | -0.20            | 20.1              | 10     | 0                   |        | 0                   |                       |     |              |                 |                     | gas reading                      |
|      |              |           | 7.20             | 15.8              | 487    | 79.5                |        | 435                 |                       |     |              |                 |                     | gas reading                      |

Plant SWPC Ambient Temperature \_\_\_\_\_  
Date 2-7-85 Barometric Pressure \_\_\_\_\_  
Test Location Kilmer Static Pressure Duct \_\_\_\_\_  
Run Number 2187PH Fuel \_\_\_\_\_  
Operator geo

[illegible]

Plant Southwestern Portland Cement

Date 7-8-85

Test Location Kila

Run Number

Operator

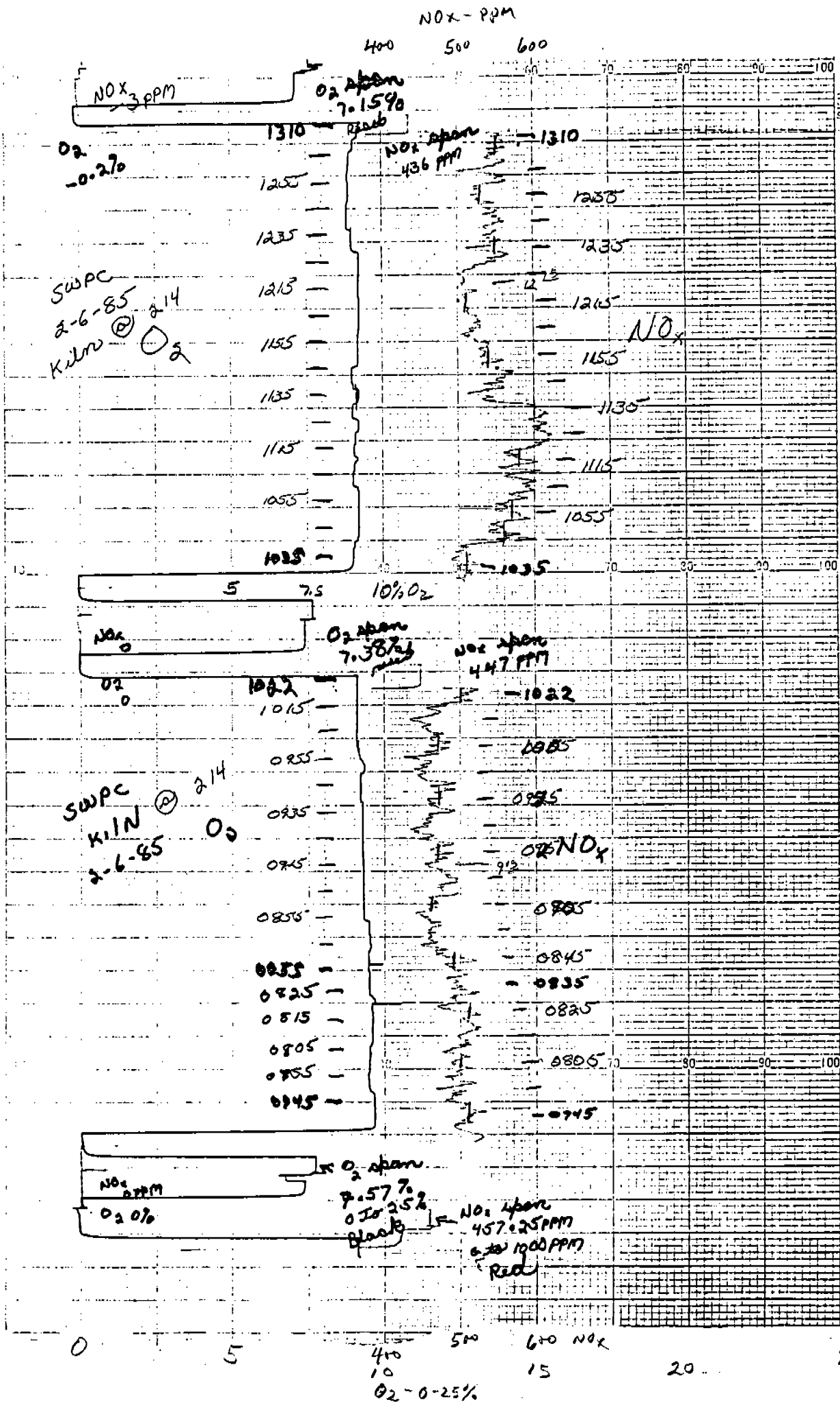
### Ambient Temperature

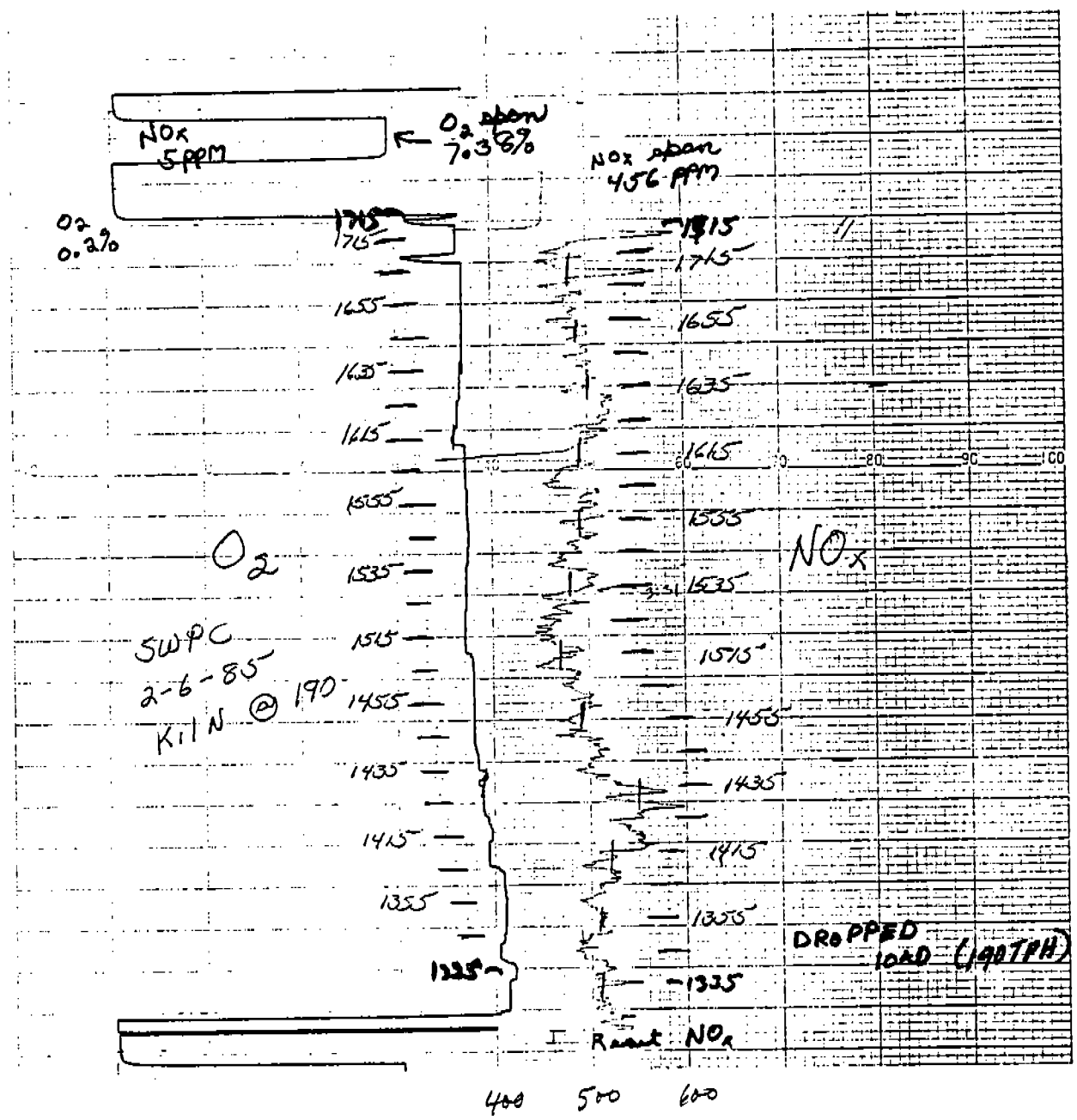
## Barometric Pressure

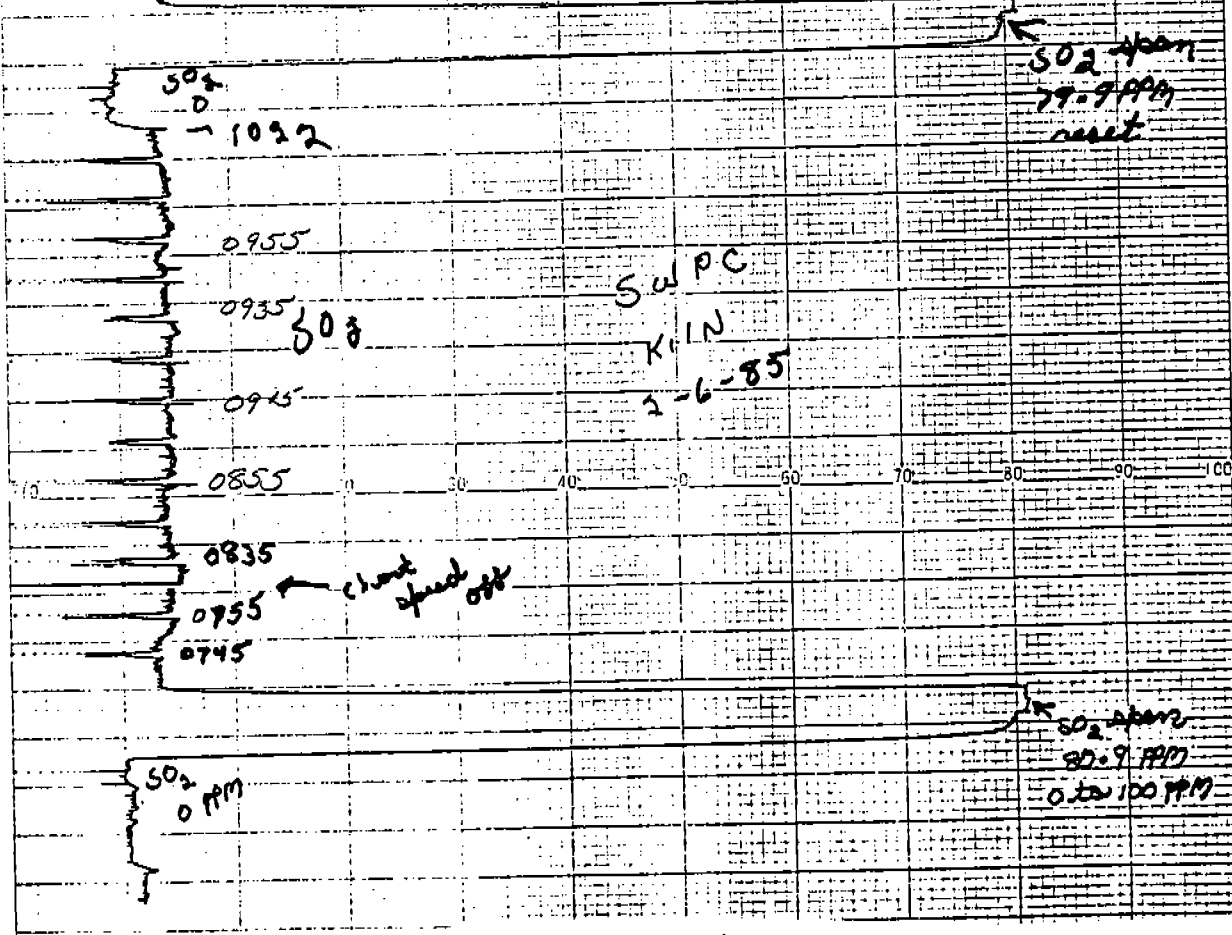
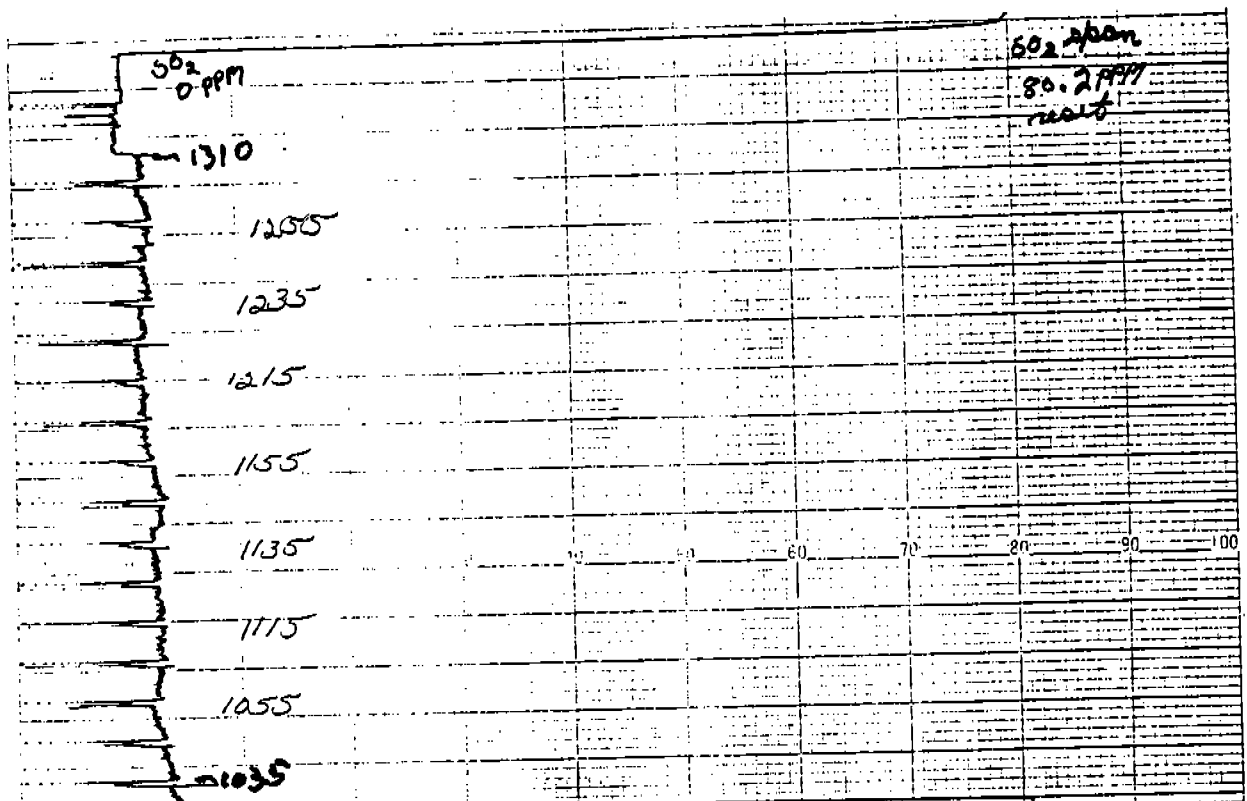
### Static Pressure Duct

Fuel

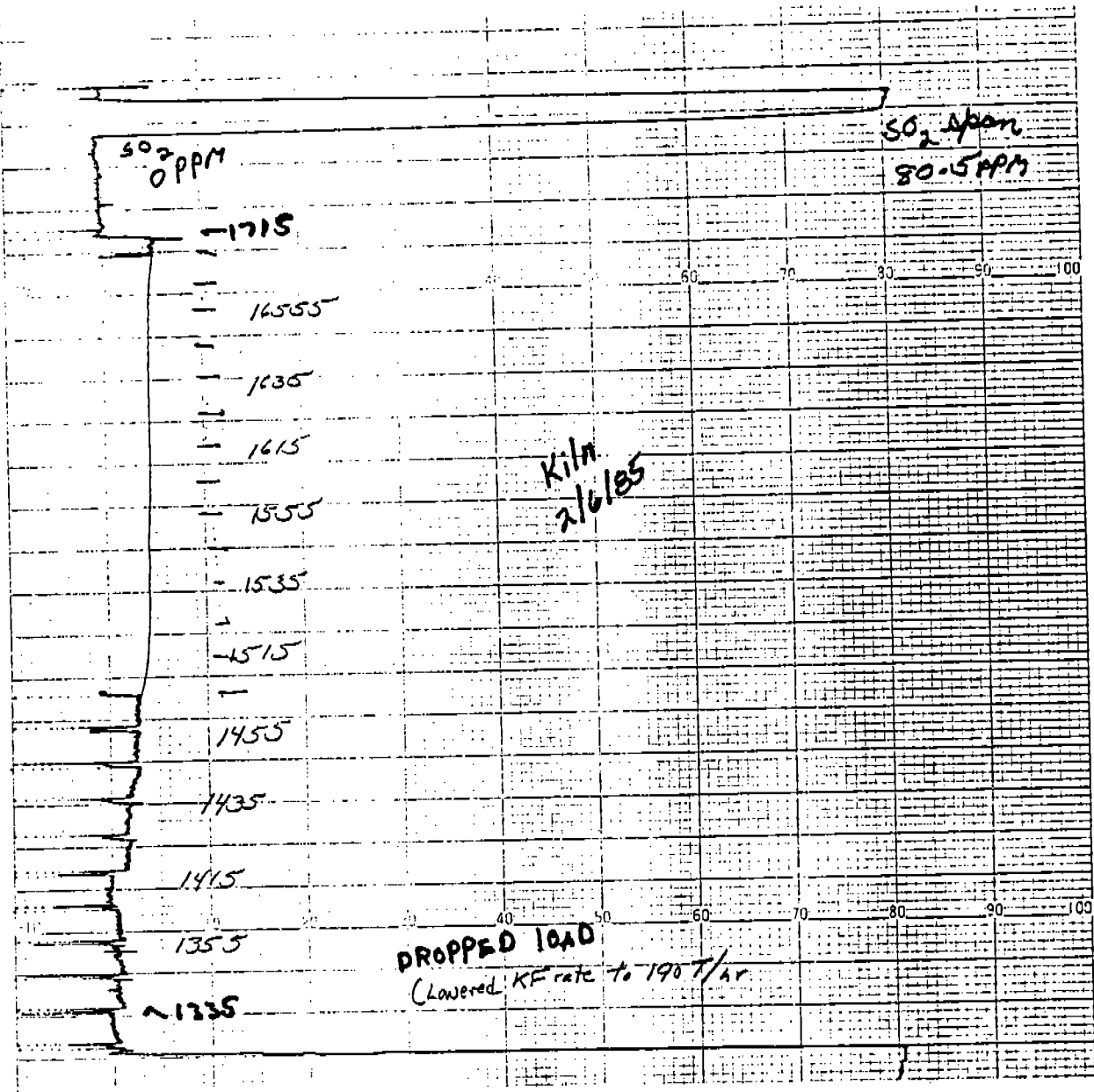
[illegible]

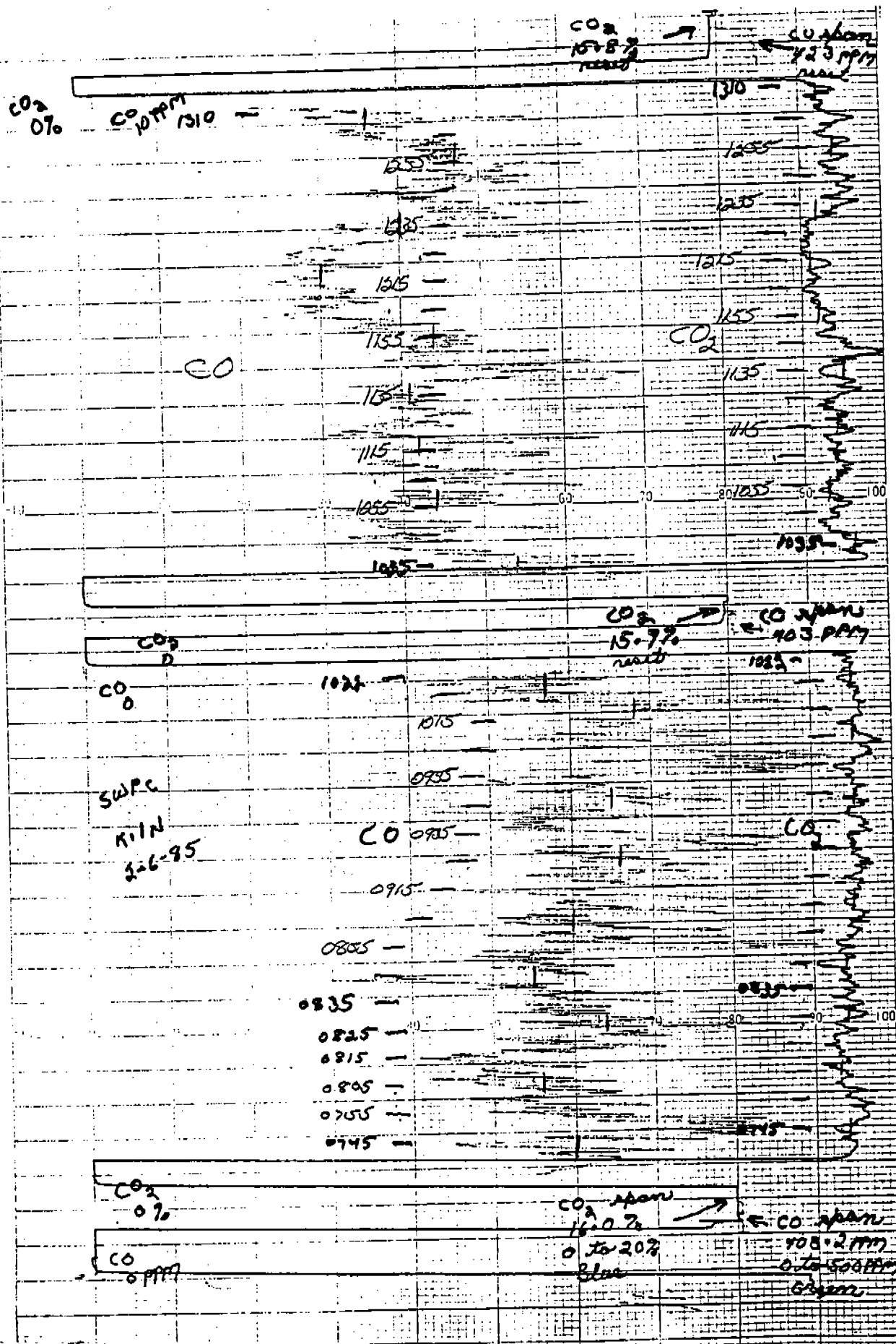


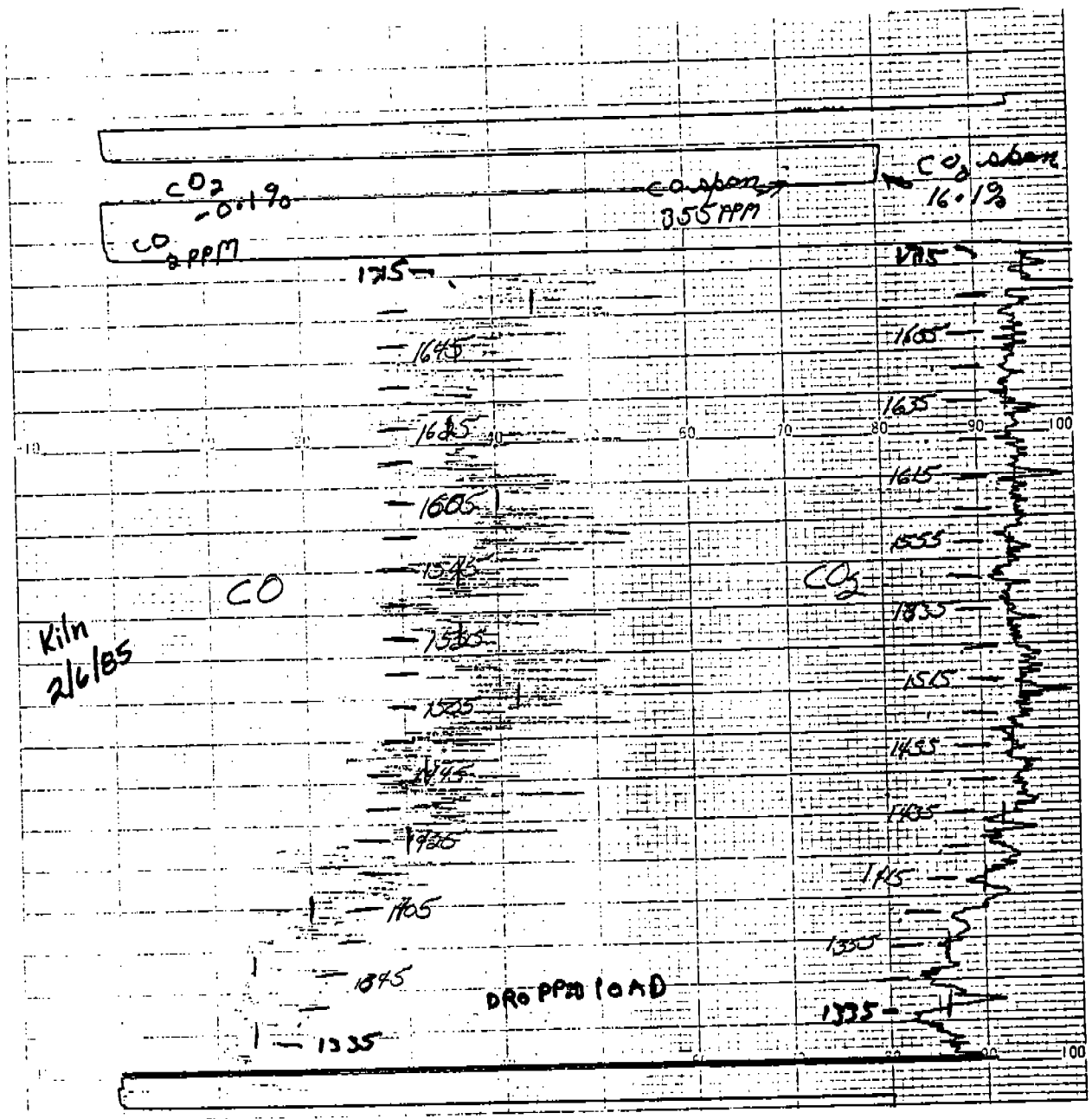


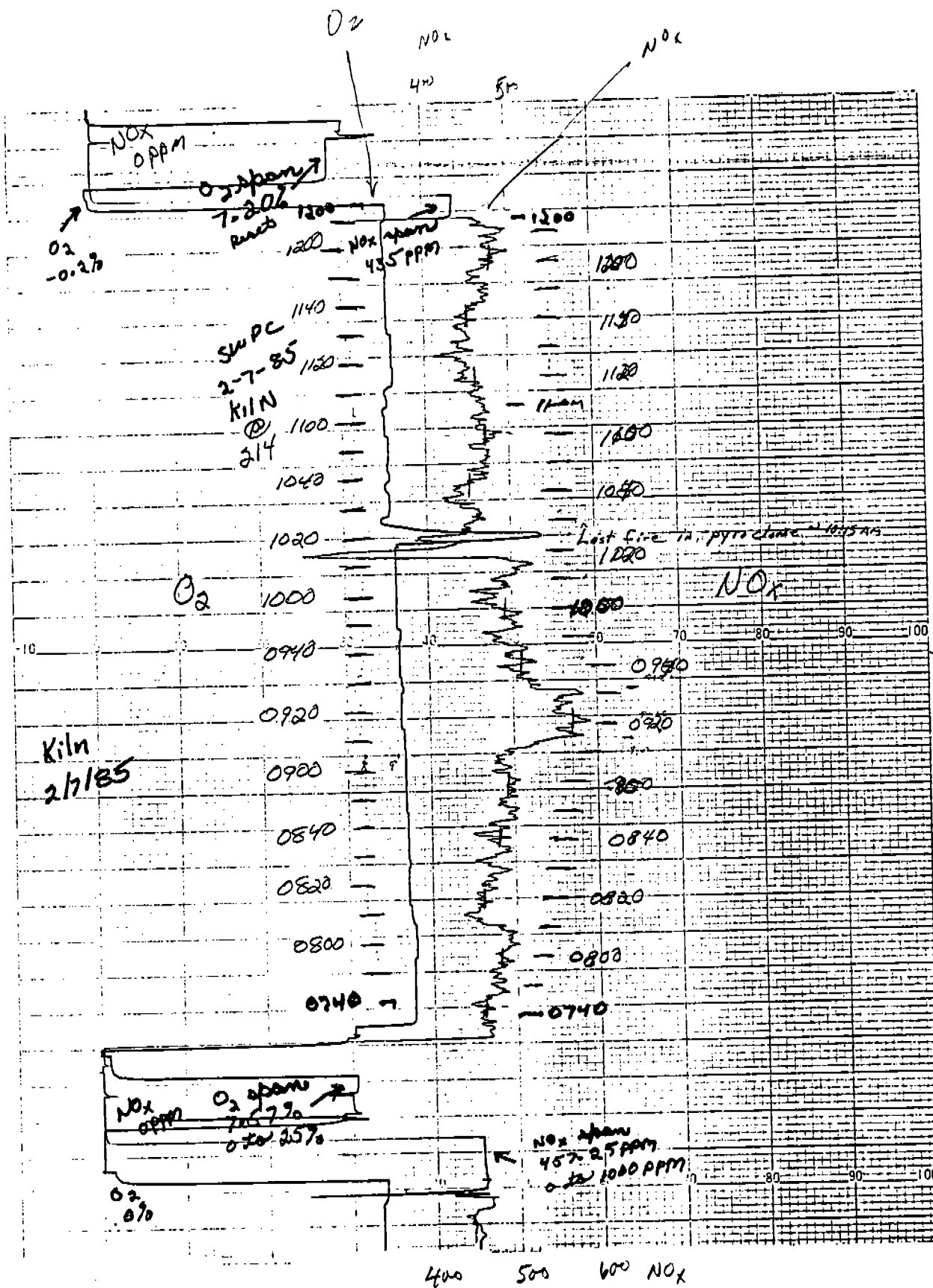


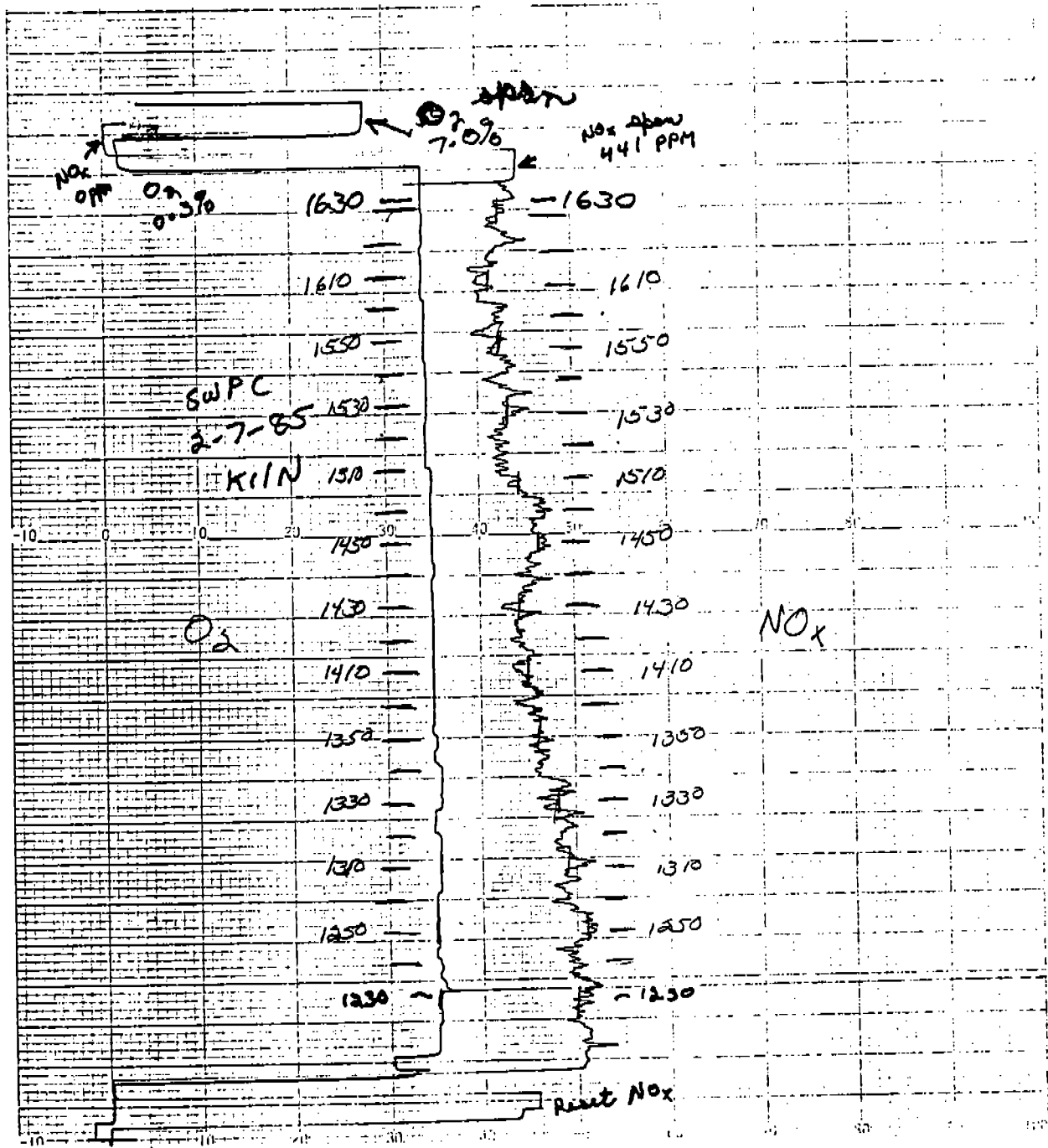


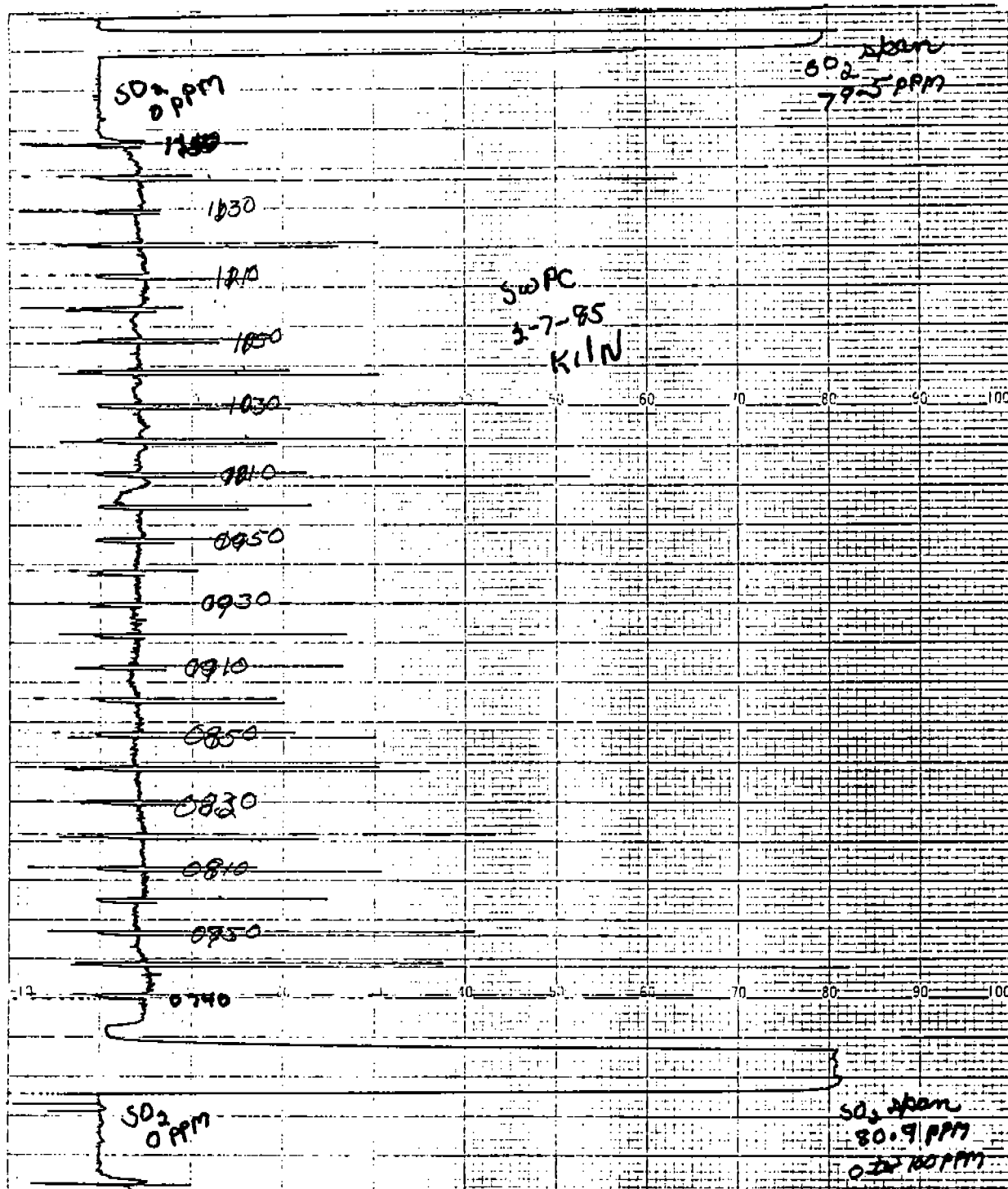


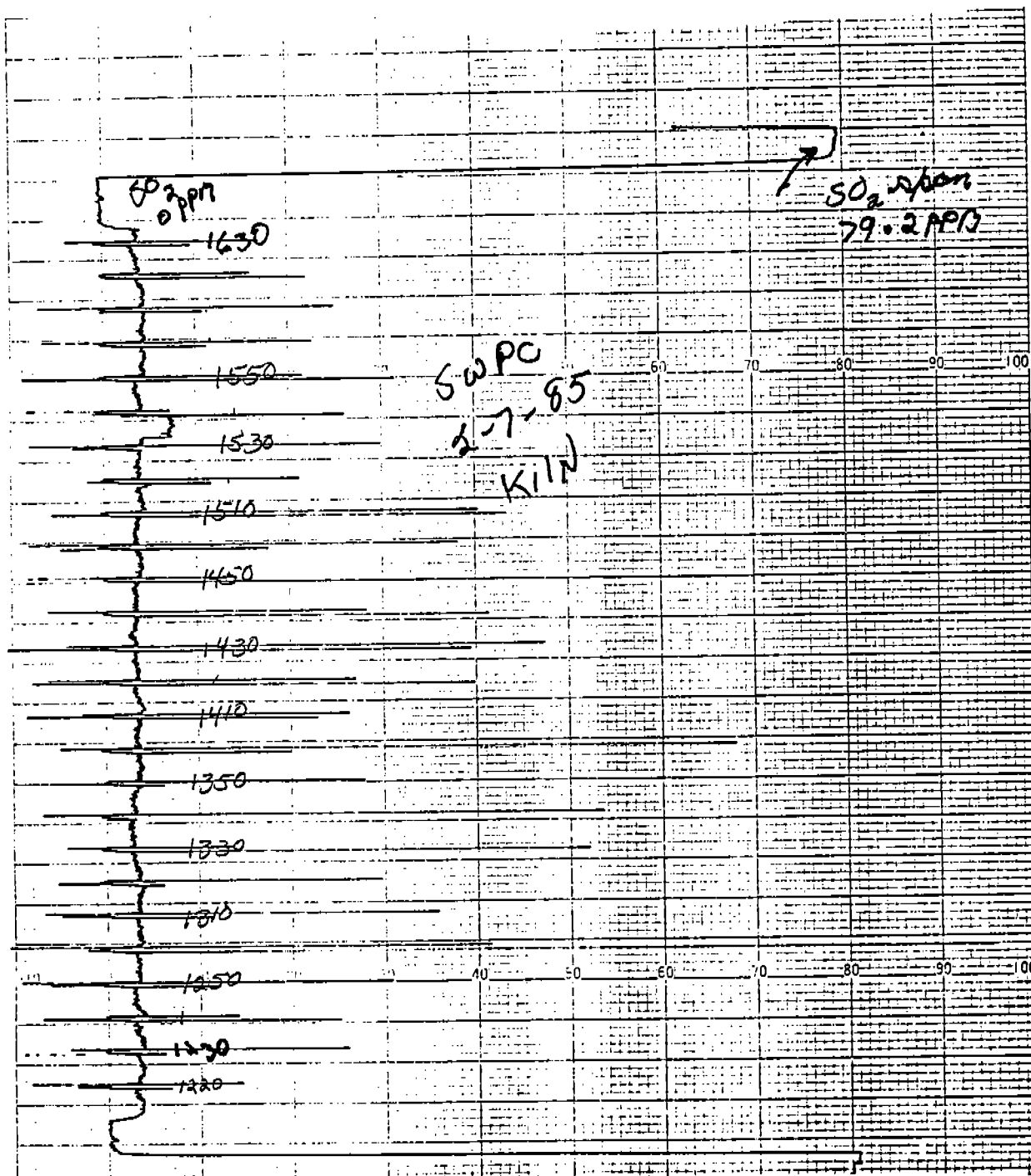


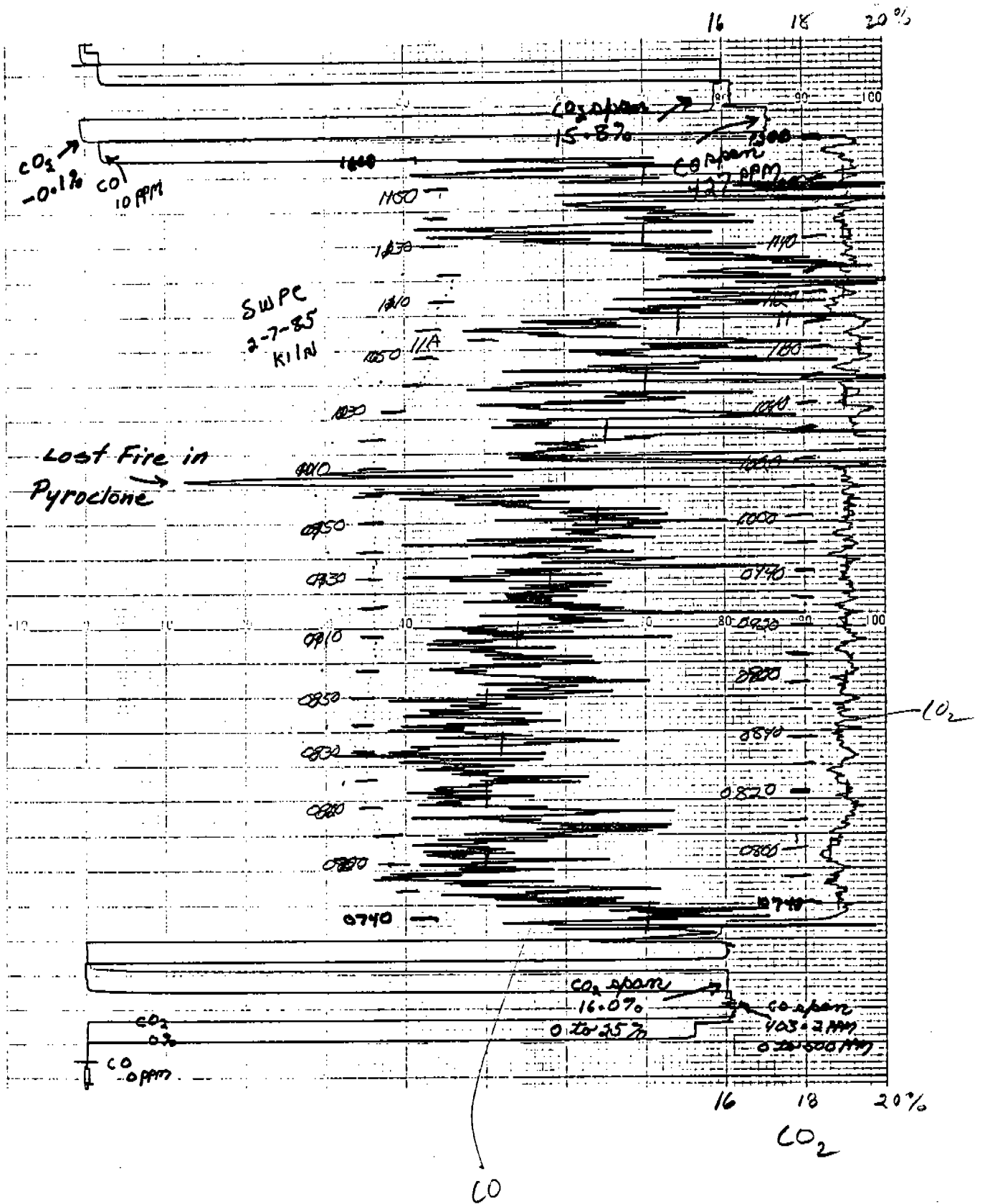






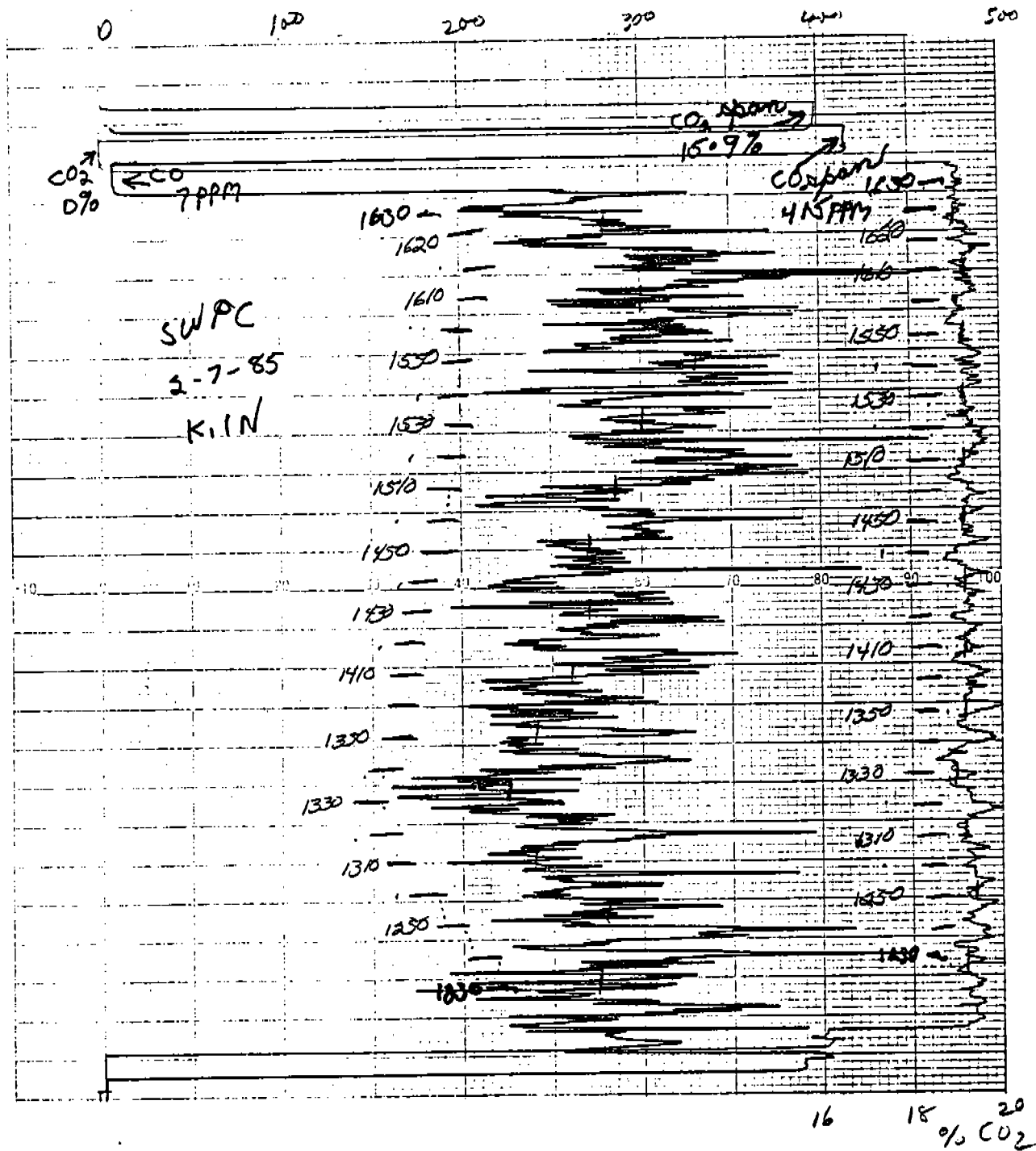




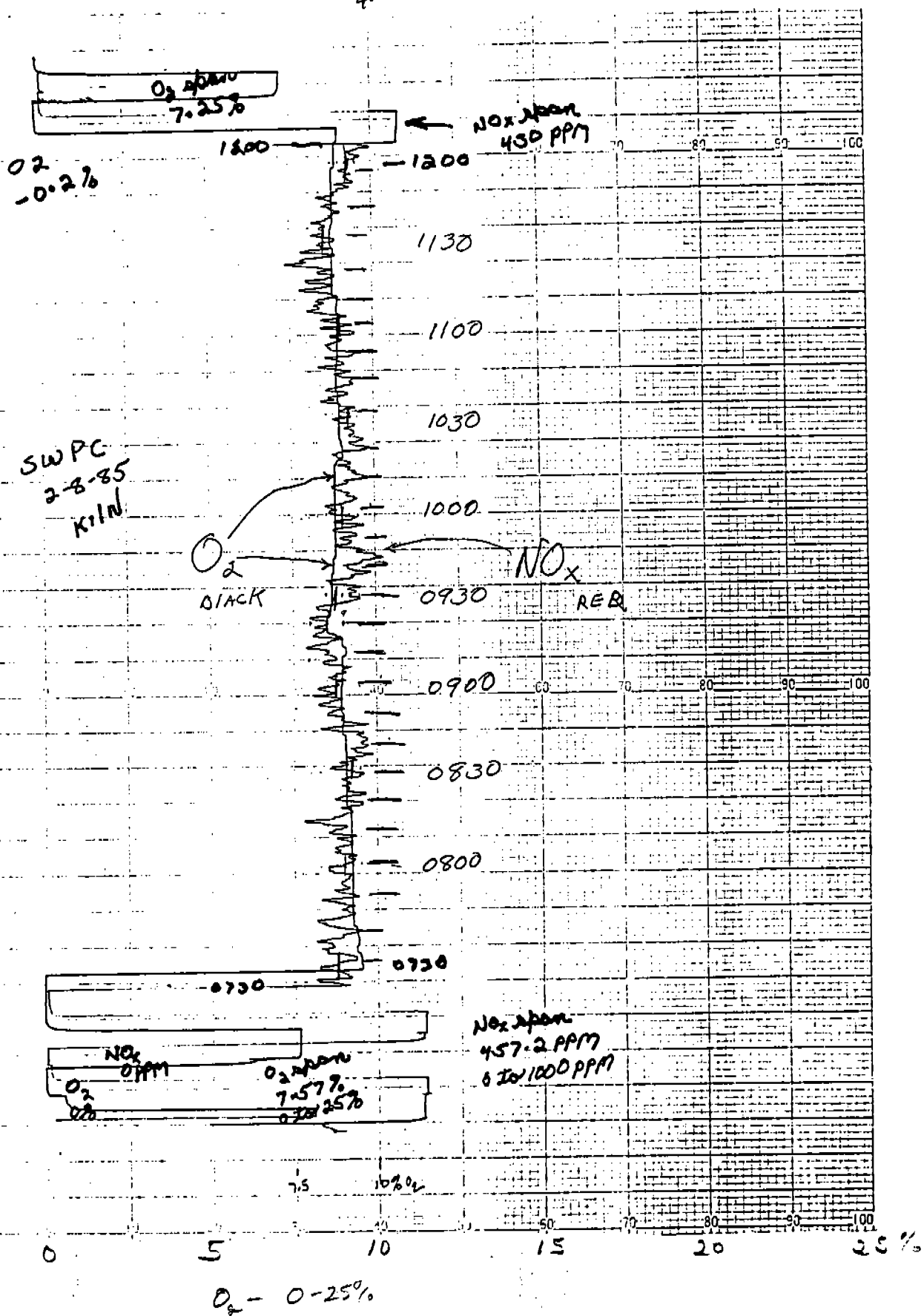


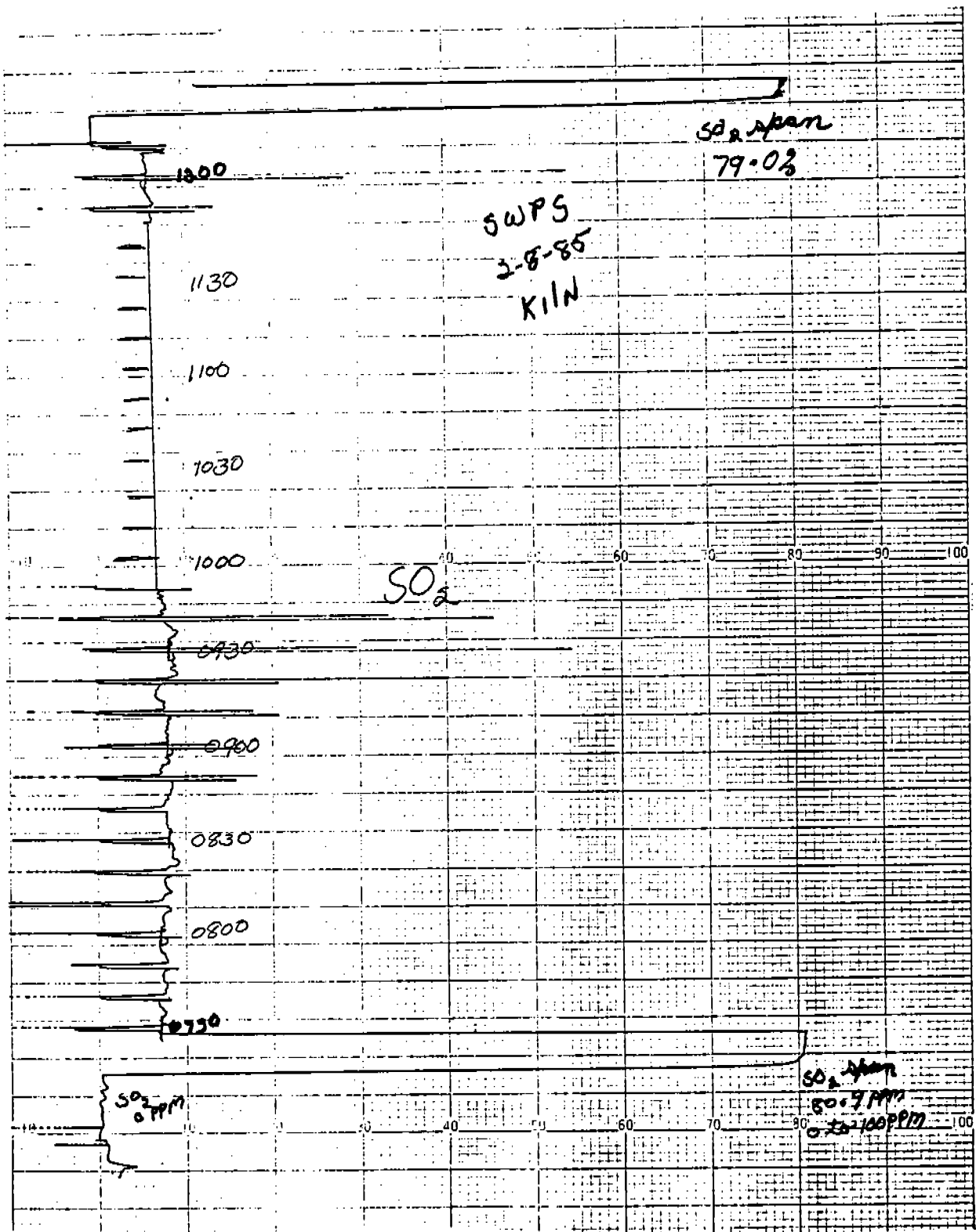


10 - 0-500 ppm



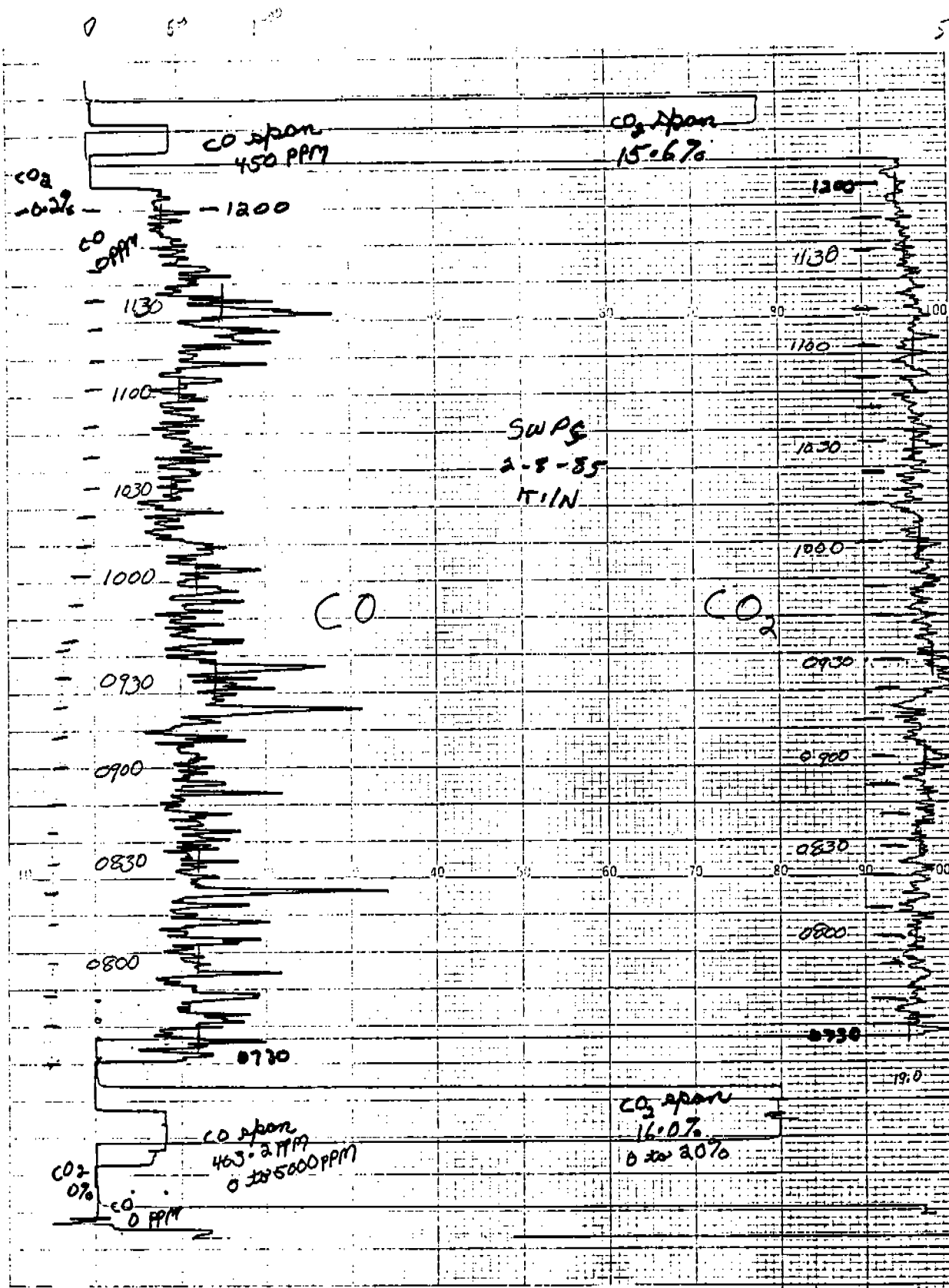
NOX - 0 - 1000 ppm  
ppm  
400 500





CO - 0 - 5000 PPM

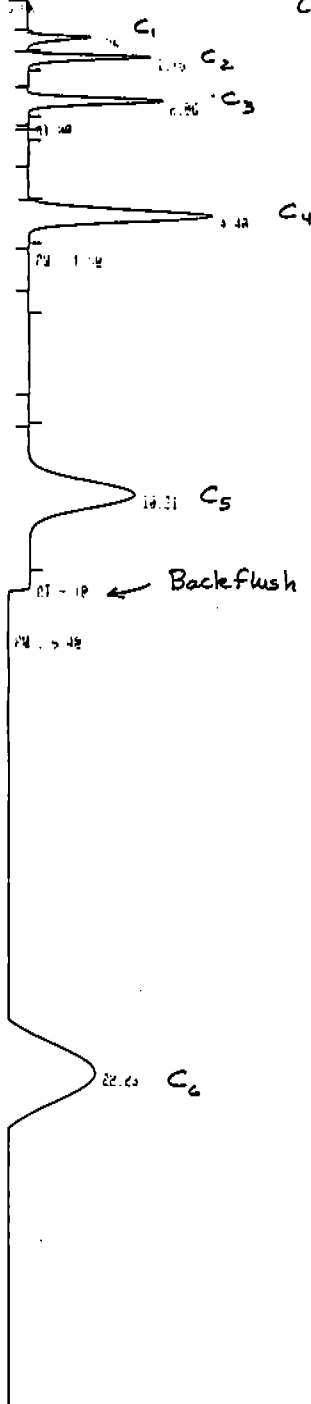
CO<sub>2</sub>  
0 - 20%



LIST: ZERO = 0.0.0

ATC 0.1 0.1  
THRESH 1.0

Initial  
Calibration  
2/6/85



STOP

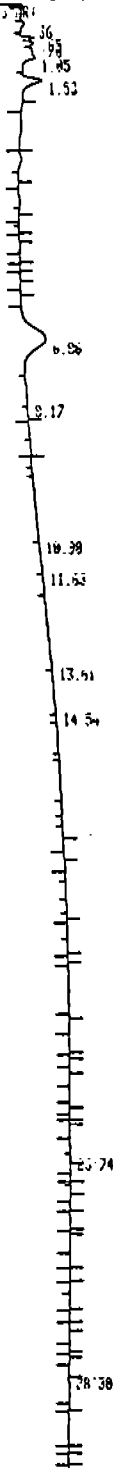
RUN # 1

| AREA# | RT     | AREA TYPE | AR/HT | AREA#  |
|-------|--------|-----------|-------|--------|
| 0.64  | 588    | CV        | 0.043 | 0.154  |
| 0.76  | 20170  | VB        | 0.115 | 5.131  |
| 1.15  | 38819  | UB        | 0.114 | 9.275  |
| 2.06  | 56734  | PM        | 0.152 | 14.433 |
| 4.40  | 72191  | BB        | 0.232 | 18.365 |
| 10.21 | 95257  | BB        | 0.651 | 24.232 |
| 22.23 | 109340 | FB        | 1.517 | 27.815 |

TOTAL AREA= 393100  
MUL FACTOR= 1.0000E+00

THRESH - 2.0  
PK WD - 0.4

Kila  
Test 1 2/5 TPH  
2/6/85

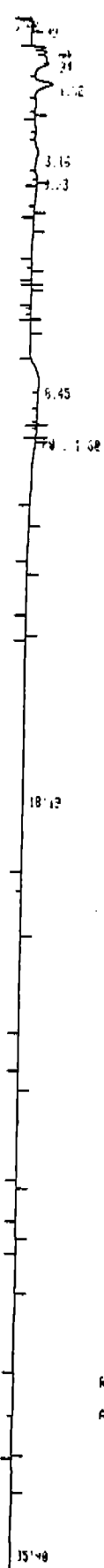


STOP

RUN # 2

| AREA# | RT   | AREA TYPE | AR/HT | AREA#  |
|-------|------|-----------|-------|--------|
| 0.36  | 344  | PP        | 0.110 | 1.721  |
| 0.65  | 628  | PV        | 0.068 | 3.141  |
| 0.76  | 342  | VV        | 0.098 | 4.711  |
| 1.05  | 2579 | VV        | 0.256 | 12.899 |
| 1.53  | 2255 | VB        | 0.167 | 11.278 |
| 6.86  | 7916 | PP        | 0.487 | 39.592 |
| 8.17  | 156  | PV        | 0.371 | 0.780  |
| 10.98 | 475  | PV        | 0.720 | 2.376  |
| 11.63 | 582  | VV        | 0.414 | 2.611  |
| 13.61 | 2353 | VV        | 1.123 | 11.799 |
| 14.54 | 1818 | VV        | 0.842 | 9.093  |

TOTAL AREA= 19994  
MUL FACTOR= 1.0000E+00

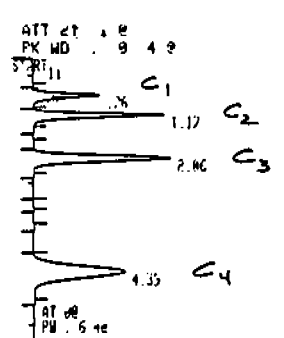


Kiln  
Test 2 190 TPH

RUN # 3

| AREA | RT   | AREA TYPE | HW/HT | AREAZ                 |
|------|------|-----------|-------|-----------------------|
| 0.09 | 242  | FB        | 0.106 | 2.242                 |
| 0.64 | 785  | BY        | 0.004 | 6.552                 |
| 0.76 | 1161 | VV        | 0.092 | 10.790 C <sub>1</sub> |
| 0.94 | 1848 | VV        | 0.156 | 17.175                |
| 1.52 | 2942 | VV        | 0.136 | 27.342                |
| 3.16 | 831  | PF        | 0.295 | 7.723                 |
| 3.73 | 53   | PV        | 0.055 | 0.493                 |
| 8.45 | 2378 | BY        | 0.564 | 27.677                |

STOP  
TOTAL AREA= 10.760  
MUL FACTOR= 1.0000E+00



Final  
Calibration

ATT 21  
PK WD 9 4 2  
5.45

STOP

RUN # 4

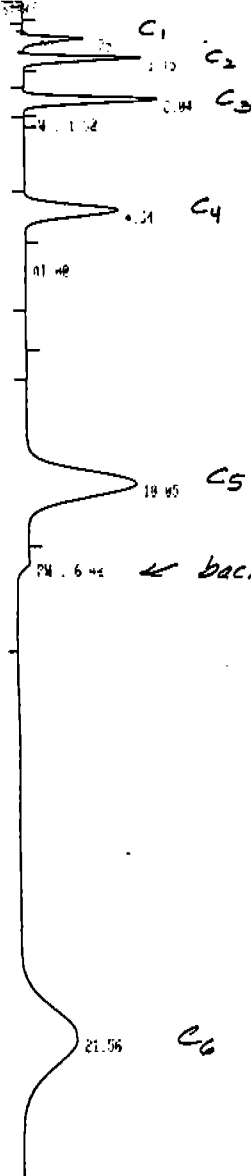
| AREA  | RT     | AREA TYPE | HW/HT | AREAZ  |
|-------|--------|-----------|-------|--------|
| 0.11  | 368    | PV        | 0.157 | 0.895  |
| 0.64  | 575    | BY        | 0.048 | 0.149  |
| 0.76  | 19278  | VB        | 0.185 | 4.981  |
| 1.17  | 57727  | PB        | 0.184 | 9.751  |
| 2.06  | 53188  | BB        | 0.145 | 14.264 |
| 4.39  | 78481  | PB        | 0.280 | 18.217 |
| 10.20 | 92372  | BB        | 0.686 | 23.874 |
| 22.20 | 110930 | I BH      | 1.565 | 28.670 |

TOTAL AREA= 386910  
MUL FACTOR= 1.0000E+00

LIST: 27.0 = 0.0.0

411.27 4.9  
PK MU 4.9

*Initial  
Calibration*



RUN # 5

JAN/07/85 11:11:59

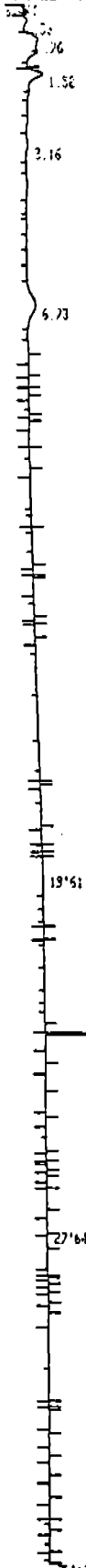
AREA%

| RT    | AREA   | TYPE | AN/MT | AREA4  |
|-------|--------|------|-------|--------|
| 0.64  | 367    | VP   | 0.038 | 0.091  |
| 0.75  | 20474  | VP   | 0.122 | 5.065  |
| 1.15  | 39642  | PB   | 0.121 | 9.807  |
| 2.04  | 57861  | PB   | 0.155 | 14.314 |
| 4.34  | 73901  | PB   | 0.297 | 18.262 |
| 10.05 | 97013  | PD   | 0.645 | 24.061 |
| 21.56 | 114970 | BD   | 1.514 | 29.441 |

TOTAL AREA= 404230  
MUL FACTOR= 1.0000E+00

ATT 27.0 1.2  
PK MU 0.4 2

*Kiln #2  
Test 3 218TPH  
2/7/85*



*electrical  
noise  
(no peak)*

RUN # 6

JAN/07/85 11:47:26

AREA%

| RT    | AREA | TYPE | AN/MT | AREA4  |
|-------|------|------|-------|--------|
| 0.33  | 372  | PP   | 0.117 | 2.205  |
| 0.76  | 2906 | VP   | 0.275 | 17.228 |
| 1.52  | 2215 | VP   | 0.191 | 13.131 |
| 3.16  | 525  | PP   | 0.257 | 3.112  |
| 6.73  | 3133 | VP   | 0.479 | 18.574 |
| 23.16 | 7717 | DB   | 0.015 | 45.749 |

TOTAL AREA= 16868  
MUL FACTOR= 1.0000E+00

SAMPLE HANDLING/LOG-IN

Date 2/5/85, 2/6/85 Test Location Raw Mill 2 Kiln 2  
Finish Mill 2 Clinker

|     | Sample Type                                  | Volume | Comments |
|-----|----------------------------------------------|--------|----------|
| 1.  | 85 5872 <u>5 Ace RH1</u><br>Meth Sample Test |        |          |
| 2.  | 85 5873 <u>5 FLT RH1</u><br>Meth Sample Test |        |          |
| 3.  | 855874 <u>5 Ace FM1</u><br>Meth Sample Test  |        |          |
| 4.  | 855875 <u>5 FLT FM1</u><br>Meth Sample Test  |        |          |
| 5.  | 855876 <u>5 Ace KI</u><br>Meth Sample Test   |        |          |
| 6.  | 85 5877 <u>5 FLT KI</u><br>Meth Sample Test  |        |          |
| 7.  | 85 5878 <u>5 Ace CI</u><br>Meth Sample Test  |        |          |
| 8.  | 85 5879 <u>5 FLT CI</u><br>Meth Sample Test  |        |          |
| 9.  | 85 5880 <u>5 Ace K2</u><br>Meth Sample Test  |        |          |
| 10. | 855881 <u>5 FLT K2</u><br>Meth Sample Test   |        |          |
| 11. | 855882 <u>5 Ace C2</u><br>Meth Sample Test   |        |          |
| 12. | 855883 <u>5 FLT C2</u><br>Meth Sample Test   |        |          |

CHAIN OF CUSTODY

JS

geo



SAMPLE HANDLING/LOG-IN

Date 2/7/85, 2/8/85

Test Location Kila, Raw Mill  
Clinker, Finish Mill

|     | Sample Type                                               | Volume | Comments |
|-----|-----------------------------------------------------------|--------|----------|
| 1.  | 855885 <u>5</u> <u>FLT</u> <u>K3</u><br>Meth Sample Test  |        |          |
| 2.  | 85 5884 <u>5</u> <u>Ace</u> <u>K3</u><br>Meth Sample Test |        |          |
| 3.  | 855886 <u>5</u> <u>ACE</u> <u>#2</u><br>Meth Sample Test  |        |          |
| 4.  | 85 5887 <u>5</u> <u>MF</u> <u>#2</u><br>Meth Sample Test  |        |          |
| 5.  | 855888 <u>5</u> <u>ACE</u> <u>2</u><br>Meth Sample Test   |        |          |
| 6.  | 85 5889 <u>5</u> <u>MF</u> <u>2</u><br>Meth Sample Test   |        |          |
| 7.  | 85 5890 <u>5</u> <u>ACE</u> <u>3</u><br>Meth Sample Test  |        |          |
| 8.  | 85 5891 <u>5</u> <u>MF</u> <u>3</u><br>Meth Sample Test   |        |          |
| 9.  | 855892 <u>5</u> <u>Ace</u> <u>C3</u><br>Meth Sample Test  |        |          |
| 10. | 855893 <u>5</u> <u>FLT</u> <u>C3</u><br>Meth Sample Test  |        |          |
| 11. | 855894 <u>5</u> <u>Ace</u> <u>FM3</u><br>Meth Sample Test |        |          |
| 12. | 855895 <u>5</u> <u>FLT</u> <u>FM3</u><br>Meth Sample Test |        |          |

CHAIN OF CUSTODY

JS

SAMPLE HANDLING/LOG-IN

Date 2/8/85 Test Location all

|     | Sample Type                                                | Volume | Comments |
|-----|------------------------------------------------------------|--------|----------|
| 1.  |                                                            |        |          |
| 2.  | 855896 <u>5</u> <u>BACE</u> <u>all</u><br>Meth Sample Test |        |          |
| 3.  | 855897 <u>5</u> <u>BFLT</u> <u>all</u><br>Meth Sample Test |        |          |
| 4.  |                                                            |        |          |
| 5.  |                                                            |        |          |
| 6.  |                                                            |        |          |
| 7.  |                                                            |        |          |
| 8.  |                                                            |        |          |
| 9.  |                                                            |        |          |
| 10. |                                                            |        |          |
| 11. |                                                            |        |          |
| 12. |                                                            |        |          |

CHAIN OF CUSTODY

 \_\_\_\_\_  
 \_\_\_\_\_

ANALYTICAL REPORT

SAMPLE TYPE Filterable Particulate

DATE 2/11/85

SAMPLE COMPONENT 100mm filter

ANALYST SK

REQUESTED BY SWPC

ANALYTICAL METHOD Gravimetric

| Sample ID<br>No. | Test<br>No. | Sample<br>Volume | Sample<br>Aliquot | Titer mls<br>or<br>(Absorbance) | Analytical Result<br>(total sample) <u>grams</u> |                 |
|------------------|-------------|------------------|-------------------|---------------------------------|--------------------------------------------------|-----------------|
|                  |             |                  |                   |                                 | Uncorrected                                      | Blank corrected |
| Kiln 2           |             |                  |                   |                                 |                                                  |                 |
| 10-270           | K1          |                  |                   |                                 | -0.00175                                         | 0.00000         |
| 10-299           | K2          |                  |                   |                                 | -0.00020                                         | 0.00000         |
| 10-271           | K3          |                  |                   |                                 | -0.00149                                         | 0.00000         |
| Clinker          |             |                  |                   |                                 |                                                  |                 |
| 10-295           | C1          |                  |                   |                                 | 0.07411                                          | 0.07416         |
| 10-293           | C2          |                  |                   |                                 | 0.05082                                          | 0.05087         |
| 10-297           | C3          |                  |                   |                                 | 0.05354                                          | 0.05359         |
| Raw Mill         |             |                  |                   |                                 |                                                  |                 |
| *2               |             |                  |                   |                                 |                                                  |                 |
| 10-292           | Rm1         |                  |                   |                                 | 0.00362                                          | 0.00367         |
| 10-294           | Rm2         |                  |                   |                                 | 0.00342                                          | 0.00347         |
| 10-296           | Rm3         |                  |                   |                                 | 0.00414                                          | 0.00419         |
| Finish Mill      |             |                  |                   |                                 |                                                  |                 |
| *12              |             |                  |                   |                                 |                                                  |                 |
| 10-298           | Fm1         |                  |                   |                                 | 0.00003                                          | 0.00008         |
| 10-272           | Fm2         |                  |                   |                                 | -0.00017                                         | 0.00000         |
| 10-300           | Fm3         |                  |                   |                                 | 0.00012                                          | 0.00017         |
| 10-269           | Blk.        |                  |                   |                                 | -0.00005                                         |                 |

ANALYTICAL REPORT

SAMPLE TYPE Front Half Wash

DATE 2/11/85

SAMPLE COMPONENT Acetone

ANALYST SK

REQUESTED BY SLPC

ANALYTICAL METHOD Gravimetric

| Sample ID No.   | Test No. | Sample Volume | Sample Aliquot | Titer mls or (Absorbance) | Analytical Result (total sample) grams |                 |
|-----------------|----------|---------------|----------------|---------------------------|----------------------------------------|-----------------|
|                 |          |               |                |                           | Uncorrected                            | Blank corrected |
| Kiln 2          | K1       | 227           | 227            |                           | 0.01342                                | 0.01233         |
|                 | K2       | 225           | 225            |                           | 0.00838                                | 0.00720         |
|                 | K3       | 178           | 178            |                           | 0.01055                                | 0.00970         |
| Clinker         | C1       | 218           | 218            |                           | 0.16643                                | 0.16538         |
|                 | C2       | 210           | 210            |                           | 0.02534                                | 0.02433         |
|                 | C3       | 189           | 189            |                           | 0.00952                                | 0.00861         |
| Raw Mill #2     | Rm1      | 249           | 249            |                           | 0.01665                                | 0.01545         |
|                 | Rm2      | 137           | 137            |                           | 0.01767                                | 0.01701         |
|                 | Rm3      | 202           | 202            |                           | 0.01857                                | 0.01760         |
| Finish Mill #12 | Fm1      | 255           | 255            |                           | 0.02996                                | 0.02874         |
|                 | Fm2      | 199           | 199            |                           | 0.02478                                | 0.02382         |
|                 | Fm3      | 149           | 149            |                           | 0.00688                                | 0.00616         |
|                 | Blk.     | 100           | 100            |                           | 0.00048                                |                 |

# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 1 Date 2/6/85 Location Kiln #2 Stack

|                                 |                        |                     |                                 |
|---------------------------------|------------------------|---------------------|---------------------------------|
| $T_m$ <u>74.04</u>              | $V_m$ <u>85.657</u>    | $O_2$ <u>9.17</u>   | Stack ID " <u>160</u>           |
| $T_s$ <u>381.08</u>             | $\delta$ <u>1.0098</u> | $CO_2$ <u>18.70</u> | Stack Area $Ft^2$ <u>139.63</u> |
| $\sqrt{\Delta P}$ <u>0.4927</u> | $P_b$ <u>26.46</u>     | Static <u>-0.33</u> | Test Time <u>180</u>            |
| $\Delta H$ <u>1.74</u>          | $V_{1c}$ <u>77.5</u>   | $C_p$ <u>0.84</u>   | $N_d$ <u>0.3207</u>             |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m, std} = \left( \frac{S_t + 460}{29.92} \right) (\delta) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 75.9941$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

$$(V_{m, std} + V_{w, std}; R-04) \quad V_{w, std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{1c}) = 3.6479$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w, std}}{V_{w, std} + V_{m, std}} = 0.0458$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 31.36$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d (1 - B_{wo}) + 18(B_{wo}) = 30.75$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 26.44$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 35.99$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

301453.93

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 159580.76$$

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w, std} + V_{m, std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 98.86$$

# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 2 Date 2/6/85 Location Kiln #2

|                                 |                        |                     |                                 |
|---------------------------------|------------------------|---------------------|---------------------------------|
| $T_m$ <u>74.67</u>              | $V_m$ <u>81.805</u>    | $O_2$ <u>9.30</u>   | Stack ID " <u>160</u>           |
| $T_s$ <u>362.75</u>             | $\gamma$ <u>1.0098</u> | $CO_2$ <u>18.69</u> | Stack Area $Ft^2$ <u>139.63</u> |
| $\sqrt{\Delta P}$ <u>0.4647</u> | $P_b$ <u>26.43</u>     | Static <u>-0.18</u> | Test Time <u>120</u>            |
| $\Delta H$ <u>1.57</u>          | $V_{lc}$ <u>73.9</u>   | $C_p$ <u>0.84</u>   | $N_d$ <u>0.3207</u>             |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m,std} = \left( \frac{S_t + 460}{29.92} \right) (\gamma) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 72.3753$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

$$(V_{m,std} + V_{w,std}; R-04) \quad V_{w,std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{lc}) = 3.4785$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w,std}}{V_{w,std} + V_{m,std}} = 0.0459$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 31.38$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d (1 - B_{wo}) + 18(B_{wo}) = 30.76$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 26.42$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 33.58$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 152409.33$$

281368.64

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w,std} + V_{m,std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 98.79$$

# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 1 Date 2/6/85 Location Clinker GBF

|                                 |                        |                     |                                |
|---------------------------------|------------------------|---------------------|--------------------------------|
| $T_m$ <u>74.40</u>              | $V_m$ <u>52.698</u>    | $O_2$ <u>20.9</u>   | Stack ID " <u>130</u>          |
| $T_s$ <u>358.13</u>             | $\gamma$ <u>0.9993</u> | $CO_2$ <u>0.0</u>   | Stack Area $Ft^2$ <u>92.18</u> |
| $\sqrt{\Delta P}$ <u>0.6379</u> | $P_b$ <u>26.46</u>     | Static <u>-0.48</u> | Test Time <u>72</u>            |
| $\Delta H$ <u>1.57</u>          | $V_{lc}$ <u>3.8</u>    | $C_p$ <u>0.84</u>   | $N_d$ <u>0.2680</u>            |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m,std} = \left( \frac{S_t + 460}{29.92} \right) (\gamma) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 46.2141$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

$$(V_{m,std} + V_{w,std}; R-04) \quad V_{w,std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{lc}) = 0.1789$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w,std}}{V_{w,std} + V_{m,std}} = 0.0039$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 28.84$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d(1 - B_{wo}) + 18(B_{wo}) = 28.79$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 26.42$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 47.50$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 149158.17$$

262703.56

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w,std} + V_{m,std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 101.34$$

# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 3 Date 2/7/85 Location K/n

|                                 |                        |                     |                                 |
|---------------------------------|------------------------|---------------------|---------------------------------|
| $T_m$ <u>74.88</u>              | $V_m$ <u>85.880</u>    | $O_2$ <u>9.10</u>   | Stack ID " <u>160</u>           |
| $T_s$ <u>380.29</u>             | $\theta$ <u>1.0098</u> | $CO_2$ <u>19.04</u> | Stack Area $Ft^2$ <u>139.63</u> |
| $\sqrt{\Delta P}$ <u>0.4935</u> | $P_b$ <u>26.52</u>     | Static <u>-0.33</u> | Test Time <u>120</u>            |
| $\Delta H$ <u>1.74</u>          | $V_{lc}$ <u>78.7</u>   | $C_p$ <u>0.84</u>   | $N_d$ <u>0.3207</u>             |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m,std} = \left( \frac{S_t + 460}{29.92} \right) (\theta) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 76.2440$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

$$(V_{m,std} + V_{w,std}; R-04) \quad V_{w,std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{lc}) = 3.7044$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w,std}}{V_{w,std} + V_{m,std}} = 0.0463$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 31.40$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d(1 - B_{wo}) + 18(B_{wo}) = 30.78$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 26.50$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 35.97$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 159877.81$$

301 330.71

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w,std} + V_{m,std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 98.99$$



# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 2 Date 2/6/85 Location Clinker GBF

|                                 |                        |                     |                                |
|---------------------------------|------------------------|---------------------|--------------------------------|
| $T_m$ <u>76.25</u>              | $V_m$ <u>56.928</u>    | $O_2$ <u>20.9</u>   | Stack ID " <u>130</u>          |
| $T_s$ <u>377.83</u>             | $\delta$ <u>0.9993</u> | $CO_2$ <u>0.0</u>   | Stack Area $Ft^2$ <u>92.18</u> |
| $\sqrt{\Delta P}$ <u>0.6925</u> | $P_b$ <u>26.43</u>     | Static <u>-0.50</u> | Test Time <u>72</u>            |
| $\Delta H$ <u>1.81</u>          | $V_{lc}$ <u>3.8</u>    | $C_p$ <u>0.84</u>   | $N_d$ <u>0.2680</u>            |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m,std} = \left( \frac{S_t + 460}{29.92} \right) (\delta) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 49.7283$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

$$(V_{m,std} + V_{w,std}; R-04) \quad V_{w,std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{lc}) = 0.1789$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w,std}}{V_{w,std} + V_{m,std}} = 0.0036$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 28.84$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d (1 - B_{wo}) + 18(B_{wo}) = 28.80$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 26.39$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 52.21$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

288759.65

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 159950.21$$

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w,std} + V_{m,std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 101.68$$

# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 3 Date 2/8/85 Location Clinker 6BF

|                                 |                        |                     |                                |
|---------------------------------|------------------------|---------------------|--------------------------------|
| $T_m$ <u>74.44</u>              | $V_m$ <u>55.262</u>    | $O_2$ <u>20.9</u>   | Stack ID " <u>130</u>          |
| $T_s$ <u>361.67</u>             | $\gamma$ <u>0.9993</u> | $CO_2$ <u>0.0</u>   | Stack Area $Ft^2$ <u>92.18</u> |
| $\sqrt{\Delta P}$ <u>0.6481</u> | $P_b$ <u>26.43</u>     | Static <u>-0.30</u> | Test Time <u>72</u>            |
| $\Delta H$ <u>1.62</u>          | $V_{lc}$ <u>6.6</u>    | $C_p$ <u>0.84</u>   | $N_d$ <u>0.2680</u>            |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m,std} = \left( \frac{S_t + 460}{29.92} \right) (\gamma) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 48.4111$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

$$(V_{m,std} + V_{w,std}; R-04) \quad V_{w,std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{lc}) = 0.3107$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w,std}}{V_{w,std} + V_{m,std}} = 0.0064$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 28.84$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d(1 - B_{wo}) + 18(B_{wo}) = 28.77$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 26.41$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 48.40$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

267692.89

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 150857.46$$

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w,std} + V_{m,std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 104.96$$

# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 1 Date 2/5/85 Location Finish Mill

|                          |                       |                     |                                |
|--------------------------|-----------------------|---------------------|--------------------------------|
| $T_m$ <u>56</u>          | $V_m$ <u>89.659</u>   | $O_2$ <u>20.9</u>   | Stack ID " <u>60</u>           |
| $T_s$ <u>186</u>         | $\delta$ <u>27.35</u> | $CO_2$ <u>0.0</u>   | Stack Area $Ft^2$ <u>19.63</u> |
| $\Delta P$ <u>0.3330</u> | $P_b$ <u>0.9698</u>   | Static <u>-0.11</u> | Test Time <u>120</u>           |
| $\Delta H$ <u>1.78</u>   | $V_{1c}$ <u>135.4</u> | $C_p$ <u>0.84</u>   | $N_d$ <u>0.3652</u>            |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m, std} = \left( \frac{S_t + 460}{29.92} \right) (\delta) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 81.7199$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

$$(V_{m, std} + V_{w, std}; R-04) \quad V_{w, std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{1c}) = 6.3733$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w, std}}{V_{w, std} + V_{m, std}} = 0.0723$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 28.84$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d (1 - B_{wo}) + 18(B_{wo}) = 28.05$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 27.34$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 21.95$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

25854.70

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 17913.99$$

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w, std} + V_{m, std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 102.69$$

# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 2 Date 2/7/85 Location Finish Mill

|                                 |                        |                      |                                |
|---------------------------------|------------------------|----------------------|--------------------------------|
| $T_m$ <u>78.78</u>              | $V_m$ <u>83.960</u>    | $O_2$ <u>30.9</u>    | Stack ID " <u>60</u>           |
| $T_s$ <u>195.25</u>             | $\delta$ <u>0.9698</u> | $CO_2$ <u>0.0</u>    | Stack Area $Ft^2$ <u>19.63</u> |
| $\sqrt{\Delta P}$ <u>0.3148</u> | $P_b$ <u>27.28</u>     | Static <u>-0.115</u> | Test Time <u>120</u>           |
| $\Delta H$ <u>1.52</u>          | $V_{lc}$ <u>156.8</u>  | $C_p$ <u>0.84</u>    | $N_d$ <u>0.3652</u>            |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m,std} = \left( \frac{S_t + 460}{29.92} \right) (\delta) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 73.0523$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

$$(V_{m,std} + V_{w,std}; R-04) \quad V_{w,std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{lc}) = 7.3806$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w,std}}{V_{w,std} + V_{m,std}} = 0.0918$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 28.84$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d (1 - B_{wo}) + 18(B_{wo}) = 27.84$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 27.27$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 21.00$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

24740.67

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 16503.85$$

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w,std} + V_{m,std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 99.65$$

# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 3 Date 2/8/85 Location Finish Mill

|                                 |                        |                     |                                |
|---------------------------------|------------------------|---------------------|--------------------------------|
| $T_m$ <u>61.47</u>              | $V_m$ <u>84.695</u>    | $O_2$ <u>20.9</u>   | Stack ID " <u>60</u>           |
| $T_s$ <u>185.81</u>             | $\delta$ <u>0.9698</u> | $CO_2$ <u>0.0</u>   | Stack Area $Ft^2$ <u>19.63</u> |
| $\sqrt{\Delta P}$ <u>0.3193</u> | $P_b$ <u>27.18</u>     | Static <u>-0.11</u> | Test Time <u>120</u>           |
| $\Delta H$ <u>1.53</u>          | $V_{lc}$ <u>140.5</u>  | $C_p$ <u>0.84</u>   | $N_d$ <u>0.3652</u>            |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m,std} = \left( \frac{S_t + 460}{29.92} \right) (\delta) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 75.8621$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

$$(V_{m,std} + V_{w,std}; R-04) \quad V_{w,std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{lc}) = 6.6133$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w,std}}{V_{w,std} + V_{m,std}} = 0.0802$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 28.84$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d(1 - B_{wo}) + 18(B_{wo}) = 27.97$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 27.17$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 21.14$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

24902.51

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 17007.08$$

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w,std} + V_{m,std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 100.42$$

# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 1 Date 2-5-85 Location Row Mill #2

|                                 |                       |                     |                                |
|---------------------------------|-----------------------|---------------------|--------------------------------|
| $T_m$ <u>62.54</u>              | $V_m$ <u>98.406</u>   | $O_2$ <u>20.9</u>   | Stack ID " <u>72</u>           |
| $T_s$ <u>152.42</u>             | $\theta$ <u>29828</u> | $CO_2$ <u>0.0</u>   | Stack Area $Ft^2$ <u>38.27</u> |
| $\sqrt{\Delta P}$ <u>0.7164</u> | $P_b$ <u>26.45</u>    | Static <u>-0.47</u> | Test Time <u>130</u>           |
| $\Delta H$ <u>1.86</u>          | $V_{1c}$ <u>100.0</u> | $C_p$ <u>0.840</u>  | $N_d$ <u>0.2530</u>            |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m, std} = \left( \frac{S_t + 460}{29.92} \right) (\theta) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 86.8368$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

( $V_{m, std} + V_{w, std}$ ; R-04)

$$V_{w, std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{1c}) = 4.7070$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w, std}}{V_{w, std} + V_{m, std}} = 0.0514$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 28.84$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d (1 - B_{wo}) + 18(B_{wo}) = 28.28$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 26.42$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 46.77$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

79,345.90

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 56,826.04$$

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w, std} + V_{m, std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 103.22$$

# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 2 Date 2/7/85 Location Raw Mill

|                                 |                        |                     |                                |
|---------------------------------|------------------------|---------------------|--------------------------------|
| $T_m$ <u>66.83</u>              | $V_m$ <u>99.898</u>    | $O_2$ <u>20.9</u>   | Stack ID " <u>72</u>           |
| $T_s$ <u>171.33</u>             | $\gamma$ <u>0.9828</u> | $CO_2$ <u>0.0</u>   | Stack Area $Ft^2$ <u>26.27</u> |
| $\sqrt{\Delta P}$ <u>0.2442</u> | $P_b$ <u>26.52</u>     | Static <u>-0.35</u> | Test Time <u>120</u>           |
| $\Delta H$ <u>1.93</u>          | $V_{1c}$ <u>86.8</u>   | $C_p$ <u>0.84</u>   | $N_d$ <u>0.2530</u>            |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m,std} = \left( \frac{S_t + 460}{29.92} \right) (\gamma) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 87.6826$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

$$(V_{m,std} + V_{w,std}; R-04) \quad V_{w,std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{1c}) = 4.0857$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w,std}}{V_{w,std} + V_{m,std}} = 0.0445$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 28.84$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d(1 - B_{wo}) + 18(B_{wo}) = 28.35$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 26.49$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 49.03$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

83170.26

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 58851.19$$

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w,std} + V_{m,std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 100.64$$

# ISOKINETIC CALCULATIONS

Standard temperature,  $S_t$  68 (XEQ 60 or 68); 29.92 inches Hg

Test 3 Date 2/7/85 Location Raw Mill

|                                 |                        |                     |                                |
|---------------------------------|------------------------|---------------------|--------------------------------|
| $T_m$ <u>76.12</u>              | $V_m$ <u>106.869</u>   | $O_2$ <u>20.9</u>   | Stack ID " <u>72</u>           |
| $T_s$ <u>169.62</u>             | $\delta$ <u>0.9828</u> | $CO_2$ <u>0.0</u>   | Stack Area $Ft^2$ <u>28.27</u> |
| $\sqrt{\Delta P}$ <u>0.7839</u> | $P_b$ <u>26.52</u>     | Static <u>-0.35</u> | Test Time <u>120</u>           |
| $\Delta H$ <u>2.16</u>          | $V_{lc}$ <u>100.8</u>  | $C_p$ <u>0.84</u>   | $N_d$ <u>0.2530</u>            |

1. Volume of dry gas sampled at standard conditions (dscf)

(R-17)

$$V_{m,std} = \left( \frac{S_t + 460}{29.92} \right) (\delta) V_m \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right) = 92.2257$$

2. Stack gas moisture condensed at standard conditions (scf)

(R-18)

$$(V_{m,std} + V_{w,std}; R-04) \quad V_{w,std} = 8.9148 \times 10^{-5} (S_t + 460) (V_{lc}) = 4.7447$$

3. Stack gas proportion of water vapor, by volume

(R-19)

$$B_{wo} = \frac{V_{w,std}}{V_{w,std} + V_{m,std}} = 0.0489$$

4. Stack gas dry molecular weight (lb/lb mole)

(R-21)

$$MW_d = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28(\%N_2 + \%CO) = 28.84$$

5. Stack gas molecular weight (lb/lb mole)

(R-22)

$$MW_s = MW_d (1 - B_{wo}) + 18(B_{wo}) = 28.31$$

6. Pressure stack, in. Hg

(R-23)

$$P_s = P_b + \left( \frac{P_{static}}{13.6} \right) = 26.49$$

7. Stack gas velocity, at stack conditions (ft/sec)

(R-24)

$$V_s = 85.49(C_p)(\sqrt{\Delta P})_{avg} \sqrt{\frac{T_s + 460}{P_s(MW_s)}} = 51.58$$

8. Stack gas volume at standard conditions (dscfm)

(R-26)

(ACFM; R-25)

$$Q_s = 60(1 - B_{wo}) V_s A_s \left( \frac{S_t + 460}{T_s + 460} \right) \left( \frac{P_s}{29.92} \right) = 61796.58$$

87506.78

9. Test percent isokinetic

(R-02)

$$\%I = \frac{9142.88(T_s + 460)(V_{w,std} + V_{m,std})}{(S_t + 460) \theta V_s P_s (D_n)^2} = 100.80$$



TEST 1, 2, 3

LOCATION Kim

EMISSION RATE DATA -- 68°F

Standard Temperature,  $S_t = 68^\circ\text{F}$ ; 29.92 inches Hg

XEQ FF

XEQ RAT

ENTER: R-17  $V_{m, \text{std}}$

R-26  $Q_s$

R-22  $O_2\%$

| Test 1           | Test 2           | Test 3           | Average          |
|------------------|------------------|------------------|------------------|
| <u>75.9941</u>   | <u>72.3753</u>   | <u>76.2440</u>   |                  |
| <u>159580.76</u> | <u>152109.33</u> | <u>159897.81</u> | <u>157195.97</u> |
| <u>9.17</u>      | <u>9.30</u>      | <u>9.10</u>      | <u>9.19</u>      |

# LAB DATA

|                                    |                |                |                |  |
|------------------------------------|----------------|----------------|----------------|--|
| Front Half Wash (g)                | <u>0.01233</u> | <u>0.00720</u> | <u>0.00970</u> |  |
| Mass Filter (g)                    | <u>0.00000</u> | <u>0.00000</u> | <u>0.00000</u> |  |
| Back Half Catch (g)                |                |                |                |  |
| Front Half Sulfate (mg $H_2SO_4$ ) |                |                |                |  |
| Back Half Sulfate (mg $H_2SO_4$ )  |                |                |                |  |
| $H_2O_2$ Catch (mg $H_2SO_4$ )     |                |                |                |  |

# RESULTS

|                           |    |               |               |               |               |
|---------------------------|----|---------------|---------------|---------------|---------------|
| F Factor                  | 1  |               |               |               |               |
| Filt. Particulate gr/dscf | 6  | <u>0.0025</u> | <u>0.0015</u> | <u>0.0020</u> | <u>0.0020</u> |
| Filt. Particulate lb/hr   | 7  | <u>3.42</u>   | <u>2.00</u>   | <u>2.69</u>   | <u>2.70</u>   |
| Total Particulate gr/dscf | 8  |               |               |               |               |
| Total Particulate lb/hr   | 10 |               |               |               |               |
| Total Sulfate gr/dscf     | 11 |               |               |               |               |
| Total Sulfate lb/hr       | 13 |               |               |               |               |
| $SO_3$ ppm                | 14 |               |               |               |               |
| $SO_3$ lb/hr              | 15 |               |               |               |               |
| $SO_2$ ppm                | 16 |               |               |               |               |
| $SO_2$ lb/hr              | 17 |               |               |               |               |
| $SO_2$ @ 3% $O_2$         | 18 |               |               |               |               |
| $SO_2$ lb/MMBtu           |    |               |               |               |               |
| S lb/MMBtu                |    |               |               |               |               |

EMISSION RATE DATA -- 68°F

Standard Temperature,  $S_t = 68^\circ\text{F}$ ; 29.92 inches Hg

XEQ FF

XEQ RAT

ENTER: R-17  $V_{m, \text{std}}$

R-26  $Q_s$

R-22  $O_2\%$

| Test 1           | Test 2           | Test 3           | Average          |
|------------------|------------------|------------------|------------------|
| <u>46.2141</u>   | <u>49.7283</u>   | <u>48.4111</u>   |                  |
| <u>149158.17</u> | <u>159950.21</u> | <u>150857.46</u> | <u>153321.95</u> |
| <u>20.9</u>      | <u>20.9</u>      | <u>20.9</u>      |                  |

LAB DATA

|                                    |                |                |                |  |
|------------------------------------|----------------|----------------|----------------|--|
| Front Half Wash (g)                | <u>0.16538</u> | <u>0.02433</u> | <u>0.00861</u> |  |
| Mass Filter (g)                    | <u>0.07416</u> | <u>0.05087</u> | <u>0.05359</u> |  |
| Back Half Catch (g)                |                |                |                |  |
| Front Half Sulfate (mg $H_2SO_4$ ) |                |                |                |  |
| Back Half Sulfate (mg $H_2SO_4$ )  |                |                |                |  |
| $H_2O_2$ Catch (mg $H_2SO_4$ )     |                |                |                |  |

RESULTS

|                                     |    |               |               |               |               |
|-------------------------------------|----|---------------|---------------|---------------|---------------|
| F Factor                            | 1  |               |               |               |               |
| Filt. Particulate gr/dscf           | 6  | <u>0.0800</u> | <u>0.0233</u> | <u>0.0198</u> | <u>0.0410</u> |
| Filt. Particulate lb/hr             | 7  | <u>102.25</u> | <u>31.99</u>  | <u>25.63</u>  | <u>53.29</u>  |
| Total Particulate gr/dscf           | 8  |               |               |               |               |
| Total Particulate lb/hr             | 10 |               |               |               |               |
| Total Sulfate gr/dscf               | 11 |               |               |               |               |
| Total Sulfate lb/hr                 | 13 |               |               |               |               |
| SO <sub>3</sub> ppm                 | 14 |               |               |               |               |
| SO <sub>3</sub> lb/hr               | 15 |               |               |               |               |
| SO <sub>2</sub> ppm                 | 16 |               |               |               |               |
| SO <sub>2</sub> lb/hr               | 17 |               |               |               |               |
| SO <sub>2</sub> @ 3% O <sub>2</sub> | 18 |               |               |               |               |
| SO <sub>2</sub> lb/MMBtu            |    |               |               |               |               |
| S lb/MMBtu                          |    |               |               |               |               |

TEST 1, 2, 3

LOCATION Finish Mill

EMISSION RATE DATA -- 68°F

Standard Temperature,  $S_t = 68^\circ\text{F}$ ; 29.92 inches Hg

| XEQ FF                          |                 |                 |                 |                 |
|---------------------------------|-----------------|-----------------|-----------------|-----------------|
| XEQ RAT                         |                 |                 |                 |                 |
| ENTER: R-17 $V_{m, \text{std}}$ | Test 1          | Test 2          | Test 3          | Average         |
| R-26 $Q_s$                      | <u>81.7199</u>  | <u>73.0523</u>  | <u>75.8621</u>  |                 |
| R-22 $O_2\%$                    | <u>17913.99</u> | <u>16503.85</u> | <u>17007.08</u> | <u>17141.64</u> |
|                                 | <u>20.9</u>     | <u>20.9</u>     | <u>20.9</u>     |                 |

LAB DATA

|                                    |                |                |                |  |
|------------------------------------|----------------|----------------|----------------|--|
| Front Half Wash (g)                | <u>0.02874</u> | <u>0.02382</u> | <u>0.00616</u> |  |
| Mass Filter (g)                    | <u>0.00008</u> | <u>0.00000</u> | <u>0.00017</u> |  |
| Back Half Catch (g)                |                |                |                |  |
| Front Half Sulfate (mg $H_2SO_4$ ) |                |                |                |  |
| Back Half Sulfate (mg $H_2SO_4$ )  |                |                |                |  |
| $H_2O_2$ Catch (mg $H_2SO_4$ )     |                |                |                |  |

RESULTS

|                           |    |               |               |               |               |
|---------------------------|----|---------------|---------------|---------------|---------------|
| F Factor                  | 1  |               |               |               |               |
| Filt. Particulate gr/dscf | 6  | <u>0.0054</u> | <u>0.0050</u> | <u>0.0013</u> | <u>0.0039</u> |
| Filt. Particulate lb/hr   | 7  | <u>0.84</u>   | <u>0.71</u>   | <u>0.19</u>   | <u>0.58</u>   |
| Total Particulate gr/dscf | 8  |               |               |               |               |
| Total Particulate lb/hr   | 10 |               |               |               |               |
| Total Sulfate gr/dscf     | 11 |               |               |               |               |
| Total Sulfate lb/hr       | 13 |               |               |               |               |
| $SO_3$ ppm                | 14 |               |               |               |               |
| $SO_3$ lb/hr              | 15 |               |               |               |               |
| $SO_2$ ppm                | 16 |               |               |               |               |
| $SO_2$ lb/hr              | 17 |               |               |               |               |
| $SO_2$ @ 3% $O_2$         | 18 |               |               |               |               |
| $SO_2$ lb/MMBtu           |    |               |               |               |               |
| S lb/MMBtu                |    |               |               |               |               |

CM SO<sub>2</sub>, NO<sub>x</sub>, HC, CO EMISSION RATE DATA 3/6/85

Standard Temperature, St 68 (XEQ 60 or 68); 29.92 inches Hg

7:45-10:20 10:35-1:10 2:35-5:15 \*

| ENTER                                                | Test 1            | Test 2            | Test 3            | Average |
|------------------------------------------------------|-------------------|-------------------|-------------------|---------|
| R-22 O <sub>2</sub> %                                | <u>9.36</u>       | <u>9.12</u>       | <u>9.52</u>       |         |
| R-26 Q <sub>s</sub>                                  | <u>159 580.76</u> | <u>159 580.76</u> | <u>152 109.33</u> |         |
| R-15 NO <sub>x</sub> ppm                             | <u>486.67</u>     | <u>548.89</u>     | <u>498.33</u>     |         |
| R-15 SO <sub>2</sub> ppm                             | <u>4.00</u>       | <u>2.00</u>       | <u>3.00</u>       |         |
| R-15 CO ppm                                          | <u>306.11</u>     | <u>210.00</u>     | <u>157.92</u>     |         |
| <u>C<sub>1</sub>, &gt; C<sub>1</sub></u> R-15 HC ppm |                   | <u>2.56/49.1</u>  | <u>3.16/23.51</u> |         |

XEQ FF

XEQ SO<sub>2</sub>

F Factor

N-14  
O<sub>2</sub>-32  
46

RESULTS:

MW = 46

|                                         |               |               |               |                |
|-----------------------------------------|---------------|---------------|---------------|----------------|
| NO <sub>x</sub> 1b/hr                   | <u>556.50</u> | <u>627.65</u> | <u>543.16</u> | <u>575.5 -</u> |
| NO <sub>x</sub> ppm @ 3% O <sub>2</sub> | <u>754.89</u> | <u>834.29</u> | <u>783.55</u> | <u>791</u>     |
| NO <sub>x</sub> 1b/MMBtu                |               |               |               |                |
| NO <sub>x</sub> 1b/Bbl                  |               |               |               |                |

See next page for Average  
SF = 7.45%

MW = 64.1

|                                         |             |             |             |  |
|-----------------------------------------|-------------|-------------|-------------|--|
| SO <sub>2</sub> 1b/hr                   | <u>6.37</u> | <u>3.19</u> | <u>4.56</u> |  |
| SO <sub>2</sub> ppm @ 3% O <sub>2</sub> | <u>6.20</u> | <u>3.04</u> | <u>4.72</u> |  |
| SO <sub>2</sub> 1b/MMBtu                |             |             |             |  |
| SO <sub>2</sub> 1b/Bbl                  |             |             |             |  |

MW = 28

|                            |               |               |               |  |
|----------------------------|---------------|---------------|---------------|--|
| CO 1b/hr                   | <u>213.02</u> | <u>146.14</u> | <u>104.75</u> |  |
| CO ppm @ 3% O <sub>2</sub> | <u>474.82</u> | <u>319.19</u> | <u>248.31</u> |  |
| CO 1b/MMBtu                |               |               |               |  |
| CO 1b/Bbl                  |               |               |               |  |

MW = 16

|                            |  |                   |                   |  |
|----------------------------|--|-------------------|-------------------|--|
| HC 1b/hr                   |  | <u>1.02/19.52</u> | <u>1.20/8.91</u>  |  |
| HC ppm @ 3% O <sub>2</sub> |  | <u>3.89/74.63</u> | <u>4.97/36.97</u> |  |
| HC 1b/MMBtu                |  |                   |                   |  |
| HC 1b/Bbl                  |  |                   |                   |  |

\* 190 TPH

CM SO<sub>2</sub>, NO<sub>x</sub>, HC, CO EMISSION RATE DATA 2/7/85Standard Temperature, S<sub>t</sub> 68 (XEQ 60 or 68); 29.92 inches Hg

| ENTER |                     | 7:40 - 12:00      | 12:30 - 4:30     | Test 3 | Average |
|-------|---------------------|-------------------|------------------|--------|---------|
|       |                     | Test 1            | Test 2           |        |         |
| R-22  | O <sub>2</sub> %    | <u>9.12</u>       | <u>8.71</u>      |        |         |
| R-26  | Q <sub>s</sub>      | <u>159897.81</u>  | <u>159897.81</u> |        |         |
| R-15  | NO <sub>x</sub> ppm | <u>480.71</u>     | <u>454.62</u>    |        |         |
| R-15  | SO <sub>2</sub> ppm | <u>4.08</u>       | <u>3.38</u>      |        |         |
| R-15  | CO ppm              | <u>305.77</u>     | <u>273.08</u>    |        |         |
| R-15  | HC ppm              | <u>7.61/15.37</u> |                  |        |         |

XEQ FF

XEQ SO<sub>2</sub>

F Factor \_\_\_\_\_

## RESULTS:

MW = 46

|                 |                         |               |               | Avg 74.2<br>ppm | Avg 75<br>ppm          |
|-----------------|-------------------------|---------------|---------------|-----------------|------------------------|
| NO <sub>x</sub> | lb/hr                   | <u>550.78</u> | <u>520.89</u> | <u>535.8</u>    | <u>559.8</u>           |
| NO <sub>x</sub> | ppm @ 3% O <sub>2</sub> | <u>730.45</u> | <u>667.57</u> | <u>699</u>      | <u>754 ppm</u><br>@ 3% |
| NO <sub>x</sub> | lb/MMBtu                |               |               |                 |                        |
| NO <sub>x</sub> | lb/Bbl                  |               |               |                 |                        |

MW = 64.1

|                 |                         |             |             |  |  |
|-----------------|-------------------------|-------------|-------------|--|--|
| SO <sub>2</sub> | lb/hr                   | <u>6.51</u> | <u>5.40</u> |  |  |
| SO <sub>2</sub> | ppm @ 3% O <sub>2</sub> | <u>6.20</u> | <u>4.96</u> |  |  |
| SO <sub>2</sub> | lb/MMBtu                |             |             |  |  |
| SO <sub>2</sub> | lb/Bbl                  |             |             |  |  |

MW = 28

|    |                         |               |               |  |  |
|----|-------------------------|---------------|---------------|--|--|
| CO | lb/hr                   | <u>213.20</u> | <u>190.41</u> |  |  |
| CO | ppm @ 3% O <sub>2</sub> | <u>464.63</u> | <u>401.00</u> |  |  |
| CO | lb/MMBtu                |               |               |  |  |
| CO | lb/Bbl                  |               |               |  |  |

MW = 16

|    |                         |                    |  |  |  |
|----|-------------------------|--------------------|--|--|--|
| HC | lb/hr                   | <u>3.03/6.12</u>   |  |  |  |
| HC | ppm @ 3% O <sub>2</sub> | <u>11.56/23.36</u> |  |  |  |
| HC | lb/MMBtu                |                    |  |  |  |
| HC | lb/Bbl                  |                    |  |  |  |

CM SO<sub>2</sub>, NO<sub>x</sub>, HC, CO EMISSION RATE DATA2/8/85Standard Temperature, S<sub>t</sub> 68 (XEQ 60 or 68); 29.92 inches Hg7:30 am - 12:00 pm

| ENTER                    | Test 1        | Test 2 | Test 3 | Average |
|--------------------------|---------------|--------|--------|---------|
| R-22 O <sub>2</sub> %    | <u>8.96</u>   |        |        |         |
| R-26 Q <sub>s</sub>      |               |        |        |         |
| R-15 NO <sub>x</sub> ppm | <u>358.00</u> |        |        |         |
| R-15 SO <sub>2</sub> ppm | <u>2.10</u>   |        |        |         |
| R-15 CO ppm              | <u>575.00</u> |        |        |         |
| R-15 HC ppm              |               |        |        |         |

XEQ FF

XEQ SO<sub>2</sub>

F Factor

## RESULTS:

MW = 46

NO<sub>x</sub> lb/hrNO<sub>x</sub> ppm @ 3% O<sub>2</sub>NO<sub>x</sub> lb/MMBtuNO<sub>x</sub> lb/Bbl

MW = 64.1

SO<sub>2</sub> lb/hrSO<sub>2</sub> ppm @ 3% O<sub>2</sub>SO<sub>2</sub> lb/MMBtuSO<sub>2</sub> lb/Bbl

MW = 28

CO lb/hr

CO ppm @ 3% O<sub>2</sub>

CO lb/MMBtu

CO lb/Bbl

MW = 16

HC lb/hr

HC ppm @ 3% O<sub>2</sub>

HC lb/MMBtu

HC lb/Bbl

Avg of 6 runs  
718