

Note: This is a reference cited in *AP 42, Compilation of Air Pollutant Emission Factors, Volume I Stationary Point and Area Sources*. AP42 is located on the EPA web site at [www.epa.gov/ttn/chief/ap42/](http://www.epa.gov/ttn/chief/ap42/)

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**USS CLAIRTON WORKS  
RESULTS OF THE  
COMPLIANCE DEMONSTRATION  
OF THE #3 BATTERY COMBUSTION STACK**

**Prepared for:**

**USS CLAIRTON WORKS  
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CLAIRTON, PA**

**Prepared by:**

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3000 TECH CENTER DRIVE  
MONROEVILLE, PA 15145**

**PROJECT NO. 601050-06**

**SEPTEMBER 1990**

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## **ABSTRACT**

On August 1, 1990, a compliance test program was conducted for USS Clairton Works, Clairton, PA, on the #3 Battery Combustion Stack operated at the Clairton Coke and Coal Chemical Works. The purpose of the testing was to determine the (1) concentration and mass emissions of particulate matter, and (2) presence of visible emissions from the stack as required by the Amended Mon Valley Consent Decree, Paragraph V.A.(6) and Appendix 4.A. The results of the testing showed an average particulate matter concentration and emission rate of 0.012 gr/scfd and 3.86 lb/hr, respectively. The allowable concentration is 0.030 gr/scfd. Thus, the emissions from the stack are in compliance. No visible emissions were observed from the stack during any of the tests.

## **1.0 INTRODUCTION**

On August 1, 1990, a compliance test program was conducted for USS Clairton Works, Clairton, PA, on the #3 Battery Combustion Stack operated at the Clairton Coke and Coal Chemical Works. The purpose of the testing was to determine the (1) concentration and mass emissions of particulate matter, and (2) presence of visible emissions from the stack as required by the Amended Mon Valley Consent Decree, Paragraph V.A.(6) and Appendix 4.A.

Testing was performed by the Air Quality Engineering Division of Keystone Environmental Resources, Inc. (Keystone). The test crew was comprised of Mark Grunebach, Manager of the Monitoring Services Department, and Richard Casselberry. Visible emissions determinations were performed by Ken Kuiros and Jim McKoy of Environmental Technical Services (ETS). Keystone and ETS are sister companies under the Chester Environmental Group. All test procedures were witnessed by Phil Lawrence of the Allegheny County Health Department.

## **2.0 METHODOLOGIES**

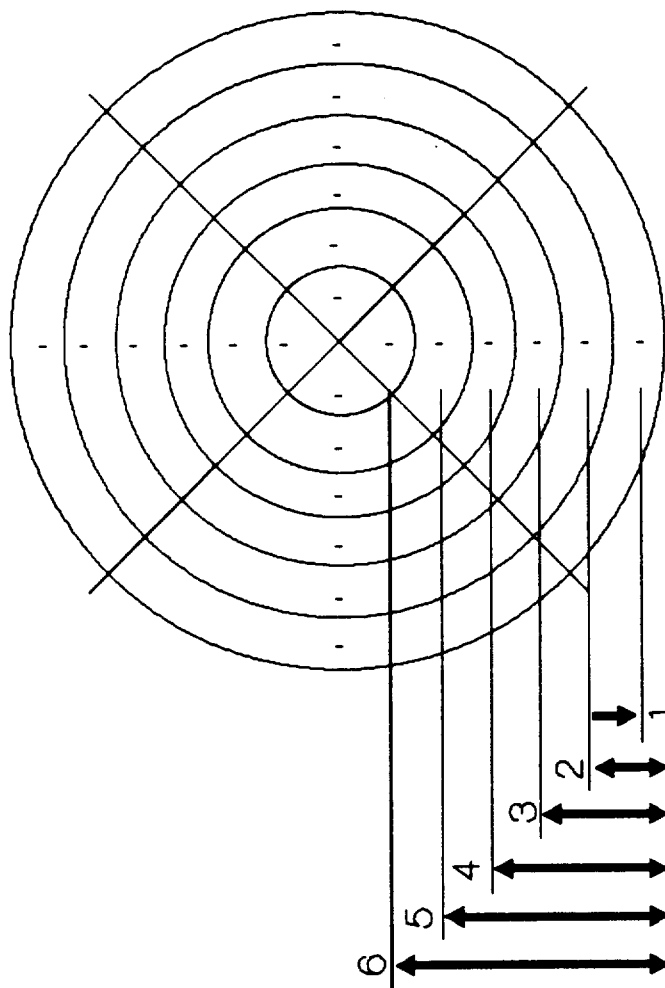
Particulate matter sampling was performed in accordance with EPA Stationary Source Sampling Methods 1 through 5. The gas volume sampled for each 120 minute test was greater than 50 dry standard cubic feet.

The process exhaust exited through a 114" diameter stack. A total of 24 traverse points (12 per diameter) were sampled; the traverse points were calculated in accordance with EPA Method 1. Sampling was conducted through 4 equally spaced ports, with each traverse point sampled for 5 minutes. A schematic diagram of the stack and traverse points is presented in Figure 2-1.

A total of three test runs were performed. During each test, gas concentrations of CO<sub>2</sub>, O<sub>2</sub>, and N<sub>2</sub> (by difference) were determined with the use of a Fyrite apparatus as specified by EPA Method 3.

Clean up of the sampling train included an acetone rinse of the front-half components. The water soluble and water insoluble portions of the front-half of the sampling train were determined as a total. The rinses were dried, desiccated, and weighed to a constant weight. These weights were added to the filter weights to determine the total catch. These procedures followed the methodology of EPA Method 5.

All visible emissions determinations were performed in accordance with EPA Stationary Source Sampling Method 9. Visible emissions were recorded for the duration of each particulate matter test.

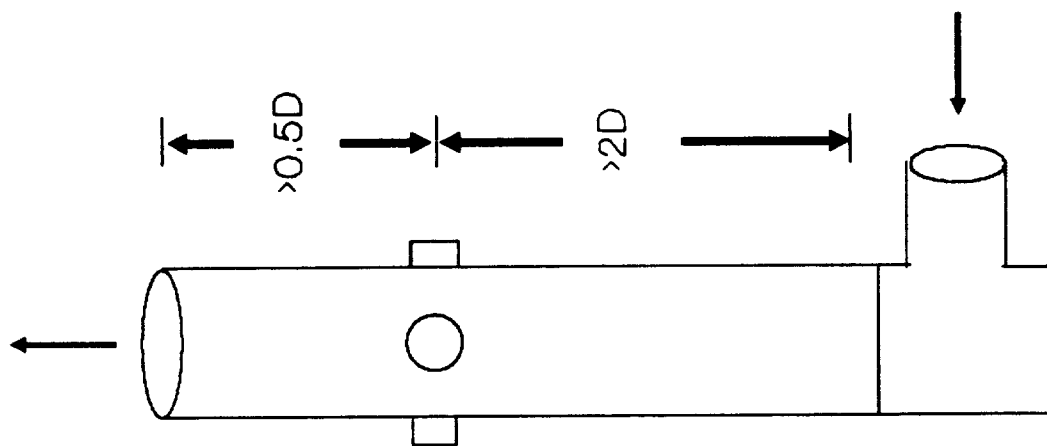


Distance  
(in.)

2.4  
7.6  
13.5  
20.2  
28.5  
40.6

Traverse  
Point

1 2 3 4 5 6



2-1a

Stack Diameter (in.) = 114  
D

ACTIVITY  
No.

REVISION

TITLE

SCHEMATIC DIAGRAM OF THE  
STACK AND TRAVERSE POINTS

FIGURE 2-1

### 3.0 RESULTS

All testing was performed during periods of normal plant operation. To validate this, copies of the operational data can be found in Appendix A.

The probes and sampling trains were operate in accordance with EPA Stationary Source Sampling Methods 1 through 5. Copies of the pre-test calibration results, post-test calibration results, and the results of an audit conducted with a critical orifice provided by the Allegheny County Health Department can be found in Appendix B.

Copies of the field data sheets for the particulate matter sampling can be found in Appendix C. The emissions calculations for each test can be found in Appendix D. The results have been summarized in Table 3-1. The average particulate matter concentration and emission rate are 0.012 grains per standard cubic foot dry (gr/scfd) and 3.86 pounds per hour (lb/hr), respectively.

As promulgated by the Amended Mon Valley Consent Decree, Paragraph V.A.(6), the particulate matter standard for #3 Battery Combustion Stack is 0.030 gr/scfd. Thus, the emissions from the stack are in compliance.

Table 3-1 also lists other pertinent stack and sampling parameters including the stack gas flow rate in units of actual cubic feet per minute (acfm) and standard cubic feet per minute (scfm), moisture content of the stack gas, stack gas temperature, gas volume sampled for each test (scfd), and the isokinetics value for each test. The isokinetics value is equal to the ratio of the average linear gas velocity sampled through the probe nozzle to the average stack gas velocity. An isokinetics value between 90% and 110% is considered acceptable.

Copies of the field data sheets for the visible emissions determinations can be found in Appendix E. No visible emissions were observed during any of the three tests. As promulgated by the Amended Mon Valley Consent Decree, Paragraph V.A.(6), the visible emissions shall not equal or exceed 20% opacity for a period or periods

**USS CLAIRTON WORKS  
CLAIRTON, PA**

**TABLE 3-1**

**PARTICULATE MATTER EMISSIONS DATA**

| <b><u>EMISSIONS</u></b> | <b><u>TEST<br/>#1</u></b> | <b><u>TEST<br/>#2</u></b> | <b><u>TEST<br/>#3</u></b> | <b><u>AVERAGE</u></b> |
|-------------------------|---------------------------|---------------------------|---------------------------|-----------------------|
| gr/dscf                 | 0.011                     | 0.010                     | 0.014                     | 0.012                 |
| lb/hr                   | 3.41                      | 3.09                      | 5.08                      | 3.86                  |

**STACK  
CONDITIONS**

|                         |       |       |       |       |
|-------------------------|-------|-------|-------|-------|
| Flow (acfm)             | 80021 | 84075 | 91948 | 85348 |
| Flow (scfm)             | 41492 | 43398 | 47781 | 44224 |
| Moisture<br>Content (%) | 14.16 | 14.14 | 13.36 | 13.89 |
| Stack<br>Temp. (°F)     | 541   | 545   | 539   | 542   |

**SAMPLING  
CONDITIONS**

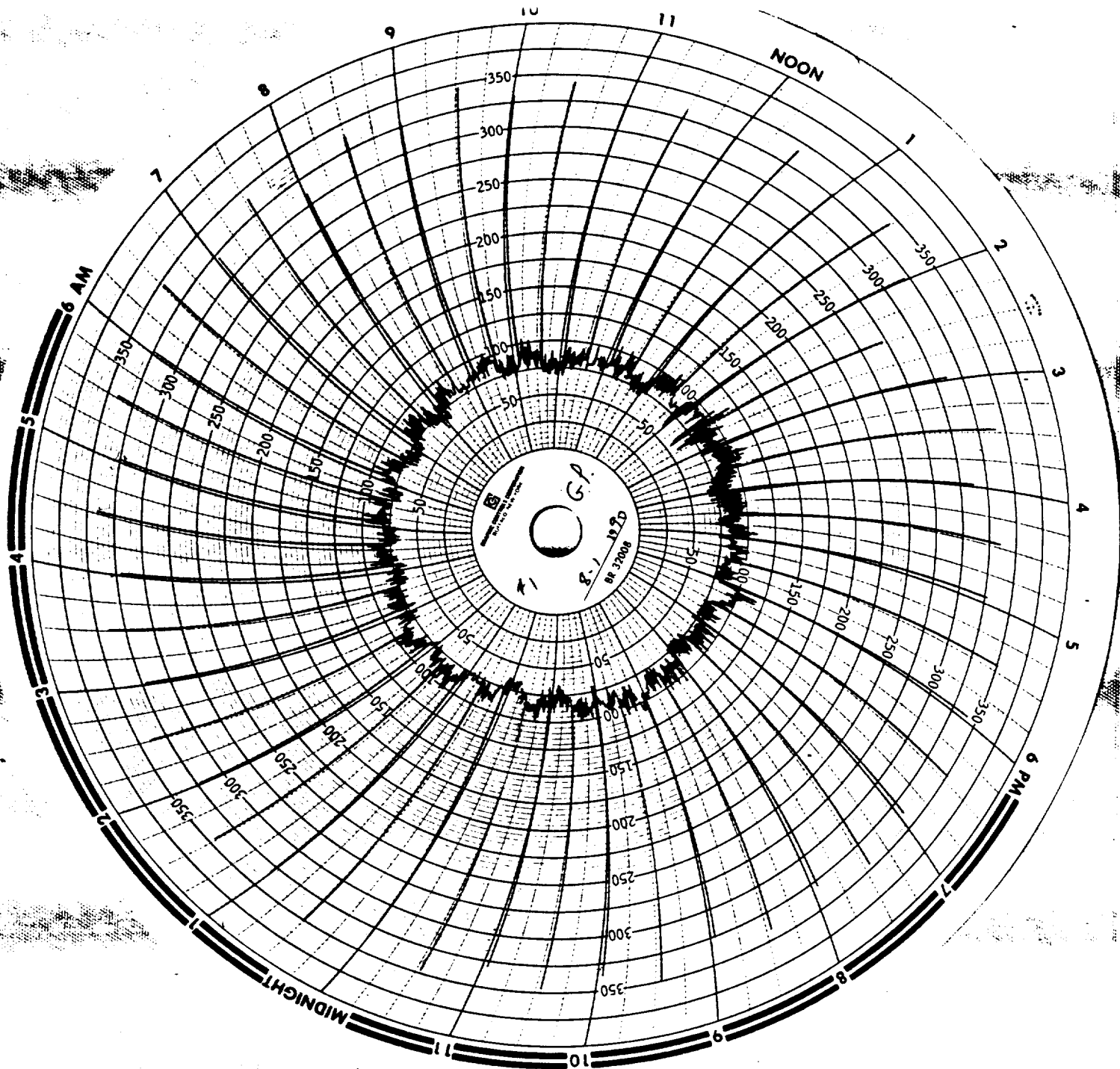
|                         |        |        |        |  |
|-------------------------|--------|--------|--------|--|
| Sampling<br>Time (min)  | 120    | 120    | 120    |  |
| Sample<br>Volume (scfd) | 75.613 | 79.819 | 88.581 |  |
| Isokinetics<br>(%)      | 92.33  | 93.16  | 93.07  |  |

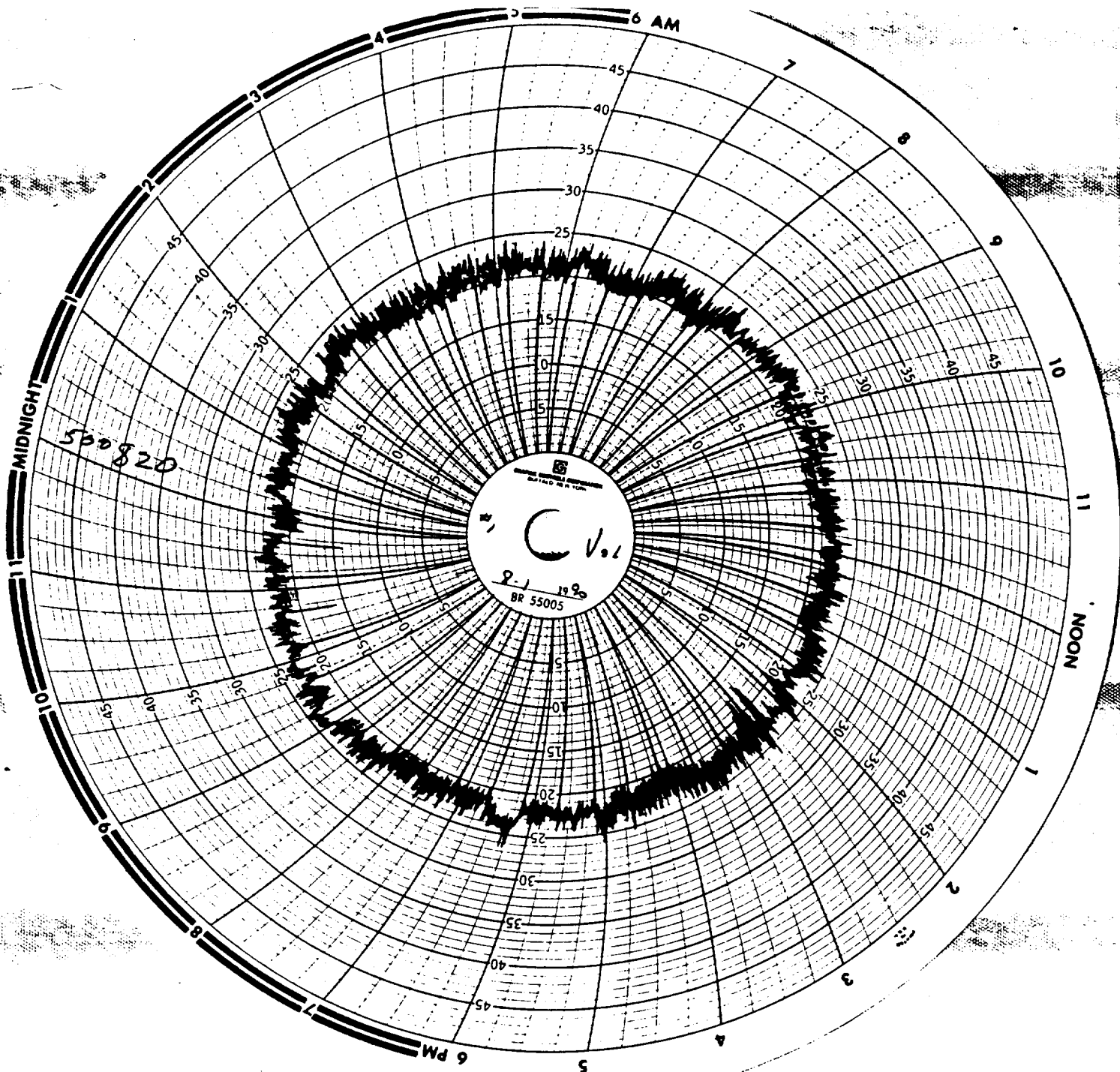


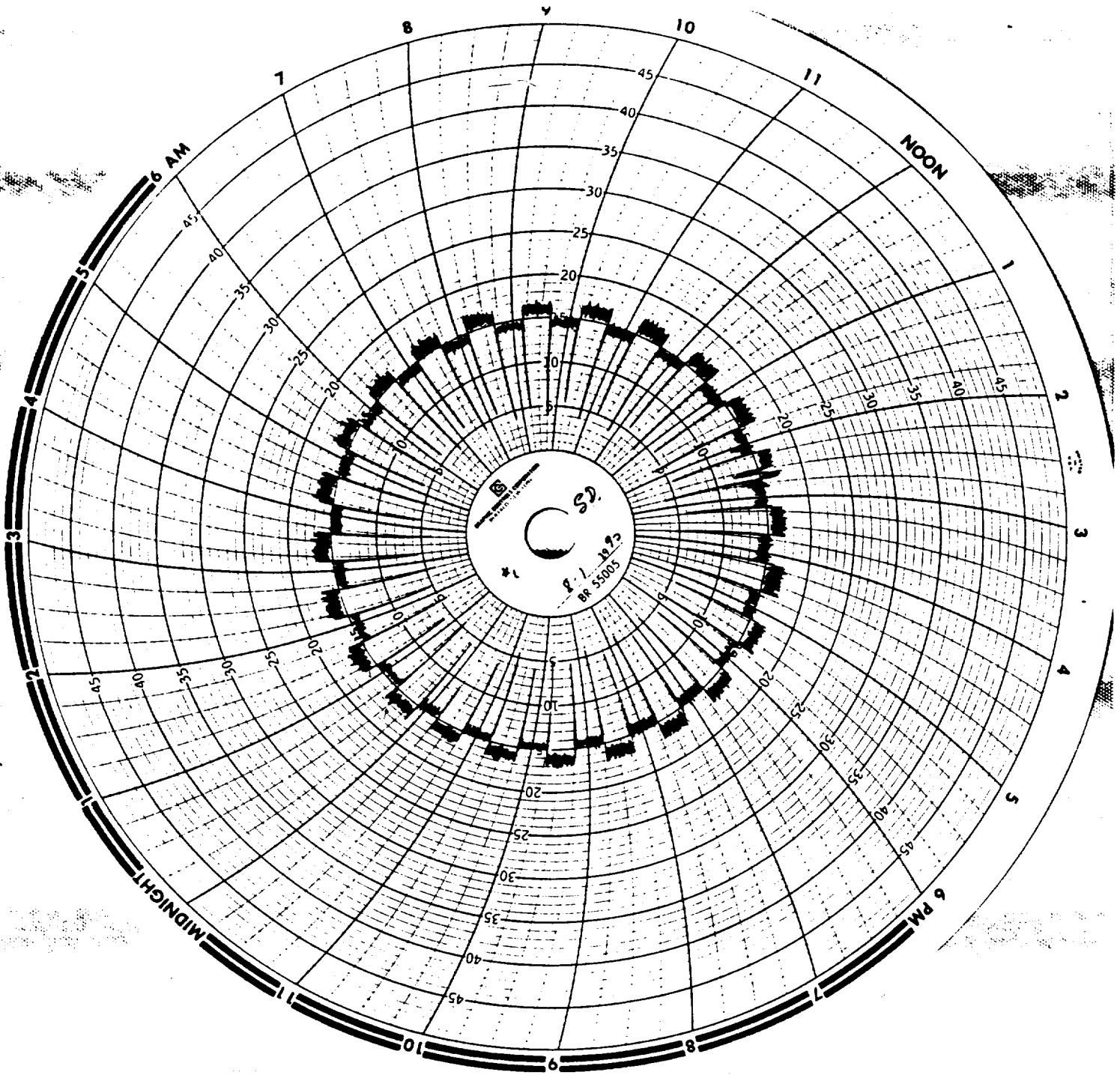
aggregating in excess of 3 minutes in any 60-minute period and shall never equal or exceed 60% opacity. Thus, the emissions are in compliance.

**USS CLAIRTON WORKS  
RESULTS OF THE  
COMPLIANCE DEMONSTRATION OF THE  
#3 BATTERY COMBUSTION STACK**

**APPENDIX A  
OPERATIONAL RECORDS**







# ROUTING SCHEDULE FOR BATTERIES

| STO # | PUSH  | CHARGE | STATION | EARLIEST | DESIRED | LATEST |
|-------|-------|--------|---------|----------|---------|--------|
| 1     | A23/1 | A21/1  | 1       | 11:45    | 12:00   | 12:20  |
| 2     | B23/1 | B21/1  | 1       | 11:51    | 12:06   | 12:26  |
| 3     | B23/1 | B21/1  | 1       | 11:57    | 12:12   | 12:32  |
| 4     | A23/1 | A21/1  | 1       | 12:03    | 12:18   | 12:38  |
| 5     | B23/1 | B21/1  | 1       | 12:09    | 12:24   | 12:44  |
| 6     | B23/1 | B21/1  | 1       | 12:15    | 12:30   | 12:50  |
| 7     | A23/1 | A21/1  | 1       | 12:21    | 12:36   | 12:56  |
| 8     | B23/1 | B21/1  | 1       | 12:27    | 12:42   | 13:02  |
| 9     | B23/1 | B21/1  | 1       | 12:33    | 12:48   | 13:08  |
| 0     | A23/1 | A21/1  | 1       | 12:39    | 12:54   | 13:14  |
| 1     | A23/1 | A21/1  | 1       | 12:45    | 13:00   | 13:20  |
| 2     | B23/1 | B21/1  | 1       | 12:51    | 13:06   | 13:26  |
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| 6     | B23/1 | B21/1  | 1       | 14:15    | 14:30   | 14:50  |
| 7     | A23/1 | A21/1  | 1       | 14:21    | 14:36   | 14:56  |
| 8     | B23/1 | B21/1  | 1       | 14:27    | 14:42   | 15:02  |
| 9     | B23/1 | B21/1  | 1       | 14:33    | 14:48   | 15:08  |
| 0     | A23/1 | A21/1  | 1       | 14:39    | 14:54   | 15:14  |
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| 8     | B23/1 | B21/1  | 1       | 15:27    | 15:42   | 16:02  |
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| 0     | A23/1 | A21/1  | 1       | 21:39    | 21:54   | 22:14  |
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| 7     | A23/1 | A21/1  | 1       | 24:21    | 24:36   | 24:56  |
| 8     | B23/1 | B21/1  | 1       | 24:27    | 24:42   | 25:02  |
| 9     | B23/1 | B21/1  | 1       | 24:33    | 24:48   | 25:08  |
| 0     | A23/1 | A21/1  | 1       | 24:39    | 24:54   | 25:14  |
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| 8     | B23/1 | B21/1  | 1       | 25:27    | 25:42   | 26:02  |
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| 8     | B23/1 | B21/1  | 1       | 26:27    | 26:42   | 27:02  |
| 9     | B23/1 | B21/1  | 1       | 26:33    | 26:48   | 27:08  |
| 0     | A23/1 | A21/1  | 1       | 26:39    | 26:54   | 27:14  |
| 1     | A23/1 | A21/1  | 1       | 26:45    | 27:00   | 27:20  |
| 2     | B23/1 | B21/1  | 1       | 26:51    | 27:06   | 27:26  |
| 3     | B23/1 | B21/1  | 1       | 26:57    | 27:12   | 27:32  |
| 4     | A23/1 | A21/1  | 1       | 27:03    | 27:18   | 27:38  |
| 5     | B23/1 | B21/1  | 1       | 27:09    | 27:24   | 27:44  |
| 6     | B23/1 | B21/1  | 1       | 27:15    | 27:30   | 27:50  |
| 7     | A23/1 | A21/1  | 1       | 27:21    | 27:36   | 27:56  |
| 8     | B23/1 | B21/1  | 1       | 27:27    | 27:42   | 28:02  |
| 9     | B23/1 | B21/1  | 1       | 27:33    | 27:48   | 28:08  |
| 0     | A23/1 | A21/1  | 1       | 27:39    | 27:54   | 28:14  |
| 1     | A23/1 | A21/1  | 1       | 27:45    | 28:00   | 28:20  |
| 2     | B23/1 | B21/1  | 1       | 27:51    | 28:06   | 28:26  |
| 3     | B23/1 | B21/1  | 1       | 27:57    | 28:12   | 28:32  |
| 4     | A23/1 | A21/1  | 1       | 28:03    | 28:18   | 28:38  |
| 5     | B23/1 | B21/1  | 1       | 28:09    | 28:24   | 28:44  |
| 6     | B23/1 | B21/1  | 1       | 28:15    | 28:30   | 28:50  |
| 7     | A23/1 | A21/1  | 1       | 28:21    | 28:36   | 28:56  |
| 8     | B23/1 | B21/1  | 1       | 28:27    | 28:42   | 29:02  |
| 9     | B23/1 | B21/1  | 1       | 28:33    | 28:48   | 29:08  |
| 0     | A23/1 | A21/1  | 1       | 28:39    | 28:54   | 29:14  |
| 1     | A23/1 | A21/1  | 1       | 28:45    | 29:00   | 29:20  |
| 2     | B23/1 | B21/1  | 1       | 28:51    | 29:06   | 29:26  |
| 3     | B23/1 | B21/1  | 1       | 28:57    | 29:12   | 29:32  |
| 4     | A23/1 | A21/1  | 1       | 29:03    | 29:18   | 29:38  |
| 5     | B23/1 | B21/1  | 1       | 29:09    | 29:24   | 29:44  |
| 6     | B23/1 | B21/1  | 1       | 29:15    | 29:30   | 29:50  |
| 7     | A23/1 | A21/1  | 1       | 29:21    | 29:36   | 29:56  |
| 8     | B23/1 | B21/1  | 1       | 29:27    | 29:42   | 30:02  |
| 9     | B23/1 | B21/1  | 1       | 29:33    | 29:48   | 30:08  |
| 0     | A23/1 | A21/1  | 1       | 29:39    | 29:54   | 30:14  |
| 1     | A23/1 | A21/1  | 1       | 29:45    | 30:00   | 30:20  |
| 2     | B23/1 | B21/1  | 1       | 29:51    | 30:06   | 30:26  |
| 3     | B23/1 | B21/1  | 1       | 29:57    | 30:12   | 30:32  |
| 4     | A23/1 | A21/1  | 1       | 30:03    | 30:18   | 30:38  |
| 5     | B23/1 | B21/1  | 1       | 30:09    | 30:24   | 30:44  |
| 6     | B23/1 | B21/1  | 1       | 30:15    | 30:30   | 30:50  |
| 7     | A23/1 | A21/1  | 1       | 30:21    | 30:36   | 30:56  |
| 8     | B23/1 | B21/1  | 1       | 30:27    | 30:42   | 31:02  |
| 9     | B23/1 | B21/1  |         |          |         |        |

| SEQ # | PUSH  | CHARGE | STATION | EARLIEST | DESIRED | LATEST |
|-------|-------|--------|---------|----------|---------|--------|
| 1     | B16/3 | B14/3  |         | 7:45     | 8:0     | 8:20   |
| 2     | A18/1 | A16/1  |         | 7:51     | 8:6     | 8:26   |
| 3     | A18/2 | A16/2  |         | 7:57     | 8:12    | 8:32   |
| 4     | A18/1 | A16/1  |         | 8:03     | 8:18    | 8:38   |
| 5     | A18/3 | A16/3  |         | 8:09     | 8:24    | 8:44   |
| 6     | A18/2 | A16/2  |         | 8:15     | 8:30    | 8:50   |
| 7     | B18/3 | B16/3  |         | 8:21     | 8:36    | 8:56   |
| 8     | A20/1 | A18/1  |         | 8:28     | 8:43    | 9:3    |
| 9     | B20/2 | B18/2  |         | 8:34     | 8:49    | 9:9    |
| 10    | B20/1 | B18/1  |         | 8:40     | 8:55    | 9:15   |
| 11    | A20/3 | A18/3  |         | 8:46     | 9:1     | 9:21   |
| 12    | B20/3 | B18/3  |         | 8:52     | 9:7     | 9:27   |
| 13    | A20/3 | A18/3  |         | 8:58     | 9:13    | 9:33   |
| 14    | A20/1 | A200/1 |         | 9:4      | 9:19    | 9:40   |
| 15    | B20/2 | B200/2 |         | 9:11     | 9:26    | 9:46   |
| 16    | B20/3 | B200/3 |         | 9:17     | 9:32    | 9:52   |
| 17    | A20/3 | A200/3 |         | 9:23     | 9:38    | 9:58   |
| 18    | B20/3 | B200/3 |         | 9:29     | 9:44    | 10:4   |
| 19    | B20/3 | B200/3 |         | 9:35     | 9:50    | 10:10  |
| 20    | A20/4 | A200/4 |         | 9:41     | 9:56    | 10:16  |
| 21    | B20/2 | B200/2 |         | 9:48     | 10:3    | 10:23  |
| 22    | A20/4 | A200/4 |         | 9:54     | 10:9    | 10:29  |
| 23    | A20/3 | A200/3 |         | 10:0     | 10:15   | 10:35  |
| 24    | A20/4 | A200/4 |         | 10:6     | 10:21   | 10:41  |
| 25    | B20/3 | B200/3 |         | 10:12    | 10:27   | 10:47  |
| 26    | A20/6 | A200/6 |         | 10:18    | 10:33   | 10:53  |
| 27    | B20/2 | B200/2 |         | 10:25    | 10:40   | 11:0   |
| 28    | B20/3 | B200/3 |         | 10:31    | 10:46   | 11:6   |
| 29    | A20/6 | A200/6 |         | 10:37    | 10:52   | 11:12  |
| 30    | A20/6 | A200/6 |         | 10:43    | 10:58   | 11:18  |
| 31    | B20/3 | B200/3 |         | 10:49    | 11:4    | 11:24  |
| 32    | A20/8 | A200/8 |         | 10:55    | 11:10   | 11:30  |
| 33    | B20/8 | B200/8 |         | 11:1     | 11:16   | 11:36  |
| 34    | A20/8 | A200/8 |         | 11:8     | 11:23   | 11:43  |
| 35    | A20/3 | A200/3 |         | 11:14    | 11:29   | 11:49  |
| 36    | A20/8 | A200/8 |         | 11:20    | 11:35   | 11:55  |
| 37    | B20/3 | B200/3 |         | 11:26    | 11:41   | 12:1   |
| 38    | A20/0 | A200/0 |         | 11:32    | 11:47   | 12:7   |
| 39    | B20/2 | B200/2 |         | 11:38    | 11:53   | 12:13  |
| 40    | A20/1 | A200/1 |         | 11:45    | 12:0    | 12:20  |
| 41    | A20/3 | A200/3 |         | 11:51    | 12:6    | 12:26  |
| 42    | B20/3 | B200/3 |         | 11:57    | 12:12   | 12:32  |
| 43    | A20/3 | A200/3 |         | 12:3     | 12:18   | 12:38  |
| 44    | A20/1 | A200/1 |         | 12:9     | 12:24   | 12:44  |
| 45    | C20/1 | C200/1 |         | 12:15    | 12:30   | 12:50  |
| 46    | C20/1 | C200/1 |         | 12:21    | 12:36   | 12:56  |
| 47    | C20/1 | C200/1 |         | 12:28    | 12:43   | 13:3   |
| 48    | A20/3 | A200/3 |         | 12:34    | 12:49   | 13:9   |
| 49    | A20/3 | A200/3 |         | 12:40    | 12:55   | 13:15  |
| 50    | B20/3 | B200/3 |         | 12:46    | 13:1    | 13:21  |
| 51    | B20/3 | B200/3 |         | 12:52    | 13:7    | 13:27  |
| 52    | C20/3 | C200/3 |         | 12:58    | 13:13   | 13:33  |
| 53    | A20/3 | A200/3 |         | 13:5     | 13:20   | 13:40  |
| 54    | B20/3 | B200/3 |         | 13:11    | 13:26   | 13:46  |
| 55    | B20/3 | B200/3 |         | 13:17    | 13:32   | 13:52  |
| 56    | A20/3 | A200/3 |         | 13:23    | 13:38   | 13:58  |
| 57    | A20/3 | A200/3 |         | 13:29    | 13:44   | 14:4   |
| 58    | C20/3 | C200/3 |         | 13:35    | 13:50   | 14:10  |
| 59    | A20/1 | A200/1 |         | 13:41    | 13:56   | 14:16  |
| 60    | B20/3 | B200/3 |         | 13:48    | 14:3    | 14:33  |
| 61    | A20/3 | A200/3 |         | 13:54    | 14:9    | 14:39  |
| 62    | A20/3 | A200/3 |         | 14:0     | 14:15   | 14:45  |
| 63    | A20/3 | A200/3 |         | 14:6     | 14:21   | 14:51  |
| 64    | B20/3 | B200/3 |         | 14:12    | 14:27   | 14:57  |
| 65    | A20/3 | A200/3 |         | 14:18    | 14:33   | 15:3   |
| 66    | B20/3 | B200/3 |         | 14:24    | 14:39   | 15:9   |
| 67    | B20/3 | B200/3 |         | 14:31    | 14:46   | 15:6   |
| 68    | A20/3 | A200/3 |         | 14:37    | 14:52   | 15:12  |
| 69    | A20/3 | A200/3 |         | 14:43    | 14:58   | 15:18  |
| 70    | B20/3 | B200/3 |         | 14:49    | 15:4    | 15:24  |
| 71    | A20/1 | A200/1 |         | 14:55    | 15:10   | 15:30  |
| 72    | B20/3 | B200/3 |         | 15:1     | 15:16   | 15:36  |
| 73    | A20/3 | A200/3 |         | 15:8     | 15:23   | 15:43  |
| 74    | A20/3 | A200/3 |         | 15:14    | 15:29   | 15:49  |
| 75    | A20/3 | A200/3 |         | 15:20    | 15:35   | 15:55  |
| 76    | B20/3 | B200/3 |         | 15:26    | 15:41   | 16:1   |
| 77    | A20/3 | A200/3 |         | 15:32    | 15:47   | 16:7   |
| 78    | B20/3 | B200/3 |         | 15:38    | 15:53   | 16:10  |

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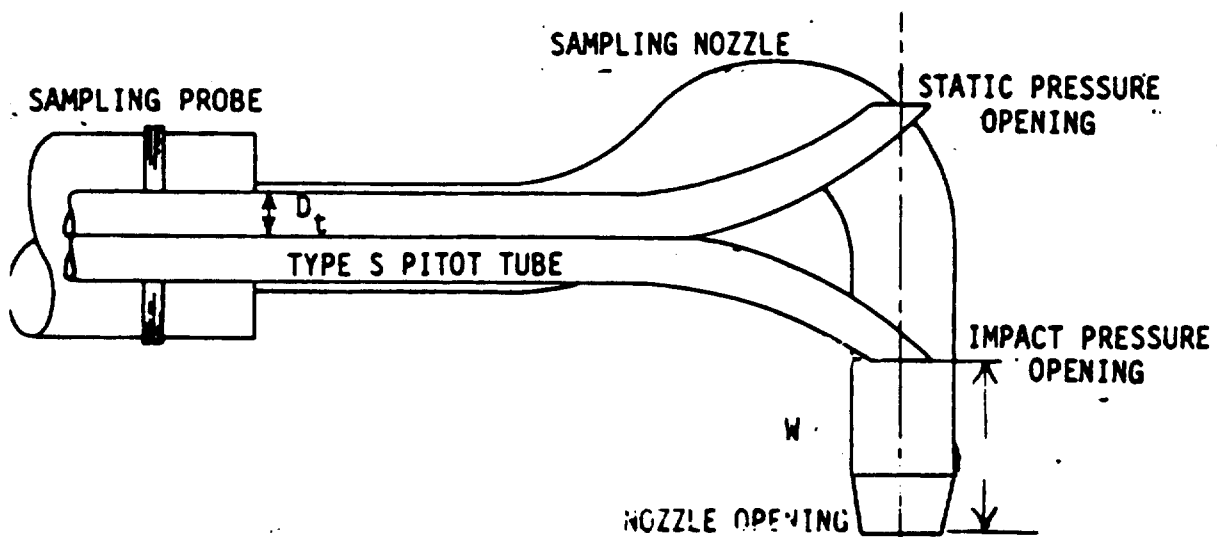
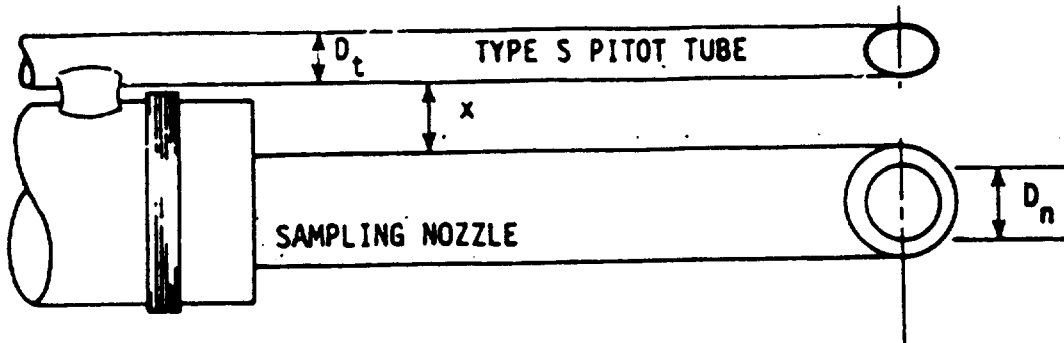
BX 4 TURN

| SEQ # | PUSH  | CHARGE | STATION | EARLIEST | DESIRED | LATEST |
|-------|-------|--------|---------|----------|---------|--------|
| 1     | B11/1 | B0/0   |         | 3:45     | 4:00    | 4:20   |
| 2     | A11/3 | A9/1   |         | 3:51     | 4:06    | 4:26   |
| 3     | A11/3 | A9/1   |         | 3:57     | 4:12    | 4:32   |
| 4     | B11/3 | B9/3   |         | 4:03     | 4:18    | 4:38   |
| 5     | A11/3 | A9/1   |         | 4:09     | 4:24    | 4:44   |
| 6     | B11/3 | B11/1  |         | 4:15     | 4:30    | 4:50   |
| 7     | B13/1 | B11/1  |         | 4:21     | 4:36    | 4:56   |
| 8     | A13/3 | A11/3  |         | 4:27     | 4:42    | 5:02   |
| 9     | A13/3 | A11/3  |         | 4:33     | 4:48    | 5:08   |
| 10    | B13/3 | B11/3  |         | 4:39     | 4:54    | 5:14   |
| 11    | A15/1 | A13/1  |         | 4:45     | 5:00    | 5:20   |
| 12    | B15/2 | B13/2  |         | 4:51     | 5:06    | 5:26   |
| 13    | B15/3 | B13/3  |         | 4:57     | 5:12    | 5:32   |
| 14    | A15/3 | A13/3  |         | 5:03     | 5:18    | 5:38   |
| 15    | A15/3 | A13/3  |         | 5:09     | 5:24    | 5:44   |
| 16    | B15/3 | B13/3  |         | 5:15     | 5:30    | 5:50   |
| 17    | A17/1 | A15/1  |         | 5:21     | 5:36    | 5:56   |
| 18    | B17/2 | B15/2  |         | 5:27     | 5:42    | 6:02   |
| 19    | B17/1 | B15/1  |         | 5:33     | 5:48    | 6:08   |
| 20    | A17/3 | A15/3  |         | 5:39     | 5:54    | 6:14   |
| 21    | B17/3 | B15/3  |         | 5:45     | 6:00    | 6:20   |
| 22    | A17/3 | A15/3  |         | 5:51     | 6:06    | 6:26   |
| 23    | A19/1 | A17/1  |         | 5:57     | 6:12    | 6:32   |
| 24    | B19/2 | B17/2  |         | 6:03     | 6:18    | 6:38   |
| 25    | A19/3 | A17/3  |         | 6:09     | 6:24    | 6:44   |
| 26    | B19/3 | B17/3  |         | 6:15     | 6:30    | 6:50   |
| 27    | A19/3 | A17/3  |         | 6:21     | 6:36    | 6:56   |
| 28    | B19/3 | B17/3  |         | 6:27     | 6:42    | 7:02   |
| 29    | B21/1 | B19/1  |         | 6:33     | 6:48    | 7:08   |
| 30    | B21/2 | B19/2  |         | 6:39     | 6:54    | 7:14   |
| 31    | B21/3 | B19/3  |         | 6:45     | 7:00    | 7:20   |
| 32    | A21/3 | A19/3  |         | 6:51     | 7:06    | 7:26   |
| 33    | B21/3 | B19/3  |         | 6:57     | 7:12    | 7:32   |
| 34    | B21/3 | B19/3  |         | 7:03     | 7:18    | 7:38   |
| 35    | A23/1 | A21/1  |         | 7:09     | 7:24    | 7:44   |
| 36    | B23/2 | B21/2  |         | 7:15     | 7:30    | 7:50   |
| 37    | B23/3 | B21/3  |         | 7:21     | 7:36    | 7:56   |
| 38    | A23/3 | A21/3  |         | 7:27     | 7:42    | 8:02   |
| 39    | B23/3 | B21/3  |         | 7:33     | 7:48    | 8:08   |
| 40    | A23/3 | A21/3  |         | 7:39     | 7:54    | 8:14   |
| 41    | B23/3 | B21/3  |         | 7:45     | 8:00    | 8:20   |
| 42    | A23/3 | A21/3  |         | 7:51     | 8:06    | 8:26   |
| 43    | B23/3 | B21/3  |         | 7:57     | 8:12    | 8:32   |
| 44    | A23/3 | A21/3  |         | 8:03     | 8:18    | 8:38   |
| 45    | A23/3 | A21/3  |         | 8:09     | 8:24    | 8:44   |
| 46    | B23/3 | B21/3  |         | 8:15     | 8:30    | 8:50   |
| 47    | B23/3 | B21/3  |         | 8:21     | 8:36    | 8:56   |
| 48    | A23/3 | A21/3  |         | 8:27     | 8:42    | 9:02   |
| 49    | B23/3 | B21/3  |         | 8:33     | 8:48    | 9:08   |
| 50    | A23/3 | A21/3  |         | 8:39     | 8:54    | 9:14   |
| 51    | B23/3 | B21/3  |         | 8:45     | 9:00    | 9:20   |
| 52    | A23/3 | A21/3  |         | 8:51     | 9:06    | 9:26   |
| 53    | B23/3 | B21/3  |         | 8:57     | 9:12    | 9:32   |
| 54    | A23/3 | A21/3  |         | 9:03     | 9:18    | 9:38   |
| 55    | B23/3 | B21/3  |         | 9:09     | 9:24    | 9:44   |
| 56    | A23/3 | A21/3  |         | 9:15     | 9:30    | 9:50   |
| 57    | B23/3 | B21/3  |         | 9:21     | 9:36    | 9:56   |
| 58    | A23/3 | A21/3  |         | 9:27     | 9:42    | 10:02  |
| 59    | B23/3 | B21/3  |         | 9:33     | 9:48    | 10:08  |
| 60    | A23/3 | A21/3  |         | 9:39     | 9:54    | 10:14  |
| 61    | B23/3 | B21/3  |         | 9:45     | 10:00   | 10:20  |
| 62    | A23/3 | A21/3  |         | 9:51     | 10:06   | 10:26  |
| 63    | B23/3 | B21/3  |         | 9:57     | 10:12   | 10:32  |
| 64    | A23/3 | A21/3  |         | 10:03    | 10:18   | 10:38  |
| 65    | B23/3 | B21/3  |         | 10:09    | 10:24   | 10:44  |
| 66    | A23/3 | A21/3  |         | 10:15    | 10:30   | 10:50  |
| 67    | B23/3 | B21/3  |         | 10:21    | 10:36   | 10:56  |
| 68    | A23/3 | A21/3  |         | 10:27    | 10:42   | 11:02  |
| 69    | B23/3 | B21/3  |         | 10:33    | 10:48   | 11:08  |
| 70    | A23/3 | A21/3  |         | 10:39    | 10:54   | 11:14  |
| 71    | B23/3 | B21/3  |         | 10:45    | 11:00   | 11:20  |
| 72    | A23/3 | A21/3  |         | 10:51    | 11:06   | 11:26  |
| 73    | B23/3 | B21/3  |         | 10:57    | 11:12   | 11:32  |
| 74    | A23/3 | A21/3  |         | 11:03    | 11:18   | 11:38  |
| 75    | B23/3 | B21/3  |         | 11:09    | 11:24   | 11:44  |
| 76    | A23/3 | A21/3  |         | 11:15    | 11:30   | 11:50  |
| 77    | B23/3 | B21/3  |         | 11:21    | 11:36   | 11:56  |
| 78    | A23/3 | A21/3  |         | 11:27    | 11:42   | 12:02  |
| 79    | B23/3 | B21/3  |         | 11:33    | 11:48   | 12:08  |
| 80    | A23/3 | A21/3  |         | 11:39    | 11:54   | 12:14  |
| 81    | B23/3 | B21/3  |         | 11:45    | 12:00   | 12:20  |
| 82    | A23/3 | A21/3  |         | 11:51    | 12:06   | 12:26  |
| 83    | B23/3 | B21/3  |         | 11:57    | 12:12   | 12:32  |
| 84    | A23/3 | A21/3  |         | 12:03    | 12:18   | 12:38  |
| 85    | B23/3 | B21/3  |         | 12:09    | 12:24   | 12:44  |
| 86    | A23/3 | A21/3  |         | 12:15    | 12:30   | 12:50  |
| 87    | B23/3 | B21/3  |         | 12:21    | 12:36   | 12:56  |
| 88    | A23/3 | A21/3  |         | 12:27    | 12:42   | 13:02  |
| 89    | B23/3 | B21/3  |         | 12:33    | 12:48   | 13:08  |
| 90    | A23/3 | A21/3  |         | 12:39    | 12:54   | 13:14  |
| 91    | B23/3 | B21/3  |         | 12:45    | 13:00   | 13:20  |
| 92    | A23/3 | A21/3  |         | 12:51    | 13:06   | 13:26  |
| 93    | B23/3 | B21/3  |         | 12:57    | 13:12   | 13:32  |
| 94    | A23/3 | A21/3  |         | 13:03    | 13:18   | 13:38  |
| 95    | B23/3 | B21/3  |         | 13:09    | 13:24   | 13:44  |
| 96    | A23/3 | A21/3  |         | 13:15    | 13:30   | 13:50  |
| 97    | B23/3 | B21/3  |         | 13:21    | 13:36   | 13:56  |
| 98    | A23/3 | A21/3  |         | 13:27    | 13:42   | 14:02  |
| 99    | B23/3 | B21/3  |         | 13:33    | 13:48   | 14:08  |
| 100   | A23/3 | A21/3  |         | 13:39    | 13:54   | 14:14  |

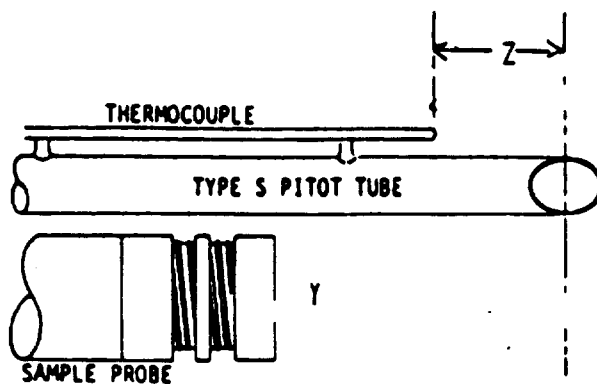


**USS CLAIRTON WORKS  
RESULTS OF THE  
COMPLIANCE DEMONSTRATION OF THE  
#3 BATTERY COMBUSTION STACK**

**APPENDIX B  
PRE-TEST AND POST-TEST  
CALIBRATION AND AUDIT RESULTS**



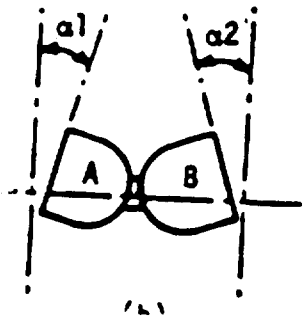
$D_n$  = Nozzle diameter  
 $D_t$  = 3/16 to 3/8"



$W \geq 0$   
 $X \geq 3/4"$  for 1/2" Nozz  
 $Y \geq 3"$   
 $Z \geq 2"$

# GEOMETRIC PITOT CALIBRATION

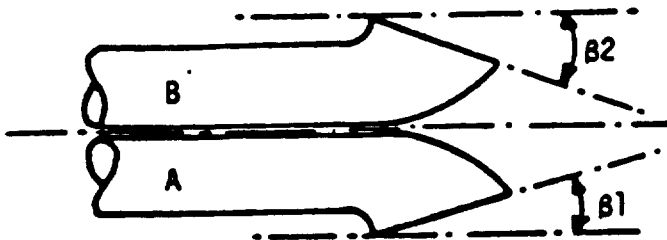
Probe No. 7-1  
 Date 6/29/90  
 Initials HTS



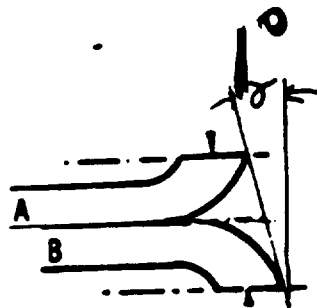
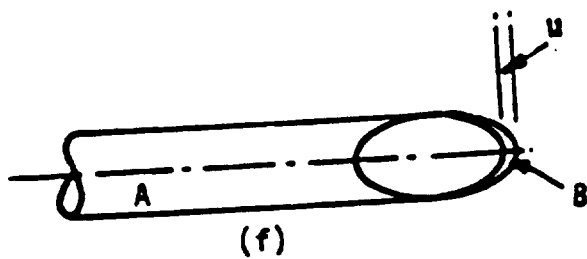
$\alpha 1, \alpha 2 < 10^\circ$

$\alpha 1 = 2^\circ$   
 $\alpha 2 = 1^\circ$   
 $\beta 1 = 2^\circ$   
 $\beta 2 = 4^\circ$   
 $A = 1.059$   
 $\mu = .018$   
 $V = 0$   
 $W = 0$   
 $X = 2\frac{3}{4}"$   
 $Y = 2\frac{3}{4}"$   
 $Z = 2\frac{3}{4}"$   
 $U_t = 380$

pre-test

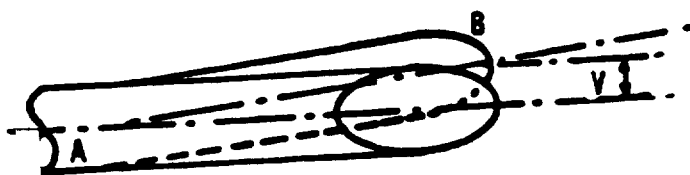


$\beta 1, \beta 2 < 5$

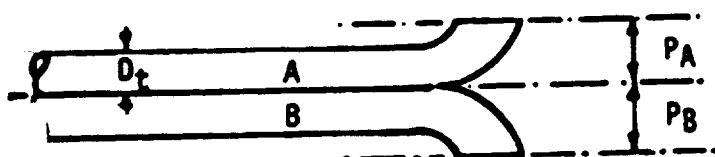


$$\mu = A \sin \theta$$

$$V = A \sin \theta$$



A-SIDE PLANE



B-SIDE PLANE

.399 .570  
 $1.05 D_t < P < 1.50 D_t$   
 $P_A = P_B$   
 $2.10 D_t < A < 3.00 D_t$   
 .798 1.14

# GEOMETRIC PITOT CALIBRATION

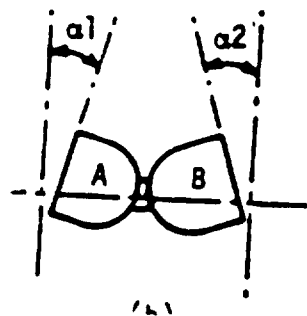
Probe No. 7-1

Date 8-20-90

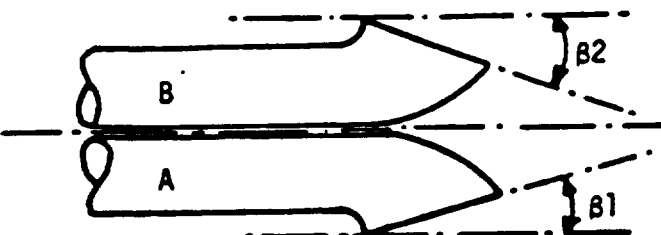
Initials gjm

post-check

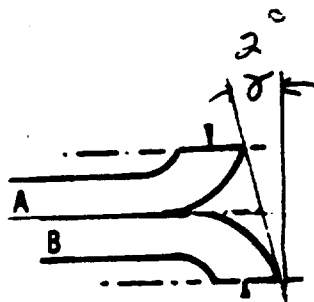
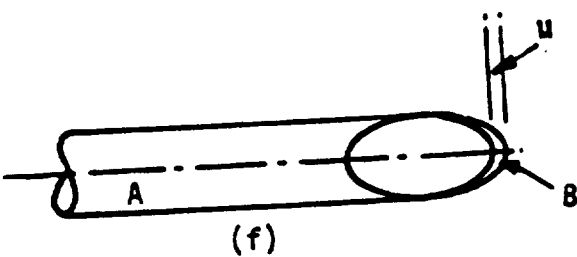
$\alpha 1 = 4^\circ$   
 $\alpha 2 = 1^\circ$   
 $\beta 1 = 3^\circ$   
 $\beta 2 = 0$   
 $A = 1.055$   
 $u = .036$   
 $V = .036$   
 $W = \geq 0$   
 $X = .825$   
 $Y = \geq 3$   
 $Z = \geq 2$   
 $D_t = 38$



$\alpha 1, \alpha 2 < 10^\circ$

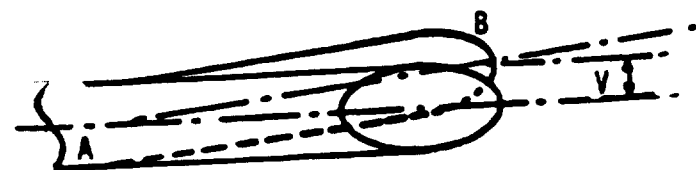


$\beta 1, \beta 2 < 5$

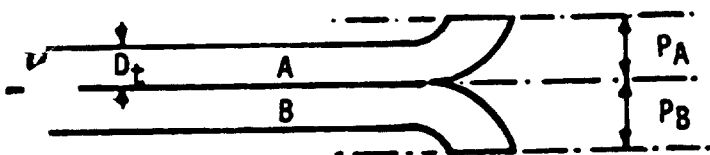


$$\mu = A \sin \theta$$

$$V = A \sin \theta$$



A-SIDE PLANE



B-SIDE PLANE

405 .579

$$1.05 D_t < P < 1.50 D_t$$

$$P_A = P_B$$

$$2.10 D_t < A < 3.00 D_t$$

.811

1.14

B-3

# GEOMETRIC PITOT CALIBRATION

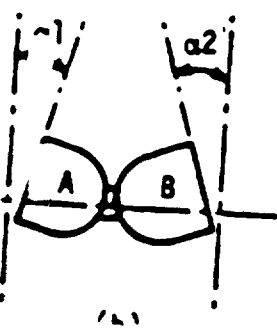
Probe No. 1-6

Date 6-29-90

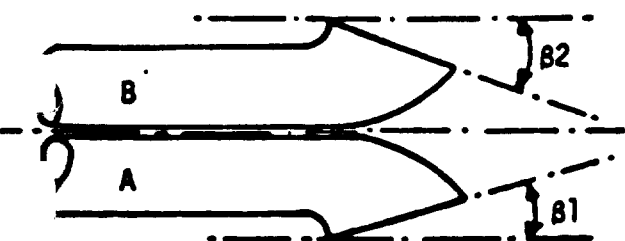
Initials ATS

$\alpha_1 = 4^\circ$   
 $\alpha_2 = 3^\circ$   
 $\beta_1 = 1^\circ$   
 $\beta_2 = 3^\circ$   
 $A = .988$   
 $\mu = .034$   
 $V = .069$   
 $W = > 0$   
 $X = > 3/4$   
 $Y = > 3/4$   
 $Z = > 2^\circ$   
 $D_t = .385$

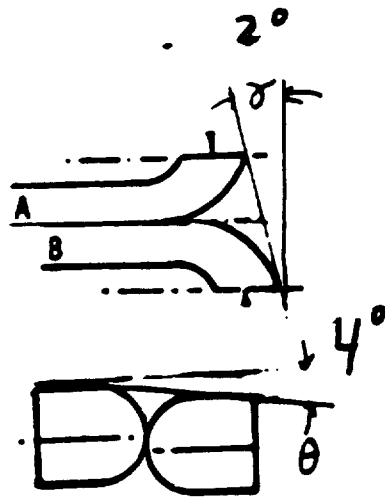
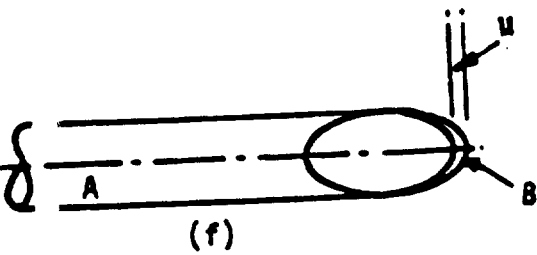
pre test



$\alpha_1, \alpha_2 < 10^\circ$



$\beta_1, \beta_2 < 5$

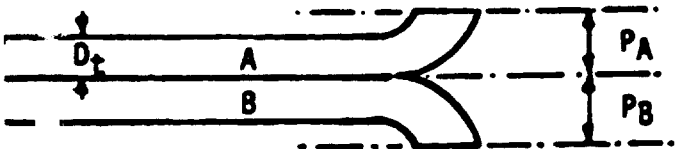


$$\mu = A \sin \theta$$

$$V = A \sin \phi$$



A-SIDE PLANE



B-SIDE PLANE

.404 .5775  
 $1.05 D_t < P < 1.50 D_t$   
 $P_A = P_B$   
 $2.10 D_t < A < 3.00 D_t$   
.808 1.155

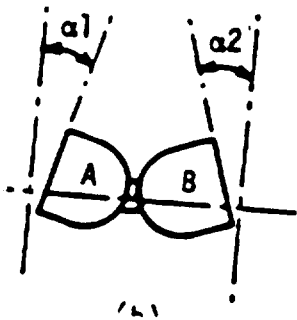
# GEOMETRIC PITOT CALIBRATION

Probe No. 7-2

Date 8-30-90

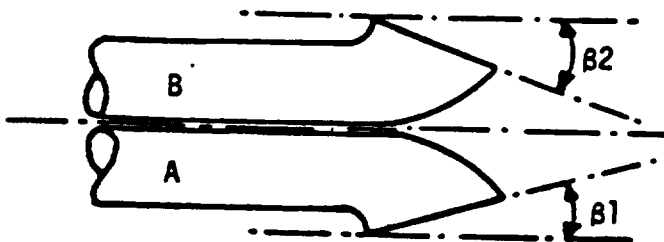
Initials BNJ

post-check

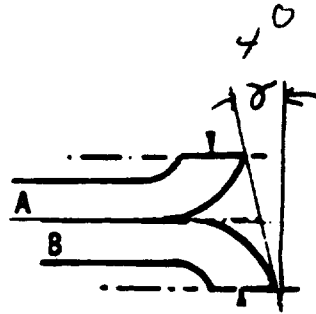
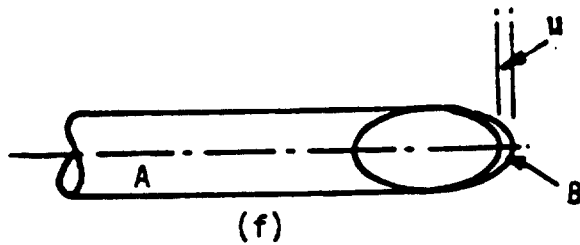


$\alpha 1, \alpha 2 < 10^\circ$

$\alpha 1 = 1^\circ$   
 $\alpha 2 = 3^\circ$   
 $\beta 1 = 4^\circ$   
 $\beta 2 = 1^\circ$   
 $A = 962$   
 $\mu = .067$   
 $V = .033$   
 $W = 20$   
 $X = .989$   
 $Y = 2.3'$   
 $Z = 2.2''$   
 $D_t = .376$



$\beta 1, \beta 2 < 5$

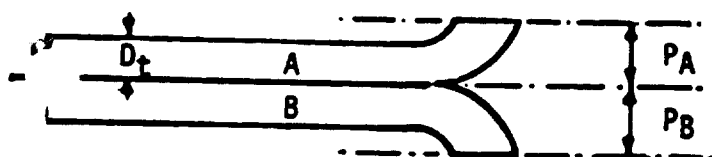


$$\mu = A \sin \theta$$

$$V = A \sin \theta$$



A-SIDE PLANE



B-SIDE PLANE

374

564

$$1.05 D_t < P < 1.50 D_t$$

$$P_A = P_B$$

$$2.10 D_t < A < 3.00 D_t$$

.989

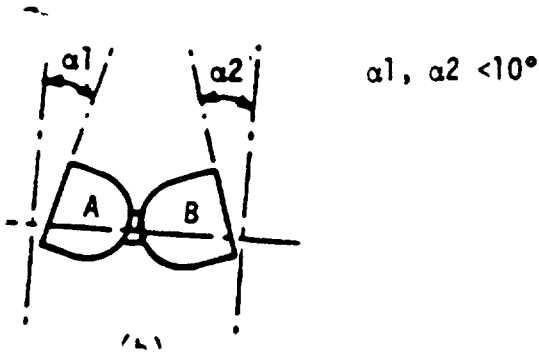
1.128

B-5

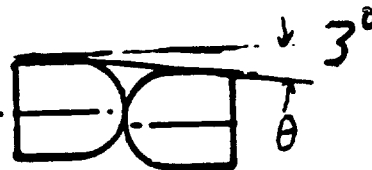
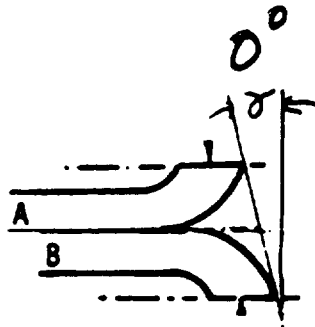
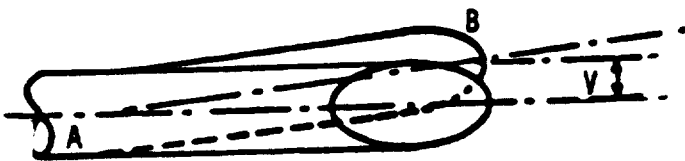
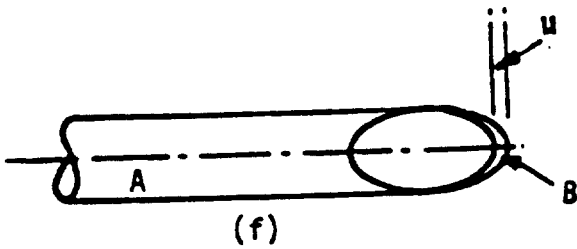
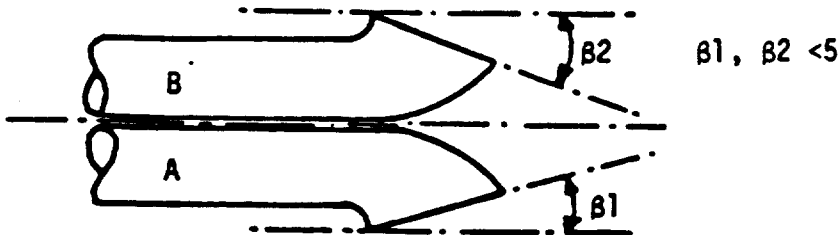
# GEOMETRIC PITOT CALIBRATION

Probe No. 7-3  
 Date 6/29/90  
 Initials ATS

*pre-test*



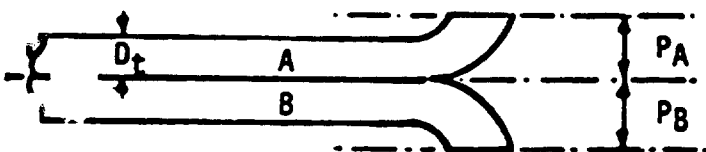
$\alpha 1 = 4^\circ$   
 $\alpha 2 = 2^\circ$   
 $\beta 1 = 9^\circ$   
 $\beta 2 = 1^\circ$   
 $A = .954$   
 $u = 0$   
 $V = .050$   
 $W = 70$   
 $X = 73/4^\circ$   
 $Y = 73''$   
 $Z = 92''$   
 $U_t = .376$



$$u = A \sin \theta$$

$$V = A \sin \theta$$

A-SIDE PLANE



B-SIDE PLANE

.39 .564

$$1.05 D_t < P < 1.50 D_t$$

$$P_A = P_B$$

$$2.10 D_t < A < 3.00 D_t$$

.799 1.128

# GEOMETRIC PITOT CALIBRATION

Probe No. 2-3

Date 8-20-90

Initials g17

post-check

$\alpha_1 = 2^\circ$

$\alpha_2 = 2^\circ$

$\beta_1 = 1^\circ$

$\beta_2 = 0^\circ$

$A = .961$

$\mu = .016$

$V = .067$

$W = .30$

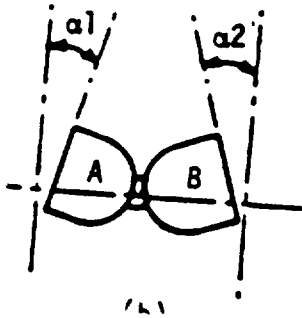
$X = .945$

$Y = .33$

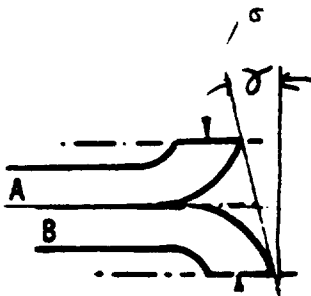
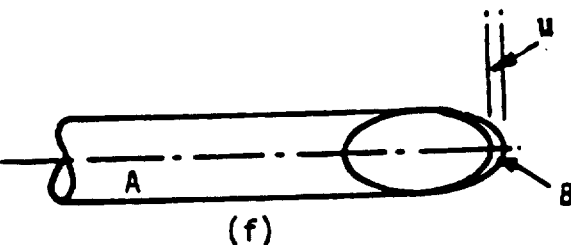
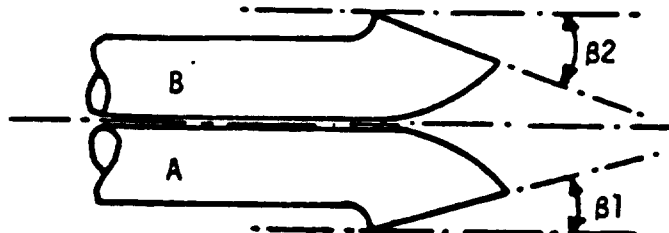
$Z = .32$

$U_t = .327$

$\alpha_1, \alpha_2 < 10^\circ$

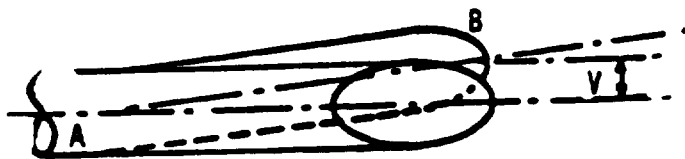


$\beta_1, \beta_2 < 5$

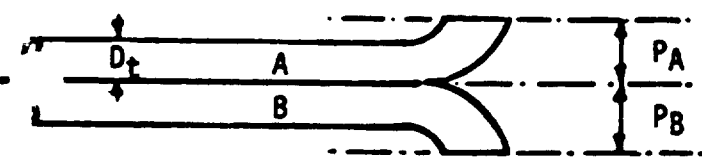


$$\mu = A \sin \sigma$$

$$V = A \sin \theta$$



A-SIDE PLANE



B-SIDE PLANE

.385

.565

$$1.05 D_t < P < 1.50 D_t$$

$$P_A = P_B$$

$$2.10 D_t < A < 3.00 D_t$$

.771

1.13



# CONTROL BOX CALIBRATION

## THREE POINT CALIBRATION

BOX NO. 1  
DATE 6-12-90  
BP 29.1  
OPERATOR TJM

|             | TIME  | WET TEST METER         |                          |                | PRESSURE | DRY TEST METER            |                            |                            |                            | ORIFICE | VOLUME  | METER CORRECT | ORIFICE COEFFICE |
|-------------|-------|------------------------|--------------------------|----------------|----------|---------------------------|----------------------------|----------------------------|----------------------------|---------|---------|---------------|------------------|
|             |       | TEMP<br>T <sub>W</sub> | VOLUME<br>V <sub>M</sub> | P <sub>W</sub> |          | TEMP IN<br>T <sub>I</sub> | TEMP OUT<br>T <sub>O</sub> | TEMP AVG<br>T <sub>A</sub> | TEMP OUT<br>T <sub>D</sub> |         |         |               |                  |
| START       |       |                        |                          | 0.000          | 29.10    |                           |                            |                            |                            | 0.50    | 464.200 |               |                  |
| HALF        |       |                        | 78.0                     |                |          |                           | 94.0                       | 92.0                       | 93.0                       |         |         |               |                  |
| STOP        | 11.50 |                        |                          | 5.000          |          |                           |                            |                            |                            |         | 469.118 |               |                  |
| CALCULATION | 11.50 |                        | 538.0                    | 5.057          | 29.10    |                           |                            |                            |                            | 553.0   | 29.14   | 4.918         | 1.0555 1.475     |
| START       |       |                        |                          | 0.000          | 29.10    |                           |                            |                            |                            | 1.00    | 470.000 |               |                  |
| HALF        |       |                        | 78.0                     |                |          |                           | 98.0                       | 91.0                       | 94.5                       |         |         |               |                  |
| STOP        | 8.43  |                        |                          | 5.000          |          |                           |                            |                            |                            |         | 474.977 |               |                  |
| CALCULATION | 8.43  |                        | 538.0                    | 5.057          | 29.10    |                           |                            |                            |                            | 554.5   | 29.17   | 4.977         | 1.0445 1.580     |
| START       |       |                        |                          | 0.000          | 29.10    |                           |                            |                            |                            | 2.00    | 476.000 |               |                  |
| HALF        |       |                        | 78.0                     |                |          |                           | 99.0                       | 92.0                       | 95.5                       |         |         |               |                  |
| STOP        | 6.12  |                        |                          | 5.000          |          |                           |                            |                            |                            |         | 480.920 |               |                  |
| CALCULATION | 6.12  |                        | 538.0                    | 5.057          | 29.10    |                           |                            |                            |                            | 555.5   | 29.25   | 4.920         | 1.0558 1.663     |
| AVERAGE     |       |                        |                          |                |          |                           |                            |                            |                            |         |         |               | 1.0519 1.573     |

# POST TEST

BOX NO. 1  
 DATE 8-15-90  
 BP 29.03  
 OPERATOR MGG

|             | TIME | WET TEST METER |                |                | PRESSURE | DRY TEST METER |                |                |                |                | METER CORRECT | ORIFICE COEFFICE |        |                |
|-------------|------|----------------|----------------|----------------|----------|----------------|----------------|----------------|----------------|----------------|---------------|------------------|--------|----------------|
|             |      | TEMP           | VOLUME         |                |          | TEMP IN        | TEMP OUT       | TEMP AVG       | ORIFICE        | VOLUME         |               |                  |        |                |
|             |      | T <sub>W</sub> | V <sub>W</sub> | P <sub>W</sub> |          | T <sub>I</sub> | T <sub>O</sub> | T <sub>A</sub> | P <sub>D</sub> | V <sub>D</sub> |               |                  | Y      | H <sub>g</sub> |
| START       |      |                |                | 0.000          | 29.03    |                |                |                |                |                | 1.50          | 139.400          |        |                |
| HALF        |      |                | 77.0           |                |          |                | 94.0           | 85.0           | 89.5           |                |               |                  |        |                |
| STOP        | 7.22 |                |                | 5.000          |          |                |                |                |                |                |               | 144.422          |        |                |
| CALCULATION | 7.22 |                | 537.0          | 5.057          | 29.03    |                |                |                | 549.5          | 29.14          | 5.022         | 1.0264           | 1.753  |                |
| START       |      |                |                | 0.000          | 29.03    |                |                |                |                |                | 1.50          | 145.600          |        |                |
| HALF        |      |                | 77.0           |                |          |                | 94.0           | 84.0           | 89.0           |                |               |                  |        |                |
| STOP        | 7.18 |                |                | 5.002          |          |                |                |                |                |                |               | 150.643          |        |                |
| CALCULATION | 7.18 |                | 537.0          | 5.059          | 29.03    |                |                |                | 549.0          | 29.14          | 5.043         | 1.0216           | 1.733  |                |
| START       |      |                |                | 0.000          | 29.03    |                |                |                |                |                | 1.50          | 152.700          |        |                |
| HALF        |      |                | 77.0           |                |          |                | 94.0           | 83.0           | 88.5           |                |               |                  |        |                |
| STOP        | 7.12 |                |                | 5.001          |          |                |                |                |                |                |               | 157.744          |        |                |
| CALCULATION | 7.12 |                | 537.0          | 5.058          | 29.03    |                |                |                | 548.5          | 29.14          | 5.044         | 1.0203           | 1.707  |                |
| AVERAGE     |      |                |                |                |          |                |                |                |                |                |               | 1.0228           | 1.731  |                |
| DIFFERENCE  |      |                |                |                |          |                |                |                |                |                |               | 2.85%            | -9.14% |                |

# MAGNAHELIC CALIBRAATION

DATE 8-15-90  
OPERATOR MGG

| P 0-10     |           | P 0-.5     |           | H          |           |
|------------|-----------|------------|-----------|------------|-----------|
| MAGNEHILIC | MANOMETER | MAGNEHILIC | MANOMETER | MAGNEHILIC | MANOMETER |
| 0.50       | 0.50      | 0.50       | 0.50      | 4.00       | 4.00      |
| 1.00       | 1.00      | 0.40       | 0.40      | 3.00       | 3.00      |
| 2.00       | 2.00      | 0.30       | 0.30      | 2.00       | 2.00      |
| 4.00       | 4.00      | 0.20       | 0.20      | 1.00       | 1.00      |
| 6.00       | 6.00      | 0.10       | 0.10      | 0.50       | 0.50      |
| 8.00       | 8.00      |            |           |            |           |

# LEAK CHECK

DATE 8-15-90  
OPERATOR MGG

|     | START CF | STOP CF | VOL   | TIME   | LEAK RATE |
|-----|----------|---------|-------|--------|-----------|
| DRY | 138.270  | 138.413 | 0.143 | 10.000 | 0.023     |
| WET | 0.000    | 0.371   | 0.371 |        |           |

# PYROMETER CALIBRATION

DATE 04-28-88  
OPERATOR AGL

| mV input | temp<br>°F | temp rdg<br>°F |
|----------|------------|----------------|
| 0.18     | 40         | 40.0           |
| 0.40     | 50         | 50.0           |
| 0.84     | 70         | 70.0           |
| 1.29     | 90         | 90.0           |
| 1.74     | 110        | 110.0          |
| 2.66     | 150        | 150.0          |
| 3.82     | 200        | 200.0          |
| 6.09     | 300        | 301.0          |
| 8.31     | 400        | 400.0          |
| 10.57    | 500        | 500.0          |

# PYROMETER CHECK

DATE 8-6-90  
OPERATOR TM

| mV input<br>°F | temp<br>°F | temp rdg |
|----------------|------------|----------|
| 0.18           | 40         | 40.0     |
| 0.40           | 50         | 50.0     |
| 0.84           | 70         | 70.0     |
| 1.29           | 90         | 90.0     |
| 1.74           | 110        | 110.0    |
| 2.66           | 150        | 150.0    |
| 3.82           | 200        | 200.0    |
| 6.09           | 300        | 300.0    |
| 8.31           | 400        | 400.0    |
| 10.57          | 500        | 500.0    |

Name: KEYSTONE ENV. RES.Phone: 825-9761Date: 8/21/90 Train ID: BOX 1 DGM Cal. Factor, Y: 1.0519 Orifice No.: BAPC-2Type of Meter Box: NAPP 100 Type of Pump: DIAPHRAM

|                                     |                 | Run Number |                          |                          |                        |
|-------------------------------------|-----------------|------------|--------------------------|--------------------------|------------------------|
|                                     |                 | Example    | <u>1</u>                 | <u>2</u>                 | <u>3</u>               |
| <u>DGM</u>                          |                 |            |                          |                          |                        |
| Final reading                       | ft <sup>3</sup> | 966.461    | <u>338.857</u>           | <u>345.980</u>           | <u>353.061</u>         |
| Initial reading                     | ft <sup>3</sup> | 946.602    | <u>331.900</u>           | <u>339.000</u>           | <u>346.100</u>         |
| Difference, V <sub>m</sub>          | ft <sup>3</sup> | 9.859      | <u>6.957</u>             | <u>6.980</u>             | <u>6.966</u>           |
| Percent Accuracy, ZA                |                 |            |                          |                          |                        |
| Inlet/Outlet temperatures           |                 |            |                          |                          |                        |
| Initial                             | °F.             | 108/88     | <u>77.174</u>            | <u>78.176</u>            | <u>77.175</u>          |
| After 5 minutes                     |                 | 110/88     | <u>77.174</u>            | <u>78.175</u>            | <u>78.175</u>          |
| After 10 minutes                    |                 | 111/88     | <u>77.174</u>            | <u>78.175</u>            | <u>78.175</u>          |
| Final                               |                 | 112/89     | <u>76.174</u>            | <u>77.175</u>            | <u>77.175</u>          |
| Avg. temperature, t <sub>d</sub>    | °F/°R           | 99.3/559.3 | <u>75.4</u> <u>535.4</u> | <u>76.5</u> <u>536.5</u> | <u>76.3</u> <u>536</u> |
| Time, θ                             | min             | 15.0       | <u>15.0</u>              | <u>15.0</u>              | <u>15.0</u>            |
| Orifice man. rdg., delta H          |                 | 1.35       | <u>0.65</u>              | <u>0.65</u>              | <u>0.65</u>            |
| Bar. pressure, P <sub>bar</sub>     |                 | 29.75      | <u>28.981</u>            | <u>28.98</u>             | <u>28.98</u>           |
| Ambient temperature, t <sub>a</sub> | °F/°C           | 74/23.3    | <u>82.127.8</u>          | <u>82.127.8</u>          | <u>82.127</u>          |
| Pump vacuum                         | in. Hg          | 18.8       | <u>19.5</u>              | <u>19.5</u>              | <u>19.5</u>            |
| V <sub>m</sub> (std) <sup>*</sup>   | ft <sup>3</sup> | 9.2815     |                          |                          |                        |
| DGM cal. factor, Y <sub>c</sub>     |                 | 1.0593     |                          |                          |                        |
| *V <sub>m</sub> (std)(M)            | m <sup>3</sup>  | 0.2629     |                          |                          |                        |

\*If you calculate dry gas volume in English Units, use the conversion factor of 0.02832 m<sup>3</sup>/ft<sup>3</sup> to obtain the volume in metric units.

VOLUMETRIC FLOW DEVICE CALCULATION SHEET

Eq. 8-1  $V_m(\text{std}) = V_m Y \left( \frac{T_{\text{std}}}{T_m} \right) \left( \frac{P_{\text{bar}} + \frac{\Delta H}{13.6}}{P_{\text{std}}} \right)$

Run #1  $V_m(\text{std})' = V_m \times Y \times \frac{528}{T_m} \times \left( \frac{P_{\text{bar}} + \frac{\Delta H}{13.6}}{29.92} \right)$

$V_m(\text{std})' = \frac{(6.957)(1.0519)(0.9862)(0.9704)}{7.002} \text{ ft}^3 \text{ (round to 3 decimals)}$

$V_m(\text{std})' = \frac{6.731}{7.002} \text{ ft}^3$

Run #2  $V_m(\text{std})' = \frac{(6.986)(1.0519)(0.9842)(0.9704)}{7.011} \text{ ft}^3$

$V_m(\text{std})' = \frac{6.740}{7.011} \text{ ft}^3$

Run #3  $V_m(\text{std})' = \frac{(6.966)(1.0519)(0.9845)(0.9704)}{6.999} \text{ ft}^3$

$V_m(\text{std})' = \frac{6.728}{6.999} \text{ ft}^3$

$V_{\text{std}}(\text{M}) = \frac{V_m(\text{std})' \text{ Run \#1} + V_m(\text{std})' \text{ Run \#2} + V_m(\text{std})' \text{ Run \#3}}{3}$

$V_{\text{std}}(\text{M}) = \frac{7.004}{6.733} \text{ ft}^3$

(To Be Completed By Auditor)

$\% A = \frac{V_{\text{std}}(\text{M}) - V_{\text{std}}(\text{A})}{V_{\text{std}}(\text{A})} \times 100 \leq \pm 3\%$

$\% A = \frac{\quad}{\quad} \times 100$

$\% A = \frac{\quad}{\quad} \%$

**USS CLAIRTON WORKS  
RESULTS OF THE  
COMPLIANCE DEMONSTRATION OF THE  
#3 BATTERY COMBUSTION STACK**

**APPENDIX C**

**FIELD DATA SHEETS FOR  
PARTICULATE MATTER EMISSIONS**

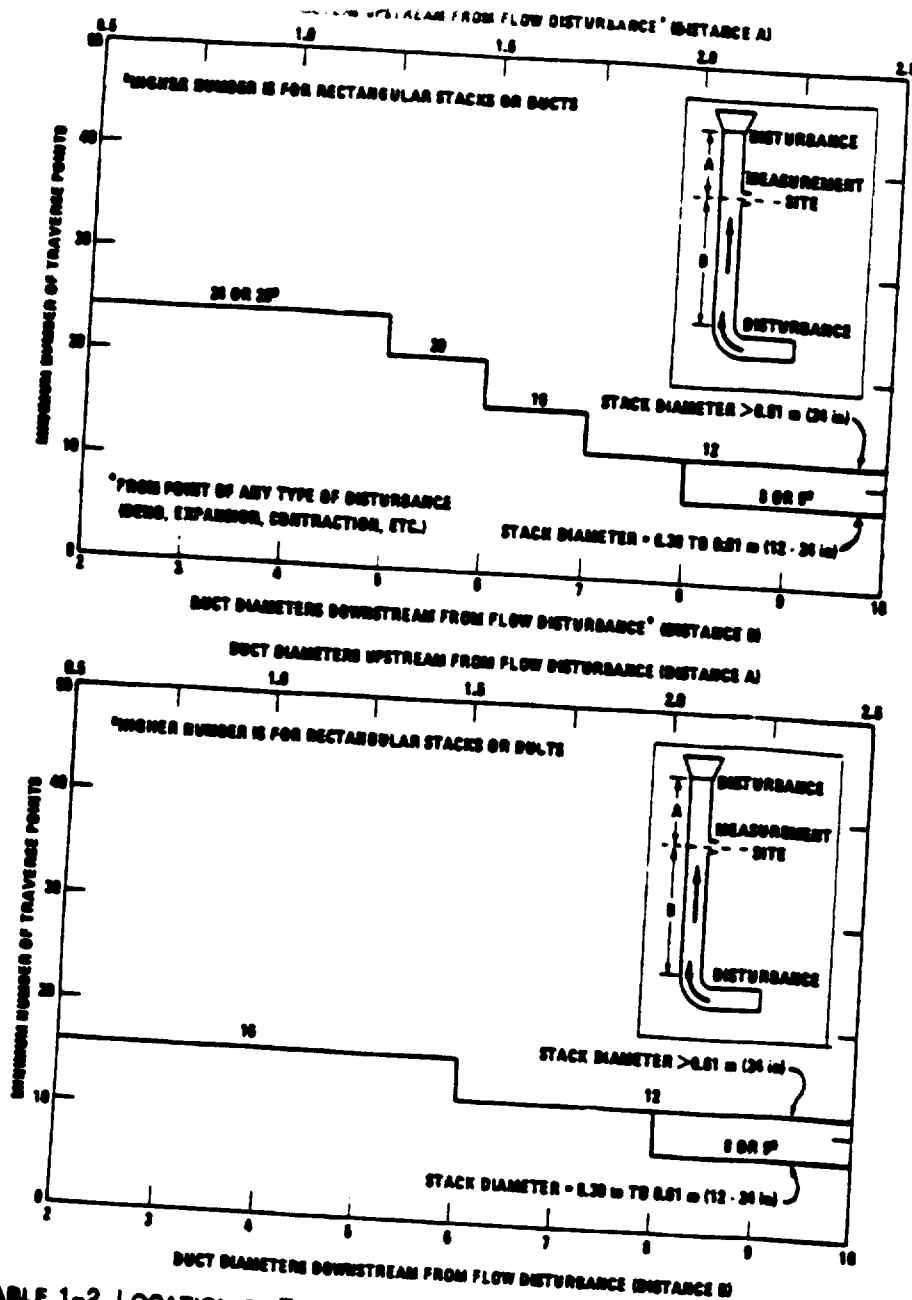


TABLE 1-2. LOCATION OF TRAVERSE POINTS IN CIRCULAR STACKS

(Percent of stack diameter from inside wall to traverse point)

| Traverse point number on a diameter | Number of traverse points on a diameter— |      |      |      |      |      |      |      |      |      |      |      |
|-------------------------------------|------------------------------------------|------|------|------|------|------|------|------|------|------|------|------|
|                                     | 2                                        | 4    | 6    | 8    | 10   | 12   | 14   | 16   | 18   | 20   | 22   | 24   |
| 1                                   | 14.6                                     | 6.7  | 4.4  | 3.2  | 2.6  | 2.1  | 1.8  | 1.6  | 1.4  | 1.3  | 1.1  | 1.1  |
| 2                                   | 86.4                                     | 25.0 | 14.6 | 10.5 | 8.2  | 6.7  | 5.7  | 4.9  | 4.4  | 3.9  | 3.5  | 3.2  |
| 3                                   |                                          | 75.0 | 29.8 | 19.4 | 14.6 | 11.8 | 9.9  | 8.5  | 7.5  | 6.7  | 6.0  | 5.6  |
| 4                                   |                                          | 83.3 | 70.4 | 32.3 | 22.8 | 17.7 | 14.6 | 12.5 | 10.9 | 9.7  | 8.7  | 7.9  |
| 5                                   |                                          |      | 85.4 | 67.7 | 34.2 | 25.0 | 20.1 | 16.9 | 14.6 | 12.9 | 11.6 | 10.5 |
| 6                                   |                                          |      | 86.6 | 69.6 | 35.6 | 26.9 | 22.0 | 18.8 | 16.5 | 14.6 | 13.2 | 12.1 |
| 7                                   |                                          |      |      | 88.5 | 77.4 | 64.4 | 36.8 | 26.3 | 23.6 | 20.4 | 18.0 | 16.1 |
| 8                                   |                                          |      |      | 89.8 | 85.4 | 75.0 | 63.4 | 37.5 | 29.6 | 25.0 | 21.8 | 19.4 |
| 9                                   |                                          |      |      |      | 91.8 | 82.3 | 73.1 | 62.5 | 38.2 | 30.6 | 26.2 | 23.0 |
| 10                                  |                                          |      |      |      | 97.4 | 86.2 | 79.9 | 71.7 | 61.8 | 38.8 | 31.5 | 27.2 |
| 11                                  |                                          |      |      |      |      | 93.3 | 85.4 | 78.0 | 70.4 | 61.2 | 38.3 | 32.3 |
| 12                                  |                                          |      |      |      |      | 97.9 | 90.1 | 83.1 | 76.4 | 68.4 | 60.7 | 38.8 |
| 13                                  |                                          |      |      |      |      |      | 94.3 | 87.5 | 81.2 | 75.0 | 68.5 | 60.2 |
| 14                                  |                                          |      |      |      |      |      | 96.2 | 91.5 | 85.4 | 79.6 | 73.8 | 67.7 |
| 15                                  |                                          |      |      |      |      |      |      | 96.1 | 90.1 | 83.5 | 78.2 | 72.8 |
| 16                                  |                                          |      |      |      |      |      |      | 98.4 | 92.5 | 87.1 | 82.0 | 77.0 |
| 17                                  |                                          |      |      |      |      |      |      |      | 95.6 | 90.3 | 85.4 | 80.6 |
| 18                                  |                                          |      |      |      |      |      |      |      | 98.6 | 93.3 | 88.4 | 83.9 |
| 19                                  |                                          |      |      |      |      |      |      |      |      | 96.1 | 91.3 | 86.6 |
| 20                                  |                                          |      |      |      |      |      |      |      |      | 98.7 | 94.0 | 89.5 |
| 21                                  |                                          |      |      |      |      |      |      |      |      |      | 96.5 | 92.1 |
| 22                                  |                                          |      |      |      |      |      |      |      |      |      | 98.9 | 94.5 |
| 23                                  |                                          |      |      |      |      |      |      |      |      |      |      | 96.8 |
| 24                                  |                                          |      |      |      |      |      |      |      |      |      |      | 98.9 |

TABLE 1-1. CROSS-SECTION LAYOUT FOR RECTANGULAR STACKS

| Number of traverse points | Layout |
|---------------------------|--------|
| 9                         |        |
| 12                        |        |
| 16                        |        |
| 20                        |        |
| 24                        |        |
| 28                        |        |
| 32                        |        |
| 36                        |        |
| 40                        |        |
| 44                        |        |
| 48                        |        |
| 52                        |        |
| 56                        |        |
| 60                        |        |
| 64                        |        |
| 68                        |        |
| 72                        |        |
| 76                        |        |
| 80                        |        |
| 84                        |        |
| 88                        |        |
| 92                        |        |
| 96                        |        |
| 100                       |        |

## STACK SAMPLING DATA SHEET

CLR-203

PLANT: CLAIMED

LOCATION: BATTERY STACK #3

ACTIVITY NO: \_\_\_\_\_

CONTROL BOX OPERATOR \_\_\_\_\_

PROBE HANDLER \_\_\_\_\_

CLEAN UP \_\_\_\_\_

DATE: 8-1-90

TEST NO.: CLR-B53-1

NOZZLE: (199) #55

STATIC PRESSURE PS: -1.2

PORT DIRECTION: 29 A, B

BAROMETRIC PRESSURE 29.49

AM: 1.573

METER CORRECTION: 1.0519

PITOT CORRECTION: 1.84

CONTROL BOX NO.: 1

PHOTOGRAPH SET POINT: \_\_\_\_\_

LENGTHS OF UMBILICAL \_\_\_\_\_

HOT BOX NO.: 6

COLD BOX NO.: 6

PROBE NO.: 37-3

FILTER NO.: 452

STACK DIA.: 114"

\_\_\_\_\_ x 25'

\_\_\_\_\_ x 50'

| Point | Time | Meter Reading (dry) CF | Velocity HD In. H <sub>2</sub> O | Orifice ΔH In. H <sub>2</sub> O Reg. Act. | Meter Temp. °F |        | Vacuum Vm In. Hg | Stack Temp. T <sub>s</sub> °F | Probe Temp. T <sub>p</sub> °F | Imp. Temp. T <sub>i</sub> °C/°F | Hot Box Temp. T <sub>h</sub> °F | Comments |
|-------|------|------------------------|----------------------------------|-------------------------------------------|----------------|--------|------------------|-------------------------------|-------------------------------|---------------------------------|---------------------------------|----------|
| 40.6  | 0948 | 638.907                | 1.07                             | 1.73 1.73                                 | In 70          | Out 75 | 8.0              | 527                           | 200                           | Ficed down 148                  | 250                             | Sm/PT    |
| 28.5  |      |                        | 1.065                            | 1.60 1.60                                 | In 82          | Out 73 | 7.5              | 522                           | 260                           |                                 |                                 |          |
| 20.2  |      |                        | 1.07                             | 1.73 1.73                                 | In 84          | Out 74 | 8.0              | 530                           |                               |                                 |                                 |          |
| 13.5  |      |                        | 1.06                             | 1.48 1.48                                 | In 89          | Out 79 | 7.5              | 525                           |                               | 57                              |                                 |          |
| 7.6   |      |                        | 1.045                            | 1.11 1.11                                 | In 89          | Out 78 | 5.0              | 522                           |                               |                                 |                                 |          |
| 2.4   | 1018 | 657.431                | 1.035                            | 0.86 0.86                                 | In 89          | Out 79 | 4.5              | 519                           |                               |                                 |                                 |          |
| 40.6  | 1020 | 657.431                | 1.065                            | 1.60 1.60                                 | In 88          | Out 82 | 7.5              | 545                           | 260                           |                                 | 260                             |          |
| 28.5  |      |                        | 1.07                             | 1.73 1.73                                 | In 94          | Out 83 | 8.0              | 550                           |                               |                                 |                                 |          |
| 20.2  |      |                        | 1.07                             | 1.74 1.74                                 | In 95          | Out 85 | 8.0              | 565                           |                               | 56                              |                                 |          |
| 13.5  |      |                        | 1.07                             | 1.74 1.74                                 | In 96          | Out 86 | 8.0              | 545                           |                               |                                 |                                 |          |
| 7.6   |      |                        | 1.05                             | 1.24 1.24                                 | In 97          | Out 87 | 6.0              | 535                           |                               |                                 |                                 |          |
| 2.4   | 1050 | 677.358                | 1.04                             | 1.0 1.0                                   | In 97          | Out 88 | 5.0              | 530                           |                               |                                 |                                 |          |

| Impinger No. | Final | Initial | Difference |
|--------------|-------|---------|------------|
| 1 100ml      | 748.9 | 549.5   | 200.4      |
| 2 100ml      | 538.1 | 494.0   | 44.1       |
| 3 242        | 457.7 | 453.4   | 4.3        |
| 4 5160       | 676.2 | 660.5   | 15.7       |
| 5            |       |         |            |

Pitot K 7.5  
 Check = 0.1 K 7.5  
 Rec'd = 0.1 K 7.5  
 Rec'd = 0.1 K 7.5

| ORSAT           | 1    | 2    | 3 |
|-----------------|------|------|---|
| CO <sub>2</sub> | 4.0  | 3.5  |   |
| O <sub>2</sub>  | 12.5 | 12.5 |   |
| CO              |      |      |   |
| N               |      |      |   |

| LEAK CHECK | In Hg | Rate |
|------------|-------|------|
| Before     | 6.0   | 1.00 |
| After      | 6.0   | 1.00 |







STACK SAMPLING DATA SHEET

PLANT: CLARIANT DATE: 8-1-90 AM: 1:573 HOT BOX NO.: 5  
LOCATION: BATTERY STACK #3 TEST NO.: CLR-CS3-2 METER CORRECTION: 1.0519 COLD BOX NO.: 5  
ACTIVITY NO.: 499 #55 NOZZLE: 499 #55 PITOT CORRECTION: 1.84 PROBE NO.: 7-1  
CONTROL BOX OPERATOR: A.B STATIC PRESSURE PS: -1.2 CONTROL BOX NO.: 1 FILTER NO.: 463  
PROBE HANDLER: A.B PORT DIRECTION: A.B NOMOGRAPH SET POINT: 25 STACK DIA.: 114  
CLEAN UP: 2949 BAROMETRIC PRESSURE 29.49 LENGTHS OF UMBILICAL 25 x 50

| Point | Time | Meter Reading (dry) CF | Velocity MD In. H <sub>2</sub> O | Orifice ΔH In. H <sub>2</sub> O |      | Meter Temp. °F |     | Vacuum Vm In. Hg | Stack Temp. T <sub>st</sub> °F | Probe Temp. T <sub>p</sub> °F | Imp. Temp. T <sub>i</sub> °C/°F | Hot Box Temp. T <sub>h</sub> °F | Comments |
|-------|------|------------------------|----------------------------------|---------------------------------|------|----------------|-----|------------------|--------------------------------|-------------------------------|---------------------------------|---------------------------------|----------|
|       |      |                        |                                  | Req.                            | Act. | In             | Out |                  |                                |                               |                                 |                                 |          |
| 40.6  | 1228 | 715.137                | 1.065                            | 1.65                            | 1.65 | 103            | 100 | 7.0              | 551                            | 260                           | Ficed down 468                  | 255                             | 5-1/8"   |
| 28.5  |      |                        | 1.075                            | 1.90                            | 1.90 | 108            | 101 | 8.0              | 570                            |                               |                                 |                                 |          |
| 20.2  |      |                        | 1.075                            | 1.85                            | 1.85 | 110            | 100 | 8.0              | 579                            |                               | 58                              |                                 |          |
| 13.5  |      |                        | 1.08                             | 1.97                            | 1.97 | 110            | 101 | 8.5              | 583                            |                               |                                 |                                 |          |
| 7.6   |      |                        | 1.065                            | 1.60                            | 1.60 | 111            | 100 | 7.0              | 577                            |                               |                                 |                                 |          |
| 2.4   | 1258 | 736.668                | 1.05                             | 1.23                            | 1.23 | 111            | 102 | 6.0              | 575                            |                               |                                 |                                 |          |
| 40.6  | 1300 | 736.668                | 1.065                            | 1.60                            | 1.60 | 108            | 101 | 7.0              | 530                            | 260                           | Ficed down 468                  | 255                             |          |
| 28.5  |      |                        | 1.065                            | 1.60                            | 1.60 | 113            | 103 | 7.0              | 536                            |                               |                                 |                                 |          |
| 20.2  |      |                        | 1.075                            | 1.85                            | 1.85 | 114            | 103 | 8.0              | 549                            |                               |                                 |                                 |          |
| 13.5  |      |                        | 1.075                            | 1.85                            | 1.85 | 115            | 104 | 8.0              | 545                            |                               | 56                              |                                 |          |
| 7.6   |      |                        | 1.06                             | 1.48                            | 1.48 | 114            | 104 | 6.5              | 542                            |                               |                                 |                                 |          |
| 2.4   | 1330 | 758.048                | 0.055                            | 1.36                            | 1.36 | 114            | 105 | 6.0              | 540                            |                               |                                 |                                 |          |

| Initial | Final | Impinger No. | Difference |
|---------|-------|--------------|------------|
| 538.9   | 727.8 | 1 100ml      | 188.9      |
| 501.3   | 545.0 | 2 100ml      | 43.7       |
| 446.1   | 472.7 | 3 20ml       | 26.6       |
| 657.7   | 677.2 | 4 5.16ml     | 19.5       |

PITOT Check 215  
Red = 0.1K 5 sec  
GAGE = 0.1K 5 sec

| LEAK CHECK |          | ORSAT           |      |
|------------|----------|-----------------|------|
| In Hg      | Rate     | 1               | 2    |
| Before 5.0 | 4.02 CFH | 4.0             | 3.5  |
| After 5.0  | 4.02 CFH | 12.5            | 13.5 |
|            |          | CO <sub>2</sub> | CO   |
|            |          | 13.5            | 13.0 |

**STACK SAMPLING DATA SHEET**

PLANT: CLINTON DATE: 8-1-90 ΔH:            HOT BOX NO.:             
 LOCATION: BATTAY STACK #3 TEST NO.: CLRCS3-2 METER CORRECTION:            COLD BOX NO.:             
 ACTIVITY NO.:            NOZZLE:            PITOT CORRECTION:            PROBE NO.:             
 CONTROL BOX OPERATOR:            STATIC PRESSURE PS:            CONTROL BOX NO.:            FILTER NO.:             
 PROBE HANDLER:            PORT DIRECTION: LD MONOGRAPH SET POINT:            STACK DIA.:             
 CLEAN UP:            BAROMETRIC PRESSURE 29.49 LENGTHS OF UMBILICAL 25' x 50'

| Point | Time | Meter Reading (dry) CF | Velocity HD in. H <sub>2</sub> O | Orifice ΔH in. H <sub>2</sub> O Reg. Act. | Meter Temp. °F In Out | Vacuum Vm in. Hg | Stack Temp. °F | Probe Temp. °F | Imp. Temp. °C/°F | Hot Box Temp. °F | Comments |
|-------|------|------------------------|----------------------------------|-------------------------------------------|-----------------------|------------------|----------------|----------------|------------------|------------------|----------|
| 40.6  | 1335 | 758.048                | 1.055                            | 1.36 1.36                                 | 106 102               | 6.0              | 530            | 260            | iced down 68     | 255              | 5 m/pt   |
| 28.5  |      |                        | 1.07                             | 1.73 1.73                                 | 103 105               | 8.0              | 533            |                |                  |                  |          |
| 20.2  |      |                        | 1.07                             | 1.73 1.73                                 | 116 105               | 8.0              | 525            |                |                  |                  |          |
| 13.5  |      |                        | 1.065                            | 1.60 1.60                                 | 116 107               | 7.0              | 527            |                | 59               |                  |          |
| 7.6   |      |                        | 1.05                             | 1.23 1.23                                 | 115 105               | 6.0              | 524            |                |                  |                  |          |
| 2.4   | 1405 | 778.208                | 1.04                             | 1.99 1.99                                 | 114 106               | 4.5              | 523            |                |                  |                  |          |
| 40.6  | 1413 | 778.208                | 1.065                            | 1.60 1.60                                 | 112 104               | 7.0              | 535            | 260            | iced down 68     | 250              |          |
| 28.5  |      |                        | 1.065                            | 1.60 1.60                                 | 115 106               | 7.0              | 535            |                |                  |                  |          |
| 20.2  |      |                        | 1.06                             | 1.48 1.48                                 | 115 105               | 7.0              | 545            |                |                  |                  |          |
| 13.5  |      |                        | 1.055                            | 1.36 1.36                                 | 114 105               | 6.0              | 551            |                |                  |                  |          |
| 7.6   |      |                        | 1.045                            | 1.11 1.11                                 | 113 104               | 5.0              | 539            |                | 60               |                  |          |
| 2.4   | 1443 | 797.565                | 1.04                             | 1.99 1.99                                 | 113 104               | 5.0              | 532            |                |                  |                  |          |
| 40.6  |      |                        |                                  |                                           |                       |                  |                |                |                  |                  |          |
| 28.5  |      |                        |                                  |                                           |                       |                  |                |                |                  |                  |          |
| 20.2  |      |                        |                                  |                                           |                       |                  |                |                |                  |                  |          |
| 13.5  |      |                        |                                  |                                           |                       |                  |                |                |                  |                  |          |
| 7.6   |      |                        |                                  |                                           |                       |                  |                |                |                  |                  |          |
| 2.4   |      |                        |                                  |                                           |                       |                  |                |                |                  |                  |          |

| Impinger No. | Final | Initial | Difference |
|--------------|-------|---------|------------|
| 1            |       |         |            |
| 2            |       |         |            |
| 3            |       |         |            |
| 4            |       |         |            |
| 5            |       |         |            |

| LEAK CHECK |       |      |  | ORSAT |   |   |  |
|------------|-------|------|--|-------|---|---|--|
| Before     | in Hg | Rate |  | 1     | 2 | 3 |  |
|            |       |      |  |       |   |   |  |
|            |       |      |  |       |   |   |  |
|            |       |      |  |       |   |   |  |
|            |       |      |  |       |   |   |  |

## STACK SAMPLING DATA SHEET

PLANT: CLARION DATE: 8-1-90 ΔH: 1.573 HOT BOX NO.: 7  
 LOCATION: BATTERY/Stack #3 TEST NO.: CLR-C53-3 METER CORRECTION: 1.0519 COLD BOX NO.: 7  
 ACTIVITY NO.: NOZZLE: 499 #55 NOZZLE CORRECTION: 1.84 PROBE NO.: 7-2  
 CONTROL BOX OPERATOR: STATIC PRESSURE PS: -1.2 CONTROL BOX NO.: 1 FILTER NO.: 454  
 PROBE HANDLER: PORT DIRECTION: A, B MONOGRAPH SET POINT: STACK DIA.: 114  
 CLEAN UP: BAROMETRIC PRESSURE 29.49 LENGTHS OF UMBILICAL 25' × 50'

| Point  | Time | Meter Reading (dry) CF | Velocity in. H <sub>2</sub> O | Orifice ΔH in. H <sub>2</sub> O Reg. Act. | Meter Temp. Tm °F In Out | Vacuum Vm in. Hg | Stack Temp. Ts °F | Probe Temp. Tp °F | Imp. Temp. TI °C/°F | Hot Box Temp. TH °F | Comments |
|--------|------|------------------------|-------------------------------|-------------------------------------------|--------------------------|------------------|-------------------|-------------------|---------------------|---------------------|----------|
| 40.6   | 1512 | 798.025                | 1.075                         | 1.85 1.85                                 | 112 105                  | 6.0              | 549               | 260               | iced down 468       | 255                 | Sm/PT    |
| 28.5   |      |                        | .08                           | 1.97 1.97                                 | 117 107                  | 6.0              | 539               |                   |                     |                     |          |
| 20.2   |      |                        | .09                           | 2.22 2.22                                 | 118 108                  | 7.5              | 546               |                   | 61                  |                     |          |
| 13.5   |      |                        | .085                          | 2.10 2.10                                 | 118 107                  | 6.5              | 554               |                   |                     |                     |          |
| 7.6    |      |                        | .085                          | 2.10 2.10                                 | 118 107                  | 6.5              | 547               |                   |                     |                     |          |
| 2.4    | 1542 | 820.115                | .07                           | 1.73 1.73                                 | 118 107                  | 5.5              | 545               |                   |                     |                     |          |
| Port-B |      |                        |                               |                                           |                          |                  |                   |                   |                     |                     |          |
| 40.6   | 1544 | 820.115                | .09                           | 2.22 2.22                                 | 113 107                  | 7.5              | 527               | 260               | iced down 468       | 250                 |          |
| 28.5   |      |                        | .085                          | 2.10 2.10                                 | 117 107                  | 6.5              | 521               |                   |                     |                     |          |
| 20.2   |      |                        | .09                           | 2.22 2.22                                 | 116 106                  | 7.5              | 518               |                   | 62                  |                     |          |
| 13.5   |      |                        | .09                           | 2.22 2.22                                 | 117 106                  | 7.5              | 521               |                   |                     |                     |          |
| 7.6    |      |                        | .075                          | 1.95 1.95                                 | 117 106                  | 6.0              | 523               |                   |                     |                     |          |
| 2.4    | 1614 | 844.806                | .07                           | 1.82 1.82                                 | 117 107                  | 6.0              | 518               |                   |                     |                     |          |
| 6      |      |                        |                               |                                           |                          |                  |                   |                   |                     |                     |          |

| Initial | Final | Impinger No. | Impinger No. | Initial | Difference |
|---------|-------|--------------|--------------|---------|------------|
| 557.8   | 779.4 | 1 reel       | 1 reel       | 557.8   | 221.6      |
| 549.0   | 594.8 | 2,000 ml     | 2,000 ml     | 549.0   | 45.8       |
| 445.4   | 450.4 | 3 reel       | 3 reel       | 445.4   | 5.0        |
| 695.0   | 712.3 | 450 cc       | 450 cc       | 695.0   | 17.3       |
|         |       | 5            | 5            |         |            |

P.T. Check  
 Red = O.K. 15 sec  
 Green = O.K.

| LEAK CHECK | in Hg | Rate  |
|------------|-------|-------|
| Before     | 5.0   | 1.00% |
| After      |       | 1.00% |

| ORSAT           | 1    | 2    | 3 |
|-----------------|------|------|---|
| CO <sub>2</sub> | 4.0  | 4.0  |   |
| O <sub>2</sub>  | 12.0 | 12.0 |   |
| CO              |      |      |   |
| N               |      |      |   |

# STACK SAMPLING DATA SHEET

PLANT: Clairton DATE: 8-1-90 AM#:

LOCATION: BATTERY STACK #3 TEST NO.: CLR-53-3 COLD BOX NO.:

ACTIVITY NO: NOZZLE: 799 #55 PITOT CORRECTION: PROBE NO.:

CONTROL BOX OPERATOR STATIC PRESSURE PS: -1.2 CONTROL BOX NO.: FILTER NO.:

PROBE HANDLER PORT DIRECTION: C, B, C, D MONOGRAPH SET POINT: STACK DIA.:

CLEAN UP BAROMETRIC PRESSURE 29.49 LENGTHS OF UMBILICAL x 25' x 50'

[illegible]

| Impinger No. | Final | Initial | Difference |
|--------------|-------|---------|------------|
| 1            | 779.4 | 557.8   | 221.6      |
| 2            | 594.8 | 549.0   | 45.8       |
| 3            | 450.4 | 445.4   | 5.0        |
| 4            | 712.3 | 695.0   | 17.3       |
| 5            |       |         |            |

| LEAK CHECK |       | ORSAT |                 |   |   |
|------------|-------|-------|-----------------|---|---|
|            | In Hg | Rate  | 1               | 2 | 3 |
| before     |       |       |                 |   |   |
| after      |       |       |                 |   |   |
|            |       |       | CO <sub>2</sub> |   |   |
|            |       |       | O <sub>2</sub>  |   |   |
|            |       |       | CO              |   |   |
|            |       |       | N               |   |   |

**USS CLAIRTON WORKS  
RESULTS OF THE  
COMPLIANCE DEMONSTRATION OF THE  
#3 BATTERY COMBUSTION STACK**

**APPENDIX D  
PARTICULATE MATTER  
EMISSIONS CALCULATIONS**

Plant: Clairton Steel Date: 8/3/90

Activity No. 601050-06

### PARTICULATE REPORTING FORM

| Test Number | Component | Molecular Weight | Cyclone Weight | Particulate Filter Weight (g) | Insol. Part. in Front Half | Insol. Part. in Back Half | Soluble Part. in Back Half | Soluble Part. in Front Half |
|-------------|-----------|------------------|----------------|-------------------------------|----------------------------|---------------------------|----------------------------|-----------------------------|
| CLR-CS3-1   |           |                  |                | 0.0480                        |                            |                           |                            | 0.0069                      |
| CLR-CS3-2   |           |                  |                | 0.0431                        |                            |                           |                            | 0.0071                      |
| CLR-CS3-3   |           |                  |                | 0.0680                        |                            |                           |                            | 0.0144                      |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
|             |           |                  |                |                               |                            |                           |                            |                             |
| D-1         |           |                  |                |                               |                            |                           |                            |                             |

AIR QUALITY ENGINEERING  
USX CLAIRTON COKE WORKS  
CLAIRTON  
COMBUSTION STACK 3

DATE: .....8-1-90  
CHARGE #: ...150-601050  
TEST #: .....CLR-CS3-1

1. EMISSION RESULTS

| PARAMETER   | GR/SCFD | LB/HR   |
|-------------|---------|---------|
| PARTICULATE | .01118  | 3.41358 |

2. STACK CONDITIONS

|                       |        |
|-----------------------|--------|
| FLOW (ACFM)           | 80021. |
| (SCFM)                | 41492. |
| MOISTURE CONTENT (%)  | 14.16  |
| STACK TEMPERATURE (F) | 540.7  |

3. SAMPLING CONDITIONS

|                    |        |
|--------------------|--------|
| SAMPLE TIME (MIN.) | 120.0  |
| SCFD GAS SAMPLED   | 75.613 |
| PERCENT ISOKINETIC | 92.33  |



# AIR QUALITY ENGINEERING

USX CLAIRTON COKE WORKS  
CLAIRTON COMBUSTION  
CLR-CS3-1 8-1-90

## FIELD DATA AND VELOCITY CALCULATIONS

| POINT | TIME   | METER<br>READING<br>(DRY) CF | DELTA P<br>IN. H2O | ORIFICE<br>DELTA H<br>REQ ACT | METER<br>TEMP<br>DEG F<br>IN OUT | VACUUM<br>IN. HG. | STACK<br>TEMP<br>DEG | CORRECTED<br>VELOCITY<br>FFT/SEC |
|-------|--------|------------------------------|--------------------|-------------------------------|----------------------------------|-------------------|----------------------|----------------------------------|
| 40.6A | 948.0  | 638.907                      | .070               | 1.73 1.73                     | 70. 75.                          | 8.0               | 527.                 | 20.9                             |
| 28.5  |        |                              | .065               | 1.60 1.60                     | 82. 73.                          | 7.5               | 522.                 | 20.1                             |
| 20.2  |        |                              | .070               | 1.73 1.73                     | 84. 74.                          | 8.0               | 530.                 | 21.0                             |
| 13.5  |        |                              | .060               | 1.48 1.48                     | 89. 79.                          | 7.5               | 525.                 | 19.4                             |
| 7.6   |        |                              | .045               | 1.11 1.11                     | 89. 78.                          | 5.0               | 522.                 | 16.7                             |
| 2.4A  | 1018.0 | 657.431                      | .035               | .86 .86                       | 89. 79.                          | 4.5               | 519.                 | 14.7                             |
| 40.6B | 1020.0 | 657.431                      | .065               | 1.60 1.60                     | 88. 82.                          | 7.5               | 545.                 | 20.3                             |
| 28.5  |        |                              | .070               | 1.73 1.73                     | 94. 83.                          | 8.0               | 550.                 | 21.2                             |
| 20.2  |        |                              | .070               | 1.74 1.74                     | 95. 85.                          | 8.0               | 565.                 | 21.3                             |
| 13.5  |        |                              | .070               | 1.74 1.74                     | 96. 86.                          | 8.0               | 545.                 | 21.1                             |
| 7.6   |        |                              | .050               | 1.24 1.24                     | 97. 87.                          | 6.0               | 535.                 | 17.8                             |
| 2.4B  | 1050.0 | 677.358                      | .040               | 1.00 1.00                     | 97. 88.                          | 5.0               | 530.                 | 15.8                             |
| 40.6C | 1055.0 | 677.358                      | .060               | 1.49 1.49                     | 96. 90.                          | 7.3               | 525.                 | 19.4                             |
| 28.5  |        |                              | .065               | 1.62 1.62                     | 100. 91.                         | 7.5               | 536.                 | 20.3                             |
| 20.2  |        |                              | .065               | 1.62 1.62                     | 101. 91.                         | 7.5               | 542.                 | 20.3                             |
| 13.5  |        |                              | .060               | 1.49 1.49                     | 101. 92.                         | 7.3               | 530.                 | 19.4                             |
| 7.6   |        |                              | .045               | 1.11 1.11                     | 102. 93.                         | 5.0               | 532.                 | 16.8                             |
| 2.4C  | 1125.0 | 696.413                      | .040               | 1.00 1.00                     | 103. 94.                         | 5.0               | 525.                 | 15.8                             |
| 40.6D | 1128.0 | 696.413                      | .065               | 1.62 1.62                     | 101. 96.                         | 7.5               | 550.                 | 20.4                             |
| 28.5  |        |                              | .060               | 1.49 1.49                     | 108. 98.                         | 7.3               | 562.                 | 19.7                             |
| 20.2  |        |                              | .050               | 1.25 1.25                     | 108. 98.                         | 6.0               | 570.                 | 18.1                             |
| 13.5  |        |                              | .055               | 1.38 1.38                     | 109. 99.                         | 6.6               | 571.                 | 19.0                             |
| 7.6   |        |                              | .040               | 1.00 1.00                     | 109. 99.                         | 5.0               | 560.                 | 16.1                             |
| 2.4D  | 1158.0 | 714.868                      | .040               | 1.00 1.00                     | 109. 100.                        | 5.0               | 558.                 | 16.1                             |

### O R S A T

CO2 3.8  
O2 12.5  
CO .0  
N 83.8

IMPINGER NO. 1 200.4

2 44.1

3 4.3

4 .0

ABSORBED H2O 15.7

### CONTROL BOX CALIBRATIONS

|         | FACTOR | DATE    |
|---------|--------|---------|
| ORIFICE | 1.573  | 6-12-90 |
| METER   | 1.0519 | 6-12-90 |
| PITOT   | 0.84   | 6-29-90 |

### LEAK CHECK

|         | RATE       | IN. HG |
|---------|------------|--------|
| INITIAL | LT 0.02CFM | 6.0    |
| FINAL   | 0.005CFM   | 9.0    |

CONTROL BOX NO. 1

PROBE NO. 7-3

NOZZLE NO. 55

# AIR QUALITY ENGINEERING

USX CLAIRTON COKE WORKS  
CLAIRTON COMBUSTION  
CLR-CS3-1 8-1-90

## STACK SAMPLING CALCULATIONS

|    |                                          |         |
|----|------------------------------------------|---------|
| A. | BAROMETRIC PRESSURE IN. HG.....          | 29.49   |
| B. | AVG. DELTA H (IN H2O).....               | 1.40    |
| C. | METER PRESSURE (IN. HG.).....            | 29.59   |
| D. | STATIC PRESSURE (IN. H2O).....           | -1.20   |
| E. | STATIC PRESSURE (IN. HG.).....           | -.088   |
| F. | STACK PRESSURE (IN. HG.) (A+E).....      | 29.40   |
| G. | STACK DIAMETER (IN.).....                | 114.00  |
| H. | STACK AREA (SQ. FT.).....                | 70.88   |
|    | NOZZLE DIAMETER.....                     | .4990   |
| I. | NOZZLE AREA (SQ. FT.).....               | .001358 |
| J. | AVG. STACK TEMP (DEG. R.).....           | 1000.7  |
| K. | AVG. METER TEMP (DEG. R.).....           | 552.2   |
| L. | CONDENSATE VOL. (ML).....                | 248.8   |
| M. | ABSORBED H2O (ML).....                   | 15.7    |
| N. | TOTAL H2O (ML).....                      | 264.5   |
| O. | METERED GAS (CF).....                    | 75.961  |
| P. | GAS METER CORRECTION.....                | 1.0519  |
| Q. | CORRECTED METERED GAS (CF).....          | 79.903  |
| R. | H2O GAS VOLUME (CF) (0.00267N(K/C).....  | 13.179  |
| S. | TOTAL SAMPLED VOLUME (CF) (Q+R).....     | 93.082  |
| T. | PERCENT H2O (100R/S).....                | 14.16   |
|    | THEORETICAL MAXIMUM.....                 | 100.00  |
|    | PERCENT WATER USED.....                  | 14.16   |
| U. | SCFD GAS SAMPLED (528*Q*C/(29.9*K))..... | 75.613  |

## V. MOLECULAR WEIGHT OF STACK GAS

| COMPONENT                           | ORSAT-DRY<br>VOL.PCT./100 | X | MOISTURE<br>CORRECTION<br>(1-T/100) | X | MOLECULAR<br>WEIGHT | = | WEIGHT<br>PER MOLE |
|-------------------------------------|---------------------------|---|-------------------------------------|---|---------------------|---|--------------------|
| CO2                                 | .038                      | X | .8584                               | X | 44.0                | = | 1.42               |
| CO                                  | .000                      | X | .8584                               | X | 28.0                | = | .00                |
| O2                                  | .125                      | X | .8584                               | X | 32.0                | = | 3.43               |
| N2                                  | .838                      | X | .8584                               | X | 28.2                | = | 20.27              |
| H2O                                 |                           | X | T/100= .1416                        | X | 18.0                | = | 2.55               |
| MOLECULAR<br>WEIGHT OF<br>STACK GAS |                           |   |                                     |   |                     |   | = 27.67            |

|     |                                               |        |
|-----|-----------------------------------------------|--------|
| W.  | PITOT CORRECTION.....                         | .840   |
| X.  | AVERAGE CORRECTED VELOCITY (FPS).....         | 18.82  |
|     | [85.49*W*SQRT{(J*DELTA P)/(V*F)}]             |        |
| Y.  | AVG. FLOW RATE (CFM) (X*H*60).....            | 80021. |
| Z.  | STACK FLOW RATE (SCFM) (528*Y/J*F/29.92)..... | 41492. |
|     | STACK FLOW RATE (DRY).....                    | 35617. |
| AA. | SAMPLE TIME (SEC).....                        | 7200.  |
| BB. | PERCENT ISOKINETIC.....                       | 92.33  |
|     | (J*100*U*29.92)/(528*X*AA*I*F*(1-T/100))      |        |

# AIR QUALITY ENGINEERING

USX CLAIRTON COKE WORKS  
 CLAIRTON COMBUSTION  
 CLR-CS3-1 8-1-90

| PARAMETER   | CYCLONE<br>WT. (G) | MATL.ON<br>FILTER(G) | INSOL.MATL.<br>IN PROBE(G) | SOL.MATL.<br>IN PROBE(G) |
|-------------|--------------------|----------------------|----------------------------|--------------------------|
| PARTICULATE | .00000             | .04800               | .00000                     | .00690                   |

| PARAMETER   | INSOL.MATL.<br>IN IMP. (G) | SOLUBLE MATL.<br>IN IMP. (G) |
|-------------|----------------------------|------------------------------|
| PARTICULATE | .00000                     | .00000                       |

PARTICULATE .05490

ALL MATLS. .05490

| PARAMETER   | GR/SCFD | LB/HR   |
|-------------|---------|---------|
| PARTICULATE | .01118  | 3.41358 |

Emission rates are based on EPA Method 5.

AIR QUALITY ENGINEERING  
USX CLAIRTON COKE WORKS  
CLAIRTON  
COMBUSTION STACK 3

DATE: .....8-1-90  
CHARGE #: ...150-601050  
TEST #: .....CLR-CS3-2

1. EMISSION RESULTS

| PARAMETER   | GR/SCFD | LB/HR   |
|-------------|---------|---------|
| PARTICULATE | .00969  | 3.09353 |

2. STACK CONDITIONS

|                       |        |
|-----------------------|--------|
| FLOW (ACFM)           | 84075. |
| (SCFM)                | 43398. |
| MOISTURE CONTENT (%)  | 14.14  |
| STACK TEMPERATURE (F) | 545.2  |

3. SAMPLING CONDITIONS

|                    |        |
|--------------------|--------|
| SAMPLE TIME (MIN.) | 120.0  |
| SCFD GAS SAMPLED   | 79.819 |
| PERCENT ISOKINETIC | 93.16  |

# AIR QUALITY ENGINEERING

USX CLAIRTON COKE WORKS  
CLAIRTON COMBUSTION  
CLR-CS3-2 8-1-90

## FIELD DATA AND VELOCITY CALCULATIONS

| POINT | TIME   | METER               | DELTA P | ORIFICE |         | METER         |        | VACUUM | STACK       | CORRECTED           |
|-------|--------|---------------------|---------|---------|---------|---------------|--------|--------|-------------|---------------------|
|       |        | READING<br>(DRY) CF |         | DELTA H | REQ ACT | TEMP<br>DEG F | IN OUT |        | TEMP<br>DEG | VELOCITY<br>FFT/SEC |
| 40.6A | 1228.0 | 715.137             | .065    | 1.65    | 1.65    | 103.          | 100.   | 7.0    | 561.        | 20.5                |
| 28.5  |        |                     | .075    | 1.90    | 1.90    | 108.          | 101.   | 8.0    | 570.        | 22.1                |
| 20.2  |        |                     | .075    | 1.85    | 1.85    | 110.          | 100.   | 8.0    | 579.        | 22.2                |
| 13.5  |        |                     | .080    | 1.97    | 1.97    | 110.          | 101.   | 8.5    | 583.        | 23.0                |
| 7.6   |        |                     | .065    | 1.60    | 1.60    | 111.          | 100.   | 7.0    | 577.        | 20.7                |
| 2.4A  | 1258.0 | 736.668             | .050    | 1.23    | 1.23    | 111.          | 102.   | 6.0    | 575.        | 18.1                |
| 40.6B | 1300.0 | 736.668             | .065    | 1.60    | 1.60    | 108.          | 101.   | 7.0    | 530.        | 20.2                |
| 28.5  |        |                     | .065    | 1.00    | 1.00    | 113.          | 103.   | 7.0    | 536.        | 20.2                |
| 20.2  |        |                     | .075    | 1.85    | 1.85    | 114.          | 103.   | 8.0    | 549.        | 21.9                |
| 13.5  |        |                     | .075    | 1.85    | 1.85    | 115.          | 104.   | 8.0    | 545.        | 21.8                |
| 7.6   |        |                     | .060    | 1.48    | 1.48    | 114.          | 104.   | 6.5    | 542.        | 19.5                |
| 2.4B  | 1330.0 | 758.048             | .055    | 1.36    | 1.36    | 114.          | 105.   | 6.0    | 540.        | 18.7                |
| 40.6C | 1335.0 | 758.048             | .055    | 1.36    | 1.36    | 106.          | 102.   | 6.0    | 530.        | 18.6                |
| 28.5  |        |                     | .070    | 1.73    | 1.73    | 113.          | 105.   | 8.0    | 533.        | 21.0                |
| 20.2  |        |                     | .070    | 1.73    | 1.73    | 116.          | 105.   | 8.0    | 525.        | 20.9                |
| 13.5  |        |                     | .065    | 1.60    | 1.60    | 116.          | 107.   | 7.0    | 527.        | 20.2                |
| 7.6   |        |                     | .050    | 1.23    | 1.23    | 115.          | 105.   | 6.0    | 524.        | 17.7                |
| 2.4C  | 1405.0 | 778.208             | .040    | .99     | .99     | 114.          | 106.   | 4.5    | 523.        | 15.8                |
| 40.6D | 1413.0 | 778.208             | .065    | 1.60    | 1.60    | 112.          | 104.   | 7.0    | 535.        | 20.2                |
| 28.5  |        |                     | .065    | 1.60    | 1.60    | 115.          | 106.   | 7.0    | 535.        | 20.2                |
| 20.2  |        |                     | .060    | 1.48    | 1.48    | 115.          | 105.   | 7.0    | 545.        | 19.5                |
| 13.5  |        |                     | .055    | 1.36    | 1.36    | 114.          | 105.   | 6.0    | 551.        | 18.8                |
| 7.6   |        |                     | .045    | 1.11    | 1.11    | 113.          | 104.   | 5.0    | 537.        | 16.9                |
| 2.4D  | 1443.0 | 797.565             | .040    | .99     | .99     | 113.          | 104.   | 5.0    | 532.        | 15.9                |

### O R S A T

CO2 3.8  
O2 13.0  
CO .0  
N 83.3

IMPINGER NO. 1 188.9  
2 43.7  
3 26.6  
4 .0  
ABSORBED H2O 19.5

### CONTROL BOX CALIBRATIONS

|         | FACTOR | DATE    |
|---------|--------|---------|
| ORIFICE | 1.573  | 6-12-90 |
| METER   | 1.0519 | 6-12-90 |
| PITOT   | 0.84   | 6-29-90 |

### LEAK CHECK

|            | RATE    | IN.HG |
|------------|---------|-------|
| INITIAL LT | 0.02CFM | 5.0   |
| FINAL LT   | .008CFM | 10.0  |

CONTROL BOX NO. 1

PROBE NO. 7-1

NOZZLE NO. 55

# AIR QUALITY ENGINEERING

USX CLAIRTON COKE WORKS  
CLAIRTON COMBUSTION  
CLR-CS3-2 8-1-90

## STACK SAMPLING CALCULATIONS

|    |                                          |         |
|----|------------------------------------------|---------|
| A. | BAROMETRIC PRESSURE IN. HG.....          | 29.49   |
| B. | AVG. DELTA H (IN H2O).....               | 1.51    |
| C. | METER PRESSURE (IN. HG.).....            | 29.60   |
| D. | STATIC PRESSURE (IN. H2O).....           | -1.20   |
| E. | STATIC PRESSURE (IN. HG.).....           | -.088   |
| F. | STACK PRESSURE (IN. HG.) (A+E).....      | 29.40   |
| G. | STACK DIAMETER (IN.).....                | 114.00  |
| H. | STACK AREA (SQ. FT.).....                | 70.88   |
|    | NOZZLE DIAMETER.....                     | .4990   |
| I. | NOZZLE AREA (SQ. FT.).....               | .001358 |
| J. | AVG. STACK TEMP (DEG. R.).....           | 1005.2  |
| K. | AVG. METER TEMP (DEG. R.).....           | 567.8   |
| L. | CONDENSATE VOL. (ML).....                | 259.2   |
| M. | ABSORBED H2O (ML).....                   | 19.5    |
| N. | TOTAL H2O (ML).....                      | 278.7   |
| O. | METERED GAS (CF).....                    | 82.428  |
| P. | GAS METER CORRECTION.....                | 1.0519  |
| Q. | CORRECTED METERED GAS (CF).....          | 86.706  |
| R. | H2O GAS VOLUME (CF) (0.00267N(K/C))..... | 14.274  |
| S. | TOTAL SAMPLED VOLUME (CF) (Q+R).....     | 100.980 |
| T. | PERCENT H2O (100R/S).....                | 14.14   |
|    | THEORETICAL MAXIMUM.....                 | 100.00  |
|    | PERCENT WATER USED.....                  | 14.14   |
| U. | SCFD GAS SAMPLED (528*Q*C/(29.9*K))..... | 79.819  |

## V. MOLECULAR WEIGHT OF STACK GAS

| COMPONENT                           | ORSAT-DRY<br>VOL. PCT./100 | X | MOISTURE<br>CORRECTION<br>(1-T/100) | X | MOLECULAR<br>WEIGHT | = | WEIGHT<br>PER MOLE |
|-------------------------------------|----------------------------|---|-------------------------------------|---|---------------------|---|--------------------|
| CO2                                 | .038                       | X | .8586                               | X | 44.0                | = | 1.42               |
| CO                                  | .000                       | X | .8586                               | X | 28.0                | = | .00                |
| O2                                  | .130                       | X | .8586                               | X | 32.0                | = | 3.57               |
| N2                                  | .832                       | X | .8586                               | X | 28.2                | = | 20.16              |
| H2O                                 |                            | X | T/100= .1414                        | X | 18.0                | = | 2.54               |
| MOLECULAR<br>WEIGHT OF<br>STACK GAS |                            |   |                                     |   |                     |   | = 27.69            |

|     |                                               |        |
|-----|-----------------------------------------------|--------|
| W.  | PITOT CORRECTION.....                         | .840   |
| X.  | AVERAGE CORRECTED VELOCITY (FPS).....         | 19.77  |
|     | [85.49*W*SQRT{(J*DELTA P)/(V*F)}]             |        |
| Y.  | AVG. FLOW RATE (CFM) (X*H*60).....            | 84075. |
| Z.  | STACK FLOW RATE (SCFM) (528*Y/J*F/29.92)..... | 43398. |
|     | STACK FLOW RATE (DRY).....                    | 37264. |
| AA. | SAMPLE TIME (SEC).....                        | 7200.  |
| BB. | PERCENT ISOKINETIC.....                       | 93.16  |
|     | (J*100*U*29.92)/(528*X*AA*I*F*(1-T/100))      |        |

# AIR QUALITY ENGINEERING

USX CLAIRTON COKE WORKS  
 CLAIRTON COMBUSTION  
 CLR-CS3-2 8-1-90

| PARAMETER   | CYCLONE<br>WT. (G) | MATL.ON<br>FILTER(G) | INSOL.MATL.<br>IN PROBE(G) | SOL.MATL.<br>IN PROBE(G) |
|-------------|--------------------|----------------------|----------------------------|--------------------------|
| PARTICULATE | .00000             | .04310               | .00000                     | .00710                   |

| PARAMETER   | INSOL.MATL.<br>IN IMP.(G) | SOLUBLE MATL.<br>IN IMP.(G) |
|-------------|---------------------------|-----------------------------|
| PARTICULATE | .00000                    | .00000                      |

|             |        |
|-------------|--------|
| PARTICULATE | .05020 |
|-------------|--------|

|            |        |
|------------|--------|
| ALL MATLS. | .05020 |
|------------|--------|

| PARAMETER   | GR/SCFD | LB/HR   |
|-------------|---------|---------|
| PARTICULATE | .00969  | 3.09353 |

Emission rates are based on EPA Method 5.

AIR QUALITY ENGINEERING

USX CLAIRTON COKE WORKS  
CLAIRTON  
COMBUSTION STACK 3

DATE: .....8-1-90  
CHARGE #: ...150-601050  
TEST #: .....CLR-CS3-3

1. EMISSION RESULTS

| PARAMETER   | GR/SCFD | LB/HR   |
|-------------|---------|---------|
| PARTICULATE | .01433  | 5.08315 |

2. STACK CONDITIONS

|                       |        |
|-----------------------|--------|
| FLOW (ACFM)           | 91948. |
| (SCFM)                | 47781. |
| MOISTURE CONTENT (%)  | 13.36  |
| STACK TEMPERATURE (F) | 538.5  |

3. SAMPLING CONDITIONS

|                    |        |
|--------------------|--------|
| SAMPLE TIME (MIN.) | 120.0  |
| SCFD GAS SAMPLED   | 88.581 |
| PERCENT ISOKINETIC | 93.07  |



# AIR QUALITY ENGINEERING

USX CLAIRTON COKE WORKS  
CLAIRTON COMBUSTION  
CLR-CS3-3 8-1-90

## FIELD DATA AND VELOCITY CALCULATIONS

| POINT | TIME   | METER<br>READING<br>(DRY) CF | DELTA P<br>IN. H2O | ORIFICE<br>DELTA H<br>REQ ACT | METER<br>TEMP<br>DEG F<br>IN OUT | VACUUM<br>IN. HG. | STACK<br>TEMP<br>DEG | CORRECTED<br>VELOCITY<br>FFT/SEC |
|-------|--------|------------------------------|--------------------|-------------------------------|----------------------------------|-------------------|----------------------|----------------------------------|
| 40.6A | 1512.0 | 798.025                      | .075               | 1.85 1.85                     | 112. 105.                        | 6.0               | 549.                 | 21.9                             |
| 28.5  |        |                              | .080               | 1.97 1.97                     | 117. 107.                        | 6.0               | 539.                 | 22.5                             |
| 20.2  |        |                              | .090               | 2.22 2.22                     | 118. 108.                        | 7.5               | 546.                 | 23.9                             |
| 13.5  |        |                              | .085               | 2.10 2.10                     | 118. 107.                        | 6.5               | 554.                 | 23.3                             |
| 7.6   |        |                              | .085               | 2.10 2.10                     | 118. 107.                        | 6.5               | 547.                 | 23.2                             |
| 2.4A  | 1542.0 | 820.115                      | .070               | 1.73 1.73                     | 118. 107.                        | 5.5               | 545.                 | 21.1                             |
| 40.6B | 1544.0 | 820.115                      | .090               | 2.22 2.22                     | 113. 107.                        | 7.5               | 527.                 | 23.7                             |
| 28.5  |        |                              | .085               | 2.10 2.10                     | 117. 107.                        | 6.5               | 521.                 | 22.9                             |
| 13.5  |        |                              | .090               | 2.22 2.22                     | 116. 106.                        | 7.5               | 518.                 | 23.6                             |
| 7.6   |        |                              | .075               | 1.95 1.95                     | 117. 106.                        | 6.0               | 523.                 | 21.6                             |
| 2.4B  | 1614.0 | 844.806                      | .070               | 1.82 1.82                     | 117. 107.                        | 6.0               | 518.                 | 20.8                             |
| 40.6C | 1617.0 | 844.806                      | .080               | 2.10 2.10                     | 110. 105.                        | 6.5               | 540.                 | 22.5                             |
| 28.5  |        |                              | .080               | 2.10 2.10                     | 116. 105.                        | 6.5               | 545.                 | 22.5                             |
| 20.2  |        |                              | .075               | 1.94 1.94                     | 115. 105.                        | 6.0               | 555.                 | 21.9                             |
| 13.5  |        |                              | .070               | 1.81 1.81                     | 115. 106.                        | 5.5               | 561.                 | 21.2                             |
| 7.6   |        |                              | .060               | 1.55 1.55                     | 114. 105.                        | 5.0               | 553.                 | 19.6                             |
| 2.4C  | 1647.0 | 867.247                      | .050               | 1.29 1.29                     | 114. 105.                        | 5.0               | 545.                 | 17.8                             |
| 40.6D | 1650.0 | 867.247                      | .070               | 1.81 1.81                     | 108. 104.                        | 6.0               | 526.                 | 20.9                             |
| 28.5  |        |                              | .080               | 2.08 2.08                     | 114. 104.                        | 6.5               | 528.                 | 22.3                             |
| 20.2  |        |                              | .065               | 1.68 1.68                     | 114. 105.                        | 5.5               | 533.                 | 20.2                             |
| 13.5  |        |                              | .065               | 1.68 1.68                     | 114. 105.                        | 5.5               | 535.                 | 20.2                             |
| 7.6   |        |                              | .065               | 1.68 1.68                     | 113. 104.                        | 5.5               | 537.                 | 20.2                             |
| 2.4D  | 1720.0 | 889.803                      | .060               | 1.55 1.55                     | 113. 103.                        | 5.5               | 540.                 | 19.5                             |

### O R S A T

|     |      |                |       |
|-----|------|----------------|-------|
| CO2 | 4.0  | IMPINGER NO. 1 | 221.6 |
| O2  | 12.0 | 2              | 45.8  |
| CO  | .0   | 3              | 5.0   |
| N   | 84.0 | 4              | .0    |
|     |      | ABSORBED H2O   | 17.3  |

### CONTROL BOX CALIBRATIONS

|         | FACTOR | DATE    |
|---------|--------|---------|
| ORIFICE | 1.573  | 6-12-90 |
| METER   | 1.0519 | 6-12-90 |
| PITOT   | 0.84   | 6-29-90 |

### LEAK CHECK

|            | RATE    | IN. HG |
|------------|---------|--------|
| INITIAL LT | 0.02CFM | 5.0    |
| FINAL LT   | .005CFM | 8.0    |

CONTROL BOX NO. 1

PROBE NO. 7-2

NOZZLE NO. 55

# AIR QUALITY ENGINEERING

USX CLAIRTON COKE WORKS  
CLAIRTON COMBUSTION  
CLR-CS3-3 8-1-90

## STACK SAMPLING CALCULATIONS

|    |                                          |         |
|----|------------------------------------------|---------|
| A. | BAROMETRIC PRESSURE IN. HG.....          | 29.49   |
| B. | AVG. DELTA H (IN H2O).....               | 1.89    |
| C. | METER PRESSURE (IN. HG.).....            | 29.63   |
| D. | STATIC PRESSURE (IN. H2O).....           | -1.20   |
| E. | STATIC PRESSURE (IN. HG.).....           | -.088   |
| F. | STACK PRESSURE (IN. HG.) (A+E).....      | 29.40   |
| G. | STACK DIAMETER (IN.).....                | 114.00  |
| H. | STACK AREA (SQ. FT.).....                | 70.88   |
|    | NOZZLE DIAMETER.....                     | .4990   |
| I. | NOZZLE AREA (SQ. FT.).....               | .001358 |
| J. | AVG. STACK TEMP (DEG. R.).....           | 998.5   |
| K. | AVG. METER TEMP (DEG. R.).....           | 570.2   |
| L. | CONDENSATE VOL. (ML).....                | 272.4   |
| M. | ABSORBED H2O (ML).....                   | 17.3    |
| N. | TOTAL H2O (ML).....                      | 289.7   |
| O. | METERED GAS (CF).....                    | 91.778  |
| P. | GAS METER CORRECTION.....                | 1.0519  |
| Q. | CORRECTED METERED GAS (CF).....          | 96.541  |
| R. | H2O GAS VOLUME (CF) (0.00267N(K/C).....  | 14.887  |
| S. | TOTAL SAMPLED VOLUME (CF) (Q+R).....     | 111.428 |
| T. | PERCENT H2O (100R/S).....                | 13.36   |
|    | THEORETICAL MAXIMUM.....                 | 100.00  |
|    | PERCENT WATER USED.....                  | 13.36   |
| U. | SCFD GAS SAMPLED (528*Q*C/(29.9*K))..... | 88.581  |

## V. MOLECULAR WEIGHT OF STACK GAS

| COMPONENT                           | ORSAT-DRY<br>VOL.PCT./100 | X | MOISTURE<br>CORRECTION<br>(1-T/100) | X | MOLECULAR<br>WEIGHT | = | WEIGHT<br>PER MOLE |
|-------------------------------------|---------------------------|---|-------------------------------------|---|---------------------|---|--------------------|
| CO2                                 | .040                      | X | .8664                               | X | 44.0                | = | 1.52               |
| CO                                  | .000                      | X | .8664                               | X | 28.0                | = | .00                |
| O2                                  | .120                      | X | .8664                               | X | 32.0                | = | 3.33               |
| N2                                  | .840                      | X | .8664                               | X | 28.2                | = | 20.52              |
| H2O                                 |                           | X | T/100= .1336                        | X | 18.0                | = | 2.40               |
| MOLECULAR<br>WEIGHT OF<br>STACK GAS |                           |   |                                     |   |                     |   | = 27.78            |

|     |                                               |        |
|-----|-----------------------------------------------|--------|
| W.  | PITOT CORRECTION.....                         | .840   |
| X.  | AVERAGE CORRECTED VELOCITY (FPS).....         | 21.62  |
|     | [85.49*W*SQRT((J*DELTA P)/(V*F))]             |        |
| Y.  | AVG. FLOW RATE (CFM) (X*H*60).....            | 91948. |
| Z.  | STACK FLOW RATE (SCFM) (528*Y/J*F/29.92)..... | 47781. |
|     | STACK FLOW RATE (DRY).....                    | 41397. |
| AA. | SAMPLE TIME (SEC).....                        | 7200.  |
| BB. | PERCENT ISOKINETIC.....                       | 93.07  |
|     | (J*100*U*29.92)/(528*X*AA*I*F*(1-T/100))      |        |

AIR QUALITY ENGINEERING

USX CLAIRTON COKE WORKS  
 CLAIRTON COMBUSTION  
 CLR-CS3-3 8-1-90

| PARAMETER   | CYCLONE<br>WT. (G) | MATL.ON<br>FILTER(G) | INSOL.MATL.<br>IN PROBE(G) | SOL.MATL.<br>IN PROBE(G) |
|-------------|--------------------|----------------------|----------------------------|--------------------------|
| PARTICULATE | .00000             | .06800               | .00000                     | .01440                   |

| PARAMETER   | INSOL.MATL.<br>IN IMP.(G) | SOLUBLE MATL.<br>IN IMP.(G) |
|-------------|---------------------------|-----------------------------|
| PARTICULATE | .00000                    | .00000                      |

|             |        |
|-------------|--------|
| PARTICULATE | .08240 |
|-------------|--------|

|            |        |
|------------|--------|
| ALL MATLS. | .08240 |
|------------|--------|

| PARAMETER   | GR/SCFD | LB/HR   |
|-------------|---------|---------|
| PARTICULATE | .01433  | 5.08315 |

Emission rates are based on EPA Method 5.

**USS CLAIRTON WORKS  
RESULTS OF THE  
COMPLIANCE DEMONSTRATION OF THE  
#3 BATTERY COMBUSTION STACK**

**APPENDIX E  
FIELD DATA SHEETS  
FOR VISIBLE EMISSIONS**

①

## VISIBLE EMISSIONS OBSERVATIONS FORM

TEST: 1<sup>ST</sup>  
CLA-03-1

3

OBSERVER: K. KUIPERSDATE: 8/1/90START  
1<sup>ST</sup> TEST  
9:45FACILITY: USX CARTEROBSERVATION: START TIME: 9:48END TIME: 10:48

OBSERVATION POINT:

Maple Park LotSOURCE: #3 - STACKDISTANCE: 950'DIRECTION FROM: S/WHEIGHT: 200'

WIND:

SPEED: 7 MPHDIRECTION: NTEMPERATURE: 68SKY CONDITION: HAZYBACKGROUND: SKYREADING CONDITIONS: FAIRCOLOR OF EMISSION: —TOTAL No. OF READINGS: 240No. READINGS  $\geq$  20% 0No. READINGS  $\geq$  60% 0GREATEST OPACITY: 0CREW: C FOREMAN: SHELTON

COMMENTS:

|    |   |   |   |   |
|----|---|---|---|---|
| 0  | 0 | 0 | 0 | 0 |
| 1  | 0 | 0 | 0 | 0 |
| 2  | 0 | 0 | 0 | 0 |
| 3  | 0 | 0 | 0 | 0 |
| 4  | 0 | 0 | 0 | 0 |
| 5  | 0 | 0 | 0 | 0 |
| 6  | 0 | 0 | 0 | 0 |
| 7  | 0 | 0 | 0 | 0 |
| 8  | 0 | 0 | 0 | 0 |
| 9  | 0 | 0 | 0 | 0 |
| 10 | 0 | 0 | 0 | 0 |
| 11 | 0 | 0 | 0 | 0 |
| 12 | 0 | 0 | 0 | 0 |
| 13 | 0 | 0 | 0 | 0 |
| 14 | 0 | 0 | 0 | 0 |
| 15 | 0 | 0 | 0 | 0 |
| 16 | 0 | 0 | 0 | 0 |
| 17 | 0 | 0 | 0 | 0 |
| 18 | 0 | 0 | 0 | 0 |
| 19 | 0 | 0 | 0 | 0 |
| 20 | 0 | 0 | 0 | 0 |
| 21 | 0 | 0 | 0 | 0 |
| 22 | 0 | 0 | 0 | 0 |
| 23 | 0 | 0 | 0 | 0 |
| 24 | 0 | 0 | 0 | 0 |
| 25 | 0 | 0 | 0 | 0 |
| 26 | 0 | 0 | 0 | 0 |
| 27 | 0 | 0 | 0 | 0 |
| 28 | 0 | 0 | 0 | 0 |
| 29 | 0 | 0 | 0 | 0 |

|    |   |   |   |   |
|----|---|---|---|---|
| 30 | 0 | 0 | 0 | 0 |
| 31 | 0 | 0 | 0 | 0 |
| 32 | 0 | 0 | 0 | 0 |
| 33 | 0 | 0 | 0 | 0 |
| 34 | 0 | 0 | 0 | 0 |
| 35 | 0 | 0 | 0 | 0 |
| 36 | 0 | 0 | 0 | 0 |
| 37 | 0 | 0 | 0 | 0 |
| 38 | 0 | 0 | 0 | 0 |
| 39 | 0 | 0 | 0 | 0 |
| 40 | 0 | 0 | 0 | 0 |
| 41 | 0 | 0 | 0 | 0 |
| 42 | 0 | 0 | 0 | 0 |
| 43 | 0 | 0 | 0 | 0 |
| 44 | 0 | 0 | 0 | 0 |
| 45 | 0 | 0 | 0 | 0 |
| 46 | 0 | 0 | 0 | 0 |
| 47 | 0 | 0 | 0 | 0 |
| 48 | 0 | 0 | 0 | 0 |
| 49 | 0 | 0 | 0 | 0 |
| 50 | 0 | 0 | 0 | 0 |
| 51 | 0 | 0 | 0 | 0 |
| 52 | 0 | 0 | 0 | 0 |
| 53 | 0 | 0 | 0 | 0 |
| 54 | 0 | 0 | 0 | 0 |
| 55 | 0 | 0 | 0 | 0 |
| 56 | 0 | 0 | 0 | 0 |
| 57 | 0 | 0 | 0 | 0 |
| 58 | 0 | 0 | 0 | 0 |
| 59 | 0 | 0 | 0 | 0 |

(2)

## VISIBLE EMISSIONS OBSERVATIONS FORM

Test: 1<sup>st</sup>  
CLR-CS3-1OBSERVER: K. KUIROSDATE: 8/1/90FACILITY: USX-DARTONOBSERVATION: START TIME: 10:45 AEND TIME: 11:45 AOBSERVATION POINT:  
Hole Port LtSOURCE: #3-STACKDISTANCE: 950'DIRECTION FROM: S/WHEIGHT: 200'

WIND:

SPEED: 12 MPHDIRECTION: S/WTEMPERATURE: 68SKY CONDITION: PT CloudyBACKGROUND: STYREADING CONDITIONS: Fair

COLOR OF EMISSION: \_\_\_\_\_

TOTAL No. OF READINGS: 240No. READINGS  $\geq$  20% 0No. READINGS  $\geq$  60% 0GREATEST OPACITY: 0CREW: C FOREMAN: Sheltor

COMMENTS: \_\_\_\_\_

3

|     |    |   |   |   |   |
|-----|----|---|---|---|---|
|     | 0  | 0 | 0 | 0 | 0 |
| 10+ | 1  | 0 | 0 | 0 | 0 |
| 20  | 2  | 0 | 0 | 0 | 0 |
| 30  | 3  | 0 | 0 | 0 | 0 |
| 40  | 4  | 0 | 0 | 0 | 0 |
| 50  | 5  | 0 | 0 | 0 | 0 |
| 60  | 6  | 0 | 0 | 0 | 0 |
| 70  | 7  | 0 | 0 | 0 | 0 |
| 80  | 8  | 0 | 0 | 0 | 0 |
| 90  | 9  | 0 | 0 | 0 | 0 |
| 100 | 10 | 0 | 0 | 0 | 0 |
| 110 | 11 | 0 | 0 | 0 | 0 |
| 120 | 12 | 0 | 0 | 0 | 0 |
| 130 | 13 | 0 | 0 | 0 | 0 |
| 140 | 14 | 0 | 0 | 0 | 0 |
| 150 | 15 | 0 | 0 | 0 | 0 |
| 160 | 16 | 0 | 0 | 0 | 0 |
| 170 | 17 | 0 | 0 | 0 | 0 |
| 180 | 18 | 0 | 0 | 0 | 0 |
| 190 | 19 | 0 | 0 | 0 | 0 |
| 200 | 20 | 0 | 0 | 0 | 0 |
| 210 | 21 | 0 | 0 | 0 | 0 |
| 220 | 22 | 0 | 0 | 0 | 0 |
| 230 | 23 | 0 | 0 | 0 | 0 |
| 240 | 24 | 0 | 0 | 0 | 0 |
| 250 | 25 | 0 | 0 | 0 | 0 |
| 260 | 26 | 0 | 0 | 0 | 0 |
| 270 | 27 | 0 | 0 | 0 | 0 |
| 280 | 28 | 0 | 0 | 0 | 0 |
| 290 | 29 | 0 | 0 | 0 | 0 |

|     |    |   |   |   |   |
|-----|----|---|---|---|---|
|     | 30 | 0 | 0 | 0 | 0 |
| 20  | 31 | 0 | 0 | 0 | 0 |
| 30  | 32 | 0 | 0 | 0 | 0 |
| 40  | 33 | 0 | 0 | 0 | 0 |
| 50  | 34 | 0 | 0 | 0 | 0 |
| 60  | 35 | 0 | 0 | 0 | 0 |
| 70  | 36 | 0 | 0 | 0 | 0 |
| 80  | 37 | 0 | 0 | 0 | 0 |
| 90  | 38 | 0 | 0 | 0 | 0 |
| 100 | 39 | 0 | 0 | 0 | 0 |
| 110 | 40 | 0 | 0 | 0 | 0 |
| 120 | 41 | 0 | 0 | 0 | 0 |
| 130 | 42 | 0 | 0 | 0 | 0 |
| 140 | 43 | 0 | 0 | 0 | 0 |
| 150 | 44 | 0 | 0 | 0 | 0 |
| 160 | 45 | 0 | 0 | 0 | 0 |
| 170 | 46 | 0 | 0 | 0 | 0 |
| 180 | 47 | 0 | 0 | 0 | 0 |
| 190 | 48 | 0 | 0 | 0 | 0 |
| 200 | 49 | 0 | 0 | 0 | 0 |
| 210 | 50 | 0 | 0 | 0 | 0 |
| 220 | 51 | 0 | 0 | 0 | 0 |
| 230 | 52 | 0 | 0 | 0 | 0 |
| 240 | 53 | 0 | 0 | 0 | 0 |
| 250 | 54 | 0 | 0 | 0 | 0 |
| 260 | 55 | 0 | 0 | 0 | 0 |
| 270 | 56 | 0 | 0 | 0 | 0 |
| 280 | 57 | 0 | 0 | 0 | 0 |
| 290 | 58 | 0 | 0 | 0 | 0 |
|     | 59 | 0 | 0 | 0 | 0 |

(3)

VISIBLE EMISSIONS OBSERVATIONS FORM

3

TEST. 1<sup>ST</sup> 4<sup>2ND</sup> TEST CLR-CS3-2  
CLR-CS3-1

OBSERVER: K. Kucinas

DATE: 8/1/90

FACILITY: USX-Clinton

OBSERVATION: START TIME: 11<sup>48</sup>A  
END TIME: 12<sup>48</sup>P

OBSERVATION POINT:  
Maule Bank Lot

SOURCE: #3-STACK

DISTANCE: 950'

DIRECTION FROM: S/W

HEIGHT: 800'

WIND:

SPEED: 9 MPH

DIRECTION: N/W

TEMPERATURE: 68

SKY CONDITION: PT. Cloudy

BACKGROUND: SKY

READING CONDITIONS: Fair

COLOR OF EMISSION: \_\_\_\_\_

TOTAL No. OF READINGS: 240

No. READINGS  $\geq$  20% 0

No. READINGS  $\geq$  60% 0

GREATEST OPACITY: 0

CREW: C FOREMAN: SHULTON

COMMENTS: \_\_\_\_\_

|      | 0  | 1 | 2 | 3 | 4 |
|------|----|---|---|---|---|
| 48   | 0  | 0 | 0 | 0 | 0 |
| 11 A | 1  | 0 | 0 | 0 | 0 |
| 50   | 2  | 0 | 0 | 0 | 0 |
| 3    | 3  | 0 | 0 | 0 | 0 |
| 4    | 4  | 0 | 0 | 0 | 0 |
| 5    | 5  | 0 | 0 | 0 | 0 |
| 6    | 6  | 0 | 0 | 0 | 0 |
| 55   | 7  | 0 | 0 | 0 | 0 |
| 8    | 8  | 0 | 0 | 0 | 0 |
| 9    | 9  | 0 | 0 | 0 | 0 |
| 10   | 10 | 0 | 0 | 0 | 0 |
| 11   | 11 | 0 | 0 | 0 | 0 |
| 12   | 12 | 0 | 0 | 0 | 0 |
| 13   | 13 | 0 | 0 | 0 | 0 |
| 14   | 14 | 0 | 0 | 0 | 0 |
| 15   | 15 | 0 | 0 | 0 | 0 |
| 16   | 16 | 0 | 0 | 0 | 0 |
| 5    | 17 | 0 | 0 | 0 | 0 |
| 18   | 18 | 0 | 0 | 0 | 0 |
| 19   | 19 | 0 | 0 | 0 | 0 |
| 20   | 20 | 0 | 0 | 0 | 0 |
| 21   | 21 | 0 | 0 | 0 | 0 |
| 10   | 22 | 0 | 0 | 0 | 0 |
| 23   | 23 | 0 | 0 | 0 | 0 |
| 24   | 24 | 0 | 0 | 0 | 0 |
| 25   | 25 | 0 | 0 | 0 | 0 |
| 26   | 26 | 0 | 0 | 0 | 0 |
| 15   | 27 | 0 | 0 | 0 | 0 |
| 28   | 28 | 0 | 0 | 0 | 0 |
| 29   | 29 | 0 | 0 | 0 | 0 |

|    | 30 | 31 | 32 | 33 | 34 |
|----|----|----|----|----|----|
| 30 | 0  | 0  | 0  | 0  | 0  |
| 31 | 0  | 0  | 0  | 0  | 0  |
| 29 | 32 | 0  | 0  | 0  | 0  |
| 33 | 33 | 0  | 0  | 0  | 0  |
| 34 | 34 | 0  | 0  | 0  | 0  |
| 35 | 35 | 0  | 0  | 0  | 0  |
| 36 | 36 | 0  | 0  | 0  | 0  |
| 25 | 37 | 0  | 0  | 0  | 0  |
| 38 | 38 | 0  | 0  | 0  | 0  |
| 39 | 39 | 0  | 0  | 0  | 0  |
| 40 | 40 | 0  | 0  | 0  | 0  |
| 41 | 41 | 0  | 0  | 0  | 0  |
| 30 | 42 | 0  | 0  | 0  | 0  |
| 43 | 43 | 0  | 0  | 0  | 0  |
| 44 | 44 | 0  | 0  | 0  | 0  |
| 45 | 45 | 0  | 0  | 0  | 0  |
| 46 | 46 | 0  | 0  | 0  | 0  |
| 35 | 47 | 0  | 0  | 0  | 0  |
| 48 | 48 | 0  | 0  | 0  | 0  |
| 49 | 49 | 0  | 0  | 0  | 0  |
| 50 | 50 | 0  | 0  | 0  | 0  |
| 51 | 51 | 0  | 0  | 0  | 0  |
| 40 | 52 | 0  | 0  | 0  | 0  |
| 53 | 53 | 0  | 0  | 0  | 0  |
| 54 | 54 | 0  | 0  | 0  | 0  |
| 55 | 55 | 0  | 0  | 0  | 0  |
| 56 | 56 | 0  | 0  | 0  | 0  |
| 45 | 57 | 0  | 0  | 0  | 0  |
| 58 | 58 | 0  | 0  | 0  | 0  |
| 59 | 59 | 0  | 0  | 0  | 0  |

START  
TEST-2  
CLR-CS3-2

(4)

## VISIBLE EMISSIONS OBSERVATIONS FORM

3 TEST-CLR-CS3-2

OBSERVER: K. Kuiras ARC3-2DATE: 8/1/90FACILITY: USX-DARTONOBSERVATION: START TIME: 12<sup>48</sup> PEND TIME: 1<sup>25</sup> P

OBSERVATION POINT:

Hagler Park LotSOURCE: #3-STACKDISTANCE: 950'DIRECTION FROM: S/WHEIGHT: 200'

WIND:

SPEED: 6 MPHDIRECTION: NTEMPERATURE: 71SKY CONDITION: Clear-A-ClearBACKGROUND: SKYREADING CONDITIONS: GoodCOLOR OF EMISSION: —TOTAL NO. OF READINGS: 240NO. READINGS  $\geq$  20% 0NO. READINGS  $\geq$  60% 0GREATEST OPACITY: 0CREW: C FIREMAN: SHelton

COMMENTS:

ARC3-2  
Cont'd  
2nd  
12-1

|    |   |   |   |   |
|----|---|---|---|---|
| 0  | 0 | 0 | 0 | 0 |
| 1  | 0 | 0 | 0 | 0 |
| 2  | 0 | 0 | 0 | 0 |
| 3  | 0 | 0 | 0 | 0 |
| 4  | 0 | 0 | 0 | 0 |
| 5  | 0 | 0 | 0 | 0 |
| 6  | 0 | 0 | 0 | 0 |
| 7  | 0 | 0 | 0 | 0 |
| 8  | 0 | 0 | 0 | 0 |
| 9  | 0 | 0 | 0 | 0 |
| 10 | 0 | 0 | 0 | 0 |
| 11 | 0 | 0 | 0 | 0 |
| 12 | 0 | 0 | 0 | 0 |
| 13 | 0 | 0 | 0 | 0 |
| 14 | 0 | 0 | 0 | 0 |
| 15 | 0 | 0 | 0 | 0 |
| 16 | 0 | 0 | 0 | 0 |
| 17 | 0 | 0 | 0 | 0 |
| 18 | 0 | 0 | 0 | 0 |
| 19 | 0 | 0 | 0 | 0 |
| 20 | 0 | 0 | 0 | 0 |
| 21 | 0 | 0 | 0 | 0 |
| 22 | 0 | 0 | 0 | 0 |
| 23 | 0 | 0 | 0 | 0 |
| 24 | 0 | 0 | 0 | 0 |
| 25 | 0 | 0 | 0 | 0 |
| 26 | 0 | 0 | 0 | 0 |
| 27 | 0 | 0 | 0 | 0 |
| 28 | 0 | 0 | 0 | 0 |
| 29 | 0 | 0 | 0 | 0 |

50  
55  
1 P

|    |   |   |   |   |
|----|---|---|---|---|
| 30 | 0 | 0 | 0 | 0 |
| 31 | 0 | 0 | 0 | 0 |
| 32 | 0 | 0 | 0 | 0 |
| 33 | 0 | 0 | 0 | 0 |
| 34 | 0 | 0 | 0 | 0 |
| 35 | 0 | 0 | 0 | 0 |
| 36 | 0 | 0 | 0 | 0 |
| 37 | 0 | 0 | 0 | 0 |
| 38 | 0 | 0 | 0 | 0 |
| 39 | 0 | 0 | 0 | 0 |
| 40 | 0 | 0 | 0 | 0 |
| 41 | 0 | 0 | 0 | 0 |
| 42 | 0 | 0 | 0 | 0 |
| 43 | 0 | 0 | 0 | 0 |
| 44 | 0 | 0 | 0 | 0 |
| 45 | 0 | 0 | 0 | 0 |
| 46 | 0 | 0 | 0 | 0 |
| 47 | 0 | 0 | 0 | 0 |
| 48 | 0 | 0 | 0 | 0 |
| 49 | 0 | 0 | 0 | 0 |
| 50 | 0 | 0 | 0 | 0 |
| 51 | 0 | 0 | 0 | 0 |
| 52 | 0 | 0 | 0 | 0 |
| 53 | 0 | 0 | 0 | 0 |
| 54 | 0 | 0 | 0 | 0 |
| 55 | 0 | 0 | 0 | 0 |
| 56 | 0 | 0 | 0 | 0 |
| 57 | 0 | 0 | 0 | 0 |
| 58 | 0 | 0 | 0 | 0 |
| 59 | 0 | 0 | 0 | 0 |

20  
25  
30  
35  
40  
45



VISIBLE EMISSIONS OBSERVATIONS FORM

TEST-CLR-CS-3-2

OBSERVER: K. KUIROS

DATE: 8/1/90

FACILITY: 45X-CLINATION

OBSERVATION START TIME: 1:48 P

END TIME: 2:48 P

OBSERVATION POINT: Naple Park Lot

SOURCE: #3-STACH

DISTANCE: 950'

DIRECTION FROM: S/W

HEIGHT: 200'

WIND:

SPEED: 6 MPH

DIRECTION: N

TEMPERATURE: 74

SKY CONDITION: PT. Cloudy/Clean

BACKGROUND: SKY

READING CONDITIONS: Good

COLOR OF EMISSION: —

TOTAL No. OF READINGS: 240

No. READINGS >= 20% 0

No. READINGS >= 60% 0

GREATEST OPACITY: 0

CREW: C. FOREMAN: SHELTON

COMMENTS: —

45X-CLINATION  
Test

|    |   |   |   |   |
|----|---|---|---|---|
| 0  | 0 | 0 | 0 | 0 |
| 1  | 0 | 0 | 0 | 0 |
| 2  | 0 | 0 | 0 | 0 |
| 3  | 0 | 0 | 0 | 0 |
| 4  | 0 | 0 | 0 | 0 |
| 5  | 0 | 0 | 0 | 0 |
| 6  | 0 | 0 | 0 | 0 |
| 7  | 0 | 0 | 0 | 0 |
| 8  | 0 | 0 | 0 | 0 |
| 9  | 0 | 0 | 0 | 0 |
| 10 | 0 | 0 | 0 | 0 |
| 11 | 0 | 0 | 0 | 0 |
| 12 | 0 | 0 | 0 | 0 |
| 13 | 0 | 0 | 0 | 0 |
| 14 | 0 | 0 | 0 | 0 |
| 15 | 0 | 0 | 0 | 0 |
| 16 | 0 | 0 | 0 | 0 |
| 17 | 0 | 0 | 0 | 0 |
| 18 | 0 | 0 | 0 | 0 |
| 19 | 0 | 0 | 0 | 0 |
| 20 | 0 | 0 | 0 | 0 |
| 21 | 0 | 0 | 0 | 0 |
| 22 | 0 | 0 | 0 | 0 |
| 23 | 0 | 0 | 0 | 0 |
| 24 | 0 | 0 | 0 | 0 |
| 25 | 0 | 0 | 0 | 0 |
| 26 | 0 | 0 | 0 | 0 |
| 27 | 0 | 0 | 0 | 0 |
| 28 | 0 | 0 | 0 | 0 |
| 29 | 0 | 0 | 0 | 0 |

|    |   |   |   |   |
|----|---|---|---|---|
| 30 | 0 | 0 | 0 | 0 |
| 31 | 0 | 0 | 0 | 0 |
| 32 | 0 | 0 | 0 | 0 |
| 33 | 0 | 0 | 0 | 0 |
| 34 | 0 | 0 | 0 | 0 |
| 35 | 0 | 0 | 0 | 0 |
| 36 | 0 | 0 | 0 | 0 |
| 37 | 0 | 0 | 0 | 0 |
| 38 | 0 | 0 | 0 | 0 |
| 39 | 0 | 0 | 0 | 0 |
| 40 | 0 | 0 | 0 | 0 |
| 41 | 0 | 0 | 0 | 0 |
| 42 | 0 | 0 | 0 | 0 |
| 43 | 0 | 0 | 0 | 0 |
| 44 | 0 | 0 | 0 | 0 |
| 45 | 0 | 0 | 0 | 0 |
| 46 | 0 | 0 | 0 | 0 |
| 47 | 0 | 0 | 0 | 0 |
| 48 | 0 | 0 | 0 | 0 |
| 49 | 0 | 0 | 0 | 0 |
| 50 | 0 | 0 | 0 | 0 |
| 51 | 0 | 0 | 0 | 0 |
| 52 | 0 | 0 | 0 | 0 |
| 53 | 0 | 0 | 0 | 0 |
| 54 | 0 | 0 | 0 | 0 |
| 55 | 0 | 0 | 0 | 0 |
| 56 | 0 | 0 | 0 | 0 |
| 57 | 0 | 0 | 0 | 0 |
| 58 | 0 | 0 | 0 | 0 |
| 59 | 0 | 0 | 0 | 0 |

END TEST #2

(1)

VISIBLE EMISSIONS OBSERVATIONS FORM

3

Test-CLR-CS-3-3

OBSERVER: Mc Koy

DATE: 8/1/90

FACILITY: USX-CLARKTON

OBSERVATION: START TIME: 2:48 P

END TIME: 3:48 P

OBSERVATION POINT:

Maple Ave parking lot  
#3

SOURCE: Battery art Stack

DISTANCE: 950'

DIRECTION FROM: S/W

HEIGHT: 200'

WIND:

SPEED: 7-m MPH

DIRECTION: → East

TEMPERATURE: 75°-77

SKY CONDITION: P. Cloudy

BACKGROUND: SKY

READING CONDITIONS: Good

COLOR OF EMISSION: Black

TOTAL No. OF READINGS: 240

No. READINGS ≥ 20% 0

No. READINGS ≥ 40% 0

GREATEST OPACITY: 10%

CREW: C FOREMAN: R. Shultz

COMMENTS: \_\_\_\_\_

|         |    |   |   |   |   |
|---------|----|---|---|---|---|
|         |    |   |   |   |   |
| 248     | 0  | 0 | 0 | 0 | 0 |
| 2 P     | 1  | 0 | 0 | 0 | 0 |
| 50      | 2  | 0 | 0 | 0 | 0 |
|         | 3  | 0 | 0 | 0 | 0 |
|         | 4  | 0 | 0 | 0 | 0 |
|         | 5  | 0 | 0 | 0 | 0 |
|         | 6  | 0 | 0 | 0 | 0 |
| 55      | 7  | 0 | 0 | 0 | 0 |
|         | 8  | 0 | 0 | 0 | 0 |
|         | 9  | 0 | 0 | 0 | 0 |
|         | 10 | 0 | 0 | 0 | 0 |
|         | 11 | 0 | 0 | 0 | 0 |
| 300     | 12 | 0 | 0 | 0 | 0 |
| 3 P     | 13 | 0 | 0 | 0 | 0 |
|         | 14 | 0 | 0 | 0 | 0 |
|         | 15 | 0 | 0 | 0 | 0 |
|         | 16 | 0 | 0 | 0 | 0 |
| 5       | 17 | 0 | 0 | 0 | 0 |
|         | 18 | 0 | 0 | 0 | 0 |
|         | 19 | 0 | 0 | 0 | 0 |
|         | 20 | 0 | 0 | 0 | 0 |
|         | 21 | 0 | 0 | 0 | 0 |
| 10      | 22 | 0 | 0 | 0 | 0 |
|         | 23 | 0 | 0 | 0 | 0 |
| 312     | 24 | 0 | 0 | 0 | 0 |
| start   | 25 | 0 | 0 | 0 | 0 |
| test #3 | 26 | 0 | 0 | 0 | 0 |
|         | 27 | 0 | 0 | 0 | 0 |
| 15      | 28 | 0 | 0 | 0 | 0 |
|         | 29 | 0 | 0 | 0 | 0 |

|    |    |   |    |   |   |
|----|----|---|----|---|---|
|    |    |   |    |   |   |
| 30 | 0  | 0 | 0  | 0 | 0 |
| 31 | 0  | 0 | 0  | 0 | 0 |
| 20 | 32 | 0 | 0  | 0 | 0 |
|    | 33 | 0 | 0  | 0 | 0 |
|    | 34 | 0 | 0  | 0 | 0 |
|    | 35 | 0 | 0  | 0 | 0 |
|    | 36 | 0 | 0  | 0 | 0 |
| 25 | 37 | 0 | 0  | 0 | 0 |
|    | 38 | 0 | 0  | 0 | 0 |
|    | 39 | 0 | 0  | 0 | 0 |
|    | 40 | 0 | 0  | 0 | 0 |
|    | 41 | 0 | 0  | 0 | 0 |
| 30 | 42 | 0 | 0  | 0 | 0 |
|    | 43 | 0 | 0  | 0 | 0 |
|    | 44 | 0 | 0  | 0 | 0 |
|    | 45 | 0 | 0  | 0 | 0 |
|    | 46 | 0 | 0  | 0 | 0 |
| 35 | 47 | 0 | 0  | 0 | 5 |
|    | 48 | 5 | 10 | 5 | 5 |
|    | 49 | 5 | 5  | 0 | 0 |
|    | 50 | 0 | 0  | 0 | 0 |
|    | 51 | 0 | 0  | 0 | 0 |
| 40 | 52 | 0 | 0  | 0 | 0 |
|    | 53 | 0 | 0  | 0 | 0 |
|    | 54 | 0 | 0  | 0 | 0 |
|    | 55 | 0 | 0  | 0 | 0 |
|    | 56 | 0 | 0  | 0 | 0 |
| 45 | 57 | 0 | 0  | 0 | 0 |
|    | 58 | 0 | 0  | 0 | 0 |
|    | 59 | 0 | 0  | 0 | 0 |

(7)

## VISIBLE EMISSIONS OBSERVATIONS FORM

OBSERVER: McKoyDATE: 1 August 1990FACILITY: USC Clinton worksOBSERVATION: START TIME: 3:48 PM  
END TIME: 4:48 PM

OBSERVATION POINT:

Maple Ave Parking lot  
#3SOURCE: Battery drift stacksDISTANCE: 0.950'DIRECTION FROM: SW of "HEIGHT: 0.200'

WIND:

SPEED: 7- mphDIRECTION: > ETEMPERATURE: 75-77°SKY CONDITION: P. CloudyBACKGROUND: SKYREADING CONDITIONS: GoodCOLOR OF EMISSION: N/ATOTAL No. OF READINGS: 240No. READINGS  $\geq$  20% 0No. READINGS  $\geq$  60% 0GREATEST OPACITY: 0CREW: D FOREMAN: Kasper

COMMENTS: \_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

#3 Stack

|    |   |   |   |   |
|----|---|---|---|---|
| 0  | 0 | 0 | 0 | 0 |
| 1  | 0 | 0 | 0 | 0 |
| 2  | 0 | 0 | 0 | 0 |
| 3  | 0 | 0 | 0 | 0 |
| 4  | 0 | 0 | 0 | 0 |
| 5  | 0 | 0 | 0 | 0 |
| 6  | 0 | 0 | 0 | 0 |
| 7  | 0 | 0 | 0 | 0 |
| 8  | 0 | 0 | 0 | 0 |
| 9  | 0 | 0 | 0 | 0 |
| 10 | 0 | 0 | 0 | 0 |
| 11 | 0 | 0 | 0 | 0 |
| 12 | 0 | 0 | 0 | 0 |
| 13 | 0 | 0 | 0 | 0 |
| 14 | 0 | 0 | 0 | 0 |
| 15 | 0 | 0 | 0 | 0 |
| 16 | 0 | 0 | 0 | 0 |
| 17 | 0 | 0 | 0 | 0 |
| 18 | 0 | 0 | 0 | 0 |
| 19 | 0 | 0 | 0 | 0 |
| 20 | 0 | 0 | 0 | 0 |
| 21 | 0 | 0 | 0 | 0 |
| 22 | 0 | 0 | 0 | 0 |
| 23 | 0 | 0 | 0 | 0 |
| 24 | 0 | 0 | 0 | 0 |
| 25 | 0 | 0 | 0 | 0 |
| 26 | 0 | 0 | 0 | 0 |
| 27 | 0 | 0 | 0 | 0 |
| 28 | 0 | 0 | 0 | 0 |
| 29 | 0 | 0 | 0 | 0 |

Test- CLR-CS-3-3

|    |   |   |   |   |
|----|---|---|---|---|
| 30 | 0 | 0 | 0 | 0 |
| 31 | 0 | 0 | 0 | 0 |
| 32 | 0 | 0 | 0 | 0 |
| 33 | 0 | 0 | 0 | 0 |
| 34 | 0 | 0 | 0 | 0 |
| 35 | 0 | 0 | 0 | 0 |
| 36 | 0 | 0 | 0 | 0 |
| 37 | 0 | 0 | 0 | 0 |
| 38 | 0 | 0 | 0 | 0 |
| 39 | 0 | 0 | 0 | 0 |
| 40 | 0 | 0 | 0 | 0 |
| 41 | 0 | 0 | 0 | 0 |
| 42 | 0 | 0 | 0 | 0 |
| 43 | 0 | 0 | 0 | 0 |
| 44 | 0 | 0 | 0 | 0 |
| 45 | 0 | 0 | 0 | 0 |
| 46 | 0 | 0 | 0 | 0 |
| 47 | 0 | 0 | 0 | 0 |
| 48 | 0 | 0 | 0 | 0 |
| 49 | 0 | 0 | 0 | 0 |
| 50 | 0 | 0 | 0 | 0 |
| 51 | 0 | 0 | 0 | 0 |
| 52 | 0 | 0 | 0 | 0 |
| 53 | 0 | 0 | 0 | 0 |
| 54 | 0 | 0 | 0 | 0 |
| 55 | 0 | 0 | 0 | 0 |
| 56 | 0 | 0 | 0 | 0 |
| 57 | 0 | 0 | 0 | 0 |
| 58 | 0 | 0 | 0 | 0 |
| 59 | 0 | 0 | 0 | 0 |

8

VISIBLE EMISSIONS OBSERVATIONS FORM

OBSERVER: McKoy

DATE: 1 August, 1990 4:48

FACILITY: USC Clinton

OBSERVATION: START TIME: 4:48 PM  
END TIME: 5:20 PM

OBSERVATION POINT:  
Central Ensign Trailer Area

SOURCE: #3 Battery Draft Stack

DISTANCE: ~400'

DIRECTION FROM: NW "OR"

HEIGHT: ~200'

WIND:

SPEED: 12 MPH

DIRECTION: → N

TEMPERATURE: 76°

SKY CONDITION: P. Cloudy

BACKGROUND: SKY

READING CONDITIONS: Good

COLOR OF EMISSION: N/A

TOTAL No. OF READINGS: 132

No. READINGS ≥ 20% 0

No. READINGS ≥ 60% 0

GREATEST OPACITY: 0

CREW: 20 FOREMAN: Karpaul

COMMENTS: \_\_\_\_\_

#3 Stack

|    |   |   |   |   |
|----|---|---|---|---|
| 0  | 0 | 0 | 0 | 0 |
| 1  | 0 | 0 | 0 | 0 |
| 2  | 0 | 0 | 0 | 0 |
| 3  | 0 | 0 | 0 | 0 |
| 4  | 0 | 0 | 0 | 0 |
| 5  | 0 | 0 | 0 | 0 |
| 6  | 0 | 0 | 0 | 0 |
| 7  | 0 | 0 | 0 | 0 |
| 8  | 0 | 0 | 0 | 0 |
| 9  | 0 | 0 | 0 | 0 |
| 10 | 0 | 0 | 0 | 0 |
| 11 | 0 | 0 | 0 | 0 |
| 12 | 0 | 0 | 0 | 0 |
| 13 | 0 | 0 | 0 | 0 |
| 14 | 0 | 0 | 0 | 0 |
| 15 | 0 | 0 | 0 | 0 |
| 16 | 0 | 0 | 0 | 0 |
| 17 | 0 | 0 | 0 | 0 |
| 18 | 0 | 0 | 0 | 0 |
| 19 | 0 | 0 | 0 | 0 |
| 20 | 0 | 0 | 0 | 0 |
| 21 | 0 | 0 | 0 | 0 |
| 22 | 0 | 0 | 0 | 0 |
| 23 | 0 | 0 | 0 | 0 |
| 24 | 0 | 0 | 0 | 0 |
| 25 | 0 | 0 | 0 | 0 |
| 26 | 0 | 0 | 0 | 0 |
| 27 | 0 | 0 | 0 | 0 |
| 28 | 0 | 0 | 0 | 0 |
| 29 | 0 | 0 | 0 | 0 |

Test - CIR-CS-3-3

|    |   |   |   |   |
|----|---|---|---|---|
| 30 | 0 | 0 | 0 | 0 |
| 31 | 0 | 0 | 0 | 0 |
| 32 | 0 | 0 | 0 | 0 |
| 33 |   |   |   |   |
| 34 |   |   |   |   |
| 35 |   |   |   |   |
| 36 |   |   |   |   |
| 37 |   |   |   |   |
| 38 |   |   |   |   |
| 39 |   |   |   |   |
| 40 |   |   |   |   |
| 41 |   |   |   |   |
| 42 |   |   |   |   |
| 43 |   |   |   |   |
| 44 |   |   |   |   |
| 45 |   |   |   |   |
| 46 |   |   |   |   |
| 47 |   |   |   |   |
| 48 |   |   |   |   |
| 49 |   |   |   |   |
| 50 |   |   |   |   |
| 51 |   |   |   |   |
| 52 |   |   |   |   |
| 53 |   |   |   |   |
| 54 |   |   |   |   |
| 55 |   |   |   |   |
| 56 |   |   |   |   |
| 57 |   |   |   |   |
| 58 |   |   |   |   |
| 59 |   |   |   |   |

#3 Test ended