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PARTICULATE MATTER EMISSION TESTS FOR NO. 1 COKE BATTERY COMBUSTION STACK AT REPUBLIC STEEL, CLEVELAND, OHIO

Ralph Pape and Jim Steiner

Acurex Corporation
Energy & Environmental Division
485 Clyde Avenue
Mountain View, California 94042

May 1980

ACUREX FINAL REPORT 80-60/EE

Prepared for
EPA Project Officer — John R. Busik
EPA Task Officer — Larry Kertcher

Enforcement Division
U.S. Environmental Protection Agency
230 South Dearborn Street
Chicago, Illinois 60606

Contract 68-01-4142
Task 19

510323

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SUMMARY

Particulate mass tests were performed on the no. 1 coke battery combustion stack of Republic Steel located in Cleveland, Ohio.

Test results show that particulate mass emission rates (2.4 to 3.5 lbs/hr) were lower when there were many ovens (5-7) being pushed and charged. Test results obtained while only a few ovens (0-2) were being pushed and charged were higher (4.7 to 7.5 lbs/hr). The same trend was noted for condensible organic emission rates. Condensible inorganic and condensible sulfate emission rates were grouped closely for tests performed with a few ovens being pushed and charged. However, those emission rates varied widely for those tests performed while many ovens were being charged and pushed.

SECTION 1

INTRODUCTION

At the request of the Enforcement Division of EPA Region V, the Energy & Environmental Division of Acurex Corporation undertook a test program at the no. 1 coke oven combustion stack of Republic Steel located in Cleveland, Ohio to determine particulate mass emission rates.

Particulate mass measurements were made on July 16 and 17, 1979 using an EPA Method 5 sampler. Simultaneous to the mass tests, opacity readings were made by a certified opacity reader. In addition, the impinger catch was evaluated for condensible inorganics, organics, and sulfates.

Section 2 of this report provides a summary of the coke plant operation; Sections 3 and 4 describe the sampling and analysis procedures used during the tests, while Section 5 presents the results of the tests. Appendices A, B and C describe the sampling equipment used to collect the samples, the pretest preparation and the equipment calibration procedures. Appendix D of this report presents the raw data collected during the test program.

SECTION 2

PROCESS DESCRIPTION

This section of the report summarizes the operating characteristics of the no. 1 coke battery at the Republic Steel plant in Cleveland, Ohio.

Republic Steel operates a 51 oven coke battery at its Cleveland works in Ohio. This battery has been in operation since January 20, 1977. The gas collecting system is made up of two offtakes, one located at each end of the oven. The volatile products liberated during the coking process pass through the battery's dual collecting main, the coke byproducts plant and are used to heat the ovens in the battery. The products of combustion then leave the battery via the waste gas stack. There are no pollution control devices serving the stack. Naturally induced stack draft is used to keep the pressure in the collecting main at -23 mm of H_2O on the push side and -22 mm of H_2O on the coke side. The stack draft draws air required for combustion through an air box at the bottom of the regenerator chambers.

The coal (approximately 0.9 to 1.2 percent sulfur) used for the coking operation is charged through three openings in the top of the oven. Each oven is charged with approximately 15 tons of coal. A leveling bar on the pusher is used to level the piles before the coking operation begins. The coke ovens are fired with coke oven gas (not desulfurized) (Table 2-1) with the firing taking place from either the

Table 2-1. Average Fuel Gas Flow to Battery

Date	Time	Push Side (cfm)	Coke Side (cfm)
7/16/79	0800	240,000	245,000
	1100	235,000	235,000
	1230	235,000	240,000
	1300	240,000	235,000
	1400	240,000	245,000
7/17/79	0800	235,000	240,000
	1300	235,000	245,000
	1500	235,000	245,000

coke side or the push side. More gas is fired on the coke side of the oven since it is approximately 3 inches wider and hence, contains more coke to heat up than the pusher side of the oven. Firing of the coke ovens is reversed every 30 minutes to keep the ovens operating within the safe temperature range of the silica refractories. The coking operation is complete when the skin temperature of the coke is at 1900°F to 2000°F. This usually takes from 17 to 18 hours.

Once the charge has been fully coked the oven is ready to be pushed. The coke guide and the quench car are moved into place and the doors of the oven are removed. The pusher then pushes the coke out of the oven, through the coke guide and into the quenching car for transportation to the quench tower where the coke is cooled for use.

Particulate mass tests were conducted on the waste gas stack. Each test was 96 minutes long and traversed 48 points in the stack. During each of the 4 tests, firing of the coke ovens was reversed and several

ovens were pushed and charged (see Table 2-2). The H_2S concentration in the coke oven gas was 353 grains/100 ft³ and 381 grains/100 ft³ on July 16, 1979 and July 17, 1979. The organic sulfur content was 20 grains/100 ft³.

Table 2-2. Plant Operating Data

Test No.	Date	Time	Oven No.	Time Pushed	Time Charged
60	7/16/79	0824-1109	194	0823	0837
			204	0845	0859
			214	0912	0926
			224	0934	0948
			176	0945	1003
			196	1000	1018
			206	1045	1130
61	7/16/79	1211-1412	*	*	*
62	7/17/79	0748-0958	178	0725	0818
			198	0752	0845
			208	0812	0915
			218	0835	0930
			171	0905	0943
63	7/17/79	1053-1243	221	1050	1215
			173	1225	1240

*No oven charged or pushed

SECTION 3

SAMPLING PROCEDURES

This section of the report describes the procedures used by Acurex personnel to conduct the particulate mass and volumetric flowrate determinations.

3.1 PRELIMINARY MEASUREMENTS

Before conducting particulate mass or volumetric gas flowrate determinations, preliminary measurements were made to determine:

- Sampling site location and number of sampling points to be used
- The velocity, temperature, pressure, composition and moisture content of the gases to be sampled.

This information was used to select the proper nozzle site for isokinetic sampling. EPA Methods 1 through 4 were used to conduct the preliminary measurements.

3.2 SAMPLING SITE AND SAMPLING POINT LOCATIONS

The sampling ports in the no. 1 coke battery combustion stack were located approximately 6 diameters downstream of an elbow and approximately 11 diameters upstream of the stack exit (Figure 3-1). The maximum number of sampling points (according to EPA Method 1) was chosen to give the most representative sample. Figure 3-2 gives the sampling point locations. Sample points 1 through 5 were relocated to point 6 because the sample ports extended 13 inches into the stack from the inside wall.

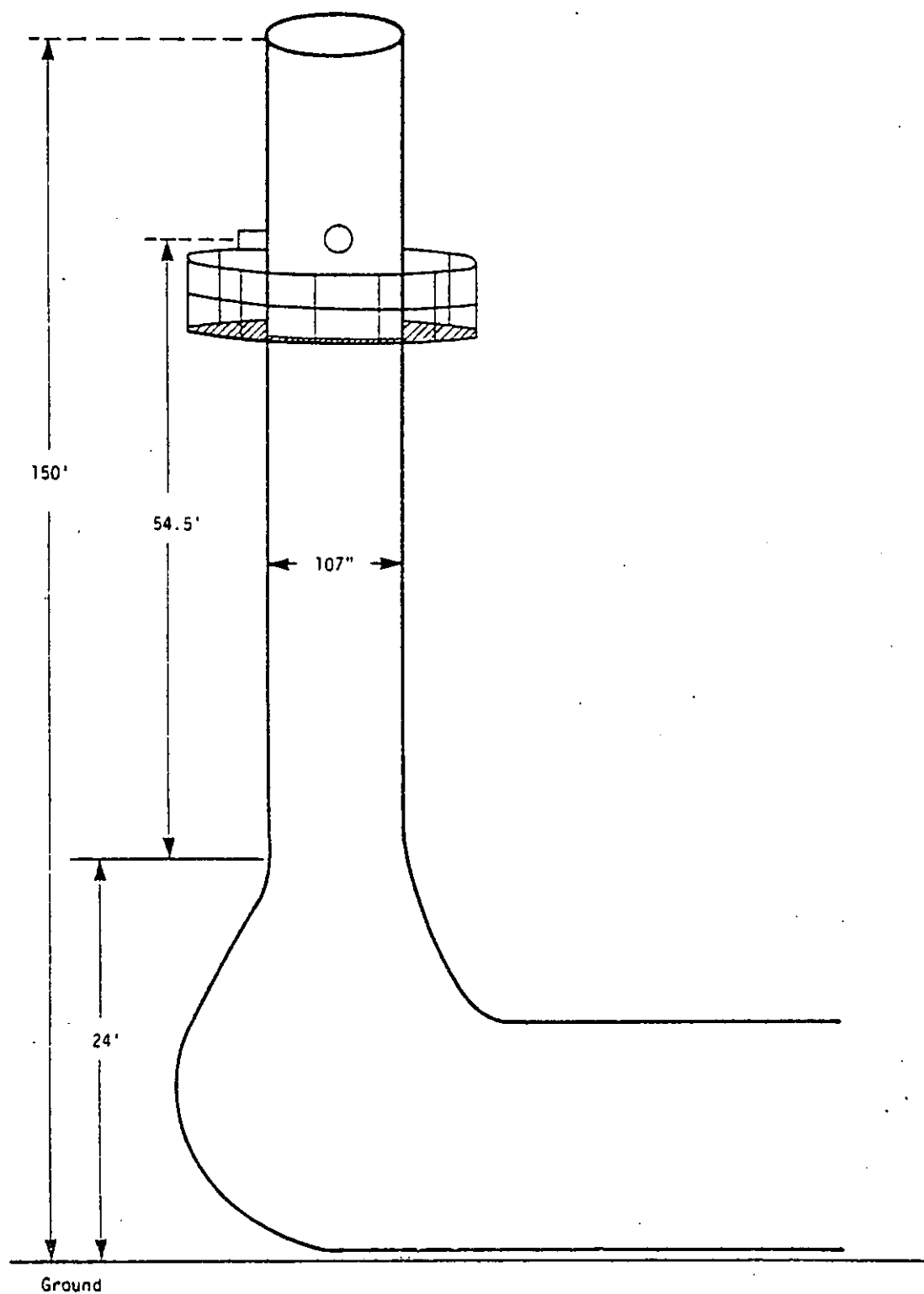
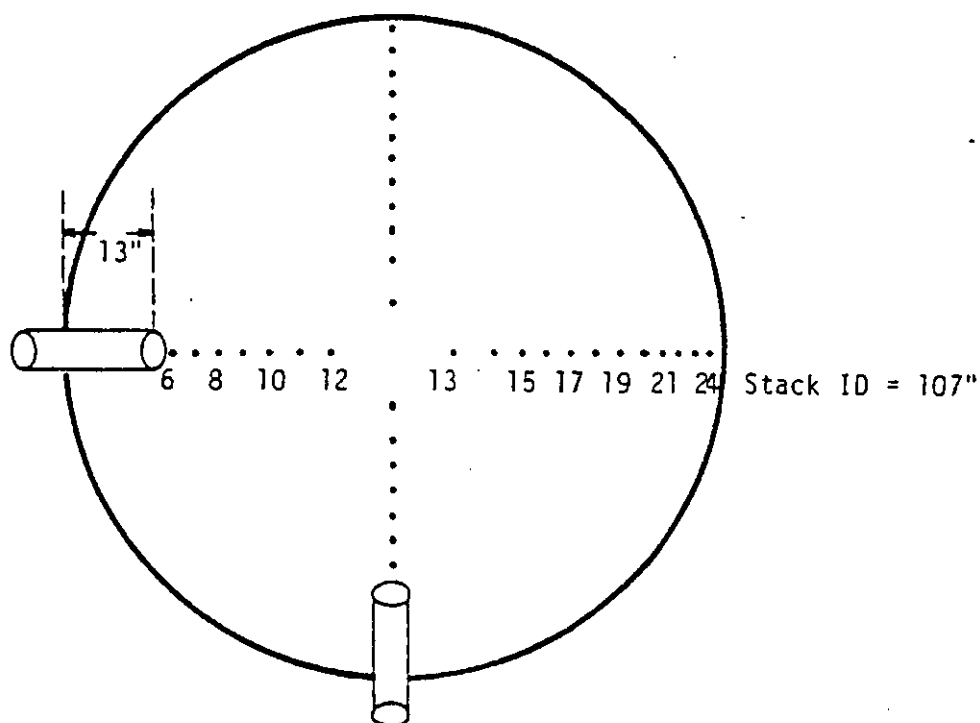


Figure 3-1. No. 1 Coke Oven combustion stack sampling site.



Sample Point	Location from Inside Wall	Sample Point	Location from Inside Wall
1	1.2" - 14.1"	13	64.4"
2	3.4" - 14.1"	14	72.4"
3	5.9" - 14.1"	15	77.9"
4	8.5" - 14.1"	16	82.4"
5	11.2" - 14.1"	17	86.2"
6	14.1"	18	89.8"
7	17.2"	19	92.9"
8	20.8"	20	95.8"
9	24.6"	21	98.5"
10	29.1"	22	101.1"
11	34.6"	23	103.6"
12	42.6"	24	105.8"

Figure 3-2. Sampling point locations.

The sample ports were situated at 90° angles to each other and the stack was traversed in both directions for each test.

3.3 PREPARATION AND SAMPLING PROCEDURES FOR PARTICULATE MASS TESTS

Prior to conducting a particulate mass measurement, the sampling train was thoroughly cleaned in the Mobile Emission Monitoring van situated outside the BOF shop and set up using the procedures outlined in Figure 3-3.

The prepared sampling train components were then transported to the sampling site, assembled and leak checked according to EPA Method 5 procedures. Figure 3-4 outlines the procedures used by the test crew to conduct particulate mass tests on the no. 1 coke oven combustion stack.

Upon receiving direction from the process observer, the particulate mass tests were started. At the same time opacity observations were being made from a location near the Republic Steel offices, approximately 750 feet northeast of the combustion stack. Opacity readings were taken every 15 seconds during the testing period.

During the test periods, the process observer monitored the following process data:

- Average fuel gas flow during test period
- Stack draft
- Time and number of ovens charged
- Time and number of ovens pushed
- Average quantity of coal charged per oven

3.4 SAMPLE RECOVERY PROCEDURES

After the completion of a particulate mass test, the sampling train was disassembled at the sampling site and those components from which a sample was to be recovered were sealed and transported to the mobile van

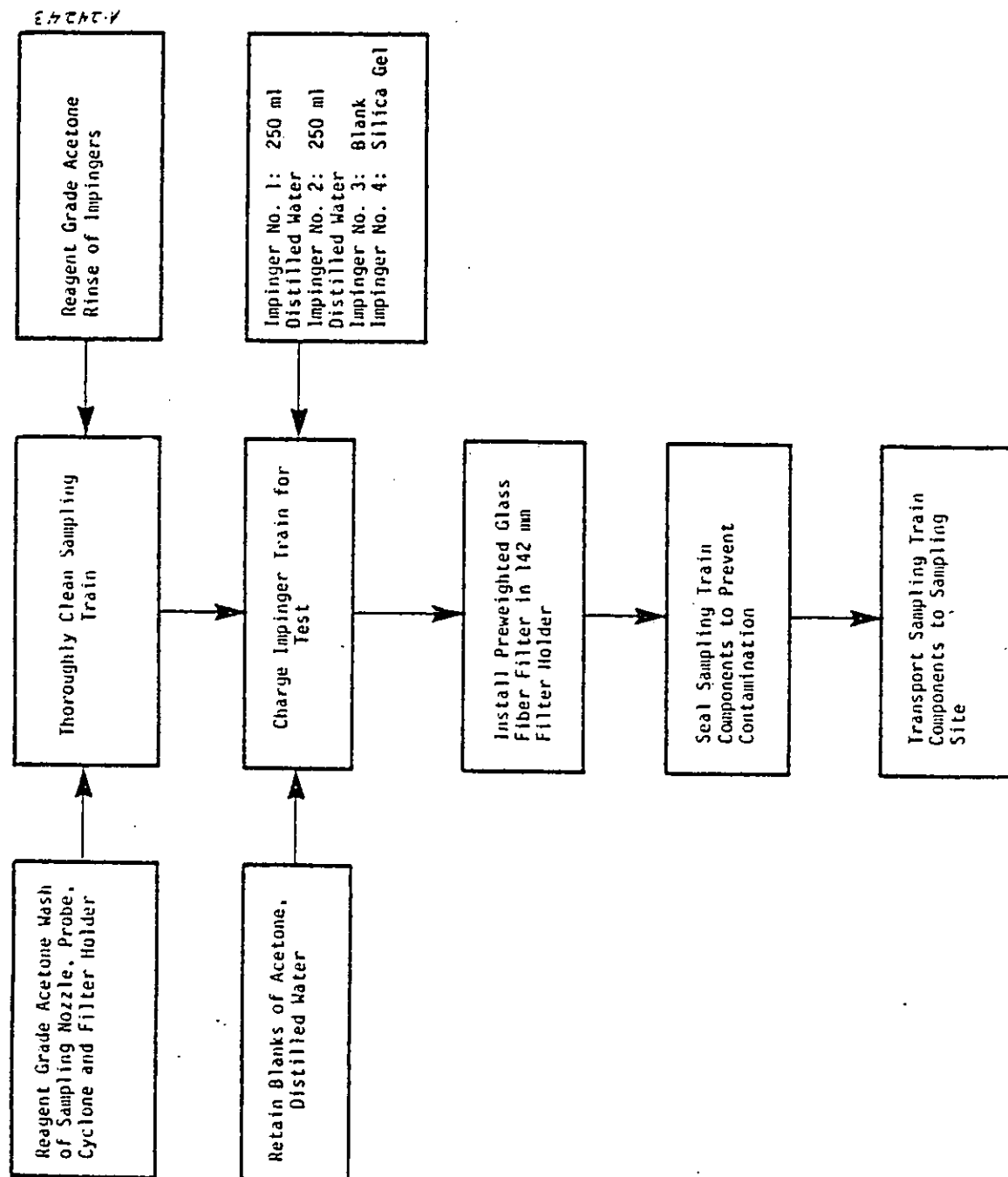


Figure 3-3. Preparation procedures for a particulate mass sampling train.

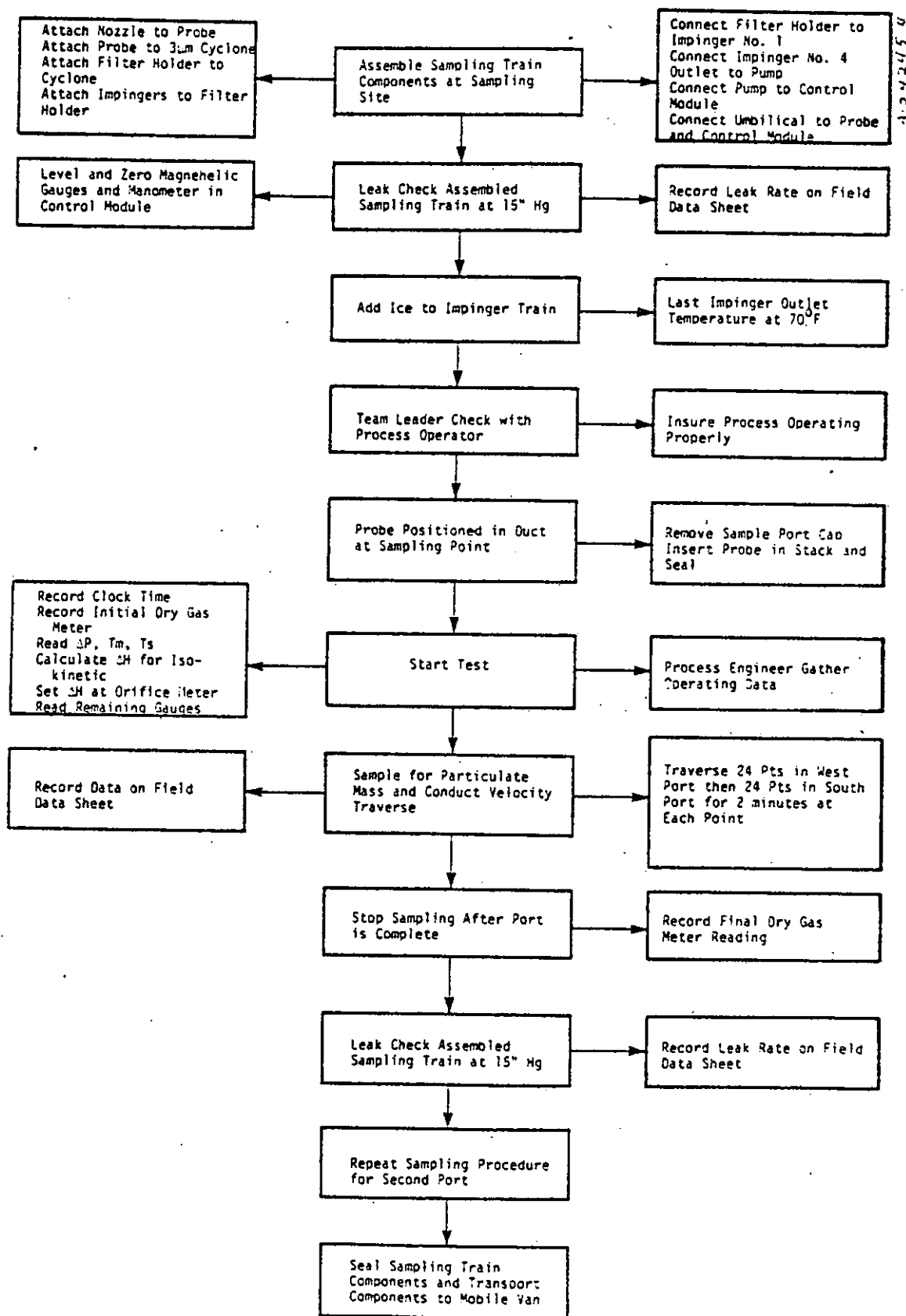


Figure 3-4. Sampling procedures for particulate mass tests performed on the No. 1 coke oven combination stack.

for recovery and analysis. Figure 3-5 illustrates the sample recovery procedures employed for the particulate mass sampling train. The collected samples were sealed in labeled plastic (solids) and amber glass (liquids) containers.

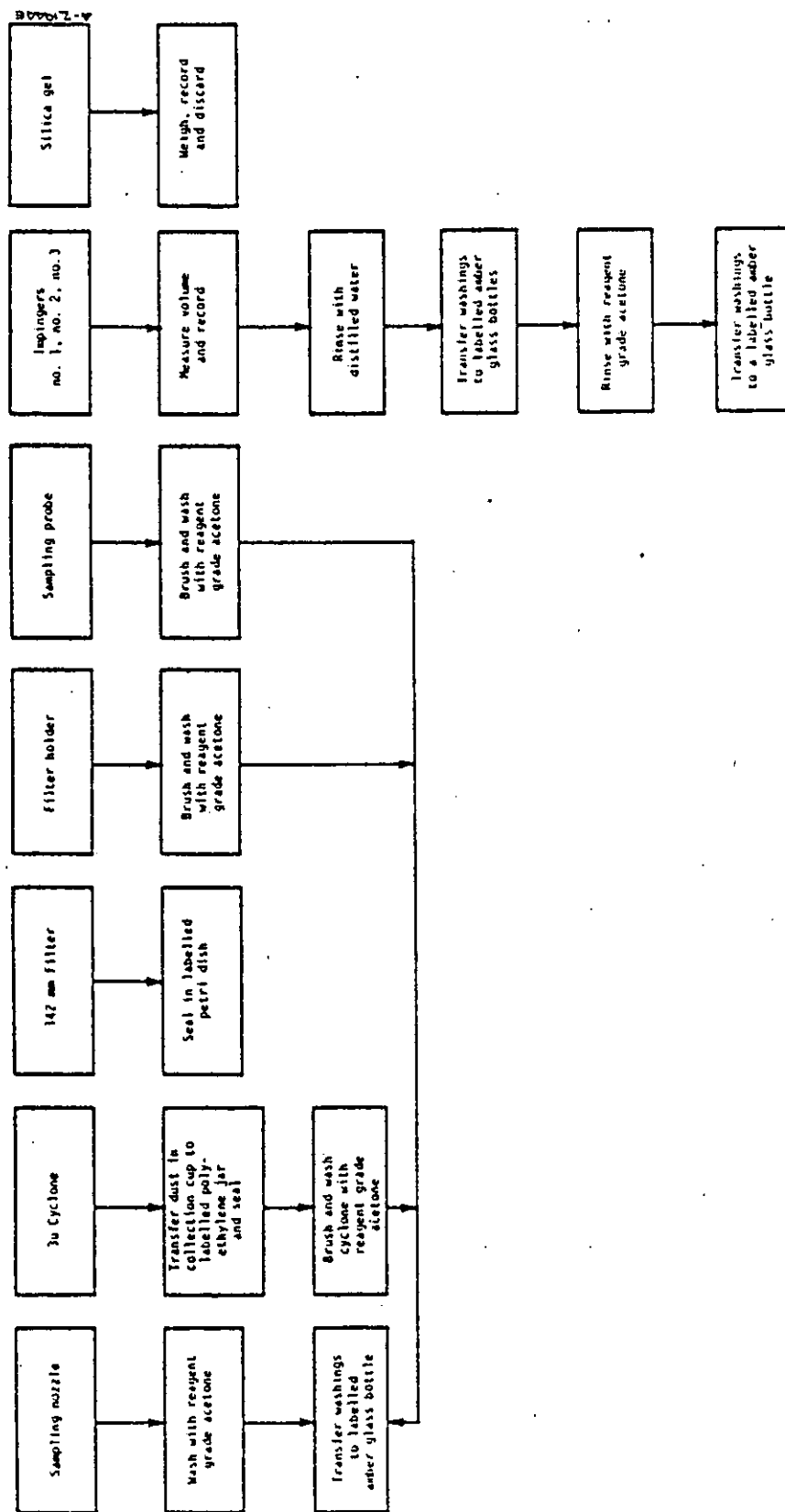


Figure 3-5. Sample recovery procedures for particulate sampling train.

SECTION 4

SAMPLE ANALYSIS PROCEDURES

This section of the report describes the procedures used to analyze the samples collected from the Republic Steel coke battery in Cleveland, Ohio. Analysis was performed on site in the Acurex mobile lab facilities which was stationed outside the BOF shop. Figure 4-1 illustrates the mobile lab.

4.1 ANALYSIS OF THE PARTICULATE SAMPLES

Figure 4-2 is a flowchart illustrating the step by step procedures used to analyze the entire catch of the particulate mass sampling train. The procedure used to evaluate the back half catch of the mass train was obtained from EPA Region V. Deviation from this procedure included performing analysis immediately on site in the mobile lab and addition of cyclone dust catches to cyclone acetone washes to minimize the number of particulate mass samples to be analyzed. Due to rapid changes in particulate mass filter weights caused by the presence of H_2SO_4 , final filter weights were extrapolated from time versus weight curves. These curves can be found in Appendix D.

Sulfate analysis was done by the EPA barium-thorin titration method. All samples and blanks were filtered through ion-exchange columns containing Dowex Resin 50W-X8 100 to 200 mesh to remove any interferents.

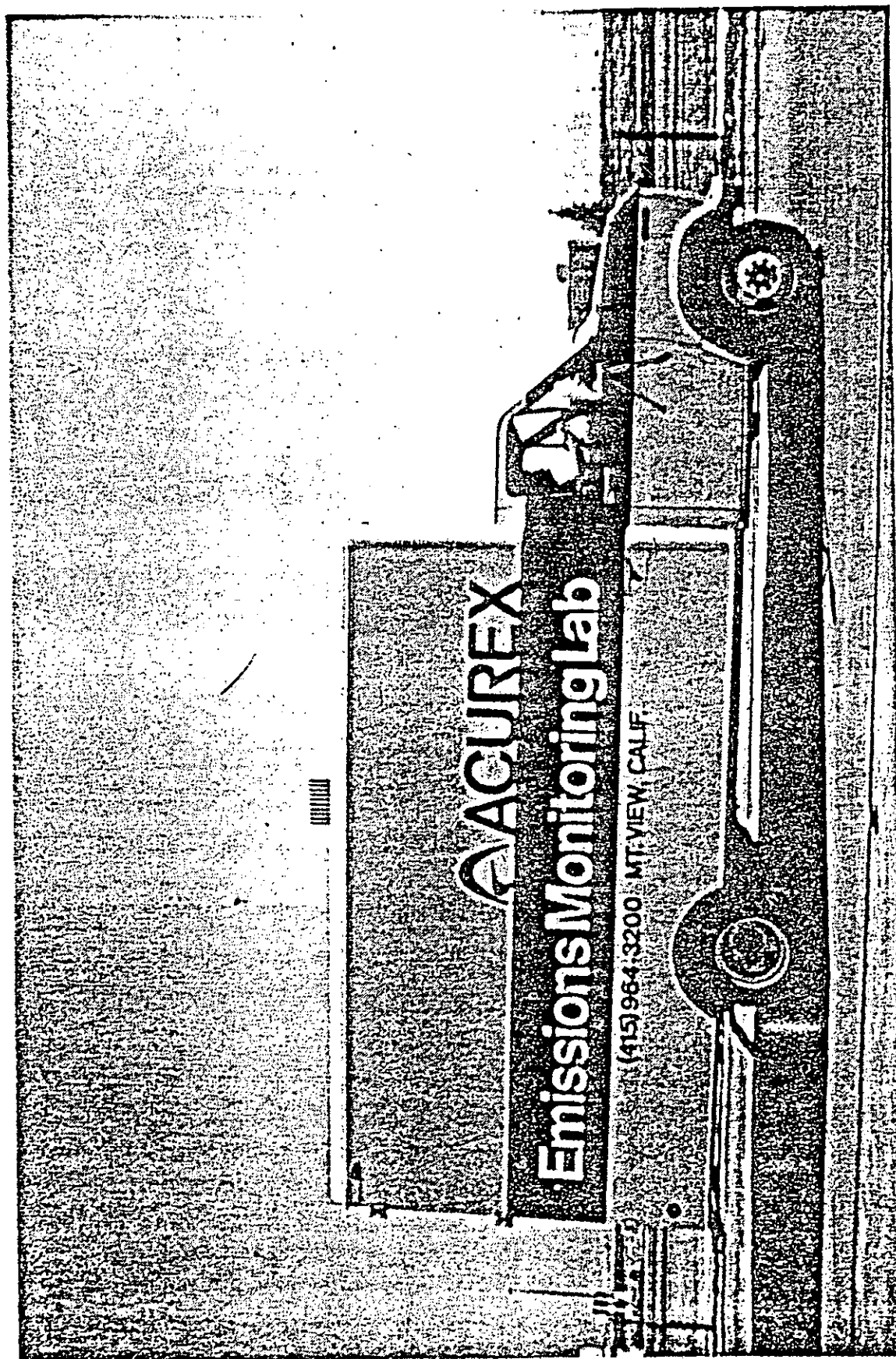


Figure 4-1. Acurex mobile emission monitoring laboratory.

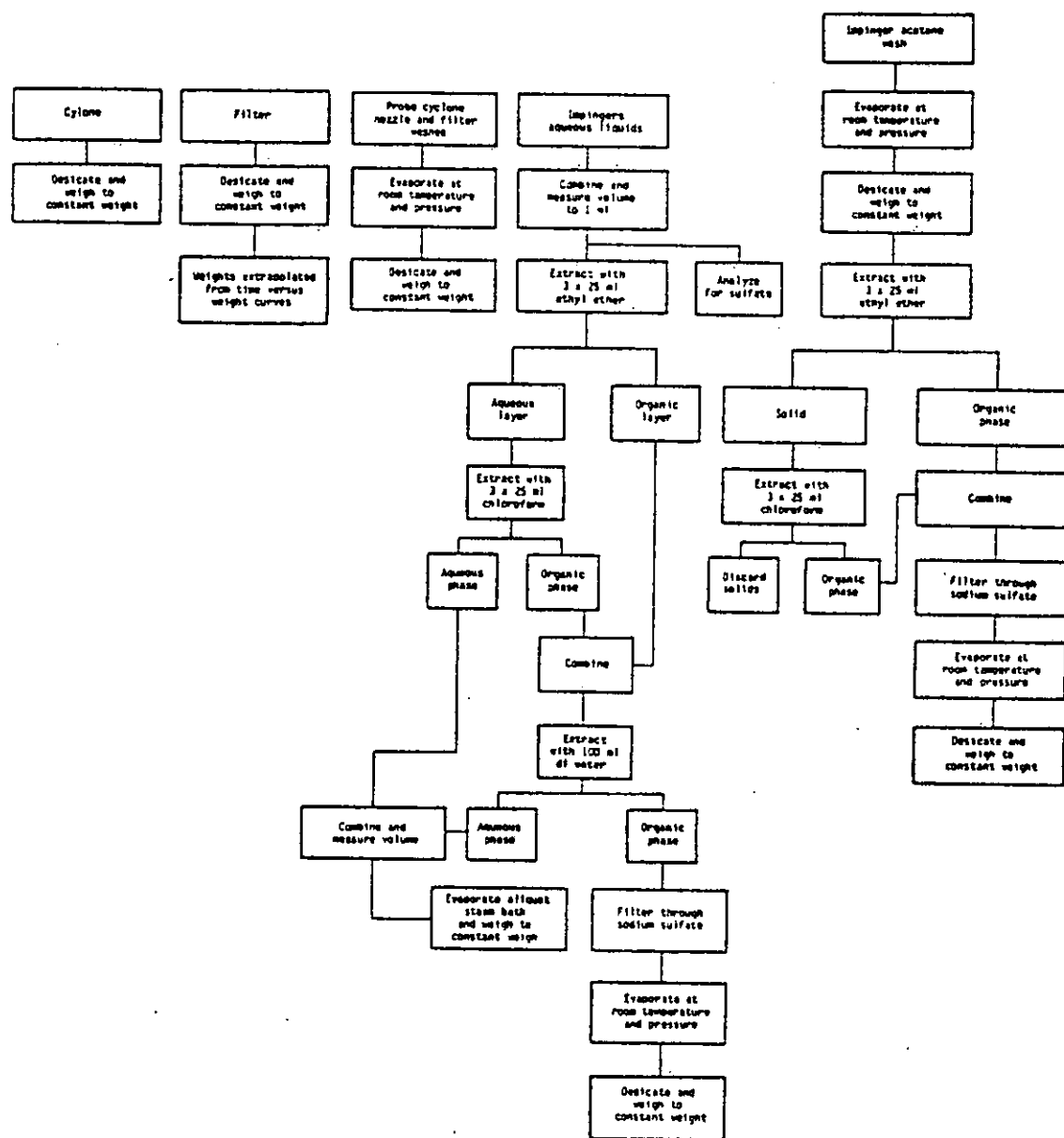


Figure 4-2. Sample analysis scheme for particulate mass train.

Barium perchlorate was standardized daily against 0.0100 N H_2SO_4 . All samples were assigned an I.D. number in a log book for chain of custody.

4.2 QUALITY ASSURANCE

Field analysis performed fell largely into two categories -- sulfate analysis using the barium thorin titration method, and particulate quantification of various samples (i.e., impinger catches, acetone washes, organic extracts etc.). A quality control program was made part of the sulfate analysis and quality assurance program monitored the latter analysis. The aluminum weighing tins used in quantification were baked at 350°F for 3 hours to drive off oils left on the aluminum by the manufacturing process. After baking, the tins were dessicated and then tarred to ± 0.1 mg. After dessicating for 24 hours, the tins were weighed on a Mettler Model H51AR analytical balance. The tins were then redessicated for 24 hours before being weighed a second time. The maximum weight difference was required to be 0.3 mg. This process was repeated every 24 hours until the weight difference met tolerance.

All solvents used were nanograde including the solvents used for glassware rinsing. Blank acetone samples were taken daily from the acetone squeeze bottles in use.

All water used, including that used for glassware washing, was deionized and provided by Republic's laboratory. Blanks of this water were taken daily from the main storage container.

Filters were visually inspected for imperfections prior to original tare. Like the tins, original tare tolerance was ± 0.1 mg. Final weights of the particulate mass filters changed too rapidly (due to presence of H_2SO_4) for normal tare procedures. Filter weights were extrapolated from time versus weight curves. Blank filters were carried with and run

along with the sample filters, through the drying and weighing processes to ± 0.3 mg.

A quality control program, including duplicates and spikes, was added to the quality assurance program for the sulfate analysis. Analyses of samples collected from the four particulate mass tests conducted at the No. 1 coke oven combustion stack were analyzed along with samples collected from 42 mass tests conducted at the BOF shop. Duplicates of samples were run -- a minimum of one in seven samples. Titrant was required to agree within ± 0.5 ml of original. These same samples were then spiked with approximately 150 percent of their original concentration, with a required percent recovery of 100 ± 5 percent. All blanks were analyzed in the same manner as their corresponding samples (i.e., through ion-exchange columns etc.). The results are summarized in Table 4-1.

Table 4-1. Quality Assurance Results

Date	Duplicate Percent	Recovery Percent
7-09-79	± 0.0	101.0
7-04-79	± 0.0	101.0
7-05-79	± 0.0	98.4
7-19-79	± 0.0	104.0
7-19-79	± 0.0	102.0
7-19-79	± 0.0	100.9

SECTION 5

STACK TEST RESULTS

This section of the report summarizes the results of the particulate mass emission tests conducted on the no. 1 coke battery combustion stack.

Tables 5-1 and 5-2 summarize the particulate mass data obtained for the coke plant test program. Table 5-1 presents pertinent flue gas data such as volumetric flowrate, oxygen and carbon dioxide concentration, stack gas velocity and stack gas temperature. Table 5-2 presents the particulate and condensible emission rates. All four tests were conducted within the ± 10 percent isokinetic sampling guideline required by EPA Method 5. Upon completion of each test each filter was visibly inspected; all filters for all four tests were intact, were not torn, and showed no signs of penetration. The average sampling probe and filter temperatures were within the $248 \pm 25^{\circ}\text{F}$ criteria required by EPA Method 5.

Particulate test results (Table 5-2) show that particulate mass emission rates for tests 60 and 62 were lower than particulate mass emission rates for tests 61 and 63. Plant operating data (Table 2-2) shows that during test 60 there were 7 ovens pushed and 6 ovens charged and during test 62 there were 4 ovens pushed and 5 ovens charged. Approximately 10 tons of coke are pushed from each oven. During test 61 there were no ovens charged or pushed and during test 63 there were 2

Table 5-1. Particulate Mass Test Sampling Data

Test No.	Date	Start Test	Test Time (min)	Stack Gas Moisture (%)	Oxygen Concentration (%)	Carbon Dioxide Concentration Temp (%)	Stack Gas Temp (°F)	Stack Gas Pressure (in. Hg)	Average Velocity (fps)	Stack Gas Volumetric Flowrate (dscfm)	Percent Isokinetic
60	7-16	0824	96	8.2	12.4	4.0	576	29.52	23.3	40300	96.9
61	7-16	1211	96	14.0	11.5	4.2	600	29.53	25.3	40100	101.2
62	7-17	0748	96	12.7	13.4	3.5	609	29.60	23.9	38300	100.5
63	7-17	1053	96	13.8	11.3	4.2	610	29.60	24.6	38800	100.9

Table 5-2. Particulate and Condensible Emission Rates

Test No.	Date	Volume of Gas Sampled (dscf)	Particulate Mass (mg)	Particulate ^a Mass Concentration (gr/dscf)	Particulate ^a - Mass Emission Rate (lbs/hr)	Condensible Organic Concentration (gr/dscf)	Condensible Organic Emission Rate (lbs/hr)	Condensible Inorganic Concentration (gr/dscf)	Condensible Inorganic Emission Rate (lbs/hr)	Condensible Sulfate Concentration (gr/dscf)	Condensible Sulfate Emission Rate (lbs/hr)	Total ^b Emission Rate (lbs/hr)
60	7-16	40,300	39.7	0.010	3.5	0.0001	0.04	0.0091	3.15	0.0103	6.32	6.69
61	7-16	40,100	56.0	0.014	4.7	0.0042	1.46	0.0685	23.54	0.0526	18.08	29.70
62	7-16	38,300	84.5	0.007	2.4	0.0009	0.29	0.3105	101.91	0.1744	57.23	104.60
63	7-16	38,800	88.2	0.023	7.5	0.0036	1.18	0.0848	28.19	0.0563	18.72	36.87
Average ± Standard Deviation				0.013 ± .007	4.5 ± 2.2	0.0022 ± 0.0020	0.74 ± 0.68	0.1182 ± 0.1322	39.20 ± 43.21	0.0754 ± 0.0682	25.09 ± 22.17	44.47 ± 42.11

^aFront half catch (nozzle, probe, cyclone, filter)

^bFront half plus back half catch (condensible organic and inorganic)

ovens pushed and 2 ovens charged. This grouping indicates that the particulate mass emission rate is lower when more ovens are pushed and charged. Condensible emission test results are also more variable when there are many ovens being charged and pushed. During these operations the doors to the oven are open and the negative draft will cause in-leakage. The O_2 concentration in Table 5-1 shows that tests 60 and 62 (many ovens being charged) measured from 1 to 2 percent higher O_2 than tests 61 and 63 (few ovens being charged). The variation in the number of ovens pushed and charged during this test program is considered to be typical.

Opacity readings (Table 5-3) were 0 percent throughout the particulate mass test runs except for a 30 second period of 10 percent opacity. This occurred during test 61 which was the only test where no charging or pushing took place.

Table 5-3. Visible Emission Readings

Date	Test No.	Particulate Test Time Interval	Opacity Reading Interval	No. of Opacity Readings	Range of Readings (%)	Average Opacity Readings (%)
7-16-79	60	0824-0912	0823-0912	196	0 - 0	0.0
		1021-1109	1018-1107	196	0 - 0	0.0
7-16-69	61	1211-1259	1207-1257	200	0 - 10	0.1
		1324-1412	1320-1409	196	0 - 0	0.0
7-17-79	62	0748-0836	0748-0836	192	0 - 0	0.0
		0910-0958	0910-0959	196	0 - 0	0.0
7-17-79	63	1053-1141	1053-1142	196	0 - 0	0.0
		1155-1243	1155-1244	196	0 - 0	0.0

APPENDIX A

SAMPLING EQUIPMENT

This section of the report describes the sampling equipment used by Acurex to sample the particulate emissions from the no. 1 coke oven combustion stack.

A.1 PARTICULATE SAMPLING EQUIPMENT

The particulate mass tests were conducted using the following sampling train:

- A 316 stainless steel sampling nozzle properly sized for isokinetic sampling;
- A 316 stainless steel lined sampling probe 10 feet long, equipped with a thermocouple to measure probe temperature, a thermocouple to measure stack gas temperature, and an S-type pitot tube to measure velocity pressure;
- A 316 stainless steel 3 μ cyclone for large particulate collection;
- A teflon coated stainless steel 142 mm filter holder;
- An impinger train containing four glass bottles to collect moisture and condensable material escaping the filter and cyclone;
- A 10-cfm carbon vane pump modified for very low leakage around the shaft;

- A control module to monitor temperature, pressure, and flowrate throughout the sampling train.

For a list of the specific equipment used for each particular test, refer to Table A-1.

A.1.1 Sampling Probe

A heated 316 stainless steel lined probe 10 feet in length was used to isokinetically extract samples from the ducts. The probe had a closed loop temperature control system to keep the probe temperature at 250°F as required by EPA Method 5. The probe was equipped with an S-type pitot tube to measure the stack gas velocity pressure and a thermocouple to measure the stack gas temperature.

A.1.2 Cyclone and Filter Holder

For the particulate mass tests, a 316 stainless steel cyclone with a 3 μ aerodynamic diameter cut point was used to capture large particulates (Figure A-1). A 316 stainless steel, teflon coated 142 mm filter holder containing a glass fiber filter was used to capture the particulates escaping the cyclone. The oven has its own closed loop temperature control system to maintain the cyclone and filter temperature at 250°F.

Table A-1. Sampling Equipment Used During Particulate Mass Tests

Test No.	Date	Probe Length (ft.)	Probe Liner	Pitot Coeff.	Nozzle Dia. (in.)	Orifice Coeff. (K ₀)	Control Unit No.
60	7/16/79	10	ss	.786	.429	.708	0039
61	7/16/79	10	ss	.786	.429	.708	0039
62	7/17/79	10	ss	.786	.745	1.787	0039
63	7/17/79	10	ss	.786	.429	.708	0039

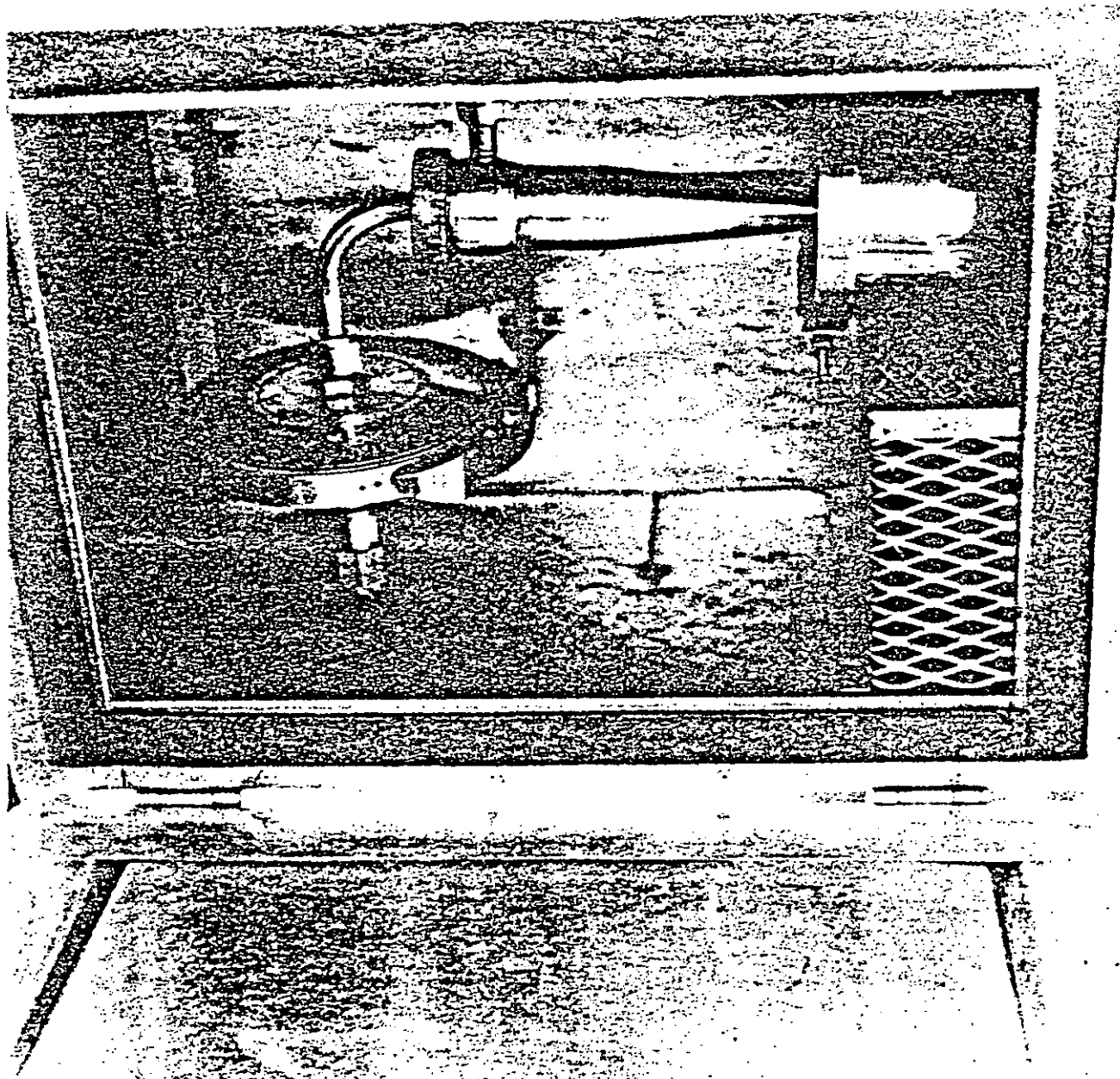


Figure A-1. One cyclone and filter in oven for particle mass tests.

The oven contains a fan to insure the uniform distribution of heat in the oven.

A.1.3 Impinger Train

The impinger train for the particulate mass tests was immersed in an icebath and consisted of four glass impinger bottles equipped with teflon caps and 316 stainless steel stems, connector tubes and fittings. The first two bottles contained 250 ml of distilled water, the third bottle was blank, and the fourth contained a known amount of silica gel. The temperature of the gases leaving the last impinger was monitored with a thermocouple. The impingers were used to collect moisture and condensable material (inorganic and organic) that escaped collection by the cyclone and filter.

A.1.4 Control Module

The control module monitors the temperatures, pressures and flowrates throughout the sampling train. For these tests, the orifice ΔH was indicated on a 0-6" magnehelic gauge whose smallest division was 0.1" H_2O . The velocity pressure of the stack gases is indicated on a 0-0.5" or a 0-4" magnehelic.

The control module contained a Rockwell Model 415 dry gas meter to measure the total volume of gas sampled to the nearest 0.005 ft³. An orifice meter (after the dry gas meter) was used to measure the instantaneous flowrate through the sampling train to insure sampling was being done isokinetically.

Finally, the control module had an 8-position thermocouple switch to measure temperatures throughout the sampling train. Figure A-2 illustrates all the aforementioned components of the Acurex High Volume Stack Sampler used for conducting the test program at the no. 1 coke oven combination stack.

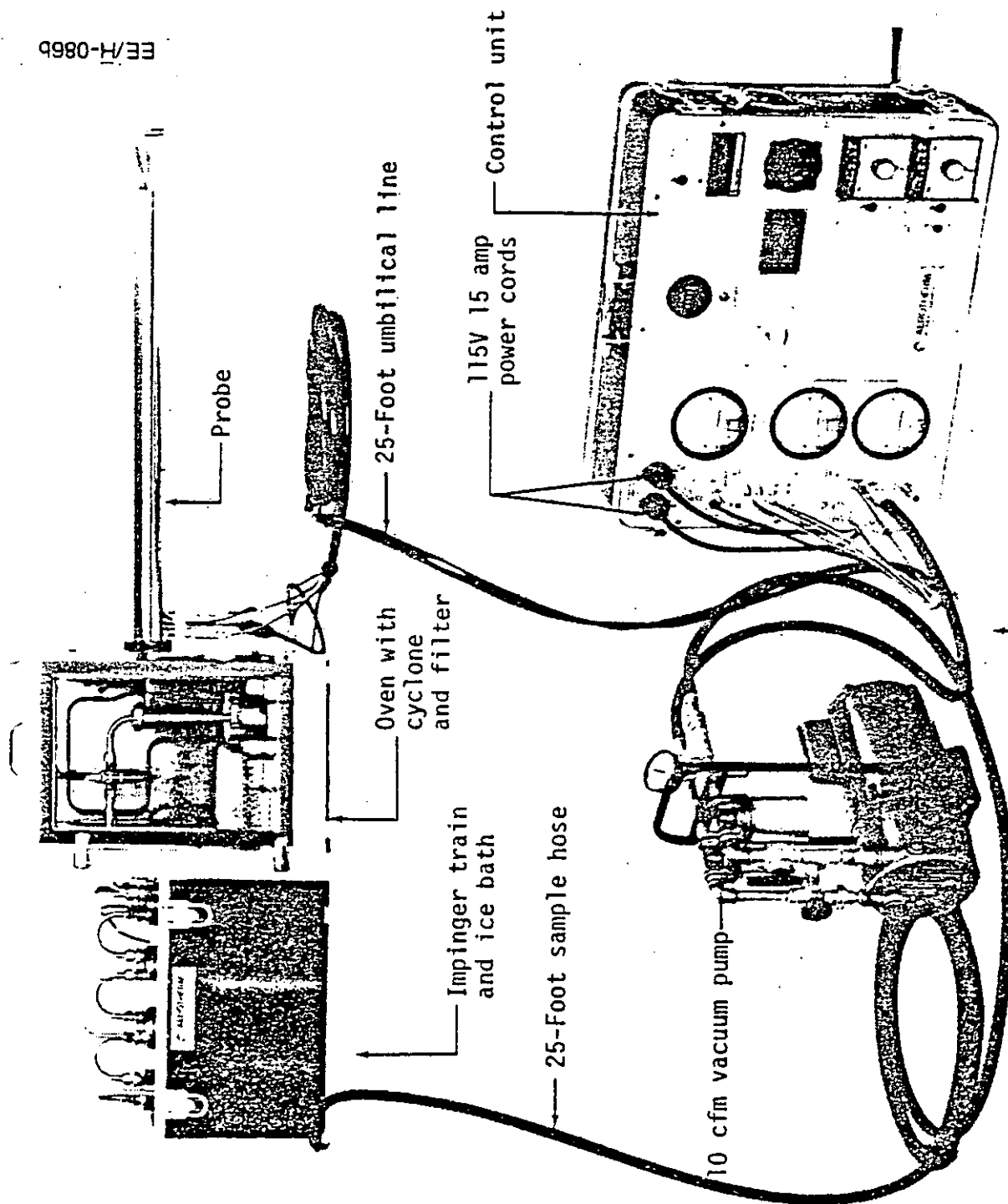


Figure A-2. Acurex high volume stack sampler.

APPENDIX B

PREPARATION OF THE SAMPLING EQUIPMENT

Before stack tests in the field can be conducted, sampling equipment must be carefully prepared to make reliable field measurements and to minimize costly delays due to equipment breakdown. This section of the report describes the preparations made by Acurex personnel prior to conducting the field tests at Republic Steel, Cleveland.

B.1 SAMPLING NOZZLES

All sampling nozzles to be used in the field tests were inspected and sharpened if necessary to minimize both gas streamflow disturbances and particulate impacting on the edge of the nozzle. Those nozzles which had been nicked or damaged were sharpened. The internal diameters of the sampling nozzles were measured with a micrometer to insure accurate values for the nozzle diameter when calculating the isokinetic sampling rates for the particulate tests.

B.2 SAMPLING PROBE

A heated 316 stainless steel lined sampling probe was used during the test program.

B.3 PROBE HEATER AND OVEN HEATER

Before the equipment was packed, and the probe and oven heaters and their temperature controllers were checked out in the laboratory by setting the temperature controllers at 250°F and turning the heaters

on. The system was left on for approximately 5 minutes to make sure that the heaters were working and the temperature controllers were holding the temperatures at 250°F.

B.4 UMBILICAL CORD

The umbilical cord which connects the probe to the control module was inspected and the polyflow tubing inside the umbilical cord checked for cracks and leaks. The quick disconnects were also inspected and checked to make sure they were operating properly.

B.5 IMPINGER ASSEMBLY

The impinger sampling train consisted of four glass impinger bottles (in place of the Lexan bottles normally used). All parts were inspected before they were shipped to the site. All the glassware was cleaned in a chromic acid bath. Replacement impinger bottles were taken in case of breakage.

B.6 VACUUM PUMP

The vacuum pumps were operated in the laboratory to measure their free flow capacity and leak rate at maximum vacuum. The vacuum pumps were found to be leak tight.

B.7 GLASS FIBER FILTERS

The glass fiber filters were obtained from Schleicher and Schuell and were equivalent to the MSA 1106 BH glass fiber filters specified by EPA Method 5. The filters were placed into individual plastic petri dishes and put in a dessiccator for conditioning over silica gel for at least 24 hours. The filters were then taken to the balance room and weighed to the nearest 0.01 milligram on a Mettler Model H51AR analytical balance. After weighing, each filter was returned to the plastic petri

dish, which was sealed with masking tape and labeled with the filter number. This information was also recorded in the filter record book.

B.8 CHEMICALS

Several types of chemicals were purchased for the field tests. Analytical reagent grade acetone from J. T. Baker (Resi-Analyzed) and Mallinckrodt (Nanograde) was used to rinse the front half and back half of the sampling train. Deionized water from Republic Steel's laboratory was used in the impinger train and was also used to rinse the impinger train for sample recovery (followed by acetone rinse). Chloroform and ether were analytical reagent grade chemicals.

Silica gel grade Type 4, from MC/B Company, was used to dry the sample gases. Silica gel is equivalent to Drierite, the desiccant specified by EPA Method 5.

B.9 FILTER HOLDER ASSEMBLY

The two filter holder assemblies were cleaned and inspected to insure the teflon gaskets were in good shape. Each assembly was equipped with new gaskets if required and tested for leaks before they were sent to the site. The filter halves had recently been teflon coated so that the internal surfaces were smooth and resistant to chemical attack.

APPENDIX C

CALIBRATION PROCEDURES

After the sampling equipment was inspected and prepared, various pieces of the sampling train were calibrated. This section describes these calibration procedures.

C.1 DIGITAL TEMPERATURE INDICATOR AND THERMOCOUPLES

The Acurex High Volume Stack Sampler uses a digital temperature indicator with an 8-point thermocouple selector switch. The selector switch permits temperature to be monitored at each of the following locations: stack gas, probe, oven, impinger train outlet, gas meter inlet, gas meter outlet, and two spare locations. The digital temperature indicator operates over a range of 0°F to 1500°F with an accuracy of $\pm 4^\circ\text{F}$. All temperatures in the sampling train are measured by chromel-alumel thermocouples.

The digital temperature indicator for the control module was checked in two ways. For the first check, a thermocouple was immersed in an ice bath at 32°F and the leads from the thermocouple connected to one of the spare locations on the control module. The reading on the digital temperature indicator was then observed and compared with that of the ice bath. For the second check, the oven controller was set at 250°F. The temperature of the oven was then displayed by the digital temperature indicator and compared to the temperature measured by a mercury-in-glass

thermometer. The zero and span of the digital temperature indicator was adjusted if the readings disagreed with either the ice bath or the oven temperature.

C.2 MAGNEHELIC GAUGES

Normally, magnehelic gauges are used in the control module to display the velocity pressure in the stack and the pressure drop across the orifice meter. These magnehelic gauges were calibrated against the Dwyer inclined manometer described in Section C.4.

The calibration procedure was a simple one. First the Dwyer inclined manometer and the magnehelic gauge to be calibrated were zeroed and leveled in the control module. Tee taps were installed in both the high-pressure and low-pressure sides of the magnehelic gauge. One side of the tee tap was connected to the orifice meter and the other side connected to the inclined manometer. A constant volume of gas was pumped through the orifice meter in the control module, and the readings on the magnehelic gauge and the Dwyer inclined manometer were observed. If the readings differed, the magnehelic gauge was adjusted and the calibration was repeated until the readings agreed. The calibration procedure was repeated at several different flowrates.

C.3 DRY GAS METER AND ORIFICE METER

The control module of the sampling train contains a dry gas meter and an orifice meter. The dry gas meter measures the total volume of gas sampled during the test. The orifice meter is used to measure the rate at which the stack gas is sampled.

A Rockwell Model 415 gas meter (illustrated in Figure C-1) is used to simultaneously calibrate the dry gas meter and orifice meter in the control module. This calibration standard is the same type of meter that

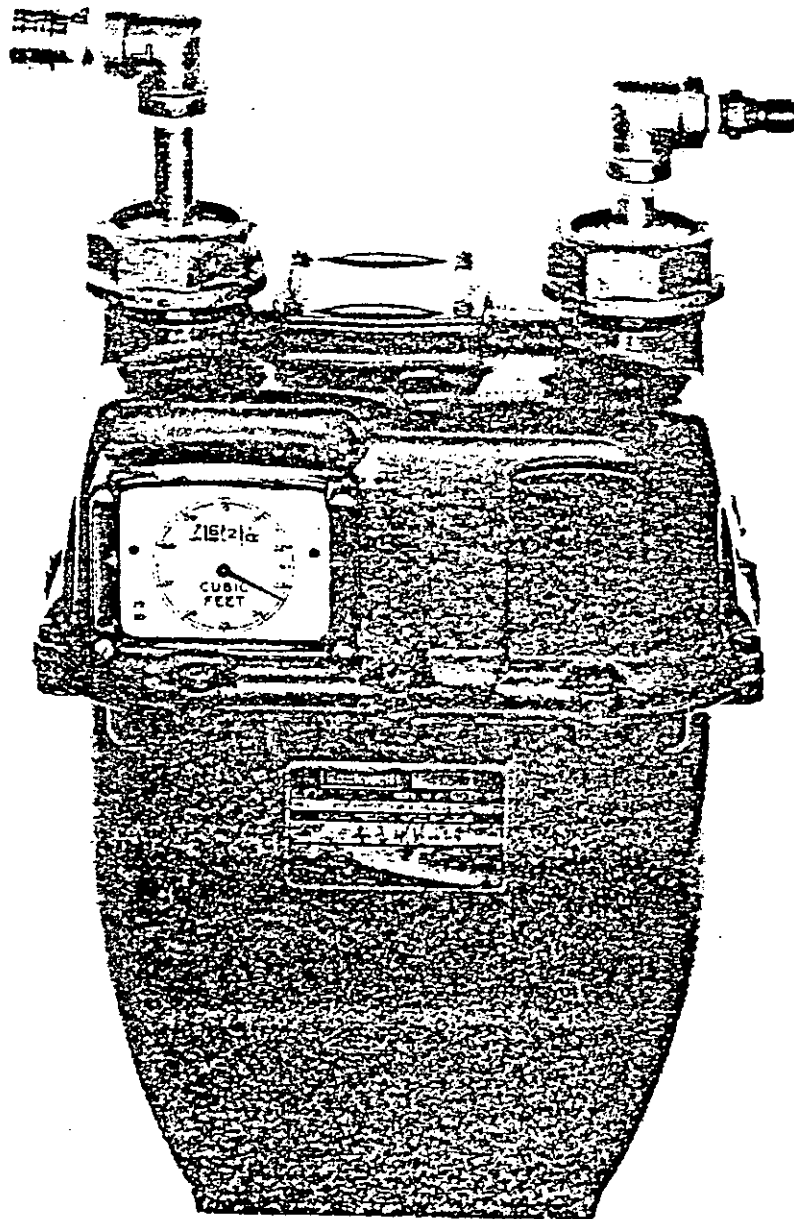


Figure C-1. Rockwell Model 415 gas meter calibration standard.

is used in the control module of the sampling train. The accuracy of this Rockwell meter has been verified against a National Bureau of Standards traceable bell prover maintained by the Pacific Gas & Electric Company.

Before performing a calibration, the Rockwell gas meter and the control module to be calibrated were left overnight in the Laboratory to come to thermal equilibrium. The next day, the magnehelic gauges in the control module were zeroed and leveled and the following components were arranged in series: the calibration standard, a vacuum pump, and the control module to be calibrated. Calibration information and the initial readings on the calibration standard gas meter and the gas meter in the control module were recorded on the data sheet shown in Figure C-2.

The vacuum pump was then turned on with the valves closed. Next, the valves were opened, the ΔH across the orifice magnehelic gauge was set at a particular value, and the timer in the control module was started. The initial inlet and outlet temperatures at the calibration standard meter were measured with chromel-alumel thermocouples. The inlet and outlet temperatures of the dry gas meter in the control module were measured by thermocouples installed in the meter and the temperatures were displayed on the digital temperature indicator. The flowrate through the assembled components was maintained at a constant rate (as indicated by the reading on the orifice magnehelic gauge) for a known length of time, ranging from 2 to 4 minutes, until at least 10 cubic feet of air had passed through the system.

At the completion of a calibration run, the final dry gas meter readings and the final inlet and outlet dry gas meter temperatures were recorded. The same procedure was repeated at four different flowrates to calibrate the orifice meter over its entire useful range. The data from

Date 5/23/75
Time 1400
Barometric Pressure 30.24
Ambient Temperature 74.7

Orifice Meter 6039, .358
Orifice Repeatability
Primary Calibration Meter
Control Module 0639

Operator P. Seay, Miller
Hot Bulb Temperature

PETER CALIBRATION DATA

Orifice Diameter ID (in. wg.)	Orifice Repeatability ΔP (in. wg.)	Primary Meter ΔP (in. wg.)	Dry Test Meter P _{ag} (in. wg.)	Gas Volume Primary Meter V _p (ft. ³)	Gas Volume Dry Test Meter V _d (ft. ³)	Temperature						Time t (min.)	a	b	
						Primary Meter			Dry Test Meter						
						Inlet, T _{di} (°F)	Outlet, T _{do} (°F)	Avg., T _{da} (°F)	Inlet, T _{di} (°F)	Outlet, T _{do} (°F)	Avg., T _{da} (°F)				
	0.2														
	0.4														
	0.6														
.52	0.8			6.42 4.77	6.32 4.15	73	74	73.5	75	73	74.25	3.5	1.74	5.14	
	1.0														
	1.2														
	1.4														
	1.6														
1.85	1.8			6.42 4.77	6.32 4.15	73	74	73.5	75	73	74.25	3.5	1.74	5.14	
	2.0														
	2.2														
	2.4														
	2.6														
2.82	2.8			6.42 4.77	6.32 4.15	73	74	73.5	75	73	74.25	3.5	1.74	5.14	
	3.0														
	3.2														
	3.4														
	3.6														
3.82	3.8			6.42 4.77	6.32 4.15	73	74	73.5	75	73	74.25	3.5	1.74	5.14	
	4.0														
	4.2														
	4.4														
	4.6														
	4.8														
	5.0														
Average															

Figure C-2. Meter Calibration Data Sheet

these calibrations were then used to calculate the calibration constants for the dry gas meter and the orifice meter in the control module.

The formula used to calculate the calibration constant for the dry gas meter is as follows:

$$\alpha = \frac{V_d \left(P_{\text{bar}} + \frac{\Delta H_o}{13.6} \right) \left(\frac{T_{\text{pi}} + T_{\text{po}}}{2} + 460 \right)}{V_p P_{\text{bar}} \left(\frac{T_{\text{di}} + T_{\text{do}}}{2} + 460 \right)}$$

where

α = calibration constant for dry gas meter in the control module

V_d = total volume of gas passing through the dry gas meter in the control module, ft^3

V_p = total volume of gas passing through the calibration standard meter, ft^3

P_b = barometric pressure, inches Hg

ΔH_o = pressure drop across the orifice meter in the control module, inches H_2O

13.6 = conversion factor, inches H_2O /inches Hg

T_{di} = inlet temperature of dry gas meter in the control module, $^{\circ}\text{F}$

T_{do} = outlet temperature of dry gas meter in the control module, $^{\circ}\text{F}$

T_{pi} = inlet temperature of calibration standard meter, $^{\circ}\text{F}$

T_{po} = outlet temperature of calibration standard meter, $^{\circ}\text{F}$

460 = conversion factor, $^{\circ}\text{F}$ to $^{\circ}\text{R}$

The meter readings obtained during the field tests were divided by α to obtain the true volume.

The calibration constant for the orifice meter was determined using the following formula:

$$K_o = \frac{V_p}{t \frac{T_{do} \Delta H_o}{P_{bar} M_m}^{1/2}}$$

where

K_o = calibration constant for the orifice meter in the control module

V_p = total volume of gas passing through the calibration standard meter, ft^3

T_{do} = outlet temperature of dry gas meter in the control module, $^{\circ}R$

t = calibration time, minutes

ΔH_o = pressure drop across the orifice meter in the control module, inches H_2O

P_{bar} = barometric pressure, inches Hg

M_m = molecular weight of the air, 28.96 lb/lb-mole

An average calibration constant was determined for the dry gas meter and orifice meter in the control module by averaging the individual test results. The calibration data for the control module used during the field tests is presented in Figure C-2.

C.4 S-TYPE PITOT TUBE

The S-type pitot tube attached to the sampling probe measures the volumetric stack gas flowrate and the velocity at each sampling point so that an isokinetic sampling rate can be determined. Before being taken into the field, the S-type tube for the sampling train was calibrated in the Acurex Wind Tunnel illustrated in Figure C-3 using the United Sensor

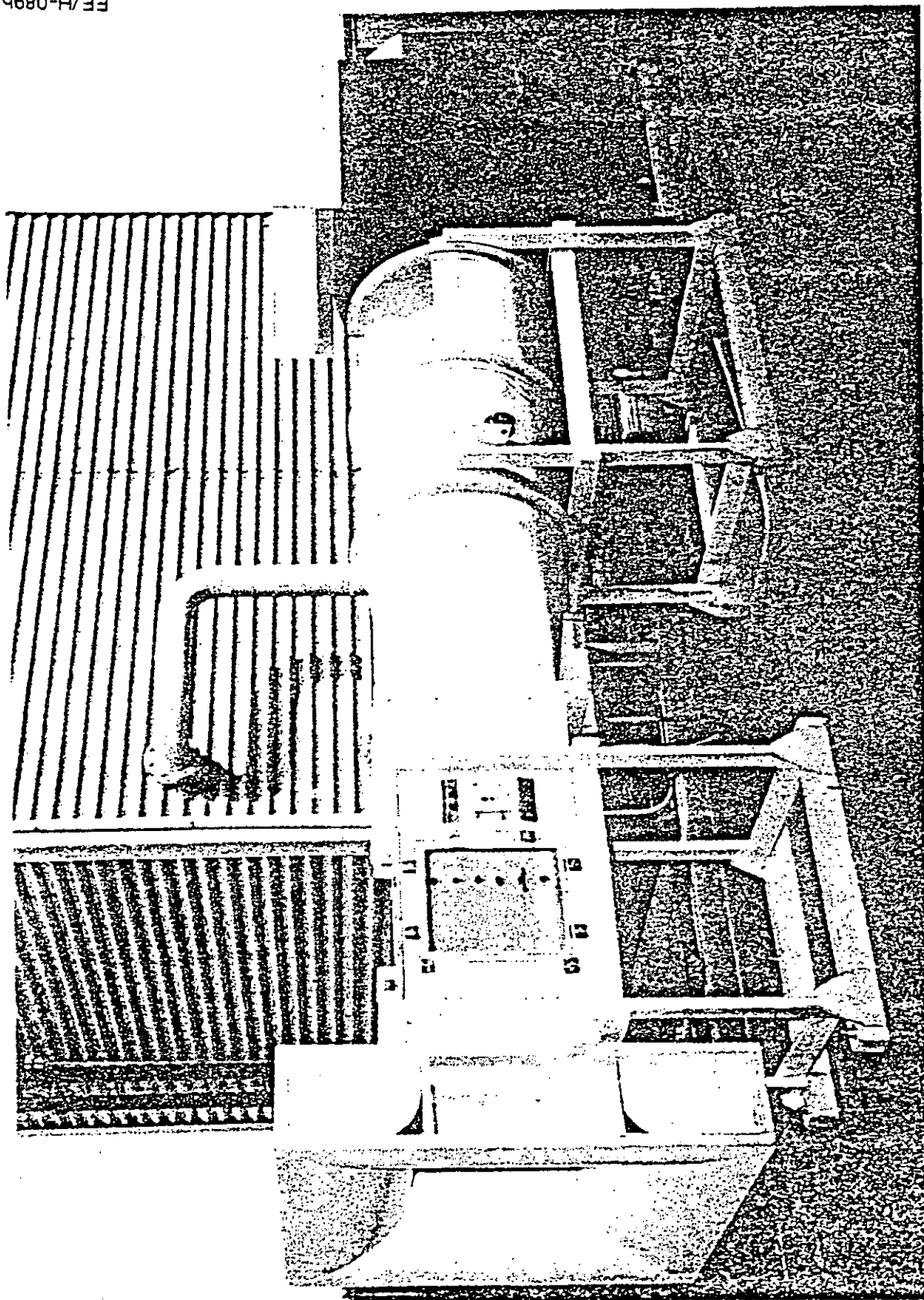


Figure C-3. Acurex calibration wind tunnel.

Hemispherical nose standard pitot tube shown in Figure C-4. The coefficient for this standard pitot tube is 0.99.

The velocity pressure sensed by the standard pitot tube was indicated on the Dwyer inclined manometer shown in Figure C-5. This manometer has a full scale range of 0 to 4 inches of water and can measure differences as small as 0.01 inch of water. In addition, the inclined manometer is equipped with a valve system which allows the operator to change from the standard pitot tube to the S-type tube being calibrated without disconnecting any tubes, thereby eliminating any unnecessary movement of the manometer. The valve system on the manometer also has a vent position which allows the manometer to be zeroed at any time. The manometer has a built-in level gauge so that the operator can check the level at any time.

The following steps were taken in calibrating the S-type pitot tube. First, the wind tunnel was leveled to ensure that the test section was horizontal. The wind tunnel fan was then turned on and the outlet dampers were adjusted to provide the desired velocity in the wind tunnel. The inclined manometer was positioned on a box near the wind tunnel and the standard pitot tube was connected to the inclined manometer with tygon tubing. At the same time, the S-type pitot tube was connected to the manometer using polyflow tubing and quick disconnects. Both the tygon and polyflow lines were inspected to make sure there were no leaks or cracks. The inclined manometer was then zeroed and leveled. Before beginning the actual calibration run, the data at the top of the pitot tube calibration data sheet, Figure C-6, was recorded.

The standard pitot tube was inserted into the wind tunnel through holes on the far side of the tunnel, as shown in Figure C-3, with the nose

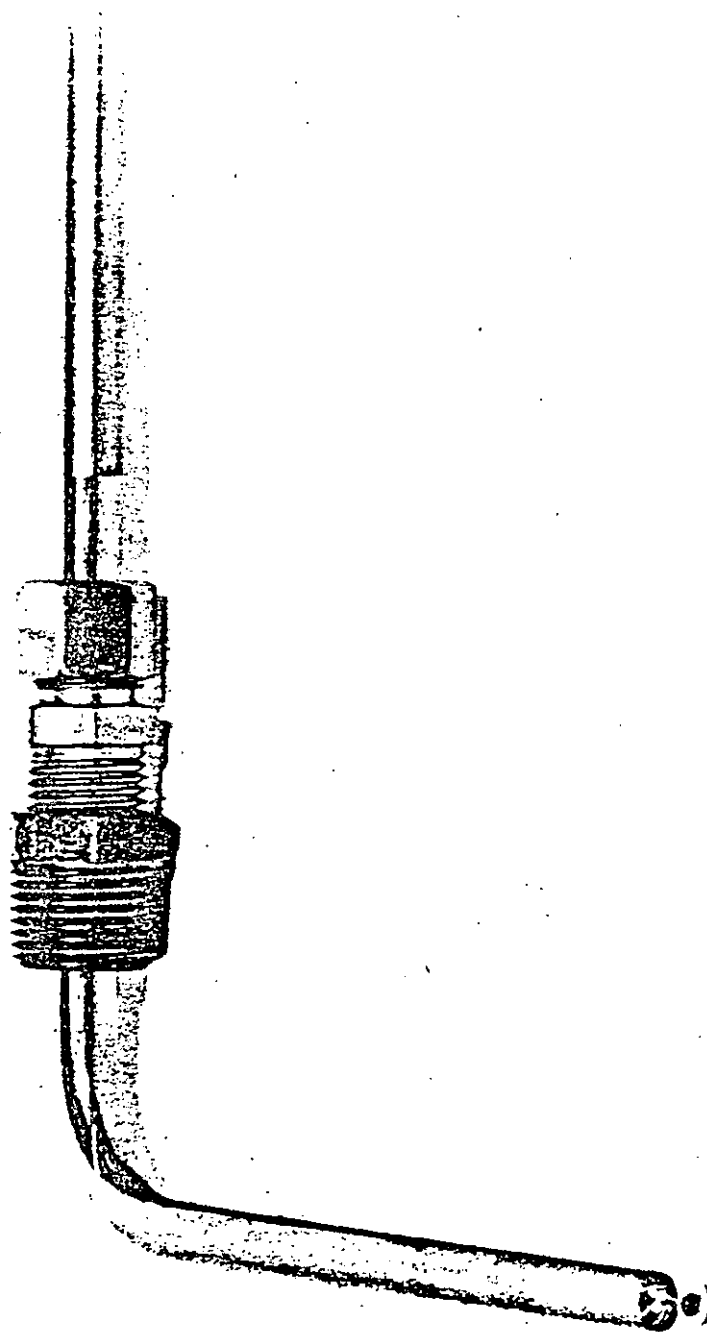


Figure C-4. United sensor hemispherical nose standard pitot tube.

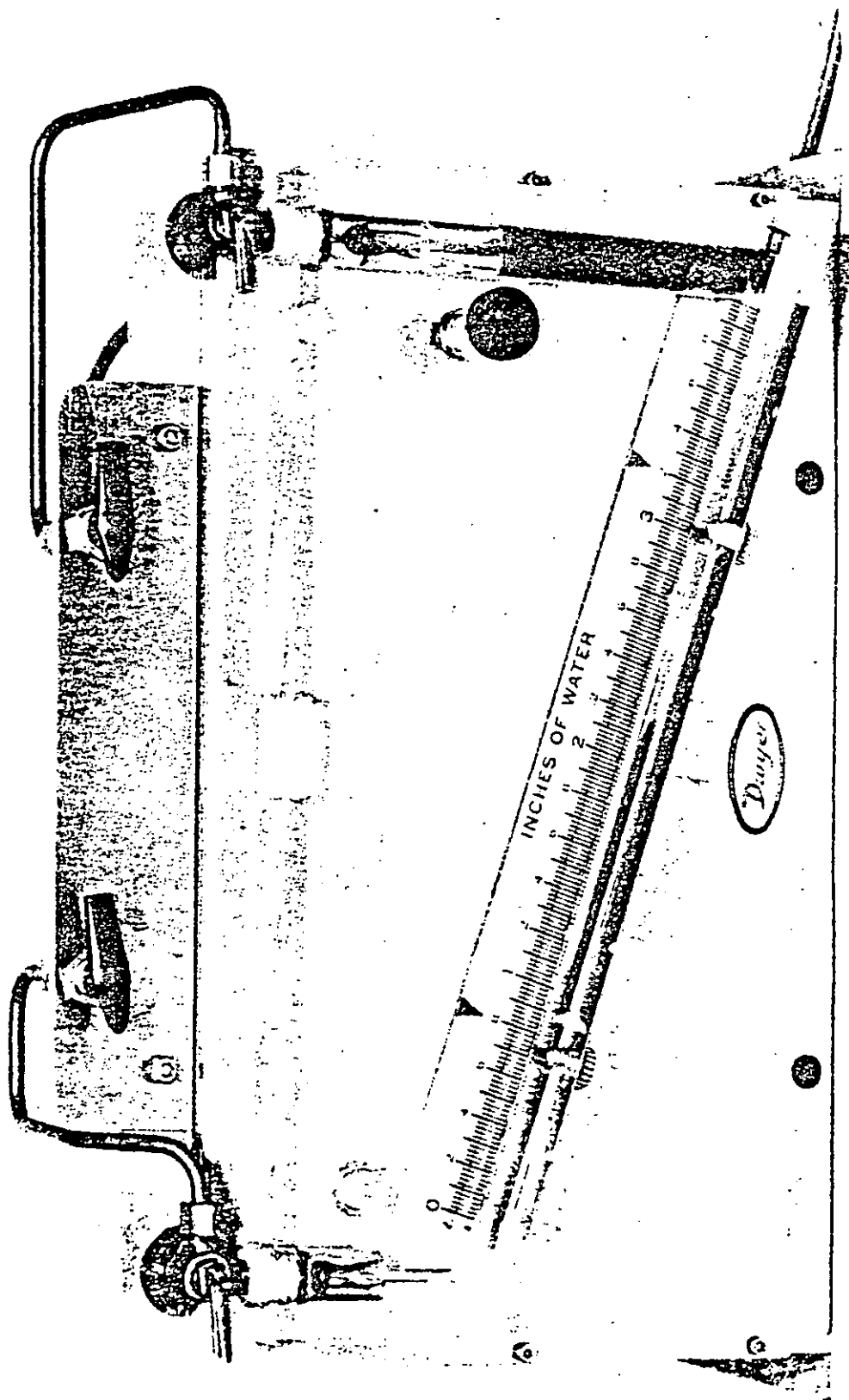


Figure C-5. Dwyer inclined manometer.

AMBIENT TEMP 68°F

TEST PITOT TUBE

STANDARD PITOT TUBE *United Sensor* NOZZLE-PITOT SPACING

TEST SECTION LOCATION Aerotherm

Wigzel Tunnel
OPERATORS Gilchrist, Kaufman

NOZZLE SIZE 1/2"

PITOT-TC SPACING

PITOT TUBE CALIBRATION DATA

[illegible]

Average Cg upper = .783

Average Cp. lower = .787

CP. Avg. = .786

Figure C-6. Pitot tube calibration data sheet.

of the pitot tube positioned at the centerline of the wind tunnel facing directly into the gas streamlines. The operator could look through a plexiglass window to ensure that the pitot tube was pointed in the proper direction at all times. With the standard pitot tube properly positioned in the test section, the valve system on the inclined manometer was opened. The velocity pressure measured by the standard pitot tube and indicated on the inclined manometer was recorded and the standard pitot tube was withdrawn from the wind tunnel.

The S-type pitot tube, attached to the sampling probe with the sampling nozzle and thermocouple in place, was then inserted through the near side of the wind tunnel so that the S-type tube tip was at the centerline of the wind tunnel. Inserting the sampling probe assembly into the wind tunnel was made easier by a bracket adjacent to the plexiglass window, as shown in Figure C-3. The bracket was clamped tightly around the sampling probe to ensure that the assembly did not move in the wind tunnel. The bracket also made a seal with the inside of the wind tunnel wall so that the surfaces were flush and no flow disturbance was created at the wall. The tips of the S-type pitot tube were aligned and pointed directly into the gas streamlines, with the operator observing the position of the tips through the plexiglass window.

The valve system on the inclined manometer was then switched to the S-type pitot tube, and the velocity pressure measured by the lower leg of the S-type pitot tube and indicated by the inclined manometer, was recorded. This procedure was repeated several times in order to calibrate the S-type pitot tube over a wide range of velocities.

The formula used to calculate the coefficient for the S-type pitot tube for each sampling probe is as follows:

$$C_{P_{S\text{-type}}} = 0.99 \frac{P_{\text{std}}^{1/2}}{P_{S\text{-type}}^{1/2}}$$

where

$C_{P_{S\text{-type}}}$ = coefficient of the S-type pitot tube

P_{std} = velocity pressure measured by the standard pitot tube,
inches H₂O

$P_{S\text{-type}}$ = velocity pressure measured by the S-type pitot tube,
inches H₂O

0.99 = coefficient of the standard pitot tube

The average coefficients for the upper and lower legs of the S-type pitot tube were calculated by averaging the individual coefficients of each calibration run. These average values were recorded on the calibration data sheet. The 10 foot 316 ss lined probe used during the field tests was calibrated in accordance with the aforementioned procedures. Figure C-6 shows the calibration data for the S-type pitot tube and sampling probe that was used during the field test program.

C.5 METTLER ANALYTICAL BALANCE

A Mettler Model H51AR balance, which can be read to 0.01 mg, was used to weigh the glass fiber filters and the chemicals used to prepare solutions. This balance is checked twice a year by the Mettler Instrument Corporation against National Bureau of Standards weights to ensure its accuracy. In addition, a set of Class S National Bureau of Standards weights were brought into the field to check the accuracy of this balance periodically.

APPENDIX D
RAW DATA SHEETS

ACUREX Corporation Republic Steel 7/16/79 Date Test Location Run Number Stack Diameter inches Duct Dimensions in. x in. Start Time Operator

Page 1 of 3
 Barometric Pressure 29.61
 Static Pressure -1.2
 Stack Pressure 29.52
 Probe Number 10
 Pilot Coefficient 0.786
 Pilot Number P11
 Meter Box Number 0039
 Orifice Coefficient .708

PARTICULATE TEST FIELD DATA SHEET

Nozzle Size & Number 429
 Molecular Weight
 BWO
 FILTER DATA
 NUMBER TARE FINAL WT
 IMPINGER VOLUMES
 TIME CO₂ O₂ CO
 10.20 4% 12.8% 0%
 10.50 4% 12% 0%
 11.3.7
 SILICA GEL

SAMPLE POINT	CLOCK TIME	VELOCITY HEAD ΔP in wg	ORIFICE METER ΔH in. wg	GAS METER VOLUME FT ³	STACK	PROBE	TEMPERATURES °F				OVEN	GAS METER		PUMP VACUUM in. Hg	√ΔP	Leak Rate
							IMPINGER	ORGANIC MODULE				IN	OUT			
5	0	.05	.78	543.147	450	254	72				260	P8	P8		.22	
5	2.0	.06	.95	543.112	425	260	66				267	P7	P7		.24	
5	4.0	.05	.78	543.112	450	260	66				267	P7	P7		.22	
5	6.0	.078	1.08	546.21	452	254	63				267	P7	P7		.24	
5	8.0	.06	1.10	547.58	307	253	63				267	P7	P7		.24	
6	10.0	.06	1.10	548.80	314	254	63				268	P6	P6		.24	
7	12.0	.075	1.02	549.81	574	260	64				267	P6	P6		.27	
8	14.0	.075	.99	550.96	609	258	64				267	P6	P6		.27	
9	16.0	.08	1.05	552.11	614	258	64				268	P7	P7		.28	
10	18.0	.09	1.17	553.25	622	264	65				267	P7	P7		.3	
11	20.0	.09	1.17	554.43	624	267	66				268	P7	P7		.3	
12	22.0	.09	1.17	555.62	628	267	67				268	P6	P6		.3	
13	24.0	.11	1.42	556.87	634	268	68				268	P6	P6		.33	
14	26.0	.13	1.67	558.19	640	267	69				268	P7	P7		.34	
15	28.0	.14	1.79	559.64	642	266	68				268	P7	P7		.37	
16	30.0	.14	1.79	561.17	645	267	69				268	P7	P7		.37	
17	32.0	.14	1.79	562.72	648	267	67				267	P7	P7		.37	
18	34.0	.145	1.84	564.27	652	270	69				267	P7	P7		.38	
19	36.0	.14	1.79	565.82	654	269	68				267	P7	P7		.37	
20	38.0	.14	1.86	567.37	603	270	67				268	P7	P7		.37	
AVG/TOTAL																

SAMPLE POINT	CLOCK TIME	VELOCITY HEAD ΔP in. wg	ORIFICE METER ΔH in. wg	GAS METER VOLUME FT ³	STACK	PROBE	TEMPERATURES °F				IMPINGER	ORGANIC MODULE	OVEN	GAS METER		PUMP VACUUM in Hg	√ΔP	
														IN	OUT			
5	0	.05	.70	605.845	560	259	✓	✓	✓	✓	69		263	96	96		.22	Leak Check
5	2	.045	.63	606.84	561	262	✓	✓	✓	✓	70		262	98	97		.21	.014 / 15" Hg
5	4	.05	.70	607.77	561	263	✓	✓	✓	✓	68		264	98	97		.22	
5	6	.05	.70	608.71	560	265	✓	✓	✓	✓	68		262	97	97		.22	At 10" OK
5	8	.045	.63	609.68	567	264	✓	✓	✓	✓	68		262	98	97		.21	
6	10	.11	1.54	610.61	568	266	✓	✓	✓	✓	69		263	98	97		.33	
7	12	.14	1.95	611.94	568	267	✓	✓	✓	✓	69		263	98	97		.37	
8	14	.14	1.91	612.37	568	269	✓	✓	✓	✓	69		264	98	97		.37	
9	16	.145	1.9	615.17	637	263	✓	✓	✓	✓	68		262	97	97		.38	
10	18	.134	1.82	616.54	644	265	✓	✓	✓	✓	68		263	97	97		.37	
11	20	.145	1.88	618.07	647	267	✓	✓	✓	✓	68		264	97	97		.38	
12	22	.13	1.76	619.61	600	265	✓	✓	✓	✓	68		267	97	98		.36	
13	24	.13	1.74	621.12	610	266	✓	✓	✓	✓	69		267	97	98		.36	
14	26	.13	1.74	622.60	612	267	✓	✓	✓	✓	69		266	97	98		.36	
15	28	.125	1.67	624.08	617	263	✓	✓	✓	✓	69		263	97	98		.35	
16	30	.12	1.59	625.52	621	264	✓	✓	✓	✓	68		266	97	98		.34	
17	32	.125	1.65	626.94	624	265	✓	✓	✓	✓	69		263	97	98		.35	
18	34	.125	1.65	628.40	627	264	✓	✓	✓	✓	69		265	97	98		.35	
19	36	.115	1.51	629.83	630	266	✓	✓	✓	✓	69		267	97	98		.34	
20	38	.115	1.51	631.23	633	267	✓	✓	✓	✓	69		268	97	98		.34	
AVG/TOTAL	96		1.51	65.738	600	25.771								98	98		.33	

ACUREX Corporation
Plant Republic Steel Cleveland
Date 7-16-79
Test Location Coke Stack
Run Number #61

243

PARTICULATE TEST FIELD DATA SHEET 2

Barometric Pressure
Static Pressure
Stack Pressure
Probe Number
Filter Coefficient
Pilot Number
Meter Box Number
Orifice Coefficient

Nozzle Size & Number
Molecular Weight
BWO

FILTER DATA		
NUMBER	TAIRE	FINAL WT

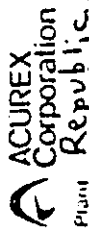
IMPINGER VOLUMES	TIME	CO ₂	O ₂	CO
SILICA GEL				

Operator JARMAN

SAMPLE POINT	CLOCK TIME	VELOCITY HEAD ΔP in. wg	ORIFICE METER ΔH in. wg	GAS METER VOLUME FT ³	TEMPERATURES °F				PUMP VACUUM in. Hg	√ΔP
					STACK	PROBE	IMPINGER	ORGANIC MODULE	OVEN	GAS METER IN OUT
21	40	.12	1.57	632.61	636	267	70		269	97 98
22	42	.13	1.7	634.01	638	267	70		263	97 98
23	44	.11	1.43	635.47	642	265	71		264	96 98
24	46	.11	1.43	636.81	642	267	70		267	96 98
end	48			638.211						
5	48	.07	1.06	638.211	490	257	72		273	98 99
5	50	.065	.98	639.11	491	265	70		269	98 99
5	52	.08	1.2	640.51	495	266	69		268	98 99
5	54	.075	1.13	641.79	500	265	68		263	98 99
5	56	.075	1.13	642.99	503	262	68		263	98 99
6	58	.08	1.19	644.21	504	265	69		261	98 99
7	60	.08	1.14	645.47	550	266	69		262	98 99
8	62	.085	1.15	646.69	605	267	69		263	98 99
9	64	.09	1.2	647.17	613	267	69		263	98 99
10	66	.10	1.34	649.23	615	267	68		267	98 99
11	68	.10	1.35	650.45	618	267	68		269	98 99
12	70	.105	1.4	651.77	623	267	69		267	98 99
13	72	.115	1.52	653.10	628	265	69		265	99 99
14	74	.125	1.65	654.59	633	264	70		265	99 99
AVG/TOTAL										

1324

510377



Plant Republic steel

Date 7/17/79

Test Location Coke stack #1

Run Number 62

Stack Diameter inches 107

Duct Dimensions in. x in.

Start Time 0748

Operator JARMAN

Barometric Pressure 29.76

Static Pressure -1.3" H₂O

Stack Pressure -

Probe Number 10

Pilot Coefficient 0.786

Pilot Number P11

Meter Box Number 0039

Orifice Coefficient 1.787

PARTICULATE TEST FIELD DATA SHEET

Nozzle Size & Number 745

Molecular Weight

BWO

FILTER DATA

NUMBER	TAPE	FINAL WT

IMPINGER VOLUMES	TIME	CO ₂	O ₂	CO
553.1	7.58	3.7	13.2	0
	9.35	3.3	13.6	0
SILICA GEL				

SAMPLE POINT	CLOCK TIME	VELOCITY HEAD ΔP in. wg	ORIFICE METER ΔH in. wg	GAS METER VOLUME FT ³	STACK	PROBE	IMPINGER	ORGANIC MODULE	OVEN	GAS METER		PUMP VACUUM in. Hg	√ΔP	Leak Rate
										IN	OUT			
5	0	.03	1.84	671.772	550	260	70		268	84	85		.17	12.01549
5	2	.035	.49	674.79	553	256	64		263	84	85		.18	
5	4	.04	.79	676.32	557	262	63		260	84	85		.2	
5	6	.07	1.37	679.21	561	264	67		258	84	85		.24	
5	8	.07	1.36	682.14	567	268	60		262	84	85		.26	
6	10	.09	1.72	685.43	569	277	67		268	85	87		.3	
7	12	.09	1.36	688.91	585	272	67		266	88	85		.26	
8	14	.095	1.79	692.60	602	267	68		266	89	85		.30	
9	16	.10	1.89	696.31	606	266	68		268	89	85		.31	
10	18	.11	2.08	700.13	609	267	69		266	92	86		.33	
11	20	.11	2.07	704.01	613	264	69		267	93	86		.33	
12	22	.11	2.07	707.91	618	271	69		267	94	86		.33	
13	24	.13	2.43	711.89	622	269	69		269	94	86		.36	
14	26	.125	2.33	716.12	627	269	68		267	94	86		.35	
15	28	.14	2.62	720.37	631	270	68		267	97	87		.37	
16	30	.14	2.61	724.77	633	272	69		267	98	88		.37	
17	32	.135	2.53	729.12	636	272	69		267	100	88		.36	
18	34	.13	1.42	733.67	640	269	68		269	100	88		.38	
19	36	.14	2.6	738.01	643	270	69		267	100	89		.38	
20	38	.14	2.6	742.41	646	269	69		268	101	89		.38	
AVG TOTAL														

36.685

Date

7-17-79

Barometric Pressure

29.07

Test Location

Coke Stack

Static Pressure

-1.3

Run Number

#63

Stack Pressure

10 ft

Stack Diameter inches

107

Pilot Coefficient

1.786

Duct Dimensions in x in

11

Pilot Number

0039

Start Time

1053

Meter Box Number

708

Operator

JARMAN

Orifice Coefficient

708

FILTER DATA

NUMBER	TARE	FINAL WT

IMPINGER VOLUMES	TIME	CO ₂	O ₂	CO
205				
SILICA GEL				

SAMPLE POINT	CLOCK TIME	VELOCITY HEAD ΔP in. wg.	ORIFICE METER ΔH in. wg.	GAS METER VOLUME FT ³	TEMPERATURES °F			IMPINGER	GAS METER		OVEN	PUMP VACUUM in Hg		ΔP	Leak Check
					STACK	PROBE	IMPINGER	ORGANIC MODULE	IN	OUT		IN	OUT		
5	0	.03	.41	855.273	567	255	72		86	86	280			.17	Leak Check
5	2	.03	.41	856.04	570	257	71		85	86	281			.17	.008 / 16" Hg
5	4	.035	.48	856.77	573	267	70		85	86	281			.19	
5	6	.035	.47	857.54	576	267	70		85	86	281			.19	
5	8	.035	.47	858.34	579	261	69		75	86	273			.19	
6	10	.08	1.08	859.14	581	262	68		84	86	266			.28	
7	12	.09	1.21	860.25	583	272	68		84	86	271			.3	
8	14	.095	1.27	861.45	585	264	69		84	86	273			.31	
9	16	.11	1.44	862.98	611	268	69		84	86	268			.33	
10	18	.12	1.58	864.05	608	270	70		84	86	266			.35	
11	20	.125	1.63	865.45	617	270	69		84	86	266			.35	
12	22	.12	1.55	866.89	623	269	69		85	86	269			.35	
13	24	.125	1.61	868.30	628	273	70		85	86	267			.35	
14	26	.125	1.60	869.69	631	272	69		86	86	267			.35	
15	28	.13	1.67	871.10	635	269	68		86	86	268			.36	
16	30	.135	1.73	872.55	638	268	69		86	86	268			.37	
17	32	.14	1.77	874.0	641	270	69		87	86	268			.37	
18	34	.14	1.8	875.48	644	270	69		87	86	268			.37	
19	36	.13	1.67	876.99	647	277	68		87	87	268			.36	
20	38	.12	1.58	877.13	607	279	69		87	87	269			.35	
AVG/TOTAL			1.27	607	607				85	86				.30	

25.097

VISIBLE EMISSION OBSERVATION RECORD

Company Republic Steel

Date 7/16/79

Time First Sighted Plume

Time Start 0823

Time Stop 0912

Air Temperature 79°F

Relative Humidity 75%

Wind Speed 5-7 MPH

Wind Direction out of West

Sky Condition Clear

Background Blue Sky

Plume Characteristics: Continuous: ☐ Yes ☒ No

Color _____ Dispersion Description _____

Stack Height 150 (ft) Observer Location 750 (ft) NE of stack

Sun Location: ☐ Back of Observer ☒ Left Shoulder ☒ Right Shoulder ☐ Other _____

Emission Point Stack of ~~blast~~ combustion stack AD-1 coke Battery

Min	0	15	30	45
01	0	0	0	0
02	0	0	0	0
03	0	0	0	0
04	0	0	0	0
05	0	0	0	0
06	0	0	0	0
07	0	0	0	0
08	0	0	0	0
09	0	0	0	0
10	0	0	0	0
11	0	0	0	0
12	0	0	0	0
13	0	0	0	0
14	0	0	0	0
15	0	0	0	0
16	0	0	0	0
17	0	0	0	0
18	0	0	0	0
19	0	0	0	0
20	0	0	0	0

Min	0	15	30	45
21	0	0	0	0
22	0	0	0	0
23	0	0	0	0
24	0	0	0	0
25	0	0	0	0
26	0	0	0	0
27	0	0	0	0
28	0	0	0	0
29	0	0	0	0
30	0	0	0	0
31	0	0	0	0
32	0	0	0	0
33	0	0	0	0
34	0	0	0	0
35	0	0	0	0
36	0	0	0	0
37	0	0	0	0
38	0	0	0	0
39	0	0	0	0
40	0	0	0	0

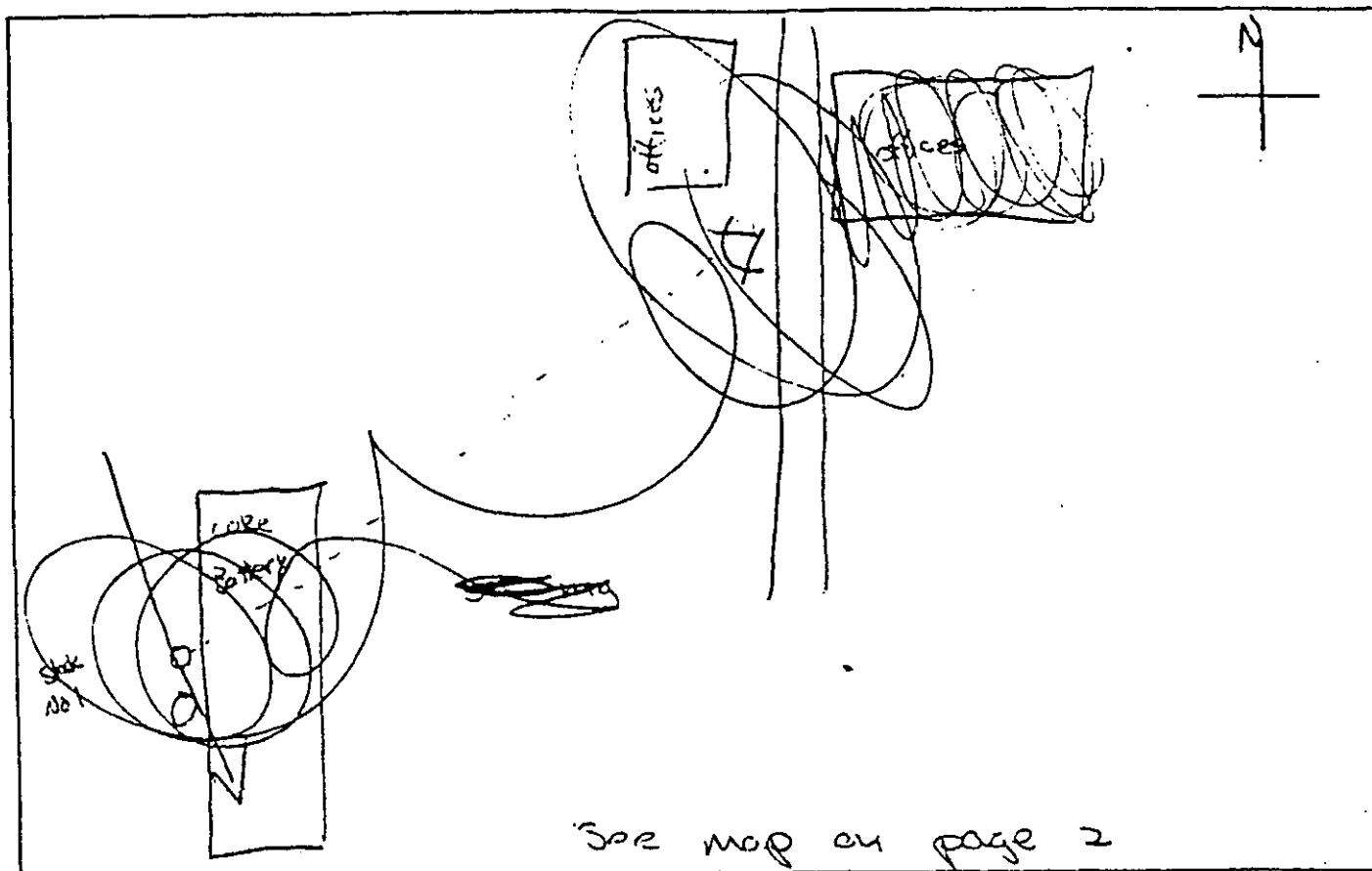
Min	0	15	30	45
41	0	0	0	0
42	0	0	0	0
43	0	0	0	0
44	0	0	0	0
45	0	0	0	0
46	0	0	0	0
47	0	0	0	0
48	0	0	0	0
49	0	0	0	0
50				
51				
52				
53				
54				
55				
56				
57				
58				
59				
60				

NOTES Test 60

Inspector Pete Kaufmann

Date 7/16/79

MAP



Symbols

Sun = ☼

Plume direction = →

Water Vapor Condensate None

Point where plume observed =

Observer = ✕

Photographs: ☐ File ☐ Enclosed ☒ None

Comments

Signature

Pat K. J. ...

Date

7/16/79

510386

VISIBLE EMISSION OBSERVATION RECORD

Company _____
 Date _____ Time First Sighted Plume _____
 Time Start 1018 Time Stop 1107
 Air Temperature _____ Relative Humidity _____
 Wind Speed _____ Wind Direction _____
 Sky Condition _____ Background _____
 Plume Characteristics: Continuous: ☐ Yes ☐ No
 Color _____ Dispersion Description _____
 Stack Height _____ (ft) Observer Location _____ (ft) _____ of stack
 Sun Location: ☐ Back of Observer ☐ Left Shoulder
☐ Right Shoulder ☐ Other _____

Emission Point

Min	0	15	30	45
01	0	0	0	0
02	0	0	0	0
03	0	0	0	0
04	0	0	0	0
05	0	0	0	0
06	0	0	0	0
07	0	0	0	0
08	0	0	0	0
09	0	0	0	0
10	0	0	0	0
11	0	0	0	0
12	0	0	0	0
13	0	0	0	0
14	0	0	0	0
15	0	0	0	0
16	0	0	0	0
17	0	0	0	0
18	0	0	0	0
19	0	0	0	0
20	0	0	0	0

Min	0	15	30	45
21	0	0	0	0
22	0	0	0	0
23	0	0	0	0
24	0	0	0	0
25	0	0	0	0
26	0	0	0	0
27	0	0	0	0
28	0	0	0	0
29	0	0	0	0
30	0	0	0	0
31	0	0	0	0
32	0	0	0	0
33	0	0	0	0
34	0	0	0	0
35	0	0	0	0
36	0	0	0	0
37	0	0	0	0
38	0	0	0	0
39	0	0	0	0
40	0	0	0	0

Min	0	15	30	45
41	0	0	0	0
42	0	0	0	0
43	0	0	0	0
44	0	0	0	0
45	0	0	0	0
46	0	0	0	0
47	0	0	0	0
48	0	0	0	0
49	0	0	0	0
50				
51				
52				
53				
54				
55				
56				
57				
58				
59				
60				

NOTES Test 60 continued

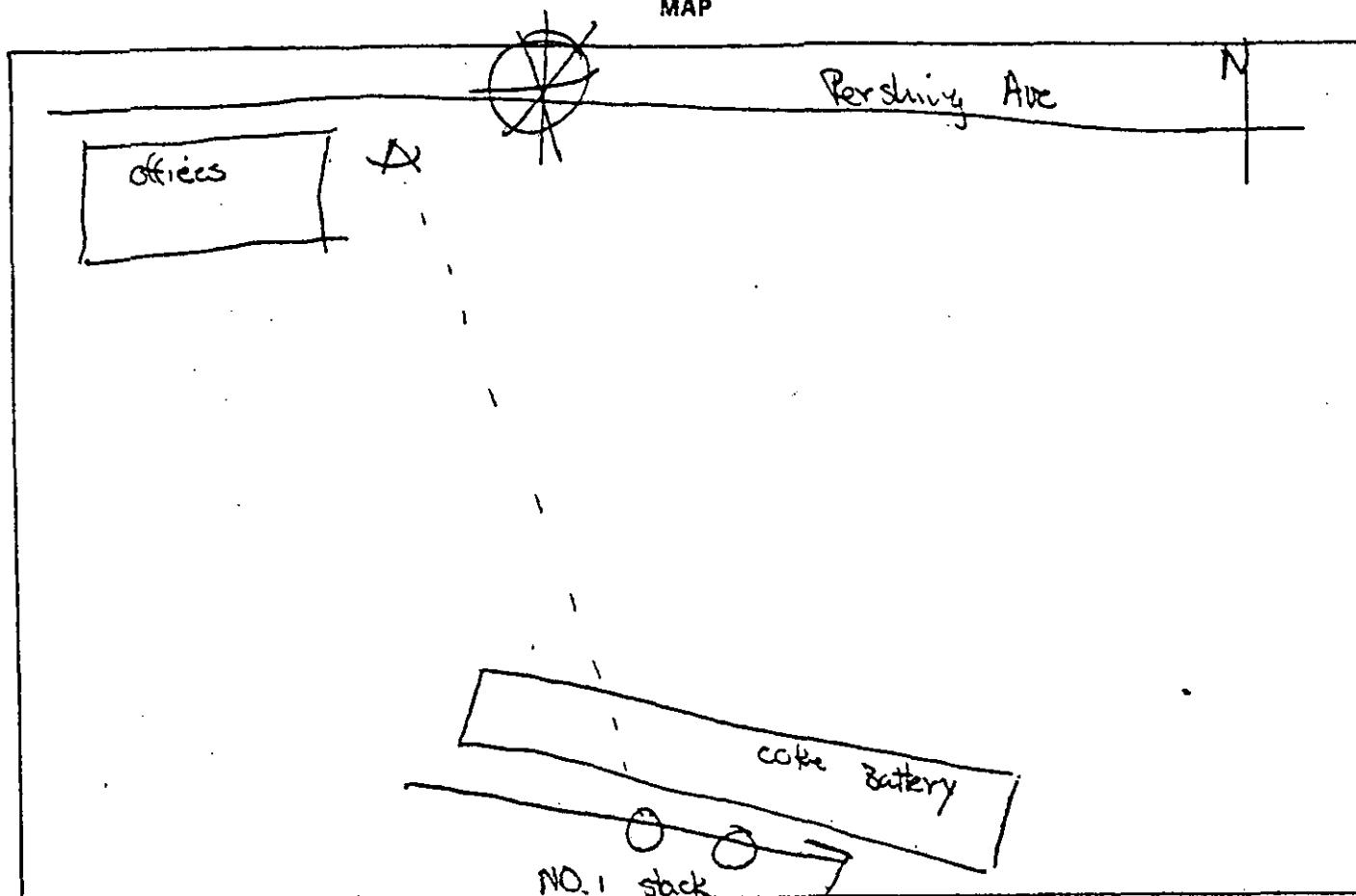
Inspector

Patt Kaysman

Date

7/16/79

MAP



Symbols

Sun =

Plume direction =

Point where plume observed =

Observer =

Water Vapor Condensate

Photographs: ☐ File ☐ Enclosed ☐ None

Comments

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Signature *Pete Kaufman*

Date 7/16/79

510388

VISIBLE EMISSION OBSERVATION RECORD

Company Republic Steel
 Date 7/16/79 Time First Sighted Plume 12:11
 Time Start 12:07 Time Stop 12:57
 Air Temperature 84°F Relative Humidity 70%
 Wind Speed 3-7 MPH Wind Direction out of NW
 Sky Condition clear Background blue sky
 Plume Characteristics: Continuous: ☐ Yes ☐ No
 Color Black Dispersion Description lofting
 Stack Height 150 (ft) Observer Location 750 (ft) NW of stack
 Sun Location: ☐ Back of Observer ☐ Left Shoulder
☐ Right Shoulder ☒ Other ahead

Emission Point No. 1 stack coke Battery

Min	0	15	30	45
01	0	0	0	0
02	0	0	0	0
03	0	0	0	0
04	0	0	10	10
05	0	0	0	0
06	0	0	0	0
07	0	0	5	0
08	0	0	0	0
09	0	0	0	0
10	0	0	0	0
11	0	0	0	0
12	0	0	0	0
13	0	0	0	0
14	0	0	0	0
15	0	0	0	0
16	0	0	0	0
17	0	0	0	0
18	0	0	0	0
19	0	0	0	0
20	0	0	0	0

Min	0	15	30	45
21	0	0	0	0
22	0	0	0	0
23	0	0	0	0
24	0	0	0	0
25	0	0	0	0
26	0	0	0	0
27	0	0	0	0
28	0	0	0	0
29	0	0	0	0
30	0	0	0	0
31	0	0	0	0
32	0	0	0	0
33	0	0	0	0
34	0	0	0	0
35	0	0	0	0
36	0	0	0	0
37	0	0	0	0
38	0	0	0	0
39	0	0	0	0
40	0	0	0	0

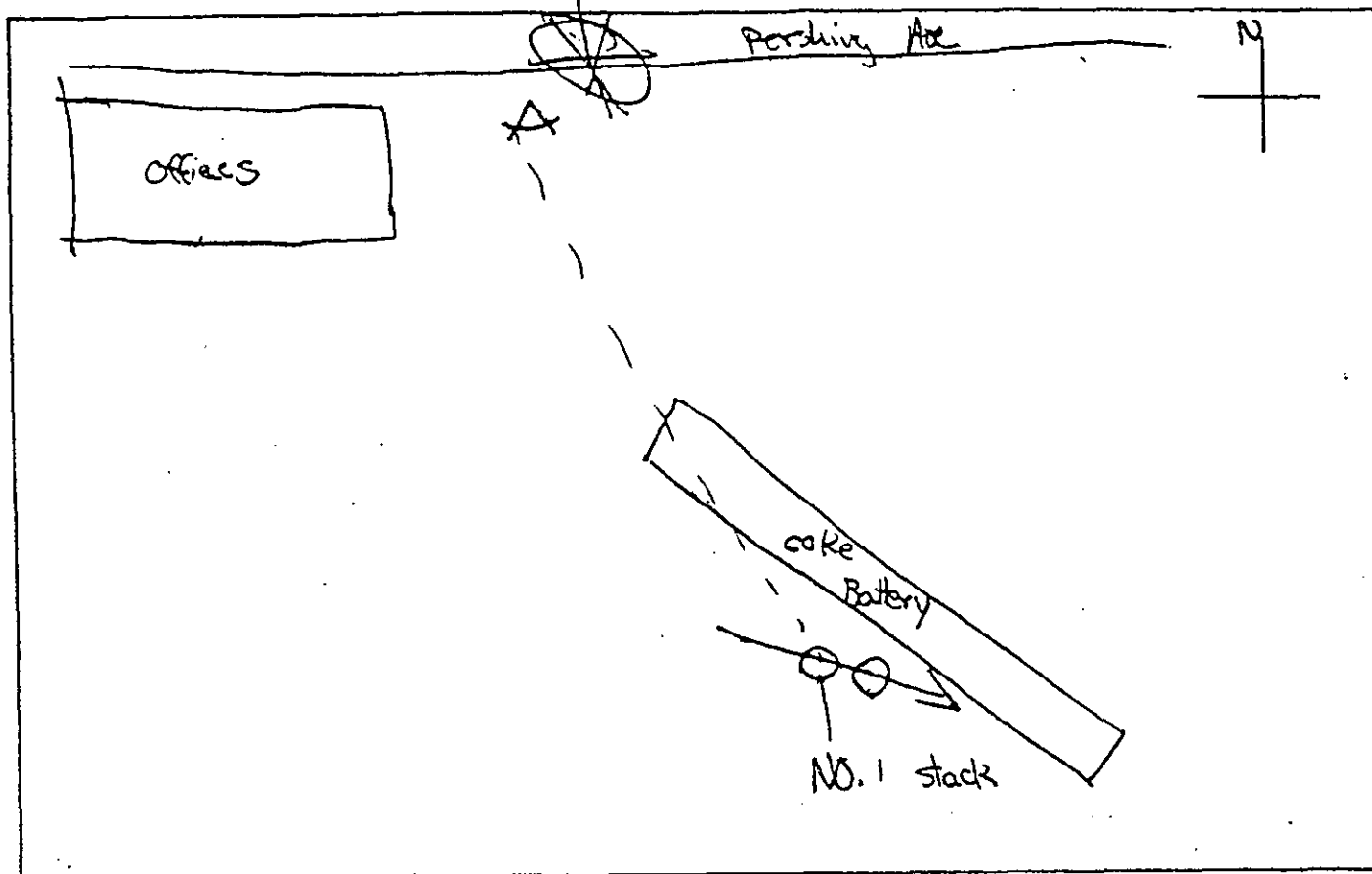
Min	0	15	30	45
41	0	0	0	0
42	0	0	0	0
43	0	0	0	0
44	0	0	0	0
45	0	0	0	0
46	0	0	0	0
47	0	0	0	0
48	0	0	0	0
49	0	0	0	0
50	0	0	0	0
51				
52				
53				
54				
55				
56				
57				
58				
59				
60				

NOTES Test 61

Inspector Pete Kaufman

Date 7/16/79

MAP



Symbols

Sun =

Plume direction =

Point where plume observed =

Observer =

Water Vapor Condensate None

Photographs: ☐ File ☐ Enclosed ☒ None

Comments

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Signature Ritt Kaufman

Date 7/16/79

510390

VISIBLE EMISSION OBSERVATION RECORD

Company _____

Date _____

Time First Sighted Plume _____

Time Start 1320

Time Stop 1409

Air Temperature _____

Relative Humidity _____

Wind Speed _____

Wind Direction _____

Sky Condition _____

Background _____

Plume Characteristics:

Continuous:

☐ Yes

☐ No

Color _____

Dispersion Description _____

Stack Height _____

(ft)

Observer Location _____

(ft)

of stack

Sun Location:

☐ Back of Observer

☐ Left Shoulder

☐ Right Shoulder

☒ Other Other

Emission Point _____

Min	0	15	30	45
01	0	0	0	0
02	0	0	0	0
03	0	0	0	0
04	0	0	0	0
05	0	0	0	0
06	0	0	0	0
07	0	0	0	0
08	0	0	0	0
09	0	0	0	0
10	0	0	0	0
11	0	0	0	0
12	0	0	0	0
13	0	0	0	0
14	0	0	0	0
15	0	0	0	0
16	0	0	0	0
17	0	0	0	0
18	0	0	0	0
19	0	0	0	0
20	0	0	0	0

Min	0	15	30	45
21	0	0	0	0
22	0	0	0	0
23	0	0	0	0
24	0	0	0	0
25	0	0	0	0
26	0	0	0	0
27	0	0	0	0
28	0	0	0	0
29	0	0	0	0
30	0	0	0	0
31	0	0	0	0
32	0	0	0	0
33	0	0	0	0
34	0	0	0	0
35	0	0	0	0
36	0	0	0	0
37	0	0	0	0
38	0	0	0	0
39	0	0	0	0
40	0	0	0	0

Min	0	15	30	45
41	0	0	0	0
42	0	0	0	0
43	0	0	0	0
44	0	0	0	0
45	0	0	0	0
46	0	0	0	0
47	0	0	0	0
48	0	0	0	0
49	0	0	0	0
50				
51				
52				
53				
54				
55				
56				
57				
58				
59				
60				

NOTES

Test 61 continued

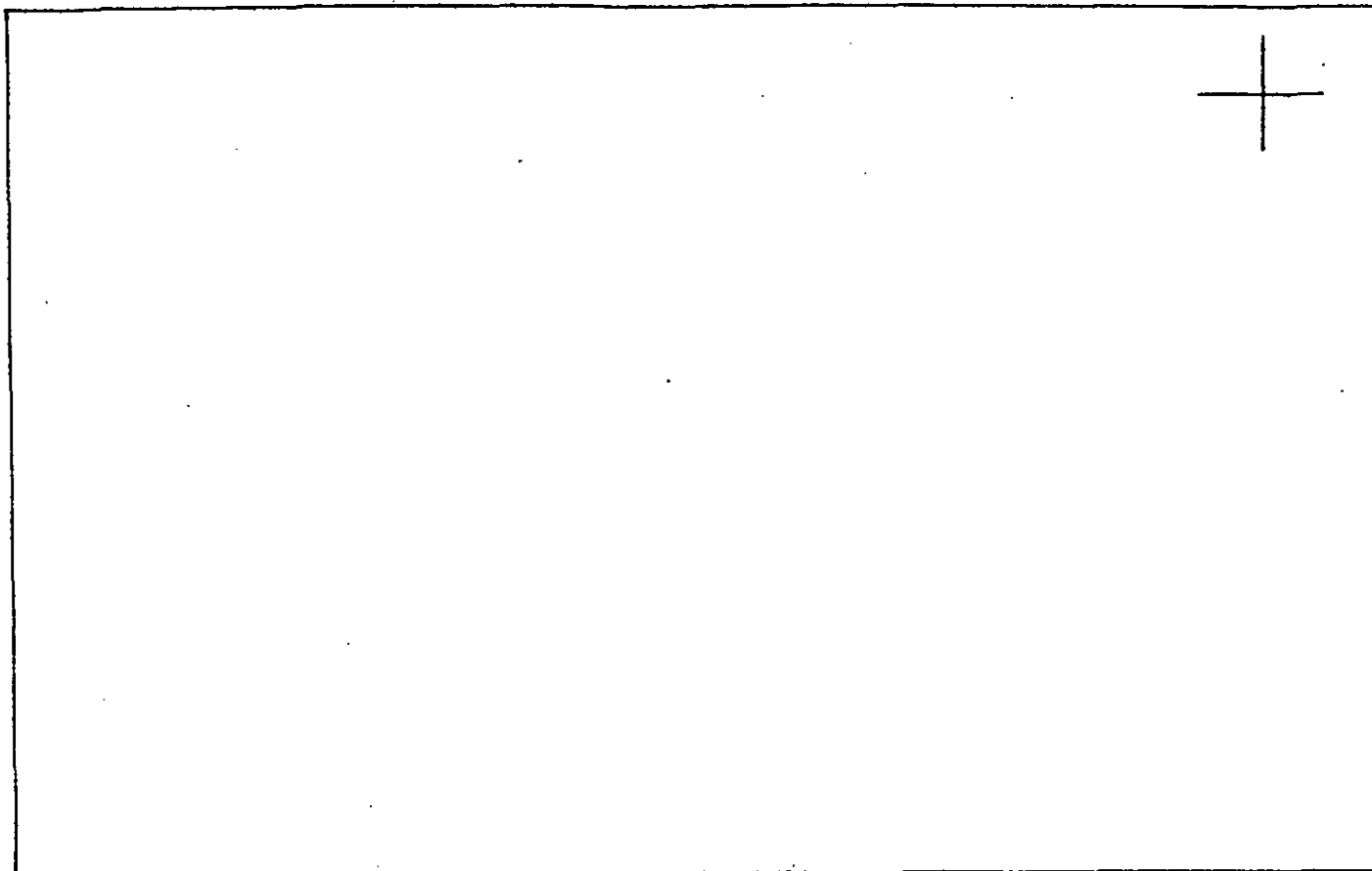
Inspector

Rita K. Korman

Date

7/16/79

MAP



Symbols

Sun =

Plume direction =

Point where plume observed =

Observer =

Water Vapor Condensate

Photographs: ☐ File ☐ Enclosed ☐ None

Comments

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Signature

Date

7/16/79

510392

VISIBLE EMISSION OBSERVATION RECORD

Company Republic Steel
 Date 7/17/79 Time First Sighted Plume _____
 Time Start 0748 Time Stop 0836
 Air Temperature 71°F Relative Humidity 70%
 Wind Speed 0-5 MPH Wind Direction out of NE
 Sky Condition Partly cloudy Background Blue Sky (some white cloud)
 Plume Characteristics: Continuous: ☐ Yes ☒ No
 Color _____ Dispersion Description _____
 Stack Height 150 (ft) Observer Location 750 (ft) N of stack
 Sun Location: ☐ Back of Observer ☒ Left Shoulder
☐ Right Shoulder ☐ Other _____

Emission Point No. 1 stack Coke Battery

Min	0	15	30	45	Min	0	15	30	45	Min	0	15	30	45
01	0	0	0	0	21	0	0	0	0	41	0	0	0	0
02	0	0	0	0	22	0	0	0	0	42	0	0	0	0
03	0	0	0	0	23	0	0	0	0	43	0	0	0	0
04	0	0	0	0	24	0	0	0	0	44	0	0	0	0
05	0	0	0	0	25	0	0	0	0	45	0	0	0	0
06	0	0	0	0	26	0	0	0	0	46	0	0	0	0
07	0	0	0	0	27	0	0	0	0	47	0	0	0	0
08	0	0	0	0	28	0	0	0	0	48	0	0	0	0
09	0	0	0	0	29	0	0	0	0	49	0			
10	0	0	0	0	30	0	0	0	0	50				
11	0	0	0	0	31	0	0	0	0	51				
12	0	0	0	0	32	0	0	0	0	52				
13	0	0	0	0	33	0	0	0	0	53				
14	0	0	0	0	34	0	0	0	0	54				
15	0	0	0	0	35	0	0	0	0	55				
16	0	0	0	0	36	0	0	0	0	56				
17	0	0	0	0	37	0	0	0	0	57				
18	0	0	0	0	38	0	0	0	0	58				
19	0	0	0	0	39	0	0	0	0	59				
20	0	0	0	0	40	0	0	0	0	60				

NOTES Test 62

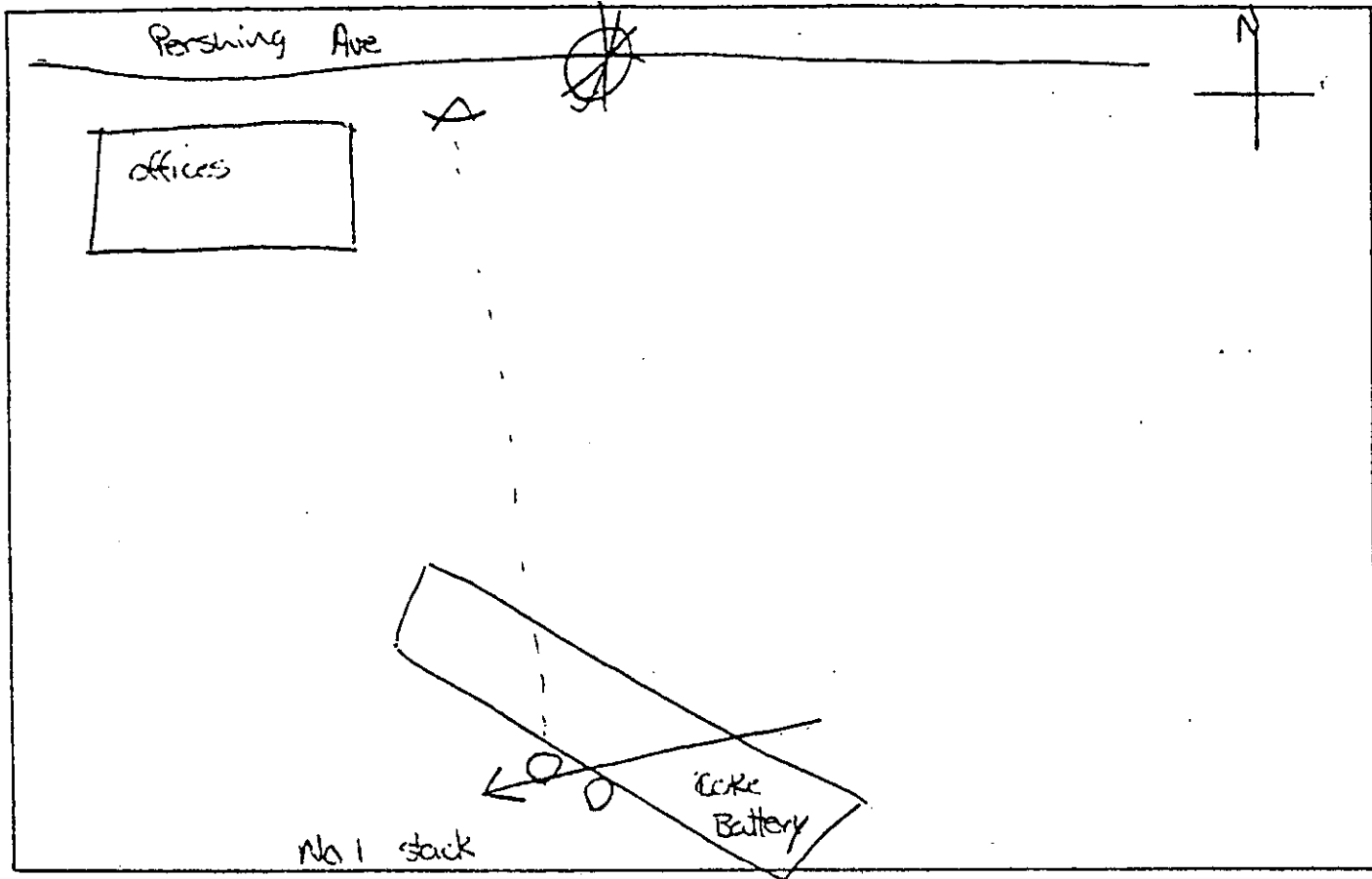
Inspector

John K. Johnson

Date

7/17/79

MAP



Symbols

Sun =

Plume direction =

Water Vapor Condensate *None*

Point where plume observed =

Observer =

Photographs: ☐ File ☐ Enclosed ☒ None

Comments

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Signature *Beta Kaufmann*

Date *7/17/79*

510394

VISIBLE EMISSION OBSERVATION RECORD

Company _____

Date _____

Time First Sighted Plume _____

Time Start 0910

Time Stop 0959

Air Temperature _____

Relative Humidity _____

Wind Speed _____

Wind Direction _____

Sky Condition _____

Background _____

Plume Characteristics:

Continuous:

☐ Yes

☐ No

Color _____

Dispersion Description _____

Stack Height _____

(ft)

Observer Location _____

(ft)

of stack

Sun Location:

☐ Back of Observer

☐ Left Shoulder

☐ Right Shoulder

☐ Other _____

Emission Point

Min	0	15	30	45
01	0	0	0	0
02	0	0	0	0
03	0	0	0	0
04	0	0	0	0
05	0	0	0	0
06	0	0	0	0
07	0	0	0	0
08	0	0	0	0
09	0	0	0	0
10	0	0	0	0
11	0	0	0	0
12	0	0	0	0
13	0	0	0	0
14	0	0	0	0
15	0	0	0	0
16	0	0	0	0
17	0	0	0	0
18	0	0	0	0
19	0	0	0	0
20	0	0	0	0

Min	0	15	30	45
21	0	0	0	0
22	0	0	0	0
23	0	0	0	0
24	0	0	0	0
25	0	0	0	0
26	0	0	0	0
27	0	0	0	0
28	0	0	0	0
29	0	0	0	0
30	0	0	0	0
31	0	0	0	0
32	0	0	0	0
33	0	0	0	0
34	0	0	0	0
35	0	0	0	0
36	0	0	0	0
37	0	0	0	0
38	0	0	0	0
39	0	0	0	0
40	0	0	0	0

Min	0	15	30	45
41	0	0	0	0
42	0	0	0	0
43	0	0	0	0
44	0	0	0	0
45	0	0	0	0
46	0	0	0	0
47	0	0	0	0
48	0	0	0	0
49	0	0	0	0
50				
51				
52				
53				
54				
55				
56				
57				
58				
59				
60				

NOTES

Test 62 continued

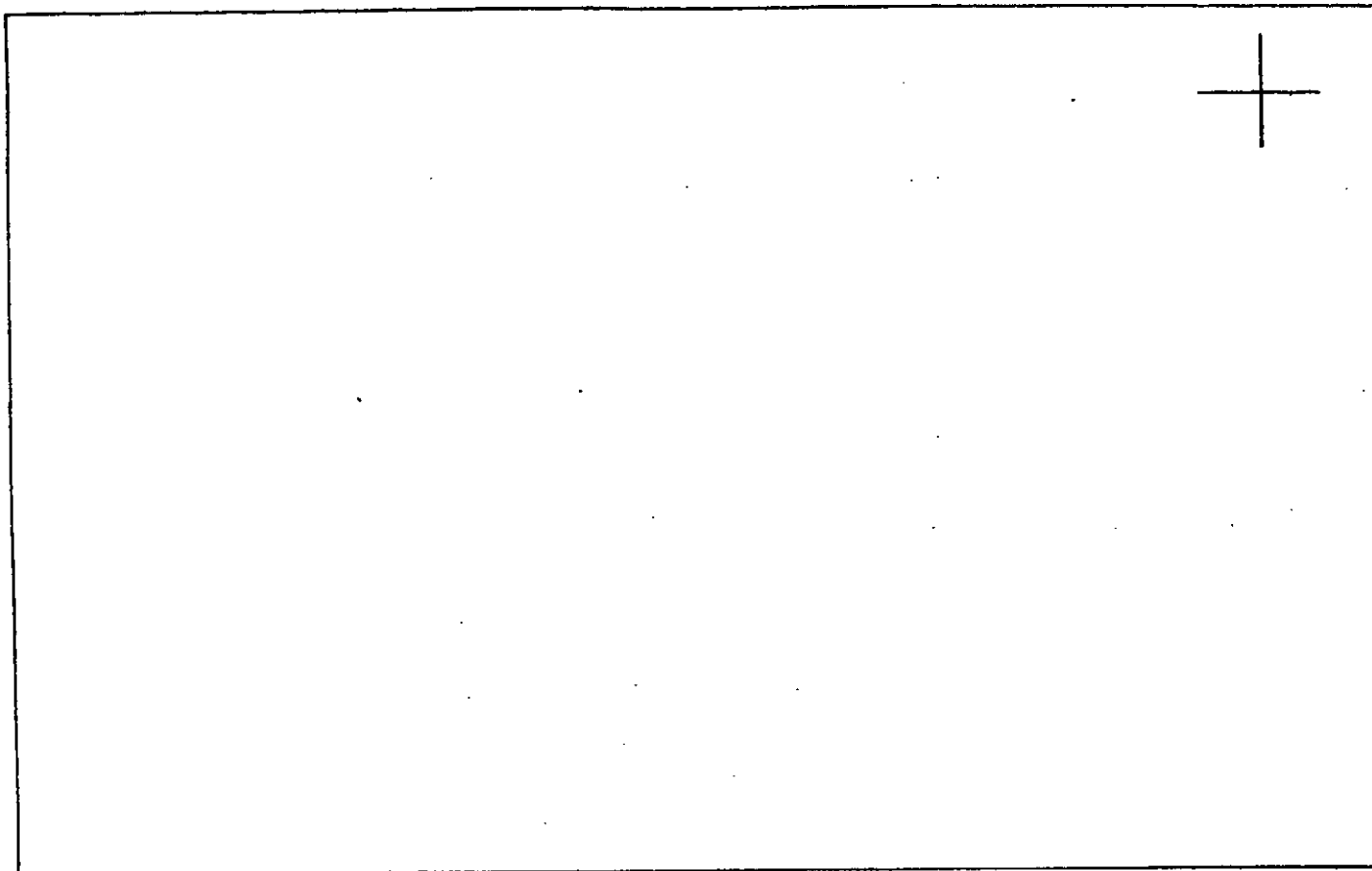
Inspector

Pat Kuyfman

Date

7/17/19

MAP



Symbols

Sun =

Plume direction =

Point where plume observed =

Observer =

Water Vapor Condensate _____

Photographs: ☐ File ☐ Enclosed ☐ None

Comments _____

Signature

Date 7/17/71

510396

VISIBLE EMISSION OBSERVATION RECORD

Page 1 of 2

Company Republic Steel

Date 7/17/79

Time First Sighted Plume

Time Start 1053

Time Stop 1142

Air Temperature 76°F

Relative Humidity 60%

Wind Speed 0-5 mph

Wind Direction Out of NE

Sky Condition Partly Cloudy

Background Blue sky occasional cloud

Plume Characteristics: Continuous: ☐ Yes ☒ No

Color

Dispersion Description

Stack Height 150

(ft) Observer Location 750 (ft) N of stack

Sun Location: ☐ Back of Observer
☐ Right Shoulder

☒ Left Shoulder
☐ Other

Emission Point NO. 1 stack coke Battery

Min	0	15	30	45
01	0	0	0	0
02	0	0	0	0
03	0	0	0	0
04	0	0	0	0
05	0	0	0	0
06	0	0	0	0
07	0	0	0	0
08	0	0	0	0
09	0	0	0	0
10	0	0	0	0
11	0	0	0	0
12	0	0	0	0
13	0	0	0	0
14	0	0	0	0
15	0	0	0	0
16	0	0	0	0
17	0	0	0	0
18	0	0	0	0
19	0	0	0	0
20	0	0	0	0

Min	0	15	30	45
21	0	0	0	0
22	0	0	0	0
23	0	0	0	0
24	0	0	0	0
25	0	0	0	0
26	0	0	0	0
27	0	0	0	0
28	0	0	0	0
29	0	0	0	0
30	0	0	0	0
31	0	0	0	0
32	0	0	0	0
33	0	0	0	0
34	0	0	0	0
35	0	0	0	0
36	0	0	0	0
37	0	0	0	0
38	0	0	0	0
39	0	0	0	0
40	0	0	0	0

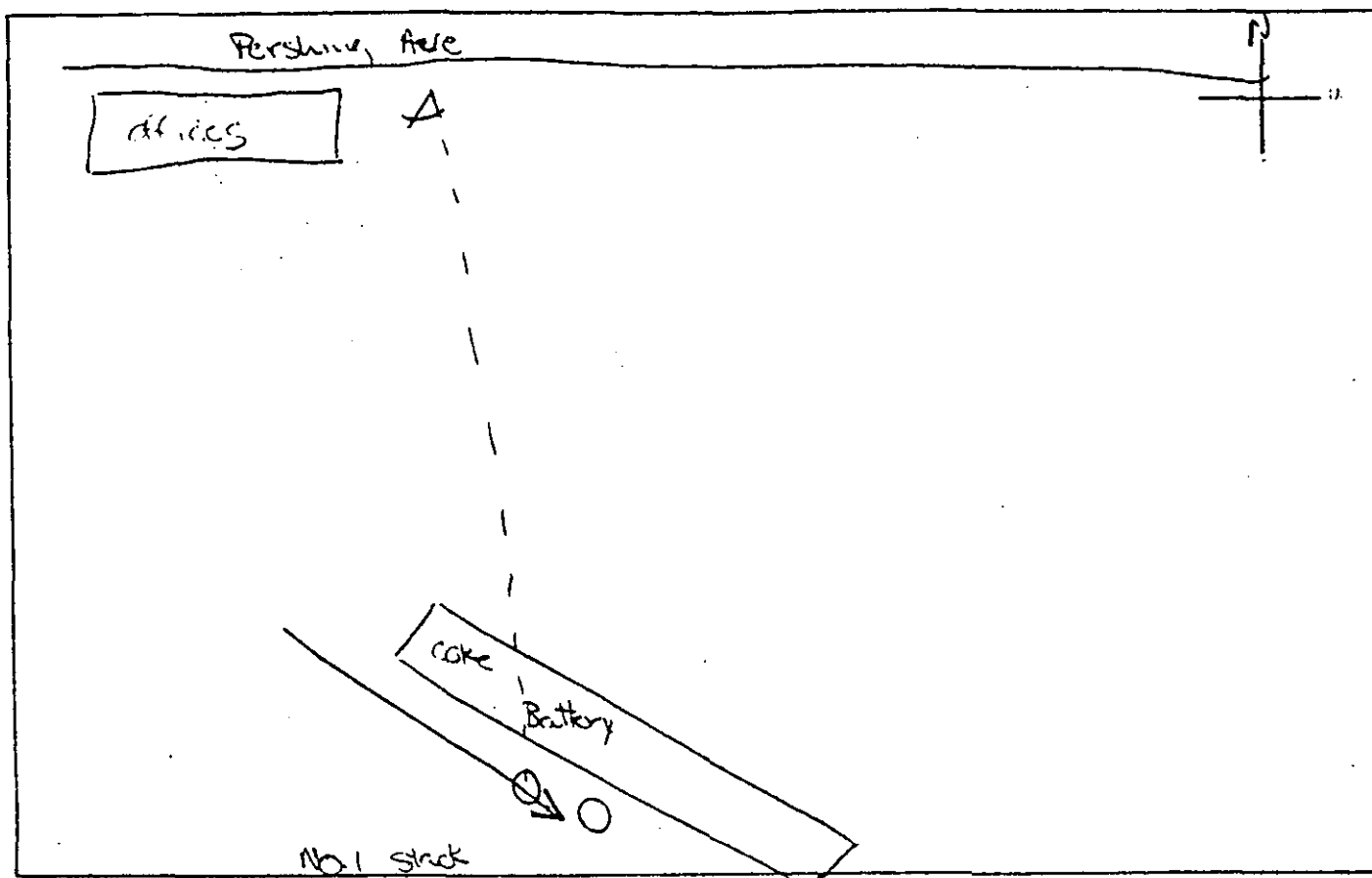
Min	0	15	30	45
41	0	0	0	0
42	0	0	0	0
43	0	0	0	0
44	0	0	0	0
45	0	0	0	0
46	0	0	0	0
47	0	0	0	0
48	0	0	0	0
49	0	0	0	0
50				
51				
52				
53				
54				
55				
56				
57				
58				
59				
60				

NOTES Test 63

Inspector Rita Kaufman

Date 7/17/79

MAP



Symbols

Sun =

Plume direction =

Point where plume observed =

Observer =

Water Vapor Condensate None

Photographs: ☐ File ☐ Enclosed ☒ None

Comments

Signature

Date 7/17/79

510398

Page 2 of 2
VISIBLE EMISSION OBSERVATION RECORD

Company _____
Date _____ Time First Sighted Plume _____
Time Start 1155 Time Stop 1244
Air Temperature _____ Relative Humidity _____
Wind Speed _____ Wind Direction _____
Sky Condition _____ Background _____
Plume Characteristics: Continuous: ☐ Yes ☐ No
Color _____ Dispersion Description _____
Stack Height _____ (ft) Observer Location _____ (ft) _____ of stack
Sun Location: ☐ Back of Observer ☐ Left Shoulder
☐ Right Shoulder ☐ Other _____

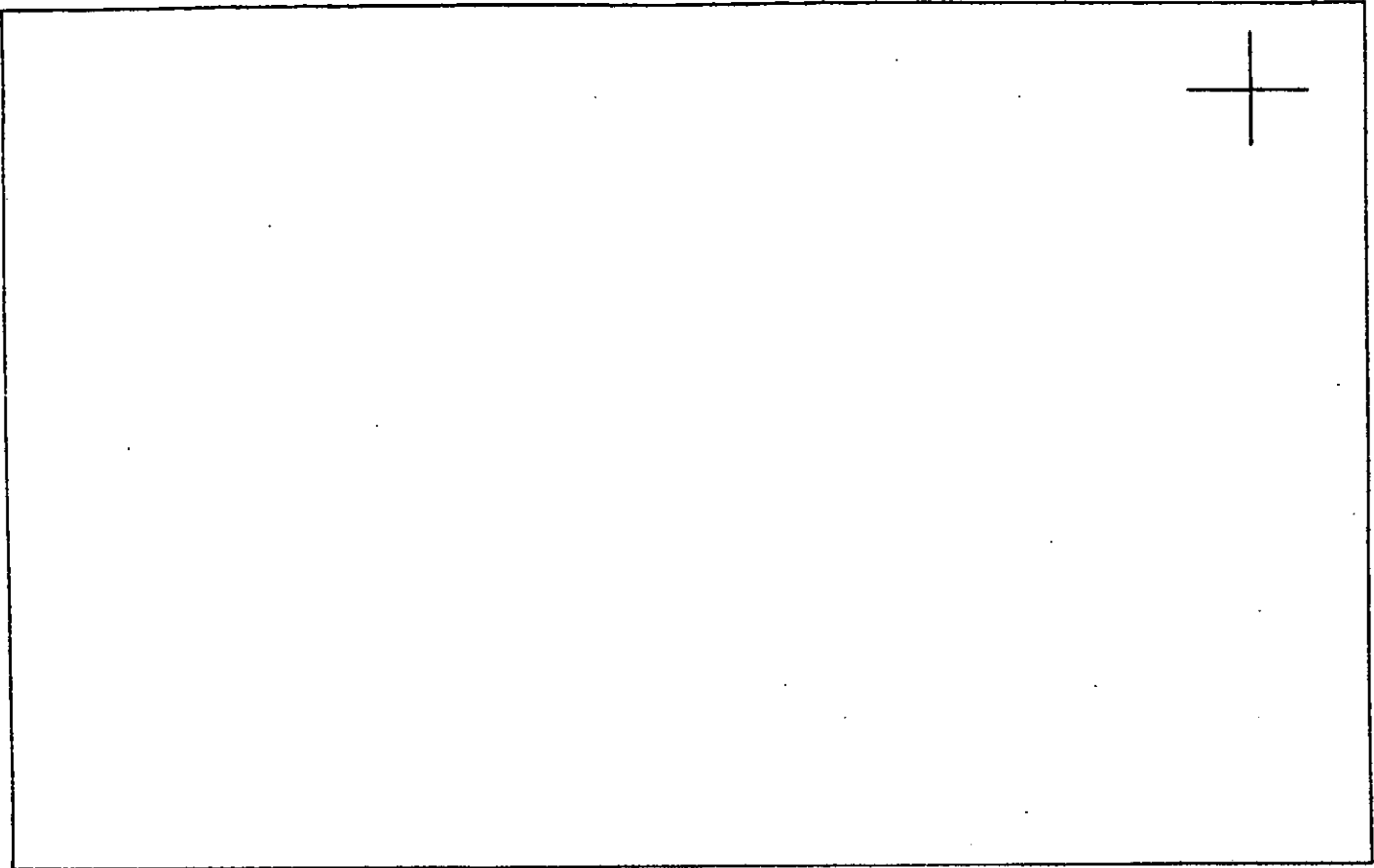
Emission Point _____

Min	0	15	30	45	Min	0	15	30	45	Min	0	15	30	45
01	0	0	0	0	21	0	0	0	0	41	0	0	0	0
02	0	0	0	0	22	0	0	0	0	42	0	0	0	0
03	0	0	0	0	23	0	0	0	0	43	0	0	0	0
04	0	0	0	0	24	0	0	0	0	44	0	0	0	0
05	0	0	0	0	25	0	0	0	0	45	0	0	0	0
06	0	0	0	0	26	0	0	0	0	46	0	0	0	0
07	0	0	0	0	27	0	0	0	0	47	0	0	0	0
08	0	0	0	0	28	0	0	0	0	48	0	0	0	0
09	0	0	0	0	29	0	0	0	0	49	0	0	0	0
10	0	0	0	0	30	0	0	0	0	50				
11	0	0	0	0	31	0	0	0	0	51				
12	0	0	0	0	32	0	0	0	0	52				
13	0	0	0	0	33	0	0	0	0	53				
14	0	0	0	0	34	0	0	0	0	54				
15	0	0	0	0	35	0	0	0	0	55				
16	0	0	0	0	36	0	0	0	0	56				
17	0	0	0	0	37	0	0	0	0	57				
18	0	0	0	0	38	0	0	0	0	58				
19	0	0	0	0	39	0	0	0	0	59				
20	0	0	0	0	40	0	0	0	0	60				

NOTES Test 63 continued

Inspector Pete Kaufman Date 7/17/79

MAP



Symbols

Sun =

Plume direction =

Point where plume observed =

Observer =

Water Vapor Condensate

Photographs: ☐ File ☐ Enclosed ☐ None

Comments

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Signature

~~Robert Kaufmann~~

Date 7/17/79

510400

Cleveland, C. H. C.

FRONT HALF RESULTS (Particle Mass: 70.1)

[illegible]

REPUBLIC IRON & STEEL

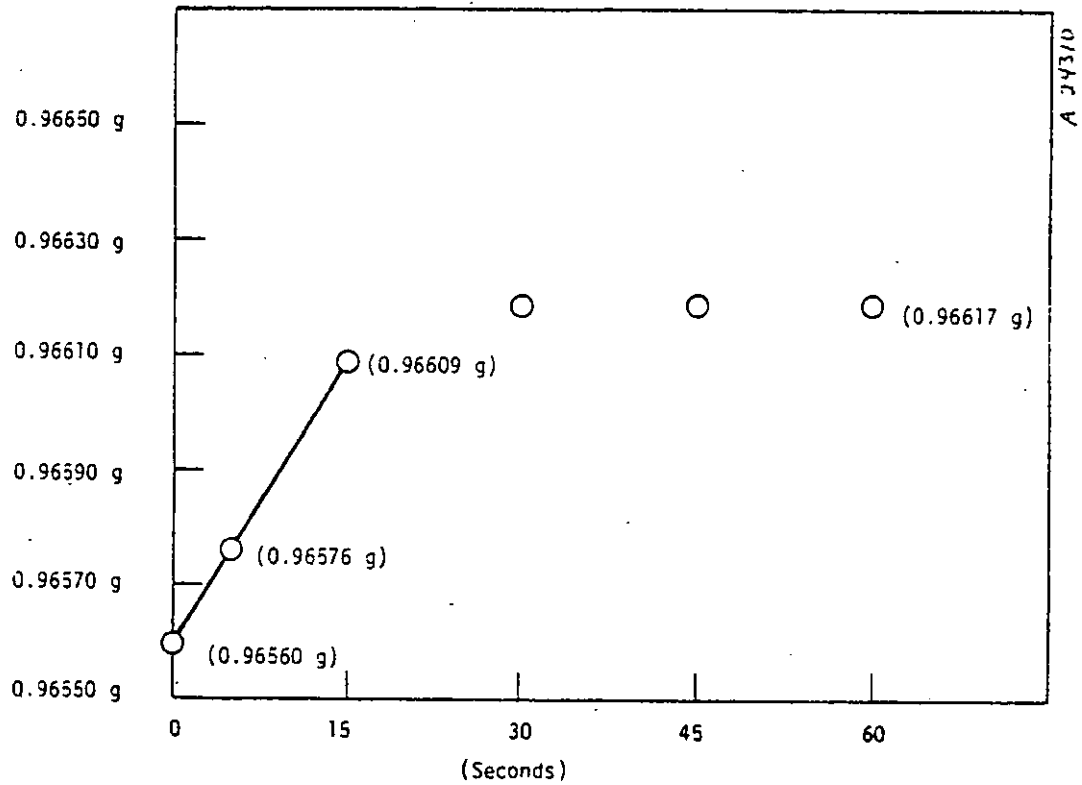
Test #60 "Coke Stack"

Original tare = 0.93510 g

Filter #JMC 522102

Blank weight = <0.1 mg

Particulate loading = 30.5 mg



REPUBLIC IRON & STEEL

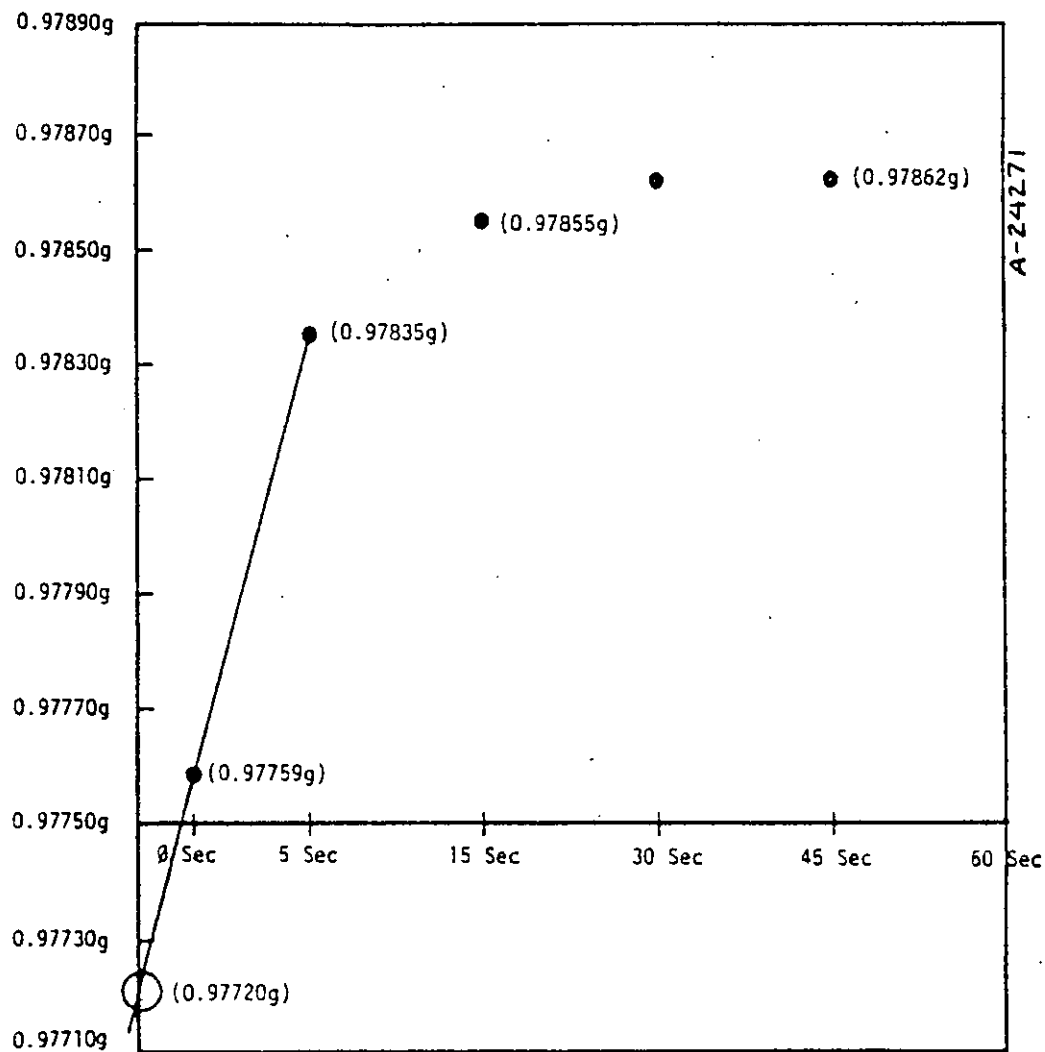
Test #61

Filter #JMC 52241

Original tare = 0.93170g

Blank weight = <0.1 mg

Particulate loading = 45.5 mg



REPUBLIC IRON & STEEL

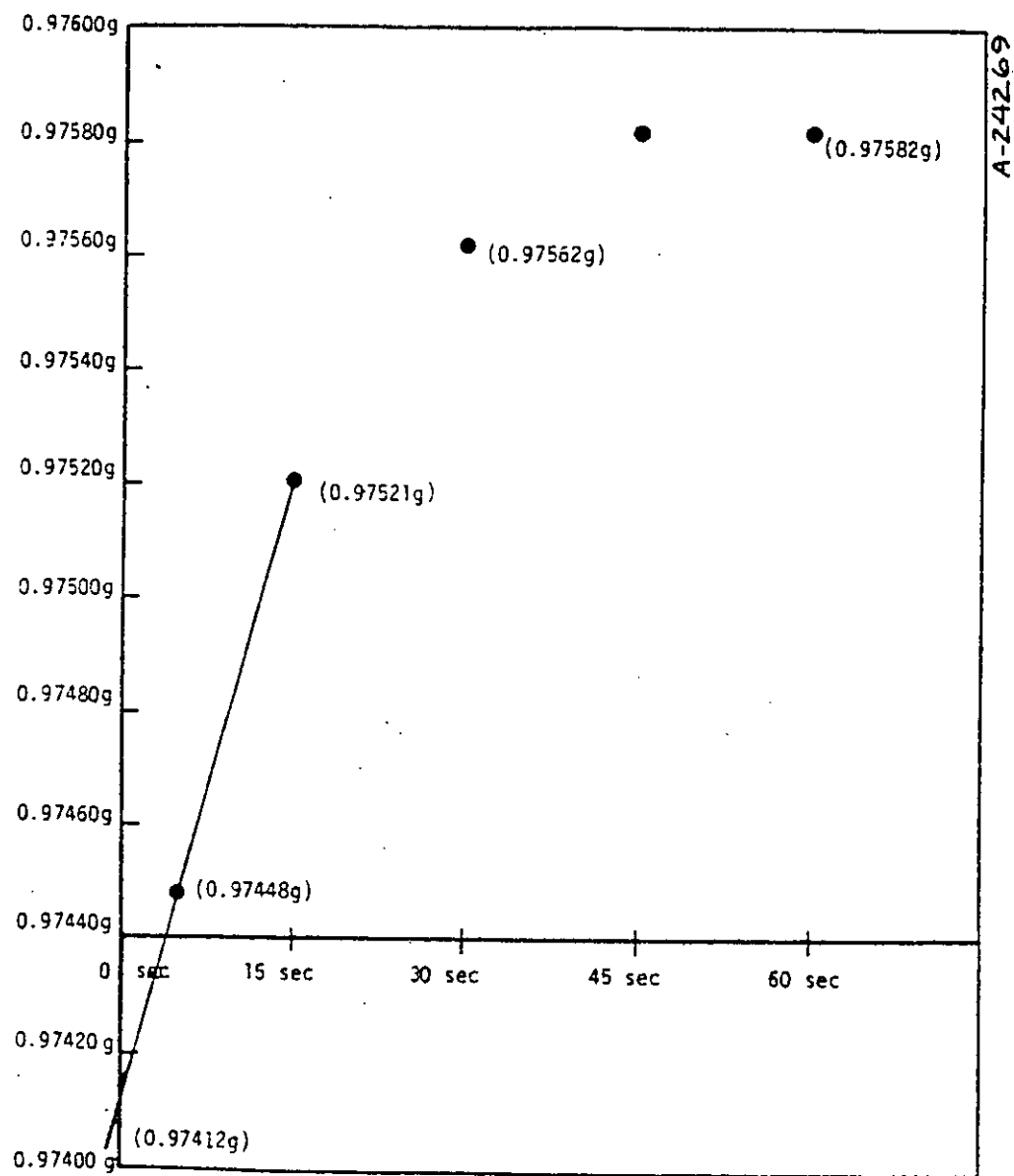
Test #62 "Coke Stack"

Original tare = 0.91810g

Filter #JMC 52246

Blank weight = <0.1 mg

Particulate loading = 560 mg



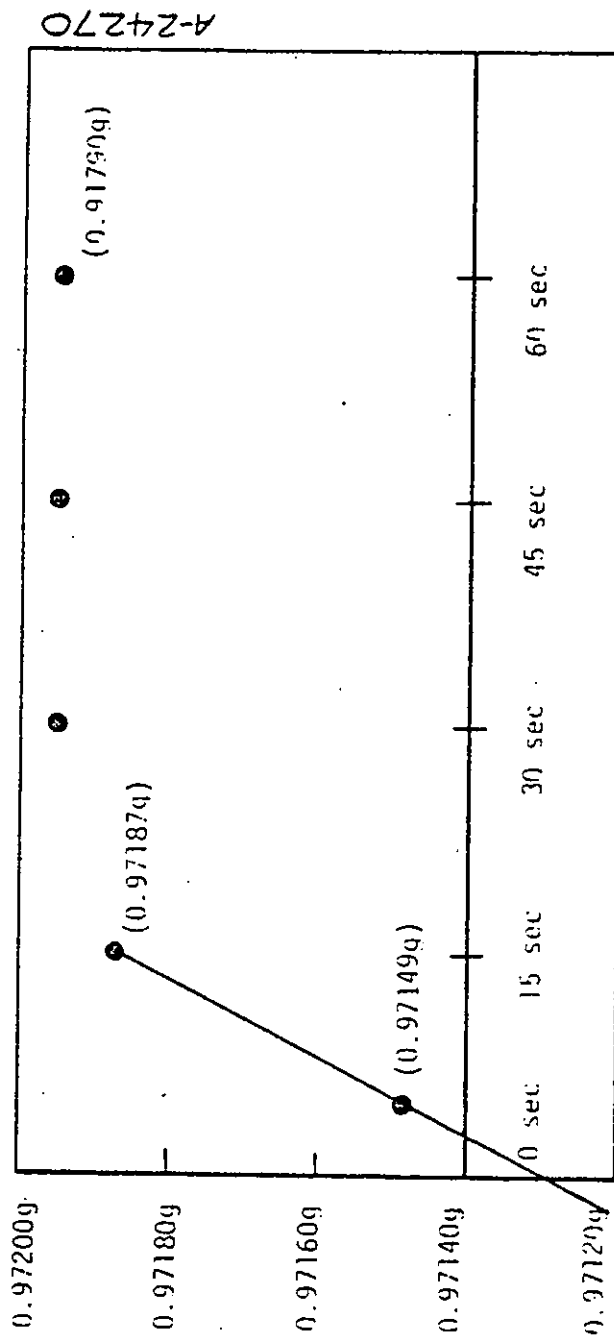
REPUBLIC IRON & STEEL

Test #63 "Coke Stack" Original tare = 0.92180g

Filter #JMC 52263

Blank weight = <0.1 mg

Particulate loading = 49.5 mg



BACK HALF RESULTS. (Particle Mass Tests)

[illegible]

Republic Steel
Book half Inorganic condensable particulate

RUN #	Uncorrected	Blank Corrected
Test 46	120.3	<0.1
47	112.6	<0.1
48	69.4	<0.1
49	106.8	<0.1
50	69.6	<0.1
51	70.9	<0.1
52	16.0	<0.1
54	120.8	10.4
55	131.7	20.4
56	14.6	<0.1
57	21.4	<0.1
58	11.0	<0.1
60	194.8	35.6
61	453.3	277.8
62	3833.2	3596.8
63	542.2	331.6

REPUBLIC IRON & STEEL
"SULFATE ANALYSIS IMMERSION METHOD"

"SULFATE ANALYSIS INTERIMINATION"

Simple dilution
1 ml to 100 ml

PARTICULATE CALCULATIONS

1. Volume of dry gas sampled at standard conditions, 68°F, 29.92 inch Hg (scf)

$$V_{m_{std}} = 17.64 \frac{V_m}{\alpha} \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460}$$

$$60.247 = 17.64 \left(\frac{62.180}{987} \right) \left(\frac{29.61 + \frac{1.34}{13.6}}{88 + 460} \right)$$

2. Stack gas moisture condensed at standard conditions (scf)

$$V_{w_{std}} = 0.04707 V_{l_c}$$

$$5.352 = 0.04707 (113.7)$$

3. Stack gas proportion of water vapor, by volume

$$B_{wo} = \frac{V_{w_{std}}}{V_{w_{std}} + V_{m_{std}}} = \frac{5.352}{5.352 + 60.247}$$

$$0.082 =$$

4. Stack gas dry molecular weight (lb/lb-mole)

$$MW_d = 0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)$$

$$29.14 = 0.44 (4) + 0.32 (12.4) + 0.28 (83.6)$$

5. Stack gas molecular weight (lb/lb-mole)

$$MW_s = MW_d (1 - B_{wo}) + 18 (B_{wo})$$

$$28.23 = 29.14 (1 - 0.082) + 18 (0.082)$$

6. Pressure stack, in. Hg

$$P_s = P_b + \frac{P_{st}}{13.6}$$

$$29.52 = 29.61 + \frac{-1.2}{13.6}$$

7. Stack gas velocity at stack conditions (ft/sec)

$$V_s = 85.49 (C_p) (\sqrt{\Delta P})_{avg} \sqrt{\frac{T_{s,avg} + 460}{P_s MW_s}}$$

$$23.30 = 85.49 (0.786) (0.311) \sqrt{\frac{1036}{29.52 (28.23)}}$$

8. Stack gas volume at standard conditions (scfm)

$$Q_s = 60 (1 - B_{wo}) V_{s,avg} A_s \left(\frac{528}{T_{s,avg} + 460} \right) \left(\frac{P_s}{29.92} \right)$$

$$40,300 = 60 (1 - 0.082) (23.30) \left(\frac{\pi \frac{8.92^2}{4}}{67.49} \right) \left(\frac{528}{1036} \right) \left(\frac{29.52}{29.92} \right)$$

9. Test percent isokinetic

$$\%I = \frac{17.33 (T_s + 460)}{\theta V_s P_s D_n^2} [0.04707 (V1_c) + Vm_{std}]$$

$$96.9 = \frac{17.33 (1036) (5.352 + 60.247)}{96 (23.30) (29.52) (0.429)^2}$$

10. Particulate matter concentration, gr/scf

$$C_s = 15.432 \frac{M_p}{Vm_{std}}$$

$$0.010 = 15.432 \frac{0.0397}{60.247}$$

11. Emission rate of particulate matter, lb/hr

$$ER = 0.00857 (Q_s) C_s$$

$$3.512 = 0.00857 (40,300) (0.010)$$

12. Percent excess air at sampling point

$$\% EA = \frac{100 [\%O_2 - 0.5 (\%CO)]}{0.264 [\%N_2 - (\%O_2 - 0.5 \times \%CO)]}$$