

Note: This is a reference cited in AP 42, *Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at www.epa.gov/ttn/chief/ap42/

The file name refers to the reference number, the AP42 chapter and section. The file name "ref02_c01s02.pdf" would mean the reference is from AP42 chapter 1 section 2. The reference may be from a previous version of the section and no longer cited. The primary source should always be checked.

AP42 Section:	11.7
Reference:	9
Title:	Metropolitan Ceramics, Canton, Ohio, Tunnel Kiln #3 Exhaust Stack, Particulate, SO ₂ , NO _x , Hydrofluoric Acid Emission Evaluation, Conducted - November 17-18, 1993, Envisage Environmental Incorporated, Richfield, OH, December 16, 1993.

Envisage Environmental Incorporated

P.O. Box 152, Richfield, Ohio 44286

Phone (216) 526-0990

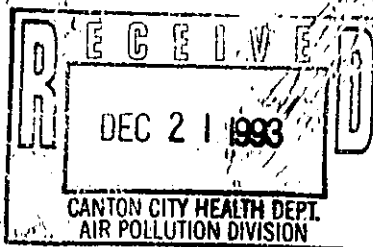
REPORT NO. 93

COMPANY Met

TITLE Comp

DATE 11-17/18-93

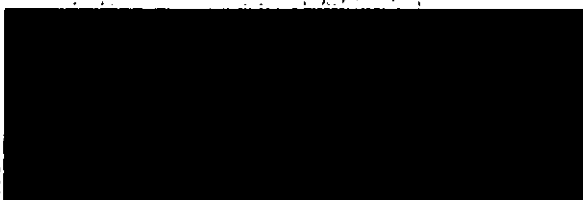
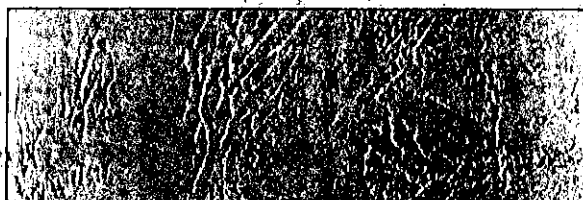
AP-42 Section	<u>11.7</u>
Reference	<u>9</u>
Report Sect.	<u>4</u>
Reference	<u>5</u>



METROPOLITAN CERAMICS
CANTON, OHIO

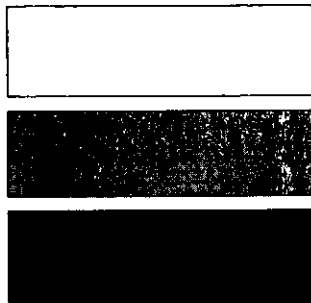
TUNNEL KILN #3 EXHAUST STACK
PARTICULATE, SO₂, NO_x, HYDROFLUORIC ACID
EMISSION EVALUATION

CONDUCTED - NOVEMBER 17-18, 1993



SOURCE EVALUATION RESULTS

PREPARED BY



**Envisage
Environmental
Incorporated**

P.O. Box 152 Richfield, Ohio 44286
Phone (216) 526-0990

Envisage Environmental Incorporated




December 16, 1993

Mr. Philip McGuinness
Metropolitan Ceramics Inc.
1201 Millerton Road S.E.
Canton, Ohio 44707

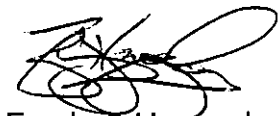
Dear Mr. McGuinness:

The following report is the result of the particulate, hydrofluoric acid, nitrogen oxides, and sulfur dioxide emission evaluation conducted on November 17 & 18, 1993 at the Metropolitan Ceramics Inc., Canton, Ohio. Testing was performed at the exhaust stack serving the # 3 Tunnel Kiln.

The results are true and accurate to the degree specified in the pertinent sections of the Code of Federal Regulations, in force at the time of testing concerning source sampling for the above compounds.

I am looking forward to answering any questions you may have and assisting you in the future.

Respectfully submitted,



Frank J. Hezoucky
Manager, Source Sampling
ENVISAGE ENVIRONMENTAL INC.

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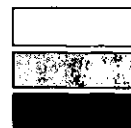
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INTRODUCTION



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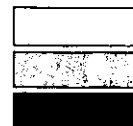
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Phone (216) 526-0890

INTRODUCTION

On November 17 & 18, 1993 Envisage Environmental Inc. conducted a particulate, hydrofluoric acid, nitrogen oxides, and sulfur dioxide emission evaluation at the Metropolitan Ceramics Inc., Canton, Ohio. The testing was performed at the exhaust stack serving the # 3 Tunnel Kiln. The operation of the kiln and systems involved were monitored throughout the duration of the testing by Metropolitan Ceramics Inc. personnel.

The purpose of the evaluation was to determine the emission rates from the unit to verify compliance with the applicable emission limitations set forth by the Ohio EPA. The Envisage testing team consisted of Messrs. Gregory Sinkovich, James Gray, Eric Hevener, Jamie Kingsborough, David Donelson, and Terry Campbell. Mr. Philip McGuinness, Metropolitan Ceramics, coordinated the testing. The Ohio EPA was also present during the testing and was represented by Mr. Rick Miller.

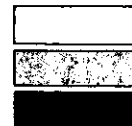
Results are presented in this report for pounds per hour and grains per dry standard cubic foot of emitted particulate, hydrofluoric acid, nitrogen oxides, sulfur dioxide, as well as the various velocity, volumetric and temperature measurements associated with these tests.



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DESCRIPTION OF PROGRAM



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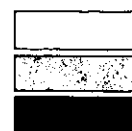
DESCRIPTION OF PROGRAM

The testing was conducted at the exhaust stack serving the # 3 Tunnel Kiln. The emission test consisted of three (3) test runs of USEPA Methods 1 - 5, 6C, 7E, and 13. Each of the tests were performed over a sixty (60) minute period. Test methods 1-2, 6C and 7E were performed on November 17, 1993, and test methods 1-5, and 13 were performed on November 18, 1993.

Particulate and hydrofluoric acid sampling, consisted of twelve (12) sample/traverse points being utilized in each of the two (2) ports for a total of twenty four (24) sample/traverse points. The samples were withdrawn for two and one half (2.5) minutes at each sample/traverse point. Samples were taken from the gas streams isokinetically through a .61 inch nozzle and a five (5) foot Pyrex lined probe. The entire length of the probe was heated and attached to a standard EPA Method 1-5 sample train. The hot box temperature was maintained between 223 and 273 degrees Fahrenheit. Exit gas temperature of the impingers was maintained below 68 degrees Fahrenheit with an ice bath. The nozzle, probe and connecting glassware were cleaned before testing and at the conclusion of each test run. Leak checks of the pitot tube lines and the sample train were all acceptable by EPA regulations.

Testing for sulfur dioxide was performed in accordance with USEPA Method 6C, Determination of Sulfur Dioxide Emissions from Stationary Sources (instrumental analyzer procedure). A single representative sampling point was utilized in the gas stream. Samples were withdrawn at a constant rate through a heated Teflon sample line. Samples were relayed to a Bovar photometric infrared analyzer which performs continuous analysis of sulfur dioxide.

Testing for nitrogen oxides was performed in accordance with USEPA Method 7E, Determination of Nitrogen Oxides Emissions from Stationary Sources. A single representative sampling point was utilized in the gas stream. Samples were withdrawn at a constant rate through a heated Teflon sample line. Samples were relayed to a Meloy Chemiluminizer which performs continuous analysis of total oxides of nitrogen.



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DESCRIPTION OF PROGRAM - continued

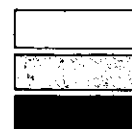
All constant emission monitors were calibrated before and after each sample run with USEPA Protocol I calibration gases.

Flue gas analysis was conducted by drawing an integrated air bag sample and analyzing it on a Hays Republic Model 621A "Orsat" Portable Gas Analyzer. The average of these readings for each run were used in calculating the emission rates.

Calibration of the equipment used, including the dry gas meter, temperature measuring devices, orifice meter, and the "S" type pitot tube was conducted within 60 days of the test date. Copies of the data are included in this report.

All analytical procedures were performed in accordance with the methods specified in the Code of Federal Regulations, Title 40, Part 60, Volume 43. Blanks were collected and analyzed on the distilled water, and acetone used in the evaluation. The residue from the distilled water was less than could be measured on a 0.1 milligram analytical balance and was considered zero. The acetone blank was recorded and incorporated into the results.

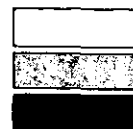
The example equations included in this report uses the figures from Run # 1.



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TEST RESULTS SUMMARY



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TEST RESULTS SUMMARY

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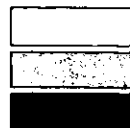
Metropolitan Ceramics

Tunnel Kiln #3 Exhaust Stack

PARAMETER		RUN # 1	RUN # 2	RUN # 3	
Particulate Emissions					X
Pounds/hour	3	0.9018	0.7821	0.8487	0.8442
Grains/dscf		0.0152	0.0132	0.0138	
NOx Emissions					
Pounds/hour	5	3.05	2.59	3.13	2.92
Pounds/dscf		6.18E-06	5.26E-06	6.07E-06	
Sulfur Dioxide Emissions					
Pounds/hour	14.25	2.05	2.05	1.88	1.99
Pounds/dscf		4.16E-06	4.16E-06	3.66E-06	
Hydrofluoric Acid Emissions					
Pounds/hour	2.2	1.92	1.95	2.11	1.99
Grains/dscf		0.0323	0.0328	0.0344	
System Flow Rates					
Feet/second		8.91	8.89	9.11	
ACFM		10,493	10,477	10,734	
DSCFM		6,928	6,916	7,160	
Moisture Content					
Volume percent		6.20	6.61	6.25	
Stack Temperature		262	258	254	

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TEST RESULTS DETAILED



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TEST RESULTS
Metropolitan Ceramics
Tunnel Kiln #3 Exhaust Stack

9

SAMPLE TRAIN # 1					
	Symbol	Units	RUN # 1	RUN # 2	RUN # 3
Time of Day			0927 1013	1046 1150	1222 1327
1 Gas Volume-dry, std.	Vmstd	cu. ft.	43.18	43.39	43.18
2 Condensate Vapor Vol.	Vwstd	cu. ft.	2.85	3.07	2.88
3 Gas Stream Moisture	Bws	vol. dec	0.0620	0.0661	0.0625
4 Mol. Wt-flue gas (dry)	Msd	lb/lb mo.	30.01	30.03	30.01
5 Mol. Wt-flue gas (wet)	Ms	lb/lb mo.	29.27	29.23	29.26
6 Flue Gas Velocity	Vs	ft/sec	8.91	8.89	9.11
7 Flue Gas Volume-Actual	ACFM	cu. ft.	10,493	10,477	10,734
8 Flue Gas Volume-Std.	DSCFM	cu. ft.	6,928	6,916	7,160
9 Particulate Conc.	Cs				
- Probe		gr/dscf	0.0034	0.0026	0.0031
- Filter		gr/dscf	0.0118	0.0106	0.0107
- Hydrogen Fluoride		gr/dscf	0.0323	0.0328	0.0344
- Total Particulate		gr/dscf	0.0152	0.0132	0.0138
10 Emission Rate	E				
- Probe		lb/hr	0.2016	0.1539	0.1908
- Filter		lb/hr	0.7002	0.6282	0.6579
- Hydrogen Fluoride		lb/hr	1.9198	1.9456	2.1098
- Total Particulate		lb/hr	0.9018	0.7821	0.8487
11 Isokinetic Rate	I	%	100.5	101.2	97.2



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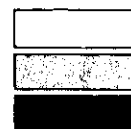
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TEST RESULTS

9A

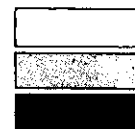
Metropolitan Ceramics
Tunnel Kiln #3 Exhaust Stack

			Constant Monitor Sampling		
	Symbol	Units	RUN # 1	RUN # 2	RUN # 3
Time of Day			0927 1013	1046 1150	1222 1327
1 Gas Stream Moisture	Bws	vol.dec	0.0643	0.0651	0.0491
2 Mol.Wt-flue gas (dry)	Msd	lb/lb mo.	30.01	30.03	30.01
3 Mol.Wt-flue gas (wet)	Ms	lb/lb mo.	29.24	29.24	29.42
4 Flue Gas Velocity	Vs	ft/sec	10.02	10.02	10.22
5 Flue Gas Volume-Actual	ACFM	cu. ft.	11,803	11,805	12,034
6 Flue Gas Volume-Std.	DSCFM	cu. ft.	8,228	8,218	8,577
7 Concentrations.	Cs				
- Nitrogen Oxides		lbs/dscf	6.18E-06	5.26E-06	6.07E-06
- Sulfur Dioxide		lbs/dscf	4.16E-06	4.16E-06	3.66E-06
8 Emission Rate	E				
- Nitrogen Oxides		lb/hr	3.05	2.59	3.13
- Sulfur Dioxide		lb/hr	2.05	2.05	1.88


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SAMPLE POINT LOCATION DIAGRAM



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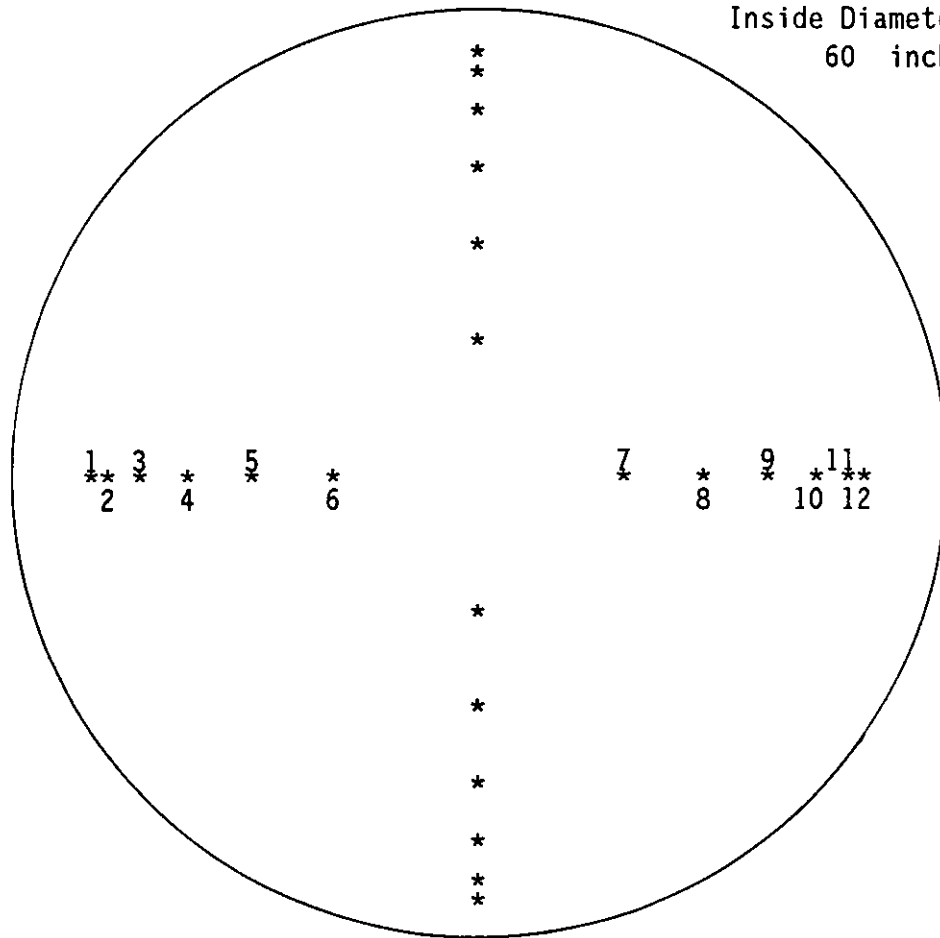
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SAMPLE POINT LOCATIONS

11

Metropolitan Ceramics
Canton, Ohio
3 Tunnel Kiln Exhaust

Inside Diameter =
60 inches



<u>Point #</u>	<u>Distance From</u> <u>Inside Wall</u>	<u>Point #</u>	<u>Distance From</u> <u>Inside Wall</u>
1	58.7 inches	7	21.4 inches
2	56.0 inches	8	15.0 inches
3	52.9 inches	9	10.6 inches
4	49.4 inches	10	7.1 inches
5	45.0 inches	11	4.0 inches
6	38.6 inches	12	1.3 inches



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LABORATORY SECTION



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LABORATORY SUMMARY SHEET

13

Metropolitan Ceramics
Tunnel Kiln #3 Exhaust Stack

SAMPLE TRAIN # 1

	Symbol	Units	RUN # 1	RUN # 2	RUN # 3
1 Sampling Time	t	minutes	60.0	60.0	60.0
2 Barometric Pressure	Pb	in. Hg	28.78	28.78	28.78
3 Static Pressure	Pg	in. H2O	-0.02	-0.02	-0.02
Stack Pressure	Ps	in. Hg	28.78	28.78	28.78
4 Gas Meter Volume	Vm	cu. ft.	45.06	45.83	45.79
5 Stack Area	A	sq. ft.	19.63	19.63	19.63
6 Nozzle Diameter	Dn	dec. in.	0.61	0.61	0.61
7 Meter Temperature		degrees F	72.1	78.6	80.1
	Tm	degrees R	532.1	538.6	540.1
8 Stack Temperature		degrees F	261.5	258.5	253.8
	Ts	degrees R	721.5	718.5	713.8
9 Velocity Head	^P	in. H2O	0.134	0.134	0.138
10 Orifice Pressure	^H	in. H2O	1.55	1.56	1.06
11 Carbon dioxide	CO2	%	8.4	8.5	8.4
12 Oxygen	O2	%	16.5	16.5	16.4
13 Carbon monoxide	CO	%	0.0	0.0	0.0
14 Nitrogen	N2	%	75.1	75.0	75.1
15 Pitot Coefficient	Cp		0.84	0.84	0.84
16 Water Collected	Vlc	ml	60.6	65.2	61.2
Sample Weight:	Mn				
17 - Probe		g	0.0095	0.0073	0.0087
18 - Filter		g	0.0330	0.0298	0.0300
19 - Hydrogen Fluoride		g	0.0905	0.0923	0.0962



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LABORATORY SUMMARY SHEET

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Metropolitan Ceramics
Tunnel Kiln #3 Exhaust Stack

			Constant Monitor Sampling		
	Symbol	Units	RUN # 1	RUN # 2	RUN # 3
1 Sampling Time	t	minutes	60.0	60.0	60.0
2 Barometric Pressure	Pb	in. Hg	28.78	28.78	28.78
3 Static Pressure	Pg	in. H2O	-0.02	-0.02	-0.02
Stack Pressure	Ps	in. Hg	28.78	28.78	28.78
4 Stack Area	A	sq. ft.	19.63	19.63	19.63
5 Stack Temperature		degrees F	221.7	222.0	217.6
	Ts	degrees R	681.7	682.0	677.6
6 Velocity Head	^P	in. H2O	0.155	0.155	0.159
7 Carbon dioxide	CO2	%	8.4	8.5	8.4
8 Oxygen	O2	%	16.5	16.5	16.4
9 Carbon monoxide	CO	%	0.0	0.0	0.0
10 Nitrogen	N2	%	75.1	75.0	75.1
11 Pitot Coefficient	Cp		0.84	0.84	0.84
12 Sample Weight:	Mn				
- Nitrogen Oxides		PPM	51.8	44.0	50.8
- Sulfur Dioxide		PPM	25.0	25.0	22.0



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NSL ANALYTICAL SERVICES, INC.

QUALITY MATERIALS & ENVIRONMENTAL TESTING SINCE 1945

7650 HUB PARKWAY, CLEVELAND, OHIO 44125
PHONE: (216) 447-1550 FAX: (216) 447-0716Envisage Environmental, Inc.
P.O. Box 152
Richfield, OH 33286

Attn: Frank Hezoucky

Date: 15 December 1993
Report#: 12073-33E
Lab#: 17077-17082
PO#:

DEC 15 1993

Client Description: Liquid/Filters J/N 93-2007

<u>Envisage Description</u>	<u>Hydrofluoric Acid (mg/l)</u>
1 250 ml	360.0
2 255 ml	360.0
3 250 ml	360.0

<u>Envisage Description</u>	<u>Hydrofluoric Acid (ug/filter)</u>
1A 1008 NA	480.0
2A 953 NA	480.0
3A 952 NA	1200.0

We certify the above analysis to be the true results based on the designated samples.

Roger Daniels, Environmental Manager

LABORATORY SHEET

COMPANY METRO CERAMICSDATE 11-18-93Part # HF

16

LOCATION H₂O

RUN	1	2	3	
CASE	45	88	64	
WATER				
IMPINGERS				
FINAL	250.00	255.00	250	
INITIAL	200.00	200.00	200.00	
NET	50	55	50	
SILICA GEL				
FINAL	241.9	241.5	242.5	
INITIAL	231.3	231.3	231.3	
NET	10.6	10.2	11.2	
PARTICULATE	16	15	11	
PROBE				
FINAL	128.7167	158.2129	165.7368	
INITIAL	205	110	130 mL	
NET				
FILTER	0008	*953	952	
FINAL	16499	16417	16450	
INITIAL	16169	16119	16150	
NET				
IMPINGERS				
FINAL				
INITIAL				
NET				

ORSAT ANALYSIS WORK SHEET

17

DATE: 18 Nov 93

LOCATION: Metro Ceramics

OPERATOR: D. Donelson

RUN # 1

	1		2		3		
	ACTUAL	NET	ACTUAL	NET	ACTUAL	NET	AVERAGE
CO ₂	8.4	8.4	8.4	8.4	8.5	8.5	
O ₂	24.9	16.5	24.9	16.5	25.0	16.5	
CO	24.9	0	24.9	0	25.0	0	

RUN # 2

	1		2		3		
	ACTUAL	NET	ACTUAL	NET	ACTUAL	NET	AVERAGE
CO ₂	8.6	8.6	8.5	8.5	8.5	8.5	
O ₂	25.1	16.5	25.0	16.5	25.0	16.5	
CO	25.1	0	25.0	0	25.0	0	

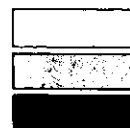
RUN # 3

	1		2		3		
	ACTUAL	NET	ACTUAL	NET	ACTUAL	NET	AVERAGE
CO ₂	8.4	8.4	8.5	8.5	8.4	8.4	
O ₂	24.8	16.4	24.9	16.4	24.9	16.5	
CO	24.8	0	24.9	0	24.9	0	

COMMENTS: _____



EMISSION SAMPLING EQUIPMENT SPECIFICATIONS



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Equipment and Specifications
U.S.E.P.A. Reference methods 1-5

Control Unit (Meter Box)

Equipment Designation

Envisage Environmental Inc.
☒ Anderson Samplers
Remanufactured R.A.C.

Control Unit #'s MB- 08 & 09
Control Unit #'s MB- 01 - 02
Control Unit #'s MB- 03 - 07

Sample Box

☒ E.E.I.
Remanufactured R.A.C.
E.E.I. Special Design

SB- 01, 02 & 05 - 07
SB- 03 & 04
SB- 08 - 11

Impingers - per sample train (each set changed for each test run)

☒ E.E.I.
☒ E.E.I.

3 Modified Smith Greenburg type
1 Smith Greenburg type

Probes

Length

Lining types

☒ E.E.I.	3 foot	SS, PYREX, QUARTZ, TEFLON
☒ E.E.I.	5 foot	SS, PYREX, QUARTZ, TEFLON
☒ E.E.I.	3 foot	SS, PYREX, TEFLON
☒ E.E.I.	7 foot	SS, PYREX, TEFLON
☒ E.E.I.	10 foot	SS, PYREX, TEFLON
☒ E.E.I.	12 foot	SS, PYREX, TEFLON
☒ E.E.I.	15 foot	SS, PYREX, TEFLON
☒ E.E.I.	24 foot	SS, TEFLON

Temperature Sensors

Equipment Designation

Omega Engineering
Thermo Electric
☒ Fluke 51
Fisher Scientific
Fisher Scientific

PY- 01 & 02
PY- 03 - 08
PY- 01 - 02 - 03 - 04 - 05
Mercury Thermometer
Bimetallic Thermometer

Pressure Gauges

Type

☒ Dwyer Incline Manometer
Dwyer Magnehelic
☒ Dwyer Magnehelic
Dwyer "U" Tube Manometer
Dwyer "U" Tube Manometer
Dwyer Microtactor (Micro - Manometer)

Oil, 0 - 10 inch water
Magnetic/Mechanical 0 - 1 inch water
Magnetic/Mechanical 0 - 10 inch water
Mercury, 36 inches
Water, 72 inches
Water, 0 - 1 inches of water

Chemicals and Reagents

☒ Water
☒ Acetone
☒ Silica Gel
☒ Stopcock Grease

Deionized/ Distilled
Reagent Grade (<0.001% residual)
5 - 16 Mesh
Acetone- Insoluble & Heat Resistant



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P.O. Box 152 - Richfield, Ohio 44286
Phone (216) 526-0990

FIELD DATA SHEETS



**Envisage
Environmental
Incorporated**

P.O. Box 152 Richtfield, Ohio 44286
Phone (216) 526-0990

PLANT Neuro. (Siam)DATE 11/13RUN# 1CASE# 45 LOCATIONpage 1 of 3

POINT NUMBER	SAMPLE TIME	GAS METER READING	VELOCITY HEAD (Ap)	ORIFICE PRESSURE	STACK TEMP	GAS METER TEMP IN	GAS METER TEMP OUT	PUMP VACUUM	FILTER HOLDER	IMPINGER TEMP
1	0/11.21	843.50	.02	1.7	26.2	58	55	4	250	45
2	2.5	845.55	.02	1.7	26.2	63	67	4	250	48
3	5	847.55	.02	1.7	26.2	74	69	5	250	48
4	7.5	849.47	.02	1.7	26.5	76	69	5	245	45
5	10	851.45	.02	1.7	26.5	77	66	5	249	48
6	12.5	853.55	.02	1.7	26.5	78	67	5	250	48
7	15	855.36	.02	1.7	26.5	79	68	5	250	48
8	17.5	857.35	.02	1.7	26.5	80	69	5	250	48
9	20	859.78	.03	2.5	26.4	81	67	87	250	48
10	22.5	861.70	.02	1.7	26.4	81	68	5	250	48
11	25	863.68	.02	1.7	26.4	82	68	5	250	48
12	27.5	865.70	.02	1.7	26.1	81	66	5	250	48
1	30	867.63	.02	1.7	26.0	66	62	5	250	45
2	32.5	869.56	.02	1.7	25.6	70	67	5	250	48
3	35	871.54	.02	1.7	25.6	75	68	5	247	48
4	37.5	873.56	.02	1.7	25.6	79	69	5	250	48
5	40	875.60	.02	1.7	26.0	79	65	5	250	48
6	42.5	877.52	.02	1.7	26.0	81	68	5	250	48
7	45	879.52	.02	1.7	26.1	81	67	5	250	48
8	47.5	881.42	.02.01	.84	26.1	81	69	4	250	45
9	50	882.86	.01	.84	26.1	880	69	4	250	48
10	52.5	884.29	.01	.84	26.0	80	70	4	250	48
11	55	885.70	.01	.84	26.0	29	70	4	250	48
12	57.5	887.13	.01	.84	26.0	79	69	4	250	48
	60/12.36	888.56								

SAMPLE TRAIN LEAK CHECKS

PITOT TUBE LEAK CHECKS

PRE-TEST 0 CFM @ 15 "Hg POST-TEST 0 CFM @ 15 "HgPRE-TEST #2 0.0 POST-TEST #2 0.0#4 0.0#4 0.0

21

45.06

0.018

1.554

261.542°F

72.063°F

POINT NUMBER	SAMPLE TIME	GAS METER READING	VELOCITY HEAD (AP)	ORIFICE PRESSURE	STACK TEMP	GAS METER TEMP IN	GAS METER TEMP OUT	PUMP VACUUM	FILTER HOLDER	IMPINGER TEMP
1	0/129	888.83	.02	1.7	256	80	70	4.0	238	50
2	2.5	890.89	.02	1.7	259	81	70	4.0	240	50
3	5	892.90	.02	1.7	260	82	71	4.0	240	50
4	7.5	894.87	.02	1.7	260	83	72	4.0	241	50
5	10	896.91	.02	1.7	259	83	72	4.0	242	50
6	12.5	898.86	.02	1.7	260	83	72	4.0	243	51
7	15	900.82	.02	1.7	260	83	72	4.0	244	52
8	17.5	902.79	.02	1.7	259	84	73	4.0	245	52
9	20	904.78	.02	1.7	259	85	73	4.0	246	54
10	22.5	906.75	.02	1.7	258	85	73	4.0	246	54
11	25	908.76	.01	.84	258	85	74	4.0	248	54
12	27.5	910.19	.01	.84	259	85	74	4.0	249	55
1	30	911.68	.02	1.7	257	84	73	4.0	245	55
2	32.5	913.59	.02	1.7	255	84	73	4.0	244	55
3	35	915.55	.02	1.7	256	82	73	4.0	243	57
4	37.5	917.52	.02	1.7	256	82	73	4.0	242	57
5	40	919.46	.02	1.7	257	83	74	4.0	240	58
6	42.5	921.48	.02	1.7	257	84	75	4.0	240	58
7	45	923.43	.02	1.7	258	85	75	4.0	242	59
8	47.5	925.37	.02	1.7	259	86	75	4.0	243	60
9	50	927.35	.02	1.7	259	86	75	4.0	245	60
10	52.5	929.20	.02	1.7	260	86	75	4.0	247	62
11	55	931.23	.01	.84	260	87	75	4.0	248	62
12	57.5	933.20	.01	.84	259	87	75	4.0	250	62
140	60/	934.66								

PITOT TUBE LEAK CHECKS

SAMPLE TRAIN LEAK CHECKS

PRE-TEST ☒ CFM @ 1.5" Hg POST-TEST ☒ CFM @ 15" Hg PRE-TEST #2 0.02 G.S. POST-TEST #202 (a) 6.5

45.85 0.018 1.557 258.458°F #4 0.02 G.S. 78.563°F #4 0.02 6.5

POINT NUMBER	SAMPLE TIME	GAS METER READING	VELOCITY HEAD (AP)	ORIFICE PRESSURE	STACK TEMP	GAS METER IN	GAS METER TEMP OUT	PUMP VACUUM	FILTER HOLDER	IMPINGER TEMP
1	0.322	938.19	.02	1.7	256	80	72	4.0	238	52
2	25	940.35	.02	1.7	258	80	72	4.0	238	52
3	5	942.19	.02	1.7	254	82	72	4.0	239	52
4	7.5	944.28	.02	1.7	253	82	73	4.0	240	54
5	10	946.15	.02	1.7	254	83	73	4.0	240	54
6	12.5	948.14	.02	1.7	252	83	73	4.0	241	55
7	15	950.12	.02	1.7	253	84	74	4.0	242	55
8	17.5	952.10	.02	1.7	254	85	74	4.0	243	55
9	20	954.08	.02	1.7	252	85	74	4.0	244	56
10	22.5	954.04	.02	1.7	253	86	74	4.0	245	56
11	25	957.98	.02	1.7	254	86	74	4.0	248	58
12	27.5	959.92	.02	1.7	255	87	74	4.0	248	59
1	30	961.88	.01	1.7	253	87	75	4.0	250	60
2	32.5	963.28	.02	1.7	253	88	75	4.0	250	60
3	35	964.67	.02	1.7	253	88	75	4.0	252	60
4	37.5	966.60	.02	1.7	254	88	76	4.0	253	60
5	40	968.51	.02	1.7	254	88	76	4.0	254	61
6	42.5	970.44	.02	1.7	255	87	76	4.0	255	61
7	45	972.35	.02	1.7	253	87	76	4.0	255	62
8	47.5	974.35	.02	1.7	253	87	77	4.0	253	62
9	50	976.22	.02	1.7	254	88	77	4.0	252	62
10	52.5	978.16	.02	1.7	254	88	77	4.0	250	63
11	55	980.08	.02	1.7	253	88	77	4.0	248	63
12	57.5	982.04	.01	1.7	252	88	77	4.0	248	63
	60	983.98		1.84						

SAMPLE TRAIN LEAK CHECKS

PITOT TUBE LEAK CHECKS

PRE-TEST 0 CFM @ 15 "Hg POST-TEST 0 CFM @ 15 "Hg PRE-TEST #2 0.6.2 POST-TEST #2 0.6.3
 PRE-TEST #4 0.6.4 POST-TEST #4 0.6.4

45.74 0.019 1.378 1.058 753.75°F 80.003

PLANT Adropolitan Ceram: 15 DATE 11/17/63 RUN# 40-1 LOCATION K/Ln page 1 of 1

POINT NUMBER	VELOCITY PRESSURE Ap	TEMPERATURE	TEMPERATURE	Vap
1	.02		205	.141
2	.02		205	.141
3	.03		206	.173
4	.03		206	.173
5	.03		210	.173
6	.03		212	.173
7	.04		212	.20
8	.03		213	.173
9	.03		213	.173
10	.03		214	.173
11	.03		214	.173
12	.02		215	.141
1	.02		209	.141
2	.02		212	.141
3	.02		215	.141
4	.03		215	.173
5	.03		217	.173
6	.03		219	.173
7	.02		222	.141
8	.02		225	.141
9	.02		225	.141
10	.02		225	.141
11	.02		225	.141
12	.02		225	.141

PITOT TUBE LEAK CHECKS

PRE-TEST #2 0.06.1
#4.0870

POST-TEST #2 18.65
#4.6851

214.96

.158

POINT NUMBER	VELOCITY PRESSURE AP	TEMPERATURE DRY T _s	TEMPERATURE WET T _{sw}	AP
1	.03	231		.173
2	.03	232		.173
3	.03	230		.173
4	.03	225		.173
5	.03	227		.173
6	.03	227		.173
7	.03	229		.173
8	.02	231		.141
9	.02	230		.141
10	.02	230		.141
11	.01	231		.10
12	.01	231		.10
1	.02	221		.141
2	.02	224		.141
3	.02	224		.141
4	.03	225		.173
5	.03	229		.173
6	.03	231		.173
7	.03	230		.173
8	.03	230		.173
9	.02	230		.141
10	.02	230		.141
11	.02	229		.141
17	.01	224		.100

PRE-TEST #2 00.4.2
#4 00.5.7
PILOT TUBE LEAK CHECKS
POST-TEST #2 00.6.4
#4 00.6.8

CS
18

251

228.38

PLANT METRIC POLYMER CEMENTS DATE 11/17/93 RUN# 80352 LOCATION Kilm page 601

POINT NUMBER	VELOCITY PRESSURE AP	TEMPERATURE DRY T _S	TEMPERATURE WET T _{SW}	WAP
1	.02	215		.141
2	.02	217		.141
3	.02	218		.141
4	.03	218		.173
5	.03	220		.173
6	.03	220		.173
7	.03	221		.173
8	.03	221		.173
9	.025	221		.158
10	.025	220		.158
11	.025	217		.158
12	.02	215		.141
1	.02	209		.141
2	.02	209		.141
3	.02	211		.141
4	.03	212		.173
5	.03	212 212		.173
6	.03	213		.173
7	.03	214		.173
8	.03	216		.173
9	.025	216		.158
10	.025	215		.158
11	.02	212		.141
12	.02	212		.141

PRE-TEST#2 086.9 POST-TEST#2 085.0
#4 086.0 #4 085.9

PITOT TUBE LEAK CHECKS

215.58

158

POINT NUMBER	VELOCITY PRESSURE Δp	TEMPERATURE DRY T_s	TEMPERATURE WET T_{sw}	Δp
1	.03	211		.173
2	.03	213		.173
3	.03	213		.173
4	.035	215		.187
5	.035	215		.187
6	.03	217		.173
7	.03	217		.173
8	.03	217		.173
9	.02	220		.141
10	.02	221		.141
11	.02	221		.141
12	.02	221		.141
1	.02	216		.141
2	.02	218		.141
3	.025	218		.158
4	.025	221		.158
5	.025	223		.158
6	.03	223		.173
7	.03	225		.173
8	.025	225		.158
9	.025	227		.158
10	.025	226		.158
11	.02	225		.141
12	.02	223		.141

PITOT TUBE LEAK CHECKS
 PRE-TEST #2 0.49 POST-TEST #2 0.70
 #4 0.59 #4 0.61

219.63

.160

CALIBRATION SECTION



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CALIBRATION FREQUENCY

The frequency of calibration is dictated by the Code of Federal Regulations, Volume 42, Number 160, August 18, 1977. The regulations state that you must "use methods and equipment which have been approved by the Administrator to calibrate the orifice meter, pitot tube, dry gas meter, and probe heater. Recalibrate after each test".

The methods of calibration are determined from "maintenance, Calibration, and Operation of Isokinetic Source Sampling Equipment," published by the U.S.EPA Office of Air Program Publications APTD-0576. Per the above listed regulations, the equipment was checked after the stack test and values of Y, Cp(Test), and nozzle diameter had not appreciably changed from the acceptable tolerances.

NOZZLE DIAMETER CALIBRATION

I.D. of nozzles are checked immediately prior to and immediately following the stack test. If the prior deviation exceeds $\pm .001$ inches on an average or $\pm .002$ inches maximum, the nozzle is reworked.

BAROMETER CALIBRATION

The aneroid barometers used by Envisage are calibrated to our mercury in glass barometer which is NBS traceable. Calibration occurs before and after each field use.



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THERMOCOUPLE CALIBRATION

DATE: September 30, 1993

Type: K	Low		Medium		High		Average
Sensor #	Reading	Ref	Reading	Ref	Reading	Ref	Deviation
1	40	41	80	79	212	212	0.67
2	40	40	79	79	212	212	0.00
3	41	40	79	80	212	212	0.67
4	40	40	79	79	212	212	0.00
5	41	41	79	79	212	212	0.00
6	43	43	79	79	212	212	0.00
7	44	45	79	79	212	212	0.33
8	43	44	80	80	212	212	0.33
9	44	44	80	80	212	212	0.00
10	44	44	80	80	212	213	0.33
11	44	45	80	80	212	213	0.67
12	45	45	80	80	212	212	0.00
13	45	45	79	79	212	212	0.00
14	42	41	79	79	212	212	0.33
15	42	41	79	79	212	212	0.33
16	41	41	80	80	212	212	0.00
17	40	40	80	80	212	212	0.00
18	40	40	80	80	212	213	0.33
19	40	41	81	81	212	212	0.33
20	41	41	81	81	212	212	0.00
21	42	42	81	81	212	212	0.00
22	42	42	81	81	212	212	0.00
23	42	42	81	81	212	212	0.00
24	43	43	81	81	212	212	0.00



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"S" TYPE PITOT TUBE CALIBRATION

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"S" Type Pitot Tube (Probe) # 501 - 5 ft Probe

Calibration Date: September 30, 1993

$$C_p = C_{std} \sqrt{\frac{\Delta p_{std}}{\Delta p_p}} \quad (\text{EPA Equation 2-2})$$

where:

C_p = Coefficient of Type S pitot tube, dimensionless

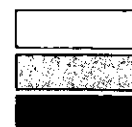
C_{std} = Coefficient of Standard Pitot Tube (0.99), dimensionless

Δp_{std} = Velocity head measured by standard pitot tube, inches H_2O

Δp_p = Velocity head measured by Type S pitot tube, inches H_2O

	Δp_{std}	Δp_p	C_p
Side A	0.23	0.32	0.839
Side B	0.23	0.32	0.839
Side A	0.46	0.63	0.846
Side B	0.46	0.63	0.846
Side A	0.82	1.14	0.840
Side B	0.82	1.14	0.840

Average - 0.84



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CONTROL UNIT CALIBRATION
(English Units)

Date 9-7-93

Metering System
Identification: 893-795

Barometric pressure, $P_b = \underline{29.39}$ in. Hg

Model Number 90-800

Orifice manometer setting ΔH in. H_2O	Spirometer (wet meter) gas volume V_w ft^3	Dry gas meter volume V_m ft^3	Temperatures				Time θ min
			Spirometer (wet meter) t_w $^{\circ}F$	Dry Gas Meter			
				Inlet t_i $^{\circ}F$	Outlet t_o $^{\circ}F$	Average t_m $^{\circ}F$	
1.0	5	5.193	75.2	115	82	98.5	8.80
2.0	5	5.184	75.0	121	82	101.5	6.33
4.0	5	5.195	76.4	125	84	104.5	4.50

Calculations

ΔH in. H ₂ O	Y	$\Delta H@$
	$\frac{V_w P_b (t_m + 460)}{V_m \left[P_b + \frac{\Delta H}{13.6} \right] (t_w + 460)}$	$\frac{0.0317 \Delta H}{P_b (t_o + 460)} \left[\frac{(t_w + 460) \theta}{V_w} \right]^2$
1.0	1.00	1.76
2.0	1.01	1.83
4.0	1.00	1.85
Average	1.00	1.81

Y = Ratio of reading of wet test meter to dry test meter; tolerance for individual values ± 0.02 from average.

$\Delta H@$ = Orifice pressure differential that equates to 0.75 cfm of air @ 68°F and 29.92 inches of mercury, in. H₂O; tolerance for individual values ± 0.20 from average.

Calibrated by: 

EMISSION SAMPLING NOMENCLATURE



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A	=	Cross sectional area of stack or duct, ft. ² .
A_n	=	Cross sectional area of nozzle entry plane, ft. ² .
B_{ws}	=	Water vapor in gas stream, proportion by volume.
C	=	Nomograph correction factor, dimensionless.
C_s	=	Concentration of particulate matter in gas stream, dry basis-corrected to standard conditions, gr/dscf.
D_n	=	Nominal diameter of probe nozzle entry plane, in.
E	=	Particulate Emission Rate, lb./hr.
ΔH	=	Average pressure differential across orifice, in. of H ₂ O.
$\Delta H_{\odot}$	=	Orifice meter calibration factor, in. of H ₂ O.
I	=	Percent of isokinetic sampling, %.
K_p	=	Pitot tube constant, 85.49 ft./sec.
M_d	=	Molecular weight of gas, dry basis, lb./lb.-mole.
M_a	=	Total amount of particulate matter collected, g.
M_s	=	Molecular weight of gas, wet basis, lb./lb.-mole.
M_w	=	Molecular weight of water, 18 lb./lb.-mole.
P_{bar}	=	Barometric pressure, in. of H _g .
P_g	=	Pressure differential from gas stream to atmosphere, (static pressure) in. of H ₂ O.
P_s	=	Absolute gas stream pressure, ($P_{bar} + P_g/13.6$) in. of H _g .
P_{std}	=	Absolute pressure at standard conditions, 29.92 in. of H _g .
P_w	=	Density of water, 0.0022 lb./ml.

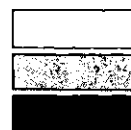


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SAMPLING NOMENCLATURE - continued

- $\bar{P}_{avg}$ = Average of the square roots of the velocity head readings, in. of H_2O .
 Q = Volumetric flow rate at gas stream conditions, A.C.F.M.
 Q_{std} = Dry volumetric gas flow rate corrected to standard conditions, D.S.C.F.M.
 R = Ideal gas constant, 21.85 in. of H_2 -ft³/ °R-lb.-mole.
 t = Total sampling time, minutes.
 T_m = Average dry gas meter temperature, °R.
 T_s = Average absolute gas stream temperature, °R.
 T_{std} = Standard absolute temperature, 528° rankine.
 V_{lc} = Volume of water collected in impingers and silica gel, ml.
 V_m = Volume of gas sample measured at meter box (meter conditions), ft.³.
 $V_{m(std)}$ = Volume of gas sample measured at meter box (corrected to standard conditions), ft.³.
 V_s = Average gas stream velocity, ft./sec.
 $V_{w(std)}$ = Volume of water vapor in gas sample (standard conditions), ft.³.
13.6 = Specific gravity of mercury (H_g).
%CO₂ = Percent by volume of CO₂ in gas stream (dry basis).
%O₂ = Percent by volume of O₂ in gas stream (dry basis).
%CO = Percent by volume of CO in gas stream (dry basis).
%N₂ = Percent by volume of N₂ in gas stream (dry basis).



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EMISSION SAMPLING CALCULATIONS



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1) Volume of dry gas sampled through meter box at standard conditions,

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$$V_{m(std)} = V_m \left[\frac{T_{std}}{T_m} \right] \left[\frac{P_b + \frac{\Delta H}{13.6}}{P_{std}} \right]$$

(EPA Equation 5-1)

Where:

$V_{m(std)}$ = Volume of gas sample measured at meter box (corrected to standard conditions), ft^3 .

V_m = Volume of gas sample measured at meter box (meter conditions), ft^3 .

T_{std} = Standard absolute temperature, 528° Rankine.

T_m = Average dry gas meter temperature, $^{\circ}R$.

P_{bar} = Barometric Pressure, in. Hg.

ΔH = Average pressure differential across orifice, in. H_2O .

13.6 = Specific gravity of mercury (Hg).

P_{std} = Absolute pressure at standard conditions, 29.92 in. Hg.

Example: Run 1

V_m = 45.06 ft^3
 T_m = 532.1 $^{\circ}R$
 ΔH = 1.55 in. H_2O
 P_{bar} = 28.78 in. Hg

$$\begin{aligned} V_{m(std)} &= 45.06 \left[\frac{528.0}{532.1} \right] \left[\frac{28.78 + \frac{1.55}{13.6}}{29.92} \right] \\ &= 45.06 \quad (0.9922) \quad (0.9657) \\ &= 43.18 \quad ft^3 \end{aligned}$$

2) Volume of water vapor collected at standard conditions,

$$V_{w(std)} = V_{lc} \left[\frac{P_w}{M_w} \right] \left[\frac{(R)(T_{std})}{P_{std}} \right]$$

(EPA Equation 5-2)

Where:

- $V_{w(std)}$ = Volume of water vapor in gas sample (standard conditions) ft^3 .
 V_{lc} = Volume of water collected in impingers & silica gel, ml.
 P_w = Density of water, 0.0022 lb/ml.
 M_w = Molecular weight of water, 18 lb/lb-mole.
 R = Ideal gas constant, 21.85 in. Hg-ft³/°R-lb-mole.
 T_{std} = Standard absolute temperature, 528 ° Rankine.
 P_{std} = Absolute pressure at standard conditions, 29.92 in. Hg.

Example: Run 1

$$V_{lc} = 60.6 \text{ ml}$$

$$\begin{aligned}
 V_{w(std)} &= 60.6 \left[\frac{0.0022}{18.0} \right] \left[\frac{(21.85)(528.0)}{29.92} \right] \\
 &= \underline{\underline{2.85}} \text{ ft}^3
 \end{aligned}$$



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3) Moisture content of gas stream,

$$B_{ws} = \frac{V_{w(std)}}{V_{m(std)} + V_{w(std)}}$$

(EPA Equation 5-3)

Where:

B_{ws} = Water vapor in gas stream, proportion by volume.

$V_{w(std)}$ = Volume of water vapor in gas sample (standard conditions) ft^3 .

$V_{m(std)}$ = Volume of gas sample measured at meter box (corrected to standard conditions), ft^3 .

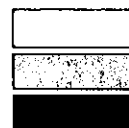
Example: Run 1

$$V_{w(std)} = 2.85 \text{ ft}^3$$

$$V_{m(std)} = 43.18 \text{ ft}^3$$

$$B_{ws} = \frac{2.85}{43.18 + 2.85}$$

$$= \underline{0.0620}$$



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4) Dry Molecular Weight of gas in gas stream,

$$M_d = 0.440 (\%CO_2) + 0.320 (\%O_2) + 0.280 (\%N_2 + \%CO)$$

(EPA Equation 3-2)

Where:

 M_d = Molecular weight of gas, dry basis, lb/lb-mole.0.440 = Molecular weight of CO_2 divided by 100.0.320 = Molecular weight of O_2 divided by 100.0.280 = Molecular weight of N_2 or CO (same for both compounds) divided by 100.% CO_2 = Percent by volume of CO_2 in gas stream (dry basis).% O_2 = Percent by volume of O_2 in gas stream (dry basis).

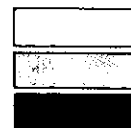
% CO = Percent by volume of CO in gas stream (dry basis).

% N_2 = Percent by volume of N_2 in gas stream (dry basis).Example: Run 1% CO_2 = 8.4% O_2 = 16.5

% CO = 0.0

% N_2 = 75.1

$$\begin{aligned}
 M_d &= 0.440 (8.4) + 0.320 (16.5) + 0.280 (75.1) \\
 &= 3.696 + 5.280 + 21.028 \\
 &= \underline{30.00} \text{ lb/lb-mole}
 \end{aligned}$$



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5) Molecular Weight of gas in gas stream,

$$M_s = M_d (1 - B_{ws}) + M_w (B_{ws})$$

(EPA Equation 2-5)

Where:

- M_s = Molecular weight of gas, wet basis, lb/lb-mole.
 M_d = Molecular weight of gas, dry basis, lb/lb-mole.
 B_{ws} = Water vapor in gas stream, proportion by volume.
 M_w = Molecular weight of water, 18 lb/lb-mole.

Example: Run 1

$$M_d = 30.00 \text{ lb/lb-mole}$$

$$B_{ws} = 0.0620$$

$$\begin{aligned}
 M_s &= 30.00 (1 - 0.0620) + 18 (0.0620) \\
 &= 28.145 + 1.115 \\
 &= \underline{\underline{29.26}} \text{ lb/lb-mole}
 \end{aligned}$$



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6) Average Gas Stream Velocity,

42

$$V_s = K_p C_p \Delta P_{avg} \sqrt{\frac{T_s}{P_s M_s}} \quad (\text{EPA Equation 2-9})$$

Where:

V_s = Average gas stream velocity, ft/sec.

K_p = Pitot tube constant, $85.49 \frac{\text{ft}}{\text{sec}} \left[\frac{(\text{lb/lb-mole})(\text{in.Hg})}{(^{\circ}\text{R})(\text{in.H}_2\text{O})} \right]^{1/2}$

C_p = Pitot tube coefficient, dimensionless.

ΔP_{avg} = Average of the square roots of the velocity head readings, $(\sqrt{\bar{P}}) (\text{in.H}_2\text{O})$.

T_s = Average absolute gas stream temperature, $^{\circ}\text{R}$.

P_s = Absolute gas stream pressure, $(P_{bar} + P_g/13.6) \text{ in.Hg}$.

P_{bar} = Barometric Pressure, in. Hg.

P_g = Pressure differential from gas stream to atmosphere, (static pressure) in.H₂O.

M_s = Molecular weight of gas, wet basis, lb/lb-mole.

Example: Run 1

C_p = 0.84

ΔP_{avg} = 0.134 in.H₂O^{1/2}

T_s = 721.5 $^{\circ}\text{R}$

P_s = $P_{bar} + P_g/13.6 = 28.78 + (-0.02/13.6) = 28.78 \text{ in.Hg}$

M_s = 29.26 lb/lb-mole

$$V_s = (85.49)(0.84)(0.134) \sqrt{\frac{721.5}{(28.78)(29.26)}}$$

= 8.91 ft/sec



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7) Volumetric Flow Rate at Gas Stream Conditions,

$$Q = A \times V_s \times 60$$

Where:

Q = Volumetric flow rate at gas stream conditions, A.C.F.M.

A = Cross sectional area of stack or duct, ft^2 .

V_s = Average gas stream velocity, ft/sec.

60 = Conversion factor from seconds to minutes.

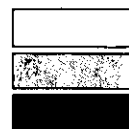
Example: Run 1

$$A = 19.63 \text{ ft}^2$$

$$V_s = 8.91 \text{ ft/sec}$$

$$Q = (19.63) (8.91) 60$$

$$= \underline{\underline{10,494 \text{ ACFM}}}$$



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8) Volumetric Flow Rate at Standard Conditions,

44

$$Q_{sd} = 60 (1 - B_{ws}) V_s A \left[\frac{T_{std}}{T_s} \right] \left[\frac{P_s}{P_{std}} \right]$$

(EPA Equation 2-10)

Where:

Q_{sd} = Dry volumetric gas flow rate corrected to standard conditions, S.C.F.M.

60 = Conversion factor from seconds to minutes.

B_{ws} = Water vapor in gas stream, proportion by volume.

V_s = Average gas stream velocity, ft/sec.

A = Cross sectional area of stack or duct, ft².

T_{std} = Standard absolute temperature, 528^o Rankine.

T_s = Average absolute gas stream temperature, ^oR.

P_s = Absolute gas stream pressure, ($P_{bar} + P_g/13.6$) in.Hg.

P_{bar} = Barometric Pressure, in. Hg.

P_g = Pressure differential from gas stream to atmosphere, (static pressure) in.H₂O.

P_{std} = Absolute pressure at standard conditions, 29.92 in. Hg.

Example: Run 1

B_{ws} = 0.0620

V_s = 8.91 ft/sec

A = 19.63 ft²

T_s = 721.5 ^oR

P_s = $P_{bar} + P_g/13.6 = 28.78 + -0.02/13.6 = 28.78$ in.Hg

$Q_{sd} = 60 (1 - 0.0620) (8.91) (19.63) \frac{528.0}{721.5} \frac{28.78}{29.92}$
 = 6,929 SCFM



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9) Gas Stream Particulate Concentration,

$$C_s = 15.43 \text{ gr./g} \left[\frac{M_n}{V_{m(\text{std})}} \right]$$

(EPA Equation 5-6)

Where:

C_s = Concentration of particulate matter in gas stream, dry basis-corrected to standard conditions, gr/dscf.

M_n = Total amount of particulate matter collected in probe wash and on filter, g.

$V_{m(\text{std})}$ = Volume of gas sample measured at meter box (corrected to standard conditions), ft³.

Example: Run 1

$$M_n = 0.0425 \text{ g}$$

$$V_{m(\text{std})} = 43.18 \text{ ft}^3$$

$$C_s = 15.43 \left[\frac{0.0425}{43.18} \right]$$

$$= \underline{\underline{0.0152 \text{ gr/dscf}}}$$



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10) Particulate Emission Rate,

$$E = Q_{sd} C_s \left[\frac{1 \text{ pound}}{7000 \text{ grains}} \right] \left[\frac{60 \text{ minutes}}{1 \text{ hour}} \right]$$

Where:

E = Particulate Emission Rate, lb/hr.

Q_{sd} = Dry volumetric gas flow rate corrected to standard conditions, S.C.F.M.C_s = Concentration of particulate matter in gas stream, dry basis-corrected to standard conditions, gr/dscf.Example: Run 1

$$Q_{sd} = 6,929 \text{ ft}^3$$

$$C_s = 0.0152 \text{ gr/dscf}$$

$$E = (6,929) (0.0152) \left[\frac{60}{7000} \right]$$

$$= \underline{\underline{0.90}} \text{ lb/hr}$$



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11) Percent of Isokinetic Sampling,

47

$$I = \frac{100 T_s}{60} \left[\frac{K_3 V_{lc}}{A_n} + \left(\frac{V_m}{T_m} \right) \left(\frac{P_{bar} + \frac{\Delta H}{13.6}}{P_s} \right) \right] \quad (EPA Equation 5-7)$$

Where:

- I = Percent of Isokinetic sampling, %.
 T_s = Average absolute gas stream temperature, °R.
 K₃ = Constant, 0.002669 in.Hg-ft³/ml-°R.
 V_{lc} = Volume of water collected in impingers & silica gel, ml.
 V_m = Gas sample volume measured at meter box (meter conditions), ft³.
 T_m = Average dry gas meter temperature, °R.
 P_{bar} = Barometric Pressure, in. Hg.
 ΔH = Average pressure differential across orifice, in. H₂O.
 t = Total sampling time, minutes.
 V_s = Average gas stream velocity, ft/sec.
 P_s = Absolute gas stream pressure, in.Hg.
 D_n = Nominal diameter of probe nozzle tip, inches.
 A_n = Cross sectional area of nozzle, ft².

Example: Run 1

T _s	=	721.5 °R	ΔH	=	1.55 in.H ₂ O
V _{lc}	=	60.6 ml	t	=	60.0 min.
V _m	=	45.06 ft ³	V _s	=	8.91 ft/sec
T _m	=	532.1 °R	P _s	=	28.78 in.Hg
A _n	=	0.0020294 ft ²	P _{bar}	=	28.78 in.Hg

$$I = \frac{721.5 (100)}{60 (0.0020294)} \left[0.002669 (60.6) + \left(\frac{45.06}{532.1} \right) \left(\frac{28.78 + \frac{1.55}{13.6}}{28.78} \right) \right]$$

$$= 100.5 \%$$



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9) Gas Stream NOx Concentration,

$$C_{nox} = \frac{ppm \left[\frac{MW}{M.V.} \right] \left[\frac{1 \text{ Pound}}{453.59 \text{ grams}} \right]}{10^6}$$

Where:

C_{nox} = Concentration of Nitrogen Oxides (as NO₂) in gas stream, dry basis at standard conditions, lb/dscf.

ppm = Average concentration of NOx as measured at detector

MW = Molecular Weight of Compound used for comparison and/or instrument calibration, g/g-mole.

M.V. = Volume occupied by one mole of gas at standard conditions of 68° Fahrenheit and 29.92" Hg, 0.849531 ft³/mole.

Example: Run 1

PPM = 51.8 ppm

MW = 46.010 g

$$C_{nox} = \frac{51.8 \left[\frac{46.010}{0.849531} \right] \left[\frac{1 \text{ Pound}}{453.59 \text{ grams}} \right]}{10^6}$$

$$= \frac{6.185 \times 10^{-6}}{10^6} \text{ lb/dscf}$$



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10) NOx Emission Rate,

$$E_{nox} = Q_{sd} C_{nox} \left[\frac{60 \text{ minutes}}{1 \text{ hour}} \right]$$

Where:

E = NOx Emission Rate, lb/hr.

Q_{sd} = Dry volumetric gas flow rate corrected to standard conditions, S.C.F.M.

C_{nox} = Concentration of NOx in gas stream, dry basis, corrected to standard conditions, lb/dscf.

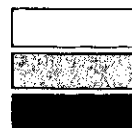
Example: Run 1

$$Q_{sd} = 8,245 \text{ ft}^3$$

$$C_{nox} = 6.185 \times 10^{-6} \text{ lb/dscf}$$

$$E = (8,245) (6.185 \times 10^{-6}) (60)$$

$$= \underline{\underline{3.060 \text{ lb/hr}}}$$



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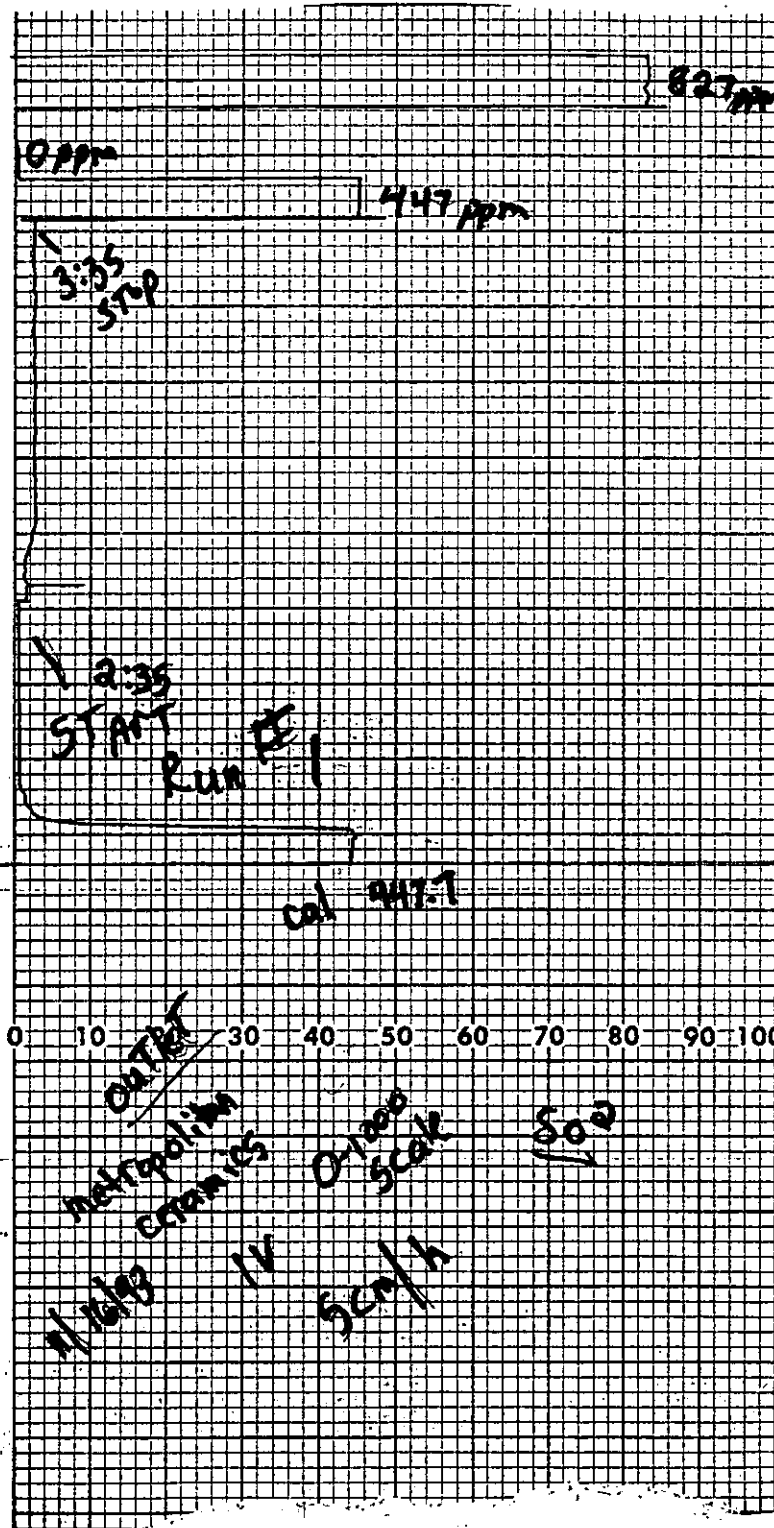
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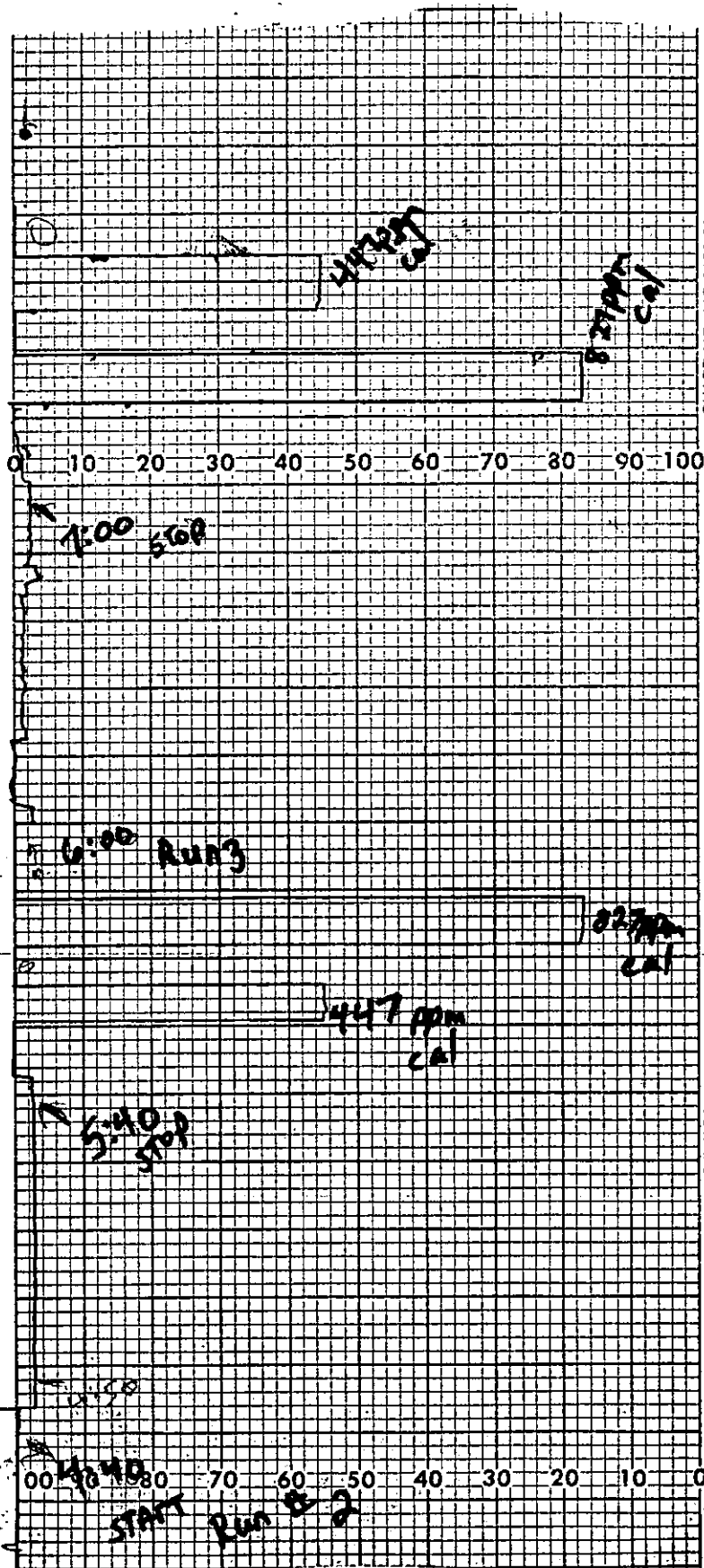
CHART RECORDINGS



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11/17/93

NO_x

Run #1

53

PM 49 & 88 ppm Calibration gases

0-100 scale

0 2:40 = 60 ppm

1. 60 ppm

21. 40

41. 50

2. 60 ppm

22. 45

42. 40

3. 60

23. 40

43. 40

4. 60

24. 40

44. 40

5. 60

25. 50

45. 50

6. 60

26. 50

46. 50

7. 60

27. 55

47. 60

8. 60

28. 50

48. 60

9. 60

29. 50

49. 55

11/17

2:50 10. 60

3:10 30. 55

3:30 50. 50

11. 60

31. 50

51. 55

12. 50

32. 55

52. 55

13. 55

33. 55

53. 55

14. 60

34. 55

54. 50

15. 60

35. 50

55. 50

16. 50

36. 50

56. 50

17. 50

37. 50

57. 50

18. 50

38. 50

58. 40

19. 50

39. 55

59. 40

3:00 20. 40

3:20 40. 55

3:40 60. 40

End cal. 49 ppm for 49 ppm cal gas

89 ppm for 88 ppm cal gas

0 for 0

NOx

49288 ppm cal gas
Run 2

0-100 scale

54

4:40	0	40ppm	21	50	41	40
1	45		22	45	42	40
2	45		23	50	43	40
3	40		24	45	44	40
4	50		25	40	45	40
5	50		26	45	46	40
6	50		27	45	47	40
7	50		28	50	48	40
8	50		29	50	49	40
9	50	5:10	30	45	5:30	50 40
10	50		31	45	51	40
11	50		32	40	52	40
12	50		33	45	53	40
13	50		34	40	54	40
14	40		35	40	55	40
15	45		36	40	56	40
16	45		37	40	57	40
17	45		38	40	58	40
18	45		39	40	59	35
19	40	5:20	40	40	5:40	60 35
5:00	20	45				

Post cal →

48 for 49 ppm cal gas

88 for 88 ppm cal gas

0 for 0

NO_x

Run 3

49.28 ppm cal gas

0-100 scale

55

6:00 0 30 ppm

1 35 21 55 41 50

2 30 22 60 42 45

3 40 23 50 43 45

4 45 24 50 44 50

5 50 25 50 45 50

6 40 26 55 46 50

7 40 27 60 47 50

8 50 28 55 48 40

9 50 29 50 49 40

6:10 10 60 6:30 50 6:50 50

11 60 31 50 51 50

12 60 32 50 52 55

13 60 33 50 53 55

14 50 34 50 54 50

15 50 35 55 55 50

16 50 36 50 56 50

17 55 37 55 57 50

18 50 38 50 58 55

19 55 39 50 59 60

6:20 20 50 6:40 40 6:00 60

post cal

for 49 ppm cal gas

for 88 ppm cal gas

STACK TEST
OBSERVATION REPORT
METROPOLITAN INDUSTRIES
15 76 05 1149 P006
NOVEMBER 17 & 18, 1993

*unglazed
ceramic
tile*

On the above date, I arrived at Metropolitan Industries, located at 1201 Millerton Rd. SE on the outskirts of Canton, to observe a stack test on a new 150' stainless steel stack for P006. This source is the #3 tunnel kiln for the tile "firing". At that time, the #3 tunnel kiln was the only kiln connected to the stack. The #1 & #2 kilns are scheduled to be connected to the stack some time in December of 1993. The ductwork is run to the current #1 & #2 kiln emission stacks, but the final connections have not been made. These ductwork extensions were sealed off from the outside air (at this time since not connected) by valves installed for such a purpose as to isolate each kiln exhaust, if necessary. These valves were in the closed position during all testing. The testing was to be done by Envisage Environmental Inc. The weather on November 17, was cold and rainy. In fact, tornado warnings were issued for Stark County. Because of the conditions, it was determined to postpone the particulate and Hf portion of the test, and to run only that for SO₂, NO_x and CO. The rest of the parameters would be done on the 18th. My contacts were Mr. Philip McGuinness of Metropolitan, and Eric Hevener & James Gray of Envisage on the 17th, and Greg Sinkovich of Envisage on the 18th. My job was to observe the test runs and to conduct VE observations utilizing Method 9.

The information obtained from Philip McG. concerned the P006 source. The maximum temperature in the peak compartment was running at 1150°C. The feed rate was set at 90% capacity (36 cars per day). That is 40 minutes per car. Each car contained 1.848 Tons of tile products. At 90% capacity, that is 66.528 T/D. 100% would be 73.92 T/D. These tiles were of the same consistency for the entire test - 40% clay and 60% shale. This particular mixture is called a "250" mix. Tile samples were collected by Philip McG. to correspond to the SO₂ testing. Such tiles were collected ahead of time to correspond to the cars. Once it was calculated which cars were in what position at a particular time during the testing, those tile samples were pulled for composite testing. (At the current time, all composite sample tests are run by Stark Ceramics, with intermittent sample checks done by NSL for cross checking. I received a year to date printout of all the composite sampling that has been done, and the results of the tests. See the attached printout.) Philip McG. also informed me that Envisage was asked by Metropolitan to include two more parameters in their testing, just to document that Metropolitan does not have a problem with them. Those two parameters are VOC and Pb. The VOC was to be run with the other gases, and the Pb would be tested for by a separate sampling train at the time of the Particulate and Hf testing. While talking with Philip McG., he informed me (when he saw the P006 copy of PTI conditions and STC's I had with me) that there was a typo and mistake made, and of which Dan Schiltz, of our office, had already submitted a modification to OEPA for. On page 4 of Application No. 15-883, 14.25 lbs SO₂/yr should read *52.77 lbs SO₂/hr or 19.26 lbs SO₂/hr. The * was to denote combined emissions from P004, P005 and P006.

My observations on the 17th consisted of watching only one run on the gas sampling end of the test. VOC, NO_x, SO₂ and CO were all checked by utilizing CEM's (continuous emission monitors). The SO₂ and CO used strip charts for recording results. The VOC and NO_x recordings were done by hand, every minute. I observed the equipment being calibrated using EPA Protocol 1 gases. Each run was conducted for one hour, with the standardized gases being run after each run to verify the results. Since I only observed the first run, I can only account for what I saw during that time period. Everything appeared scientifically correct, to my knowledge, with the exception of what I observed concerning the SO₂ CEM operation. It appeared that this unit was sensitive to pressure flow of gas through the unit. This is

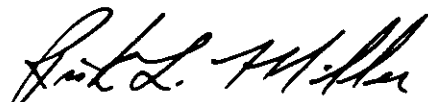
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15 76 05 1149 P006
NOVEMBER 17 & 18, 1993
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understandable, and it appeared that all precautions were taken as to control the amount of gas flowing through the unit. All gas samples were feed pumped into a glass manifold which had an excess flow port at the end. A line was run from this manifold to the SO₂ CEM and another pump was installed after the CEM in order to pull the sample through the machine at a steady rate. This setup appeared fine. However, what did not make sense was that the CEM indicated that the standard SO₂ sample readings could be altered by changing the Protocol 1 gas tank regulator setting.(?) As the pressure increased, the concentration increased. After working with the unit to initially calibrate it, the sampling was done and then the standards run through the unit again. However, the regulator was moved in the process of checking the standards instead of leaving it set as it was during the calibration process. In my own personal opinion, this should invalidate the test for SO₂. The following information is what I recorded concerning the standard checks and a quick, visual average of the readings (in ppm) during the stack testing:

<u>POLLUTANT</u>	<u>AVER. TEST RDG.</u>	<u>STD.</u>	<u>✓</u>	<u>STD.</u>	<u>✓</u>	<u>STD.</u>	<u>✓</u>
CO	≈ 4	702	704	200	192	97.1	83
SO ₂	≈ 22	827	815			447.7	?
NO _x	≈ 60			88.1	89	49.48	48.5
VOC	≈ 10	800	750			56	≈ 50

Results will have to be looked at in order to make a final determination.

My observations on the 18th consisted of doing VE readings on the emissions from the 150' stack while the P006 source was operating at 90% capacity. All dampers were observed being checked to assure they were closed. This test period was to determine particulate, Hf and Pb emission levels, if any. During this testing period, Envisage appeared to have some problems with getting a correct stack temperature and flow rate. Originally, their instruments showed no flow velocity and a stack temperature of about 150°F. Metropolitan checked their stack exhaust temperature at the source and indicated that they were emitting exhaust about 300°F. Without Metropolitan making any adjustments, Envisage kept working and eventually established a stack temperature of about 256°F and a Δp (velocity indicator) of .02" (H₂O). This made sense because the source (P006) is a long way from the stack (about 264'). Before starting, the temperature and velocity were lost again, but Greg Sinkovich was able to re-establish readings. The first two runs were done during periods in which the background for the VE's was a grayish sky. By the third run, the sky had cleared to a blue background. It is assumed that the readings during the third run are more representative of the emissions from the source. Especially since a continuous flow of emissions could be detected while standing directly below the stack before and between the first two runs. Leak check observations could not be made by myself because all equipment was on the stack platform, about 75' above the ground, and in which a safety harness was essential in order to climb the stack ladder. Other than the noted problems, everything else appeared to be o.k.


Rick L. Miller
Staff Field Inspector

METRO.
BRICK

TK3TESTS.XLS

EMISSION DATA FOR COMPLIANCE TEST 11/17/93 & 11/18/93 TK#3

PRODUCTION CLAY/SHALE SAMPLES FOR SULFUR DETERMINATION

CAR #'s FROM END OF ZONE 6 TO START OF ZONE 2

TEST 1 48,194,183,5,152,30,105,73,173,91,41,9,20,82,21.
TEST 2 5,152,30,105,73,173,91,41,9,20,82,21,81,83,4,130.
TEST 3 152,30,105,73,173,91,41,9,20,82,21,81,83,4,130,107.

SAMPLES TO NSL		SAMPLES TO STARK			AVERAGE
	% SULFUR			% SULFUR	% SULFUR
TEST 1	0.059	TEST 1	A	0.076	
			B	0.072	0.069
TEST 2	0.055	TEST 2	A	0.068	
			B	0.07	0.06433
TEST 3	0.04	TEST 3	A	0.06	
			B	0.076	0.05867

CARBON AND SULFUR TESTING**1993**

DAILY CLAY/SHALE SAMPLES OF 10gms TOTAL COLLECTED TO REPRESENT THE DAYS PRODUCTION COLOR, ACCUMULATED FOR A 7 DAY PERIOD, TO GIVE A COMPOSITE SAMPLE FOR TESTING AT STARK CERAMICS FOR CARBON AND SULFUR CONTENT

3.10.93. MONTHLY AVERAGE SULFUR % NOT TO EXCEED 0.1% S. limit

E.G. 310 PRODUCTION COLOR (70% SHALE, 30% CLAY) REPRESENTED BY 7gms SHALE AND 3gms CLAY

SAMPLE DATES	PRODUCTION COLORS		CARBON %	SULFUR %	TOTAL %	MONTH AVER % Sulfur	KILN Schedule o.p.d	Average Wet Tons/can	Wet Tons/Kiln/day	Dry Tons TOTAL /kiln/day
12/30...1/10	507,57X		0.21	0.126	0.336		35	2.2	77	64.68
1/11...1/17	57X,105		0.229	0.136	0.365		35	2.2	77	64.68
1/18...1/24	105,107		0.233	0.134	0.367		35	2.2	77	64.68
1/25...1/31	105,107,308,250		0.219	0.212	0.431	0.152	35	2.2	77	64.68
2/1...2/7	250,350	#3 B/jay	0.241	0.052	0.293		35	2.2	77	64.68
2/8...2/14	310		0.241	0.188	0.429		35	2.2	77	64.68
2/15...2/21	310,31X		0.277	0.11	0.387		35	2.2	77	64.68
*2/22...2/28	31X,507		0.151	0.104	0.255	0.10	35	2.2	77	64.68
*3/1...3/7	507,		0.22	0.082	0.302		32-3.4.93	2.2	73	61.512
3/8...3/14	507,101,57X		0.293	0.136	0.429		35-3.12.93	2	70	58.992
3/15...3/21	57X,15X		0.266	0.092	0.358		35	2	70	58.8
3/22...3/28	15X,105		0.241	0.09	0.327		32-3.28.93	2.2	70	58.8
3/29...4/4	310		0.147	0.176	0.323	0.1144	32	2.2	70	58.8
4/5...4/11	310,31X	FL	0.223	0.068	0.291		32	2.2	70	58.8
4/12...4/18	31X,505		0.226	0.124	0.35		32	2.2	70	58.8
4/19...4/25	505,107		0.289	0.208	0.497		32	2.2	70	58.8
4/26...5/2	107,308,250	Sad/Brk	0.223	0.14	0.363	0.135	32	2.2	70	58.8
*5/3...5/9	250,105,		0.272	0.178	0.45		32	2.2	70	58.8
*5/10...5/16	105,507		0.368	0.182	0.55		32	2.2	70	58.8
*5/17...5/23	507,57X		0.285	0.238	0.523		32	2.2	70	58.8
*5/24...5/30	57X,310		0.285	0.196	0.481	0.198 0.1	32	2.2	70	58.8
5/31...6/6	310		0.118	0.078	0.196		35-6.1.93	2.2	77	64.68
6/7...6/13	310,31X	S of clays	0.227	0.086	0.313		35	2.2	77	64.68
6/14...6/20	31X,109		0.159	0.078	0.237		35	2.2	77	64.68
6/21...6/27	109,240,107		0.245	0.12	0.365	0.0905	35	2.2	77	64.68
6/28...7/4	507		0.166	0.188	0.354		35	2.2	77	64.68
7/5...7/11	507,57X		0.191	0.132	0.323		39-7.7.93	2.2	85.8	72.072
7/12...7/18	57X		0.234	0.09	0.324		40-7.13.93	2.2	88	73.92
7/19...7/25	57X,105	New North	0.288	0.314	0.602		40	2.2	88	73.92
7/26...8/1	240,250,	No grog	0.178	0.099	0.277	0.1646	40	2.2	88	73.92
8/2...8/8	308,310		0.248	0.105	0.353		38-8.2.93	2	76	63.84
8/9...8/15	310		0.13	0.01	0.14		40-8.5.93	2.2	88	73.92
8/16...8/22	310,350,31X	31X MIX	0.181	0.058	0.239		40	2.2	88	73.92

To date Average 0.1293 M/LOW 0.1317

ALL FIGS

M/HIGH 0.1357

av of avs

* SAMPLES SENT TO NSL FOR CROSS CHECKS

CARBON AND SULFUR TESTING**1993**

DAILY CLAY/SHALE SAMPLES OF 10gms TOTAL COLLECTED TO REPRESENT THE DAYS PRODUCTION COLOR, ACCUMULATED FOR A 7 DAY PERIOD, TO GIVE A COMPOSITE SAMPLE FOR TESTING AT STARK CERAMICS FOR CARBON AND SULFUR CONTENT

E.G. 310 PRODUCTION COLOR (70% SHALE, 30% CLAY) REPRESENTED BY 7gms SHALE AND 3gms CLAY

SAMPLE DATES	PRODUCTION COLORS		CARBON %	SULFUR %	TOTAL %
8/23...8/29	31X.310.101	SMPL "B"	0.171	0.07	0.241
8/30...9/5	101,BISQ	SMPL "B"	0.256	0.178	0.434
9/6...9/12	507clay grog	SMPL "B"	0.21	0.182	0.392
9/13...9/19	507,57X	SMPL "B"	0.243	0.13	0.373
9/20...9/26	57X		0.24	0.186	0.568
9/27...10/3	57X . 107 . 310	310 80:20	0.231	0.168	0.405
10/4...10/10	310		0.157	0.048	0.205
10/11...10/17	310,31X	labstclay	0.116	0.044	0.16
10/18...10/24	31X.105	prodstclay	0.202	0.134	0.336
10/25...10/31	105,15X308250				
11/1...11/7	250,507				
11/8...11/14	507				
11/15...11/21					
11/22...11/28					
11/29...12/5					
12/6...12/12					
12/13...12/19					
12/20...12/26					

0.0608

0.1688

KILN Schedule c.p.d	Average Wet Tons/car	Wet Tons/Kiln/day	Dry Tons TOTAL /kiln/day
38	2.2	83.6	70.224
37	2.2	81.4	68.376
38-9.5.93	2.2	83.6	70.224
39-40	2.2	85.8	72.072
40	2.2	88	73.92
38-40	2.2	88	73.92
40-38	2.2	88	73.92
40	2.2	88	73.92
40	2.2	88	73.92
40	2.2	88	73.92
35	2.2	77	64.68
36	2.2	79.2	71.28
		0	0
		0	0
		0	0
		0	0
		0	0
		0	0

To date Average 0.1287 M/LOW 0.128
ALL FIGS M/HIGH 0.1311
av of avs

1993
YEAR AVERAGE %

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* SAMPLES SENT TO NSL FOR CROSS CHECKS

SCHEDULE OF 40 c.p.d thru'put 73.92 tons/day 2.2 tons average /car*0.84(-16% for moisture content)
0.1287% S IS EQUAL TO 69.4486 TONS SO2/KILN/YEAR

0.1311% S IS EQUAL TO 70.7437 TONS SO2/KILN/YEAR

Envisage Eric Hevener } w/d.
James Gray }
Greg Sinkovich - Thurs.

Particulate Sampling - Observation Checklist

Date: 11/17/93 & 11/18/93
Observer(s): Rick L. Miller - Center LAA

Facility: Metropolitan Industries 15 76 05 1149
Source: POO G #3 Kila (Tunnel Kila)
Test Firm: Envisage Environmental Inc.

Sampling Method(s):
RM 5 ☒; SA ☒; SB ☒; SD ☒; SE ☒; SF ☒; 8 ☒; 12 ☒; 17 ☒;
or other ☒ (If other, please describe.) 1-5, 6C, 7E, 10 & 13A

Are there any modifications to the specified reference method(s)?
Yes ☐; No ☒ (If yes, please describe modification.)

Do the inlet (if applicable) and outlet sampling locations meet the requirements specified in RM 1?
Yes ☒; No ☐ (If no, how was (were) the location(s) modified to allow sampling?)

If inlet/outlet sampling is being performed, are the samples being taken simultaneously? NA
Yes ☐; No ☒ (If no, be sure that the source operating parameters are the same when they switch from one to the other.)

If cyclonic flow is present and other sampling locations do not exist, how will the samples be withdrawn? NA
Directional probe technique ☐; Alignment technique ☐; other ☐
(If other, please describe.)

Is the sampling train set up properly, in accordance with the reference method or as agreed upon in the pre-test meeting?
Yes ☒; No ☐ (If no, correct problems and continue, if possible.)

Check to ensure that the sampling equipment has been recently calibrated (i.e., meter box, thermometers/thermocouples, pitot tubes, etc.) OK ☒; not OK ☐

Type of filter: Glass fiber
Is the filter assembly positioned properly?
Yes ☒; No ☐ (If no, adjust and continue, if possible. Please note that the filter may be changed during the test run; however, it is recommended that the entire filter assembly be changed.)

CO ~4	702 704	200 192	97.1	83
SO ₂ ~22	827 815		147.7	
NO _x ~60		88.1 89	49.48	18.5
VOC ~10	800 750		56	~50

blue - gas std. red - corresponding reading on Nitrogen
is less. If the sampling was stopped during the test run to
change a sampling train component, be sure the sampling train is
leak-checked again.)

Periodically record readings from the test firm's raw data
sheet(s) (i.e., delta H, delta P, initial gas volume, filter
numbers, filter box temperatures, etc.). Or photocopies of the
raw data sheets may be requested from the test firm. (Attach the
readings and/or photocopies to this checklist.)

Check to ensure that the sample train recovery procedures are
conducted properly (i.e., filter handling, probe wash, liquid
transfers, appropriate sample recovery solution(s), recovery of
nozzle catch, etc.).

Will there be additional sampling and/or analyses performed
(i.e., particle size distributions, back-half analysis, HCl
analysis, metals analysis, etc.)?

Yes ☒; No ☐ (If yes, please describe.) (13A) ^{HF} Fluorides (6C) SO₂
(7E) NO_x (10) CO

Metropolitan is having VOC & Pb analysis done also to document
results for their own purpose.

Optional checks/verifications:

The test firm may be asked to do a ten (10) minute run on their
dry gas meter for calibration verification. Operate the meter at
the delta H setting obtained from the test firm's calibration
sheet. Record the volume collected, the dry gas meter
temperature and the barometric pressure. Calculate a dry gas
meter calibration check value, Y_c, as follows:

$$Y_c = \frac{10}{V_m} \frac{[0.0319 * T_m]^{1/2}}{P_{bar}}$$

Where:

Y_c = dry gas meter calibration check value (dimensionless)
10 = ten minute verification run

Compare the Y_c value with the dry gas meter calibration factor Y
to determine that: 0.97 Y < Y_c < 1.03 Y. If the Y_c value is not
within this range the meter should be recalibrated and if
completed the run and/or test should be voided.

The test firm may be required to perform at least one actual
moisture determination. (This check should be performed after
the first run.)

Measure or have the test firm remeasure the nozzle diameter to
verify it's calibration. (This should be performed for each
nozzle utilized.)

Control Equipment - Compliance Demonstration Checklist

Electrostatic Precipitators (ESP):

Type (i.e., hot-side, cold-side, etc.): _____

Number of chambers (sections): _____

Number of fields/chamber: _____

Number and identification of the fields out of service during the test period: _____

Indicate the secondary voltage and current for each operating field: _____

Indicate the spark rate from each operating field: _____

Indicate the ESP's rapping sequence: _____

Indicate the temperature necessary to bring the ESP on line: _____

Additional information or comments: _____

* * * * *

Fabric Filter (baghouse):

Type of filtration (pulse jet, reverse air, shakers, etc.): _____

Number of compartments: _____

Number of bags/compartment: _____

Indicate pressure drop: _____

Indicate operating temperature: _____

Indicate the flow rate to the system: _____

Indicate the bag cleaning sequence: _____

Additional information or comments: _____

* * * * *

1201 Millerton Rd. SE
Canton, OH 44707

Mr. Philip McGuinness 484-8453

Ohio EPA Source Number	Source Identification/ Description	BAT Determination	Applicable Federal and OAC Rules	Permit Allowable Mass Emissions and/ or Control & Usage Requirements
P006	Natural Gas Fired Tile Tunnel Kiln; Kiln #3	Limit of Sulfur Content in Raw Mater- ials; Limit Of Amount of Raw Materials Used In a Day; Natural Gas Usage; 45 meter High Stack For Sources P004, P005 and P006	3745-31-05 3745-17-07 3745-18-06 (D)(1) 3745-17-11	3 lbs PM/hr 13.14 tons PM/yr <u>14.25 lbs SO₂/yr</u> *231.13 tons SO ₂ /yr 5 lbs NO _x /hr 21.9 tons NO _x /yr 2.2 lbs Fluorides/ hr; 9.64 tons Fluorides/yr

* The combined SO₂ emissions from P004, P005 and P006.

*52.77 lbs SO₂/hr.

1926 lbs SO₂/hr

Modification

SUMMARY
TOTAL PERMIT TO INSTALL ALLOWABLE EMISSIONS

Pollutant	Tons/Year
SO ₂	231.13 **
PM ²	13.14
NO _x	21.9
Fluorides	9.64

** Combined emissions from P004, P005 and P006.

PERFORMANCE TEST REQUIREMENTS

The permittee shall conduct, or have conducted, performance testing on the air contaminant source(s) in accordance with procedures approved by the Agency. Two copies of the written report shall be submitted and signed by the person responsible for the test, describing the test procedures followed and the results of such tests. The Director, or an Ohio EPA representative, shall be allowed to witness the tests, examine testing equipment, and require the acquisition or submission of data and information necessary to assure that the source operation and testing procedures provide a valid characterization of the emissions from the source and/or the performance of the control equipment.

ADDITIONAL SPECIAL TERMS AND CONDITIONS

1. The sulfur content of the raw materials (clay and shale) used in kilns [#1 (P004), #2 (P005) and #3 (P006)] shall not exceed .157% on a monthly weighted average. This limit may be adjusted based on the stack test results after startup. A weekly analysis of sulfur content taken from daily clay and shale samples should be determined.

At any one time, only two the three kilns can be using a 100% clay mix with no shale. The third kiln must be using a mix with a shale content of at least 40%.

No more than 79 tons of raw materials shall be used in each kiln in any one day.

The facility shall maintain monthly records which:

1. list the average sulfur content (percent) of daily clay and shale composite samples;
2. list the clay and sulfur content of mixes used in each kiln each day; and
3. list the daily tonnage of the clay and shale used in each kiln.

These monthly records shall be retained in the facility files for at least two (2) years and shall be made available for inspection upon request of the Director or any authorized representative of the Director during normal business hours.

This facility shall submit quarterly reports to the Canton City Health Department, Air Pollution Control Division, 420 Market Ave North, Canton, Ohio 44702, which summarize:

1. the monthly weighted average sulfur content of the raw materials (clay and shale) used;
2. the daily clay and shale content of raw material used; and
3. the daily tonnage of the raw materials (clay and shale) used in each of the three kilns.

These quarterly reports shall be submitted by February 15, May 15, August 15 and November 15 of each year and shall cover the previous calendar quarter.

2. The stack servicing kiln (P006) will be a minimum of 45 meters high above the ground.

PLANT Devo. CeramDATE 11/13RUN# 1CASE# 45 LOCATIONpage 1 of 3

POINT NUMBER	SAMPLE TIME	GAS METER READING	VELOCITY HEAD /Ap	ORIFICE PRESSURE	STACK TEMP	GAS METER TEMP IN	GAS METER TEMP OUT	PUMP VACUUM	FILTER HOLDER	IMPINGER TEMP
1	0/11.21	843.50	.02	1.7	262	58	55	4	250	45
2	35	845.55	.02	1.7	262	63	67	4	250	48
3	5	847.55	.02	1.7	262	74	69	5	250	48
4	75	849.47	.02	1.7	265	76	69	5	245	48
5	10	851.45	.02	1.7	265	77	66	5	249	48
6	12.5	853.55	.02	1.7	265	78	67	5	250	48
7	15	855.36	.02	1.7	265	79	68	5	250	48
8	17.5	857.35	.02	1.7	265	80	69	5	250	48
9	20	859.78	.03	2.5	264	81	67	5	250	48
10	22.5	861.70	.02	1.7	264	81	68	5	250	48
11	25	863.63	.02	1.7	264	82	68	5	250	48
12	27.5	865.70	.02	1.7	261	81	66	5	250	45
1	30	867.63	.02	1.7	260	66	62	5	250	45
2	32.5	869.56	.02	1.7	256	70	67	5	250	45
3	35	871.59	.02	1.7	256	75	63	5	247	48
4	37.5	873.56	.02	1.7	256	79	69	5	250	48
5	40	875.60	.02	1.7	260	79	65	5	250	48
6	42.5	877.52	.02	1.7	260	81	63	5	250	48
7	45	879.52	.02	1.7	261	81	67	5	250	48
8	47.5	881.42	.0201	.84	261	81	69	4	250	45
9	50	882.56	.01	.84	261	80	69	4	250	48
10	52.5	884.29	.01	.84	260	80	70	4	250	48
11	55	885.70	.01	.84	260	79	70	4	250	48
12	57.5	887.13	.01	.84	260	79	69	4	250	48
	60/12.36	883.56								

SAMPLE TRAIN LEAK CHECKS

PILOT TUBE LEAK CHECKS

PRE-TEST 0 CIN @ 15 "Hg POST-TEST 0 CIN @ 15 "HgPRE-TEST #2 0.0 @ 6.0 POST-TEST #2 0 @ 6.0114 @ 6.0114 @ 6.0

HP

PLANT 12-12 (Cofam) DATE 11/18/13 RUN# 2 CASE# 83 LOCATION

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POINT NUMBER	SAMPLE TIME	GAS METER READING	VELOCITY HEAD Δp	ORIFICE PRESSURE	STACK TEMP	GAS METER TEMP IN	GAS METER TEMP OUT	PUMP VACUUM	FILTER HOLDER	IMPINGER TEMP
1	0/12.9	888.83	.02	1.7	256	80	70	4.0	238	50
2	2.5	890.89	.02	1.7	259	81	70	4.0	240	50
3	5	892.90	.02	1.7	260	82	71	4.0	240	50
4	2.5	894.87	.02	1.7	260	82	72	4.0	241	50
5	10	896.91	.02	1.7	259	83	72	4.0	242	50
6	12.5	898.86	.02	1.7	260	83	72	4.0	243	51
7	15	900.82	.02	1.7	260	83	72	4.0	244	52
8	17.5	902.79	.02	1.7	259	84	73	4.0	245	52
9	20	904.78	.02	1.7	259	85	73	4.0	246	54
10	22.5	906.75	.02	1.7	258	85	73	4.0	246	54
11	25	908.76	.01	.84	258	85	74	4.0	248	54
12	27.5	910.19	.01	.84	259	85	74	4.0	249	55
1	30	911.68	.02	1.7	257	84	73	4.0	245	55
2	32.5	913.59	.02	1.7	255	84	73	4.0	244	55
3	35	915.55	.02	1.7	256	82	73	4.0	243	57
4	37.5	917.52	.02	1.7	256	82	73	4.0	242	57
5	40	919.46	.02	1.7	257	83	74	4.0	240	58
6	42.5	921.48	.02	1.7	257	84	75	4.0	240	58
7	44.5	923.43	.02	1.7	258	85	75	4.0	242	59
8	47.5	925.37	.02	1.7	259	86	75	4.0	243	60
9	50	927.35	.02	1.7	259	86	75	4.0	245	60
10	52.5	929.20	.02	1.7	260	86	75	4.0	247	62
11	55	931.23	.01	.84	260	87	75	4.0	248	62
12	57.5	933.20	.01	.84	259	87	75	4.0	250	62
240	60/	934.66								

SAMPLE TRAIN LEAK CHECKS

PITOT TUBE LEAK CHECKS

PRE-TEST 0 CFM @ 12 "Hg POST-TEST 0 CFM @ 15 "Hg

PRE-TEST #2 0.5 POST-TEST #20 6.5
 #4 0.5 #4 6.5

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PLANT Metro (Parric) DATE 18 Nov 63 NUM 3 CASE# 64 LOCATION page of

POINT NUMBER	SAMPLE TIME	GAS METER READING	VELOCITY HEAD (Ap)	ORIFICE PRESSURE	STACK TEMP	GAS METER IN	GAS METER OUT	PUMP VACUUM	FILTER HOLDER	IMPTIGER TEMP
1	0 322	938.19	.02	1.7	256	80	72	4.0	238	52
2	25	940.35	.02	1.7	258	80	72	4.0	238	52
3	5	942.19	.02	1.7	254	82	72	4.0	239	52
4	7.5	944.28	.02	1.7	253	82	73	4.0	240	54
5	10	946.15	.02	1.7	254	83	73	4.0	240	54
6	12.5	948.14	.02	1.7	252	83	73	4.0	241	55
7	15	950.12	.02	1.7	253	84	74	4.0	242	55
8	17.5	952.10	.02	1.7	254	85	74	4.0	243	55
9	20	954.08	.02	1.7	252	85	74	4.0	244	56
10	22.5	954.04	.02	1.7	253	86	74	4.0	245	56
11	25	957.98	.02	1.7	254	86	74	4.0	245	58
12	27.5	959.92	.02	1.7	254	86	74	4.0	248	58
1	30	961.88	.01	.84	255	87	74	4.0	248	59
2	32.5	963.28	.02	1.7	253	87	75	4.0	250	60
3	35	964.67	.02	1.7	253	88	75	4.0	250	60
4	37.5	966.60	.02	1.7	254	88	75	4.0	252	60
5	40	968.51	.02	1.7	254	88	76	4.0	253	60
6	42.5	970.44	.02	1.7	255	88	76	4.0	254	61
7	45	972.35	.02	1.7	253	87	76	4.0	255	61
8	47.5	974.35	.02	1.7	253	87	76	4.0	255	62
9	50	976.22	.02	1.7	254	87	77	4.0	253	67
10	52.5	978.16	.02	1.7	254	88	77	4.0	252	62
11	55	980.08	.02	1.7	253	88	77	4.0	250	63
12	57.5	982.04	.01	.84	252	88	77	4.0	248	63
60		983.98								

SAMPLE TRAIN LEAK CHECKS

PILLOT TUBE LEAK CHECKS

PRE-TEST 0 CFM @ 15" Hg POST-TEST 0 CFM @ 15" Hg PRE-TEST #2 0.6:2 POST-TEST #2 0.6:3
 #4 0.6:4 #4 0.6:4

(P3)

PLANT Metro Ceramics

DATE

8/23/93

RUN#

CASE# 81

LOCATION

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of

POINT NUMBER	SAMPLE TIME	GAS METER READING	VELOCITY HEAD /AP	ORIFICE PRESSURE	STACK TEMP	GAS METER TEMP IN	GAS METER TEMP OUT	PUMP VACUUM	FILTER HOLDER	IMPINGER TEMP
1	0 11.23	533.87	.02	2.3	753	102	62	5	235	50
2	2.5	535.83	.02	2.3	751	101	63	5	237	50
3	5	531.98	.02	2.3	260	98	63	5	238	50
4	7.5	540.11	.02	2.3	260	96	63	5	239	50
5	10	542.26	.02	2.3	265	95	63	5	240	51
6	12.5	544.42	.02	2.3	264	95	63	5	240	51
7	15	546.64	.02	2.3	265	94	63	5	242	51
8	17.5	549.10	.02	2.3	264	93	63	5	243	52
9	20	551.25	.03	3.55	263	94	63	5	243	52
10	22.5	553.44	.02	2.3	264	96	63	5	244	52
11	25	555.63	.02	2.3	256	96	63	5	246	52
12	27.5	557.84	.02	2.3	263	96	63	5	248	53
1	30	560.38	.02	2.3	264	95	63	5	250	53
2	32.5	562.49	.02	2.3	265	96	63	5	250	55
3	35	564.70	.02	2.3	256	95	61	5	246	55
4	37.5	566.86	.02	2.3	259	98	62	5	245	55
5	40	569.10	.02	2.3	260	99	62	5	243	55
6	42.5	571.20	.02	2.3	261	101	63	5	240	58
7	45	573.39	.02	2.3	261	101	64	5	240	58
8	47.5	575.55	.01	1.1	263	101	64	5	242	58
9	50	577.17	.01	1.1	264	101	64	5	243	59
10	52.5	578.78	.01	1.1	262	102	64	5	247	60
11	55	580.33	.01	1.1	261	102	65	5	246	60
12	57.5	581.90	.01	1.1	262	101	64	5	245	61
	60	583.47								

SAMPLE TUBES LEAK CHECKS

POT TUBE LEAK CHECKS

PRE-TEST 0 CFH @ 15 "Hg POST-TEST 0 CFH @ 15 "Hg
PRE-TEST #2 0 CFH @ 6.0 POST-TEST #2 0 CFH @ 6.0
PRE-TEST #4 0 CFH @ 6.0 POST-TEST #4 0 CFH @ 6.0

Date

PK

PLANT Metro Ceramics DATE 18 Nov 93 RUN# 2 CASE# 38

page of

LOCATION

POINT NUMBER	SAMPLE TIME	GAS METER READING	VELOCITY AP	VELOCITY HEAD	ORIFICE PRESSURE	STACK TEMP	GAS METER HI	TEMP OUT	PUMP VACUUM	FILTER HOLDER	HIPPIER TEMP
1	0	583.53	.02		2.3	250	86	56	5.0	238	52
2	2.5	585.40	.02		2.3	251	86	56	5.0	240	52
3	5	587.47	.02		2.3	260	89	57	5.0	240	52
4	7.5	589.56	.02		2.3	260	90	56	5.0	245	52
5	10	591.9	.02		2.3	259	89	57	5.0	245	52
6	12.5	593.60	.02		2.3	260	92	58	5.0	240	52
7	15	595.69	.02		2.3	260	93	58	5.5	240	52
8	17.5	597.79	.02		2.3	260	94	57	5.5	238	52
9	20	599.85	.02		2.3	258	95	58	5.5	239	52
10	22.5	601.89	.02		2.3	258	97	61	5.5	246	52
11	25	604.0	.01		1.1	258	97	61	5.5	246	52
12	27.5	605.6	.01		1.1	258	96	62	5.5	246	52
1	30	607.1	.02		2.3	249	94	60	5.0	237	52
2	32.5	609.0	.02		2.3	253	93	59	5.0	240	52
3	35	611.1	.02		2.3	249	94	60	5.0	240	52
4	37.5	613.25	.02		2.3	250	90	60	5.5	245	52
5	40.0	615.30	.02		2.3	250	90	60	5.5	245	52
6	42.5	617.49	.02		2.3	253	89	62	5.5	247	52
7	45	619.50	.02		2.3	255	90	61	5.5	247	52
8	47.5	621.59	.02		2.3	257	90	62	5.5	248	52
9	50	623.70	.02		2.3	255	91	62	5.5	250	52
10	52.5	625.82	.02		2.3	254	92	62	5.5	250	52
11	55	627.50	.01		1.1	254	93	63	5.5	246	52
12	57.5	629.0	.01		1.1	255	87	62	5.5	248	52
	60	630.4									

SAMPLE TRAIN LEAK CHECKS

PITOT TUBE LEAK CHECKS

PRE-TEST 0 CTH @ 15 "Hg POST-TEST 0 CTH @ 15 "Hg

PRE-TEST #2 0 @ 15 "Hg POST-TEST #2 0 @ 15 "Hg

PRE-TEST #1 0 @ 15 "Hg POST-TEST #1 0 @ 15 "Hg

76

20N 4/28

PLANT Metro Ceramics DATE 18 Nov 93 RUN# 3

CASE# 16

page of

LOCATION

POINT NUMBER	SAMPLE TIME	GAS METER READING	VELOCITY HEAD, /AP	ORIFICE PRESSURE	STACK TEMP	GAS METER IN	GAS METER TEMP OUT	PUMP VACUUM	FILTER HOLDER	IMPINGER TEMP
1	0	630.6	.02	2.30	250	97	65	6.0	240	54
2		632.67	.02	2.30	250	98	66	6.0	243	54
3	5	634.05	.02	2.30	253	99	69	6.0	242	54
4		636.54	.02	2.30	251	92	65	6.0	242	54
5	10	638.39	.02	2.30	251	91	65	6.0	245	54
6		640.50	.02	2.30	253	90	65	6.0	248	54
7	15	642.35	.02	2.30	252	90	65	6.0	250	54
8		644.32	.02	2.30	252	90	65	6.0	250	54
9	20	646.30	.02	2.30	254	92	66	6.0	254	54
10		648.29	.02	2.30	252	92	65	6.0	254	54
11	25	650.25	.02	2.30	251	93	65	6.0	255	54
12		652.15	.02	2.30	250	93	67	6.0	254	54
1	30	654.20	.01	1.10	251	94	66	5.0	250	54
2		655.70	.01	1.10	249	81	65	5.0	250	54
3	35	657.14	.01	1.10	249	82	65	5.0	249	54
4		658.65	.01	1.10	250	82	64	5.0	251	56
5	40	660.60	.02	2.30	249	84	64	5.0	249	56
6		662.70	.02	2.30	250	88	64	9.0	250	56
7	45	664.79	.02	2.30	251	88	64	9.0	247	56
8		666.90	.02	2.30	252	98	66	9.0	249	56
9	50	668.79	.02	2.30	250	101	66	9.0	245	56
10		671.89	.02	2.30	244	102	67	9.0	249	56
11	55	673.25	.02	2.30	252	103	67	9.0	248	56
12		675.40	.02	2.30	252	103	68	9.0	250	56
	60	677.50								

SAMPLE TRAIN LEAK CHECKS

PITOT TUBE LEAK CHECKS

PRE-TEST 0 CTH @ 15 "Hg POST-TEST 0 CTH @ 15 "Hg PRE-TEST #2 0 16.5 POST-TEST #2 0 16.5 PRE-TEST #4 0 6.2 POST-TEST #4 0 6.2

APPENDIX K

DEPA STACK TEST REVIEW SUMMARY FORM

APPLICATION NUMBER 1576051149 P006FACILITY NAME METROPOLITAN CERAMICSSOURCE DESCRIPTION (OR SCC CODE) KILN No. 3CONTROL EQUIPMENT NONEDATE(S) OF TEST NOV 17-18, 1993FINAL TEST REPORT RECEIVED ON DEC 21, 1993POLLUTANT(S) TESTED PM, SO₂, NO_x, HFTEST METHOD 1-5, 6C, 7E, 13TEST FIRM ENVISAGE ENVIRONMENTAL INC.

EMISSION RATES:									
	PM	SO ₂	NO _x	HF		PM	SO ₂	NO _x	HF
ACTUAL (lb(s)/hr)	0.84	1.99	2.92	1.99	ALLOWABLE	3	14.25	5	2.2

OPERATING RATES:

DURING TEST 5544 $\frac{LB}{HR}$ MAXIMUM 6160 $\frac{LB}{HR}$

EMISSION FACTOR:

COMMENTS: ALL TESTS PASSED. BIG MARGIN OF SO₂ IS BECAUSE MUCH OF S WAS CHEMICALLY BOUND TO CLAY AND NOT RELEASED TO BECOME SO₂

I HEREBY VERIFY THAT THE INFORMATION CONTAINED WITHIN THE STACK TEST REPORT HAS BEEN REVIEWED AND IT HAS BEEN DETERMINED THAT THE TEST PROCEDURES, ANALYSES AND CALCULATIONS ARE:

☒ AN ACCEPTABLE DEMONSTRATION OF CONFORMANCE WITH THE APPROVED TESTING METHODOLOGY.☐ AN UNACCEPTABLE DEMONSTRATION OF CONFORMANCE WITH THE APPROVED TESTING METHODOLOGY.

12/21/93

DATE OF REVIEW

REVIEWED BY Indy Jasko

- BASED ON 5 RUN AVERAGE
-- SPECIFY APPLICABLE UNITS
*** SPECIFY IN UNITS OF MASS INPUT

Run #11

VISIBLE EMISSION OBSERVATION FORM

COMPANY NAME <i>Metropolitan Industries</i>		
LOCATION <i>1201 Millerton Rd. SE</i>		
CITY <i>Canton</i> STATE <i>OH</i> ZIP <i>44707</i>		
PROCESS EQUIPMENT <i>Tile Tunnel Kiln #3</i>	OPERATING MODE <i>75 T/D MAX</i>	
CONTROL EQUIPMENT	OPERATING MODE	

DESCRIBE EMISSION POINT <i>Top of Red. Staircase stack - 5' in dia.</i>	
HEIGHT ABOVE GROUND LEVEL START <i>750'</i> END	HEIGHT RELATIVE TO OBSERVER START <i>150'</i> END
DISTANCE FROM OBSERVER START <i>700'</i> END	DIRECTION FROM OBSERVER START <i>N</i> END
VERTICAL ANGLE TO OBS. PT. START <i>15°</i> END	DIRECTION TO OBS. PT. START <i>N</i> END

DESCRIBE EMISSIONS START <i>continuous</i> END	
EMISSION COLOR <i>Blue/white</i>	IF WATER DROPLET PLUME ATTACHED ☐ DETACHED ☐ NA ☒
DISTANCE OF OBSERVATION POINT FROM EMISSION OUTLET START <i>4-5'</i> END	

DESCRIBE PLUME BACKGROUND START <i>sky</i> END	
BACKGROUND COLOR START <i>gray/white</i> END	SKY CONDITIONS START <i>broken</i> END
WIND SPEED <i>4-5 mph</i>	WIND DIRECTION START <i>E-SE</i> END
AMBIENT TEMP START <i>43°F</i> END	WET BULB TEMP RH PERCENT

STACK WITH PLUME SUN WIND	SOURCE LAYOUT SKETCH 	DRAW NORTH ARROW
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ADDITIONAL INFORMATION

FORM NUMBER		PAGE <i>1</i> OF <i>6</i>			
OBSERVATION DATE <i>11/18/93</i>		START TIME <i>11:23</i>	END TIME <i>11:53</i>		
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25	5	5	5	0	
26	0	0	0	0	
27	0	0	0	0	
28	0	5	0	5	
29	0	0	5	0	
30	0	0	0	5	

OBSERVER'S NAME (PRINT) <i>Rick L. Miller</i>		DATE <i>11/18/93</i>
OBSERVER'S SIGNATURE <i>Rick L. Miller</i>		
ORGANIZATION <i>Canton LAA</i>		
CERTIFIED BY <i>ETA</i>		DATE <i>9/93</i>

CONTINUED ON VEO FORM NUMBER				
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DATA REDUCTION TABLE

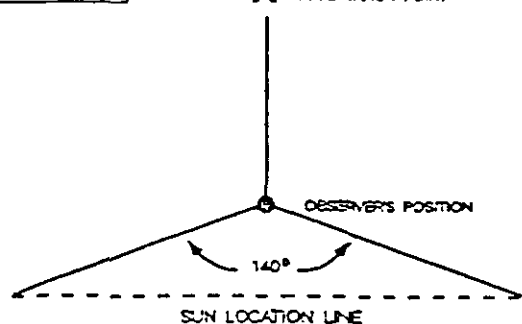
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FORM NUMBER PAGE 2 OF 6

OBSERVATION DATE 11/12/93	START TIME 11:53	END TIME 12:23
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25	0	0	0	0	
26	0	0	0	0	
27	0	0	0	0	
28	5	0	5	0	
29	0	0	0	0	
30	0	0	0	0	

STACK WITH PLUME  SUN  WIND 	SOURCE LAYOUT SKETCH <u>same</u> X OBSERVATION POINT DRAW NORTH ARROW 
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ADDITIONAL INFORMATION

OBSERVER'S NAME (PRINT) Rich L. Miller

OBSERVER'S SIGNATURE <i>Robert L. Miller</i>	DATE <i>11/18/93</i>
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ORGANIZATION Cantor LAA

CERTIFIED BY FIA DATE 9/93

CONTINUED ON VEO FORM NUMBER					
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VISIBLE EMISSION OBSERVATION FORM

COMPANY NAME Metropolitan Industries

LOCATION 1201 Millerston Rd SE

CITY Canton STATE OH ZIP 44707

PROCESS EQUIPMENT Tile Tunnel Kila #3 OPERATING MODE 757/0 max

CONTROL EQUIPMENT _____ OPERATING MODE _____

DESCRIBE EMISSION POINT
Top of Red. Stainless stack - 5' in dia.

HEIGHT ABOVE GROUND LEVEL START ~150' END _____

DISTANCE FROM OBSERVER START ~700' END _____

VERTICAL ANGLE TO OBS. PT. START 15° END _____

HEIGHT RELATIVE TO OBSERVER START ~150' END _____

DIRECTION FROM OBSERVER START N END _____

DIRECTION TO OBS. PT. START N END _____

DESCRIBE EMISSIONS
START intermittent END _____

EMISSION COLOR Black IF WATER DROPLET PLUME

START int. END _____ ATTACHED ☐ DETACHED ☐ NA ☒

DISTANCE OF OBSERVATION POINT FROM EMISSION OUTLET
START 4-5' END _____

DESCRIBE PLUME BACKGROUND
START 5' kg END _____

BACKGROUND COLOR gray/ult SKY CONDITIONS overcast

WIND SPEED 1-5 mph WIND DIRECTION E-SE

AMBIENT TEMP 44°F WET BULB TEMP _____ RH PERCENT _____

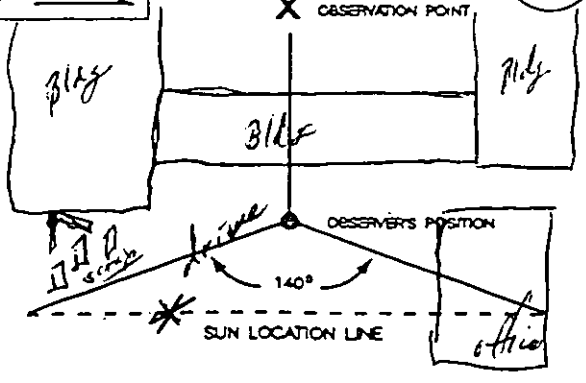
STACK WITH PLUME 

SUN 

WIND 

SOURCE LAYOUT SKETCH

DRAW NORTH ARROW 

OBSERVATION POINT 

DESCRIPTORS POSITION

SUN LOCATION LINE

ADDITIONAL INFORMATION

FORM NUMBER _____ PAGE 3 OF 6

OBSERVATION DATE		START TIME		END TIME	
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25	0	0	0	0	
26	0	0	0	0	
27	0	0	0	0	
28	0	0	0	0	
29	0	0	0	0	
30	0	0	0	0	

OBSERVER'S NAME (PRINT) Rich L. Miller

OBSERVER'S SIGNATURE Rich L. Miller DATE 11/18/93

ORGANIZATION Canton LAA

CERTIFIED BY ETA DATE 9/93

CONTINUED ON VEO FORM NUMBER _____

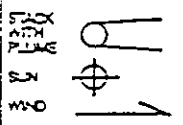
DATA REDUCTION TABLE

[illegible]

FORM NUMBER	PAGE 4 OF 6
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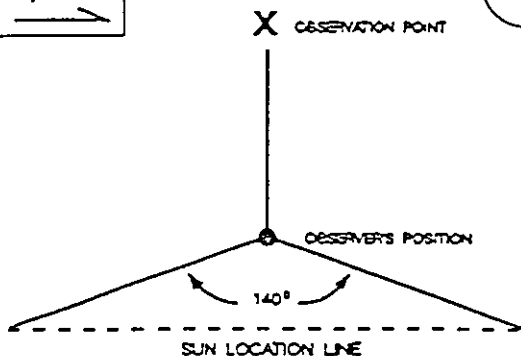
OBSERVATION DATE 11/18/93	START TIME 13:55	END TIME 14:25
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7	0	0	0	0	*switching pen to
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25	5	5	0	0	
26	0	0	0	0	
27	0	0	0	0	
28	0	0	0	0	
29	0	0	0	0	
30	0	0	0	0	



SOURCE LAYOUT SKETCH

DRAW NORTH ARROW



ADDITIONAL INFORMATION

OBSERVER'S NAME (PRINT) _____

OBSERVER'S SIGNATURE	DATE
----------------------	------

ORGANIZATION *Cantor LAA*

CERTIFIED BY: ETA DATE: 9/93

CONTINUED ON VEO FORM NUMBER _____

Run #3

VISIBLE EMISSION OBSERVATION FORM

COMPANY NAME
Metropolitan Industries

LOCATION
1701 Millerton Rd. SE

CITY
Canton STATE
OH ZIP
44707

PROCESS EQUIPMENT
Tile Tunnel Kilm #3 OPERATING MODE
25 T/D max.

CONTROL EQUIPMENT
OPERATING MODE

DESCRIBE EMISSION POINT
Top of Rad. stainless steel - 5' in dia.

HEIGHT ABOVE GROUND LEVEL
START *~150'* END

HEIGHT RELATIVE TO OBSERVER
START *~150'* END

DISTANCE FROM OBSERVER
START *~750'* END

VERTICAL ANGLE TO OBS. PT.
START *15°* END

DIRECTION FROM OBSERVER
START *NE* END

DIRECTION TO OBS. PT.
START *NE* END

DESCRIBE EMISSIONS
START *intermittent* END *(detached)*

EMISSION COLOR
START *whit.* END

IF WATER DROPLET PLUME
ATTACHED ☐ DETACHED ☐ NA ☒

DISTANCE OF OBSERVATION POINT FROM EMISSION OUTLET
START *4-5'* END

DESCRIBE PLUME BACKGROUND
START *sky* END

BACKGROUND COLOR
START *blue* END

WIND SPEED
START *1-3 mph* END

WIND DIRECTION
START END

AMBIENT TEMP
START *45°F* END

WET BULB TEMP
RH PERCENT

STACK WITH PLUME
SUN
WIND

SOURCE LAYOUT SKETCH
DRAW NORTH ARROW

OBSERVATION POINT

OBSERVER'S POSITION

SUN LOCATION LINE

140°

Blg.

Drive

ADDITIONAL INFORMATION

FORM NUMBER

PAGE *5* OF

OBSERVATION DATE
11/18/93

START TIME
15:21

END TIME
15:51

SEC MIN	0	15	30	45	COMMENTS
1	0	0	0	0	
2	0	0	5	5	<i>excellent blue background</i>
3	5	5	5	5	<i># bright sun</i>
4	5	5	5	5	
5	5	5	5	5	
6	5	5	5	5	
7	5	5	5	5	
8	5	5	5	5	
9	5	5	5	5	
10	5	5	5	0	
11	5	5	5	5	
12	5	5	5	5	
13	5	5	5	5	
14	0	5	0	5	
15	5	5	5	5	
16	5	5	5	5	
17	5	5	5	5	
18	5	5	5	5	
19	5	5	5	5	
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21	5	5	5	5	
22	5	5	5	5	
23	5	5	5	5	
24	5	5	5	5	
25	5	5	5	5	
26	5	5	5	5	
27	5	5	5	5	
28	5	5	5	5	
29	5	5	5	5	
30	5	5	5	5	

OBSERVER'S NAME (PRINT)
Rich L. Miller

OBSERVER'S SIGNATURE
Rich L. Miller DATE
11/18/93

ORGANIZATION
Canton L. Ind.

CERTIFIED BY
ETA DATE
9/93

CONTINUED ON VEO FORM NUMBER

DATA REDUCTION TABLE

[illegible]

FORM NUMBER	PAGE 6 OF 6
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OBSERVATION DATE 11/18/93	START TIME 15:51	END TIME 16:31
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SEC MIN	0	15	30	45	COMMENTS
1	5	5	5	5	
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3	5	5	5	5	
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11	5	0	5	5	
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23	5	5	5	5	
24	5	5	5	5	
25	5	5	5	5	
26	5	5	5	5	
27	5	5	5	—	semi-blocked view
28	5	5	5	5	
29	5	5	5	5	
30	5	5	5	5	

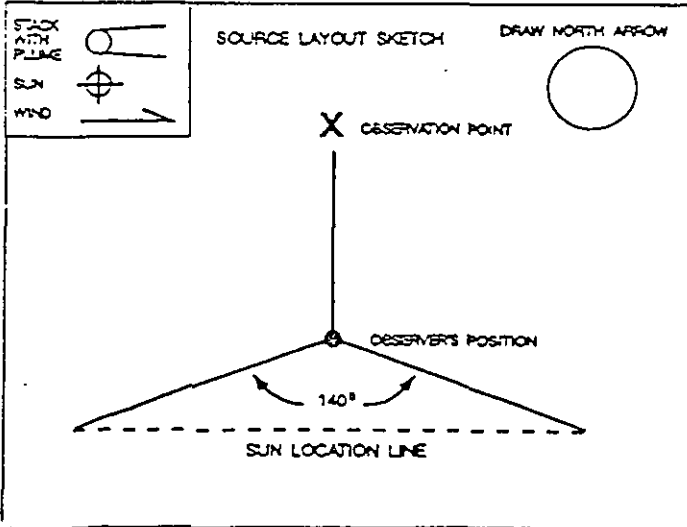
OBSERVER'S NAME (PRINT) Rich L. Miller

OBSERVER'S SIGNATURE <i>Paul L. Miller</i>	DATE 11/18/43
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ORGANIZATION Carter LHA 1-1

CERTIFIED BY ETA DATE 9/93

CONTINUED ON VEO FORM NUMBER				
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OPTIONAL INFORMATION